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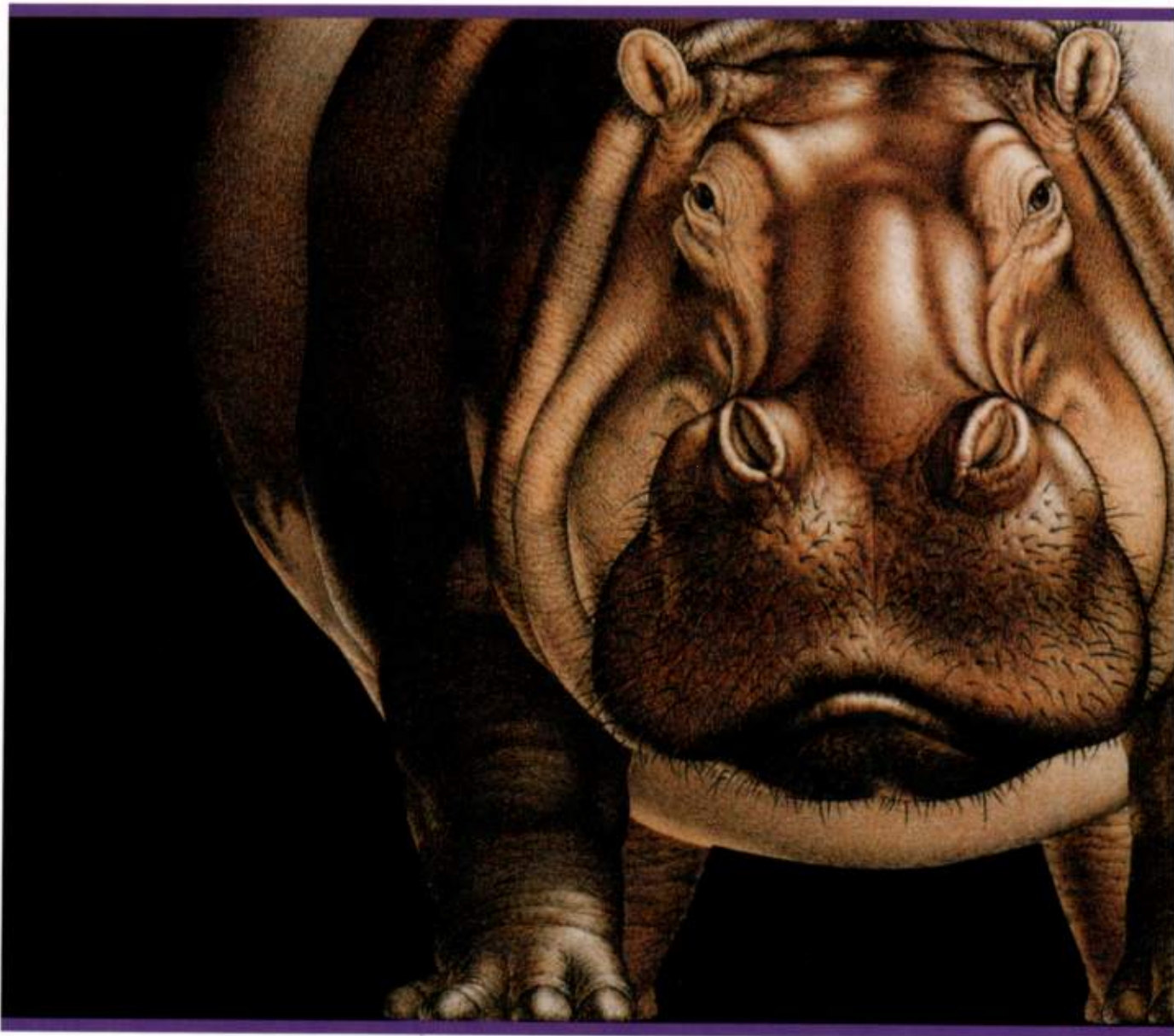
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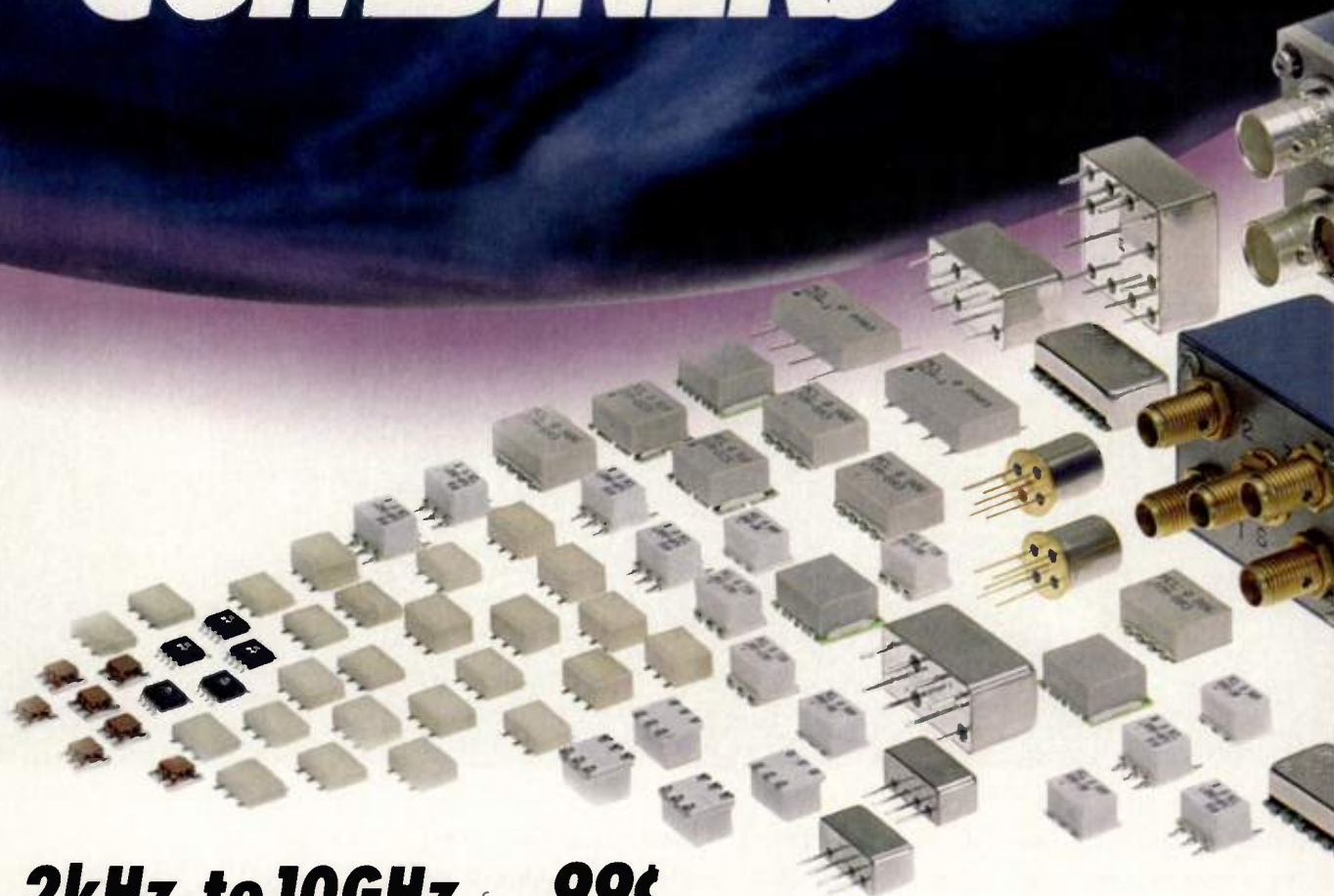
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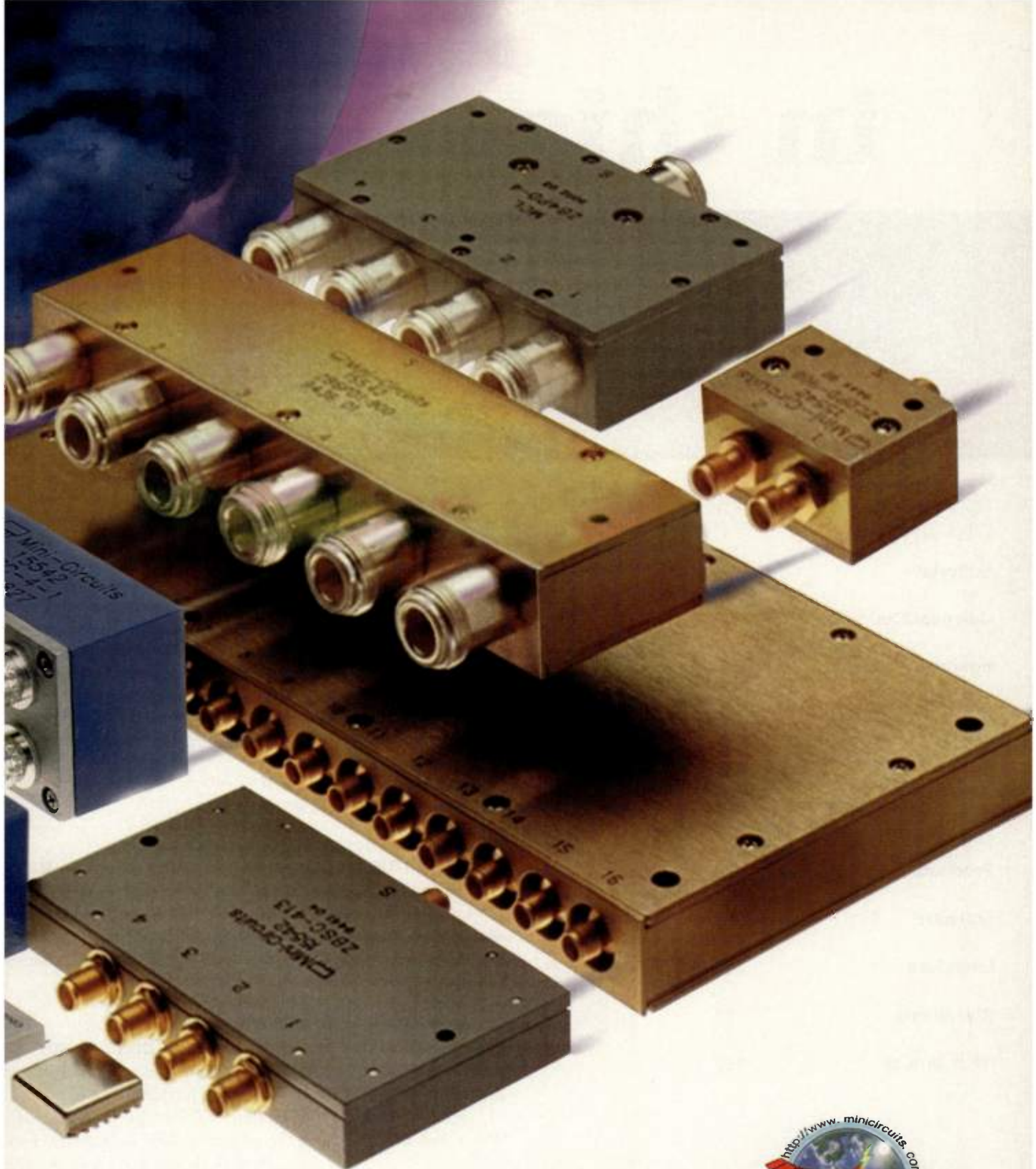
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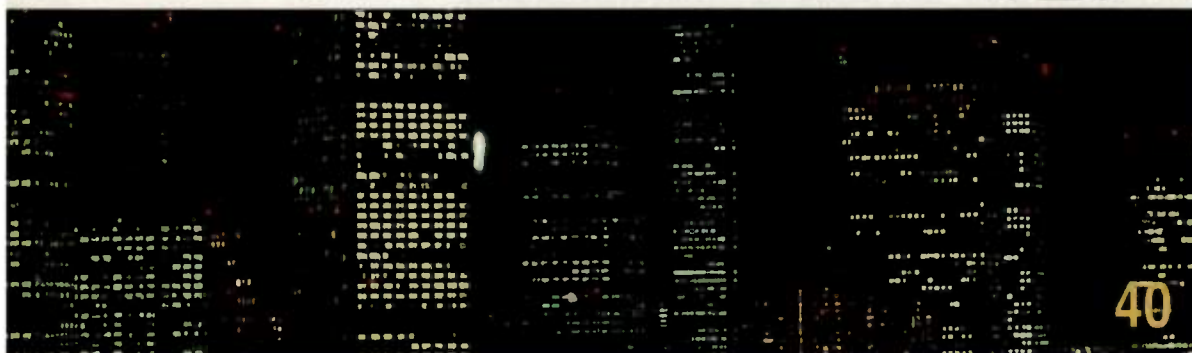
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EMI

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Spread spectrum and PLL technology combine to reduce EMI—Combining state-of-the-art spread spectrum and PLL design offers 10 dB improvement in measured EMI.

— By I-The Sha, Albert Chen, Kuang-Yu and Jeffry Keip

TX/RX

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Embedded antennas—technology for next generation handsets—External antennas have long been the bane for handsets and their designers. Embedded antennas may be the solution they've been looking for. — By David McCartney

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Wireless Communication

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Fixed wireless communications for the mass market—With an open market for many communications services, the current challenge is to offer a cost-effective package of services to both consumers and small businesses.

— By Abel Ghanem

Tutorial:

Amplifiers

48

3.7 Watt Ka-band power module for local multi-point distribution systems applications

Crowding of lower frequencies promise to open a host of Ka-band multipoint distribution applications and products.

—By Carlton T. Creamer, James J. Komiak, Wendell Kong, P.C. Chao, Kirby Nichols, Christopher O'Neil, Scott MacKelvey, Paul D. Cooper and Dana Wheeler

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JCA018-204	0.5-18.0	25	4.0	2.5	10	20	20
JCA018-300	0.5-18.0	30	3.8	2.5	0	10	10
JCA018-303	0.5-18.0	27	5.0	2.5	7	17	17
JCA018-400	0.5-18.0	37	3.8	2.5	0	10	10
JCA018-403	0.5-18.0	35	5.0	2.5	7	17	17
JCA018-504	0.5-18.0	40	5.0	2.5	10	20	20
JCA218-200	2.0-18.0	15	5.0	2.5	10	20	20
JCA218-206	2.0-18.0	17	5.0	2.5	15	25	25
JCA218-300	2.0-18.0	23	5.0	2.5	10	20	20
JCA218-306	2.0-18.0	22	5.0	2.5	15	25	25
JCA218-307	2.0-18.0	20	5.0	2.5	21	31	31
JCA218-400	2.0-18.0	29	5.0	2.5	10	20	20
JCA218-406	2.0-18.0	30	5.0	2.5	15	25	25
JCA218-407	2.0-18.0	30	5.0	2.5	21	31	31
JCA218-506	2.0-18.0	35	5.0	2.5	15	25	25
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RF editorial

I got the wireless Internet blues

By Roger Lesser
Editor
roger_lesser@intertec.com



Educating Roger

During an editor's day event hosted by Ericsson Microelectronics, Morgan Hill, CA, I got hands on experience "building" a surface mount device. After doing a pick and place procedure and then moving to gold wire bonding, I didn't come close to making a working device. The capacitor I placed was skewed and my wire-bonding job was just as humorous.

In the time it took me to "build" my device, the ladies who helped guide me through the process could have built dozens. My thanks to Phi Pham for her guidance, Beatrix Brakee for her patience, and Emelia Szczylewski for allowing me to get in the way of what was a very professional operation. (Of course, I'm showing off my effort like a first grader who brings home that piece of "art" that ends up on the refrigerator.)

Bluetooth and beyond

This year's Wireless Symposium was memorable for one reason—the amount of emphasis on Bluetooth. A year or so ago, we heard a lot of talk but saw little reality. This year, companies like Ericsson and Texas Instruments made a point of demonstrating they are ready to field products that support the wireless connectivity applications that Bluetooth envisions. I left San Jose with a feeling that maybe, just maybe, we are seeing the reality behind Bluetooth's potential and not just hype.

Beyond the Internet?

After a day at home I was winging my way to New Orleans and CTIA. I was looking forward to CTIA to see just what the handset manufacturers and carriers were doing with wireless connectivity. Well, to be honest, I was also looking forward to New Orleans, too. I love the blues and took advantage of seeing Buddy Guy.

After listening to Bill "it's a windowful world" Gates wax philosophical

about the wireless Windows environment Microsoft envisions, it was off to the show floor. It was then that I thought back to Buddy Guy. For within a matter of a few hours, "I Got the Wireless Internet Blues."

I'm concerned there is way too much attention being paid to wireless Internet at the expense of other wireless connectivity applications. The Bluetooth special interest group (SIG) notes: Bluetooth is "The technology that propels you into a new dimension in wireless connectivity." Does that mean just the Internet?

I have to admit, at this point in the drive to wireless connectivity and interoperability, wireless Internet applications make sense—especially with the zeal consumers are showing for the Internet. A zeal that is causing the FCC to look at frequencies as commodities that can be sold or leased. The FCC credits the Internet as one of the drivers behind their action, noting that the volume of traffic on the Internet doubles every 100 days. Most of the increase is coming from wireless devices.

OK, call me an Internet curmudgeon, but I see the day when the consumer will realize there has to be more to wireless connectivity than surfing the Net or getting e-mail. Bluetooth and WAP use the Internet as a piece of the connectivity puzzle, and will depend on it for other wireless connectivity capabilities. And that's the rub. Internet connectivity is part of the solution not the entire solution.

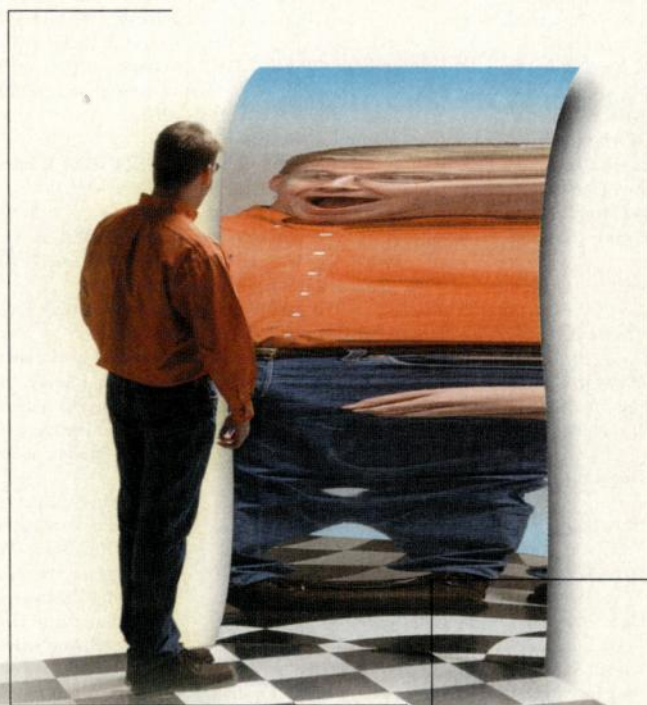
The Bluetooth SIG and WAP communities need to get the word out to the consumer now that they can offer more than Internet connectivity. Take a page from Bill "Austin Powers" Gates on how to build anticipation. But, do more than build anticipation. Educate the consumer. Then get ready for the real wireless explosion.

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Editorial Forum



*By Ramona Isbell,
Executive Editor*

Much ado in the ITU

The International Telecommunications Union (ITU) has had a busy year so far. At the top of the union's "to-do" list is the continued development of next-generation wireless services and systems under the auspices of "Working Party 8F," which is a group of experts assigned to this task. The goal of this newly created ITU group is to act as a forum for user requirements — and as a catalyst for translating those realities into technical reality. In a nutshell, this means the Working Party 85 needs to provide firm guidance during IMT-2000's continuous system development.

The team had its first meeting in March under the leadership of chairman Stephen Blust of U.S.-based Bell-South Cellular. He, along with three vice-chairs and more than 150 industry representatives, addressed such issues as spectrum needs, higher data rate capabilities, Internet Protocol (IP)-based service and system needs beyond IMT-2000. Dealing with these issues and the ever-changing industry needs will be not be simple. If Blust can live up to his aspirations, he'll need to maintain strong synergy among the powerful representatives from the industry's regulators, manufacturers and international operators, along with the folks from the ITU.

An even more significant ITU action is its recent commitment to re-engineer itself to better meet the evolving telecommunications market. A 27-member Reform Advisory Panel (RAP), set up by ITU Secretary-General Yoshio Utsumi, has identified key principles to guide the ITU's reform. One key point in the reform agenda is to define the ITU's future role in Internet governance.

To date, the Internet phenomenon has progressed without any formal guidance or government regulation. It's commendable of the ITU to realize that as the Internet continues its march into voice telephony and mobile communications, a strong organization with harmonized global leadership can play an effective role in shaping this emerging market.

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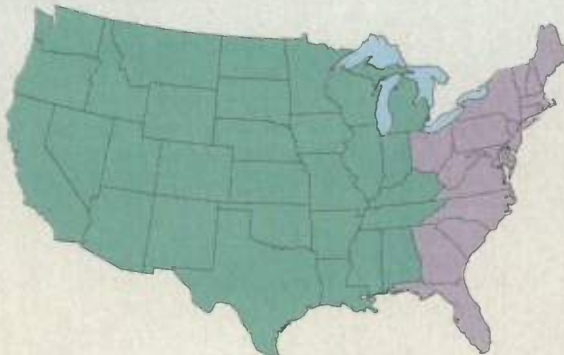
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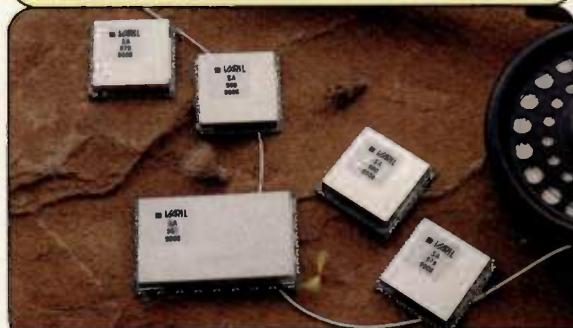
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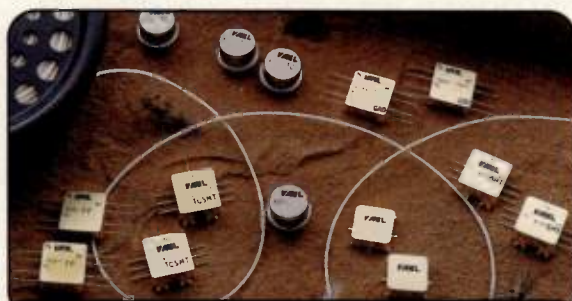
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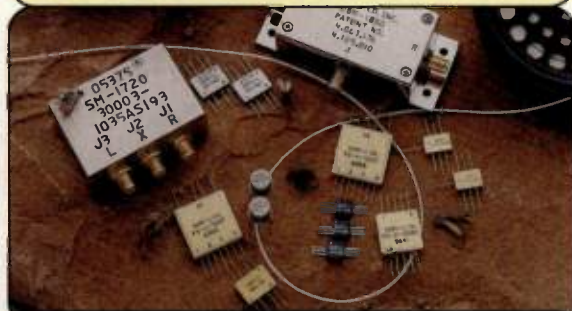
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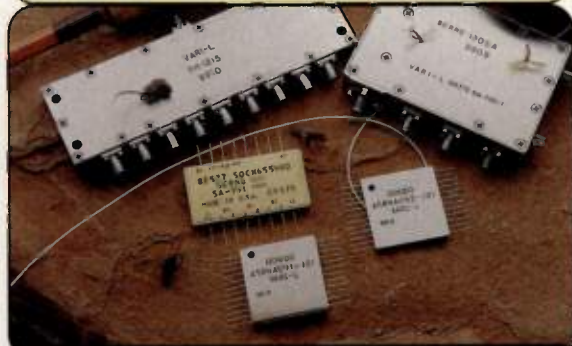
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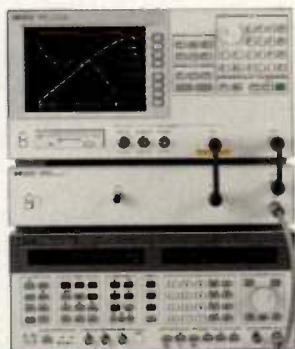
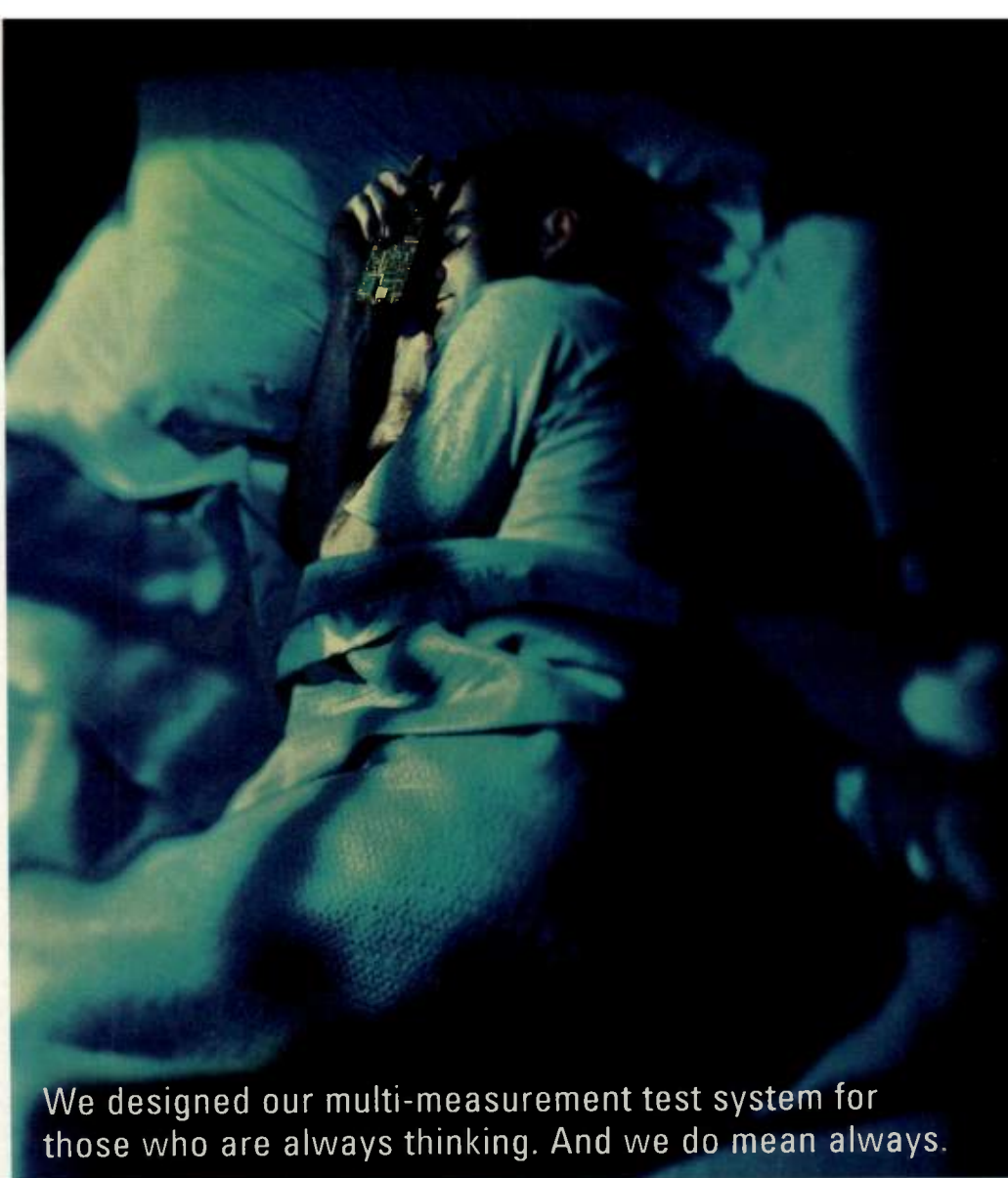
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RF calendar

- April 10-12 DSP World Spring Design Conference—San Jose**—Information: Miller Freeman. Tel. 415.538.3848 or 888.239.5563; e-mail dspworld@mfi.com.
- 10-14 IEEE IFIP 2000 Network Operations and Management Symposium—Honolulu**—Information: Cayle Weisman, IEEE Communications Society. Tel. 212.705.8941; Fax 212.705.8999; e-mail noms2000@comsoc.org.
- April 26-28 Global Wireless Convergence—4th Annual Summit 2000—Cancun**—Information: Universal Wireless Communications Consortium, 1800 - 112th Ave, NE, #260E, Bellevue, WA 98004-2937. Tel. 425.372.8922; Web site www.uwcc.org.
- May 1-3 Internet Device Builder Conference—Santa Clara, CA**—Information: IDB 2000 Customer Service. 611 Route 46 West, Hasbrouck Heights, NJ 07604. Tel. 888.947.3734; Fax 201.393.6297; Web site www.iDeviceBuilder.com.
- 8-10 Embedded Systems Conference—Napa, CA**—Information: Miller Freeman. Tel. 415.538.3848; Fax 888.239.5563; e-mail esc@mfi.com.
- 16-17 Broadband Wireless Access—London**—Information: Laura Sykes. Tel. +44.171.636.1976. Web site www.ibctelecoms.com/bwa.
- 18 Wireless Networks: The Third Generation—Washington, DC**—Information: Telcordia Technologies. Tel. 800.521.2673. Web site www.telecom-info.tecordia.com.
- 21-24 50th Electronic Components and Technology Conference—Las Vegas, NV**—Information: Jim Bruorton. Tel. 864.963.6621. Web site www.ectc.net.
- June 4-8 Supercomm 2000—Atlanta**—Information: Tel. 800.278.7372; Web site www.supercomm2000.com.
- 11-16 2000 IEEE MTT-S International Microwave Symposium—Boston**—Information: Web site www.ims2000.org.
- 14-19 IEEE International Conference on Third Generation Wireless Communications—Silicon Valley, CA**—Information: Willie W. LU, 1960 Linden Lane, Milpitas, CA 95035. e-mail wvlu@ieee.org; Web site www.3Gwireless.com.
- 18-22 IEEE International Conference on Communications—New Orleans**—Information: Richard W. Miller, Tel. 504.528.2553; e-mail r.w.miller@ieee.org; Web site www.icc00.org.

