# ELECTRONIC DESIGN

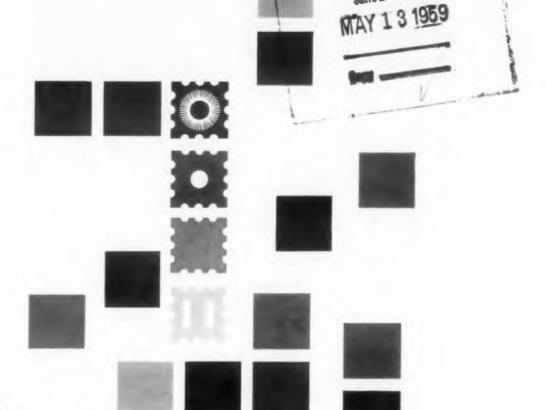
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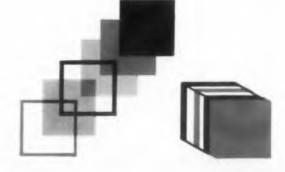




An ELECTRONIC DESIGN Staff Report:

MICROELECTRONICS...

a new concept in packaging

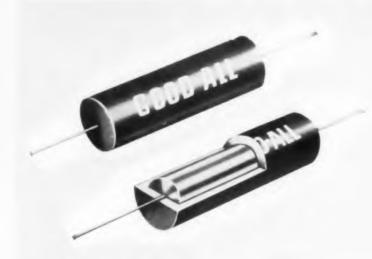


## Canadian General Electric Co., Ltd.

New streamlined transformers, molded in Epon resins, have superior insulation and dielectric strength. Accuracy and over-all performance are greatly improved.



## Specify Epon® Resins...



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New Epon resin-molded 600 UE capacitors have superior moisture resistance. Offer rugged, trouble-free performance because Epon resin assures high dielectric strength, low leakage.

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plexity of components are reduced.

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Epon resins can be adapted to a wide variety of formulations designed to meet your specific needs. Write now for full information including a list of suppliers of Epon resin-based formulations and manufacturers of automatic mixing, metering, and dispensing equipment.

SHELL CHEMICAL CORPORATION 50 West 50th St., New York 20, N.Y.

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## HIGHLIGHTS OF ISSUE



## Microelectronics (Cover) . . . . 32

Microminiaturization of electronic circuits is one of the most significant developments in electronics today. Extremely broad in scope, its implications excite the imagination of even the most inveterate designer. Radical new forms of conventional components and entirely new processes of making them are here now. Microelectronics presents a new frontier to be conquered for the frustrated designer of conventional components. There are new exciting challenges at every turn. Our staff report summarizes progress to date of the various groups working in this fast-moving area. The report further cites problems that must be solved before the electronics industry can realize the full potential of microminiaturization.

## Use two Time Constants . . . . 18

Sometimes it's not safe to assume step input to a circuit. Hughes Richard Muller shows better approximations to use when a square wave input has been rounded.

## New Ripple Reduction . . . . 30

A quick, clear design procedure for using transistors instead of reactors in ripple reduction. Saves weight and volume.

## Rechargeable "Dry" Cells . . 52

Designed to replace carbon-zinc dry cells, the new nickel-cadmium batteries are gaining popularity. Sonotone's line is one of the most complete.

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April 29, 1959 Vol. 7 M B ER

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## CONTENTS

Electronics Assists in Picking Astronauts **Behind the News** 

**Washington Report** New Concept in R & D Planning

> **Editorial** Not a Breakthrough But a Revolution

Special Report **MICROELECTRONICS** A New Concept in Packaging

Electronic components are changing shape. Latest developments and trends are covered in this ELECTRONIC DESIGN staff report.

How To Determine Circuit Response With Two Time Constants, **Features** R. S. Muller

> Synchronous Motor 22

Space Coordinate Transformation, G. H. Steinberg

Cast Silicon I-R Domes

The New Look in Ripple Reduction, B. Daien

Component Design Data Random Reliability Notes

Design Data on Rechargeable Dry Cells

**Ideas for Design** Radio Frequency Manhole Cover

**Russian Translations** 100 Nonlinear and Parametric Phenomena in Radio Engineering,

Part 17, A. A. Kharkevich

German Abstracts 112 Attenuation in the Passband of Filters

Time Delays in P-N Junctions

**Departments New Products** 98 Careers

> 84 New Literature 114 Meetings

88 **Patents** 116 Report Briefs

Standards & Specs 120 Advertisers' Index



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## used in Hughes Airborne Armament Control System

The F-102A all weather interceptor and many other planes in the U. S. and Canadian Air Defense Commands are fully equipped with this system developed and manufactured by the Hughes Aircraft Company. G-V thermal time delay relays are relied upon in all of these systems.

In both military and industrial equipment, G-V thermal relays are providing long, dependable, proven service in time delay applications, voltage and current sensing functions and circuit protection.

Write for extensive application data and catalog material.



## **G-V CONTROLS INC.**

LIVINGSTON, NEW JERSEY





# SILICON PNP TRANSISTORS in quantity production

Other significant advantages include:

Low saturation voltage
Twenty volts BVEBO
Low noise type available in both PNP and NPN
Minimum change in characteristics with temperature, current, and voltage

Suitability for complementary circuits

For both PNP and NPN Silicon Transistors specify RAYTHEON

FOR LARGE SIGNAL APPLICATIONS (Temperature Range -65°C to +160°C)

70-5 0 335°	Туре	Igo or Igo at Vca = 20 Vdc pA	V <sub>CE</sub> max volts	HPET ave.	rb' f = 1Mc ohms	kilohms	Noise Figure db (max.)	f = 100Kc ave.	lab ave. Kc
0.260.	2N327A	0.005	-40	15	1200	500	30	65	200
_ III N	2N328A	0.005	-35	30	1400	500	30	65	300
E3-44	2N329A	0.005	-30	60	1500	500	30	65	400
N	2N619	0.005	50	15	2000	500	30	35	200
	2N620	0.005	40	30	2500	500	30	35	350
N N	2N621	0.005	30	60	2700	500	30	35	500

ffor PNP, In = -0.1mA; VCE = -0.5V; for NPN, In = 0.5mA; VCE = 1.5V

FOR SMALL SIGNAL APPLICATIONS (Temperature Range -65°C to +160°C)

TO-5	Туре	Igo or Ico at Vcm = 20 Vdc	Vce max. volts	hfe* ave,	hie* max, ohms	hoe* max. µmhos	Noise* Figure db	cob f = 100Kc ave. μμf	f <sub>æ</sub> b ave. Kc
0.260°	2N1034	0.005	-40	15	3000	70	30	65	200
	2N1035	0.005	-35	30	3000	85	30	65	300
N N	2N1036	0.005	-30	60	3000	100	30	65	400
E3-44	2N1037	0.005	-35	30	3000	85	15	65	250
I	2N1074	0.005	50	15	3500	70	30	35	200
ALVA .	2N1075	0.005	40	30	3500	85	30	35	350
	2N1076	0.005	30	60	3500	100	30	35	500
N	2N1077	0.005	30	25	3500	85	15	35	300

\*Vc = 5V; Iz = 3mA



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## BEHIND THE NEWS

## Electronics Assists in Picking Astronauts

THE FINAL seven candidates for Project Mercury were evaluated and selected with the help of electronic transducers. Known as Mercury astronauts, one of the candidates will be chosen in about two years to probe outer space in a manned satellite.

To pick the seven final candidates from a field of 32, the volunteers were put through a rigorous battery of physiological and psychological tests. During many of the tests various electronic transducers were used to detect the men's bodily reactions. General areas of concern were the men's

nervous, respiratory and circulatory systems.

During the tests cardiograms of heart muscle contraction were made. Heart stroke and sounds were also studied. To determine the response of the nerves they were stimulated electrically. And tracings of electric currents produced by the brain were made.

Other tests included making audiograms with and without background noises, and voice tape recordings. Electronic devices were used to measure blood pressure, breathing and air volume rate, and skin temperature and resistance. These tests went on for seven and a half days and three evenings at the Lovelace Clinic in Albuquerque, N.M. See ELECTRONIC DESIGN, Mar. 4, page 20, for data on devices that may be used in these tests.

## Medical Data Sent While Astronaut Orbits

While the chosen astronaut orbits the earth he will be rigged with medical electronic equipment that will telemeter his physiological conditions to ground stations. Estimating the value of medical electronic equipment used during flight, one





Complete shore-based receiving unit (above), developed by the U. S. Navy Medical Dept., will permit a constant watch on the physical condition of animal and human occupants of space vehicles. The technique will also enable isolated medical practitioners who need the services of medical specialists located at distant points to transmit all essential data to the specialists by telephone. If a consultant is not available at the time of the call, data can be recorded on magnetic tape for later playback.

**Electrodes** are being attached to a Navy officer (left) in a new technique which will permit a constant watch on the space man's blood pressure, temperature, breath sounds, heart sounds and brain waves. Electrocardiograms are superimposed on carrier waves and transmitted over world-wide radio and telephone circuits.

## NEW MASER CIRCULATOR FOR L-BAND



AVAILABLE IMMEDIATELY FOR YOUR APPLICATION.

	CLLI	CLL2
Frequency range	$1260 \pm 25 \ mc$	1400 ± 25 mc
Isolation		
Minimum	20 db	20 db
Maximum	25 db	25 db
Insertion loss		
Minimum	0.3 db	0.3 db
Maximum	0.4 db	0.4 db
Power Average	5 watts	5 watts
VSWR		
Minimum	1.08	1.08
Maximum	1.25	1.25
Weight (max.)	9.0 lbs.	9.0 lbs.
Max. dimension	$7\frac{1}{2}$ in.	$7\frac{1}{2}$ in.

## MINIATURE, THREE-PORT DEVICE WITH COAXIAL FITTINGS MEASURES ONLY 7½ INCHES, WEIGHS 9 POUNDS

An entirely new Raytheon technique has made possible the design of an extremely small low-frequency circulator. The three-port device has Type N coaxial connections and is designed for use with masers and parametric amplifiers at L-band.

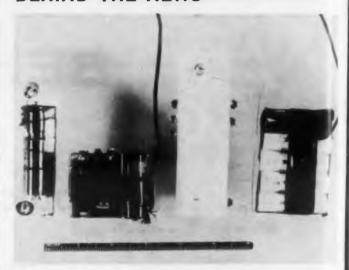
The new circulator, designated CLL1, combines an extremely low insertion loss of 0.3 db with 25 db isolation and VSWR of less than 1.1 centered at any frequency from 900 to 1,600 mc. With a permanent magnet, as illustrated, performance is typically 0.4 db and 20 db with a maximum VSWR of 1.25 over any 50 mc band. However, with a tuned magnetic field, the same performance is obtainable over a 100 mc band.

To learn more about this significant development or other important Raytheon advances in microwave ferrite devices, please write stating your particular area of interest to the address below.

RAYTHEON MANUFACTURING COMPANY SPECIAL MICROWAVE DEVICES WALTHAM 54, MASSACHUSETTS



## BEHIND THE NEWS



This subminiature electrocardiogram equipment is being used in experiments conducted for space travel. It was designed for use on ambulatory or exercising patients as a portable electrocardiograph and will enable medical researchers to collect important medical data as man responds to space. From left to right is: electrocardiogram amplifier; transformers; fm oscillator; dry cell batteries.

knowledgeable person said: "If he ever gets in trouble we'll probably know about it before he does."

The National Aeronautics and Space Administration is directing Project Mercury. It will pick and launch one of the seven astronauts into space. The astronaut will circle the earth two or three times at an approximate altitude of 125 miles in a one-ton capsule. Plans are for the satellite to splash-land somewhere in the Atlantic Ocean.

## **Space Medicine Interests Navy Too**

While the names of the seven Mercury astronauts and data on how they were selected was being released in Washington, D.C., a conclave in San Francisco watched a closed-circuit TV presentation of "Medicine Prepares For The Space Age."

At the meeting many of the medical problems and peculiarities of man's coming flights into space were outlined by Captain Norman L. Barr, USN, Director of Astronautics Div. Dr. Barr has developed systems for gathering physiological information from pilots in air and from animal and human occupants of earth orbiting vehicles. The equipment used in these systems permits transmission of electrocardiograms, electroencephalograms, body temperature and other physiological measurements. Some of the Navy's recent activities in Medical Electronics are shown in the accompanying photographs.

## Channeling Millimeter Waves Big Challenge

Being so short, millimeter waves are not only difficult to generate but hard to control-and they remain so, as concluded by those who attended the three day symposium on millimeter waves earlier this month in New York. However the fruits of millimeter wave application continue to tantalize many engineers and scientists, mainly because of the great number of messages that can be transmitted on a single transmission line. It was estimated that at least three hundred thousand telephone messages could be sent at once on a transcontinental transmission line. In addition to radio, telephone and television applications, millimeter waves should prove useful in determining the densities of hot ionized gases created by atomic reactions and calculating the atomic weights of nuclei.

## **Getting Strong Signal is Problem**

However a number of problems will have to be resolved before millimeter waves can be successfully harnessed. Because of the small tube size needed to generate such waves, it is difficult to obtain a sufficiently high signal level. The problem is one of generation and detection. Second, an efficient means of transmitting the waves must be achieved with minimal losses. Presently waves are transmitted along rectangular or circular waveguides. Because of their low signal power, millimeter waves can not be transmitted readily through the atmosphere, since the elements absorb much of their energy. However in space-platform applications, millimeter waves can be efficiently used for communication because of the rarefied atmosphere.

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At the present time 4 mm generation is possible but no one has successfully made for commercial use 1 and 2 mm devices.

## **Expect To Transmit TV**

Despite the problems that confront the millimeter-wave engineer and scientist, they showed little pessimism at the symposium. All eventually expect to achieve their goals in the not too distant future. One of the possibilities they envision is the ability to handle several hundred television channels at once on a transmission line. This is possible because of the great frequency range of millimeter waves. The spectrum is greater than the combined ranges of radio, television and radar.

Held from April 1st to the 3rd, the symposium was cosponsored by the Office of Naval Research and the Air Force Office of Scientific Research and arranged by the Polytechnic Institute of Brooklyn in conjunction with the Institute of Radio Engineers.

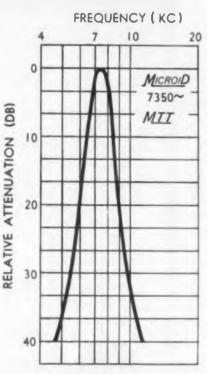
SHRUNK BY EXPERTS

Burnell & Co. may not be experts in the art of head shrinking. But when it comes to toroids, filters and related networks, Burnell has the know-how to solve an infinite variety of small space problems. The new MICROID ® filters by Burnell & Co. are a notable achievement in the shrinking of filters which can be designed for low pass or band pass applications.

For example, as a low pass filter, Type *MLP* starts at 400 cps. Physical size is 11/16" x 1-11/16" x 1/2" max. For higher frequencies from 5 kc up to 100 kc, size is 3/4" x 1" x 1/2".

The band pass filter, Type MII pictured here, ranges from 7,350 cycles

up to 100 kc. Physical size is 1/2" x 19/32" x 15/16", weight .3 ounces, band width 15% at 3 db and + 60% — 40% at 40 db. Wherever space and performance are critical requirements, miniaturized MICROID ® low pass and band pass filters provide utmost reliability as well as more unit surface economy on printed circuit boards. Completely encapsulated, they are ideally suited to withstand high acceleration, shock and vibration environments.



® REGISTERED TRADE MARK



PIONEERS IN TOROIDS, FILTERS AND RELATED NETWORKS

EASTERN DIVISION
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CIRCLE 5 ON READER-SERVICE CARD



The compact '909' Perforated Tape Strip Reader now makes it possible to process information from perforated tape into digital data computer systems at high speed and low cost. Simple to operate by clerical personnel, the '909' is completely transistorized, and will give maximum performance with complete reliability.

The '909' is a compact unit, suitable for console or rack mounting. Here are some of the performance features, available for the first time in equipment of this type:

- \* Character reading speeds up to 1000 char/sec.
- \* Simple In-Line threading
- 3 Millisec starting time
- Stops on STOP Character, (0.2 millisec) and will read next character after start
- 100 x 10° operation pinch roll
- Photo Diode Head reads any tape (including oiled yellow teletype tape)
- Reads 5, 6, 7 or 8 level tape with sprocket channel
- Ambient temperature up to 125° F. with 10,000 hour life
- Built to meet requirements of MIL-E-4158A

## Specifications

Tape Speed:

10 to 100 ips Tape Width:

Any Standard Width Power Requirements:

115V, 60 Cycle, 1 Phase

Remote/Level Inputs

Contact your Potter representative or call or write direct for further information.



Engineering Quality

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Potter has career opportunities for qualified engineers who like a challenge, and the freedom to meet it.

CIRCLE 6 ON READER-SERVICE CARD

## BEHIND THE NEWS

# Can "Power Saver" Alleviate World's Power Shortage



The United States consumed 567 billion kilowatt-hours of electricity last year. This figure will surely skyrocket in the next few years. To meet this problem, engineers at Texas Instruments' Industrial Instrumentation Division in Houston and at the Semiconductor

the accompanying photos.

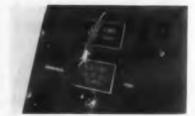
What's really unique about this great achievement is that it didn't cost the government a cent. There was no research and development contract—no cost plus fixed fee. The TI engineers did all the necessary work on this project at home—during off hours.

Components Division in Dallas developed the unique "Power Saver" shown in action in

The "Power Saver" operates on Murphy's Law, which deals with the obstinacy of inanimate objects. The sign over the power switch reads: Caution—Do Not Turn On Switch. When the operator turns it on (he always does), a mechanical arm emerges, turns off the switch, then withdraws.













ELECTRONIC DESIGN • April 29, 1959

## U.S. to Play Major Role in Paris Computer Conference

Strong world-wide position of U.S. computer technology has been confirmed in the final program plans for the forthcoming global computer conference sponsored by the United Nations organization in Paris, June 15-20. The formal technical program will feature 23 of 55 papers from United States computer experts.

More than 2500 scientists, engineers, and mathematicians meeting at the Western Joint Computer Conference, March 2-6, heard the first official details of the program just finalized in Paris by consultants to UNESCO from the thirteen participating nations. It also was the first public announcement of the high honors accorded to certain leading computer specialists from the United States in appointing them to official positions for the global event.

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A special new session has been added to the formal program which will explore "Computer Techniques of the Future." It was also disclosed that U. S. manufacturers of computer and data control systems would have considerable exhibit space in AUTO-MATH 59, a major equipment exhibit held in conjunction with the conference.

## Electronic Instrument Inside Concrete Mixer

Electronics is helping builders make better concrete. An electronic instrument to measure the water content of damp sand, with an error of only a fifth of one per cent, has been produced by Shaw Moisture Meters, England.

The measuring probe of the "Sandmaster" moisture meter is fixed inside the sand hopper of a concrete-making machine. The gage is located where the operator can see it easily and tell at a glance how much water to add.

The moisture content of the sand is measured by the ease or difficulty with which an electric current passes through it at a frequency of 100 mc.

From Transistor Center, U.S.A....

# PHILCO. announces a new family of LOW COST Medium Power

Introducing a completely new family of PNP germanium transistors, especially designed to meet rigid military and industrial specifications...at lowest possible prices.

These transistors are available in production quantities, for use in teletypewriters, control

amplifiers, ignition systems, mobile radios and desk calculators (2N1124); servo amplifiers, voltage regulators and pulse amplifiers (2N1125, 2N1126, 2N1127); medium power audio and switching applications (2N1128, 2N1129, 2N1130).

Also available in quantities 1-99 from your local Philco Industrial Semiconductor Distributor.

Make Philco your prime source of information for all transistor applications. Write to Lansdale Tube Company, Division of Philco Corporation, Lansdale, Pa., Dept. ED-459.

**Alloy Junction Transistors** 

	TYPE	V <sub>CB</sub> Max. (Volts)	V <sub>CES</sub> Max. (Volts)	Peak Ic (Amps)	P Max. (Watts)	F .ь (MC)	Beta	Applications	PRICE
	2N1124	40	35	0.5	0.3	0.4 Min	h <sub>fe</sub> 40 Min	For high voltage general purpose use in amplifier and switching, Small signal beta controlled.	* 1.30
1	2N1125	40	40	0.5	0.3	1.0 Min	h <sub>fe</sub> 50-150 @ 0.5 amp	For high voltage, higher frequency industrial amplifier and switching systems. Large signal beta controlled.	\$1.90
L	2N1126	40	35	0.5	1.0	0.4 Min	h <sub>fe</sub> 40 Min	1 watt version of 2N1124 for servo amplifiers and relay actuators. Small signal beta controlled.	\$1.80
#	2N1127	40	40	0.5	1.0	1.0 Min	h <sub>FE</sub> 50-150 <b>@</b> 0.5 amp	1 watt version of 2N1125 for servo amplifiers and control systems. DC beta controlled.	\$2.40
0	2N1128	25	18	0.5	0.15	1.0	h <sub>fe</sub> 70-150	For low distortion, high level driver and output application. Small signal beta controlled.	\$ .95
	2N1129	25	25	0.5	0.15	0.75	h <sub>FE</sub> 100-200 @ 0.1 amp	For high gain general purpose amplifier and switching. Typical DC beta 165.	\$1.10
	2N1130	30		0.5	0.15	0.75	h <sub>ге</sub> 50-165 @ 0.1 amp	For higher voltage, higher level amplifier and switching applications. Typical DC beta 125.	\$ .95

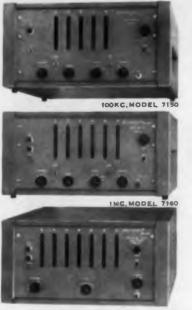
Available in Production Quantities—Also Available from Local Distributors

PHILCO CORPORATION

LANSDALE TUBE COMPANY DIVISION
LANSDALE, PENNSYLVANIA



## The right counter for every purpose



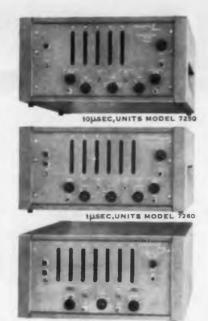
IOMC.MODEL 7170

## **EPUT® METERS**

Long considered standard nent for making rapid, equipment for making rapid, precise frequency measure-ments, Berkeley EPUT meters are now available with over twenty standard modifications designed for an ever-broadening variety of applications. Most EPUT meters are equipment to make period measureped to make period measure-ments of low frequency sig-



5210 PORTABLE



### TIME INTERVAL METERS

The full line offers meters of four degrees of precision ranging from a tenth of a millisecond to a tenth of a microsecond. Versatile 7000 Series instruments feature selectable sensitivity for noise discrimination, trigger level adjustable over a wide range slone selecover a wide range, slope selection and very high input im-8220 PORTABLE,100 UNITS



BEHIND THE NEWS



## "Hotshot" Wind Tunnel

A new 40-in. "hotshot" wind tunnel now being built by Boeing will give the company its seventh operating wind tunnel and the largest privately owned hypersonic tunnel in the country.

Shown is an 8-in. pilot model which has been in operation since mid-1958. This "hotshot" tunneloften called an "electric-arc-discharge wind tunnel"-gives Boeing testing capabilities in the Mach 10 to 27 range.

A "hotshot" tunnel consists of a capacitor bank for storing electrical energy, an arc-discharge chamber for containing high pressure-high temperature air, a nozzle, a test section to hold the model and a vacuum system for lowering the pressure in the test section. A plastic diaphragm maintains the pressure differential between the arc chamber and the test section until the moment of

In a typical test run, the capacitor bank is charged to capacity and compressed air is forced into the arc chamber. When an arc is struck, the air in the arc chamber becomes ionized. This high temperature-high pressure plasma rupture the plastic diaphragm and permits a high-energy shock wave to rush through the nozzle and into the test section. The shock wave is followed by a hypersonic flow of air.

Although the actual test lasts only about 1/25th of a second, ultra-high-speed oscillograph recorders can record data at 160 inches of paper per second on 36 channels.

The new hypersonic tunnel, as well as this pilot model, will enable the testing of models up to satellite Mach numbers.

Don't forget to mail your renewal form to continue receiving ELECTRONIC DESIGN.

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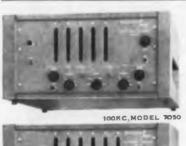
EU

## UNIVERSAL EPUT AND TIMERS

Combining the functions of an EPUT meter and time interval meter in a compact economical package, these instruments are widely preferred as gen-eral purpose laboratory equipment for precise frequency and time measurement. Unlversal instruments feature as many as ten distinct operating functions.



8230 PORTABLE







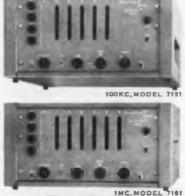
## **GATING COUNTERS**

The counting interval of these instruments can be accurately controlled by a broad variety of input signals. Widely useful as a systems building block, several of these units will perform as EPUT meters or time interval meters when considering the properties. interval meters when operated in conjunction with an inde pendent source of time sig-



### INDUSTRIAL TOTALIZING COUNTERS

Berkeley makes rugged counters with top speeds from 125 cps to 10,000 cps and capacities up to one billion counts. Model 5805 utilizes miniature magnetic amplifiers for long-term trouble-free





## PRESET EPUT METERS

These instruments will create direct digital indications of rotating speed, flow, pressure, temperature and similar physical quantities in any desired units—for example, rpm, gals/sec, psl, etc. Direct indication is made possible by a counting interval variable over a wide range in small increments.



MODEL 5420 SERIES



## COUNTER-CONTROLLERS

Counters which deliver output signals when selected numbers are reached are widely used for precise control of diverse operations. Output signals may be relay closures, sharp voltage pulses or changes in de level. 5400 Series instruments operate at speeds up to 40,000 counts per second and deliver. counts per second and deliver output signals at one or two preset totals. 5800 Series con-



MODEL 5020 SERIM

preset totals. 3800 series con-trollers utilize miniature mag-netic amplifiers for maximum reliability in in-dustrial control applications. Operable at speeds up to 5000 counts per second, these units are obtainable with from 1 to 12 preset points.

Write for Catalog C706.

## Beckman'

## Berkeley Division

2200 Wright Avenue, Richmond 3, California a division of Beckman Instruments, Inc.

CIRCLE & ON READER-SERVICE CARD

## Soviets Claim "World's Most Powerful" Computing Machine

A computing machine the Russians call "the most powerful in the world" is solving scientific puzzles at Kiev University, while another "unique" computer is working out problems of efficient exploitation of Soviet oil fields.

The Kiev computer, a differential analyzer, is described by a Russian writer as "incorporating 24 integrators and characterized by a high degree of automation in all of its units."

The solver of oil-field problems is said to illustrate Soviet mastery in series production of "specialized analog computers capable of investigating dynamic systems and other processes described by differential equations of the order 6 to 32."

The "matrix-type electrointegrator" has a matrix of resistors and capacitors at 20,000 points, a feature said to make it "a unique machine of this class."

One is a universal digital computer which will figure complex scientific and engineering problems at a rate of 20,000 operations per second. Its circuit will contain a series of storage units, one for internal storage of 2047 numbers, one for intermediate storage for 4096 numbers, and a third for external storage of 100,000 numbers.

The Russians describe the second machine as one of the first small-size universal digital computers with circuits using transistors, ferrites, and miniature tubes. Circuits of its control and arithmetic units incorporate transistors and semiconductor diodes.

The computer is designed to operate at a speed of 2000 to 2500 single-address operations a second. Internal ferrite storage will be 2048 forty-column binary digits of 4096 commands. External storage will consist of two magnetic tape units, each holding 70,000 forty-column digits.

## Japanese Interpreter

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An experimental electronic computer which can translate English into Japanese has been successfully produced at the Industrial Technology Institute's Electric Laboratory in Tokyo.

The new invention, the first such machine ever made in Japan, was described by Dr. Shigeru Takahashi at the meeting of the Telecommunication Academy's Electronic Computer Research Committee at Osaka University's Department of Technology. The translating machine, christened Tamato," was completed last December by Dr. Takahashi with collaboration of five other electronic specialists in the electric laboratory.

"Yamato" can translate first year junior high school English to Japanese.

High capacitance for low voltage circuits ...

## NEW TANTAPAK\* CAPACITORS

SPRAGUE'S TANTAPAKS are the newest members of the Tantalex\* family of tantalum electrolytic capacitors. TANTAPAKS have as much as 2400 μf at 10 volts d-c or as little as 140 μf at 75 volts d-c. Five case sizes—ranging from less than a cubic inch to a mere 3½ cubic inches—are identical to Type CP-90 paper capacitors. Standard footed and spade-lug brackets simplify mounting. All units are dual-voltage rated for operation at both 85°C and 125°C under 2000 hour life tests.

The construction of TANTAPAK Type 200D capacitors assures excellent shock and vibration resistance. Glass-to-metal solder-seal terminals provide positive hermetic sealing. There are no electrolyte leakage problems.

Porous tantalum anodes give better leakage and temperature coefficient characteristics than foil-type capacitor sections of comparable ratings. In addition, the impedance and equivalent series resistance of Type 200D are superior to foil units at high temperatures and frequencies.

Get complete information by writing for Engineering Bulletin No. 3705. Address request to Technical Literature Section, Sprague Electric Co., 347 Marshall Street, North Adams, Massachusetts. SPRAGUE 200 D

SPRAGUE 200 D

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ELECTRONIC DESIGN • April 29, 1959



## **Aerovox CERAFIL Capacitors**

Remarkable new design concepts and modern construction features of Cerafil Capacitors make it possible to obtain extremely high capacities per unit volume. These ultra-miniature ceramic capacitors offer a logical solution to circuit designers concerned with extremely miniaturized assemblies and equipments.

Cerafil Capacitors are the smallest ceramic units manufactured in the electronic industry. They are designed specifically for airborne and space-borne equipments, computer circuits, hearing aids and other critical applications where space and weight requirements are at an absolute premium.

Cerafil capacitors are available in working voltages of 30, 50 and 100 VDC, and in capacities from 10 mmf to 100,000 mmf. Type C80 (100 VDC) of this rugged ceramic unit of high reliability is designed for operation at temperatures from -55°C to +85°C. Type C80T (50 VDC) is rated at 125°C. Types C80 and C80T will meet or surpass all the applicable requirements of MIL-C-11015A

\*Actual size of a 1000 mmf unit @ 100 vdc. Mective February 1, 1959

REROVOX

Available at local Aerovox Parts Distributors nationally!

Write today for complete technical information of these ultra-miniature CERAFIL CAPACITORS...

OLEAN, NEW YORK

CORPORATION

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## BEHIND THE NEWS

## **New Field Effect** Semiconductor Tetrode Is Almost "Universal" Component

LUNCTIONS of a transformer, gyrator, isolator, non-distorting modulator, or short-circuit stable negative resistance can be duplicated by a new four-terminal semiconductor device developed by Bell Telephone Laboratories. Labeled a "fieldeffect tetrode," the device has no analog, either in electron tubes or previous tran-

### Construction

The tetrode, Fig. 2, is composed of a disc of semiconductor with a diffused junction. A circular trench is cut and etched into each face of the disc, to within 1 mil of the junction on either side. Two leads are then attached to each face, one inside the trench, the other outside. When a voltage is applied across the junction, the thickness of the depletion layer adjacent to it is increased or decreased, depending on the direction of the biasing voltage. This in turn increases

or decreases the resistance of each "channel" between the bottom of the trench and the junction.

## **Unusual Applications**

Depending on the polarity of the biasing voltage, the tetrode will function either as a transformer or a gyrator. As a transformer, it has a very decided size advantage for low frequency use, although it does not afford de isolation. As a gyrator, it should be of considerable circuit interest. (A gyrator is a non-reciprocal four terminal network which behaves similarly to a transformer, while exhibiting a 180 deg difference in phase shift depending on the direction of transmission.) One important gyrator function is impedance inversion. For example, it should be possible to use the new device to convert the reactance of a miniature capacitor into that of a high-O inductor.

If the device is biased properly, it will



Fig. 1. Inventors R. M. Warner Jr. and H. A. Stone, Jr. inspect model of field-effect tetrode

E.E

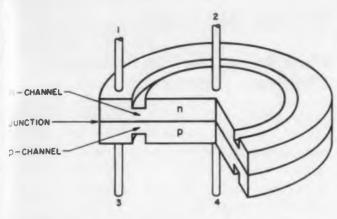


Fig. 2. Note circular trench etched into face of upper and lower section of field effect tetrode.

function as an isolator, allowing passage of alternating current in one direction only.

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### **Distortionless Modulator**

According to its inventors, H. A. Stone, Jr. and R. M. Warner, Jr., one of the most important applications for the new device may be as a distortionless modulator, or electronically controlled resistor for large signals. In this use, a relatively low frequency control-voltage varies the width of the depletion layer, and thus the resistance of the device. Simple capacitors act as high-pass filters to isolate the control-voltage from the signal, if the frequency ratio is maintained at a high level. The signal voltage does not appear across the junction and has no effect on the depletion layer. Therefore, it can be magnitudes higher than the control voltage, without being distorted by self-modulation. For the same reason, it is not limited by junction capacitance.

### Stable Negative Resistance

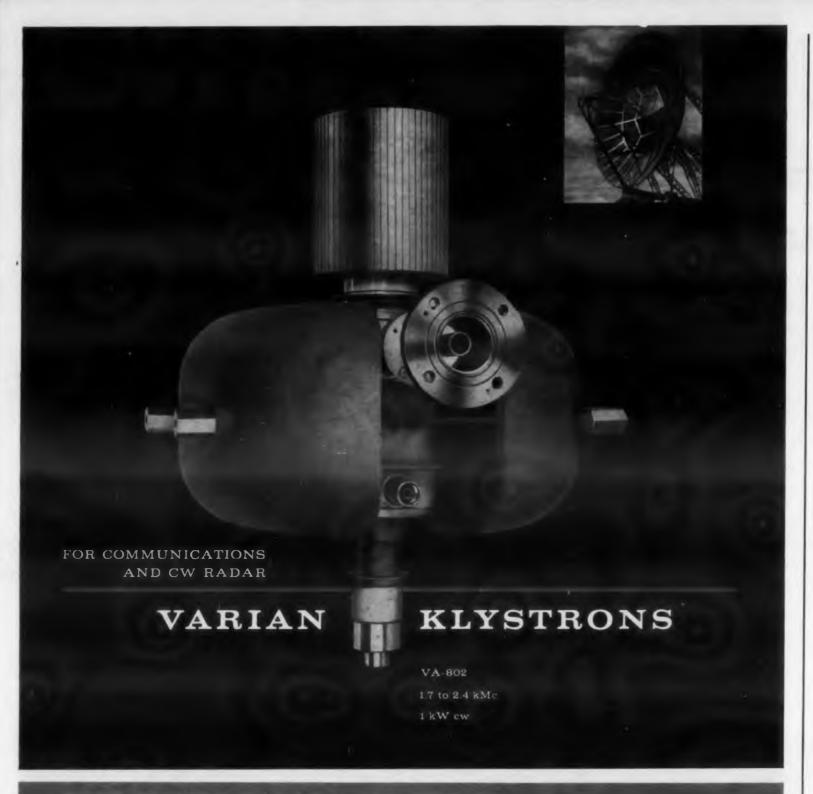
If a direct connection is made between the inner lead on one face and the outer lead on the other, the device will function as a two-terminal a-c short-circuit stable negative resistance. In the experimental models produced at Bell Laboratories, this performance has been achieved over a range of about 30 to 250 v, at 0.6 to 0.1 ma, in a boron-doped silicon crystal with a phosphorous diffused junction.

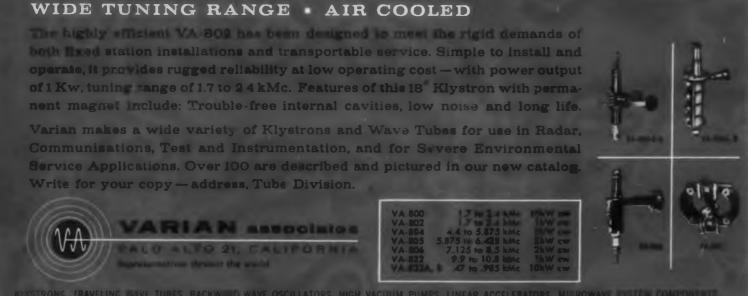
While the practical development of the field effect tetrode is still in a very early stage, it shows potential characteristics in a single device which previously either could not be obtained at all, or only through extensive circuitry.

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dependability with ..... LUMPED CONSTANT 10 millimicroseconds - 100 milliseconds Delay Time Impedance 50 - 3000 ohms Delay to Rise Time Ratio up to 50 - 1 Low attenuation characteristics SOLID DELAY LINES Delay Time 3 - 4000 microseconds Impedance 50 - 2000 ohms Center Frequency 5 - 100 megacycles Spurious to 60 db Low attenuation characteristics Band width to 50% of Carrier Frequency Trained Personnel Modern production facilities Prototypes Complete quality control Packaging to Military specifications Minimum size and weight is prime design factor Richard D. Brew and Company, Inc. 90 Airport Rd. Concord, N. H. Brochures Available On Request

CIRCLE 11 ON READER-SERVICE CARD





## CIRCLE 12 ON READER-SERVICE CARD

## BEHIND THE NEWS

## Moon Relay Link Ties Pentagon to 50th State Outpost

Communications between Washington and Pearl Harbor will make use of the moon as a passive relay station in the coming year. After nine years of research work by the Naval Research Labs., a feasible system for reflecting radio and radar signals off the moon has been developed. Known as the Communication Moon Relay Project, the system theoretically could handle all military communications between Washington and the military command center of the Pacific.

Two and one-half seconds will be required for the uhf signals to complete the trip to the moon and back; about 4500 miles lie between Washington and Pearl Harbor. Signals will be transmitted from 84 ft. diam. parabolic antennas at Annapolis, Md., and received by similar antennas at Cheltingham, Md., about 15 miles from Washington. Two similar stations will be located at Wakiawa and Opana in the Pacific.

The fact that the moon must be in sight of both links poses the obvious limitation to the system. Radio contact can vary from four to fourteen hours daily depending on the orbit of the moon. This disadvantage is outweighed, say Navy officials, by the improved reliability of message transmission. Noise interference and ionosphere-caused blackouts will not mar system operation.

In addition, the system is virtually jam-proof an important military consideration. In order to jam the moon circuit, an enemy would require a station located within several miles of the main sites. Theoretically, the enemy could bounce signals off the moon at the same frequency, but this attempt could easily be thwarted by switching frequency at predetermined intervals.

## **Ultra-High Speed Flash**

Flash X-ray equipment for use in recording explosion processes and measuring the speed of hyper-velocity objects has been announced by Zenith Radio Research Corporation. Utilizing a newly developed air-core pulse transformer and special "triggering" circuits, the equipment performs with a degree of reliability and accuracy which has never before been achieved by flash X-ray systems.

Unlike other flash X-ray equipment in which capacitors apply the full accelerating voltage directly to the flash X-ray tube, Zenith's equipment stores the energy at a relatively low potential. The pulse transformer, steps it up to the required peak accelerating voltage only when the tube's operation is desired. Full accelerating voltage is within the range of 60-120 kv.

## NEWS BRIEFS . . .

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TION employing man-made clouds which reflect radio signals has been patented by Henri Busignies, president of the ITT Laboratories of International Telephone and Telegraph Corporation. The system utilizes clouds of metallic chaff or ionized materials off which the radio signals, transmitted from earth, are reflected back to earth at distant points and picked up by radio receivers. The materials are sent aloft by various methods such as guns, aircraft including guided missiles, balloons, and rockets. They also can be expelled as ionized gas in the exhaust of aircraft such as rockets.

• • MANUFACTURERS OF PERMANENT MAGNETS recently organized the Permanent Magnet Producers' Association, a national trade association designed to promote the progress and development of this industry. The basic program for the PMPA is to expand the program of magnet standardization with respect to magnetic and physical properties for the benefit of industries utilizing permanent magnets. In addition, it will collect and disseminate reliable technical information, from domestic and foreign sources, as an aid for the designer using permanent magnets.

Headquarters for the PMPA have been established at 27 East Monroe Street, Chicago 3, Ill.

• • ESTABLISHMENT OF THE NUCLEAR INSTRUMENTATION ASSOCIATION has been jointly announced by a group of prominent nuclear instrument manufacturers. Creation resulted from the increased importance of nucleonics and nuclear instrumentation within the field of electronics.

Purpose of the Nuclear Instrumentation Association is to give industry support to research, development and production in the U. S. The new national trade organization will be expanded to represent major manufacturing segments of the nucleonics industry.

• • A NEW METHOD IN THE THEORY OF SUPERCONDUCTIVITY by N. N. Bogoliubov, V. V. Tolmachev, and D. V. Shirkov, will be published in April by Consultants Bureau, Inc., 227 W. 17th St., New York 11, N.Y. The book, a complete English translation of the recent Russian work, will be cloth bound and priced at \$5.75.

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GENERAL INSTRUMENT SEMICONDUCTOR DIVISION Radio Receptor / silicon diodes CHARACTERISTICS high speed • high conductance • high temperature high voltage • high back resistance Including the industry's most versatile diode with uniform General Instrument semiconductor enexcellence in all parameters gineering has made possible these Radio Receptor diodes with a range of GENERAL PURPOSE
TYPES FAST RECOVERY TYPES HIGH CONDUCTANCE TYPES characteristics never before available to the industry. 1N456 1N625 1N461 1N482 1N484A 1N457\* 1N462 1N626 1N482A 1N484B The types listed here are just a small 1N458\* 1N463 1N482B 1N485 sampling of the complete line which 1N628 1N483 1N485A can be supplied in volume quantities 1N629 1N483A 1N485B for prompt delivery. Write today for 1N483B 1N486 1N486A 1N484 full information. \* JAN Types PLUS a large group of special DR numbers developed by General Instru-ment Corporation with characteristics that far exceed any of the standard types listed above! Semiconductor Division GENERAL INSTRUMENT CORPORATION 65 Gouverneur Street Newark 4 N.J. GENERAL INSTRUMENT CORPORATION INCLUDES F W SICKLES DIVISION AUTOMATIC MANUFACTURING DIVISION, RADIO RECEPTOR COMPANY, INC. AND MICAMOLD ELECTRONICS MANUFACTURING CORPORATION ISUBSIDIARIES! GENERAL INSTRUMENT DISTRIBUTORS Baltimore D & H Distributing Co. \* Chicago Merquip Co. \* Cleveland Pioneer Electronic Supply \* Los Angeles; Valles Electronics Supply Co. Burbank \* Milwaukee: Radio Parts Co. Inc. \* New York City Hudson Radio & Television Corp. Sun Radio & Electronic Co. \* Philadelphia Herbach & Radioman Inc. \* San Diego Shanks & Wright Inc. \* San Francisco Pacific Wholesale Co. \* Seattle Seattle Radio Supply \* Tulsa Oil Capitol Electronics

CIRCLE 13 ON READER-SERVICE CARD



## Small-World Resistors with out-of-this-world Reliability

Miniaturization is a severe test of performance, for reliability tends to shrink faster than size. Here, where critical equipment had to be made smaller, yet more reliable, Bendix-Pacific pinned performance to the reliability of IRC precision film resistors.

IRC Molded Metal Film Resistors combine excellent stability on load with a low, controlled temperature coefficient that is far superior to other precision film resistors. They exceed requirements for extremely close design tolerances and have excellent high frequency characteristics. Where these superior characteristics are not required, IRC Molded Deposited Carbon Resistors offer excellent all-around performance and economy. Both types available in ½, ¼, 1 and 2 watt sizes . . . and exceed MIL-R-10509B specifications. For design data, write for Bulletins B-3 and B-9.



INTERNATIONAL RESISTANCE CO. Dept 333, 401 N. Broad St., Phila. 8, Pa. In Canada: International Resistance Co., Ltd., Toronto, Licensee



New Subcarrier Oscillator typical of integrated reliability and miniaturization achieved in telemetry equipment by Bendix-Pacific Division of Bendix Anation Corp., North Hollywood, Cal.

CIRCLE 14 ON READER-SERVICE CARD

## WASHINGTON REPORT



**Ephraim Kahn** 

## New Concept in R & D Planning

Present concepts of research and development would be vastly changed if the military adopt a proposal that has been suggested by Dr. William H. Martin, Director of R & D for the Army. As he sees it, R & D should continue through the first stage of the production cycle. If major production changes are needed, they should be worked into the design before the pilot run has been completed.

## Leadtime Could be Halved

Furthermore, Dr. Martin believes that the agency sponsoring the development program should be held responsible for all work until the "bugs" have been worked out of any new device. Object of this extensive change in R & D responsibility is to shorten leadtime to about four years from the eight now customary.

Increased automation must necessarily go along with the greater complexity of modern weapons. States Dr. Martin: "This applies especially in the microminiaturization of electronic components, where the designs of the device to be made by automatic machinery have to be compatible and concurrent with the designs of this machinery, and consequently must be able to react on each other."

Industry support for this change in R & D concept is solicited. The Army, for example, wants and needs "more organizations which are proficient in both development and production and whose management has the concept and the experience of handling as a prime contractor the over-all job from the systems point of view."

Some aspects of Dr. Martin's plan for R & D acceleration are bound to create a stir in Congress. The Armed Services have, in the past, come in for sharp criticism from both the House and Senate Small Business Committees for alleged over-emphasis on the use of negotiated contracts in military buying—particularly those involving larger firms. Nevertheless, Dr. Martin implies that competitive bidding is not appropriate for new and untried products that are still basically in the development stage. It is only after this period is over that the military is "ready to break into the systems concept of responsibility by the primary contractor and 'peel off' direct purchasing of some of the supporting equipment.

As Dr. Martin sees it, the four-year development cycle would require the services of a "project manager," and provision for funds for the entire cycle would have to be made at the time the program was set up. Though these are "objectives and not regulations to be applied to every project regardless of its magnitude or urgency," he believes that they "should be valid for the more important projects."

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## Possible Approaches

Guidelines for putting this proposal into practice would include:

- Adequate basic research and development programs to provide a reservoir of new concepts, knowledge, and components, and that each project be backed by a well-drawn plan prior to its authorization.
- Development cycle end only after acceptable and tested items have been produced in the course of the first production run.
- Responsibility by a single contractor for development, preparation for production, initial production, and support materials.
- Maximum stress be placed on the Qualitative Military Characteristics of the product throughout the development cycle, with the R & D agency primarily responsible for seeing to it that QMC are properly adjusted to available technology, economical quality production, reliability, and timely availability.
- Close relations with the contractor and the development agency be maintained by the logistics and user agencies to insure that their interests are properly effective in the development of the design.
- Designation, by the development agency, of an employee as project manager, responsible for the progress of the venture and for coordinating the participation of other government agencies.
- No more than a four year lead-time be planned from inception of a project to operational availability of its end-product, and that the availability of funds be geared to this rate of progress.

## **EIA Group to Visit USSR**

Ray C. Ellis, Vice President of Raytheon Manufacturing Co. and Chairman of the International Department of the Electronic Industries Association (EIA) will head a six-man delegation of American electronics specialists leaving shortly for a three-week visit to the USSR. The group will meet with its Soviet counterpart and visit electronics laboratories and plants.

This is the time of our annual subscription renewal.

ELECTRONIC DESIGN • April 29, 1959

## Feeds, stakes and fuses Eyelets in PRINTED CIRCUIT Boards



 Some of the plants using Edward Segal Model NR-ESSM eyeleting machines—in many cases, batteries of them, include:

Bendix Aviation Co., Kansas City, Mo. Federal Telephone & Radio Division of I.T.T., Clifton, N. J.

Bell Telephone Laboratories, Whippany, N. J.

Laboratory of Electronics, Boston, Mass.

Melpar, Inc., Arlington, Va.

Sandia Corp., Albuquerque, New Mexico

Western Electric Co., Greensboro, N. C. . . . and many others.

Economical, too. They frequently pay for themselves in a few months or less.

This revolutionary development in printed circuit board production is obsoleting manual eyelet attaching and soldering. Many of the leading manufacturers in America\* find that Segal's new Model NR-ESSM is a completely dependable automatic method of making continuous electrical circuits of the printed elements on opposite sides of a board — or a single side if desired.

This unique machine stakes and solders simultaneously, sets up to 30 eyelets a minute, top and bottom, with never a reject.

Model NR-ESSM is just one of many efficient Edward Segal machines. There's Model NRLT for example, for cold staking flat and funnel type eyelets, and Model LSD that automatically feeds and stakes tube pins and turret terminals with equal reliability. For full details on these or any other machine to improve your eyelet attaching production, write Section ED-4

Edward Segal engineers can recommend and supply you with eyelets for every phase of printed circuit work.



MANUFACTURERS OF EYELETING MACHINERY, SPECIAL HOPPERS AND FEEDING DEVICES 132 Lafayette Street, New York 13, N. Y. Telephone: WOrth 6-3935

Chicago 22: A. J. Horne, Inc., 1958 West North Avenue
California: Dolliver & Bro., 5108 East Washington Blvd., Los Angeles 22;
619 Mission Street, San Francisco 5

CIRCLE 15 ON READER-SERVICE CARD



The Burndy "Hyliner," a mobile demonstration unit, recently left Burndy's Norwalk headquarters for its second transcontinental tour. The Hyliner is a deluxe bus which was converted into a traveling demonstration and display vehicle to introduce Burndy's Omaton Division and its products to the nation's manufacturers of electrical and electronic products.



The Hyliner began its first tour in August 1956 after being dedicated by Connecticut's Governor Abraham Ribicoff. Since then nearly 80,000 engineers have visited the Hyliner during its 70,000 miles of crisscrossing the U.S. and Canada.

After completing its initial tour the Hyliner returned to Burndy headquarters for outfitting with the latest displays and demonstration equipment. Alan E. Aune, OEM Sales Manager, states that heavy emphasis is being placed on connections for electronic equipment, such as new HYFEN® and STAPIN® methods. During the current tour, he added, smaller, more intimate groups from each plant visited will tour the Hyliner.

During the Hyliner's first tour, many new lines of HYFEN connectors were perfected including the new coax HYFEN which has already been adopted by several large manufacturers of conputers as well as military missile guidance control equipment manufacturers.

Samples of all the latest connectors and connection techniques, including all types of installation tooling, will be demonstrated.

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piece block. Mates with existing solder types.

COAX MODULOK

... Modular terminal block, Modules snap together or apart and are mounted on cadmiumplated steel track.





for conductors, guarantees a uniform indent for measurable quality control. There is no heat to damage insulation.

parts make installation

circumferential position.

CONNECT RELIABLY

...tool-controlled crimp provides strain relief

easy-tool crimps

contacts in any

FOR OTHER REQUIREMENTS OR APPLICATIONS, CONTACT OMATON DIVISION

Toronto, Canada Norwalk, Connect.

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## **EDITORIAL**

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## Not a Breakthrough But a Revolution

There is a revolution going on in the components industry. Microcircuitry, or more generally, microelectronics, is no longer simply a blue-sky topic for luncheon speakers. The cover story of the last issue of Electronic Design and special report in this issue, "Microelectronics . . . a new concept in Packaging", bears witness to the fact.

It is not easy to describe the transformation going on but the 18 pages that follow will give you an "operational definition" in the P. W. Bridgman sense. A study of the report will show the work of not one or two government labs but the results of at least 60 organizations. If you were at the IRE National Convention, you saw the Army's micro-modules at the RCA booth and the solid circuits at the Texas Instrument booth—the same solid circuits predicted as coming but at least five years away.

RCA's micro-modules are for sale. Texas Instrument says theirs will be available shortly. This means that in two years operational equipment using microelectronics will be available. Since at least 85% of today's electronics equipment can be built the micro-module way, today's engineer is witnessing the beginning of a revolution.

Whether the conversion will take depends on a number of factors. There will be of course widespread passive resistance if the owners of production machinery do not invest in new machinery. Currently, the components portion of the electronics industry, excluding tubes and transistors, produces products having a value of only \$1.3 billion, but the practices of this small group determine the form factor of the product of a \$7.9 million original equipment market.

There will be changes, therefore, only as production machinery for the new techniques is funded. We see this coming. The stakes are worth it: smaller size, greater reliability, lower costs. If the military finances but one company, the rest will follow as no one can afford not to be prepared to share in the new market. If components manufacturers do not rise to the challenge, weapon system contractors will take the lead. Once they do, the revolution will come to pass. Since microelectronics by automation is economical, producers can control not only the military market but the consumer and industrial market as well. Microelectronics products produced by automation will be cheaper than the coolie-labor products and the world market, too, will belong to the victors.

Jame & Kepthe



## **How To Determine Circuit Response**

The simplifying assumption is perhaps one of the most useful tools in the design engineers arsenal. But it can be a treacherous one.

"Let us assume a step input," is one of the most popular of these tools. It is extremely convenient, but unless used carefully, it can lead to unexpected circuit response.

Richard Muller, a Fellow of the National Science Foundation, shows when the assumption is "safe," and what "safer" assumptions can be made when necessary.

## With Two Time Constants

Richard S. Muller

Hughes Aircraft Co. Culver City, Calif.

THOUGH no real waveforms can have zero rise time, practical calculations of network response usually assume that driving waveforms are square. This approximation is often valid, often not. When the approximation leads to troublesome errors, it is profitable to consider simplifications which may permit more accurate calculations while still avoiding the laborious, exact approach.

The step response of a single time constant network consists of a single exponential term which can be easily manipulated to yield an explicit solution for time. But if the driving waveform is rounded so it has a finite rise time, the response equation has two exponential terms. The driving wave's rise time contributes the second time constant.

In this case, an explicit solution for time is not attainable. An exact approach demands a laborious graphical technique.

### A Transistor's Step Response

To illustrate the problem, consider a network which has a transformed response to a step input which takes the form

$$\frac{A}{s(s+D)}$$

Such an equation is, for example, characteristic of the transistor step response derived by Easely.<sup>1</sup> In the common emitter configuration, for in-

stance, the form of the equation is

$$I_c = \frac{A \ I_{b1}}{s(s+D)}$$

where  $I_{b1}$  is the magnitude of the base current step and  $I_{o}$  is the output (collector) current.

If the driving waveform is not square, but rounded as by capacitive shunting, it is likely to be of the form

$$I_b = I_{b1} (1 - \epsilon^{-Gt})$$

instead of the simple step  $I = I_{b1}$ .

