Super-MWDX-5 Phasing Unit Mark Connelly - WATION - 07 FEB 1993

The Super-MWDX-5 is a phasing unit with enhanced capabilities over the MWDX-5 described in my article of OCT 1991 (available as NRC / IRCA reprints). Added features include transformers for use as part of a noise-reducing antenna system, additional controls to give better nulling ability, and a jack for a "spare antenna" usable for broadband monitoring and quick parallel checks / scanning during DXpeditions. A metal box is used for superior shielding and mechanical ruggedness. A new hardware scheme was developed to "float" the tuning capacitors from chassis ground. This method should be of value to builders of balanced loops that also require a tuning capacitor isolated from chassis ground. The Super-MWDX-5 may be used for two-wire phasing or loop-vs.-wire phasing. In either case, nulls may be obtained that differ in directivity from those achievable with a standard loop; the result is potentially different DX from the loggings acquired with a loop alone. Nulling midwest "clears" to log Europeans at an East Coast US/Canada QTH is definitely a job better suited to phasing than looping. The MWDX-5 article gives useful background information on phasing as well as a list of other articles on the subject. The Super-MWDX-5 uses the BBA-CI broadband amplifier which has good strong-signal handling performance; the BBA-B used on MWDX-4 style phasers could be substituted in rural areas for reduced battery drain.

Organization of article

Table 1: Controls and Input / Output Connectors

Table 2: S1 Bandswitch Settings Chart

text: Operating the Super-MWDX-5

two-wire phasing loop vs. wire phasing

output amplification

New features - notes on noise reducing antenna systems, spare antenna input

Building the Super-MWDX-5

Table 3: hole-drilling list

Table 4: "upper level" parts list

Table 5: (A1) BBA-C1 broadband amplifier card parts list

Table 6: small hardware parts list

Table 7: wiring / component connections

Table 8: control orientation conventions

Figure 1: Super-MWDX-5 input section schematic

Figure 2: Super-MWDX-5 bandswitch / combining section schematic

Figure 3: Super-MWDX-5 output section schematic

Figure 4: (M1) BBA-C1 broadband amplifier card schematic

Figure 5: (M1) BBA-C1 broadband amplifier card assembly

Figure 6: Super-MWDX-5 switch details

Figure 7: C1, C2 mounting details

Figure 8: Options for the Super-MWDX-5

Table 1: Super-MWDX-5 Controls and Input / Output Connectors

Con	tro	IS.	

location	designation	operational description	
left side	S3	Ground Mode switch	
top	CI	Line I tuning capacitor	
top	C2	Line 2 tuning capacitor	
	RI	Line 1 level pot	
top	R2	Line 2 level pot	
	R3	Null vernier (Q-balance) po	ot
top	SI	Bandswitch	
top	S2	Function switch	
top		Input Coupling (length) sw	itch
top	S4		iicii
top	S5 S6	Output switch Wire / Loop switch (Line 2)	input)
Input / Output	t Connectors		
location	designation	operational description	connector type
		Line I wire input	banana jack
left side	11	Line 2 wire input	banana jack
left side	J2		banana jack
left side	13	earth ground input I	banana jack
left side	J4	earth ground input 2	BNC jack
left side	18	Loop input	BNC jack
right side	J5	RF output	
right side	16	B+ in	phono jack
right side	J7	9V battery holder	Keystone 1290
right side	19	spare antenna input	BNC jack

Table 2: S1 Bandswitch Settings Chart

Ranges are usually a bit greater than those shown. These ballpark values are for 50-m. / 164-ft. wires and the S4 coupling switch set to the "Normal" position. Other positions and wires may alter ranges somewhat.

The Super-MWDX-5 family of phasing units has frequency coverage characteristics as noted in the following table:

* MODEL: standard Super-MWDX-5 * (LWBC: 130-285; MW: 430-1800)

SI	SI Knob	Min.	Max.		L ["Tap"		
Pos.	Pointer "o'clock"	Freq. kHz	Freq. kHz	L#	uH	Mouser Part #	
1	9:30	130	180	L1,L13 L7,L19	4700 1000	434-1120-473K 43LR103]	
2	10:30	180	285	L2,L14 L8,L20	2200 470	434-1120-223K 43LR474]	
3	11:30	430	630	L3,L15 L9,L21	470 100	43LR474 43LR104]	
4	12:30	630	880	L4,L16 L10,L22	220 47	43LR224 43LR475]	
5	1:30	880	1260	L5,L17 L11,L23	100 22	43LR104 43LR225]	;
,6	2:30	1260	,1800	L6,L18 L12,L24	47 10	43LR475 43LR105]	

SI	S1 Knob	Min.	Max.		L ["Tap"	
os.	Pointer	Freq.	Freq.		ductor Val	
#	"o'clock"	kHz	kHz	L#	uH	Mouser Part #
-	0.20	145	230	LI,LI3	3900	434-1120-3931
1	9:30	143	230	L7,L19	820	43LR824]
2	10:30	230	375	L2,L14	1500	434-1120-1531
-	*		•	L8,L20	330	43LR334]
3	11:30	375	620	L3,L15	560	43LR564
				L9,L21	120	43LR124]
4	12:30	620	1050	L4,L16	220	43LR224
• .				L10,L22	47	43LR475]
5	1:30	1050	1600	L5,L17	82	43LR825
•	•		•	LII,L23	18	43LR185]
6	2:30	1600	2700	L6,L18	33	43LR335
				L12,L24	6.8	43LR686]
MOD	EL: Super-MWI	X-5B * (exte	ended LW: 90			
SI	SI Knob	Min.	Max.	"Main'	'L ["Tap"	L]
os.	Pointer	Freq.	Freq.		nductor Va	
#	"o'clock"	kHz	kHz	L#	uH	Mouser Part #
	0.20		120	11112	10000	424 1422 45
!	9:30	90	130	L1,L13	10000	434-1120-1041
2	10:30	130	180	L7,L19 L2,L14	2200 4700	434-1120-2231
-	10.30		100	L8,L20	1000	
3 .	11:30	180	285	L3,L15	2200	43LR103] 434-1120-2231
			-	L9,L21	470	43LR474]
4	12:30	285	430	L4,L16	1000	43LR103
	•			L10,L22	220	43LR224]
5	1:30	430	630	L5,L17	470	43LR474
			* .	L11,L23	100	43LR104]
6	2:30	630	880	L6,L18	220	43LR224
				L12,L24	47	43LR475]
MOD	EL: Super-MWD	X-5C * (MW	, tropical: 37:	5-6500)		
SI	S1 Knob	Min.	Max.	"Main"	L ["Tap"	L)
os.	Pointer	Freq.	Freq.	Tank I	nductor Va	lues
#	"o'clock"	kHz	kHz	L#	uH	Mouser Part #
	==:==	-	*****		====,=	**********
1	9:30	375	620	LI,LI3	560	43LR564
-				L7,L19	120	43LR124]
2	10:30	620	1050	L2,L14	220	43LR224
3	11:30	1050	1600	L8,L20	47	43LR475]
	11:30	1030	1000	L3,L15	82 18	43LR825
4	12:30	1600	2700	L9,L21 L4,L16	33	43LR185] 43LR335
:	"	1000	2700	L10,L22	6.8	43LR686]
5	1:30	2700	4000	L5_L17	12	43LR125
	*			L11,L23	2.7	43LR276]
6	2:30	4000	6500	L6,L18	4.7	43LR476
				L12,L24	1	43LR106]
	EL: Super-MWD	X-5D * (anti-	ended tropical		-12500)	
SI	SI Knob	Min.	Max.		L ["Tap"	11
os.	Pointer	Freq.	Freq.		ductor Val	
#	"o'clock"	kHz	kHz	L#	uH	Mouser Part #
=	==;==					=========
1	9:30	1260	1800	LI,LI3	47	43LR475
-				L7,L19	10 .	43LR105]
2	10:30	1800	2800	L2,L14	22	43LR225
	•			L8,L20	4.7	43LR476]
3	11:30	2800	4000	L3_L15	10	43LR105
-	•		•	L9,L21	2.2	43LR226]
4	12:30	4000	6500	L4.L16	4.7	43LR476
				L10,L22	1	43LR106]
5	1:30	6500	8800			