RF courses

- **Georgia Institute of Technology—Infrared Technology and Applications**—Apr 4-7;
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- **UCLA—Microelectromechanical Systems: Technology, Design and, Application**—April 24-28; **Charge Coupled Devices / CMOS Imaging Sensors and Cameras**—May 8-12; **Compression for Digital TV**—May 10-12; **Digital Signal Processing: Theory, Algorithms, and Implementation**—May 15-19; **Honeycomb Sandwich Structures**—May 16-19; Information: Information Systems and Technical Management Short Courses, Los Angeles, CA. Tel. 310.825.3344; e-mail mhenness@unex.ucla.edu; Web site www.uclaextension.org/shortcourses.
- **Virginia Tech—Antennas: Principles, Design and Measurements**—May 22-25, Orlando. Information: Dr. Warren Stutzman, Virginia Tech, Electrical Engineering Dept., Blacksburg, VA 2401-0111. Tel. 540.231.8401; Web site www.usit.com/antenna.
- **Henry Ott Consultants—Electromagnetic Compatibility Engineering**—Apr 26-28, East Hanover, NJ. Information: Henry Ott Consultants, 48 Baker Road, Livingston, NJ 07039. Tel. 973.992.1793; Fax 973.533.1442.
- **University of Missouri-Rolla—Grounding and Shielding Electronic Systems; Circuit Board Layout to Reduce Noise Emission and Susceptibility**—April 12-14, Columbus, OH; April 17-19, Chicago IL, June 5-7, Minneapolis, MN, Aug. 16-18, Baltimore, MD. Information: Continuing Education office. Tel. 573.341.4132. Web site www.umsr.edu/~conted.
- **Besser Associates—RFIC Techniques for Wireless Applications**—April 10-12, Mountain View, CA; **RF CMOS Design**—April 13-14, Mountain View, CA; **Frequency Synthesis Technology and Applications in Wireless Systems**—April 17-19, Mountain View, CA; **Applied RF Techniques I**—April 24-28, Mountain View, CA; **Advanced Wireless and Microwave Techniques**—May 8-12, Mountain View, CA. Information: Continuing Education office. Tel. 573.341.4132. Web site www.bessercourse.com.
- **National Institute of Standards and Technology—Understanding the Characteristics of Clocks and Oscillators, Making Precise Time and Frequency Measurements, and Synchronizing Precision Time Systems**—June 13-16, Boulder, CO. Information: Wendy Ortega Henderson, Tel. 303.497.3693. Web site www.boulder.nist.gov/t.



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Will WAP lead the way by 2003?

Wireless Application Protocol (WAP) and Bluetooth technology may represent the greatest revenue potential for U.S. and Western European mobile operators, according to a recently released study by VisionGain, United Kingdom.

The WAP Report predicts that by 2003, 95% of handsets shipped by manufacturers to Western Europe and the United States will be WAP-enabled; 70% will incorporate Bluetooth technology. Of the 1,000 plus mobile users VisionGain surveyed throughout Europe, more than 50% said they would consider replacing their wireline with a wireless handset.

Citing the confluence of wireless and IP network prevalence as setting the stage for more widespread wireless data adoption, the report views WAP as a critical transition protocol to emerging mobile multimedia arena.

"VisionGain believes that WAP offers operators a way of differentiating themselves from their competition and an opportunity to test near-3G services," said Bill Patterson, VisionGain's senior analyst.

New cellular standards published by TIA

The Telecommunications Industry Association (TIA) has published a new standard "Mobile Station-Base Station Compatibility Standard for Enhanced 800 MHz Analog Standard," TIA/EIA-691; and a new interim standard, "Base Station-Mobile Station Compatibility Specification for 800 MHz Cellular, Auxiliary and Residential Services," TIA/EIA/IS - 91-A. These technical requirements form a compatibility standard for a cellular radio telecommunications system. Their purpose is to ensure that a mobile station can obtain services in any cellular system manufactured according to both standards. These requirements do not cover equipment performance or measurement procedures.

Home connectivity market to reach \$5.7 billion by 2004

The worldwide home networking equipment and residential gateway market is expected to grow from more than \$600 million in 2000 to more than \$5.7 billion by 2004, according to recent research by Cahner In-Stat Group.

This growth will be spurred by the

growing interest in home connectivity from numerous technology industries.

"All aspects of the connected home—communications, entertainment and home systems management will be interconnected in the future using networking and Internet technology," said Mike Wolf, senior analyst for Cahners In-Stat Group.

The networked home will move from today's first generation products, such as basic PC adapter cards and simple gateways, to tomorrow's, where connectivity technology is embedded in recognizable devices that non-technical users are familiar and comfortable with.

New connectivity—based services, enabled through home networking technology, will help drive growth in this market. Additional voice lines, home management and monitoring, as well as new value added entertainment services will create a \$3 billion connectivity services market by 2004.

Companies team to develop 3G radio chip

Analog Devices, Norwood, MA, and Mitsubishi Electric, Japan, have developed a radio chip for use in third generation (3G) cellular phones. The direct conversion radio chip is used in cellular handsets for the W-CDMA. Direct conversion (zero IF) eliminates the intermediary frequency section of traditional radio technologies. Direct conversion enables radio designers to take a high frequency of RF input signal directly to baseband or low frequencies, eliminating scores of components and boosting efficiency.

The new chip includes variable-gain amplifiers, baseband channel filters, and a wide-range logarithmic amplifier for RSSI detection. It consumes low power and the direct conversion architecture eliminates many of the oscillators and filters required by receivers.

Photon switch aids photon, electron conversion

Agilent's photonic switching platform is an optical technology capable of routing communications traffic without the costly conversion from photons to electrons and back to photons.

This ability to manage communications traffic in the optical domain has

been called the "missing link" for the next-generation all-optical network. By eliminating the equipment needed to translate the basic light signals into electrical signals for the purpose of routing those signals, improvements in capacity and cost reductions are made possible.

The switch—based on a combination of inkjet and planar lightwave circuit technologies—is already in trials with several industry company's for integration into complex communications network elements.

EMC product standard changes for converters

The EMC product standard for "variable-speed drives" frequency converters EN 618003 has been supplemented by Annex A11. The new standard contains a number of changes and more details than the 1997 published standard.

The new version mandates that equipment be sold with the warning label. "This equipment is not designed to be run from a low-voltage household supply network, as it is liable to cause radio interference." The annex now defines limit values for this equipment with respect to line-run noise parameters between 0.15 and 30 MHz, depending on the dimensions of the converter. The principle of protection of adjacent installations remains unchanged.

Contracts

Qualcomm will replace Burlington's mobile units—Qualcomm, San Diego, announced Burlington Motor Carriers, Daleville, IN, has elected to replace its currently installed mobile communications system units with Qualcomm's OmniTracs Mobile information management systems units.

Motorola, Telefon AB L.M. Ericsson win Turkish contract—Motorola, Northbrook, IL, and Telefon AB L.M. Ericsson, Sweden, have won contracts with more than \$2 billion to provide mobile phone equipment in Turkey.

IFR wins \$8.1 million British contract—IFR Systems, Wichita, KS, has won a contract from British Telecommunications, UK, valued at \$8.1 million, over three years to supply calibration and maintenance services for BT's electronic test equipment used in field and laboratory applications throughout the UK.

Continued on page 18



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BUSINESS BRIEFS

Power Amplifier patent awarded—Anadigic's, Warren, NJ, has been granted a US patent for its single-chip power amplifier architecture. The company has been awarded a total of 18 patents and has five patents pending.

Psion, Motorola to develop wireless Internet devices—Hand-held computer manufacturer Psion, UK, has announced plans to develop mobile Internet access devices with Motorola, Northbrook, IL. They expect to launch the products worldwide during the first half of 2001. Psion and Motorola will market the wireless devices separately, but the new products will carry the logos of both companies.

Qualcomm forms agreement with Telson—Qualcomm, San Diego, has entered into a worldwide CDMA subscriber unit license agreement with Telson Information & Communications of Korea. Under the agreement, Qualcomm has granted Telson I&C a license under Qualcomm's proprietary CDMA technology and patents to develop, manufacture and sell subscriber unit products for cdmaOne, cdma2000 and HDR air interface technologies.

Rogers, Kuraray to develop new circuit material—Rogers, Rogers, CT, and Kuraray, Japan, have signed an agreement to develop LCP-based film technology into circuit materials for specific market applications.

Microchip Technology opens new design center—Microchip Technology, Chandler, AZ, has opened a design center in Bangalore, India. The new design center will support design and development efforts for the company's integrated circuits, embedded software and applications and local sales operations.

Varetis, Hewlett-Packard Mobile E-services join forces—Varetis AG, formerly pc-plus Infor-

matik AG, Germany, has joined Hewlett-Packard Mobile E-services Bazaar to better facilitate the application of wireless application protocol (WAP) technology in the expanding field of e-services.

Metricom selects Hirschmann as antenna supplier—Metricom, Los Gatos, CA, has selected Hirschmann, Pine Brook, NJ, as a supplier of custom designed wired access point antennas. The Hirschmann antennas provide RF communications at both the 900 MHz band and the 2.4 GHz band.

Calibre, Infineon team to dual source products—Calibre, San Jose, a cordless connectivity hardware and software subsystems supplier, has reached an agreement with Infineon Technologies, Germany, to dual source selected products in their IrDA compatible data transceiver product lines.

RF Micro Devices, ShareWave team to design radio—RF Micro Devices, Greensboro, NC, has collaborated with ShareWave, El Dorado Hills, CA, on the design of the radio used by ShareWave's OEM customers.

Pulse forms new group—Pulse, San Diego, has formed a group dedicated to developing and supporting a broad range of off-the-shelf electronic components for the cable market.

Quake Wireless, Samsung form alliance—Quake Wireless, San Diego, has entered into a strategic alliance with Samsung Electro-Mechanics, Korea. Samsung will manufacture Quake's satellite communications products that enable companies to track, monitor, and provide two-way data communications capabilities between fixed and mobile assets worldwide.

Agilent, SyntheSys form licensing agreement—Agilent Technologies, Palo Alto, CA, has

signed a licensing agreement with SyntheSys Research, Menlo Park, CA, for its error-analysis technology. This technology will allow engineers the ability to uncover the causes behind errors in digital components and system hardware.

Ultra RF, GHz form strategic alliance—Ultra RF, Sunnyvale, and GHz Technology, Santa Clara, have formed a strategic alliance. Under alliance terms, Ultra RF will supply ultra gold silicon LDMOS wafers to GHz for inclusion in devices targeting avionics, broadcast and other non-wireless applications.

Adicom Wireless, Dragon Telecommunications team up—Adicom Wireless, Hayward, CA, has forged an alliance with Dragon Telecommunications, China. The company has signed a contract with Piono High Tech, a subsidiary of GDT in Shenzhen, Guangdong province, to manufacture and market Adicom's Aditus family of wireless access products under the Piono name throughout China.

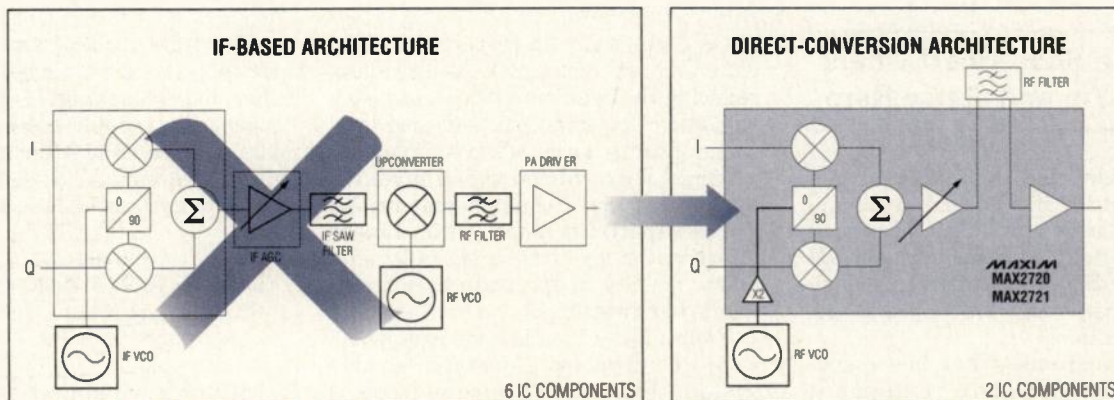
Ultima Communication, Silicon Wave form license agreement—Ultima Communication, Carlsbad CA, and Silicon Wave, San Diego, have formed a cross-license agreement for protocol software for the implementation of Bluetooth wireless technology. Under the agreement, both companies will be allowed to deliver complete software solutions to OEM's looking to add Bluetooth functionality to their products, while minimizing the development cycle.

Panasonic, Mitel, Philsar team—Panasonic, Japan, is co-developing a module for next generation Bluetooth systems with Mitel Semiconductor and Philsar Semiconductor. The trio's product will be a complete module designed to accelerate the development of Bluetooth systems with low power consumption cost and time to market.

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Spread spectrum and PLL technology combine to reduce EMI

Combining state-of-the-art spread spectrum and PLL design offers 10 dB improvement in measured EMI.

By I-The Sha, Albert Chen,
Kuang-Yu, and Jeffry Keip

This article will examine the design parameters of a spread spectrum clock generator that uses advanced PLL technology to reduce measured EMI by 10 dB. The result is a design solution to pass tough FCC Class B system qualification.

A numerical model has been successfully developed to implement spread spectrum in Phase-Locked Loops (PLLs). Using this patent pending technology, a modulating signal is generated by circuitry injected into the feedback path of the PLL.

Spread spectrum clock generators are a proven and reliable method to reduce the spectral amplitude of EMI components over a substantial bandwidth. The spread spectrum clock block diagram is shown in Figure 1. This technique includes modulation inside closed loop operation.

By spreading the bandwidth, the amplitude of the synthesized clock sig-

nal is decreased with respect to its fundamental and harmonics. As a result of reducing the peak amplitudes, the peak radiated electromagnetic emission level is significantly lower when compared to a typical narrow band signal produced by conventional frequency generators. Spread spectrum clock generation is effective for lowering a signal's peak power density in spectrum by increasing its bandwidth.

From Figure 1, a time-varying model would be developed by state variable system. Finite difference method is applied to develop the numerical model. Then, the best modulating profile is determined by the least square error method. A 4.5 to 5.5 MHz reference frequency following the input divider is recommended. That range of reference frequency optimizes the resolution of modulation shape and silicon area occupied.

Numerical modeling

A state variable PLL in time-varying model can be derived as:

$$dx/dt = A(t) \cdot x(t) + B \cdot u(t) \quad (1)$$

The state variable $x(t)$ is a 3×1 vector. $A(t)$ is a 3×3 time-varying matrix that makes equation (1) be a nonlinear model. B is simply a constant and $u(t)$ is a 3×1 vector. After applying finite difference method to equation (1), the discrete system is defined by equation (2).

$$x(N+1) = A(N+1) \cdot x(N) \cdot \Delta t(N+1) + B \cdot u(N) \cdot \Delta t(N+1) + x(N) \quad (2)$$

Δt is a time step between the present and next cycle. For the given trial values of $A(N+1)$, $x(N)$ and $\Delta t(N+1)$, $x(N+1)$ can be solved to match an modulation waveform by least square error theory. The equation is iterated until optimal results are received.

Modulation profile

The shape of the modulation waveform is critical to maximum EMI reduction. The modulation profile used to accomplish the greatest reduction in EMI is shown in Figure 2. The period of the modulation is shown as a percentage of the period length along the x-axis. The amount that the frequency is varied is shown along the y-axis. The modulation profile is also shown as a percentage of the total frequency spread. The modulating signal has a frequency of approximately 31 KHz. Actually, any modulating frequency can be achieved by using feedback path control.

As shown in Figure 3, each harmonic of a modulated clock has a much lower amplitude than that of an unmodulated signal. The reduction in amplitude is dependent on the harmonic number, the frequency deviation, the percentage of spread, and the modulation frequency.

Spread spectrum jitter

The cycle-to-cycle jitter induced by the modulating clock is insignificant compared to the PLL's original cycle-to-cycle jitter. For example, applying a 100 MHz clock with $\pm 1\%$ deviation to Figure 2, the

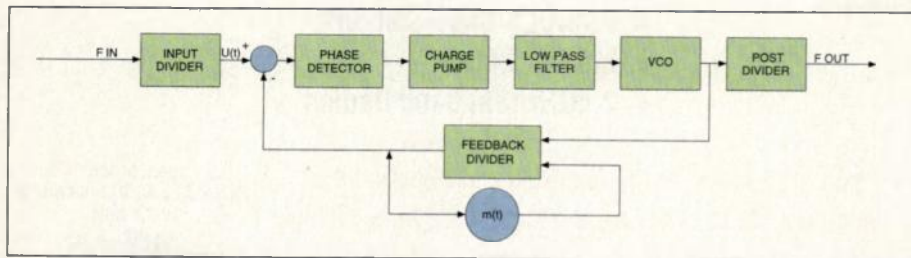


Figure 1. Block Diagram of spread spectrum PLL.

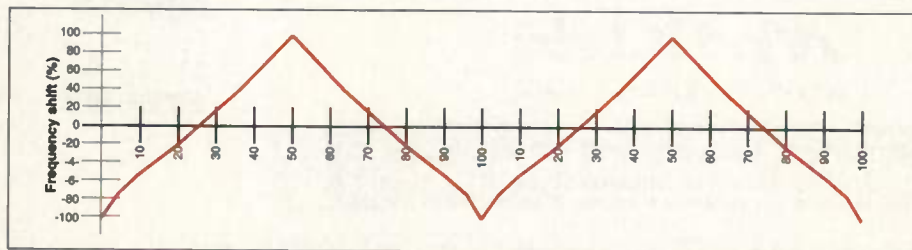


Figure 2. Lexmark modulation waveform profile.

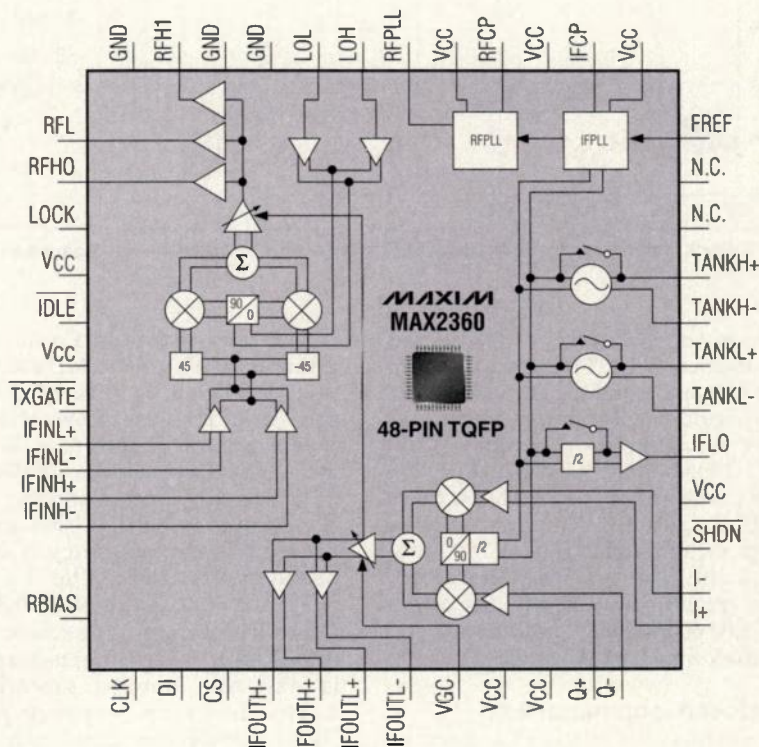
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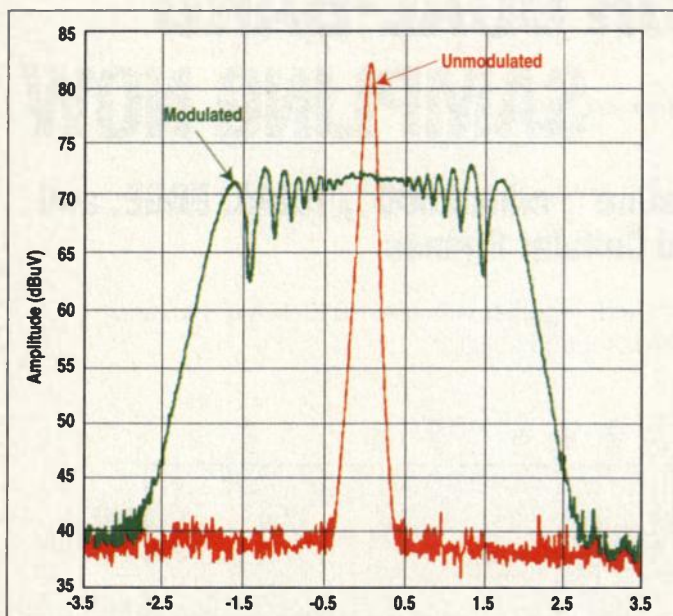


Figure 3. Clock harmonic with and without SSCG modulation in the frequency domain.

period of the waveform is 50 kHz at 100% location. A 100 MHz clock points to 0% of frequency shift. Then the peak-to-peak period displacement from f_{\min} (-100%) to f_{\max} (+100%) equals $(1/(100 \text{ MHz}(1-1\%)) - 1/(100 \text{ MHz}(1+1\%))) = 200 \text{ ps}$. One half period of modulation takes $10 \mu\text{s}$ from f_{\min} to f_{\max} . Thus, the number of clock cycles is $10 \mu\text{s}/10 \text{ ns} = 1000$ in a half modulation period. Therefore, spread spectrum only contributes, on average, $200 \text{ ps}/1000 = 0.2 \text{ ps}$ jitter to a 100 MHz clock with $\pm 1\%$ deviation.

PLL closed loop bandwidth

The bandwidth of the PLL must be larger than the modulation frequency to allow the modulation signal pass through. Equation 3, a transfer function developed from Figure 1, shows the PLL bandwidth in the frequency domain. VCO is the vco gain of the PLL. CP is the charge pump current and C_1 , C_2 , R_1 are the components in the loop filter. FBD is the number of feedback divider. $m(t)$ is used for modulating signal.

$$H(s) = \frac{VCO \cdot \frac{cp}{C_1} \left(s + \frac{1}{R \cdot C_2} \right)}{\left(s^3 + \frac{C_1 + C_2}{R_1 \cdot C_1 \cdot C_2} \cdot s^2 + cp \cdot \frac{VCO}{C_1 \cdot FBS} \cdot s + \frac{cp \cdot VCO}{R_1 \cdot C_1 \cdot C_2 \cdot FBD} \cdot \frac{1}{1 + FBD \cdot m(t)} \right)}$$

Equation 3. The transfer function.

The parameters in Equation 3 are given as VCO = 50.43 MHz/v, $C_1 = 500 \text{ pf}$, $C_2 = 2000 \text{ pf}$, $R_1 = 5 \text{ k}$, FBD = 45 and $cp = 1 \text{ mA}$. Figure 4 shows the normalized transfer function in Bode plot form. The -3dB point is located at 100 KHz which is larger than the modulation frequency, but still low enough to prevent high frequency noise from passing through it. The 2 dominate poles can be found at 59.97 KHz using MathCad. Damping factor of PLL is 0.444. After inverse Laplace transform is taken to a unit step times Equation 3, the unit step response presents PLL's acquisition time from one frequency to another frequency.

Measurement and results

This feedback path modulation technique has been successfully designed into two product families. In Figure 5, a 50 KHz modulating frequency is used to modulate a clock. The target deviation of the profile is $\pm 0.5\%$. Test results show a 49.78 KHz frequency modulation signal spreading a 100.2785 MHz

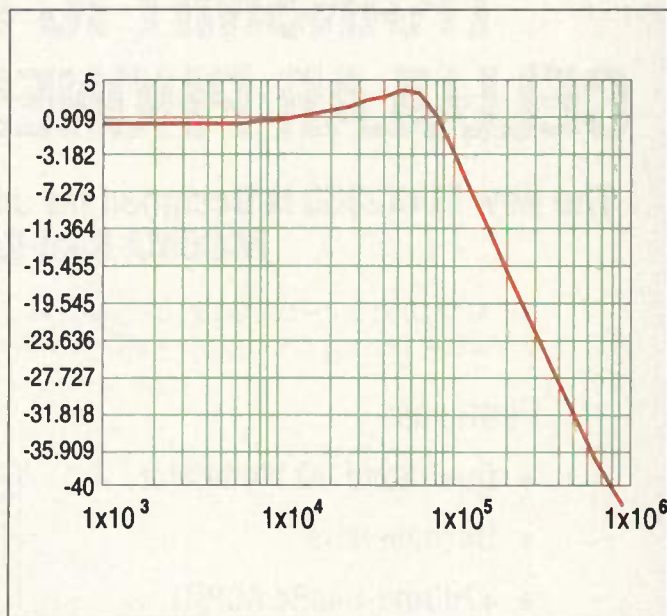


Figure 4. PLL Closed loop bandwidth.

with peak-peak 0.986 MHz deviation. The measurements show the error from target profile to be 1.635% maximum in peak-peak deviation and 0.44% maximum in modulation frequency.

Meanwhile the jitter shows only 1 p increase after turning on the spread spectrum features. Figures 6 show unmodulated and modulated 100 MHz clock jitter measurements, respectively.

Comparing the modulated and unmodulated fifth harmonic of the clock spectrum measures 8.33 dB reduction in Figure 7.

Products and applications:

There are many different families of devices with spread spectrum PLL incorporated in them. The family upon which this article is based is a single PLL based device which can be provided in 8 or 16 pin SOIC's. Various existing options simply take an input signal

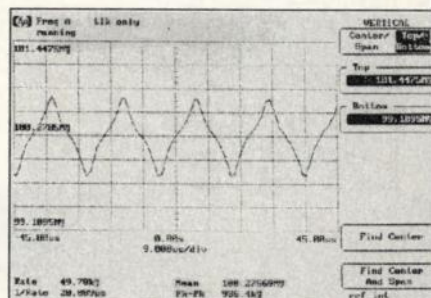
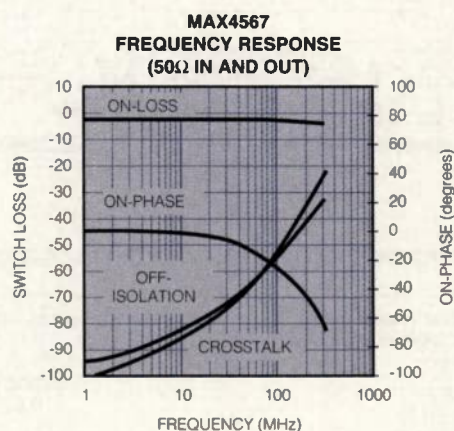


Figure 5. Modulation waveform generated by W48S101 product.

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MAX4546	Dual SPDT	20	1	0.5	-80/50	-80/50	0.004	16-Pin DIP, SOIC, QSOP
MAX4547	Dual SPDT (High- Isolation Pinout)	20	1	0.5	-82/55	-84/55	0.004	16-Pin DIP, SOIC, QSOP
MAX4565	Quad SPST	60	2.5	2	-80/55	-80/55	0.02	20-Pin DIP, SOIC, SSOP
MAX4566	Dual SPDT	60	2.5	2	-80/55	-80/55	0.02	16-Pin DIP, SOIC, QSOP
MAX4567	Dual SPDT (High- Isolation Pinout)	60	2.5	2	-83/55	-87/55	0.02	16-Pin DIP, SOIC, QSOP

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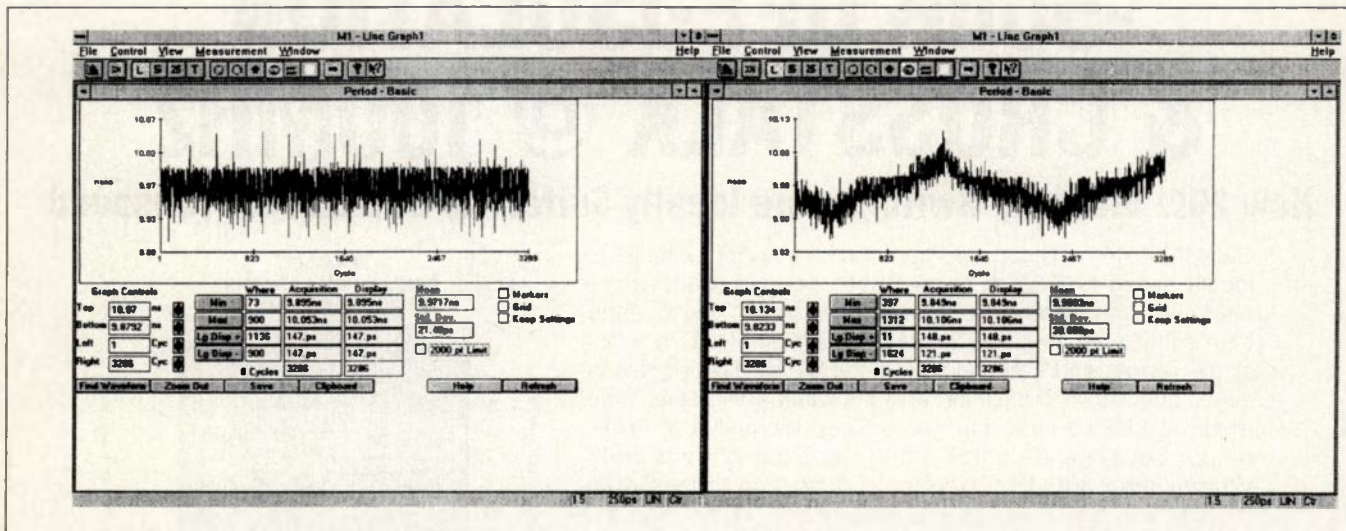


Figure 6. Test results showing the largest displacement of 147ps induces cycle-to-cycle jitter at unmodulated 100MHz clock and 148ps cycle-to-cycle jitter at a modulated 100MHz clock.