Such a driving waveform would yield a transformed response equation of the form

$$I_e = I_{b1} \left[ \frac{A}{s(s+D)} - \frac{A}{(s+G)(s+D)} \right]$$

since

$$L[I_b(t)] = \frac{1}{s} - \frac{1}{(s+G)} I_{b1}$$

which implies that

$$I_{\epsilon} = I_{b1} \left\{ \left[ \frac{A}{D} \left( 1 - \epsilon^{-Dt} \right) \right] - \left[ \left( \frac{A}{D - G} \right) (\epsilon^{-Gt} - \epsilon^{-Dt}) \right] \right\}$$
 (1)

Eq (1) is the type under consideration. The first term is the step response of a network with a single time constant 1/D. The second is due to

the finite rise time of the driving waveform. As its time constant 1/G approaches zero, the rise time of the driving wave approaches zero and the output approaches the step response.

## How Accurate Is The Single Time Constant Approximation

The important question that arises with this example is "What is the relative magnitude of G with respect to D, which would allow considering the step response alone with negligible error?" If one thinks in terms of time constants, the consideration is of the ratio of the circuit time constant 1/D, to the driving waveform's time constant 1/G.

For negligible error, the second term in Eq (1) must be negligible compared with the first. If, for example, the ratio of these two terms is set at 0.1, it should be interesting to see what restriction this places on the magnitude of G with respect to D.

Accordingly, set

$$\left(\frac{D}{D-G}\right)\frac{(\epsilon^{-G\iota} - \epsilon^{-D\iota})}{(1 - \epsilon^{-D\iota})} < 0.1$$
(2)

Probably G will have to be significantly larger than D to make  $\varepsilon^{-Gt} \ll \varepsilon^{-Dt}$  at all but very small t's. Hence, the effective requirement is

$$\left(\frac{D}{G-D}\right)\left(\frac{1}{\epsilon^{Dt}-1}\right) \leqslant 0.1$$

ELECTRONIC DESIGN • April 29, 1959

which leads to

$$\epsilon^{Di} > \frac{9D + G}{G - D}$$
 (3)

Eq (3) gives a quantitative statement to the evident fact, that as consideration is extended to smaller and smaller response times, the approximation demands greater and greater disparity in the exponential time constants. The expression also indicates that the error decreases with time since the inequality becomes easier to fulfill with increasing t.

At this juncture, the designer must decide in what time range his interest lies. Then, using Eq (3), he can determine the required G to D ratio.

Continuing with the example of transistor step response equations, and specifying that response times of interest will be less than 1/2 the time constant of the dominant exponential, insert  $t = 1/2 \times 1/D$  in Eq (3).

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$$\epsilon^{1/2} > \frac{9D + G}{G - D}$$

which leads to a required G = 16.4 D. If the 10 per cent error point had been set at t = 1/D, the required G would be 6.25 D. These values justify the neglect of  $\varepsilon^{-at}$  when compared with  $\varepsilon^{-Dt}$  in Eq. (2).

From this example, it is evident that a large deviation of one time constant from another may be necessary to permit neglect of the effect of one with respect to the effect of the other. In this instance, recognition of the finite rise time of the forcing function is necessary unless this wave is characterized by an exponential with about 1/15 the rise time of the response.

## **Two Time Constant Consideration**

When the first order approximation becomes too inaccurate, some recognition of both time constants becomes imperative.

It is helpful to examine plots of the actual response of the system of Eq (1) for different ratios of the two time constants. A careful inspection may point out a simplified approach that would bypass graphical techniques and yield a readily calculable explicit solution for response time.

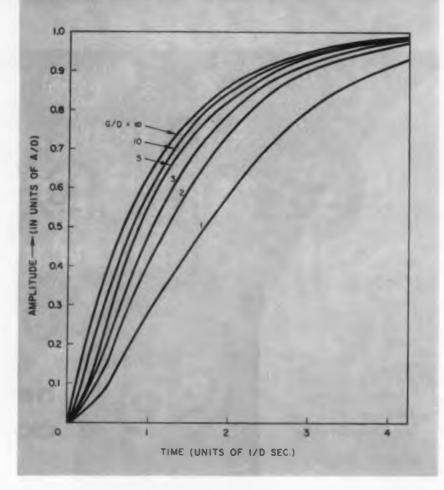
Fig. 1 is a family of such curves for various values of G. As G approaches D, the response approaches the form

$$\frac{I_{\epsilon}}{I_{b}}(t) = \frac{A}{D} (1 - \epsilon^{-Dt} - Dt \epsilon^{-Dt})$$

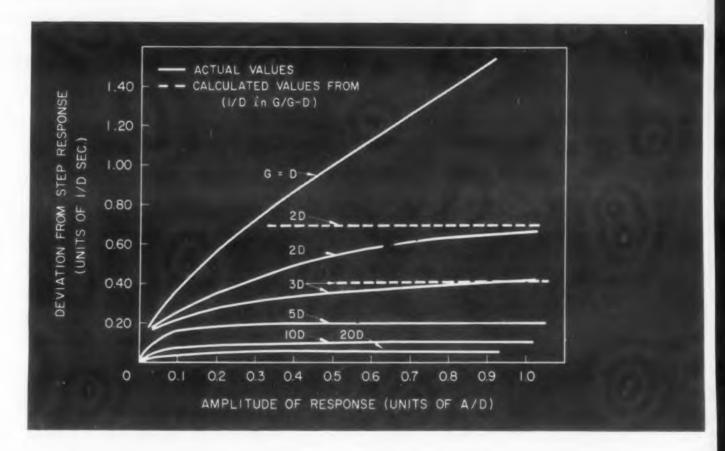
From this graph, a second plot, more useful to the circuit designer, may be obtained.

If the time lag between the step response and the actual response is plotted, (Fig. 2) as a func-

Fig. 1. The actual response of a system compared with the estimated response assuming a square driving waveform for various ratios of system time constants 1/D to driving-wave time constants 1/G.



**Fig. 2.** Deviations of actual network response from step input response.



tion of the amplitude, an interesting fact appears. For G/D ratios of three or more, the time deviation of the actual response from the step response rapidly approaches a constant, independent of the response amplitude.

As  $\hat{G}$  becomes greater than D, the term in  $\varepsilon^{-at}$  rapidly tends to become negligible compared with  $\varepsilon^{-Dt}$ . Hence, the correction term to the step response approaches

$$=\frac{A}{G-D}\,\epsilon^{-D\,t}\tag{4}$$

Now, for any given amplitude C, the step response equation determines a value t' as follows:

$$t' = \frac{1}{D} \ln \left( \frac{A}{A - DC} \right) \tag{5}$$

Using the correction approximation of Eq (4),



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the true response is closely approximated by

$$C = \frac{A}{D} \left[ 1 - \frac{G}{G - D} \epsilon^{-Dt} \right]$$

which yields

$$t = \frac{1}{D} \left[ ln \left( \frac{A}{A - DC} \right) + ln \left( \frac{G}{G - D} \right) \right]$$
 (6)

Hence, the time added to the step response approaches the difference between Eq (6) and

$$\frac{1}{D} ln \left( \frac{G}{G - D} \right)$$
 (7)

The dotted family of curves on Fig. 2 is calculated from this equation. For G = 5D and higher, at amplitudes greater than two tenths of the final value, they nearly overlay the true curves. Even for G = 2D, the calculated curve, which is the true curve's asymptote, is a fair correction above about half the final amplitude.

## **Simplified Calculations**

This fact simplifies calculations for the two time constant case a great deal. It allows consideration of the second exponential via a simple additive term to the explicit solution for time, achieved by considering one time constant equal

Consider a specific application. From Easely's calculations (which add the effect of collector capacity to the transistor response equations, and were derived first by Ebers and Moll<sup>2</sup>), explicit solutions for "turn-on" and "turn-off" time were

Since they are explicit for a single time constant, these same expressions can be modified by the correction term given in Eq (7) to account for a nonsquare input to a transistor amplifier. The following sample problem illustrates a typical design situation in which these observations apply.

## Sample Problem

It is desired to "turn on" a common emitter transistor with a current pulse which has a rise time (to  $1/\epsilon$  of the final value) of 0.06 µsec.

What magnitude should the base current have to achieve a "turn on" time of 0.43 usec, if the transistor has the following properties?

$$f_{\alpha \ min} = 15.9 \ \mathrm{mc} \ (\omega_{\alpha \ min} = 100 \times 10^6)$$
 $C_{c \ max} = 10 \ \mu\mu\mathrm{f}$ 
 $r_{c \ min} = 200 \ \mathrm{K}$ 
 $\alpha_{o \ min} = 0.95$ 

The final current required is  $I_{c1} = 10$  ma into 1 K load  $R_L$ .

**Design Procedure** 

From the input wave rise time of 0.06 usec, one may determine G. Thus

$$G = \frac{1}{t_{*}} [1 - \ln(\epsilon - 1)]$$

$$= \frac{0.46}{0.06 \times 10^{-6}} = 7.67 \times 10^{6}$$

From Easely's paper

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$$D = \frac{(1 - \alpha_o + R_L/r_c) (\omega_\alpha)}{(1 + R_L C_c \omega_\alpha)}$$

$$= \frac{(1 - 0.95 + 1/200) (100 \times 10^6)}{(1 + 10^3 \times 10 \times 10^{-12} \times 100 \times 10^6)} = 2.75 \times 10^6$$

$$G = \frac{7.67}{2.75} D = 2.79 D$$

Hence, the step response is  $(1/D) \ln (2.79/$ 1.79) = 0.44/D shorter than the actual response. Since 1/D equals 0.364 usec, the actual response is  $0.44 \times 0.364 = 0.16 \mu sec$  longer than the step response. Thus, for an overall "turn on" time of 0.43 usec, the time to be inserted in the step response equation is 0.43-0.16, or 0.27 usec. Thus, by Eq (3)

$$0.27 \times 10^{-6} = \left(\frac{2}{0.055 \times 100 \times 10^{6}}\right)$$

$$ln\left(\frac{I_{b1}}{I_{b1} - 0.9 (10 \times 10^{-3}) \left(\frac{0.055}{0.95}\right)}\right)$$

and the required base "turn on" current is

$$I_{b1} = \frac{2.1 \ (0.521 \times 10^{-3})}{1.1} = 1.0 \ \text{ma}$$

### Approximations Are "Safe"

The correction embodied in Eq (7) tends to be undefined as G approaches D. This is to be expected since the approximation which leads to this term, through Eq (4), becomes further and further removed from reality. However, Fig. 2 shows that the correction term is quite accurate for values of G three or four times the value of D, and may be helpful as a first order calculation for if the G as small as two times the magnitude of D.

In any case, the correction term always exceeds the actual error. Hence, any design based on calculated response time will be on the "safe"

### References

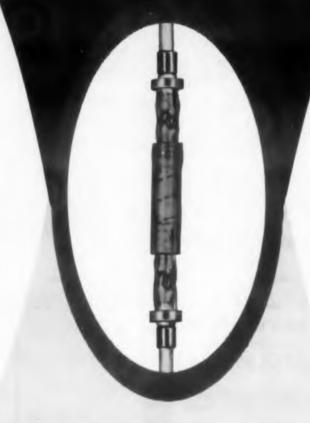
The Effect of Collector Capacity on the Transient Response of Junction Transistors, J. W. Easely, IRE fransactions on Electron Devices, Vol. ED-4, No. 1, pg. 6. large Signal Behavior of Junction Transistors, J. J. thers and J. L. Moll, Proc. IRE, Vol. 42, Dec. 1954, pp.

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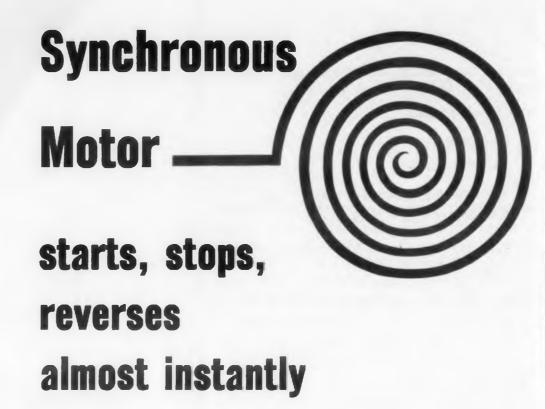
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47 PROSPECT STREET . WOBURN, MASS.

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ESIGNED for electronic control systems, this synchronous motor can start, stop, and reverse itself almost instantly. The small, maintenance-free unit operates at constant speed and produces a high torque.

Applications of the motor, called Slo-Syn and made by The Superior Electric Co., Bristol, Conn., include: remote control systems; numerical control systems; and automatic machines and apparatus. It is an enclosed, permanent-magnet type synchronous ac motor.

## **Electrical Characteristics**

The motor combines a speed of 72 rpm with a 150 oz-in. torque. Speed is synchronous with line frequency and at 60 cps it remains at a constant 72 rpm without gear reduction. Because the motor is

self-starting, no additional starting means are necessary.

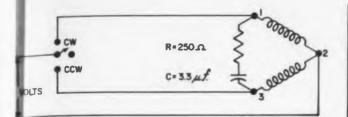
TORQUE - OZ.

Spinning the motor forward, instantly reversing or stopping it can be done with a single-pole, three-position switch since the unit has but three leads. The motor will start or stop in less than 0.025 sec, or about 1.5 cycles. Electrical or mechanical braking is not needed because it will stop in less than 5 deg of motor shaft rotation.

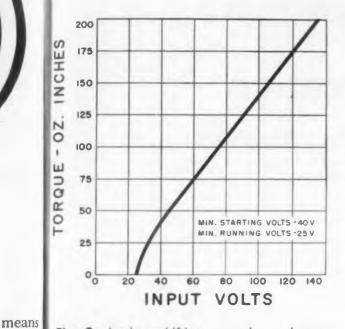
There is no excessive inrush current when the motor is turned on because the starting current is nearly identical to the operating current (0.3 amp max at 60 cps). The correct set of phase-shifting components is specified for nominal 60 cps duty. And with these components the motor will operate satisfactorily at any frequency between 40 and 70 cps. Rated for 50 C temperature rise at 40 C maximum



Fig. 1. This exploded view shows the various parts of the synchronous motor. No lubrication of the bearings is required for the life of the motor since the shaft is mounted on two prelubricated ball bearings.



**Fig. 2.** This graph shows the motor's torque at various input voltages, 60 cps.



**Fig. 3.** A phase-shifting network, as shown, must be used to operate the motor when the power source is a single phase.

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ambient under continuous operation, the unit weighs 6.5 lb.

### **Physical Dimensions**

Shaft diameter of the motor is 3/8 in. and its length is 1 x 3/16 in. The motor has a 4.25 in. diameter and a 4.75 in. depth.

When the synchronous motor is adapted for use as an incremental positioning device, de electrical pulses are converted into either 200 or 400 precise increments for one revolution of the motor shaft. The motor will maintain its rated torque for any stepping position. And since no ratchets are used, each step is made instantly without slip or clatter.

A phase-shifting network, required when the motor operates from a single phase source, can be had in an enclosure that is mounted on the end of the motor.

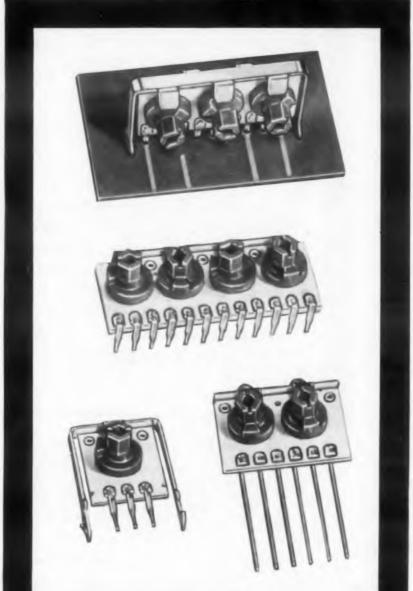
For more information on this synchronous motor, turn to the Reader-Service card and circle 101.

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Wattage Rating: 14 watt at 70°C. ambient

Breakdown Voltage: 1250 volts RMS, between adjacent

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End Resistance: Less than 1% of total

Initial Torque: 2 inch ounces average

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Freq. Range KMC	B a n d	Wave- guide Number	Bendix Type Number	RETMA Type No.	Mount Type	Recommended Mode of Operation (Note 2)	Anode Current Ma (Note 1)	Tube Drop Volts (Note 1)	Tune Excess Noise Ratio DB (Note 3)
1.12-1.70	L	RG-69/U	RXB103085 TD-21 TD-29 TD-33	6881 7101	10°E 90°H 90°H 90°H	D.C. D.C. A.C. and D.C. A.C. and D.C.	250 250 250 250 250	130 65 130 75	15.2 15.2 18.0 15.2
2.6-3.95	S	RG-48/U	TD-12 TD-22 TD-31 TD-32 TD-34 TD-35 TD-38	6358 6782	10°E 90°H 10°E 10°E 10°E 90°H 10°E	D.C. A.C. and D.C. A.C. and D.C. A.C. and D.C. D.C. A.C. and D.C. PULSE*	250 250 250 250 250 250 250 (250)	80 45 85 140 155 80 (90)	15.2 15.2 15.2 18.0 18.0 18.0 15.2
3.30-4.90	S	WR-229	TD-24 TD-30	6852	10°E	A.C. and D.C. A.C. and D.C.	250 250	65 110	15.2 18.0
3.95-5.85	C	RG-49/U	TD-10 TD-39 RXB103422	6356	10°E 10°E 10°E	D.C. PULSE® D.C.	250 (250) 250	70 (80) (110)	15.2 15.2 18.0
5.85-8.20	X	RG-50/U	TD-10 TD-39 RXB103422	6356	10°E 10°E 10°E	D.C. PULSE* D.C.	250 (250) 250	70 (80) (110)	15.2 15.2 18.0
8.20-12.40	X	RG-52/U	TD-11 TD-23 TD-40 RXB103093 RXB103394	6357 6882	10°E 10°E 90°H 90°H	D.C. D.C. PULSE* D.C. A.C. and D.C.	200 200 (200, 200 (100)	75 115 (85) (35) (50)	15.2 18.0 15.2 15.2 15.2
12.4-18.00	K	RG-91/U	TD-18 RXB103399 RXB10340J TD-41 RXB103411 RXB103254	6684	10°E 10°E 10°E 10°E 90°H 90°H	D.C. D.C. A.C. and D.C. PULSE® A.C. and D.C. D.C.	200 200 (100) 200 (100) 200	70 (110) (65) (80) (50) (40)	15.2 18.0 15.2 15.2 15.2 15.2
18.0-26.5	K	RG-53/U	TD-13 RXB103423 TD-42 RXB103411	6359	10°E 10°E 10°E 90°H	D.C. D.C. PULSE® A.C. and D.C.	200 200 (200) (100)	65 (100) (75) (50)	15.2 18.0 15.2 15.2
26.5-40.0	K	RG-96/U	RXB103251		10°E	DC.	(150)	(120)	15.2

NOTE 1: Anode current and tube drop are D.C. values. Values in parentheses are tentative.

NOTE 2: D.C. operation—Cathode at one end only.
A.C. and D.C. operation—Cathodes at both ends.
Pulse operation—Cathode at one end specially designed for pulse operation.

NOTE 3: The Excess Noise Ratio in DB is 10 log  $(\frac{T \text{ eff}}{290} - 1)$ 

\*If the anode current during the "on time" of a square pulse (of greater than 100 micro sec. duration) is nominally the same as the rated D.C. anode current, the tube drop during this period will be approximately the same as the rated D.C. tube drop.

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## Space Coordinate **Transformation**

Using High-Precision Resolvers

Gilbert H. Steinberg

Reeves Instrument Corp. Garden City, N. Y.

Problems in space navigation require detection of the vehicle's attitude in reference to fixed space coordinates. This article shows how resolvers are combined to transform velocity vectors and angles from one coordinate system to another.

Gil Steinberg is manager for resolver and gyro products for Reeves. He's interested in educating engineers on the capabilities of resolvers in coordinate transformation and wrote this article as a step that direction. Current and future trends, he says, indicate more and more use of "amplifierless" chains.

MODERN computer techniques for navigation and guidance usually involve linear transformations of vectors and angular relationships between two or more coordinate systems. Many aircraft and ships are supplied with a central inertial space reference system to and from which all guidance and fire control data are referred. The most convenient and efficient method presently available for solving transformation is through the use of high precision resolver chains.

Simplified representation of a resolver, Fig. 2(a), shows essentially a rotatable transformer with two windings in space quadrature on both primary and secondary. Fig. 2(b) illustrates the standard schematic representation of a resolver. The output equations are:

$$C = A\cos\theta - B\sin\theta$$

$$D = B\cos\theta + A\sin\theta \tag{1}$$

These equations describe a simple two dimen-

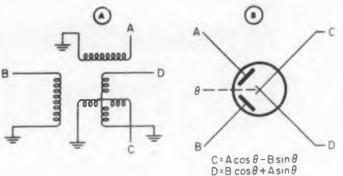


Fig. 2. Simplified circuit of resolver (a) and standard symbol (b).

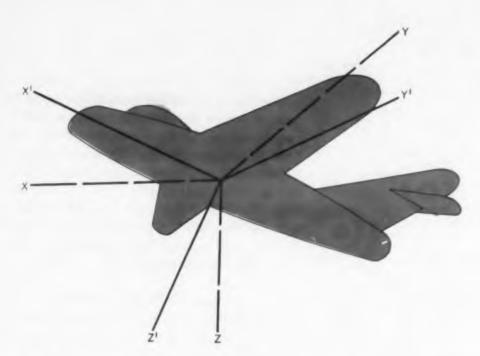


Fig. 1. Typical coordinate transformation problem x, y and z are fixed space coordinates; x', y' and z' are aircraft coordinates.

onal coordinate rotation. As shown in Fig. 3, and B are the (x, y) components of the vector in the original coordinate system and C and are the (x', y') components in the new coordiate system, rotated through an angle  $\theta$  with espect to the original coordinates. In matrix noation these equations can be represented as:

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$$\begin{bmatrix} C \\ D \end{bmatrix} = \begin{bmatrix} \cos\theta & -\sin\theta \\ \sin\theta & \cos\theta \end{bmatrix} \begin{bmatrix} A \\ B \end{bmatrix} \tag{2}$$

Since both coordinate systems are orthogonal, he inverse of the transposition matrix is equal to e transposed matrix and therefore:

$$\begin{bmatrix} A \\ B \end{bmatrix} = \begin{bmatrix} \cos\theta & \sin\theta \\ -\sin\theta & \cos\theta \end{bmatrix} \begin{bmatrix} C \\ D \end{bmatrix} \tag{3}$$

Equation (3) describes a coordinate rotation om the new coordinate system (x', y') back to e original system.

Equations 2 and 3 describe a coordinate rotaon through one degree of freedom. This can be strumented using only one resolver. The same sic techniques can be expanded to cover codinate rotation through 3 degrees of freedom.

## **Three Possible Rotations**

Assume (Fig. 1) that the aircraft is in level th; that is, the aircraft coordinates coincide ith the space coordinates. Three coordinate ro-

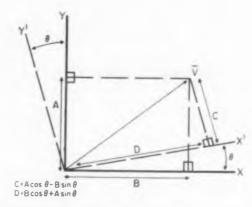
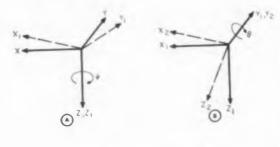


Fig. 3. Simple two-dimensional rotation.



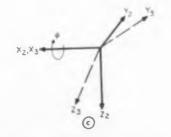
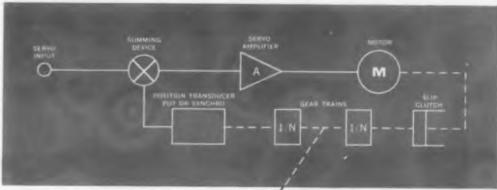


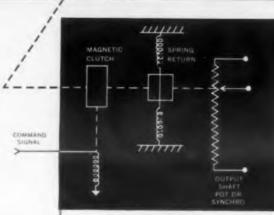
Fig. 4. Transformation from space coordinates to aircraft coordinates, around z axis (a),  $y_1$  axis (b) and  $x_2$  axis (c).

To provide an output Potentiometer-Transducer which can be readily engaged with a minimum angular error to a servomechanisms gear train when energized by an external command signal. The transducer must accurately return to a specified null position when the command signal is removed.



## A SOLUTION:

Provide an electro-magnetic clutch, spring return mechanism and rotary potentiometer. Assemble these parts into the required package with the resultant difficulties brought about by the mounting and coupling problems with a consequent increase in cost.



## THE OPTIMUM SOLUTION:

Technology Instrument Corporation's west coast engineering facilities developed and offer a unitized package consisting of an electro-magnetic clutch, spring return mechanism and rotary potentiometer as one compact assembly. The clutch will transmit high torque without slippage and has negligible angular engagement

error. TIC's unique spring return mechanism will accurately return the output

transducer to the desired null, yet requires low driving torque. TIC's unitized assembly replaces three (3) individual components with their inherent assembly difficulties.

## unitized package

## **GENERAL** INFORMATION:

Shaft Position Transducers can be linear or nonlinear potentiometers, synchros, linear transformers or digitizers. Spring return mechanism can be supplied designed to return to any desired point. A built-in slip clutch can also be furnished if the input torque can exceed the rating of the

## TIC UNITIZED PACKAGE HAS MANY APPLICATIONS,

SUCH AS: Auto pilots, altitude controllers, machine controllers, measurement and control problems, speed control, process control of temperature and flow, differential measurement, expanded scale servos, or any other problem requiring an

output, commencing at some specified servo position determined by an external command signal.



## TECHNOLOGY INSTRUMENT CORPORATION

Technology Instrument Corp. of Calif. North Hollywood, Calif. Acton Laboratories, Inc., Acton, Mass. Tucson Instrument Corp., Tucson, Ariz. Servotrol, Inc., Chicago, III. Altomac Corp., Canton, Mass.

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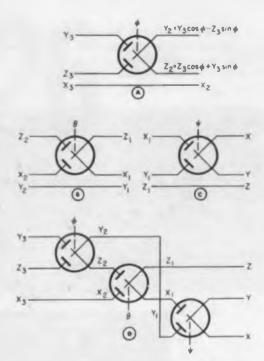


Fig. 5. To determine the vector in terms of space coordinates, three rotations are instrumented as in (a), (b) and (c), and tied together to complete the system (d).

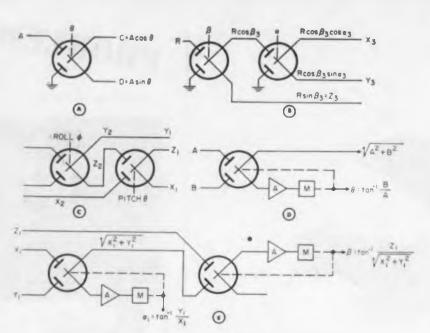


Fig. 6. Resolver with one input grounded (a); conversion from spherical coordinates to rectangular coordinates (c); transformation (d) from one rectangular coordinate system  $(x_2, y_2, z_2)$  to another  $(x_1, y_1, z_1)$ ; converting from rectangular coordinates to spherical coordinates (e).

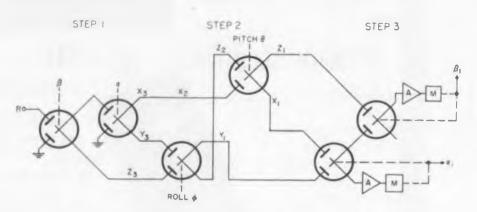


Fig. 7. Solution to antenna stabilization problem is instrumented like this.

tations are possible: (1) a rotation about the z' axis (yaw), (2) rotation  $\theta$  about the y' axis (pitch), and (3) rotation  $\phi$  about the x' axis (roll). It is apparent that space coordinates can be transformed to aircraft coordinates through successive coordinate rotations about each of the three axes.

The converse is also true: aircraft coordinates can be transformed to space coordinates by three successive rotations about fixed axes. The order in which the rotations are made will determine the final form of the transformation equations. While any order is correct and will give the same final results, to be consistent with current practice in the aircraft industry the angles will be taken in the order  $\psi$ ,  $\theta$ ,  $\phi$ , when transforming from space coordinates to airplane coordinates. The reverse order  $\phi$ ,  $\theta$ ,  $\psi$ , is taken when transforming from aircraft coordinates to space coordinates.

First rotation, Fig. 4(a), is taken about the z axis. The equations of this transformation are:

$$X_1 = X\cos\psi + y\sin\psi$$
  $X = X_1\cos\psi - Y_1\sin\psi$ 

$$Y_1 = Y \cos \psi - x \sin \psi$$
  $Y = Y_1 \cos \psi + X_1 \sin \psi$   
 $Z_1 = Z$   $Z = Z_1$  (4)

Second rotation, Fig. 4(b), is taken about the  $y_1$  axis. The equations of this transformation are:

$$x_2 = x_1 \cos \theta + z_1 \sin \theta \qquad x_1 = x_2 \cos \theta + z_2 \sin \theta$$

$$Y_2 = Y_1 \qquad Y_1 = Y_2$$

$$Z_2 = Z_1 \cos \theta + X_1 \sin \theta \qquad Z_1 = Z_2 \cos \theta - X_2 \sin \theta \quad (5)$$

Third rotation, Fig. 4(c), is taken about the  $x_2$  axis. The equations are:

$$X_3 = X_2$$
  $X_2 = X_3$   
 $Y_3 = Y_2 \cos \phi + Z_1 \sin \phi$   $Y_2 = Y_3 \cos \phi - Z_2 \sin \phi$   
 $Z_3 = Z_2 \cos \phi - Y_2 \sin \phi$   $Z_2 = Z_3 \cos \phi + Y_3 \sin \phi$  (6)

To illustrate the use of resolvers in this type of coordinate transformation let us assume we are given a vector  $(x_3, y_3, z_3)$  in the aircraft coordinate system. We are also given the angle information, which is supplied by gyros. We wish to determine the vector in terms of the space coordinates (x, y, z). This involves a successive ro-

tation through the angles  $\phi$ ,  $\theta$ ,  $\psi$ . The first rotation is into the  $(x_2, y_2, z_2)$  coordinate system using the equations:

$$X_2 = X_3$$

$$Y_2 = Y_3 \cos \phi - Z_3 \sin \phi$$

$$Z_2 = Z_3 \cos \phi + Y_3 \sin \phi$$
(7)

The Y<sub>2</sub>, Z<sub>2</sub> equations are similar to the simple case of a two dimensional rotation. This is because each of the three rotations keeps one axis fixed. Therefore, we can instrument the set of Equations 7 as shown in Fig. 5(a). In like manner the other two rotations can be instrumented as shown in Fig. 5(b) and 5(c). All that remains is to tie together the proper terminals as shown in Fig. 5(d) and we have mechanized the complete solution to our problem.

## **Convert Angular Systems**

It is frequently necessary to transform angles, instead of vectors, from one coordinate system to another. A typical example of this type of transformation is an antenna stabilization problem. We have a target at bearing angle as and depression angle β<sub>8</sub> with respect to the aircraft coordinates and wish to stabilize the antenna with respect to the pitch and roll of the aircraft. Pitch and roll angles are supplied by a gyro reference system. We can stabilize the antenna by deriving angles  $\alpha_1$ ,  $\beta_1$ , in the (x, y, z) coordinate system.  $\alpha_1$  and  $\beta_1$  are called respectively the antenna train and antenna depression angles. In this case we can neglect the yaw angle. In order to convert these angles we assume a vector R with a bearing angle  $\alpha_3$  and a depression angle  $\beta_3$ . Then:

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$$X_3 = R \cos \beta_3 \cos \alpha_3$$
  
 $Y_3 = R \cos \beta_3 \sin \alpha_3$   
 $Z_3 = R \sin \beta_3$ 

Also:

$$\alpha_3 = \tan^{-1} \frac{y_3}{x_3}, \ \beta_3 = \tan^{-1} \frac{z_3}{\sqrt{x^2 + y^2}}$$
 (8)

And, in general:

$$\alpha_n = \tan^{-1} \frac{y_n}{x_n}$$

$$\beta_n = \tan^{-1} \frac{z_n}{\sqrt{x_n^2 + y_n^2}}$$
(9)

Using this analysis we break our problem into three steps:

(1) Given angles  $\alpha_3$  and  $\beta_3$  and a reference voltage R we first instrument Equations (8) to put the problem in terms of the vector coordinates  $(x_3, y_3, z_3)$ .

(2) The coordinates must be rotated back through

roll and pitch angles to give us the coordi $s(x_1, y_1, z_1).$ 

Using Equations (9) we derive the antenna ing angle α<sub>1</sub> and the antenna train angle

o solve Equations (8), consider the output nations of a resolver with one input grounded, shown in Fig. 6(a). The equations are:

 $C = A \cos \theta$ 

 $D' = A \sin \theta$ 

By combining 2 resolvers with one input of each grounded, Fig. 6(b), we have solved Equation (8) as required in Step 1.

Step 2 is similar to the three axis problem except that we eliminate the yaw angle resolver. The schematic is shown in Fig. 6(c).

Step 3 involves finding the arc tangents using the coordinates derived in Step 2. This can be instrumented using the circuit shown in Fig. 6(d). The servo drives the rotor of the resolver until there is a zero output on the servo input winding. At this position the other winding has maximum coupling with the flux vector formed by the two inputs. Therefore, the outputs are =  $\tan^{-1} B/A$  and  $\sqrt{A^2 + B}$  as shown. Using this technique we can instrument Step 3 as shown in

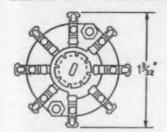
Combining the proper terminals of Steps 1, 2 and 3, we have the solution as shown in Fig. 7. Note from Fig. 7 that one of the outputs of the resolver which is driven to  $\beta_1$  is R. A rough check of the accuracy of the chain could be made by comparing this R voltage with the original reference voltage. Since lengths of vectors do not change during coordinate transformations these voltages should be equal.

## **Practical Applications Vary**

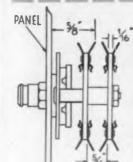
In actual system applications, the output of one resolver cannot be fed directly into a second esolver without introducing some loading errors nto the system. The accepted method of avoidng these loading effects is through the use of solation amplifiers, with one amplifier being used for each winding. When used in conjunclion with resolvers having special feedback windings compensation for temperature and frequency changes can also be made. Overall accuracies of better than 6 minutes have been ich eved in chains when compensated resolvers and isolation amplifiers were employed.

By using special loading networks and therhis ors in place of the amplifiers, resolver chains can be simplified. While this method has the virtue of convenience and simplified circuitry, it Is goined at the expense of some loss in system accuracy. . .

8, 10, 12 pos. miniature switch



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## SPECIFICATIONS.

Index —Double ball bearing, hill and valley type with stainless steel spring. Fixed and adjustable stops, and locating key available.

Shalls and Bushings - 1/4" shaft with 3/8-32 bushing is standard, 5/32" shaft with 3/8-32 bushing and 1/8" shaft with 1/4-32 bushing can be supplied also. Water seal bushings optional.

5 actions -8, 10, or 12-position, stacked in any number up to a total depth of three inches. The 12-position section provides up to 18 insulated contacts—12 on front, 6 on back. No insulating blocks are needed on back.

Poles	8-Position (45° throw)	10-Position (36° throw)	12-Position (30° throw		
1 pole	2 to 8	2 to 10	2 to 12		
2 poles	2 to 4	2 to 5	2 10 6		
3 poles	2 to 3	2 to 4	2 to 5		
4 poles	2	2 to 3	2 to 3		
5 poles		2	2		
6 poles			2		

Slip -Solid spring-silver alloy or silver-plated spring brass, fastened by solid rivets.

maulation - Stator is silicone fiber glass, meeting specification MIL-P-997 type GSG; rotor is KEL-F®, known for its excellent mechanical and electrical properties.

Finish - Commercial or 50 and 200-hour salt spray.



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LECTRONIC DESIGN • April 29, 1959

27



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Typical Electrical Characteristics at 25°C

2N1147 Series has solder lugs	2N1147	2N1147A	2N1147B	2N1147C
2N1146 Series has standard pins	2N1146	2N1146A	2N1146B	2N1146C
Collector to Emitter Voltage	30V	40V	60V	75V
Shorted Base (IC = 1 amp)	(Min)	(Min)	(Min)	(Min)
Saturation Voltage	1.0V	1.0V	1.0V	1.0V
(IC = 15 amps)	(Max)	(Max)	(Max)	(Max)
DC Current Gain (IC = 5 amps)	60-150	60-150	60-150	60-150
DC Current Gain (IC = 15 amps)	35	35	35	35
Absolute Maximum Ratings				
Collector Current Collector to Base Voltage Collector to Emitter Voltage Power Dissipation at 70°C	15 amps	15 amps	15 amps	15 amps
	40V	60V	80V	100V
	40V	60V	80V	100V
Case Temperature Junction Temperature	25W	25W	25W	25W
	95°C	95°C	85°C	95°C

TECHNICAL DATA

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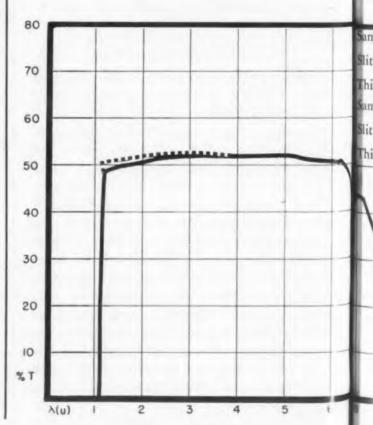
Ballistically spherical castings of polycrystall silicon shown at the IRE Show. In the foreground crude casting. After etching, the dome looks like one at the rear—note the mosaic polycrystal patte To right and left are polished domes.

## **Cast Silicon I-R** Domes

BLANKS, DOMES, flats and prisms of pusilicon for infrared systems are available production quantities. Cast from polycrystalli silicon instead of being ground, laboriously, fro a large single crystal, the new material show optical transmission and scatter characteristics most identical to the single-crystal parts.

Manufactured by Hughes Products Semica ductor Division, Newport Beach, Calif., the put polycrystalline material is cast and polished w

Fig. 1. (below) Comparison of transmission and em sivity of cast polycrystalline and single-crystal silia over a 1-14 micron wavelength range.



very little waste of raw silicon. The design of infrared optics for military and commercial systems becomes considerably more economical than here-

Casting, as a practical, in-production method for making infrared missile domes, was revealed for he first time at the IRE show in late March. The thiny, bluish domes shown above are ballistically spherical, pass infrared wavelengths, are opaque to light. In an infrared system an aspheric silicon lens would be protected by the dome, focus infrared radiation on a cooled or uncooled detector. Cooled detectors, which work in the three to five micron range, operate in an ambient on the order of 30 K and might consist of PbSe, InSb or GeAu. Environment ambient detectors work at 25 C, might consist of PbSe or PbTe.

A comparison graph of transmission characteristics shows no significant difference between the cast material and grown single-crystal silicon. See

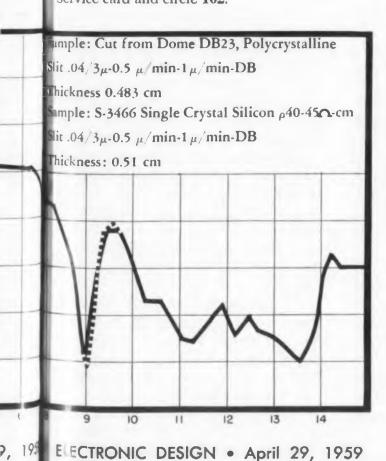
Scattering was compared, again showed no significant difference, within the ±5 per cent accuracy of the test. In the test, a single crystal aspheric lens focused a collimated beam on a pinhole in front of a band-pass filter (3.0 to 4.2 micron) and a cooled PbSe detector. The beam, from an 800 K source, was chopped at 90 cps. ristics Sample domes were placed in front of the lens.

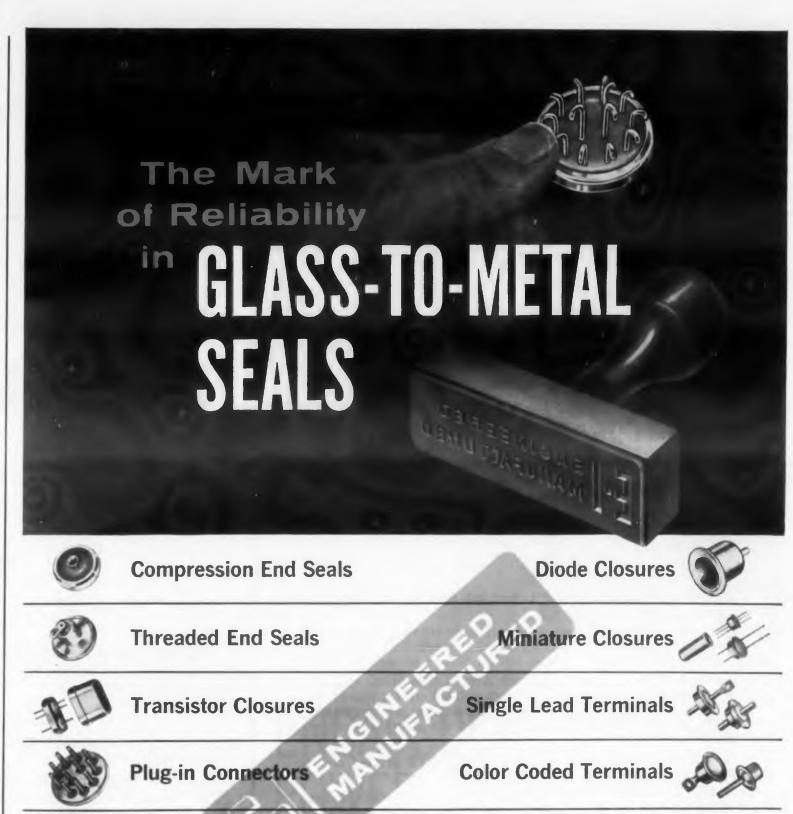
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Density of cast polycrystalline silicon is the Semico same as single-crystal-it is apparently entirely free of voids. It has approximately 80 per cent of hed will the breaking stress and modulus of elasticity of the single-crystal silicon.

and em For further information on cast polycrystalline tal silical silicon infrared components, turn to the Reader's-Service card and circle 102.







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**Custom Sealing Service** 



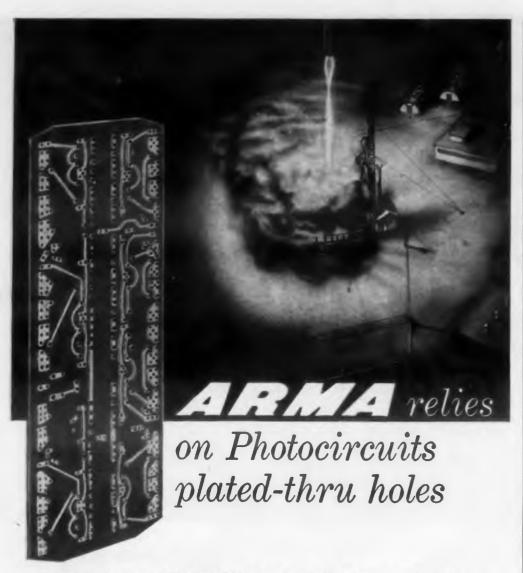
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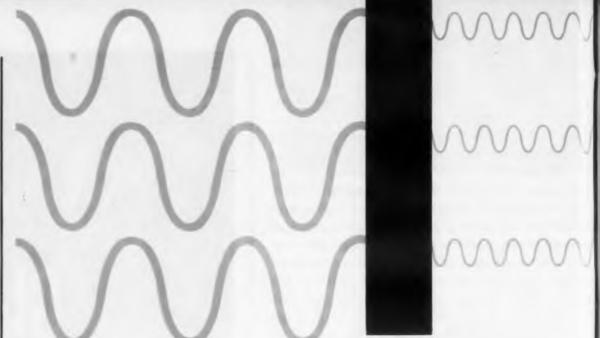
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# The New Look In Ripple Reduction

Bernard Daien

Kearfott Company, Inc. Clifton, N. J.

Engineers often use voltage regulators—not for regulation—but for ripple reduction. They pay for this in size, weight, and transistor dissipation. They don't have to.

ARGE ripple reductions are possible with substantial weight and volume savings when transistors replace reactors.

The cascaded emitter follower shown in the figure offers lower impedance and better stability than many previous circuits that performed essentially the same function. The divider across the input provides a constant fraction of the supply voltage to the base of the driver transistor. A capacitor filters this base voltage, leaving only the dc component.

The output voltage depends on this filtered dc, and is relatively independent of the collector ripple.

Several important differences distinguish this circuit from the series voltage regulator, which it resembles.

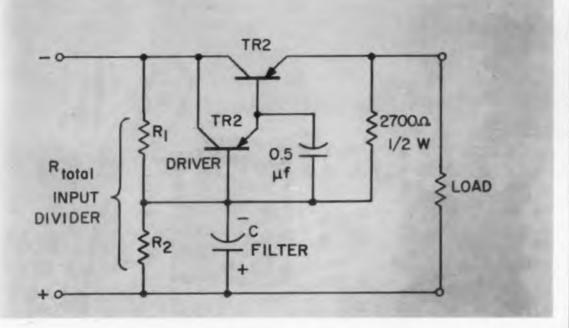
• The output is a constant fraction of the dc input. Hence a change in input level appears at the output. This eliminates

the rapid increase in transistor dissipation which occurs in the series regulator as the input rises and the transistor must absorb the difference between the rising input and the fixed output voltage. Since dissipation is reduced, the de-rippler handles heavy currents with a smaller heat sink, resulting in compact design

■ In the de-rippler the output is always less than the input. In a regulator, the input may fall below the fixed reference in which case the circuit drops out of regulation and the output ripple rise sharply.

To prevent dropout, an LC filter nust precede the regulator. It must have enough energy storage to maintain the input voltage during an undervoltage period. The ripple reducer does not dropout during undervoltage.

■ Dc overvoltage will destroy a true eg



This circuit can knock down ripple by a factor of 200. (Tr 2 can be several transistors in parallel for high load currents.)

ulator long before it would even overload the ripple reducer. Since the de-rippler's output follows the input, it is quite difficult to develop sufficient voltage across the transistors to punch through.

## **Quick Design Procedure**

Values for the components in the figure are calculated as follows:

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$$R_{total} = \frac{\beta_1 \beta_2 E_{in}}{10 I}$$

$$R_1 \approx \frac{R_{total} (1 + 0.5 E_r)}{1.1 E_{in}}$$

dissipation where  $E_r$  is the peak to peak input ripple,  $E_{in}$  is the nominal dc input voltage,  $\beta_1$ or must and  $\beta_2$  are the dc beta's of transistors and 2, and I is the maximum load cur-

The capacitor C is best chosen by substitution. Increasing its value will reduce the ripple till the desired reduction is obtained. Ripple reduction by factors of more than 200 are quite realistic.

The final step is to choose suitable transistors and heat sinks. The dissipation required of the transistors is approximated by the following expressions. For transistor 1

$$P_d = I \left( 1.5 + 0.5 E_r \right)$$

$$\frac{\beta_2}{\beta_2}$$

For transistor 2

 $P_d = I (1.5 + 0.5 E_r)$ 

The maximum voltage across transistors should be held to about 1.5 plus the peak to peak input ripple.

The maximum voltage across transistors is

$$E_{max} \cong E_r + 1.5$$

## A Typical Design

A 28 v bench supply, operating from the 60 cycle line, had a 2.8 v peak to peak ripple. The ripple reducer had to provide a 24 v output with no more than 15 mv peak to peak ripple. Output current was 1 amp.

An equivalent filter would have required a 0.8 henry choke with a 4 ohm resistance. It would have weighed 2 lb. and taken up 2-1/2 x 3 x 2-1/2 in. In addition it would have required filter capacitors and mountings.

The de-rippler, in a can no larger than the choke alone, weighed 1-1/4 lb. Net saving was four cubic inches and one pound with no attempt at miniaturization.

## For Higher Temperatures

The formulas given here apply when the transistors are germanium. Where higher temperatures call for silicon transistors, which are less efficient, the dissipation and voltages will be somewhat higher.

## WHY ENCAPSULATED?

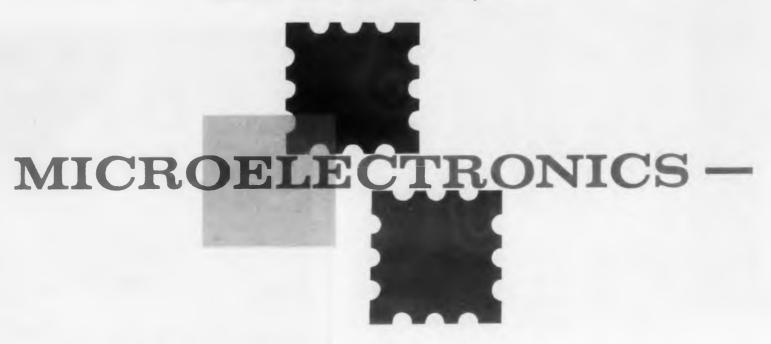
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## a new concept in packaging

Laurence D. Shergalis

Associate Editor

Less than two years ago, the flat-wafer concept of making ultraminiature electronic circuits was still in the laboratory. Since that time, with a boost from the Signal Corps and Diamond Ordnance Fuze Laboratories, the concept has developed rapidly. Industry is becoming more aware that a revolution in electronics packaging is taking place. To bring our readers up to date, *ELECTRONIC DESIGN* presents in this special report the latest techniques, processes and the current status of the work in microminiaturization.

M ICROMINIATURIZATION or microelectronics has never been clearly defined. But basically, it means making an electronic circuit as small as possible. Advantages of microcircuits are:

- Lower weight. They require little or no support and will withstand more g's.
- Better reliability. Microminature devices will perform through a wider temperature range at reliabilities about 50 per cent higher than standard units.
- Less space. Eliminating bulk and weight permits higher density packaging, thus permitting better systems for aircraft and missiles with greater fuel and payloads.

Assembly of electronics circuits has followed the classical method of hooking together a group of components with wires. Each resistor, capacitor, transformer, etc. is complete in itself and provided with leads, terminals or other forms of connecting devices.

These components are placed on a chassis and connected together with wires. More recently, they have been connected with printed wiring. But

the classical form factor remains the same. For example, resistors are generally round with axial leads. Their general shape has not changed much in the past 40 pears.

New materials and methods of production have resulted in making these devices somewhat smaller (Fig. 1). This decrease in size has been called miniaturization. The common hearing aid is a good example. But the degree of miniaturization has been limited by the relatively poor utilization of space by these classically-shaped components.

With the advent of printed wiring, engineers began printing conductors, resistors and capacitors. Concentrated effort toward improving techniques of making these flat-type components and flat-type circuits has led to different approaches to microminiaturization.

## Two Basic Philosophies

One approach to the problem is concerned with putting an entire circuit on one small flat plate. The other approach is that of placing one component on an extremely small flat plate and combining these plates to form a circuit (Fig. 2).

Both of these philosophies have valid reasons for their existence and are not in competition with each other. Each has its advantages and disadvantages for particular applications.

Diamond Ordnance Fuze Laboratories, Washington, D. C. is one center of activity of work by the military in utilizing the concept of placing the entire circuit on one plate (Fig. 3). Their 2D program (2D for two-dimensional) is aimed at putting as much circuitry as possible on one flat plate. But the method is economical only where a great number of these plates bearing the identical circuit must be reproduced. It will not pay if a relatively small number of these units are to be produced. A great deal of independent research by private industry is also in progress.

To gain the advantage of economical production for almost any number of units, the U. S. Army Signal Corps has initiated an extensive research, design and development program based upon the concept of micro-modular construction. Here, Fig. 4, components are constructed on 0.3-in. sq wafers and assembled in standard-size modules of standard shapes. Each module is a complete circuit assembly. But they are generally larger than the 2D units.

Defense Electronic Products of RCA is leader contractor on this project for the Signal Corps. Their objective is to provide a production oriented microminiaturization concept. Over 25 companies are actively engaged in various phases of this pro-

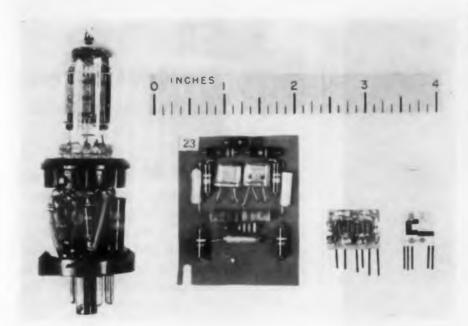
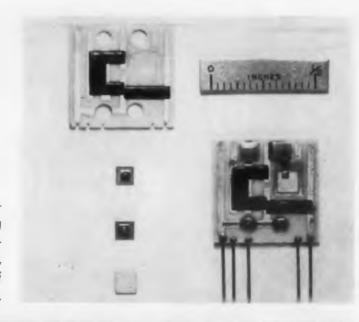
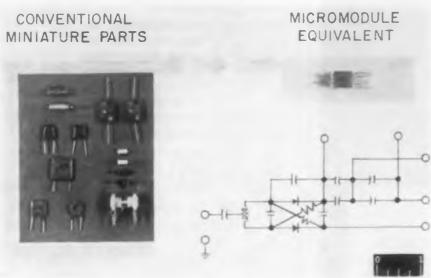


Fig. 1. Module using a standard miniature tube (left) compared to a transistor version (second from left), a "hearing aid" form of the same circuit (second from right) and the flatwafer version (right).

Fig. 3. Typical circuit assembly on one wafer using the DOFL approach. Complete module, lower right, has a component density of 2800 components per cu in.





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Fig. 2. Discriminator Micro-Module (right) contains the same number of components shown at the left.

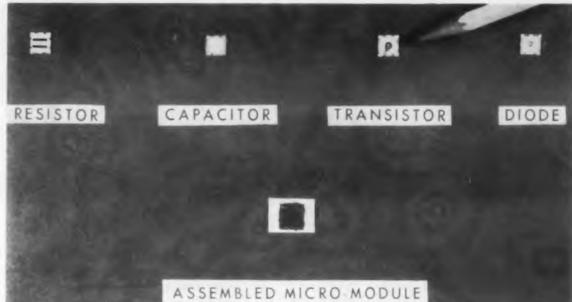


Fig. 4. Component parts of a typical micro-module.

