

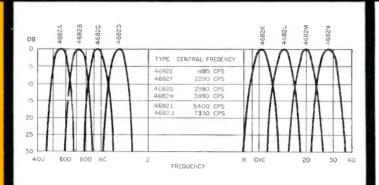
FILTERS

FOR EVERY APPLICATION



TELEMETERING FILTERS

UTC manufactures a wide variety of band pass filters for multi-channel telemetering. Illustrated are a group of filters supplied for 400 cycle to 40 KC service. Miniaturized units have been made for many applications. For example a group of 4 cubic inch units which provide 50 channels between 4 KC and 100 KC.



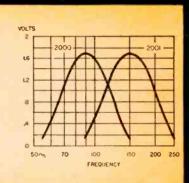






Dimensions: (3834) 1½ x 1¾ x 2-3/16", (2000, 1) 1½ x 1¾ x 1¾ x 15%".

VOLTS 8 6 2 200 500 INC FREQUENCY



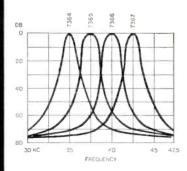
AIRCRAFT FILTERS

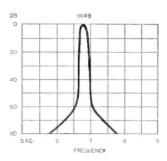
UTC has produced the bulk of filters used in aircraft equipment for over a decade. The curve at the left is that of a miniaturized (1020 cycles) range filter providing high attenuation between voice and range frequencies.

Curves at the right are that of our miniaturized 90 and 150 cycle filters for glide path systems.

CARRIER FILTERS

A wide variety of carrier filters are available for specific applications. This type of tone channel filter can be supplied in a varied range of band widths and attenuations. The curves shown are typical units.



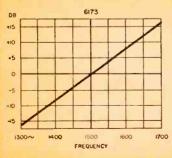


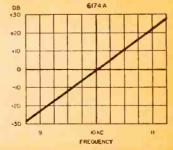


Oimensions: (7364 series) 1% x 1% x 2¼". (8649) 1½ x 2 x 4".

DISCRIMINATORS

These high Q discriminators provide exceptional amplification and linearity. Typical characteristics available are illustrated by the low and higher frequency curves shown.







Dimensions: (6173) 1-1/16 x 13/8 x 3". (6174A) 1 x 11/4 x 21/4".

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For full data on stock UTC transformers, reactors, filters, and high Q coils, write for Catalog A.

A McGRAW-HILL PUBLICATION . VOL. 30 . NO. 12 . DECEMBER 1, 1957

ISSUE AT A GLANCE

Testing Superpower Klystron. Tube shown being lowered into test tank delivers

	up to 1,000,000 watts peak power r-f (See p 182)COVER
М.	How Transistors Operate Under Atomic Radiation. Results of nuclear tests show that effects can be controlled by feedback
inn, To- ster laig est, P.	Transmitter Circuits for Suppressed-Carrier A-M. Up-to-date transmitting techniques improve efficiency of a-m systems
rard arry eles) litor	Toroid Measures Spot Weld Current. Voltage developed by coil around welding electrode is converted to steady-state meter reading
Ma- Roy C.	Dual-Purpose Circuitry Cuts Transceiver Size. Reflex circuitry permits design of 1,750-channel transceiver using only 28 tubes
n L. 1 J, reen Bar-	Flat-Field Generator Speeds Color Tv Testing. Provides composite color video signals of any hue and saturation as well as luminance signalp 139 By Richard W. Cook
sing As- ager Fred iger.	Spot Scanner Counts Micron-Sized Particles. Moving target indicator spots and counts particles such as bacteria colonies
iger. ified arch. Con- iller.	Transistor Relays Have Low Idling Current. Electronic relays require only a few microamperes

Digital-Analog Converter Provides Storage. Transistorized converter changes eight

Clamp-On Microammeter Measures A-C Current. Small toroidal current trans-

By H. N. Putschi, J. A. Raper and J. J. Suran

By G. F. Montgomery and C. Stansbury

By Stanley Boyle

former clamped about unknown current measures microamperes p 152

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electronics

December 1, 1957 Vol. 30, No. 12

Published three times a month with an additional issue in June, by McGraw-Hill Publishing Company, Inc., James H. McGraw (1860-1948) Founder.

Executive, Editorial, Circulation and Advertising Offices: McGraw-Hill Building, 330 W, 42 St., New York 36, N. Y.

Longacre-4-3000. Publication Office 99-129 North Broadway, Albany 1. N. Y. See panel below for directions regarding subscription on change of address. Donald C. McGraw, President; Joseph A. Gerardi, Executive Vice President; L. Keith Goodrich, Vice President and Treasurer; John J. Cooke, Secretary; Nelson Bond, Executive Vice President, Publications Division; Ralph B. Smith, Vice President and Editorial Director; Joseph H. Allen, Vice President and Director of Advertising Sales; A. R. Venezian, Vice President and Circulation Coordinator.

Single copies \$1.00 for Engineering Edition and 50¢ for Business Edition in United States and possessions, and Canada; \$2.00 and \$1.00 for all other foreign countries. Buyers' Guide \$3.00. Subscription rates-United States and possession, \$6.00 a year; \$9.00 for two years. Canada, \$10.00 a year, \$16 for two years. All other countries \$20.00 a year, \$30.00 for two years. Three year rates accepted on renewals only, are double the one-year rate. Second class mail privileges authorized at Albany, N. Y. Printed in U.S.A. Copyright 1957 by McGraw-Hill Publishing Co., Inc.— All Rights Reserved. Title registered in U. S. Patent Office. BRANCH OFFICES: 520 North Michigan Avenue, Chicago 11; 68 Post Street, San Francisco 4; McGraw-Hill House, London E. C. 4; National Press Bldg., Washington, D. C. 4; Architects Bldg., 17th & Sansom Sts., Philadelphia 3; 1111 Henry W. Oliver Bldg., Pittsburgh 22; 1510 Hanna Bldg., Cleveland 15; 856 Penobscot Bldg.. Detroit 26; 3615 Olive St., St. Louis 8; 350 Park Square Bldg., Boston 16; 1321 Rhodes Haverty Bldg., Atlanta 3; 1125 West Sixth St., Los Angeles 17: 1740 Broadway, Denver 2. ELECTRONICS is indexed regularly in The Engineering Index.

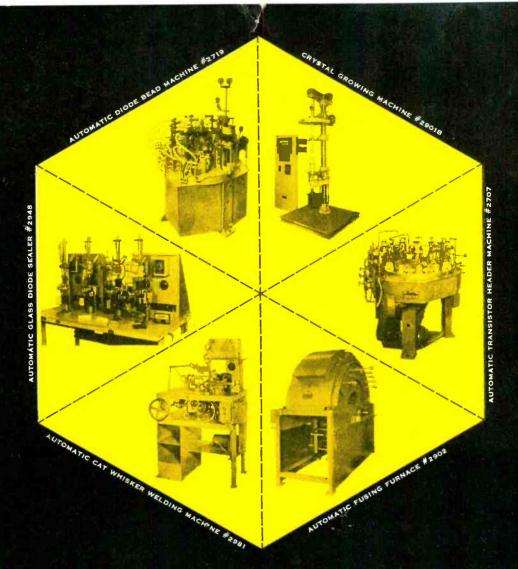
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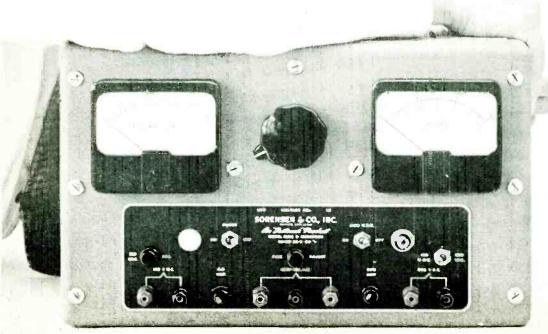
filament supply and all but the 300-B and 1000-BB offer 0-150 volt regulated bias.

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*Only 0.15% maximum variation on the 0-300. and 0.25% on the 0-600 models.



		SPEC	IFICATION	IS		
	Model	300B*	325BB	500BB	600B	1000BB
	Output Voltage VDC	0-300	0-325	0-500	0-600	200-1000
	Output Current Ma	0-150	0-125	0-300	0.500	0-500
	Regulation Accuracy	±0.15%**	±0 5%	±0.5%	==0.25%	0.5%
	Ripple (MV-RMS)	5 max.	5 max.	5 max.	3 max.	20 max.
į	Bias Supply (VDC)	Mg colored	0-150	0-150	0-150	tegition 1
	Max. Bias Circ. Imp. (Ohms)	More	25000	25000	50000	
	Max. Int. Imp. (Ohms)	2.0	2.0	2.0	2.0	2.0
	AC Voltage (CT Unreg.)		6.3/10 amps	6.3/10 amps	6.3/15 amps	
	Filament Voltages (Unreg.)	6.3 at 5 amps, se parallel (two		description .	****	
	· may be co	nnected posi	tive or m	egative.	n series	or paralle

or ±0.3 volts, whichever is greater

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MARCONI'S SPEED SSB CHECKS

HF SPECTRUM ANALYZER
TYPE OA 1094

The Marconi OA 1094 Analyzer gives an immediate panoramic display of the frequency spectra of signals in the band 3 to 30 MC. It brings speed and convenience to the alignment of SSB communication transmitters and drives. Intermodulation distortion, hum level and carrier compression, the bandwidth of FSK and on/off keyed signals—these can all be seen at a glance and evaluated directly against the CRT graticule. A crystal-controlled first local oscillator insures a drift-free display at sweep widths as low as 100 cps. Highly-selective IF crystal filters provide 60 db discrimination between components as little as 60 cps apart.

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Frequency Range: 3 to 30 MC in 9 bands with separate fixed drivefrequency input.

Sweep Width: Continuously variable up to 30 KC.

Sweep Duration: 0.1 to 30 sec in 6 steps.

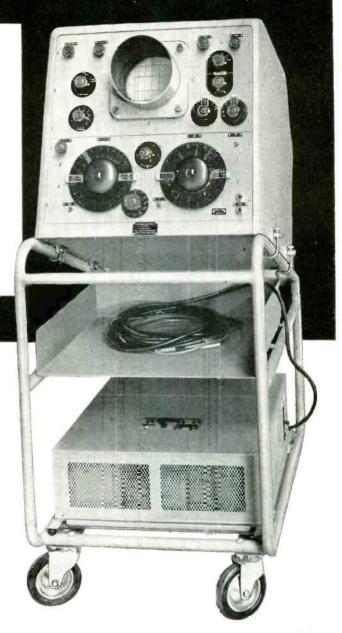
Amplitude Measurement Range: 0 to -30 db and -30 to -60 db relative

to reference signal.

IF Bandwidths: 6, 30, and 150 cps.

CRT: 6-inch diameter with long-persistence phosphor.





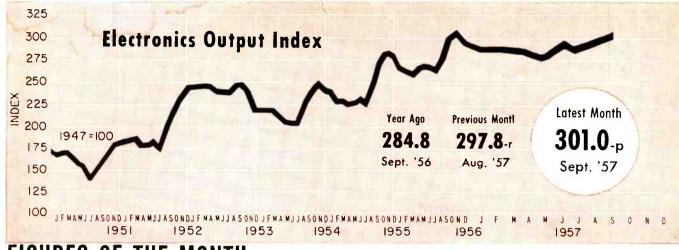
Designed and developed by communication engineers of the British General Post Office for use at their HF point-to-point transmitter stations, the OA 1094 is manufactured by Marconi Instruments under GPO authority.

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FIGURES OF THE MONTH

	Latest Month	Previous Month	Year Ago		Latest Month	Previous Month	Yea Ago
RECEIVER PRODUCT	TION		.3-	BROADCAST STATION		141011111	/ tgc
(Source: RETMÁ)	Sept. '57	Aug. '57	Sept. '56	(Source: FCC)	Aug. '57	July '57	Aug. '56
Television sets, total		673.734	894,211	TV stations on air	528	522	50°
With UHF	87,040	88,615	96,785	TV stations CPs—not on air	133	132	11
Color sets	nr	nr	nr	TV stations - new requests	77	78	4
Radio sets, total		965,724	1,319,189	A-M stations on air	3,113	3,095	2,93
Auto sets	446,419	301,971	349,790	A-M stations CPs—not on air	148	155	11
				A-M stations — new requests	340	340	26
				F-M stations on air	532	531	52
DECENTED CALES				F-M stations CPs-not on air	30	31	2
RECEIVER SALES				F-M stations—new requests	37	25	
(Source: RETMA) Television sets, units	Sept. '57 705,247	_		COMMUNICATION AL	JTHORIZA	TIONS	
Radio sets (except auto)		510,097 710,553	763,908	(Source: FCC)	Aug. '57	July '57	Aug. '56
Radio sees rexcept auto	875,500	710,555	756,345	Aeronautical	54.138	51,463	50.64
				Marine	65,226	64,067	58,43
DECENANC TUDE O				Police, fire, etc	23,710	23,550	21,15
RECEIVING TUBE S	ALES			Industrial	36,837	36,261	31,14
(Source: RETMA)	Sept. '57	Aug. '57	Sept. '56	Land transportation	9,708	9,652	9,14
Receiv. tubes, total units	44.382.000	43.029.000	44,432,000	A <mark>mate</mark> ur	165,860	163,994	150,56
Receiv. tubes, value		\$34,886,000	\$35,093,000	Citizens radio	29,892	28,864	19,99
Picture tubes, total units	1,071,662	930,296	1,267,045	Disaster	347	347	330
Picture tubes, value	\$20,819,036	\$17,984,185	\$21,709,064	Experimental	806 2,921	797 2,856	730 2,412
				EMPLOYMENT AND P	AYROLLS		
		-Quarterly Fig		(Source: Bur, Labor Statistics)	Aug. '57	July '57	Aug / E 4
INDUSTRIAL	Latest	Previous	Year		_		Aug. '56
TUBE SAL ES	Quarter	Quarter	Ago	Prod. workers, comm. equip.	409,800-р	393,700-r	392,300
(Source: NEMA)	2nd '57	1st '57	2nd '56	Av. wkły. earnings, comm Av. wkły. earnings, radio	\$77.81 -p \$75.81 -p	\$75.85 -r \$75.24 -r	\$75.76 \$73.75
Vacuum	\$10,191,621	\$11,224,707	\$7,680,250	Av. wkly. hours, comm	39.9 -p	375.24 -r 39.1 -r	40.3
Gas or vapor	\$2,758,630	\$3,332,357	\$2,983,488	Av. wkly. hours, radio	39.9 -p	39.6 -r	40.3
modulation tubes	\$17,177,922	\$15,359,108	\$16,254,025	SEMICONDUCTOR SAL	ES ESTIM	ATES	
Gaps and T/R boxes	\$1,589,670	\$1,409,463	\$1,238,469				
				Transistors, Units	Sept. '57 3,231,000	Aug. '57 2,709,000	Sept. '56 1,115,000
MILITARY PROCUR	EMENT				-,,000	-,,0,,000	_/225,500
Source: Defense Dept.)		4th '56	1st '56	STOCK PRICE AVERAGE	ES		
Army		\$56,185,000	\$40,490,000	(Source: Standard and Poor's)	Sept. '57	Aug. '57	Sept. '56
Vavy		\$34,210,000	\$28,700,000	Radio-tv & electronics	46.57	47.28	55.44
Air Force			\$124,828,000	Radio broadcasters	58.39	60.63	69.83
Total-Electronics			\$194,018,000		revised	nr-not report	

FIGURES OF THE YEAR

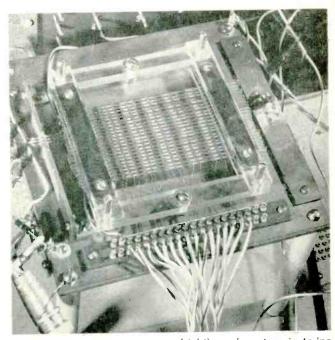
Television set production Radio set production Television set sales Radio set sales (except auto) Receiving tube sales Cathode-ray tube sales

TOTALS FOR	FIRST NINE MONTHS 1956 Percent Change	1956 Total
4,589,164	5,259,271 —12.7	7,357,029
10,3 <mark>7</mark> 6,3 <u>54</u>	9,535,896 + 8.8	13,981,800
4,452,081	4,603,626 - 3.2	6,804,756
5,840,372	5,405,052 + 8.0	8,332,077
341,663, <mark>00</mark> 0	347,43 <mark>6</mark> ,000 — 1.7	464,186,000
7,308,552	8,087,352 — 9.6	10,987,021

INDUSTRY REPORT

electronics-December 1 • 1957





CHECKING memory characteristics (left) and setting up an experimental magnetic memory array (right) are key steps in trying

Crossed Wires: New Concept In Memory Devices

Foresee systems simpler to fabricate and more economical to manufacture

Word of a new concept in memory devices is spreading quickly throughout industry this week.

It is claimed the concept will make possible memory systems which are simpler to fabricate and more economical to make than existing systems.

The concept has been named the "Twistor". It has emerged from exploratory work by A. H. Bobeck at Bell Telephone Laboratories.

► Applications—The firm claims

such devices may have extensive applications in computers and electronic switching systems where rapid-access, high capacity memories are necessary.

The concept, says Bell, opens the way for the construction of magnetic memory arrays by merely interweaving horizontal copper wires and vertical magnetic wires—much as window screen is woven. Such a device would be similar in appearance to a ferrite core array, but without the cores, and would operate in much the same way as a core array.

A characteristic of wire made

of magnetic material gives the "Twistor" name to the new concept. Torsion applied to such a wire shifts the preferred direction of magnetization from a longitudinal to a helical path.

▶ Possibilities—Thus, the coincidence of a circular and a longitudinal magnetic field can then be used to insert information into this wire in the form of a polarized helical magnetization, and the magnetic wire itself can be used as a sensing means.

Investigations are now underway to determine optimum size and composition for the magnetic wires. It appears that a conductor

plated with magnetic material may have some advantages.

Diameters as small as onethousandth of an inch appear to be feasible. At least 10 bits per inch may be stored on such a wire without adverse interaction.

► Advantages — In conventional magnetic core memory devices, conductors must be threaded through the cores to make up a suitable matrix. When a ferrite sheet is employed, either a threading or a plating operation is necessary to suitably locate the conductors.

However, with the "Twistor," says the firm, the ferrite material is completely eliminated and no threading or plating is necessary. Speed of operation and output of the "Twistor" are said to be comparable to ferrite memory systems.

Present indications are that the drive circuits for a "Twistor" array can be readily transistorized. Thus, the company claims, a memory system using the new concept will retain all of the advantages of ferrite core or sheet systems, and will be much simpler and more economical to manufacture.

Military Uses More Civil Radar

Armed forces constitute expanding market for slightly modified gear

More commercial radar equipment is finding its way, with only slight modifications, into military applications these days.

Latest move of this kind involves Raytheon's small-boat, search radar, "Mariners Pathfinder 1,500," that will be installed on 133 Navy light personnel and vehicle surface craft (LCPL's and LCV's). The gear is designated AN/SPS-35. First deliveries are scheduled to begin this month. Total contract amounts to \$548,700.

▶ Refinements — First marketed commercially in 1955, the civilian Pathfinder is now aboard more than 1,000 smaller vessels.

The military version has two added refinements. A variable range marker and counter has been added which tells the user the target's exact distance. On the commercial model, the distance must be visually estimated between range rings. Possible range scales on the 10-in scope are 1, 2, 4, 8, 16 and 32 miles. Second addition is a true north indicator. Commercial model offers only relative bearing.

Navy plans to install the radar in only a percentage of its landing craft. During an invasion



Modified civilian search radar will provide Navy with low-cost all-weather guidance for small amphibious craft

landing, radar-equipped squad leaders can check not only their own positions, but can monitor the other craft as well.

▶ Performance — The equipment can detect an 18-in buoy as close as 50 yards. Land can be picked up as far away as 32 miles. Power requirements are low, using only the craft's regular batteries. To make replacement parts more available, common radio and tv tubes have been used.

Two other civilian radars now adapted for military use are RCA's 50-mile-range weather avoidance radar now available to USAF planes as the AN/APS-69 (ELECTRONICS, Sept. 20, 1957), and GPL's RADAN doppler navigation set, converted for USAF use and designated the AN/APN-102 (ELECTRONICS, Oct. 10, 1957).

Calls Components Key To Future Air Force

But officer says new designs, materials, techniques—not refinements—are top needs

NEW MATERIALS, new techniques and new design concepts are today's ranking needs in the field of high temperature electronic components.

It's now time to stop placing emphasis on refinements of existing technology. Such refinements will not be enough to meet future needs.

These views were expressed recently by Col. J. S. Lambert, Air Research and Development Center. He spoke at the third annual meeting of IRE's Professional Group on Electronic Devices in Washington, D. C.

"The key to the Air Force's future rests in the development of high temperature electronic components," Lambert said.

▶ Needs—But before it is possible to design the components needed, it is necessary to get more information on electrical and physical properties of materials now in use; then follow with new and better materials.

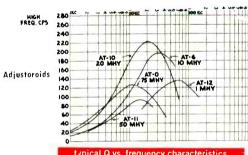
Lambert also thinks means of cooling, shielding and protecting electronic equipment from the more severe environmental conditions are only stop gaps. They will be followed by a number of high temperature components giving more flexibility in equipment design. He says there must be components available which are intrinsic to severe environments.

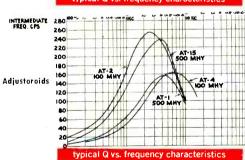
The highest temperature that commercial components in general are being designed to work in is 85 C. Air Force is attempting to hit 125 C; non-conventional applications may reach up to 500 C.

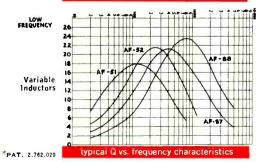
► Applications—For high temperature applications, AF reports that high temperature transistors will not be used. There will be electronic tubes, even though indium phosphide and gallium arsenide

(Continued on page 10)









The new subminiature **Burnell Adjustoroids®** utilizing an ingenious patented method of magnetic biasing cover a wide range of frequencies, occupy less space and are available at low cost.

New **Burnell Adjustoroids** possess in addition to all the outstanding characteristics of non-adjustable toroids:

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Hermetic sealing to meet Government MIL E # 15305-A specifications.

If your adjustoroid needs can't be met from our stock catalogue, we'll be glad to manufacture to your specifications.

Len	gth/ Dia.	Width	n Hgt.	Wt. I	Jseful Freq. Range	Max Q	Max L in hys
AT-0	11/16		1"	2 oz	1 kc to 20 kc	10 kc	3 hys
AT-1	13/4	13/4	11/4"	71/4 oz	2 kg to 10 kc	4 kc	15 hys
AT-2	23/4	23/4	21/4"	24 oz	Below 2.5 kc	2.5 kc	125 hys
AT-4	11%4		11/4"	4 oz	1 kc to 16 kc	6 kc	15 hys
AT-6	11/16		1"	2 oz	10 kc to 100 kc	30 kc	.75 hys
AT-10	11%4		11/4"	4 oz	3 kc to 50 kc	20 kc	.75 hys
AT-11	45/64	45/64	3/4"	.83 oz	2 kc to 25 kc	15 kc	5 hys
AT-12	45/64	45/64	3/4"	.83 oz	15 kc to 150 kc	60 kc	.5 hys
AT-15	131/12		17/8"	14 oz	Below 5 kc	4 kc	125 hys
AF-51	11%4		2"	5 oz	30 cps to 500 cps	120 cps	1'000 hys
AF-52	11%4		2"	5 oz	50 cps to 1 kc	250 eps	1000 hys
AF-87	45/64	45/64	11/4"	1.7 oz	90 cps to 2 kc	400 cps	80 hys
AF-88	45/64	45/64	11/4"	1.7 oz	1.6 kc to 4 kc	800 cps	42 hys



EASTERN DIVISION 10 PELHAM PARKWAY PELHAM MANOR, N. Y. PELHAM 8-5000 TELETYPE: PELHAM 3633



PACIFIC DIVISION 720 MISSION STREET SOUTH PASADENA, CALIFORNIA RYAN 1-2841 TELETYPE: PASACAL 7578 are among those showing great promise as possible materials for high temperature semiconductor devices.

Meantime, the ceramic tube is being adopted. In cases of the smaller ceramic tubes, the AF thinks that operation at 300 C could be maintained for reasonably long periods. Printed circuits probably will be used to assemble components for high temperature applications.

Custom Tubes Produce Unexpected Markets

ELECTRONICS survey shows today's unique tube may be common item of tomorrow

INCREASING demands of an expanding electronics industry today generate a need for new special-characteristic vacuum tubes. Yet tubes developed for a single highly-specific purpose often find or help create many other applications. A spot check of tube manufacturers reveals that many of today's custom-made tubes may be the common shelf-replacements of tomorrow.

- ► Forerunner Made-to-order to meet given specifications or to satisfy specific circuit requirements, the custom tube occasionally sires a new tube line. A few years ago Tung-Sol Electric was asked to develop a tube to operate off the 12-volt supply in a hybrid automotive radio. In response they designed and produced 1,000 12K5 tetrode class A amplifiers. By 1956 sales of the 12K5 blossomed beyond 1,000,000. Concurrently, Tung-Sol came up with a whole line of hybrid radio tubes whose sales last year reached 4,000,000. Of the 21 hybrid radio tubes currently registered with EIA, 12 were Tung-Sol designed.
- ► Obstacles Cost of retooling, limited volumes, prospective saleability and future applications are some factors the tube manufac-

Business Briefs

- ► Harris-Intertype purchases all stock of Gates Radio of Quincy, Ill., for cash. Amount of purchase was not disclosed. Gates produces commercial broadcasting equipment. Harris makes equipment and supplies for the printing industry. Acquisition of Gates provides an operating basis for broader development in electronics, comments the purchaser.
- ▶ Electronic Specialty Co. of Los Angeles acquires the Cado division of Electromation, Inc., Santa Monica, Calif. Cash plus stock were given in payment, but amounts were not revealed. Cado's patented lobing switch and subminiature coaxial switch were prime attractions for the purchaser. The purchased division will become part of Electronic Specialty's Radiating Systems Division.
- ▶ Payson & Trask, New York venture capital firm, makes investment in Photomechanisms, Inc., Huntington, N. Y. Photomechanisms specializes in photographic instrumentation. Its subsidiary, F. B. MacLaren and Co., designs and manufactures electronics for servomechanisms, subsystems and servo systems.
- ▶ Cubic Corp., San Diego, Calif., takes over assets of Digital, Inc., another small San Diego electronics firm. Purchase terms were not disclosed. Cubic develops and produces missile ranging and tracking systems. The acquisition is a step in planned expansion of Cubic's commercial activities.
- ▶ KDI, Rochester, N. Y., acquires precision products division of Gruen Industries of Cincinnati through cash purchase. Amount was not disclosed. Acquired Gruen division will be known as the Precision Products Co. of Cincinnati, a division of KDI. The division will remain under Paul Robert, former Gruen division manager. KDI manufactures automation equipment.

turer considers before accepting custom tube orders. But no single consideration is decisive.

While concerned with the size of initial order and necessary retooling, Sylvania reports it may undertake custom-tube work as an obligation to a good customer. Tung-Sol is not too concerned about quantity as developmental costs are usually absorbed in the first order.

In developing custom tubes, United Electronic in Newark prefers small orders, perhaps not exceeding ten tubes. With this small quantity, the firm can easily make modifications and improvements at the customer's request after observing initial performance. Quantity production and EIA registration may follow when marketing outlook is promising.

Among the 40 tubes specially developed by United, only a few of which are EIA registered, are high-vacuum rectifiers, clipper diodes, and special triodes designed for radar applications.

► Stages—The transient nature of the custom tube designation is illustrated by the varying stages of

(Continued on page 12)

SOLID-ELECTROLYTE TANTALEX CAPACITORS

new dimensions in

miniaturization and reliability

This solid-electrolyte Tantalex Capacitor (shown $1\frac{1}{2}$ times actual size) is rated at 4.7 μ F, 10 volts d-c, and is only $\frac{1}{8}$ in diameter by $\frac{1}{4}$ long.

Now, circuit designers in computers and military electronics have an electrolytic capacitor that offers greater miniaturization than ever before . . . with no sacrifice in reliability. Sprague's recently announced solid-electrolyte Tantalex Capacitors find ideal application in the transistor circuits of these critical fields.

The tiny sintered tantalum anode of Type 150D Tantalex Capacitor is impregnated with a solid, non-corrosive, semi-conductor material which cannot leak under any circumstance. It combines true miniaturization with electrical stability previously unobtainable in an electrolytic capacitor of any type.

Thermal coefficient of these capacitors is sufficiently low and linear so that for the first time a circuit designer can think of an electrolytic in terms of parts per million capacitance change. Nominal value is +500 ppm/°C. The

capacitor may be used without derating over a range from +85°C to as low as -80°C, a temperature at which no other electrolytic has proved useful.

Solid construction permits the Type 150D to withstand the severe shock and vibration encountered in missile and ballistic applications. Hermetic sealing makes it completely immune to humid atmospheric conditions.

Complete performance data covering the wide range of sizes and ratings are in Engineering Bulletin 3520B, available on letterhead request to the Technical Literature Section, Sprague Electric Company, 35 Marshall Street, North Adams, Mass.

* * *

Sprague, on request, will provide you with complete application engineering service in the use of Tantalex Capacitors.



SPRAGUE COMPONENTS:

CAPACITORS • RESISTORS • MAGNETIC COMPONENTS • TRANSISTORS • INTERFERENCE FILTERS • HIGH TEMPERATURE MAGNET WIRE • PULSE NETWORKS • PRINTED CIRCUITS

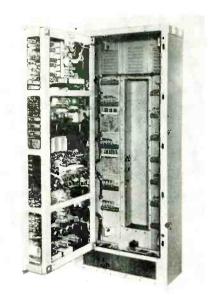
development of several United tubes. Their 542 rectifier, with 30 kv peak inverse rating and 100 ma average current, has recently been developed but is not yet in production. Clipper-diode 546, developed for high-power radar applications, has been made in only small quantities. Both of these tubes are still in the custom stage.

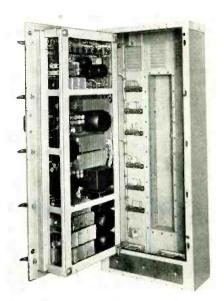
The small external anode diode 545 with a 5 kv peak inverse rating was specially made for power-supply use. Designed for immersion in oil for full ratings, the tube is now used as an air-cooled rectifier by customers other than its original purchaser. Although not EIA registered, it is being produced by the thousands and passing out of the custom stage.

Developed for fire control systems the clipper-diode 583 has left the custom stage and is produced by several companies.

► Modifications — Custom tubes often evolve through modification of existing tube types to satisfy special applications. For example, the request for a small 2C253 high-mu triode for a flightsimulation application led General Electronic of Patterson to make tube changes. The tube normally handles 1.5 ma plate current and has a transconductance of 750 to 1,000 micromhos. Since only a few microamps were desired, tube operation was near the knee of the plate characteristic and the gm was reduced to 250-300. The desire for a 2C253 with smaller-thanrated plate current necessitated tube redesign and eventual tube redesignation.

On the borderline of the custom tube designation are the many modified, long-life and ruggedized versions of existing vacuum tubes. Tube manufacturers often specially treat tubes to withstand shock and vibration and to extend tube life. Ericsson, the Swedish tube makers, use gold-plated tungsten wire in control grids to reduce secondary emission and guarantee longer life. And they gold plate tube pins to provide better high frequency performance. United uses a bonded thorea filament on some tubes to provide longer life.





DESIGN PLANNING of new components with easily removed plug-in modules and built-in spares (left), and systems with good terminal board accessibility (right) is one way industry is meeting the challenge to retain a high-maintainability level of modern electronics as . . .

Meeting Airs Upkeep Problems

Industry, military leaders discuss maintenance issue in California this month

ONE OF THE SERIOUS problems confronting the military today is the efficient maintenance of sophisticated electronics equipment. The development of high-performance weapons requires top-flight maintainability. And the more complex the equipment, the more qualified the maintainence man must be. Although we have made remarkable advances in the development of equipment, it can be generally said that maintenance-skill levels have decreased. This problem places a heavy burden upon efficiency of the armed forces.

► The Letter—Last March, General C. S. Levine of the Air Force wrote to Dr. R. G. Baker of Electronic Industries Association. He requested that the electronics industry be alerted to support a program devoted to provide design-for-maintenance in future equipment that would alleviate the maintenance burden. He felt confident that industry would meet this latest challenge. He said that in no other way can we invest so

little and gain so much in effectiveness for the Air Force.

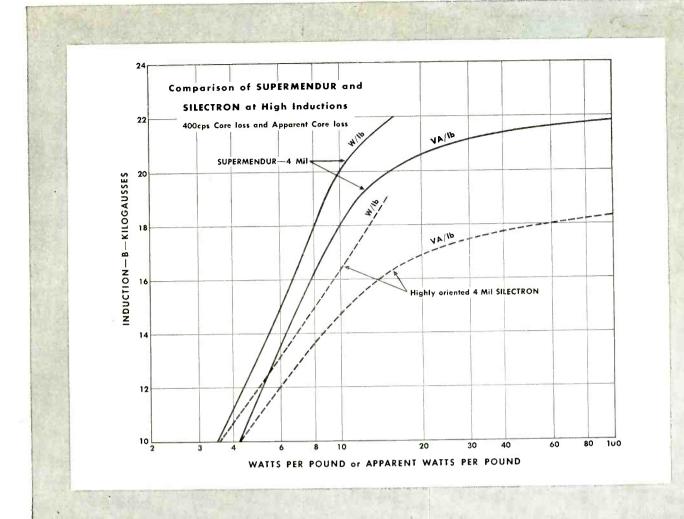
▶ The Conference—The General's letter was one of the major reasons for considering the EIA Conference On Maintainability Of Electronic Equipment which is being held at the University of Southern California this month (18th and 19th). The General's problem is not unique to the Air Force, but applies to the other services as well as to our whole economy.

The conference provides an exchange of ideas in problem areas. Projected solutions will be advanced by both the military and private industry.

Technical sessions and panel discussions are planned to avoid academic and theoretical papers. The conference is confined to practical or applied papers. Plans are laid for conducting essentially identical sessions on the East Coast next spring.

► Techniques—Papers will be presented on advanced maintenance techniques for missiles, digital computers and radar, where search, fire control, aerodynamic navigation and warmens delivery

(Continued on page 14)



Announcing

SUPERMENDUR

A New Rectangular-Loop Core Material

For Miniaturized Transformers and Magnetic Amplifiers

Supermendur, an oriented cobalt-iron-vanadium alloy, combines the high saturation flux density of the cobalt-iron alloys with the desired hysteresis loop rectangularity of the oriented 50% nickel-irons. This gives it unique characteristics in the range of inductions from 16 to 22 kilogausses which permit miniaturization and weight reduction for toroidal transformers and magnetic amplifiers.

Coercive forces substantially lower than those of previously available cobalt-iron alloys are obtained. In the graph above, the lower core losses and excitation obtained with Supermendur show a decided improvement in high density characteristics compared with oriented silicon steel.

Supermendur can be processed in tape form to thicknesses

of 2 mils or less. Maximum utilization of its hysteresis loop rectangularity and high permeability at high induction requires a gapless or wound core type of construction particularly suited to thin tape.

Specific advantages of Supermendur cores in toroidal transformers are: high operating induction, low core loss, low exciting current and high permeability at high induction. In magnetic amplifiers or saturable reactors, they include: rectangular hysteresis loop, high saturation induction and moderate excitation at high induction. Advantages in all uses are: thin tape, small size and low weight.

Supermendur is manufactured under license arrangement with the Western Electric Company. • Call on us for more information or engineering assistance.

WSW 6921

Technical Information and Samples

Requests for sample toroidal cores of Supermendur in 4 and 2 mil thicknesses will be processed as rapidly as possible. Technical data will be released as it becomes available. When writing, state application, frequency, size, gage, characteristics desired and quantity required.

ADDRESS DEPT. E-712

THE ARNOLD ENGINEERING COMPANY



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are all integrated. Complete consideration will be given to the ease and speed with which maintenance can be accomplished. Offered will be design techniques which will lead to convenient and rapid methods of locating faults and ease of replacement of components.

Cabinet designs, shown in the photographs, are presented as examples of RCA design techniques by R. M. Jacobs and B. F. Rogers. Those not attending the conference may get copies of the complete proceedings from Engineering Publishers, GPO Box 1151, New York 1.

Uses of Transistor Limited in Radio-Tv

Cost, though dropping, still makes vacuum tube choice of home-instrument designers

THE TRANSISTOR may have solved many problems for the industrial electronics designer, but the cost-conscious home-instruments man must think twice before specifying it. Engineers in this field agree today that for them the vacuum tube is hardly beginning to show signs of obsolescence.

- ► Cheaper Transistors—Prices of semiconductor components steadily dropping as production and sales rise, but they cannot yet compete dollar-wise with the tube. They are therefore used only where other advantages over tubes take precedence. Where space is a problem, or low hum, noise or freedom from microphonics is important, the transistor is frequently used. It is also employed in some instances where resistance to shock is a factor, or small low-voltage power supplies are essential.
- ► Varied Utilization—Thus in the 1958 tv receiver, where size is determined by the picture tube, the

Military Electronics

► Anti-submarine rocket called ASROC, that can be launched from a ship a comfortable 200 miles from its target, is now being developed by Minneapolis-Honeywell for BuOrd. Described as a torpedo with a rocket, the weapon is aimed for the vicinity of the target and released. Once in the target area, the torpedo is turned loose from the rocket and seeks out the enemy sub or ship by means of "a searching device"—probably infrared.

ASROC, without the rocket, can be launched from an aircraft. Maximum range is probably shorter but ASROC's operation, once it hits the water, is basically the same.

Librascope is making the fire-control system. Launching system responsibility belongs to Universal Match. Payload will be produced by GE, turned over to BuOrd who will issue it in turn to prime contractor Minneapolis-Honeywell.

- ► Wagtail, air-to-ground, electronically guided rocket, is said to be using a "new type guidance method." Series of development contracts held by Minneapolis-Honeywell with the Air Force Armament Center, Elgin AFB, Fla., has gone considerably beyond the \$\frac{1}{2}\$ million mark announced earlier.
- ▶ New digital computer for military aircraft has been developed by Ramo-Wooldridge under contract with Westinghouse. Completely transistorized, the new RW-30 performs computations for navigation, fire control, bombing and weapons control. Complete computer has a volume of 4.19 cu ft and weighs 203 lbs. Subminiaturized packaging techniques and silicon semiconductor circuitry are used throughout. It can conduct 4,000 complete arithmetic operations per second, including access time, and requires 400 watts of power.

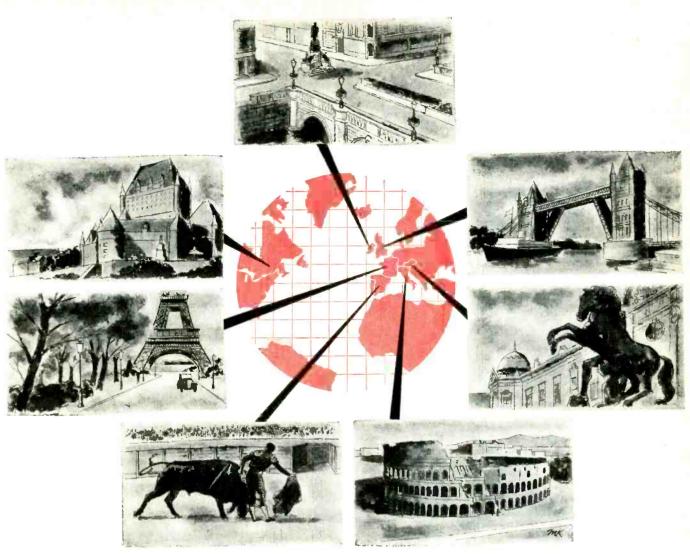
transistor is almost nowhere to be seen. In home and auto radios and hi-fi sets, transistor uses are increasing slowly. But in the portable radio field the transistor really comes into its own, and there is used almost exclusively.

► Smaller TV—The trend in tv picture tubes is toward exclusive use of the 110-degree deflection type, which permits shorter tubes and consequently shallower cabinets. Most circuit improvements for the year have concentrated in this area, while one manufacturer has gone to the extreme in packaging,

with a tube face that extends out from the front of the cabinet, which is only 10 inches deep. Advantage claimed is the mounting of speakers on the front of the cabinet very close to the picture screen.

► Radio Growing—Radio sets of all types continue on the upswing, with most large production lines having reached the optimum in automation. Circuitry remains for the most part conventional, although research continues on the reflex and other cost-cutting cir-

(Continued on page 16)



Here, too, we make Nichrome*

Perhaps you didn't know that the world-famous alloy Nichrome is produced not only in The United States, but also in 6 Driver-Harris plants in England, Ireland, France, Italy, Austria, Spain, and in Canada by The B. Greening Wire Company. Also, Nichrome is a registered trade-mark in 55 nations.

At first, fifty-odd years ago, we manufactured electrical resistance alloys for furnace elements and domestic heating appliances only. Today we produce 132 different high nickel alloys in many different forms and in hundreds of sizes, for almost every kind of domestic and industrial application—of which Nichrome is the most illustrious.

Whenever you buy Nichrome, you are assured of the unsurpassed and unvarying quality which has made Nichrome the supreme world standard for electrical-resistance and heat-

resistant alloys. This uniformly high quality, which we jealously guard as our most priceless possession, results from the technical excellence, the productive skill, and the quality controls the Driver-Harris craftsmen have gained in over 50 years of experience—and which are maintained with equal rigor in all Driver-Harris plants here and abroad. The result is a continuous benefit to the entire electrical, electronic, and heat-treating industries.

*I.M. Reg. U. S. Pat. Off.



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MAKERS OF THE MOST COMPLETE LINE OF ALLOYS FOR THE ELECTRICAL, ELECTRONIC, AND HEAT-TREATING INDUSTRIES

cuit trickery. Seasoned designers, however, feel that this is just the history of early radio repeating itself, and that as transistor prices continue to fall this type of development will fall by the way-side.

► More Hi-fi—Most major companies are taking a deep plunge into hi-fi, for the first time this season. While leaving the components field to the specialized small operators who pioneered it, big-company concentration is strictly on packaged merchandise for the home. Innovations this year include much emphasis on tape recorders, stereo and extension speakers.

► Auto Mobile-Portable—Biggest news in auto radios this year is the pull-out system which doubles as a portable. Fully transistorized, the unit uses the 12-volt car battery in mobile service, but only 6 volts from a group of heavyduty penlite cells as a portable. A standard built-in miniature speaker is used in the portable, but a 6x9 oval automatically cuts in for auto use.

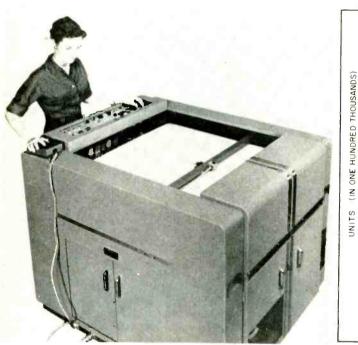
An additional power transistor is used to drive the car speaker, making the system a 9-transistor portable and 10-transistor mobile set. Separate antennas are also used for the two types of service. No vibrator is used, and this appears typical of a trend. Other

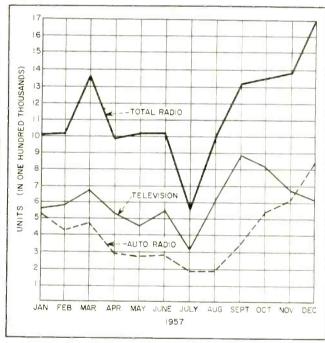
systems are now often hybrid, using tubes in low-power stages and transistors in the output, thus obviating the need for voltage step-up through the vibrator and vastly simplifying the power supply.