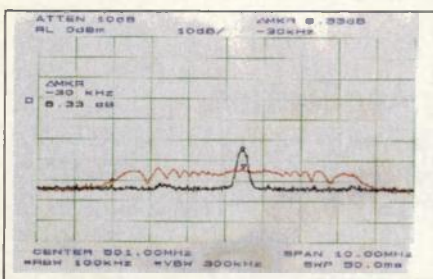


Figure 7. Graph of EMI at 5th harmonic.

and offer at the output 1to6 copies of the input with a selected spread spectrum component added. Some options offer simple multiplication of input frequencies on top of the spread spectrum addition, and through metal mask variations on the base, the device has the ability to provide a wide variety of output frequencies for any given input. A wide variety of systems including printers, fax machines, home video game systems, and disk drives have found spread spectrum clocks useful for some of the frequencies required by their components. Some types of drivers (print heads for example) will not function acceptably using today's spread spectrum clocks, but future devices are under development as possible solutions for such applications.

A second family of products utilizing spread spectrum technology has two PLLs, but only one of them offers the SSCG feature. This is a line of clock generators for 66 and 100 MHz chip set requirements. Virtually all motherboard manufacturers have embraced the SSCG technology.

Conclusions

The numerical model of spread spectrum control in feedback path is a nonlinear differential system. Finite difference is a very powerful method to solve time-varying nonlinear system solutions. Least square error is a popular numerical method to apply to fit a curve. It always follows the ideal spread spectrum waveform closely. Therefore, the modulation profile is mathematically derived as providing maximized reduction of EMI over a given variation range, without adding any significant amount of cycle-to-cycle clock jitter. All the measured results show good match to target design. Theoretically, feedback modulation is not only able to achieve any deviation precisely, but also to have better EMI reduction. Higher resolution and smooth profile are desired for modulating profile that reduces more power density in all harmonics.

RF

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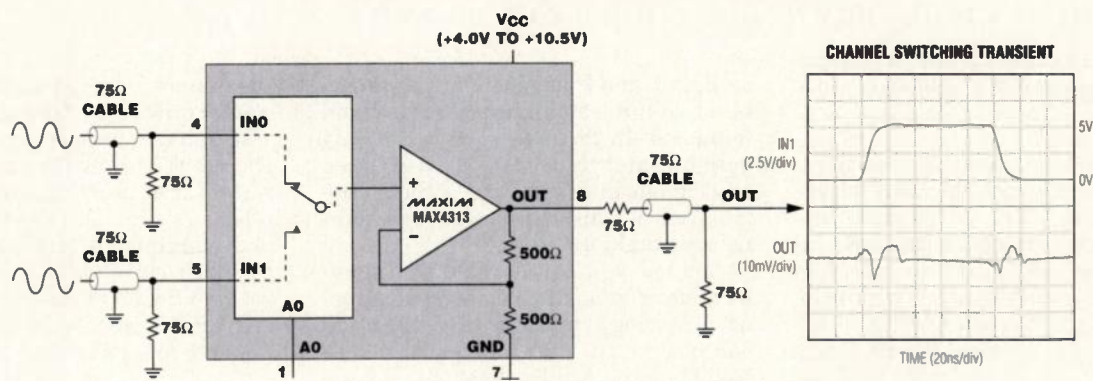
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MAX4310	2	1	280	60	0.06/0.08	460	40	10
MAX4313	2	Fixed gain of 2	150	40	0.09/0.03	540	40	10
MAX4311	4	1	345	40	0.06/0.08	430	40	10
MAX4314	4	Fixed gain of 2	127	78	0.09/0.03	430	40	10
MAX4312	8	1	265	35	0.06/0.08	345	40	10
MAX4315	8	Fixed gain of 2	97	46	0.09/0.03	310	40	10

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Embedded antennas—technology for next generation handsets

External antennas have long been the bane for handsets and their designers. Embedded antennas may be the solution they've been looking for.

By David McCartney

Today, wireless handsets represent a mere shadow of their technological past. Just a few years ago, the ratio of mobile to portable handsets in cellular was 90% mobile to 10% portable. In contrast, today's ratio is 95% portable to 5% mobile. During this transition, there have been several hundred or more technological innovations applied to the current crop of modern wireless handsets. These innovations have empowered manufacturers to increase performance, reduce weight and size and reduce cost.

For example, handset designers have migrated from 14 V to 3 V. They have developed dynamic usage and application DSPs and have gone from analog

to digital, and from single-mode, single-band to dual-mode, dual/triple-band handsets. In fact, just about the only design aspect that has not experienced any significant innovation is the antenna. Well, it's about time antenna technology caught up.

And today, it has — thanks to significant developments in embedded antenna technology that just may mean the end of problem-ridden external antennas. Long the Achilles heel of any wireless handset, external antennas have suffered from breakage issues, performance issues, cost issues, and, finally, ergonomic issues.

Next generation antennas

Embedded antennas, especially patch antennas, are not new. But they have met with limited success mainly due to the limitations of performance

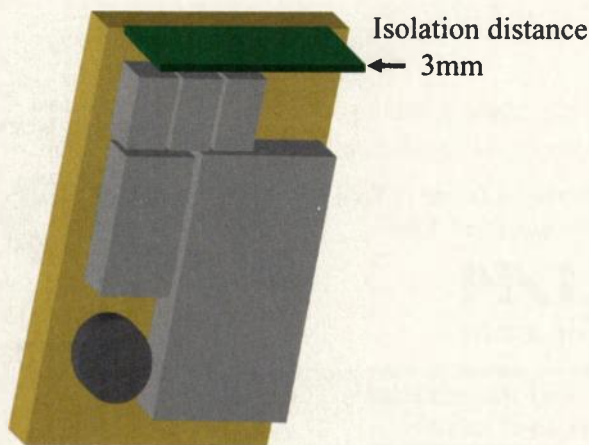
(designers have demanded whip-like performance). Ongoing antenna research and development has provided the market with products that eliminated this performance issue. New offerings provide both embedded omnidirectional antennas with 1 dBi to 5 dBi gain, voltage standing wave ratio (VSWR) of less than 2:1, and significant cost reduction when compared to today's whips.

Embedded antenna design criteria

Antennas are being developed on both proprietary and open designs and several series of antennas are available for use in cellular and PCS wireless handsets. These antennas are a highly efficient resonator designed to act as the frequency-determining element (like an asymmetrical dipole antenna. The

Perpendicular

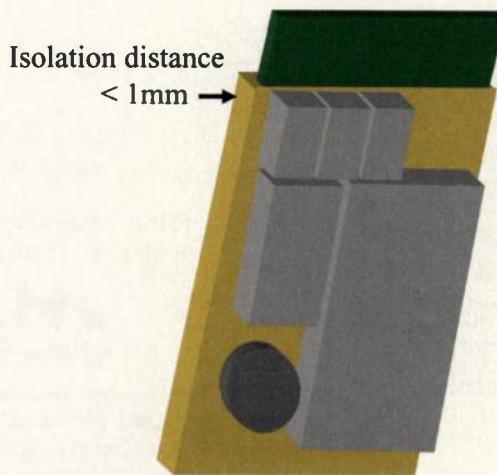
Phone increased in length by 3mm isolation distance and antenna thickness (3.8mm for PCS)



Perpendicular — phone increased in length by 3 mm isolation distance and antenna thickness.

Parallel

Phone increased in length by antenna height (10.2mm for PCS) plus small isolation distance



Parallel — phone increased in length by antenna height plus small isolation distance.

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2WAY-180°	2	1.00-2.49
3WAY	11	0.50-4.20
4WAY	38	0.67-8.40
5WAY	4	0.80-1.80
6WAY	11	0.80-5.00
7WAY	1	1.81-1.99
8WAY	28	0.80-8.40
9WAY	2	0.80-4.80
10WAY	5	0.75-2.40
12WAY	5	0.80-4.20
16WAY	8	0.80-4.80
32WAY	1	0.95-1.75

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Get Your Hands Off the Antenna

Embedded antennas (like all antennas) face the challenges of coverage by the hand and the resulting detuning to the antenna. As handset designers start working with this new embedded antenna alternative, the major mechanical issue becomes the location of the antenna in relation to the hand. As handsets become increasingly smaller, the hand detuning issue is an even more critical factor for the industrial designer, the electrical engineer, and finally the marketing department that must promote the device.

In addition, designers today want to maximize reception and minimize the rate at which the body blocks or absorbs the power radiating from wireless antennas. Because the position of the antenna, relative to the user, affects the absorption rate, the application of embedded antennas offer designers a new alternative. The search for a less obtrusive antenna than the monopole (whip) has led RangeStar to develop directional embedded antennas that do not

require extension of the handset case. The top-mounted and back-mounted versions of these embedded antennas offer the designer new alternatives as well as an increase in performance.

Specifically the back-mounted embedded antenna, which is placed at the top rear of the handset, places the handset chassis between the user and the antenna during a call. This C energy pattern redirects, in the case of RangeStar's 'C' planar antenna, up to 15dB front to back. This placement substantially reduces the peak specific absorption rate (SAR) in the user's head. These new SAR reduced embedded antennas have encouraging application potential.

The radiation characteristics of these medium-to-high SAR reduction antennas can now achieve the bandwidths necessary for today's cellular/PCS and cordless applications. Thus they hold tremendous promise for the future, with continued improvements in performance and cost in cellular/PCS or cordless handsets worldwide.

Low SAR 1.8 GHz/1.9 GHz C-Planar antennas

Size	1.2 x 0.8 x 0.25
Weight	2.5 grams, nominal
performance	3 to 4 dB over whip
Applications	Cellular phones, WLANs, hearing impaired wireless products

Moderate SAR 1.8GHz/1.9 GHz R-planar Antennas

Size	1 x 0.5 x 0.09
weight	1.8 grams, nominal
Performance	1 to 2 dB over whip
Applications	1.9 GHz cellular/PCS phones where PWB space is available on or above existing PCB

Omni antenna for 800/900 MHz, 1.8/1.9 GHz and dual band

Size	1.25 x 0.5 x 0.03
Weight	1 gram nominal
Performance	gain comparable to whip
Applications	800 MHz, 900 MHz and dual-band cellular/PCS, cordless phones and WLL

second half of the dipole is provided by the Printed Circuit Board (PCB) of the wireless device.

To assist with the design and implementation of these new embedded antennas, it is necessary to understand certain design criteria. Such criteria include antenna isolation, ground plane length and feed points. These design elements are critical to achieving the best-embedded antenna performance in a handset.

Antenna isolation

The first criteria, antenna isolation from the transceiver circuitry, is needed to prevent detuning of the antenna element. It can be achieved by mounting the antenna at right angles to the PCB and leaving a small separation between the components and the antenna, or by mounting the antenna parallel to the PCB or at the end of the PCB.

The performance figures of the two configurations are similar, and the trade-off between the two mounting methods is the overall length of the device, which depends on isolation distance and antenna dimensions.

• **Isolation Distance** — With the parallel design, no isolation distance is required other than to ensure that the PCB ground plane is not touching or located behind the antenna. Therefore isolation distance is typically less than 1 mm. In the case of perpendicular mounting, the antenna element must be some 3 mm from any active elements or the ground plane on the PCB.

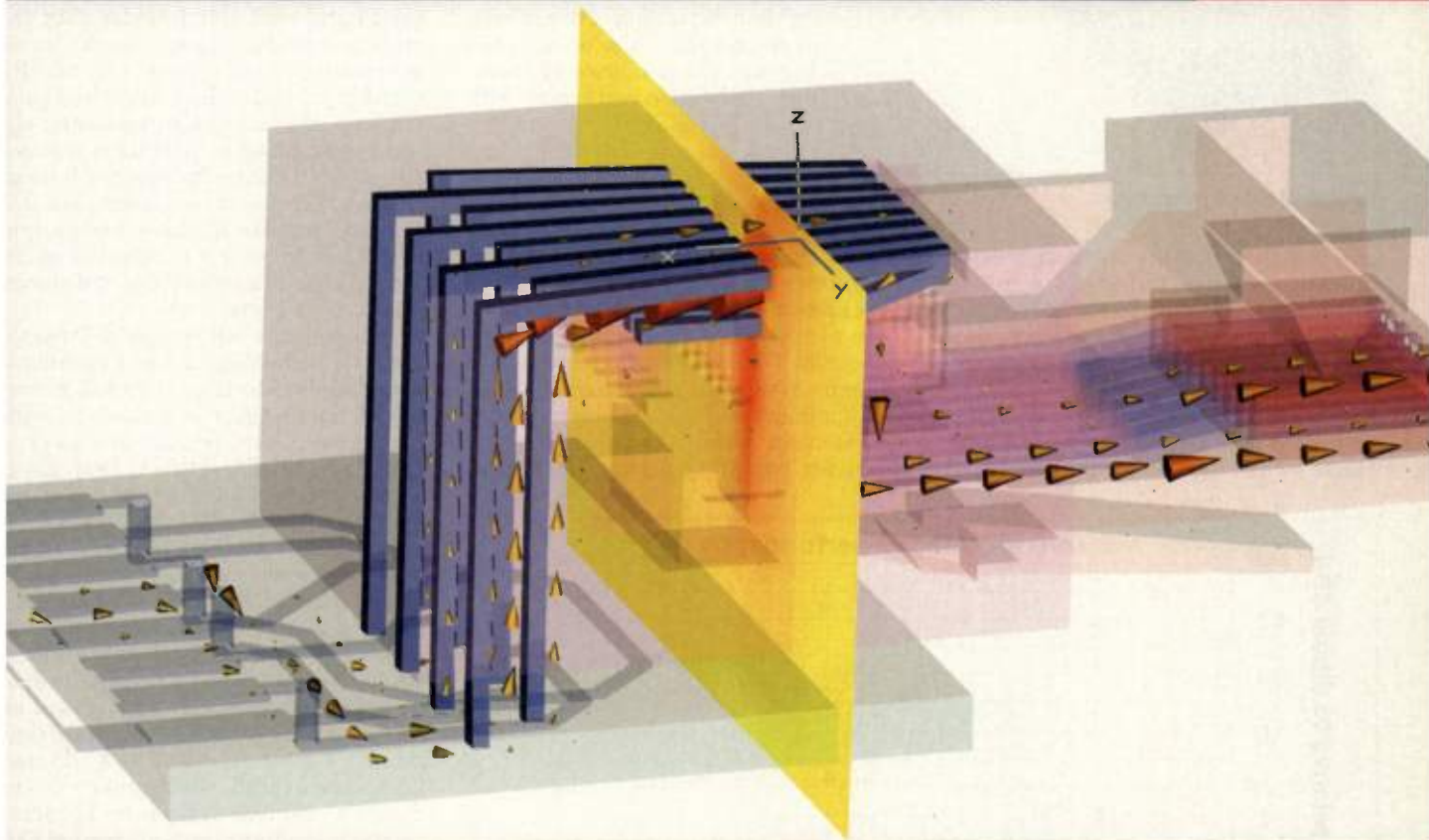
• **Antenna Dimensions** — In the perpendicular design, an antenna's dimensions are not a factor in overall length of the device. There is no increase in height other than that necessary for the isolation distance. With the parallel mounting, the length has to be increased by the height of the antenna which can be anywhere from 10 mm to 17 mm for current designs.

With the emphasis manufacturers place on minimal phone footprint designers focus on the perpendicular mounting configuration for most applications—with the exception of fold phones, which offer excellent platform for parallel mounting.

Ground plane length

Because these new antennas in effect use the ground plane as the main radiating element, the effect of overall ground plane length on the performance

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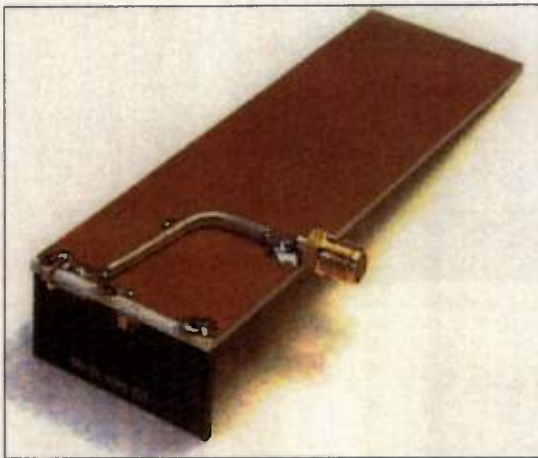
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Example of ground plane design.

and radiation pattern of the embedded antenna is critical. The effects of ground plane size on a manufacturers' cellular band antennas have been formally documented. A typical antenna was mounted on ground planes ranging from 3 to 5.5 inches in half-inch steps. For each ground-plane size, the antenna was tuned to the U.S. cellular frequency

band, and Smith charts and gain patterns were recorded.

The data shows that the antenna favors a 1.5 inch by 4.5 inch ground plane for both VSWR bandwidth and gain performance. Any deviation from this size diminishes the bandwidth and gain performance.

Increasing handset designers' understanding of the effects of ground plane size on the tuning and performance of these new embedded antennas will allow for maximum performance.

Feed points

The final essential design criteria is the ability to feed the embedded antenna. This is where embedded antennas can offer significant advantage as compared to existing external antennas. With the dualband external antenna in use today, designers have to use a minimum of three diplexers. Next generation antennas can offer the designer two alternatives: the single

feed point and the dual feed point.

Single/dual-port T-planar antenna theory

•Single RF Port

Traditional cellular/PCS handset have been designed with a single feed point for their existing antenna networks. A single feed point antenna allows for the rapid integration of a dual-band embedded device into the standard product design, with a minimum number of changes to the RF matching circuitry. In a single feed point antenna, the independent antenna elements are joined to produce a common RF port. This introduces some interaction between the two elements, but it is minimal compared with other design and, more importantly, because of the trace design, it is predictable and stable.

•Dual RF Ports

A significant advantage of T-planar antenna technology is the flexibility it gives handset designers. This flexibility allows the designer to review the additional components that are used in their antenna network designs to accommodate single feed point devices such as whips.

The ability to offer independent RF ports to the antenna for the two band allows the designer to evaluate the use of diplexers and/or band switches and the reduction or elimination of these devices can significantly reduce component count and cost. From an electrical perspective, the dual feed point T-planar antenna design increases overall performance of the device's antenna system by reducing losses in the antenna-matching network. And, with the use of independent feeds, further reduction of the interaction of the two antenna elements can be achieved.

One additional advantage of the dual feed point design, indicated by previous research, is the potential to make the

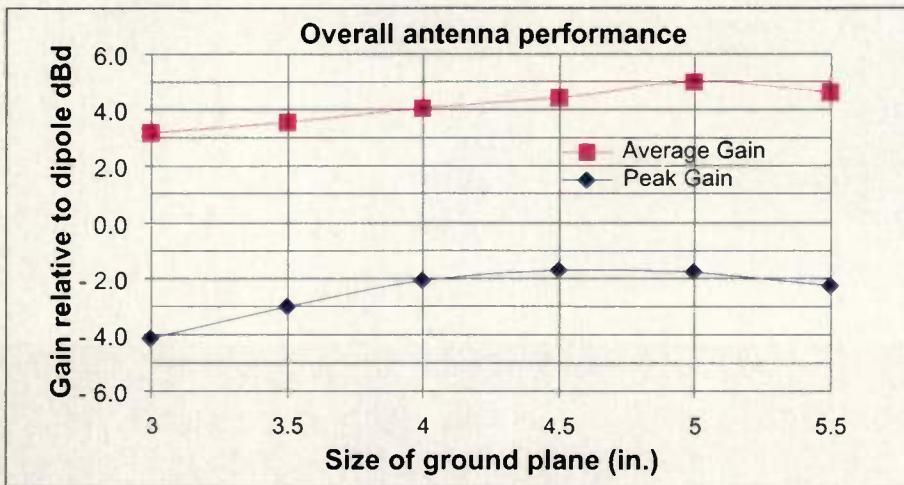
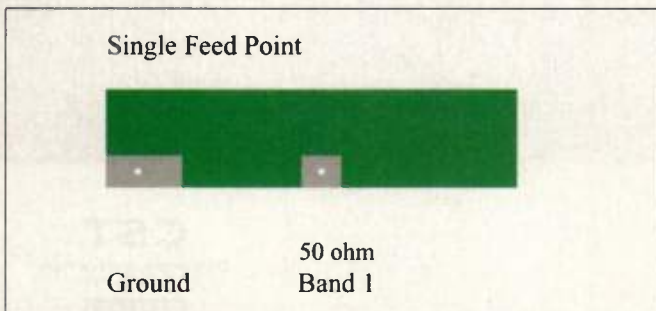
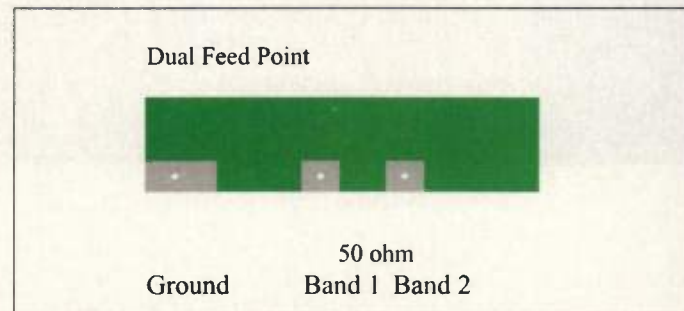


Chart of the overall antenna performance relative to the ground plane.



Single RF (feed) port design.



Dual RF (feed) port design.

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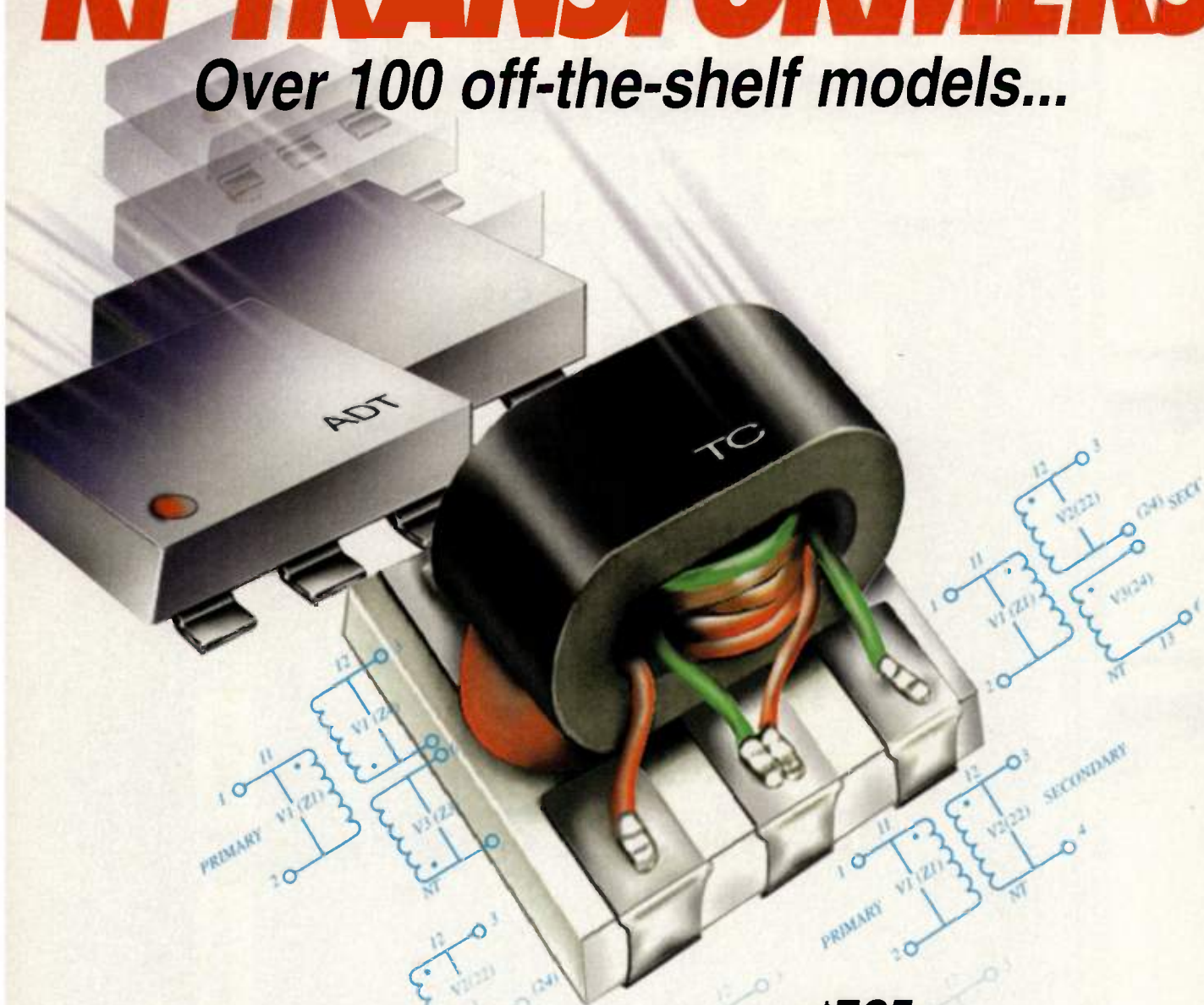
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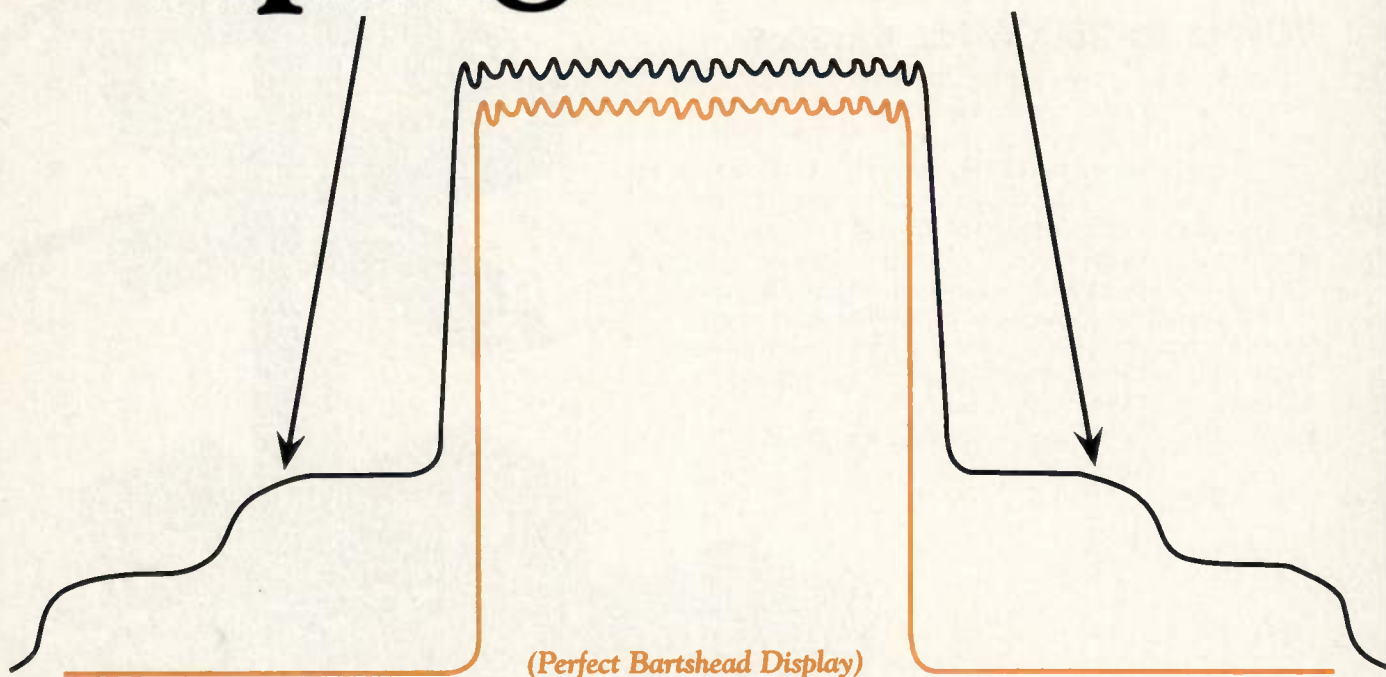
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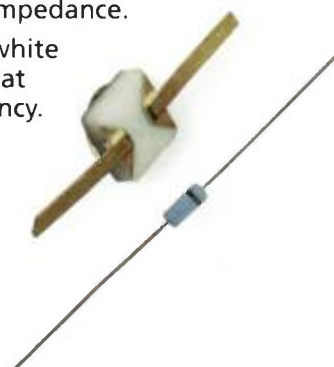
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NC346V	0.1 GHz – 55 GHz	7 – 21 dB

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NC5115	50 GHz – 75 GHz	WR-15
NC5110	75 GHz – 110 GHz	WR-10

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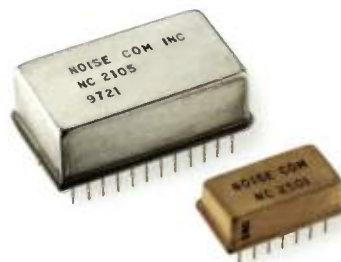
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UFX7108	100 Hz – 500 MHz	+10 dBm
UFX7112	1 MHz – 2 GHz	+0 dBm
UFX7218	2 GHz – 18 GHz	-20 dBm
UFX7911	5 MHz – 1 GHz	+30 dBm



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device smaller as the interaction between the two antenna elements is decreased.

Such an antenna design can operate within a single cellular/PCS band or operate simultaneously in a dual band environment as seen in Europe (900/1800MHz) and the United States (800/1900MHz). The key to operating simultaneously in two frequency bands is the selection of trace designs for two elements that are independent of one another. Current designs allow for either one or two RF feed points for dual band operation, with both solutions at 50 Ω impedance.