# Nor P RESISTOR Formed by applying ahmic or non-nectifying contacts to a semiconductor wafer. Formed by utilizing the capacitance of a relatively large area of P-N junction. DISTRIBUTED CAPACITOR Formed by cambining the resistive and capacitive elements. TRANSISTOR Formed by utilizing diffused-base transistor techniques DIODE Formed by diffused-base methods

Forms of Texas Instruments, Inc. compo-

nents that are integrated into solid circuits.

Last month Texas Instruments Inc. announced a major advance in microcircuitry. Complete working circuits have been made, each measuring less than 1/4 x 1/8 x 1/32-in. They have a theoretical packaging potential of over 25 million parts per cubic foot as compared to the Micro-Module's packing density of about 500,-000 parts per cubic foot.

So far TI has succeeded in making develop-

So far TI has succeeded in making development models incorporating only transistors, diodes, resistors and capacitors. Inductors still present a problem, however.

Two working circuits have been completed. One is a multivibrator circuit containing as integral parts the equivalent of 12 components—two transistors, two capacitors and eight resistors.

The other is a phase shift oscillator containing five resistors, three capacitors and one transistor.

All these components are integral parts of one piece of solid semiconductor material. Either silicon or germanium may be used. Manufacturing techniques used involved controlled masking, etching and diffusion.

Greatest potential for these solid circuits is in applications where large numbers of repetitive circuits are required. The computer field would use units of this type to great advantage.

Samples or production units of the solid-circuit type will not be available for about a year, TI says. And then probably only a limited number of circuit types.

RCA announced last month their version of the solid circuit. Dr. Irving Wolff, vp, research, RCA Laboratories, said that their development of a computer logic circuit makes possible packaging densities up to 100 million parts per cubic foot. An important element in this development is the utilization of the uni-polar transistor.

Both active and passive elements can be built into a small piece of silicon as small as 0.000016 cubic in. To date, RCA has built only the computer logic circuit in this form. Investigation of other base materials such as gallium arsenide and indium phosphide is continuing.

RCA also recently announced the availability of their micro-modules (*ELECTRONIC DESIGN*, April 15, page 28). Sample quantities are available for sale to designers of military equipment.





gram with RCA and the Signal Corps with we over 100 others interested in participating.

As a result of the present micro-programs, the industry is expected to see increased use of digital equipment. In aircraft and missiles, the digital approach to instrumentation is becoming more common. This means packaging densities going up to a possible million components per cubic ft. An automatic machinery is being developed to hand the microcomponents which will result in great decreased production costs.

## Resistors

Several methods of making resistors are now it use. RCA, in their Micro-Module program has prepared resistors using a duPont metal glas frit-ink. The properties of this new type ink provide a temperature coefficient of the order of 150 ppm/C.

Several inks have been used with resistivity from 100 ohms per square to 35 K ohms per square Firing is done in a continuous belt tunnel kiln about 1300 F.

Resistors of the type shown in Fig. 5 are being used because they allow some adjustment. Resistor elements of this type are being supplied by Coming Glass and have tin oxide as the resistive material. Thus, resistors are available to the program with resistances ranging from 47 ohms to 100 k ohms.

Both Glass Products Co. and Mallory are supplying tin oxide type resistors in the Micro-Module program. Weston Electrical Instrument Co. is supplying 250 metal film resistor elements. The Weston process consists of metallizing the whole wafer first and then scribing the required resistor and dividing lines. Temperature coefficient of these units has been found to be less than 5 ppm/C. Value of the resistance changed about half a per cent during handling, but work is in progress to determine if this change can be prevented by suitable coating.

Weston, now Daystrom-Weston Instruments. Div. of Daystrom Inc., is making wafer-type resistors commercially available in small quant ties. They expect to go into production in about months. Units now offered have resistance range from 100 ohms to 1/4 megohm, with four resistance on a wafer. Obviously these four can be connected in series. Power rating is 1/8 w at 70 C or 1/6 at 125 C. Later, units ranging from 10 ohns to

CIRCLE 29 ON READER-SERVICE CARD

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Fig. 5. How the resistor pattern is laid out on both sides of the micro-module wafer.

I megohm will be available. These Weston units fulfill the requirements of MIL-R-10509C.

Allen Bradley and Chicago Telephone Supply Co. are also working on metal film resistors in conjunction with the program. Centralab is providing some carbon composition type resistors for evalua-

Nichrome film resistors are also being made at RCA for the program. The metal film is applied by vacuum deposition through an organic film mask previously applied to the wafer. The organic film, Kodak photo resist, is applied as a solution by brushing, is air dried and then baked at 100 C for 15 minutes. The coated wafers are placed on a photographic plate having the resistive pattern design and exposed to an ultraviolet light. Then they are developed, the result being a positive photographic plate containing the open lines of the resistive pattern. The resistive film is deposited by vacuum deposition. Nichrome alloy (80 Ni:20 Cr is deposited to give a resistive value of 50 ohns per square.

Resistor patterns are made from a drawing to deermine line length and configuration based on the 50 ohms per square value. The design is then

NEW **ECONOMY** OF CIRCUIT DESIGN with new NPN power transistors

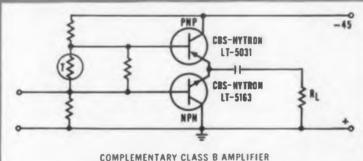
### ...in complementary push-pull circuits

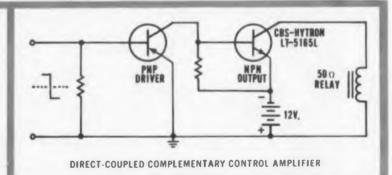
These new NPN transistors in the complementary push-pull circuit eliminate input and output transformers with many resulting advantages:

1. Economy. 2. Miniaturization. 3. Improved frequency response. 4. Ease of applying negative feedback.

### ... in complementary cascade circuits

CBS-Hytron NPN power transistors are also intended for singleended cascade output circuits, and three types are designed for use with inductive loads such as output transformers, motors and relays. The simplified direct-coupled circuits permit economies through elimination of components.





### FIRST COMPREHENSIVE LINE OF NPN POWER TRANSISTORS

Туре	Max. W Diss. (25°C Ambient°)	Max. VcBo	Max V <sub>CES</sub>	Min. hpe (I <sub>C</sub> = 0,5A)	Max, Thermal Res. °C/W	Similar PNP Types
	FO	R RESIST	IVE-LOA	DCIRCUIT	S	
2N326 LT-5165 LT-5163 LT-5164	7 12 12 12	35 35 60 80	35† 30± 45# 60#	30 30 30 30	8 5 5 5	LT-5025 LT-5025 LT-5031 LT-5039
	FO	RINDUCT	TIVE-LOA	D CIRCUIT	S	
LT-5165L LT-5163L LT-5164L	12 12 12	35 60 80	30¢ 45¢ 60¢	30 30 30	5 5 5	LT-5031 LT-5039 LT-5048

All seven types have: Max. collector current, 3 amps; storage temperature. -65 to +85°C; min. cutoff frequency, 150 kc. \*Adequate heat sink required tices = 1 ma. max.  $fl_{CES} = 10 \text{ ma}.$ dlcss = 300 ma.

New design economies in complementary push-pull and cascade circuits are made possible by these CBS-Hytron NPN power transistors. They feature high voltages . . . up to 80 volts. Their proven reliability (they meet the MIL-19500A specification) is what you might expect from specialists in reliable NPN switching and PNP power transistors. Check the typical circuits and abbreviated data for this versatile and comprehensive line. Write for complete technical Bulletin E-332 . . . and, if you wish, for Bulletin E-288 on CBS-Hytron PNP power transistors for complementary circuits.

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CBS-HYTRON, Semiconductor Operations

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CIRCLE 30 ON READER-SERVICE CARD



produced on Mylar film using black photographic tape to form the proper configuration. Master patterns have been worked out to provide resistor values ranging from 1 ohm to 33 K ohms.

Problems have been encountered in obtaining fine lines using the photo resist. Feathery edges were noticed and these are believed to be a result of internal reflection of light in the glass wafers. Ceramics also show a similar lack of sharpness due to their rough surfaces.

Tin oxide film resistors have also been produced. Resistance values of 25 to 1000 ohms per square have been obtained. Coatings prepared on glass plates were found to be easily reproducible. Steatite and Fotoceram are also being used as substrate material.

Practical resistors of platinum-gold alloy have been produced by the Royal Radar Establishment, England. They are in production and are reported to have excellent temperature characteristics. An alloy of 80 per cent gold and 20 per cent platinum gives a resistivity of 60 microhms per cm in a thickness of 100 Angstroms. Temperature coefficient is 0.025 per cent. An alloy of 60/40 gold-platinum has been found to have a resistivity of 75 microhms per cm in the same thickness with a temperature coefficient of 0.06 per cent.

This same group is also engaged in making high resistance units from films of nickel chromium. Problems have arisen in making the extremely fine lines required. Meanwhile, engineers at the Royal Radar Establishment are continuing their search for alloys offering much higher resistance. This group has been engaged in work similar to that of the Diamond Ordnance Fuze Labs. They report that their work in making actual resistors can be adapted to making an entire circuit. The necessary resolution required for units of this type can be obtained by photomechanical processes.

Recent research at Bell Telephone Laboratories promises some interesting results in this area using the old technique of cathode metal sputtering. In this process, ionized gas molecules bombard a cathode, dislodging atoms of metal which then redeposit on nearby surfaces.

A plate of the metal to be deposited is used as a cathode. The substrate on which the film is to be deposited is placed near it. After evacuation, argon or other suitable gas is introduced and maintained at a pressure of about 40 microns. When a voltage is applied, ionized atoms of gas bombard the cathode dislodging metal atoms or clusters of atoms which then deposit on the substrate.

Sputtering is one of the most convenient methods available for the production of thin films of the high-melting point metals. Thickness of the films may be controlled within narrow tolerances.

Tantalum and titanium, melting at 3000 C and 1670 C respectively have been laid down. These film show sufficiently high resistivity to be useful as resistors.

### **Need Fine Lines**

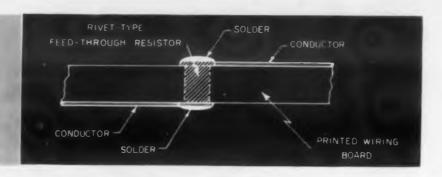
Being able to produce extremely fine lines is important in the production of precision resistors suitable for microminiature circuitry. Bell Labs has been successful through the sputtering technique in making lines only 1 mil wide. At Diamond Ordnance Fuze Labs., lines 2.5 mils wide with 2.5 mil spacing have been successfully reproduced.

At Bell Labs another development possibly more suited to the DOFL 2D approach rather than the Micro-Module approach is the "rivet type" resistor shown in Fig. 6. Length of the resistor is equal to the thickness of the printed wiring board or the substrate on which it will be used. The resistor then, acts as a feedthrough connection between the two sides of the board. Since the ends are flush with the board surface, the connections occupy no space and the resistor is completely hidden within the thickness of the board. International Resistance Co. is also reported to be developing a resistor of the same type.

### **Capacitors**

Diamond Ordnance Fuze Laboratories has done some work on vacuum deposition of silicon monoxide dielectric capacitors. This material has

**Fig. 6.** Cross section of Bell Lab's rivettype resistor mounted in the thickness of a printed-wiring board.



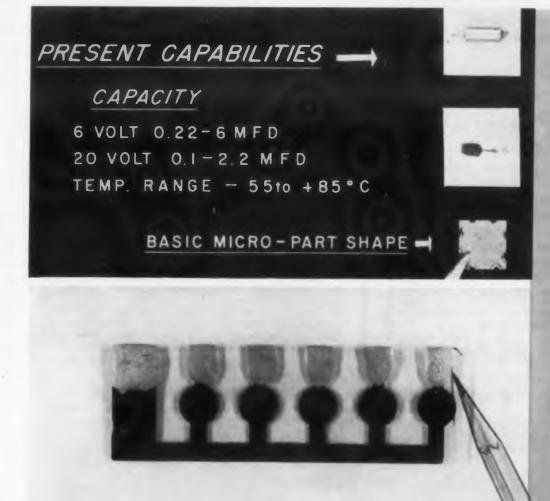


Fig. 7. Solid tantalum electrolytic capacitor of the current type (top). The sintered slug, bottom, has been adapted for the micro-module wafer.

Fig. 8. Bell Telephone Labs used a sputtering technique to make these miniature tantalum-oxide capacitors.

received a great deal of attention because of its ease of deposition. Using outer layers of various metals, it was found possible to obtain a wide range of capacitance per unit area, breakdown voltage, insulation resistance, dielectric constant and dissipation factor. The best values found were those using gold as the electrode film. It has high conductivity, resists oxidation and is easy to de-

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Fused silica was also used as a capacitor dielectric in experimental work at DOFL. It has excellent stability and its dielectric breakdown strength is 15,000 v per mil, the highest known. So far, the best experimental capacitors using

vacuum evaporation techniques were made using dielectrics of silicon oxide and aluminum oxide. Values given for these units show a capacitance of 0.005 microfarads per square cm and an insulation resistance of 100 kilomegohms. Loss factor was less than 1 per cent.

Thin-film ceramic capacitors promising to fulfill the needs of the Signal Corps Micro-Module program were developed at RCA's Advanced Development Laboratories. Initial work produced samples in the range of 150 µµf and 300 µµf. The 150 µµf capacitors contain a 0.001 layer of dielectric material while the 300 µµf units contained twice that amount. Gold was the electrode material: film was a silica-titanate compound on a ceramic base. All the units had a Q greater than 1000 measured at 100 kc. Temperature coefficient was less than plus or minus 100 ppm/C between 25 and 300 C. Breakdown strength was better than 600 v dc below 85 C.

### **Making Miniature Dielectrics**

Both Mallory and Magnavox are supplying tantalytic capacitor elements to the Micro-Module program. RCA has also been engaged in the development of dry electrolytics for the program. Work has been directed toward the development of tantalytic capacitors made with sintered tantalum slugs to achieve the extremely small size necessary. A capacitance range of 1 to 50 µf is being incorporated into the module structure. An example is illustrated in Fig. 7.

R. W. Berry of Bell Labs has produced printed capacitors, Fig. 8, by a combination of cathode sputtering and chemical methods. A tantalum film of proper shape and size is first sputtered on to the substrate. Then it is anodically oxidized to form a tantaluum oxide dielectric film. The counter electrode, a gold film, is then evaporated onto the dielectric to form the complete capacitor sindwich.

Aerovox Corp. has done some development work in the Micro-Module program. One of their new designs and techniques developed is exemplifind in their Cerafil capacitors announced re-(Continued on page 38)



These synchronously-driven choppers handle d-c signals as small as 10 \* volt. SPDT switching action. Sensitive, stable performance. Ideal for computers, servomechanisms, balancing circuits. Available with special features such as fungus proofing, grounded housing, mica-filled base, various contact percentages. Weight: 10 ounces. Prices from \$36.

Driving coils in 60-50, 40 and 25cycle converters are energized by 6.3 volt a-c. 400-cycle converters use 18 volts. Other specifications on chart at right.

MINNEAPOLIS-HONEYWELL, Wayne and Windrim Avenues. Philadelphia 44, Pa.

	ELECT	TRICAL CHAI	RACTERISTICS	5		
Part No.	354210-2	354210-3	354210-1	354210-4	355081	
Modulation Frequency	20-30 cycles	-30 cycles 40-45 cycles 50-65 cycles 50-65 cycles				
Switching Action (SPDT)	Each conta	(Make-before-break) Each contact closed 55% of each cycle (±2%) Other actions, as specified  (Break-before- make). Each contact closed 47% of each cycle			360-440 cycles Each contact closed 57% of each cycle (± 7%)	
Driving Coil Requirements		6.3 v, 60 ma at	rated frequency		18 v. 94 ma at rated frequency	
Contact Rating		100 micros	vatts at 6 v max.	; 1.0 ma max.		
Electrostatic Stray Pickup	2 x 10 <sup>-4</sup> volts per ohm of input circuit impedance				2 x 10-10	
Electromagnetic Stray Pickup	Less tha	Less than 2 x 10 <sup>-6</sup> volts, constant to within 2 x 10 <sup>-7</sup>				
Phase Shift	Output	voltage lags dr	iving phase by	17° ± 5°	Lags driving phase by 45° to 50°	
Symmetry		With	in 2%		Within 7%	
Shielding	Frame	Frame and coil shield, grounded through pin No. 2				
Load Characteristics		R	esistive or Indu	ctive		
Vibration Resistance	Output vi	Output voltage varies less than 2% with rates of vibration fro				
Weight			10 oz.		8.5 oz.	
Special Features	sist	-8816-A for anti- ant wiring, hern ble with side plu	netically sealed	case.	All 400-cycle converters are treated as shown at left	

## Honeywell Hist in Control



CIRCLE 31 ON READER-SERVICE CARD



One of the most promising developments in the field of microcapacitors is the monolithic structure for ceramic capacitors. Developed by Sprague Electric Co., these units are currently being incorporated into the Signal Corps Micro-Module program.

Sprague's capacitors are high-dielectric constant barium titanate units made by a layering process, Fig. 9. This capacitor consists of five active dielectrics. An early model, for example, consisted of layers each 0.0025-in. thick, occupying a volume of 0.620 by 0.355 by 0.018 in. Capacitance of a unit this size is 0.4  $\mu$ f.

Sprague manufactures two groups of capacitors by this process. One group utilizes a high dielectric constant material for bypass and coupling applications, and the other utilizes low dielectric constant materials for resonant circuits and other applications requiring high stability. Lead configuration of these units may be modified for particular applications.

Erie Resistor Corp. is marketing the Corning WL-4 miniature fixed capacitor. It is especially designed for printed-circuit applications.

Summing up the problems involved in making these extremely small units, industry must find a way to obtain high stability and low temperature coefficient. Very thin films are not practical if they are unstable. Stability will then be the dominant factor in developing a readily reproducible microcapacitor.

### Inductors

For the Micro-Module program, inductors for rf filters, both fixed and variable, and inductors to be used as transformers must meet the require-

Table 1—Characteristics of Ferrite and Metal
Magnetic Films

	Metal	Ferrite
Operating Speed	30 mµsec	1 µsec
Drive Power	400 ma into 5 ohms (transistor)	800 ma into 50 ohms (tube)
Repetition Rate	5 mc	500 kc

ments of MIL-C-15305A. Miniature ferrite core inductors are also undergoing development to be compatible with the program (Fig. 10). Variable inductors are being considered for tuning applications, although the Signal Corps has found electric tuning particularly attractive for certain applications.

Audio, power, and pulse transformers and inductors are also under development for the Micro-Module program. These units will be required to meet MIL-T-27A.

A zero temperature coefficient is required for most inductor applications. Ferrite material with NPO (zero temperature coefficient) characteristic was investigated to determine the effects of various protective coatings. Some coatings tried seemed to subject the ferrite core to undue stress and strain under varying temperatures. This, of course, nullified the NPO characteristic of the ferrite. A foam coating avoids the problem, and further investigation may reveal other suitable coatings.

RCA and the Signal Corps are looking for cores of higher permeability. They have studied results of adding molybdenum, cobalt, barium and yttrium to nickel-zinc ferrites. Ferrites with low temperature coefficients and high Q (greater than 100) for operation at 50 mc have been prepared. Inductance ranges up to 1.5 mh.

Coil impregnants are also being sought in connection with the Micro-Module program. Some epoxy resins have been tested, but no definite conclusions have yet been reached.

Properties of the impregnant must include corrosion resistance, moisture resistance, resistance to

thermal shock, and the necessary electrical properties. It must also be nonreacting with the adhesive used in bonding the coil or with the wire insulation. Work in this area is continuing.

At the Royal Radar Establishment, experiments show that metal is preferable to ferrite as a magnetic film, Table 1. Metal films have superior properties and are easier to evaporate as an alloy. Both metal and ferrite films have rectangular hysteresis loops and are suitable for use in memory planes.

These films consist of nickel-iron in the ratio of 8 to 1. Thickness must be limited to less than a micron or so because of excessive eddy current losses.

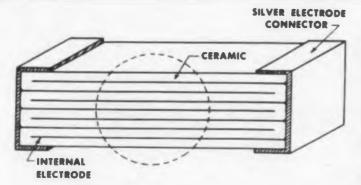
Varo Mfg. Co. has made inductors by vacuum evaporation techniques. In a simple rf or i-f transformer, a mask was used to deposit a spiral of pure metal on each side of a substrate. The inductance is controlled by the shape of the mask. The thickness of the substrate, which is the separation of the primary and secondary coils, controls the mutual inductance. Thus bandwidth can be controlled.

Inductors made by vacuum deposition possess the advantage of small size and, more important, reproductibility. By careful control of the substrate thickness and by using the same mask, these vacuum evaporated transformers come out the same.

### **Semiconductors**

Conventional semiconductor components are relatively large because of their cases. Actually the working material is a very small percentage of the total volume. To overcome the problem of the large transistor package, several techniques have been investigated at Diamond Ordnance Fuze Laboratories for working with caseless transistors. These techniques allow the active element of the transistors to be incorporated as an integral part of a ceramic printed plate, as shown in Fig. 11.

One of the most impressive developments in this area is the extension of photolithographic techniques for the fabrication of transistors. An-



**Fig. 9.** Construction of the Sprague Monolithic capacitor.



Fig. 10. Possible method of mounting a toroid on a micro-module wafer.

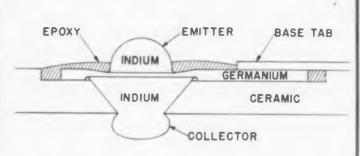


Fig. 11. Transistor integrated into a printedwiring board.

other method is to mask the transistor on the cenamic plate so that the leads may be vacuum deposited to connect the base and emitter contacts to the printed wiring.

In addition, two methods of encapsulating transistors have been developed, one nonhermetic and the other hermetic. The sealed units have been subject to various environments with no change in transistor characteristics.

Two methods have been developed by RCA for microminiature transistors for the Micro-Module program. One method consists of sealing the transistor element between two wafers. Each wafer is recessed to accommodate the transistor.

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In the second method, the transistor is placed in a recess in the wafer and covered with a metal lid. This circular lid is sealed to the wafer. Several methods of rf heating are being tried to effect the seals.

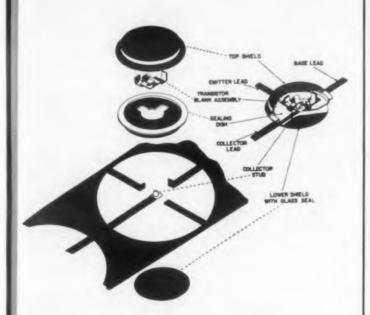


Fig. 12. Parts of Philco's micro-module transistor.

Philco's Advanced Research and Development group of the Lansdale Tube Co. is developing semiconductor devices for the Micro-Module program. These devices are expected to afford size and weight reductions of about 10 times that of current components, and may achieve packing densities of 500,000 to 600,000 components per cubic foot. Packing density of current equipment at best is about one-tenth that.

Basic components of a microminiature high-frequency transistor are shown in Fig. 12. The strip for electrode forming is 0.002-in. thick copper.

Hermetic sealing was a problem here, too. A minimum seal length of 0.05-in. is necessary for a reliable seal. This amount of seal length was obtained in the design shown.

An automatic production technique (Fig. 13) was worked out by Philco. Transistor elements





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MICROELECTRONICS'
PROGRESS

are dropped into the proper holes provided in the continuous strip. A cutter then slices the strip into individual wafers. Because the transistors are hermetically sealed, no special method of insertion is required.

### **Other Components**

Selenium rectifiers, diodes, crystals, relays, switches, miniature lamps, batteries are among the many other components now being developed in the microminiature size. Midland Mfg. is developing microminiature crystals for the Micro-Module program. These are to operate at frequencies of 7, 10, 20, 45.1, and 70 mc. Other companies also involved in the design of similar units include Bulova, Hycon Eastern and McCoy Electronics. Union Thermoelectric has also submitted a proposal in connection with the Signal Corps program.

Both Varo Mfg. and Servomechanisms, Inc. have reported work on thin film diodes using vacuum evaporation techniques. They feel that field-effect transistors may be possible using this technique also.

Miniature lamps have been developed at Diamond Ordnance Fuze Labs. Smallest of these, Fig. 14, is 0.1-in. long and consumes only 25 ma at about 1 volt. They are designed to operate on the limited currents available in most transistor circuits. They provide a very small source of il-

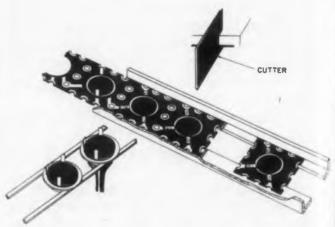
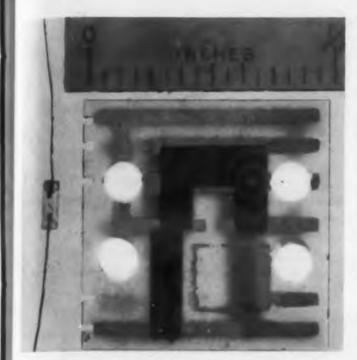


Fig. 13. Production of Philos's micro-transistors. Transistors are dropped into holes on the strip (left), then the leads are soldered and the wafers cut from the strip part of the strip part



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Fig. 14. Microminiature lamp is 0.1-in. long, draws about 25 ma at 1 v.

lumination that has been found to be visible from any point in a normally lighted room.

Batteries for microminiature applications are not yet in existence. RCA and the Signal Corps report that no work has been done in this area yet. However, the tentative specifications require batteries to have a nominal voltage of 15 volts with taps at 1.5, 3, 6, 9, and 12 volts also. Their energy yield shall not be less than 6500 milliwatt hours per cubic inch for the first 20 per cent drop. There will be a minimum of eight microminiature cell sizes with capacity ratings ranging from 10 milliwatt hours to 2000 mwh. Further, the batteries will be required to deliver at least 90 per cent of their rated performance at the end of 12 months storage at 70 F.

Switching and relay operations for all types of microminiature circuits will have to be carried out by transistors and other static means wherever possible. Other than that, the mechanical relays will have to be miniaturized as much as possible.

### **Assembled Units**

Both Diamond Ordnance Fuze Laboratories and the Signal Corps are doing a great deal of development work to find the best means to assemble all of these microminature components to the best advantage. Besides these two groups, many independent laboratories and industry groups have been engaged in the problem. Some of them are working in conjunction with these groups; others are working independently.

Among the private firms working on microminiaturization programs, one, Cleveland Metal Specialties Co. is already offering a microminiature computer circuit for sale. They have been No stoop, no squint, no painful nagging backache\*

## Buy this Testmobile and tilt your 'scope so you can read it!

Obsoleting all previous concepts in one brilliant breakthrough, -hp- engineers have achieved the ultimate device—the revolutionary 115A Oscilloscope Testmobile. Employing the radical Supermarket Cart principle (first described 1906 by A. and P.) -hp- 115A actually tilts an oscilloscope so you can read it, and lets you push it from place to place! Scope may be tilted up to 30° in 7½° increments; heavy chromed tube steel construction; big, locking, rubber-tired wheels; removable bottom basket; size 40" high x 23" wide x 29" deep, folds for shipment or storage; lightweight, only 28 lbs., \$80.

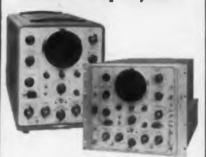
with thanks to our friends at Philco and Anacin

Still further probing the Unknown, -hp-engineers achieved the -hp-116A Storage Unit and 117A Storage Drawers. The 116A is a sophisticated cube known as a "box." It holds up to 3 plug-in units for -hp-150A/AR 'scopes; prevents dust and elbows in the circuitry. Yours for \$22.50. The 116A also holds up to three 117A drawers which in turn hold tools, solder, components and bubble gum. -hp-117A, a modest \$10.

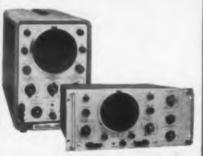
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engaged with work for Diamond Ordnance Fuze Labs, and their approach follows that of building an entire circuit of one printed-wiring wafer (Fig. 15). A binary counter made up of these commercially available units is shown in Fig. 16.

Denver Research Institute of the University of Denver has been active in all phases of microminiaturization in use today. W. A. Alford, R. W. Buchanan, and R. D. Seibel are generally responsible for work at DRI and have been concerned with design of conventional tube circuitry to achieve maximum packaging density and printed circuitry with tube and/or transistor components.

An internally sponsored microcircuitry program was started at DRI with a multivibrator chosen as the test circuit. This circuit has been realized by two techniques: 1. Resistive and conductive inks and 2. Vapor deposition. Fig. 17 illustrates the multivibrator made with resistive and conductive inks. Passive elements made with vacuum deposition techniques are shown in Fig. 18. In both cases, Raytheon CK-28 transistors were used for the active elements. An operating range of from 30 to 100 kc has been obtained by variation of the RC parameters.

One of the potted multivibrators is shown in Fig. 19 with a conventional circuit beside it for comparison. The final size of the potted unit is 3/8-in. in diameter and 5/16-in. tall. Resistor elements used in this circuit are representative of high and low values required in this circuitry. Deposits of manganese can apparently be used for resistances from 20 to about 500 ohms. Tellurium is also a good resistor material for the range between 1000 and 200,000 ohms. These materials have been vacuum deposited and a 5 per cent tolerance was obtained.

In the work to date, a disk of 0.020 thick barium titanate has been used for the dielectric base. Much difficulty was encountered in the mechanical processing of the barium. Other methods are being investigated.

One possible technique for obtaining the required dielectric involves the use of aluminum foil anodized on one side followed by vacuum deposition of an aluminum or silver layer on top of the oxide. Thus, capacitor plates are formed by the original foil and the deposited material with an aluminum oxide dielectric.

Work at Denver Research Institute also covers the problem of removing the case from transistor and diode elements. One method merely involves getting the commercial units from the manufacturer without the cases and putting the active elements into the proper place in the circuit.

The other technique would use microcircuitry approaches. Coupled with this are investigations of vacuum deposition and special heat treating processes. Effects of aging and potting of circuit components is also being studied.

### **Black-Box Circuits**

Varo Mfg. Co. has been concerned with fabrication of a functionally complete circuit rather than an assembly of components. These circuits are achieved by the alternate deposition of the connecting materials on a suitable substrate in the proper configuration and sequence.

Varo started on this project in 1956, the objective was to perform research and development in this field for use in the Army-Navy Instrumentation program. Their work has resulted in a concept that translates a lumped-constant circuit into one of distributed constants.

For example, a substrate of a high dielectric constant is used with a deposited film of conducting material on one side and a resistive film on the other. The result is a distributed-constant RC network of much smaller size than its lumped-constant equivalent.

Other circuitry made experimentally by Varo

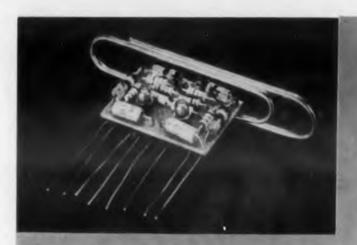


Fig. 15. Commercially available wafer-type circuit for a binary counter, being produced by Cleveland Metal Specialties Co.

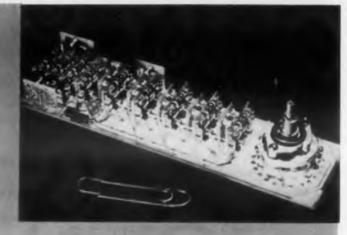


Fig. 16. Complete binary counter made of wafer-mounted circuits patterned after the DOFL technique.

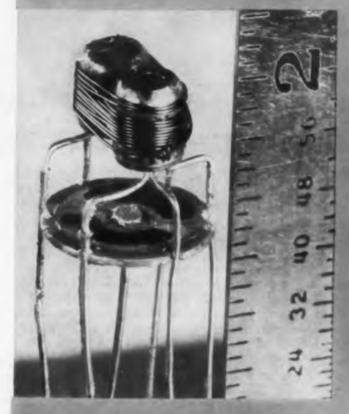


Fig. 17. Microminiaturized multivibrator made with resistive and conductive inks. Denver Research Institute made this unit.



Fig. 18. Passive elements of a multivibrator circuit made by vacuum deposition techniques.

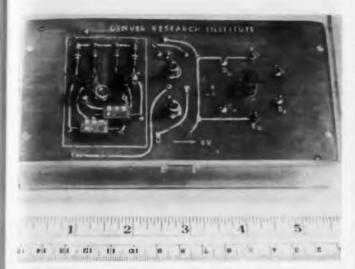


Fig. 19. Standard multivibrator unit (left) mounted on same printed-wiring board with Denver Research Institute's potted unit (right).

using their microcircuitry on parallel fabrication technique includes carrier generators, dc amplifiers, multivibrators as well as potentiometers, strain gauges, thermocouples and thin film magnetic memory elements.

Bell Telephone Laboratory has also been developing some concepts in microminature circuits. Their approach, like DOFL's and Varo's is to make one circuit per wafer. They prefer to think of wafers in many sizes. For example, circuits are being built on wafers 1, 2, and 3 in. square. As many components as is necessary should go on one board, they feel. And this depends entirely on the circuit subfunction rather than how many components could be jammed into that space.

International Resistance Co. is examining the microminiature problem from the production versus unit cost approach. In other words, they are more concerned with problems of reproducibility, testing, packaging, production machinery and yield factor. There must be an interaction between the production process and the product to achieve microelectronic packages that are worth making at all.

About 16 circuits made up of the Signal Corps Micro-Modules have been assembled and checked. These include rf and if amplifiers, signal generators, oscillators and others. Up to ten wafers are used in the assembly.

Several experimental units have also been built for demonstration recently. One is the RCA fountain pen radio. Also, RCA engineers have assembled various pieces of military communications equipment for demonstration.

Work in microelectronics at Wright Air Development Center Components Laboratory and the Air Force Cambridge Research Center has been underway for over a year. ARDC programs lean more toward basic research of existing physical Phenomena and their possible application to micominiaturization. (Continued on page 44)

### **MAGNESIUM**



### **NEW ALLOY DAMPS** VIBRATIONS IN U.S. ARMY NIKE HERCULES

Dow announces a new lightweight magnesium alloy with superior damping capacity for electronic bases, housings. K1A CASTINGS used on Nike Hercules guidance control system. Large sand casting is a housing for electronic guidance components. Small die casting is a mounting plate used within housing.

Damping capacity-the ability of a material to reduce vibration by absorbing energy-is a highly important factor in electronic equipment used in missiles and aircraft. The performance of sensitive instruments can be severely affected by high energy vibrations generated in missiles in take-off and flight.

A big step forward in solving this increasingly critical problem is the development of KIA, a new magnesium alloy. Used in electronic bases and housings, this lightweight alloy eliminates complex mounting and suspension systems that often take up precious weight and space in missiles.

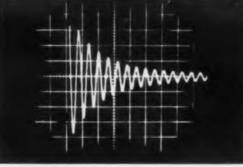
This new magnesium alloy has vibration damping characteristics much better than cast iron, aluminum or other magnesium alloys. Its heat conductivity and diffusivity are approximately twice that of standard magnesium alloys, thus making possible substantially reduced environmental temperatures for electronic instruments. Welding and machining have no adverse effect on the damping properties of K1A.

Bell Telephone Laboratories has done extensive work in determining properties and characteristics for the alloy, and in establishing its suitability for Western Electric's work on the guidance control system of the Nike Hercules. K1A is now available in the form of sand and die castings.

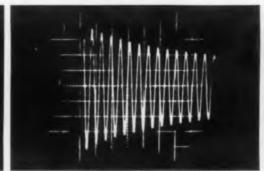


**NEW BROCHURE on damping** characteristics of magnesium discusses K1A, other mag alloys. Contact the Dow sales office OF THE DOW CHEMICAL COMPANY, Midland, Michigan, Magnesium Sales Dept. 1310BC4-29.

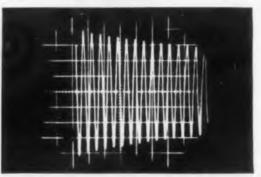
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355 ALUMINUM



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Fig. 20. Typical wafer-mounted flip-flop made by MF Electronics Inc. Pencil points to transistor leads, Generous allowance after bending puts more strain on the board rather than the leads. (Right)



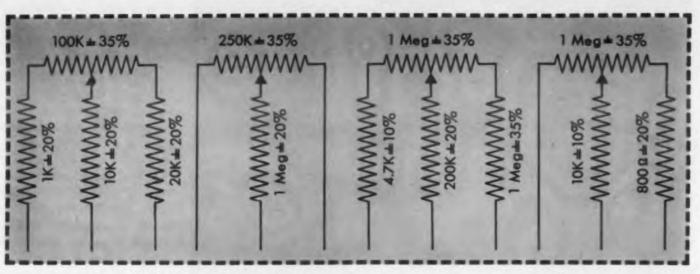
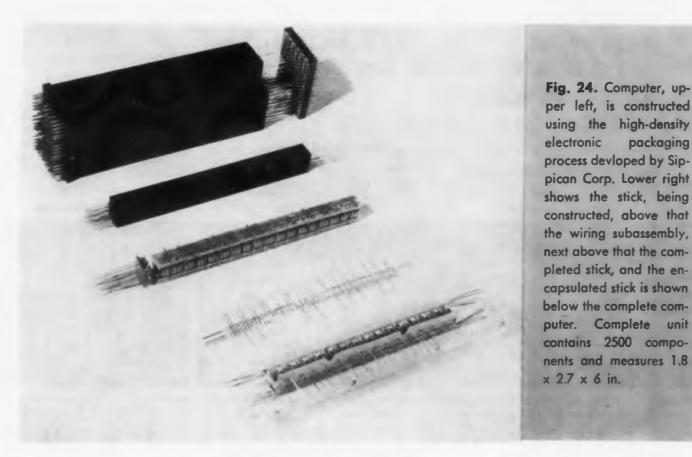


Fig. 22. Typical circuit for the variable-resistor assembly shown in Fig. 21.



per left, is constructed using the high-density electronic packaging process devloped by Sippican Corp. Lower right shows the stick, being constructed, above that the wiring subassembly, next above that the completed stick, and the encapsulated stick is shown below the complete computer. Complete unit contains 2500 components and measures 1.8  $\times$  2.7  $\times$  6 in.



Fig. 21. Miniature variable resistors. This Centralab plate is 2-1/4 in. long. Capacitors and fixed resistors may be screened on the other side.



Fig. 23. Centralab's tour-stage transistor amplifier, below, compared to wafer-type assembly of the same circuit, top. Single stage amplifier made by layering techniques is at the right.

Modules about the size of a postage stamp have been produced by M F Electronics Co. These units are in the form of flip-flops, multivibrators, oscillators and others. They are about 5/16-in. thick and have a components density up to 125,000 parts per cubic foot.

A typical flip-flop made by M F Electronics Co. (Fig. 20) shows on method for mounting transistors in tight places. Here the transistors have been inserted into the board through hole placed so that when the leads are bent, the strain will be taken by the board. This relieves the strain on the glass header and special bending tools are not required.

Centralab introduced the concept of packaged circuits in connection with military devices manufactured during World War II. Their basic philosophy of their approach has been to develop packaging methods of maximum flexibility that can be adapted to the specific requirements of a given product or circuit.

The objective on their standard PEC Couplates has been to design a package that is essentially two dimensional, eliminating thickness as a dimension of the circuit. A thin ceramic plate with wiring, resistors, capacitors and other components, printed or screened on it, is the basic form. Many times, however, to achieve maximum component density and take advantage of the space available, custom built shapes are used. The plate also serves as a base for the attachment of other components, such as variable resistors, transistors, diodes, etc., that cannot readily be reduced to a two dimensional form.

A typical example of this technique is illustrated in the multiple miniature variable resistor shown in Fig. 21. In addition to the four variable resistors, as many as nine fixed resistors can be screened on the same ceramic plate. Fig. 22 is its schematic. Fixed capacitors, transistors and other components can be attached to the reverse side of the ceramic base plate and, where fewer variable resistors are required, the entire package can be made proportionally smaller.

In some applications, Centralab found that the two dimensional concept results in a package that requires a larger area than might be available in the equipment. Under these circumstances a layering technique (not to be confused with module construction), utilizing several ceramic plates, is used. Under certain circumstances this might result in a package of greater thickness, but of such a shape (Fig. 23) as to be better adapted to the available space. Here, the Centralab TA-11 unit contains a transistorized four stage amplifier constructed on a ceramic plate. This same four stage amplifier constructed by a layering technique is shown directly above the TA-11.

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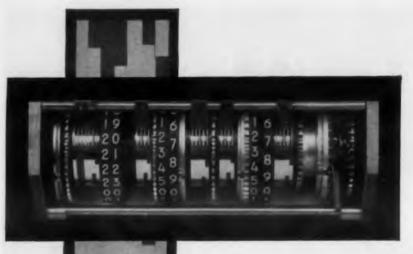
### **Packaging with Standard Parts**

High Density Electronic Packaging is the name used by Sippican Corp. to describe their method of assembly. Their objective has been to develop an economic process for improving packaging density by more than one order of magnitude over the best density obtainable with printed circuit techniques. This has resulted in a series of developments in layout technique and positioning devices which use photographic processes.

Sippican uses spot welding for making most of the connections and have developed ways of achieving totally "hard" cabling systems which eliminate the "haywire" needed for conventional assemblies. They are using a variety of techniques for heat removal with considerable success.

High Density Electronic Packaging is complementary rather than competitive with both major Micro-Module programs. The standardized modules contemplated in the Signal Corps program will demand interconnections, and the module groups so developed will need cabling systems of one sort or another. High Density Electronic Packaging is a process involving a depth





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Dielectric (Volts DC)												
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	(2) Inertia	measured	at maxi	mum trip		(4) At	room tem	perature.				

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of techniques, but two of its major features are a system for highly compact intramodular wiring and a number of techniques for "hard" intermodule cabling. These techniques, which are themselves in a state of rapid evolution, support

the Micro-Module program.

High Density Electronic Packaging (Fig. 24) results in a density of well beyond one order magnitude improvement over printed circuit techniques, the typical 30x reduction in space being approximately 1.5 orders of magnitude. The density figure obtainable over a complete system with High Density Packaging, using currently available and well-proven components, runs in the region of 1 or 2 x 105 components per cubic foot. Announced objectives of the micro-module program are considerably below this density level: 600,000 components per cubic foot being a figure which is often mentioned in relation to parts of systems, with 250,000 per cubic foot mentioned for complete systems.

### **Variable Components**

It is generally agreed that variable components should not be used. Variable capacitors are too bulky and may be replaced with a few smaller components. Electric tuning by means of Pacific Semiconductor's Varicap is one possible way to eliminate variable capacitors.

RCA and the Signal Corps eliminate the usual variable tuning of if transformers by using a deposited metal capacitor which is tuned by eating part of one electrode away with an abrasive spray Thus, an if amplifier is tuned by "sanblasting" the capacitors until the right value is reached.

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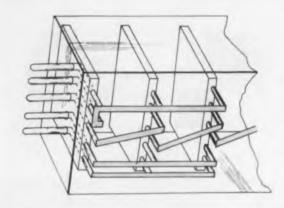
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While rotating, or adjustable components can be made very small, the limiting factor is the size of the operator's hand or fingers that has to turn the knob. There is little problem when the adjust ment is made by means of a screwdriver. But a continuously tunable radio receiver or a device requiring manual switching or operation of any kind cannot be made so small that the controls cannot be operated.

### Interconnection of Modules

Interconnection of microminiature devices is of great concern to everyone working in the fild Here reliability becomes a problem. More important is the fact that the connections between n od



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Fig. 25. How a stack of DOFL's 2D wafers can be interconnected. Interconnection wires are deposited by copper reduction.

ules or components may become larger than the assembly itself.

Methods for connecting extremely small wafers having volumes of about 0.005 cu in. have been under investigation at Diamond Ordnance Fuze Labs. Their basic technique involves stacking the wafers so that all leads protrude from one side of the assembly (Fig. 25).

The assembly is then encapsulated and the side containing the leads is faces off to expose the crosssections of the wires. These are the interconnecting points. Interconnecting these points was accomplished using chemically deposited copper or by printed silver wiring.

Finer connections were produced using the deposited metal method than with the screened silver method. In the latter method, ink flows through the stencil, resulting in wider lines than desired. It should be noted also that interconnecting lines have a finite resistance and must be taken into account in the circuit.

Interconnections of the Signal Corps Micro-Modules are made between the wafers by conductors placed in the groove cut into the edges. By properly positioning the wafers and locating component leads, an entire circuit can be wired using the 12 connecting wires.

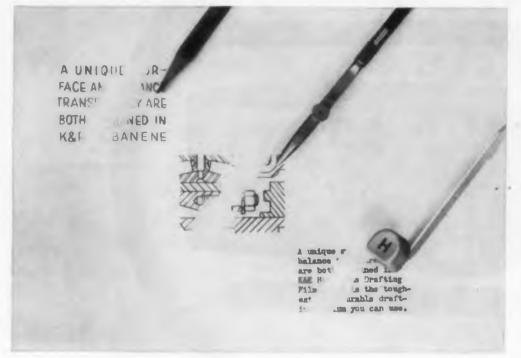
To interconnect the modules, RCA and the Signal Corps are investigating the use of Flexprint, a flexible printed-wire cable made by Sanders As-

According to Sanders, a Flexprint wiring system provides a degree of space conservation proportional to that offered by the module itself, while affording the production uniformity characteristic of its photo-mechanical manufacturing process. Sanders' chief efforts have been directed toward increasing the density of interconnecting wiring within and between assemblies of both conventional and micro-size. The ultimate size of a funclional cluster or train of modules depends to a great extent, they feel, on the physical characterislies of the wiring system used to interconnect its individual units. (Continued on page 48)



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**Range of Three Regular Instruments!** 

It's the most versatile Sweep Generator in the electronics industry... this one instrument covers all your needs from 1/2 MC to 1200 MCS, for IF's, radar, video, telemetering and communications!

Specifications: In two ranges—0.5 MC to 400 MC and 275 MC to 1200 MC the instrument supplies a sweep signal with center at any frequency from 500 KC to 1000 MC and with sweep widths as broad as 400 MC and as narrow as 100 KC. The RF output—carefully monitored by matched, crystal diodes feeding a two-stage, push-pull AGC amplifier—is flat within  $\pm 0.5$  db at full sweep width up to 800 MCS and +1.5 db from 800 MCS to 1200 MCS. When using sweep widths as narrow as 20 MCS flatness at any center frequency is approximately \$126000  $\pm 0.15$  db.

.25 volt RMS on VHF-.5 volt RMS on UHF!

## SWEEP WIDTHS!

From 100 KC up to 400 MCS!

### OUTPUT!

Flat to  $\pm .5$  db on widest sweep width!

### **MODEL 900A IS NOW IN QUANTITY PRODUCTION!**

Write today for on the spot demonstration of this versatile instrument!



ELECTRONICS CORPORATION Industrial Products Division

The Jerrold Building CIRCLE 39 ON READER-SERVICE CARD Philadelphia 32, Pa.

MICROELECTRONICS' **PROGRESS** 

Bending radius is the most significant figure in terms of volume saving if the full potential of the micromodule concept is to be realized, and the amount of space occupied by each bend in the wiring system must be held to a minimum if the overall group is to be packaged in the most effective manner. Sanders' experiments indicate flexible printed wiring interconnection of two mircromodules at a volume penalty of only 0.014-in. This is the thickness of copper conductor that can be bent back on itself while still providing adequate (0.0012-in.) insulation at the outside radius of the 180 deg bend. One form of flexible interconnection is shown in Fig. 26.

Sanders estimates a volume saving of 50 per cent achieved by making interconnections on a flat layer of flexible circuitry and post-forming the layer around a module grouping, Fig. 27, instead of making wire interconnections. The saving is 90 per cent compared with conventional printed circuit techniques at a standard center-to-center distance of 0.4-in.

Complex wiring harnesses have also been constructed using a new matrix-forming technique which permits feeder connections to be attached at any point along a main conductor by either spot welding or soldering, with complete insulation of the joint from both atmosphere and adjoining circuits. Investigations in the area of sonic welding indicate that this method of joining conductors is also capable of development, with the possibility of permitting further reductions in the size of both micromodules and interconnections.

### **Production**

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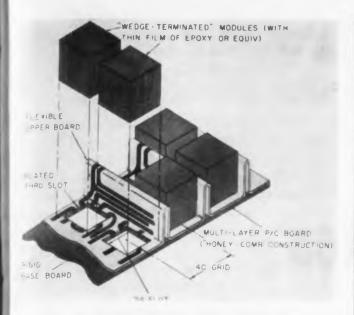
ELEC

Saving space and weight is not the only advantage of microminiature devices. Since the parts are generally uniform, they lend themselves easily to automatic production methods.

Micro-Module wafers were designed with production in mind, and equipment has been de-



Fig. 26. Flexible printed wiring harness developed by Sanders Assoc. for interconnection of micro-modu es



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Fig. 27. How Sander's Flexprint wiring can be formed to make the interconnections between modules.

signed for automatic assembly of the wafers. While this is preliminary equipment, the final phase of the program will involve the design and construction of prototype production machinery. All phases from production of the components, their assembly and their integration into equipment subassemblies is part of the program.

Diamond Ordnance Fuze Laboratories has conducted a survey of equipment now available or adaptable to production of these units. Their survey covers all types of circuit elements, discusses their properties as related to physical handling, and some equipment that might do the job.

### For the Future

Engineering samples of Micro-Modules will be available to the military for prototype development late this year. Copies of 17 types of components currently under development will be supplied to equipment manufacturers. They will familiarize themselves with a few working models. Status of the Signal Corps Micro-Module program will be detailed in the May 13th issue of ELEC-TRONIC DESIGN in an article by Vincent Kublin.

Circuit designers will have a major role in the future of microelectronics. Their job will be to design circuits to eliminate large volume components. Almost every branch of science will be involved in microminiaturization.

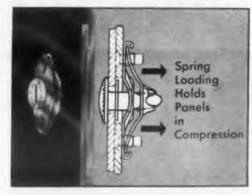
And the importance of the concept is well illustrated by a statement made recently by W. Waiter Watts, Group Executive Vice President of RCA. He said, "At the risk of appearing brash, I want to make clear at the outset my belief that the revolution now taking place in materials, devices and techniques in what we call electronic components will reshape the entire electronics industry in the next few years."

## Quick-Opening Fasteners

## Selecting Small Fastenings for Metal Closures

"Use captive fasteners wherever feasible . . . Avoid the use of loose washers and loose nuts . . . Fasteners on equipment covers should be operable either with no tools or with standard hand tools"\*

(John D. Folley, Jr. & James W. Altman, Research Scientists, American Institute



### Quarter-Turn Fastener

Lion Fasteners open and close with a 1/4 turn, hold sheets tightly under the compression of a rugged spring. Quickly operated and fully retained in the outer panel, they are approved under U.S. Government military specifications. Stud and receptacle float for easy alignment and simplified hole preparation. Flush, oval, wing, knurled, ring, and key head styles available. Sizes-No. 2, No. 5, and High Strength for extra heavy duty.

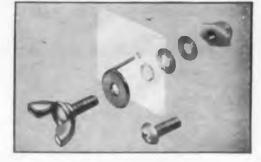


Cabinet Latch

Just drill a hole, push the fastener stem through, and slide the special push-on

clip into place. No welds, screws, bolts or rivets: the fastener is permanently installed in seconds!

Adjustable to any grip length or panel thickness, the pawl is fixed in place by a single set screw. The fastener's brightly finished knob is set off by a plated washer. Also furnished with screwdriver operated flush head.



### Adjustable Panel Latch

Small doors and panels can be fastened with greatest speed and lowest cost with the Southco Adjustable Latch.

The entire fastener is quickly installed through two holes punched in the door, no bolts or rivers are needed.

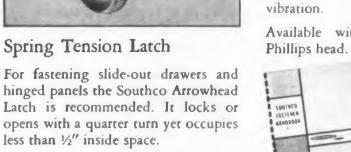
It operates with a quarter turn, requires no striker plate. An extra twist after the nylon pawl is engaged pulls up the door to form a seal and eliminate vibration.

Available with wing, knurled, or

Free

Fastener

Handbook



Doors are held under spring tensiona push against the arrowhead knob relaxes this tension, allows operation with fingertip ease. Drill a single hole for installation—no fastening to the door is necessary. No striker plate is needed.

Pawl stop is eliminated—arrowhead shows at a glance exact position of



Send for your free copy of Fastener Handbook No. 9, just released. Gives complete engineering data on these and many other special fasteners. Forty-eight pages, in two colors.

Write on your letterhead to Southco Division, South Chester Corporation, 235 Industrial Highway, Lester, Pa.



\* Quotation from "Designing Electronic Equip-ment for Maintainability"; Machine Design, July 12, 1956.

ELECTRONIC DESIGN • April 29, 1959

## **Random Reliability Notes**

ESPITE the plethora of papers written on Reliability In Electronics, the topic continues to provoke discussions and disputes. The final chapter on the subject has not been written, and there is still much talk on such related matters as cost and methods of achievement. That reliability is desirable is one of the few areas where agreement exists.

Explaining why unreliability exists, H. T. Hallowell, president of the Standard Pressed Steel Co., told the Franklin Institute recently that in satellites, in missiles and even in consumer appliances, performance criteria are being set on the basis of price in an attempt to save "pennies." He said that the consumer repair bill was 20 billion dollars annually.

### Failure Rate in a Typical Electronic System

Element	Population Density Ratio	Quantity Per System	Failure Rate Per 1,000,000 Hrs.	System Failure Rate 1,000,000 Hrs.	Failure Rate %
Tubes, Transistors	1	100	1	100	2.71
Connectors	1.01	101	.8	80.8	2.2
Diodes	1.1	110	4.5	495	13.4
Gyros	.01	1	50	50	1.35
Inductors	.02	2	2	4	.1
Motors	.03	3	50	150	4.06
Potentiometers	.26	26	40	1040	28.25
Relays	.15	15	25	375	10.23
Resistors (fixed)	4.4	440	1.4	616	16.76
Switches	.11	11	10	110	2.9
Transformers	.09	9	10	90	2.44
Choppers	.01	1	5	5	.13
Printed Ckt. Board	.2	20	1	20	.54
Soldered Connection	10	1000	.4	400	10.84
Capacitors	1.8	180	.84	151.2	4.09
				Total 3687.0	

This data was extracted from inherent reliability studies made at Autotechnics, Division of North American Aviation, Inc. In the typical system 3687 failures occurred during an operating period of one million hours. The Mean-Time-To-Failure, the reciprocal of the failure rate, is 271.2 hours. The data was in a paper presented by I. G. Rabbin at the recent EIA Conference on Reliable Electrical Connections.