* MODEL: Super-MWDX-5E * (reduced coupling efficiency) (90-8800)

8800

2:30

Note: For this configuration, S1 is a 2-pole, 12-position switch. The inductors on the S1A section (L1 through L12) are switched across the C1 stator to R1 arm path. The arm of R1 is tied to a 68 ohm resistor to GND rather than to an S1C "tap L" section. The inductors on the S1B section (L13 through L24) are switched across the C2 stator to S6 "Wire" path. The S6 "Wire" pin is tied to a 68 ohm resistor to GND rather than to an S1D "tap L" section. Output levels with Super-MWDX-5E are reduced from thos achievable with models utilizing the S1C/S1D "tap L" architecture.

12500

LIIL23

L6,L18

L12,L24

0.47

0.22

43LR477

43LR106

43LR227

SI Knob	Min.	Max.			
		Freq.	Tank Ir	iductor Va	lues
"o'clock"	kHz	kHz	L#	uH	Mouser Part #
==;==					
6:00	90	130	LIL13	10000	434-1120-104K
7:00	130	180	L2.L14	4700	434-1120-473K
8:00	180	285			434-1120-223K
9:00	285	430	LAL16		43LR103
10:00	430	630			43LR474
11:00	630	880			43LR224
12:00	880	1260			43LR104
1:00	1260	1800			43LR475
2:00	1800		100000000000000000000000000000000000000		
3:00					43LR225
					43LR105
					43LR476
3:00	6500	8800	L12,L24	2.2	43LR226
	Pointer "o'clock" ==:== 6:00 7:00 8:00 9:00 10:00 11:00 12:00 1:00 2:00	Pointer Freq. "o'clock" kHz	Pointer Freq. Freq. Freq.	Pointer Freq. Freq. Tank Ir "o'clock" kHz kHz L# 6:00 90 130 L1_L13 7:00 130 180 L2_L14 8:00 180 285 L3_L15 9:00 285 430 L4_L16 10:00 430 630 L5_L17 11:00 630 880 L6_L18 12:00 880 1260 L7_L19 1:00 1260 1800 L8_L20 2:00 1800 2800 L9_L21 3:00 2800 4000 L10_L22 4:00 4000 6500 L11_L23	Pointer Freq. kHz kHz L# uH 6:00 90 130 L1,L13 10000 7:00 130 180 L2,L14 4700 8:00 180 285 L3,L15 2200 9:00 285 430 L4,L16 1000 11:00 430 630 L5,L17 470 11:00 630 880 L6,L18 220 12:00 880 1260 L7,L19 100 1:00 1260 1800 L8,L20 47 2:00 1800 2800 L9,L21 22 3:00 2800 4000 L10,L22 10 4:00 4000 6500 L11,L23 4.7

Operating the Super-MWDX-5

Figures 1 through 3 are the schematics of the Super-MWDX-5. Please refer to them during the discussion of phasing procedure. Use wires at least 15m./50 ft. in length. There should be some angular or distance separation between the wires for optimum results in two-wire applications. See Tables 2 and 8 for physical positioning of switches.

*********************************** *** Super-MWDX-5 Two Wire Phasing Procedure ***

1.0 Phasing Steps (2-wire)

(COMMENTS) The best method of nulling when the two antennas are delivering comparable signal levels (e. g. within 6 dB) differs from that to be used when there is a considerable strength difference (e. g. one of the Beverages or longwires is already throwing a partial null on the dominant; or, one of the wires is considerably longer than the other and, therefore, consistently provides more signal). Unlike previous phasers, the Super-MWDX-5 provides both Q-skewing (R3) and non-Q-skewing (R1, R2) level adjustment methods to handle a wide variety of nulling situations. Certain nulls may be achieved best by a blend of both methods; as operator experience with the unit increases, nulling judgment improves and getting to the desired DX becomes a considerably faster procedure. Nulling procedures sound complicated at first, but are quickly executed once learned. The user should practice during non-skip daylight conditions on "graveyard" and regional channels having discernable subdominants to get familiar with operation of the controls before attempting night-time nulls of unsteady signals. As with a loop, solid nulls of skip stations above 1 MHz in the 50 to 500 mile range are difficult because of the rapid changes in vertical (and sometimes horizontal) arrival angles inherent when dealing with high-angle skip. Such nulls are better when using phased Beverages than when using a loop or phased shorter wires.

1.1 ** INITIALIZATION OF SWITCHES **

Set frequency-range switch S1 to the correct range for the frequency of operation (see Table 2). Set S3 to Common (unless using an antenna system with noise-reduction transformers). Set Input Coupling switch S4 to Normal (or to a different position, depending on experimentation that leads to having determined the best position for a given antenna system). Set S5 Output switch to Phaser / Unamplified. Set S6 to Wire. S2 will be set subsequently.