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RF

About the author

David McCartney is the Executive Vice President of RangeStar.

His responsibilities span product development, engineering, marketing and sales. A wireless industry veteran with more than two decades of experience, McCartney served most recently as vice president of marketing and sales for Bosch Telecom, where he guided the market introduction of the Bosch World 718, the first wireless phone to permit seamless international roaming. His career also includes tenures with Motorola and Ericsson, where he held management positions in marketing, sales, operations and international business development. McCartney received a BS degree from Iowa State University and a MBA degree from Lynchburg College. He can be reached at RangeStar's Web site—www.rangestar.com or email at info@rangestar.com

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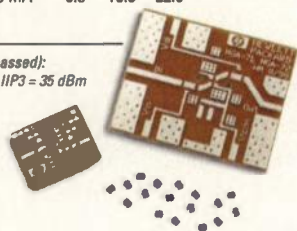
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Typical performance @ 2 GHz

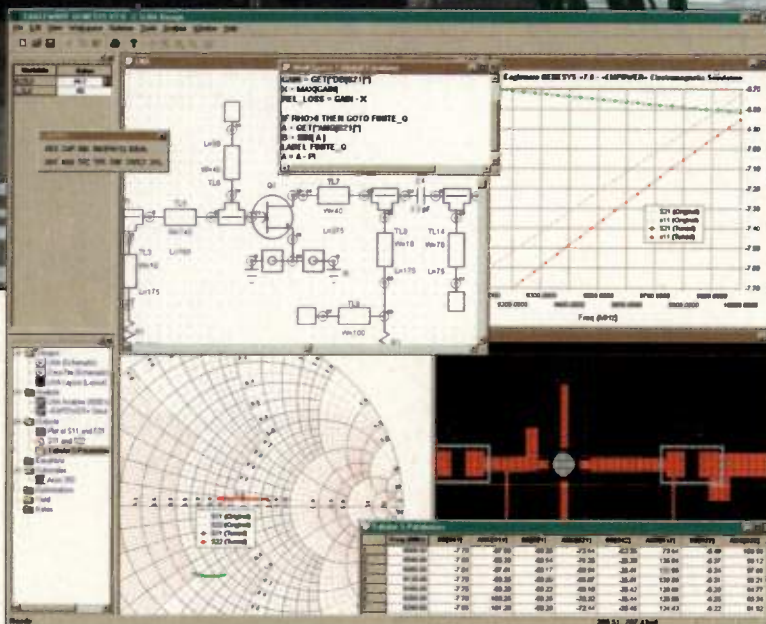
Part Number	Bias	NF (dB)	Gain (dB)	IP3 (dBm)
MGA-72543* (input)	3V, 5-60 mA	1.5	14.4	3.5-14.8
ATF-34143 (output)	4V, 60 mA	0.5	17.5	31.5
ATF-35143 (output)	2V, 15 mA	0.4	18.0	21.0
ATF-38143 (output) coming soon	2V, 10 mA	0.5	16.0	22.0

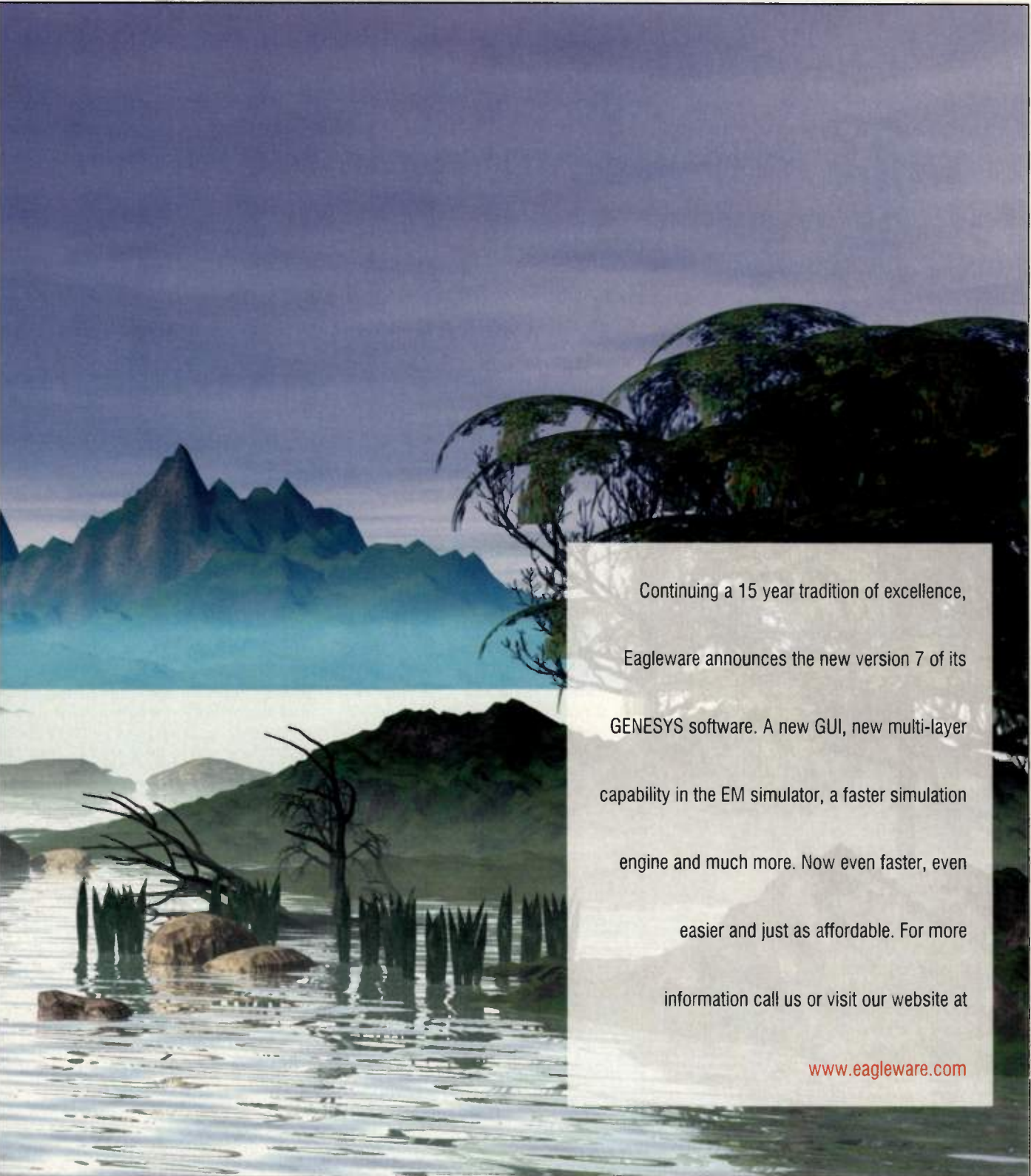
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Fixed wireless communications for the mass market

With an open market for many communications services, the current challenge is to offer a cost-effective package of services to both consumers and small businesses.

By Adel Ghanem, Ph.D.

Fixed wireless could provide the best opportunity for a competitive alternative to wireline communications services but so far has had a minimal impact. The obvious competitive “no-brainer” has become an implementation and success story “no-gainer.”

A closer look at the reasons why suggests the opportunity has not passed us by. We’ve merely been focusing attention on selling solutions destined for mediocre success—and/or failure—from the start.

It’s time to take advantage of the lessons learned from past successes and failures. By concentrating efforts on sound RF principles, innovative technology, efficient design and pro-competitive public policy and regulations, we can provide fixed wireless solutions that offer an economic and competitive alternative to everything the wireline public network has to offer—voice, data, even video

What’s needed

First and foremost, a competitive fixed wireless offering needs to be focused on the mass market as opposed to the current focus on the high-end, large business users. A solution that isn’t de-

signed with the residential and small office home office (SOHO) market in mind at the outset is less likely to be an economic alternative in hindsight.

There is no lack of telecommunications alternatives for high-end business customers. And as these solutions—wireline and wireless—become more and more competitive, they could become economic options for medium-size businesses. But they will likely never become an economic alternative for the residential and SOHO markets. From the capacity, functionality, and ease of installation points of view, they weren’t designed with those customers in mind—a major distinction.

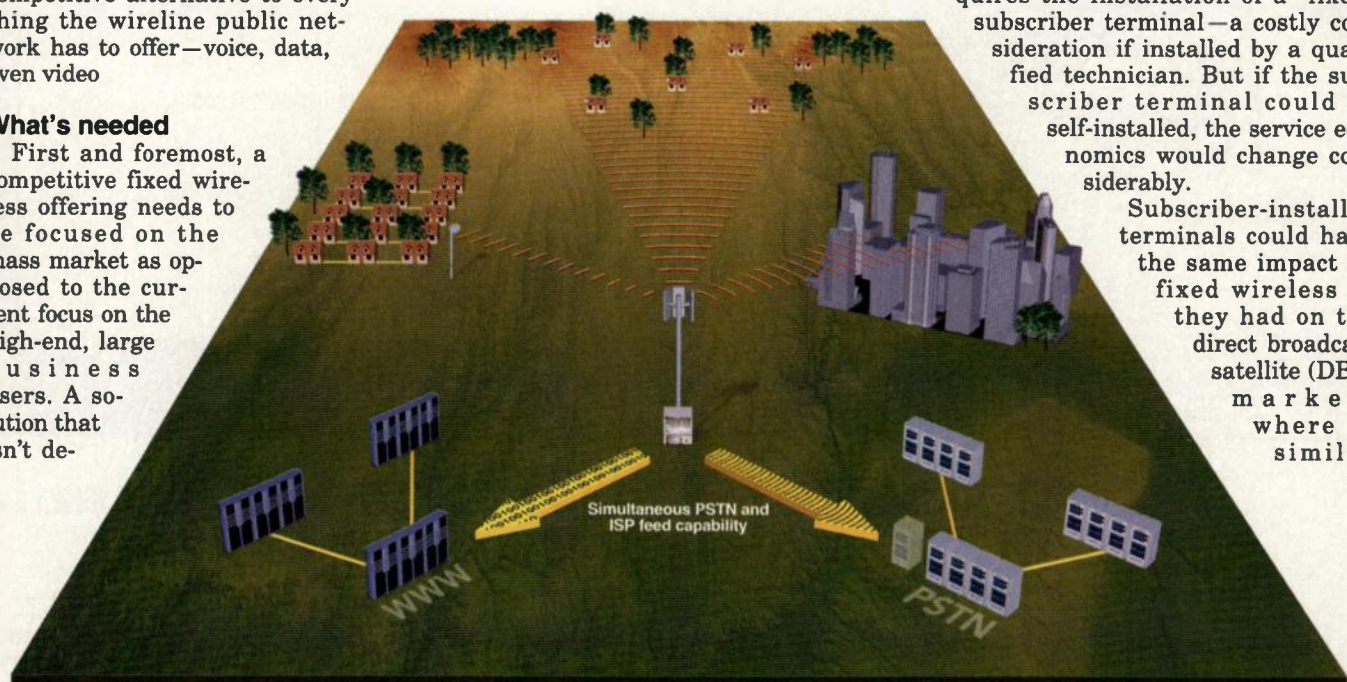
The economics of the mass market are all about cost and price. This isn’t a new or major revelation. Cellular and personal communications system (PCS) carriers have proven that we sell a lot more wireless service with free or \$49 phones than with \$249 or \$1,499 phones.

But it’s a well known fact that cellular networks and service weren’t, initially, designed for the mass market. Actually, cellular was once viewed as having very limited market potential. It is a good example of a technology application which found/developed a sizeable market and continues to reinvent itself to become more acceptable and affordable to a wider audience.

Fixed wireless solutions, designed for the mass market, need special attention paid to technologies and specifications that allow cost effective networks to be built. PCS carriers helped drive efforts to incorporate cost-saving technologies into their networks because without a lower operating cost—and corresponding lower overall service costs—there was little hope of attracting customers away from cellular.

Fixed wireless networks present similar challenges and bigger opportunities. By definition, fixed wireless requires the installation of a “fixed” subscriber terminal—a costly consideration if installed by a qualified technician. But if the subscriber terminal could be self-installed, the service economics would change considerably.

Subscriber-installed terminals could have the same impact on fixed wireless as they had on the direct broadcast satellite (DBS) market where similar



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ERA-2SM	DC-6000	15.2	12.4	4.6	26.0	40	2.00
ERA-3	DC-3000	20.8	12.1	3.8	23.0	35	2.10
ERA-3SM	DC-3000	20.2	11.5	3.8	23.0	35	2.15
ERA-4	DC-4000	13.5	▲17.0	5.5	▲32.5	65	4.15
ERA-4SM	DC-4000	13.5	▲16.8	5.2	▲33.0	65	4.20
ERA-5	DC-4000	18.8	▲18.4	4.5	▲33.0	65	4.15
ERA-5SM	DC-4000	18.5	▲18.4	4.3	▲32.5	65	4.20
ERA-6	DC-4000	11.3	▲18.5	8.4	▲36.5	70	4.15
ERA-6SM	DC-4000	11.3	▲17.9	8.4	▲36.0	70	4.20

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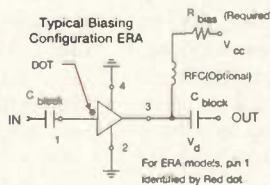
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problem existed. Initially, special technicians were required for all satellite installations, which delayed the overall service penetration. The solution to this dilemma was a self-installation kit and a bit of innovative technology.

Today, the self-directing installation kit guides the subscriber through the process. A signal at the set-top receiver tells them when the satellite dish is positioned properly for the strongest signal strength. By removing a major implementation cost and hurdle, the service is applicable and appealing to a wider audience, while improving the overall economics of the business plan.

All of the above-described factors play a role today in fixed wireless implementations. And they further suggest what else needs to change. Meeting these conditions for economic, competitive, self-installed fixed wireless equipment and services suggests efforts should be concentrated on finding solutions that operate in lower, rather than higher, frequency bands—counter to all existing efforts to date.

Wireless systems operating in lower frequency bands reduce the point-to-point or line-of-sight requirements, making self-installation possible and eliminating a major cost and implementation hurdle. And that factor alone will have a major impact on the economics of fixed wireless infrastructure and implementations.

Furthermore, the availability of spectrum in the lower or sub-2.5 GHz frequency bands suggests other RF technologies, such as time-division duplexing (TDD), must be considered for fixed wireless applications. Lower frequencies allow for a less complex RF solution and TDD implementations worldwide have proven efficient, cost-effective and viable for mass-market applications.

Fixed wireless systems based on TDD technology and operating in sub-2.5 GHz offer the best opportunity for a cost-effective, competitive alternative to wireline telecommunications services. And competitive service providers—wireless or wireline—should concentrate efforts on seeing these solutions are given a fair opportunity to be brought to market.

The search for higher ground: an historical perspective

Prior to the Telecommunications Act

of 1996 there wasn't much emphasis on mass-market competitive local exchange services. And given the state-of-the-art in wireless technology, lower frequencies weren't a fixed wireless service option. It is difficult to say—from a chicken-and-egg perspective—which came first or mattered most, but both prevented serious consideration and development of cost-effective fixed wireless solutions.

The lack of competitive incentive prior to 1996 is perhaps easiest to explain. Although fixed wireless offers no-brainer status as a competitive local exchange alternative, there wasn't a carrier group particularly interested in pursuing the residential opportunity—wireless or wireline.

From 1992 on, most of the wireless attention was centered on PCS spectrum auctions and bringing competitive alternatives to the "cellular" duopoly. Mobility was key in every wireless business plan and although fixed wireless was not prohibited in any way, it did not reflect the interests of auction participants or the best perceived market opportunity for the available spectrum.

Likewise, in the same time frame on the wireline side, competitive local exchange carriers (CLECs) were still known as competitive access providers (CAPs). All their efforts were concentrated on constructing fiber optic rings and providing lower cost and reliable wireline telecommunications service alternatives for lucrative business customers. Residential and SOHO subscribers were not on the radar screen.

Cable TV companies expressed interest and "dabbled" in telecommunications trials but the complexities of providing high-reliability telephone services ran counter to their existing operations. So despite their interest in expanding the service offerings to their residential customer base, their existing cable plant prevented execution of the strategy.

With the only available lower frequency spectrum being "reserved" for mobility applications and a general lack of interest in competitive residential local exchange services, fixed wireless applications garnered very little service interest.

The impact of available wireless technologies factored into the fixed wireless development equation as well. At the time, most wireless equipment manufacturers developed solutions

based on state-of-the-art frequency division duplexing (FDD) access schemes to support the needed high-speed mobility.

In contrast to TDD, FDD divides a transmission into transmit (upband) and receive (downband) frequencies separated by a guard band of a specific size. The use of FDD for wireless applications was widely accepted and in many respects the defacto standard. In fact, the PCS spectrum allocations were established with FDD duplexing in mind.

The selection of FDD by equipment manufacturers for mobility applications led to the same choice for fixed wireless. Despite the lack of interest within the U.S., fixed wireless became a preferred solution for basic telecommunications in many competitive offering worldwide, especially in underdeveloped regions. To compete for these worldwide contracts, vendors needed to include fixed wireless systems in the product line. For obvious reasons of convenience and economies of scale, equipment manufacturers developed fixed wireless solutions, from their stable of available mobility solutions that were already based on FDD technology.

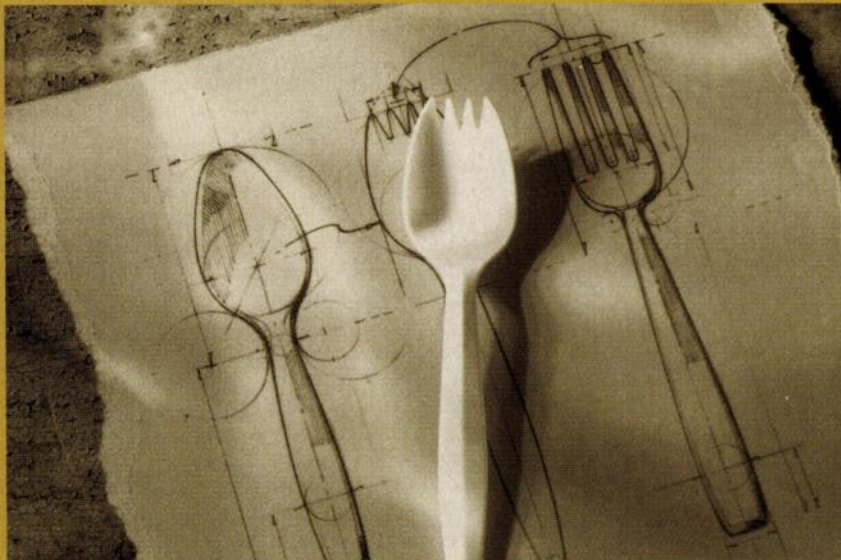
In turn, the use of FDD in product offerings pushed fixed wireless applications into higher and higher frequency bands where paired-bands could still be allocated. The lack of large blocks of spectrum—required for FDD—in the U.S. and most of the world prevented consideration of lower frequency applications.

This fluke of logic, convenience and/or progression of events, is why fixed wireless solutions have encountered only mediocre success from the start. Fixed wireless developed into higher frequency wireless mobility "adaptation" instead of a lower frequency "designed for the masses" efficient, economic alternative to wireline hold on residential access.

Low frequency advantages

It's not that it isn't possible to construct an efficient, cost-effective fixed wireless system at higher frequencies. But given the alternative of lower versus higher frequency solutions who wouldn't choose sub-2.5 GHz?

Wireless technology gets better and more stable every day but some basic facts and laws of physics will never change. A rainstorm still wipes out



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wireless transmission at 24 GHz and even a simple rainy day can block signals at 3 GHz.

Even foliage and building obstructions have a greater impact at higher frequencies. For example, a 3.6 GHz fixed wireless installation in Poland worked perfectly following its fall installation but ground to a halt in spring. The strange phenomenon design engineers failed to account for was the annual reappearance of tree leaves.

At lower frequencies, Mother Nature would not have had an impact. And while design options include raising antennas to "see" over the trees, trees will continue to grow and the problem will likely reoccur.

Urban fixed wireless deployments can be even more disconcerting. Building heights and other obstructions force the use of sophisticated modeling tools and experienced technicians for mapping and installation on a sight-by-sight basis. Certainly not an economic, low-cost alternative.

In-building penetration could also benefit from lower frequency transmission and impact fixed wireless applications. Who hasn't noticed the difference between in-building penetration of cellular and PCS frequencies in the U.S.? Because of its sub 1.0 GHz frequency, cellular exhibits greater in-building penetration when compared to PCS at 1.9 GHz. Even in the middle of a building you will likely receive a cellular call, whereas PCS transmission in the lobby of many high-rise buildings gets dicey. Now consider the implications of these same frequencies on fixed wireless where you don't have the option of "walking" the antenna for better reception.

In fact, all wireless applications at high frequencies require line-of-sight transmission for optimal performance. This restriction alone can kill the economics of an urban or even suburban fixed wireless application.

In contrast, lower frequencies don't require line-of-sight, nor is it necessary to pinpoint antennas with laser-beam precision. Signals are more tolerant and can bend around and penetrate a wider range of structures. And imagine the impact on a fixed wireless business case if the subscriber terminal could be self-installed or placed within the home or business.

The business case drives all wireless

ventures and the "numbers" have to work. Low frequency fixed wireless has a business case advantage in the overall cost of system equipment. For the same output power, the cell size is larger at lower frequencies, requiring fewer base stations and reducing infrastructure costs.

For example, a fixed wireless application in a sub-2.5 GHz frequency provides a cell size range of 15-25 km. With that coverage, many urban and suburban applications could be handled with a single cell and base station.

In contrast, at higher frequencies the laws of physics shrink the cell radius and coverage for the same system output power. It forces operating in a micro rather than macro cellular environment with corresponding effects on design, equipment costs and ease of installation. Not to mention that high-frequency transceivers are just more complex and require greater attention to detail.

In totality, the combination of all these factors suggest lower frequencies are the economic choice for fixed wireless applications if providers are serious about providing a "competitive" alternative to wireline.

Enter TDD

Yet, that assertion contains a Catch-22 of sorts. With the last sub-2.5 GHz spectrum going to PCS mobility applications there hasn't been sufficient lower frequency spectrum available.

Taken at face value, the assertion is true. There isn't sufficient lower frequency spectrum to accommodate fixed wireless or even other mobility applications—if FDD is the duplexing assumption.

That frequency quandary forced manufacturers, carriers, governments and regulators worldwide to search, select and set-aside spectrum blocks at higher frequencies for fixed wireless applications. But the logic behind the search for a frequency "home" that meets the needs and requirements of a particular wireless "technology" is counterintuitive. FDD isn't required or necessary for many fixed wireless applications.

Selecting wireless technologies and frequencies that maximize the economics and business case of a mass-market application should have been the thrust. And under those assumptions, time division duplexing in sub-2.5 GHz frequency bands is the log-

ical choice.

For starters, TDD spectrum could be squeezed into any available contiguous spectrum. Because the transmission is time-slot, rather than frequency-based, it requires a single contiguous chunk of spectrum for transmitting and receiving. Its "Ping Pong" transmission approach is very effective for fixed applications and slow-speed mobility.

TDD transceivers are also significantly less complex and more cost effective than FDD transceivers on both the subscriber and base station side. For the base station, TDD eliminates the need for expensive duplexers. With subscriber equipment, the transceiver is much simpler and more cost effective to implement.

One reason is TDD's channel reciprocity. Because it uses the same channel for transmitting and receiving channel characteristics seen at the base station could be considered as identical to those of the subscriber unit. This channel reciprocity simplifies the TDD equipment design considerably.

There have been past concerns about TDD and its susceptibility to echo and difficulty with synchronization. But the industry and technology has evolved to ensure these concerns are no longer valid. Proper system design and technology innovations have significantly reduced the potential of echo in even the longest TDD links. Further, with global positioning satellite (GPS) technology, all cells can be synchronized to the same clock, guaranteeing the synchronization between the transmit and receive time slots in all adjacent cells thereby eliminating possible inter-cell interference.

The only remaining concern surrounding TDD technology is that it hasn't received sufficient market attention as a competitive fixed wireless alternative. It's not that there aren't successful TDD implementations worldwide. In fact, TDD success stories include wireless PBX technologies (like personal handiphone systems {PHS} in Japan, digital european cordless telephone {DECT} in Europe) and a number of fixed wireless advanced code-division multiple access (A-CDMA)¹ implementations around the world. By design, PHS and DECT take a micro-cellular approach while A-CDMA offers the wide-area and high capacity coverage of a macro-cellular design.



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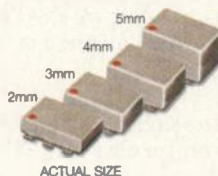
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ADE-1ASK	3	2-600	+7	5.3	50**	16	3.95
ADE-2ASK	3	1-1000	+7	5.4	45**	12	4.25
ADE-6	5	0.05-250	+7	4.6	40	10	4.95
ADE-12	2	50-1000	+7	7.0	35	17	2.95
ADE-4	3	200-1000	+7	6.8	53**	15	4.25
ADE-14	2	800-1000	+7	7.4	32	17	3.25
ADE-901	3	800-1000	+7	5.9	32	13	2.95
ADE-5	3	5-1500	+7	6.8	40**	15	3.45
ADE-13	2	50-1600	+7	8.1	40**	11	3.10
ADE-20	3	1500-2000	+7	5.4	31	14	4.95
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The encouraging fact is that TDD can offer an efficient, cost-effective infrastructure alternative for competitive fixed wireless applications targeted at a mass market—if lower frequencies can be made available.

What needs to happen

The challenge of finding lower-frequency available spectrum isn't as large an "if" as it might first appear. But there are a number of factors needing sufficient attention to bring lower frequency fixed wireless TDD applications to market.

First and foremost we need to generate more serious attention to providing a competitive alternative to incumbent local exchange carrier (ILEC) telecommunications services. And that attention should be concentrated on encouraging fixed wireless applications.

Regional bell operating companies (RBOCs) are slowly being allowed into the long distance market because local exchange competition "exists." But that competition is hardly ubiquitous and there are really no serious alternatives available for the mass-market residential customer aside from using the RBOCs own outside plant facilities.

AT&T has switched local exchange access strategies a number of times from the wireless "Project Angel" to a \$100 billion gamble on cable TV infrastructure. Apparently it is "serious" about local exchange alternatives, but hasn't yet hit on a killer, cost-effective strategy (perhaps we should take another look at recently announced fixed wireless products using newly developed CDMA/TDD technologies).

Making lower frequency fixed wireless TDD applications a possibility requires cooperation from the FCC and other regulatory bodies to ensure rules and regulations support rather than hinder the opportunity for a mass-market success story. That could include removing requirements that suggest, dictate or favor specific technologies, such as FDD. Taking a bold step and encouraging or specifying the use of TDD for specific spectrum allocations is another option.

Existing unintentional restrictions include mobile antenna output power requirements. Because mobile applications use omnidirectional antennas, output power is restricted to reduce radiation patterns and possible interfer-

ence among the mobile units. But the same requirements aren't necessary for fixed wireless applications.

With fixed wireless using directional antennas, transmit power can remain high without creating the same interference problems. The results are increased link budgets, resulting in wider and better coverage for the same or reduced cost — a plus for cost-effective, mass-market implementations.

Eliminating the restriction could open up D, E and F allocations in the PCS bands for fixed wireless consideration. Many of these PCS auction winners have yet to deploy because the spectrum allocations are limited in size to support high capacity mobile networks. Rather than sit on valuable spectrum or introduce yet another risky mobile application, perhaps TDD-based fixed wireless deserves a second look.

Additional lower frequency spectrum is now available with more to come in the future. Examples include the upcoming 700 MHz auction of vacated television channel frequencies and spectrum in the 400 MHz range now used by analog services being phased out.

Recent moves by the FCC regarding the 700 MHz frequencies suggest more of an FDD slant. But while it is possible to construct a paired band out of the available 30 MHz to allow for FDD applications, using the band for TDD implementations eliminates the need for significant guard bands and hence increases the available spectrum for wireless communications services.

Lastly, a concerted effort by equipment manufacturers to explore and expand TDD options is warranted. Carriers have been "pushed" into higher frequency applications because FDD solutions are what wireless equipment manufacturers have had to offer.

The future

Wireless equipment vendors need to focus energies on turning out TDD applications that ensure the competitive success of a mass-market fixed wireless alternative to wireline. That translates to modular equipment configurations that offer a "pay as you grow" philosophy for prospective carriers without the deep pockets of an AT&T or MCI WorldComm.

Carriers can not depend on a "build it and they will come" wireless equip-

ment mentality. As sure a bet as alternative residential and SOHO local exchange service may appear — considering the unmet demand for inexpensive, high-bandwidth Internet connections — carriers still need scalable solutions, providing cost-effective implementations and realistic returns for 100 or 100,000 subscribers.

These equipment, regulatory and competitive environment goals are attainable and the alternative of TDD-based fixed wireless access solutions is realistic. But the cycle of technology dictating wireless solutions needs to end.

Communications services for the mass-market require solutions designed to incorporate every frequency, wireless technology and implementation advantage possible. Lower frequency TDD fixed wireless applications are the real competitive opportunity. Adapting what's convenient and available should not be an option.

RF

About the author

Adel Ghanem, Ph.D., has served as Adicom's President and Chief Executive Officer since December 1995. Prior to co-founding Adicom, Dr. Ghanem was vice president of technology development at TCSI corporation and the director of access systems with Southwestern Bell. Dr. Ghanem has also worked at Pacific Bell, and L. M. Ericsson. Dr. Ghanem received a Ph.D. in Electrical and Computer Engineering from SUNY. Adicom is located at 26142 Eden Landing Road, A-1, Hayward, California, 94545. Tel. 510.781.5520. www.adicomwireless.com.