More reasons behind unreliability: Equipment and part manufacturers compete with each other on the basis of design, price, delivery, and more recently, reliability or trouble-free operation. So explained R. F. Edwards in a paper called "The Reliability Game" at this year's IRE Convention.

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The control system in use by these groups is a democratic one that sets the punishment level for poor reliability at that of the manufacturer of the parts with the most marginal reliability.

"The solution is simply to alter the wording of the purchase contracts all down the line to reflect the true value of reliability. This will automatically change the structure of the organizations to those more suited to produce reliable products."

### The Cost Of Reliability

On the subject of cost we reported in the January 7, 1959, issue of ELECTRONIC DESIGN that, "Extensive tests are fine for reliability—but the price is high in dollars and time."

Even before the issue had been mailed we received a letter from one of our readers who reported: . . . If a supplier has a single High Reliability Specification against which to process his parts, he can certainly do the processing much more economically than by manufacturing pieces against a number of individual customer's specifications. An a matter of fact, our Specification S-1002 only cost a 30% premium over base prices which is not only much less expensive than we could process against customer specifications, but really is a very nominal sum for the customer to pay in order to have a good reliability assurance.

". . . Many of our customers are dropping their own processing specifications in favor of purchas-

ing pieces against our standard document." This letter cheering the merits of standardization came from C. H. Tuttle, Jr., of Vitramon, Inc.

### Milspecs Reduce Costs Says One Reader

High reliability military specifications are not raising costs writes another one of our readers.

"... Every large manufacturer of capacitors has made application for Q.P.L. testing under Mil-C-26244 (USAF). Within several months one of the largest capacitor companies was able to reduce prices approximately 25%." So says F. J. Ruther of Dayton, Ohio.

Mil-C-26244 specifies both a failure rate and limits on confidence numbers.

### Milspecs Confuse Says Another

Speaking of Milspecs in general and mentioning Mil-C-26244 in particular, a representative of a capacitor company we recently interviewed said: "Milspecs sometimes hinder. In Mil-C-25, the bible, tab construction is called for. This is unreliable, compared to extended-foil construction, though somewhat smaller and cheaper. Mil-C-25 doesn't recognize today's high vibration requirements, calling for only 55 vps.

"Other specs attempt to supplement this spec. Mil-C-14157 and Mil-C-26244 are two of them. They create confusion and havoc in the field. To get a high reliability product, which 14157 and 26244 call for, we have to charge for the production process because more quality control is involved. But many companies demand high reliability and are unwilling to pay for it." He said that Mil-C-14157 and Mil-C-26244 should be combined and used as a universal spec because they are very similar.

And so the debate continues.

### **Computers Will Play Bigger Part**

"Future military performance requirements may preclude important selections of alternate solutions to tradeoff problems by informal means," said D. Ehrenpreis at an IRE Long Island Chapter Meeting, speaking on Reliability. He is a consulting engineer serving the Countermeasures Division of the Sperry Gyroscope Co.

"Formal calculations with mathematical relationships will provide a more logical engineering-like approach to decision-making.

"It is predicted that one major aid in meeting the challenge of today for developing future mili-

tary electronic equipment will be the greater use of high-speed digital computers.

"Organizations must become aware of the types of problems which lend themselves ideally to solution by analog or digital computers. The next step is to set up and arrange the analytical format for minimum computer programming and rental time."

# New all-epoxy PAK® system drastically cuts encapsulation costs!

Assembly Time and
Reject Rate Greatly Reduced

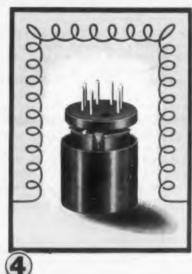
The E-Pak System consists of an all-epoxy header with embedded lead wires, a cured epoxy shell and a premetered epoxy pellet. The three may be custom-made for your component and are available from one source.



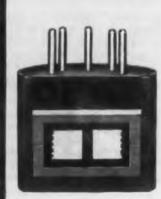




After the component is soldered to the epoxy header, a premetered pellet is dropped into the cured epoxy shell. The cover and component are then inserted into the shell.



The entire package is then heated; the pellet automatically melts and cures, embedding the component and sealing the cover. In cases where encapsulation is desired without embedment, a self-sealing epoxy cover is available.



You now have a solid, chemically-inert seal from within; there is no solder, no flux, no acid to endanger component reliability. Your component is hermetically sealed and embedded in cured epoxy forever.

Write today for complete information and samples.

## EPOXY PRODUCTS, INC.

A Division of Joseph Waldman & Sons

137 Coit Street, Irvington, New Jersey

ESsex 5-6000

CIRCLE 41 ON READER-SERVICE CARD



## CHOPPERS

MICROMINIATURE LIGHTWEIGHT NONMECHANICAL

INERTIALESS LOW POWER LOW LEVEL STABLE RUGGED LONG LIFE LINEAR HIGH SPEED HIGH EFFICIENCY



Model: Type:	50 Germanium	60 Germanium	70 Silicon
Temperature Range:	$-55^{\circ}$ C, to $+85^{\circ}$ C	-55° C to +90° C	−55° C to +130° C
Sq. Wave Drive Volt.:	1 to 10v. p-p	1 to 15 v. p-p	5 to 20 v. p-p
DC Input Voltage:	to 12 v	to 15 v	to 20 v
Chopping Freq.:	DC to 100 kcps	DC to 100 kcps	DC to 200 kcps
Alpha Cutoff Freq.:	900 kilocycles	One megacycle	5 megacycles
Temperature Drift:	.04% per °C	.02% per °C	.03% per °C
Random Noise:	25uv rms	10uv rms	50uv rms
Weight:	3 grams	1 gram	2 grams

### DESCRIPTION

The transistor chopper (or modulator) is a solidly encapsuled unit designed to alternately connect and disconnect a load from a signal source. It may also be used as a demodulator to convert on a.c. signal to d.c. It is capable of linearly switching or chopping voltages over a wide dynamic range which extends down to a fraction of a millivolt and up to 10 volts. Unlike mechanical choppers which can only be designed to operate over a narrow and comparatively low frequency range due to mechanical limitations, this transistorized chopper is an inertialess device that can be driven from d.c. to hundreds of kilocycles.

The switching circuitry used operates the transistors in a manner which provides stability and freedom from drift over a wide temperature range. Only carefully selected transistors are utilized.

The noise figure of the transistor chopper is competitive with mechanical choppers for many uses. Furthermore, the noise level will not increase with usage.

This unit is practically immune to the effects of shock and vibration making it ideal for military, missile, and portable applications; or where power conservation, miniaturization and elimination or maintenance are a necessity. The transistor chopper has an inherently long life and is not subject to contact bounce, wear, pitting or burning.

### TYPICAL APPLICATIONS

Chopper (modulator).

Demodulator.

Low, medium level switching.

D.C. amplifier stabilization.

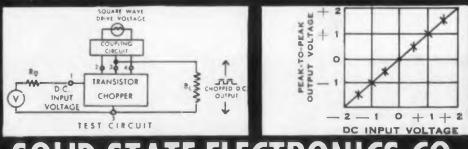
High speed servomechanisms.

Replace less sensitive diode modulators.

Thermocouple instrumentation.

Low, medium level D.C. instruments.

Low level commutators for telemetering.
Carrier for lower frequency signals.
Digital meters.
Portable equipment.
Low power source equipment.
Minimum maintenance equipment.
Multiplex switching equipment.



### SOLID STATE ELECTRONICS CO.

8158 ORION AVE., VAN NUYS, CALIF. ST. 2-605

CIRCLE 42 ON READER-SERVICE CARD

### COMPONENT DESIGN DATA

## Design Data on Rechargeable Dry Cells

N ICKEL-CADMIUM sealed cells have achieved extremely high interest among design engineers in the past few months, with the advent of lines of standard dry-cell replacements. We review here some of the later developments in rechargeable dry cells.

Sealed nickel-cadmium batteries of French design, distributed and partly manufactured by Gulton Industries, Metuchen, N. J., cover a wide range of sizes, the most popular being a button cell and a D cell. Capacities range from 100 mah to 1750 mah.

D-Ac, a pressed powder type of nickel-cadmium battery from Germany has been marketed to some extent in the United States by Burdgess Battery Co., Freeport, Ill., and Gould National Batteries, Nicad Div., Easthampton, Mass.

Of entirely American manufacture, a very complete line of dry-cell replacements is being marketed by Sonotone Corp., Elmsford, N. Y. It includes the

1/3-C, 1/2-C, 1 x 0.225, 1 x 1/4, 1/4-D D and F sizes, as well as the very popular "pencil light" AA size used in meters and portable test equipment. Employed in equipment drawing 360 ma, the Model S101 AA battery should last an hour before recharging; at 90 ma, about 4-1/2 hours; at 20 ma, some 21 hours. Discharge curves for the Sonotone Model S103 D Cell are shown in Fig. 1. This battery is designed to replace the D-size dry cell. Note the relative flatness of the curves. During continuous use until discharge, little deterioration of performance is observed in equipment using the battery.

An outgrowth of work in reliable space platform batteries, the rechargeable sealed sintered-plate Ni-Cd cells are claimed to last "for the life of the product" in which they are used. Life tests to 10,000 cycles have been made, and 20,000 cycles without deterioration is hoped for

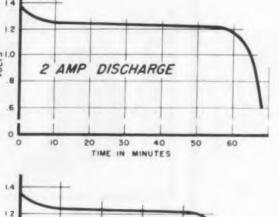
Any of the batteries can be stored without deterioration at temperatures of —65 to 160 F. A standard recharging will bring the cell back to full operating charge. A cell will maintain a usable charge for six months without recharging.

Sealed sintered-plate construction, claims Sonotone, is the key to the batteries' long life.

Each cell is made up of plates which have a foundation of nickel wire mesh. Sintered to the mesh is a carbonyl nickel powder which forms a porous surface, giving a larger area than would be possible using a flat plate.

Nickel oxide is the active material in the positive plate, cadmium in the negative. The electrolyte is a 30 per cent by weight solution of potassium hydroxide in distilled water. The entire construction is sealed.

The low internal resistance of the sintered plates allows a high discharge rate-limited only by the short circuit peak. Pulse discharges as high as 40 times capacity are possible.



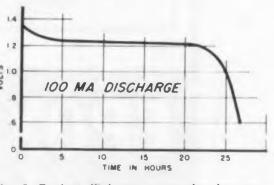


Fig. 1. Typical discharge curves showing constant current output.



Fig. 2. Sonotone rechargeable battery has built in charger.

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Sealed Ni-Cd cells can be discharged over a temperature range of -40 to 160 F. At -40 F the cell delivers 50 to 70 per cent of the room temperature capacity, while at 125 F it delivers from 80 to 95

So far the only battery package conlaining a built-in charger is the flashlight cell of Fig. 2. It is the size of two end-toend D cells. Per-cycle use in a flashlight s about two continuous hours. To recharge, the top is unscrewed and the cell plugged into a standard 110 vac wall eceptacle. A built-in transformer steps lown the voltage: and a silicon diode rectifies it. Optimum charging rate is 16 lours-at this rate the cell can be left plugged in for months without any damge, It will last at least 10,000 charging

Cost of the flashlight battery is on the order of \$5.00 for small orders, less than half that for large orders. For batteries without the internal charging mechanism. in hexpensive charger can be purchased rom Sonotone.

For further information on these recha geable sealed sintered-plate Ni-Cd es cacell turn to the Reader's-Service card and ircle 103.

## **CUT COSTS OF TEST EQUIPMENT BY 20% WITH Technical Information Service**

Case histories have shown that companies waste up to 20% of their annual expenditures for test equipment.

A prime cause is the failure to make the best buy obtainable because each company did not know the full range of available equipment. Collecting and maintaining complete, timely, and accurate product information is difficult—could cost as much as \$25,000 a year to service—and yet could be incomplete and

A prodigious number of crucial engineering and purchasing man-hours are squandered in test equipment procurement. Track-ing down sources of supply takes days and, often, weeks. Key personnel are trapped by protracted correspondence and sales interviews while obtaining full specifications and prices. When modifications are involved, workloads increase geometrically. This costly routine must be repeated every time new purchases

Now, for the first time, you can plug these hidden profit leaks through the use of a completely new concept in instrument evaluation for procurement.

Technical Information Service (TIS) provides you with complete, timely product information about all available electronic test equipment. In a matter of minutes you can possess detailed descriptions of equipment produced by every manufacturer in the business, from the largest to the smallest, without bias in favor of either. What's more, the descriptions include the full specifications, price, and the names and addresses of local sales representatives—all you need to initiate procurement.

Consider the benefits enjoyed by clients of Technical Information Service.

### SINGLE SOURCE OF SUPPLY INFORMATION

Clients have the only central source of supply information designed specifically for their electronic test equipment requirements. Completely categorized, up-to-the-minute information makes the user a technical expert capable of quickly evaluating complete spec-by-spec comparisons of competitive equipment. Since TIS maintains accurate files by constant check of all sources for additions and changes in specifications and prices, clients may make inquiry by phone or letter on any test instrument problem

With such information at their fingertips, clients can make their purchases with total awareness of what the market has to offer. Procurement is made with minimal demands on key personnel and their time. Many clients find that this accelerated purchasing procedure has earned an extra bonus in expediting tight-schedule projects for which the test equipment is needed.

### COMPLETE, ACCURATE INFORMATION

Clients receive detailed data on more than 4,500 separate instruments manufactured by some 400 different companies. Constant review of the entire instrument field by graduate engineers keeps data on specifications, prices, and models up to date at all times.

Suppliers are queried on incomplete or dubious information, if necessary, before their products are included in any TIS release.

Since all products are described without charge and without

advertising claims, small and large manufacturers are on equal footing. Their instruments speak for themselves with bald facts, free of slanted claims or persuasive case histories. Clients make their own evaluations from complete, factual information.

### SUPPLIER RESEARCH SERVICE LOCATES "CUSTOM" INSTRUMENTS

Often, seemingly built-to-order requirements can be satisfied by minor modification to standard instruments. The complete listing of all large and small manufacturers of stock items provides a ready reference for such inquiry, either directly by the client or through the efforts of TIS.

In those cases where unique equipment is a necessity, TIS Supplier Research surveys the market for the client, collecting all the pertinent information he requires to initiate serious negotiations with suppliers.

### COMPLETE PRIVACY

Whether TIS is locating sources for unique requirements or providing information on standard equipment, clients maintain a cloaked identity during all stages of inquiry. The Client conducts negotiations with the suppliers in whom he is interested.

### FOUR-VOLUME DIRECTORY

Clients of the tax-deductible Technical Information Service receive a free, four-volume, handsomely bound encyclopedia of standard equipment and sources published twice a year and supplemented constantly. Three volumes are devoted to descriptions of equipment. The fourth volume is an extensive cross-index of manufacturers and their representatives. Completely free of advertising, the directories give clients a complete, factual picture of all standard electronic test instruments. Clients of Technical Information Service receive both the Directories and Supplier Research Service.

### PROVEN IN USE

For the past two years TIS has served such clients as General Electric, M.I.T., Lincoln Labs., General Motors, NASA, Litton Industries, Naval Ordnance Lab., Hewlett-Packard, Lockheed Aircraft, Western Electric, RCA, Marconi Instruments, Eglin AFB, American Bosch Arma, and hundreds of others. The merit of TIS is proven by the fact that many clients have contracted additional service for other departments and projects.

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One subscriber saved more than three times the cost of TIS within a week! You will have the key to how it was done when you go through the TIS brochure which tells all . . . shows how TIS reduces even the hidden, seldom-counted costs of the old-fashioned way of instrument procurement. Send for your copy of this FREE brochure today. No obligation. Use the convenient coupon below.

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TITLE

CIRCLE 43 ON READER-SERVICE CARD

### **MULTI-WIRE FABRIC**

Depending on the diameter of the wires used, this flat belt of interwoven copper wires can pass through a clearing of less than 1/32 in. high. The teflon-coated wires are run side by side in perfect alignment. These are woven together by cross threads of nylon, fiber glass or teflon yarn. Wires are of different colors to provide immediate identification for each individual wire from either end. Designed for aircraft or missile applications, the wire fabric can be made any width, the number of wires per inch being determined by the diameter of the coated wire used.

The Fletcher Works, Inc., Dept. ED, Philadelphia, Pa.

CIRCLE 44 ON READER-SERVICE CARD

## **NEW PRODUCTS**

Covering all new products that might generally be specified by an electronics engineer engaged in the design of original equipment.

### **ROTARY SWITCH**

Any wafer of this rotary switch lifts out instantly without unsoldering or disassembling for fast, easy cleaning or instant replacement. Switches are available in sizes approximately 2 x 2 in., 3 x 3 in., and 4 x 4 in. with lengths to accommodate up to 36 wafers. There is an almost unlimited choice of switch circuit configurations. All connections are to a single bank of receptacles and are accessible from one side of the aluminum housing. Contacts are silver, gold or rhodium plated on a copper base.

Chicago Dynamic Industries, Inc., Precision Products Div., Dept. ED, 1725 Diversey Blvd., Chicago 14, Ill.

CIRCLE 45 ON READER-SERVICE CARD





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### **CIRCUIT PACKAGES**

These circuit packages can be used to simplify equipment assembly, reduce production errors, and increase reliability, They contain semiconductor devices and other components connected to provide the desired circuit. Many different types of circuit packages are available, including: bridge rectifiers; phase comparators; diode switches; amplifiers; and flip-flops. The final assembly is light weight and free from atmospheric effects.

Raytheon Mfg. Co., Semiconductor Div., Dept. ED, 215 First Ave., Needham Heights 94, Mass.

CIRCLE 46 ON READER-SERVICE CARD



### **INDUCTORS**

These metallized glass inductors are designed for tuned circuit applications at frequencies above 30 mc. Operating temperature range: from -55 to +125 C. The temperature coefficient ranges from 8 to 16 ppm per deg C for an inductor without cores or tuning devices. Inductance values for the standard units range from 0.05 to 0.1 µh in increments of 0.01 µh, and from 0.1 to 1.3 µh in increments of approximately 0.1 µh.

Corning Glass Works, Electronic Components Dept., Dept. ED, Bradford, Pa.

CIRCLE 47 ON READER-SERVICE CARD



### **MAGNETIC AMPLIFIER**

Ingineered to perform as an AND, OR or NOT gate, or as a bi-stable memory device, this magnetic amplifier has all-static construction. Called the PMC-785 logic type magnetic amplifier, the unit is made primarily for missile control and checkout applications. It operates from a 70 v center-tapped transformer on a 115 v line at 400 cps, has a 2.5 msec response, and accepts a minimum input signal of only 3 mw.

Pacific Magnetic Corp., Electronic Center, Dept. ED, Romoland, Calif.

CIRCLE 48 ON READER-SERVICE CARD

### Creative Microwave Technology MMMM

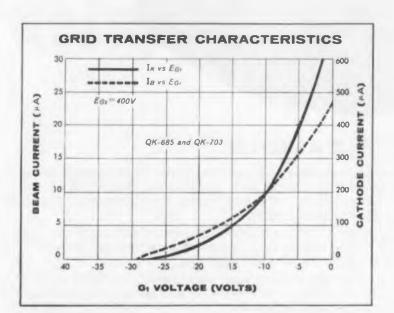
Published by Microwave and Power Tube Division, Raytheon Manufacturing Company, Waltham 54, Mass., Vol. 1, No. 4

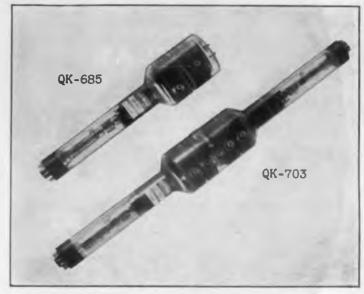
### NEW KILO-LINE RECORDING STORAGE TUBES SPECIALLY DESIGNED FOR SCAN CONVERSION

To meet the need for low-noise, high-resolution devices for frequency and scan conversion, Raytheon scientists and engineers have developed two new storage tubes: the single-gun QK-685 and the dual-gun QK-703. These tubes are now available in production quantities.

Both types incorporate a specially designed tetrode electron gun for higher resolutions — 1,000 TV lines at 50% modulation — and better control over beam cut-off than conventional triode guns. A new multiple collimating lens improves background uniformity and results in shading-to-signal ratios of less than 10%.

The ability of the dual-gun type to read and write simultaneously makes this tube particularly applicable to slow-down video and conversion from PPI to TV scan patterns for "Bright Display."





Typical Operating Characteristics

Anode Voltage
Resolving Power
Magnetic Focus
Electrostatic Focus
Output Capacitance

Maximum Deflection Angle

4,000 Vdc (Max.)

1,000 Lines (Nom.)

700 Lines (Nom.)

QK-685 and QK-703

QK-685—10 μμf (Nom.) QK-703—20 μμf (Nom.)

TYPICAL RESOLUTION CURVE

100
20
20
400 500 600 700 800 900 1000 1100 1200 1300

RESOLUTION (NUMBER OF TV LINES)

Excellence in Electronics



You can obtain detailed application information and special development services by contacting: Microwave and Power Tube Division, Raytheon Manufacturing Company, Waltham 54, Massachusetts

A LEADER IN CREATIVE MICROWAVE TECHNOLOGY



GAR-3 Super FALCON

Playing follow-the-leader at 50 millisecond intervals, three Super Falcon missiles rocket ahead of their diamond-shaped supersonic shock waves. Homing in on radar, these deadly air-to-air missiles locate, track, and destroy their prey, with the same killer instinct of the birds they're named after.

Hughes Aircraft, the developer and manufacturer of these missiles and the Armament Control System that triggers them, specified Hitemp magnet and Teflon\* wire for their missile, and Teflon wire for its control system.

Hitemp Wires, Inc., the leading specialist in high temperature insulated wires and cables, proudly answers roll call with those developers and manufacturers enlisted in defending our American birthright—Freedom.

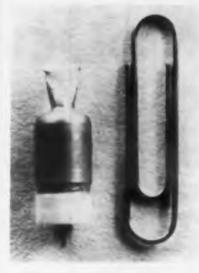
### HITEMP WIRES, INC.

1200 SHAMES DRIVE, WESTBURY, NEW YORK

Registered trademark for Du Pont fluorocarbon resins.

CIRCLE 50 ON READER-SERVICE CARD

### **NEW PRODUCTS**



Voltage Regulator Tubes Provide 1%

regulation

ED

solve

func

maki

Spic

200

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ohm

born

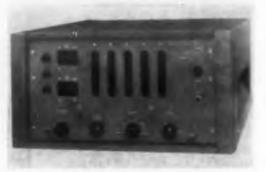
ELE(

These metal ceramic, corona discharge voltage in., regulator tubes cover a range from 400 to 4000 v in. Regulation is better than 1% from 10<sup>-11</sup> to 10<sup>-12</sup> in. amp, and the prebreakdown current is less than load 10<sup>-12</sup> amp at room temperature. The units are resistant to shock and vibration and operate from 4 tion -55 to +200 C. Overall length is under 1 in and OD is 0.3 in.

Radiation Research Corp., Dept. ED, 1114 First Ave., New York 21, N.Y.

CIRCLE 51 ON READER-SERVICE CARD

## Frequency Counter Limit indicating



Frequency meter model 7153 indicates whether metered frequency is below, within, or above two selected limits by lighting one of three panel lamps. Relay contact closures, occurring at the same time the panel lamps are lit, may be used to actuate audible alarms or to control the source of the input frequency. The unit has a range of dc to 100 kc and a sensitivity of 0.1 v rms into limeg.

Beckman Instruments, Inc., Berkeley Div., Deple ED, 2200 Wright Ave., Richmond 3, Calif.

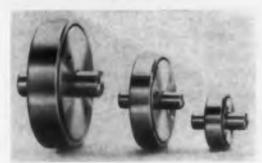
CIRCLE 52 ON READER-SERVICE CARD

This is the time of our annual subscription renewal.

ELECTRONIC DESIGN . April 29, 95

### **Rotary Positioning Controls**

For loads to 200 in.-lb



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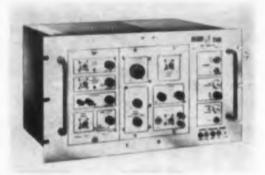
Loads from inch ounces to 200 in.-lb can be positively and accurately held in an infinite number of positions for clockwise or counterclockwise rotation by these rotary positioning controls. Diameters are 3/4 and 1-1/4 in. with a depth of 5/16 in., and 1-3/4 in. with a depth of 5/8 in. The 3/4 in. model is rated for loads to 50 in.-oz, the 1-1/4 in. for loads to 50 in.-lb, and the 1-3/4 in. for loads to 200 in.-lb. Designed for applications as no-back devices, valve and potentiometer positioners, dial controls, clutches, and couplings, the units have zero backlash, low breakaway torques, and rotating speeds to 3800 rpm.

Reid Controls, Reid Metal Products, Inc., Dept. ED. 2021 N. Lincoln St., Burbank, Calif.

CIRCLE 53 ON READER-SERVICE CARD

### **Pulse Generator**

Uses plug-in adaptors



Model MPG-4A pulse generator is designed to solve a variety of pulse problems with a series of plug-in trigger generators. The pulses it generates are readily adaptable to the measurement of magnetic material saturation properties, circuit step function response, precise time delays, and other factors. The plug-in trigger generators permit the separation of trigger and pulse forming circuitry, making available a variety of triggering modes for specialized needs. Any pulse width from 0.3 to 200 usec may be obtained, and any pulse amplitude from 10 to 175 v may be achieved in a 93 ohm resistive load. Rise time is 0.02 usec, decay time is 0.08 usec, and pulse top is flat within 5% of total amplitude.

PCA Electronics, Inc., Dept. ED, 16799 Schoenborn St., Sepulveda, Calif.

CIRCLE 54 ON READER-SERVICE CARD

ESC advances the art of delay lines...

by design!



# I45 to 1 delay time/rise time ratio

At one time the 145 to 1 delay time/rise time ratio of ESC's Model 51-43 was considered impossible—today this unit is revolutionizing delay line applications and providing greater design freedom for America's electronics industry. Such advances in the art of delay lines could come from only ESC—America's leading manufacturer devoted to the design, development and production of custom-built and stock delay lines.



WRITE TODAY FOR COMPLETE TECHNICAL DATA.

exceptional employment opportunities for engineers experienced in computer components...excellent profit-sharing plan.

CORPORATION

ORATION 534 Bergen Boulevard, Palisades Park, New Jersey

Distributed constant delay lines - Lumped-constant delay lines - Variable delay networks - Continuously variable delay lines - Pushbutton decade delay lines - Shift registers - Pulse transformers - Medium and low-power transformers - Filters of all types - Pulse-forming networks - Miniature plug-in encapsulated circuit assemblies

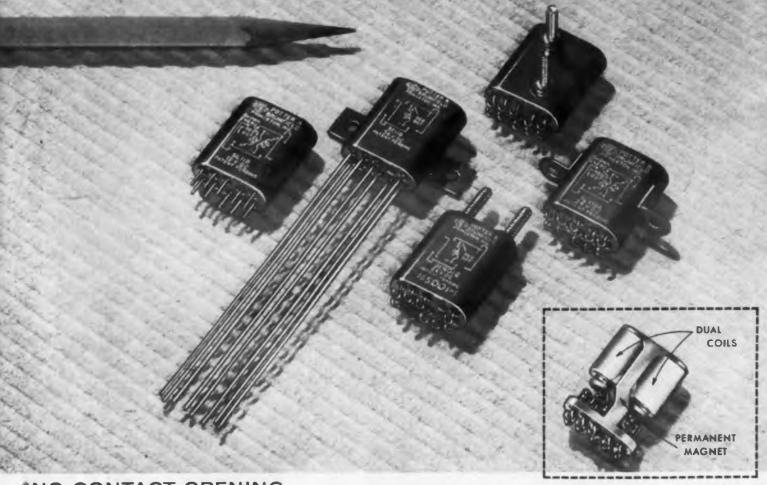
CIRCLE 55 ON READER-SERVICE CARD

ELECTRONIC DESIGN • April 29, 1959

P&B MICRO-MINIATURE RELAYS LEAD IN

## performance

SHOCK: 100g\* VIBRATION: 30g to 2000 cps\*

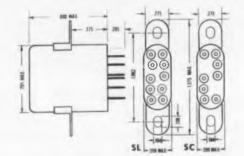


### \*NO CONTACT OPENING

New P&B crystal-case size relays, the SC and the SL (magnetic latching), show amazing shock and vibration capabilities. They absorb shocks of 100g and vibrations 30g to 2000 cps. without contact openings!

A highly efficient magnetic structure utilizing a permanent magnet makes possible at least twice the contact pressure found in DPDT relays of comparable size. One watt of power for three milliseconds operates either relay. Transfer time is unusually fast —0.5 milliseconds maximum.

For more information, contact your P&B sales engineer, or write Potter & Brumfield, Princeton, Indiana.



SL—dual coil latching relay. Operates on o 1 watt, 3 ms. pulse at nominal voltage. Permanent magnet latch locks the armature in either position.

SC—non-latching relay with series-connected dual coils. Operates on approximately 1 watt at nominal voltage. Coils must remain energized to hold the armature in the operate position.

### SC and SL Series Engineering Data GENERAL:

Insulation Resistance: 10,000 megohms, min. Breakdown Voltage: 1,000 V. RMS. Shock: 100g.

Vibration: 30g 55 to 2000 cps.; 0.195" max.

excursions from 10-55 cps.

Temperature Range: -65° C. to + 125° C.

Weight: 15 grams without mounting bracket.

Operate Time: 3 MS. max. with 550 ohm coil

@ 24 V. DC. (SL: 630 ohm coil at 24 V. DC).
Transfer Time: 0.5 MS max.

Terminals: (1) Plug-in for microminiature receptacle of printed circuit board.

(2) Hook end solder for 2 #24 AWG wires.
(3) 3" flexible leads.

Enclosure: Hermetically sealed.

### CONTACTS:

Arrangement: 2 Form C.

Material: Optional

Load: 2 amps. (a 28 V. DC, resistive; 1 amp (a 115 V. 60 cycles AC, resistive.

Pressure: SC-16 grams min.; SL-20 grams min. COIL:

Power: Approx. 1.0 watt at Nominal Voltage.
Resistance: SL-40 to 10,000 ohms: SC-35
to 20,000 ohms.

Duty: Continuous.

MOUNTINGS:

Bracket, stud and plug-in.

PAB STANDARD RELAYS ARE AVAILABLE AT YOUR LOCAL ELECTRONIC PARTS DISTRIBUTOR



### POTTER & BRUMFIELD INC.

PRINCETON, INDIANA . SUBSIDIARY OF AMERICAN MACHINE & FOUNDRY COMPANY

### **NEW PRODUCTS**

### **Axial Blower**

Delivers up to 169 cfm

This axial blower will deliver up to 169 cfm and can deliver 100 cfm against a static pressure of 3.5 in. of H<sub>2</sub>O. It is powered by the company's type FC motor and operates at 115 v or 200 v ac, 400 cps, three phase. Power input at peak air volume is 120 w. The unit is 2-3/8 in long and 2.812 in. in diameter with the 3-in. servo ring attached.

Globe Industries, Inc., Dept. ED, 1784 Stanley Ave., Dayton 4, Ohio.
CIRCLE 109 ON READER-SERVICE CARD

### FM-FM Telemetry Transmitter

Meets IRIG requirements

Available in two models which cover 215 to 235 and 235 to 260 mc, the type 86600 fm-fm telemetry transmitter meets all IRIG requirements. Spurious and harmonic output are 60 db down from the carrier level and power output is 2 w minimum at a plate supply of 125 v dc. ±5% at 130 ma. The carrier frequency adjusts to within ±0.001% of the assigned frequency, and frequency stability is ±0.01% from -25 to +85 C.

Gilfillan Bros., Inc., Dept. ED, 1815 Venice Blvd., Los Angeles 6.

CIRCLE 110 ON READER-SERVICE CARD

### Flexible Printed Circuits

### Single or multiple layers

These flexible printed circuits consist of etched copper patterns bonded between thin flexible sheets of plastic insulating materials such as Kel-F, Teflon, and epoxy. Available in single or multiple layers, the circuits are low cost, space and weight saving, and reliable.

International Resistance Co., Dept ED, 401 N. Broad St., Philadelphil

CIRCLE 111 ON READER-SERVICE CARD

**← CIRCLE 112 ON READER-SERVICE CARD** 



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(above) Setting up a diffraction image for a research study in near-infrared optics (left) Nation's first successful re-entry tests were conducted with the Lockheed X-17 (bottom right) Research and Development facility in the Stanford Industrial Park at Palo Alto, California, provides the latest in technical equipment

### RECONNAISSANCE



### **EXPANDING THE FRONTIERS OF SPACE TECHNOLOGY**

Lockheed Missiles and Space activities in reconnaissance are among the most advanced in industry. They include such areas as radar, optics, infrared and TV. Work in the fields of radar and data link is concerned with research, design and development of systems and equipment for missile tracking, command guidance, detection and relay of information. Noise modulation techniques are under study as part of statistical communication theory and implementation of automatic space communication systems. Of special significance is the development of a radar firing error indicator that measures the intercept trajectory between target and attacking missile.

Solid state work in infrared embraces the development of new systems and sub-systems for long range infrared communications, surveillance, range findings and target tracking. Considerable work is being conducted in optical devices and systems employing optics. Capability in this area also extends to scanners, encoders, detectors, read-out devices, and analytics of information processing.

Opportunities exist for engineers and scientists of inquiring mind to contribute to the solution of new problems in these fields. If you are experienced in physics, mathematics, chemistry, or one of the engineering sciences, we invite your inquiry. Write: Research and Development Staff, Dept. D3-21, 962 W. El Camino Real, Sunnyvale, California. U.S. Citizenship required.

"The organization that contributed most in the past year to the advancement of the art of missiles and astronautics." NATIONAL MISSILE INDUSTRY CONFERENCE AWARD

Lockheed

MISSILES AND SPACE DIVISION

BUNNYVALE, PALO ALTO, VAN NUYS,
BANTA CRUZ, BANTA MARIA, CALIFORNIA
CAPE CANAVERAL, FLORIDA
ALAMOGORDO, NEW MEXICO \* HAWAII

Weapons Systems Manager for the Navy POLARIS FBM; DISCOVERER SATELLITE; Army KINGFISHER: Air Force Q-5 and X-7

Unusual career opportunities for qualified scientists and engineers ... write Avce/Crosley today.

## Avco/Crosley

## From Crosley... Command Receivers for Drones and Missiles

Designed and manufactured by Avco's Crosley Division, Command Receivers are standard equipment aboard most of the nation's missiles. Their job:

To receive and act upon instructions from the ground to destroy the missile when its flight path indicates the missile has gone awry.

In a missile configuration, the Command Receiver weighs only 12 pounds, has three channels and incorporates a decoder and power supply in a simple pressurized package.

A second version of the Command Receiver, employing 12 channels for radio communication, is used in highperformance drones and decoys. In such applications, the Command Receiver actuates control surfaces, directs engine operation and opens the recovery parachute—all by radio-conveyed instructions from the ground.

### A Product of Crosley Engineering,

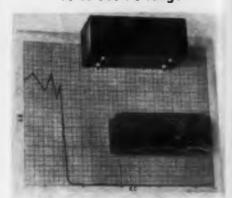
the Command Receiver has proven itself for the future by the job it is doing in the missiles and drones of today.

For more information, write to: Vice-President, Marketing-Defense Products, Dept. L-49, Crosley Division, Avco Corporation, 1329 Arlington Street, Cincinnati 25, Ohio.



### **NEW PRODUCTS**

SSB Crystal Filters
10 to 500 kc range



Ranging from 10 to 500 kc, these SSB filters have high bandwidth ratios and good shape factors. With a carrier frequency of 85 kc, an upper side band unit has a 3 db bandwidth of 3.4 kc and an attenuation band over 40 db. A shape factor of 1.08 is obtained in the slope region. Using a more complex design, a 60 db attenuation can be achieved with a similar shape factor. Insertion loss is about 9 db. Dimensions of this unit are 5 x 2 x 2 in. Bandwidth ratios of better than 10% may be reached with side band crystal filters from 60 to 200 kc, and ratios of 2 to 3% are obtainable from 10 to 60 and 200 to 500 kc.

Bulova Watch Co., Electronic Div., Dept. ED, Woodside 77, N.Y.

CIRCLE 60 ON READER-SERVICE CARD

### **Precision Potentiometer**

Watertight

A 1/2 in. watertight potentiometer, the model APW 1/2 has a glass-to-metal solder sealed header and terminal lugs that are installed with a glass-to-metal seal and positioned for easy wiring. It has an O ring shaft seal per Mil-E-5272A specifications, and the terminal board is solder sealed to the case. Suited for high temperature use, the unit is available with mechanical rotation stops, special winding angles, and resistance values to 100 K.

Waters Mfg., Inc., Dept. ED, Boston Post Rd., Wayland, Mass.

CIRCLE 61 ON READER-SERVICE CARD

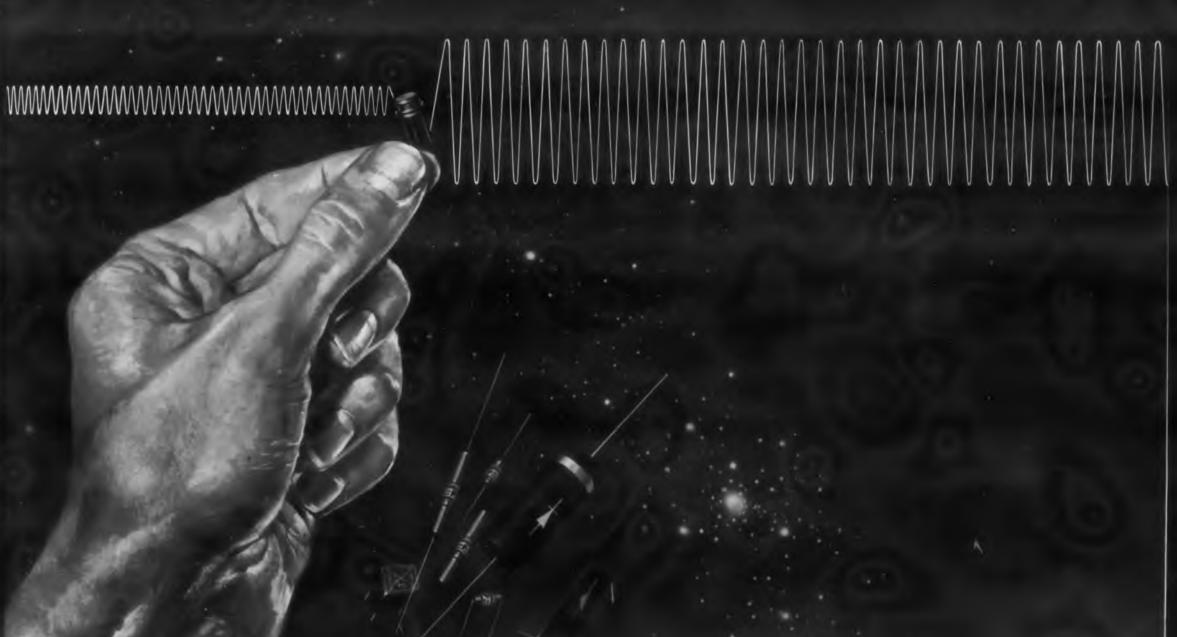
← CIRCLE 62 ON READER-SERVICE CARD

CIRCLE 63 ON READER-SERVICE CARD

ADVANCED

SEMICONDUCTOR PRODUCTS

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### Very High Frequency Silicon Power Transistors

N-P-N Triple-diffused silicon mesa

### VHF POWER AMPLIFIER TYPES

XT-518 TYPICAL 70 MC POWER GAIN 10 db WITH 75 mw POWER OUTPUT; 4 db WITH 250 mw POWER OUTPUT.  $V_{CB} = 75V$ ,  $I_{C} = 30 \text{ mA}$ 

XT-519 TYPICAL 70 MC POWER GAIN 10 db WITH 250 mw POWER OUTPUT; 4 db WITH 500 mw POWER OUTPUT- $V_{CB} = 75V$ ,  $I_{C} = 30$  mA.

XT-520 TYPICAL 70 MC POWER GAIN 10 db WITH 500 mw POWER OUTPUT; 4 db WITH 750 mw POWER OUTPUT.  $V_{CB} = 75V$ ,  $I_C = 30$  mA.

See Footnotes 1 and 2.

### ABSOLUTE MAXIMUM RATINGS (25" ± 3°C except as noted)

Collector-Base Voltage 160 Vac Peak 120 Vdc Collector Current 75 mAde Emitter-Base Voltage 4 Vdc VEB Junction Temperature 150°C Collector Dissipation 2.8 W @ 25°C case temp. 2.25 W (a 50°C case temp. 1.1 W @ 100°C case temp.

### OTHER ELECTRICAL CHARACTERISTICS (25° = 3°C except as noted)

Symbol	Characteristics	Test Conditions	Min.	Typical	Max.	Unit
1cBO	Emitter Cutoff Current Collector Cutoff Current Collector Cutoff Current	$V_{EB} = 2V, I_C = 0$ $V_{CB} = 10V, I_E = 0$ $V_{CB} = 100V, I_E = 0$			100 1.5 1.0	μΑ Αμ mA
hje	HF Current Gain	V <sub>CB</sub> = 50V, I <sub>C</sub> = 30mA, f = 70mc.	10	1.5		
hje	LF Current Gain	V <sub>CB</sub> = 50V, I <sub>C</sub> = 30mA, f = 1kc		13		
Th'	HF Base Resistance	V <sub>CH</sub> = 12V, I <sub>E</sub> = -10mA, f = 150mc.			100	ohm
Cuh	Output Capacitance <sup>3</sup>	$V_{CB} = 50V, I_E = 0$ I = 140kc			7.5	μμΙ
re+re'	Emitter Resistance	$I_E = -10$ mA $I_C = 0$ f = 1kc		7		ohm
1,'	Collector Series Resistance	le = -20mA, le = 10mA, f = 1kc		15		ohm

cotnotes:

1 Case temperature 50°C maximum.

2 Neutralized common emitter power gain with input and output conjugate matching.

3 Includes approximately 1.5µµf header capacitance.

### VHF POWER OSCILLATOR TYPES

XT-515 OSCILLATOR POWER OUTPUT 250 mw MIN. @ 70 mc.  $V_{CB} = 80V$ ,  $I_{C} = 30$  mA.

XT-518 OSCILLATOR POWER OUTPUT 500 mw MIN, @ 70 mc.  $V_{CB} = 90V$ ,  $I_{C} = 30$  mA.

XT-517 OSCILLATOR POWER OUT PUT 750 mw MIN. @ 70 mc.  $V_{CB} = 100V$ ,  $I_C = 30 \text{ mA}$ 

1.1 W @ 100°C case temp

See Footnotes 1 and 2.

### ABSOLUTE MAXIMUM RATINGS (25° = 3 C except as noted)

160 Vac Peak Collector-Base Voltage 120 Vdc Collector Current 75 mAdc Emitter-Base Voltage VEB 3 Vdc 150°C Junction Temperature 2.8 W @ 25°C case temp. Collector Dissipation 2.25 W @ 50°C case temp.

### OTHER ELECTRICAL CHARACTERISTICS (25° ± 3°C except as noted)

Symbol	Characteriatics	Test Conditions	Typical	Max.	Unit
IEBO ICBO ICBO	Emitter Cutoff Current Collector Cutoff Current Collector Cutoff Current	$V_{EB} = 1V, I_{C'} = 0$ $V_{CB} = 10V, I_{E'} = 0$ $V_{CB} = 100V, I_{E'} = 0$		100 1 5 1 0	μΑ Α mA
hje	LF Current Gain	V <sub>C'B</sub> = 50V, I <sub>C'</sub> = 30mA f = 1 kc	6		
r <sub>b</sub> '	HF Base Resistance	$V_{CB} = 12V$ , $I_E = -10$ mA f = 150mc.	60		ohm
Cob	Output Capacitance <sup>3</sup>	$V_{CB} = 50V, I_E = 0$ I = 140kc	4.0		μμΙ
$\tau_e + \tau_e'$	Emitter Resistance	$I_E = -10$ mA, $I_C = 0$ f = 1kc	7		ohm
r <sub>c</sub>	Collector Series Resistance	$I_E = -20$ mA, $I_C = 10$ mA f = 1kc	15		ohm

Footnotes

1. Case temperature 50°C maximum.

2. Power output in parallel line oscillator

3. Includes approximately 1.5 µµt header capacitance

### Eight new EIA types Fast Recovery Silicon Diffusion Computer Diodes

ACTUAL SIZE

Type	Min. Sat.	Min. Fwd. Current		n Reverse	Reverse Recovery Characteristics		
Number (		6 LOv	25 C	100 C	Reverse Res. (ohms)	Max Recov.	
1N78	9 30	10	1 (20)1	30   20v1	200 K	0.5	
1N79	1 30	50	5 (200)	30 20vi	200K	0.5	
IN79	2 30	100	5 i 20vi	30 + 20 v i	100K	0.5	
1N79	3 60	10	1 (50v)	30  50v	200 K	0.5	
IN79	60	50	5 (50v)	30   50vi	200K	0.5	
180	1 150	10	1 125v:	30   125vi	200 K	0.5	
IN80	150	50	5 125vi	50 - 125v	200 K	0.5	
1 N80	200	50	10 175v	50 175v	200 K	0.5	

### ...added to the broadest line of Fast Recovery Silicon Computer Diodes in the industry!

### MILITARY TYPES

Type	Min. Sat. Voltage	Min. Fwd.	Maximum Reverse Current (#8)			Recovery
Number	(i 100 µa	(a · 1.0 v	25 C	100°C	Reverse Res. (ohms)	Max, Recov. Time (#2)
*1N643	200	10	025 : 10v:	5 (10v)	200 K	0.3
•1N662	100	10	1 : 100v1	15 (100v) 20 (10v)	100 K	0.5
\$1N663	100	100	20 (50v) 5 (75v)	100 50vi 50 (75v)	200 K	0.5

\*Mil-E-1/1171 (SigC). #Mil-E-1 1139 (SigC) §Mil-E-1/1140 (SigC)

### HIGH CONDUCTANCE TYPES

PS700	30	100	5 (20)	25 (20)	100 K	1.0
PS701	60	50	5 (45v)	50 i 45v i	100 K	0.5
PS702	100	75	20 (75v)	50 75v	200 K	1.0
PS703	100	50	5 (75v)	50 (75v)	100 K	0.5
P5704	150	50	5 (75v)	50 (75v)	100K	0.5
PS705	200	50	5 (75v)	50 (75v)	100 K	0.5

### MEDIUM CONDUCTANCE TYPES

PS720	30	3	5   20v)	25 : 20v :	100 K	0.5
PS721	60	5	5 -45vi	50 (45v)	100 K	0.3
PS722	100	5	5 : 75v1	50 (75v)	100K	0.3
PS723	200	3	20 (175v)	100 : 175v:	100 K	0.3
PS724	150	4	20 (125v)	100 - 125vi	100 K	0.3

### LOW CONDUCTANCE TYPES

1N625	30	4 (ii 1.5v	1 (20vi	30 (20v)	400 K	lusec
1N626	50	4 60 1.5v	1 + 35v+	30 (35v)	400 K	lusec
1N627	100	4 (iii 1.5v	1 (75v)	30 i 75v)	400 K	lµsec
1N628	150	4 (a 1 5v	1 (125v)	30   125v	400 K	1µsec
1N629	200	4 (a. 15v	1 (175v)	30 (175v)	400 K	1µsec

### Please Note:

All specifications and information contained herein are current as of:

April 28, 1959

### **Zener Diodes** 500 mW Power Dissipation

ACTUAL SIZE

### LOW VOLTAGE GROUP

PSI Type Elect Number Equiv	Flore	Zener Voltage		Maximum Dynamic	Maximur Cur	At	
	Equiv.	E- Min.	E: Max.	Resistance	1 (σ 25 C ιμΑι	In (a 100 C	Inverse Voltage
PS6465	1N465	2.0	3.2	60	75	100	1
PS6466	1N466	3.0	3.9	55	50	100	1
PS6467	IN467	3.7	4.5	45	5	100	1
PS6468	1N468	4.3	5.4	35	5	100	1.5
PS6469	1 N469	5.7	6.4	20	5	100	15
PS6470	18470	6.2	8.0	10	5	50	3.5

1. Measured at 10mA DC Zener current with 1mA RMS signal superposed

PSI Type Elect. Number Equiv.	Flore	Zener Voltage (α 200 μA (α 25 C		Maximu Cui	At	
	Equiv.	E: Min.	E Max.	1ε(α 25 C μΑι	1. (a 100 C ·μ¶)	Voltage Vi
PS6313	1N1313	7.5	10	5	5	6.8
PS6314	1N1314	9	12	5	5	8.2
PS6315	1N1315	11	14.5	5	5	100
PS6316	1N1316	13.5	18	.5	5	12.0
PS6317	1N1317	17	21	-5	5	15.0
PS6318	1N1318	20	27	1	10	180
				4		

### HIGH VOLTAGE GROUP

		Zener Voltage		Maximur		At
	Elect. Equiv.	E Min,	E Max	P (σ 25 C μA)	⊮ (α 100 C - μA)	Voltage V
PS6319	1N1319	25	32	1	10	22
PS6320	LN1320	30	39	1	10	27
PS6321	1 11 1321	37	45	1	10	33
PS6322	1N1322	43	54	1	10	39
PS6323	-IN1323	52	64	1	10	47
PS6324	1N1324	62	80	1.0	50	56
PS6325	IN1325	75	100	10	50	68
PS6326	1N1326	90	120	10	50	82
PS6327	1N1327	110	145	10	50	100

MAXIMUM Power Dissipation 500 mW (42 25 C Operating Range - 65 C to 200 C

### For Employment Opportunities

Write PSI Technical Staff Placement, 10451 West Jefferson Blvd., Culver City, Calif.

### Pacific Semiconductors, Inc.

A SUBSIDIARY OF THOMPSON RAMO WOOLDRIDGE INC.



### Standard Encapsulations

A variety of assemblies can be furnished for matched pairs and quads, ring modulators, full wave and bridge rectifiers and many other applications.

many other applications.

Numerous lead arrangements are possible in these three basic configurations. Up to four diodes or rectifiers can be encapsulated in the "S" or "T" packages. Up to 12 units can be contained in the "R" package. The number of units contained determines its maximum length.



% ACTUAL SIZE

"S" Package

Leads .020" diameter, 1" minimum length. Spaced on .1" grid centers.

ion

Vest

NC.

### DIMENSIONS

	"R" Package	"S" Package	"T" Package
Length	.375" to 1.75"	.45"	.50"
Width	.25"	39"	_
Height	.50	.40"	_
Diameter	_	-	375"

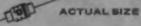
### Non-Linear Resistors

ACTUAL SIZE

-			-	
PSI Type	E / (e: 1mA - volts-	Min IMA	Max Dyn Res	In (a 25 C
PS594	0.62 = 10%	100	60	1.0 (u - 5v
PS594G	062 - 5%	100	60	10 m - 5v
PS595	0 62 • 10%	250	60	50 w - 5v
PS595G	0.62 * 5%	250	60	50 m - 5v

### Silicon

### General Purpose Diodes



EIA	Minimum Saturation Voltage			rerse Current DC Operating a @ volts)	Maximum Average Rectified Current (mA)	
TYPE	(a 100 pa (a 25°C (volts)	+ 1 (1 VDC (mA)	6. 25°C	(à 150°C	64 25°C	(a 150°C
1N456 1N456A	135 80	#0 100	025 @ 25 .025 @ 25	5 & 25 5 & 25	90 200	70
*1N457 1N457A	70 70	100	025 @ 60 025 @ 60	5 (a. 60 5 (a. 60)	75 200	70
*1N458 1N458A	150 150	100	025 @ 125 025 @ 125	5 (a 125 5 (a 125	55 200	70
*1N459 1N459A	200 200	3 100	025 (a. 175 025 (a. 175	5 @ 175 5 @ 175	40 200	70
1N461 1N461A	30 30	15 100	5 @ 25 5 @ 25	30 @ 25 30 @ 25	60 200	70
1N462 1N462A	70 70	5 100	.5 (a. 60 .5 (a. 60	30 (a. 60 30 (a. 60	50 200	70
1N463 1N463A	200 200	100	5 (a 175 5 (a 175	30 (a 175	30 200	70
1 N464 1 N464A	150 150	100	5 @ 125 5 @ 125	<b>30</b> € 125 30 € 125	40 200	70

\*JAN Types

OTHER ABSOLUTE MAXIMUM RATINGS
Power Dissipation 0.5 Walts (a. 25°C. Power Dissipation 0.25 Walts (a. 150°C. 1. Second Surge Current 1.5 Amperes 25°C. Storage and Operating Temperature Range 80°C to 200°C.

