

The Aerovox Hi-Farad Condenser

Operates efficiently over a wide range of temperatures

EXPERIMENTS made to determine the effects of wide variations of temperatures on our Hi-Farad Condensers and those of competitive makes of wet electroly of the property of Hi-Farad DRY Electrolytic condensers in this regard.

Best Results Obtained When Operated in Cool Section of Receiver

As is the case with wax paper concleasers, it is essential that all types of electrolytic condensers be placed in the coolest section of the receiver or amplifier assembly. If the temperature of the air surrounding any electrolytic condenser is raised to 120 degrees Fahrenheit (approximately 49 degrees Centigrade), no harm or appreciable change in characteristics will occur.

Best results are obtained with the Aerovox Hi-Farad Condenser when a temperature of 120 degrees F. is not exceeded, in the space surrounding the condenser, when the condenser is oper-500 votts peak. On lower voltages, such as 475 volts peak, a temperature of 120 degrees F. is not excessive. At 450 volts peak, a temperature of 120 degrees may be used and at 400 volts peak, a temperature of 120 degrees F. will not cause any excessive degrees F. will not cause any excessive leakage current to flow.

When subjected to temperatures as high as 170 degrees F. (approximately 77 C.) which is far in excess of the



Aerovox Triple-8Mfd. Dry Electrolytic Condenser 500 Volts D. C. Peak

temperatures encountered in actual operation, the leakage current of electrolytic condensers will increase.

In wet electrolytic condensers which employ an ageous solution, loss of solution, due to evaporation results in loss of capacity and shortened lie. Enough solution may be lost under high temperature conditions to render the condenser inoperative in a comparatively short time.

The non-ageous (non-water) composition and special ingredients used in Hi-Farad condensers provide stable characteristics which prevent any possibility of evaporation under operating conditions. Aerovox Hi-Farad Condensers Will Not Freeze

The electrolyte used in wet electrolytic condensers will freeze and render the condenser inoperative at temperatures ranging from 21 to 29 degrees R, temperatures normally met with in winter transportation when shipping of radio receivers and equipment is at its height, or in normal outdoor operation in cold weather.

Martows Hi-Parad DRY Electrolytic Condensers are still operative at temperatures as low as 40 degrees below zero F. The fact that they remain operative at such low temperatures makes it possible to use them in receivers, amplifiers, public address systems and sound recording apparatus systems and sound recording apparatus in cold or unheated places during the winter months.

The only change in characteristics of Hi-Farad condensers at extremely low temperatures is a drop in capacity to approximately 50% of their normal rating when operated at temperatures as low as 40 degrees below zero F. Arts. Hi-Parad on denser to equire only a short exposure to normal room temperatures to regain their full, normal capacity ratings.

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THIS BOOK GIVES THE LATEST AND MOST COMPLETE INFORMATION ON ELECTROLYTIC CONDENSERS

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If you want to know whether leakage is a reliable indicator of lifering efficiency; what electrolyte characteristics are necessary for efficient electrolytic condenser action; how the filtering efficiency of various types of electrolytic condenser compares with paper condenser compares with paper condenser you will find the information in this book. A copy is yours for the asking.



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organ of the Aerovox Wireless Corporation. It is published to bring to the Radio Experimenter and Engineer authoritative, first hand information on condensers and resistances for radio work.

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The Essential Factors in the Design of Receiver and Amplifier Systems

Part IV*

By the Engineering Department, Aerovox Wireless Corporation

A TRANSFORMER coupled amplifer is used when only low plate voltages are available and where it is desired to use but few tubes. From a single high-mu tube used in a resistance or impedance coupled stage and its associated input and output circuits a gain of about 20 can be obtained. From a single tube and

associated input and output circuits again of about 20 can be obtained. From a single tube and

NOTE: The first, second and third instalments of this article appeared in Vel. 3, Nos. 5, 6

Raders whose subscription begins with this issue. (December) and with the there is no charge or obligation. Merely write to a charge or obligation. Merely write to pretain. 70 Weshingon St. Brookship, Nr. V.

Fig. 10

associated input and output transformers a gain of from 60 to 100 can be obtained. As in the case of the resistance coupled amplifier, an analysis of the frequency response must be considered, from the standpoint first of low frequencies and second of high frequencies. Fig. 9 is the fundamental diagram of a single stage of transformer coupled audio amplification. Fig. 10 is the approximate equivalent circuit at low frequencies. In the latter circuit Mu Eg is the signal voltage in the plate circuit, Rp is the a. c. plate resistance of the tube, La is the leakage reactance of the transformer, L is

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the inductance of the primary of can be neglected. Essentially we back, there was a pronounced the transformer and C is the input capacity of V2 together with the distributed capacity of the transformer windings.

> TABLE 2. Percentage of total Voltage Across L

At low frequencies the reactance of C is very large in comparison with the reactance of L and therefore at low frequencies the available signal voltage divides between Rp and L. The percentage of the total voltage that appears across L depends upon the ratio of the reactance of L (XI) to Rp and varies as indicated in column 2 of Table 2. Let us apply the same criteria to the performance of this transformer coupled circuit as were used in discussing the resistance coupled amplifier, and state that the voltage amplification at 50 cycles should not fall to less than 90 percent. From Table 2, we find that the reactance of L(XI) should therefore be approximately twice as great as Rp at 50 cycles to maintain a voltage amplification of 90 percent. If the tube is a type 327 Rp will be approximately 10,000 ohms and therefore the reactance of L must be 20,000 ohms. The reactance of a coil is determined as follows:

X1 = 6.28 fL

where

X1 Rp

4.0

X1 is the reactance in ohms f is the frequency in cycles per second

L is the inductance in henries. In this case X1 must be 20,000 ohms when f is 50 cycles. Therefore L must be

20.000 6.28×50

= 66.6 henries Therefore a transformer which is to give 90 percent response at 50 cycles must have a primary inductance of about 67 henries. If the inductance of the primary is smaller the response falls off at low frequencies.

At high frequencies the reactance of L is very large in comparison with that of C and therefore the voltage divides between Rp, La and C, and L

then have a circuit consisting of peak in the curve around the fre-Rp. La and C in series. At a certain frequency La and C will produce a resonant circuit, the overall impedance of the circuit will thereby be decreased, and more current will flow, tending to increase the voltage across C, which is the voltage applied to the following tube. However the voltage across C is inversely proportional to the frequency and this helps to prevent an undue rise. In some transformers, especially those made a few years capacity.

quency at which La and C were resonant. The point at which resonance occurs should be made high in frequency, which means that the magnetic coupling between the windings must be practically complete

To obtain good frequency response characteristics in a transformer coupled amplifier therefore it is necessary to use transformers having a high primary inductance, low leakage and low distributed

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Page 2



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