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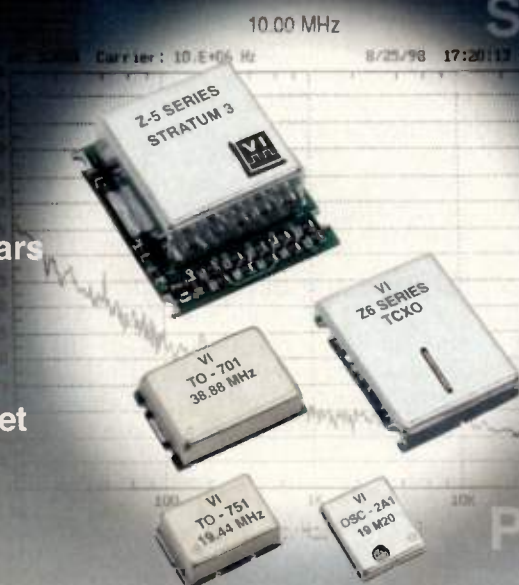
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3.7 Watt Ka-band power module for local multi-point distribution systems applications

Crowding of lower frequencies promise to open a host of Ka-band multipoint distribution applications and products.

By Carlton T. Creamer,
James J. Komiak,
Wendell Kong, P.C. Chao,
Kirby Nichols,
Christopher O'Neil,
Scott MacKelvey,
Paul D. Cooper
and Dana Wheeler

As demand for broadband data distribution increases and as lower frequency bands become saturated, communications providers are increasingly focusing on Ka-band for next generation terrestrial systems. A number of terrestrial wireless systems currently exist including local, multi-point distribution systems (LMDS) at frequencies of 27 to 30 GHz, and digital radio at 28 and 38 GHz. Considerable growth in these areas is projected. Designers of these systems require low cost solid state power amplifiers (SSPAs) as the output stages for radio transmitters. The moderate power requirements range from 1 to 5 W.

This article describes the design, fabrication and test of a 3.7 W, Ka-band high power module. These results were achieved using gallium arsenide pseudomorphic high-electron mobility transistors (GaAs pHEMT), monolithic microwave integrated circuit based (MMIC) power amplifiers designed and fabricated using 0.15 μm fully selective gate recess technology.

Approach

The LMDS module design exploits recent advances in Ka-band power MMIC amplifier design and fabrication. The newly developed chips include the power Amplifier MMIC and the driver Amplifier MMIC. [1].

The output periphery is 6.4 mm with a 3.2:1 2nd to 1st stage ratio (2 mm 1st stage).

The measured 3 dB compressed out-

put power is > 34 dBm (> 33 dBm at 1 dB compression) with a dB associated power gain and a 25% power added efficiency at 30 GHz. From 28 to 33 GHz, the 3 dB compressed output power is > 32 dBm. The driver MMIC is a similar two-stage Class AB design with a 3.33:1 aspect ratio (600 μm driving 2 mm). Saturated 3 dB gain compression chip power averaged 28.0 dBm and 13 dB associated power gain at 30 GHz. From 28 to 33 GHz, the 3 dB compressed output power is > 25 dBm. The drain bias for the chip set is +4.5 volts (See figures 1 and 2.)

The third MMIC amplifier used as a simple gain block is a commercially available 26 to 40 GHz balanced LNA design (not shown).

LMDS module design

Figure 3 presents the module block diagram. The projected performance is summarized in the table below the figure. The

major elements of the power module design are the MMIC amplifiers, a two way signal combiner and a package

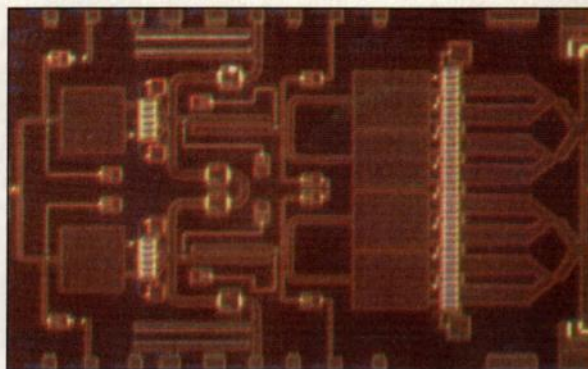


Figure 1. Two-stage output amplifier.

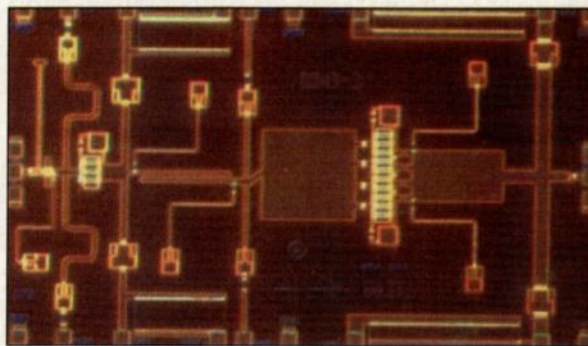


Figure 2. Two-stage driver amplifier.

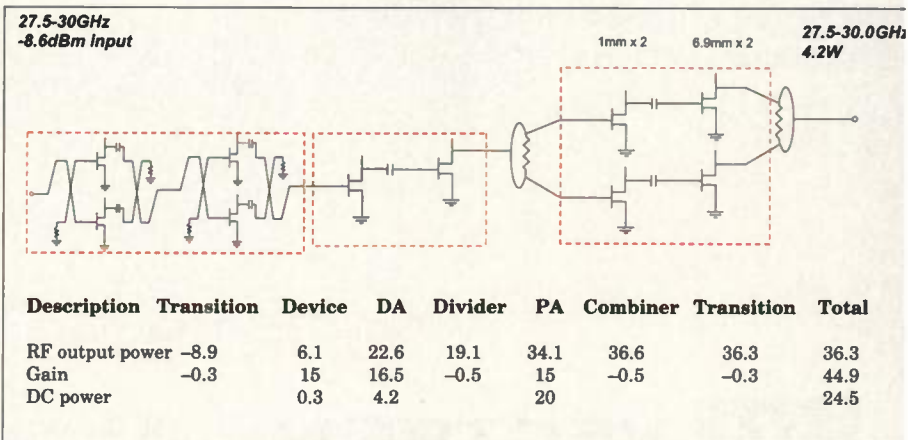
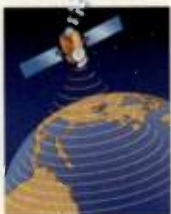


Figure 3. Block diagram of the Ka-band power amplifier and value table.

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		Midband (dB)	Flat (±dB)		NF(dB)	IP3(dBm)		
ZJL-5G	20-5000	9.0	±0.55	15.0	8.5	32.0	80	129.95
ZJL-7G	20-7000	10.0	±1.0	8.0	5.0	24.0	50	99.95
ZJL-4G	20-4000	12.4	±0.25	13.5	5.5	30.5	75	129.95
ZJL-6G	20-6000	13.0	±1.6	9.0	4.5	24.0	50	114.95
ZJL-4HG	20-4000	17.0	±1.5	15.0	4.5	30.5	75	129.95
ZJL-3G	20-3000	19.0	±2.2	8.0	3.8	22.0	45	114.95
ZKL-2R7	10-2700	24.0	±0.7	13.0	5.0	30.0	120	149.95
ZKL-2R5	10-2500	30.0	±1.5	15.0	5.0	31.0	120	149.95
ZKL-2	10-2000	33.5	±1.0	15.0	4.0	31.0	120	149.95
ZKL-1R5	10-1500	40.0	±1.2	15.0	3.0	31.0	115	149.95

NOTES:

1. Typical at 1dB compression.
2. ZKL dynamic range specified at 1GHz.
3. All units at 12V DC.



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isolate the electronics from the operating environment and complete the thermal path. Solid state Ka-band amplifiers, that incorporate combining schemes, require low loss solutions in order to achieve the highest power levels while preserving DC to RF efficiency. A simple single section Wilkinson

combiner realized as an MIC circuit fabricated on .010" Al_2O_3 , was selected for this application. It provides efficient signal combining with adequate bandwidth. The design was initially analyzed using Libra and completed by performing a 2-dimensional EM simulation of the layout. The predicted

insertion loss is < 0.5 dB.

Package design

A properly designed millimeter wave power amplifier package includes a light weight, hermetic mode free enclosure, a low loss transition from the microstrip environment inside the package to the user interface (in this case, coax), and DC bias and distribution circuitry. Materials are carefully selected to maintain low thermal impedance, and CTEs that match closely to the hybrid and MMIC components. We chose a light weight aluminum package and copper moly carriers, that screw into the housing floor, to provide low thermal impedance. The transition is a simple air-line design that mates to a glass to metal seal and V-connector. Low and high pass DC filtering circuits are incorporated as part of the power distribution. Resistive dividers are used to reduce gate bias supply to quiescent levels. Smaller resistance values are favored at the cost of slightly higher power consumption from the minus supply. This is done to minimize gate voltage variations under RF drive and helps to preserve overall module efficiency.

Integration and test results

Two modules were assembled and

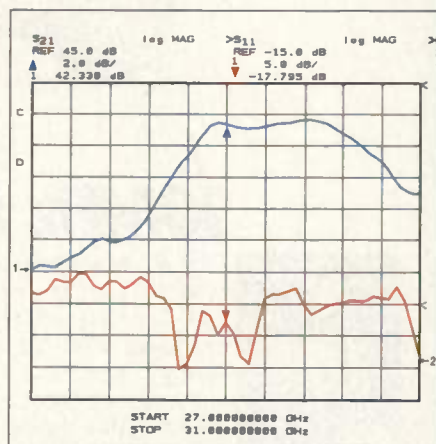


Figure 4. Small signal gain and input.

tested. The results were very similar and only the results of the first module are reported here. The module operates from a +5.0 volt drain supply and a 1.0 V gate supply. It consumes 24.5 W of power at quiescent bias.

The measurements included gain, input return loss, output power, power added efficiency (PAE) and

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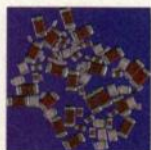
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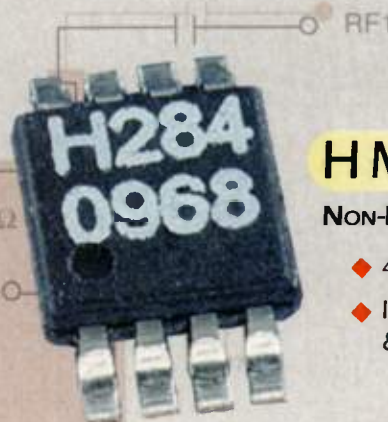
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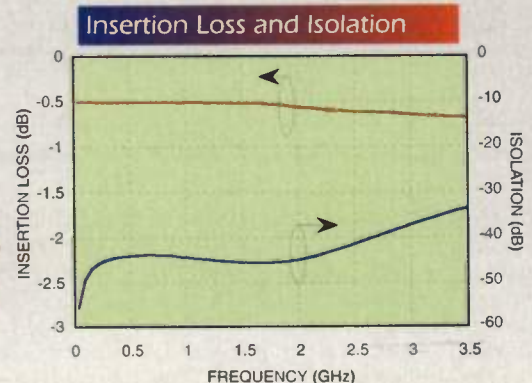
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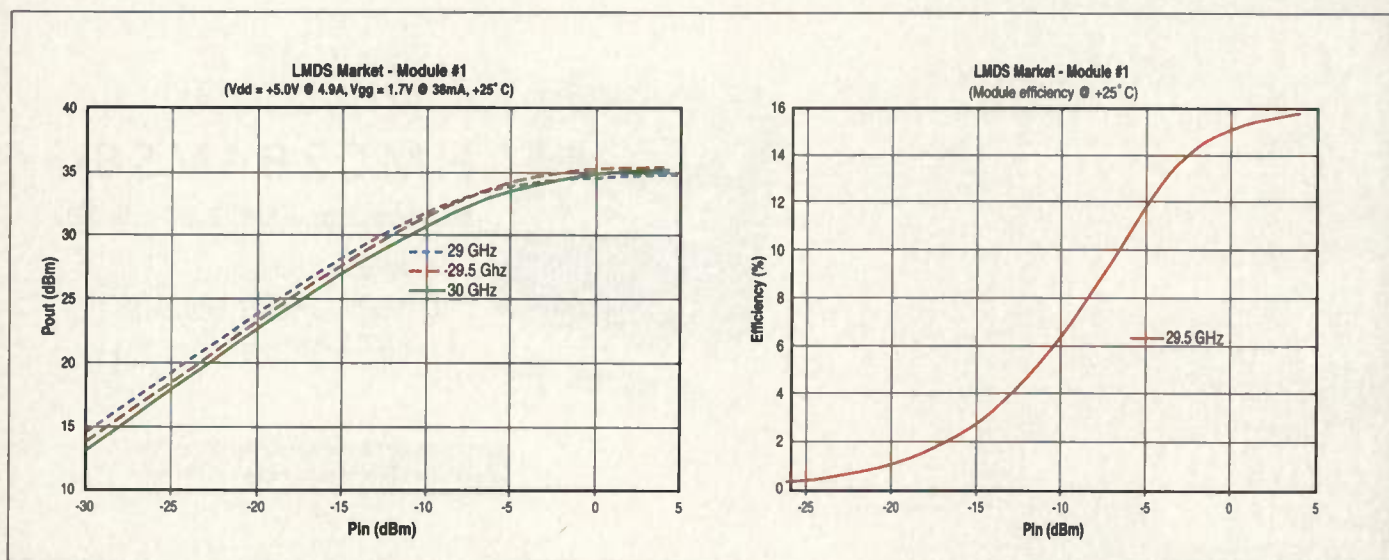


Figure 5. Output power and P.A.E. vs. Input power of the LMDS module.

intercept point. Overall performance was excellent.

Small signal gain averaged 42.5 dB and was centered at 29.5 GHz. The 1.0 dB bandwidth is 1.7 GHz. This was achieved with minimal tuning and is close to the projected performance. The input match was better than 1.62:1 across the full 1B bandwidth. The results are shown in Figure 4.

Measured saturated output power was 3.72 W (35.7 dBm) at 29.5 GHz. 1.0 dB gain compression power was 32.8 dBm (1.9 W). The power added efficiency was 15.8% at saturation. Transfer curves are shown in Figure 5.

The results matched the projected results within 0.6 dB (note that the

MMIC data used for purposes of the performance projection is from pulsed on-wafer measurement at 25% duty cycle). This is primarily due to higher channel temperatures as a result of packaging and CW operation. Even small thermal resistances of the attachment and mounting surface materials result in substantial temperature increases when handling large power dissipations.

Intercept point

Two tone measurements of the module were made at four power levels ranging from 100 mW to 1.0 W output power at 29.5 GHz. Upper and lower third order intercept point (TOI) values

are shown in Figure 6. Average magnitude of the upper and lower TOI is 38.6 dBm at an output power of 1.0 W.

Conclusion and recommendations

A high gain, multi-watt Ka-band power amplifier module for LMDS applications has been successfully demonstrated using high power commercially available power chips fabricated in the Sanders foundry. Producing the lowest cost final product will require implementation of alternative packaging technologies that are in development.

RF

References:

- [1] J. J. Komiak, W. Kong, P.C. Chao, K. Nichols, "3 Watt Ka-Band MMIC HPA and Driver Amplifier Implemented in a Fully Selective 0.15 um Power PHEMT Process," 1998 IEEE GaAs IC Symposium.

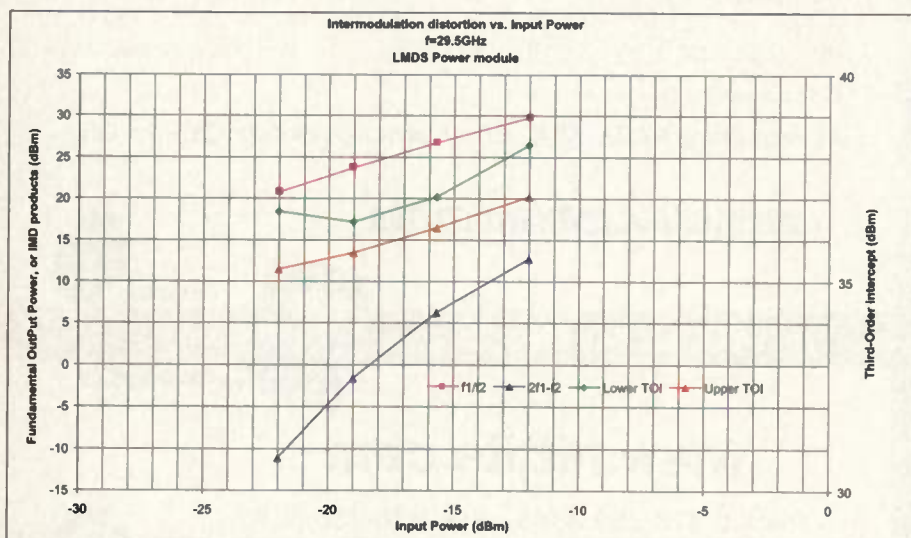
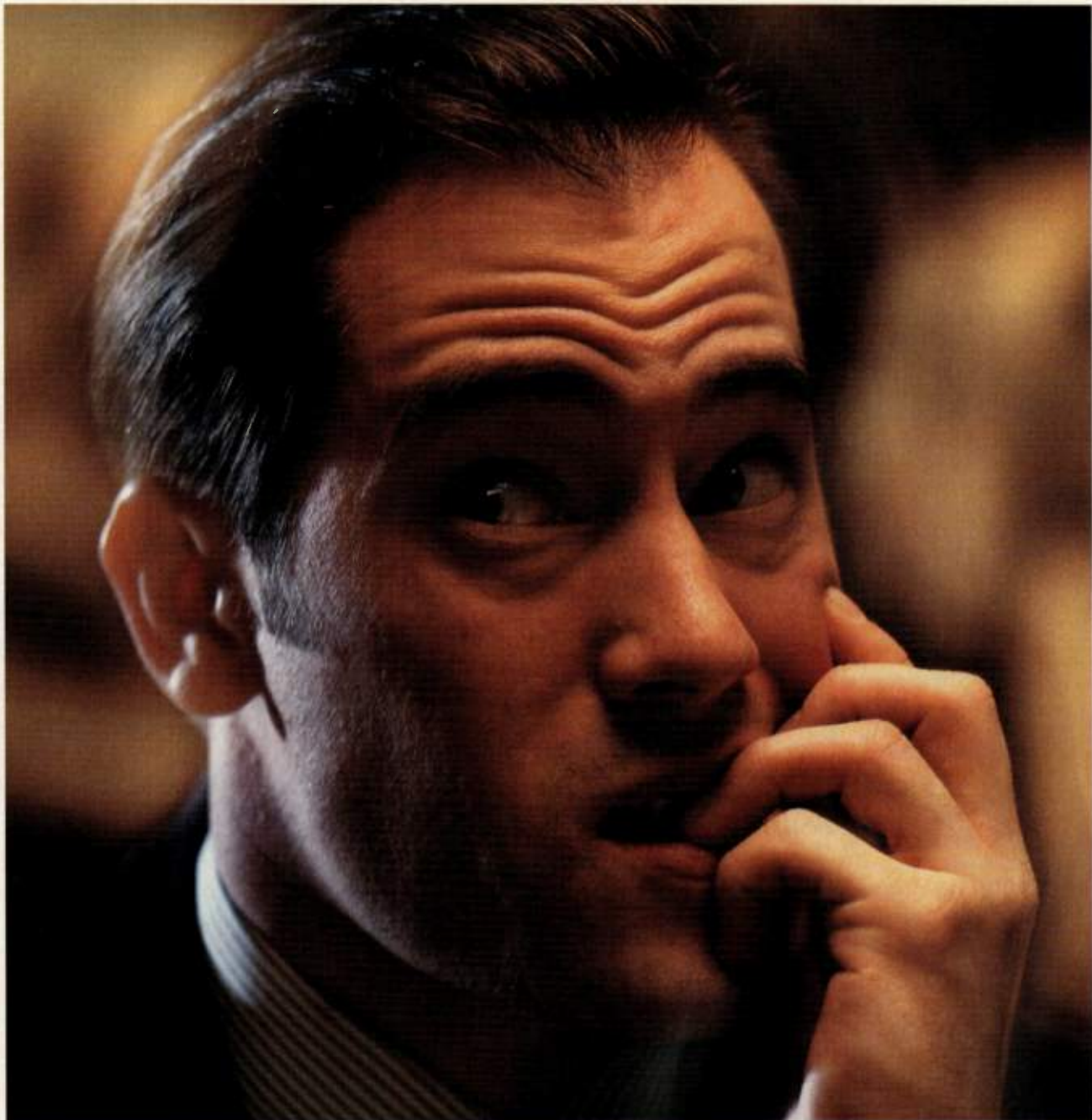


Figure 6. Photo of LMDS Ka-band amplifier.

About the authors

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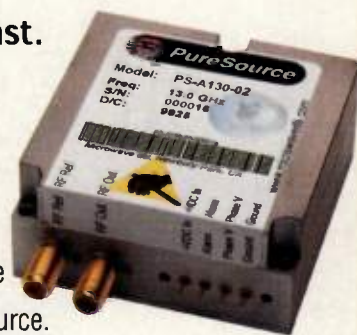
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Time and Frequency

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High performance oven controlled crystal oscillators

Raltron Electronics' OX-2000 series of OCXO are available in frequencies from 1 MHz to 160 MHz and are package in the popular 14-pin DIP configuration. The line features stability of ± 0.1 ppm from 0°C to 50°C and meets ANSI Stratum-3 requirements, including ± 4.6 ppm total stability over its lifetime and ± 0.37 ppm over a holdover period that includes variations in temperature, supply voltage, load variations and 24 hour aging. The 14-pin DIP packages measure less than 10 mm in height for OCXOs to 60 MHz and 12.7 mm in height for OCXOs above 60 MHz to frequency limits, which include SONET and ATM applications. The device design uses contemporary semiconductor-heating for the unit's crystal and oscillator components to insure the product reaches thermal stability and specifications within 1.5 minutes. The units consume less than 2.5 W during warmup and less than 1 W, steady state at 25°C .

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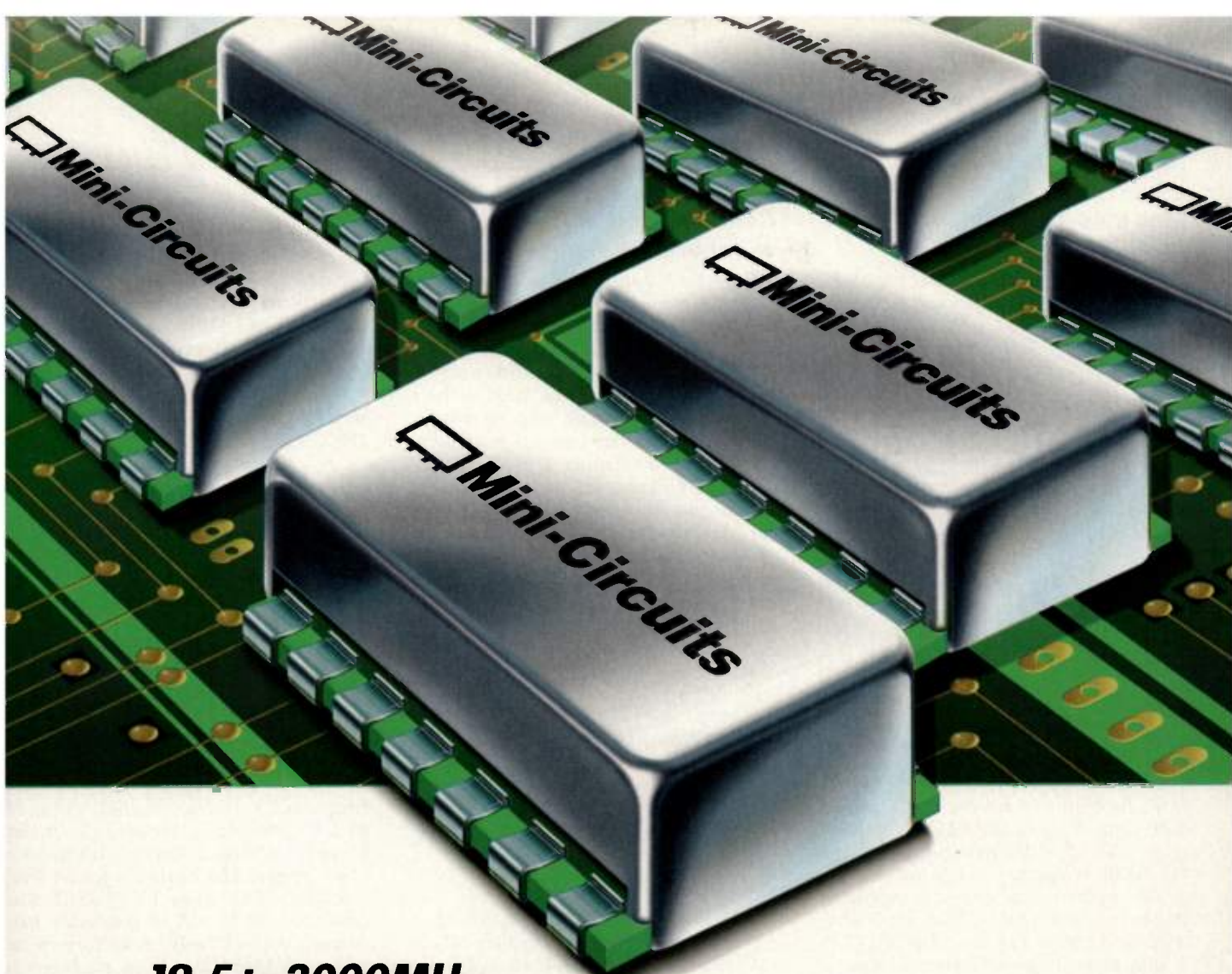


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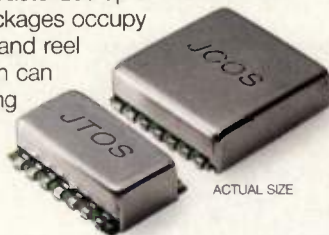
features 1.1:1 linearity over frequency and temperature and can be utilized in designs that can take error voltage directly from the IC's charge pump circuitry. The oscillator provides a -5 dBm of output into a 50 W load and is designed to operate over the commercial range of -30°C to $+85^{\circ}\text{C}$. The device also pulls less than 2 MHz with a 14 dB return loss, any phase and uses less than 2 MHz/V within a 5% change in supply voltage.

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12.5 to 3000MHz SURFACE MOUNT VCO's from \$13⁹⁵

Time after time, you'll find Mini-Circuits surface mount voltage controlled oscillators the tough, reliable, high performance solution for your wireless designs. JTOS broadband models span 12.5 to 3000MHz with linear tuning characteristics, low -120dBc/Hz phase noise (typ. at 100kHz offset), and excellent -25dBc (typ) harmonic suppression. JCOS low noise models typically exhibit -132dBc/Hz phase noise at 100kHz offset, and phase noise for all models is characterized up to 1MHz offset. Miniature J leaded surface mount packages occupy minimum board space, while tape and reel availability for high speed production can rocket your design from manufacturing to market with lightning speed. Soar to new heights...specify Mini-Circuits surface mount VCO's.



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JTOS/JCOS SPECIFICATIONS

Model	Freq. Range (MHz)	Phase Noise (dBc/Hz) SSB @ 10kHz Typ.	Harmonics (dBc) Typ.	V _{DC} 1V to:	Current (mA) @ +12V DC Max.	Price Sea. (5-49)*
JTOS-25	12.5-25	-115	-26	11V	20	18.95
JTOS-50	25-47	-108	-19	15V	20	13.95
JTOS-75	37.5-75	-110	-27	16V	20	13.95
JTOS-100	50-100	-108	-35	16V	18	13.95
JTOS-150	75-150	-106	-23	16V	20	13.95
JTOS-200	100-200	-105	-25	16V	20	13.95
JTOS-300	150-280	-102	-28	16V	20	15.95
JTOS-400	200-380	-102	-25	16V	20	15.95
JTOS-535	300-525	-97	-28	16V	20	15.95
JTOS-765	485-765	-98	-30	16V	20	16.95
JTOS-1000W	500-1000	-94	-26	16V	25	21.95
JTOS-1025	685-1025	-94	-28	16V	22	18.95
JTOS-1300	900-1300	-95	-28	20V	30	18.95
JTOS-1550	1150-1550	-101	-20	...	30	19.95
JTOS-1650	1200-1650	-95	-20	13V	30	19.95
JTOS-1750	1350-1750	-101	-16	...	30	19.95
JTOS-1910	1625-1910	-92	-13	12V	20	19.95
JTOS-1950	1550-1950	-103	-14	...	30	19.95
JTOS-2000	1370-2000	-95	-11	22V	30 (@8V)	19.95
JTOS-3000	2300-3000	-90	-22	...	25 (@5V)	20.95
JCOS-820WLN	780-860	-112	-13	...	25 (@9V)	49.95
JCOS-820BLN	807-832	-112	-24	14V	25 (@10V)	49.95
JCOS-1100LN	1079-1114	-110	-15	...	25 (@8V)	49.95

Notes: *Prices for JCOS models are for 1 to 9 quantity. **Required to cover frequency range. ***Tuning Voltage for JTOS-3000 is 0.5 to 12V, JTOS-1550, JTOS-1750, and JTOS-1950 is 0.5 to 20V, and JCOS-820WLN and JCOS-1100LN is 0 to 20V. For additional spec information and details about 5V tuning models available, consult RFAF Designer's Guide, our Internet Site, or call Mini-Circuits.

DESIGNER'S KITS AVAILABLE

K-JTOS1 \$149.95 (Contains 1ea. all JTOS models except JTOS-25, -1000W, -1300 to -3000).
K-JTOS2 \$99.95 (Contains 1ea. JTOS-50, -100, -200, -400, -535, -765, -1025).
K-JTOS3 \$114.95 (Contains 2ea. JTOS-1300, -1650, -1910).