### Silicon

### **High Conductance Diodes**

ACTUAL SIZE

PSI or EIA TYPE	Minimum Saturation Voltage DC (a 25 C (volts)			Maximum Inverse Maximum DC ( Voltage  ua (a volt	Maximum Average Rectified Current (mA)		
NUMBER	(a 25 C (volts)	(a 100 mA	200 mA	25 C	150 C	25 C	150 C
1N482	40	1.1		250 (n - 30v	30	125	50
1N482A	40	1.0		025 (n - 30v	15	200	70
1N482B	40	10		025 (a - 30v	5	200	70
PS603	40		10	.250 (ii - 30v	30	200	100
PS604	40		1.0	.025 (a - 30v	15	200	100
PS605	40		10	025 (11 - 30v	5	200	100
1N483	80	11		250 (a - 60v	30	125	50
1N483A	80	1.0		.025 (17 - 60v	15	200	70
1N483B	80	10		025 (11 - 60v	5	200	70
PS609	80		10	250 (a - 60v	30	200	100
PS610	80		1.0	025 m - 60v	15	200	100
PS611	80		1.0	025 (a - 60v	5	200	100
1N484	150	11		250 (a - 125v	30	125	50
1N484A	150	1.0		025 (a - 125v	15	200	70
1N484B	150	10		025 (a - 125v	5	200	70
PS615	150		1.0	250 (a - 125v	30	200	100
PS616	150		1.0	025 (a - 125v	15	200	100
PS617	150		1.0	.025 (a - 125v	5	200	100
1N485	200	1.1		250 (a - 175v	30	125	50
1N485A	200	1.0		.025 (a - 175v	15	200	70
1N485B	200	10		025 (a - 175v	5	200	70
PS621	200		1.0	250 (a - 175v	30	200	100
PS622	200		1.0	025 (a - 175v	15	200	100
PS623	200		1.0	025 (a - 175v	5	200	100
1 N 486	250	11		250 (a - 225v	50	125	50
1N486A	250	10		050 (a - 225v	25	200	70
1N486B	250	1.0		050 (a - 225v	10	200	70
PS627	250		1.0	250 (u - 225v	50	200	100
PS628	250		1.0	050 (a - 225 v	25	200	100
PS629	250		1.0	050 G - 225 V	10	200	100
1 N487	230	1.1		250 (a - 300v	50	125	50
1N487A	330	1.0		100 (a - 300v	25	200	70
PS632	330		1.0	250 (a - 300v	50	200	100
PS633	330		1.0	100 (a - 300y	25	200	100
1N488	420	11	, ,	250 (a - 380v	50	125	50
1N488A	420	10		100 m - 380v	25	200	70
PS636	420	1.0	1.0	250 (a - 380v	50	200	100
PS637	420		1.0	100 (r) - 380v	25	200	100

OTHER ABSOLUTE MAXIMUM RATINGS:
Maximum Power Dissipation 0.5 Watts (ii. 25°C Maximum Power Dissipation 0.25 Watts (ii. 150°C Maximum I Second Surge Current I.5 Amperes (ii. 25°C Storage and Operating Temperature Range – 80° to 200°C

### Varicap

### Voltage-Variable Capacitor

TEI

### ACTUAL SIZE

		pat -	III 4VUC	(S. 4ADC	10. 141 84 8	Austa D.C
	MO	DULATION, A	C AND OTH	ER APPLICA	ATIONS	
V - 7	1	3 0 18	13	18	43	25
V 10	10	4 3-76	13	18	43	25
V-12	12	5 2-31	13	18	43	25
V 15	15	6 5 39	13	18	43	25
V-20	20	10 50	7.0	18.7	40.2	20
V 27	27	14-70	7.0	15.7	33.8	70
V 33	33	17-85	7.0	14.6	31.4	20
V-39	35	20-100	7.0	15.1	32.4	20
V-47	47	24 120	7.0	15.4	32 4	20
V 56	56	32-145	7.0	135	748	15
V 68	68	39-175	9.0	14.0	25 B	15
V 82	82	47 210	9.0	130	239	15
V-100	100	57 260	8.0	11.0	20 2	15
		I .	I .	1		

### HIGH VOLTAGE TYPES TUNING AND OTHER APPLICATIONS

V-7E	7	15 180	3 0	4.5	22.5	100
V-10E	10	2 2 - 26 0	3.5	5.5	27.5	100
V 12L	12	2 7 - 31 0	4.0	6.5	32 5	100
V-158	15	3 3 39 0	4.5	7.5	17.5	100
V-20E	20	5 0 50 0	7.0	18 7	78.5	70
V-27E	27	7 0 70 0	10	15.7	63 5	65
V-33E	33	9 0 85 0	7.0	14.6	56.5	60
V-39E	39	11 0-100 0	7.0	15 1	55 8	55
V-47E	47	14 0 120 0	7.0	15.4	538	50
V-561	56	20 0 145 0	7.0	135	413	10

\*C range specified from 0.1 volts to maximum working voltage

"VARICAP" is the registered trade mark of silicon voltage variable capacities manufactured by Pacific Semiconductors. Inc.

## NEW!

Now available! Two
new semiconductor devices
which may revolutionize
present concepts of
Micro-Miniaturization
and Electrical circuitry!

### 1. PSI microdiode

A major advance in micro-miniaturization. Volume and weight of these new PSI types are approximately 1/20th of present subminiature diodes. Six Fast Recovery Silicon Computer Microdiodes are now available.



### 2. PSI High Q Varican

A complete new approach to advanced circuit design is possible with these new High Q Varicap voltage-variable capacitors. Six types with Q Factors of 50 and 100 and 10, 22, 47 mmf. capacitance are available in standard subminiature package.

Phone, wire or write for complete specifications, delivery schedules and prices.

### Silicon

### Subminiature Rectifiers



ACTUAL SIZE

### MEDIUM POWER TYPES

EIA TYPE NUMBER	MAXI	MUM RA	TINGS	ELECTRICAL CHARACTERISTICS				
	Peak Inv. Voltage (v)	Maximum Avg. Rectified Current (mA) <sup>1</sup>		Minimum Saturation Voltage as 100°C	Maximum Reverse Current @ PIV (µA)		Max. Avg. Voltaga Drep (a. lu – 460 mA	
		€ 25°C	@ 180°C		(6) 4.14 (bW)		€ 25°C (v)1	
					6 25°C	6n 100°C		
1 N645	225	400	150	275	0.2	15	1.0	
1 N646	300	400	150	360	0.2	15	1.0	
1N647	400	400	150	480	0.2	20	1.0	
1 N648	500	400	150	600	0.2	20	10	
1 N649	600	400	150	720	0.2	25	1.0	

### 400 MILLIAMPERE PSI TYPES

400 mA @ 25°C150 mA @ 150°C								
PSI TYPE NUMBER	M	AXIMUM RATIR	ELECTRICAL CHARACTERISTICS					
	Peak Recurr. Inveres Voltage (volts)	Maximum RMS Input Voltage <sup>1</sup> (volta)	Maximum Average Rectified Current <sup>1</sup> (mA)	DC Forward Voltage & Specified Current & 25°C (volte & mA)	Maximum Average Inverse Current <sup>2</sup> 6: 100°C			
		@ 150°C		(a. 25°C				
PS 405	50	15	150	1.5 60 500	500			
PS 410	100	70	150	1.5 @ 500	500			
PS 415	150	105	150	1.5 @ 500	500			
PS 420	200	140	150	1.5 (4, 500	500			
PS 425	250	175	150	1.5 (% 500	500			
PS 430	300	210	150	1.5 (a. 500	500			
PS 435	350	245	150	1.5 (st. 500	500			
PS 440	400	280	150	1.5 (a 500	500			
PS 450	500	350	125	1.5 @ 500	500			
PS 460	600	420	125	1.5 (a, 500	500			

### 250 MILLIAMPERE PSI TYPES

			250 mA	(a 25°C 140 m/	€ 100°C
PS 005	50	35	140	1 (= 100	100
PS 010	100	70	140	1 (a) 100	100
PS 015	150	105	140	1 6 100	100
PS 020	200	140	140	1 (0, 100	100
PS 025	250	175	140	1 (m. 100	100
PS 030	300	210	140	1 (a, 100	100
PS 035	350	245	140	1 (2 100	100
PS 040	400	280	140	1 (a 100	100
PS 050	500	350	140	1 (a. 100	100
PS 060	600	420	140	1 (0 100	100

Resistive or inductive load

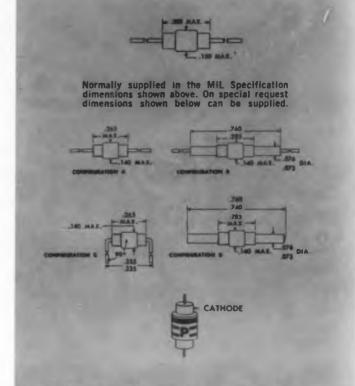
Averaged over one cycle for half wave resistive or choke input circuit with rectifier operating
at full rated current and maximum RMS input.
 Storage and Operating Temperature Range —65°C to 200°C.

500 MA TYPES IN MINIATURE PACKAGE ALSO AVAILABLE.



EIA Typo	Longth Inches	HWR	Max. Rtgs. ns. Load at Ambient	Electrical Characteristics at 25°C Ambient		
		Peak Inverse Voltage Volta	Max. Rectified DC Output Current MA	Fixiward DC Volt Drop at Rated DC Current Volts	Reverse DC Current at Rated PIV MA	
IN1139	43%	3600	6.5	27.0	025	
IN1140	21/2	3600	65	18.0	025	
IN1141	43%	4800	60	36.0	025	
IN1142	21/2	4800	50	24.0	025	
IN1143	45%	6000	90	45.0	025	
IN1143A	45/14	6000	65	30 0	025	
IN1144	61/4	7200	50	54.0	025	
IN1145	43/10	7200	60	36.0	025	
IN1146	61/ta	8000	45	60.0	025	
IN1147	61/14	12000	45	60.0	.025	
IN1148	61/10	14000	50	52.0	025	
IN1149	61/4	16000	43	60.0	025	

Silicon Very High Voltage



### **Physical Characteristics**

HERMETICALLY SEALED — Glass-to-metal fused and metal-to-metal welded seals.

TERMINALS - Tinned copper leads .020 inches diameter. Lead length 11/4 inch minimum.

MARKING — Wide color band indicates cathode end. (Wide band indicates positive bias on Varicaps.) Type number designated by color bands reading from cathode.

ALL DIMENSIONS SHOWN IN INCHES — Patented under one or more of the following United States Patents: No. 2815474, No. 2827403. Other patents pending.

### Silicon

### **HighVoltage Rectifiers**

& ACTUAL SIZE

EIA TYPE NUMBER	Peak Inverse Voltage @ 25 & 100°C (volta)	Continuous DC Voltage (d) 25 & 100 C (volta)	Rec	erage tified rrent nA) @ 190°C	RMS Input Voltage (d. 25 & 100°C (volts)	Max. DC Fwd. Voltage Drep (al 100mA DC 25°C	
1N1730	1000	1000	200	100	700	5	
1N1731	1500	1500	200	100	1050	5	
101732	2000	7000	200	100	1400	9	
1N1733	3000	3000	150	75	2100	12	
1N1734	5000	5000	100	50	3500	18	

Maximum DC Reverse Current (a: Rated PIV = 25°C 10µA 100°C 100µA Maximum Surge Current (8msec.) (a: 25 & 100°C = 2.5 Amps. Length = 1N1730 and 1N1731 50°, 1N1732, 1N1733 and 1N1734 10° Diameter = 375° (1N1734 10°) Leads (030° diam., 11√2° long on all units.

PSI

Ottawa -227 Laurier Ave. West • CE 2-8504

Storage and Operating Temperature Range - 55°C to 150°C

## Pacific Semiconductors, Inc.

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Philadelphia -320 Huntingdon Pike, Rockledge • Pilgrim 2-8089

Madeira Beach, Fla. -P.O. Box 8215 • Phone 7-6126

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• OLive 3-7850

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Electronic Supply Corporation and Kierulff Electronics, Inc. •
OAKLAND—Elmar Electronic Supply. Inc. • PHOENIX—Radio Specialties Corporation • SALT LAKE CITY—Standard Supply Company • SEATTLE—C & H Supply Company.

## Four Layer Diodes Switch 30 to 200 v



A high power four layer diode, type AD is a self-actuated silicon switch similar in function to a relay or gas tube. It is turned on by a voltage pulse and turned off by dropping the current or reversing the voltage. To match circuit requirements, it is available with switching voltages of 30, 40, 50, and 200 v and holding currents of 5 to 45 ma. Compact and rugged, it can handle 300 ma steady dc or a 20 amp pulse current. A string of four in series will switch 800 v, resulting in a peak power of 16 kw for magnetron pulsing, radar beacons, and other modulator applications. The unit can also be used for pulse generator circuits, detonator firing circuits, and de to de power conver-

Shockley Transistor Corp., Dept. ED, Stanford Industrial Park, Palo Alto, Calif.

CIRCLE 64 ON READER-SERVICE CARD

### Noise Figure Test Set

For 200 mc operation

The NF-200 noise figure test set checks tube performance in rf tuners or preamplifiers at 200 mc. It uses a GE ceramic 7077 tube and a 200 mc amplifier of 100 db gain. An integral 3 db attenuator, an output meter, and a separate filtered detector output are included. The unit is designed to JETEC 5.4 subcommittee specifications and may also be supplied for other frequencies in the lift, vhf, and uhf ranges.

LEL, Inc., Dept. ED, 380 Oak St., Copiague, N.Y.

CIRCLE 65 ON READER-SERVICE CARD

CIRCLE 66 ON READER-SERVICE CARD

## 50% lighter... 40% Smaller... Daven's new miniature Egg Crate LC Filters

Now, for airborne and missile applications, Daven offers a miniature version of the popular Egg Crate LC Filter; 50% lighter and 40% smaller than any previous filter!

Frequency range is 0.4 MC to 60.0 megacycles . . . temperature range is  $-55^{\circ}$ C. to  $+125^{\circ}$ C . . . different physical configurations are available depending on allowable space.

The new Filter is suitable for pulse-type circuits and those where the phase shift characteristics must be uniform. It can be pre-tuned in the actual circuit, thus eliminating additional adjustment during assembly. With new production facilities,

these Filters are available in quantity, and each unit is identical in performance to the prototype.

Utilizing no critical materials, the LC Filter is also excellent for medium and wide band-width filters. It can be used for bandwidths down to 0.5%, if under-coupled response is permitted.

Daven's extensive engineering staff, also producing other types of filters extending into the low audio range, is ready to assist you in your filter problems. Just send details of your specific requirement.

THE DAVEN CO.



LIVINGSTON, NEW JERSEY

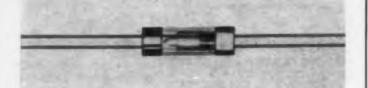
TODAY, MORE THAN EVER, THE DAVEN ® STANDS FOR DEPENDABILITY



### **NEW PRODUCTS**

**Current Sensitive Switch** 

Operates continuously at 750 F



The Pyristor switch is a single shot, current sensitive unit for testing circuitry, bypassing squibs, and protecting devices against surge currents. It is also applicable in current operated triggering devices. Hermetically sealed, the unit is spst, normally open or closed. It operates continuously from -100 to +750 F and for 30 min at 1000 F. It meets MIL-E-5272B humidity requirements and withstands 250 g, 2 to 4 msec shocks and 20 to 20,000 cps, 40 g vibration. It can be used at any altitude.

Thermocal, Inc., Dept. ED, 1627 Colorado St., Santa Monica, Calif.

CIRCLE 67 ON READER-SERVICE CARD

### **Precision Strain Indicator**

Tests strain gage transducers

For strain gage transducer testing and production line quality control, the model LC-261 automatic strain indicator has 0.005% resolution, 0.02% linearity, 0.01% repeatability, and 0.05% absolute accuracy. The unit is a true mv per v indicator. Instrument calibration is continuously adjustable from 1 to 15 mv per v and is independent of input and output impedance from 60 to 1000 ohms. Input power to the transducer is regulated dc voltage, continuously adjustable from 5 to 15 v, and instrument calibration is independent of transducer supply voltage and zero balance adjustment.

Bytrex Corp., Dept. ED, 294 Centre St., Newton 58, Mass.

CIRCLE 68 ON READER-SERVICE CARD

### High Voltage Resins

Withstand high temperatures

Impregnating and encapsulating Aritemp 215 and 221 epoxy resins pass the requirements for class H insulating compounds. Transformer coils impregnated with 221 and encapsulated in 215 will resist 8 kv for more than 1000 hr at temperatures to 200 C. Both resins are one component systems that require no mixing of catalyst and resin.

Aries Labs, Inc., Dept. ED, 45-33 Davis St., Long Island City 1, N.Y.

CIRCLE 69 ON READER-SERVICE CARD

## NOM!

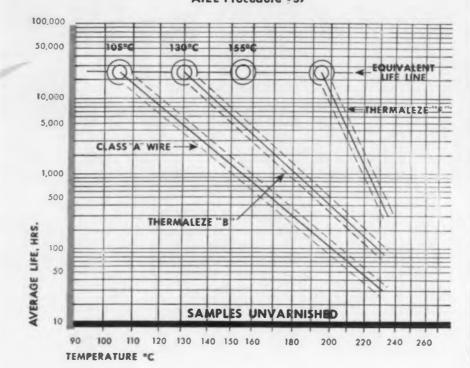
A HIGH TEMPERATURE FILM WIRE DEVELOPED BY PH

APPLIED RESEARCH TO MEET 155°C (CLASS "F"

## THERMA



### AGED DIELECTRIC TWISTS AIEE Procedure #57



PHELPS DODGE

PERFORMANCE...

## 

F

155°C

- Dielectric twist performance establishes Thermaleze F as exceeding (155° C) Class "F".
- Better factor of safety because of improved "heat shock" characteristics.
- Good film flexibility under Class "F" conditions.
- Good balance of electrical, chemical and physical properties.
- Ideal for Class "F" stator windings and high temperature layer or random wound coils.
- Presently available in square and rectangular wire; also in round wire, sizes #8-40.

Any time your problem is magnet wire, consult Phelps Dodge for the quickest, easiest answer!

FIRST FOR

LASTING QUALITY

-FROM MINE

LTO MARKET!



## PHELPS DODGE COPPER PRODUCTS

INCA MANUFACTURING DIVISION

FORT WAYNE, INDIANA

CIRCLE 70 ON READER-SERVICE CARD

ELECTRONIC DESIGN • April 29, 1959

### Commutators

Have 50 channel capacity



These solid state commutators have a 50 channel capacity and a 24 kc sampling rate. Called Radiplex's, they provide asynchronous operation and high common-mode noise rejection. Two models are available: a high level unit with a full scale input of  $\pm 10$  v and a resolution of  $\pm 2$  mv; and a low level unit with a full scale input of  $\pm 10$  v and a resolution of  $\pm 10$   $\mu v$ . Both models have a self-contained power supply.

Radiation, Inc., Dept. ED, P.O. Box 37, Mel-

bourne, Fla.

CIRCLE 71 ON READER-SERVICE CARD

### **Power Transistors**

Have 25 amp dc collector current



Power transistors 2N1162 through 2N1165 have a 25 amp de collector current, 50 or 80 v collector to base voltage, and 35 or 60 v collector to emitter voltage. Maximum junction temperature is 90 C continuous and 100 C intermittent, and collector dissipation for mounting base temperature of 30 C is 50 w. The units are germanium pnp, alloy junction type with collector common to the case. Designed for high current switching and audio applications, they are hermetically sealed in a standard TO-3 package and meet MIL-T-19500A specifications.

Motorola Inc., Semiconductor Products Div., Dept. ED, 5005 E. McDowell Rd., Phoenix, Ariz. CIRCLE 72 ON READER-SERVICE CARD

Don't forget to mail your renewal form to continue receiving ELECTRONIC DESIGN.





# MAGNETICS and MICROWAVE

Creative Imagination was for James Clerk Maxwell the catalyst that united a profound physical intuition and a formidable mathematical capacity in a brilliant formulization of electromagnetics—the basis of all today's practical electromagnetic applications.

At National Co. creative imagination is transmuting observed physical phenomena and mathematically formulated theory in such applications as long range microwave transmission—extending further our practical control of physical phenomena.

The implications of these new means of communications are manifold and the applications multitudinous.

National Co. is a community of minds and talents that enjoys the challenge and the prestige of success in such advanced fields as multipath transmission, noise reduction, correlation techniques for signal processing. Tropospheric scatter systems, lonospheric scatter systems, molecular beam techniques, long range microwave transmission and missile checkout equipment using microwave and digital techniques.

National Co. has grown with the Tradition of New England electronics. Your needs and problems receive exceptional attention at National Co., because, here, creativity is required, recognized and rewarded.

Write or phone

\*tuned to tomorrow Nationa! ~ .

National Company, Inc., Malden, Mass.

MANUFACTURERS OF MATERIEL AND EQUIPMENT FOR U.S. DEFENSE

### **NEW PRODUCTS**

### Airborne Receiver Rack

### For telemetry

Airborne receiver rack ATR-100 contains four of the company's type 1403 crystal controlled phase-lock telemetry airborne receivers; one type SDU-203 spectrum display unit; and one type CSD-170 crystal storage drawer. The type 1403 receivers operate in the 215 to 260 mc range and offer a choice of two second i-f amplifiers of different bandwidths, one of 500 kc at the 3 db points with an attenuation of 60 db 500 kc each side of center frequency and the other of 100 kc with better than 60 db attenuation 250 kc each side of center frequency. They have a noise figure of less than 8 db.

Nems-Clarke Co., Dept. ED, 919 Jesup-Blair Dr., Silver Spring, Md.

CIRCLE 73 ON READER-SERVICE CARD

### High Power Isolator

### Provides 6 db isolation

Over its 350 to 400 mc frequency range, isolated model IUH2 provides over 6 db isolation. The unit has a maximum insertion loss of 1 db and can operate at average power levels above 10 kw. Peak power capacity is 10 mw. Without transitions, the isolator is 10 in. high, 27 in. wide, and 36 in. long.

Raytheon Mfg. Co., Special Microwave Device Group, Dept. ED, River Bldg. 2, Waltham 54, Mass.

CIRCLE 74 ON READER-SERVICE CARD

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### K Band Magnetron

### For missile use

Built for missile applications, type M4154 fixed frequency K band magnetron delivers a minimum peak power of 20 kw. It withstands severe shock and 30 g vibration at 20 to 2000 cps.

Sylvania Electric Products, Inc., Special Tube Operations, Dept. ED. Mountain View, Calif.

### **Transducers**

### Converts frequency to voltage

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Model SMC-15 Magacycler converts pulse rates of as low as 0 to 3 cps to linearly varying dc output. The SMC 5000 converts signals of 0 to 1250 cps up to 0 to 5000 cps to the desired linear dc output. The maximum frequency detected can be adjusted with a built-in attenuator through a more than 4 to 1 frequency detected can be adjusted with a built-in attenuator through a more than 4 to 1 frequency range. Full range linearity of better than 0.5% is standard while Red Line units are linear to as low as 0.1%. Standard temperature sensitivities are better than 100 ppm per degree C, with the Red Line units offering under 50 ppm from -60 to

Pioneer Magnetics Inc., Dept. ED, 5858 Wilshire Blvd., Los Angeles 36, Calif.

CIRCLE 77 ON READER-SERVICE CARD

## Sonic Delay Line Lag type



For use with signals in the sonic frequency range, the F344 lag type delay line has an impedance of 1100 ohms, a bandwidth of 15 kc, and a total delay of 76 µsec ±1%. Taps are provided at each 9.5 µsec, and loading is prevented by precision isolation resistors. Insertion loss is 0.2 db at 15 kc and 3 db at 30 kc; phase linearity is 1%; and vswr is 0.5 db. The unit can be used individually or cascaded for longer delays.

Control Electronics Co., Inc., Dept. ED, 10 Stepar Place Hunting-ton Station, N.Y.

CIRCLE 78 ON READER-SERVICE CARD

CIRCLE 79 ON READER-SERVICE CARD ➤

EIECTRONIC DESIGN • April 29, 1959



Choose from This Wide Range of G-E Ratings

Rated Volts	Surge	NOMIN	NOMINAL CAPACITAN		FARADS
	Volts	Case Size 2" x 4 1/8"	Case Size 2½" x 4½"	Case Size 3" x 4 1/8"	Case Size 3" x 5 5/8"
3 5	5 7	45,000 25,000	70,000 45,000	100,000	150,000 120,000
10	15	20,000	32,000	50,000	75,000
15	20	1 <i>5</i> ,000	25,000	36,000	54,000
25	35	8,700	13,500	21,500	37,000
25	40	7,000	11,000	17,000	25,000
35	45	6,000	9,200	14,200	21,500
50	75	<b>4</b> ,000	7,000	10,000	15,000
75	100	-,		7,000	10,000
100	135			<b>4,</b> 500	7,000
150	185	1,250	2,400	3,250	5,000
200	250	900	1,450	2,250	3,500
250	300	700	1,250	2,000	2,500
300	350	575	1,050	1,600	2,100
350	400	450	750	1,200	1,600
400	475	350	625	1,000	1,400
450	525	300	550	850	1,300

NOTE: Operating temperatures  $-20 \, \text{C}$  to  $+65 \, \text{C}$ . For 85 C applications, another range of units is available with the same physical styles.

GENERAL ELECTRIC HAS EXTENDED ITS LINE of computer-grade Alumalytic capacitors to include unit ratings up to 150,000 micro-

include unit ratings up to 150,000 microfarads. These higher ratings are available in a new case size— $3'' \times 5\frac{5}{8}''$ .

RELIABLE PERFORMANCE AND LONG LIFE are built into General Electric's entire line of Alumalytic capacitors, using the highest purity materials. For example, 99.99% pure aluminum foil anodes insure an oxide-film dielectric with fewest points of high leakage current. This is essential for trouble-free operation and long shelf life.

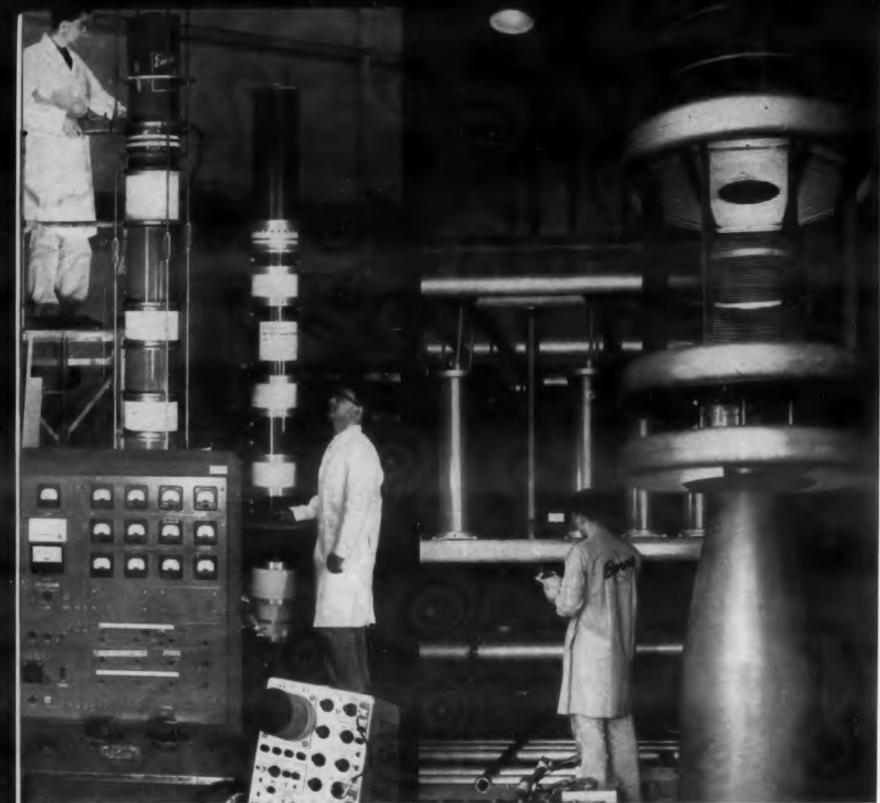
**QUALITY IS MAINTAINED DURING MANU- FACTURE** with stringent in-process controls. Filtered air and controlled humidity prevent variables due to weather changes. A strict inspection is the final check for uniform product quality.

FOR FURTHER INFORMATION OR QUOTA-TION, contact your nearest General Electric Apparatus Sales Office, or write Section 449-9, General Electric Company, Schenectady 5, N. Y.

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Progress Is Our Most Important Product

GENERAL ELECTRIC



artion of Eimac's extensive super-power klystron production and test area.

High-voltage d.c. supply used in manufacturing Eimac super-power klystrons

## SUPER-POWER UHF KLYSTRONS FOR SPACE RADAR NOW IN FULL PRODUCTION AT EIMAC

Tracking fast-moving ballistic missiles and satellites at great distances requires exceptionally powerful radar equipment. Eimac super-power amplifier klystrons, capable of one and one-quarter megawatt peak power and 75 kw average power at ultra-high frequencies, have made these new "space radars" possible. Development of these klystrons, the world's largest electron tubes, has been completed at Eimac and full power tubes have been delivered. They are now being manufactured in production quantities. In addition to radar, Eimac super-power klystrons can be used in linear accelerator and

high-power tropo-scatter applications.

Production of these tubes is being carried on at the Eimac High-Voltage Laboratory in San Bruno, California, where development work was done. Complete facilities are available there for the fabrication, assembly, pumping and testing of these giant tubes. Two power supplies, each capable of producing 120,000 volts d.c. at two and four amperes are used in production and testing operations.

This success in developing and placcing these tubes in full production in a relatively short time is indicative of Eimac's extensive experience in the field of high-power UHF electron devices. Other Eimac amplifier klystron types are used widely in military and commercial tropo-scatter networks throughout the world.

For high power at ultra-high frequencies investigate the many advantages of Eimac external-cavity amplifier klystrons.

### EITEL-McCULLOUGH, INC.



San Carlos . California

### **NEW PRODUCTS**

### Thermoelectric Material

For cooling small volumes

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These thermoelectric bismuth telluride compositions cool or regulate the temperature of small volumes. Thirty grams of the material in a cooling junction with a temperature difference of 40 C can handle about 1/2 to 3/4 w heat load at its cold junction. With smaller temperature differences, this heat load can be considerably increased.

Merck & Co., Inc., Dept. ED, Lincoln Ave., Rahway, N.J.

CIRCLE 80 ON READER-SERVICE CARD

### **Digital Voltmeter**

Has automatic range switching

The model 520 digital voltmeter has automatic range and polarity switching throughout its 0 to ±1200 v de range. It also has a momentary, three-position lever switch which permits instant checking of both calibration and zero. This switch may be operated while the instrument is in use, thus providing an absolute check of any measurement. The unit can operate digital printers directly and has 0.1% full scale accuracy and 20 meg input impedance.

Franklin Electronics Inc., Dept. ED, Bridgeport, Pa.

CIRCLE 81 ON READER-SERVICE CARD

### VTVM

Has dc to 1500 mc frequency range

The model 1041B vtvm has a frequency range from dc to 1500 mc and a frequency response that is flat to within  $\pm 0.2$  db from 50 cps to 500 mc, or -0.5 to +3 db from 20 cps to 1500 mc. Its ranges are 25 mv to 300 v ac; 10 mv to 1 kv, dc; and 0.02 ohm to 500 meg. Center zero facilities are provided on all dc ranges.

Marconi Instruments, Dept. ED, 111 Cedar Lane, Englewood, N.J.

CIRCLE 82 ON READER-SERVICE CARD

✓ CIRCLE 83 ON READER-SERVICE CARD

#### Instrument Knobs

#### **Aluminum**

With a special opening through which numbers or indications can be read, these aluminum instrument knobs unmistakably show their position. They are available in 12 colors.

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Vemaline Products Co., Dept. ED, Hawthorne, N.J.

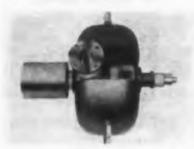
CIRCLE 84 ON READER-SERVICE CARD

#### Q Meter Covers 1 kc to 300 mc

This Q meter covers 1 kc to 300 mc and measures Q from 5 to 1000. It provides accuracies of  $\pm 5\%$  at 100 mc,  $\pm 12\%$  at 200 mc, and  $\pm 20\%$  at 300 mc. Delta Q controls are provided to facilitate batch testing. A complete range of accessories, including test inductors and series and dielectric loss test jigs is available.

Marconi Instruments, Dept. ED, 111 Cedar Lane, Englewood, N.J. CIRCLE B5 ON READER-SERVICE CARD

Klystron
Rated at 1 kw cw

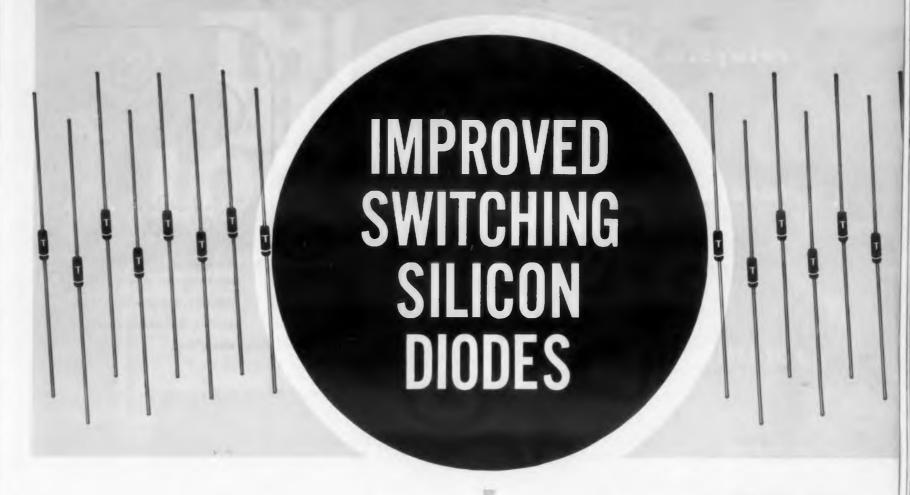


Model VA-802, 1 kw cw, air-cooled, 4-cavity klystron can be continuously tuned from 1700 to 2400 me and is focused with a permanent magnet. Designed specifically for forward scatter communication systems, it is suitable for both fixed station and transportable service. Power gain of each tube is from 40 to 50 db. Power output into flat line for a vswr of 1.1 or less is 1000 w, and rf drive power—for maximum efficiency tuning—is 0.1 w max. Typical efficiency is 40%.

Varian Associates, Dept. ED, 611 Hansen Way, Palo Alto, Calif.

CIRCLE 86 ON READER-SERVICE CARD ➤ CIRCLE 87 ON READER-SERVICE CARD

#### A NEW PRODUCT FROM TRANSITRON...



Transitron's advanced solid-state development program has now produced the industry's most versatile selection of computer switching diodes.

High forward conductance and 0.3 microsecond inverse recovery are combined with low 125°C leakage currents. The performance of logic circuits in the 10 ma region is improved with the low capacity (3  $\mu\mu$ f) 1N806-1N807 diodes. Higher current circuitry can be reliably operated using 1N808-1N809 diodes.

For less stringent temperature environments, Transitron also provides a selection of standard 100°C fast switching diodes.

Production quantities of all types are immediately available from stock. Small quantity requirements can be obtained from your authorized Transitron distributor.

#### FAST SWITCHING SILICON DIODES, SUBMINIATURE GLASS PACKAGE

Minimum		Max. Rev. Current		Minimum Saturation	Reverse Recovery (256 JAN)				
	Forward Current @ 1 V		d Voltage y volts)	Voltage @ 100 µa. (25°C)	Max. Rec. Time	Rec. Level	1	V	
Туре	(ma)	25°C	125°C	(volts)	µsес	μа	ma	volts	
1N809	100	1.0 @ 200	50 @ 200	220	0.3	350	30	35	
1N808	100	1.0 @ 100	50 @ 100	110	0.3	350	30	35	
1 N807	4.	.5 @ 175	50 (a) 175	200	0.3	100	5	40	
1 N 8 0 6	4.	.5 @ 100	50 @ 100	110	0.3	100	5	40	
		25°C	100°C	25°C					
1N663	100	5 @ 75	50 @ 75	100	0.5†	200	5	40	
1N658	100	.05 @ 50	25 @ 50	120	0.3	500	5	40	
1N659	6	5 @ 50	25 @ 50	55	0.3	88	30	35	
1N660	6	5 @ 100	50 @ 100	110	0.3	88	30	35	
1N661	6	10 @ 200	100 @ 200	220	0.3	88	30	35	
1N643	10	1 @, 100	15 @ 100	200	0.3†	200	5	40	
1N662	10	20 @ 50	100 (a, 50	100	0.5†	400	5	40	

• Maximum 1 mc capacity = 3  $\mu\mu$ f (-10 Volts)

† IBM Modified "Y" Circuit

Temperature Range -55°C to 150°C

For complete data, write for bulletins PB-51 and TE-1350

TRANSISTORS • RECTIFIERS • DIODES • REGULATORS • VOLTAGE REFERENCES



-

electronic corporation • wakefield, massachusetts



Since their introduction a short time ago, AMPHENOL Micro-Ribbon connectors have been used in an ever-increasing number of high-reliability applications: Radioactivity recorders, relays, telephone equipment, computer modules, satellites—in hundreds of miniaturized applications where there can be no compromise with reliability.

Micro-Ribbons are the *first* miniature rack & panel connectors to provide increased reliability over their standard-size counterparts. With an improved "ribbon" contact (no tiny pin contacts to bend and misalign), Micro-Ribbons mate smoothly and efficiently, have easy insertion and extraction. Both mating members are self-wiping, self-cleaning members with double contact action at all times.

Contacts	Rack & Panel Pluga	Mating Receptacles	Cable-to-Chassis Plugs	Mating Receptacles
14	57-10140	57-20140	57-30140	57-40140
24	57-10240	57-20240	57-30240	57-40240
36	57-10360	57-20360	57-30360	57-40360
50	57-10500	57-20500	57-30500	57-40500

Investigate the features and specifications of AMPHENOL Micro-Ribbon connectors—write for complete information.



connector division

AMPHENOL-BORG ELECTRONICS CORPORATION

chicago 50, illinois



off-the-shelf delivery . . .

To provide you with the advantage of off-the-shelf delivery, along with factory pricing and single-source expediting.

AMPHENOL MICRO-RIBBONS

and other standard AMPHENOL components are carried in stock by Industrial Electronic Parts Distributors.

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AMPHENOL Distributor in your
area who can have AMPHENOL
components at your door today
or tomorrow! Take advantage
of this time and money saving
service on your next
requirement for moderate
quantities of standard
AMPHENOL Components.

Your local AMPHENOL salesman can supply you with the names of the Distributors in your area who stock the AMPHENOL products you require.

SERVICE TO INDUSTRY
THROUGH AUTHORIZED
ELECTRONIC PARTS DISTRIBUTORS



#### **NEW PRODUCTS**

#### **Power Sources**

Have adjustable output power

Designed to permit accurate calibration of bidirectional power monitors and termination wattmeters, model 215 power sources have output power that is adjustable from 20 to 100% of rated power. Tuning is continuous over the frequency ranges. Four models are available covering 25 to 50, 50 to 150, 150 to 470, and 470 to 1000 mc. The units are self-contained including power supply and are supplied in bench cabinets or for rack mounting.

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Sierra Electronic Corp., Dept. ED, 3885 Bohannon Dr., Menlo Park, Calif.

CIRCLE 88 ON READER-SERVICE CARD

#### **VHF Transceivers**

For local or remote control

Model 90C vhf transceiver and its remote control version, model 90CR, incorporate a 90 channel 118 to 127 mc transmitter and a tunable 108 to 128 mc receiver. They also contain a transistorized power supply and modulator. Shock mounted in a standard glove compartment opening, the units draw 2.2 amp at 28 v dc.

Dare, Inc., Dept. ED, Troy, Ohio.
CIRCLE 89 ON READER-SERVICE CARD

#### X Band Magnetrons

For missile and airborne use

Magnetron 2J42B and 6027H are fixed frequency X band devices designed especially for missile and other airborne applications. Minimum peak power outputs are 14 kw and 18 kw respectively. The tubes withstand 5 g vibration at 10 to 500 cps with less than 3 mc frequency shift and less than ±0.5 mc frequency modulation. They also withstand 50 g shock for 4 msec and may be operated up to 60,000 ft.

Sylvania Electric Products, Inc., Special Tube Operations, Dept. I.D., Mountain View, Calif.

CIRCLE 90 ON READER-SERVICE CAR

← CIRCLE 91 ON READER-SERVICE CARD

#### **FM-AM Generator**

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An fm-am signal generator for narrow band mobile work, model 995A/4 covers 1.5 to 220 mc. It drifts less than 0.002% per 10 min and has both stepped and continuous incremental frequency controls. An internal fm noise of less than 25 cps enables it to measure 70 to 80 db adjacent channel rejection at 25 kc channel spacing.

Marconi Instruments, Dept. ED, 111 Cedar Lane, Englewood, N.J. CIRCLE 92 ON READER-SERVICE CARD

#### Oscilloscope

Monitors up to seven channels

Designed for continuous function monitoring of up to seven channels simultaneously in one rack unit, the model 218A oscilloscope provides a means for viewing and evaluating complex voltages. Mainly for use with tape recording and data handling systems, it is suited for measuring and analyzing mechanical quantities through a transducer. Such quantities include stress, strain, vibration, pressure displacement, and acceleration.

Sierra Electronic Corp., Dept. ED, 3885 Bohannon Dr., Menlo Park, Calif.

CIRCLE 93 ON READER-SERVICE CARD

#### Microwave Ferrites

Low loss

These microwave ferrites are low loss magnesium manganese compounds. Type M-022, for general applications at C band frequencies and above, can be used in Faraday rotation and reciprocal phase shifting devices. Type M-032, for use in the S band and below, has low saturation moment and narrow line width. It can be used in resonance isolators and performs well in coaxial phase shifters down to several hundred mc.

Motorola, Inc., Solid State Electronics Dept., Dept. ED, 3102 N. 56t'. St., Phoenix, Ariz.

CIRCLE 94 ON READER-SERVICE CARD ➤ CIRCLE 95 ON READER-SERVICE CARD ➤



# General Electric small panel meters

BIG LOOK styling of General Electric's new small panel meters adds functional beauty to your products and equipment. Distinctive design creates the illusion of bigness, yet these new meters fit into the same panel space as old style meters. You get big border-to-border scale . . . modern, clean-line design . . . your choice of seven attractive colors . . and widest selection of scales.

Up to 28% longer scales allow accurate readings. Tough neoprene gaskets provide complete protection of internal parts and movements from dirt, dust or water. Best of all, General Electric BIG LOOK meters are competitively priced. And you can plan on fast delivery, too, from a national network of authorized stocking distributors and G-E Apparatus Sales Offices.

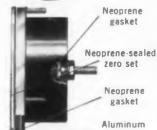
Let G.E.'s BIG LOOK in panel meters help you improve the appearance and reliability of your equipment at low cost. Get the full story. Just contact your G-E Apparatus Sales Engineer, or write for bulletin GEA-6678, Sect. 593–303, General Electric Co., Schenectady, N. Y.



SELF-SHIELDED CORE-MAG-NET, used in d-c milliammeters below 5 MA and all microammeters, permits mounting of meters on magnetic or non-magnetic panels without special calibration.



ALL A.C METERS utilize moving-iron mechanisms plus magnetic damping to settle the pointer quickly and accurately.



COMPLETELY SEALED CASES protect internal parts of instrument from harmful contaminants. Even zero-set is sealed with a neoprene Oring.

Progress Is Our Most Important Product





IS M. SCHNEIDERMAN, PROJECT ENGINEER ON THE DUAL, USING HIS UNIT FOR ONE OF ITS MANY APPLICATIONS

## AN ULTRA-HIGH SENSITIVITY **DUAL-BEAM OSCILLOSCOPE OFFERING** A GREAT VARIETY OF DISPLAYS

The Du Mont DUAL (Type 411) is a dual beam oscilloscope of high sensitivity embodying an unusually varied selection of displays. It is a true dual-beam scope employing a multigun cathode ray tube. Each vertical channel may be operated independently of the other, with complete amplitude calibration facilities on both.

#### BRIEF SPECIFICATIONS

SENSITIVITY (both channels identical): Through amplifier, ac or dc-100 uvolts/ major scale division (1 mv full scale).

FREQUENCY RESPONSE: dc to 100 kc

**SYNCHRONIZATION SOURCE:** External. power line or internal pickoff from either Y-amplifier; syncs on either polarity.

SWEEP SPEEDS: Calibrated sweeps, 19 fixed steps ranging from 1 sec/cm to 1 usec/cm in a 1-2-5 sequence. Uncalibrated sweep (through amplifier), continuously variable from 1 sec/cm to 2 usec/cm.

SWEEP EXPANSION: Up to five times full scale on either channel independently with no on-screen distortion.

VERTICAL EXPANSION: Up to three time full scale.

VOLTS/DIVISION RANGES: VOLTS PER DI-VISION switch settings .001, .01, .1, 1 and 10 with MULTIPLIER switch settings x .1, x .5, x 1, x 2, and x 5.

POWER SOURCE: 115/230 volts ± 10%, single phase 50 — 400 cps. Transistorized heater regulation on all critical amplifier circuits.

CATHODE-RAY TUBE: 5 ARP-, operating at 2500 volts.

MECHANICAL: Size: Type 411, 171/2" x  $13\frac{1}{2}$ " x  $23\frac{1}{4}$ " overall. Type 411-R,  $17\frac{1}{2}$ " x 19" (panel),  $13\frac{1}{2}$ " (behind panel) x 21",  $1\frac{3}{4}$ " protrusion in front of panel. Weight approx. 70 pounds.

HAND-CRAFTED WIRING THROUGHOUT

**\$995**00

PRICE: Type 411 & 411-R F.O.B. Clifton, N.J., U.S.A.



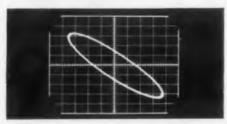
**EXPANDED TIME BASE DISPLAY** — With a signal from one channel applied on a calibrated time base, that same signal (or a different one) may be displayed on an expanded time base through the other channel. X5 expansion is available on either channel

**DUAL-BEAM DISPLAY** — Outputs of the ultra-

high-sensitivity deflection amplifiers of each

channel are applied on identical time bases

for clear and accurate comparison.



**ULTRA-HIGH-SENSITIVITY X-Y PLOTTING** — At the turn of a front panel control, outputs of the two deflection amplifiers may be applied to the X-Y axes of one channel, providing the most sensitive identical X-Y amplifier scope available. In this condition there is still an unused channel to display either of the above signals against time.

> WRITE FOR COMPLETE INFORMATION

INSTRUMENT DIVISION

Allen B. Du Mont Laboratories, Inc. • 760 Bloomfield Ave., Clifton, N. J.

#### **NEW PRODUCTS**

#### Tube Shield Liner and Shields

Dissipates up to 50% of heat



The Therma-flex liner with the NW type shield will reduce the bare bulb temperature of tubes by more than 50% and when used with the TR type shield will reduce the tenperature by approximately 35%. They are available in shields for all standard size miniature tubes as well as some of the larger noval type tubes such as the 6094. The shields and liners have been designed to meet the requirements of MIL-S-9372, MIL-S-19786 and SCL6307/2.

International Electronic Research Corp., Dept. ED, 145 W. Magnolia Blvd., Burbank, Calif.

CIRCLE 96 ON READER-SERVICE CARD

#### Switching Transistors

High gain

Power transistors 2N1136, A, and B; 2N1137, A, and B; and 2N1138, A, and B are designed for use in power switching and control circuits. They are provided in current gain ranges of 50 to 100, 75 to 150, and 100 to 200 at a collector current of 3 amp dc. Featuring a flat beta curve, they have a 5 amp maximum current rating and can switch power up to 400 w. Collector to emitter breakdown voltage ratings are 40. 70, and 80.

Bendix Aviation Corp., Red Bank Div., Semiconductor Products, Dept. ED, 201 Westwood Ave., Long Branch, N.J.

CIRCLE 97 ON READER-SERVICE CARD ← CIRCLE 98 ON READER-SERVICE CAFD

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#### Converters

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Model AC-1 manual ranging and AC-2 automatic ranging converters are designed for use with the company's digital voltmeters. They have a 30 cps to 20 kc range, 0.01% linearity, 0.02% stability, and 10 meg input impedance. Full-wave rectification provides an accuracy of ±0.1% and 2 digits on four ranges.

Cubic Corp., Dept. ED, 5575 Kearny Villa Rd., San Diego 11,

CIRCLE 105 ON READER-SERVICE CARD

#### **Transfer Function** Analyzer

Tests automatic control systems

Designed to test the frequency response of automatic control systems, this transfer function analyzer has a 0.5 cps to 10 kc range. It can deal with phase differences from 0 to . The 360 deg, amplitude differences to 70 db, and harmonic distortion to 100%. The equipment consists of the company's AD-880-A/1 two phase low frequency decade oscillator; AD-729-B/100 low frequency phasemeter; and AD-925-A tunable filter.

> Muirhead Instruments, Inc., Dept. ED, 677 Fifth Ave., New York 22,

CIRCLE 106 ON READER-SERVICE CARD

#### Instrument Calibration Standard

Has digital readout

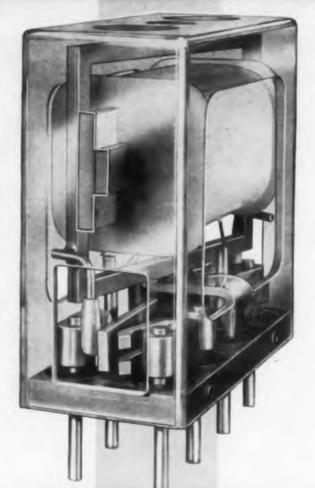
A digital reading instrument calibration standard, the model 1294 supplies de voltages from 1 mv to <sup>2</sup> kv in 12 full scale ranges; dc current from 10 µa to 30 amp in 12 full scale ranges; and ac voltages and currents over the same span with 14 e 40, full scale ranges for each function. Accuracy is  $\pm 0.1\%$  for dc and  $\pm 0.3\%$ Bank for ac functions, and ac indication is Dept. true rms. Printed readout is avail-Long able as an option.

Radio Frequency Labs, Inc., Dept. ED, Boonton, N.J.

CIRCLE 107 ON READER-SERVICE CARD CIRCLE 108 ON READER-SERVICE CARD >

#### 4 times actual size

Mock-up of CLARE Type F Relay enlarged to show operating mechanism. Note bifurcated contacts which enable this relay to handle a wide variety of contact loads.



#### With this O

#### You can handle contact loads from 3 amperes down to 1 microampere, 1 millivolt

#### SPECIFICATIONS

SPEC	IFICATIONS
Ambient Temperature	65° C to +125° C.
Shock	.65 Gs for 11 milliseconds.
	.5-75 cps at maximum excursion of $\frac{1}{4}$ inch, 75-2000 cps at 20 Gs acceleration.
	. Sea level—1000 volts rms between terminals and frame, and between adjacent circuits; 750 volts rms between contacts of a set. At 80,000 ft., 350 volts rms.
	.1000 megohms minimum at 125° C.
Coils	. Coils up to 10,000 ohms available for a wide range of voltage or current operation.
Nominal Operating Power.	. 250 milliwatts.
Pickup Time	.3.5 milliseconds nominal.
Dropout Time	.1.5 milliseconds nominal.
Contact Arrangement	.2 pdt (2 form C).
Contact Rating	3 amps resistive at 28 volts d-c or 115 volts a-c; also will handle loads of 1 microampere @ 1 millivolt reliably.
Contact Resistance	.0.03 ohm maximum.
	.500,000 operations minimum at 2 amps; 100,000 operations minimum at 3 amps; 1,000,000 operations minimum at 1 amp.
Enclosure	Hermetically sealed, filled with dry nitrogen at 1 atmosphere pressure.
Mounting	All popular mounting arrangements available.
Terminals	Printed circuit; solder; plug-in (matching socket available). Variations of printed-circuit terminal length on 1/10-inch grid spacing available.
Weight	.17 grams.
Military Specifications	MIL-R-25018, except as to contact





**ACTUAL SIZE** All popular mounting arrangements are available. Terminal arrangements nicely suited to 1/10 Inch grid spacing.



• In one relay—the Type F—CLARE provides a precise component of unusual flexibility for long life operation under a wide variety of contact loads.

Tests have shown a performance of over 22,500,000 operations at 0.1 ampere, 115 volts a-c. Minimum contact life at 3 amperes is 100,000 operations. Contacts have carried 1 microampere, 1 millivolt for 700,000 operations with a failure resistance of 500 ohms, with no misses recorded.

This amazing low-level life is primarily a result of the use of gold plated contacts. These same contacts, however, will carry up to 3 amperes.

A special plug-in mounting arrangement that will stand extreme shock and vibration is now available.

The CLARE Type F Relay is hermetically sealed, operates perfectly in a wide range of temperatures, withstands heavy shock and vibration—is fast and more than moderately

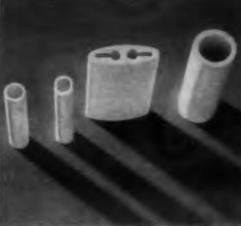
Send for Engineering Bulletin No. 124 Write or call C. P. Clare & Co., 3101 Pratt Blvd., Chicago 45, Illinois. In Canada: C. P. Clare Canada Ltd., 2700 Jane Street, Toronto 15. Cable

Address: CLARELAY.

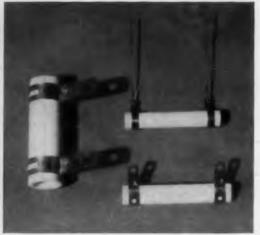
FIRST in the industrial field



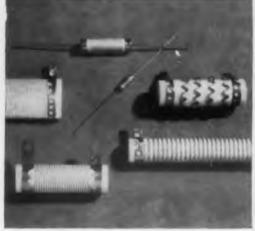
tough tests for incoming material



specially selected ceramic core materials



rigid, low resistance terminals



finest alloy resistance wire

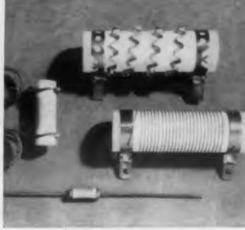
THIS IS A

YOU CAN

RESISTOR

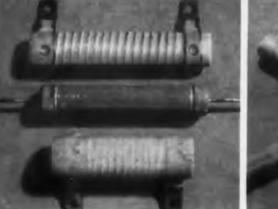
STAKE YOUR

REPUTATION ON

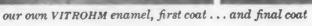


spot welded or silver brazed junctions









#### Built-in VITROHM reliability, from core to final vitreous enamel, lets you solder these resistors in and forget 'em

They come in a tremendous variety of sizes, shapes and ratings, but all Ward Leonard VITROHM resistors have one thing in common: They're built for maximum reliability.

Take just one point - ceramic cores, for example: Made by Ward Leonard to exacting specs, the cores feature low-porosity, high-dielectric-strength ceramic for maximum moisture exclusion and good electrical insulation. What's more, the thermal coefficient of linear expansion of ceramic is specially selected to make the core compatible with resistance wire, enamel and terminals . . . to prevent cracking, crazing, peeling, or layer separation.