Battery-Operated Tv

Swiss railway officials recently saw demonstrations of a battery-operated industrial tv system developed by Britain's Pye Ltd.

The portable equipment operated off two 12-volt car batteries in series to show rail alignment to engineers watching a receiver inside a moving train.





COMPETENT secretary with half a day of special training operates push button controls (left) to generate production report (right)

Board Automatically Plots Business Trends

Integrator and memory also convert statistical information into easy-to-read bar charts

USERS of data processing equipment can now concurrently generate a continuous graphical presentation of digital information.

Digital-to-graphical conversion

medium, available for the first time, is the Dataplotter developed by Electronic Associates. It was recently demonstrated at the National Business Show in New York.

Information is fed into the plotter by punched cards, punched paper tape, magnetic tape, or a manually operated key-

board. An electronic memory device stores the initial input point until the next point is received. A special integrating circuit produces a signal which causes the recording pen to draw a continuous line between the two points on coordinate paper. This process

(Continued on page 20)

Laboratory Accuracy Production-Line Speed



Type 1605-A Impedance Comparator

No manual balancing. Phase-angle and impedance-magnitude differences between the unknown and a standard impedance are read directly from two meters.

An impedance bridge for dynamic measurement of impedance changes caused by varying environmental conditions.

Can be readily incorporated into automatic-sorting equipment.

Wide Range of Internal-Test Frequencies 100, 1000, 10,000 and 100,000 cps.

Impedance Range

Resistance: 2 ohms to 20 megohms Capacitance: 40 µµf to 500 µf Inductance: 20 μ h to 10,000 μ h

Direct-Reading Meter Ranges

Impedance-Magnitude Differences: C.3%, 1%, 3%, and 10% of full scale. Phase-Angle Differences: .003, .01, .03, 0.1 radians full scale.

Over-All Accuracy

3% of full scale (.01% over-all accuracy on 0.3% impedance magnitude range).

\$790

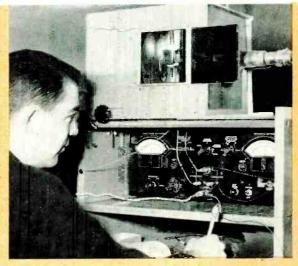
manufacturers of vitreous enamel dielectric capacitors, have taken full advantage of the Impedance

Comparator's versatility:

The Impedance Comparator's ability to perform dynamic measurements without instrument readjustments allows considerable convenience in development. Capacitors, placed in a test cabinet containing a heating lamp and reflector, are measured for changes in dissipation factor and capacitance with temperature. The continuous measuring feature of the bridge eliminates any need for thermostatic heat control; the operator simply records thermocouple temperature and Comparator readings to obtain an accurate plot of conditions.

A statistical sampling of capacitors from each production lot is subjected to accelerated life tests at 130°C and 150% of rated voltage for 250 hours. These life-test measurements for dissipation factor and capacitance give information as to dielectric quality. Pre-production samples are also measured to determine mean and extreme capacity values so that the distribution of each production lot is known. Accurate data from the Impedance Comparator make effective production control at "VITRAMON" a certainty.





A G-R Type 722 Precision Capacitor, converted for guarded operation, is used as a standard. Easy and rapid testing provided by the "No-Knob" balancing feature of the Impedance Comparator permits "VITRAMON" to perform a 100 per cent check of production lots without significant increases in labor costs.



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RAYTHEON SILICON and GERMANIUM

The types pictured and charted on these pages possess the characteristics and the dependability to merit your specification and your confidence.

	DUN	DED SIL	LUN DI	DDE2	
Туре	Peak Inverse Volts	Forward Current (min.) at + IV mAdc	Average Rectified Current mAdc (25°C)	Reve Curr µA	
1N300	15	15	65	0.001	10
1 N300A	15	30	80	0.001	10
1N432	40	10	55	0.005	10
1N432A	40	20	70	0.005	10
1 N301	70	5	45	0.05	50
1N301A	70	18	65	0.05	50
1 N460	90	5	45	0.1	75
1N460A	90	15	60	0.1	75
1N303	125	3	40	0.1	100
1 N303 A	125	12	55	0.1	100
1N433	145	3	40	0.1	125
1 N433A	145	10	50	0.1	125
1N434	180	2	35	0.1	150
1N434A	180	7	45	0.1	150
1 N302	225	1	30	0.2	200
1N302A	225	5	40	0.2	200
CK863	300	12	20	0.3	275
CK863A	300	3	30	0.3	275

GOLD BONDED GERMANIUM DIODES

D	Туре	Peak Inverse Volts	Average Rectified Current (max.) mAdc	Consect at - 10V
	1 N305	60	125	2
	1N306	15	150	2
8	1N307	125	50	5

CENERAL PHRPOSE GERMANIUM DIODES

	OLD THE REAL	- 1 0 1111 0	OL GENTINA	114 0 114 0	TOPLO	
E	Туре	Peak Inverse Volts	Average Rectified Current (max.) mAdo	Reverse Current μΑ at V		
	1N66	60	50	800	-50	
ш	1N67	80	35	50	-50	
3	1 N68	100	35	625	— <u>1</u> 00	
	1 N294	60	50	800	-50	
	1N297	80	35	100	-50	
	1N298	70	50	250	-40	
	VHF and U	HF		1		
	1N295	40	35	200	100	
	CK715	40	35			

	0		Ottall HEOTH	1 ba 110		
C	Туре	Peak Inverse Volts	Average Rectified Current Amps. (125°C*)	Reverse Current (max.) at FIV mAdc		
	CK774	25	5	5		
	CK775	60	5	5		
	CK775-1	125	5	5		
8	CK776	200	5	5		
	CK777	325	5	5		

Case Temperature













ACTUAL SIZE

YOUR DESIGN IS BETTER YOUR PRODUCT PERFORMS BETTER

when you use RAYTHEON SEMICONDUCTORS

DIODES and RECTIFIERS



DIFFUSED JUNCTION SILICON RECTIFIERS

A			STUD	TYPE				В	WIRE	-IN TYPE	SOLD COMPANY
Туре	Peak Inverse Volts	Average Rectified Current Amps. (150°C)	Reverse Current (max.) at PIV µA	Туре	Pea∺ Inverse Volts	Average Rectified Current Amps. (135°C)	Reverse Current (max.) at PIV µA	Туре	Peak Inverse Volts	Average Rectified Current Amps. (150°C)	Reverse Current (max.) at PIV µA
CK846 CK847 CK848 CK849 CK850 CK851	100 200 300 400 500 600	1.0 1.0 1.0 1.0 1.0 1.0	2 2 2 2 2 2 2	1N253 1N254 1N255 1N256	95 190 380 570	1.0 0.4 0.4 0.2	10 10 10 20	1N537 1N538 1N539 1N540 CK844 CK845	100 200 300 400 500 600	0.25 0.25 0.25 0.25 0.25 0.25	2 2 2 2 2 2



SEMICONDUCTOR DIVISION

Silicon and Germanium Diodes and Transistors • Silicon Rectifiers

Newton, Mass.: 55 Chapel St., Blgelow 4-7500 New York: 589 Fifth Ave., Plaza 9-3900 Chicago: 9501 Grand Ave., Franklin Park, TUxedo 9-5400 Los Angeles: 5236 Santa Monica Blvd., NOrmandy 5-4221 takes 1% seconds and is repeated for each incoming point.

It is felt the Dataplotter will enable non-mathematically trained people to interpret the flood of facts and figures turned out by high speed electronic computers and data processing equipment. Also, hard pressed management personnel can reduce reports, studies, profit and loss statements, break-even figures, or forecasts, into comprehensive graphs much faster and cheaper than at present

- ▶ Physical makeup—Except for the memory and integrating circuits, this plotter contains the same components and functions found in EA's Variplotter. Since it was designed with compatibility in mind, the Dataplotter can be used without modification by companies having IBM or similar output equipment.
- ► Accuracy—Plotter is accurate to

within 0.015 thousandths of an inch over a 30-inch pen translation. Drawings can be made on postage-stamp size paper or 30-by-30-inch sheets. Vacuum plate holder prevents paper from wrinkling.

- ► Versatility—It is possible to extend plots at future dates by inserting original plus additional data. Pen will retrace over first plot and continue the graph. If point plotting is desired, twelve dots symbols are provided to identify input information. Twopen and four-pen carriages can be used to simultaneously plot as many as four related variables.
- ► Applications—First unit manufactured was purchased by Photonics of Columbus, Ohio to help plot lateral profiles of proposed new highways. Federal Reserve intends to use the device for preparing a greater number of charts for annual presentation to Con-

gress. Anticipated future markets include: brokerage houses for keeping constant visual records of stock trends in relationship to Dow-Jones averages; insurance companies for preparing actuarial graphs; chain stores for giving hour-by-hour plot of sales as against sales of previous day, week or year; factories for making daily plots of inventory, expense and payroll data; and topographical mapping for drawing accurate profiles of terrain features.

► Cost—Unit is currently selling for \$22,000 with 120-day delivery. Custom models for particular applications can be made for additional cost. By March, EA expects to be able to provide 30-day delivery. A transistorized version of the plotter is presently being designed. A demonstration unit is installed at the Princeton Computation Center at Princeton, New Jersey.

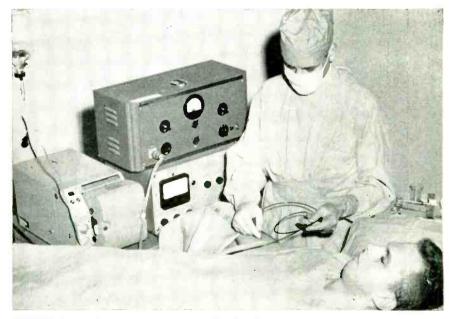
Manometer Checks Blood Pressure in Veins

Sturdy meter now permits measuring of blood flow to sick person's heart

RAPID ELECTRONIC developments have frequently facilitated advances in medical technology. Still another example of this is now provided by the recent disclosure that the Gauer pressure manometer for measuring blood pressure in the veins has been in effective use at the Veterans Administration Hospital in Durham, North Carolina.

While measurements of arterial pressure have been commonplace, means of measuring blood flow to the heart have only recently been found. The Gauer manometer, about 12 mm in length and 3 mm in diameter can easily be inserted into the vein and passed up into the chambers of the heart.

► Description — Blood pressure variations depress a small rubber-capped disk at the end of the



DOCTOR inserts tiny manometer into patient's vein

manometer. This compresses a tiny coil spring which displaces a piston. Soft iron, acting as the armature of a differntial transformer, is attached to the opposite end of the piston. As the piston position is varied through pressure altera-

(Continued on page 22)

NEW T/PLOTTER CUTS VIBRATION TEST TIME 50% to 75%

Automatically Plots Detailed Curves of Transmissibility

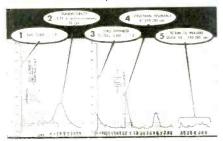


Immediate evaluation of system transmissibility is made possible by the new Barry-Insco T/Plotter which automatically draws a continuous curve of transmissibility. The T/Plotter eliminates data processing and conversion, and ends laborious point-by-point recording, calculating, and curve plotting. And because the recorded curve is continuous, there is no danger of missing significant peaks through arbitary choice of points in the plotted curve.

How it works

Vibration pickups on the shaketable and on the test specimen feed their a-c voltage outputs into identical amplifiers and rectifiers in separate channels of the T/Plotter. The instrument's servo system responds to the difference between the two voltages, which is a measure of transmissibility.

Fast scan over the entire frequency spectrum quickly shows resonance points, and slow scan provides detailed analysis of these resonances, (see curves below).

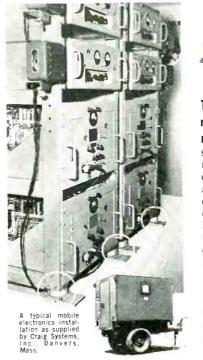


Measurement range

The T/Plotter can be set for full-scale ranges of 0.2, 1.0, 10, and 100. Any standard laboratory vibration pick-up can be used. Frequency range is from 5 to 4000 cps. Accuracy is $\pm 2\%$ above 2000 cps. Chart speed is variable from 6 to 960 inches per hour, in 16 steps.

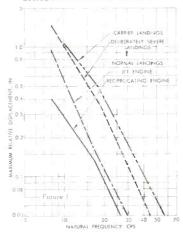
Released time for laboratory equipment and personnel, resulting from the faster and more accurate measurements possible with the T/Plotter, expands the capacity of present lab facilities — without adding space, shaketables, control or metering apparatus to existing equipment. Write for Bulletin 57-04 that tells how you can cut vibration-test time 50

How to design for RELIABILITY UNDER SHOCK and VIBRATION



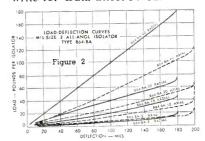
To protect electronic gear against road shock during travel over rough terrain, Barry Cup-mounts supporting equipment racks of mobile air-traffic-control units combine effective protection against high-impact shock with efficient isolation of vibration frequencies above 45 cps. This isolates the structural resonances of the vehicle, with no amplification of vibration from tires and springs. In other applications, these mounts protect against the high transients of gun-fire shock. Details of load ratings, sizes, and characteristics - with useful data on choosing Cup-mounts - are yours in Barry Product Bulletin 56-02, free on request.

LANDING-SHOCK CURVES





To protect sensitive electronic equipment in jet aircraft against landing shocks, while maintaining in-flight vibration isolation, mounts must be able to withstand the severe conditions indicated by the curves of Fig. 1, plotted from actual measured landing shocks. ALL-ANGL Barry Mounts, having natural frequencies above 25 cps, keep shock displacements within reasonable limits. Loaddeflection curves, for this family of isolators that give protection under high thrust loads applied in any direction, are shown in Fig. 2. For complete performance data on ALL-ANGL Barry Mounts, write for Data Sheet 57-02.







707 PLEASANT STREET, WA

WATERTOWN 72, MASSACHUSETTS

tions, the relative coupling of the transformer changes.

The transformer functions as one leg of a bridge circuit of a two-stage amplifier.

Physicians hope that with further use of the manometer many unanswered questions about heart failure and circulatory disorders can be answered.

Oil Industry Looks To Computers

Increased computer orders brighten prospects for petroleum progress

RAPID ADVANCES in computer technology are making better, faster and more efficient computers an actuality. Some industries which previously considered the cost of purchasing or renting high-speed computers and the training of personnel to be prohibitive are now turning to electronics.

In the oil industry alone a 45 percent increase in the number of computers now in use is predicted by a survey conducted by *Petroleum Week*, a McGraw-Hill publication. The replies from electronics' people of 37 leading oil companies indicate that 84 large and mediumsized computers are now in use and orders for 38 more units have been placed.

- ► Conversion—Electronic retooling is still in the early stages. But 19 companies, recognizing the need for an integrated electronic program, have installed formal committees at the policy level to develop and administer activity.
- ► Application—Present computer uses divide fairly evenly between accounting and scientific research, but electronics experts envision a greater emphasis upon scientific and operations research. Other applications include refinery operations and planning, refinery simulation and research and development.

All firms have made studies, costing from \$1,000 to \$500,000, into computer uses for oil.

FCC Actions

- ► Amends table of tv assignments, giving channel 13 to Fajardo, P. R., taking channel 12 from Charlotte Amalie, Virgin Islands, and assigning it to Aguadilla-Arecibo, P. R., in place of channel 13.
- ► Changes its rules so that cutoff date for consolidating and designating broadcast applications for hearing conforms to cutoff date for such applications granted without hearing.
- ► Grants permission to RCA Communications for point-to-point transmissions to and from Nicosia, Cyprus, both directly and through its relay station at Tangier.
- ► Assigns channel 12 to Mankato, Minn.; changes offset carrier requirement for that channel from even to minus in Brainerd, Minn., and from minus to plus in Ironwood, Mich.
- ▶ Proposes to delete channel 227 from Tacoma, Wash., substitute channel 284 for 279 in Olympia, Wash., and 289 for 284 in Centralia, Wash. Purpose is to add class A channel 280 to Tacoma.
- ► Denies request of Maryland & Virginia Milk Producers Association for control station of Special Industrial Radio Service in urban Washington, D. C.
- ▶ Provides for licensing of Land and Mobile Radiopositioning stations to operate speed measuring devices that use cw emissions at 2,455 and 10,525 Mc. Operation of such devices above 890 Mc continues on a developmental basis.
- ► Grants Western Union permission to increase message rates from Gibraltar and Malta to the U.S. and possessions, gives the telegraph company authority to reduce service at one station, discontinue 15 others.

► Financing—Most of the surveyed companies insist upon a projected economic payout for computers before placing orders.

Furthermore, 25 firms reported that they would probably continue to rent, rather than buy, large and medium-sized computers. Eight electronics' people were unsure about what company policy would be.

▶ Improvements—Among the computer characteristics desired by oil people are self-editing and common language features, unlimited storage and validity checking devices on all types of machines.

Transistors Slash Telemetering Costs

As systems grow larger, transistors reduce needs in power and repair

Transistorization of multichannel telemetering and control systems can save money in operation and maintenance, according to an investigation made by the Warren Manufacturing Co. In addition, weight is reduced by 75 percent (compared with tube systems) and

(Continued on page 24)

HIGH Output (1.0 v. RMS into 70 ohms) WIDE Range (2-220 Megacycles. All At Fundamental) and CONCTANT OUTDUT

(Fast Acting AGC)



SPECIFICATIONS

Range: Fundamental frequency 2 to 220 mc., continuously variable in 10 switched overlapping bands. Direct reading frequency dial

RF Output: 1.0 v. RMS into 70 ohms, metered. Flat within ±0.5 db over widest sweep and frequency band.

Sweep Width: Continuously variable to ± 30% of center frequency to maximum of at least 30mc.

Sweep Rate: Continuously variable 10 to 40 cps.; also locks at line frequency.

Attenuator: Switched 20, 20, 10, 6, and 3 db plus continuously variable 6 db.

Power Supply: Electronically regulated 105 to 125 v. A. C. 50 - 60 cycles

Vari-Sweep

ALL-ELECTRONIC HIGH LEVEL SWEEPING OSCILLATOR OR, (with sweep off) CONTINUOUSLY TUNED CW SIGNAL SOURCE

- Operates On Fundamental Frequency, Therefore Stable Narrow-Band Sweeps
- 1.0 v. RMS (into 70 ohms) Output Flat to ±0.5 db Over Widest Sweep
- Output Automatically Held Constant (AGC) Over Complete Range
- Variable Sweep Width (to 30 mc. PLUS)
 Variable Center Frequency
- Direct Reading Frequency Dial Accurate To ±4.0%
- High Accuracy Attenuator
- Sweep Repetition Rates Down to 10 cps

Price: \$695. FOB Plant



Combined Video and IF Sweeping Oscillator with Marks
SPECIFICATIONS

Frequency Range: Continuously variable, 50 kc to 50 mc.

Sweep Width: Linear, continuously

variable, 4.0 mc to 50 mc.

Sweep Rate: Variable around 60 cps;

Sweep Rate: Variable around 60 cps; locks to line frequency.

Amplitude: 1.0 v, peak-to-peak, into nom. 70 ohms. Flat within ±0.5 db over widest sweep.

Attenuators: Switched 20, 20, 10, 6 and 3 db, plus continuously variable 3 db.

Markers: Eight sharp, pulse-type, crystalpositioned, internal and external markers.

Price: \$695.00 F.O.B. Factory. Substitute markers, \$10.00. Additional markers, \$20.00 each.



ELECTRIC COMPANY

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Dept. E-12



Series 1205

Reset Magnetic Counter



It's the *Original Equipment idea . . . which simply means that, when you're figuring on electrical or mechanical counters in any new product, it pays to design them in, when you begin.

For then Veeder-Root quite likely can save you time and money by adapting or modifying a standard counter to your needs, instead of a special which you might specify on your own. This solves the counter problem . . . and saves you time in engineering, purchasing and assembly.

What's more, you give your product new sales-advantages: Direct-reading digits, instead of hard-to-read dials and verniers . . . instant remote indication if needed . . up-to-the-minute performance records that serve as a basis for production-Countrol, and as proof of your performance guarantee. So don't let counters take a back seat in your new-product plans. Design them in, when you begin . . . it pays in many ways. Do you have the newest Veeder-Root Catalog? Write

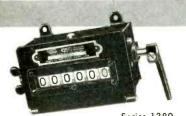


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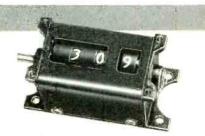




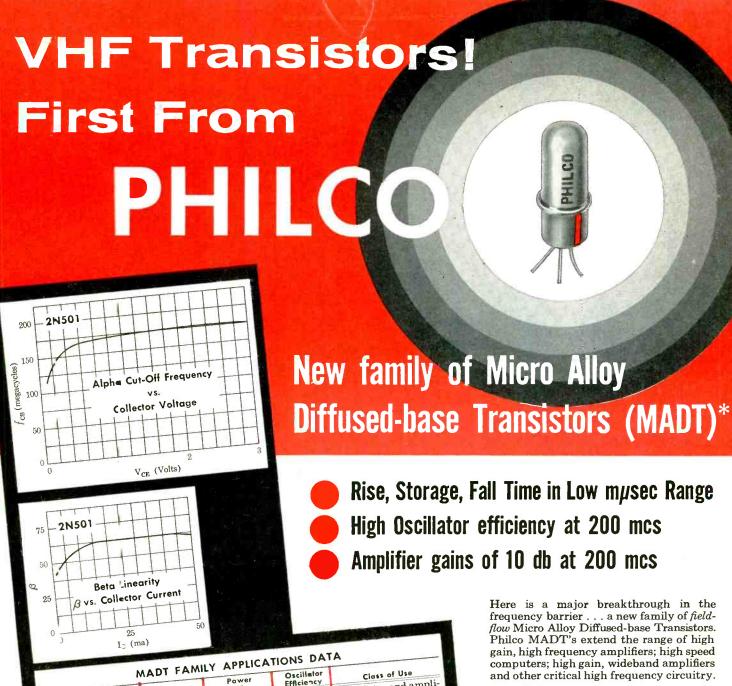
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Power Gain oscillator and ampli-fier to 100 mcs Efficiency 25% at 100 mcs (min) €max 10 db at 100 mcs TYPE* 250 mcs oscillator to 400 mcs 25% at 200 2N499 Ultra high-speed switch typic $t_r=12~m\mu sec;$ (18 max.); $t_s=7~m\mu sec;$ (12 max.); $t_f=4~m\mu sec;$ (10 max.). In circuit with current gain of 10 and voltage turnoff. mcs (min) 2N500 amplifier to 250 mcs 2N501 10 db at 500 mcs 200 mcs amplifier to 100 mcs 2N502T 11 db at 100 mcs(min. high gain IF amplifier 2N503 46 db at

*Ava lable in voltage ratings up to 35V and dissipction ratings to 100 mw. †In _ETEC TO-5 Case (widely known as JETEC 30 Case).

MADT's are available to various voltage and frequency specifications for design of high performance transistorized equipment through the entire VHF and part of the UHF spectrum. These transistors range in f_{max} from 250 mc to as high as 1000 mc. MADT gains are typically 10 db at 200 mc and greater than 16 db at 100 mc. A low cost general purpose unit is available which will deliver typically 18 db at 50 mc and 32 db at 10 mc.

Make Philco your prime source of information for high frequency transistor applications.

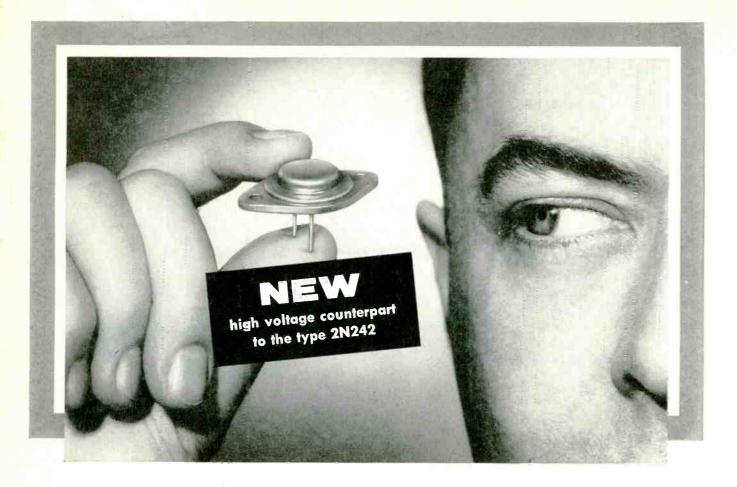
Write to Lansdale Tube Company, Division of Philco Corporation, Lansdale, Pa., Dept. E-1257

*Trademark Philco Corporation for Micro Alloy Diffused-base Transistor

PHILCO. CORPORATION

LANSDALE TUBE COMPANY DIVISION LANSDALE, PENNSYLVANIA





Sixty Volt Power Transistor Type 2N296

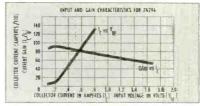
Sylvania develops a high voltage power transistor with optimum performance factors for a wide range of circuit applications.

Now Sylvania offers type 2N296, a PNP germanium alloy transistor designed for high voltage power amplifier or switching applications where supply voltages are 25-30 volts. The new unit is already finding growing use in computer, telephone and aircraft circuits.

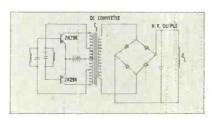
The new 2N296 is physically identical with Sylvania type 2N242 and can be used as its high voltage companion.

Here are the general features of the new 2N296

- 25 Watts. Max. Dissipation (Mounting base maintained at 25° C)
- 2 Amps Collector Current
- 60 Volts Max. Collector Voltage
- 0.8 Saturation Voltage (Typical)
- 20 Minimum Current Gain
- 85° C Storage Temperature
- 100° C Junction Temperature (Operating)
- Temperature Gradient (from junction to mounting base) 3° C/Watt
- New Welded Hermetic Seal Construction



Input and Gain Characteristics for Type 2N296



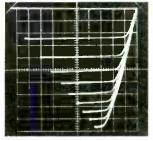
Transistorized DC Converter with Type 2N296

Call or write your Sylvania representative for complete particulars on the new 2N296 60-volt power transistor.

SYLVANIA ELECTRIC PRODUCTS INC. 1740 Broadway, New York 19, N.Y. In Canada: Sylvania Electric (Canada) Ltd. Shell Tower Bldg., Montreal

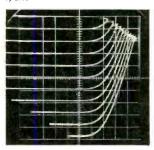


NEW TRANSISTOR-CURVE TRACER



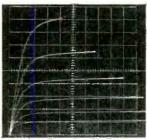
HIGH COLLECTOR CURRENT

PNP transistor, collector current vs collector voltage with constant-current base steps Collector sweep is 0 to 5 v with a 0.25-ohm load, base current is 50 ma/step. Vertical deflection is 1000 mo/div, horizontal 0.5 v/div



HIGH INPUT CURRENT

PNP transistor, callector current vs collector voltage with base grounded and constant-current emitter steps. Collector sweep is 0 to 1.5 v, emitter current 200 ma/step. Vertical deflection is 200 ma/div, horizontal 0.1 v/div. Zero voltage is et center scale.



LOW INPUT CURRENT

NPN transistor, collector current vs collector voltage with constant-current base steps. Collector sweep is 0 to 1.5 v, base current 1 microamp/step. Vertical deflection is 10 microamp/div, hasizontal 0.1 v/div.

has 10-AMPERE COLLECTOR SUPPLY
2.4-AMPERE BASE SUPPLY

Displays 4 to 12 curves per family with input current from 1 MICROAMP/STEP to 200 MILLIAMPS/STEP



The Tektronix Type 575 traces characteristic curves for both PNP and NPN transistors on the face of a cathode-ray tube. Seven d ffer-

ent types of curves can be plotted. Vertical deflection is calibrated in collector current, base voltage, base current and base source voltage. Horizontal deflection is calibrated in collector voltage, base voltage, base current and base source voltage. Collector current supply is capable of 10 amperes from 0 to 20 v, 1 ampere from 0 to 200 v. Constant current or constant voltage step supply to either base or emitter is calibrated in 17 values from 1 microamp/step to 200 milliamps/step, and in 5 values from 0.01 v/step to 0.2 v/step with 24 values of driving resistance from 1 ohm to 22 kilohms. Input steps are adjustable from 4 to 12 per family, with repetitive or single-family display.

TYPE 575 TRANSISTOR-CURVE TRACER . . . \$925

f.o.b. Portland, Oregon

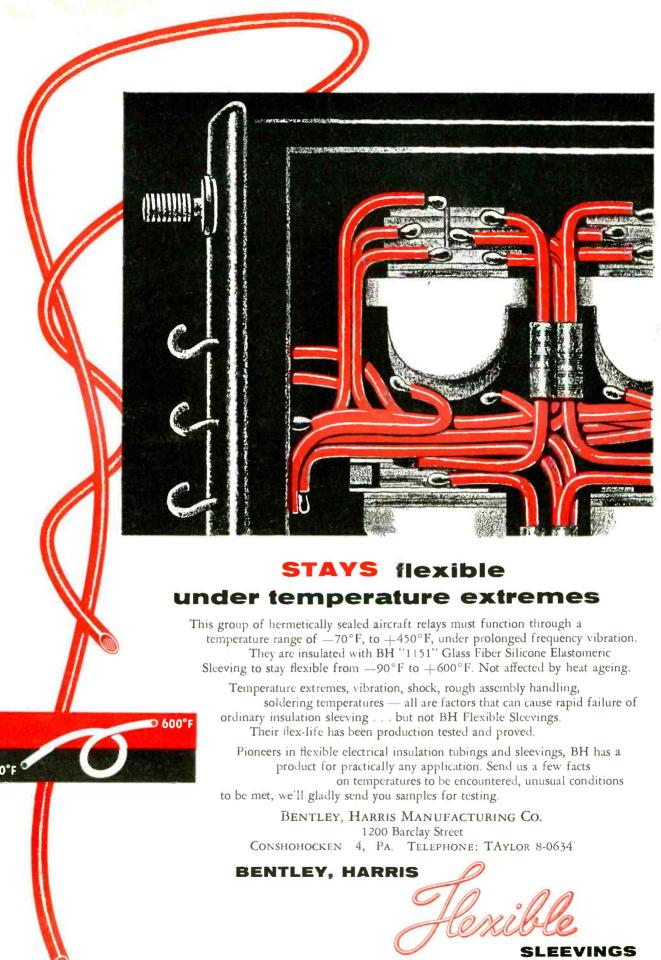
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First shipments against a sizeable backlog accurred early in November, Please check with your Tektronix Field Engineer or Representative for current Type 575 shipping schedule.

> ENGINEERS—interested in furthering the advancement of the oscilloscope? We have openings for men with creative design ability. Please write Richard Ropiequet, Vice President, Engineering.



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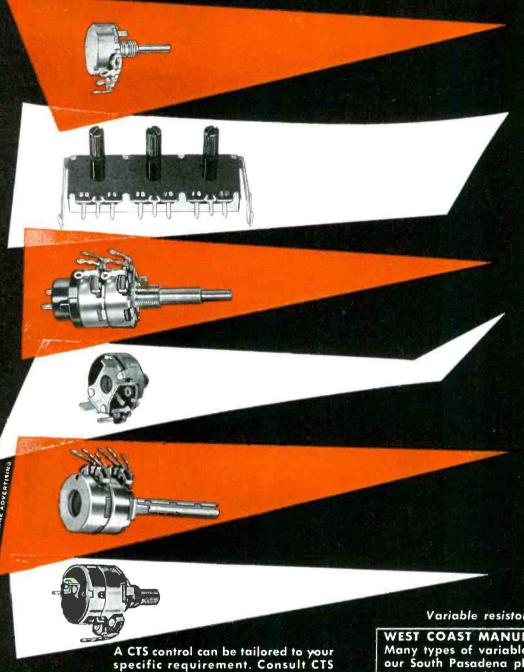
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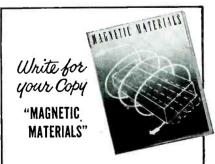


for HEARING AIDS

or RECORDING HEADS



or ANY MAGNETIC MATERIALS JOB ...



This 32-page book contains valuable data on all Allegheny Ludlum magnetic materials, silicon steels and special electrical alloys. Illustrated in full color, includes essential information on properties, characteristics, applications, etc. Your copy gladly sent free.

ADDRESS DEPT. E-96

You can *rely* on core materials like the Allegheny 4750 components illustrated above, in your receivers, recording heads or microphone assemblies.

In fact, whether your equipment is small or large, the extra-broad line of A-L magnetic materials will solve your magnetic core problems. It includes all grades of silicon steel sheets or coil strip, as well as Allegheny Silectron (grain-oriented silicon steel), and a wide selection of high-permea-

bility alloys such as 4750, Mumetal, Permendur, etc.

Our service on these materials also includes complete facilities for the fabrication and heat treatment of laminations. (For users of electrical sheets and strip, our lamination know-how is a real bonus value!) Either way, we'll welcome the chance to serve you. Allegheny Ludlum Steel Corporation, Oliver Building, Pittsburgh 22, Pa.

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For the record...

it's IMMEDIATE-PRINT scope photos

with the DUMONT 302

- NOW, ULTRA-FAST TRANSPARENT POLAROID-LAND FILM FOR HIGH SPEED RECORDING!
- CONTACT AND PROJECTION PRINTS: .. NO IMAGE REVERSAL.
- EASY, INEXPENSIVE CONVERSION TO VARIETY OF STANDARD ROLL AND CUT FILMS.
- CLICK-STOP SLIDE PERMITS MULTIPLE EXPOSURES ON SINGLE FRAME FOR GREATER FILM ECONOMY AND EASY, DIRECT WAVEFORM COMPARISON.
- FULL BINOCULAR VIEWING SIMULTANEOUS WITH RECORDING.
- MOUNTS QUICKLY AND EASILY ON ANY STANDARD 5" SCOPE. NO ADDITIONAL SUPPORTS REQUIRED.
- EASY ACCESS FOR LENS AND SHUTTER ADJUSTMENT.
- BUILT-IN DATA RECORDING SYSTEM.

SPECIFICATIONS

- Wollensak-Du Mont 75 mm f/2.8 three element lens, or 75 mm f/1.9 six element lens.
- . Image reduction ratio 2.25:1.
- Alphax #2 shutter, bulb and 1/25 to 1/100 sec. with f/2.8 lens. Alphax #3 shutter, time, bulb and 1 sec. with f/1.9 lens.
- · Writing rate dependent upon film used.
- . Mounting clamp for use on any standard 5" scope

Type 302 with f/2.8 lens \$314.00 Type 302 with f/1.9 lens



The Du Mont Type 302 Recording Camera provides the most convenient and flexible means for applying the many advantages of the immediate-print Polaroid-Land process to oscilloscope recording.

And now the utility of the Polaroid-Land process has been greatly extended with the development of the new Polaroid-Land projection film - a transparent base material with a specified emulsion speed of 1000 (ASA).

This new film not only permits contact and projection prints, and eliminates image reversal, but also enables use of the Polaroid-Land process in recording ultra-high-speed phenomena — even single transients.

Utility of the 302 is further broadened by the availability of adapter backs which permit the camera to use various standard roll and cut films. Write for full information ...

WHATEVER YOUR REQUIREMENTS . . . DU MONT HAS THE CAMERA



TYPE 352

High-speed, single frame 35 mm featuring automàtic film advance. 8 frames/sec. au-tomatically. Wollensak f/1.5 lens. \$648.00



TYPE 339

Immediate-print type utiliz-ing Polaroid film. Special f/2.8 lens for distortion-free images. Binocular viewing of screen. \$246.00



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General purpose camera accepting backs for roll-film, film-pack, or cut film. Converts to Type 302 for Polaroid recording, f/1.9 lens \$369.00, f/2.8 lens \$292.00



TYPE 296

Low-cost, general-purpose single-frame camera. Uses standard casette wound 35 mm film. Corrected f/2.8 lens. Viewing port. \$164.50



TYPE 321-A

Permits either continuous or single-frame recording. Perforated or unperforated film or paper in 100 or 400 foot reels. Variable film drive speeds from 0.8 to 10,800 in./min. 321-A with f/1.5 lens \$1270.00, 321-A with f/2.8 lens \$1120.00. (50 cps models available)



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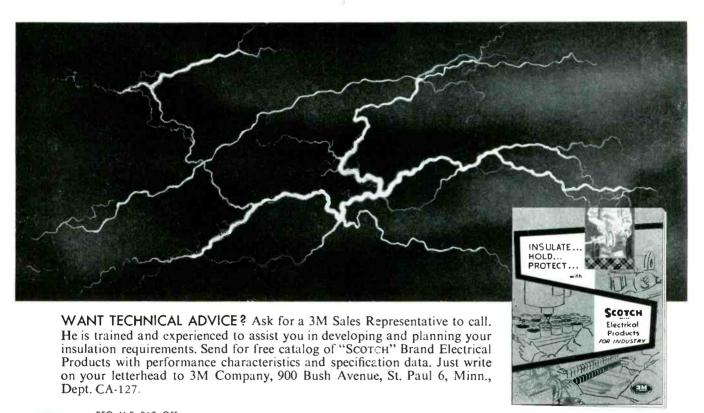
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with SCOTCH Electrical Products!

CONSIDER THE VARIETY: "SCOTCH" Brand Electrical Products come in many forms ... each planned to do a specific job better, easier, more dependably:

"SCOTCH" Brand Pressure-Sensitive Tapes (they stick at a touch!) insulate . . . strengthen . . . pad . . . hold . . . identify. There are thermosetting tapes for maximum adhesion and varnish resistance . . . tapes with temperature performance ranges from Class O to Class H . . . tapes that offer dielectric strengths up to 19,000 V . . . others to fill space requirements down to .002" thin. There are rigid and flexible epoxy resins for embedment, encapsulation, and dipping.

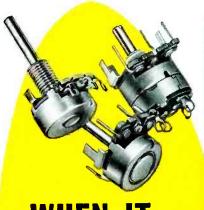
DEPEND ON THE QUALITY: All "SCOTCH" Brand Electrical Products are designed and formulated with valuable non-corrosive features in 3M's own laboratories—America's most progressive electrical insulation laboratories. Constant quality control assures you that when you design with "SCOTCH" Brand in mind, the product functions the way you want it to.



SCOTCH Electrical Products

The term "SCOTCH" is a registered trademark of Minnesota Mining and Manufacturing Company, St. Paul 6, Minn. Export Sales Office: 99 Park Ave., New York 16, N.Y. In Canada: P.O. Box 757, London, Ontario.





WHEN IT COMES TO MINIATURE CONTROLS...

CHECK THE OVERALL SIZE...

including switch, if needed. For practical space-saving ability, Stackpole miniature "F" Controls lead the way — only 0.637" in diameter behind the panel for the entire length of both control and switch.





Photos show side and rear views of a Stackpole F Control with 2-pale switch. Dotted lines indicate behind-panel space accupied by a conventional "miniature" control.

Notice how Stackpale's small switch size perfectly complements the miniature control ... saves precious chassis space where it's needed the mast.

FEEL and HEAR THE SWITCH ACTION...



for the tease-proof, positive "feel" and audible "click" only a true snap-action switch provides. "B"—Series switches used on "F" Controls have the same time-proven mechanism as larger Stackpole control switches. They're U.L. Inspected for 1 amp. @ 125v ac-dc; 4 amps @ 25v dc.

CHECK THE COMPLETENESS OF BOTH CONTROL and SWITCH LINES

Printed wiring, wire-wrap, or standard lug terminals as well as fold-tab or threaded bushing mountings are available on all Stackpole miniature "F" controls. Both SPST and DPST switches can be supplied.

STACKPOLE

VARIABLE RESISTORS

Electronic Components Division

STACKPOLE CARBON COMPANY, St. Marys, Pa.

In Canada: Canadian Stackpale Ltd., 550 Evans Ave., Etobicoke, Taronta 14, Ont.

FIXED & VARIABLE COMPOSITION RESISTORS • SLIDE & SNAP SWITCHES • IRON CORES • CERAMIC MAGNETS
FIXED COMPOSITION CAPACITORS • CERAMAG® FERROMAGNETIC CORES
HUNDREDS OF CARBON, GRAPHITE, AND METAL POWDER PRODUCTS.



This is what Taylor means by better printed circuits... the unretouched photograph above is an enlargement of the miniature etched test coil shown at right. Here is a dramatic illustration of exactly what Taylor means by saying rolled copper-clad laminates give you better printed circuits. Enlarged 375 times, this photograph shows how the .002" wide conductors are parallel and free

of pits, pinholes and lead inclusions.

Here's proof of why you'll be satisfied with your printed circuits . . . if they're made with Taylor copper-clad laminates. You're assured of a uniform material, offering consistently satisfactory etching . . . better production rates.

For more detailed information on Taylor copper-clad laminates . . . for a discussion on how these laminates can help you produce better printed circuits . . . contact your nearest Taylor sales office.

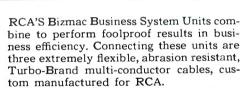
TAYLOR FIBRE CO., PLANTS IN NORRISTOWN, PA. AND LA VERNE, CALIFORNIA

INTEGRATED MANUFACTURER & FABRICATOR OF Phenolic—Melamine—Silicone—Epoxy—Copper-Clad and Combination Laminates • Vulcanized Fibre TAYLOR
Laminated Plastics
Vulcanized Fibre

FIRST AND LARGEST PRODUCER OF ROLLED COPPER-CLAD LAMINATES FOR BETTER PRIMTED CIRCUITS

BRAND MULTI-CONDUCTOR CABLE GIVES RCA'S BIZMAC SYSTEMS...

- · top signal fidelity
- · freedom from cross talk



RCA says, "Brand cables transmit signals between our Bizmac units with high fidelity and without disrupting cross talk between signal lines."

One Brand cable (a) transmits a five micro-second pulse "write signal." Low impedance drive allows transmission of signals through 400 feet of balanced lines. The cable has nine twisted pairs of AWG 22 color coded conductors. The shielding of #36 tinned copper wires is braided over the conductor assembly. The over-all jacket is of .030" brown plastic. Another cable (b) transmits "tape control" signals which have a five micro-second pulse with about a three micro-second rise time across the conductors. Each of the 12 pairs of conductors are shielded with a #36 tinned soft copper braid, and the over-all jacket is of .030" red polyvinyl chloride. The other cable (c) transmits "read signals" that resemble a full sine wave whose period is 70 micro-seconds. The 12 twisted pairs of AWG 22 conductors have a tinned copper over-all shielding braided over the conductor assembly. The over-all jacket is of .030" black vinyl plastic.

The accumulated experience of the William Brand & Co., Incorporated Engineering, Research and Production Departments is always available. You are invited to use these services in the solution of any of your wire and/or cable problems.

THE WILLIAM BRAND & CO., INCORPORATED CONNECTICUT WILLIMANTIC 3 electrical and electronic wires and cables . harnesses and cable assemblies . plastic and coated insulating tubings * identification markers



Variety—you can choose from a wide range of finishes for magnesium

Smart, modern furniture is just one example of how finishes for magnesium are widening design horizons. Whether for appearance, protection, or a combination of both, the right finish is available. Magnesium can be painted, chemically treated, electroplated, and coated with plastic or rubber.