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US 67 INT'L 68

CIRCLE READER SERVICE CARD

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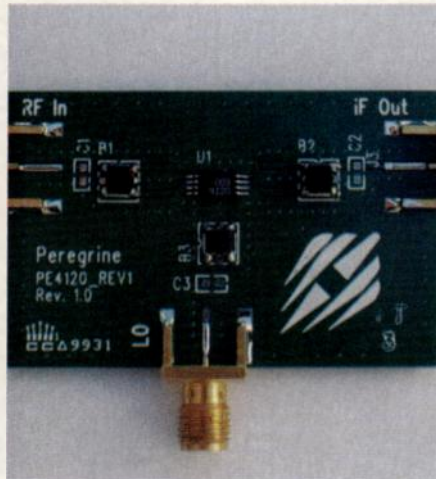
The Design Engineers Search Engine Provides ACTUAL Data Instantly From MINI-CIRCUITS At: <http://www.minicircuits.com>

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F 234 Rev. E

Low-loss, high-linearity MOSFET quad mixer

Peregrine Semiconductor's high-linearity MOSFET quad mixer that is



designed to provide functions ranging from frequency conversion to phase detection at up to 2.5 GHz. A conversion loss of 6 dB across its entire operating frequency range makes the device appropriate for such applications as cellular and PCS base stations and cable modems. The PE4120 is manufactured using the company's proprietary UTSi process and features 500 MHz to 2.5 GHz frequency functionality, and mixes IF and LO frequencies to provide a RF output. The IP3 of the device is 28 dBm, LO-IF isolation is 36 dB and LO-RF isolation is 34 dB. The device functions from -40°C to $+85^{\circ}\text{C}$ and is offered in 8-pin TSSOP and SOT-23 packages.

Peregrine Semiconductor
INFO CARD 117

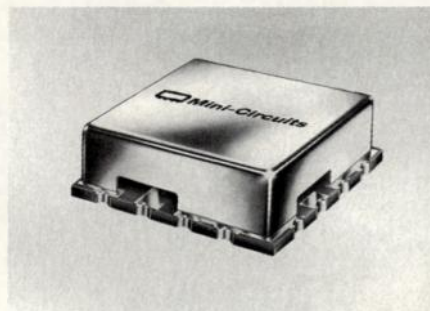
Dual band programmable noise generator

Noise Com offers a new dual-band VXI9000 series programmable noise generator. The VXIbus device has the ability to switch between two noise bands, within the same instrument, providing dual frequency capability. Available options include a signal and noise combiner, 0.1 dB precision attenuator steps for both the signal and noise path and custom noise filtering. Frequency ranges are available from 10 Hz to 40 GHz.

Noise Com
INFO CARD 118

Cellular band VCOs and wideband PCS mixer

Two new components from Mini-Circuits have been introduced for the cellular and PCS markets. The ROS-900PV VCOs works with a 4.5 V supply voltage and 0.5 to 5 V minimum to maximum tuning voltage, making them suitable for integration with monolithic PLL chips and commercial synthesizers. The VCOs feature a 1 MHz, typical, modulation bandwidth, excellent tuning linearity and -102 dBc/Hz typical phase noise at 10 kHz offset. The ADE-42MH wideband microwave mixer features 5 MHz to 4.2 GHz band-



width, low midband conversion loss of 7.5 dB typical. Midband, typical IP3 is +17 dBm and typical L-R and L-I isolation is 29 and 26 dB respectively.

Mini-Circuits
INFO CARD 119

Chipset level support for wireless networking

Fox Electronics is now stocking a standard, off-of-the-shelf crystal oscillator designed for Intersil's PRISM I, II, and III chipsets has been announced by Fox Electronics. The F4106-440 CMOS oscillator is offered in an industry standard 5 X 7 mm ceramic SMD package.

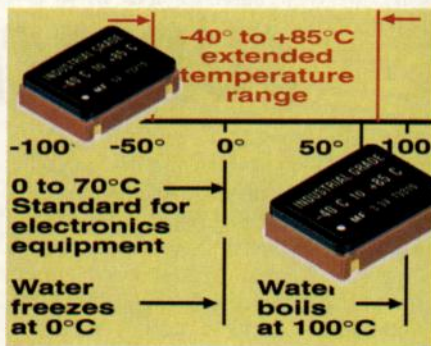


Offering stability of $\pm 25\text{ ppm}$ the oscillator features 3.3 V operation, a 1.4 mm low profile footprint, a frequency of 44 MHz and a standard operating temperature of -10°C to $+70^{\circ}\text{C}$. Also available is an extended temperature version (-40°C to $+70^{\circ}\text{C}$) and a special 22 MHz version for PRISM I.

Fox Electronics
INFO CARD 120

Industry grade SMD clock oscillators

Miniature industrial grade clock oscillators have been developed by MI Electronics. The surface mount devices T3312 and T3212, are based upon military-grade manufacturing and feature a design based upon inverted mesa crystals and rugged multilayer gold/ceramic packaging. The devices feature 5 ps RMS jitter over a the extended temperature range of -40°C to $+85^{\circ}\text{C}$. The devices offer time and frequency reference signals from 20 kHz to 100 MHz. Accuracy is maintained to $\pm 50\text{ ppm}$ over the full temperature range. The devices operate from 3.3 VDC (T3312) or 5V (T3212) and draw 35 and 45 mA of maximum load current, respectively. Waveform symmetry is 45/55 and both models are



capable of driving both CMOS and TTL Loads. Technically, the device holds $\pm 50\text{ ppm}$ frequency stability over the specified temperature range and long-term drift for the devices is specified at $\pm 1\text{ ppm/year}$, with first year drift of less than $\pm 3\text{ ppm}$.

MF Electronics
INFO CARD 121

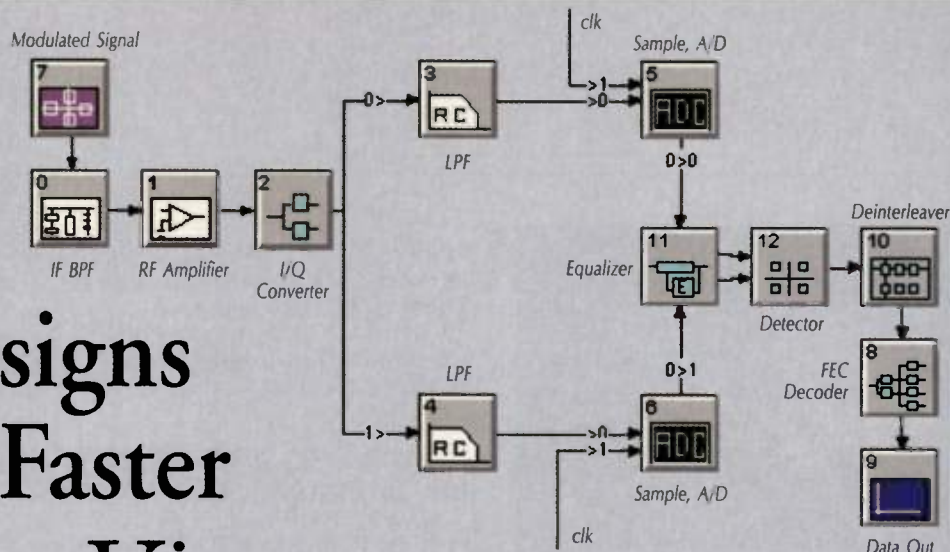
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What They're Saying About SystemView

"No other program with so much simulation power is as easy to use. When you finish a session with SystemView you realize that you've spent all the time applying engineering principles and none of the time struggling with the computer."

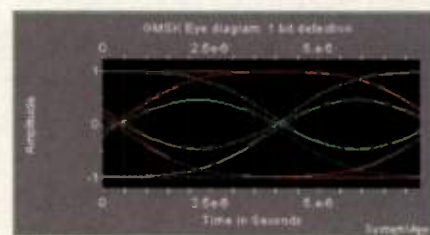
- Richard Chick, MIT Lincoln Labs -

"We use SystemView very heavily, not only in the brainstorming/prototyping stage, but also throughout the development process — right up to the point where we're actually building silicon."

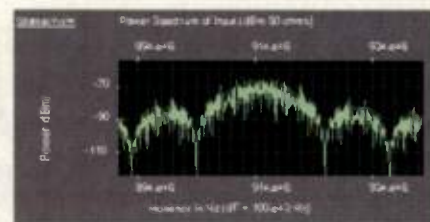
- Steven Hall,
CommQuest Technologies -

"For digital filter design, SystemView was indispensable due to its accurate simulation of the fixed point arithmetic mode employed on the actual DSP processor used in my design."

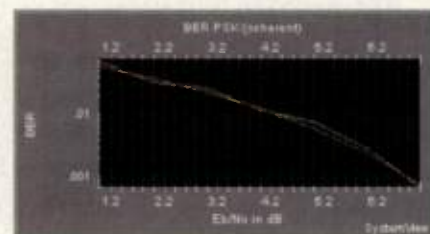
- Bisla Balvinder,
Itron -



GMSK Eye Diagram (1-bit Detection)



Input Power Spectrum

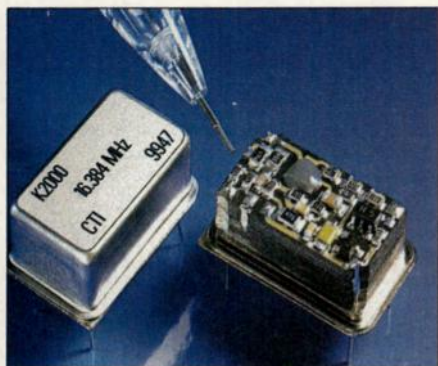


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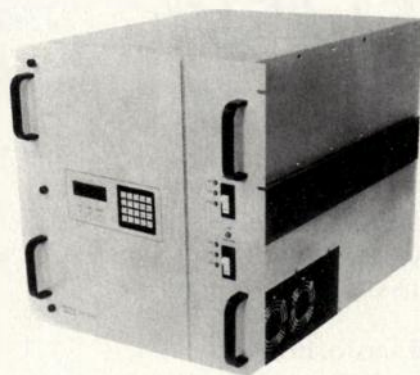


dBc/Hz at 10 Hz and voltage pull/hold in function is greater than ± 10 ppm. The series is available as standard to 20 MHz with options to 38.88 MHz.

Champion Technologies
INFO CARD 122

IF switching matrix offers low crosstalk

Matrix Systems has debuted the model 13098 200 MHz IF switching



matrix. The device is capable of switching up to 128, each, inputs and outputs. The device covers the 70 MHz band with ± 20 MHz and the 160 MHz band with ± 40 MHz. Features include a three-stage architecture with auto routing, non-blocking full fan out, 60 dB isolation at 200 MHz, solid state contacts, RS-232 and IEEE-488 interface, switchpoint status feedback, redundant signal paths and power supplies. Additionally, the unit can be programmed via a keypad input and offer low crosstalk.

Matrix Systems
INFO CARD 123

designed for Stratum 3 timing and synchronization applications. Housed in hermetically sealed DIL 14 packages, the devices are intended for either +5 or +12 VDC supply voltages. Frequency stability is less than ± 0.1 ppm after aging, from 0° C to +70° C for the 12 V model. Overall frequency stability, including temperature, voltage, load and aging is less than 370 ppb/day. The devices will hold frequency to within ± 4 ppm over 10 years. Phase noise is less than -95

Time and frequency simulation software

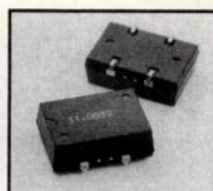
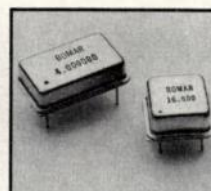
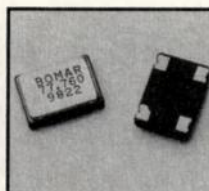
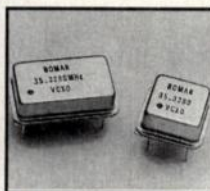
Optotek's transient analysis simulator, MMICAD Waveform software improves the application of time-domain simulation by predicting waveforms in fast, nonlinear circuits. MMICAD WAVEFORM can also use complex, externally-defined waveforms such

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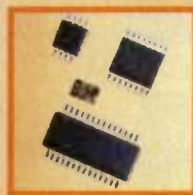
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TEMIC Semiconductors offers SiGe ICs, such as U7006B, that feature extremely high integration. With fewer components, you design smaller, lighter phones. High efficiency and low supply voltage (e.g. T0930: PAE > 50%, $V_s = 1.8$ V) mean they are also lower in power consumption. This lets you both slim down bulky batteries and extend talk-time. Our SiGe products deliver high gain and low noise figures (e.g. U7006B: $G_p = 19$ dB, NF = 1.6 dB @ 2 GHz), enabling higher sensitivity at low supply current. Available now, benefit from our full SiGe range being manufactured in high volume.

P/N	Description	Application
✓ U7004B/ U7006B	1.9-GHz PA + LNA	DECT RF Front End
✓ T0930	900-MHz PA	2-way pager
✓ TST0950	900-MHz LNA	GSM, ISM
✓ TST0912	900-MHz PA	GSM

PA: Power Amplifier

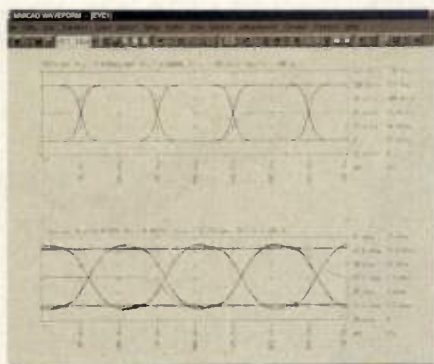
LNA: Low Noise Amplifier

www.temic-semi.com/sige.htm

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INFOCARD 34



as Pseudo Random Bit Sequences (PRBS) or WCDMA. MMICAD waveform can be used to advantage in the design of GaAs ICs for use in high speed optical communication modules, improved RF/microwave packages, or nonlinear transmission lines. The new software is intended for the design of circuits where difficulties are experienced with conventional time domain and/or harmonic balance simulators. The new simulator is constructed as a two-component, character mode exe-

cutable comprising the S-parameter-to-impulse data converter that transforms the S-parameter circuit response to an equivalent impulse response in the time domain and the time domain simulator itself. Each component is constructed as a stand-alone executable running under Microsoft Windows 95/98/NT and can interface with the other components of the MMICAD CAE/CAT software suite (for example, the MMICAD Linear Simulator and LASIMOTM transistor parameter extractor).

Optotek
INFO CARD 124

Versatile OCXO for GPS and Stratum 3E

A new line of oven controlled crystal oscillators has been introduced by C-MAC. The OCXOs claim stability of ± 0.002 ppm across an operating temperature range of -20°C to $+75^{\circ}\text{C}$. The devices are built around SC cut quartz crystals and can be used in



GPS applications as well as economical Stratum 3E switching. The device are available in frequency from 2. MHz to 20 MHz, or up to 40 MHz with some degradation in stability. The CFPO-4 series is designed on a smaller footprint, thereby finding a home in basestation CDMA and GSM and SONET/SDH systems as well.

C-MAC Frequency Products
INFO CARD 125

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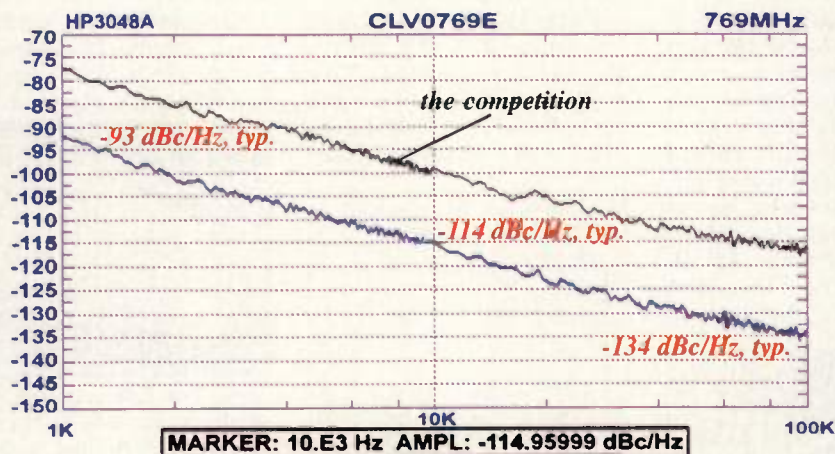
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Part No:	Freq. Range:	V _{tune}	Φ _n at 10kHz	V _{supply}
CLV0769E	734-804	1-4	-112	5
CLV0815E	806-824	0.5-4.5	-113	5
CLV0945E	936-953	0.5-4.5	-114	5
CLV1320E	1295-1335	1-5	-113	5
CLV1525E	1500-1550	0.3-4.7	-110	5



Learn more about Z-COMM's CLV product line by visiting our web site at <http://www.zcomm.com/> for datasheets, outline drawings, tape and reel specifications, and application notes, as well as our complete product catalog and custom VCO inquiry form.

Come to the source ... Z-COMM.

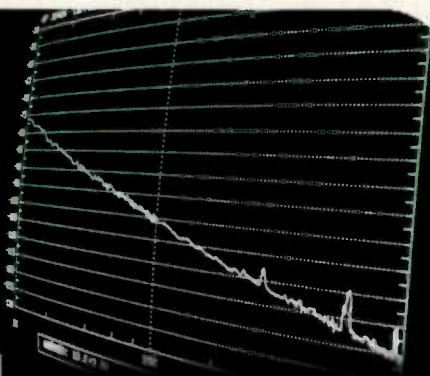


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RF products

Cable network and interference analyzer

Telecom Analysis Systems has added the TAS 8250 test system to its product line. The tester is designed to emulate critical hybrid fiber/coax (HFC) cable network impairments in a controllable laboratory instrument. It's designed for evaluating the transmission performance of cable modem termination systems, set-top boxes, HDTV equipment and IP telephony products. It can emulate both upstream (5 to 42 MHz) and downstream (50 to 860 MHz) HFC channel characteristics. Impairments emu-

lated by the device include amplitude tilt, IMD, group delay distortion, noise and interference. A built-in diplex filter combines the upstream and downstream channels from the CMTS or headend into a single interface, allowing single or multiple subscriber devices to be tested. Taskit software can be used to provide a GUI for controlling the set and it can be integrated with either the TAS 4500 or HP 89441 for additional testing capabilities.

TAS
INFO/CARD 126



Spread spectrum data transceiver

RF Neulink has released a spread spectrum data transceiver for use in the 2.4 GHz band. The SS9600 data transceiver is designed for point-to-



point and point-to-multipoint data communications. The unit integrates a built-in modem with data rates of up to a 9600 bp/s over-the-air rate. The system employs true frequency hopping and multiple units can be combined to offer a system with up to 238 units. Operating in the 2.4 GHz unlicensed band, the unit is plug-and-play and contains built-in, self adjusting power control.

RF Neulink
INFO/CARD 127

Dual-band down converter chip

A dual-band downconverter chip for GSM and TDMA cellular phones has been developed by Motorola. The chip is contained in a single, 24-pin plastic TQFP SMT package. Each downconverter in the MC13740A contains a low-noise gain-selectable amplifier, a buffered LO output and a mixer. The mixer's

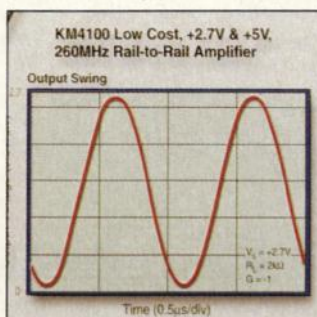


linearity and selectable gain provide the ability to meet cellular system linearity, while maintaining low power consumption. Offering open collector outputs and off-chip LNA matching, the device is usable in GSM900, DCS1800 PCS1900 and TDMA applications.

Motorola
INFO/CARD 128

2.7 and 5.0 volt rail-to-rail amplifiers

Kota Microcircuits has announced a family of rail-to-rail amplifiers. The models KM4100 (single with disable) and KM4200 (dual) are single supply

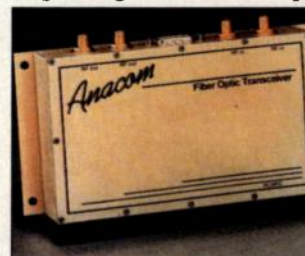


voltage feedback amplifiers. Designed for low power, battery powered commercial applications such as GSM, W-CDMA basestations, portable instrumentation, set top boxes and computers. Features include low supply currents (4.2 mA), 150 V/µs slew rates and ±90 mA of output current. They are available in SOT23-5 and SOT23-6 packaging (varies with model).

KOTA Microcircuits
INFO/CARD 129

Four channel WDM transceiver

Anacom systems has introduced the AC 234 fiber optic transceiver pair for transmitting RF signals over fiber opti-



cable. The link is designed for applications where there are expensive, or limited availability of fiber optics. The device can transmit two broadband channels, simultaneously, both directions over a single fiber cable. Designed for use PCS/PCN, cellular and WI applications, the device utilizes wavelength division multiplexing (WDM) to accomplish transmitting the tv pairs. the device accepts tv independent RF signals via two coax connectors from the base station and convert them into optical signals. I installation location between the remote antenna location and the base.

Anacom Systems
INFO/CARD 130

NEW PRODUCTS

NO.69

RF/IF MICROWAVE COMPONENTS



FROM
\$4.45

RF TRANSFORMERS HAVE 4:1 IMPEDANCE 200 TO 1400MHz

Broad band TCM4-14 surface mount RF transformers from Mini-Circuits operate in the 200 to 1400MHz band with 4:1 impedance ratio. Referenced to midband loss (0.8dB typ), insertion loss is 1dB from 800MHz to 1000MHz, 2dB in the 300 to 1300MHz range, and 3dB band wide when operated within -20°C to +85°C (max.). Open case design has plastic base with solder plated leads, and applications include impedance matching and baluns. RF power is 250mW (max.).



FEATURED PRODUCT

FROM
\$7.95

3000 TO 4000MHz MIXER IS TEMPERATURE STABLE

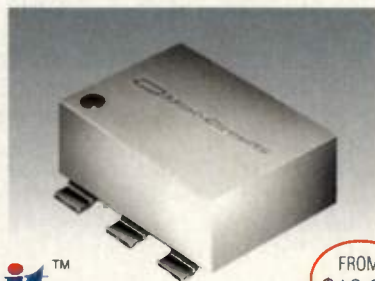
Higher frequency designs will benefit from Mini-Circuits patented family of MBA model Blue Cell™ mixers, which deliver a unique combination of low conversion loss, superb temperature stability, thin 0.07" profile, and low cost. This level 13 (LO) MBA-35MH model spans 3000MHz to 4000MHz with 22dB L-R, 14dB L-I isolation and low 5.1dB midband conversion loss (all typ). Operating temperature is -40°C to +85°C (max.) and applications include satellite and PCMCIA.



FROM
\$19.95

1550 TO 1720MHz VCO HAS LINEAR TUNING

The ROS-1720 voltage controlled oscillator from Mini-Circuits operates within the 1550MHz to 1720MHz band targeting PCS and DCS applications with low -141dBc/Hz SSB phase noise typical at 1MHz offset, wide 3dB modulation bandwidth typical at 18000kHz, and 28-34MHz/V (typ) linear tuning sensitivity. Housed in a miniature 0.5"x0.5"x0.18" industry standard package, typical power output is 7dBm.



FROM
\$12.95

50 TO 200MHz MAGIC-TEE OPERATES WITH LOW LOSS

Mini-Circuits has introduced a versatile 2way-0°/180° power splitter and combiner for the 50 to 200MHz band. Model AMT-2 typically has low insertion loss (0.25dB S-1 and S-2, 0.8dB J-1 and J-2), very good 1.10:1 input/1.12:1 output VSWR, plus excellent 0.1dB amplitude and 1 degree phase unbalance. Designed for 50 ohm systems, this 4 port hybrid covers IF receiver and satellite applications. Maximum power input as a splitter is 0.5W.

824 TO 849MHz COAXIAL AMPLIFIER FEATURES LOW NOISE

This 824 to 849MHz cellular band ZQL-900LN low noise amplifier from Mini-Circuits typically provides high 16.5dB gain (±0.2dB flatness), ultra-low 1.0dB noise figure, and 22.5dBm maximum power output at 1dB compression. High +35dBm IP3 helps suppress noisy intermodulation products, and operating temperatures range from -40°C to +70°C maximum. Equipped with 50 ohm SMA-Female connectors.



FROM
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2W SMA ATTENUATORS AVAILABLE IN DESIGNER'S KIT

Six different DC to 18GHz fixed attenuators from Mini-Circuits "BW" series are now available at a special evaluation price in designer's kit form. Kit number K-BW2 contains units that display nominal attenuation values of 3dB, 6dB, 10dB, 20dB, 30dB, and 40dB. Built tough to handle 2W average, 125W peak power, these miniature stainless steel precision attenuators are ideal for matching, test set-ups, and instrumentation applications. Available from stock.

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AMPLIFIERS

Broadband driver amplifier

EiC's Model EC-1017 is an internally matched broadband driver amplifier optimized for commercial mobile applications. The device offers power down

capability and high linearity. The amplifier operates with voltages of +3.5 to +5.0VDC. It provides +17 dBm of saturated output power when operating from a +3.5 VDC supply. Typical gain is 9 dB at 1.9 GHz, with +15 dBm of output power at 1dB compression. Third order intercept point is +25 dBm with a noise figure at 5 dB and an

input loss return of 11 dB. The amplifier typically draws 55 mA current from a +3.5 VDC supply and consumes 1 μ A, or less, in power-down mode. It is supplied in a plastic, surface-mount SOIC-8 slug package.

EiC
INFO/CARD 131

Rail-to-rail 1MHz SC70 op amp with 1 μ A shutdown

Maxim Integrated Products has introduced the Max4400/Max4401 rail-to-rail op amps. The devices include a 1 μ A shutdown and come in SC70 packages. These devices consume 320 μ A in normal operation and achieve a 1 MHz gain-bandwidth product. Operating from a single +2.5V to +5.5V supply, these unity gain stable op amps are ideal for portable/batter-powered applications. They offer low power consumption without sacrificing bandwidth or gain accuracy. The Max4400 is offered in 5-pin SC70 and 5-pin SOT23 packages. They are specified over the temperature range of -40° to +125° C.

Maxim
INFO/CARD 132

80 db ultra high dynamic range chip

The model SDLVAC-0120-80 is a 300 MHz to 2 GHz successive detection logarithmic video amplifier chip (SDLVA-chip). It offers a -75 to +10 dBm dynamic range with a log slope of 25 mV/dB (10 to 50 mV/dB available). The log linearity is ± 1.0 dB over the operating temperature range of -40° C to +85° C typical. The chip provides 20 MHz video bandwidth and a limited IF output of -20 dBm minimum. It operates from +5 VDC @ +80mA and -5 VDC @ -135mA and measures 0.50" x 0.35" x 0.09".

Planar Monolithics
INFO/CARD 133

InGaP CDMA amplifier

Celeritek's new CHP 1232-PM is a CDMA 50 Ω matched 6 mm square power amplifier module for PCS wireless local loop and other high bandwidth wireless data markets. The InGaP HBT amplifier module offers a smaller footprint than similar products, integrates (14) supporting components, and has been specifically developed to meet the

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continuing requirements for small, low-cost, high capacity wireless voice and data applications. It is a linear efficient three-stage power amplifier developed for PCS CDMA handsets and infrastructure systems, WCDMA 3G handsets and wireless local loop (WLL) subscriber units that operate in the 1.85 to 1.91

GHz frequency range. Typical features include operation as low as 3.2 volts from a single positive supply, 30 dB gain at operating output power, 35% linear power added efficiency, and +28 dBm output power (IS-98 CDMA mode).
Celeritek
INFO/CARD 134

2.25 KW C-Band TWT Amplifier

The 2.25 kW C-Band TWT amplifier model VZC-6967B4, has been refined to provide an improved user interface and CE certification for European safety requirements. It works with earlier models of 2.25 kW TWTAs and fixed satellite service applications.

CPI
INFO/CARD 135

Wireless communication modules

Ericsson has released a series of wireless communication modules designated as the GM25, GM22, DM10 and DM20. The GM22 is a dual band GSM module handling voice, SMS and fax. The GM25 is a dual band GSM module handling voice, SMS, fax and data. The DM10 is a dual band AMPS and TDMA, 850 MHz module, handling voice, SMS, fax and data. Finally, the DM20 for AMPS 850 MHz and TDM 850/1900 MHz module, handling voice, SMS, fax and data.

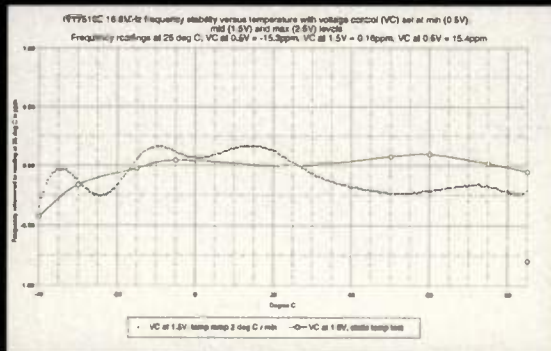
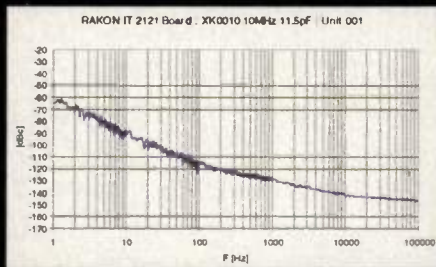
Ericsson
INFO/CARD 136

More innovation from Rakon

The leaders in crystal technology present the 7500 series oscillators. Featuring outstanding temperature stability and no frequency perturbations, at low cost.

Rakon's new IT7500 and IVT7500 oscillators lead the way for a new generation of products. The 7500 series features an analogue IC for temperature compensation. This analogue IC has no erratic frequency jumps unlike previous digital compensation attempts. The unit can operate on any supply voltage between 2.7 and 5.5 volts, and consumes only 1.2mA typically. Clipped Sinewave frequency outputs ranging from 10MHz to 26MHz are available.

Both the IT7500 and IVT7500 provide excellent temperature stability performance for low cost, making it the oscillator of choice for GSM/TDMA/AMPS cellular phones, PCMCIA CDPD cards, two-way pagers and many other wireless applications.