1.2 ** INITIALIZATION OF POTENTIOMETERS **

Set level pots R1 (Line 1) and R2 (Line 2) to fully counterclockwise (minimum attenuation). R3 settings will be made subsequently.

1.3 ** CONNECTIONS **

Connect longwire #1 to J1 and connect longwire #2 to J2. coaxial cable is used (as in a noisereduction transformers scheme), BNC or SO-239 to dual-banana-plugs adapters should be sed to connect Line I to J1 (center) / J3 (shield) and Line 2 o J2 (center) to J4 (shield). Otherwise, an available ground ay be connected to J3 and J4. Connect phaser's output (J5), via coaxial cable, to the input of the receiver to be used, or to a tunable preamp, between phaser and receiver. Connect a 9V battery to the J7 battery holder and plug P1 into J6, or connect the plug of an 8V to 16V DC power source to J6.

1.4 ** PEAK LINE I **

S2 on Line 1 / R3 at center) OR (S2 on Null-a / R3 fully CCW) Tune Line 1 by peaking desiredfrequency signal strength with C1. At this time, leave C1 at its peaked-signal position.

NOTE THE SIGNAL STRENGTH (observe S-meter, if available, or note audible level). [At this time, other positions of Input Coupling switch S4 may be tried to see if greater signal transfer is possible. Re-adjustment of C1, and possibly S1, may be needed to re-establish a peaked condition. In any event, the peak should have reasonable Q (be well defined) and C1 should not be set too close to fully CW or fully CCW. In most cases, \$4 on Normal will provide good enough signal levels and reasonably sharp tuning not overly affected by differences in length between the two wires to be phased.]

1.5 ** PEAK LINE 2 **

(S2 on Line 2 / R3 at center) OR (S2 on Null-a & R3 fully CW) Tune Line 2 by peaking the desired-frequency signal strength with C2. At this time, leave C2 at its peaked-signal position

NOTE THE SIGNAL STRENGTH (observe S-meter, if available, or note audible level).

1.6 ** DETERMINE POTENTIOMETER TO ADJUST **

If the dominant-station signal level noted when peaking Line 1 with C1 (step 1.4) is comparable (within 6 dB on meter, or not audibly different) to the strength noted when peaking Line 2 with C2 (step 1.5):

Adjust R3 to search for a null while trying the Null-a and Null-b positions of S2. If a distinct null is found, leave S2 and R3 at the best null-producing settings and proceed to step 1.7a. If a null is not found: Switch S3 between Line 1 and Line 2 while adjusting R3 to make the observed signals equal on the

S-meter (or not audibly different). R3 should, at this point, be close to its center position. Then, proceed to step 1.7a. If the dominant-station signal level noted when peaking Line 1 with C1 (step 1.4) is noticeably

greater than the strength noted when peaking Line 2 with C2 (step 1.5): Set R3 to its center position. Adjust R1 to search for a null while trying the Null-a and Null-b positions of S2. If a distinct null is found, leave S2 and R1 at the best null-producing settings and proceed

to step 1.7b. If a null is not found: Switch S3 between Line 1 and Line 2 while adjusting R1 to make the observed signals equal on the S-meter (or not audibly different). Then, proceed to step 1.7b.

If the dominant-station signal level noted when peaking Line 1 with C1 (step 1.4) is noticeably lower

than the strength noted when peaking Line 2 with C2 (step 1.5): Set R3 to its center position. Adjust R2 to search for a null while trying the Null-a and Null-b positions of S2. If a distinct null is found, leave S2 and R2 at the best null-producing settings and proceed

to step 1.7c. If a null is not found: Switch S3 between Line 1 and Line 2 while adjusting R2 to make the observed signals equal on the S-meter (or not audibly different). Then, proceed to step 1.7c.

1.7 ** CAPACITOR / POTENTIOMETER INTERACTIVE ADJUSTMENTS FOR NULL ** Perform procedure 1.7a, 1.7b, or 1.7c as determined by step 1.6.

1.7a (Prior adjustment: R3)

If R3 is at center position, or CCW from center: Set S2 to Null-a. Adjust C1 to improve the null. If the null isn't well-defined or CI is near the CW or CCW end of its range: Set S2 to Null-b and re-adjust CI for the null. Interactively adjust R3 and CI to get the best available null with these controls.

If R3 is CW from center: Set S2 to Null-a. Adjust C2 to improve the null. If the null isn't welldefined or C2 is near the CW or CCW end of its range: Set S2 to Null-b and re-adjust C2 for the null. Interactively adjust R3 and C2 to get the best available null with these controls.

1.7b (Prior adjustment: R1 - e. g. R1 is not fully CCW)

Set S2 to Null-a. Adjust C2 to improve the null. If the null isn't well-defined or C2 is near the CW or CCW end of its range: Set S2 to Null-b and re-adjust C2 for the null. Interactively adjust R1 and C2 to get the best available null with these controls.

1.7c (Prior adjustment: R2 - e. g. R2 is not fully CCW)

Set S2 to Null-a. Adjust C1 to improve the null. If the null isn't well-defined or C1 is near the CW or CCW end of its range: Set S2 to Null-b and re-adjust C1 for the null. Interactively adjust R2 and C1 to get the best available null with these controls.

1.8 ** FINAL TOUCH UP TO GET MAXIMUM NULL **

Do the final null "touch-up" with an interactive adjustment of C1, C2, and R3.

*** Super-MWDX-5 Loop vs. Wire Phasing Procedure ***

2.0 Phasing Steps (Loop vs. Wire)

NOTES: The loop should be equipped with a Q-spoiling resistor of approximately 22K across its parallel-tuned LC tank. A 50K potentiometer (initially set to center) might be substituted; it can provide an added control over nulling if desired. The pot or fixed resistor should be easily removable (switch or clips) to facilitate stand-alone (high-O) loop usage.

A loop used in a phasing application is usually oriented for best directivity toward desired DX signals, whether or not that position reduces the dominant. Sometimes orienting the loop for MAXIMUM dominant signal pick-up, or for dominant level equal to that from the wire, can actually help nulling.

2.1 ** INITIALIZATION OF SWITCHES **

Set frequency-range switch S1 to the correct range for the frequency of operation (see Table 2). Set S2 Function switch to Line 1; set S3 to Common (unless using an antenna system with noise-reduction transformers). Set Input Coupling switch S4 to Normal (or to a different position, depending on experimentation that leads to having determined the best position for the wire being used). Set S5 Output switch to Phaser / Unamplified, and set S6 to Loop.

2.2 ** INITIALIZATION OF POTENTIOMETERS **

Set level pots R1 (Line 1) and R2 (Line 2) to fully counterclockwise (minimum attenuation). Set Null Vernier (Q-Balance) pot R3 to center position.