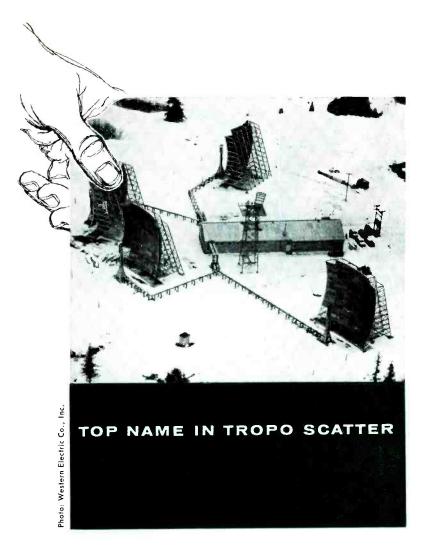
To meet the rigorous standards set by the aircraft industry, there are air dried and baked paint finishes with excellent adhesion, maximum imperviousness and good wear resistance. Various types of chemical pickling provide the right

paint base. Anodizing provides exceptional corrosion, heat and abrasion resistance. In addition, any metal which can be applied by electroplating may be deposited on magnesium.

What about your products? If you're not making use of magnesium lightness, strength and durability—and the variety of finishes for magnesium—there's no better time to start than right now. Contact your nearest Dow sales office or write to us for more information. The DOW CHEMICAL COMPANY, Midland, Michigan, Department MA 1405M.

YOU CAN DEPEND ON





Detailed information and technical data on the tropospheric scatter radio equipment for four major projects has recently been published by REL.

Entitled *Top name in tropo scatter*, this manual describes the radio apparatus developed and manufactured by REL for the first major project, Polevault; for the largest, White Alice; for AN/FRC-39; and for the Texas Towers, AN/FRC-56.

If you have a specialized interest in this field, a free copy is yours for the asking from REL, world leader in tropo scatter equipment.

Creative careers at REL await a few exceptional engineers. Address resumes to James W. Kelly, Personnel Director.

Radio Engineering Laboratories Inc.

A subsidiary of Dynamics Corporation of America

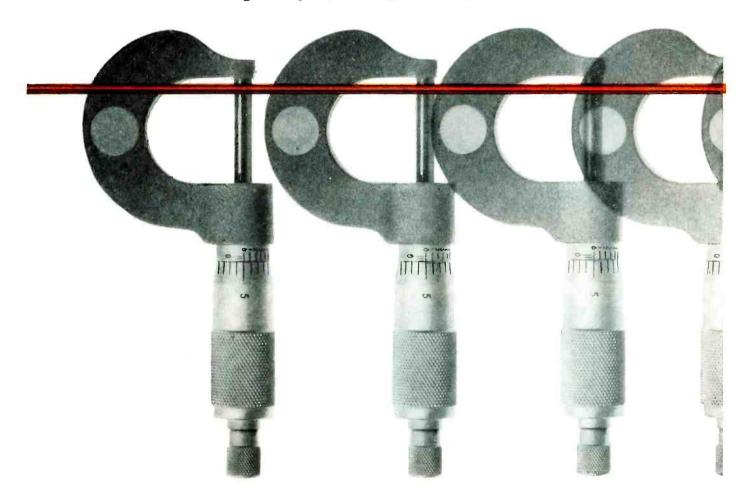
29-01 Borden Ave · Long Island City 1, NY

STillwell 6-2100 · Teletype: NY 4-2816

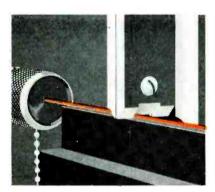
Canadian representative: AHEARN & SOPER CO - 384 BANK ST - OTTAWA



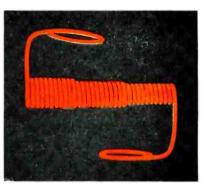
Behind the quality of Phelps Dodge FORMVAR...



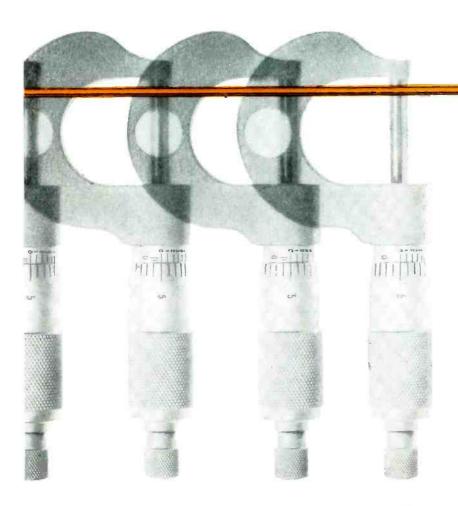
CAREFUL CONTROL OF FINELY



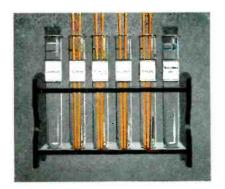




Film flexibility



BALANCED PROPERTIES



Solvent resistance

Phelps Dodge Formvar magnet wire has a high quality and balance of essential properties that are the result of carefully controlled testing throughout the manufacturing process. These balanced properties offer greater abrasion resistance, exceptional film flexibility, improved solvent resistance and high product uniformity-factors that serve to make Phelps Dodge Formvar the standard "yardstick" for the electrical equipment industry. Phelps Dodge Formvar is available in round, square and rectangular shapes.

Any time magnet wire is your problem, consult Phelps Dodge for the quickest, easiest answer!

PHELPS DODGE COPPER PRODUCTS

INCA MANUFACTURING DIVISION

FORT WAYNE, INDIANA



FIRST FOR
LASTING QUALITY
-FROM MINE
TO MARKET!





For Contacts Which Don't Exist Look to GENERAL PLATE

SINGLE TOP-LAY STRIP STOCK (TOP)
DOUBLE INLAY STRIP STOCK (BOTTOM)

OVERLAY PART TOP-LAY PART

You can profit by using General Plate clad metals.

Paradoxical statement? Not at all — it's merely another way of saying that at G.P. you're not limited to yesterday's thinking in solving tomorrow's contact problems.

For beyond the tremendous variety of contacts already in production at G.P., are the know-how of G.P. engineers and the versatility of G.P. clad metals which combine to offer you better contact performance at lower cost.

Here are a few examples of new contact ideas which are now in commercial use at G.P.

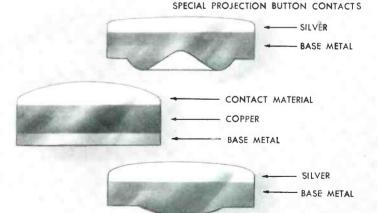
Clad Electrical Contact Tapes — designed for high speed mechanized assembly — ideal for miniaturization — give increased performance at reduced cost.

New Metal Bonding Processes — offer improved contact materials—include silver cadmium oxides, refractory metal mixtures and platinum group metals, as well as all regular silver materials.

New Clad Button Projection — designed and produced to meet your specific application requirements — facilitate easier welding, provide better conductivity.

Single and Double Inlay-Overlay-Top-Lay — made by G.P.'s new exclusive P.T. cladding process — achieves permanent bonding of preferred contact metals to practically any malleable base metal without intermediate bonding agents.

Trimetal Clad Projection Welding Contacts — a copper conductor between contact face and backing — provides higher specific heat with lower surface temperatures — gives greater contact capacity and longer life at lower cost.



With 41 years of General Plate metal cladding experience behind the emphasis now being put on G.P. electrical contacts, it will pay you to investigate. Technical data bulletins are available on request —just let us know what types of contacts you are interested in.

METALS & CONTROLS

General Plate Division

CORPORATION

1312 Forest Street, Attleboro, Mass.

FIELD OFFICES: NEW YORK, CHICAGO, DETROIT. MILWAUKEE, LOS ANGELES

Transitron

Silicon Transistors



ACTUAL

Features ...

- Low I co, typically under .02 μα
- Operation to 175°C
- 200 mw Power Rating
- High Frequency Operation
- High Temperature Tested
- Excellent Stability
- Welded Hermetic Seal

Туре	Minimum Common Emitter Current Gain, B	Maximum Collector Voltage Vee Peak (volts)	Typical Cut-off Frequency (mc)	Maximum Collector Cut-Off Current at 25°C at Ve Max. (ua)
ST42	40	45	11	.5
ST32	40	30	11	.5
ST12	40	15	11	.5
ST33	30	30	17	.5
ST13	30	15	17	.5
ST41	20	45	10	.5
ST31	20	30	10	.5
STII	20	15	10	.5
2N332	9	45	7	50
2N332	18	45	9	50
2N333	18	45	11	50
2N335	37	45	10	50

. . . for high temperature operation

Transitron's NPN silicon transistors are designed for a wide range of small signal applications in the power range up to 200 mw. They will provide dependable operation up to 175°C in circuits such as RF and IF amplifiers, video and audio amplifiers, servo control, switching, and many others.

Manufactured by diffusion in the liquid phase during crystal growth, these transistors are essentially free of parameter drift and instability common in conventional grown junction transistors. Through close process control, these units have exceptionally low I₀₀ up to their maximum voltage and temperature ratings. As a result, performance reliability can be achieved even at higher voltage levels.

For environmental stability, extensive temperature cycling and storage as well as mechanical and hermetic seal tests are included as a regular part of the manufacturing process.

Send for Bulletin TE-1353

Transitron

electronic corporation * wakefield, massachusetts





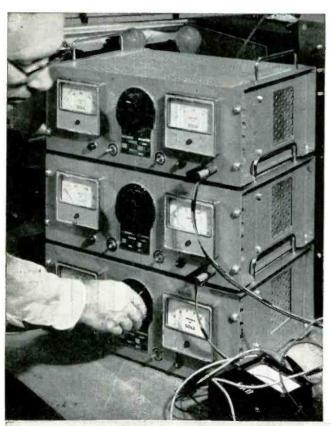








COMPACT, CONVENIENT three-high stacking of the new adjustable Sola Constant Voltage DC Pawer Supply is shown in the typical laboratory bench setup above. Below, engineer "dials" specific test voltage desired from each of the three standard models of "DC Solavolts" shown.



A versatile DC supply for men who design or test electrical and electronic equipment prototypes

Do you design or test "prototypes?" If so, and you're seeking a laboratory source of high-current DC voltage, it will pay you to use the "DC Solavolt." It's a moderately-priced, adjustable, regulated dc power supply that provides unusual stability with intermittent, variable, or pulse loads. Output voltage is regulated to within $\pm 1\%$ though supply voltage may vary as much as $\pm 10\%$. Ripple is held to 0.1% or less.

Electrical specifications of the six stock "DC Solavolts" available appear in the table below:

All Inputs 100-130 volts, 60 cps

Catalog Number	Regulated Adjustable	Rated Loadings in Amperes		Ripple* Voltage—
Stock Vo	Output Voltage Range	At max. Voltage Setting	t max. At min. oltage Voltage	% of Total Output
28510	5-35	7.0	7.0	0.10
28520	25-60	4.0	6.0	0.05
28530	30-90	2.8	4.0	0.04
28540	60-180	1.4	2.0	0.03
28550	150-250	1.0	1.5	0.02
28560	250-400	0.6	0.75	0.02

^{*}Figures in this column cover ripple voltages measured at full rated load and input of 115 volts.

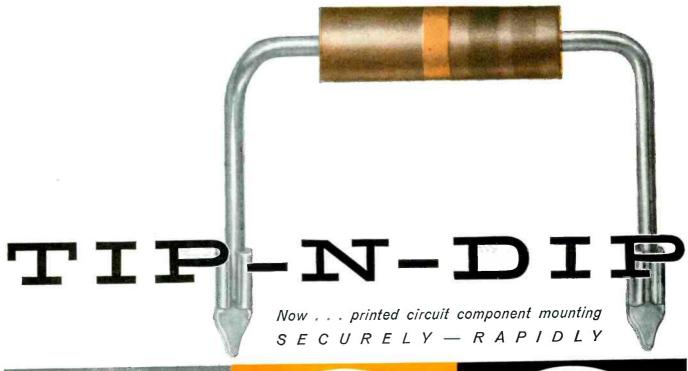
Along with these laboratory standards of performance, the DC Solavolt offers compactness, low weight, high efficiency, and high short-time overload capacity. All stock models occupy only 7" of height and 12½" of depth on a standard 19" relay rack frame. There are no tubes to replace, no compensating adjustments are needed, and no maintenance is required. Carrying handles, available as accessory equipment, provide "oneman" portability and self-stacking. Your local electronic distributor, who stocks the DC Solavolt, will be happy to give you further information.



Write for Bulletin
SOLA ELECTRIC CO.
4633 W. 16th Street, Chicago 50

SOLA Constant Voltage
DC POWER SUPPLIES

CONSTANT VOLTAGE TRANSFORMERS • LIGHTING TRANSFORMERS • CONSTANT VOLTAGE DC POWER SUPPLIES SOLA ELECTRIC CO., 4633 West 16th Street, Chicago 50, Illinois, Bishop 2-1414 • BRANCH OFFICES: Boston, Mass.; Cleveland, Ohio; Kansas City, Ma.; Los Angeles, Calif.; New York, N. Y.; Philadelphia, Pa.; San Francisco, Calif.; Wallingford, Conn. • Representatives in Other Principal Cities Sola Electric (Canada) Ltd., Toronto 17, Ontario: 102 Laird Drive, Mayfair 4554





The A-MP Component Tip provides these new advantages to manufacturers using printed circuit techniques:

- · eliminates the need for eyelets or thru-plating on two-sided boards
- prevents cold solder problems by eliminating any movement of the component during dipping cycle
- permits bridging or offsetting of components—for air circulation and elimination of temperature influence
- · design promotes solder-wicking and uniform solder deposit
- protects fine semi-conductor leads from heat and assembly damage

AMP-engineered, high-speed, automatic tipping machines provide an easy and economical method for applying A-MP Component Tips to leads of single-piece or belted components.

Additional Information is available on request.

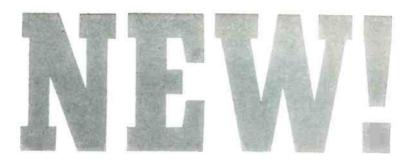
AMP INCORPORATED



3340 Eisenhower Boulevard, Harrisburg, Pa.

Wholly Owned Subsidiaries: Aircraft-Marine Products of Canada Ltd., Toronto, Canada Aircraft-Marine Products (Great Britain) Ltd., London, England • Societe AMP de France, Le Pre St. Gervais, Seine, France • AMP-Holland N. V.'s-Hertogenbosch, Holland Distributor in Japan: Oriental Terminal Products Co., Ltd., Tokyo, Japan





The color film that changed the standards of still photographers everywhere is now available as a 16mm motion picture stock.

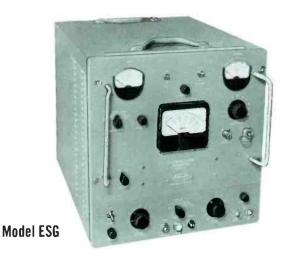
SUPER ANSCOCHROME 16mm FILM

Daylight-exposure index 100

◆ This premium color emulsion, widely accepted and acclaimed in still work, has been made available in 16mm width for motion picture photography. Its speed of 100 makes it the most useful film for all phases of industrial cinematography where speed and superb color renditions are called for. Super Anscochrome's improved curve conformity, characteristic of all Anscochrome emulsions, provides a color balance that has never been achieved in any other color film. It combines high speed, good latitude, clean highlights and superior shadow area penetration—all so desirable for high speed motion analysis, stress studies and data recording as well as routine work where a reserve of speed is needed. And, Super Anscochrome's high speed does *not* mean a loss of quality. Its design is such that the speed becomes an added feature to the already outstanding characteristics of Anscochrome emulsions.

Also available in 35mm and 70mm. Ansco, Binghamton, New York. A Division of General Aniline and Film Corporation.





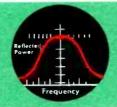
All Electronic

MICROWAVE SWEEP GENERATOR

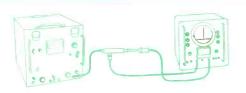
- Dynamic Measurements, Rapidly
- High Power Source

1,000 to 15,000 mc





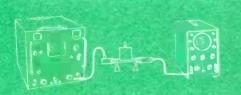
MEASUREMENT OF VSWR OR PERCENT POWER REFLECTION
By employing an ESG along with a Rapid Scan Ratio-Scope (Model VS-1) in a reflectometer system set-up, accuracies equivalent to those obtained with the use of a slotted line can be achieved, by an untrained technician, in a fraction of the time formerly required. A two-to-one frequency range is provided. 7 interchangeable microwave oscillator units enable measurements to be made at microwave frequencies of 1000 to 15,000 mc.

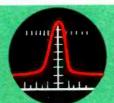




ATTENUATION MEASUREMENT

Broadband attenuation measurements are easily made with an ESG and Rapid Scan Ratio-Scope (Model VS-1). Attenuation of the unit under test is read directly on the ratio-scope indicator. Attenuation measurements can be made either at single frequency or over a band of frequencies (ESG sweeps its full frequency range).





MEASUREMENTS OF Q

The use of a Model ESG enables rapid visual instantaneous measurement of high and low Q. This cuts down engineering man hours when compared with laborious point-to-point Q measurements. The diagram shows a typical set-up utilizing a standard oscilloscope.



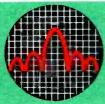


FILTER ALIGNMENT AND BANDPASS MEASUREMENTS

Because of the ESG's rapid sweep, the complete characteristics of a filter can be observed and measured instantaneously, utilizing a standard oscilloscope. The ESG's high power output enables determination of the filter's offband response. Dynamic measurements across the entire frequency range of the filters are possible because the stable backward wave oscillator in the ESG sweeps the full frequency range of the filter.







ANTENNA PATTERN MEASUREMENTS

By using an ESG to feed an antenna under test, accurate pattern measurements can be obtained over long distances and over a wide frequency range. This because of the ESG's high stable power output from 10 milliwatts to 1 watt. Provision is made in the instrument for amplitude modulation from external source and internal 1000 cps and 456 kc square wave modulation is provided.



POLARAD ELECTRONICS CORPORATION

43-20 34th Street, Long Island City 1, New York

REPRESENTATIVES: Abington, Albany, Atlanta, Baltimore, Boeing Field, Chicago, Cleveland, Dayton, Denver, Detroit, Englewood, Fort Worth, Kansas City, Los Angeles, Orlando, Portland, Rochester, St. Louis, Stamford, Sunnyvale, Syracuse, Washington, D.C., Westbury, Westwood, Wichita, Winston-Salem, Canada: Arnprior, Ontario. Resident Representatives in Principal Foreign Cities. Polarad Model ESG Microwave Sweep Generator utilizes stable backward wave oscillators to make possible rapid dynamic tests of broadband and narrowband microwave systems and components. This instrument covers the frequency range from 1000 to 15,000 mc by use of 7 interchangeable microwave oscillator units, each of which can be purchased separately. The ESG can be externally modulated, providing a pulse rise time less than 0.15

Contact Polarad or your nearest Polarad representative for complete details.

Polarad Model VS-1 Rapid Scan Ratio-Scope is available to provide visual presentation of VSWR and attenuation.

SPECIFICATIONS: Basic Unit: Model E-B

INTERCHANGEABLE PLUG-IN UNITS

MODEL	FREQUENCY RANGE	POWER OUTPUT	MODEL	FREQUENCY RANGE	POWER OUTPUT
Model E-L1	1,000 to 2,000 mc	80 to 1,000 mw	Model E-C2	4,800 to 9,600 mc 6,500 to 11,000 mc 7,500 to 15,000 mc	20 to 150 mw
Model E-L2	1,600 to 3,200 mc	80 to 1,000 mw	Model E-XI	6,500 to 11,000 mc	20 to 100 mw
Model E-S1	2,000 to 4,000 mc	80 to 800 mw	Model E-X2	7,500 to 15,000 mc	15 to 40 mw
Model F-C1	3.600 to 7.200 mc	25 to 400 mw			

CODE MODULATED MULTIPLE-PULSE MICROWAVE SIGNAL GENERATOR 950-10,750 mc

An integrated mobile instrument.
Generates multi-pulse modulated carrier for missiles, beacons, radar, D M E, Tacan, Loran...
provides 5 independently adjustable pulse channels.
Variable pulse width, delay and repetition rate; and pulse time modulation.

SPECIFICATIONS:

Frequency Range:

Band 1: 950 to 2400 mc.

Band 2: 2150 to 4600 mc. Band 3: 4450 to 8000 mc

Band 4: 7850 to 10,750 mc

Frequency Accuracy: ±1%

RF Power Output: 1 milliwatt

(0 DBM)

Attenuator:

Output Range: 0 to —127 DBM Output Accuracy: ±2 db Output Impedance: 50 ohms nominal

RF Pulse Characteristics:

- a. Rise Time: Better than 0.1 microsecond as measured between 10 and 90% of maximum amplitude of the initial rise.
- b. Decay Time: Less than 0.1 microsecond as measured between 10 and 90% of maximum amplitude of the final decay.
- c. Overshoot: Less than 10% of maximum amplitude of the initial rise.

Internal Pulse Modulation:

No. of Channels: 1 to 5 independently on or off

Repetition Rate: 40 to 4000 cps. Pulse Width: 0.2 to 2.0 micro-

Pulse Delay: 0 to 30 microseconds

Accuracy of Pulse Setting: 0.1 microsecond

Minimum Pulse Separation: 0.3 microsecond

Initial Channel Delay: 2 microseconds from sync. pulse

Internal Square Wave: 40-4000 pps (separate output)

Pulse Time Modulation:

Frequency: 40-400 cps any or all channels

Required Ext. Mod.: 1 volt rms min.

Maximum deviation: ±0.5 microsecond

Power Input (built-in power supply) 105/125 v. 60 cps 1200 watts.



FOUR INTERCHANGEABLE MICROWAVE OSCILLATOR UNITS -- all stored in the

instrument ... each with UNI-DIAL control ... precision power monitor circuit to maintain 1 mw power output reference level ... keying circuit to assure rapid rise time of modulated r-f output ... non-contacting chokes.

PRECISION OSCILLOSCOPE WITH BUILT-IN WIDE BAND RF DETECTOR for viewing

the modulation envelope and accurately calibrating the r-f pulse width, delay, and group repetition rate. Equipped with built-in calibration markers.

FIVE INDEPENDENTLY ADJUSTABLE

PULSE CHANNELS— each channel features variable pulse width and delay; has provisions for external pulse-time modulation. Repetition rate for each group of pulses can be varied.

SELF-CONTAINED POWER SUPPLIES

— Model B operates directly from an AC line through an internal voltage regulator. The coded multipulse generator is equipped with an electronically regulated low voltage DC supply. Klystron power unit adjusts to proper voltage automatically for each interchangeable tuning unit.

Model E

Contact your Polarad representative or write to the factory for detailed information.

POLARAD ELECTRONICS CORPORATION

43-20 34th Street, Long Island City 1, New York



REPRESENTATIVES: Abington, Albany, Atlanta, Baltimore, Boeing Field, Chicago, Cleveland, Dayton, Denver, Detroit, Englewood, Fort Worth, Kansas City, Los Angeles, Portland, Rochester, St. Louis, Stamford, Sunnyvale, Syracuse, Washington, D. C., Westbury, Westwood, Wichita, Winston-Salem, Canada: Arnprior, Ontario. Resident Representatives in Principal Foreign Cities.

ENGINEERING REPORT

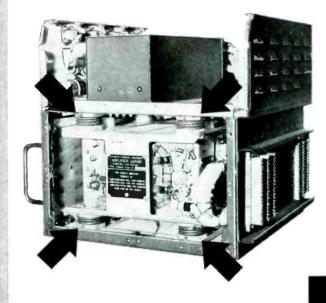
A Case History of Environmental Control

PROBLEM

VIBRATION • SHOCK AND COOLING

POWER TUBE FAILURE during environmental testing of the Servo-Amplifier in the flight stabilization system of Chance Vought's F8U-1 Crusader.

SOLUTION



ENGINEERED MOUNTING SYSTEM:

Robinson Model 1514 all-metal light-weight mounting system to protect entire Servo-Amplifier assembly. Highly damped Met-L-Flex resilient elements are incorporated in an opposed cushioning design. Resulting center-of-gravity suspension system assures all attitude protection for power tube and other electronic components.

The Servo-Amplifier assembly was isolated with no increase in over-all equipment dimensions.

SPECIAL FEATURE:

Range of environmental protection is extended by screened cooling apertures designed as part of the combined chassis and mounting.

PERFORMANCE:

Natural frequency of the mounting system is between 15-21 c.p.s. After 15 G drop tests on all six sides, there was no loss of isolation efficiency which remained as high as 90% at 55 c.p.s. with .060 inches excursion.

RESULT:

- 1. Increased operational reliability of Chance Vought's supersonic Crusader.
- 2. Another contribution to the weapons system reliability program pioneered by Chance Vought Aircraft, Inc. in cooperation with Robinson engineers.

ROBINSON CONTROL IS RELIABILITY CONTROL

ROBINSON AVIATION, INC.

Teterboro, New Jersey
West Coast Engineering Office, Santa Monica, California

FREQUENCY STANDARDS



PRECISION FORK UNIT

TYPE 50

Size 1" dia. x 334" H.* Wght., 4 oz.

Frequencies: 240 to 1000 cycles

Accuracies:-

Type 50 ($\pm .02\%$ at -65° to 85° C) Type R50 ($\pm .002\%$ at 15° to 35°C) Double triode and 5 pigtail parts required Input, Tube heater voltage and B voltage

Output, approx. 5V into 200,000 ohms

FREQUENCY STANDARD

TYPE 50L

Size 334" x 41/2" x 51/2" High Weight, 2 lbs.

Frequencies: 50, 60, 75 or 100 cycles

Accuracies:-

Type 50L (\pm .02% at -65° to 85°C) Type R50L (\pm .002% at 15° to 35°C)

Output, 3V into 200,000 ohms

Input, 150 to 300V, B (6V at .6 amps.)



*3%" high 400 - 1000 cv.

PRECISION FORK UNIT

TYPE 2003

Size 11/2" dia. x 41/2" H.* Wght. 8 oz.

Frequencies: 200 to 4000 cycles

Accuracies:-

Type 2003 ($\pm .02\%$ at -65° to 85° C) Type R2003 (±.002% at 15° to 35°C) Type W2003 ($\pm .005\%$ at -65° to 85° C)

Double triode and 5 pigtail parts required Input and output same as Type 50, above

FREQUENCY STANDARD

TYPE 2005

Size, 8" x 8" x 71/4" High Weight, 14 lbs.

Frequencies: 50 to 400 cycles (Specify)

Accuracy: ±.001% from 20° to 30°C

Output, 10 Watts at 115 Volts Input, 115V. (50 to 400 cycles)





*3½" high

400 to 500 cy.

optional

FREQUENCY STANDARD

TYPE 2007T TRANSISTORIZED

Size 11/2" dia. x 41/2" H.* Wght. 7 ozs.

Frequencies: 240 to 1000 cycles Accuracies:-Same as 2003, above Type 2007S-Silicon type Input, 28V.

Output, Multitap, 75 to 100,000 ohms

*31/2" in 2007S, 400 to 800 cycles.



TYPE 2121A

Size 8¾" x 19" panel Weight, 25 lbs.

Output: 115V 60 cycles, 10 Watt

Accuracy: ±.001% from 20° to 30°C

Input, 115V (50 to 400 cycles)





FREQUENCY STANDARD

TYPE: 2001-2

Size 334" x 41/2" x 6" H., Wyht. 26 oz.

Frequencies: 200 to 3000 cycles Accuracy: ±.001% at 20° to 30°C

Output: 5V. at 250,000 ohms Input: Heater voltage, 6.3 - 12 - 28

B voltage, 100 to 300 V., at 5 to 10 ma.

FREOUENCY STANDARD

TYPE 2111C

Size, with cover 10" x 17" x 9" H.

Panel model 10" x 19" x 8 34" H. Weight, 25 lbs.

Frequencies: 50 to 1000 cycles Accuracy: (±.002% at 15° to 35°C)

Output: 115V, 75W. Input: 115V, 50 to 75 cycles.





ACCESSORY UNITS

for TYPE 2001-2

L-For low frequencies multi-vibrator type, 40-200 cy.

D-For low frequencies counter type, 40-200 cy.

H-For high freqs, up to 20 KC.

M-Power Amplifier, 2W output.

P-Power supply.

This organization makes frequency standards within a range of 30 to 30,000 cycles. They are used extensively by aviation, industry, government departments, armed forces—where maximum accuracy and durability are required.

WHEN REQUESTING INFORMATION PLEASE SPECIFY TYPE NUMBER

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Assure long-lasting protection of vital connections under a wide range of extreme environmental conditions

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With characteristics of construction and performance never before combined in compact, rugged, lightweight standardized connectors, they exceed NEC requirements and classes A, B, C and E of military specifications MIL C-5015C.

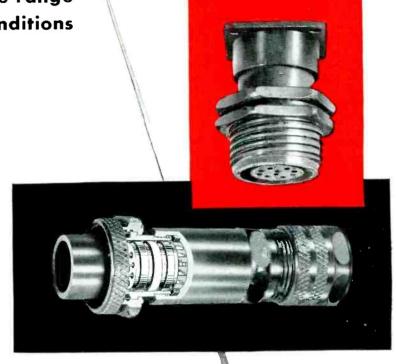
FEATURES

Tough, lightweight shell: Strength comparable to mild steel, yet weighs only $\frac{1}{3}$ as much.

Anodic coating: Gives shell toughness of case-hardened steel. Takes up to 1800 volts to penetrate coating. "Sandwich" insulation: Silicone laminate floats between two rigid discs. Silicone disc absorbs shock, lets contacts align themselves freely; rigid discs impart just the right amount of restraint, Gives all advantages of both flexible and rigid mountings.

Chamber sealing: Silicone insulation disc positively and completely prevents water, gas, moisture or dust from passing into shell.

Wide range of pin and socket configurations: Configurations from 2 to 100 poles available. Within each form size all inserts are interchangeable and reversible.



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Temperature	—80 F. to 225 F.		
Pressure	300 PSI External, 200 PSI Internal		
Chemical Resistance	Most acids, most alkalis, oil		
Corrosion Resistance	Salt Spray: 300 days without failure		
Dust Resistance	Exceed requirements of MIL C-5015C		
Shock Resistance	50G Minimum		
Vibration	Exceed 20G to Method II of Mil C-5015C		
Humidity & Moisture Resistance	Exceed Class E. Spec. of Mil C-5015C		
Air Leakage Meet Class E Spec. of Mil C-5015			

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the PYLE-NATIONAL company

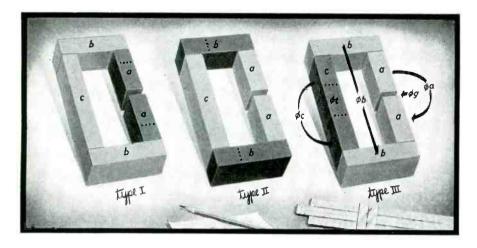


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How You Can Save Time Estimating Leakage Factors for Magnetic Circuits

Computing even approximate values for leakage flux in magnetic circuits is a time consuming job. The research department of Indiana Steel recently undertook a series of studies, supported by the U.S. Air Force, to simplify these computations. Dr. R. K. Tenzer reported the results of this work, which reduce the time in computing leakage flux up to 90% by diminishing the number of mathematical operations necessary.

The investigations were done on circuits with permanent magnets; the results were also found applicable to unsaturated electromagnetic circuits when the coilcovered parts were treated as permanent magnet parts.

After checking values obtained by this method with actual measured values for many Type I, II, and III magnetic circuits, deviations were found to be less than $\pm 10\%$.

Leakage Flux, Leakage Factor

Because of magnetic leakage, only a part of the total flux through the neutral zone of the permanent magnet is found in the air gap. The difference between these two values is known as leakage flux. Mathematically this is:

$$\phi_L = \phi_t - \phi_g. \tag{1}$$

In practical design, leakage is best considered as a factor stated thus:

$$\sigma = \frac{\phi_t}{\phi_g} = 1 + \frac{\phi_L}{\phi_g}.$$
 (2)

For simplification, the flux can be assumed to follow three basic, probable paths: ϕ_a between parts a, ϕ_b between parts b, and ϕ_c along part c. The equation above then becomes:

$$\sigma = 1 + \frac{\phi_a + \phi_b + \phi_c}{\phi_g}.$$
 (3)

With $\phi = mmf \times P$, this formula can be written:

$$\sigma = 1 + \frac{1}{P_o} \left(\frac{mmf_o}{mmf_o} P_o + \frac{mmf_b}{mmf_o} P_b + \frac{mmf_c}{mmf_o} P_c \right) . \tag{4}$$

Letting the mmf ratios be denoted by K,

$$\sigma = 1 + \frac{1}{P_g} \left(K_a P_a + K_b P_b + K_c P_c \right) . \tag{5}$$

This becomes the basic equation for numerical calculations of leakage factors after introducing simple expressions for leakage permeances and mmf ratios.

Simplified Leakage Permeances

The following formulas have been found satisfactory for leakage permeances between soft steel parts:

$$P_a = 1.7 \times U_a \times \frac{a}{a + L_g}$$
 where U is (6)

cross-section perimeter

$$P_b = 1.4 \times b \times \sqrt{\frac{U_b}{c} + .25} \tag{7}$$

where U_b/c is greater than .25 and less than 4. The total length of part b is used.

Since permanent magnets have a neutral zone which does not contribute to leakage, the value of 2/3 of the magnet's total length is used when computing leakage permeances—this is the effective length a' and b' to compute P'; thus the two equations above become:

$$P'_{a} = 1.7 \ U_{a} \frac{.67a}{.67a + L_{a}}$$
 (6a)

and

$$P'_{b} = 1.4 \times .67b \sqrt{\frac{U_{b}}{c} + .25} = .67 P_{b}.$$
 (7a)

When part c consists of a permanent magnet (Type III) its permeance can be calculated as:

$$P_c = .5 U_c. ag{8}$$

The permeance of the air gap itself is

$$P_{g} = A_{g}/L_{g} . {9}$$

Simplified MMF Ratios

Simplifying the *mmf* ratios is done by neglecting the reluctance in *soft steel parts*; so

$$mmf_a = mmf_b = mmf_g \text{ or } K_a = K_b = 1$$

 $(mmf_c = 0 \text{ so } K_c = 0).$ (10)

Since the mmf along permanent magnet parts is not constant, integral values (\overline{mmf}) are used. Experiments showed that 2/3 of the mmf, was the effective mmf for leakage flux between permanent magnet parts; thus

$$\overline{mmf_a} = \overline{mmf_b} = \overline{mmf_c} = 2/3 \ mmf_g$$

or

$$K_a = K_b = K_c = 2/3.$$
 (11)

Basic Formulas

By inserting the permeances for soft steel into equation (5), the general formula becomes:

$$\sigma = 1 + \frac{L_o}{A_o} \left(K_a \times 1.7 \ U_a \frac{a}{a + L_o} + K_b \times 1.4 \ b \sqrt{\frac{U_b}{c} + .25} + K_c \times .5 \ U_c \right). \tag{12}$$

This formula contains only constants and dimensions; and by the two following rules this can be modified into the three basic equations for the Type I, Type II, and Type III circuits.

Rules: (1) For leakage flux paths between soft steel parts, use total lengths and constant K of 1. (2) For leakage flux paths between permanent magnet parts, use 2/3 of lengths and K of .67.

The following provide the leakage factors for the three types of circuits:

$$Type \text{ I:}$$

$$\sigma = 1 + \frac{L_{\varrho}}{A_{\varrho}} \times .67 \times 1.7 \ U_{a} \frac{.67a}{.67a + L_{\varrho}}$$

$$Type \text{ II:}$$

$$\sigma = 1 + \frac{L_{\varrho}}{A_{\varrho}} \left(1.7 \ U_{a} \frac{a}{a + L_{\varrho}} + .67 \times .67 \times 1.4b \sqrt{\frac{U_{b}}{c} + .25} \right)$$

$$Type \text{ III:}$$

$$\sigma = 1 + \frac{L_{\varrho}}{A_{\varrho}} \left(1.7 \ U_{a} \frac{a}{a + L_{\varrho}} + 1.4b \sqrt{\frac{U_{b}}{c} + .25} + .67 \times .5 \ U_{c} \right)$$

For variations on these basic formulas, write today for the April-June issue of *Applied Magnetics* which also shows examples of the formulas in use.

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Write today for your copy of the newest edition of the Indiana Permanent Magnet Design Manual No.6.Write to Dept. A-12.

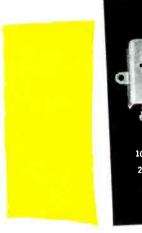


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THE HEART



is an Airpax. Chopper

A chopper amplifier extends the range of this null-reading VTVM down to 0 ± 0.01 DC volt. An Airpax Type 175 chopper modulates the input signal at 60 CPS so that it can readily be amplified and then the chopper synchronously rectifies the signal and returns it to the DC portion of the meter.

Here is another example of how a reliable chopper helps provide the stability essential to modern electronic equipment. This particular instrument is one of the precision laboratory meters developed by John Fluke Manufacturing Co., Seattle, Washington.

Type 175 chopper is one of the Airpax family of miniature choppers. For full details just write to

CHARACTERISTICS OF TYPE 175 CHOPPER

Drive

Frequer cy - - - - 60 \pm 3 CPS Voltage - - 6.3 \pm 0.6 RMS volts

Contacts

Dwell Time - 167 ± 10 electrical deg.
Balance - within 15 electrical deg.
Phase angle - 20 ± 5 electrical deg.
Voltage - - up to 100 DC volts
Current - - - - up to 2 MA
Noise - - 50 microvolts average
Life - - - - 2,000 hours

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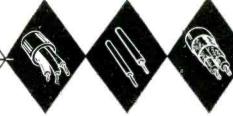




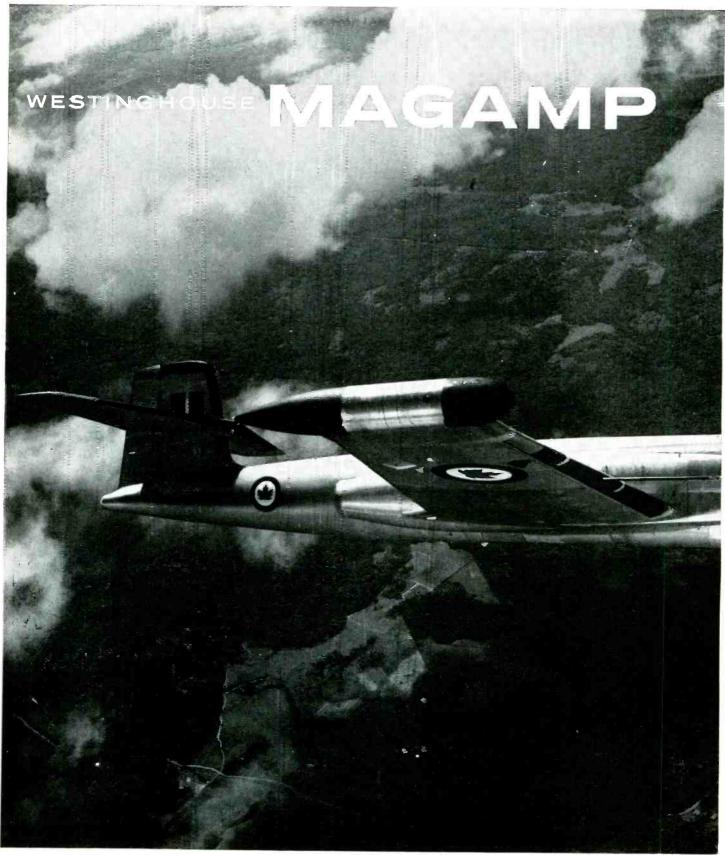
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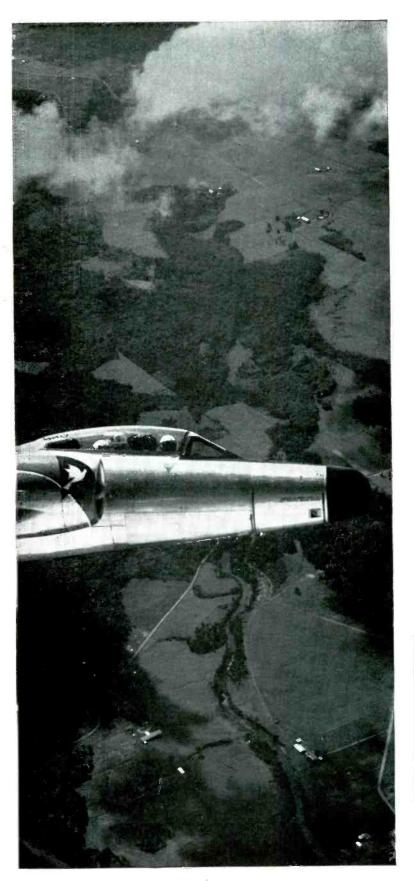
WORCESTER, MASSACHUSETTS







Another Example of CREATIVE MAGAMP ENGINEERING By Westinghouse



World's Lightest Magnetic Amplifier Regulator Unit...Capable of Voltage Regulation Plus or Minus 1 Volt up to 120°C.

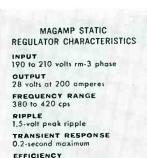
The high altitude missile-carrying CF-100 Mark VI, designed and developed by Avro Aircraft Ltd., of Canada, is undergoing advanced flight testing. Complete dependability and fast response are critical in control and power supply components for these all-weather aircraft. That's why Westinghouse transformer-rectifier unit with MAGAMP* static control was specified — it assures electrical system reliability over a wide range of temperatures and altitudes on aircraft and guided missiles.

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maintenance or adjustments.