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SUBSYSTEMS

RAM-based baseband chipset for GSM handsets

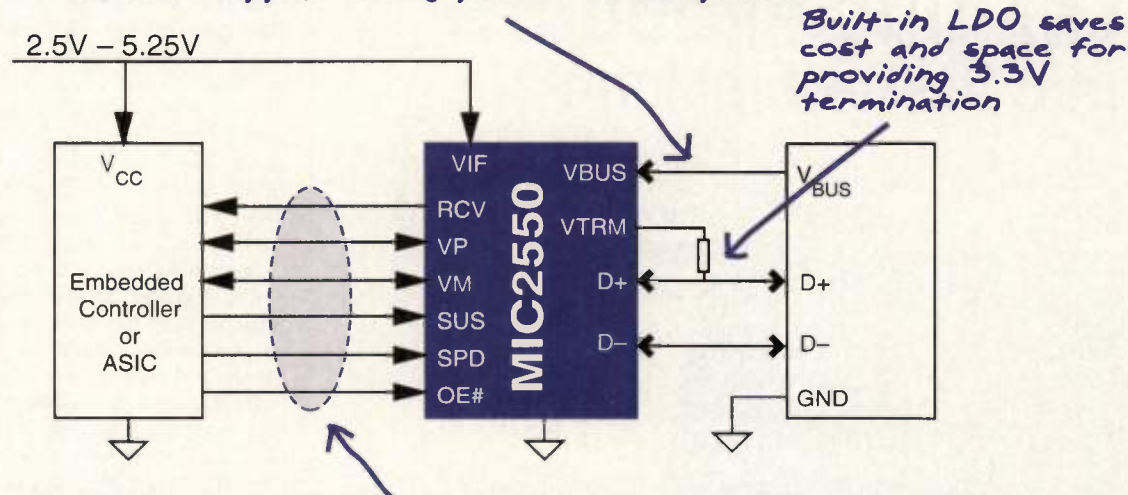
Analog's AD20msp430 SoftFor chipset is the first completely RAM-based baseband chipset for wireless handsets. The device is a next generation GSM baseband chipset that provides cellular phone manufacturers with the functionality to customize features and options entirely in software. Network operators can also add or remove features over the airwaves. As a RAM-based chipset, GSM phone manufacturers can load different software versions to support an entire family of high-end to low-end phones using common hardware platform. The chipset allows designers to build applications, such as GSM mobile phone, PDA-type platforms and Internet appliances that accommodate 2.5G wireless data communication standards, including GPRS and HSCSD and are forward compatible with future 3G cellular standards.

Analog devices
INFO/CARD 137

USB Transceiver for Less

(Less Power Consumption, Space & Cost)

Transceiver supply current is direct from USB, not system supply, saving power consumption



MIC2550 interface runs from same supply as ASIC, making input and output signals fully compliant

The Good Stuff

- ◆ Compliant to USB specifications
- ◆ Interfaces to standard SIE interface
- ◆ Unique dual supply voltage operation
- ◆ Low and full speed support
- ◆ Operates down to 2.5V
- ◆ Integrated LDO for speed termination voltage
- ◆ Low power suspend mode
- ◆ Low height TSSOP package

Micrel's new USB transceiver will save your next USB peripheral design time, cost, and reduce design complexity.

The MIC2550 employs a unique dual supply voltage design which allows operation down to 2.5V on the system side, and connects directly to the USB voltage bus. An integrated LDO provides the speed termination voltage without requiring additional space or cost.

With the MIC2550, you can operate your embedded controller or ASIC from 2.5V to 5.5V without additional voltage translation circuitry or special I/O cells to support USB's 3.3V signalling.

In addition, the MIC2550 takes its operating power direct from the USB voltage bus, decreasing power consumption from the system battery.

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TDMA IC's for cellular/PCS phone applications

The TriQuint TQ5122, cellular frequency band receiver and the TQ5622, PCS frequency band receiver, are complementary devices designed for use in IS-136, TDMA or equivalent wireless handsets. Both

are low current devices that include a power down or sleep mode to extend both standby and talk times in wireless applications. They include an LNA mixer, LO buffer and IF buffer amplifier and operate from a single 2.8 V power supply. Additionally, they are designed to minimize the number of external bypass and matching ele-

ments to keep board space and cost to a minimum.

TriQuint Semiconductor
INFO/CARD 138

32-Channel digital receiver for FPDP connectivity

The Pentek model 6536 is a multichannel VME board that accepts digitized data from four parallel inputs at sampling rates up to 40 MHz. The device has been developed for application into original equipment manufacturer's and systems integrator's products. The unit is designed for addressing high-speed processing tasks including summation of multiple channels for beamforming applications, direction finding, demodulation decryption and other signal analysis tasks, such as medical imaging and analysis of many forms of radar or sonar signals. The device can be configured with up to 32 channels of narrowband receivers to perform frequency down conversion, lowpass filtering and decimation of the sampled output. Each of the 32 receiver can independently select any one of the four A/D input sources.

Pentek
INFO/CARD 139

IrDA-compatible transceiver enables handheld devices

IrDA-compatible infrared transceiver in a sunk mounting package that can be affixed to the edge of a printed circuit board. With a 115.2 kbp/s maximum data rate, the transceiver is offered in a notched surface-mount "Dracula" package measuring 13 mm x 7.5 mm. Its height profile of 1.8 mm over the PCB will enhance the ability of designers to slenderize IR-enabled palmtops and other mobile systems while providing IR connectivity at distances up to 1 meter.

Vishay
INFO/CARD 140

TEST AND MEASUREMENT

Monopulse beacon radar test set

The Monopulse Beacon test set is specifically designed for field technicians to certify Monopulse Secondary

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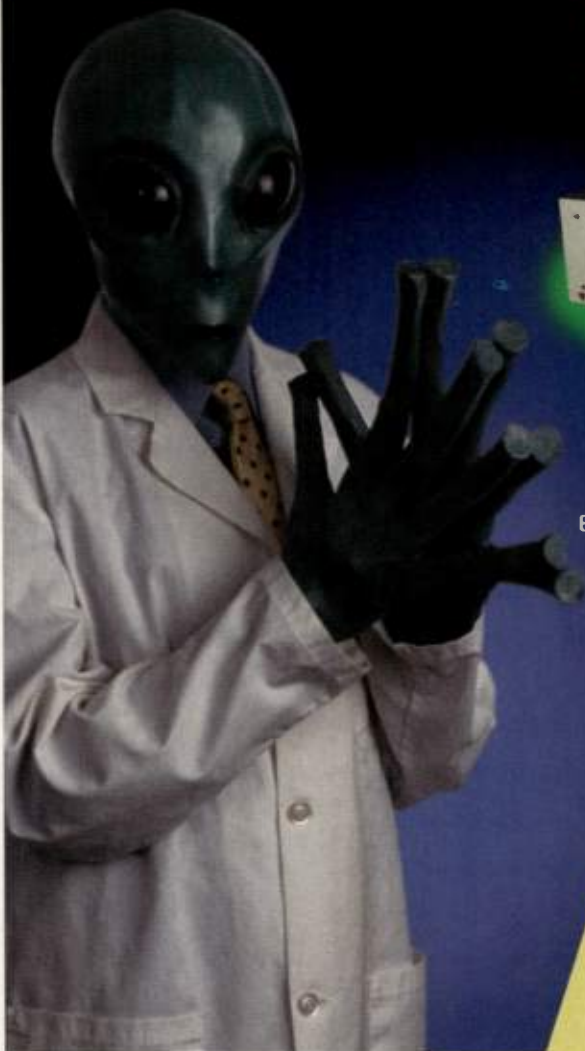
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INFOCARD 47



Surveillance Radar (MSSR) system sensitivity and target detection. It provides the ability to test the MSSR from end-to-end, through the injection of ATCRBS signals or mode S RF test targets into the MSSR front end. MSSR test targets can be observed at various points in the MSSR system and when used for overall system sensitivity, can be processed through to the controller's display. The MBTS primary functions include measuring and calibrating receiver sensitivity, measuring and calibrating fixed thresholds, measuring and calibrating sensitivity time constant curves, measuring and calibrating delta/sum threshold, measuring and calibrating sum/omni threshold and testing and alignment of receivers, using pulsed and CW monopulse receiver signals.

Freestate Electronics
INFO/CARD 141

Multi-channel digital pulse generator

The Model 555 digital pulse gener-

ator from Berkeley is capable of digital delay and pulse generation of multi-channel, 1 ns-resolution timing, delaying, gating, pulsing and syncing functions. Each channel provides both delay and width functions, so a 2 channel model 555 provides the same delay and width functionality of competitive 4-channel units. The 555 is available in 2, 4 and 8 channel configurations and can provide precise delays and widths with 1 ns resolution for times up to 100 seconds. These pulses are synchronized to a common trigger or an internal trigger.

Berkeley Nucleonics
INFO/CARD 142

Amplifier for IEC measurements

The 150W1000 is a broadband test amplifier offering 150 W minimum power and frequency response from 80-1000 MHz. The unit is designed to provide a margin of power when testing to IEC 10V/m requirements at 3 meters from 80 to 90 MHz. This addresses the issue of lower power am-

plifiers that may not be able to generate a sufficiently strong field at the bottom end of the frequency range. The amplifier is equipped with a DCI that provides local and remote control of the amplifier. A four line digital display, menu assigned softkeys, rotary knob, and four dedicated switches offer control and status reporting capability. Operational presentation of forward and reflected power, control status and reports of internal amplifier status are also provided.

Amplifier Research
INFO/CARD 143

B series offers cable and antenna analyzer

Anritsu's latest hand-held instruments from their site master cable antenna analyzer product family feature increased rejection of interference signals, distance-to-fault measurement capabilities, enhanced range and a number of other features. With the Site Master B series, network operators and service providers can pinpoint problems much faster and more accurately than

Innovation

JFW has designed and manufactures over 1200 different programmable attenuators. Features include wide attenuation ranges, optional step sizes, various package styles and connector options to provide system designer the flexibility required in today's global market.

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6GHz

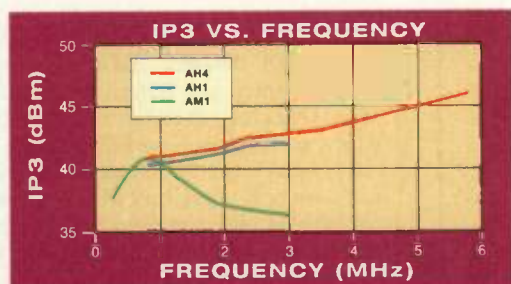
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Higher Frequency...
41dBm IP3 UP TO 6GHz**



**LOWER FREQUENCY
High Performance**



Need Higher Frequency? You need Watkins-Johnson's new AH4 amplifier.



High IP3 up to 6 GHz is what our new AH4 is all about. Combined with a low noise figure, it's the perfect choice for today's multichannel wireless systems. Drawing only 150mA and operating from a single positive supply, the AH4 delivers an IP3 of 41dBm. A great price combined with the outstanding linear efficiency up to 6 GHz makes this a versatile amplifier. It is perfect for multiple sockets, reducing overall part count.



Need lower frequency performance? Both the AH1 and AM1 offer low noise figures which, together with their inherent high IP3, deliver superior performance at the best price in the industry.

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INFOCARD 51

before. Other features include a high-resolution full VGA display, field-replaceable NiMH battery that consistently provides 2.5 hours of operating time and enough memory to store up to 200 time and date stamped measurements and can be custom labeled.

Anritsu
INFO/CARD 144

Wideband vector signal analyzer

The Agilent 89600 series VSA offers a 36 MHz bandwidth capacity for measuring RF signals up to 2.7 GHz. Applications include cellular and satellite communications, digital video and local multipoint distribu-

tion service (LDMS). It is also available with a VXI-based front end using one or two baseband inputs covering bandwidths to 40 MHz. The 89600 is an integrated solution of VXI hardware and measurement software that resides on PC using Windows NT. It is designed for use as a PC hosted VSA for communications design. The device offers design simulation, modeling and documentation in a single integrated interface.

Agilent
INFO/CARD 145

Low profile EL choke coil

The D31FU is a low profile unshielded inductor designed for use as an EL inverter IC choke coil. The coils are available in 0.10 to 1.2 mH inductance values have a 3.3 mm x 3.3 mm footprint with a height profile of only 1.7 mm maximum. The series can be used for electro-luminescent backlighting implementation in portable applications including cellular phones, pagers, personal digital assistants, handheld test equipment and chronographs. The inductors are packaged on tape and reel in 3,000 piece quantities.

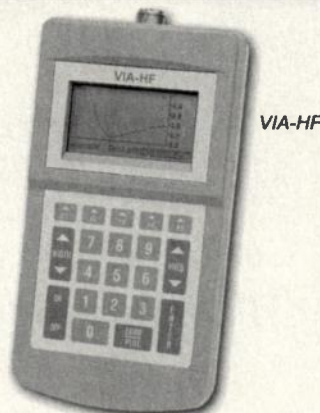
Toko
INFO/CARD 146

AEA VIA Impedance ANALYZER

The AEA Division of Tempo specializes in hand-held test instruments for the wireless communications industry

We are pleased to introduce the new *VIA-HF Impedance Analyzer* in the same compact and portable package as the AEA SWR Analyst products. This product offers virtually all the features of the SWR Analyst products plus many additional features such as Graphical presentation of Impedance, Resistance, and Reactance curves. The *distance to the nearest short or open* in a coaxial cable can easily be determined. You can tune antennas, receivers and most tuned circuits over the **frequency range of 100 kHz to 54 MHz with resolution of 1kHz/div. to 2 MHz/div. for a 20 MHz wide display.**

The VIA-HF includes a *Relative Field Strength* indicator mode plus an RS-232 port for connection to a PC. *Windows 95/2000 compatible VIA Director Software* (included) allows printing out multiple overlapping curves.



Curves can also be stored to hard disk and can be easily inserted into report documents. A simple loop probe on the end of a short piece of coax lets the VIA-HF be used as a sophisticated *"RF Dipper"* or for injecting a *signal-tracing* signal into a receiver. The signal generator mode places a trigger pulse on the RS-232 port.

See complete information on these and other AEA products on our website.

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PASSIVE COMPONENTS

Dual tracking precision trimmer capacitors

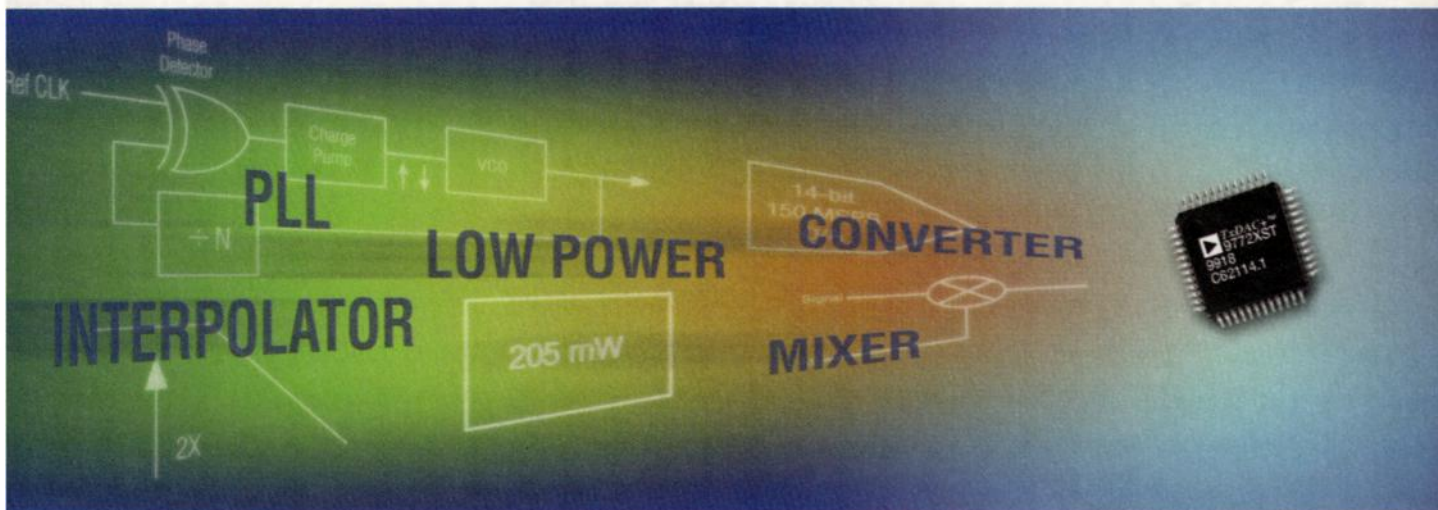
Voltronics has expanded its line of dual tracking precision trimmer capacitors to work in the GHz range. The tuning screw of the split stator style adjusts two capacitors at the same rate and have one common terminal. The sapphire dielectric part, V6152, tunes from 0.5 to 3.5 pF, is 0.48" long and can be used to over 2 GHz. At 250 MHz, the Q is over 1500 and it can be tuned over 10 full turns.

Voltronics
INFO/CARD 147

Ultra-low ESR microwave capacitors

ATC's 600 series capacitors offer an ESR of 80 mΩ at 1 GHz. Designed around RF and Microwave applications, this NPO capacitor supports requirements where low loss and high

ELIMINATE TRANSMIT MIXERS WITH THIS 14-BIT, 150 MSPS DIRECT-IF DAC.



Third generation TxDAC+® shortens the distance from processor to antenna.

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internal PLL and $f_s/4$ digital mixer, the AD9772 combines the power of high-performance signal processing with an outstanding third generation core. It delivers superior baseband performance with SFDR beyond 75dBc for a 2 to 35 MHz band, and 75 dB ACPR performance. It's available in a 48-lead LQFP and is priced at \$32.18*. For software digital radios, point-to-point

microwave, WLL or third generation base stations, this DAC is built for the communications needs of the next millennium.



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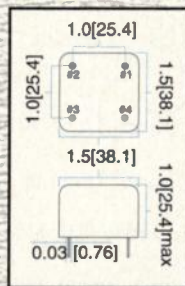
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performance are paramount. With up to 100 pF in a 0603 case size, the 60 series has a rated voltage of 250 volt. All parts are available laser marked and in tape and reel.

American Technical Ceramics
INFO/CARD 148

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1ohm
INFO/CARD 149

Inductor series comes in surface mount package

The Model DR333-7 series SMD filter inductors have high-energy storage capacity to provide efficient filtering of "ripple" in the input or output channels of the power supply. Available with frequency range of 0.1 to 10 MHz, a broad selection on standard inductance values and current ratings up to 3.6 A, the series are effective in filtering 2nd and 3rd order harmonics of the ripple frequency in DC-DC converter power supplies rated at 50 W and lower. The series is available in five different model families and designed in a wide range of performance configurations. Inductance ranges available are from 0.47 μ H ($\pm 10\%$) at 1 kHz with a DCR of 20 Ω to 0.075 A. Operation temperature is -40 to +85°C.

Datatronics
INFO/CARD 150

High speed decoupler in a 0508 package

AVX has expanded its line of IDCs to include a 0508 chip with a measured inductance of 110 pH and available in capacitance values of up to 1. μ F. The 05058 IDC connects with eight vias to power and ground planes offering a solution for the high speed decoupling necessary with today's high-speed microprocessors.

AVX
INFO/CARD 151

BIPOLAR

AMPLIFIERS

STANDARD OPTIONS

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- Integrated Limiters
- Input Bias Tee for Fiberoptic Photodetectors



FREQUENCY (MHz)	MODEL NUMBER	GAIN (dB, Min.)	GAIN FLATNESS (±dB, Max.)	VSWR IN/OUT	NOISE FIGURE F ₁ F ₂ F ₃ (dB, Max.)			OUTPUT POWER (dBm, Min.)	DOMESTIC PRICE (1-9 PCS)
0.01 - 200	AU-1442	35	0.5	2.0:1	1.2	1.2	1.2	5	\$300
0.01 - 200	AU-1447	56	0.5	2.0:1	1.2	1.2	1.2	12	\$325
0.01 - 500	AU-1310	30	0.5	2.0:1	1.3	1.4	1.5	8	\$300
0.01 - 500	AU-1332	45	0.5	2.0:1	1.3	1.4	1.5	10	\$325
0.01 - 1000	AM-1300	27	0.75	2.0:1	1.4	1.6	1.8	8	\$325
0.01 - 1000	AM-1431	35	0.75	2.0:1	1.4	1.6	1.8	10	\$350
0.02 - 1000	AM-1551	38	1.0	2.0:1	1.4	1.6	1.8	15	\$350
1 - 100	AU-3A-0110	55	0.5	2.0:1	1.2	1.2	1.2	12	\$300
1 - 200	AU-1464	35	0.5	2.0:1	1.2	1.2	1.2	6	\$275
1 - 200	AU-1494	56	0.5	2.0:1	1.2	1.2	1.2	11	\$300
1 - 500	AU-2A-0150	30	0.5	2.0:1	1.3	1.4	1.5	8	\$275
1 - 500	AU-3A-0150	45	0.5	2.0:1	1.3	1.4	1.5	10	\$300
1 - 500	AU-4A-0150	60	0.5	2.0:1	1.3	1.4	1.5	10	\$325
1 - 1000	AM-2A-000110	26	0.75	2.0:1	1.4	1.6	1.8	8	\$300
1 - 1000	AM-3A-000110	35	0.75	2.0:1	1.4	1.6	1.8	8	\$325
1 - 1000	AM-4A-000110	51	1.0	2.0:1	1.4	1.6	1.8	9	\$350
5 - 300	AU-1021	24	0.5	2.0:1	2.4	2.5	2.7	20	\$275
5 - 300	AU-1525	61	0.5	2.0:1	1.2	1.2	1.3	20	\$350
100 - 1000	AM-1412	35	0.75	2.0:1	1.4	1.6	1.8	15	\$350
100 - 2000	AM-1526	9	1.0	2.0:1	8	5.5	5.5	20	\$350
200 - 2000	AMMIC-1427	20	1.5	2.2:1	4.2	4.3	4.6	14	\$375
500 - 1000	AM-2A-0510	24	0.5	2.0:1	1.4	1.5	1.6	0	\$300
500 - 1000	AM-3A-0510	38	0.5	2.0:1	1.4	1.5	1.6	9	\$325
500 - 2000	AM-3A-0520	29	0.75	2.0:1	1.4	1.9	2.4	3	\$350
1000 - 2000	AM-3A-1020	29	0.5	2.0:1	1.8	2.1	2.4	10	\$325
1000 - 2000	AM-1477	39	1.0	2.0:1	1.8	2.1	2.4	15	\$350
1000 - 2000	AM-4A-1020	40	0.75	2.0:1	1.8	2.1	2.4	10	\$350

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CABLES AND CONNECTORS

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Coaxial Components
INFO/CARD 152

New line of MHV connectors

The MHV connector series provides shielded disconnects where high voltages are present and the BNC type interface required. Center contacts are recessed within lengthened dielectric material to provide protection against electrical shock when handling unmatched connectors. These non-constant impedance MHV connectors are built to MIL-39012 interface specification and feature nickel-plated, machined brass bodies, gold-plated pins and contracts and Teflon insulation for enhanced performance.

RF connectors
INFO/CARD 153

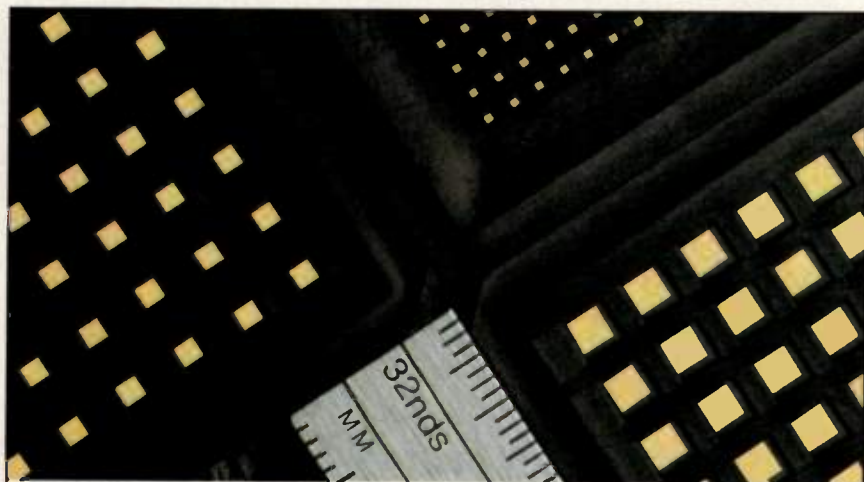
Vertical, low profile TNC connector

Die cast vertical TNC, CTP-TV-042 for 50Ω and the CTP-7TV-042 for 75Ω connectors are die cast zinc with nickel plating. The connector center is phosphor bronze with gold plating and the insulator is PE606. This combination allows the jack to perform properly over the life of the end product. The frequency range is DC to 4 GHz. Applications include cell phone, aircraft, communication antennas as well as other RF applications.

Connect-Tech Products
INFO/CARD 154

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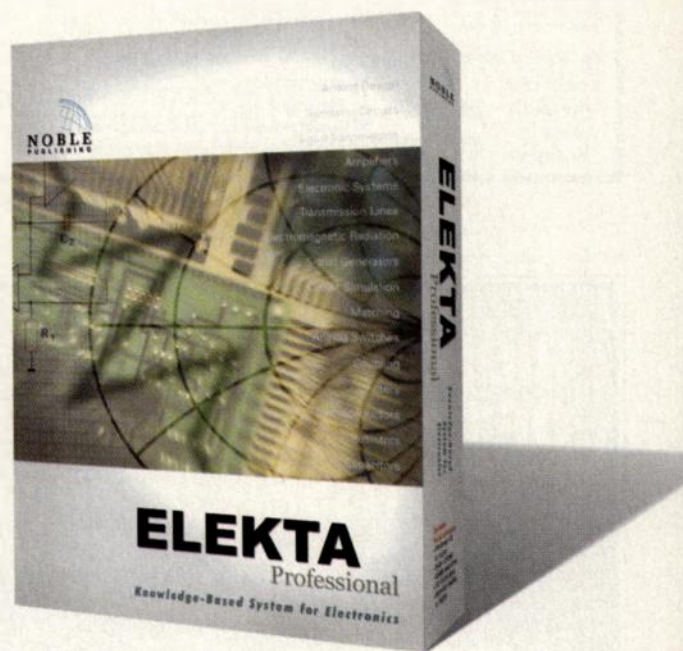
You have questions...

How many microvolts is -85 dBm at 50 ohms?
What is the spectral content of QPSK?
What the resistor color code and standard values?
How do digital IIR and FIR filters work?
What mixer spurs result from 70 MHz RF and 18.1 MHz LO?
How does an active filter work?
How do I wind a 120 nH inductor?
What capacitor resonates with 2.2 μ H at 10.7 MHz?
What VSWR corresponds to 12 dB return loss?
What's the effect of reducing Q from 300 to 100?
What is Miller effect?
How do I perform two-port transformations?
How is bias set on bipolar transistors and FETs?
What are the basics of SPICE analysis?
What do all those noise parameters mean?
How do I make a 700 Hz active bandpass filter?
What are Maxwell's equations?
Can I graph the $\sin(x)/x$ curve?
What dimensions do I need for a 50 ohm microstrip?
How do I match 25 +j40 ohms to my 75 ohm system?
Where can I find a review of Kirchoff's Laws?
How much antenna gain does my system need?
How do I bias a BFR91 or 2N2222 transistor?
Will I get bad crosstalk between lines on my p.c. board?
Can I perform basic transfer function math?
How can a beginner learn about components at RF?
What's the difference between linear and non-linear?
What is the capacitance of two 1x1 cm plates spaced 1 mm?
Why do we use feedback?
I know RF, but where can I find digital basics?
Can I do vector to scalar conversions?
What is the AC impedance of a parallel R-C network?
What is a conductor's skin depth at 900 MHz?
What do those thermal resistance numbers mean?
Can I visualize the field lines between capacitor plates?
What is the mismatch loss of a 5.22:1 VSWR?
How do I simulate a darlington pair amplifier?
What are the resistor values for a 50 ohm 6 dB pad?
Should I use a pi or tee matching network in my circuit?

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**Andrew
INFO/CARD 155**

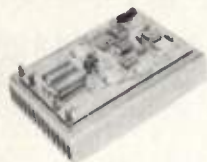
Low loss cable assemblies for communication devices

Lightweight aluminum cable assem-

blies that offer the electrical characteristics of copper jacketed, low loss semi-rigid cable assemblies are now available with a soft, lightweight Aluminum outer conductor. These low-loss cable assemblies are supplied with crimp- or conventional connectors. The cables are designed for electronics applications where lightweight and easy-to-bend qualities are applicable. Typical applications include Instrumentation television, HF communication and aviation. The cables offer VSWR of 1.35 to 18 GHz for assemblies with tv straight connectors, 1.40:1 to 18 GHz for assemblies with one straight connector and one right angle connector and 1.45:1 to 18GHz for assemblies with two right angle connectors.

**RFcircuits
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The NT2800 is a complete, single chip, FM/FSK transmitter IC, which will operate in any 26 MHz band from 800 MHz to 1.0 GHz, on a 2.7 to 3.3 supply. The device integrates on-chip VCO, phase-locked loop, and reference oscillator. Tuning is accomplished via 3-wire serial interface. Power output +1.5 dBm at 50 Ω and packaging is 16-pin TSSOP.

**Numa Technologies
INFO/CARD 157**

PHEMT GaAs IC high linearity SPDT switch

Alpha Industries' PHEMT GaAs FET IC high linearity SPDT switch features +2.5 to +5V linear operation and input power levels greater than +3 dBm. The AS191-73 transmit/receive switch features low insertion loss (0.1 dB @ 0.9 GHz), high isolation (27 dB @ 0.9 GHz) and can be used in many analog and digital wireless communication systems including cellular, GSM and DECT applications.