2.3 ** CONNECTIONS **

Connect longwire #1 to J1 and connect the loop (coax.) to J8. If coaxial cable is used on Line 1, a BNC or SO-239 to dual-banana-plugs adapter should be used to connect to J1 (center) / J3 (shield). Earth ground may be connected to J4. Connect the phaser's output (J5), via coaxial cable, to the input of the receiver to be used, or to a tunable preamp, between phaser and receiver. Connect a 9V battery to the J7 battery holder and plug P1 into J6, or connect the plug of an 8V to 15V DC power source to J6. Connect the loop to its power source.

2.4 ** PEAK LINE | **

Tune Line I by peaking desired-frequency signal strength with C1. At this time, leave C1 at its peaked-signal position.

[At this time, other positions of Input Coupling switch S4 may be tried to see if greater signal transfer is possible. Re-adjustment of C1, and possibly S1, may be needed to re-establish a peaked condition. In any event, the peak should have reasonable Q (be well defined) and C1 should not be set too close to fully CW or fully CCW. In most cases, S4 on Normal will provide good enough signal levels and reasonably sharp tuning.}

2.5 ** PEAK LINE 2 **

Set S2 Function switch to Line 2. Tune Line 2 by peaking the desired-frequency signal strength with the loop's tuning capacitor. Leave this capacitor at its peaked-signal position

2.6 ** DETERMINE LINE HAVING STRONGER DOMINANT-SIGNAL LEVEL ** Note the difference in the strength of the dominant signal to be nulled as you switch S2 between Line I and Line 2.

2.7 ** INITIATE NULL **

The potentiometer that will be adjusted initially will be that corresponding to the antenna line having the stronger peaked level (from step 2.6): adjust R1 if Line 1 is stronger; R2 if Line 2 is stronger. Set S2 to Null-a. Adjust the pot determined above (R1 or R2) to search for a null of the dominant. Try this again with S2 set to Null-b. Leave S2 on the position yielding the better-defined null.

If a well-defined null was not obtained; set the pot of the stronger line such that signal level of the dominant is the same when S2 is switched from Line 1 to Line 2. Set S2 to the position (Null-a or Null-b) having the lower level of dominant signal / greater evidence of subdominant signals.

Adjust the tuning capacitor (C1 or the loop tuning capacitor) of the line OPPOSITE of that whose pot was adjusted. Adjust this capacitor for best nulling of the dominant. If the null is not easily obtained or tends to occur at the end of the capacitor's adjustment range; set S2 to the other null position (e. g. Nullb if you had started on Null-a). In rare cases, better results may be obtained by re-peaking the capacitor (e. g. go back to S2 on Line I if C1 was just adjusted and re-adjust C1 for a peak), and then adjusting the capacitor of the SAME line as the pot that was offset from its fully-counterclockwise position. Again, this adjustment should be tried with \$2 on Null-a and on Null-b to see which position results in the better null and in the adjusted tuning capacitor being closer to the center of its mechanical range at null.

2.8 ** COMPLETE THE NULL **

Once as much nulling as possible has been obtained by alternately adjusting the pot (R1 or R2) and tuning capacitor (the loop tuning capacitor or C1) determined by Step 2.7; do the final null "touch-up" with an interactive adjustment of C1, the loop tuning capacitor, and R3. Slight physical re-positioning of the loop may also help to finalize the null. If a 50K pot (initially set to center, ~25K) had been installed across the loop coil (instead of the approximately- 22K fixed resistor), it may also be touched up for null completion.

3.0 *** Output Amplification ***

3.1 If more gain is required after nulling, set \$5 to Phaser / Amplified. Occasionally a slight touchup of the pots and tuning capacitors might be required to get the best null. This generally occurs only with portable receivers that leak some pickup from their internal ferrite rod or whip antennas.

Besides the enhanced controllability of nulls mentioned in the above nulling procedures, Super-MWDX-5 affords two other critical improvements over its predecessors:

Compatibility with noise-reducing antenna systems

If Input Coupling switch S4 is set to the Noise-Reduction mode and Ground Mode switch S3 is set to the Float position, the phasing unit may be interfaced correctly with coaxial inputs from low noise antenna systems consisting of a wire antenna and a "field site" earth ground fed to the primary of a (field site) stepdown transformer in the 4:1 to 12:1 range; either a Mini-Circuits T9-1-X65 or Nick Hall-Patch's homebrew version consisting of an Amidon FT50-43 core with 35 turns primary / 11 turns secondary will work well. The lower impedance output of this field-site transformer is paralleled with 270 to 330 ohms;

one secondary lead goes to the shield of the coaxial cable going to the operator's "shack" and the other secondary lead goes to the center conductor of this coaxial cable through a small series resistor in the 5 to 12 ohin range. The resistors form a low-loss matching pad to reduce the degree of mismatch. Excessive mismatch can compromise the shielding effectiveness of the coaxial cable. One such low-noise set-up can be phased against a loop or, even better, against a second low-noise antenna system with different directional properties. In any event, the "shack end" of a Line I low-noise coaxial feed is connected to J1 (center) and J3 (shield) of the phasing unit; similarly, if such a coaxial feedline is to be used for Line 2, it should be connected to J2 (center) and J4 (shield).

For further discussion of noise-reduction schemes, the reader is advised to consult my articles "Another Look at Noise-Reducing Antenna Systems" (6 JUL 1992), "Bevmatcher" (15 JAN 1991), the Nick Hall-Patch / John Bryant article "Impedance Matching a Beverage Antenna to a Receiver" in Proceedings 1988, and the 1991 noise-reducing inverted-L articles by Dallas Lankford and Denzil Wraight. The reader should be advised that the noise being reduced is LOCAL electrical noise of the type caused by TV sweep oscillator harmonics, light dimmer buzz, and the like. These antenna systems cannot, singly, reduce static from lightning bolts. Such noise CAN be nulled by phasing two antennas if it is coming from far enough away as to approximate a point source not having great incoming-angle variation over time (it is then treated as a "dominant signal" as if it were a broadcast station interfering with desired DX).