And there's the same meticulous care with all the other elements that go to make up a finished VITROHM resistor: terminals, spot welded or brazed junctions, resistance wire, and last but not least, W/L VITROHM enamel, formulated and manufactured in our own modern enamel smelting plant...provides complete electrical and mechanical protection.

To insure reliability in your product ... specify VITROHM's. Write for data packed catalog #15, and list of stocking Electronic Distributors: Ward Leonard Electric Co., 77 South Street, Mount Vernon, N.Y. (In Canada: Ward Leonard of Canada Ltd., Toronto.) 9.4

CIRCLE 56 ON READER-SERVICE CARD



LIVE BETTER ... Electrically

Result- Engineered Controls Since 1892



RESISTORS RHEOSTATS RELAYS CONTROLS DIMMERS

#### **NEW PRODUCTS**

#### **Taper Pin Connectors**

**Dual** row



Type UPCC-FDTP printed card connectors have two rows of taper pin terminals linked mechanically and electronically for use with AMP 53 taper pins. Available with 7, 11, 15, 19, 23, or 32 contacts, they may also be obtained in custom con-

U. S. Components, Inc., Dept. ED, 454 E. 148th St., New York 55, N.Y.

CIRCLE 57 ON READER-SERVICE CARD

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#### **Telemetering Equipment** Modular



Transistorized airborne or ground based telemetering equipment for data acquisition, K-series modules can be supplied as systems or as individual units. The current line consists of: electronic commutators for time-division multiplexing of high level data signals; mechanical commutators for time-division multiplexing of high and low level signals; low level amplifiers for raising millivolt commutated inputs to the 0 to 5 v level; pulse width keyers for coding commutator outputs; and low voltage system power supplies. The units operate from -55 to +100C and withstand 30 g, 5 to 2000 cps vibration and 200 g, 11 msec shocks.

Applied Science Corporation of Princeton, Dept. ED, P.O. Box 44, Princeton, N.J.

CIRCLE 58 ON READER-SERVICE CARD

Don't miss an issue of ELECTRONIC DESIGN; return your renewal card

# Static Inverters Have high stability



Model 12-115-60AC static inverters have non-saturating timeconstant design which permits frequency stability over as much as ±60% of the input dc voltage. Efficiency up to 95% is obtained by elimination of zener diodes and other voltage regulation devices. Standard units have square-wave output, both sinusoidal output is available. The completely transistorized units are protected against overload and short circuit, and operating temperature range is -40to +70 C. Input voltage: 12 v dc. Output voltage: 115 v ac, rms. And output power is 175 va continuous, 250 va intermittent.

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Static Inverters Corp., Dept. ED, 2501 East 68th St., Long Beach, Calif.

CIRCLE 113 ON READER-SERVICE CARD

#### **Precision Potentiometer**

#### Noise free

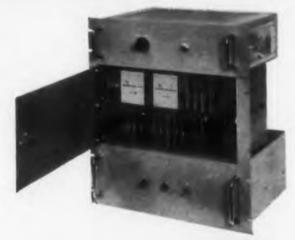
A 4 w, multisection, wirewound potentiometer, model 158 provides noise free operation from -55 to +105 C. It is available in resistances up to 150 K and has an independent linearity of  $\pm 0.25\%$ , resistance tolerance of  $\pm 5\%$ , and resolution of 0.05%. Insulation resistance is 100,000 meg and life expectancy is 5 million revolutions. Special models are available with 0.2% independent linearity,  $\pm 1\%$  resistance tolerance, 0.025% resolution, 500,000 meg insulation resistance, and a -65 to +150 C temperature range.

New England Instrument Co., Dept. ED, 320 Main St., Woonsocket, R.I.

CIRCLE 114 ON READER-SERVICE CARD

CIRCLE 115 ON READER-SERVICE CARD ➤





TMI Type 1092-BQ8A
Core Storage Buffer

DATA SYSTEMS COMPATIBILITY—with the New TMI Core Storage Buffer

This fully transistorized unit stores up to 1092 eight-bit characters at 100-kc rate. The buffer is compactly designed for relay rack mounting and is complete with integral power supply. Ideally suited to synchronizing data systems operating at different speeds.

Features include: interlaced load and unload • capacity expansion • convenient clear control • internal checking circuits • ease of installation • economy • unit is priced 22% below previously available buffers of similar characteristics.

In addition to the Type 1092-BQ8A, TMI produces a full line of core storage buffers for an almost infinite variety of applications. Units are available in capacities from 80 to 2184 characters. Components, assemblies, and completed buffers each undergo rigorous tests. Request copy of specification #191 containing complete data.

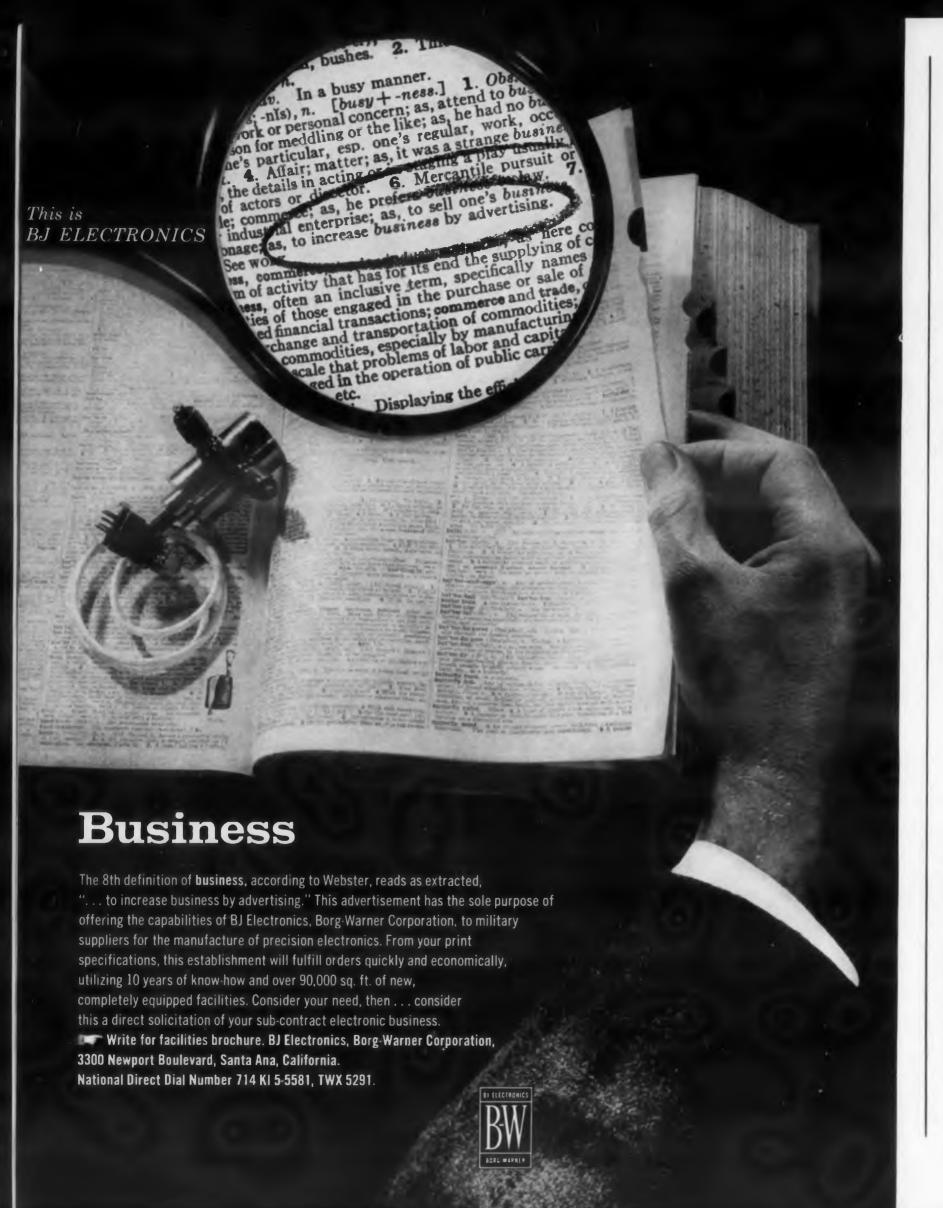
#### IMPORTANT JOB OPPORTUNITIES

Expansion to handle our increasing business activity plus research and development in new areas have created openings for qualified computer engineers. Investigate the wonderful opportunities offered by TMI in Southern California

#### 1/ TELEMETER MAGNETICS Inc.

Manufacturers of Ferrite Cores . Core Arrays . Buffers . Memories

2245 pontius avenue, los angeles 64, california • 306 "h" st., n.w. washington 13, d.c.



#### **NEW PRODUCTS**

#### Pulse-Waveform Generator

Frequencies of 0.01 to 2000 cps



Long calibrated pulses, sine, triangular and square waves can be generated with this unit. Signals are generated over a frequency range of 0.01 to 2000 cps. Pulse lengths are calibrated from 100  $\mu$ sec to 10 sec, with an accuracy of  $\pm 3\%$ . Constant duty cycle operation may be selected with calibrated pulse duty of 10 to 90% over the full frequency span. Maximum pulse amplitude is 50 v at 40 ma. Dial accuracy is  $\pm 2\%$ , frequency stability  $\pm 1\%$ , and output stability within 2%.

Kennedy Co., Dept. ED, 2487 E. Washington St., Pasadena, Calif. CIRCLE 127 ON READER-SERVICE CARD

#### Beam Switching Tube Tester

Checks all ten positions

Designed for the company's type 6700 and BD-301 beam switching tubes, the model 600 tester permits quick checking of all ten tube positions both statically and dynamically. It has an internal power supply, a spade voltage meter, a variable spade voltage control, a target current meter, and a built-in pin straightener. Other features include visual indication of beam position, manual or automatic cycling, and provision for monitoring cathode current externally and for monitoring and adjusting grid bias level.

Burroughs Corp., Dept. ED, P.O. Box 1226, Plainfield, N.J.

CIRCLE 128 ON READER-SERVICE CA D

€ CIRCLE 129 ON READER-SERVICE CATD

#### Signal Generator

Output of 4 to 410 mc

Model SG-54A standard signal generator has an output of from 4 to 410 mc. Incidental fm is less than 300 cps at 50% modulation of any rf or modulation frequency. vswr is less than 1.1 and frequency drift less than 0.001% over a 10 min period after warm-up. Output level is continuously variable from 0.1 to 100,000 mv. The carrier may be internally or externally sine wave modulated or externally pulse modulated. In pulse modulation, the rise time is better than 1 usec from 6 me to 120 me and better than 0.5 usec from 120 to to 410 mc. Frequency calibration is within 0.5% and resettability better than 0.05%. Modulated spectrum distortion is less than 3% at 50% modulation.

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Trad Electronics Corp., Dept. ED. 101 First Ave., Asbury Park, N.J. CIRCLE 130 ON READER-SERVICE CARD

#### TWT Amplifier

Provides 30 db gain

This twt amplifier provides a 30 db power gain from 12 to 16 kmc. It uses a permanent magnet twt weighing less than 5 lb and needs no electromagnet for focusing. Power supply regulation is 0.1%, ripple is 10 mv, and total weight is

Menlo Park Engineering Co., Dept. ED, 711 Hamilton Ave., Menlo Park, Calif.

CIRCLE 131 ON READER-SERVICE CARD

#### **Potentiometers**

650 ohm to 100 K range

Series T single-turn potentionieters are 7/8 in. in diameter and have standard resistances ranging from 650 ohms to 100 K. Power rating is 1.2 w at 40 C, derating to zero at 125 C. The units have standand linearity tolerances of  $\pm 0.5$  and ±0.2% and meet MIL-R-19 and NAS 710 specifications.

Beckman Instruments, Inc., Helipot Div., Dept. ED, 2500 Fullerton Rd., Fullerton, Calif.

FIRCLE 132 ON READER-SERVICE CARD CIRCLE 133 ON READER-SERVICE CARD >

# Lambda Power Supplies have been the first choice of engineers in every independent poll



The only power supplies guaranteed for 5 years

This unprecedented five-year guarantee is the strongest proof of consistent trouble-free power supply performance ever offered. It is bolstered even further by a series of independent surveys which prove that Lambda equipment is preferred by more than 50% of the engineers who specify power supplies.

#### CHECK LIST: LAMBDA REGULATED DC POWER SUPPLIES

Model	Style	Voltage Range (VBC)	Current Range (MA OC)	Regulation Impedance Ripple (Table I)		t	Output Voitage Control	Output Terminals	Size Weight (Table II)	Price (U.S. and Canada) F.D.B. Factor College Pt., N. Y.
			REGUL	ATED PO	WER	SUPPLIES — RACK	MOUN	TING		
TRANSIS	TORIZED									
LT-1095 LT-1095M	Rack	0·32 0·32	0-1000 0-1000	A	Ξ	None 21/2" rect	Rear Rear	Rear Rear	S-1 S-1	285 00 315 00
LT-2095 LT-20 <b>9</b> 5M	Rack Rack	0-32 0-32	0-2000 0-2000	B	_	None 21/2" rect	Rear Rear	Rear Rear	S-1 S-1	365.00 395.00
TUBE RE	GULATED									
C-280	Rack	0-200	0-200	C	10A	None	Rear	Rear	S-2	184.50
C-280M	Rack	0-200	0-200	C	10A	31/2" rect	Rear	Rear	S-2	214.50
C-281	Rack	125-325	0-200	C	10A	None	Rear	Rear	S-2	159.50
C-281M	Rack	125-325	0-200	C	10A	31/2" rect	Rear	Rear	S-2	189.50
C-282	Rack	325-525	0-200	C	10A	None	Rear	Rear	S-2	169.50
C-282M	Rack	325 525	0-200	C	10A	3½" rect	Rear	Rear	S-2	199.50
C-480	Rack	0-200	0 400	0	15A	None	Rear	Rear	S-2	259.50
C-480M	Rack	0-200	0 400	D	15A	31/2" rect	Rear	Rear	S-2	289.50
C-481	Rack	125-325	0 400	D	15A	None	Rear	Rear	S 2	244.50
C-481M	Rack	125 325	0 400	0	15A	3½" rect	Rear	Rear	S-2 S-2	274.50 259.50
C-482 C-482M	Rack Rack	325 525 325-525	0 400	D	15A 15A	None 31/2" rect	Rear	Rear	\$ 2	289.50
					_					
C-880	Rack	0 200	0-800	E	20A	None	Rear	Rear	S-3	340.00
C-880M C-881	Rack	0-200 125-325	0.800	E	20A	3½" rect	Rear	Rear	S-3 S-3	370,00 315.00
C-881M	Rack	125-325	0-800	E	20A 20A	None 3½" rect	Rear	Rear	2-3	345.00
C-882	Rack	325 525	0-800	Ē	20A	None	Rear	Rear	S-3	360.00
C-882M	Rack	325 525	0-800	Ē	20A	31/2" rect	Rear	Rear	5.3	390.00
C-1580	Rack	0 200	0.1500	F	30A	None	Rear	Rear	S-4	550.00
C-1580M	Rack	0 200	0-1500	F	30A	31/2" rect	Rear	Rear	5-4	580.00
C-1581	Rack	125-325	0-1500	F	30A	None	Rear	Rear	5.4	575.00
C-1581M	Rack	125 325	0-1500	F	30A	31/2" rect	Rear	Rear	S-4	605 00
C-1582	Rack	325-525	0-1500	F	30A	None	Rear	Rear	S-4	650.00
C-1582M	Rack	325-525	0.1500	F	30A	31/2" rect	Rear	Rear	5-4	680.00
28	Rack	200-325	0-100	G	3A	None	Rear	Rear	\$-5	59.50
28M	Rack	200-325	0.100	G	3A	31/2" rect	Rear	Rear	S-5	89.50
29	Rack	100-200	0-100	Н	3A	None	Rear	Rear	S-5	69.50
29M	Rack	100-200	0-100	H	3A	3½" rect	Rear	Rear	\$-5	99.50
32	Rack	200-325	0-300	J	2 @ 5		Rear	Rear	\$ 6	139 50
32M	Rack	200-325	0-300	1	205		Rear	Rear	56	169.50
										154.50
33 33M	Rack Rack	100-200	0-300	J	2 0 5		Rear Rear	Rear	S 6	184.50
50R	Rack	0-500	0-500	K	205		Frent	Fr & rear	\$-7	420.00
		0-50	Bias	ï						
		0-200	High Imped	L M		-				
			REGULATI	D POWE	R SU	PPLIES — PORTABI	E AND	BENCH		
25	Bench	200-325	0-100	6	3A	None	Frent	Frent	8-2	69.50
26	Bench	100-200	0-100	H	3A	None	Frent	Frent	S-8	79.50
50	Bench					See Model 50	R ahave		S-9	440.00
		0.500	0.200	N	2 - 5					
71	Portable	0·500 0·50 <b>0</b> ·200	0-200   Bias   High Imped	P	2 @ 5	3 1/2" rect	Frent	Frent	\$-10	310.00

#### TABLE I DC DUTPUT VOLTAGE REGULATION. IMPEDANCE, RIPPLE

	REGUL	Internal	Ripple, rms		
	Line (105-125 VAC)	Load (min to max)	(ehms)	(millivetts or %)	
	Less than	Less than	Less than	Less than	
A	0.15% or 20MV	0.15% or 20MV	0.50	1 mv	
B	0.15% or 20MV	0.15% or 20MV	0.025	1 mv	
C	0.15% et 0.3V	0.25% or 0.5V	6	3 mv	
D	0.15% er 0.3V	0.25% or 0.5V	3	3 av	
E	0.15% or 0.3V	0.25% or 0.5V	1.5	3 mv	
F	0.15% or 0.3V	0.25% er 0.5V	0.75	3 mv	
G	1%	1%	10	10 mv	
H	1%	1%	10	5 mv	
J	1%	1%	4	10 mv	
K	0.15% or 0.1V	0.5% or 0.3V	2	8 mv	
L	0.1%	unregulated	3,300	2 mv	
M	0.1%	unregulated	17,500	5 mv	
N	0.15% or 0.3V	0.15% or 0.3V	4	5 mv	
P	0.1%	unregulated	5,500	2 mv	
q	0.1%	unregulated	25.000	5 mv	

TABLE II SIZES AND WEIGHTS

	WEB				
	:has)			Net (ibs)	Shippin (lbs)
31/2	x 19	H	14%	35	65
51/4	x 19	1	14%	53	80
7	к 19	H	14%	84	100
8 3/4	д 19	H	14%	120	140
51/4	x 19	K	8	19	23
101/2	x 19	1	91/4	42	52
101/2	х 19	X	141/4	89	140
8	x 14	E	6	19	23
121/2	x 22	E	15	110	158
13	x 8%	H	141/2	49	85
	5¼ 7 8¾ 5¼ 10½ 10½ 10½ 8 12½	6% x 19 5% x 19 10% x 19 10% x 19 8 x 14 12% x 22	5½ x 19 x 7 x 19 x 6¼ x 19 x 5½ x 19 x 10½ x 19 x 8 x 14 x 12½ x 22 x	5½ x 19 x 14% 7 x 19 x 14% 6¾ x 19 x 14% 5¼ x 19 x 8 10½ x 19 x 8 10½ x 19 x 9¼ 10½ x 19 x 14¼ 8 x 14 x 6 12½ x 22 x 15	5½ x 19 x 14% 53 7 x 19 x 14% 84 8½ x 19 x 14% 120 5½ x 19 x 8 19 10½ x 19 x 8 42 10½ x 19 x 14½ 89 8 x 14 x 6 19 12½ x 22 x 15 110

#### GENERAL SPECIFICATIONS

Sufficient tolerance is incorporated in the specifications to allow for normal commercial component and tube deviations. Tube replacements may be made with any equivalent tubes meeting E.I.A. specifications.

INPUT 105-125 VAC, 50-400 CPS, single phase. Exceptions: Models 50, 50R and 71 — 105-125 VAC, 50-60 CPS.

DC OUTPUT Voltage Range: Continuously variable over ranges specified, except where otherwise noted.

Current Range: The current ranges given apply to the entire DC output voltage range, and for input voltages from 105 to 125 VAC. No "de-rating" is necessary.

Polarity: Either positive or negative terminal may be grounded.

AC OUTPUT The AC output is unregulated, isolated and ungrounded. It has a value of slightly higher than 6.3 V

(when fully loaded) at an input of 115 VAC. This value allows for voltage drop in connecting leads. Dual outputs may be connected in series or parallel.

DUTY CYCLE Continuous duty at full load.

METERS Where meters are indicated, a separate voltmeter and milliammeter are provided.

**OVERLOAD PROTECTION** Ample protection is provided against external overload and internal failure conditions by means of fuses.

Circuit breakers of the magnetic, "trip-free" type are employed in Models 50, 50R, 71 and LT series as protection against external overloads. And in the LT series, the transistor complement is independently protected by special transistor circuitry.

STYLE Rack Models are designed for mounting on standard

Bench Models are provided with compact, specially-designed, ventilated cabinets equipped with carrying handles. The power supply units may be removed from their cabinets for mounting in standard relay racks (except Models 25, 26 and 71).

RATINGS AND COMPONENTS All components used are of the highest quality and are operated well within manufacturers' ratings. Hermetically-sealed, oil-filled capacitors are used exclusively, except in LT series, where special high purity foil, long-life electrolytics are used. Can and LT series power supplies use hermetically-sealed magnetic components exclusively. Ample safety factors are provided in the design to insure the long life, and the dependable, trouble-free operation so desirable in industrial and laboratory applications.

All specifications and prices subject to change without notice.



#### LAMBDA ELECTRONICS CORP.

11-11 131 STREET . COLLEGE POINT 56, NEW YORK

INDEPENDENCE 1-8500 CABLE ADDRESS: LAMBDATRON, NEW YORK

Keep this check list handy

#### **NEW PRODUCTS**

#### Miniature RF Filters

Have 0 to 1250 mc cutoff frequencies



These lumped constant, low pass rf filters have cutoff frequencies from 0 to 1250 mc and provide sharp attenuation in the stop-band region. At a frequency of 1.2 times cutoff, attenuation is 20 db or higher; and at 1.5 times cutoff, it is at least 60 db. Units down to 100 mc cutoff are 3-1/2 in. long, including end connectors. Suited for the generation of signals for testing the frequency response of rf circuits, or in vswr measurements, the filters may also be used in transmitter or telemeter systems for missiles and aircraft. They are finished in nickel plated brass with BNC male and female end connectors. Input power is normally 10 w, maximum; impedance, 50 ohms.

Telonic Industries, Inc., Dept. ED, Beech Grove, Ind.

CIRCLE 121 ON READER-SERVICE CARD

#### **Voltage Regulator**

Has 115 v rated output

With a 150 w load and a constant frequency of 60 cps, the LVR-150 voltage regulator maintains an output voltage within  $\pm 0.5\%$  of the rated 115 v through input variations between 95 and 130 v. With a 200 w load and 105 to 130 v input variation, the output is regulated to within  $\pm 2\%$ . The unit can also regulate output voltage to within ±5% with rated load, 95 to 130 v input variation, and 50 to 63 cps frequency variation. The main assembly is housed in a 5 x 6 x 6 in. case with a four terminal input-output plug, and the diode bridge and associated components are mounted under a cover plate on the side of the main unit.

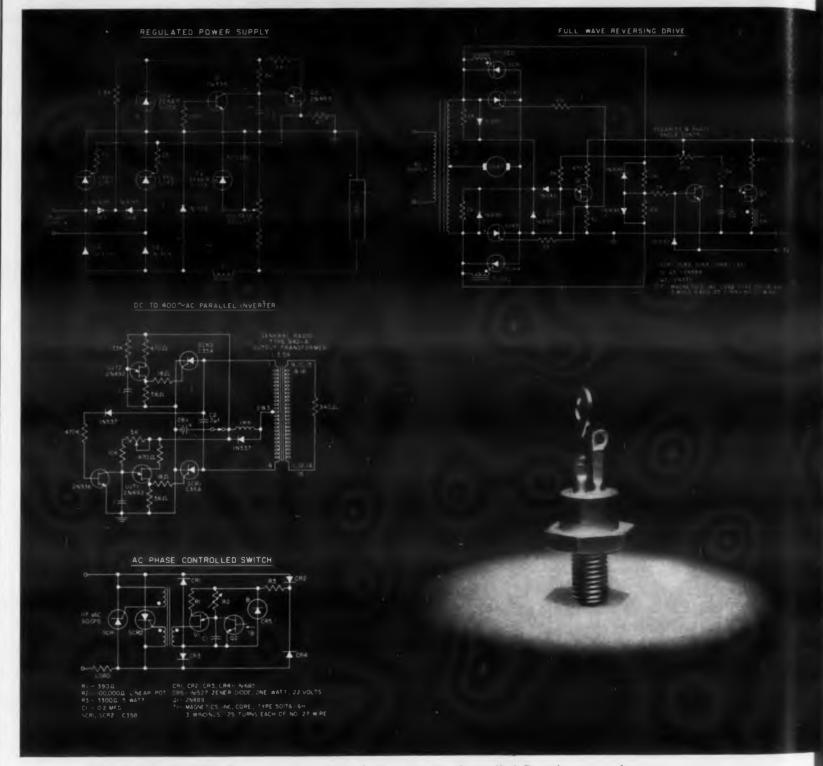
J. B. Rea Co., Inc., Electronics Div., Dept ED, 2202 Broadway, Santa Monica, Calif.

CIRCLE 122 ON READER-SERVICE CARD

Don't forget to mail your renewal form to continue receiving ELECTRONIC DESIGN.

#### General Electric Semiconductor News

#### New prices, new circuits for



FOUR BASIC CIRCUITS. Above are four basic designs for the Controlled Rectifier using the unijunction transistor as the firing means. The unijunction is a precision trigger, putting out short, high current pulses. The frequency of these pulses will not vary with the supply voltage or temperature, yet can be variably controlled with a silicon triode from a low level feedback signal. Unijunction firing circuits are easily synchronized with 60 cycle line frequency. In short, the unijunction provides the simplest and least expensive means for precision firing of the Silicon Controlled Rectifier.

General Electric's new silicon medium-current rectifiers. Types 1N2154 thru 1N2160, are ideal as companion devices to the controlled rectifier for reverse-voltage protection and, also, for applications in full-wave circuitry.

SAMPLE LIST OF POWER MANDLING AND OTHER JOBS THAT CAN NOW BE DONE BETTER BY THE G-E CONTROLLED RECTIFIER

- Converters, DC to DC, DC to AC
  Phase controlled DC power supplies, regulated & unregulated
  Frequency converter, current
  Power switch for automatic tempelectronic flash
  Reversible moor

- automatic temperature control electronic flash \* Reversible motor control \* AC variable speed induction motor
- Dynamic braking

- Light dimmers
   Thyratron replacement for relay drivers
   Pulse width conversion
- High speed printer for digital computer
   Welding control
   Ignitron firing
   Circuit breaker replace

EL

#### revolutionary G-E Controlled Rectifier

"Controlled rectifiers may revolutionize the electrical industry." This statement was made a year ago by a respected news publication. Since then samples have been studied by hundreds of firms. Many new circuits have been developed which promise important improvements in functions, reliability, simplicity, accuracy and lower cost. In just one year prices have been reduced 75 percent (see chart below). And now, the G-E Silicon Controlled Rectifier is a standard, production-line item, warranted in writing and available at sharply reduced prices.

This is the time for design engineers to exploit the inherent advantages of the Silicon Controlled Rectifier in their circuit designs. Many applications are proved...the firing circuits have been refined...the product line is stabilized . . . and it makes sound economic sense. Call or write your G-E Semiconductor Sales Representative for complete details. The Controlled Rectifier is also available from many local G-E Distributors.

HOW THE G-E CONTROLLED RECTIFIER WORKS. The Silicon Controlled Rectifier is a three junction semiconductor device for use in power control and power switching applications requiring blocking voltages up to 400 volts and load currents up to 16 amperes. Series or parallel circuits may be

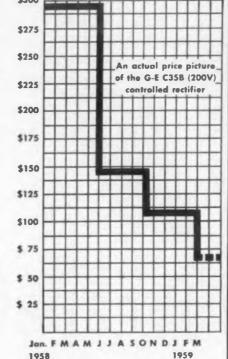
used for higher power applications.

The G-E Controlled Rectifier's reverse characteristic is similar to a normal silicon rectifier in that it represents essentially an open circuit with negative anode to cathode voltage. The forward characteristic is such that it will block positive anode to cathode voltage below a critical breakover voltage if no signal is applied to the gate terminal. However, by exceeding the forward break-over voltage or applying an appropriate gate signal the device will rapidly switch to a conducting state and present the characteristically low forward voltage drop of a single junction silicon

DETAILED NOTES are available on the application of the G-E Silicon Controlled Rectifier, plus reprints of articles that have appeared in technical journals. Write to Section S25359, Semiconductor Products Dept., General Electric Company, Electronics Park, Syracuse, New York.

STEADY PRICE DROP. Since its introduction one year ago, the price of the typical G-E Controlled Rectifier has dropped more than 75 percent. This results from improved manufacturing techniques and volume production. The G-E Controlled Rectifier is now a production-line item, warranted in writing for one year and subjected to the same quality control tests imposed on all General Electric transistors and rectifiers.

The G-E Controlled Rectifier is also available at even less cost (ZJ39L series) for use at 100°C and below, with currents up to 10 amperes.



MAXIMUM ALLOWABLE RATINGS (Resistive or Inductive Load)

NOTES on the APPLICATION of the SILICON

ONTROLLED

Continuous Peak Inverse Voltage (PIV) Transient Peak Inverse Voltage (Non-Recurrent<5 millisec.) RMS Voltage (Vams), Sinusoidal Average Forward Current (Is) Peak One Cycle Surge Current (Isorge) Peak Gate Power Average Gate Power Peak Gate Current (Is) Peak Gate Voltage (Vs) (forward) Storage Temperature Operating Temperature	150 ams 5 wat 0.5 w 2 ams 10 vol	ts atts peres	C35G 150 225 105	C35B 200 300 140	C35H 250 350 175	35C 300 400 210	C35D 400 volts 500 volts 280 volts
CHARACTERISTICS (At Maximum Ratings) Minimum Forward Breakever Voltage (V <sub>IO</sub> ) Maximum Reverse (I <sub>R</sub> ) or Forward (I <sub>S</sub> ) Leakage Current (Full Cycle Average) Maximum Forward Voltage (V <sub>I-AVG</sub> ) Maximum Gate Current To Fire (I <sub>GF</sub> ) Maximum Gate Voltage To Fire (V <sub>GF</sub> ) Typical Gate Current To Fire (I <sub>GF</sub> )	25 ma 3 vol	ts	C35G 150 6.5 rage}	C35B 200 6.0	<b>C35H</b> 250 5.5	<b>C35C</b> 300 5.0	C35D 400 volts 4.0 ma

ZJ39L Series—lower cost series with ratings similar to above, but for use up to 100°C maximum, with forward current ratings up to 10 amperes. ZJ50 Series—a high-current series now in development, and available on a prototype-sample basis.



CIRCLE 123 ON READER-SERVICE CARD

#### Temperature Monitoring System Multipoint



This continuous temperature monitoring system consists of monitor modules, each of which receives inputs from 10 thermistor probes, and an alarm indicator module. Up to 10 modules, 100 points, can be handled by one alarm indicator module, and all points are monitored simultaneously. No scanning devices are used. Designed to detect and furnish warning when the temperature at any protected point reaches a preselected high or low limit, the system can provide protection for processing equipment and all types of industrial installations. It monitors temperatures from -25 to +600 F.

Fenwal Inc., Dept. ED, Ashland, Mass. CIRCLE 124 ON READER-SERVICE CARD

#### Large Waveguide Window

#### For multimegawatt applications

This large waveguide window is designed for multimegawatt applications with the company's WR-2100 waveguide. It provides good radio frequency continuity and a standing wave ratio of 1.03 over a 10% band.

I-T-E Circuit Breaker Co., Dept. ED, 1900 Hamilton St., Philadelphia 30, Pa.

CIRCLE 125 ON READER-SERVICE CARD

#### Variable Speed Drive

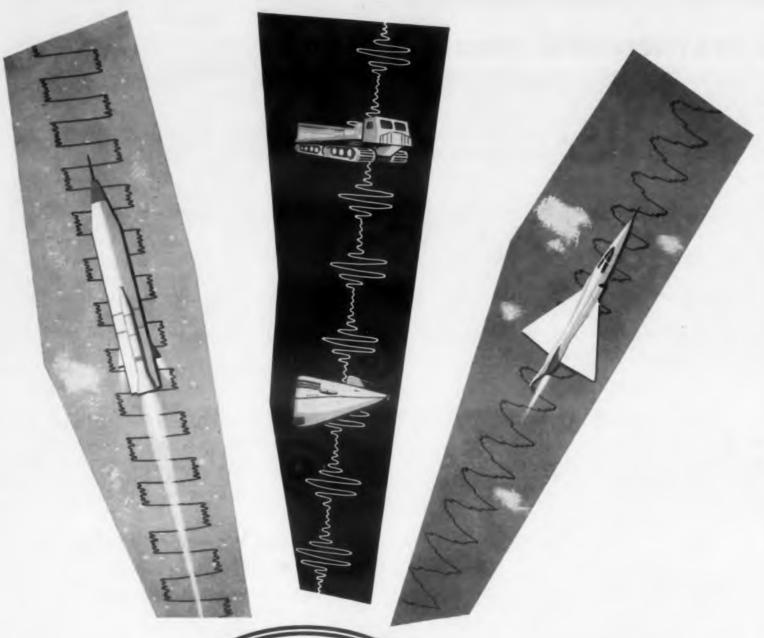
#### Has 10 turn vernier dial

For exact adjustment to any speed setting or for duplication of previous speed settings, this 2 in. square Servotran variable speed drive can be furnished with an accurately calibrated vernier 10 turn dial. The unit can provide output shaft speeds infinitely variable from 0 to 1200 rpm, forward and reverse. It is available with motors in the 1/100 to 1/40 hp range. Other models for applications requiring between 1/1000 and 1/10 hp are also available.

Humphrey, Inc., Humphrey Products Div., Dept. ED, 3794 Rosecrans St., San Diego 10, Calif.

CIRCLE 126 ON READER-SERVICE CARD

#### FOR OPTIMUM PROTECTION FROM VIBRATION/SHOCK/NOISE



utilize (LORD) capabilities

Greater reliability—your problem? LORD can help you do something about it. Protective mounting systems, designed, tested and produced at LORD, insure high reliability for sensitive equipment.

LORD is a diversified, capable technical organization, supported by modern facilities and prepared to complete challenging assignments in controlling vibration, shock and noise.

Your project can benefit from experience gained in working on Atlas, Talos, Jupiter, B-58, F-105, F11F, Convair 880, ground support, vehicular, shipboard, submarine and other advanced classified projects.

LORD is ready to work as an integral member of your team.

#### FIELD ENGINEERING OFFICES

LORD MANUFACTURING COMPANY . ERIE, PA.

ATLANTA, GEORGIA · CEdar 7-9247 BOSTON, MASS. - HAncock 6-9135 CHICAGO, ILL. - Michigan 2-6010 DALLAS, TEXAS · Riverside 1-3392 DAYTON, OHIO · BAIdwin 4-0351

A-CEdar 7-9247 DETROIT, MICH. - Diamond 1-4340

IAncock 6-9135 KANSAS CITY, MO. - WEstport 1-0138

LOS ANGELES, CAL. - HOllywood 4-7593

NEW YORK, N. Y. - Circle 7-3326

PHILADELPHIA, PA. - PEnnypacker 5-3559

SAN FRANCISCO CAL. - EXbrook 7-6280

"In Canada - Railway & Power Engineering Corporation Limited"

CIRCLE 116 ON READER-SERVICE CARD

#### **NEW PRODUCTS**

# Precision Potentiometer Operates at 230 C



The series 42 wire-wound precision potentiometer is designed to operate at temperatures up to 230 C, with a wattage rating of 0.25. Resistance change after 255 hr at 230 C is less than 0.1%. Insulation resistance is 10,000 meg min. Resistance tolerance is  $\pm 5\%$  from 1 to 100,000 ohms. Independent linearity is  $\pm 0.5\%$  and noise is less than 5  $\mu$ v. It has screw terminals for simple and positive connections and comes with bushing type mounting, although servo type can be furnished.

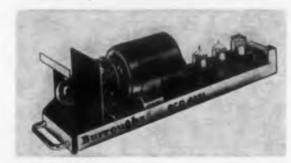
Clarostat Mfg. Co., Inc., Dept. ED, Dover, N. H. CIRCLE 117 ON READER-SERVICE CARD

#### **Decoder Modules**

For binary coded decimal information

SE

Silico



Decoder modules type BCD-8421 and BCD-4221 are designed to take the respective binary coded parallel information directly to the input of a beam switching tube and display the equivalent decimal information on a Nixie in-line indicator tube. The beam switching and Nixie tube combination has an access time of 1 µsec and an inherent memory. The modules are plug-in, printed circuit type and have display repetition rates in excess of 1 kc.

Burroughs Corp., Electronic Tube Div., Dept ED, Box 1226, Plainfield, N.J.

CIRCLE 118 ON READER-SERVICE CARD

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Circle 119 for Allied Circle 120 for Texas

ELECTRONIC DESIGN • April 29, 1959

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FILLS THE WHOLE BILL

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on **TEXAS INSTRUMENTS SEMICONDUCTORS** 

PRICES ON

Silicon Transistors: 1-999

Germanium Transistors: 1-99

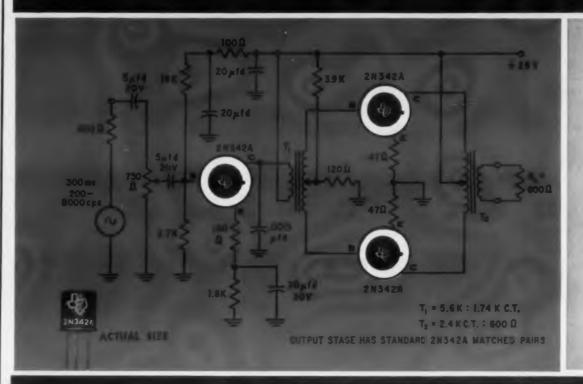
Silicon Diodes and Rectifiers: 1-999

ALLIED RADIO CORP.

100 N. WESTERN AVE. CHICAGO BO, ILLINOIS HAymarket 1-6800 TWX: CG - 2898

TI Silicon Transistor Application Note

## TRANSISTORIZED INTERCOM EXCEEDS MIL-E-5272B SPECS



#### **CIRCUIT SPECIFICATIONS**

150-mw output from -55°C to 100°C at less than 10% harmonic distortion over frequency range

Frequency response @ 25°C stable within ±2 db of 1000 cps 100 mw reference level from 200 to 8000 cps

Frequency response @ -55°C and 100°C within ±3 db of 25°C frequency response

Less than 3-db gain variation @ -55°C and 100°C compared to 25°C measurement

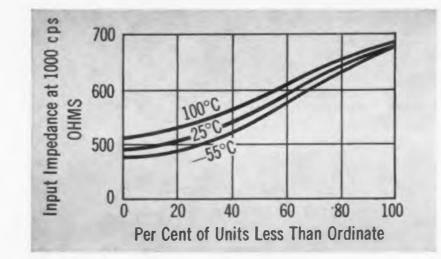
## LOUD AND CLEAR AT 100°C!

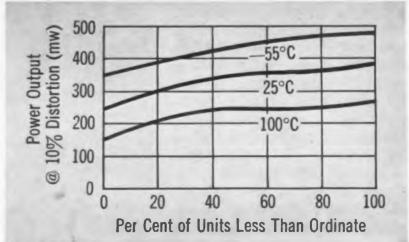
#### with TI 2N342A silicon transistors from stock

You can satisfy the 71°C equipment requirements of MIL-E-5272B at 100°C with the intercom amplifier circuit shown above — using TI 2N342A silicon transistors with . . . guaranteed 3-to-1 linear beta characteristics...85-v collector-to-emitter breakdown, giving a wide safety range with 28-v aircraft supplies . . . plus dissipation capability of 1 watt at 25 °C and 200 mw at 125 °C.

The newest addition to the use-proved TI 2N339 series introduced in 1957, this medium-power unit carries the full-year TI guarantee and is immediately available off-the-shelf from all TI distributors in 1-249 quantities. For production quantities, contact your nearest TI sales office.

TYPICAL INTERCOM AMPLIFIER PERFORMANCE CHARACTERISTICS USING 2N342A TRANSISTORS







from THE WORLD'S LARGEST SEMICONDUCTOR PLANT

#### Texas Instruments

INCORPORATED

SEMICONDUCTOR-COMPONENTS DIVISION POST OFFICE BOX 312 . 13500 N. CENTRAL EXPRESSWAY DALLAS, TEXAS

tion

#### **NEW PRODUCTS**

## Transistorized Power Inverter

Dc to sine wave ac



Model 591-J transistorized power inverter is designed to insure maximum performance from ac gyros and motors. No excess heat is created because the output waveshape, being sinusoidal, avoids the heat-producing harmonics. Unit is fully encapsulated and hermetically sealed. Nominal input voltage: either 24, 26 or 28 v dc. Output voltage: 26 and 115 v ac standard. Output frequency of 400 cps is standard, with 1200, 1500 and 2000 cps available. Output power: 40 va; operating temperatures: —55 to +71 C.

Arnold Magnetics Corp., Dept. ED, 4613 W. Jefferson Blvd., Los Angeles 16, Calif.

CIRCLE 134 ON READER-SERVICE CARD

#### **Receiving System**

For low-level beacon signals

A complete receiving system, the Microlock model 90208-2 receives low-level beacon signals from missile or satellite borne transmitters, permitting accurate measurements of position and velocity as well as recording of telemetered information. Sensitive to signals down to -150 dbm, the system is designed for use with an interferometer antenna system and operates on a phase-locked-loop principle. Angular position can be determined to an accuracy of 1 mil. The system is mounted in a standard relay rack and is furnished with power supplies and alignment and monitoring equipment.

Resdel Engineering Corp., Dept. ED, 330 S. Fair Oaks Ave., Pasadena, Calif.

CIRCLE 135 ON READER-SERVICE CARD



# M&DONNELL Lircraft Lambert-Saint Louis MUNICIPAL AIRPORT . BOX 516, ST. LOUIS, MO.



#### PERSONAL:

NAME -

McDonnell Aircraft ADDRESS -

Beautiful suburban St. Louis, Missouri AGE -

HEALTH - Excellent, growing with vigor and stability.

PHYSICAL APPEARANCE - 3,930,076 gross square feet of floor area dedicated to the mastery of air and space. A beautiful campus-like

environment featuring the most advanced facilities for creative

A total staff of 25,000; 4,000 of whom comprise our Engineering SIZE -

MILITARY SERVICE:

A prime contractor of U.S. Defense Department.

#### BUSINESS ACHIEVEMENTS:

PAST -FD-1 Phantom - First all-jet airplane to take off and land on

F2H Banshee - Famous Korean War fighter jet.

Little Henry and XVI Convertiplane - First ramjet helicopter. XVI Convertiplane made first successful conversion from helicopter to

PRESENT Talos - the airframe and power plant of this missile designed and developed at McDonnell.

Voodoo - Holder of three transcontinental speed records, the F-101B Interceptor now in quantity production.

F3H Demon - Missile carrying all weather Navy fighter now in

F4H - Production award winner for Mach 2+ all weather Navy fighter. Quail - Prime contractor for air-launched Air Force decoy missile.

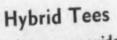
Utility Jet - Company is vigorously engaged in the Air Force UCX competition for a multi-purpose, 4-jet trainer-transport. McDonnell entry will be capable of going anywhere in the world at cruising

Electronics - Development and quantity production of an electronic automatic checkout system for IOIB aircraft. This system will completely check out the many electrical and electronic systems and sub-systems within minutes.

Space Exploration - McDonnell just awarded contract by N.A.S.A. to develop and build FIRST MANNED SATELLITE CAPSULE.

#### FUTURE OBJECTIVES -

McDonnell will continue to diversify and intensify its efforts in all areas of engineering research, development and production, related to air and space vehicles for our Armed Forces.



For large waveguides



This hybrid Tee, which can be used as either test equipment or as a functional part of a system, is made in both plain and folded types. Waveguide sizes range from WR770 through WR2300, covering a uhf frequency range of 320 to 1450 mc. Among applications are: power dividers; balanced mixers; sideband modulators; power discriminators and phase detectors.

I-T-E Circuit Breaker Co., Dept. ED, 1900 Hamilton St., Philadelphia 30, Pa.

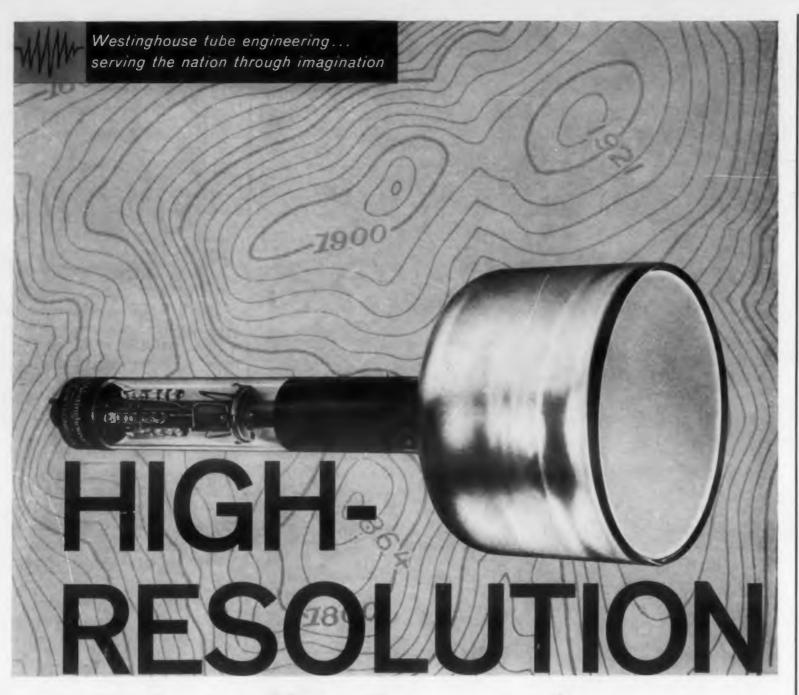
CIRCLE 136 ON READER-SERVICE CARD

#### **Insulation Testers Portable**

Portable Hipot testers S2, DC, S5 DC, and S10 DC cover 0 to 2, 0 to 5, and 0 to 10 kv dc, respectively. They incorporate a 4 in. meter for direct indication of leakage current; a direct reading, 4 in. kilovoltmeter connected directly across the output; and a dead front safety grounded control panel. They are protected against overloads and surges and provide a continuously adjustable output voltage from zero to maximum. The units can be used to measure leakage current, for breakdown testing, or as high voltage power supplies where a few milliamperes of current is adequate. They measure 8 x 14 x 8 in, and weigh 20 lb.

Peschel Electronics, Inc., Dept. ED, RFD 1, Patterson, N.Y. CIRCLE 137 ON READER-SERVICE CARD

← CIRCLE 870 ON READER-SERVICE CARD



# radar display tube

New cathode-ray tube features electrostatic-focus and offers proven performance in high-resolution radar.

The Westinghouse 5CEP11 is a high-resolution, electrostatic-focus, magnetic-deflection cathode-ray tube primarily designed for presentation of radar displays. It's particularly useful in conjunction with photographic recording systems, such as radar reconnaissance for mapping. The face-plate is optically flat, and employs gray glass for superior contrast. The 5CEP11 will produce a line width not to

exceed 0.0015" at 10 KV anode potential. Line width is measured in production at half amplitude of the light energy distribution of a single line—this is a precise measurement not subject to operator error.

The 5CEP16 is designed for flying spot scanners and also has 0.0015" line width. Sample or production quantities of either 5CEP11 or 5CEP16 are available.

YOU CAN BE SURE ... IF IT'S

Westinghouse
Electronic Tube Division, Blmira, N.Y.

CIRCLE 138 ON READER-SERVICE CARD

#### **NEW PRODUCTS**

POCKET ADDING MACHINE AND SLIDE RULE.—This 13-scale log-log slide rule has a 5 in. scale length and a six digit adding machine on its reverse side. A P scale makes it possible to find any sine and cosine of an angle without determining the angle.

Harrison Home Products Corp., Dept. ED, 565 Fifth Ave., New York 17, N.Y.

CIRCLE 139 ON READER-SERVICE CARD

LIGHTHOUSE TRIODE.—General purpose model GL-6771 is a high mu, metal ceramic unit for use in grounded grid service as a radio frequency amplifier, oscillator, or frequency multiplier. As a cw oscillator, it can be used at frequencies to 4000 mc.

General Electric Co., Power Tube Dept., Dept. ED, Schenectady 5, N.Y.

CIRCLE 140 ON READER-SERVICE CARD

MINIATURE INSTRUMENT NUTS.—Miniature turned nuts in a range of types, shapes, and sizes for use in precision instruments and miniaturized equipment. Supplied to customer specifications with standard or special threads in diameters down to 1/8 in hexagon. Lengths and diameters are held to +0.000 and -0.005 in.

Fischer Special Mfg. Co., Dept. ED, 422 Morgan Ave., Cincinnati 6, Ohio.

CIRCLE 141 ON READER-SERVICE CARD

TUBE SOCKET SAVERS.—These rugged units are designed for 7, 8, and 9 pin miniature sockets in electron tube testers.

Forway Industries, Inc., Dept. ED, 122 Green Ave., Woodbury, N.J.

CIRCLE 144 ON READER-SERVICE CARD

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SOLID STATE POWER SUPPLIES.—Miniature Transpac short-circuit and transient proof power packs cover 5 to 60 v dc in fixed and adjustable voltage types. Available in ratings to 200 ma, they operate from an input source of 105 to 125 v ac, 60 or 400 cps.

Electronic Research Associates, Inc., Dept. ED. 67 Factory Place, Cedar Grove, N.J.

CIRCLE 145 ON READER-SERVICE CARD

CHASSIS LATCH.—The 35L is designed for engaging, disengaging, and carrying equipment filled drawers from electronic racks. It has a pushbutton release mechanism on the locking device which permits quick release of multiple pin connectors commonly used with plug-in chassis. Adequate mechanical advantage is provided to engage connector plugs with forces of 400 lb.

Camloc Fastener Corp., Dept. ED, 61 Spring Valley Rd., Paramus, N.J.

CIRCLE 146 ON READER-SERVICE CARD

ELECTRONIC DESIGN • April 29, 1979

GLAR SET VERNIER .- Automatically provides vernier calibration settings to an accuracy tolerance within 1/1000 in. regardless of human errors in reading and lining up a vernier to the hairline marker and inaccuracies in the manufacture of the vernier

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los. Gelb Co., Dept. ED, 52 Arlington St., Newark 2, N.J.

CIRCLE 147 ON READER-SERVICE CARD

ULTRASONIC CLEANING TANK.-Series TH Sonogen ultrasonic cleaning tank-transducers have an integral heater, dual thermostatic control, and twim-wall costruction. Available in eight standard sizes with 1 to 32 gal tank capacity and transducer input from 65 to 1000 rf w.

Branson Ultrasonic Corp., Dept. ED, 40 Brown House Rd., Stamford, Conn.

CIRCLE 148 ON READER-SERVICE CARD

ELECTRICAL RESISTANCE PROBE.—Highly sensitive to environmental changes, this probe measures corrosion and hard-to-detect liquid and gaseous contaminants. It can detect the slightest change in humidity, ozone concentration, or water content in a nonaqueous liquid. In missile systems, it can detect corrosive conditions which may harm delicate electromechanical components long before any actual corrosion occurs.

Crest Instrument Co., Div. of Magna Products, Inc., Dept. ED, 11808 S. Bloomfield Ave., Santa Fe Springs, Calif.

CIRCLE 149 ON READER-SERVICE CARD

HIGH CURRENT TERMINAL BLOCKS.—Types T and U, respectively rated 125 and 250 amp at 750 v. have tubular type terminals for connecting wire leads without lugs. Type T accommodates AWG 6 to 1/0 wire and has 1 to 6 terminals per block. Type U has socket head screws in its terminals and accommodates AWG 4 to 250 MCM wire. Types L, O, and S, designed for the connection of leads with lugs, are rated at 750 v for 100, 125, and 225 amp, respectively, and handle up to 1, 1/0, and 4/0 AWG.

Curtis Development and Mfg. Co., Dept. ED, 3250 N. 33rd St., Milwaukee 16, Wis.

CIRCLE 150 ON READER-SERVICE CARD

PRESSURE SENSITIVE TAPE.—Thermal curing type TGV Teflon impregnated fiberglass tape has a temperature range of -100 to +500 F and adheres to any dry, clean surface. For both mechanical and electrical applications, it is available in 18 yd rolls and 1/2, 3/4, 1-1/2, and 2 in. widths.

The Connecticut Hard Rubber Co., Dept. ED, 407 East St., New Haven 9, Conn.

CIRCLE 151 ON READER-SERVICE CARD

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preamplifiers. A low-capacitance probe is an integral part

of the Type 80 Plug-In Preamplifier, which provides a calibrated deflection factor of 0.1 v/cm. Sufficient signal delay is included in the main vertical amplifier to permit displaying the leading edge of the waveform under observation.

The wide sweep range of the Type 581 includes calibrated sweeps fast enough to take advantage of its risetime capabilities. Calibrated sweeps from 0.05 µsec/cm to 2 sec/cm are available in 24 steps, and a 5-x magnifier increases the calibrated range to 0.01 µsec/cm. Sweep time is continuously adjustable from 0.01 usec/cm to 5 sec/cm.

Versatile triggering includes amplitude level control, and preset stability for operating convenience. Lockout-reset circuitry provides for one-shot sweep operation.

A new Tektronix cathode-ray tube with distributedtype vertical-deflection plates is used in the Type 581. 10-kv accelerating potential assures a bright trace, even at low sweep-repetition rates. An amplitude calibrator is also incorporated in the Type 581, with square-wave output from 0.2 my to 100 v in 18 steps.