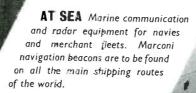
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OHMITE offers the complete line of RESISTORS to meet MIL-R-26C characteristics

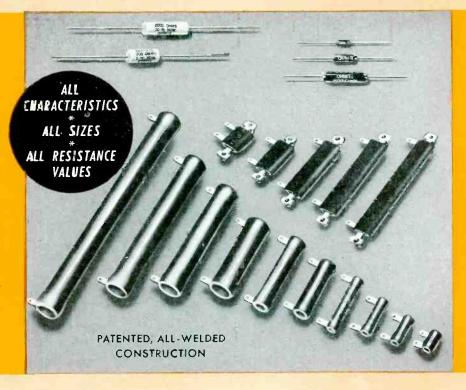


TAB- TERMINAL TYPE Characteristics V and G	Style RW-29 RW-30 RW-31 RW-32 RW-33 RW-35 RW-36 RW-37 RW-38 RW-47	Over-all Length Diameter 134"	*Watts 8 8 10 12 18 38 54 78 110 145	††Watts 11 11 14 17 26 55 78 113 159 210
TAB- TERMINAL TYPE Characteristic Y	Style RW-30 RW-33 RW-37 RW-47	Over-all Length Diameter 1" 19/32" 3" 19/32" 6" 1-5/16" 10½" 1-5/16"		†Watt 11 26 113 210
FLAT TAB- TERMINAL TYPE (Stack Mounting) Characteristics V and G	Style RW-20 RW-21 RW-22 RW-23 RW-24	Width and Over-all Thickness Length of Core 2½" 3½" 1-3/16" 4¾" x 6" ¼" 7¼"	*Watts 15 22 37 47 63	††Watt 21 31 53 68 91
AXIAL- TERMINAL TYPE Characteristics V and G	†Watts free	Length of Core** Diameter 138" 15/32" 2" 15/32" 1" 5/16" 178" 11/32" ½" 3/16" air MIL Characteristic "G." air MIL Characteristic "Y." air MIL Characteristic "Y."	*Watts 5 10 5 8 2.5 **1-½	††Wat 7 14 6, 11 3

Even including resistors wound with the finest wire size (.00175)

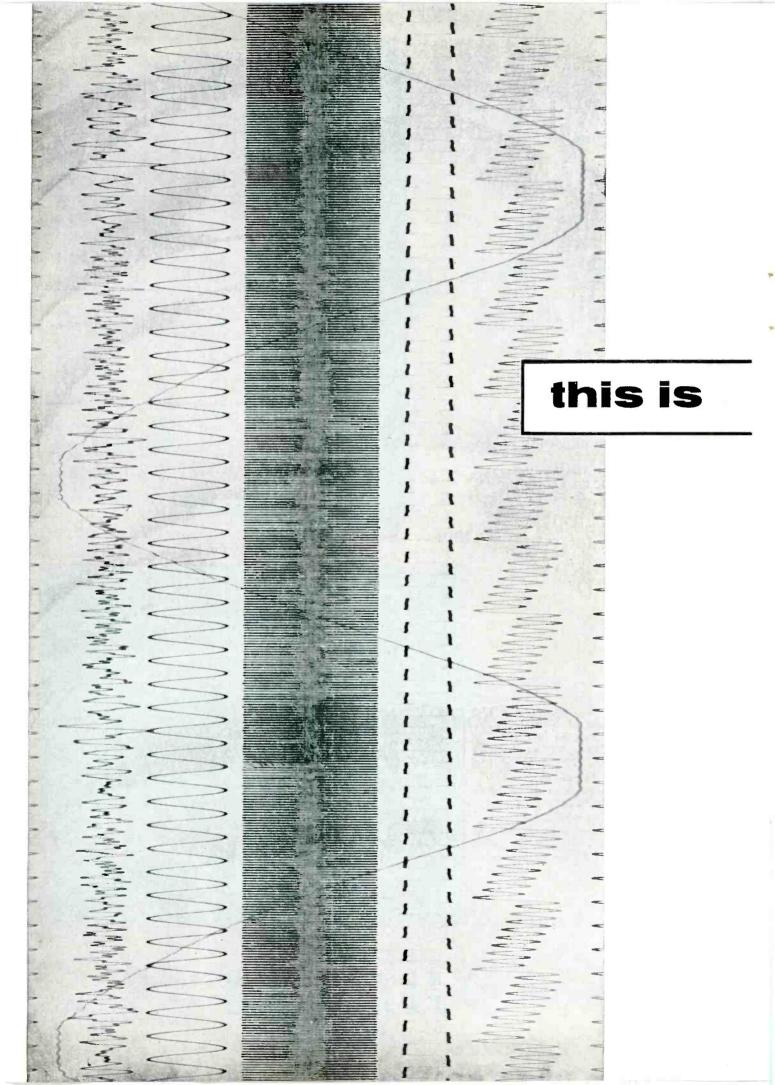
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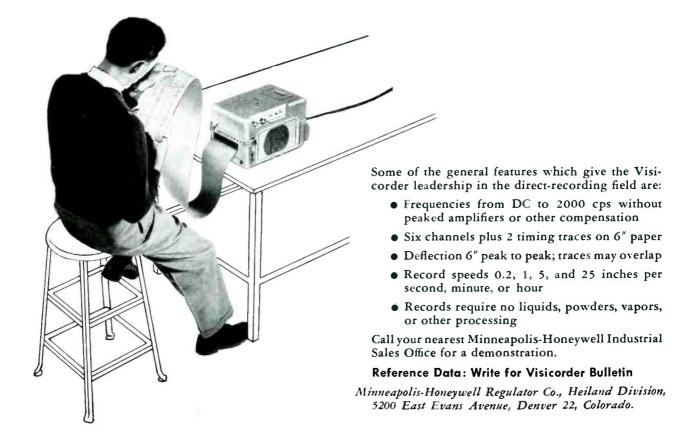


This Visicorder Oscillograph record* is a symbol of the leadership that is typical of Honeywell engineering. In laboratories all over the world the Visicorder's instantly-readable direct records are showing the way to new advances in rocketry, control, computing, product design and component test and in nuclear research.

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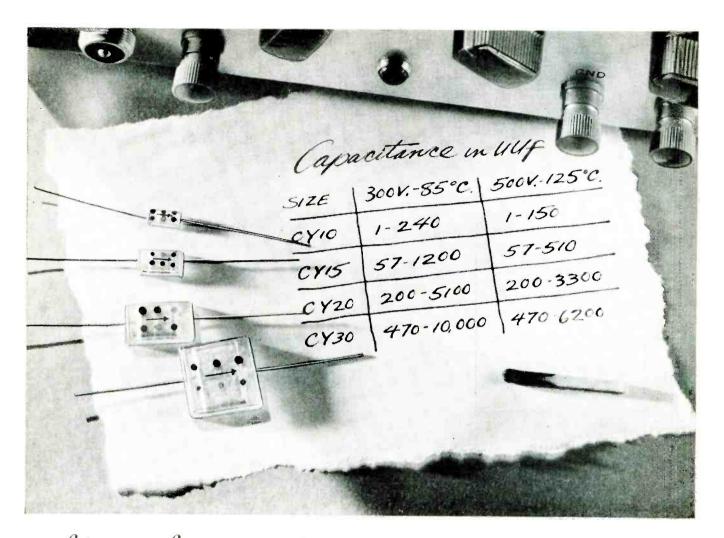
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CY15	57-1200	57-510
CY20	200-5100	200-3300
CY30	470-10,000	470-6200

85° C., the average change in capacitance of these units is less than 0.4% after 1,000 hours, less than 0.6% after 10,000 hours.

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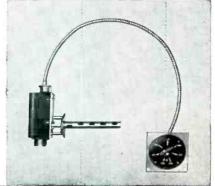
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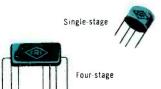








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Continued on next page . . .







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MODEL 1 RADIOHM

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Model 3 Radiohm®

now with I.C.E.*

The Centralab Model 3 Radiohm, with its exclusive *Interfused Composition Element, provides unbelievable wattage dissipation, yet is smaller than a dime.

This miniature rotary potentiometer, with its rugged element, is ideally suited for high-temperature operations in both commercial and military applications.

Advanced design features offer you both standard and lockingtype bushings. Each is available with sealed construction to meet today's demand for a unit that can be potted.

For immediate delivery in ratings from 1,000 ohms to 2.5 megohms, ask your local Centralab distributor for the JP and JL series.

typical watt-hour rating Only 10% maximum resistance change, when used at . . .

 $1\ \text{watt}$ for $1\text{-}1/2\ \text{hours}$

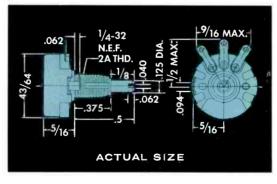
3/4 watt for 35 hours

1/2 watt for 80 hours

1/3 watt for 300 hours

1/4 watt, continuous rating





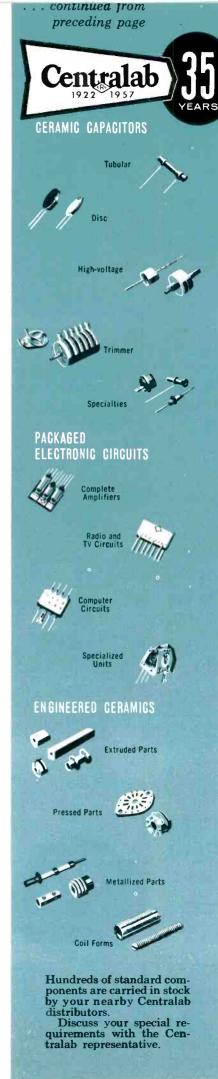
Write today for Technical Bulletin EP-63, for complete engineering data



Circle 151 Reader Service Card

A DIVISION OF GLOBE-UNION INC.

914 E. Keefe Ave. Milwaukee 1, Wis. In Canada: 804 Mt. Pleasant Road Toronto, Ontario



A.C. Ratiometer

... accurate to five parts per million!

REFERENCED TO UNITY RATIO

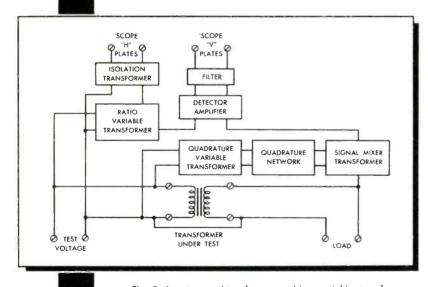


The Transformers, Inc. Ratiometer is a precision instrument to measure any voltage ratio from 0.000001 to 1.111111. Transformer ratios can be accurately measured at "no load" and under full load. Two models are available:

MODEL 204 is designed for use between 200 cps and 2,000 cps. It is supplied with plug-in units for 400 cps operation.

MODEL 206 is designed for use between 40 cps and 1,000 cps. It is supplied with plug-in units for 60 cps operation.

Plug-in units for any other frequency are supplied to order.



The Ratiometer consists of two precision voriable transformers, a calibrated quadrature injector, a filter, and a pre-amplifier. Block diagram indicates connections of the various components within the instrument.

ACCURACY

Five parts per million referenced to unity ratio.

MAXIMUM VOLTAGE

	100 1/	200
Model 204	120 V	200 cps
	180 V	300 cps
	240 V	400 cps and over
Model 206	80 V	40 cps
	120 V	60 cps
	240 V	120 cps and over

PRICE

Model 204 Ratiometer, complete with 400 cps plug-in filter and quadrature units \$865

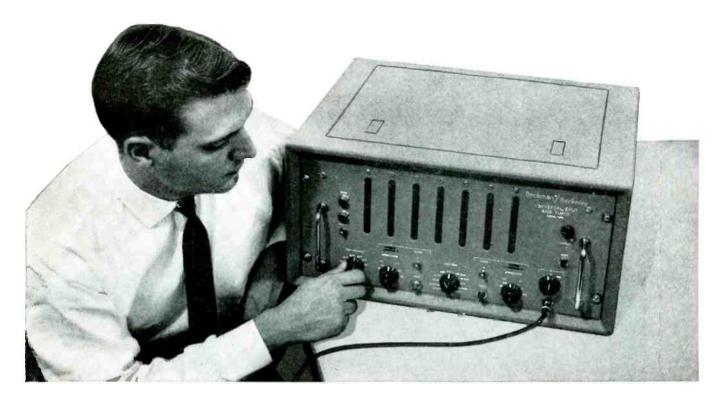
Model 206 Ratiometer, complete with 60 cps plug-in filter and quadrature

\$1235

For additional information, ask for Bulletin #204

TRANSFORMERS, INCORPORATED

200 Stage Road, Vestal, N.Y.



SMALL...SELF-CONTAINED...10 MC CAPACITY!

- Frequency measurements at 0.1 v rms over 0 cps-10 mc, without heterodyning or plug-ins
- 10 operating functions and three input channels for maximum application flexibility
- 7-place direct digital readout -- no meter indicators
- Priced at only \$1975.00

Beckman/Berkeley Model 7370 Universal EPUT® and Timer

BRIEF SPECIFICATIONS

Model 7370

Functions:

E/UT, E/UT \times 10, SCAN, COUNT, TIM, PER, PER \times 10, E/B, E/B \times 10, E/B-A, (TEST)

Ranges:

Frequency: 0 cps to 10 mc Period: 0 cps to 3 mc Time Interval: 0.3 μsec to 10^7 sec Ratio: 1 to 107 from 10 cps to 10 mc

Time Bases:

0.1 µsec to 10 sec in decade steps

Accuracy:

±1 count ±oscillator stability

Oscillator Stability:

3 parts in 107 per week

Price:

\$1975.00 F. O. B. Richmond, California

Developed specifically to meet the test instrumentation needs of today Model 7370 is a completely self-contained precision instrument capable of handling a broad range of frequency, frequency ratio, and time interval measurements easily, dependably and with extreme accuracy. The most modern counter-timer obtainable, it features three input channels for greater application flexibility; field-proved components; advanced circuitry; modular chassis construction; binary coded output from all DCU's for driving auxiliary equipment such as a digital recorder.

Half the size of conventional instruments of its type, Model 7370 weighs only 62 pounds. Input impedance is 1 megohm; available output frequencies, 1 cps to 1 mc; accuracy, ± 1 count. Built-in self-test facility checks correct operation of all frequency dividers and DCU's. Optional Standard Modifications, including provision for flow meter input, expand the laboratory and in-plant utility. Controls are functional, and so simple that non-technical personnel can be readily trained in their use.

Complete technical details on the Beckman/Berkeley Model 7370 Universal EPUT and Timer are available on request. Write to Department G12



2200 Wright Avenue, Richmond 3, California a division of Beckman Instruments, Inc.

Another NEW CLARE PLANT to give you relays of unequaled quality

- Telephone type relays (ac and dc)
- Hermetically sealed relays
- Computer relays
- Video relays
- Power relays
- Mercury-wetted contact relays
- Relay banks
- Plate circuit relays
- Stepping switches
- Lever, push and turn keys
- Other special relays



New C. P. Clare & Co. plant at Fairview, N. C. will expand manufacturing facilities which have been under way in Fairview for two years.

Before midyear 1958 CLARE will be serving customers from a new factory at Fairview, N. C.—a facility that will matter the manufacturing advantages of cur Chicago plant, itself only five years o c.

This CLARE expansion is made necessary by the tremendous growth of the electronics industry and the increasing demand for precise components, including relays whose life can be measured in billions of operations.

Facilities of virtually clinical cleanliness are required for this kind of precision. That's why CLARE plants in both

Chicago and Fairview maintain complete control of the temperature, humidity and cleanliness of the air...immaculate walls and floors...powerful, shadowless lights, for assembly of small parts.

If yours is a product whose long life, reliable performance and freedom from maintenance depends on relays, it will pay you to know ALL about CLARE relays. C. P. Clare & Co., 3101 Pratt Blvd, Chicago 45, Illinois. In Canada: C.P.Clare Canada Ltd., 2700 Jane Street, Toronto 15, Ontario. Cable Address: CLARELAY

CLARE RELAYS

FIRST in the industrial field

Multi-channel—telegraph A1 or telephone A3

High stability (.003%) under normal operating conditions

Components conservatively rated. Completely tropicalized



W. 37th

FROM GROUND TO AIR OR POINT TO POINT

Here's the ideal general-purpose high frequency transmitter! Model 446, suitable for point-to-point or groundto-air communication. Can be remotely located from operating position. Coaxial fittings to accept frequency shift signals.

This transmitter operates on 4 crystal-controlled frequencies (plus 2 closely spaced frequencies) in the band 2.5-24.0 Mcs (1.6-2.5 Mcs available). Operates on one frequency at a time; channeling time 2 seconds. Carrier power 350 watts, A1 or A3. Stability .003%. Nominal 220 volt, 50/60 cycle supply. Conservatively rated, sturdily constructed. Complete technical data on request.

Now! Complete-package, 192 channel, H.F., 75 lb. airborne communications equipment by Aer-O-Com! Write us today for details!



A-131

LABORATORY MODEL (686) A true mutual conductance analyzer that tests tubes under actual circuit operating potentials. Overall GM accuracy is 3% or better. Transconductance is measured directly without need for null adjustments or corrections, providing GM readings on all receiving type tubes. Circuit is mathematically calibrated and requires no calibrated tubes for GM circuit standardization. A real laboratory for electron tubes, Model 686 is entirely self-contained, with a filtered d-c power source, special circuitry to keep meter loading effects negligible, and a well regulated grid bias supply. WESTO

PORTABLE MODEL (981)

- Filtered d-c potentials provide better GM accuracy.
- Voltage divider network for better grid bias settings.
- Four signal levels provided protect against excessive grid current surges.
- Provision for tube interelectrode leakage measurements as high as 10 megohms.

Whether for production quality control . . . laboratory analysis of tube characteristics . . . or quick accurate servicing of electronic equipment, WESTON tubecheckers are acknowledged leaders for accuracy, time-saving facility, and long term dependability. These and other Weston test instruments are available through leading distributors. Bulletin available by writing WESTON INSTRUMENTS, Division of DAYSTROM, INC., 614 Frelinghuysen Avenue, Newark 12, New Jersey.



WESTON TEST EQUIPMENT



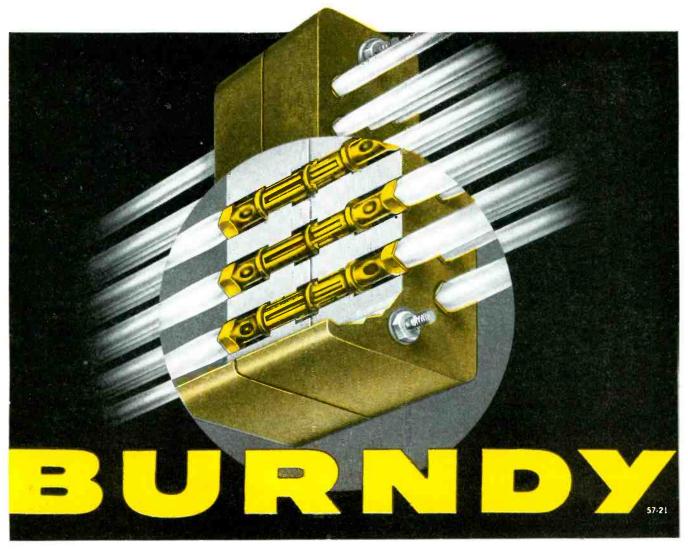
HYFEN

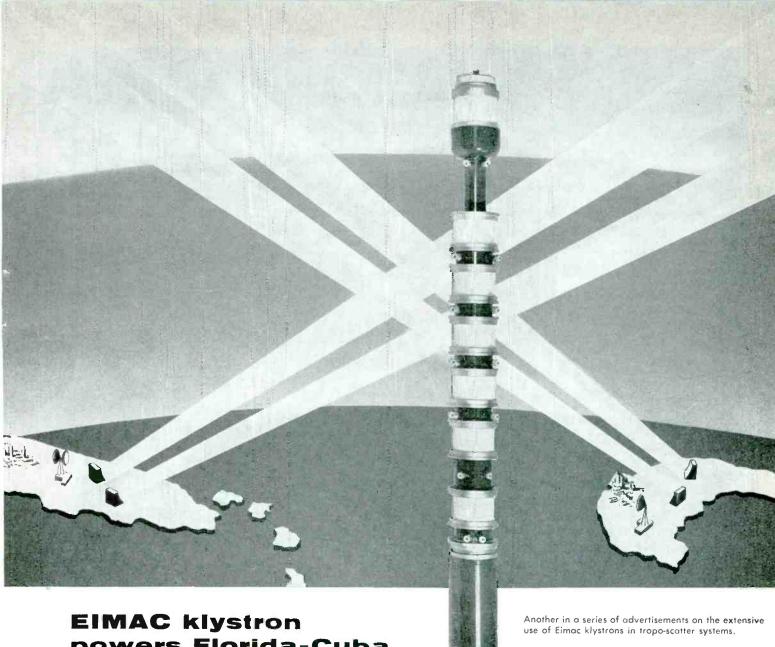
a big step toward automation of wiring

harnesses

Crimped pins and sockets snap-locked in plug or receptacle. Individual circuit removal or gang disconnect.

Hyfen ends the need for time consuming solder operations - and the high rejection rate inherent with solder. Pins and sockets are speedily crimped on wire ends by automatic installation tooling - or where more convenient, by bench or hand tools. Dies control and provide a uniform depth of indent which can be inspected by depth micrometer assuring absolute unvarying reliability. Crimping may be done before or after harness is in place. Hyfen meets or exceeds MIL specifications for voltage drop, dielectric strength, contact engaging force, and contact retention force. It provides high corrosion resistance since there are no fluxes or dissimilar metals involved. Floating contacts in both plug and receptacle make for uniform mating and disconnecting " force by the alignment flexibility provided. Hyfen principle is not limited as to size, shape of plug and receptacle nor to number or size of connections. Wire for bulletin. Burndy, Norwalk, Connect.-Scarboro, Canada





powers Florida-Cuba tropospheric bridge

Federal Telecommunication Laboratories O/H tropospheric equipment built for American Telephone and Telegraph Company and International Telephone and Telegraph Company spans the gap between Florida and Cuba, transmitting TV programs simultaneously with multi-channel telephone service.

Each site of this joint A. T. & T. and I. T. & T. system employs two transmitters and four receivers to obtain space and frequency diversity. Radio equipment has sufficient band

width to handle a television program and 120 or more telephone messages.

In the final amplifier of the FTL 12-1 System, engineers specified the Eimac 6K50,000LQ. This six cavity water cooled klystron delivers 10 kw rf output power in FTL equipment with a power gain of 1000 times and band widths to 20 mc.

EITEL-MCCULLOUGH, INC.

Eimac First for high-power amplifier klystrons.

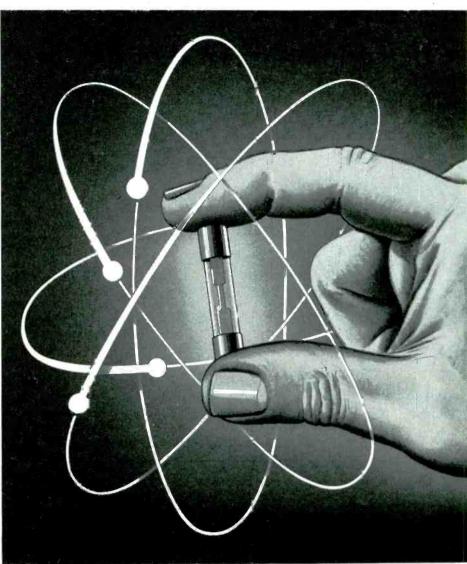


6K50,000LQ KLYSTRON AMPLIFIER

Electrical	
Power Output	
Frequency Range	
Gain	reater than 50 db. (Narrow band)
	16 KV DC
Beam Current	1.62 Amps

Mechanical	
Cathode	Bombarded
Number of Cavities.	
Overall Length.	58"
Outside Diameter	
RF circuitry including tube 26"	diameter x 61" high





ELECTRONICALLY TESTED BUSS FUSES

can help safeguard you against troubles and complaints

With BUSS fuses, dependable electrical protection is not left to chance. Every BUSS fuse is tested in a sensitive electronic device that automatically rejects any fuse not correctly calibrated, properly constructed and right in all physical dimensions.

As a result, when you specify BUSS fuses you are sure the fuse will operate properly under all service conditions. You avoid 'kicks' or complaints from users about faulty fuses failing to

protect or causing needless shutdowns.

By their unfailing dependability, BUSS fuses help you safeguard the reputation of your equipment for quality and reliability.

Should you have an unusual problem in electrical protection . . .

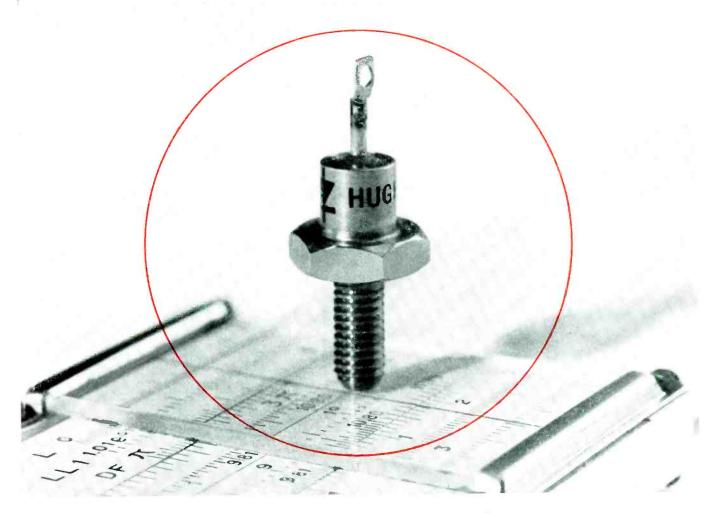
... the BUSS fuse engineers are at your service — and in many cases can save you engineering time by helping you choose the right fuse for the job. Whenever possible, the fuse selected will be available in local wholesalers' stocks, so that your device can be serviced easily.

For more information on BUSS and FUSETRON Small Dimension fuses and fuseholders . . . Write for bulletin SFB. Bussmann Mfg. Division McGraw-Edison Co., University at Jefferson, St. Louis 7, Mo.

BUSS fuses are made to protect-not to blow, needlessly



MAKERS OF A COMPLETE LINE OF FUSES FOR HOME, FARM, COMMER-CIAL, ELECTRONIC, AUTO-MOTIVE AND INDUSTRIAL USE.



announcing a new Hughes series high efficiency, medium power silicon rectifiers

For the first time, you can obtain high forward conductance and a high breakdown voltage, together in one rectifier. High forward conductance increases the efficiency of the rectifier, thereby providing *more* power to the load at lower junction temperatures. And low junction temperatures ensure long life plus reliable rectifier operation.

The unique combination of high forward conductance and high breakdown voltage permits rectifier performance never before achieved in the standard EIA Group 20 (7/16" hex.) stud mounted package. This package is welded and hermetically sealed with a glass-to-metal seal to provide complete protection from contamination and moisture penetration. Inside, where it counts, protection like this is essential.

		1
The HR10681, a typic	al	4
rectifier in the series.		
Min. Breakdown Voltage	= 600V	100
Max. Average Rectified Current @ 25°C	= 2A*	H.
Average Reverse Leakage Cur @ 2A and 420V _{rms} @ 25°C	rent ≦ 100µA	
Typical Full Load Average Forward Voltage Drop	≦ 1.0V	
Typical Dynamic Forward Resistance	≦ 0.2ohm	
*Higher currents obtainable w	vith heat sink.	actual size

Our sales engineers welcome the opportunity to discuss application of these new units to your circuitry. For address of sales office nearest you, or for complete information, write: SEMICONDUCTOR DIVISION • HUGHES AIRCRAFT CO. International Airport Station. Los Angeles 45, California

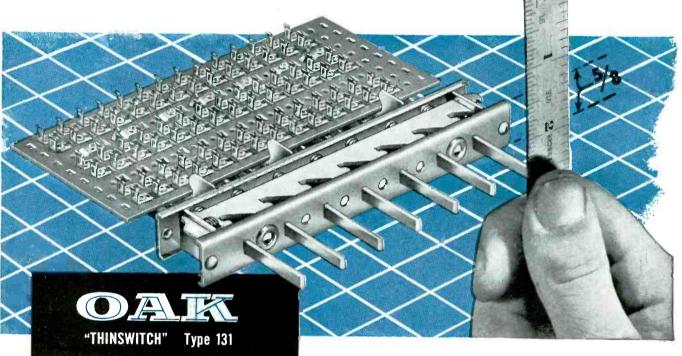
Creating a new world with ELECTRONICS





© 1957, HUGHES AIRCRAFT COMPANY

thinnest pushbutton switch



FEATURES

- Measures only 5/8" thick.
- 1 to 12 buttons, standard, with 5/8" spacing.
- Up to 14 contacts per button.
- "Floating" slider design for smooth, easy operation.
- Famous Oak double-wiping contacts.
- Highest grade phenolic punching stock.

REQUIRES 45% LESS PANEL AREA!

This new Oak switch is particularly valuable as a spacesaver in keyboards handling complicated, low-current circuits. The Type 131 can be mounted side by side on ¹¹/₆" centers, so that a bank of 10 switches, for example, requires only 6^{13} /₆".

Thus, in equipment such as computers, testers, automatic coin devices, and communications gear, the Type 131 offers extra flexibility in laying out panel areas, or actually permits a decrease in the size of the equipment.

Type 131 switches are built to your exact requirements with the same high quality materials and workmanship as other Oak switches. Call in your Oak representative, or write for full technical details.

















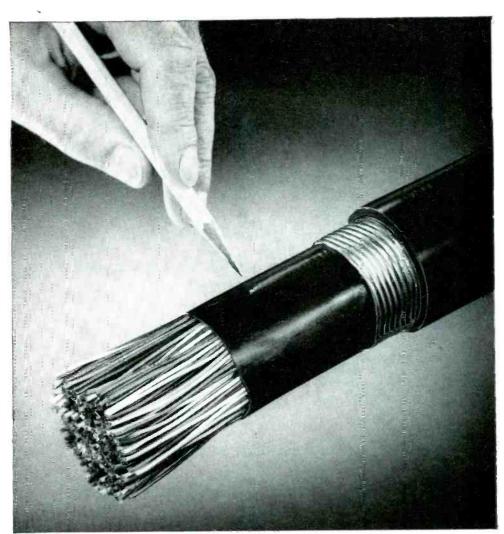
SWITCHES

ROTARY

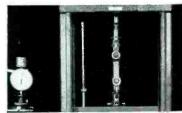
CHOPPERS

VIBRATORS SUBASSEMBLIES

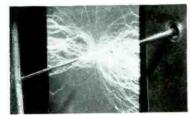
1260 Clybourn Ave., Dept. G, Chicago 10, Illinois Phone: MOhawk 4-2222



"MYLAR" offers a unique combination of properties valuable for electrical design



HIGH TENSILE STRENGTH. "Mylar" is the strongest plastic film. Instron tester shows an a verage strength of 20,000 lbs. psi.



HIGH DIELECTRIC STRENGTH. Average of 4,000 volts per mil... average power factor of 0.003 to 60 cycles... dielectric constant above 3.0 at 72°F., 1,000 cycles.



THERMAL STABILITY. "Mylar" has an effective operating range from -80° to 300°F....won't become brittle with age.

Core binder tape made with Du Pont MYLAR® helps Western Electric speed production of communication cable

PROBLEM: Western Electric's new long-life, high-dielectric communications cable posed a challenging problem for production engineers. The problem was this—how to efficiently extrude an outer jacket of polyethylene without fusing the inner pairs of wires also coated with polyethylene.

SOLUTION: After extensive tests with



BETTER THINGS FOR BETTER LIVING ... THROUGH CHEMISTRY



combinations of materials, a tape of DuPont"Mylar"*polyester film and rubber was selected to act as a heat barrier.

RESULTS: Western Electric reports that abrasion-resistant "Mylar", with its hard, durable surface, helps the core binder tape run smoothly on its equipment without snagging or tearing. Because of its high tensile strength and melting point, "Mylar" helps prevent corrugations of the

electrostatic aluminum shield from breaking through the tape and shorting the cable.

HOW CAN "MYLAR" HELP YOU? Whether you make guided missiles or tinycomponents, you may be able to capitalize on the outstanding combination of properties found in tough, transparent "Mylar" film. For a booklet containing technical data plus information on successful applications, send in the coupon below.

***MYLAR" is Du Pont's registered trademark for its brand of polyester film.

Please send the new book types of "Mylar" polyester	
	Tialo
	Title
Company	
Address	
City	State



SWEEP SIGNAL GENERATOR
TYPE 240-A

PRICE: \$1585.00 f.o.b. Boonton, N. J.



CW Output 4.5 to 120 mc



AM Modulated CW 30% at 1000 cps



Broad Band Sweep ±1% to ±30% of center frequency

In this one instrument -

A SWEEPING, CW, and AM SIGNAL GENERATOR

with Crystal-controlled Markers
4.5mc to 120mc

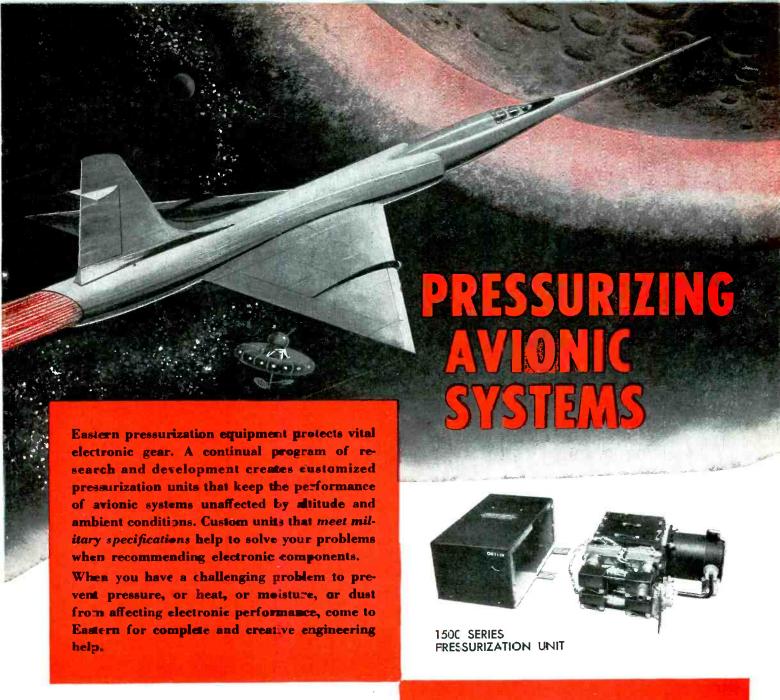
FEATURES:

- All-electronic, AGC-controlled, constant amplitude, variable width linear frequency sweep.
- Extremely low leakage can be used down to 0.1 microvolt.
- RF output level accurately monitored on both CW and sweep.
- Basic frequency accuracy of $\pm 1\,\%$ can be standardized against internal crystal to $\pm .005\,\%$.
- Internal crystal and pip interpolation markers.
- Markers do not pass through system under test internal mixer adds frequency identification to system output.

SPECIFICATIONS

- RF FREQUENCY RANGE: 4.5 to 120 mc continuously variable in five ranges accurate to $\pm 1\%$.
- RF OUTPUT VOLTAGE: 1.0 to 300,000 microvolts continuously variable as swept frequency generator same except 100,000 microvolts maximum on CW accurate to approximately ±10% of full-scale "RF Level" meter readings.
- AM MODULATION: Factory adjusted to 30% from internal 1000 cps
- RANGE OF SWEEP WIDTH: Continuously variable from $\pm 1\%$ of center frequency to ± 15 mc or $\pm 30\%$ of center frequency, whichever is smaller.
- LINEARITY OF SWEPT RF FREQUENCY: Within 10% over middle 80% of sweep excursion, within 20% over remainder.
- FLATNESS OF SWEPT RF OUTPUT: Better than 7% while sweeping for ony combination of output, center frequency, and sweep width.
- MARKER CHARACTERISTCS: Crystal birdie type markers switchable to spacing of 0.1, 0.5, or 2.5 mc accurate to ±0.005%. Two stable pip type markers adjustable to any position on the internal sweep excursion.







EASTERN PRESSURIZATION UNITS

A variety of capacities accommodates a broad range of requirements and meets appropriate government standards. Typical units operate from zero to over 70,000 feet at temperatures from -65°F to +160°F. Delivery: 0-3600 cu. in./m.n. free delivery, Discharge Pressure: 0-60 p.s.i. Standard sub-assemblies and components normally are used to create a custom-made design to fit your exact needs. Units may consist of an air pump and motor assembly, pressure switch, check valve, tank valve, terminal connectors, and dehydrator.

Write for Eastern AVIONICS BULLETIN 340

INDUSTRIES, INC.
100 Skiff St., Hamden 14, Conn.

West Coast Office: 1608 Centinela Avenue Inglewood 3, California — Phone ORegon 8-3958

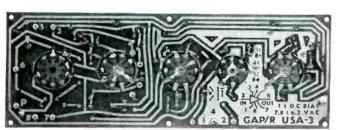


Greater System Accuracy

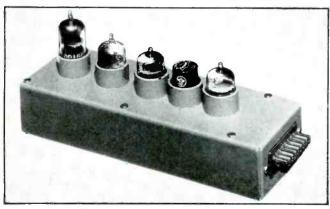
and Reliability with the

- PRINTED CIRCUIT: Economy, reliability and compactness.
- OPEN LOOP D-C GAIN: 10 million.
- LONG TERM DRIFT, NOISE and OFFSET: under 100 microvolts.
- OUTPUT VOLTAGE RANGE: ±115 volts.
- SIZE: 7" x 2½" board.
- MOUNTING: Any convenient method.
- PRICE: \$95.00.

PHILBRICK PRINTED CIRCUIT AMPLIFIER



Underside of Model USA-3 showing printed circuit, amplifier connection scheme, and connecting terminals.



Model USA-3 showing one of the several types of modular packaging available at extra cost.

Model USA-3

High performance combined with the reliability and compactness of a printed circuit design are featured in the new Philbrick Universal Stabilized Amplifier, Model USA-3. It is ideally suited for applications to instrumentation, control and analog computation. Extremely high open-loop d-c gain, wide bandwidth, low noise and wide output range are important performance characteristics of this new chopper stabilized amplifier. An interesting design feature makes this instrument safe against self-destruction, even under prolonged overload conditions or direct grounding of its output. At a price of only \$95.00, it offers more performance per dollar than any other amplifier on the market today. Write to George A. Philbrick Researches, Inc., Dept. 14, for Bulletin USA-3.

PHILBRICK

RESEARCHES, INC.

230 Congress Street, Boston 10, Massachusetts

electro-mechanical computer and control compon v Librascope

DIGITAL CONVERTERS



Most versatile line of shaft position to digital converters models for Gray, Binary, and Binary Coded Decimal Systems. Special models for sinecosine read-out. Used in digital airborne controls, machine tool controls, or wherever position data must be translated into digital form. Ask for Catalog No. E10-1

SINE MECHANISM



Provides for instantaneous solution of problems involving the sine or cosine of an angular variable. Angular rotation is converted into a displacement proportional to sine or cosine of the input. Compact, simple, self-contained design.

Ask for Catalog No. 304062



A complete line of Read-Record Heads for all types of magnetic drum memory systems. Simplicity of design, flexibility of operation, high reading signal and low current are basic character stics of these read-record heads which are used where reliable performance is essertial. Ask for latest Catalog

SC INTEGRATOR



A precision integrating mechanism for totalizing, rate determination, and differential analyzing. Can also be used as a closed loop servoelement for accurate variable speed drive. Small in size, rugged construction for long life; extreme precision.

Ask for Catalog No. 304061



Four models of precision differentials for application to problems of angular sums, angular velocity sums or sequence operations. May be installed or removed without disassembly of unit or differential. High accuracy; unlimited displacement; small radial clearance. A time-tested design.

Ask for latest information

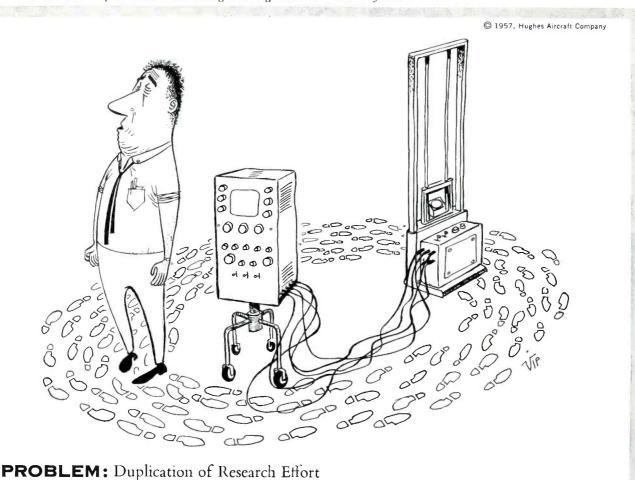
FOR MORE THAN 20 YEARS, Librascope has manufactured mechanical and electrical computers and components for military and commercial purposes.

Librascope products are designed for reliability, long-life, trouble-free performance.

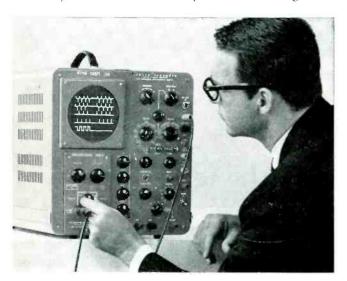
If you have a problem concerning complete computer/control systems, contact Librascope.

Fep-esentatives in principal cities





Even the most patient veteran researchers are often irked in attempting transient analysis using conventional 'scopes. Time and effort wasted in repetitious trial and error to "capture" transients can be a problem of first magnitude.



SOLUTION: Now you no longer need to put up with clusive traces. The answer to your time-duplication dilemma is the new Hughes **MEMO-SCOPE®** Oscilloscope. A storage type oscilloscope, it can instantly "freeze" any number of selected transients—retain single or successive displays brilliantly *until intentionally erased*.

HUGHES MEMO-SCOPE OSCILLOSCOPE

STORAGE TUBE—5-inch diameter Memotron® Direct Display Cathode Ray Storage Tube. Writing speed for storage: 125,000 inches per second. The optional Speed Enhancement Feature multiplies writing speed approximately four times.

OPTIONAL PREAMPLIFIER EQUIPMENT—High Sensitivity, Differential Input, Type HS/6: 1 millivolt to 50 volts per division. Dual Trace Type WB/DI/11: 10 millivolts to 50 volts per division, Four independent positions may be selected for single or double channel performance and chopped or alternate sweeps.

You will want to see this "transient recorder with a memory" demonstrated. Send for Application Data Sheet No. MSAD-A3. and ask for a Hughes representative to arrange a demonstration in your company. Make request to:

HUGHES PRODUCTS MEMO-SCOPE Oscilloscope International Airport Station, Los Angeles 45, California

Creating a new world with ELECTRONICS

HUGHES PRODUCTS



CORPORATION Silicone Dielectrics

ELECTRICAL AND ELECTRONIC NEWS

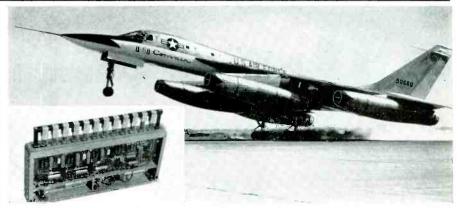
Silicone Insulated Transformers Light-Weight, Maintenance Free

Added proof that you get "more power per pound" and maximum reliability with silicone electrical insulation is provided by Moloney Electric Company's new line of 3-phase, nitrogen filled, dry-type transformers.

Take the 1500 KVA rating, for example: these units weigh only 21,000 pounds and measure less than $9\frac{1}{2} \times 5\frac{1}{2} \times 10$ feet. Silicone-insulated throughout, they can be safely installed almost anywhere regardless of high ambients, contaminated or dust laden atmospheres. In addition, these transformers are virtually maintenancefree; no liquids to maintain, no toxic fumes to guard against.

Contributing to the transformers' efficient performance are the strong, lightweight silicone-glass spacer bars laminated by Formica Company into U-shapes for maximum heat dissipation. Moloney also uses Formica's G-54 silicone-glass for phase barriers and layer insulation.

To complete this all-silicone insulating system, assembled cores and coils are impregnated with Dow Corning 997 Varnish; lead wires are covered with Silastic,* the Dow Corning silicone rubber. *T.M. REG. U.S. PAT. OFF.



SILICONE RUBBER ASSURES RELIABILITY OF ELECTRONIC "PACKAGES" ON B-58

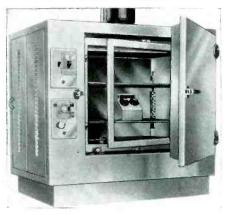
In reaching for new plateaus of performance and reliability, designers are getting an assist from Silastic*, the Dow Corning silicone rubber. Typical is the extensive use of Silastic to insulate and protect the delicate electronic "packages" in the fire control system on Convair's B-58 Hustler.

In developing the "packages," heat was a major problem encountered by the designers-the Electronics and Avionics Division of Emerson Electric Manufacturing Company. Certain rubber parts touch miniature tubes that operate at 350 F. Other rubber components, such as seals, cable grommets and clamps, are totally enclosed in packages where even the "cooling" air gets hot. Extreme cold is another problem. When the fire control system is shut off during high altitude flight, temperatures may drop to 65 below zero.

But Silastic easily withstands both extremes of temperature and physical punishment. It stays rubbery from -130 to 500 F, has excellent dielectric strength, moisture resistance and long life. That's why Emerson specified Silastic, and that's why more and more engineers are specifying Silastic for maximum serviceability and minimum maintenance cost in applications ranging from aircraft seals to industrial heaters, from traction motors to home appliances. *T.M. REG. U.S. PAT. OFF.