"Spare antenna" input

DX peditioning in Newfoundland and elsewhere has taught me the value of having a broadband antenna available with the flip of a switch without having to disconnect the phased set-up. This antenna is characteristically used for rapid bandscanning and searching for parallel frequencies. The beauty of having it go through the phasing unit is that you could have nulled out a noise or a "pest" station on medium-wave and be monitoring a rare African when the idea of checking a 60-meter parallel comes to mind. With one flip of Super-MWDX-5's Output Switch S5 to one of the spare antenna positions ("Spare / Unamplified" or "Spare / Amplified"), you are now on a third antenna, fed into J9. This could be a longwire, a Beverage, or even an untuned active whip such as the MFJ-1024. The 60-meter parallel is confirmed and then you can flip back to the phaser signal without upsetting the null whatsoever. In home set-ups, some DXers might like to feed a loop into J9 so they can switch back and forth between a two phased-wires-created-null and one created by the loop. Entirely different stations might be logged when the same dominant station has been nulled by the two different methods. It sounds weird, but it can happen. A few receivers such as the Drake R8 have their own antenna switches that let you pick one of two sources. But many don't. Sony ICF2010's and Realistic DX-440's are very popular for DX peditions. Neither has such an antenna switch.

The added features make the Super-MWDX-5 a bit more complex than the standard MWDX-5 and much more complex than the Mini-MWDX-5. A well-equipped DX shack should have a very simple phaser such as Mini-MWDX-5 as well as a full-features version such as Super-MWDX-5. The simple unit will get nulls much of the time, but the more complex (and therefore, more flexible) unit can get more DX for the operator who has the patience to master its use.

Building the Super-MWDX-5 Phasing Unit

The documentation (schematics, assembly drawings, parts lists, hole lists, etc.) serves as the starting point. The following procedure should serve as an outline for the builder.

- 1. Gather all necessary parts (see parts lists to follow). Prepare work area with appropriate tools.
- 2. Drill out chassis box, in accordance with Table 3.
- 3. Assemble the A1 (BBA-C1) Broadband Amplifier Card subassembly, per Figures 4 & 5 and Table 5
 - 4. Mount the A1 (BBA-C1) circuit card at the hole locations noted in Table 3.
 - 5. Install jacks, pots, and switches. Solder inductors onto S1 per Figure 2 and Table 2.
- 6. Install wiring and other components per Figures 1, 2, 3, 6, 7 and Tables 1-4, 6, 7, 8. Install knobs on C1, C2, R1, R2, R3, S1, S2, S4, and S5 per Tables 2, 4, and 8. Place labels near controls and jacks.
- 7. Follow Two-Wire Phasing Procedure or Loop-vs.-Wire Phasing Procedure steps given in this

Table 3: Super-MWDX-5 hole-drilling list

- X = Horizontal distance, in inches, from the vertical centerline (VCL) on the side observed. Negative values of X are left of VCL, positive values of X are right of VCL.
 - Y = Vertical distance, in inches, from the bottom horizontal edge of the side observed.
 - D = Hole diameter in inches.

Hole loci are first marked on the box with a scriber and are then drilled with a .125" bit. Subsequently, as required, the holes are enlarged to the proper size by using progressively larger bits up to that corresponding to the final desired diameter.

1.0625 0 0.3125 0 0.3125 0		125 125
1.0625 0 0.3125 0 0.3125 0	0.5 0.3 0.5 0.3	125 125
0.3125 0. 0.3125 0.	.5 0.3	125
0.3125 0.		
.0625 0.	5 0.3	125
	.25 0.1	
	.25 0.2	
	0.75	0.75 1.25 0.12

Hole	Comp.	C1 & C2 must be tapped to 6-32 th Description	x	Y	D	
# .	Desig.					
			,		,	
1	CI	Line I Tuning CapMtg.H/W I	-2.963	3.875	0.25	
2	CI	Line I Tuning Cap shaft	-2.5	3.625	0.5	
3	CI	Line I Tuning CapMtg.H/W 2	-2.037	3.875	0.25	
4	CI	Line I Tuning CapMtg.H/W 3		3.0	0.144	
5	CZ	Line 2 Tuning CapMtg.H/W I	-2.963	1.625	0.25	
6	CZ	Line 2 Tuning Cap shaft	-2.5	1.375	0.5	
7	C2	Line 2 Tuning CapMtg.H/W 2	-2.037	1.625	0.25	
8	CZ	Line 2 Tuning CapMtg.H/W 3	-2.5	0.75	0.144	
9	RI	Line I level pot - tab	-1.125	4.125	0.144	
10	RI	Line I level pot - shaft	-0.8125	4.125	0.3125	

11	S4	I C			
12	S4	Input Coupling switch-shaft	-0.625	2.375	0.375
13	' R2	Input Coupling switch - tab	-0.125	2.375	0.144
14	R2	Line 2 level pot - tab	-1.125	0.875	0.144
15	SI	Line 2 level pot - shaft	-0.8125	0.875	0.3125
16		Bandswitch - tab	0.0	3.875	0.144
	SI	Bandswitch - shaft	0.5	3.875	0.375
17	S2	Function switch - tab	0.0	1.125	0.144
18	S2	Function switch - shaft	0.5	1.125	0.375
19	S6	Wire/Loop switch - shaft	1.5	0.625	0.25
20	S6	Wire/Loop switch - tab	1.5	0.375	0.125
21	G2	grounding H/W - internal lug	1.875	2.375	0.125
22	G3	grounding H/W - internal lug	1.875	1.5	0.125
23	Al	Broadband Amp. Card-H/W 2	2.0	4.5	0.125
24	AI	Broadband Amp. Card-H/W I	3.0	4.5	0.125
25	AI	Broadband Amp. Card-H/W 4	2.0	3.5	0.125
26	AI	Broadband Amp. Card-H/W 3	3.0	3.5	0.125
27	R3	Q-balance pot - shaft	2.8125	2.25	0.3125
28	R3	Q-balance pot - tab	3.125	2.25	0.144
29	S5	Output switch - shaft	2.625	0.875	0.375
30	S5	Output switch - tab	2.625	0.375	0.144
RIGHT	SIDE				
Hole	Comp.	Description	X	Y	D
#	Desig.				-
	****				,
1	J7	battery holder - H/W I	-1.875	0.75	0.125
2	J7	battery holder - H/W 2	-1.0	0.75	0.125
3	J6	B+ input - phono jack	0.0	1.25	0.25
4	J5	RF out - BNC jack	0.0	0.5	0.25
5	J9	spare ant. in - BNC jack	1.25	1.25	0.375

Table 4: "upper level" parts list

NOTE: For bandswitch inductors, see Table 2.

*: Note follows parts list.

Vendor codes for this and subsequent parts lists:

AE = Antique Electronics	/688 W. First St.
	/Tempe, AZ 85281
	/Tel. 1-602-894-9503
DK = Digi-Key	/P. O. Box 677
	/Thief River Falls,MN 56701-0677
	/Tel. 1-800-344-4539
MCL = Mini-Circuits Lab.	/ P. O. Box 350166
	/ Brooklyn, NY 11235-0003
	/Tel. 1-718-934-4500
MOU = Mouser Electronics	/ 11433 Woodside Ave.