**TYPE 585** 

The Tektronix Type 585 has, in addition to the identical general specifications of the Type 581, a second time base generator. This time-base generator, designated TIME BASE B, acts as a delay generator, providing a wide range of calibrated sweep delay. Two modes of sweep delay are availabletriggered (delayed sweep is started after the

delay period by the signal under observation). and conventional (delayed sweep is started at the end of the delay period by the delayed trigger). Calibrated sweep delay is continuously variable over the range of 1 µsec to 10 sec. Color-correlated controls eliminate confusion, making this new highperformance oscilloscope easy to operate.

#### PRICES

TYPE 58	1, without plug-in units\$1375
TYPE 58	5, without plug-in units\$1675
TYPE 80	Plug-In Preamplifier, with Probe \$ 150

(Other plug-in preamplifiers are currently in development.) Prices f.o.b. factory.

## Tektronix, Inc.

P. O. Box 831 • Partland 7, Oregon

Phone Cypress 2-2611 • TWX-PD 311 • Cable: TEKTRONIX

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TEXTRONIX ENGINEERING REPRESENTATIVES: Howthorne Electronics, Portland, Oregon Seattle, Wash.; Hytronic Measurements, Denver, Colo., Salt Lake City, Utah

Tektronix is represented in 20 overseas countries by qualified engineering organizations

CIRCLE 152 ON READER-SERVICE CARD

# Where only the **best** is good enough...



MODEL UHR-240

#### Krohn-Hite power supplies are used

In basic electronic instruments for lab or test work, less than the best may be a dangerously bad bargain. Unexpected limitations — of reliability, range, precision — can throw out weeks of work on today's jobs, and can make tomorrow's tougher jobs untouchable.

The best instrument of its type is probably a bit more expensive, but it's worth buying . . . because you can believe in it today, and will rely on it tomorrow. An example is the Krohn-Hite Model UHR-240 ultra-high-regulation power supply. Here are some facts about it.

MAIN DC OUTPUT: zero to 500 volts, continuously adjustable, at zero to 500 milliamperes.

**REGULATION:** less than 0.001% plus 0.002 volt from no load to full load.

LINE STABILIZATION: less than 0.003% plus 0.003 volt, for 10% change.

**OUTPUT IMPEDANCE:** DC — less than  $(0.005 + 0.00002 \times \text{output volts})$  ohm; AC — less than 0.05 ohm plus 0.1 michrohenry.

RIPPLE: less than 0.1 millivolt rms.

DC BIAS OUTPUT: zero to minus 150 volts, continuously adjustable, at zero to 5 ma; regulation less than 1%.

DC HEATER OUTPUTS: 5 to 12.6 volts, adjustable, at zero to 2.5 amperes.

AC HEATER OUTPUTS: two, each 6.3 volts at 10 amperes.

There's a lot more you should know about the UHR-240... and about the other Krohn-Hite power supplies, oscillators, tunable electronic filters and amplifiers. In all of them, you'll find the same far-ahead engineering, design and construction. Because K-H instruments are good enough even for tomorrow's most critical work, they are increasingly chosen today where true reliability and precision are needed.



Write for your free copy of the new Krohn-Hite Catalog.

#### Krohn-Hite CORPORATION

580 Massachusetts Avenue, Cambridge 39, Mass.

CIRCLE 153 ON READER-SERVICE CARD

#### **NEW LITERATURE**

#### RF Chokes 15

A new rf choke coil technical data sheet contains a detailed description of the electrical parameters for the complete line of chokes which are available in a 100,000 to 1 inductance range, said by the manufacturer to be the widest range available in a small size, high-reliability line. The entire standard line of Essex chokes is described by the data sheet which lists parameters for 123 different units with inductance values from 0.1 h to 10 mh. The units shown include the logarithmic series as well as the preferred series. The data sheet announces that all Essex encapsulated choke coils are nonflammable, and it explains the company's ability to produce, on special order, choke coils with inductance values rather than the 123 standard preferred and logarithmic series listed. Essex Electronics, Berkeley Heights, N.J.

#### **Converter-Inverters**

155

A 4-page, 2-color data file describes company's Transidyne line of converter-inverters. The data file shows pictures of the various case styles and lists features and specifications of the four basic series. For your free copy of Data File 701, write Spectrol Electronics Corp., 1704 South Del Mar Avenue, San Gabriel, Calif.

#### Communication Accessories 156

Twenty-four page catalog covers toroidal coils, laminated transformers, filters, magnetic amplifiers and dc to dc converters. Basic catalog 858 includes graphs, pictures, dimensions of units, electrical characteristics and a price list. Communication Accessories Co., Lee's Summit, Mo.

#### PTFE Tubing

157

A new, three-color, four-page brochure contains prices, tolerances, sizes and application information on PTFE (polytetrafluoroethylene) tubing. A gate-fold chart lists electrical, mechanical, chemical and thermal properties of the high temperature tubing, opposite a full page of purchasing information such as price, color packaging and terms. Cross-reference charts are provided for "Super-Thin", "Thin-Wall" and "ASTM Wall" PTFE tubings by AWG size and footage. Another chart lists dimensional tolerances for all PTFE tubings by AWG size. Irvington Div., Minnesota Mining and Manufacturing Co., 900 Bush Avenue, St. Paul 6, Minn.

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- VC Oscillators
   RF Power Amplifiers
- Transistorized VCO's

Save size, weight, power, time and meney ... with a Dersett complete telemetering package. Includes power supplies, regulators, calibrators, amplifiers, the required number of VCO's, mixer and FM transmitter. Dersett also designs and manufactures individual telemetering components ... like the new transistorized VCO's which are revolutionizing power, space, and weight concepts. Dersett engineers will work closely with you on your special needs. Dersett equipment has passed the mest rigid inspections of prime contractors and military agencies. You can be sure of prompt delivery of reliable equipment. Dersett has designed many different types of belometering packages and can provide you with the smallest, lightest, lowest power equipment available. For example, one of Dersett's many models provides 9 escillators, mixer, and power supply in as little space as 2.34"x354"x554". For complete information on your specific needs call, write, or wire, Dersett, today.



ELECTRONIC DESIGN • April 29, 1959



... available immediately for any part of your operation that depends on electromechanical switching.

Proven by many years of meeting the exacting requirements of the telephone industry, these twin-contact relays of unsurpassed reliability are available in many types. The following are representative:

Type A: general-purpose relay with up to 20 Form "A" spring combinations. This relay is excellent for switching operations.

Type B: a gang-type relay with up to 60 Form "A" spring combinations.

Type BB relay accommodates up to 100 Form "A" springs.

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Type C (illustrated): two relays on the same frame. A "must" where space is at a premium.

Type E: has the characteristics of Type A relay, plus universal mounting arrangement. Interchangeable with many other makes.

Complete details and specifications on all Stromberg-Carlson relays are contained in our *new relay catalog*. Contents include: spring combinations, table of equivalents, contact data, variations and special features, plus complete mounting and cover information.

The catalog is available on request.

#### STROMBERG-CARLSON

A SIVISION OF GENERAL DYNAMICS CORPORATIO

Tel-communication Industrial Sales
116 Carlson Rd. • Rochester 3, N.Y.



CIRCLE 159 ON READER-SERVICE CARD
ELECTRONIC DESIGN • April 29, 1959

#### Cathode Ray Tubes

A new booklet lists the characteristics of television picture tubes and cathode ray tubes for specialized commercial, industrial and military applications. The 42-page booklet constitutes a complete reference to all popular tube types of American manufacturers, and characteristics and mechanical dimensions of most EIA-registered tubes. Tubes listed in the new Sylvania booklet are grouped under two general headings depending on whether they employ magnetic or electrostatic focus. Within these groups the tubes are listed numerically-alphabetically. Essential data such as maximum ratings, heater voltages, typical operations information, and bulb dimensions can be readily determined where individual data sheets are not available. Special sections on phosphor characteristics and proper tube handling highlight the presentation. Sylvania Electric Products Inc., 1740 Broadway, New York 19,

#### Potentiometer and Bridge Instruments 161

A new 64-page edition of Bulletin P1245-A, covers complete specifications of company's potentiometer and bridge instruments in indicating, recording, and controlling models. Information concerning rack mounting instruments, highspeed and multipoint instruments, and miniature instruments is included, in addition to descriptions of standard round-chart and strip-chart instruments. One section of the bulletin is devoted to sensing elements and attachments for use with Dynamaster instruments. Resistance bulbs, magnetos, photocells, conductivity cells, frequency converters, computing, totalizing, and digital read-out attachments are among those listed. A section describing the incorporation of Dynamaster instruments into other manufacturers' equipment is also included. Request Bulletin P-1245-A from The Bristol Co., Waterbury 20,

#### Transformer Catalog

162

160

"Pulse-Transformers", a 24-page catalog, is designed to assist engineers in the application of transformers to their specific needs. Complete with many tables, charts, and schematics this manual covers a brief history of low-level pulse transformers, their measurements, specifications, applications, interchangeability, dielectric ratings, manufacturing, and other data. Also included is information on some 2000 standard design transformers (available from stock), as well as ease types and specifications data to aid the engineer who requires transformers of custom design and manufacture. "Pulse Transformers" is available on request by writing PCA Electronics Inc., 16799 Schoenborn St., Sepulveda, Calif.



#### - and now for the heat test!

So you did build your own pot! Now — will it function at 150 C? It might, if you made sure to use some real cool winding wire (say, with no more than 20 parts per million temperature coefficient)! A specially-designed heat-resistant element card would also be handy to keep things cool! But you don't have to build-'em-yourself and then go through all this barbecue-broil testing, to be assured of pots with good high-temperature characteristics!

Why take "pot luck", when Ace has all these special high-temperature design features — neatly packaged in the Acepot X-500! Our exclusive design dissipates internal heat to the mounts, allowing greater dissipation at high temperature. So put away your chef's hat — and rely on Ace's four years of testing. For high temperature performance — the X-500's your answer. See your ACErep!



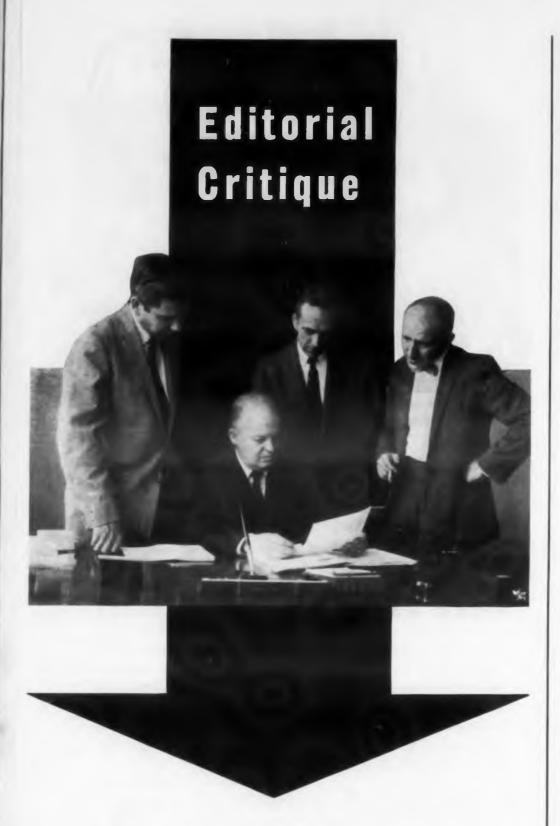
The X-500 Acepot. From  $-55^\circ$ , up to  $150^\circ\text{C}$ , with special heat-resistant elements. Excellent resolution,  $\pm 0.3\%$  linearity. ½" size, ¼-ounce. Prompt delivery.

ELECTRONICS ASSOCIATES, INC.
99 Dover Street, Somerville 44, Mass.

SOmerset 6-5130 TMX SMVL 181 West, Union WU

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Electronic Design is getting a thorough going over . . . The scene above is typical of the editorial conference held after each issue goes to press. These special meetings, called by Edward E. Grazda, Editor, help to improve editorial standards by constructive self-criticism. Editors exchange points of view, make suggestions, comment on clarity and conciseness; discuss technical points. These discussions are aimed, as always, toward making your magazine more interesting, useful, and informative. Your own reactions, ideas, and comments are often mentioned here – all helping to keep the magazine more closely tuned to the main current of reader needs and interests.

#### **NEW LITERATURE**

#### **Semiconductor Preforms**

Bulletin A-68, a 4-page illustrated technical bulletin describing high purity semiconductor preforms used in making alloy junctions in germanium and silicon devices, include information on analyses of alloys, specifications and tolerances of discs, spheres, and washer preforms, along with previously unpublished phase diagrams of semiconductor alloys. Bulletin A-68 shows typical analyses of semiconductor elements such as lead, antimony, indium, gold, gallium, cadmium, indicating the importance of minimal impurities. In addition to metallurigical information, Bulletin A-68, lists specifications and tolerances on high purity preforms produced from these alloys. Bulletin A-68 also shows company's unique facilities for the production of high purity preforms. Accurate melts, analyses their own allovs, rolls and forms these alloys, and by maintaining their own tool and die facilities can rapidly tool up to produce either small or very large production runs. Inspection facilities depicted in the bulletin show a system of close control on size and weight of preforms by mechanical, optical, and electronic methods. Accurate Specialties, Inc., 37-11 57 St., Woodside 77, N.Y.

#### **Alternators**

A new, four-page illustrated folder, detailing its dramatic new line of alternators, features silicon rectifiers in lieu of standard selenium rectifiers. According to the literature, the new type alternators provide infinite operating life and vastly reduced maintenance. The folder graphically illustrates how the new silicon rectifier because of its considerably smaller size, has been successfully combined with the basic alternator, thus providing an alternator system with only two components instead of the previous three (the alternator, the rectifier, and the regulator). More than 30 illustrations highlight design and application features. The literature also contains detailed specifications and operating information. Copies may be obtained from the Leece-Neville Co., 1374 East 51st St., Cleveland 3, Ohio.

#### **Test Equipment**

A new data folder, providing specifications and prices for transistorized digital test equipment describes 10 of the firm's standard building blocks which can be used in a wide variety of test setups, through use of patch cords. Digital Equipment Corp., Maynard, Mass.

Don't miss an issue of ELECTRONIC DESIGN; return your renewal card.

## SOMETHING NEW IN **SLOTTED SECTIONS**

165



Actually, this is a new kind of Standing Wave Detector, which completely makes obsolete the 8-foot monsters, for impedance and VSWR measurements from 100 to

The PRD Type 219 is only 8 inches long and weighs a "pocketable" four and one half pounds.

As if these facts were not startling enough, the 219 also features:

- Direct reading of VSWR
- Direct reading of angle of reflection coefficient
- Direct reading of reactive component sign • Matched load for self-calibration supplied
- Low cost
- Rugged construction

Listed below are a few of the important specifications.

Frequency Range: | 100 to 1000 mc s Residual VSWR: Minimum Input Signal:

Characteristic RF Input Connector:

Approx. 1V at 100 mc s: 0.1V at 1000 mc s for measuring a matched load 50 ohms Impedance: Detector: Crystal included BNC jack RF Dutput Connector:

**Audio Output Connector:** Dimensions:

Type N jack supplied Connector types available include types C, BNC, LT, TNC, %" coax. BNC jack

Less than 1.03

8" L x 5" W x 53/4" H Weight: 41/2 pounds f.o.b. Brooklyn, New York

Note to owners of the new PRD Catalog. E-8: Don't bother reading this ad. All these details and more can be found on page B-13. If you are unfortunate enough not to own a copy of this designers' workbook. send your request on your company letterhead please.

If all you want are specifications on the 219. fill out the inquiry card in this magazine.



#### POLYTECHNIC RESEARCH & DEVELOPMENT CO., INC.

Factory & General Office: 202 Tillary St., Brooklyn 1, N Y. **ULster 2-6800** 

Western Sales Office: 2639 So. La Cienega Blvd., Los Angeles 34, Ca if. TExas 0-1940

CIRCLE 168 ON READER-SERVICE CARE



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in the 215 mc to 245 mc telemetering band

THE MODEL REL-09 HF is a ruggedized miniature R-F power amplifier. With a solid history of reliability in current missile systems, the unit proved its indifference to the adversities of space environment by functioning perfectly while in orbit as part of the Vanguard satellite. The 5-inch. 1-pound amplifier delivers an 11-watt output to a 52-ohm load with a 1.4-watt input drive. For full specs, write for Data File ED-724-1



RHEEM MANUFACTURING COMPANY DEFENSE AND TECHNICAL PRODUCTS DIVISION

CIRCLE 169 ON READER-SERVICE CARD E ECTRONIC DESIGN • April 29, 1959

#### **Guide to Silicones**

Latest additions to the Dow Corning Silicone line include three brochures which detail the growing use of different silicone products in their respective fields of application. "1959 Guide to Dow Corning Silicones" is a 16-page illustrated brochure discussing new materials to improve products and reduce costs. Nature, properties, and applications of adhesives through water repellents are described. The four-page leaflet, "Nothing Sticks to Paper with Syl-Off Silicone Coatings" discusses the advantages of this product. "Silicones in Missile Design" is an illustrated folder describing rigid materials, rubbery materials, fluid materials, and dielectric materials for electrical and electronic systems in missile and support equipment. Dow Corning Corp., Midland. Mich.

#### **Pushbutton Switches**

This two-page data sheet covers a new series of "One-Shot" Switches. The unit consists of a pushbutton switch assembly with an electronic circuit which produces a single, microsecond length pulse with each operation. Data sheet includes photo, dimension drawing, specifications, circuit schematic, pulse curve oscillagraphs and application information. Micro Switch, Division of Minneapolis-Honeywell Regulator Co., Freeport, Ill.

171

172

#### **Electronic Components**

Catalog 558, a 12-page two-color brochure. lists Hitachi electronic receiving tubes and transistors. Also included are several types of capacitors, resistors and audio equipment. Electronic Utilities Co., Division of the Sampson Co., 2244 S. Western Ave., Chicago 8, Ill.

#### **Batteries** 173

"A Reusable Primary-The Yardney PB Silvercel® Battery," is a technical bulletin describing this recently developed battery which combines the recyclability of the secondary battery, the fast activation of the primary and the high power output of the silver-zinc system. The illustrated brochure explains the PM Silvercel battery's outstanding characteristics-highest specific power, highest specific energy and longest activated stand life yet achieved by a primary, reusability and fast activation. It compares the battery's energy and power with other battery systems, and discusses its applications, electrical characteristics (energy, power discharge rates), construction, charging, fast activation, wet stand, recycling, soaking time and other technical data. Yardney Electric Corp., 40-50 Leonard St., New York, N.Y.



#### **Pinpoints All Circuit Flaws Instantly...Plots and** Simplifies Test Procedure...Provides a Permanent Record!

DIT-MCO's revolutionary Matrix Chart is the only error location device which puts all circuit information . . . errors, circuit numbers, type of flaws, etc. . . . directly in front of the operator of this Automatic Electrical Circuit Analyzer. It plots the entire test sequence and pinpoints every circuit flaw...instantlyl Horizontal and vertical indicator lights cross reference to indicate the exact error location, circuit number and type of flaw. As errors are detected, they are recorded on the proper matrix square and the test continues.

Once the test sequence has been completed, all corrections are made direct from the Matrix Chart. This group correction feature saves up to 90% of error correction and/or interpretation time by eliminating time-consuming searches through complex manuals and wiring diagrams. After corrections have been noted on the Matrix Chart, it provides a complete record of test circuits, test specifications, instructions, results and modifications. This concise, understandable record improves interdepartmental communications and provides co-ordination through all stages of planning, production and maintenance. Non-technical personnel easily master operation of the Analyzer and use of the Matrix Chart System. The final Matrix Chart can follow the product for future overhaul and maintenance use.

DIT-MCO, Inc. employs an experienced staff of sales engineers in the field. Contact your field sales engineer or write for important facts about DIT-MCO Automatic Electrical Circuit Analyzers.



**PLUGBOARD PROGRAMMING** SPEEDS TESTING!

#### DIT-MCO, INC.

**ELECTRONICS DIVISION • BOX 04-20** 911 BROADWAY . KANSAS CITY, MO. Jumper-wired plugboard programming permits use of simple, straightforward adapter cables. Circuit modifications never present headaches because all changes are easily made by re-jumpering the readily accessible plugboards.

#### Partial List of DIT-MCO Users

Aircraft Radio Corp. Airesearch Manufacturing Co. American Bosch Arma Corp. American Machine & Foundry Co. American Motors & Amphenol Electronics Corp. Autonetics, A Division of North American Aviation, Inc. Bell Aircraft Corp. Bendix Aviation Corp. Boeing Airplane Co. Cessna Aircraft Co. Chance Vought Aircraft, Inc. Chrysler Corp. Convair Douglas Aircraft Co., Inc. Dukane Corp. Electronic Products Corp. Fairchild Aircraft Division Farnsworth Electronics Co. Frankford Arsenal General Electric Co. General Mills, Inc., Mechanical Division General Precision Laboratory, Inc. Goodyear Aircraft Corp. Grumman Aircraft Engineering Corp. Hazeltine Electronics Division, Mazeltine Corp. Hughes Aircraft Corp., Missile Systems Division Martin, Baltimare Minneapolis-Honeywell, Aeronautical Division Motorola, Inc. Northrup Aircraft, Inc. Pacific Mercury Television Mfg. Corp. Radio Corp. of America Radioplane Co. Raytheon Manufacturing Co. Servomechanisms, Inc. Sikorsky Aircraft Sperry Gyrascope Co. Summers Gyroscope Co. Sun Electric Co. The Swartwout Co., Autronic Division Temco Aircraft Corp. Thompson Products Topp Industries Inc. Trans World Airlines U.S. Naval Air Station Overhaul and Repair Depots U.S. Naval Ordnance Laboratory, White Oak Vertol Aircraft Corp. Western Electric Co. Westinghouse Electric Corp.

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PIONEERS AND SPECIALISTS IN PLASTIC CONTAINERS SINCE 1919

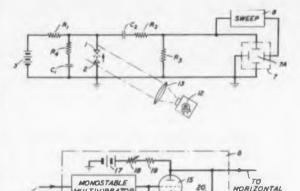
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## **PATENTS**

#### **Velocity Measurement of Relay Contacts**

Patent No. 2,864,054. Willard S. Boyle and James L. Smith. (Assigned to Bell Telephone Labs., Inc.)

Rate of closure of contacts is measured by displaying, on a calibrated oscilloscope, the time interval from arc discharge across the contacts to the time of actual contact. For fixed voltage and pressure, the spacing for arc discharge is obtained from Paschen's law; actual contact



is the instant a storage capacitor discharges.

Initially, capacitor  $C_1$  charges fully and ultraviolet lamp 12 illuminates the contact spacing with photoelectrons to insure reproducibility of the spacing for the arc. As contacts 1 and 2 move together, capacitor  $C_1$  discharges at the time the arc initiates and the crt sweep 3 is triggered. Capacitor  $C_1$  recharges as the contacts move closer and the second discharge of the capacitor, when the contacts touch, precisely marks the time of closure T on the oscilloscope display.

# System for Selectivity Energizing One of Three Circuits Responsive to Variation of Two Conditions

Shih C. Chao. (Assigned to International Business Machines Corp.)

Individual signals gate selected circuits while the signals simultaneously exclusively gate another circuit.

Battery 25 sets the pnp transistors beyond cut off. Closing switch 12 permits only transistor 1 to conduct and closing



NEW

STANDARD RELAY

#### HAS DRY CIRCUIT TO 10 AMP VERSATILITY

Completely new Babcock BR-7 miniature DPDT relay, ruggedly designed for diversified MIL-SPEC airborne and missile applications, will permit contact loads from dry circuit conditions to 10 amperes. Single size for all uses with 0.2" grid spaced header supplied for interchangeability. Specifically engineered for greater reliability, extended life and extreme sensitivity. Minimum life at 10 amps — 300,000 operations at 25°C and 100,000 operations at 125°C. Meets or exceeds applicable specifications for life, temperature, vibration (30 g min. to 2,000 cps), and shock. 480 mw pull-in for 10 amp contacts, 80 mw for 2 amp contacts, lower for SPDT and special adjustments. Can size: 1.26 x 1.07 x 0.56 in. Complete header arrangements, mounting methods and special mountings available. For Technical Bulletin, write BABCOCK RELAYS, INC., 1640 Monrovia Ave., Costa Mesa, Calif.

CIRCLE 177 ON READER-SERVICE CARD

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switch 14 causes only transistor 2 to conduct; for both instances, resistors 19 and 21 divide the input signals to hold the third transistor cut off. However, when

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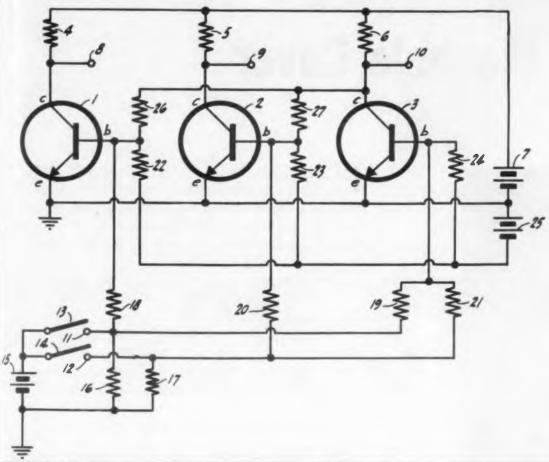
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istors rmits osing switches 12 and 14 close together, these voltage divider resistors are shorted, transistor 3 conducts and the output voltage is fed back to cut off transistors 1 and 2.





CIRCLE 178 ON READER-SERVICE CARD



# REC'S NEW DEICED TEMPERATURE PROBE

This extraordinary new Model 102D gives accurate total temperature measurement while deicing heater operates

The unique ability of this probe to permit precise total temperature measurements while deicing heat is continuously applied opens up numerous possibilities. Model 102D will deice within one minute when subjected to icing conditions defined in Section 3.5, paragraph g of MIL-P-25632A (USAF). Model 102D is designed for use at flight speeds up to Mach 2 and higher.

Tell us about your project. We welcome your inquiry for complete information on Model 102D, or any of REC's many other precision units.

**NEW CATALOG. No. 115811.** Illustrated compilation of data on over 50 different REC probes ranging from  $-260^{\circ}$  C. to  $1500^{\circ}$  C., plus REC pressure transducers and pitot-static tubes.



#### ROSEMOUNT ENGINEERING COMPANY

4914 West 78th Street

Minneapolis 24, Minn.

CIRCLE 179 ON READER-SERVICE CARD

# Radio Frequency Manhole Cover

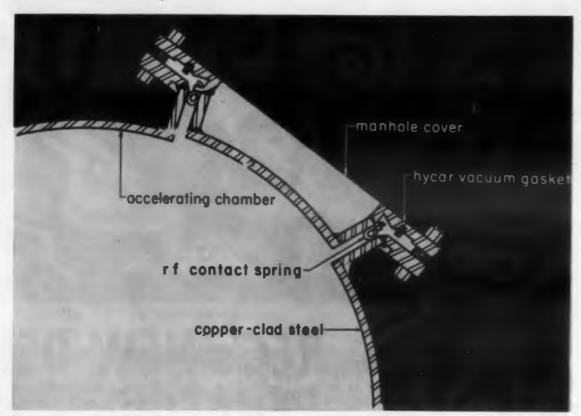


Fig. 1. Cross section of an accelerating chamber of the HILAC, showing a manhole cover and rf-contact spring.

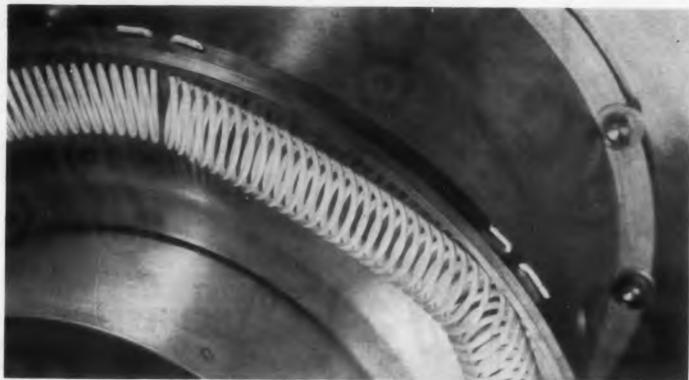


Fig. 2. Radio frequency contact for a transmission-line joint of the HILAC.

N THE heavy-ion linear accelerator (HILAC) the accelerating chambers are made of copperclad steel. The rf and vacuum cavities are integral; opening one cavity simultaneously opens the other. Therefore, all covers must have both a vacuum gasket and an rf contact.

To facilitate entry it is desirable to use only one set of clamping bolts for making both the rf contact and the vacuum seal.

An arrangement which has proved successful for the manhole covers of the HILAC is shown in Fig. 1. The unique element of this is the rf contact spring. This spring is designed so that the contact force rises to a maximum with a deflection of only 1/16 in., even though the spring diameter is 1 in.

The contact force remains almost constant with further deflection. Because of this, the spring can accommodate large surface roughness and still give a successful rf contact that can be reused indefinitely.

The HILAC has been operating for nearly two years at rated power (70 mc, 42 amp rms on a 3 per cent duty cycle) and there have been no spring replacements due to burnout. One spring section had to be replaced because of mechanical damage, but the circumstances only proved the ruggedness of the design.

One of the manhole covers was accidentally dropped when it was about a foot above the hole. The rf contact spring piloted the 400 pound cover into the hole and absorbed enough shock so that nothing was damaged except one 6 in. spring section. It took only a minute to clip off the ends of the damaged spring, insert the ends of a new one, and bend them over.

Although this design has been used only in the HILAC, it is apparent that it could be applied to other situations. For instance, in a variable-volume resonator where it is necessary to have an rf contact between a sliding piston and a cylinder wall, this spring might prove ideal.

The work on the manhole cover was done under auspices of U.S. Atomic Energy Commission.

Luther R. Lucas, Lawrence Radiation Laboratory, University of California, Berkeley, Calif.

TYPE 9234-4550 2PDT, 2AMP, MAGNETIC LATCH RELAY



(BRACKET MOUNTING, SOLDER HOOK TERMINALS, HERMETICALLY SEALED)

TYPE 9200-5091 2PDT, 2AMP, RELAY



(STUD MOUNTING, SOLDER HOOK TERMINALS, HERMETICALLY SEALED)

TYPE 9200-5072

2PDT, 2AMP, RELAY

(PLUG-IN OR PRINTED CIRCUIT MOUNTING, HERMETICALLY SEALED)

# LEACH SUBMINIATURE CRYSTAL CAN RELAYS

(SHOWN ABOVE ... ACTUAL SIZE)

torture-tested to perfection for big relay performance

These sensitive Leach subminiature relays deliver big relay performance...in a crystal can size that makes them ideal for use in missile control circuits in airborne or ground equipment and in computer and printed circuits.

Torture-tested to perfection in the Leach Production Reliability Center, these subminiatures are designed to meet the critical extremes of vibration, shock and other stringent environmental requirements in military and commercial applications.

They meet the specifications of both MIL-R-25018 and MIL-R-5757C—as well as MIL-R-6106C, including

the minimum current test requirements. Uniform contact pressure and overtravel are guaranteed for the life of these balanced-armature relays. They are available in a wide range of socket, stud and bracket mountings to meet specific customer requirements.

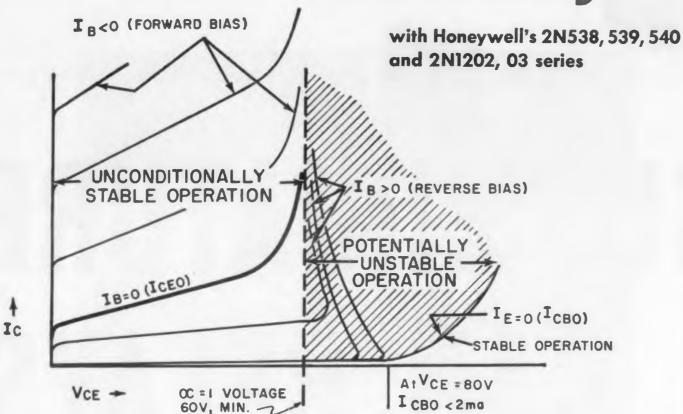
Write today for Leach Crystal Can Relay Brochure containing specifications, typical ratings and other information on these subminiatures! Or contact your nearest Leach sales representative to discuss your specific subminiature relay requirements.

LOOK TO LEACH CORPORATION

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DISTRICT OFFICES AND FIELD REPRESENTATIVES IN PRINCIPAL CITIES OF U.S. AND CANADA • EXPORT: LEACH CORP., INTERNATIONAL DIVISION

# **New Honeywell formula** for power transistor reliability



Now these Honeywell Power Transistors guarantee minimum  $\alpha=1$  voltage to insure stable operation under all bias conditions up to 60 volts. This rating permits operation of both class A and class B transformer-coupled output power amplifiers from a 28VDC source. Proper back bias extends safe operating voltage up to the collector diode design limit of 80 volts.

Contributing to the superior reliability of Honeywell Power Transistors are built-in stability through improved design and processing methods plus significant dynamic

Honeywell's 2N538, 539 and 540, and 2N1202 (characterized at ½ amp) and 2N1203 (120 volt collector diode) Power Transistor Series are rugged, hermetically sealed germanium PNP transistors suited to servo amplifier, power conversion, voltage regulation and switching applications.

These new improved Honeywell Power Transistors give you two other bonuses—new lower prices, plus 1 year warranty. For complete data on these transistors, or for a copy of Honeywell's new Technical Booklet "Fundamental Voltage Limitations of a Transistor," contact one of the following offices:

•	UNION,	NEW	JERSEY.		(MUrdock 8-9000)
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•	BOSTON.	MASSACHUSETTS	

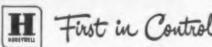
<sup>•</sup> CHICAGO, ILLINOIS.....(IRving 8-9266)

<ul> <li>LOS ANGELES,</li> </ul>	CALIFORNIA	. (RAymond 3-	6611 o
		PArkview	

• ATLANTA, GEORGIA.....(TRinity 4-9776)

Or write Minneapolis-Honeywell, Dept. ED-4-82, Minneapolis 8, Minnesota.

# Honeywell H First in Control



CIRCLE 182 ON READER-SERVICE CARD

#### IDEAS FOR DESIGN

#### **Optical Gaging Cuts Costs** Improves Efficiency

In microwave tube assembly, accurate physical measurements are essential. Bomac Laboratories. Inc., an important company in the microwave tube field, has found great economies through the use of a Kodak Contour Projector.

This instrument, shown in the photo, is used for rapid, accurate inspection of incoming material, in-process part measurements, and statistical quality evaluation.

During incoming inspection, multiple hole alignment on flat surfaces, angles of blind holes (via surface illumination), and decreasing angle slopes are but a few of the ways Bomac uses optical gaging. In many cases, components cannot readily be inspected by other means.

Furthermore, it is possible to check several dimensions of a part simultaneously with contour projection. Some of the general types of measurements include: thread forms, angles, hole locations, and the relationship between two or more parts of subassemblies.

One of the beauties of this method is that there is no wear to a light beam, no matter how often it is used. Hence, wear allowances need not be considered.



Contour projection allows for precise measurement of intricate parts.

Don't miss an issue of ELECTRONIC DESIGN; return your renewal card.

#### Shaft Turns, Syncs Scope

We needed to generate a synchronizing signal from a rotating shaft to trigger a scope. The shaft was on a "Servo Breadboard." A trigger was needed to relate mechanical and electrical rotation.

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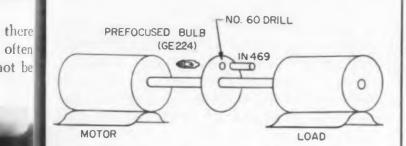
ard.

A mechanical brush contact was tried. This worked, but the contacts tended to float, at higher rpm's, giving an erratic trigger.

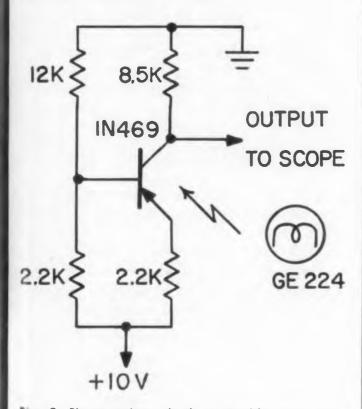
A simple method of generating the desired pulse is shown in Fig. 1. A 1N469 phototransistor is used in a simple amplifier circuit. The light source is a prefocused GE224 "Penlite" bulb. Both transistor and light are mounted by their leads in the positions shown. Fig. 2 shows the amplifier circuit.

The output trigger is approximately one to two v (depending on how critically the light source is adjusted). The rise and fall time is constant, at approximately 90 µsec, over a motor speed of 500 to 4000 rpm.

Philip L. Writer, Engineer, Computers & Controls Div., Litton Industries, Beverly Hills, Calif.



**Fig. 1.** The disk, mounted on the rotating shaft, provides a sync signal everytime the small hole allows light to strike the phototransistor.



Fg. 2. Phototransistor circuit to provide scope sync.

# FAIRCHILD SILICON MESA TRANSISTORS

#### IN BOTH POLARITIES

#### Four models of great importance to the computer-circuit designer



Important — because for high-speed switching, Fairchild's 2N696, 2N697, 2N1131 and 2N1132 are the most advanced transistors available. They are solid-state diffusion devices, a type that is certain to dominate computer-circuit applications in the future because of its superior combination of speed, power and reliability. Fairchild Semiconductor Corporation was first to offer solid-state diffused NPN silicon transistors of such high performance — and again first in offering PNP silicon transistors closely matching these NPN transistors in both high frequency and DC characteristics. All are in quantity production and available from stock.

#### Speed and power in combination

80 milli-micro-second rise time is typical. Two-watts dissipation at 25 °C. and 10 ohms maximum saturation resistance provide high-current capability even at elevated junction temperatures.

#### Utmost reliability

Storage at 300° C. in excess of 1000 hours caused no serious changes in these transistors, assuring a large safety factor at operating temperatures. Mesa construction as shown in enlarged photograph provides extraordinary ruggedness by eliminating suspension of any significant masses. Units have survived 22,000g, 4-millisecond duration shock test without damage.

#### NPN and PNP closely matched

The circuit designer need no longer be limited by unavailability of PNP transistors. Fairchild has them. And they are closely matched to the NPN transistors in DC characteristics, affording opportunities for circuit designs based on complementary symmetry.

#### PNP

Vcto - Vtto - Total dis	Collector to emitter volt Collector to base voltage Emitter to base voltage sipation at case temperatu at case temperatu CAL CHARACTERISTICS	ore 25° C.					30v 40v 5v 2 watts 1 watt
SYMBOL	CHARACTERISTIC		MIN.	TYPICAL	MAX.	TEST CON	DITIONS
hre	D. C. pulse current gain	2N1131 2N1132	15 30		45 90	Ic-150mA	Vc=10V
VIE SAT.	Base saturation voltage			1.0V	1.5V	Ic-150mA	In-15mA
VCE SAT.	Collector saturation volt	age		0.9V	1.5V	Ic=150mA	In-15mA
	Small signal current gain at f = 20mc			2.5		Ic= 50mA	AC=10A
lite.				35μμ1	45µµf	II OmA	Vc-10V
	Collector capacitance			JUMMI			
Cob Icao				.01μA	1:0, A		T= 25°

#### NPN

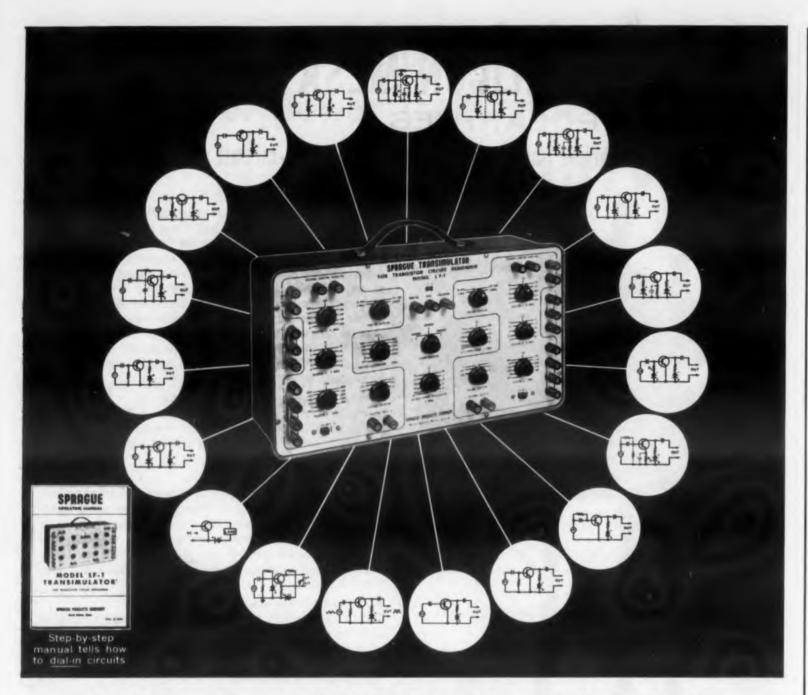
VCER - VCEO - VEEO - Total dis	TE MAXIMUM RATINGS (25° C) Collector to emitter voltage Collector to base voltage Emitter to base voltage sipation all case temperature 25° at case temperature 100  CAL CHARACTERISTICS (25° C)	C. ° C.				40v 60v 5v 2 watts 1 watt
SYMBOL	CHARACTERISTIC	MIN.	TYPICAL	MAX.	TEST CONDITIONS	
				50		
his	D. C. pulse current gain 2N69 2N69			120	Ic=150mA	Vc=10V
NE SAT.		_	1.0V		Ic=150mA	Vc=10V
VIE SAT	2N69	_	1.0V 0.5V	120		
	2N69 Base saturation voltage	_		120 1.3V	Ic=150mA	le=15mA
Ve sat.	2N69 Base saturation voltage Collector saturation voltage Small signal current gain	_	0.5V	120 1.3V	Ic=150mA Ic=150mA	1a — 15mA 1s — 15mA
Vie sat. VCE sat. hre	2N69 Base saturation voltage Collector saturation voltage Small signal current gain at f=20mc	_	0.5V 5	120 1.3V 1.5V	Ic=150mA Ic=150mA Ic= 50mA	I <sub>8</sub> -15mA I <sub>5</sub> -15mA V <sub>C</sub> -10V

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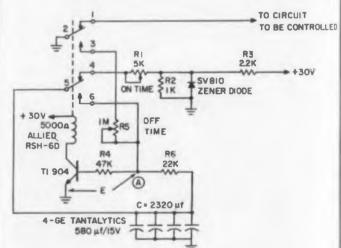
#### Ten Minute Interval Timer

A need recently arose for an interval timer which would allow another piece of equipment to be activated from 5 sec to 1 minute, then turn this equipment off and accurately wait anywhere from 3 minutes to 10 minutes. Both intervals were to be adjustable.

Since such long intervals demand very large capacitors, especially in transistorized equipment, the new and small GE Tantalytic capacitors were

The circuit, shown in Fig. 1, works as follows. Assume that at t = 0, 30 v is applied to the circuit. Immediately the zener diode assumes a reference voltage, but at the same time C, which is 2300 µf, is thrown across the zener diode terminals through R1, the charge resistance. This heavy load causes the diode to go out of regulation. Therefore, C starts to charge essentially from zero. Eventually, the zener diode regains regulation and the capacitors start to charge asymptotically to the zener's terminal voltage with a time constant as determined by R1 and C.

As C charges, the voltage across C is used to supply bias current to the base thru R4 and R6. Thus, as the base current increases, so does the collector current until the "pull in" current has been reached in the relay. At this point, (1) the controlled circuit is disconnected (pin 1 of relay),



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Fig. 1. Long interval timer takes advantage of large capacity available in small size tantalum capacitors.

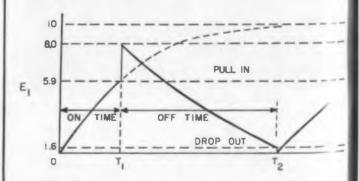


Fig. 2. Voltage at point A as a function of time.

(2) a resistor R5 is connected to ground, (3) resistor R6 is shorted out. Event 3 has particular significance, for it causes the full charged voltage of the capacitors to be used as base bias.

Fig. 2 is a plot of the voltage appearing at point A. At t1, E1 rises 2 v higher, and this adds greatly to the time interval. The capacitor then starts to discharge exponentially until at t2, insufficient bias current flows to maintain the relay energized. The process then repeats itself.

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1959

With the values shown, the on time can be varied between 3 sec to over a minute, and the off time can be varied from less than a minute to 5 minutes. With R5 removed, a time of almost 10 minutes has been obtained.

Gerald Wilner, Development Engineer, ITT Laboratories, Nutley 10, N. J.

#### TV Antenna for Radio

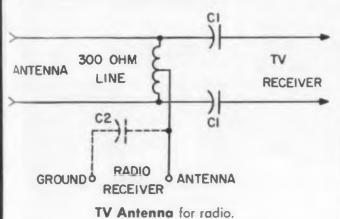
Because of its location, an outdoor TV antenna constitutes a good radio antenna, too. And its connection to the radio receiver can tremendously improve reception. However, it is bothersome to connect and disconnect the ribbon every time one wants to switch from TV to radio.

A permanent installation is easily made and well worth the trouble. The accompanying diagram shows all that is needed is a coil and two capacitors. They can be inserted anywhere in the line, generally right at the connection to the TV receiver. However, if the ribbon passes near the radio receiver, it can simply be cut at the nearest point.

A small terminal strip is used to support the coil and capacitors. The coil is but a choke to block the high TV frequencies. It can be made by winding 40 turns of hookup wire on a 1/4 in. diameter form, and is not critical. A center tap is provided.

The capacitors C1 block the low radio frequencies. They can have a value of 20 to 50 μμf. To obtain a good match at the radio input, it may be necessary to connect a capacitor C2 between antenna and ground terminals. Its value should be around 100 μμf.

Dr. A. V. J. Martin, Carnegie Institute of Technology, Pittsburgh 13, Pa.





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#### **STANDARDS** AND SPECS

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#### **Magnetic Materials**

MIL-P-55034, STABILITY OF POWDERED MAGNETIC MATERIALS (MOLDED) FOR CORES (FOR USE IN ELECTRICAL AND ELECTRONIC PARTS), 19 SEPTEM-**BER 1958** 

Covered in this spec is the evaluation of the uniformity and the stability under environmental conditions of molded, powdered magnetic materials for use as cores in such electrical and electronic parts as coils, transformers, etc. The cores covered by this spec are intended for use in applications where uniformity and stability of electrical and magnetic characteristics under adverse environmental conditions is a prime requisite. Specific performance of cores is not covered in this spec.

#### **Composition Resistors**

MIL-R-94B, VARIABLE COMPOSITION RESISTORS, AMENDMENT 1, 24 NOVEMBER 1958

A requirement was added to Acceleration and Shock that movement in the arm incurred during these tests shall not result in a resistance change greater than 10 per cent. Test procedures have been modified. The requirements of Method 205 of MIL-STD-202 have been added for shock testing.

#### Flanges, Waveguides, Fittings

MIL-F-3922, Flances, Waveguides, and Asso-CIATED FITTINGS, SUPPLEMENT 1A, 15 NOVEMBER

Improved versions of the old flanges, incorporating a modified gasket groove, have been added. The new flanges and gaskets are completely interchangeable with the old versions.

#### Aircraft Microphones

RTCA 258-58/DO-91, MINIMUM PERFORMANCE STANDARDS FOR AIRCRAFT MICROPHONES, NOVEM-BER 1958

Covered in this standard are the minimum performance standards for the sound pressure-electrical current transducer, the connector cord, and other components which form a part of the microphone such as switches, connector plugs, and amplifiers. Inasmuch as the measured values of radio performance characteristics may be a function of the method of measurement, standard test

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conditions and methods of test are recommended. Copies of this standard are available from the Radio Technical Commission for Aeronautics, Room 1072, Building T-5, 16th & Constitution Avenue, N.W., Washington 25, D.C. for \$0.25 per copy.

#### Aircraft Headsets and Speakers

RTCA 257-58/DO-90, MINIMUM PERFORMANCE STANDARDS FOR AIRCRAFT HEADSETS AND SPEAKERS, NOVEMBER 1958

Equipment covered by this standard includes the electrical current-sound pressure transducer, the connector cord, and other components which form a part of the headset or speaker assembly such as headbands, ear plugs, enclosures, connectors, amplifiers, and attenuators. Also included are standard test conditions and standard methods of test. Copies of this standard are available from the Radio Technical Commission for Aeronautics for \$0.25 each.

#### Airborne Receiving Equipment

RTCA 222-58/DO, MINIMUM PERFORMANCE STANDARDS FOR AIRBORNE ILS GLIDE SLOPE RE-CEIVING EQUIPMENT, OCTOBER 1958

Minimum performance standards under both standard test conditions and environmental test conditions are established by this standard. Also included are standard test conditions and methods of test. Copies of this standard are available from the Radio Technical Commission for Aeronautics, Room 1072, Building T-5, 16th & Constitution Avenue, N.W., Washington 25, D.C. for \$0.30 per copy.

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ASME B18.6.4, SLOTTED AND RECESSED HEAD TAPPING SCREWS AND METTALIC DRIVE SCREWS, 1958

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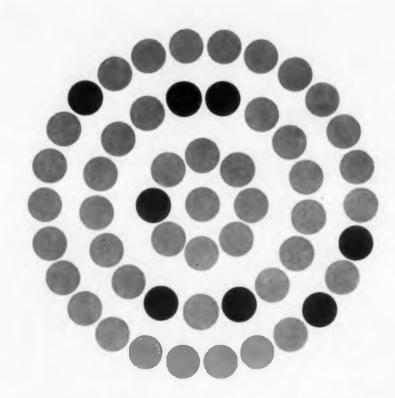
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#### **RUSSIAN TRANSLATIONS**

# **Nonlinear** and Parametric Phenomena in Radio **Engineering**

Part 17 A. A. Kharkevich

(Translated by J. George Adashko)

Chapter 2

#### **Generation of Oscillations**

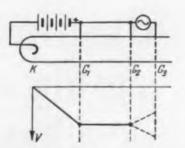
#### 28. Microwave Oscillators

The oscillator circuits already described are not suitable for the generation of microwave frequencies. This is due first to the fact that at microwave frequencies the parasitic parameters of the circuit and of the tube begin to play an important role.

By changing the method of wiring and the construction of the parts, and in particular by using special tubes that differ greatly from ordinary tubes, it is possible to generate frequencies up to 500 mc with customary circuits. Secondly, at microwave frequencies it becomes necessary to allow for the transit time of the electron in the space between the tube electrodes, since the time becomes comparable with the oscillation period.

This results, in the case of the conventional generator, in insurmountable difficulties of basic character. But, on the other hand, the same cir-

Parasitic parameters are those not taken into account in the first-approximation basic circuit, namely, lead capacitance, capacitance between individual circuit elements, capacitances to ground, inductance of leads, etc



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Fig. 98. The cathode end of a klystron tube and its voltage diagram.

cumstance can be used to construct many types of oscillators, in which the finite transit time of the electrons serves as the very basis for the oscillation mechanism.

In modern microwave practice, use is made of essentially three types of oscillators: (1) the klystron oscillator, (2) the magnetron oscillator, and (3) the backward-wave oscillator.

We shall not deal with the theory of these oscillators. However, to gain an idea of certain principles underlying the use of the finite electron velocity for the generation of microwaves, we present a brief qualitative description of the phenomena that take place in a klystron.

Klystron operation is based on velocity modulation of an electron beam with subsequent automatic conversion of the velocity modulation into density modulation of the electron beam. The term modulation is used here simply in that sense, that a certain parameter is varied by means of an applied signal.

Let us examine Fig. 98, which shows, for the time being, only a portion of the klystron. In addition to the cathode K, there are three other electrodes in the form of grids. Grid  $G_1$  serves as the accelerating electrode, and is positive relative to the cathode. An alternating voltage is applied between grids  $G_2$  and  $G_3$ . The corresponding potential diagram is shown in the lower half of Fig. 98.

The electrons emitted by the cathode are accelerated in the region K- $G_1$  and travel through region  $G_1$ - $G_2$  at a uniform speed, at which they enter the space  $G_2$ - $G_3$ . This region is under the influence of an alternating field, which either decelerates or accelerates the electrons. The electron beam that leaves the region  $G_2$ - $G_3$  is thus velocity modulated, i.e., the electrons move at different velocities. As a result, the faster electrons overtake the slower ones in the space to the right of  $G_3$ , and electron bunches, i.e., regions with increased electron density, are produced.

It is easy to see that the bunches are periodic along the klystron axis and form a traveling densily wave. The length of this wave, i.e., the distance between neighboring bunches, is

$$\lambda = v/f$$

where v is the average velocity prior to modula-

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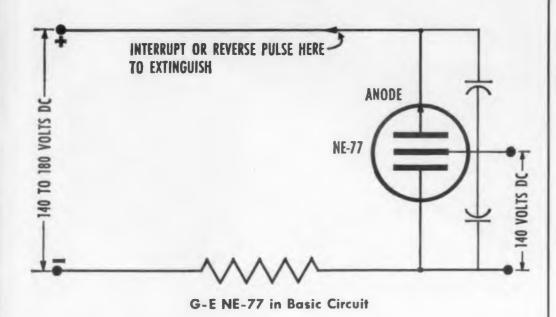
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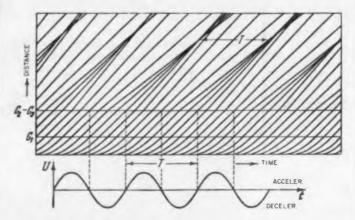


Fig. 99. This drawing shows how bunching takes place in the klystron.

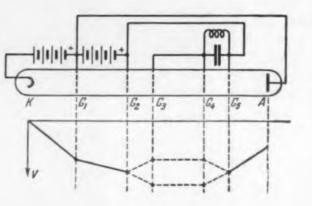


Fig. 100. The klystron oscillator.

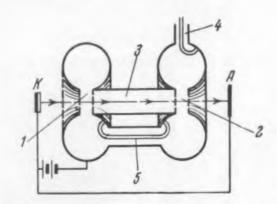


Fig. 101. A klystron with two resonant cavities. 1 and 2 represent toroidal cavity resonators. The bunching space (3) is in the form of a tube as is the feedback loop (5). The ac pickoff is at 4.

tion and f is the modulation frequency. This process is called bunching, and the combination of grids  $G_2$  and  $G_3$  is called the buncher. The space in which the bunches are formed is called the bunching space or the drift space.