Silicone Fluids on Insulators Stops Shorts and Grounds

Imaginative use of a silicone fluid has enabled Blue M Electric Company, Blue Island, Ill., to engineer faster response and more accurate heat control into its laboratory humidity cabinets.



Moisture condensation on the steatite grommets that support the resistance wire

heating elements was always a problem in these cabinets. Moisture caused such a low resistance to ground that the elements had to be sheathed. This, of course, reduced the heat-up speed and made it more difficult to maintain accurate temperatures in the cabinets.

Blue M now controls the condensation problem by simply coating the ceramic insulators with Dow Corning 200 Fluid. The resulting water-repellent silicone surface is so successful in preventing the formation of conducting moisture films that the treated insulators withstand 1000 volts to ground even with droplets of water on their surface. As a result, Blue M has been able to change to faster, more accurate "open" elements without fear of grounds or shorts.

Blue M uses a 2% solution of Dow Corning 200 Fluid in carbon tetrachloride. The insulators are dipped into this solution and baked for one hour at 575 F. No. 61

Send Coupon for More Information

DOW CORNING CORP	DRATION	- Dept. 4	824
Please send me	59	60	61
NAME	_		
TITLE			
COMPANY			
STREET			
CITYZ	ONES	TATE	

ATLANTA . BOSTON . CHICAGO . CLEVELAND . DALLAS . DETROIT . LOS ANGELES . NEW YORK . WASHINGTON, D. C. Canada: Dow Corning Silicones Ltd., Toronto: Great Britain: Midland Silicones Ltd., London: France: St. Gobain, Paris



INSULATION RESISTANCE and CAPACITANCE STABILITY

POWER FACTOR and SOAKAGE

Polystyrene Capacitors are wound with



Film Capacitors, Inc., New York, manufactures capacitors for critical AC and DC circuitry applications—such as bridge arm elements, filter network components, standards of capacitance, RF tank circuits, storage circuits and computer circuits—where stability and high Q are essential.

Natvar Styroflex film is used as the dielectric in f-c-i polystyrene capacitors because of its uniformly high shock resistance and excellent dielectric properties. Because of its bi-axial orientation during the manufacturing process, it is completely flexible in all thicknesses, and easy to handle.

If you need an insulating material with the desirable characteristics of polystyrene—plus pliability, it will pay you to investigate Natvar Styroflex.



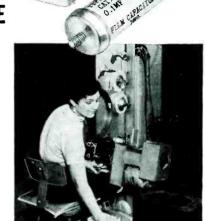
CORPORATION

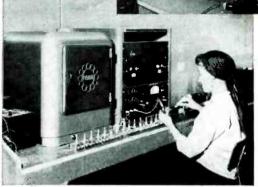
FORMERLY THE NATIONAL VARNISHED PRODUCTS CORPORATION
TELEPHONE CABLE ADDRESS

FULTON 8-8800

239 RANDOLPH AVENUE • WOODBRIDGE, NEW JERSEY

CABLE ADDRESS NATVAR: RAHWAY, N. J.





f-c-i polystyrene capacitors are available in hermetically sealed glass tubes, metal shells, bathtub cases, or metal cans. Operators like Styroflex because it winds easily, and testers find a minimum of rejects.



Natvar Products

- Varnished cambric—cloth and tape
- Varnished canvas and duck
- Varnished silk and special rayon
- Varnished—Silicone coated Fiberglas
- Varnished papers—rope and kraft
- Slot cell combinations, Aboglas[®]
- Isoglas[®] sheet and tape
- Isolastane[®] sheet, tape, tubing and sleeving
- Vinyl coated—varnished tubing and sleeving
- Extruded vinyl tubing and tape
- Styroflex® flexible polystyrene tape
- Extruded identification markers

Ask for Catalog No. 24



Microwave cooking shaves hours from food preparation time. This is a home-type electronic oven developed by Raytheon for production by appliance manufacturers.

Meals in minutes by electronics in permanent magnet equipped range

Microwave energy does the cooking in this domestic electronic oven based on Raytheon's "Radarange" for the restaurant industry. Microwaves are

far higher in frequency than broadcast waves—fact, the magnetron tube (at left) steps up the vibrations to an incredible 2,450,000,000 times a second! A vital part of the magnetron is

the Crucible Alnico permanent magnet shown in the inset.

This is one of many practical applications for Crucible Alnico permanent magnets. Crucible has been a leading producer of permanent magnets, known for their consistently higher energy product, ever since Alnico alloys were developed. You can now order them sand cast, shell molded, or investment cast to every size, shape, or tolerance needed.

It's why an increasing number of manufacturers find the answer to their magnet problem at Crucible. Crucible Steel Company of America, The Oliver Building, Mellon Square, Pittsburgh 22, Pa.

Permanent magnet is C-shaped casting at right of magnetron; box on top is filter assembly.

CRUCIBLE

first name in special purpose steels

Crucible Steel Company of America

CIRCLE 54 READERS SERVICE CARD

CIRCLE 55 READERS SERVICE CARD

HERE'S HOW TO SPECIFY

Performance-Guaranteed TAPE WOUND CORES

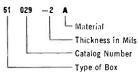
Magnetics, Inc. manufactures "Performance-Guaranteed" Tape Wound Cores using such commercially available alloy materials as Hy Mu 80, 48 Alloy and Orthonol. These alloys, when properly processed, fill the majority of applications in which tape wound cores are used today.

Each "Performance-Guaranteed" Tape Wound Core is coded by a part number which describes it in great detail. Knowing this code will greatly simplify your purchasing and assembly line practices.

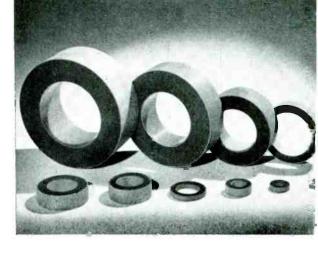
- 1. 50,000 series are Standard Cores in Phenolic Boxes 51,000 series are Standard Cores in Aluminum Boxes
- 2. Number preceding final letter is tape thickness in mils
- 3. Final letter describes the high permeability material as follows: A-Orthonol D-Hy Mu 80 H-48 Alloy

Example: A typical core number is 51029-2A

- 1. 51,000 indicates a standard core in an Aluminum Core Box.
- The number preceding final letter is 2, indicating tape thickness is 2 mils.
- 3. Final letter is A, showing Orthonol is the material.



Type of Box



For complete information, write for Catalog-Design Manual TWC-200

TABL	.E • S	TANI	DARD	SIZES	OF 1	ГАРЕ	WOUN	D COR	RES				
A ₂ Aw X 10-6	CORE NUMBER			ENSIONS (In.)		MEAN LENGTH OF	ENGTH AREA (Cm 2)						
(See Note 1)		1.D.	0.D.	Ht.	1.D.	0.D.	Ht. (See Note 3)	LAR MILS X 10-6	MAGNETIC PATH (Cm.)	.001	.002	.004 & .006	1.D./O.D. RATIO
0.004 *0.008 0.013 *0.017 *0.030	50153 50056 50057 50000 50002	0.375 0.500 0.625 0.500 0.650	0.500 0.625 0.750 0.750 0.900	0.125 0.125 0.125 0.125 0.125 0.125	0.315 0.440 0.555 0.440 0.590	0.560 0.685 0.810 0.810 0.960	0.195 0.195 0.195 0.195 0.195	0.099 0.194 0.308 0.194 0.348	3.49 4.47 5.49 4.92 6.13	0.041 0.040 0.040 0.081 0.081	0.043 0.043 0.042 0.086 0.086	0.046 0.045 0.046 0.091 0.091	0.750 0.800 0.833 0.667 0.722
0.053	50033	0.625	0.875	0.250	0.555	0.945	0.330	0.308	5.99	0.162	0.172	0.182	0.714
0.059	50003	0.750	0.938	0.250	0.680	1.010	0.330	0.460	6.74	0.121	0.128	0.135	0.800
*0.059	50076	0.625	1.000	0.188	0.555	1.070	0.268	0.308	6.36	0.182	0.193	0.205	0.625
*0.074	50011	1.000	1.250	0.125	0.930	1.320	0.195	0.864	8.94	0.081	0.086	0.091	0.800
*0.079	50007	0.625	1.000	0.250	0.555	1.070	0.330	0.308	6.36	0.242	0.257	0.272	0.625
*0.079	50061	0.750	1.000	0.250	0.680	1.070	0.330	0.462	6.93	0.161	0.171	0.181	0.750
*0.089	50106	0.750	1.125	0.188	0.680	1.195	0.260	0.462	7.38	0.182	0.193	0.205	0.667
0.118	50168	0.750	1.000	0.375	0.680	1.070	0.455	0.462	6.97	0.227	0.257	0.272	0.750
0.119	50094	0.625	1.000	0.375	0.555	1.070	0.445	0.308	6.49	0.339	0.385	0.411	0.625
*0.148	50004	1.000	1.250	0.250	0.930	1.320	0.330	0.864	8.94	0.161	0.171	0.181	0.800
0.179	50034	0.750	1.125	0.375	0.680	1.195	0.455	0.460	7.49	0.342	0.389	0.405	0.667
0.186	50115	1.125	1.375	0.250	1.045	1.445	0.330	1.090	9.99	0.161	0.171	0.181	0.818
*0.222	50029	1.000	1.375	0.250	0.930	1.445	0.330	0.864	9.39	0.242	0.257	0.272	0.727
0.237	50188	0.750	1.250	0.375	0.680	1.320	0.455	0.462	7.98	0.453	0.514	0.544	0.600
0.250	50181	0.875	1.250	0.375	0.805	1.320	0.440	0.648	8.48	0.340	0.386	0.408	0.700
*0.296	50032	1.000	1.500	0.250	0.930	1.570	0.330	0.864	9.84	0.323	0.343	0.363	0.667
*0.444	50026	1.000	1.500	0.375	0.930	1.570	0.445	0.864	9.84	0.484	0.514	0.544	0.667
*0.469	50030	1.250	1.750	0.250	1.170	1.820	0.330	1.368	11.85	0.323	0.343	0.363	0.714
*0.592	50038	1.000	1.500	0.500	0.930	1.570	0.590	0.864	9.84	0.605	0.685	0.726	0.667
*0.597	50018	1.625	2.000	0.250	1.525	2.100	0.380	2.324	14.41	0.242	0.257	0.272	0.813
*0.937	50035	1.250	1.750	0.500	1.170	1.820	0.590	1.368	11.85	0.605	0.685	0.726	0.714
*1.055	50425	1.250	2.000	0.375	1.170	2.100	0.465	1.368	12.60	0.726	0.771	0.817	0.625
*2.471	50017	2.000	2.500	0.500	1.900	2.600	0.590	3.608	17.87	0.605	0.685	0.726	0.800
.2.685	50040	1.500	2.000	1.000	1.400	2.100	1.110	1.960	13.99	1.211	1.370	1.457	0.750
*2.686	50001	1.500	2.500	0.500	1.400	2.600	0.590	1.959	15.79	1.210	1.371	1.452	0.600
*3.944 *4.947 *7.320 *9.893 *14.661	50031 50103 50128 50022 50042	2.500 2.000 2.500 2.000 2.500	3.000 3.000 3.500 3.000 3.500	0.500 0.500 0.500 1.000	2.400 1.900 2.312 1.900 2.313	3.100 3.100 3.688 3.100 3.688	0.590 0.590 0.713 1.110 1.188	5.757 3.608 5.343 3.608 5.343	21.73 19.67 23.71 19.67 23.71	0.605 1.210 1.210 2.419 2.419	0.685 1.371 1.371 2.742 2.742	0.726 1.452 1.452 2.903 2.903	0.833 0.667 0.714 0.667 0.714
*22.907	50080	2.500	3.750	1.250	2.313	3.938	1.437	5.347	24.59	3.780	4.284	4.536	0.667
*27.489	50100	2.500	3.750	1.500	2.313	3.938	1.688	5.347	24.59	4.536	5.141	5.444	0.667
*48.176	50081	3.250	4.500	1.500	3.062	4.688	1.688	9.371	30.64	4.536	5.141	5.444	0.722
*67.452	50427	3.250	5.000	1.500	3.062	5.188	1.688	9.371	32.40	6.351	7.198	7.621	0.650
*99.617	50112	4.000	5.250	2.000	3.782	5.469	2.280	14.063	36.66	6.048	6.855	7.258	0.762
*159.386	50426	4.000	6.000	2.000	3.782	6.280	2.276	14.532	39.34	9.677	10.968	11.613	0.667

*A.I.E.E. Proposed Standard Size.

Note 1— Product of window area and iron area calculated for 2 mil material.

Note 2— Part numbers listed are for phenolic cases. Specify 51000 series for aluminum cases (last three numbers remain the same).

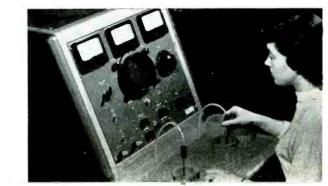
Note 3— Dimensions listed are nominal sizes for phenolic cases. For aluminum cases, add .015 to .020 inches to heights shown.

TABLE II . NAME	S OF SIMILAR	MATERIALS		
D-Hy Mu 80	H-48 Alloy	A — Orthonol		
4—79 Permatloy MO—Permatloy Mu Metal*	Carpenter 49 Allegheny 4750 Hipernik	Orthonik Deltamax Hipernik V		

This material has a different composition than the others in the same column. The characteristics of this material are such that in general it is not recommended for use in tape wound cores.

MATCHED CORES

Magnetics, Inc. will match cores within 5% over the entire voltage-current loop. Matching prior to winding results in improved yield and economical production. There is a very slight service charge for matching cores.



MAGNETICS INC. PRODUCTS

Performance-Guaranteed BOBBIN CORES

TABLE III · STANDARD CERAMIC AND STAINLESS BOBBIN CORES

	1	NOMINAL DIMENSIONS IN INCHES									
PART NO.		A	В	С	D	E	F	G			
	80002-B	.125	.140	.185	.090	.030	.200	.030			
o _z	80003-B 80023-A	.188 .250	.140 .140	.310	.210	.030	.200	.030			
CERAMIC	80004-B	.313 .313	.140 .140	.373 .435	.270	.030	.200	.030			
BB	80018-A 80009-B	.375	.140	.435	.330	.030	.200	.030			
	80017·A	.563	.140	.685	.513	.030	.200	.061			
Z	80163	.110 .110	.050	.140	.100	.005	.060	.015 .015			
ESS OBB	80164 80165	.125	.075	.185	.105	.010	.095	.030 .015			
STAINLESS STEEL BOBBIN	80166 80167	.125	.140	.155	.110	.005	.150	.030			
ST	60168	.313	.140	.373	.293	.010	.160	.030			

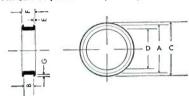
For Additional Information, Write for Bulletin BC-102

Bobbin cores are now being made in combinations of the following dimensions. Other sizes can be supplied on request.

TAPE THICKNESS: 0.000125", 0.000250", 0.0005", 0.001".

BUILD-UP: 1 wrap to several hundred. MATERIALS: 4-79 Mo Permalloy, Orthonol. *11/2-in. diam. bobbin is not standard, but can be furnished upon request.

†Not with standard bobbins if tape width is over 14-in., but can be furnished upon request.



Performance-Guaranteed POWDER CORES TABLE IV . MOLYBDENUM PERMALLOY POWDER CORES

		1.		h.\				Dimensions	(inches) bef	ore finish				
Core			ductanc e (m 000 Turn Co			0.D.			I.D.		Height			Radii
Number	μ	Min.	Nom.	Max.	Min.	Nom.	Max.	Min.	Nom.	Max.	Min.	Nom.	Max.	
55206-A2 55848-A2 55511-A2 55057-A2 55310-A2 55390-A2 55395-A5 55066-A2 55568-A2 55588-A2 55588-A2 55588-A2 55584-A2 55324-A2	125 60 26 14 125 125 60 60 26 14 125 125 125	58 28 12 6.6 77 136 65 65 28 15 106 71 101 146 248	68 32 14 7.8 90 157 75 75 32 18 127 79 117 281	83 39 17 9.2 104 179 86 86 37 20 148 91 137 195 325	.790 .790 .790 .790 .890 1.050 1.050 1.050 1.050 1.250 1.335 1.335 1.395 1.3825	.800 .800 .800 .900 1.060 1.060 1.060 1.060 1.300 1.350 1.410 1.570 1.840	.810 .810 .800 .910 1.070 1.070 1.070 1.070 1.312 1.365 1.425 1.855	.495 .495 .495 .495 .547 .575 .575 .575 .575 .780 .908 .868 .938	.500 .500 .500 .500 .550 .580 .580 .580	.505 .505 .505 .505 .505 .585 .585 .585	.240 240 .240 .240 .290 .428 .428 .428 .428 .428 .400 .333 .400 .555 .690	.250 .250 .250 .250 .300 .440 .440 .440 .440 .420 .350 .412 .570	.260 .260 .260 .260 .310 .452 .452 .452 .452 .452 .452 .452 .452	.032 .032 .032 .032 .062 .075 .075 .075 .075 .075 .062 .062

For Complete Details, Write for Bulletin PC-103

Performance-Guaranteed MAGNETIC LAMINATIONS

TABLE V · STANDARD MAGNETIC CORE LAMINATION SHAPES

111011					1991 1				2000 000 000 000 000
LAMINA- TION TYPE	STACK HEIGHT (inches)	WINDOW AREA (sq. in.) W	CROSS- SECTION AREA (sq. in.) A	W×A	LAMINA- TION TYPE	STACK HEIGHT (inches)	WINDOW AREA (sq. in.) W	CROSS- SECTION AREA (sq. in.) A	W×A
DU 1 DU 37 DU 50 EE 24-25 EE 26-27 EE 28-29 EE 186-187 EI 11 EI 12 EI 21 EI 21 EI 187	1/4 3/8 1/2 1/4 3/8 3/16 7/8 1 1/2 3/4 3/16	.5625 1.125 2.000 .125 .172 .039 .125 .574 .750 .254 .422 .082	.063 .141 .250 .063 .141 .014 .063 .766 1.000 .250 .250 .35	.035 .159 .500 .008 .024 .0005 .008 .440 .750 .064 .237	E1 375 E1 625 F 12 F 12 (Modified) F 13 F 20 F 21 Ring U-BE U1 312 U1 375	3/4 344 344 344 3/8 1/2 Variable 1/4 5/16 3/8	.234 .293 .188 .188 .190 .371 .257 Various .313 .293 .422	.141 .391 .118 .118 .141 .25 Various .063 .098 .141	.033 .115 .022 .022 .022 .052 .052 .064 Variable .020 .028 .059

Performance-Guaranteed laminations are made from any commercially available soft magnetic material. Heat treatment for specific properties may be specified but should be checked by Magnetics, Inc. Engineering Department if the Performance-Guarantee is to apply. When asking for quotations, describe, if possible:

- 1. Shape required
- 2. Grade of magnetic steel
- 3. Gauge of lamination
- 4. Surface insulation

For Complete Details, Write for Catalog ML-201.

Performance-Guaranteed MAGNETIC SHIELDS

TABLE VI . MAGNETIC SHIELDS Tube To Be Used With Magnetics, Inc. Part No. Tube Tube To Be Used With Magnetics, Inc Part No. Magnetics, Inc Part No. Tube To Be Used With Tube Tube Mfr. Mfr. RS-1, 2, 5 RS-4, 5, 6 RS-7, 8, 9 2 BP-1, 11 3 BP-1A 3 JP-1, 7 3 GPA 3 RP-1, 4, 11 3 MP1 3 RP-1 3 RP-1 3 RP-1 3 RP-1 5 AMP-1 5 BP-1 5 BPA 5 CP-1A 5 CPA 5 FP-4, 7 5 AHP & 5FP 3 JPA 5 LPA 5 RP. 7 11 Dumont RCA RCA RCA 40120 Dumont 40012 40013 40014 40024 RCA 40086 40086 Dumont RCA 40087 40087 10 SP-4 10 WP-7 Dumont Dumont Dumont Dumont Dumont RCA 40031 Dumont RCA RCA 40023 40023 40023 40007 Dumont RCA 40149 5819 K 1197 Dumont Dumont Dumont 40149 40021 Dumont RCA RCA 6363 K-1198 6364 K-1211 6199 6292 6467 931-A 40022 40007 40022 40067 40015 40148 40001 40001 40074 Dumont 5 UP-1, 7, 11 5 WP-11, 15 5 XP 5 YP Dumont RCA 40000 Dumont RCA RCA Dumont Dumont 40150 40153 40152 Dumont 40020 Dumont RCA Dumont Dumont 40055

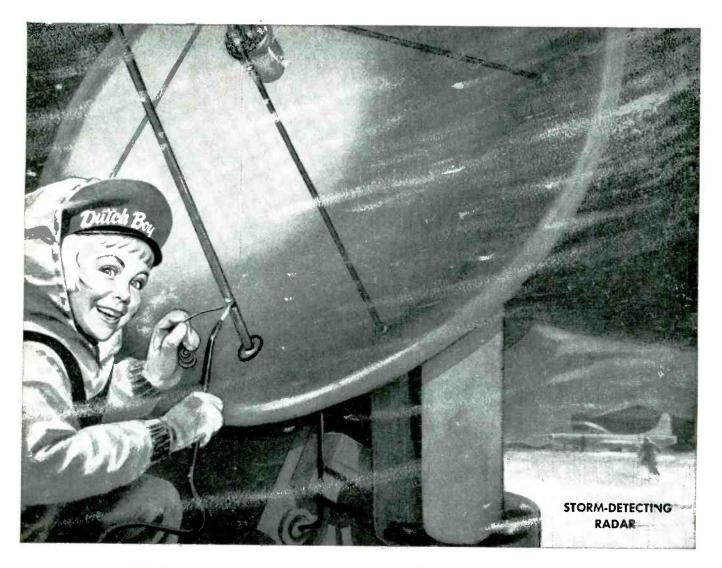
Dumont 7 MP-7, 14 RCA For Further Details, Write Sales Engineering Dept.

40019

DEPT. E-39



BUTLER, PENNSYLVANIA



What happens to soldered joints at "fifty below"?

"Dutch Boy" solder specialists tell how to make sure they hold when cold

Push temperature down and lead's strength goes up — without major loss in ductility.

Not so with tin. Below $-18^{\circ}F$, tin may suffer allotropic transformation. Gets brittle. Changes color.

Recent "Dutch Boy" research shows, as you might expect, that lead-tin solders tend to split this difference in rough proportion.

A 50-50 solder, for example, yields joints with higher tensiles at —75°F than at room temperature. But it's more brittle. At —75°F the joined metals still fail before the joint. Further down the temperature scale, joints fail first.

Increasing the lead content lowers the temperature at which joints retain good ductility. But strength does not increase as rapidly as temperatures go down.

Up to 15%, tin content has little effect on ductility. Beyond that, the loss in ductility (and in impact and fatigue resistance) that occurs as temperatures go below —18°F should be considered.

Allotropic change in tin may be inhibited with antimony

For makers of aircraft, missile and arctic electronic equipment, and for others whose products meet with extreme low temperatures, a recent proposed change in Government specs is of interest.

This proposal, which calls for 0.2 to 0.5% antimony in solders in the 40 to 70% tin range, is based on investigations showing that antimony inhibits allotropic change in tin as the thermometer falls.

Your "Dutch Boy" Solder specialist is well informed on this and other frontier areas of solder technology now under investigation at National Lead Laboratories and elsewhere. Use his specialized knowledge freely. Or write National Lead Company, 111 Broadway, New York 6, N. Y.



Sperry's combination radar test sets integrate all testing functions

Faster, simpler radar maintenance is the pay-off with the Sperry Combination Test Sets. One set does the job of three or more standard test units but requires one-quarter the space and weighs half as much! Here are the five functions each Sperry test set performs:

POWER METER: Directly measures average power of radar transmitter with accuracy of ± 1.0 db.

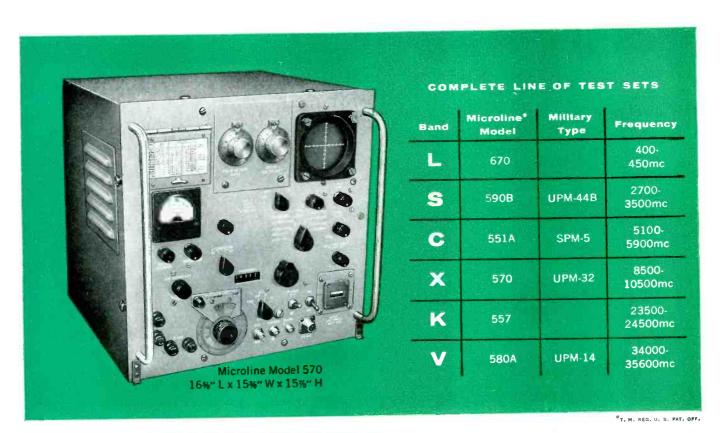
FREQUENCY METER: Indicates directly the frequency of both receiver and transmitter.

SPECTRUM ANALYZER: Accurately displays power vs. frequency spectrum of transmitter signals from single or multi-pulse systems. Display is stable at all pulse widths and repetition rates.

SYNCHROSCOPE: Simple general-purpose synchroscope functions as an "A" scope and displays radar video signals or similar wave forms—no need for auxiliary synchroscope.

SIGNAL GENERATOR: Accurately and directly calibrated output signal level is variable over complete range. Choice of pulse, frequency or external modulation.

With no additional equipment you can also measure transmitter peak power, repetition rate, transmitter pulse width, T.R. recovery time, duplexer losses, transmission line VSWR. Designed for tough operating conditions, these sets comply fully with military specification MIL-T-945A. Your nearest Sperry district office will gladly supply you with complete operating data.



MICROWAVE ELECTRONICS DIVISION



DIVISION OF SPERRY RAND CORPORATION

Brooklyn • Cleveland • New Orleans • Los Angeles San Francisco • Seattle. In Canada: Sperry Gyroscope Company of Canada, Ltd., Montreal, Quebec.



Hamilton

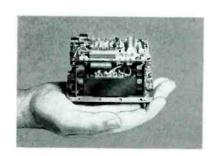
can meet your requirements for

STANDARDS DEVELOPMENT

Hamilton Watch Company's Instrument Division now offers you complete facilities for developing, designing and fabricating of frequency standards to your specifications. Complete circuitry development and packaging of miniature transistorized tuning fork frequency standards is provided.

The accuracy and stability required for precision timing systems is available to you through the experience of our research and development engineers, combined with complete production facilities.

We are ready to review your requirements.

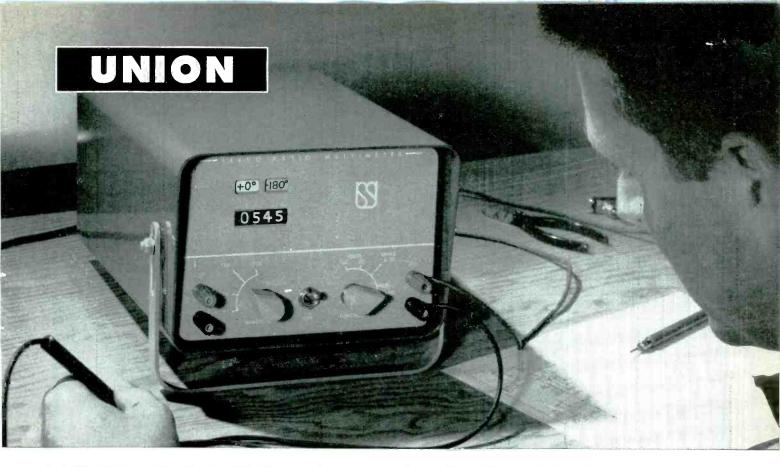


PHONE OR WRITE

giving us your specifications for prompt analysis.



HAMILTON WATCH COMPANY
5800 EAST JEWELL AVENUE • DENVER 22, COLORADO
HATHAWAY INSTRUMENT DIVISION



NEW SERVO-RATIO MULTIMETER

Combines all the functions of an AC-DC voltmeter, ohmmeter and AC-DC ratiometer in one compact portable unit

Here is a new, highly accurate test instrument designed to make life easier for those who work with computers and other electronic and electrical devices. It measures AC-DC ratios, absolute AC-DC voltages and resistance. You can also measure the gain of operational amplifiers using the 0° phase output provided.

The Servo-Ratio Multimeter computes voltage ratios by dividing the voltage to be measured by the reference voltage obtained from the computer. It is a high-impedance instrument and utilizes a motor-driven, position-type servo mechanism. Average time to obtain a reading is three seconds. Simplification and reliability are obtained through the use of printed circuits.

The front panel contains a fourdigit illuminated drum counter for readout, phase or polarity indicating lights, function switch, ON-OFF

switch, range switch, 0° phase ratio selector, input terminals and 0° phase output terminals.

The Servo-Ratio Multimeter is compact and easy to handle. It has an aluminum case and weighs only 10 pounds. The instrument can be operated in a horizontal or vertical position and has a unique carrying handle that serves as a tilt-stand when the unit is used horizontally. Write for Product Description 2005.

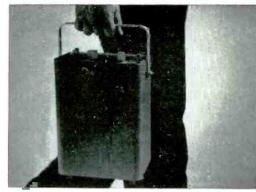
SPECIFICATIONS

Power Consumption: 50 Watts, 110 Volts, 60 cps. Reference Voltage: DC or 60 cps AC; ± 10 Volts to ± 100 Volts across 8.7K Ohme Load

to ± 100 Voits	across 8.7K Ohms Load.
Functions	Range
Ratio, AC	0.001 to 1.000 \pm 0.1% in 1 range
Ratio, DC	0.001 to 1.000 \pm 0.1% in 1 range
50 cps AC Voltage	1 Volt to 1000 Volts full scale ± 1.0% in 4 ranges
DC Voltage	1 Volt to 1000 Volts full scale ± 1.0% in 4 ranges
Ohms	10K Ohms to 10 Megohms full

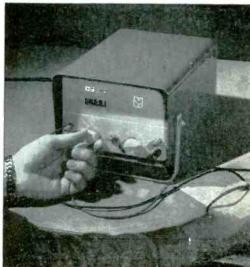
scale + 1.0% in 4 ranges Gain

0.01 to 1000 in 4 ranges



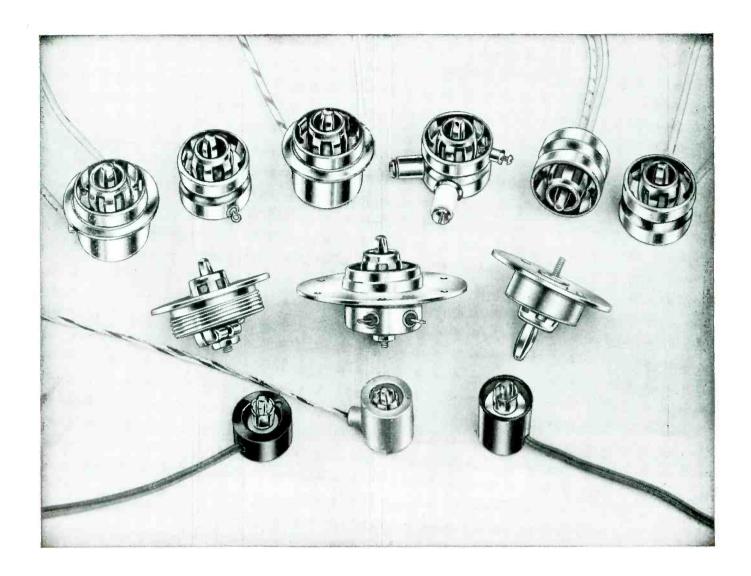
PORTABLE AND COMPACT—Weighs only 10 pounds. Size: $7\frac{1}{8}$ " x $5\frac{1}{2}$ " x 11-13/16".

SIMPLIFIES TESTING-Eliminates need for many other instruments. Has digital readout counter.



MION SWITCH & SIGNAL DIVISION OF WESTINGHOUSE AIR BRAKE COMPANY

PITTSBURGH 18, PENNSYLVANIA



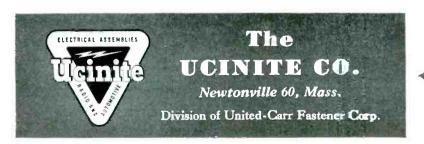
Ucinite Magnetron Connectors

Ucinite manufactures a variety of special connectors for the heater and heater-cathode terminals of magnetrons. Many of these have been adapted for special applications as to size and function to meet the sealing and mounting requirements of high temperature and high altitude operation and other special conditions.

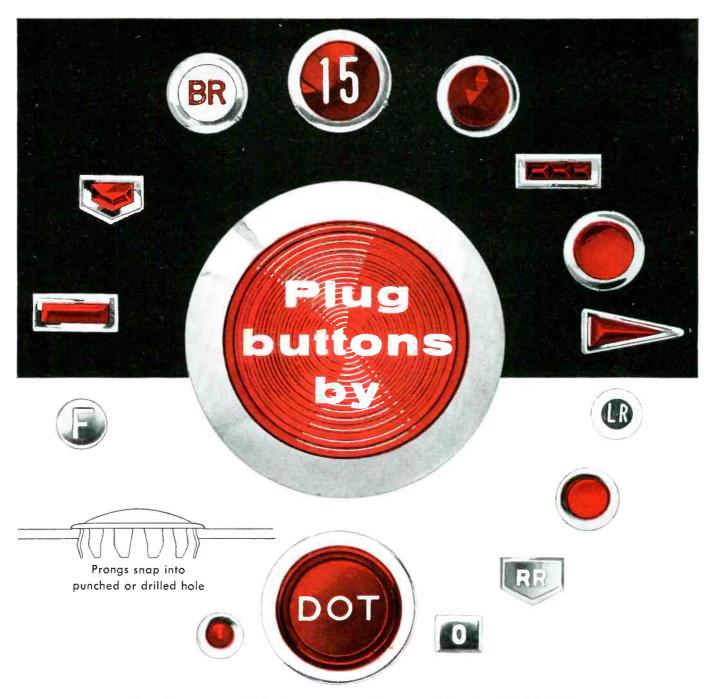
Connectors are coaxial in construction and can be supplied with built-in capaci-

tors for added protection. Connecting leads of any length can be furnished to customer's specifications.

With an experienced staff of design engineers, plus complete facilities for volume production, Ucinite is capable of supplying practically any need for metal or metal-and-plastics assemblies. Call your nearest Ucinite or United-Carr representative for full information or write directly to us.



Specialists in
ELECTRICAL ASSEMBLIES,
RADIO AND AUTOMOTIVE



CUSTOM-DESIGNED AND MASS PRODUCED TO YOUR PARTICULAR REQUIREMENTS

Dot plug buttons were originally used in automobiles to fill spaces on standard models which, on de luxe models would be occupied by such extras as cigarette lighters, radio controls and so on. They are now also widely used as lenses for indicator lights and as identification buttons on instrument and control panels of all kinds.

Available in clear or colored plastics... brass or steel in all standard finishes... embossed and enamel-filled or molded to show company insignia or other identification symbols... Dot plug buttons snap into place and stay where they're put even under conditions of extreme vibration. Yet they can be removed and replaced repeatedly without damage.

CARR FASTENER COMPANY

DIVISION OF UNITED-CARR FASTENER CORPORATION 31 Ames Street, Cambridge 42, Massachusetts





Dial indicator gage measures the critical "E" dimension.

Precision disc cathodes simplify assembly of TV picture tubes

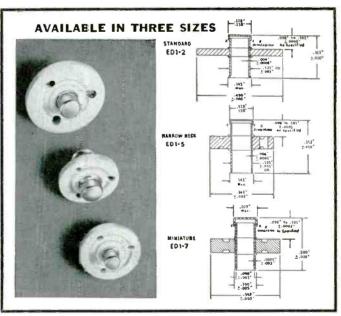
Because Superior Tube guarantees such close tolerance in disc cathode "E" dimension, makers of TV picture tubes can save the time and cost of compensating for variations.

Cathodes can be used universally in different tubes, and are interchangeable with each other during electron gun assembly. This means both manufacturing efficiency and quality control can be significantly improved.

In addition, Superior Tube precision disc cathodes offer these four important advantages:

- 1. Separate cap alloy. Permits use of best alloys for both cap and shank in varying applications.
- 2. Slight flare of shank opening. Easier insertion of heater. Less abrasion of heater coating during normal expansion and contraction.
- 3. Shadow groove in ceramic. Inhibits electrical leakage between cathode and No. 1 grid.
- 4. Chemically clean shank interior. Minimizes heater-cathode leakage.

Superior Tube disc cathodes are available in three sizes: standard, narrow neck making possible shorter tubes, and miniature for 3-gun color TV picture tubes. Write for complete information to Superior Tube Co., 2500 Germantown Ave., Norristown, Pa.



HOW SUPERIOR DOES IT—GENERAL CERAMICS CORPORATION, Keasbey, N.J., working for many years with Superior Tube's engineers, has developed mass-production methods resulting in the supply of millions of close-tolerance insulators which have greatly assisted in achieving this uniform "E" dimension. These insulators are produced under rigid quality controls. The cathode shank is double-beaded to the ceramic to insure tight fit. The cap is electrically spot-welded to the shank while held in a precision jig.



Johnson & Hoffman Mig. Corp., Mincola, N.Y.—an affiliated company making precision metal stampings and deep-drawn parts such as those used in the electron guns that go with this new cathode.

having your ups and downs?



... if they involve WIRE WOUND RESISTORS <---

has the answer

You can depend on



All Dalohm products are carefully designed and skillfully made to assure you of supreme quality and dependability, plus the widest versatility of application. Here are outstanding examples of the Dalohm line:

WIRE WOUND ENCAPSULATED PRECISION RESISTORS

Surpass MIL-R-93R

Completely impervious to penetrating effects of salt ions, humidity, moisture and corrosive gases and vapors, Dalohm's new encapsulating material has very high di-electric strength. Its coefficient of expansion matches that of the resistor wire itself, eliminating the possibility of distorted wiring and shorted turns. All are non-inductive, pi-wound.

NEW SUB-MINIATURE SIZES





- Resistance range 10 ohm to 1 megohm
 Tolerances 0.05%, 0.1%, 0.25%, 0.5%, 1%, 3%
- Powered at 0.1 watt to 0.8 watt
- Temperature coefficient 0.00002/Deg. C Maximum operating temperature 125° C.

31263			IFVIAIIIAWPD
	Length	Dia.	
	3/8"	1/8"	WWL—lugs;
22	1/4"	1/4"	WWA-axial leads;
23	. 3/8′′	1/4"	WWR — radial leads:

WWA 13	3/8	1/8
WWA and WWP 22	1/4''	1/4"
WWL and WWR 23	3/8''	1/4"
WWA, WWL, WWR, WWP 24	1/2"	1/4"
WWA 26	3/4"	1/4"
WWA, WWL, WWR, WWP 34	1/2	3/8"
WWA, WWL, WWR, WWP 36	3/4"	3/8"
WWA, WWL, WWR, WWP 38	1''	3/8"

STANDARD SIZES





WWA

WWL

- Resistance range 0.1 ohm to 5 megohms
- Tolerances 0.05%, 0.1%, 0.25%, 0.5%, 1%, 3%
- · Powered at 0.5 watt to 2 watts
- Temperature coefficient 0.00002/Deg. C
- Maximum operating temperature 125° C.

	Length	Dia.
WWA and WWL 44	1/2"	1/2"
WWA and WWL 45	5/8''	1/2"
WWA and WWL 48	1''	1/2"
WWA and WWL 4-12	11/2''	1/2"
WWA and WWL 4-16	2''	1/2"

TERMINALS

WWA—axial leads; WWL—lugs.

Also available in MIL Types RB-09, RB-15, RB-16, RB-17, RB-18, RB-19

WWP—parallel leads.

JUST ASK US:

You are invited to write for the complete catalog of Dalohm precision resistors, potentiometers and collet-fitting knobs. If none of our standard line fills your need, our staff of able engineers and skilled craftsmen equipped with the most modern equipment, is ready to help solve your problem in the realm of development, engineering, design and production. Just outline your specific situation.

PRODUCTS, INC.

1300 28th Avenue Columbus, Nebr., U.S.A. EXPORT DEPT: Pan-Mar Corp. 1270 Broadway New York 1, N.Y

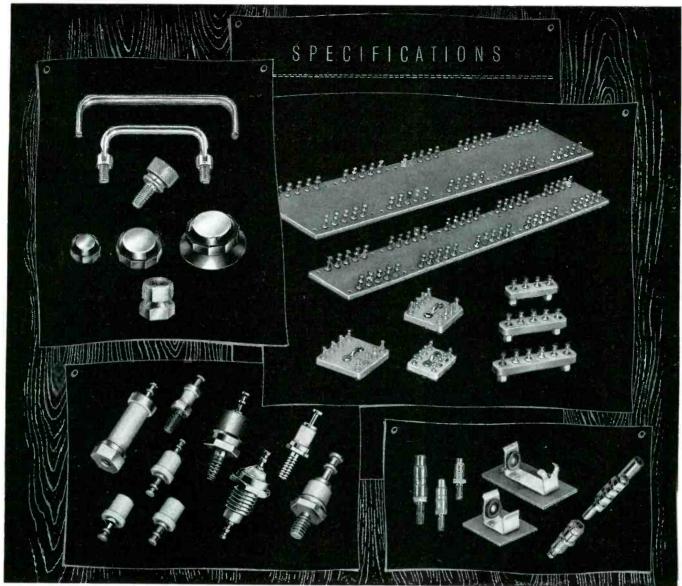


Photo shows wide variety of CTC components. Upper left, hardware, knobs, panel screws. Upper right, standard terminal boards, phenolic and ceramic. Bottom row, insulated terminals in ceramic and teflon, diode clips, battery clips, plugs and jacks. Common denominator — CTC reliability.

If specifications call for durability specify CTC hardware

Durability is not just a term at CTC — it's practically a manufacturing process! Take the above line of CTC hardware for example. CTC guarantees it and every one of its components unconditionally — in any quantity! That's high quality control — quality control that meets or betters all applicable military and government specifications. CTC quality controls the raw material, each step of production and the finished product — the result — exceptional durability.

Best of all you get this durability economically. In fact — you couldn't make such hardware items cheaper yourself! Our large selection of standard panel and chassis hardware fills most needs. If you require custom design, contact us direct.

Send for CTC's Catalog 600 — it has all the details of CTC's complete hardware line. Write to Sales Engi-

neering Dept., Cambridge Thermionic Corporation, 437 Concord Ave., Cambridge 38, Mass. On the West Coast contact E. V. Roberts and Associates, Inc., 5068 West Washington Blvd., Los Angeles 16, and 1560 Laurel St., San Carlos, Calif.

CAMBRIDGE THERMIONIC CORPORATION

makers of guaranteed electronic components custom or standard



TECHNIQUES and DEVELOPMENTS in oscillographic recording

FROM SANBORN

CIRCUIT DESIGN AND TYPICAL USES OF THE "150" CARRIER PREAMPLIFIER

One of the most frequently used plug-in front ends for Sanborn 150 Series oscillographic recording systems is the Model 150-1100 Carrier Preamplifier, since with it a "150" system can record such variables as force, temperature, strain, pressure, displacement, velocity, flow, acceleration—



GAGE FACTOR CONTROL

or any variable which can be expressed as a suitable input signal by a transducer. The "1100 Carrier" will operate with a variety of different transducers and bridge circuits, which will be mentioned later on.