MOU = Mouser Electronics

/ Santee, CA 92071 /Tel. 1-800-346-6873

RS = Radio Shack / Many locations worldwide

Item	Designator	Description/Value	Vendor	Vendor Stock #	QT
1		chassis box	MOU	537-TF-782	= ===
2	AI	BBA-CI amp. card	14100	(refer to text)	
3	(C1,2)	knob	MOU	45KN014	1
4		knob	RS	274-416	2
5	BI	9V alkaline battery	RS	23-553	1
6	C1,2	var. cap.,10-365pF	AE	CV-235	1
7	C3,4	capacitor, 33 pF	MOU	232-1000-033	2
8	C5,6	capacitor, 75 pF	MOU	232-1500-075	2
9	C7,8,9	capacitor, 0.1 uF	MOU	539-CK05104K	2
10	J1,2	red banana jack	RS	274-662	3
11	J3,4	black banana jack	RS	274-662	2
12	J5,8,9	BNC jack	RS	278-105	2
13	J6	phono jack	RS	274-346	3
14	J7 •	battery holder	MOU	534-1290	:
15	PI	phono plug	RS	274-339	:
16	R1,2	pot.,500 ohm,linear	MOU	31CT205	1
17	R3	pot., 50K, linear	MOU	31CT405	2
18	R4	resistor, 33 ohm	RS	271-007	
19	R5,6	resistor, 68 ohm	RS	271-010	2
20	* R7,8	resistor, 4.7 ohm	MOU	29SJ500-4.7	2
21	R9	resistor, I ohm	MOU	29SJ500-1.0	2
22	SI	switch/4pole/6pos.r	MOU	10WR046	:
23	\$2,5	switch/3pole/4pos.r	MOU	10YX034	2
24	S3	switch,DPDT,onoffon	RS	275-620	1
25	S4	switch/6pole/4pos.r	MOU	10WR064	:
26	S6	switch,SPDT,on-on	MOU	10TC230	:
27	T1,2,3	RF transformer,1:1	MCL	TI-6-X65	3

items: hook-up wire, buss wire, solder,labels "AS REQUIRED"

*Item 4 note: for S1, S2, S4, S5, R1, R2, R3.

*Item 14 note: Keystone 1290 or equivalent.