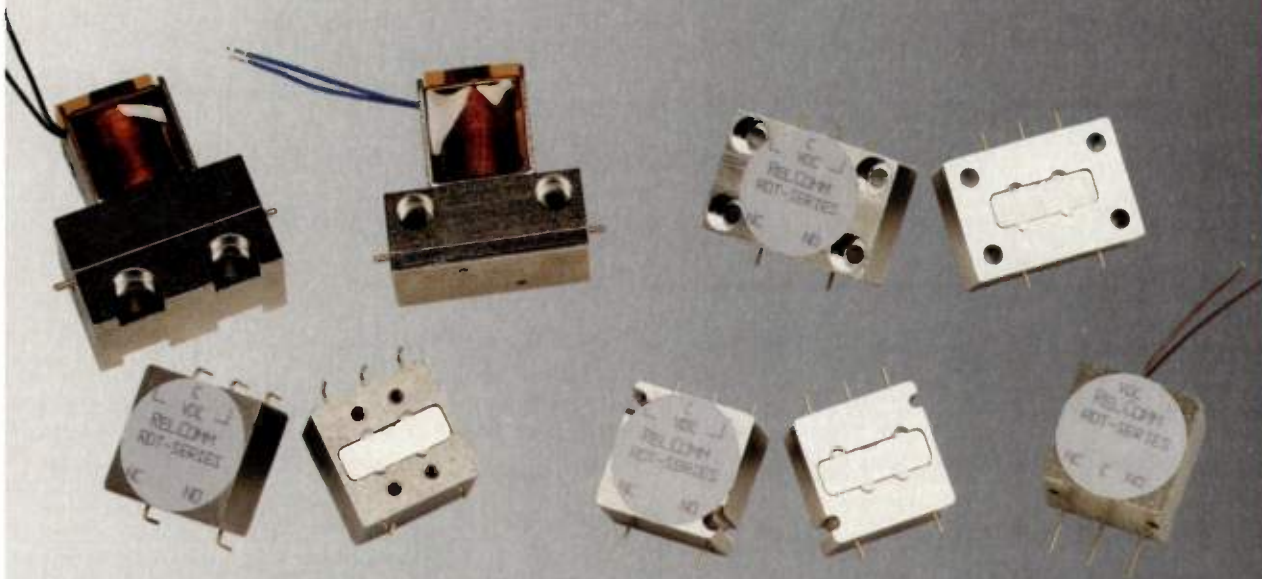
**Alpha Industries
INFO/CARD 158**

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tions for its gallium arsenide (GaAs) product family. Operating at 10 Gbps, Oki's devices can be used in long and short-haul optical communications networks. The devices include a limiting amplifier, 16:1 multiplexer and a 1:16 demultiplexer and are designed for both receive and transmitter applications at optical carrier rates of 1 Gbps (OC-192).

Oki Semiconductor
INFO/CARD 159

GaAs HBT FET LNS for L and S band receiver

A miniature GaAs heterojunction bipolar FET from NEC by California Eastern Laboratories requires a single power supply. The requirement for a second, negative supply is eliminated. Designed for use as an LNA in TDMA handset and other L and S band receiver designs, the NE5211 delivers low noise/high gain performance.

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Continued on page 8

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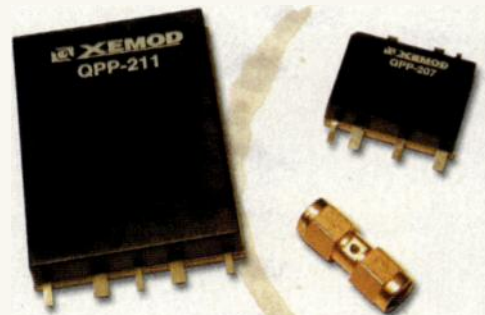
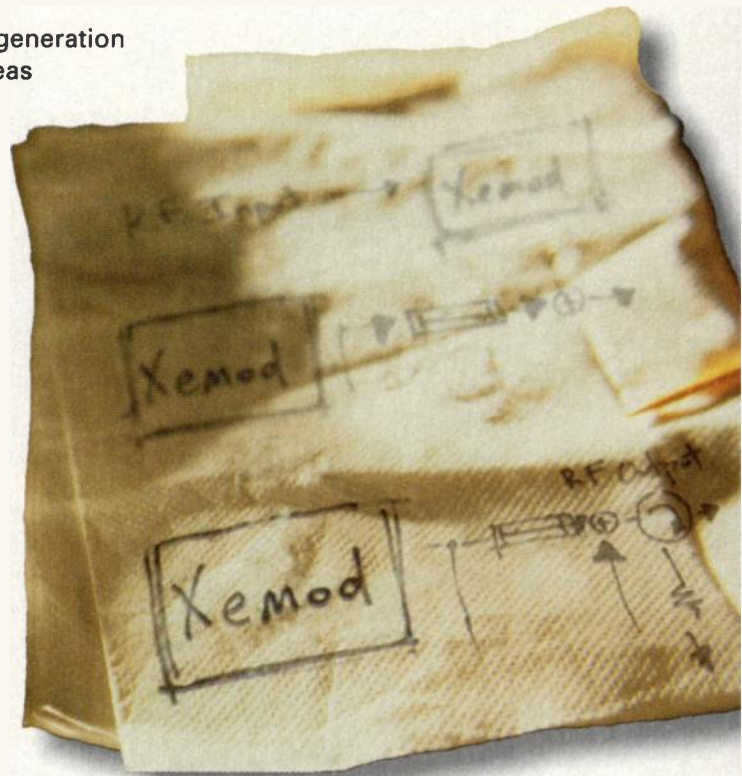
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Artech House Publishers	175	92	Maxim	162	88	United Chemi-Con	172	92
AVX	151	74	Microchip Technology	163	88	Vishay	140	68
Berkeley Nucleonics	142	70	Motorola	128	62	Voltronics	147	72
CEL	160	80	Numa Technologies	157	78	Xpedion	167	90
Celeritek	134	66	Oki Semiconductor	159	80			
C-Mac	170	92	Omron	171	92			

all current and emerging cellular standards. The AD8314 replaces discrete diode detectors and offers wireless designers a single-package, temperature-stable IC solution. Operating at up to a 2.5 GHz operating frequency with 45 dB dynamic range, the AD8314 handles a wide signal range. The AD8314 also minimizes board area due to 8-pin microSOIC packaging.

Analog Devices
INFO/CARD 161

Transmitter IC's for dual-band cellular phones

The MAX2360/ MAX2364/ MAX2362 baseband-to-PA are complete dual-band cellular phone transmitter devices by Maxim. They are designed for dual-band, tri-mode and single mode N-CDMA, TDMA, EDGE and W-CDMA cellular phones. The trio are offered in a 48-pin TQFP package.

Maxim
INFO/CARD 162

Flash MCU family offers enhanced design flexibility

Microchip Technology's 28-pin PIC16F879 and 40/44-pin PIC16F871 flash microcontrollers (MCUs), expand the PIC16F87X family of flash devices. With 2K x 14 bits of cost-effective flash memory and 64 bytes of EEPROM data memory, the MCUs have brownout detection, up to 5 MIPS performance at 20 MHz, USART communications capability for peripheral expansion, two 8-bit timers, a 16-bit timer and an operating voltage of 2.0-5.5 volts. The PIC16F870 has a 5-channel 10-bit (± 1 LSB) A/D converter. The PIC16F871 features an 8-channel 10-bit (± 1 LSB) A/D converter and a parallel slave port.

Microchip Technology
INFO/CARD 163

Class C, D and E RF power MOSFET

The ARF 450 is a matched pair of power MOSFETs in a common source

configuration. It is designed for operation in RF power amplifiers up to 120 W. Rated power dissipation is 650W and the unit operates with up to a 150 V supply.

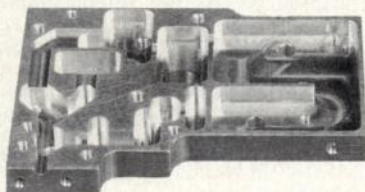
Advanced Power Technology
INFO/CARD 164

RF power transistor for GSM applications

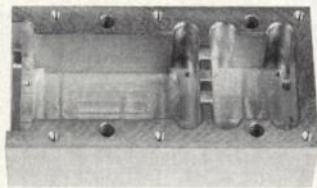
Ericsson Microelectronics has added the PTF 10149 RF power transistor to its portfolio of GSM devices. The device, based on GOLDMOS technology, is designed for use in the 92 to 960 MHz GSM band. The device output power is 70 W, and 16 dB gain. Additionally, efficiency is rated at 50%, and it has a linearity of ± 0.25 across the band. The device operates from 28 VDC with a minimum drain source breakdown voltage of 65 V runs in n-channel enhancement mode has a load mismatch tolerance of 5:1 and IMD3 is -39 dBc at 20 W PEP.

Ericsson
INFO/CARD 165

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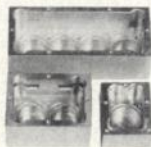


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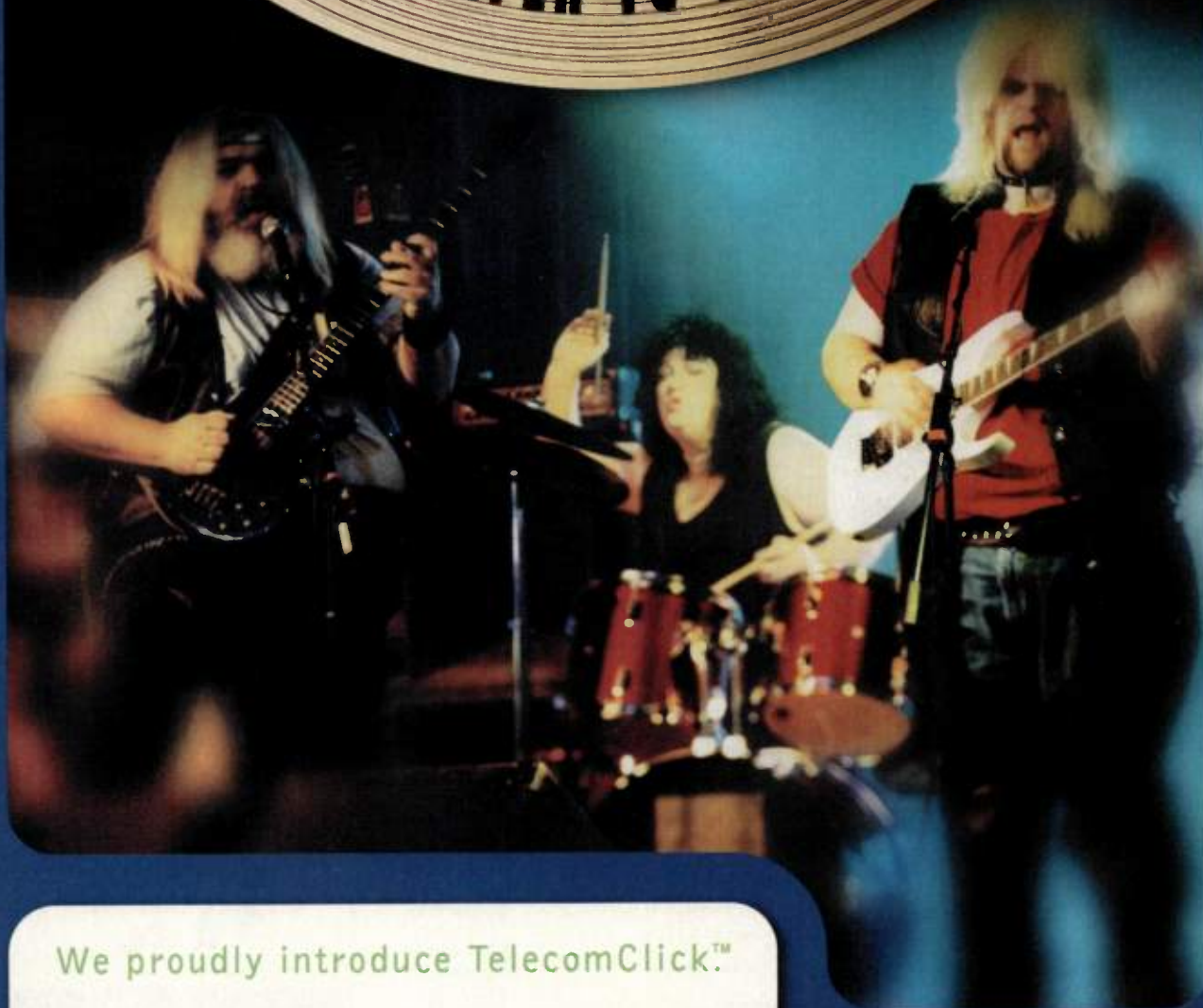
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RF software

Modem, software for CDMA design

MSM 3300 chipset and system software is Qualcomm's first multimedia enabled mobile station modem based on the MSM 3100 chipset architecture. The chipset and system software will enable the design of CDMA handsets and data devices with feature sets and high performance. Higher on-chip integration provides advanced Bluetooth, as well as multimedia features such as Qtunes, moving picture experts group (MPEG-1) Layer 3 (MP3) player software and compact media extension (CMX) musical instrument digital interface (MIDI)-based multimedia software. The package also supports GPS applications with its gpsOne position locations technology in the MSM 3300.

Qualcomm
INFO/CARD 166

Software designed to improve productivity

Xpedion Design Systems' COSSAP System Level Design product family integrates its Golden Gate family of RF simulation and behavioral modeling products. Combining the two products is designed to improve time to market and designer productivity for RF and wireless communication designs. The Golden Gate-COSSAP interface unifies bottom-up and top-down design methodologies for existing 2G and the evolving 3G and Bluetooth communication standards. Combining the power of GoldenGate with COSSAP allows designers to make critical design trade-offs at both the circuit and system level, throughout the wireless communication system development cycle.

Xpedion
INFO/CARD 167

Software suite targets 2G, 3G, Bluetooth designers

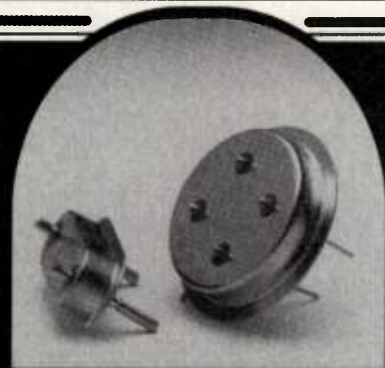
Elanix and Xpedion's integrated software suite has Elanix's system-level design software and Xpedion's golden gate/sim, RF and microwave simulation software. The suite allows designers to immediately see the impact of design changes at any level of abstraction much earlier in the design cycle, reducing development cycle times. The software is targeted to 2G, 3G and Bluetooth product designers.

Elanix
INFO/CARD 168

RF Design Online

For more information on items noted in the software column, check out the *RF Design* Web site www.rfdesign.com editorial links, for direct links to company Web sites.

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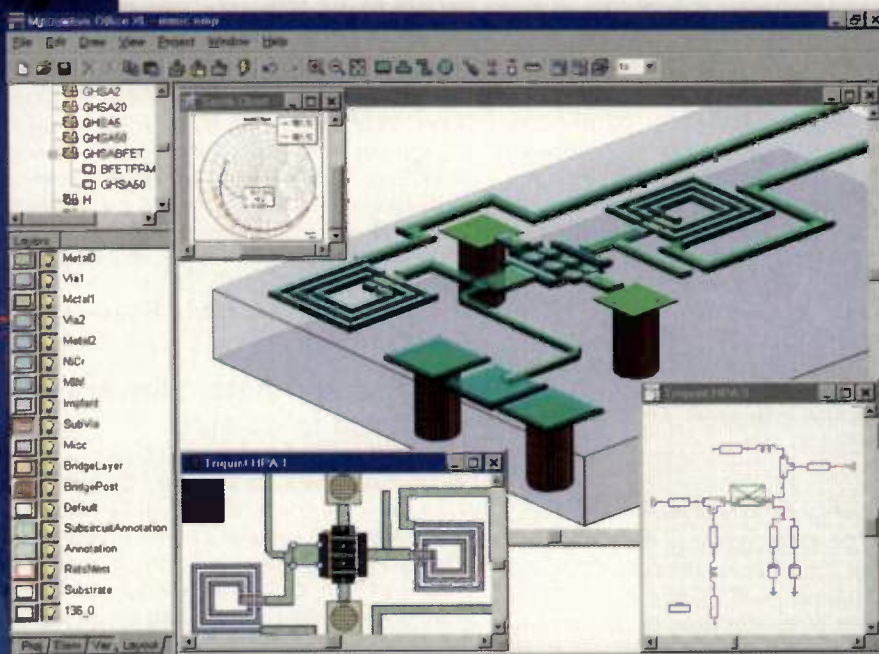
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INFOCARD 76

Guide features control components specifications

Sprague Goodman Electronics' new product selection guide offers specifications for their complete line of frequency control components. This edition includes the new Surfcoil SMT inductors and transformers, and tuning varactors to the range of air, ceramic, glass, mica, plastic, quartz, and sapphire dielectric trimmer capacitors. Specifications are given for the surface mount, inductors, metalized inductors and LC tuners, microwave tuners and tuning tools.

Sprague-Goodman
INFO/CARD 169

Data book, CD-Rom list control products, devices

C-Mac Frequency Products' Crystal Product Data Book 2000 and CD-ROM contain a large selection of the company's frequency control products with detailed specifications of hundreds of standard and custom frequency control devices. Customers can specify and order components from the book and CD-Rom using provided specifications and controlled issue numbers.

C-Mac
INFO/CARD 170

Catalog lists RFID systems, products

Omron offers a 117-page catalog featuring its line of RFID systems including tags, antennas and controllers. The catalog features information about Omron's V600 series electromagnetic RFID system, the V620 microwave RFID system and V700 series electromagnetic inductive system. It also includes a product selection guide to aid in choosing the proper model for the application, a section of complimentary products and reference information.

Omron
INFO/CARD 171

Aluminum capacitors, guidelines in catalog

United Chemi-Con offers its latest catalog of aluminum electrolytic capacitors. At 480 pages, it includes 9,000 different part numbers comprising 74 new or enhanced capacitor series. There are sizes, styles and operating characteristics for most application.

United Chemi-Con
INFO/CARD 172

Catalog offers range of frequency synthesizers

Princeton Electronic Systems' catalog features their low noise VCOs (to -112 dBc/Hz@10 KHz offset) and low noise, small footprint, synthesizers for wireless communication applications. The catalog lists the new release of 5V and 3 V VCOs and a wide range of single, dual and fixed frequency synthesizers.

Princeton Electronic Systems
INFO/CARD 173

Cooled cabinets, blowers featured in catalog

Equipto Electronics offers a catalog with information for electronic system designers who require cabinets that are cooled. The catalog also features a blower and fan selection nomograph to assist designers in evaluating their cooling requirements. Sixteen blowers and eight fan sizes are standard catalog choices, with more than 200 additional sizes available by special order. Louvering, grilling, insulation, heaters and air conditioners are also available. Other options include dust filters, fan guards, adapters for 24" panel widths and honeycomb grills to meet RFI requirements. Visit the company's Web site to request a catalog.

Equipto Electronics
INFO/CARD 174

Book offers tips to tackle CDMA problems

Artech House Publishers' *Signal Processing Applications in CDMA Communications*, by Hui Liu, is a book that details the author's in-depth research of key CDMA signal processing issues and offers solutions to problems such as diversity combining, multiuser detection, channel estimation and carrier synchronization. With a brief CDMA primer, the book features complete signal processing solutions including blind multiuser detection for CDMA systems with short codes, long codes and antenna diversities to meet the problems faced in wideband CDMA detection.

Artech House Publishers
INFO/CARD 175

On The Web

Web site offers products, data sheets

Signal Technology's Olektron Operation's updated Web site includes more than a dozen new products and a complete list of available product data sheets in PDF format. Items offered include new lines of switch combiners and multi-function log amps.

Signal Technology
INFO/CARD 176

Web site provides designers' resource

W.L. Gore & Associates Web site offers an on-line resource to designers facing EMI/RFI shielding problems. The site provides a compilation of technical, product and standards information for beginning and experienced engineers handling EMI. The resource also includes a primer on basic design for electromagnetic interference control that covers key issues and terminology; electrical and mechanical design modules; a discussion of rapid prototyping services; and information on reducing manufacturing cost. Links to related industry sites and current industry events are also on-line.

Gore
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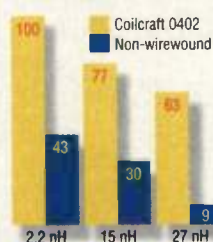


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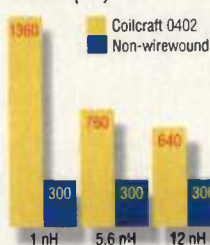


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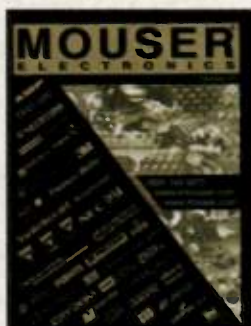
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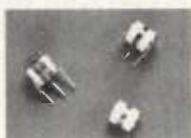
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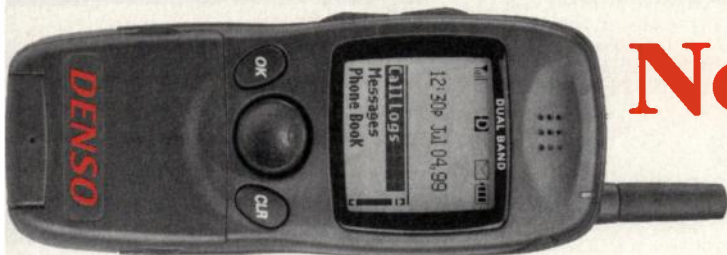
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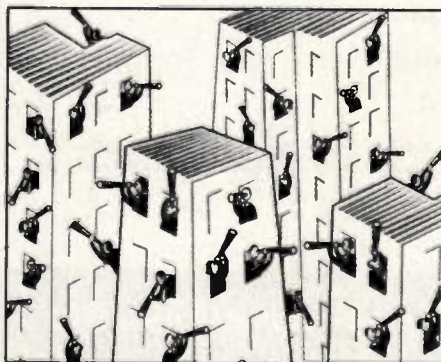
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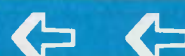
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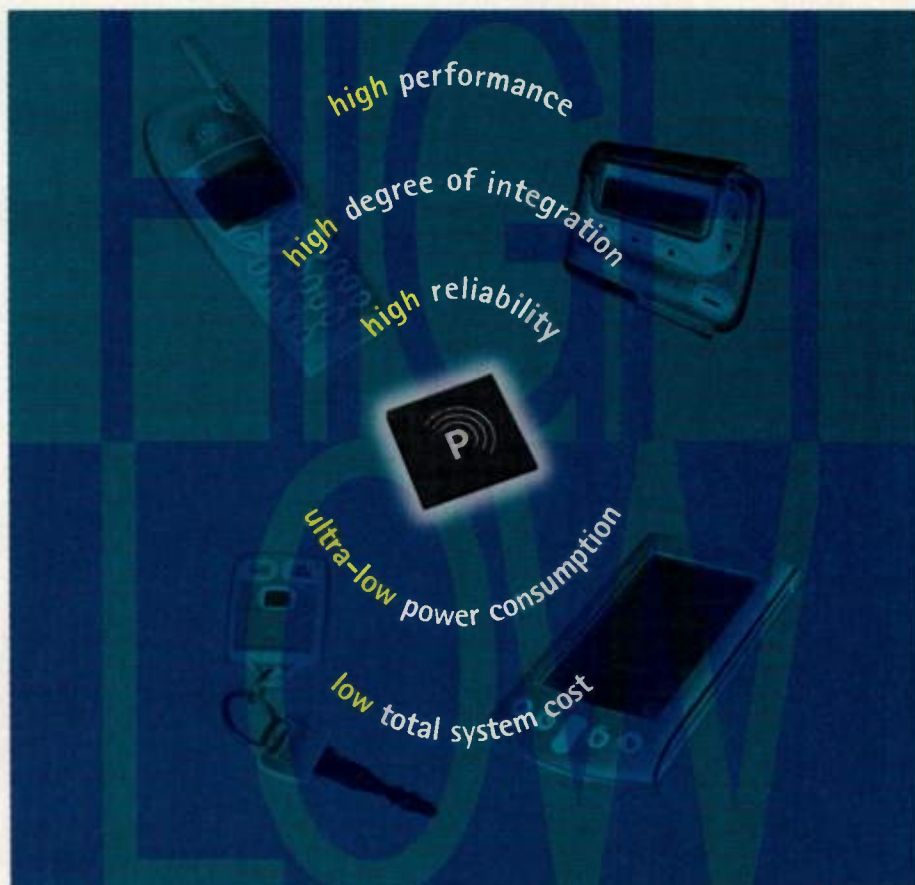
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by Ernest Worthman

I recently came across a bit of news that I find rather interesting. Good ol' Craig McCaw now has a grand scheme to salvage the hundreds of money pits circulating the earth in low orbit.

Well, I'm still smarting from the dumb decision I made to purchase Iridium stock just before the bankruptcy, gambling that Motorola would step up to the plate and make the system fly. But I lost. As we all know, Motorola let Iridium slip into bankruptcy and basically walked away. Of late, there has been some money pumped into Iridium, but only to avoid liquidation deadlines.

They're not the only one. ICO, who hasn't even got any hardware up, is also in bankruptcy and Teledesic isn't healthy either.

From a purely business perspective, I can't really blame Motorola for wanting to walk away, but it isn't that simple.

But then I have a bit of animosity towards them (that goes back 10 odd years) simply because they took an arrogant approach to the Iridium project from the start. They were seriously thinking that the public was going to buy \$3,000 phones and pay up to \$7 per minute to be able to communicate from the top of Mount Everest, but not from an underground parking structure (when it worked at all). I have to wonder what they were thinking.

Well, perhaps Motorola isn't going to just walk away. The latest scoop is that the court overlooking the bankruptcy is going to give Motorola an alternative. Either they come up with a credible buyer and a solid plan (read Craig McCaw), or they will be forced to bring the satellites out of orbit.

Now, I have been following the adventures of Craig McCaw since his vision of a nationwide ESMR network came upon the scene about 10 years

The Hindenburg of the 21st century

ago (which, of course, never came about). Then, I followed his grand plan to create Nextel (which may yet, someday, become profitable). Then he bought ICO. Now he has his eyes on Teledesic, too. He is on a mission to buy these systems for pennies on the dollar and merge Iridium, ICO and perhaps Teledesic into the next super ISP (or maybe just eliminate the competition).

Challenging, but Craig has his work cut out for him (and I still can't understand why everyone continues to throw money at him).

Actually, the idea sounds great on paper. There is a real mess out there with ISPs. Modem connections are dinosaurs. Long ago, I gave up trying to download anything more than a few kB of e-mail using a dial-up connection. DSL comes in a number of flavors but to get any real speed, you gotta pay. Cable is so load sensitive that, I suspect, once they get any real numbers on line, cable modem constipation is only a click away. Plus, everyone's got their own proprietary hardware and software. And, realistically, neither cable or DSL is widely available yet. Also, projected penetration numbers are lower than expected to date and hidden costs can be surprising.

So, in theory, if Craig McCaw could pull this off, I'd be the first in line. I think that these LEO satellites are a golden goose for this application (if the price is right). Even though these LEO satellites have a weak spot when it comes to in-building penetration, that issue is easily solved in a couple of ways.

First, most residences aren't buried in steel and concrete, and they aren't mobile. I suspect most homes will be able to receive a direct signal from a LEO ISP satellite without much positioning. Second, if the signal is too weak for direct reception...well, the

DBS systems have already solved the one. Direct TV/PC simply puts a one meter dish on the building (single or multi-unit) and distributes the signal.

The interface issue is simple as well. All you do is stall a PCI card (ISA better be dead by then) in your computer with a connector to which you connect either an antenna, or a cable.

The one "gotcha" that I worry about is the lack of reliability of the constellations. But data is much more forgiving than voice, and much more error tolerant.

On the other hand, if McCaw backers finally sense that whatever he touches turns into debt, well, let's go for plan B.

It turns out that plan B goes something like this: Instead of forcing Motorola to plummet the satellites to earth, let's round up a bunch of the latest Internet-related IPO instant millionaires and give them a shot at some adrenaline pumping action. Let Motorola buy one of those Russian MIGs for next to nothing. Then they can offer to rent this plane to these money-to-burn guys. Next, for, say \$5 million per shot, these guys get to go up and try to blast one of the satellites out of the sky on its way to self-emulation.

Not a bad idea if you ask me. I would give 66 (plus spares) young bored millionaires something really exciting to talk about. It would also net Motorola about \$66 million, and maybe some of us dumb investors will get a few of our investment bucks back. The rest could be used by Motorola to pay "what was I thinking?" fine.

Oh, the insanity...



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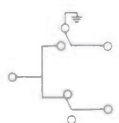
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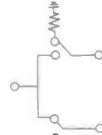
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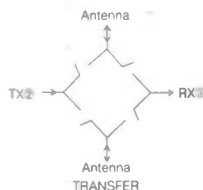
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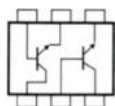
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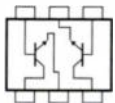
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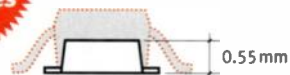
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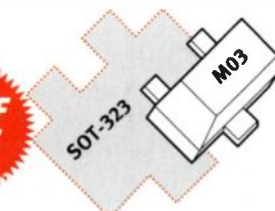
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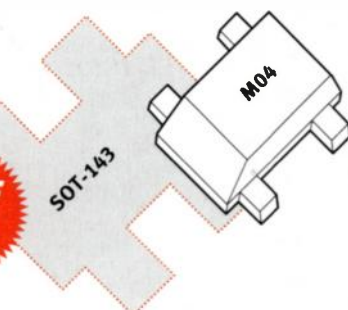


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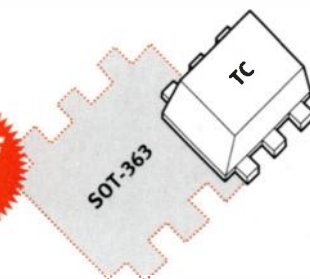
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