In the block diagram (Fig. 1),

This excitation voltage also feeds the Balancing. Calibration and Zero Suppression circuits. (The Balancing controls allow correction of resistive and reactive signal leakage from the

transducer, so that at zero load the net signal to the Preamplifier is zero. The Zero Suppression feature permits bucking out a large static load so that a small part of the load can be expanded over the full recording chart. The Gage Factor control allows the zero suppression range to be made equivalent to some convenient transducer load, or the full load rating of the transducer, and also causes the calibration signal to represent $2\,\%$ of that load.) Transducer output is fed to the transformer through the Gage Factor potentiometer, across which the Balancing-Calibration-Zero Suppression circuits develop a voltage effectively in series with the transducer output. The mixer receives a suppressed carrier AM signal and re-inserts a carrier component, to make its output a conventional AM signal whose modulation represents the transducer load. The modulation signal (whose amplitude and polarity represent magnitude and direction of transducer output) is recovered by the demodulator and fed to the output amplifier, which in turn excites the Driver Amplifier and recording galvanometer of a "150" system.

Transducers which may be used with the Carrier Preamplifier include strain gage half-bridges or full-bridges, commercial resistance or reactance bridges, differential transformers and resistance thermometer bridges. The transducer chosen should provide at least 18.0 microvolts per volt of excitation at the minimum load to be recorded, for a one cm. dellection; impedance should be 100 to 1000 olums. With strain gages, normal operation provides sensitivities of 50, 20 or 10 micro-inches per inch for each cm. on the recording, depending on the number of active gages. With resistance thermometers, if 1°C. or 2°F. per cm. stylus deflection is sufficient sensitivity, the user can construct his own resistance thermometer by including a 3 ohm coil of copper wire in one arm of an equal arm 100 ohm bridge.

Helpful information about the use of transducers with the 150-1100 Preamplifier is contained in the following Sanborn RIGHT ANGLE articles (reprints on request): Coupling Differential Transforners, Aug. and Nov. 1956; Filter Networks for use with Force Dynomometers, Nov. 1956; Calibration with 1-, 2- or 4-arm Strain Gage Bridges, Aug. 1955; Theoretical and Actual Applications of Bridge Circuits, May and Aug. 1954.

Wing flutter recording to infrared research . . . with the versatile "1100 Carrier"





Today, Carrier Preamp-equipped Sanborn "150" systems are being used for frequency response tests of process control system components; to record shaft deflections of fluid mixing equipment; in infrared research...vehicular traffic studies... submarine hull vibration measurements. Applications are limited only by the transducers available.

These are applications of only one "150" front-end; eleven more interchangeable, plug-in Preamplifiers increase the scope of Sanborn oscillographic recording systems to meet an almost infinite variety of research, production and field testing requirements. All Sanborn "150" direct writing systems record inkless traces in true rectangular coordinates; all provide 1% linearity; Basic Assemblies — equipped with your choice of Preamps — are available from one-to eight-channels, packaged in vertical cabinets, portable cases, or specially modified housings.

Technical data and help with your oscillographic recording problem are always available from Sanborn.

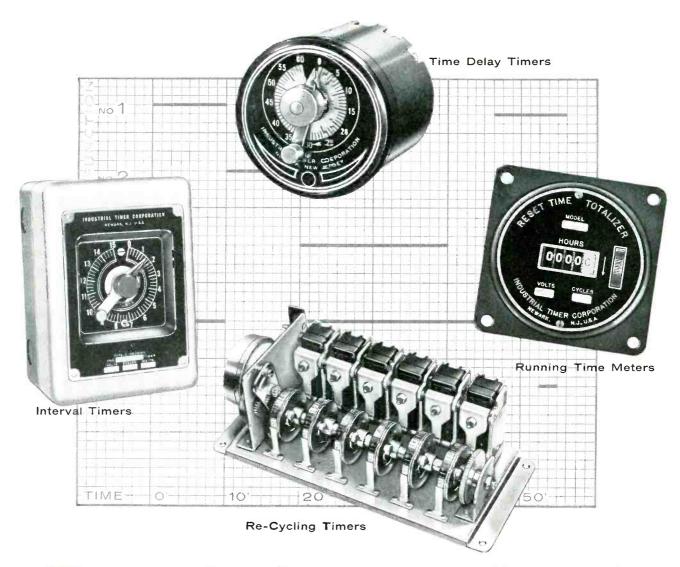




SANBORN COMPANY

INDUSTRIAL DIVISION

175 Wyman St., Waltham 54, Mass.



Timers for Automatic Control ...Standard or Special?

You'll get quick deliveries from Industrial Timer

If slow deliveries of timers have been delaying you in your automatic control projects, try us! True, your problem may be different and difficult indeed, for no two automatic control jobs are exactly alike. But our record in helping out in situations like these is excellent. For in this field we have a valuable background, twenty years of timer experience to be exact, that has provided us with the special knowledge required to supply our customers with the right answers.

How do we do it? The answer is in what we believe to be

the largest variety of standard and combination timer units anywhere in the industry. To fill the widely varying needs of our customers, we manufacture a complete line of timers in the four broad classifications illustrated above: Time Delay Timers, Re-Cycling Timers, Interval Timers, and Running Time Meters. From these our timer engineers have developed 20 basic types which they have so far combined in over 1000 different ways. Therefore—many jobs that would seem to require a special timer, are in fact, a standard timer with us.

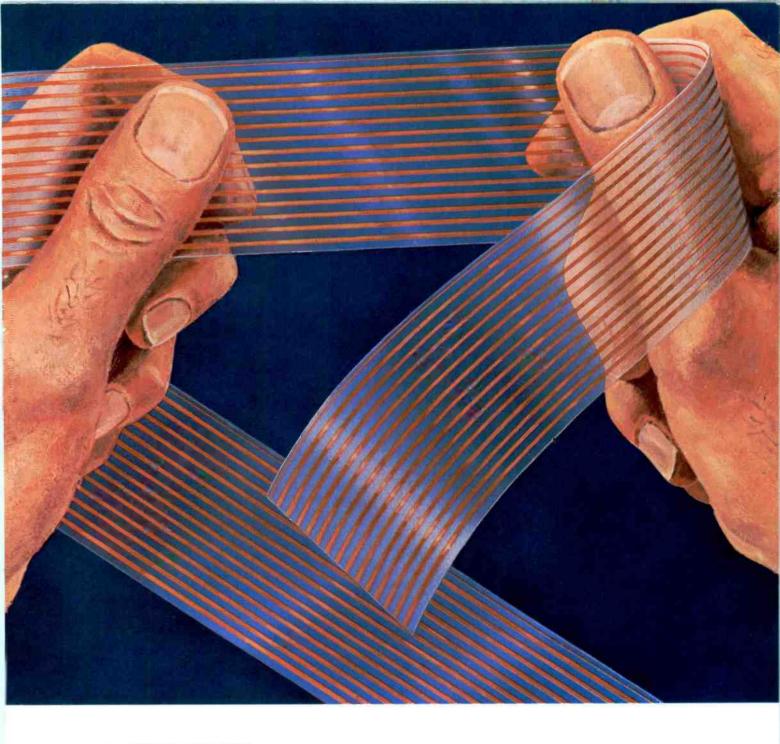
And our large stock assures you of rapid deliveries—even when we have to create a brand new timer for your special needs. So why not send us your specifications. You'll get a prompt reply and you may save yourself much lost motion.

Timers that Control the Pulse Beat of Industry



INDUSTRIAL TIMER CORPORATION

1409 McCARTER HIGHWAY, NEWARK 4, N. J.



THIN

LIGHT

FLEXIBLE

TOUGH

New...Tape Cable*

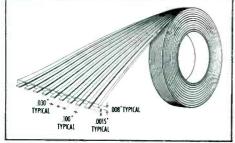
A MAJOR ADVANCE IN INTER-WIRING

Tape Cable's hair-thin copper conductors are imbedded in transparent polyester. Stripping, positioning and soldering of 40 conductor Tape Cable are accomplished in 30 seconds.

*Tape Cable is a Trade-Mark of the Tape Cable Corp.—Pat. Pend.

Full technical data on reverse side

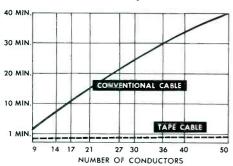
As seen in Electronics Magazine



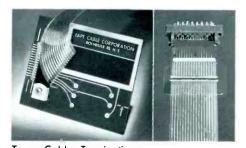
Dimensions of Standard Tape Cable



Space & Weight Comparison of Tape Cable & Conventional Cable Having Same Number of Conductors & Current Rating



Tape Cable & Conventional Cable Compared in Terms of Labor Time Consumed in Stripping, Positioning & Soldering



Tape Cable Terminations: To Printed Wiring Board & the Elco Plug

PRICE LIST 25 FOOT ROLLS OF STANDARD TAPE CABLE

TYPE	NUMBER OF CONDUCTORS	PRICE
1M3-9	9 conductor	\$ 18.90
IM3-14	14 conductor	29.40
1M3-17	17 conductor	37.40
1M3-21	21 conductor	47.90
1M3-27	27 conductor	65.70
1 M 3-30	30 conductor	76.00
1 m 3-36	36 conductor	97.20
1M3-40	40 canductor	110.60
1M3-50	50 conductor	153.30

Technical Data on Tape Cable'

The flat copper conductors in standard Tape Cable have .100" center-to-center spacing in accordance with the recommended RETMA grid pattern for printed wiring. The standard conductor is .0015" by .030". This gives Tape Cable a high conductor density, 1160 conductors per cross-section square inch as compared with only 225 for ordinary cable having #22 wire insulated with .010" wall. The total thickness of standard Tape Cable is only .008". A 100 foot roll of 30 conductor Tape Cable weighs only 1.78 pounds. This is a saving of 80% in weight over conventional cable having round conductors of the same current handling capacity. Tape Cable requires less than 20% of the space of conventional cable. Where weight and space are critical, Tape Cable is especially applicable.

Tape Cable has a conservative rating of 1 amp. and 300 volts AC. It is ideal for high frequency applications because of its low and uniform interconductor capacitance of less than 5 mmf. per foot between conductors in free air.

Save 90% of labor costs by using Tape Cable because:

- 1. All conductors are stripped simultaneously.
- 2. Positioning one conductor automatically positions all conductors, and
- 3. All connections can be dip-soldered in one operation.

Stripping of all conductors simultaneously is rapid and easy with machines readily available. Scissors are used for hand stripping. Tape Cable may be stripped on both sides for soldering, or it may be stripped on only one side for temporary or pressure connections.

It is possible to treat as many as 50 conductors as simply as a single wire in terminating and in stripping. Registering one conductor automatically registers all other conductors with mating contacts on printed wiring boards, connectors or another piece of Tape Cable.

Then, as a unit, all conductors can be dip-soldered in one operation. Edge dip-soldering of Tape Cable to printed wiring boards is readily automated for the assembly line. Harnesses and splices are completed in minutes. Complete assembly time of the 17 contact Elco connector shown is less than 3 minutes.

If you have a cable application that requires frequent or constant flexing, Tape Cable has unmatched advantages. The high flexibility of Tape Cable is the result of the extreme mechanical strength of the polyester insulation coupled with the fine grain texture of the thin copper conductors. Tape Cable has been used in applications requiring continuous flexing.

Tape Cable is available in 25, 100, 500 and 1,000 foot rolls.

YOU MAY ORDER TAPE CABLE DIRECT FROM THIS SHEET

All orders shipped with catalog and instruction booklet. Shipped Parcel Post from Rochester, N. Y. Postage prepaid.

Detailed information, samples, and assistance available from Tape Cable Corp. representatives in all sections of the U.S.A.

*Tape Cable is a Trade Mark of the Tape Cable Corp. Pat. Pend.



The exceptionally varied configuration range of Electro-Snap "standard" subminiature switches today assumes new importance for engineers from the standpoints of both low cost and proven reliability. Whatever your requirements in operating characteristics, terminal arrangements, actuation means, etc., chances are that Electro-Snap can meet them exactly—either with a switch directly from stock, or with minor modification of one of the thousands of performanceproved Electro-Snap standards.

For your next project, check with Electro-Snap on economical, dependable standard, subminiature snapaction switches. Send your specifications today for our prompt recommendations and complete technical data. Write:

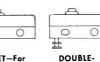
ELECTRO-SNAP SWITCH & MFG. CO. 4236 W. Lake Street, Chicago 24, III.

VA 6-3100 TWX #CG-1400

TERMINAL CONFIGURATIONS (Available for all models)









DOUBLE-TURRET—For multiple lead-in soldering STANDARD-Cross drilled for solder wiring wrap-around solder wiring

Female tubular for std. AMP male dis-connect term, connections

Choice of case material and oper, characteristics available with any terminal type

SUB-MINIATURE BASIC SWITCHES

(E4-100 Series)

STANDARD – (Model E4-103) Sub-miniature basic witch with ambient temperature of -65° to + 250° F. (See other operating characteristics at bottom of page.)

HIGH TEMPERATURE – (Model E4-107) Ambient temperature of -65° to $+350^{\circ}$ F. (Diallyll Phthalate cases with high arc resistance; high impact strength.)

HIGH CURRENT CAPACITY—(Model E4-114) 5 amps.

30V., DC, Ind. Elec. life rating: 25,000 ops.

ADJUSTABLE MOVEMENT DIFFERENTIAL—(Model E4-507) mov. diff. can be adjusted from .002" to .0005", approx.; operating force from 200 to 100 grams, approx. Also adj. contact gap. Amb. temp

-65° to + 350° F.

Actual Size:

25/32" x 1/4" x 23/64



ENVIRONMENT-FREE SUB-MINIATURE BASIC SWITCHES

(EF Series)

SEALED BASIC SWITCH—Approved on QPL—Mil. S. 6743 in accordance with dwg. Ms 25085-1. STANDARD — (Model EF-3) sealed against dust, dirt, heat, humidity and cold. Shock and vibration resistant. Amb. temp.: -65° to + 180° F.

HIGH TEMPERATURE—(Model EF-7) ambient temp. of -65° to + 325° F. Internal switch case of Diallyll Phthalate with high arc resistance; high impact strength.

Actual Size:

15/16" x 11/32" x 19/32"

(Standard switch has 12" leads)



SUB-MINIATURE BASIC SWITCHES

(Slightly larger than E4-100 Series)

LOW DEADBREAK — (Model E4-58) features low deadbreak of .0005" max. Amb. temp. -65° to $+\ 250^\circ$ F.

LOW MOVEMENT DIFFERENTIAL - (Model E4-31) Mov. diff. of .0005" max. Amb. temp.: -65° to + 350° F.

LOW OPERATING FORCE–(Model E4-41) for applications where low oper. force is desired: 135 grams \pm 5 grams. Mov. diff. .002" \pm .0005", Amb. temp.: -65° to + 350° F.

Actual Size:

 $\frac{27}{32}$ " x .260" x $\frac{23}{64}$ "



BASIC OPERATING CHARACTERISTICS

(Sub-miniature Switches—E4-100 Series)

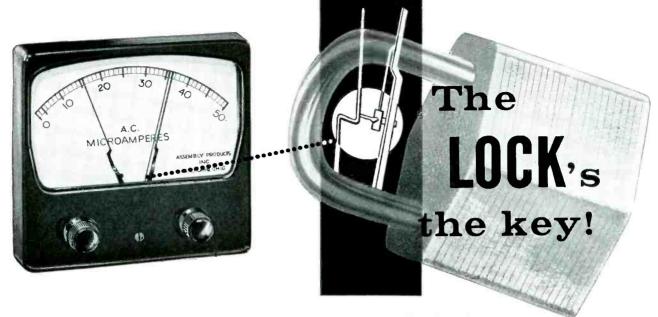
Mech. life rating—150,000 ops.

Elec. Life ratings-

150,000 ops. @ 125/250 V., AC—2.5 amps. 100,000 ops. @ 125/250 V., AC—5.0 amps.

50,000 ops. @ 30 V., DC—2.5 amps. 50,000 ops. @ 30 V., DC—4.0 amps., res.

Approved on QPL, Mil. S. 6743 in accordance with dwg. MS 25085-1. UL Approved.







The only truly dependable meter-relays are those built with locking contacts. For lasting, reliable contact action, meter-relay contacts must make firmly and break cleanly, every time.

An indicating meter with a couple of contacts stuck somewhere inside just won't do. Such an instrument may be excruciatingly accurate as an indicator, but it will fail miserably in a control application.

LET'S CLEAR THE AIR

We make these statements because there seems to be some misunderstanding about how contact meter-relays should be built and what they will do. Since they are the very



heart of our business, we have the greatest concern for their reputation.

Indeed, we think everyone who has anything to do with meter-relays will benefit from a better understanding of them.



Trouble is, a meter movement alone won't do what it should

We use a locking coil to grab and hold the contacts. When they touch, there is no fooling . . . they close. The locking coil develops thousands of times as much presstogether torque as the meter movement alone can generate. For positive separation, our meter-relays have a spring that loads when the contacts lock. When separation is desired, this spring unloads, flicking the contacts apart.

PRIMER STUFF, BUT PERTINENT

Any meter-relay which makes and breaks contacts by depending on the tiny forces inherent in a meter movement has been manufactured by whistlers-in-the-dark. Make and break must come from an auxiliary device. Without it, you'll get, at best, only a halting, exploratory type of contact. On the break, you'll get fluttering and arcing and probably sticking . . . at a point maybe 50% behind where the contact should have separated.



Operates 10,000,000 to 20,000,000 times

HERE'S HOW LOCKING PAYS OFF

Properly used, locking coil contacts will operate reliably 10 to 20 million times. Non-locking contacts will do well to make it through 100,000 cycles, and this at greatly reduced contact current.

GET YOUR MONEY'S WORTH

Meter-relays are used to do hundreds of jobs because they are extremely sensitive, indicating and adjustable. If you've never tried them, we wish you would. If you've tried them It is true that the need to unlock contacts sometimes presents circuit problems. But think of the problems if a meter-relay's contacts won't work at all! Then you don't have a meter-relay—simply a mighty expensive indicator.

and didn't make out so well, we'd like to have you try again.

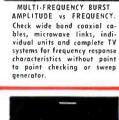
In particular, try our locking coil types so you give meterrelays a fair shake—and do yourself a good turn in the bargain.



ASSEMBLY PRODUCTS, INC., 75 Wilson Mills Road, Chesterland 4, Ohio

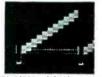
Telephone: (Cleveland, O.) HAmilton 3-4436 • TWX: Gates Mills, Ohio 25-U

ALL VIDEO TRANSMISSION TEST **STANDARDS** in a suitcase and the Portable Unit Produce the same Preclse Test Signals. Model 1003-B Video Transmission Test Signal Generator ★ Completely self contained ★ Portable 🖈 Multi-frequency burst 🖈 Stairstep 🖈 Modulated stairstep ★ White window ★ Composite sync ★ Regulated power supply. Now, Telechrome Video Transmission Test Equipment is available as a completely partable $12V_4^{\prime\prime\prime}$ standard-rack mounting unit. Everyday these Test Signals generated by Telechrome equipment, ame transmitted CoaSt-to-Coast by NBC, CBS, ABC, the Ball System, Canadian Bell and leading independent TV stations throughout the U.S. and Canada. Hundreds of network affiliated TV stations and telephone TV centers thus check incoming video signals.



WHITE WINDOW

LOW & HIGH FREQUENCY CHARACTERISTICS. Determine ringing, smears, steps, low frequency tilt, phase shift, mismatched terminations, etc. in TV signals or systems.



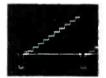
STAIRSTEP SIGNAL modulated by crystal controlled 3.579 mc for differential amplitude and differential phase measurement. Checks amplitude linearity, differential amplitude linearity and differential phase of any unit or system.

ferential phase o. a.., or system. Model 1003-C includes variable duty cycle stairstep (10-90% average picture level).

Model 608-A HI-LO (ROSS FILTER for Signal analysis.



MODULATED STAIRSTEP signal thru high pass filter. Checks differential amplitude.



MODULATED STAIRSTEP signal thru low pass filter. Checks linearity.



1004-A VIDEO TRANSMISSION TEST SIGNAL RECEIVER for precise differences to precise differences. And guin measurements. Companion for use with 1003-B.

DELIVERY 30 DAYS

Literature on the above and more than 100 additional instrements for monochrome and color TV by TE.ECHROME are available on request.

The Nation's Leading Supplier of Color TV Equipment 28 Ranick Drive Amityville, N. Y.

Lincoln 1-3600



The compact, inexpensive, portable Model 1003-8 is all that is required to generate signals for local and remote performance checking of your entire video, cable, or micro-wave facilities.



1531-A OSCILLOSCOPE CAM-ERA—Polaroid type for inscontaneous 1 to 1 ratio proto-recording from any 5" e pilloscope.

What's new for you in GANNON PLUGS



DPJ-33S

DPG-34P







new



Available in square flanged receptacle, Q02, and straight plug, Q06. Insert Diameters: $^{31}/_{44}''$, and $^{12}/_{44}''$



- ▶ Vibration
- ▶ Moisture
- Pressure



with new DPJ and DPG Connectors

New DPJ and DPG Connectors feature sealing by means of a rubber seal around the insert faces. Exceptionally good protection against vibration and undesirable pressure and moisture conditions is provided. The DPG currently is available in 5 different insert arrangements, the DPJ with 3 insert layouts. Write for Bulletin DP-101 TODAY!

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- Vibration Resistant

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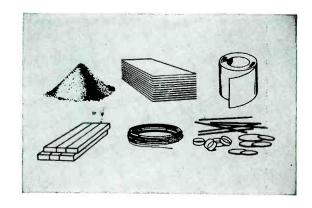
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For your information file

We have four Technical Bulletins giving engineering data on the properties and forms of Handy & Harman Silver Alloys. We Your NO. would like you to have any or all of those that particularly interest you. Your request, by number, will receive prompt attention.

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A SELF-RESONANT, SEMICONDUCTOR INTERRUPTER NO CONTACTS . NO MOVING PARTS . UNLIMITED LIFE

Completely Transistorizes Existing Power Supplies

- UNPLUG VIBRATOR, PLUG-IN VIBRISTOR. NO WIRING CHANGES REQUIRED. RIPPLE AND NOISE ARE EFFECTIVELY ELIMINATED. DUTPUTS AND OVER-ALL PERFORMANCE ARE UNCHANGED.

- NO DAMAGE RESULTS FROM ACCIDENTAL SHORTS OR OVERLOADS.
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- SYNCHRONOUS AND NON-SYNCHRONOUS MODELS AVAILABLE.

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 MAGNETIC SATURATION OF POWER TRANSFORMER NOT REQUIRED.

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 OPTIMUM PERFORMANCE OF SEMICONDUCTORS ASSURED.

 REDUCES NUMBER OF COMPONENTS SIMPLIFIES MECHANICAL DESIGN.

MODEL NO.	TYPE	VOLTS	MAX. AVE. INPUT CURRENT (AMPS)	FREQ. (CPS)	MAX. DC OUTPUT VOLTS
VT603S	S	6	3	115	400
VT610N	N	6	10	115	400
VT123S	S	12	3	115	400
VT125S	S	12	5	115	400
VT241F	F	24	1.5	400	
VT243F	F	24	3	400	

S-Synchronous

N-Non-synchronous

F-Constant Frequency

MANY OTHER MODELS AVAILABLE. DATA ON REQUEST.

VRL, long a leader in the vibrator and vibrator power supply field, proudly announces a new and complete line of transistorized power supplies and associated equipment.

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VRL has pioneered literally hundreds of power supply developments over the past decade and offers a complete design, engineering, and manufacturing service. Send us your power supply requirements for

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General Electric 5-Star Tubes

MADE LIKE A FINE WATCH FOR UNIFORM RELIABILITY!

HEATER. Wire is too critical in fineness to mecsure other than by weight...4.5 mg per 200 mm. Maximum allowable weight variation is ±1%.

cathode. Diameter .03 in, precision-held to =.0005 in. Coating is restricted to a weight variation of ±.25 mg per sq cm.

GRID WIRE. Diameter, .001 in, controlled by weight to ±15 millionths of an inch. Grid No. 1, silver-plated tungsten—No. 2, gold-plated tungsten—No. 3, molybdenum.

GRID TOLERANCES (across minor axis): No. 1, ±.0007 in. No. 2, ±.0007 in. No. 3, ±.002 in.

-GRID SIDE RODS. Held to $\pm .00015$ in.

MICA CATHODE-HOLE DIAMETER. Held to ±,00025 in.

MICA GRID-HOLE DI-AMETER. Held to ±.0005 in.

MICA HOLE SPACING. Cathode-to-grid aperture spacing is held to a max variation of ±.00025 in.

ENERAL ELECTRIC 5-Star Tubes are specially built to the industry's highest standards of craftsmanship and precision. Micro-measurements of a representative type, 5654—a few of which are given above—show the extreme accuracy of manufacture that sets these fine tubes apart from others. 5-Star Tubes are the most reliable you can specify...and the most uniform in their dependability, tube-to-tube.

A wide range of 5-star high-precision, high-reliability types—miniatures and subminiatures—is available for critical military and industrial sockets. Contact the nearest office of the Receiving Tube Department, at right!

ABOVE: greatly enlarged sectional view of a General Electric 5-Star high-reliability 5654. This tube was taken from current production.

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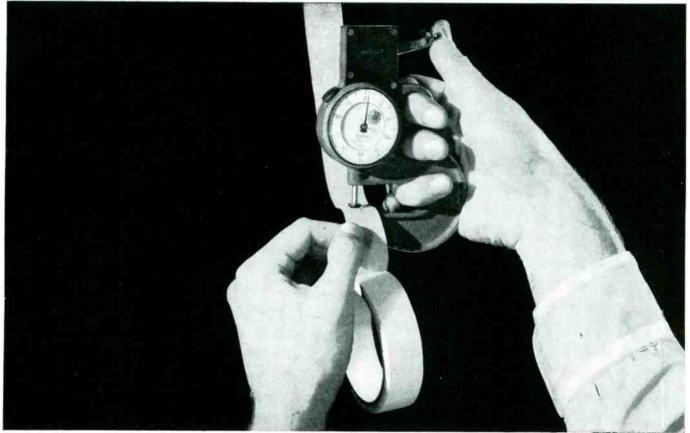
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New TEMP-R-TAPE "C"

Thermal curing pressure sensitive TEFLON* tape .0015" thick, 2500 v/m,— 100° F to 500°F temp. range

CHR's new TEMP-R-TAPE C is made with specially produced .001" cast Teflon film which provides dielectric strength higher than any other Teflon tape. To this ultra-thin backing, .0005" of thermal curing pressure sensitive silicone polymer adhesive is added. The result is a high dielectric tape (2500 v/m) which, when cured in place, has a -100°F to 500°F (-70°C to 260°C) operating temperature range and will withstand much higher temperatures for short periods of time.

As a pressure sensitive tape, TEMP-R-TAPE C is easy to apply. Once cured, it will not creep due to vibration. Curing TEMP-R-TAPE C requires only a short heat time cycle which can be varied to fit production schedules. Peel strength at room temperature is 18 oz./in. width when pressure sensitive — greater than the breaking strength of the Teflon once cured.

For complete information on TEMP-R-TAPE C and CHR's other extreme temperature pressure sensitive tapes, write today to the address below.

*duPont TM

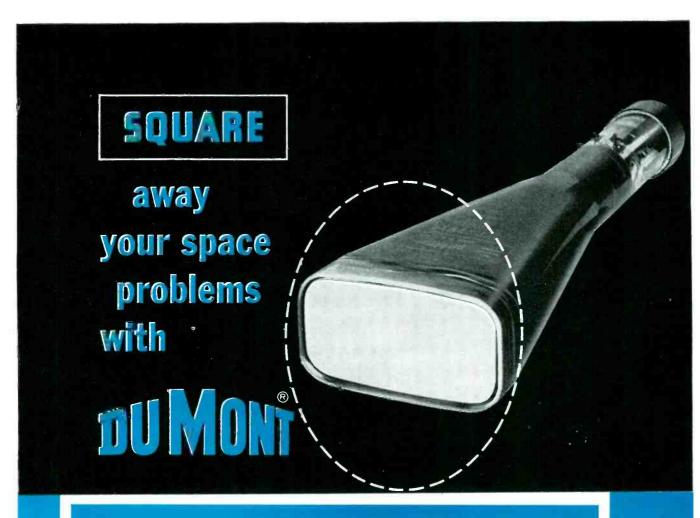
Other TEMP-R-TAPES from CHR

Skived Teflon tape with pressure sensite adhesive006" thick, -100°F to 400° to 200°C) temperature range, 1500 v/s strength. Uses: Class H insulation, nonsmold release, etc. From stock. White and Skived Teflon tape with pressure sensite	F (-70°C) m dielectric stick facing, d colors.
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adhesive013" thick, -100°F to 400° to 200°C) temp. range, 1100 v/m. Use insulation, non-stick facing. From stock.	F (-70°C s: Class H
Teflon impregnated fiberglass tape will sensitive thermal curing silicone adher thick, -100°F to 500°F (-70°C to 260 range when cured, 500 v/m. Uses: Clastion, non-stick facing. From stock.	sive006"
SR Silicone rubber coated fabric tapes ava wide variety of constructions with or wisure sensitive adhesive100°F to 500° to 260°C) temp. range. Uses: Class H ir	thout pres- F (-70°C
Nylon coated nylon fabric with pressur silicone adhesive100°F to 200°F t range. Uses: chafing strips and non-stick	emperature



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Airframe Seals • Coated Fabrics • Silicone Rubber Extrusions, Moldings, Sheet & Sponge



RECTANGULAR

CATHODE-RAY TUBES

Save valuable panel space by using Du Mont Rectangular Cathode-ray Tubes. These tubes permit a larger usable screen area in a given space by elimination of seldom-used segments of the circular screen.

Du Mont Rectangular Cathode-ray Tubes are available in electrostatic or electromagnetic types, in a wide range of screen sizes, shapes and materials. Write for complete technical details...



Rectangular screen for display of single, or superimposed patterns.



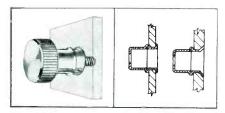
Square screen for display of two signals on a single time base.

	Tube Type	Screen Size	Focus	Deflection	Max. Anode Voltage	Length
DU MONT RECTANGULAR CATHODE-RAY TUBES	B1204 K1206 B1167 B1194 K1442	4%" x 2%" 3½" x 3½" 6" x 7%" 3" x 1½" 6½" x 6½"	Electrostatic Electrostatic Electrostatic Electrostatic Electrostatic	Electrostatic Electrostatic Electromagnetic Electromagnetic Electromagnetic	16 KV	17%" 12" 10" 10%" 123/ ₁₆ "

INDUSTRIAL TUBE SALES, ALLEN B. DU MONT LABORATORIES, INC., 2 MAIN AVENUE, PASSAIC, NEW JERSEY

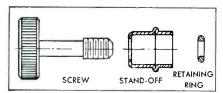
SELECT CLOSURE HARDWARE TO IMPROVE UTILITY, APPEARANCE, AND TO LOWER COST

QUICKLY INSTALLED SOUTHCO CAPTIVE PANEL SCREWS END MISALIGNMENT PROBLEM . . .



Simplicity of design contributes to clean, distinctive appearance and fast, low-cost installation. Stand-off is slipped into panel hole and secured by flaring. Screw is passed through stand-off and made captive by vinyl o-ring.

"Floating" screw design eliminates costly close tolerance manufacture and permits easy engagement regardless of panel distortion encountered under adverse use conditions.



SPECIFICATIONS

Material: Screw is brass, chrome plated; can be supplied in stainless steel.
O-ring is vinyl plastic.
Overall length of screw: 13/6"
Depth of screw head: 1/4"

Sizes:

SCREW HEAD DIAMETER	THREAD SIZE
3/4 11	1/4-20
%6"	1/4-20, 12-24
7/16 11	10-24,10-32

Length of thread: 3/8"

Screw head is supplied plain, as shown, or slotted for screw driver.

FASTENERS FASTENERS LATCHES

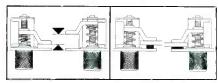
PRE-ASSEMBLED
PAWL ADJUSTS TO
DESIRED THICKNESS
AND PRESSURE



This neat, compact Southco panel and door fastener is supplied assembled, requires but two rivets or bolts for low cost installation. It is available in three models—large, intermediate and midget.

The unique feature of Southco Pawl Fasteners is the fact that, by merely turning the knob, the pawl is adjusted to a wide range of frame thicknesses. This assures a tight grip without precision setting regardless of variations in frame or door dimensions or changes that are produced by wear or warping of sheets.

Pressure exerted by the pawl on the frame is controlled in the same way, by merely turning the knob. Against gasketed frames, pressure can be easily applied to compress the gasket.



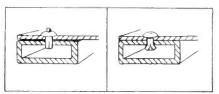
SPECIFICATIONS

Knob: Cadmium or chromium plated steel.

Head Styles: Protruding ribbed or knurled knob; flush screw driver slotted for large size only.

	LARGE	INTERMEDIATE	MIDGET
Knob diameter	7/8 "	%6 ^{††}	11/32 11
Total width	21/2"	1 3/4 11	1 1/8 11
Total height Back of panel	15/16 11	7/8 11	35/64 11
depth	1 23/32 11	11/4	7/8 !!
Knob length	1 1/8 11	15/16 11	9/32 11

FAST, HAMMER-DRIVEN BLIND RIVETS CUT INSTALLATION TIME



You "hit-the-pin" and the river's in. No special tools to limit production or require maintenance, no bucking, no finishing. For blind or open applications, Southco Drive Rivers save time, reduce costs.

Automatic "pull-up" action assures uniform, tight grip.

Southco Rivets are made of aluminum or cadmium plated steel with cadmium plated or stainless steel pins. Diameters are from 1/8" to 1/4", grip range is from 1/16" to 1/8".

Increased widespread use is due to low installed cost and elimination of down time and maintenance associated with fasteners requiring special tools.

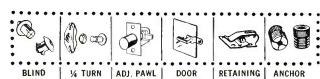
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Fastener Handbook



Send for your free copy of Handbook No. 7, just released. Gives complete data for designers on these and many other specialty fasteners. 52 pages, in two colors.

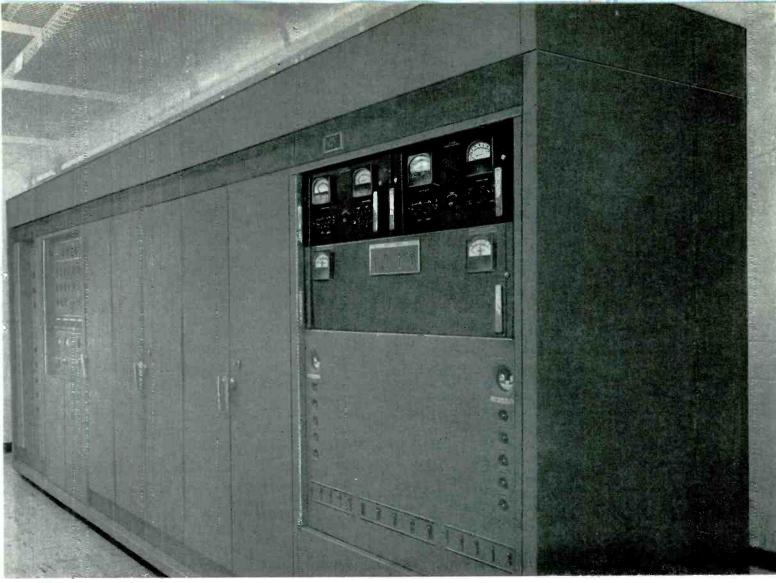
Write on your letterhead to Southco Division, South Chester Corporation, 233 Industrial Highway, Lester,



SPRINGS



RIVETS



IBM stresses need for reliability

Lambda power supplies used in SAGE computer

IBM's Kingston, N.Y., plant of their Military Products Division uses Lambda power supplies to provide the reference voltage for the marginal checking power supply system of the SAGE computer, the world's largest electronic digital computer.

The SAGE computer, whose power requirements are equal to that of a town of 15,000, must possess unprecedented reliability. It is designed to operate effectively 24 hours a day, seven days a week.

Every statistic compiled...every survey made by Lambda...has shown that Lambda power supplies are engineers' overwhelming choice, for industrial as well as military applications.

Write for the complete catalog of Lambda power supplies for all needs through 1.5 amperes. Rack, bench and portable models—for use as original equipment or components—for industrial, laboratory and military requirements.

LAMBDA'S NEWEST COM-PAK POWER SUPPLIES

Save valuable panel space • For all needs through 1.5 amperes Three voltage ranges: 0-200, 125-325, 325-525 VDC.

C-200 series — 200 MA — 5½" panel height — from \$159.50 C-400 series — 400 MA — 5½" panel height — from 244.50 C-800 series — 800 MA — 7" panel height — from 315.00 C-1500 series — 1500 MA — 8¾" panel height — from 550.00





LAMBDA Electronics Corp.

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BASIC RESEARCH More Practical Than You Think

This editorial, one of a special series on the importance of research to the American economy, deals with an aspect of our research program that may have serious consequences in future years — the lag in basic research.

An earlier editorial in this series noted: "The keen interest of U. S. business firms in scientific research points the way to a new kind of prosperity for our economy — a prosperity based on deliberate creativeness." As a result of the dramatic increase in industry's research expenditures, more new products will be introduced in the years 1957-1960 than in any previous four-year period.

A steady stream of new products and new processes means better values for consumers and lower costs for business. And thus it promises to sustain a high level of general prosperity that defies the old laws of boom and bust. But, as we look further ahead, there is a danger that the stream of research discoveries may run dry because of our neglect of basic research.

This danger was described by John Jay Hopkins, late founder and chairman of the General Dynamics Corporation: "Unless there is a revolutionary development in America of pure, not applied, science, there will come a day when there is no use in trading in your old car; because the new one is no better. The only difference between this year's television set and next year's will be the appearance of the cabinet! Scientific progress will be replaced by scientific stagnation."

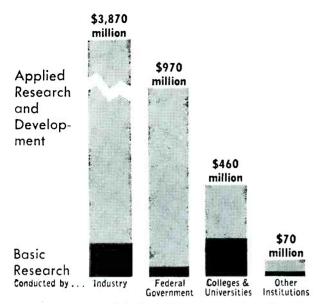
What Basic Research Is

Basic (or pure) research has been characterized as the pursuit of knowledge for its own sake rather than to fulfill some practical objective. It is generally carried out in an environment which allows the investigator the freedom to follow the lead of his curiosity. The scientist in basic research, in the words of Glenn T. Seaborg of the University of California, is not concerned with "utilitarian goals, but a search for deeper understanding of the universe and the living and inorganic phenomena within it."

Impractical as basic research may seem in its initial purpose, it is an essential prerequisite to applied research and product development. A few examples will show how some of the greatest technical advances of recent years have come from basic research projects that had no immediate practical objective:

- Radar an important military development of World War II with broadening commercial applications was the outgrowth of a basic research project whose purpose was to obtain information about the height of the ionosphere, the layer of air that lies some 25 miles above the earth's surface.
- Transistors—the miniature devices which are already vital components of hearing aids, pocket radios and a wide variety of industrial equipment—were invented at Bell Laboratories (research subsidiary of the American Telegraph and Telephone Company) following university investigations into the electrical behavior of solids.
- Neoprene a synthetic rubber was developed by duPont with the help of basic information provided by Father Nieuwland of Notre Dame, who discovered he could control the polymerization (the linking together of molecules) of a certain class of organic compounds.
- Nylon the first of the noncellulosic synthetic fibers that have revolutionized the textile industry grew out of fundamental research by Dr. Wallace Carothers on long-chain polymers.

Only 8% of All Research and Development in the U. S. is Devoted to Basic Research



Data: National Science Foundation, "Funds for Basic Research in the United States, 1953"

Industry's Stake in Basic Research

Industry traditionally has relied upon colleges and universities and other nonprofit institutions for basic research; and the U. S. has long benefited from the greater emphasis placed on basic research in Europe. It is conventional to think that business cannot, and should not, do much about "ivory tower" projects which do not have immediate practical application.

However, there is not so much in this idea as is supposed. The examples above illustrate what Caryl Haskins, president of the Carnegie Institution, has called "the widespread paradox that the most important practical consequences are commonly the least sought after." Furthermore, it is certain that, without adequate basic research, industry's efforts to produce new and better products will become progressively more difficult. And our national defense, in an age of breathtaking military applications of science, will become increasingly precarious.

In the past, our economic growth came largely through expansion into new lands or through discovery and development of rich deposits of natural resources. Such opportunities are relatively limited today. The great opportunities now lie in discovering new materials and new properties of the materials we already have. This is the job of basic research, and industry has a vital stake in it.

The chart indicates the tiny share of research efforts in the U.S. that is devoted to basic research. Only 4% of all research by industry, and only 8% of all research in the U.S., during the year 1953

(the latest for which information is available) represented fundamental research to add to overall scientific knowledge. Even in colleges and universities less than half the research performed is basic research. At least one Nobel Prize winner has expressed the belief that we need and should work toward a doubling of the proportion of our total research effort that is devoted to basic research as soon as possible.

What Business Can Do

Without anything like a staggering increase in the total cost of its research programs, industry could do much to expand our basic research effort. Companies with big research programs should, as a matter of successful survival, be devoting a share of the effort in their own laboratories to basic research. Significantly, companies that are already doing a notable job of basic research have also made an outstanding record of translating such research into new products for industry and the consumer.

Smaller companies may rightly regard the conduct of research projects with uncertain prospects of reward as a luxury. Some basic research, indeed, never results in any tangible payoff. But, with modest contributions, small companies can still have a part in the advance of basic research. They can join together with other companies on cooperative projects. They can support basic research through trade associations and technical societies. They can help research centers in universities and other nonprofit institutions. Arrangements are available in some instances whereby business firms can pay a fee to have access to work done by university researchers.

One way or another, it is up to private business firms to see that basic research moves forward. By doing so they will be laying the groundwork for the development of the new products and technology on which their growth, and the growth of the economy, depend.

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Donald CMC Graw-

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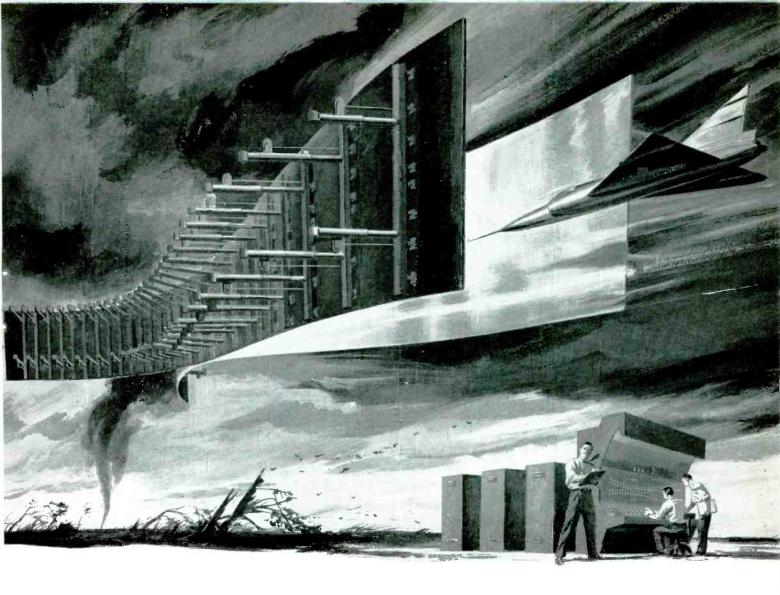
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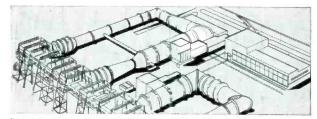
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Sketch of the project, being built by the U.S. Army Engineers for the U.S. Air Force, Arnold Engineering Development Center. Circled area locates the special walls and nozzle.