Table 5:	(AI) BBA-CI I	Broadband Amplifier card	parts list			wire #	From	То	Description
Item	Designator	Description/Value	Vendor	Vendor Stock #	QTY	======	***********	***********	**********
						4	J3	S3A arm	1°B
1	BD	perfboard:1.4"X1.4"	RS	276-1396 (cut)	1	5	J4	S3B arm	2"1
2	C1,2,5,6	capacitor, 0.1 uF	RS	272-109	4	6	S3B "Common"	S3A "Common"	0.5" B
3	C3	capacitor, 10uF tant	MOU	581-10M35	1	7	S3A "Common"	G1 internal GND lug	1.5° B
4	C4	capacitor, 0.001 uF	RS	272-126	1	8	S3A "Common"	RI CW	4" I
5	H1,2,3,4	screw, 4-40 X .25"	MOU	572-01880	4	10	GI internal GND lug	T1 pin 6	2"1
6	H1,2,3,4	spacer, 4-40 X .5"	MOU	534-1450C	3	11	G1 internal GND lug R6 side 2	T2 pin 6	2" [
8	H1,2,3 H4	split lockwasher,#4	MOU	572-00649 534-7311	1	12	TI pin 3	S3B "Terminated" S4A "Noise Reduction"	4"1
9	PI-8	solder lug, #4 flea-clip/.042 hole	MOU	574-T42-1/100	8	13	T2 pin 3	S4D "Noise Reduction"	3.5" I 4" I
10	QI	transistor, 2N3866	MOU	511-2N3866	i	14	TI pin 4	S4B "Noise Reduction"	4-1
11	R1.5.8	resistor, 4.7 ohm	MOU	29SJ500-4.7	3	15	T2 pin 4	S4E "Noise Reduction"	4"1
12	R2	resistor, 33 ohm	RS	271-007	1	16	CI rotor	S4B arm	3" [
13 -	R3,6	resistor, 680 ohm	MOU	29SJ250-680	2	17	C1 stator	S4C arm	2.5" [
14	R4	resistor, 2.7K	MOU	29SJ250-2.7K	1	18	C2 rotor	S4E arm	3"1
15	R7	resistor, I ohm	MOU	29SJ500-1.0	1	19	C2 stator	S4F arm	2" I
16	RFCI	inductor, 2200 uH	MOU	434-05-222J	1	[R7	7 side 2 connect directly to S5	A "Phaser/Amp."]	
17	UI	voltage reg., 7812	RS	276-1771	1	20	RICCW	R7 side 1	6"1
18	W	buss wire	RS	278-1341	-1'	21	RI arm	jct. L1 through L12	. 2"1
Table 6:	small hardward	e parts list, comprised of ta	hles 6A - 6	E		22	RICW	S4B "Normal"	2.5" 1
	ble 4 for vendor					23	S4B "Normal"	S4B "Short"	0.5" B
Note: N	Mounting hardw	are is supplied with the follo	owing comp	onents: J1 through J6,	J8, J9, R1, R2, R3,	24	S4E "Short"	S4E "Normal"	0.5" B
SI throug						25	S4E "Short"	G3 internal GND lug	2.5"
*** Table	A A A I moun	nting hardware ***				[C:	3 side I connect directly to S4	A "Normal"]	
Item	Designator	Description/Value	Vendor	Vendor Stock #	QTY		side I connect directly to S4	A "Short"]	
				************		26	S4C "Normal"	S4C "Short"	0.5" B
1		screw, 4-40 X.25*	MOU	572-01880	4	27	S4A "Short"	jct. C3side2/C5side2	1.5"1
2		split lockwasher,#4	MOU	572-00649	4	28	S4A arm	S4B "Long"	1. B
*** Table	6B = Cl moun	ting hardware (see Figure 7	. ***				side I connect directly to S4		
		hole locations from Table 3		te: 2 nieces at hole 1: 2	2 at hole 3: Lat		side I connect directly to S4		
hole 4.	Sumois leter to	note recations from Table 5	. Item 5 no	picces at nois 1, s		29	S4F "Normal"	S4F "Short"	0.5° B
						30	S4F "Short"	jct. C4side2/C6side2	2.5°1
Item	Designator	Description/Value	Vendor	Vendor Stock #	QTY	31	S2A "Line 2"	S4C arm	2"1"
					-	32	R3 arm	G2 internal GND lug	1.5*1
1	[1].[3]	screw, 6-32 X.4375"	DK	H157	2	33	R3 CCW	S1B arm	4"1
2	[1].[3]	rubber grommet	MOU	522-211	2 5	34 35	R3 CW	SIA arm	2.5" 1
3	see note	fiber washer, #6	MOU	534-3201 534-7312	3	36	S2A "Line I" S1A arm	S4F arm	2"1
5	[3]	solder lug. #6	MOU	572-00675		37	SIB ann	S2A "Line 2"	4-1
6	[1]	tooth lockwasher,#6	MOU	561-J632.5		38	SIC ann	S2A "Line I" S1D arm	4*1 1*1
7	[4]	nylonscrew,6-32X.5" hex nut, 6-32	MOU	572-00486		39	SID arm	G2 internal GND lug	3-1
8	[4]	split lockwasher,#6	MOU	572-00650		40	S2A arm	S2C "Null-b"	0.5° B
				372-00030		41	S6 "Wire"	jct. L13 through L24	4"1
		ting hardware (see Figure 7			h . l . 7 . l		side I connect directly to J8		
	ignators refer to	hole locations from Table 3	. Item 3 not	e: 2 pieces at hole 5; 2	at hole /; I at		side 2 connect directly to R4		
hole 8.						42	R4 side 2	S6 "Loop"	4" [
Item	Designator	Description/Value	Vendor	Vendor Stock #	QTY	43	S6 ann	R2 ann	3"1
			===			44	R2 CW	S4E "Short"	2.5" 1
1	[5].[7]	screw, 6-32 X.4375"	DK	H157	2	45	R2 CCW	T3 pin I	4" [
2	[5].[7]	rubber grommet	MOU	522-211	2		pin 3 connect directly to G2	GND lug]	
3	see note	fiber washer, #6	MOU	534-3201	5	46	S2B arm	T3 pin 4	2.5" 1
4	[7]	solder lug, #6	MOU	534-7312		47	S2C amı	T3 pin 6	2.5"
5	[5]	tooth lockwasher,#6	MOU	572-00675		48	S2B "Line 2"	G3 internal GND lug	1.5° B
6	[8]	nylonscrew,6-32X.5"	MOU	561-J632.5 572 00486	i	49	S2B "Line I"	S2A arm	1.1
7	[8]	hex nut, 6-32	MOU	572-00486 572-00650	i	50	S2B "Line I"	S2B "Line 2"	0.5" B
8	[8]	split lockwasher,#6	MOU	372-00030		51	S2B "Line 2"	S2B "Null-a"	0.5" B
*** Table	6D = grounding	hardware ***				52	S2C "Null-a"	S2C "Line 2"	0.5" B
Item	Designator	Description/Value	Vendor	Vendor Stock #	QTY	53	S2C "Line 2"	S2B "Null-b"	1"1
	-		===		-	54	S2B "Null-b"	R8 side I	3-1
1	G1,G2,G3	screw, 4-40 X.375"	MOU	572-01881	3		side 2 connect directly to S5		1601
2	G1,G2,G3	solder lug, #4	MOU	534-7311	3	55 56	S5A "Phaser/Amp." S5A "Phaser/Unamp."	S5C "Phaser/Unamp." S5A "Spare/Unamp."	1.5" I 0.5" B
3	G1,G2,G3	hex nut, 4-40	MOU	572-00484	3	57	S5A "Phaser/Unamp."	G3 internal GND lug	1.5"1
*** Table	6E = hardware	for battery holder J7 ***				58	19	S5A "Spare/Amp."	4"1
Item	Designator	Description/Value	Vendor	Vendor Stock #	QTY	59	S5A "Spare/Ainp."	S5C "Spare/Unamp."	2"1
-			===			60a '	* S5A arm	AI-PI	4" TP
1		screw, 4-40 X.375"	MOU	572-01881	2	60b	S5A "Phaser/Unamp."	A1-P2	4" TP
2		split lockwasher,#4	MOU	572-00649	2	[R9	side I connect directly to J6		
3		hex nut, 4-40	MOU	572-00484	2		side 2 connect directly to C9		
Table 7: v	wiring / compon	ent connections				[C9	side 2 connect directly to J6	ground lug]	
						61	S5B "Spare/Amp."	jct. R9side2/C9side1	2.5" [
Note		wire, approx. #22 AWG				62	S5B "Phaser/Amp."	S5B "Spare/Amp."	1.1
	B = bare solid (TP = twisted-pa					63	S5B arm	A1-P3	4" I
Len	the are maximus	m typical required amount; i	in actual pra	ctice, use the shortest	length possible to	64a	S5C "Phaser/Amp."	A1-P5	4" TP
	stray coupling.		and pro		•	64b	S5A "Phaser/Unamp."	A1-P6	4" TP
						65	S5C "Phaser/Amp."	S5C "Spare/Amp."	1-1
INSIDE B		_		Description			connect directly to C8 side 1]		
wire #	From	То		Description		66	SSC arm	C8 side 2	25"1
1		54A		3.5° I					
1 [[] co	nnect directly to	S4A arm					DE BOX	То	Description
2	R5 side 2	S3A "Terminat	ed"	1.5"1		wire#	From		Description
	nnect directly to		-			67	J7 + terminal pin	P1 plug - center pin	2"1
	nnect directly to			1		68	J7 - terminal pin	P1 plug - shield pin	2" [
3	J2	S4D arm		4" 1			connects to J6 for battery ope		
[J2 co	nnect directly to	R6 side 1]		1			and the same of the		

J4 > GND#2 IN

Table 8: control orientation conventions

Ensure that components are mounted and wired in accordance with this table; align knob pointers to ted. Orientations are as viewed from outside the chassis box assembly.