The bunching process is explained by Fig. 99, the lower half of which shows the time variation of the alternating buncher voltage. The upper portion of the diagram shows, in distance-time coordinates, the motion of the electrons. For simplicity it is assumed that the electrons leave the cathode at equal time intervals.

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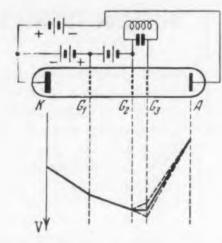


Fig. 102. The reflex klystron and its voltage diagram.

through the accelerating field, the electrons enter the buncher  $G_2$ - $G_3$ , where the electron velocity is either increased or decreased, depending on the sign of the buncher voltage (see sinusoidal curve in the lower portion of the diagram). The motion of the electrons leaving the buncher is represented by straight lines with different slopes. The steeper lines correspond to the faster electrons.

It is seen from the diagram that thanks to the different slopes, the straight lines that represent the motion of the electrons form converging beams. This is a graphic explanation of the formation of electron bunches.

The variable-density electron beam formed in the bunching space can be used to induce a current in an external circuit. For this purpose, use is made of two additional grids  $G_4$  and  $G_5$ , to which we connect a tank circuit tuned to the proper frequency. If the voltage is now picked off the tank circuit and fed back to the buncher, we obtain the klystron oscillator of Fig. 100.

The spent electrons fall on the collector A and flow through it to the cathode. The combination of grids  $G_4$  and  $G_5$  is called the catcher. To excite the system, a suitable adjustment of the phase of the feedback is necessary. For a specified construction and fixed distance between the buncher and the catcher, the phase of the feedback can be regulated by varying the accelerating voltages on  $G_1$ and  $G_2$ .

The construction of a klystron with two resonators is shown in Fig. 101, where 1 and 2 denote toroidal cavity resonators (shown in cross section). The buncher and the catcher are formed by pairs of perforated disks, which serve as capacitive inserts in the resonators. The bunching space is made in the form of a tube 3. Still another tube contains the feedback loop 5. Loop 4 serves to pick off the alternating voltage.

The reflex klystron is the most widely used. It differs from the system just considered in that the buncher and the catcher are combined. After passing through a pair of grids, which comprise the buncher, the electron beam is retarded by a nega-



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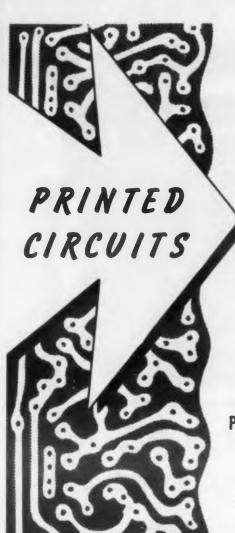
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#### **RUSSIAN TRANSLATIONS**

tive field and turns back, passing again through the same pair of grids which now serve as the catcher. The diagram of the reflex klystron and a corresponding potential diagram are shown in Fig. 102.

The bunching process in the reflex klystron is explained in Fig. 103. This diagram differs from Fig. 99 in that the lines representing the motion of the electrons that leave the buncher are not straight but parabolic (corresponding to the motion in an accelerating field of opposite direction). The electrons return to  $G_2$ - $G_3$ . Bunches are formed as a result of the difference between the initial velocities.

It is obviously necessary to tune the system in such a way that the bunches are formed in the  $G_2$ - $G_3$  zone. It should be noted that there is no separate feedback loop in the reflex klystron, and the feedback is effected through the electron beam. The reflex klystron can be tuned not only by varying the accelerating positive potentials on  $G_1$  and  $G_2$ , but also by varying the negative potential on the reflecting electrode A.

#### 29. Relaxation Self Oscillations

So far we have considered generators of oscillations that are nearly sinusoidal. Such self oscillations are called nearly-harmonic. However, in electronics we employ also self oscillations with waveforms that differ greatly from sinusoidal.

Such self oscillations, which sometimes feature abrupt jump-like changes in current or voltage, or jump-like changes in the rate of variation of these quantities (graphically represented by oscillograms in the form of broken lines) are called relaxation self oscillations.

The essential difference between the waveforms of nearly-harmonic and relaxation self oscillations is due to the difference in the arrangement and operation of the generators of these types of oscillations.

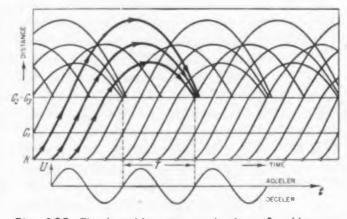


Fig. 103. The bunching process in the reflex klystron.



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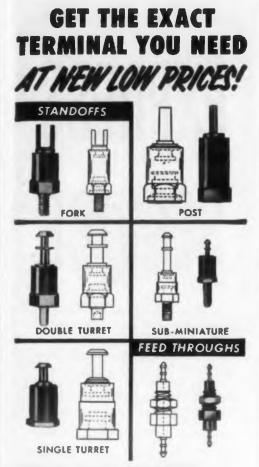
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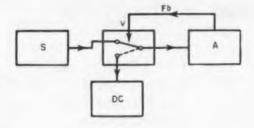
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**Fig. 104.** The mechanism of a relaxation oscillator. S is the energy source, A an accumulating (storage) element, V a valve,  $F_b$  a feedback connection, and  $D_c$  a discharge circuit.

The generator for nearly-harmonic oscillations usually contains an LC tank circuit (or an equivalent LC circuit), i.e., an oscillating system containing (at least) two reactance elements capable of energy storage. From the energy point of view, oscillations occur in the tank circuit, because the energy stored in the tank circuit is alternately concentrated entirely either in the magnetic field of the coil or in the electric field of the capacitor. This energy transfer takes place periodically.

If there are no losses, the oscillation is strictly sinusoidal. In the presence of losses the amplitude diminishes with time exponentially because the stored energy diminishes continuously. On the other hand, if the energy losses are replenished from a source, as they are in every oscillator, the oscillations are undamped, and their waveform differs from sinusoidal only in as much as this is dictated by the nonlinearity that limits the amplitude.

The mechanism of a relaxation oscillator is different. It is characterized by the fact that there is a single (in the simplest case) energy storage element. The periodic process in a relaxation oscillator consists of having the energy storing element accumulate an increasing supply of energy, until a certain definite upper level is reached. Then a certain valve discharges the accumulating element through a discharge circuit, until the energy reserve reaches a definite lower level. Now the valve operates again and makes the accumulating element resume charging.

This is explained in the block diagram of Fig. 104, in which S is the energy source, A the accumulating element, V the valve,  $F_b$  the feedback connection, and  $D_c$  the discharge circuit. It follows from this general description that the relaxation oscillator is characterized by the presence of a valve that can assume two fixed positions, one of which corresponds to charging the accumulating element, and the other to discharging.

The valve is controlled by feedback from the accumulating element. The feedback serves to operate the valve when two fixed energy levels are reached, an upper one and a lower one. It follows



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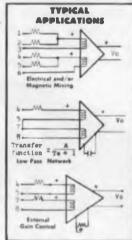


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that the swing of the relaxation oscillations does not depend on the energy balance, but is determined only by the difference between the two levels at which the valve operates.

All these general properties of relaxation oscillators can be readily understood by examining the simplest case, that of a relaxation oscillator with a gas discharge tube. The oscillator is shown in Fig.

The energy source is the battery E which charges, through resistor R, and capacitor C which serves as the accumulating element. The valve employed is the gas discharge tube T, which also serves as the circuit into which the accumulating element discharges. The oscillator operates as follows.

When the battery is connected, the capacitor starts charging. When its voltage reaches a value  $U_2$ , the "firing voltage" of Tube T, the gas in the tube ionizes and the tube resistance, which up to then was quite large, is sharply reduced to a small value r. The capacitor starts discharging rapidly into this resistance. When the voltage drops to a Value  $U_1$ , at which the ionization ceases, the resistance of the tube again rises sharply, and the capacitor-charging process is repeated.

The course of the phenomenon is shown by the oscillogram in Fig. 106, which shows time variation of the capacitor voltage. The swing of the oscillations depends only on the voltage difference  $U_2$ - $U_1$ . As to the frequency, it depends on the time constants of the charge and discharge circuits, and also on the supply voltage.

Let us evaluate the oscillation period. It consists of two sections  $\Delta t_1$  and  $\Delta t_2$ , of which the first determines the charge time and the second the discharge time. For the charge process we have

$$U = E\left(1 - e^{-\frac{t}{\tau_l}}\right)$$

where  $\tau_1 = RC$  is the time constant of the charge circuit. We can write the following two equations

Fig. 105. The simplest relaxation oscillator uses a gas tube.



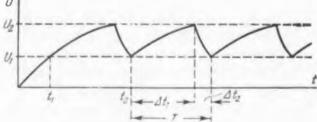


Fig. 106. Voltage variations on the capacitor in the relaxation oscillator of Fig. 105.

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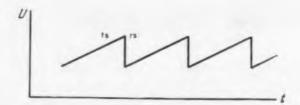


Fig. 107. A sawtooth voltage derived from a relaxation oscillator if the charge time is very large, and the discharge time very small. The letters on the figure represent the forward sweep and the return sweep.

$$U_1 = E\left(1 - \epsilon^{-\frac{t_1}{\tau_1}}\right), \ U_2 = E\left(1 - \epsilon^{-\frac{t_2}{\tau_1}}\right)$$

(see Fig. 106) from which we find

$$t_1 = \tau_1 \ln \frac{E}{E - U_1}, t_2 = \tau_1 \ln \frac{E}{E - U_2}$$

and hence also the charging time

$$\Delta t_1 = t_2 - t_1 = RC \ln \frac{E - U_1}{E - U_2}$$

This expression shows that the greater the value of E at given values of  $U_1$  and  $U_2$ , the smaller the difference between unity and the quantity under the logarithm, and the smaller the charging time. The charging process is given by the formula

$$U = U_2 \epsilon^{-\frac{1}{\tau_2}(t-t_2)}$$

where  $\tau_2 = rC$  is the time constant of the discharge circuit. When  $t = t_3$  a voltage value U = $U_1$  is reached. We obtain

$$U_1 = U_2 e^{-\frac{1}{\tau_3}(t-t_2)} = U_2 e^{-\frac{\Delta t_2}{\tau_2}}$$

hence

$$\Delta t_2 = r C \ln \frac{U_2}{U_1}$$

We now obtain the oscillation period by adding

$$T = \Delta t_1 + \Delta t_2 = C \left( R \ln \frac{E - U_1}{E - U_2} + r \ln \frac{U_2}{U_1} \right)$$

We see that the oscillation period depends on the time constants of the discharge and charge circuits, i.e., on the values of RC and rC, on the ratio of the firing and extinction voltages  $U_2$  and  $U_1$ , and on the supply voltage E.

If E and R are taken sufficiently large and r and C sufficiently small, the waveform approaches that shown in Fig. 107. A voltage of such form is called a sawtooth voltage and is extensively used in radio engineering as a sweep voltage in cathode-ray oscilloscopes, in television,

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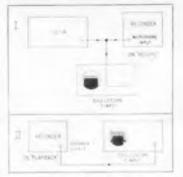
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Visual plot shows frequency response of tape recorder upon playback of test record using SG-1R, Log sweep; 40 cps to 20 kc.



Block diagram shows recorder test set-up with oscilloscope and SG-1R.



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#### **RUSSIAN TRANSLATIONS**

tion of return sweep (rs). The simplest circuit of Fig. 105 which we have analyzed does not satisfy these two requirements. The linearity of the forward sweep can be improved considerably by replacing the resistor R with a current limiter, such as a saturated diode. However, to generate a sawtooth sweep voltage it is preferable to use special, more highly developed relaxation oscillators.

#### 30. Relaxation Oscillators

One of the earliest relaxation oscillators circuits is the symmetrical multivibrator, which has retained its value to this day. The diagram of a symmetrical multivibrator is shown in Fig. 108. Both halves of the circuit can be considered as two separate generators, interconnected in such a way that one of the generators serves as the valve that controls the operation of the other.

To describe the operation of the circuit, we shall start with such a state, in which the currents and the plate circuits of the two tubes are exactly equal. This is an equilibrium state, which, however, is unstable. In fact, let the current of the first tube increase somewhat.

In this case the tube voltage becomes smaller than the initial value, and the capacitor  $C_1$  starts discharging. The discharge current, flowing through resistor  $R_{g2}$ , produces a negative voltage on the grid of the second tube. Consequently the voltage on the plate will increase and the plate current will diminish.

Owing to the increased plate voltage, capacitor  $C_2$  will start charging. The charging current, flowing through resistor  $R_{g1}$ , will produce a positive voltage on the grid of the first tube, and consequently a further increase in current of the first tube.

This analysis shows that the initial state we considered, in which the currents and the voltages of

This is an oscillator capable of generating many frequencies (in the sense of having a rich spectrum). The multivibrator was used in its time to calibrate wave meters, with the harmonic frequencies serving as reference points.

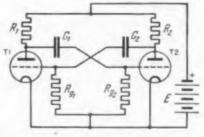


Fig. 108. The symmetrical multivibrator.



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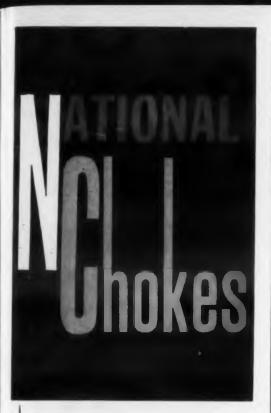
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Details about the Model 502 Milliohmmet are available in Keithley Engineering Notes Vol. 6 No. 3. Write for your copy today.



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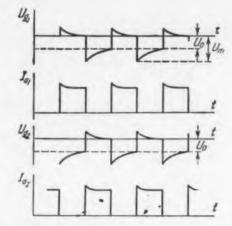


Fig. 109. Grid voltages and plate currents in the symmetrical multivibrator of Fig. 108.

both halves of the circuit are equal, is really unstable.

The increase in the current of the first tube and the increase in the negative voltage on the grid of the second tube are both very rapid. As a result, the first tube becomes saturated, and the second becomes blocked by the large negative voltage. Now capacitor  $C_1$  continues to discharge through  $T_1$  and  $R_{g2}$ ; the discharge current, and with it the negative grid voltage of  $T_2$  decreases until  $T_2$  starts conducting.

During the instant that the voltage across it drops, capacitor  $C_2$  starts discharging, and the currents and voltages change abruptly, as described above, but with the roles of two halves of the circuit interchanged.

The time variations of the plate currents and grid voltages of both halves of the circuit are shown in Fig. 109. Owing to the symmetry of the circuit, the durations of the plate current pulses are the same in both halves. Thus, the waveform of the plate current in each tube is nearly rectangular. Incidentally, by changing the parameters, it is possible to obtain also a nearly triangular form. The form of the oscillation depends on the charge and discharge time constants.

It is seen from the circuit of Fig. 108 that the time constant for charging is

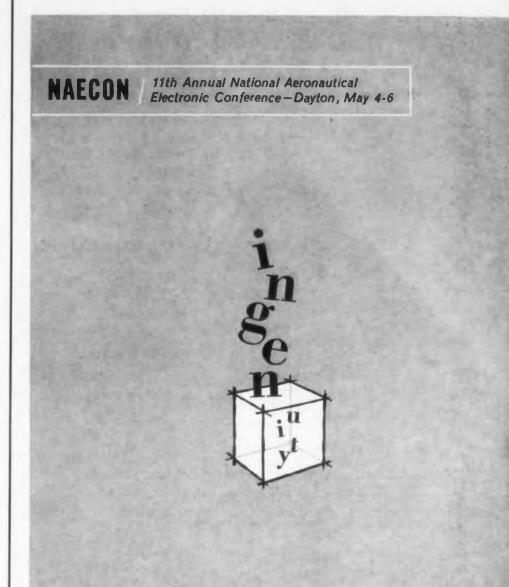
$$\tau_{\ell} = C \left( R_{g} + \frac{R_{i} R}{R_{i} + R} \right)$$

and the time constant for discharging

$$\tau_d = C \left( R + \frac{R_g \, r_g}{R_g + r_g} \right)$$

where C is the capacitance, R the resistance in the plate circuit,  $R_i$  the tube resistance (from the cathode to the anode),  $R_g$  the resistance in the grid circuit, and  $r_g$  is the tube resistance (cathode-grid).

Usually  $\tau_d \gg \tau_d$ . In this case the waveform of the oscillations is never rectangular. Knowing the time constant, it is possible to find the oscillation period. During one half of the period, the grid volt-



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age diminishes from the maximum value  $U_m$  to the cutoff value  $U_a$ . Thus

**RUSSIAN TRANSLATIONS** 

 $U_o = U_m \, \epsilon^{-\frac{1}{2} \frac{I}{\tau \dot{\epsilon}}}$ 

hence

$$T = 2 \tau_{\ell} \ln \frac{U_{m}}{U_{\phi}}$$

The cutoff voltage is a parameter of the tube. As to  $U_m$ , at the start of the discharge, i.e., directly after the current jump, it has a value.

$$U_m = E \frac{1}{1 + \frac{R_i}{R} + \frac{R_i}{R_g}}$$

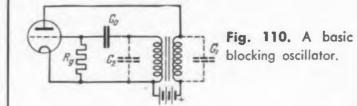
The period thus depends on the tube parameters, on the circuit parameters, and on the supply volt-

Another example of a relaxation oscillator is the blocking oscillator used principally to obtain various brief pulses (of duration down to fractions of a microsecond). The blocking oscillator circuit is shown in Fig. 110. It consists of a triode and a transformer, which couples the plate and grid circuits. The tank circuits are formed by the winding inductances and their distributed capacitances, whose equivalents are shown dotted in the dia-

The circuit of Fig. 110 can be considered as a degenerate ordinary oscillator with tuned grid and plate circuits. It is characterized by the fact that the processes that take place in the circuits are aperiodic in character and occur in intermittent sharp jumps. These jumps, called "blocking" in foreign literature are the reason for the name of this oscillator.

We shall examine the operation of this circuit from the instant when the capacitor  $C_o$  is charged and the grid is negative relative to the cathode, so that the tube is cutoff. Capacitor Co is discharged through resistance  $R_q$ . The time constant of the discharge is  $R_{\rho}C_{o}$ . When the voltage reaches a value  $U_o$ , the tube starts conducting and plate current flows.

Owing to the strong positive feedback, a positive voltage will appear on the grid, causing a further rapid rise in the plate current. This process, which is very fast, causes the anode voltage to drop almost to zero (which is the "blocking"). When the resultant grid voltage (which equals the



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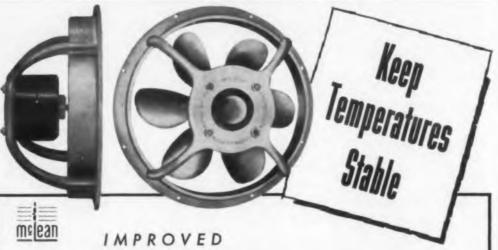
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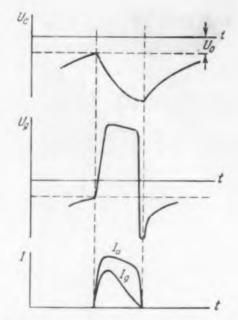


Fig. 111. Voltage and current variations in the blocking oscillator circuit.

sum of the negative voltage across  $C_o$  and the positive voltage induced by the feedback) drops to zero, grid current appears and the capacitor starts charging rapidly through the grid-cathode space, with a time constant  $C_o$   $r_o$ .

At this stage of the process the grid voltage is positive and a voltage appears on the plate. The tube has a small transconductance at this instant and changes in the grid voltage do not affect the plate current noticeably.

But later on, after the grid voltage reaches a maximum and starts diminishing, the transconductance increases. Finally, conditions favorable for the next jump are reached. The reduction in the grid voltage causes a reduction in the plate current, which causes a further reduction in the grid voltage, and the tube is cut off at very high speed. The cycle then repeats. Fig. 111 shows the time variation of the capacitor voltage  $U_c$ , of the grid voltage  $U_g$  and of the grid and plate currents  $I_g$  and  $I_{a*}$ 

The self excitation condition of the blocking generator can be written in the following form (provided  $C_1$  and  $C_2$  are very small compared with  $C_o$ ):

$$k \, S_a - \frac{1}{n \, R_s} - \frac{n}{R_\theta} - n \, S_\theta + \frac{1}{r_\theta} > 0$$

where  $S_a$  and  $S_g$  are, respectively, the transconductances of the plate and grid circuits,  $R_i$  and  $r_g$  are the internal cathode-plate and cathode-grid resistances, n is a transformation ratio and k the coupling coefficient (close to unity in our case). The minimum duration of the pulses depends on the leakage inductance of the transformer and on the parasitic capacitance  $C_1$ . The pulse repetition rate is determined essentially by the time constant for charging capacitor  $C_0$ , and is  $T \cong R_g C_0$ .

(This concludes Chapter 2. Chapter 3 starts in the next issue.)

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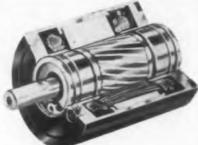
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#### **GERMAN ABSTRACTS**

E. Brenner

## Attenuation in the Passband of Filters

ILTERS which are designed on a pure-reactance basis have attenuation in the pass-band due to the losses in the reactive components, generally the coils. When high Q elements are used and attenuation constant  $\alpha_d$  can be related to the phase function  $\beta$  ( $\omega$ ) through the equation

$$\alpha_d = \frac{\omega}{2Q} \frac{d\beta}{d\omega}$$

Eq. (1) is a good approximation only when all the elements in the filter have a Q which is nearly the average value used in that equation. The use of equal Q elements does not result in

the best design because the quality which is required of each element is not the same at all frequencies, i.e. it depends on the frequency band in which the element is effective. Moreover, Eq. (1) applies only to filters in which coils and capacitors are used. When other components, such as quartz crystals, are employed, it does not apply.

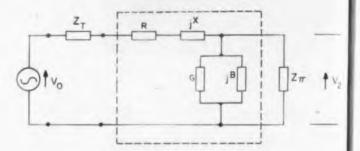


Fig. 1. Image terminated half section. The image transfer function,  $\ln ({}^{Vo}/2V_2)$  is calculated using for  $Z_T$  and  $Z_T$  the image impedances of the lossless (R=G=0) two port.

## Time Delays in P-N Junctions

WHEN p-n junction diodes are used in the sinusoidal steady state with large amplitude currents, two time delay effects are observed. When the diode is forced from the conduction into the nonconduction region, the current collapses  $\alpha/\omega$  usec after it has passed through zero. The approximate waveform is shown in Fig. 1. This time delay is due to a capacitive effect which occurs because of a storage of charge in the path regions of the junction. In the conducting direction, it is observed that the peak current amplitude, for constant impressed voltage, decreases with increasing frequency.

Denoting the life time of the charge carriers by  $\tau$ , the charge in the diode can be calculated assuming that for sufficiently large amplitudes the current waveform during conduction is sinusoidal, as shown in Fig. 1, when the voltage across the diode is sinusoidal.

The differential equation of the charging process can be written as

$$\frac{dQ}{dt} = I_m \sin \omega t - Q/\tau$$

and, subject to the initial condition Q(O) = O has the solution:

$$Q(t) = \frac{I_m \tau}{\omega \tau + \frac{1}{\omega \tau}} \left( e^{-t/\tau} + \frac{\sin \omega \tau}{\omega \tau} - \cos \omega \tau \right)$$

Hence the charge at  $\omega t = \pi/2$ , denoted by  $Q_d$  and the charge at  $\omega t = \pi$ , denoted by  $Q_d$  can be calculated as a function of frequency. The result is shown in Fig. 2. The curve for  $Q_d$  is confirmed by the experimental observation that the admittance in the conducting direction decreases with increasing frequency. Moreover, it follows that the corresponding time constant (L/r) can be approximated by  $\tau$ .

The charge  $Q_o$  controls the time delay for transition to the zero current state. Solving Eq. (1) on a new time scale, subject to the initial condition  $Q(O) = Q_o$  and replacing Q with -Q, one can solve for  $\alpha$ . The result is

$$exp\left[-(\pi+\alpha)/\omega\tau\right] = \frac{\sin\alpha}{\omega\tau} - \cos\alpha$$

Experiments indicate that the value of  $\alpha$ , as given by Eq. (3), is too large, probably because the diode is not fully discharged when the current flow ceases.

The total charge  $Q_c$  which is collected is given by

$$Q_c = \hat{I}_m \tau \frac{1 - \cos \alpha}{\alpha}$$

and its frequency dependence is also shown in Fig. 2. The difference  $Q_o - Q_c$  is the charge loss by recombination during the "reverse" time.

ELECTRONIC DESIGN • April 29, 1959

ELI

It can be shown that for the image terminated half section, shown in the Fig. 1, the image transfer function for high Q elements results in the attenuation constant  $\alpha_d$  where

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$$\alpha_d = \frac{1}{2} \left( R/Z_T + G Z_\pi \right)$$

where  $Z_T$  and  $Z_T$  are the image impedances of the half section if the losses are ignored. In terms of the Q's of the coils, it can be shown that Eq. (2) has the form

$$\alpha_d = \frac{k_1}{Q_1} + \frac{k_2}{Q_2} + \frac{k_3}{Q_3} \dots$$
 (3)

where  $k_1, k_2 \dots$  are frequency dependent "weighting factors" which are determined by the element values.

The original paper includes an elaborate example dealing with a quartz crystal filter as well as a discussion of the numerical evaluation of the weighting factors from the frequency dependence of image and driving point impedances.

Abstracted from an article by J. Boehse, Frequenz, Vol. 12, No. 12, December 1959, pp 380-383.

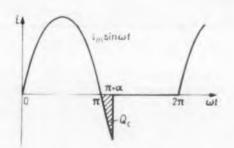


Fig. 1. Approximate current waveform for the p-n junction diode.

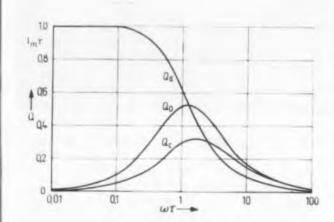


Fig. 2. Stored charge at the time  $\omega t = \pi/2$ ,  $Q_d = Q(\pi/2\omega)$ , at the instant  $\omega t = \pi$ ,  $Q_0 = (\pi/\omega)$ , and net charge  $Q_c$  as a function of (normalized) frequency.

Abstracted from an article by W. Heinlein, Archiv der Elektrischen Uebertragung, Vol. 12, No. 11, November 1959 pp 510-514.

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#### MEETINGS

#### May

- 3-7 Symposium on Electrode Processes, Philadelphia, Pa.
- 4-6 11th National Aeronautical Electronics Conference (IRE), Dayton, Ohio
- 4-8 85th Society of Motion Picture and Television Engineers Convention, Fontainbleau Hotel, Miami Beach,
- 5-7 URSI Spring Meeting (PGI, PGIT, PGGT), Washington D.C.
- 5-7 7th National Conference on Electro-Magnetic Relays, Stillwater, Okla.
- 6-8 1959 Electronics Components Conference (IRE, AIEE, EIA, WCEMA), Philadelphia, Pa.\*
- 6-8 7th Regional Technical Conference and Trade Show (IRE), Albuquerque, N. Mex.
- 11-12 Symposium on Industrial Uses of Radioisotopes, Atlanta, Ga.\*
- 11-13 National Power Instrumentation Symposium, Kansas City, Kan.
- 11-13 National Symposium (PGMT, IRE), Boston, Mass.
- 11-13 2nd Annual Joint Conference on Automatic Techniques,
  Chicago, III.\*
- 11-13 Radio Technical Commission for Marine Services Assembly Meeting, Mt. Royal Hotel, Montreal, Canada
- 12-14 Annual Frequency Control Symposium, Signal Research and Development Laboratory, Fort Monmouth, Berkeley-Carteret Hotel, Asbury Park, N.J.
- 18-20 5th Annual National Symposium on Instrumental Methods of Analysis, Houston, Tex.
- 18-20 Electronics Parts Distributors Show, Chicago, III.\*
- 18-20 Fifth National Symposium on Instrumental Methods of Analysis, Instrument Society of America, Hotel Shamrock Hilton, Houston, Tex.
- 19-21 AIEE Middle Eastern District Meeting, Baltimore, Md.
- 20-22 National Spring Meeting, Society for Stress Analysis, Sheraton Park Hotel, Washington D.C.
- 25-27 National Telemetry Conference (IAS, ISA, AIEE, ARS), Denver, Colo.\*
- 25-29 International Convention on Transistors and Associated Semi-Conductor Devices, London, England\*

#### 1959 Electronic Components Conference, May 6-8

Benjamin Franklin Hotel, Philadelphia, Pa. Sponsors: IRE, EIA, AIEE, WCEMA. Theme: New Concept for Space Age. Contact John E. Hickey, Jr., The Chilton Co., 56th & Chestnut Sts. Philadelphia 39, Pa.

#### Symposium on Industrial Uses of Radioisotopes, May 11-12

Georgia Tech. Campus, Atlanta, Ga. Sponsors: Georgia Tech., Office of Isotopes Dev. (AEC), and Lockheed Aircraft Corp. This symposium is designed to serve an eleven-state area and will show industrialists the many ways in which they can use isotopes to save time. For further information contact: Richard Wiegand, Director, Short Courses & Conferences, Georgia Institute of Technology. Atlanta, Ga.

#### Second Annual Conference on Automatic Techniques, May 11-13

Pike Congress Hotel, Chicago, Ill. Sponsored jointly by ASME, AIEE, and IRE. The meeting

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Electronic Parts Distributors Show, May 18-20

Conrad Hilton Hotel, Chicago, Ill. An expanded educational program for distributors designed to bring further benefits to the industry will be a special highlight of the show.

#### National Telemetry Conference, May 25-27

Brown Palace and Cosmopolitan Hotel, Denver, Colo. Sponsored annually by the American Rocket Society, IAS, AIEE, and ISA. Theme: Investigation of Space. Twelve Sessions are tentatively scheduled for the meeting including such subjects as: Special Telemetry Techniques for Satellites and Space Vehicles; Sub-miniaturization; Telemetering of Bio-Medical Information from Man in Space; Transistorization and Data Processing. For information contact Ralph Schmidt, AVCO Mfg. Co., 201 Lowell St., Wilmington, Mass.

International Convention on Transistors and Associated Semi-Conductor Devices, May 25-29

To be held in London, this convention has been organized by the radio and telecommunication section of Britain's Institution of Electrical Engineers to mark the tenth anniversary of the transistor. It will be the most comprehensive ever held on transistors and will cover design, manufacture, basic theory, characteristics, measurements, applications, and equivalent circuits. To provide the widest possible interest, the International Transistor Exhibition will be held at the same time. For details contact Industrial & Trade Fairs Ltd., Drury House, Russell Street, London, W. C. 2, England.

#### **Paper Deadlines**

May 10: Deadline for receipt, in triplicate, of a 100-200 word abstract and a 500-word summary of papers for the 1959 National Symposium on Telemetering to be held in San Francisco, September 28-30. July 10 is deadline for receipt of full-length papers on specially provided master sheets. Submit papers as early as possible on significant work in telemetry and related fields, such as space vehicle communication systems, satellite instrumentation, data processing equipment, new developments in telemetry equipment, and flight test electronics. Further inquiry should be directed to: George L. Larse, Program Chairman, Lockheed Aircraft Corporation, Missile Systems Division, Sumnyvale, Calif.

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T-34894 Weight: 260 grams VA: 26.4 30°C rise, 125°C ambient 6.2 KV test @ 30,000 feet



T-36196 Weight: 235 grams. VA: 32 31°C rise, 125°C ambient 5.2 KV test @ 30.000 feet

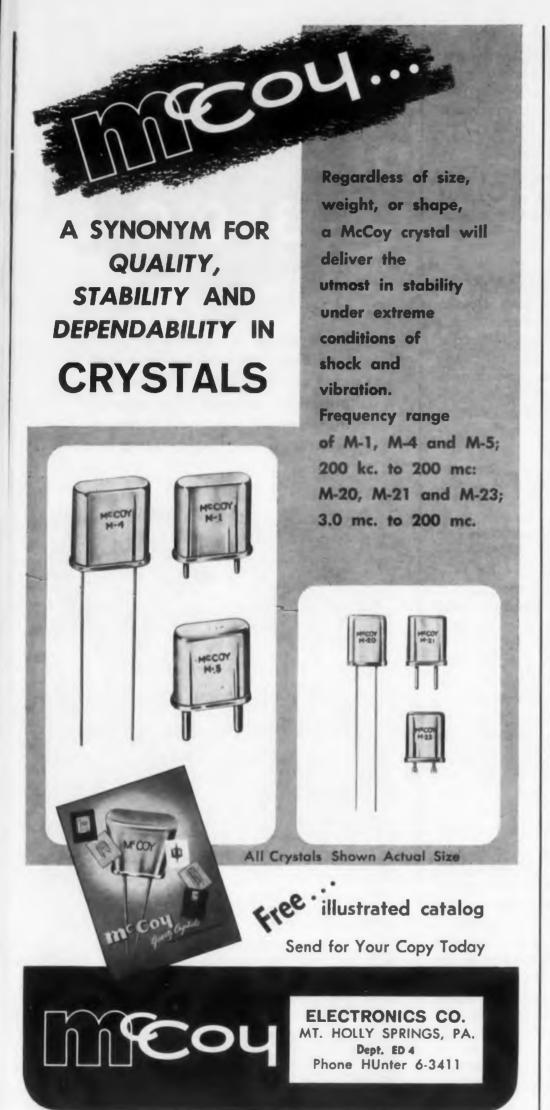
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#### REPORT BRIEFS

**Noise Sources in Radio Receivers** 

Considered in this study were problems of standard noise sources in a radio receiver, calibration of secondary standards, and their use in measuring receiver noise factors-problems which are associated with the use of the receiver in radio astronomy where noise is the intelligence measured. A review of figure of merit concepts and receiver measuring practices using gas-discharge noise sources led to formulae which are said to reduce computations to simple additions of excess noise temperature and attenuations. Hot-body noise sources were used as standards in development and calibration of gas-discharge noise sources. Studies of calibrations and source design problems disclosed sources of errors, useful design features, and special techniques valuable for receiver measurements and calibrations. Fundamentals in Noise Source Calibrations At Microwave Frequencies, J. E. Sees, Naval Research Laboratory, Jan. 1958, 24 pp, \$0.75. PB 131367 from OTS, U. S. Department of Commerce, Washington 25, D.C.

#### Electronic Materials Rated

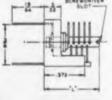
Electronic transformer materials which appear best suited for use at 500 C and under intense nuclear radiation, the severe environmental combination in which future military electronic equipment may be expected to operate, are identified in a report of recent research for the Air Force. The broad evaluation of transformer basic materials showed mica paper, glass-served silver wire, and grain-oriented silicon steel to have best properties after aging for 1000 hours. The materials were also shown to perform together as transformers. For mechanical moisture protection of transformers, an encapsulating technique using a thin ceramic coating in conjunction with a stainless steel mesh was found feasible. Tests under combined high temperature and radiation tentatively indicated that effects on both materials and transformers were primarily caused by temperature. An exception appeared to be in the dielectric breakdown strength of air. Evaluation results were expected to form a basis for a tentative design practice for construction of transformers and inductors tolerant to the severe environment. Two volumes of the research appear in a single report. Ultra High Temperature Miniaturized Power Transformers and Inductor Materials, Volumes 1 & 2, H. B. Harms, J. C. Fraser, General Electric Company for Wright Air Development Center, U. S. Air Force, May 1958, 476 pp, \$6.00. Order PB 151141 from OTS, U. S. Department of Commerce, Washington 25, D.C.



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#### **Target Data Processing Systems**

This report studies the human capabilities in tasks assigned to operators of target data processing systems using manual detection and tracking. Two aspects of detection and tracking task design are discussed. First, the type and number of tasks which can profitably be assigned to an operator are reviewed. The second discussion offers some suggestions for facilitating performance of the basic tasks of detection, tracking. and monitoring. The information is said to be particularly applicable to semiautomatic systems in which electronic data storage is provided. Some Problems in The Design of Human-Operated Target Data Processing Systems, T. J. Coonan, Naval Research Laboratory, Sept. 1958, 7 pp, \$0.50. Order PB 151113 from OTS, U.S. Department of Commerce, Washington 25, D.C.

#### **Visual Coding Dimension**

An investigation was conducted to determine whether the flash rate of a flashing light was a suitable coding dimension for the presentation of information. Results showed that no more than five discriminable steps of flash rate could be used for encoding information. The report states that the investigation showed that flash rate was not a good information code for cathode ray tube displays, but it might be a very useful code for exterior lighting displays on aircraft or on the ground. Flash Rate As A Visual Coding Dimension For Information, J. Cohen, A. J. Dinnerstein, Antioch College for Wright Air Development Center, U. S. Air Force, May 1958, 13 pp, \$0.50. Order PB 151185 from OTS, U.S. Department of Commerce, Washington 25, D.C.

#### **Aircrew Fatigue Problems**

Outlined in this report is a plan for an experimental program designed to determine the effects of confinement stresses of a five-man crew. These men would be isolated in a flight station for 120 hours. The experimental crew compartment is described and illustrated. Performance tasks, programming and recording instruments, together with the laboratory techniques planned for use in the experiment, are explained. Aircrew Fatigue Problems During Extended Endurance Flight: Phase 1—Planning. O. S. Adams, Lockheed Aircraft Corporation for Wright Air Development Center, U. S. Air Force, May 1958, 86 pp, \$2.25. Order PB 151189 from OTS, U. S. Department of Commerce, Washington 25, D.C.

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#### REPORT BRIEFS

#### Sensory Capacity as Data Source

A general survey of what is known about man's ability to make use of his sensory capacities for gathering information is presented. Some comparisons between different sense modalities are made and the problem of sensory interactions is discussed. Use of some of the subordinate sensory channels is also examined. Man's Senses As Informational Channels, G. H. Mowbray, J. W. Gebbard, Applied Physics Laboratory, Johns Hopkins University, for U.S. Armed Forces, May 1958, 71 pp, \$2.00. Order PB 151160 from OTS, U. S. Department of Commerce, Washington 25 D.C.

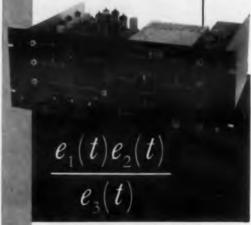
#### Vanguard Satellite Receiver

An earth satellite command receiver was developed for use in Vanguard and other United States satellites. This receiver turns on the satellite instrumentation upon command from a ground-based Minitrack station. It is a vhf double-superheterodyne type utilizing a small portion of the 108-Mc Minitrack transmitter power as the first local oscillator. The basic design of the various components provides for economical use of satellite battery power and at the same time a reasonable degree of security against accidental interrogation from unauthorized sources. Project Vanguard Report No. 35: Minitrack Report No. 6-The Vanguard Satellite Command Receiver, D. S. Hepler, U. S. Naval Research Laboratory, Sept. 1958, 11 pp, \$0.50. Order PB 151112 from OTS, U.S. Department of Commerce, Washington 25, D. C.

#### Radio Stars for Vanguard Tracking

The Mark II Minitrack System, whose function is primarily the tracking of artificial satellites, was also designed for the tracking of radio stars. A means of external calibration of the system by tracking these radio-noise sources is described and illustrated. Results obtained by this method are presented and compared with results obtained by the complex but more precise method used in calibrating Prime Minitrack stations. It is reported that the tracking of radio stars does in fact provide an adequate system calibration if sufficient data are taken. The system is described briefly and an operational analysis is made. Project Vanguard Report No. 33: Minitrack Report No. 7-Calibrating the Mark II Minitrack System with Radio Stars as Signal Sources, V. R. Simas and G. C. Kromiller, Jr., U. S. Naval Research Laboratory, Oct. 1958, 28 pp, \$0.75. Order PB 151163 from OTS, U.S. Department of Commerce, Washington 25, D. C.

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#### **Vibration Manual**

The Vibration Manual for Engineers, a Navy publication containing formulas useful to design engineers in minimizing mechanical vibration difficulties, was prepared by the Structural Mechanics Division of the Navy's David Taylor Model Basin. It updates an earlier manual having the same title (1944). The revised edition has the main purpose of expediting calculations required by the practicing engineer. Most formulas conform with a notation based on the inch-poundsecond systems of units. They are presented in case form and are illustrated and explained. A Vibration Manual for Engineers (Second Edition), R. T. McGoldrick, Structural Mechanics Division, David Taylor Model Basin, U. S. Navy, Dec. 1957, 32 pp, \$1.00. PB 131785 from OTS, U. S. Department of Commerce, Washington 25, D.C.

#### **Audio Filter**

Design of an active, low frequency, bandpass filter is described. The synthesis technique made use of RC elements with transistor negative impedance converters to obtain complex poles. Very steep skirt selectivity and 20 db of transmission gain were achieved, but the variation of filter properties with temperature limits this particular filter to use in an environment such as might be encountered normally in a laboratory. It is felt that this limitation is not fundamental and could be substantially alleviated by the use of different transistor types. Audio Filter, P. Z. Grayum, Philco Corp., 5 Dec. 56, 29 pp, microfilm \$2.70, photocopy \$4.80. Order PB 135512 from Library of Congress, Washington 25, D.C.

#### **Theory of Systems**

The first three of the five sections present complete developments of theories followed in current engineering practice. Section one discusses the tasks that can and cannot be performed by digital control systems and digital computing systems. Sections two and three contain developments of theories of discrete and of continuous mechanisms. The final two sections are specialized. One discusses weighting functions for continuous mechanisms from the point of view of functional analysis. In the last section, an important class of mechanisms known as finite automata is analyzed using algebraic techniques. Fundamental Concepts In The Theory of Systems, University of Chicago for Wright Air Development Center, U. S. Air Force, Nov. 1957, 137 pp, \$2.75, Order PB 151242 from Office of Technical Services, U. S. Department of Commerce, Washington 25, D. C.

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#### Sir Francis Drake Cracks a Case

One foggy day in 1588, a single ship of the Spanish Armada managed to sneak behind Drake's entire British fleet lying in the English Channel off Plymouth Hoe, and drop a 10 pounder smack in the middle of a bowling match between Sir Francis and his friend Walter Raleigh.

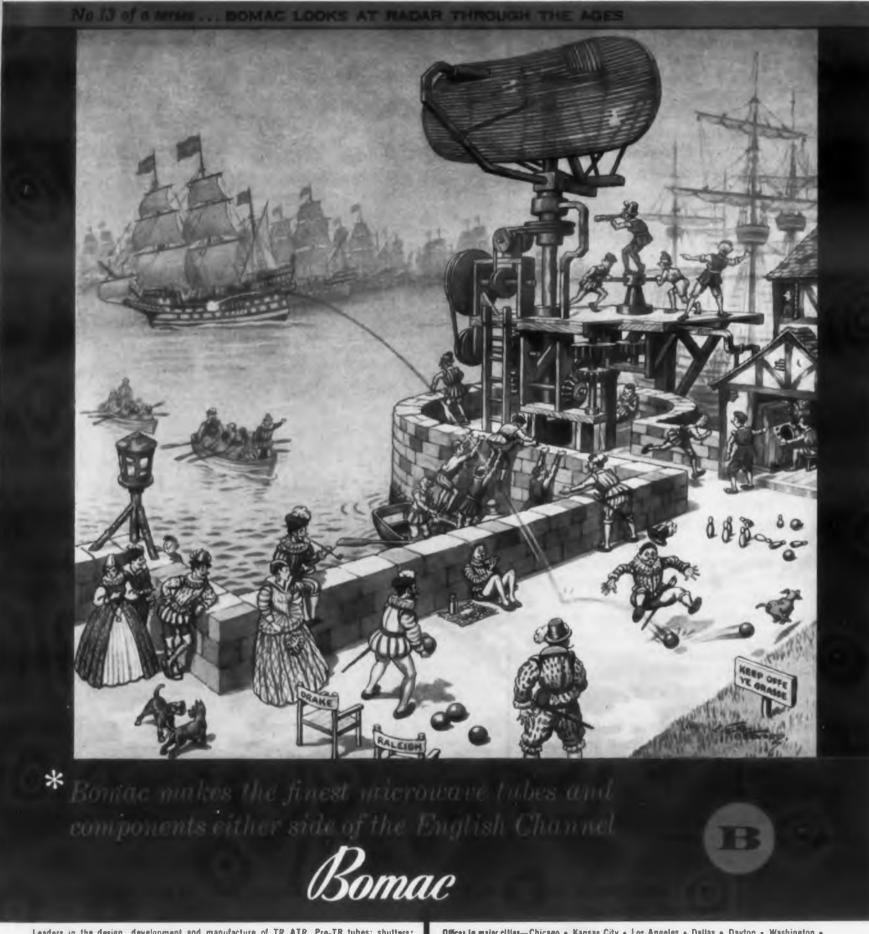
The new radar was caught completely by surprise. Had the IFF (Identification: Francis or Foe?) system failed? Was the operator tuned to the wrong Channel? Was there something wrong with the tubes? Drake was determined to find out. He was inside the shack in a trice, whatever that is. "Avast?" he roared at the radarman, "I must inspect those tubes!"

Drake picked up a magnetron and looked at it. "Aha!" he ex- to bowl over the Armada.

claimed. "Just as my razor-keen mind suspected!" With that, he seized the hapless operator by the throat and shook him like a tumblerful of sidecars. "I arrest you for stealing Bomac tubes" and substituting these inferior substitutes, WILLIAM SHAKESPEARE!"

"I confess, how'd you guess?" said Shakespeare, ever the poet.
"Elementary for a razor-keen mind like mine," answered Drake. "Only you could have conceived the cunning scheme of replacing Bomac tubes with factory seconds labeled "Bethmac" as a publicity stunt for your new play — Macbeth!"

"Yours is a razor-keen mind indeed!" marveled Shakespeare as they led him away. "I haven't even written Macbeth yet!"
"Plenty of time where you're going," said Drake — and went off



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#### **ADVERTISERS' INDEX April 29, 1959**

Advertiser	Page
AGA Div. of Elastic Stop Nut Corp. AMP, Inc. Ace Electronics Associates Acme Electric Corp. Aerovox Corp. Air Marine Motors, Inc. Airflyte Electronics Allied Radio Corp. Alpha Metals, Inc. Alto Scientific Co. Amphenol Borg Electronics Corp. Ansley, Arthur Mfg. Co. Atlas E-E Corp.	21 85 115 10 104 114 79 97
BJ Electronics Borg-Warner Corp. Babcock Relay, Inc. Bendix Aviation Corp., Pacific Div. Bendix Aviation Corp., Red Bank Div. Tubes Bendix Aviation Corp., Scintilla Div. Berkeley, Div. of Beckman Instruments, Inc. Bomac Laboratories, Inc. Brew, Richard D. & Co., Inc. Burndy Corporation Burnell & Co., Inc.	24 100
CBS-Hytron Cannon Electric Co. Centralab, Div. of Globe-Union, Inc. Chassis-Trak Corp. Chicago Dynamics Industries, Inc. Clare, C. P. & Company Clevite Transistor Products Columbus Electronics Co. Comar Electric Company Computer-Measurements Corp. Crosley Div. AVCO Mfg. Corp.	
Daven Co., The Delta-f, Inc. Dialight Corp. DIT-MCO, Inc. Dorsett Laboratorics Dow Chemical Company, The DuMont, Allen B. Labs., Inc.—Ind. Tube Div.	61 111 112 87 84 43
ESC Corporation Eitel-McCullough, Inc. (Eimac) Electrical Industries Electro Engineering Works, Inc. Electro Instruments Electro-Measurements, Inc. Electron Products, Inc. (Preco, Inc.) Epoxy Products Inc.	31 1 III 17
Fairchild Semiconductor Corp. Franklin Electronics, Inc.	93 103
G-V Controls, Inc. General Electric Co., Apparatus Div. General Electric Co., Lamp Division General Electric Co., Capacitors General Electric Co., Semiconductor Products Dept	3, 77 13 96 20
Hallamore Electronics Company Harvey-Wells Electronics, Inc. Hewlett-Packard Company Hi-Temp Wires, Inc. Holt Instrument Laboratories Hughes Aircraft Co.	114 41 56 105
International Business Machines Corp. 98 International Resistance Co Iron Fireman Mfg. Co., Electronic Div	, 99 14 45
Jerrold Electronics Corp.  Johnson Mfg. Corp.  Jordan Electronics	

Advertiser	Page
Kearfott Co., Inc., Little Falls Div. Keithley Instrument Co. Kellogg Switchboard & Supply Co. Kester Solder Co. Keuffel & Esser Krohn-Hite Corp.	46 108 88 108 47 84
Lambda Electronics Corp. Leach Corp. Leach & Northrup Co. Lermer Plastics Litton Industries, Inc., Electronic Equipment Div. Lockheed Aircraft Corp., Missile Systems Div. Lord Mfg. Co.	91 111 88
McCoy Electromes Co. McDonnell Aircraft Corp. 80 McLean Engineering Laboratories Maida Development Co. Marion Electrical Instruments Measurements Research Metron Instrument Co. Michigan Magnetics, Inc. Micro-Lectric, Div. of Micro Machine Works Minneapolis-Honeywell Co. 37 Mitchell-Rand Mig. Motorola, Inc., Western Military Electronics Center	96 114 119 115 106
National Co., Inc 64,	109
Oak Mfg. Co	27
Pacific Semiconductors, Inc. Panoramic Radio Products, Inc. Phelps Dodge Copper Products, Co. Phileo Corp., Lansdale Tube Div. Philbrick, George A., Researches, Inc. Photocircuits Corp., Polytechnic Research & Development Co. Potter & Brumfield Potter Instrument Co.	107 107 63 118 30 86 72 6
Radio Corp. of America, Electron Tube Div	1V 95 55 2 4 87 89
Segal, Edward Shell Chemical Corp. Smmons Fastener Corp. Solid State Electronics Southco, Div. of South Chester Corp. Sprague Electric Co. Spragne Products Co. Stanford Research Stromberg-Carlson Co., Div. of General Dynamics	15 r 11 101 52 49 9 94 108
Technic, Inc. Technical Information Corp. Technology Instrument Corp. Tektronix, Inc. Telemeter Magnetics, Inc. Texas Instruments, Inc. Trotel, Inc.	96 100 102 53 25 83 73 79 106 67
Varian Associates	12
Vard Leonard Electric Co. eleb, W. M., Mfg. Co. estinghouse Electric Corp., Industrial Tube Div. heelock Signals, Inc.	97 58 10 82 34 05
As o Mig., Co.	13

Page

> 74 88 40

24 100

70

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• Faster slewing speeds — Pen: 30"/sec.; Carriage: 30" sec.

- Greater accuracies Static: 0.1%; Dynamic: 0.2%.
- 0.05% internal calibration.
- High precision internal Zener diode reference.
- New improved vacuum hold-down system.
- Vernier control between ranges.
- Input function modules in rack mountable case can be removed from plotter for remote operation.
- Calibrated scales on both axes.
- Front panel gain control
- Vacuum release on front panel.
- Visible ink supply.

One basic plotter with input modules available for general purpose, computer, low level differential, time base, curve following and other specialized functions.

	Model 410 Computer Module	Model 420 General Purpose Module	Model 430 Lew Level Differential Medule	Medel 450 Curve fellower Medule	Model 460 Time Base Module
Input	Single Ended	Single-Ended	Differential	Single-Ended	Single-Ended
Ranges	0.1, 1.0, 10v in, calibrated vernier	16 steps, 1m v/in to 100 v/in, plus vernier	16 steps, 1m v in to 100 v in, plus vernier		0.1, 0.2, 0.3, 0.6, 1.0, 2.0 in/sec
Accuracy: Static Bynamic	± 0.1% F/s ± 0.2% F/s	± 0.1% F/s ± 0.2% F/s	± 0.15% F/s ± 0.2% F/s	± 0.25% F/s	(time) ± 1.0% F/s
Linearity				± 0.1% F/s	(sweep) + 0.5% F/
Input Resistance	2 megs, all ranges	1 meg to 3 megs Depending on range	1 meg to 3 megs Depending on range		
Zere Adjust	Full scale X and Y plus 9" offset	Full scale X and Y plus 9" offset	Full scale X and Y plus 9" offset		
Reference	Internal Zener diode and external + 100v computer	Internal Zener diode	internal Zener diode		Internal Zener diode
Calibration	Internal 0.1, 1.0, 10v Accurate to + 0.05%				
Common Mode Rejection			DC, 120 db AC, 100 db al 60 cps		
Max. Common Mede Voltage			50 v dc or peak ac		
Principle of Operation				60 cps magnetic induction	Electronic integration
Zero Drift				None	

imensions All Modules: 8½" W x 3½" H x 7¼" D

3540 Aero Court San Diego 11, California Model 400 Plotter Recording Size: 10" x 15"

Slewing Speed: X, 40"/sec; Y, 30"/sec
Inputs: X and Y inputs, and computer reference
Power: 115 ± 10 v, 60 cps

Dimensions: 19" W x 19½" M x 11¾" D

Ambient Temperature Range: 0-55 °C

Controls: Power off, standby, operate, pen; vacuum release; curve follower, amplifier; local, remote.

Electro Instruments, Inc.





Or, are you wisely designing "around" a dependable easy-to-obtain-in-the-field Preferred Tube Type?

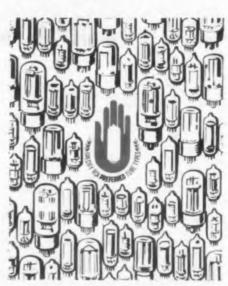
Some day, the tv or radio set you designed is going to need service. Some day, a service dealer is going to have to replace a tube type you specified. Can the service dealer replace with a *stock* tube? That is one of the big tests of an original design.

There are more than a thousand tube types you can design "around". But, the majority of today's tv and radio circuits employ less than a hundred of those types. For good reason, too. Over the years those *preferred* types have proven to be tops...in quality...in versatility...in reliability and replaceability.

If the tubes you specified for your design are Preferred Tube Types, you can bet that field replacement will not be a problem. If not—it may mean a "callback" and a customer who begins to doubt his choice of sets. Help keep them sold with Preferred Tube Types.

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