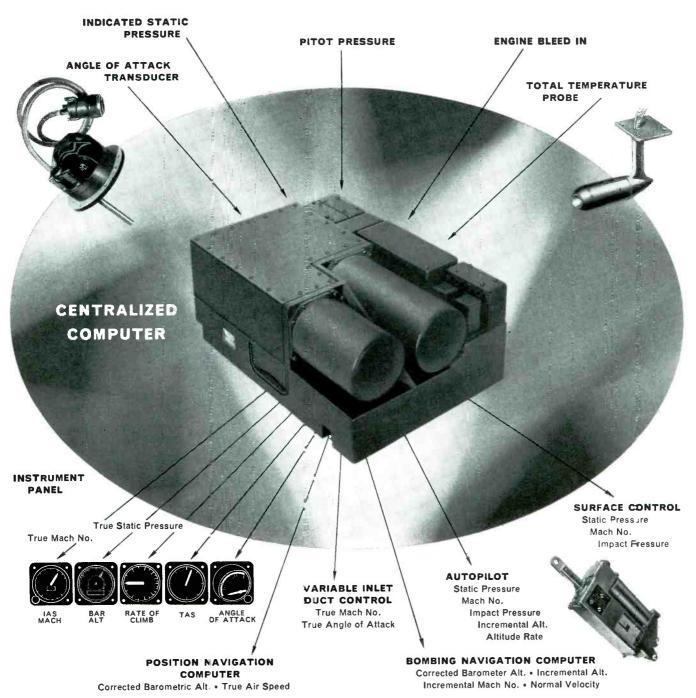


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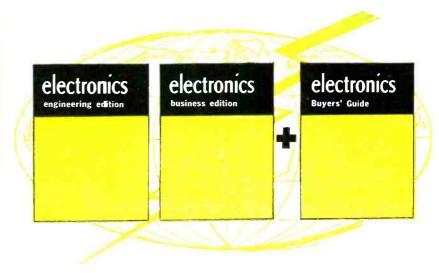
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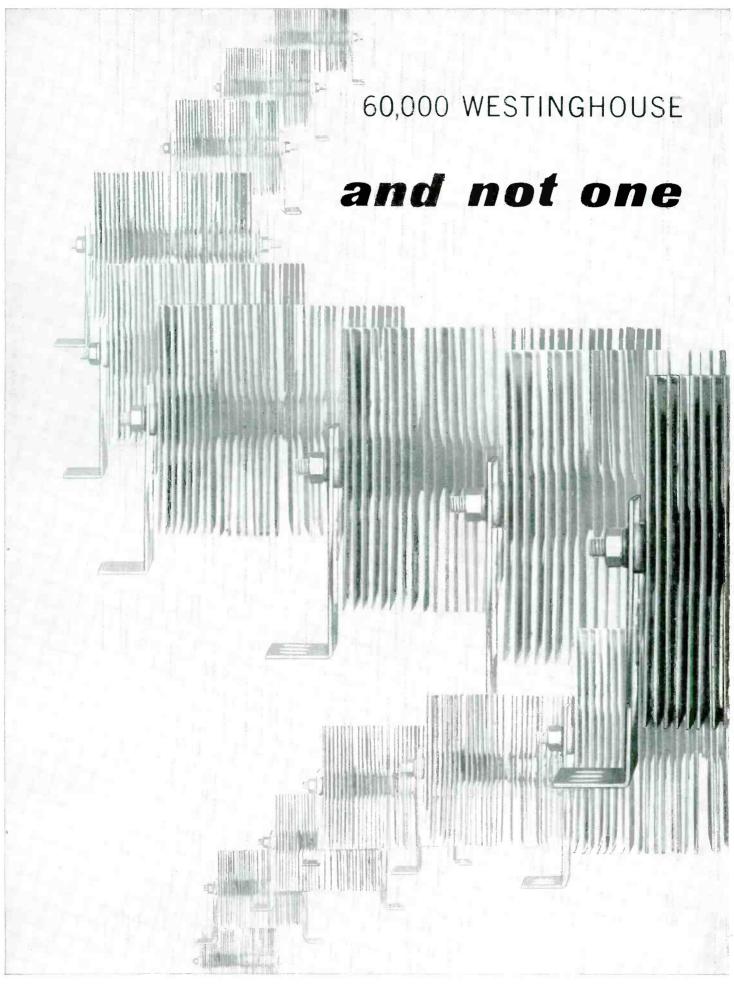




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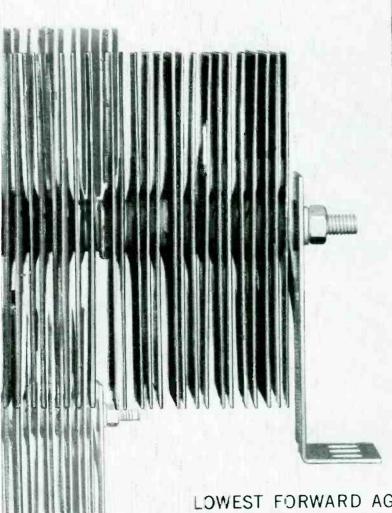
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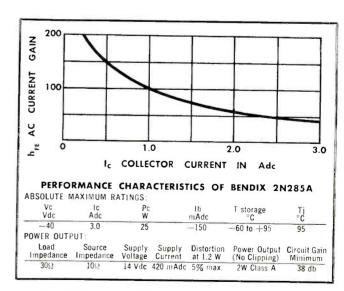
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SPECIFICATIONS

Model	Power*	Connectors	VSWR
160-1F	1 watt	Type N fem.	Less than 1.06, dc to 2 KMC;
160-1M	1 watt	Type N male	less than 1.08, dc to 4 KMC.
160-5F	5 watts	Type N fem.	Less than 1.08, dc to 4 KMC.
160-5M	5 watts	Type N male	Less man 1.00, de 10 4 kme.
160-20F	20 watts	Type N fem.	Less than 1.08, dc to 1 KMC;
160-20M	20 watts	Type N male	less than 1.15, dc to 4 KMC.
160-100F	100 watts	Type N fem.	Less than 1.2, dc to 3300 MC.
160-500F	500 watts	Type N fem.	Less IIIdii 1.2, dc 10 3300 MC.

*Up to 40° C ambient.



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Model	10 kc	3 mc			100 mc		1000 mc	2000 mc
137, 137A				73	63	53	43	37
138, 138A				59	49	39	29	
145	(52	42	32	22	12		
150				53	43	33	23	
139	50	50						

Directivity: 12 db \pm 3 db greater than coupling factor at each frequency. Impedance: Models 137 and 138 are 51.5 ohms. Models 137A, 138A, 145 and 150 are 50.0 ohms. Model 139 may be matched to most im-

Power: Usable to 1000 watts throughout frequency



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Insures sensitive readout for Sierra Directional Couplers. Low VSWR, high sensitivity to 1200 MC. 50 ohm input impedance, filtered output. Type N input, BNC output connectors.

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Hewlett-Packard 684 series Sweep Oscillators are new measuring tools deliberately designed to give you simpler, faster microwave measurements. Four models are provided, covering the G band (3.95 to 5.85 KMC), J band (5.30 to 8.20 KMC), X band (8.20 to 12.40 KMC) and P band (12.40 to 18.00 KMC).

These new instruments make possible microwave investigations and evaluations with a convenience previously associated only with lower frequency measurements. The 684 series oscillators provide a wide range of sweep speeds so that measurements of reflection, attenuation, gain etc., can be displayed on an oscilloscope or recorded in permanent form on X-Y or strip-chart recorders.

Electronic Sweeping

Specifically, the new oscillators provide either a CW or swept rf output throughout their individual bands. The instruments employ new backward wave oscillator tubes whose frequency is shifted by varying an applied potential. Thus, troublesome mechanical stops and tuning plungers are eliminated. Sweep range is continuously adjustable and independently variable; sweep rate is selected separately, and either can be changed without interrupting operation. The full band width can be covered in time segments ranging from 140 seconds (very slow for mechanical recorder operation) to 0.014 seconds (high speed for clear, non-flickering oscilloscope presentation).

Linear Frequency Change

The swept rf output from the 684 series oscillator is linear with time, and a linear sawtooth voltage is provided concurrent with each rf sweep to supply a linear time base for an oscilloscope or recorder. In addition, for convenience in recording and other operations, rf sweeps can be triggered electrically externally and single sweeps can be triggered by a front panel push button. The rf output can also be internally AM'd from 400 to 1,200 cps and externally AM'd or FM'd over a wide range of frequencies.

Rapid Visual Presentation

The variety of sweep rates and band widths available from the new oscillators insures convenience and accuracy for reflection and transmission coefficient measurements and many other production line and laboratory tests. For maximum speed, an oscilloscope such as -hp-130A/B may be used as indicated in the diagram on opposite page. For maximum information and a permanent record, an X-Y or strip chart recorder may be used.

Complete details of a rapid visual method using an oscilloscope or a maximum-data, permanent record method using a recorder may be obtained from your -hp- field engineer. Detailed discussions of these methods are also contained in the -hp- Journal, Vol. 8, No. 6, and Vol. 9, No. 1-2, available on request.

TYPICAL SPECIFICATIONS

Below are specifications for hp-686A Sweep Oscillator, 8.2 to 12.4 KMC. Specifications for hp-684A (G band), 685A (J band), and 687A (P band) are similar except for frequency range.

Types of Outputs: Swept Frequency, CW, FM, AM.
Single Frequency Operation

Frequency: Continuously adjustable 8.2 to 12.4 KMC.

Power Output: At least 10 milliwatts into matched waveguide load. Continuously adjustable to zero.

Swept Frequency Operation

Sweep: Recurrent; externally triggered; also manually triggered single sweep. Rf sweep linear with time.

Power Output: At least 10 MW into matched waveguide load. Output variations less than 3 db over any 250 MC range; less than 6 db over entire 8.2-12.4 KMC range.

Sweep Range: Adjustable in 7 steps 4.4 MC to 4.4 KMC.

Sweep Rate-of-Change: Decade steps from 32 MC/sec. to 320 KMC/sec.

Sweep Time: Determined by sweep range and rate; from 0.014 to 140 seconds over full-band.

Sweep Output: +20 to +30-volt-peak sawtooth provided at a front-panel connector concurrent with each rf sweep.

Modulation

Internal Amplitude: Square wave modulation continuously adjustable from 400 to 1200 cps; peak rf output power equals cw level.

External Amplitude: Direct coupled to 300 KC; 20 volt swing reduces rf output level from rated cw output to zero.

External Pulse: ± 10 volts or more, 5 millisecond maximum duration.

External Frequency: FM and external sweep voltages.

General

Input Connectors, Impedances: BNC; above 10.000 ohms.

Output Connector: Waveguide cover flange; SWR less than 2:1.

Power Requirements: 115/230 volts 50/60 cps ac; approximately 475 watts.

Price: -hp- 684A (3.95-5.85 KMC) \$2,265.00 -hp- 685A (5.30-8.20 KMC) \$2,265.00 -hp- 686A (8.20-12.40 KMC) \$2,615.00 -hp- 687A (12.40-18.00 KMC) \$3,115.00 (Prices above are f.o.b. factory for cabinet models. Rack mount instruments \$15.00

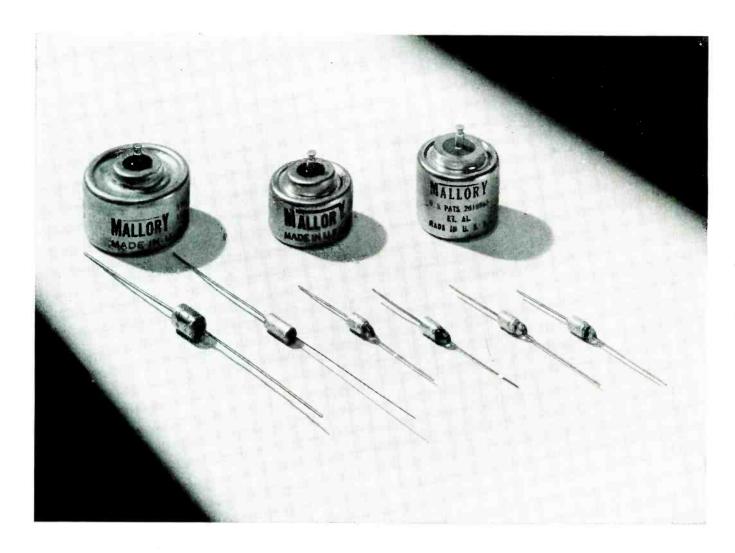
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DECEMBER 1, 1957

How Transistors Operate Under Atomic Radiation

CUMMARY — Results of tests exposing transistor amplifier and single transistor to radiation from nuclear reactor show that degrading effects of irradiation can be controlled to some degree by use of negative feedback when applicable. Radiation effects on coaxial cables showed no noticeable change in r-f transmission characteristics

By ROBERT L. RIDDLE

Senior Engineer Haller, Raymond and Brown, Inc. State College, Pa.

APPLICATION of nuclear energy to propulsion of ships, planes and other devices will require electronic equipment to operate under a wide range of nuclear radiation levels. For circuits to function properly, it will be necessary for designers to compensate for irradiation effects on active circuit elements.

Investigations have been made to find the effects of combined gamma and neutron flux on semiconductor devices. The facilities of the Pennsylvania State University pool-type research reactor were used for an experiment involving the effects of reactor radiation on an all-transistor amplifier and crystal video detector. Arrangement of the test is shown in block form in Fig. 1A.

Test Method

In general, the information desired was the overall performance

of the combined crystal detector and transistor amplifier shown in Fig. 1B. Measurements included tangential sensitivity and transfer ratio of the system (ratio of video output voltage to r-f input voltage). Also determined were r-f attenuation in a coaxial cable extending from the center of the active pile

area to the top of the pool and the h-parameters and I_{ce} measurements on a single separate transistor in the active pile area. Noise in a properly terminated coaxial cable in the active area was also measured.

The tangential sensitivity was determined under the conditions of a 1,000-mc carrier pulsed by 10-

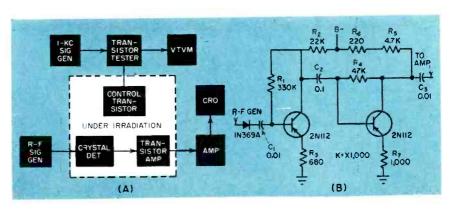


FIG. 1—Equipment setup used in irradiation study (A) with circuit of detector and transistor amplifier (B) ${}^{\circ}$



FIG. 2—Oscilloscope pattern used in determination of tangential sensitivity

Pool-type reactor. Amplifier was placed in aluminum tube for insertion in reactor

microsecond rectangular pulses at 5,000 pps. The tangential sensitivity was measured by adjusting power level so that on an oscilloscope pattern the bottom of the noise during the pulse was even with the top of the noise when the pulse was absent. A typical pattern is shown in Fig. 2. The power level input when such a picture is obtained is the tangential sensitivity.

The determination of the transfer ratio was made from the calibrated attenuator on the signal generator and a calibrated oscilloscope.

The control measurements were included so that the primary effects of radiation on the amplifier-detector system could be separated from

possible extraneous effects.

The irradiation schedule is shown in Table I with irradiation times listed for each power level. Neutron flux ϕ , in neutrons per cm²-sec, is the combined thermal and resonance flux as determined by a cadmium ratio of 9.4 and $\phi_{\rm thermal}=2.07\times 10^8\times P$ as found by activation of foils. This gives $\phi=2.32\times 10^8\times P$, where P is the reactor power in watts. Total flux ϕ includes approximately those neutrons between thermal energies and 2 ev.

The duration of each test in seconds and the integrated neutron flux is also given in the table. Gamma dose was determined from previous calibrations to be equivalent to a dose in roentgens per hour of $4.93 \times 10 \ P$. The gamma dose shown in the table is calculated from this equation. The integrated gamma dose was $3.2 \times 10^{\circ}R$.

Test Results

The results of this experiment are shown in Fig. 3. The tangential sensitivity, the most important measurement on a crystal video system, is shown in Fig. 3A and Fig. 3B. Sensitivity decreased as the experiment progressed. There is a recovery in sensitivity as soon as the reactor is turned off as shown by tests 7 and 8. Test 9, which was performed several hours later, still shows about the same sensitivity.

Upon turning the reactor on again, the sensitivity again decreased with increasing flux. The recovery after removing the apparatus from the flux field, represented by test 15, is not as pronounced as that of test 8. Slight improvement is noticed, however, several hours later.

The results of this test show that the sensitivity is affected by flux density as well as integrated flux. The dashed line represents a guess at the probable effects of integrated flux, and the solid line the actual measurements which represent a combination of permanent and temporary effects. The distance between the solid line and dashed line approximates the effects of the temporary degradation as a result of the flux density. This is indicated by the amount of effective

Table I—Exposure Time for Transistors in Reactor

Test No.	Power in watts	ϕ in Neutrons per cm ² -sec	γ flux in γ/hr	Test duration in sec	Integrated flux density in neutrons per cm ²	Remarks
1	0	0	>100		0	Zero power, residual γ only
2	0.3	0.7×10^{6}	300	420	2.9 ×108	robtantin y only
$\begin{bmatrix} 2 \\ 3 \end{bmatrix}$	10	2.3×10^{7}	793	840	1.95×10^{10}	
4 5	10^{2}	2.3×10^{8}	4.9×10^{3}	540	1.25×10^{11}	
5	10^{3}	2.3×10^{8}	4.9×10^{4}	420	9.75×10^{11}	
6 7	104	2.3×10^{10}	4.9×10^{5}	420	9.75×10^{12}	
7	5×10^{4}	1.16×10^{11}	2.5×10^{6}	480	5.56×10^{13}	
8	102	2.3×10^{8}	$\simeq 5 \times 10^3$	660	1.53×10^{11}	Reactor off
9	Reactor off		≥300	58,440		Overnight decay
-1	10^{2}	2.3×10^{3}	4.9×10^{3}	900	2.09×10^{11}	Calibrate
	0.13	3.1×10^{5}	≥300	14,280	4.3 ×109	Calibrate & off
10	10^{4}	2.3×10^{10}	4.9×10^{5}	1,020	2.37×10^{13}	
11	105	2.3×10^{11}	4.9×10^{6})		
12	105	2.3×10^{11}	4.9×106	1		
13	105	2.3×10^{11}	4.9×10^{6}	1,920	4.46×1014	
14	10^{5}	2.3×10^{11}	4.9×10^{6}	1 ' 1		
15	0	0	0	840	0	Pulled sample out of
16	0	0	0	1,020	0	aluminum tube
17	0	0	0	63,360	0	

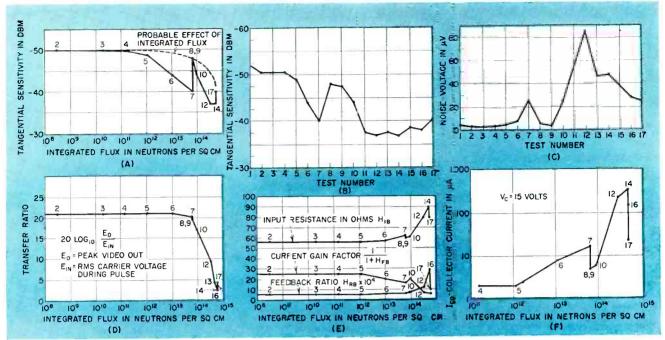


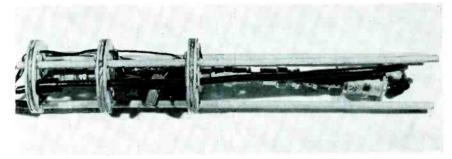
FIG. 3—Results of irradiation study shown graphically are descirbed in text. Numbers on chart indicate test

noise voltage present at the input to the crystal shown in Fig. 3C. This noise voltage is large in those tests where flux density is large. The presence of this noise at these high flux levels results in the decreased tangential sensitivity shown in Fig. 3A and Fig. 3B.

Transfer Ratio

The transfer ratio, measured as the peak-to-peak pulse output to the rms r-f input, is shown in Fig. 3D. No degradation in this ratio took place until an integrated neutron flux in excess of 1018 neutrons per sq cm was reached. From this point on, the transfer ratio dropped rapidly as the integrated flux increased. This same general trend is represented in Fig. 3E which shows the effect on the parameters of the control transistor. This transistor started to degrade at an integrated flux of slightly larger than 10¹² neutrons per sq cm.

The crystal video circuit maintained its gain for an order of magnitude longer. This is probably a result of the degeneration present in the circuit. The transfer ratio recovered slightly after the device was taken from the flux field. This recovery was gradual and may possibly be due to thermal annealing of the defects produced by irradiation. This same effect is noticed in the control transistor parameters.



Transistor amplifier used in test is slipped into aluminum pipe to center of reactor

The I_{co} of the control transistor was also monitored throughout the test and variation is shown in Fig. 3F. The increase in I_{co} may be in part due to internal gamma heating in the transistor.

There was no noticeable change in the r-f transmission through the coaxial cable used as a control. This cable was not monitored for attenuation of video signals.

The noise power produced in a 12-mc bandwidth by the properly terminated cable was -84 dbm residual. The maximum reading on this cable was -82 dbm. This is well below the level of the r-f signal used in the test and also was measured in a much broader bandwidth than that of the crystal detector and transistor amplifier.

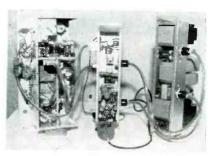
Several conclusions may be drawn from this experiment. Fission spectrum irradiation upon semiconductor devices has essentially three effects. These are transient effects resulting from flux density and gamma heating, semipermanent effects resulting from integrated flux and permanent effects resulting from integrated flux after annealing.

The transient effects caused by flux density are effective mainly in producing noise and increasing I_{co} . The gamma heating, the second transient effect, appears to increase I_{co} and degrades the transistor in the same manner as any increase in temperature. These effects disappear soon after removal from the flux field.

The semipermanent effects caused by integrated flux result from lattice damage and transmutations. The semipermanent damage results in an overall change in the characteristics of the semiconductor devices which usually degrade their operation.



Suppressed-carrier transmitter produces in excess of 100 watts of peak sideband power over the range from 2 to 32 mc



The three sub-units of the suppressedcarrier 100-w transmitter are shown cableconnected for bench testing



Modulation monitor of the one-kilowatt transmitter is visible in the upper right hand corner of the front panel. The three meters to the left of the monitor indicate final stage plate voltage, plate current and load voltage. The r-f unit, modulator and high voltage power supply are panel-mounted below the modulator panel.

Transmitter Circuits For

PUMMARY — Up-to-date transmitting techniques, used to produce suppressed-carrier double-sideband signal, improve efficiency of a-m general-purpose communications transmitters. Transmitters, capable of one-kw and 100-w peak sideband power over 2 to 32-mc frequency range use class C push-push power amplifiers with push-pull screen-grid modulation

By J. P. COSTAS and R. W. FRENCH

Defense Electronics Division General Electric Company Utica, N. Y.

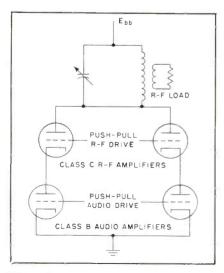


FIG. 1—Series-modulation circuit for suppressed-carrier a-m signal generation

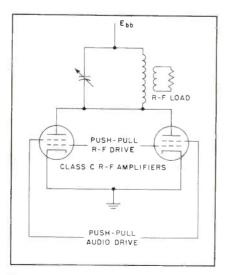


FIG. 2—Screen-grid modulation circuit for suppressed carrier a-m signal generation

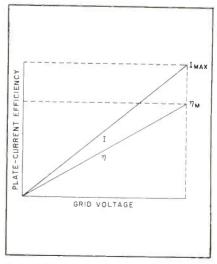


FIG. 3—Current and efficiency curves for grid-modulated class C r-f amplifier

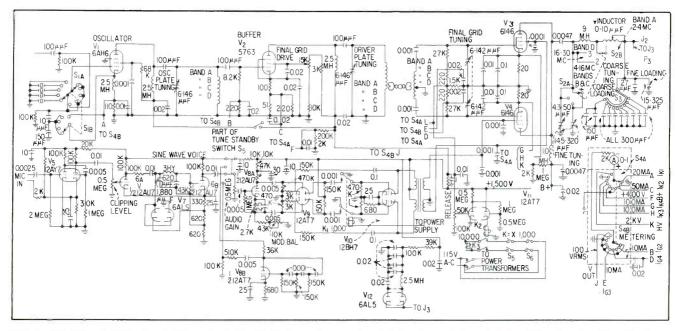


FIG. 5—Circuitry of 100-w transmitter covers the frequency range in four bands of an octave each by using plug-in coils. Nominal output impedance is 50 ohms but impedances up to 500 ohms can be matched over most of the frequency range

Suppressed-Carrier A-M

INVESTIGATIONS to find a more advanced modulating technique to replace a standard a-m system reveal that if a-m is optimized by giving it the same advantages proposed for single sideband, the optimized a-m system is the practical choice for general-purpose communications.

This article presents transmitting techniques used to produce a

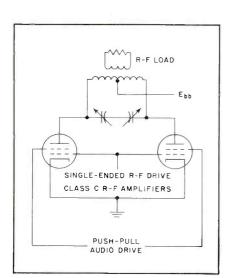


FIG. 4—Alternate screen-grid modulation

suppressed-carrier double-sideband a-m signal.

Eliminating Carrier

Suppressed-carrier a-m signals and balanced-modulator circuits for generating such signals are described in most standard texts on vacuum tube circuits. Although the carrier component in a standard a-m signal contributes nothing to the transmission of intelligence contained in the sidebands and represents a sizable percentage of the total signal power, the carrier component is mandatory for proper operation of all commonly employed second detectors.

Elimination of the carrier allows appreciable reduction in size, complexity and cost of a transmitter for a given sideband output. Recent advancements in receiver development make the presence of the carrier in the transmitted signal unnecessary.²

Series Modulation

Several configurations may be used to produce a suppressed-carrier double-sideband signal. One such circuit is shown in Fig. 1.

Although this particular arrangement has practical disadvantages, analysis of its operation is instructive.

Assuming a sinusoidal audio drive and idealized class-B operation of the audio power amplifiers, plate current then flows alternately through the class-C tubes in the form of half sine waves. The output r-f envelope is a full-wave rectified sine wave with the r-f polarity changing by 180 deg each time the envelope passes zero.

Resistive Load

Since the change in d-c plate voltage across a class-C r-f amplifier is nearly a linear function of the d-c plate current, the two r-f tubes appear as resistive loads to the class-B audio amplifiers. Thus, the d-c power drawn from the supply is converted first to audio power by the class-B audio tubes. The class-C r-f tubes receive and convert this audio power to sideband r-f power fed to the load.

Overall efficiency in the conversion of d-c power to r-f sideband power is excellent since class-B audio and class-C r-f amplifiers are

most efficient in this respect.

The overall efficiency, η_o , of the circuit in Fig. 1 is expressed as

$$\eta_0 = P_{r-t \text{ ave}}/P_{d-c} = \pi \eta_m/4$$
 (1)

Screen-Grid Modulation

In the balanced modulator shown in Fig. 2, a pair of class-C amplifiers, driven in push-pull from the r-f exciter, are screen modulated with a push-pull audio signal. A d-c bias, applied to the screens, cuts off both r-f tubes in the absence of audio drive. Both the efficiency and d-c plate current increases in a nearly linear manner with modulating voltage as shown in Fig. 3. At the peak of the modulating cycle, the class-C efficiency will be at least equal to the normal value η_m of the series-modulated circuit shown in Fig. 1. With a sinusoidal modulating signal, the current drawn from the power supply will be a rectified sine wave with a peak value of I_{max} .

The overall efficiency, η_0 , of the circuit of Fig. 2 in converting d-c power to r-f sideband power is the same as that for Fig. 1.

Peak Sideband Power

If the combined plate dissipation P_d of the two grid-modulated tubes is given, then the peak r-f power output P_{r-f} peak will be

 $P_{\text{r-f peak}} = 2 P_d/[(4/\pi \eta_m) - 1]$ (2) Equation 2 provides a quick estimate of peak sideband power output available from a given pair of tubes used in the circuit of Fig. 2 under conditions of sine-wave modulation.

In a practical screen-grid circuit, some d-c plate current flows in the

absence of modulation. In addition, the minimum instantaneous plate voltage on modulation peaks must be limited to the peak modulaton voltage on the screen grid or clipping of the modulation envelope peaks will occur. These two conditions will lower the plate efficiency.

An overall efficiency of 50 percent, based on r-f power delivered to the load, is readily obtainable in practice using sine-wave modulation. As shown in Fig. 3, the efficiency of the final stage is proportional to the amplitude of modulation voltage on the screen grid. Thus, efficiency is increased by using a modulation waveshape having a low form factor.

By using speech clipping in the modulator, a square wave is approached and the resultant increase in efficiency and average power output makes possible an even further reduction in equipment size for a given sideband power output.

Transmitter Design

The principal differences between the suppressed-carrier transmitter and a standard a-m transmitter occur in the final-stage circuitry, the method of modulation and the modulation power required. Figure 2 is a class-C push-push power amplifier with push-pull screen-grid modulation. Control grids of the tubes are driven by the r-f excitation.

An alternative circuit, Fig. 4, has the control grids in parallel and the plates in push-pull. Circuit choice is usually dictated by the plate circuit network desired.

An incidental advantage of the balanced-modulator circuit is its

self-neutralizing feature.

The modulation power required is only a few percent of the r-f output power. This low modulation power, plus elimination of the carrier, permits considerable saving in size and weight compared to a standard a-m transmitter using high-level modulation. Screen grids of the final tubes are returned to ground or to a negative bias. The low standby plate power input, in the absence of modulation, permits high output power on voice peaks without exceeding the average plate dissipation rating of the final tubes.

Distortion Compromise

Because the screen-grid voltage against plate-current characteristic becomes less linear as the screen-grid voltage is made more negative, a compromise between standby plate power input and audio distortion is necessary in establishing the value of bias to be used. Push-pull modulation reduces even-order distortion due to the nonlinear screen-grid characteristic. Distortion may also be reduced by employing r-f or audio plate-current feedback.

Modulator design for speech is straightforward. The two principal differences between this modulator and that in a plate-modulated standard a-m transmitter are: the lower output power of the former and the addition of an audio oscillator for modulation during final-stage tuning and loading adjustments.

The final-stage plate-voltage supply should have fairly good regulation as the plate current variation when voice modulation is used is similar to a class-B modulator stage.

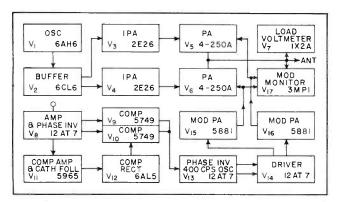


FIG. 6—Block diagram of the 1-kw transmitter uses a voice-compressor circuit in the modulator

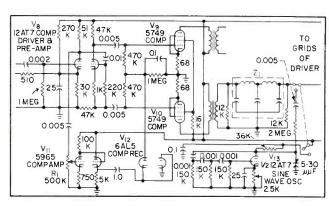


FIG. 7—Voice compressor circuit, of the 1-kw transmitter, has a linear compression range of 13 to 20 db which is set by R_1

The developmental transmitter produces over 100 watts of peak sideband power over the frequency range from 2 to 32 mc. The schematic is shown in Fig. 5.

The exciter is of conventional design. The frequency range is covered in four bands of an octave each by using plug-in coils.

A clipper-filter raises the average power output on voice operation. Stage V_{su} , an R-C phase-shift oscillator, provides a 400-cps sine wave for modulation during final-stage tuning and loading. A single 12 BH7 dual triode V_{10} , used as a class AB, modulator, provides power for modulating the pair of 6146 final tubes V_s and V_4 . Relay K_1 prevents modulation when the final stage plate voltage is off, thus protecting the final tube screen grids against damage in case of accidental modulation.

Protection

Time-delay and final-stage protection is provided by V_{11} and associated components. Relay K_2 is not energized until the equipment has been on for at least 30 seconds and unless the final-stage grid current is above a minimum predetermined value.

Because the contacts of K_2 are in the coil circuit of plate transformer relay K_3 , the mercury-vapor rectifiers are protected against premature application of plate voltage and the final tubes are protected against loss of drive. A peak detector circuit, provides an indication of output voltage, convenient when tuning and loading the final stage.

The pi-network, used to match the final tubes to the load, gives good harmonic reduction and permits matching a wide range of load impedances. Nominal output impedance of the transmitter is 50 ohms but impedances up to 500 ohms can be matched over most of the frequency range.

Complete metering of the transmitter is provided by the milliammeter and selector switch S_4 .

1-kw Transmitter

The 1-kw transmitter is capable of 1-kw peak sideband power output over the range from 2 to 32 mega-

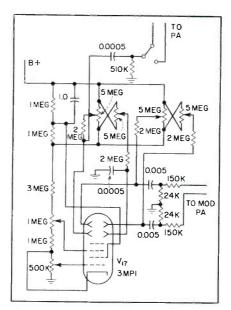


FIG. 8—Modulation monitor of the 1-kw transmitter uses a 3MP1 crt

cycles and is scaled-up version of the smaller one just described with some added refinements.

A block diagram of the 1-kw transmitter is shown in Fig. 6. A voice compressor circuit shown in Fig. 7 is used in the modulator. It has a linear compression range of 18 to 20 db, depending on the initial compression level, set by potentiometer R_1 in the grid circuit of the first triode of V_n . Attack time of the compressor is approximately 5 millisec and the release time is 0.2 sec. Above the linear compression range the compressor output falls off, preventing overmodulation and clipping of the r-f envelope. Low-pass filter Z_1 following the compressor has a cutoff of 3500 cps, with a minimum attenuation of 40 db above cutoff.

Modulation Monitor

A 3MP1 crt, V_{178} is used as a modulation monitor. The circuit is shown in Fig. 8. The bow-tie pattern obtained during modulation provides a check on modulation linearity and is useful during tuning and loading of the final stage. A 2-to-1 and 4-to-1 attenuation of the r-f signal applied to the vertical deflection plates ensures usable pattern size for a wide range of load impedance.

The exciter portion of the transmitter is bandswitched. The only bandswitching required in the final

plate circuit is the application of additional shorting contacts on the unused portion of the variable inductor, on the two highest frequency bands to prevent self-resonances of the unused portion of the inductor from occurring at the operating frequency.

Final Stage

A combination of series and parallel feed is used in the final stage plate circuit. No commercially available r-f choke was found to have sufficiently high impedance over the continuous frequency range employed to allow its use as a parallel-feed directly to the tube plates. Satisfactory operation was obtained by shunt feeding at the load end of the variable inductor, where impedance level and thus r-f voltage are much lower than at the plate end.

Line power consumption with sine-wave modulation and an output of 1-kw peak sideband power is 1,850 watts. The developmental unit weighs 310 pounds, but no special effort was made to produce a unit of minimum size and weight.

Power Gain

The transmitter simplicity which results from dsb operation, particularly the self-neutralizing feature, is especially convenient when tubes having high power gain are employed in the final.

Power gain for voice transmission, obtained by simple clipping and filtering techniques, can easily result in 10 db or more increase in average sideband power for a given peak sideband power. The high-level dsb circuit is especially useful since the tubes are operated at class-C efficiency levels. This becomes important when talking power must be kept high while space, weight, and unit input power must be kept low.

Much of the work reported here was sponsored by the Rome Air Development Center of the Air Research and Development Command under Contract AF 30(602)584.

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(2) J. P. Costas, Synchronous Communications, Proc 1RE, p 1.713, 44, Dec. 1956.

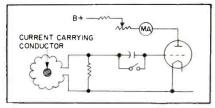
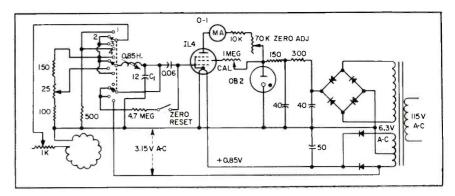


FIG. 1-Basic welding current meter

FIG. 2—Complete welding current meter has four -position selector switch; position 1, no signal input; 2, 0 to 15,000 amperes; 3, 0 to 30,000 amperes; 4, calibration



CUMMARY — Voltage developed by toroidial pickup coil around welding electrode is converted to steady-state meter reading by a-c vtvm circuit. Accuracy is within 3 percent of full-scale meter deflection for weld times of 3 to 30 cycles. Meter holds reading several minutes before needle returns to zero

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Toroid Measures



Fourteen-pound meter is completely selfcontained. Weld-time correction curve in cover increases accuracy to 1 percent. Meter readings in ma are calibrated linearly in kiloamperes of secondary welding current

Several Methods of measuring current in the secondary or welding circuit of an a-c resistance welding machine are in common use. These methods pose problems, such as the need for frequent and careful calibration, the necessity for several current transformers to cover the range of welding currents encountered, the loading of the secondary circuit with magnetic materials thereby changing its inductance, or the requirement of disconnecting and reconnecting the wiring of the welding equipment.

Basic Toroid Coil

An improvement over the standard methods of instrumentation is provided by an air-core transformer or toroidal coil placed around one of the welding electrodes and connected to a suitable circuit, as shown in Fig. 1, to permit a direct reading in terms of actual welding current.¹

The voltage developed by the toroid is a function of the rate of change of magnetic flux produced by the alternating current flowing

through the electrode and the resistive load across the toroid. Only the magnetic flux produced by a conductor inside the toroid will have any effect on this voltage. Flux produced by conductors outside the toroid, even immediately adjacent to it, will not produce any toroid voltage.

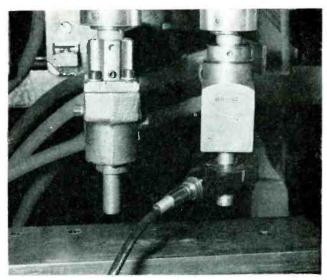
The toroid is a differentiating unit; therefore, the current flowing through the load across the toroid is 90 deg out of phase with the current in the conductor around which the toroid is placed. This presents no problem unless the welding current has a waveform other than a sine wave, such as when the current is phase shifted for heat control. With nonsinusoidal waveforms, the differentiated toroid output current will not resemble the welding current in waveform.

Practical Circuit

A peak reading a-c vtvm is employed in the circuit of Fig. 2 to measure the toroid output voltage, since welding currents normally



Engineer calibrates resistance-welding current meter. Directreading feature permits operation by nontechnical personnel



Closeup shows pickup toroid encircling welding electrode. Toroid can be used with $\frac{1}{2}$, % and $\frac{3}{4}$ in. diameter electrodes

Spot Weld Current

last for only a few cycles.

The toroid voltage is applied to the grid of the 1L4 pentode. A capacitor in the 1L4 grid circuit is charged by grid rectification to the peak value of the voltage developed by the toroid; this capacitor voltage determines the negative grid bias of the tube. The plate current passing through the tube is proportional to the grid bias and is indicated by the milliammeter.

Meter Reading

A maximum plate current of 1 ma will flow when the toroid output voltage is zero; any voltage produced by the toroid will increase the grid bias and decrease the plate current causing the meter to read backward in effect.

Meter readings in ma are calibrated linearly in terms of kiloamperes of secondary welding current; this results in a multiplication factor of one million to one.

The variable resistance in series with the meter permits adjustment of the maximum plate current to exactly 1 ma. The pushbutton

switch can be used to short the grid capacitor after each reading.

The selector switch is provided with four positions. Suitable range resistors are incorporated for the two measuring positions and adjustment is provided to make the high range exactly twice the low range. In the no-signal input position, the toroid may be left in position around the welding electrode with no meter indication.

The d-c filament supply has an adjustable output of 0.85 to 0.9 v. This voltage is critical since the filament acts as the electron source. A lower than normal filament voltage permits measuring lower welding currents, since the cathode-to-ground potential is the limiting factor on the minimum toroid voltage that will effect a change in grid bias.

Calibrator

A built-in calibration circuit applies 3.15 v from one-half of the filament winding across the range resistors to charge the grid capacitor to 3.15 v. A band on the meter

face indicates when this value of grid bias produces the correct plate current.

The 1L4 screen-grid voltage can be varied to control its gain.

The pickup coil consists of a uniformly wound toroidal coil having 12,000 turns with a resistance of approximately 270 ohms and an inductance of approximately 60 mh. The coil is encased in a resilient potting compound and provided with a screw-type, coaxial microphone connector. The low-pass filter in series with the coil attenuates frequencies over 60 cps to prevent transients, which occur when magnetic welding contactors break, from affecting the meter reading.

Although the welding current meter is actually a peak-reading instrument, calibration is in rms current values since these indicate the heating effect of a current and are commonly used in welding.

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(1) A. J. Hipperson, A Mains Operated Valve Voltmeter for the Measurement of Secondary Current in Resistance Welding Machines, Welding Research, British Welding Research Assoc., p 40, June 1948.

Dual-Purpose Circuitry

JUMMARY — Reflex circuit techniques enable design of 1,750-channel transceiver employing only 35 crystals and 28 tubes. Intended primarily for ground-to-air communications in the 225 to 400 mc range, unit may be installed in either fixed or mobile stations, Transmitter delivers at least 15 watts and receiver has sensitivity of better than 5 μv. Spuelch circuit operates on signal-plus-noise to noise ratio

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MODERN MILITARY ground-toair communication requires highly versatile and reliable radio equipment operating in the uhf range. In the set to be described only 35 crystals and 28 tubes are used to obtain 1,750 usable communication channels and to perform all transmitter and receiver functions. Remote-control facilities permit the selection of twenty channels, each of which may be preset to any of the 1,750 frequencies by a built-in memory drum accessible on the front panel.

All channels are instantly available at the manual channel-selector switches.

The receiver sensitivity is less than 5 μv for a 10-db signal-plus-noise to noise ratio. The audio output is 1 w into a 600-ohm load and 100 mw into a 120-ohm load. The transmitter output is 15 w or more across the 225 to 400-mc band.

The radio set has facilities for remote control, retransmission and interphone. It is adaptable to vehicular d-c, vehicular a-c/d-c and relay-rack a-c operation. All func-

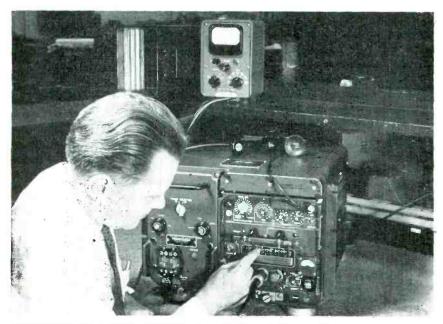
tions are detailed in the block diagram of Fig. 1.

Reflex Technique

Referring to the receive condition in Fig. 2, the first conversion ratio exceeds 7-to-1 and the second and third conversions are more than 5-to-1 each. The final i-f is 500 kc. This is advantageous for control of frequency drift with temperature and makes possible a bandwidth of 85 kc at the 6-db points and 145 kc at the 60-db points, thus assuring reception of all on-channel signals and adequate rejection of adjacent channels.

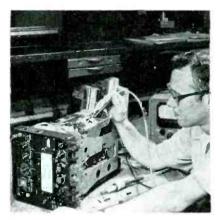
The r-f amplifier and first and second i-f amplifiers are reversed in direction by the first and second transmitter mixers. The crystal switching relay associated with the third injection oscillator is employed to index the oscillator switch 180 deg, thereby selecting the appropriate crystal to match the second i-f directly in the transmit mode of operation. This is possible because a combination of high and low side injection is used in the receive condition as tabulated in Fig. 2 for the third crystal frequency.