Side	Control	Orientation Conventions
top	CI	CCW = minimum C = 9:00; CW = maximum C = 3:00
top	C2	CCW = minimum C = 9:00; CW = maximum C = 3:00
top	RI	CCW = maximum level (no attenuation) = 7:00 CW = minimum level (maximum attenuation) = 5:00
top	R2	CCW = maximum level (no attenuation) = 7:00 CW = minimum level (maximum attenuation) = 5:00
top	R3	CCW = maximum level/Q Line 1 (min. Line 2)= 7:00 CW = maximum level/Q Line 2 (min. Line 1)= 5:00
top	SI	[see Table 2]
top	S2	Line 1 = 10:30; Line 2 = 11:30;
		Null-a = 12:30; Null-b = 1:30
left	S3	common = left; float = center; terminated = right
top	S4	long = 10:30; normal = 11:30;
		short = 12:30; noise-reduction = 1:30
top	S5	phaser + amp. = 10:30; phaser = 11:30; spare antenna = 12:30; spare antenna + amp.= 1:30
top	S6	wire = up; loop = down
		THE PROPERTY OF CALCULA

FIGURE 1: SUPER-MWDX-5 (INPUT SECTION)

S4 = INPUT COUPLING SWITCH (LONG! NORMAL! SHORT! NOISE - REDUCTION MODES)

C1 LINE 1 TUNE J1 0 WIRE #1 IN ROTOR 1:1 R5 68 O GND#1 IN WAX Q - LINE 2 FLOAT O (Q BALANCE) S3B GROUND MODE SWITCH MAX.Q - LINE 1 C2 R6 68 Ω LINE 2 TUNE 0 1 J2 10 - 365 pl WIRE #2 IN 꺵

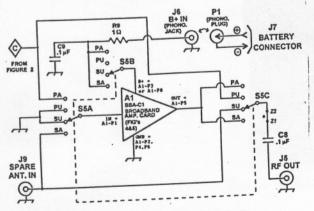
C4 = 33 pF

TOP VIEW, T3 TOP VIEW, T2 TOP VIEW. TI Hart Mores

TO FIG. 2

FIGURE 3: SUPER-MWDX-5 (OUTPUT SECTION)

(35 = OUTPUT SWITCH: PHASER AMPLIFIED! PHASER UNAMPLIFIED! SPARE ANT. UNAMPLIFIED!SPARE ANT. AMPLIFIED)



 α = See Figure 8 (Option 1) for alternate connections to circuit points 21 & 22.

FIGURE 2: SUPER-MWDX-5 (COMBINING SECTION / BANDSWITCH)

S1 = BANDSWITCH FOR INDUCTOR VALUES, SEE TABLE 2.

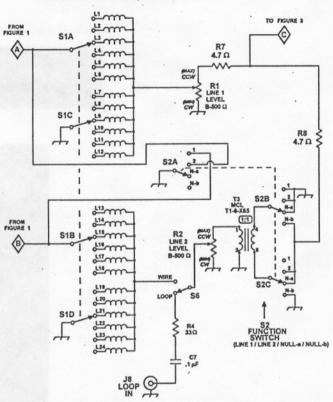


FIGURE 4: BBA-C1 IMPROVED BROADBAND AMPLIFIER CARD - SCHEMATIC (AI OF SUPER-MWDX-5 PHASING UNIT) (WAITON DX Labs - 17 MAR 1992)

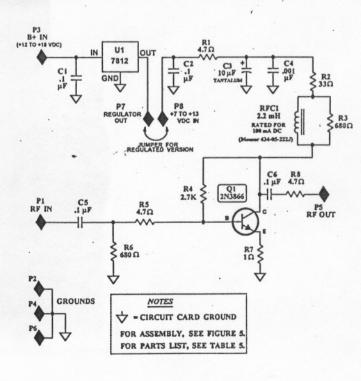
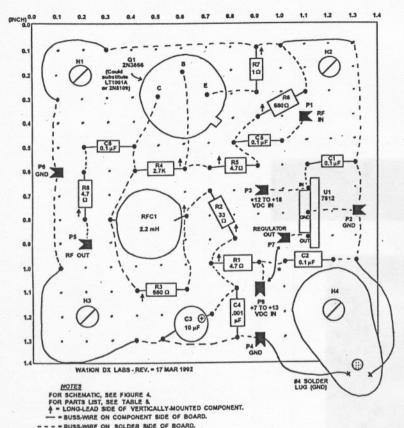


FIGURE 5: BBA-C1 IMPROVED BROADBAND AMPLIFIER CARD-ASSEMBLY



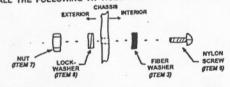
- "FLEA CLIP" TERMINAL PIN.
- OPEN SIGE

- JUMPER INSTALLED (P7 TO P5) FOR REGULATED OPERATION.

FIGURE 7: C1, C2 MOUNTING DETAILS

ITEM NUMBERS ARE ACCORDING TO TABLES 68 & 6C. HOLE NUMBERS ARE ACCORDING TO TABLE 3.

INSTALL THE FOLLOWING AT HOLE 4 AND AT HOLE 8.



CUT THE NYLON SCREW TO BE FLUSH WITH THE NUT. AFTER ASSEMBLY.

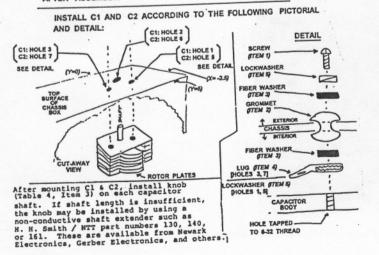


FIGURE 6: SUPER-MWDX-5 SWITCH DETAILS (SKETCH OF INTERIOR VIEW OF COMPONENTS, BOTTON COVER REMOVED) NOTE: POSITIONS, SIZES, APPROXIMATE — NOT TO SCALE

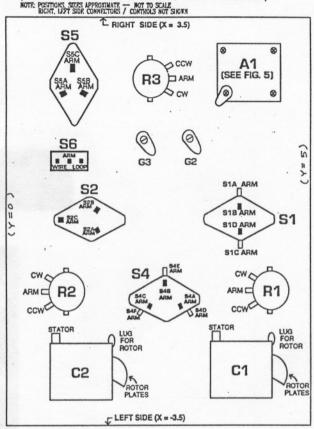


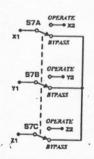
FIGURE 8: OPTIONS FOR THE SUPER-MWDX-5

Option 1 Operate / Bypass Switch

Install 3-pole, double-throw toggle switch (Mouser 10TC280) at holes drilled at: shaft = (X=0.75, Y=2.375, D=0.25); tab = (X=0.75, Y=2.625, D=0.144) .

X1, X2, Y1, Y2 are circuit points in Figure 1; Z1 & Z2 are from Figure 3.

Wires connecting X1 to X2, Y1 to Y2, and Z1 to Z2 are re-routed, as shown below:



Option 2 Use of BUF-A Buffer Amplifier (see RTL-2 Remotely-Tuned Loop article) in place of BBA-C1. BUF-B of RTL-2 could be used instead of BUF-A. Buffer-type amplifiers may offer lower current drain.