The synthesis of the transmit signal may now be traced from its origin at the third injection oscillator. From this point it is fed through the third receiver mixer tube into the passive filter which is the receiver second i-f, having a

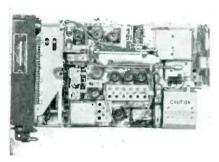


All channels are instantly available by manual switching, while any twenty of them may be preset for remote simplex-only operation

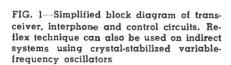
Cuts Transceiver Size



Ruggeddness of system doesn't prevent



Transceiver interior less power supply shows compact mechanical design required to maintain space requirements



frequency range of 3 to 3.9 mc. From here the signal is fed into the first transmitter mixer where it is added to the 17 to 26-mc secondinjection oscillator. Emerging from this mixer as one of the group of 100 frequencies in the range 20 to 29.9 mc, it is then amplified through the first i-f amplifier. From here it is applied to the second transmitter mixer where it is added to the first-injection oscillator system which produces 18 frequencies in the 200 to 370 mc range in 10-mc steps. At this point the signal emerges at final frequency and passes through the receiver r-f amplifier and thence to the power amplifier and antenna.

Receiving Mode

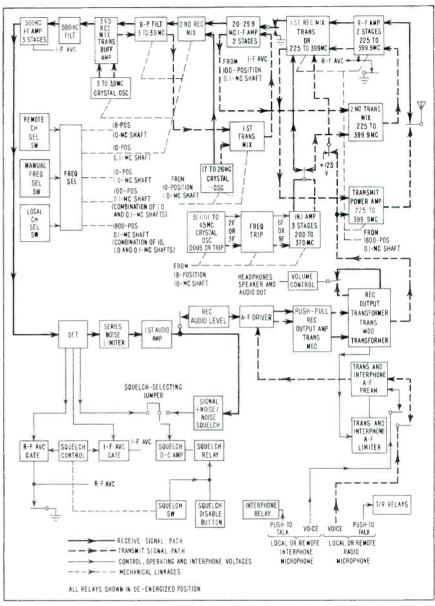
Operation of the r-f section of the receiver-transmitter in the receiving mode is straightforward as seen by the path of the 271.7-mc signal through r-f and i-f circuits.

The first and second transmitter mixer and power amplifier are disabled.

As the signal emerges from the

first transmitter mixer, Fig. 3, it is amplified in the first i-f amplifier as a 20 to 29.9-mc signal. From here it is fed to the second transmitter mixer and emerges at output frequency. It is then amplified and at the output of the driver it is well above 1 w in level. A small amount of the output of the first injection oscillator is also fed across the open contact of injection relay K_1 to the driver tube, thus heterodyning the signal back down to the 20 to 29.9-mc region.

Passing through the first i-f am-



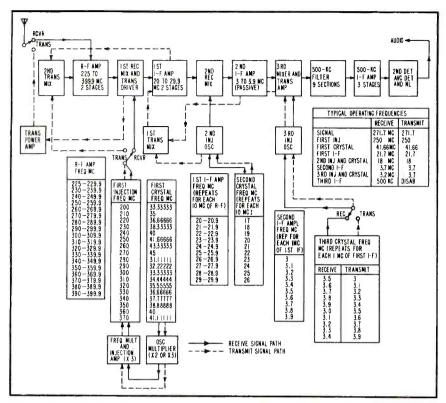


FIG. 2—Basic functional diagram and frequency plan in discrete 100-kc steps

plifier once again, this signal would create a loop oscillation. To eliminate this feedback path a contact is added to the injection-oscillator coaxial relay to ground this path. Since the contact also grounds the first coil of the first i-f amplifier transformer, in Fig. 4, the output of the first transmitter mixer is fed into the second coil of the

transformer to prevent loading of this signal.

The reflex idea is also applied to the audio circuits. The push-pull-parallel modulator and its driver are used as a low-distortion output stage for the receiver, saving two tubes and an output transformer. Since the modulator is operated class AB_2 the static plate current is

low, providing efficient operation in either the receive or transmit condition. Junction diodes are employed throughout the detector, age and squelch portions of the audio circuits.

Spurious Responses

Control of spurious outputs is obtained by several measures: use of conversion ratios of not less than 5-to-1; careful control of mixer levels; proper shielding and filtering of the three oscillator circuits; correct choice of crystal frequencies and high-level mixing in the second transmitter mixer.

The most sensitive point in the set is the first mixer grid where the i-f sensitivity is only 2 or 3 μv . Crystal frequencies are chosen such that harmonics do not fall within the i-f range when the particular crystal involved is used. In this radio set final spurious values of about 80 db are obtained without difficulty.

The set is capable of alignment without the use of a signal generator. An ordinary test voltmeter on the grids of succeeding stages is all that is required for aligning the transmitter up to the driver. At this point the antenna reflectometer is useful for the power amplifier and driver alignment. In production models the final receiver i-f amplifier is factory-aligned and the coils resin-encapsulated. Thus

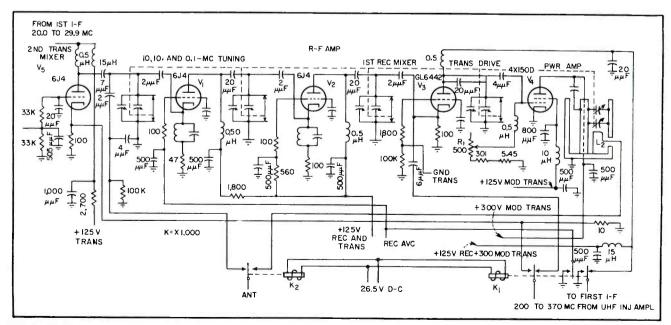


FIG. 3—Radio-frequency sections for transmitter and receiver. Not all circuits are employed in both modes of operation. Final amplifier is cavity-tuned and plate current is adjusted to optimum value by R_i

aligning the transmitter does the whole job for the receiver also.

R-f and Power Amplifier

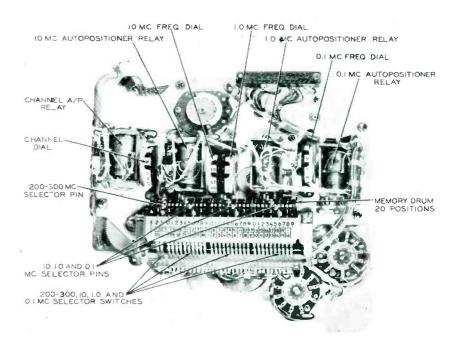
The circuit of the r-f and power amplifier unit is shown in Fig. 3. Stages V_1 and V_2 provide two cascaded stages of radio frequency amplification in transmit and receive. Stage V3 operates as a mixer in receive and as a modulated p-a driver in transmit. Stage V4 is employed as a modulated power amplifier in transmit. Both plate and screen modulation is used. Plate and screen voltages on V_4 are 300 v and 125 v respectively. The screen grid is modulated approximately 55 percent when the plate is modulated 100 percent. Variable grid leak R_1 provides a means of compensating for tube and circuit variations.

The plate current of V_4 is adjusted at 399.9 mc to an optimum value using R_1 . Coupling inductor L_2 adjusts the loading of V_4 . Stage V_5 acts as a high-level plate mixer in the transmit condition. The 20 to 29.9-mc first i-f amplifier signal is injected in the plate circuit of V_5 while the 200 to 270-mc signal is injected in the cathode circuit. Relay K_2 connects the antenna to the cathode circuit of V_4 in transmit.

The plate and screen voltages of V_* and the plate voltage to V_5 are removed when in the receive mode of operation.

Relay K_1 switches the injection from V_3 in receive to V_5 in transmit. The auxiliary contacts of K_1 disable the avc to V_1 and V_2 as well as the first i-f amplifier feedback path in the transmit mode. The interstage coupling units are uhf tuners of the variable L and C type. By varying both L and C a more constant impedance is maintained by the tuners over the nearly 2-to-1 tuning range of the receiver-transmitter. At the output is a capacitively-tuned coaxial cavity.

The circuit of the first i-f amplifier unit is shown in Fig. 4. The 20 to 29.9-mc first i-f amplifier is tuned to one of the 100 frequencies in its operating range by the 100-position 0.1-mc tuning shaft. This shaft operates to position the slugs in the coupled tuned circuits which



Detail of memory-drum tuning control used in transmitter-receiver unit

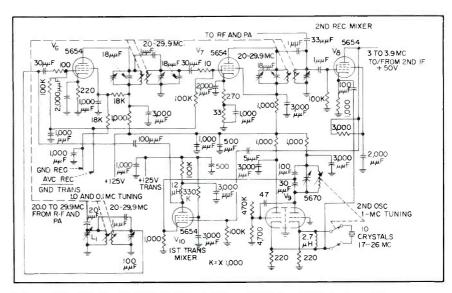


FIG. 4—Receiver first i-f also doubles as intermediate amplifier for transmitter

provide the selectivity required in the first i-f amplifier.

Stages $V_{\rm e}$ and $V_{\rm r}$ operate as cascaded amplifier stages in both receive and transmit. In receive the second receiver mixer $V_{\rm e}$ operating in conjunction with the second injection oscillator $V_{\rm e}$ converts the 20 to 29.9-mc i-f signal to within the range of 3 to 3.9 mc, the second i-f.

Oscillator $V_{\rm 0}$ and the ten 17 to 26-mc crystals provide the 1-mc injection frequencies required by $V_{\rm 0}$ and $V_{\rm 10}$ in receive and transmit respectively. First transmit mixer $V_{\rm 10}$ converts the 3 to 3.9-mc second i-f and the 17 to 26-mc crystal fre-

quency to the range of 20 to 29.9 mc for the first i-f amplifier. Stage $V_{\rm s}$ is disabled in transmit and $V_{\rm 10}$ is disabled in receive by removing plate voltage.

The circuit of the 3 to 3.9-mc second i-f amplifier and the 500-kc filter is presented in Fig. 5. The slug-tuned 0.1-mc tuning units provide the selectivity required in the second i-f amplifier.

The 10-position 0.1-mc tuning shaft determines the slug settings and is ganged to the 3 to 3.9-mc crystal-selector switch. One-half of $V_{\rm n}$ operates as an oscillator in receive and transmit. The other

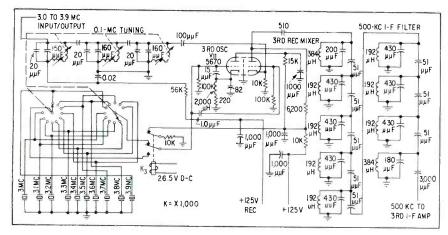


FIG. 5—Second i-f includes oscillator and filter for both transmit and receive

half operates as a mixer in receive and as a cathode follower amplifier in transmit.

In both the receive and transmit the output of the oscillator section of V_n is coupled to the grid of the mixer-amplifier section. In receive the output of the tuning circuit is coupled to the cathode of V_n . The output frequency of the oscillator mixing with the 3 to 3.9-mc second i-f results in an output of 500 kc which appears at the plate of V_n .

The output signal is fed to the 500-kc i-f filter. In transmit relay K_3 operates to shift the crystal frequency 500 kc so it matches the third i-f. The output of the oscillator is thus fed through the mixer-amplifier section of V_{11} now operating as a cathode follower. The output of the second i-f unit is then fed to the first i-f unit. No amplification of the 3 to 3.9-mc signal is necessary in the receive condition

The adjacent-channel selectivity of the receiver is determined by a 9-section lumped-constant filter. By lumping the principle selectivity-determining unit ahead of the final 500-kc i-f amplifier, where most of the gain of the receiver is concentrated, cross-modulation resulting from strong adjacent channel signals is minimized.

The third i-f amplifier contains three stages of video-coupled amplification comprising the second detector, r-f and i-f ave gates, a series noise limiter and the first receiver a-f amplifier. The circuitry is conventional.

An a-m receiver normally employs a squelch which depends on

the incoming signal level to generate enough rectified signal at the detector to operate a gate circuit.

This system, however, is susceptible to any changes in overall r-f gain between the antenna and aural detector. Factors such as tube aging and line voltage changes thus affect the squelch operating threshold. Also, since the gain of a multichannel set inherently varies somewhat across the band, squelch sensitivity is dependent on frequency.

Squelch Circuit

To eliminate these problems a squelch system is used which depends only on the relative ratio of signal and noise. If this system is set to operate at a signal-to-noise ratio of, say, a minimum readable signal level of 3 db, the squelch then opens whenever this value is reached, regardless of varying circuit conditions.

The circuit of the signal-to-noise ratio squelch is presented in Fig. 6. The output of the first receiver audio amplifier is applied to the audio input terminal of the (s + n)/n ratio sensing circuit. R_2 and

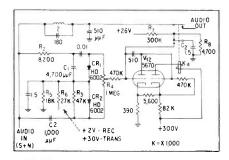


FIG. 6—Squelch system uses signal plus noise-to-noise sensing circuit

 C_1 form a low-pass R-C filter which passes voice frequencies only. The signal-plus-noise output of this filter is applied to CR_1 , which rectifies the low-frequency signals causing the end of R_2 connected to the anode of CR_1 to be negative.

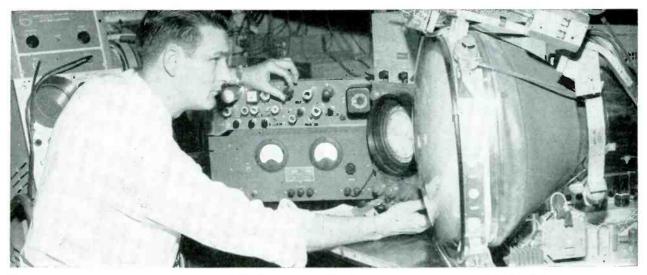
Capacitor C_2 and resistor R_3 form a highpass filter which passes only frequencies above the voice band. The output of this filter is applied to CR_2 which rectifies the noise, causing the end of R_4 connected to the cathode of CR_2 to be positive. Since the currents flowing in R_4 due to the actions of the signal-plus-noise rectifier and the noise rectifier buck each other, the d-c output fed to the grid may have a positive, negative or zero value depending on the setting of R_4 and the signal-plus-noise to noise ratio.

If it is assumed that the bandwidth of the two filters are equal, and that the two rectifiers develop equal and opposite currents in R_* , then the center of R_* would be at zero potential when no signal (noise only) is being received. When no signal or an unmodulated signal is applied, the d-c output of CR_1 and CR_2 , because of the noise, has a 1:1 ratio.

The output of CR_1 is increased because of the presence of the voice-modulated signal and a negative potential is thus applied to the grid of V_{12} , cutting off this section of the d-c amplifier. This allows the second section of V_{12} to draw plate current which energizes squelch relay K_4 . Adjusting R_4 provides a means of selecting the desired (s+n)/n ratio and also of compensating for circuit variations.

Resistors R_5 and R_8 form a bleeder which applies a slight positive bias to the grid of V_{12} . This bias is required since V_{12} energizes the squelch relay when its grid is slightly positive. Capacitor C_2 provides a delay action to prevent interruption of the audio signal during short pauses in the speech. Resistors R_7 and R_8 are used to pre-charge C_2 when the squelch relay is not operated.

The authors acknowledge the contributions of J. H. Durrer of Coles Signal Laboratories, also W. G. Klehfoth and M. W. Caquelin.



Color set is checked out with signals from flat-field generator. Receiver controls are not altered during test

Flat-Field Generator Speeds Color Tv Testing

By RICHARD W. COOK

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by generator that provides composite color video signals of any hue and saturation as well as luminance signal that is variable from black to white. Except for presenting only one color at a time, instrument can replace many functions of encoder or colorplexer in factories, laboratories and broadcast stations

OLOR RECEIVER circuit and crt phosphor purity tests usually require changing the receiver controls from their normal operating settings for flat-field analysis of each of the three primary colors.

Technique

Development of a flat-field colorsignal generator with variable saturation and variable phase from 0 to 360 deg permits making purity checks of all three primary colors without altering the receiver controls. The desired primary is simply injected into the receiver; a quick oscilloscope check insures the proper function of the receiver chroma demodulators so the desired primary color information is always fed to the correct electron gun.

When analyzing color picture tubes, small phosphor nonuniformities causing areas of difference in light output may not be readily apparent when observing one of the primary colors. Using a complimentary color, any nonuniformity of this nature shows up as a difference in hue as well as light output in that area because of the adding of the primary colors to obtain this complementary color. This difference in hue provides a more sensitive observation than simply observing light output, thus providing a more accurate analysis of the picture tube.

Designed for use with existing laboratory, broadcast or manufac-

turing facilities, the generator requires external composite-sync, burst-flag and subcarrier signals.

Circuit

Figure 1 is the block diagram and Fig. 2 the circuit diagram of the generator.

Video amplifier V_{14} provides a short rise time and sufficient gain to gate balanced chroma modulator V_2V_3 through phase splitter V_{18} ; equal and opposite polarity gating pulses are fed to the suppressors of V_2 and V_3 . Subcarrier is applied to the grid of V_2 , the grid of V_3 being grounded.

With no signal into V_2 there will be no output if the gating pulses are equal in amplitude and sym-

metrical in rise time. However, since there is an inherent clamping action by the suppressor if V_z is driven beyond cutoff, the two gating pulses will not be completely symmetrical due to the finite risetime of the gating pulse. This nonsymmetry causes small spikes on the leading and trailing edges of the blanking pulse.

While these spikes may be neglected, their amplitude is further reduced by adjusting the level of the gating pulses so V_2 just reaches cutoff. The two opposing pulses are then more identical in shape, thus decreasing the spike amplitude. Balancing potentiometer R_1 and the 1.5 to $7\mu\mu$ f trimmer reduces these spikes.

The output of the modulator is developed across tuned and damped transformer T_1 that limits the bandpass to about 2 to 5.5 mc.

Flat-Field Production

One feature of this unit is variability of the phase of the subcarrier chroma signal with respect to that of the burst, thus producing any color or signal as a flat field of video information.

Amplifier V_{44} , driven by the output of the chroma modulator, drives T_2 which provides two

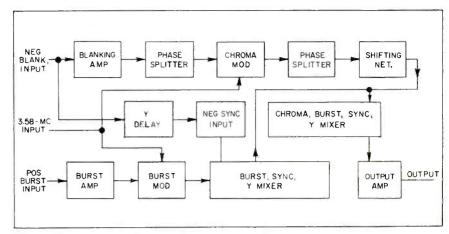


FIG. 1-Block representation of flat-field color signal generator

chroma signals 180 deg out of phase with each other. These two outputs are injected into the phase shifting network at points A and B on the continuously-variable potentiometer.

The values of the resistors and capacitors provide 90-deg phase shifted equal-amplitude signals at C and D on the potentiometer.

By vectorially adding the volttages across the various resistor and capacitor combinations, the amplitude of the output chroma signal will be found to be equal at points A, B, C and D; these will be the maximum values of subcarrier. The minimum values, approximately 3 db lower, will be found half-way between these four points. This variation in output is not objectionable since amplitudes of the subcarrier and luminance signals must be changed for each change of phase to produce a standard chrominance signal.

Burst Pulse Generation

The burst pulse is generated in a manner similar to the chroma information. It differs in that the modulator is biased off except during the burst interval. A positive burst-flag pulse applied to grounded-

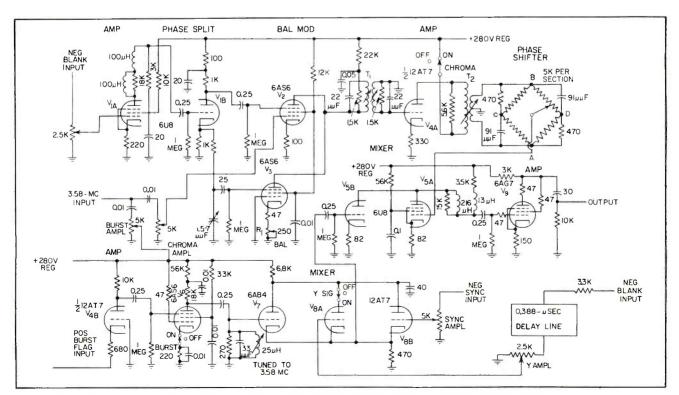


FIG. 2—Four-section continuously-variable potentiometer phase shifts chroma signals to provide variable hues

grid amplifier V_{4H} gates the modulator in the proper phase.

The burst modulator is not balanced; this results in differentiation of the leading and trailing edges of the burst flag being added to the burst signal. The heavily damped circuit across the output of this modulator reduces the amplitude of the differentiated spikes to a satisfactory level.

The burst, sync and Y signals are mixed in a cathode-coupled mixer V_{τ} , V_{sA} and V_{sB} . The burst signal is applied to the grid of V_{τ} and the sync signal is applied to the grid of V_{sB} . The Y signal is received through a delay line so as to match the chroma signal with which it will be mixed. This signal is fed to the grid of V_{sA} . The three triodes are used as cathode followers with a common load resistor.

Composite Signal

The chroma, burst, sync and Y mixing stage, V_5 , contains the various signals of the system into a composite color signal. The output of the phase shifting network is applied to the grid of V_{54} while the output of the burst, sync and Y mixer is fed to the grid of V_{58} .

The composite signal is applied to the grid of power output amplifier V_{\circ} . This is a constant-current amplifier designed to be used as a plate-loaded line driver working into a terminated 75-ohm transmission line to reduce hum on the receiving end of long lines.

Construction

The unit was built on a standard chassis, 5 by 5 by 17 in. wide. Parts placement is not critical beyond the normal practice of good layout design.

Transformer T_1 consists of two identical windings bifilar wound with #38 enamelled cotton covered wire on a $\frac{1}{4}$ -in. coil form. The coils should be wound so that the coupling may be variable for alignment purposes. Transformer T_2 , also bifilar wound on a $\frac{1}{4}$ -in. form, is tuned by a single slug and need not be shielded.

Initial Alignment

The circuits including T_1 and T_2 should be tuned broadly to 3.58 mc with a bandpass of approximately

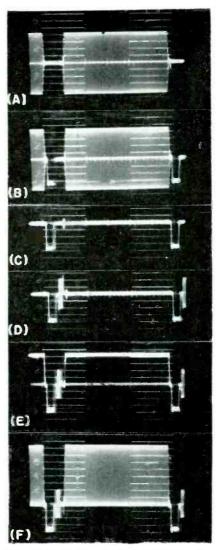


FIG. 3—Typical output waveforms for initially aligning signal generator

3.5 mc. The heavily damped tuned circuit at the grid of V_{τ} should be peaked at 3.58 mc. It may be necessary to temporarily remove the 270-ohm damping resistor to make this adjustment.

To place the unit into operation, the following procedure is suggested. Monitoring the output with a wide-band oscilloscope, increase the chroma amplitude to give 0.88-v peak-to-peak output with all other controls in their minimum gain position. Inject blanking into the system until the chroma signal just reaches zero during the normally blanked region of the signal. The desired results are illustrated in Fig. 3A. The sync amplitude is adjusted, as in Fig. 3B, to be 0.4 v.

The small spikes mentioned previously can be seen by reducing the chroma level to zero Fig. 3C.

Their amplitude may be minimized by adjusting R_1 and C_1 .

A complete video chrominance signal producing a green field may be obtained by increasing the burst amplitude to 0.4 v peak-to-peak (Fig. 3D), raising the luminance level to 0.44 v (Fig. 3E) and advancing the chroma signal until it becomes tangent to the baseline as illustrated in Fig. 3F. This signal should then be applied to a vectordisplay system or phase-measuring device and the phase of the chroma information determined with respect to the burst. Rotating the phase control to obtain a phase representative of a green color and then readjusting the chroma amplitude slightly if necessary complete the adjustments.

Applications

The preceding adjustments are only required in the initial alignment. After the unit is put into operation, the only adjustments necessary will be those determining the phase and amplitude of the chroma information and the amplitude of the luminance portion of the signal.

By substituting a square-wave for the standard blanking pulse a single color bar, a luminance signal with a very short rise time or chroma over any desired portion of the scanning lines, can be formed while leaving the remainder of the line in the black region.

This instrument can perform many functions of an encoder or colorplexer supplying the laboratory or broadcast station with an additional source of a color signal. It is especially helpful when only a color-difference or an I or Q signal is desired for alignment of decoding systems. These signals are obtainable from most encoders only when the encoder is operated in a manner that deviates from its normal condition. Where an encoder is shared by a development laboratory and a factory actively engaged in assembly line production, a change from the normal color signal is usually out of the question.

Acknowledgment is due K. E. Farr for his assistance, encouragement and contribution to the development of this unit.

VIMMARY — Moving target indicator spots and counts bacteria colonies randomly distributed over a flat surface. Spot signals from particles less than 100 microns in diameter are received from cathode ray tube and stored in a 1,000 μsec delay line. Video circuit compensates for spot-to-background density and an anticoincidence circuit determines the correct count delivered to a high-speed recorder. System has wide-range application in medical laboratories

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magnifier and a uniform light source. The count density may vary

from a few to over a thousand and

so counting accuracy depends rather

Automatic Counter

heavily on human factors.

Spot Scanner Counts

BACTERIAL COLONY COUNTING is performed daily in hundreds of biological, dairy, food industry and water testing laboratories. In this technique, a diluted sample of the material to be assayed is cultured in a Petri dish. After incubation, bacteria cells in the culture grow into colonies large enough to be visible. These colonies are counted visually with the aid of a

The bacteria colony counter, described in this article, developed under the sponsorship of the U. S. Army Chemical Corps, provides a scanning method for counting such colonies that is faster and more consistently accurate than the tedious visual measurements performed by laboratory technicians.

In any optical system of scanning, adapted to count random size particles, it is necessary to compensate for the many intercepts a small spot or aperture produces for a single particle. Various methods of solving this problem have been used and reported by other workers.^{1, 2}

Tangency Detection

A pulse storage system, similar to a radar moving target indicator, was designed to overcome the difficulties of multiple intercepts. In mti radar, pulses produced by each scan are stored in an ultrasonic delay line and compared in a cancellation circuit which produces a residue signal. The signals, displayed on the radar indicator, show only the targets in motion.³

The delay used in the system stores all pulses on each scan line

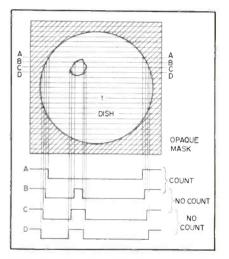


FIG. 1—Tangency detection by signal delay and anticoincidence. The system chosen counts organic and inorganic particles as they are scanned

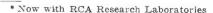
and compares them in an antico-

incidence circuit, with pulses on

the next consecutive scanning line. A time overlap logic circuit produces an output pulse only when an input pulse arrives at just one of its three input channels.

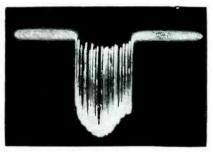
Tangency detection by signal delay and anticoincidence is illustrated in Fig. 1. The traversal time

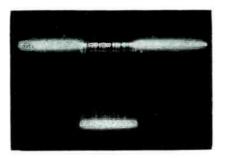
Tangency detection by signal delay and anticoincidence is illustrated in Fig. 1. The traversal time of the scanning spot is equal to time t, the delay time, so all pulses are reproduced exactly one line later. Scanning line A does not intercept the particle and does not produce a pulse. Scanning line B

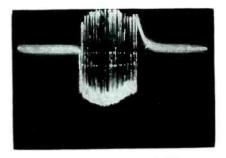




Front view of the electronic particle and bacteria colony counter







Left to right are the output waveforms of phototube, video-compensator and amplitude discriminator as system counts colonies

Micron-Sized Particles

intercepts the particle and produces a pulse, which is fed to the anticoincidence circuit. Simultaneously, information from scan line A appears at the anticoincidence circuit and, because it contains no overlap, pulse B produces a count.

On scan line C a slightly wider pulse is produced. However, the B line pulse also appears at the output of the delay line at such time as to provide a time overlap with the pulse produced by line C. Therefore, a count is not registered. Similarly, the line-D pulse is overlapped by the delayed pulse of line C and again no count is registered. The next line does not intercept the particle and no pulse is produced.

Optics

In the optical system for the line-to-line memory, shown in Fig. 2, a high-quality objective lens images the raster on the Petri dish. The condenser lenses image the exit pupil of the objective lens on the type 6292 multiplier phototube cathode, preventing the motion of the scanning spot from producing any perceptible motion of the illuminated area on the phototube. This minimizes noise or other signals produced by cathode surface nonuniformities.

The size of the scanning spot produced on the high-resolution crt is approximately 100 microns,

imaged at 1 to 1 object-image ratio on the Petri dish. The edge of the dish is masked so that protrusions on the molded edge of the dish or the meniscus of the agar do not produce spurious signals because of refraction.

Scanning pulses are idealized in Fig. 1. In actual scanning, the pulse shape is governed by phos-

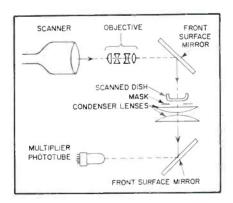


FIG. 2—Optical system uses a highresolution scanner and high-quality objective lens to image the raster on the dish that contains particles that are scanned electronically

phor persistence, spot shape, optical density and shape of the particle, density of the background materials and the system optics. Amplitude of the actual pulses vary and the curved waveshape at the bottom baseline is caused by the varying density of the culture media and nonuniform light trans-

mission of the optical system.

In any lens system, the transmission of off-axis rays will decrease with the fourth power of the cosine of the angle that these rays make with the optical axis. In a wide a considerable angle system, change in light transmission occurs. Added to these difficulties are noise factors of phototubes, nonuniformities in crt phosphors, dust in the optical system or contamination of the culture media. The circuitry compensates, in part, for some of these difficulties.

Complete System

Figure 3 is a block diagram of the automatic colony and particle counting system. The magnetic-deflection system for the type K1429P15 crt is synchronized by pulses from a high-speed standard commercial electronic counter.

The synchronizing pulses are 1 kc for the horizontal and 1 cps for the vertical, producing a 1,000 line raster with a vertical frame rate of 1 cps. Relatively low-speed scan rates reduce bandwidth requirements and need for phosphor correction. Since the electronic counter provides its own time base, it is convenient to use a one-second scan period and timing pulses from the time-base generator to synchronize the sweep circuits.

The crt phosphor and faceplate are especially fabricated to avoid

optical defects. Full protection is supplied to the crt to prevent damage in the event of scanning circuit failure.

The scanner protection circuit derives signals from the output of the magnetic sweep. These signals operate a relay which causes the 20-kv anode supply to shut down and the focusing current in the focus coil to cease in the event of sweep circuit failure. Multiplier phototube signals are transmitted by a cathode follower to a video compensation and Schmitt-trigger circuit.

Video-Compensation

The pulse shapes derived from scanning different types of cultures and particles vary greatly and it is necessary to operate on these waveforms before reliable counts are obtained. The video compensation circuit senses the density of the background material upon which the particles or colonies exist. The circuit is essentially a fast acting d-c restorer which rapidly changes the base level of the pulse depending upon the opacity of the background.

In the photograph of the waveform of the phototube output, the black level is the horizontal line at the top of the waveform and the white or background level is the curved waveshape at the bottom. Video compensation elevates the pulses to the black level or beyond so that the amplitude discriminator may be set for sensitivity only to pulses approaching this black level.

In the photograph of the output of the video compensation circuit, the baseline curvature has been partially corrected and the pulses reach an amplitude beyond the horizontal line or the black level.

Amplitude Discriminator

The amplitude-discriminator detects the signal just below the black level and resets approximately 3v below the firing level. These two levels are shown by bright marks superimposed on the pulses. Triggering and resetting action of the discriminator circuit reduces noise so the final pulses operating the delay line and the anticoincidence circuits appear as shown in the

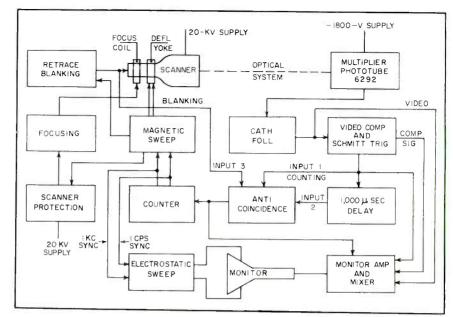


FIG. 3—Block diagram of the automatic particle and bacteria colony counter. The delay or memory system stores pulse counts for each line scan and compares them, in the anticoincidence circuit, with pulses on the next consecutive scanning line

waveform of the amplitude discriminator output pulses. All pulses have uniform amplitude and rise and fall times, simplifying delayline design and anticoincidence circuit functioning. The photometric effect produced by the circuit is one of converting objects having non-uniform density to uniformly opaque objects.

Delay Line

The 1,000- μ sec delay, exactly the time of a single horizontal traverse,

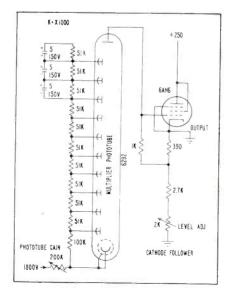


FIG. 4—Multiplier phototube signals are transmitted by a cathode follower to the video video-compensation and Schmitt trigger circuit shown in Fig. 5

is supplied by a fused quartz acoustic delay system. The 1,000- μ sec delay line is fed to the anticoincidence circuit which produces output counting pulses in accordance with tangency detection.

Waveforms from the phototube, the video compensation circuit and the amplitude discriminator can be monitored and a picture display showing an image of the scanned field, which can check the counted particles, is provided. The monitor crt is electrostatically deflected by sweep circuits and synchronized by the 1-kc and 1-cps time-base pulses of the electronic counter.

Circuits

The phototube circuit schematic is shown in Fig. 4 and the video compensating amplitude discriminator and delay line circuits are shown in Fig. 5. To avoid possible restoration distortion of the scanned signal, d-c coupling is used from the photocell through to the output of the amplitude discriminator.

Phototube output is fed to a d-c coupled amplifier whose cathode is connected to a diode detection circuit. Negative-going signals, detected by these diodes, supply a bias voltage at the grid of cathode follower $V_{\rm M}$. This bias voltage is proportional to the amount by which the negative going or white por-

tion of the signal exceeds a fixed amount determined by R_I . This bias signal is fed continuously to the second grid of amplifier V_1 to adjust its output level according to the background density of the culture medium.

Discriminator

The output of V_1 is coupled directly to amplitude discriminator circuit, V_4 . The discriminator output goes directly to one channel of the anticoincidence circuit through amplifiers V_{5B} and cathode follower V_{6} . The signal is inverted at the plate of V_{5B} and fed to the modulator. The fused-quartz delay line operates at a carrier frequency of 15 mc, supplied by the crystal oscilator at V_{7} . Driver amplifier V_{6} is grid bias modulated by the output of modulator V_{5A} .

The 15-mc modulated carrier is transmitted into and out of the quartz input and output transducers on the delay line. At the bandwidth required, about 2 mc, the signal is attenuated at the output of the delay line by approximately 100 db. Tuned amplifier V_{ν} amplifies this signal and couples it to phase splitter V_{ν} .

The carrier is demodulated by diode detectors and coupled to video amplifier $V_{11:4}$. The output passes through the cancelling channel of the anticoincidence circuit through cathode follower $V_{11:8}$. An adjustable, thermostatically controlled oven for the delay line stabilizes and adjusts the operating temperature of the fused quartz for a velocity of propagation, exactly in accordance with the 1,000 μ sec delay required.

Anticoincidence

In the anticoincidence circuit of Fig. 6, the undelayed signal output of the amplitude discriminator circuit marked input 1, is coupled to peaking amplifier V_{14} . This amplifier provides sharp pulses at both the leading and trailing edges of the pulse produced by the scanned particle and trigger circuit. The leading-edge pulse is amplified by V_{158} and coupled by cathode follower V_{164} to a diode section of V_{164}

Memory capacitor C_1 charges to about 10 volts. This charge cannot leak off except through the high

back resistance of the discharge diode section of V_{16} . The capacitor charge appears at one of the grids of the gating mixer tube V_{18} . The trailing edge pulse is amplified by V_{17B} and fed through cathode follower V_{17A} to the other control grid of V_{18} .

Gating tube V_{18} is biased so the voltage on one of the two control grids cannot turn the tube on. However, when the memory ca-

cannot conduct. This is the method of cancellation. A duplicate cancelling channel, input 3, receives horizontal and vertical flyback gating pulses and discharges the memory capacitor at the end of each line scan.

Check Marks

The picture monitor enables the operator to see whether the scanning and counting circuits are func-

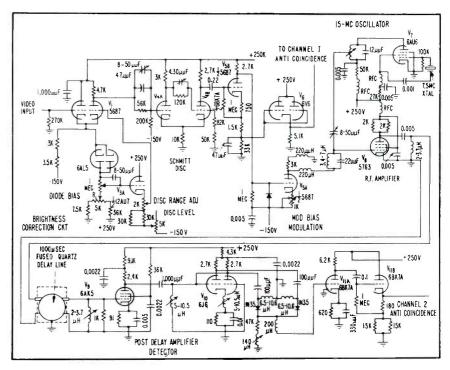


FIG. 5—The video compensation circuit senses the density of the background material upon which the particles or bacterial colonies exist

pacitor is charged and the trailingedge pulse reaches the other control grid, the tube conducts producing a sharp negative pulse at its plate. This is the counting pulse, amplified by V_{194} , coupled to cathode follower V_{194} and passed to the counter.

The output of the delay line is coupled through input 2 to cathode follower V_{18} and d-c restorer V_{12} to the discharge diode. A pulse at the output of the delay line appears at the cathode of one of the diodes of V_{18} , causing it discharge memory capacitor C_1 .

If an input-2 pulse appears at any time after the memory capacitor is charged and before the trailing edge pulse of input 1 appears, then the memory capacitor is discharged and the gating tube $V_{\rm 1s}$

tioning properly. A bright check mark or pip on the image indicates each object detected and counted by the anticoincidence circuit. Thus the monitor image shows whether all objects in the field were counted.

Effects of Particle Shape

One limitation of tangency detecting for counting is that if the object shape has a reentrant or U-shaped profile, oriented so that the first intercepting line intercepts both legs of the U, two counts will be produced. Except for the reentrant profile type of shape, the counting system is relatively insensitive to size or shape of the object. The system is not confused by objects inside of other objects provided there is a clear

space between them of at least one scanning line.

Random Orientation

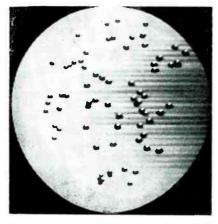
When two objects overlap in a horizontal direction they will present two tangent points to the scanning lines and produce two counts. However, in vertical overlap, perpendicular to the scanning line, the system will register only one count where two particles exist. This can produce a substantial error when colony or particle populations are high and distributed so that a large number of contiguities exist. Statistical correction factors can be used to compensate for these errors.

Counting Accuracy

The particle detector produces counts within 3 percent of those obtained by electrical probe methods when the concentrations or populations are about 100 colonies on a plate. As the population density of culture plates increases, the contiguity, increases and the machine consistently produces more count errors.

This error condition is also frequently true of technician counting where for high population densities the count is often estimated.

It is sometimes possible to count bacteria at an earlier stage in incubation. The smaller the colonies.



Monitor picture of counted colonies of bacteria as seen with equipment

the lower the probability is that colonies will be in contact.

Details on count accuracy and test results are found elsewhere.

Applications

The advantages of the particle counter lie in the freedom from human errors, in the ability to gather large masses of data in a short time and the ability to analyze much larger and therefore more representative samples.

Any objects that can be placed in a Petri dish may be counted provided they are large enough to be resolved about 0.5 mm diameter and they have sufficient optical density, about 0.3.

Particles which differ sufficiently

D-C RESTORERS 100 K +250 V -6BJ7 AMPLIFIER PEAKER + 250 V INPUT 3 +250 V +250 V INPUT FLYBACK CANCELLING 0.001 V13 DELAYED _ 5687 +250 V ₹5.6 K 0.01 10 K IK ≸ 0.01 3120-220pH 25963 K = X 1,000 CATH FOLLOWER 15963 CHARGE DISCHARGE 68J7 12AT 100 u p F CATH AMPLIFIER UNDELAYED__ 43K -150 V + 250 V + 250 V MIXER 100 ppf CATH FOLL +250 V AMPLIFIER 36BJ7 12 AT7 10 K 5 5 9 6 3 CLIPPER 001 6876 15963 0.022 0.01 MEG ₹ COUNTER **§** 5.1 K MEG MEG BIAS ADJ 20 K 43 K -150 V +250 V -150V 6.8K - 68 K

FIG. 6-Anticoincidence circuit. Charge on memory capacitor C1 determines whether gating tube can conduct hence it can be used to cancel signals

in size may be counted separately by defocusing and subtracting or by refined circuit techniques. Differential counts of colored particles may be made by using color filters in the optical system. By suitably inverting the photocell signal, the holes in an object or hyaline phage colonies in an otherwise opaque plate may be counted. Circuitry and equipment are under development to enable analysis of all such information

Scanning techniques are applied to differential blood counts; specific cell populations in tissue cultures; marine and other media; grading of dispersion and particulate matter; automatic scanning of tissue sections and exfoliated cells for malignancies; radiation damage evaluation on a per cell basis; pollen counts; testing of micron filters and oil filters; fermentation controls; spray and aerosol generator testing and autoradiograph grain counting.

Sample Preparation

Accuracy of the results depends on sample preparation techniques. Just as the development of the electron microscope required the evolution of special sample techniques peculiar to its requirements, so the flying-spot scanner will stimulate a search for superior methods of sample preparation.

The counting speed provided by flying spot scanning and the type of circuits shown in this article are ultimately capable of scanning and counting up to one million particles per second.

The development work leading to the design and construction of this instrument was made possible by the U.S. Army Chemical Corps at Fort Detrick, Maryland. The authors appreciate the valuable technical assistance contributed by Mr. Nelson E. Alexander of the Chemical Corps.

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Transistor Relays Have Low Idling Current

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CUMMARY — Electronic relays of remote-control devices operate electromechanical relays requiring 2 or 3 watts; consume few microamperes when idling. Circuits for c-w audio and pulsed-video control signals are shown

REMOTE radio control equipments require receivers which will run continously with the lowest possible standby battery drain and which will deliver, on demand, 2 or 3 watts of power to a rugged and reliable heavy-current relay to turn on gasoline-electric generators or other equipment.

This article describes two types of transistor relays which can be used at the output end of the receiver to convert the signal waveform into useful d-c power. The control signal may be a carrier modulated at 1,000 cps or it may consist of short pulses from a microwave transmitter.

Basic Circuit

The basic circuit shown in Fig. 1 follows a cascade complementary arrangement. Input transistor, Q_1 should be of silicon to ensure that its idling current (I_{co}) at zero bias will be about 1 or 2 μ a. A germanium transistor can be used with -1.5-v base bias, but the I_{co} will usually be higher than that of the silicon types with no bias.

Input transistor, Q_1 acts as a single-ended class-B amplifier for the signal voltage. The 2- μ f capacitor from collector to ground filters the half-sine wave output of Q_1 and provides a smooth d-c bias for Q_2 .

The effective input impedance is about 8,000 ohms and an input signal of 2 to 3 vrms will develop 8 v d-c across a 15-ohm output load in the emitter circuit of Q_2 . Power gain of the relay is 30 to 40 db, depending on the input level. Effi-

ciency of the output transistor varies with the signal level and ranges up to 70 percent.

A 6-v d-c 0.5-amp dpdt relay operates satisfactorily when substituted for R_L . Idling power is $\frac{1}{2}$ mw, compared to 4 w delivered power when the relay trips.

Pulse-Sensitive Circuit

When pulses of 1 or 2- μ sec duration are used for signaling, the circuit of Fig. 1 is not satisfactory and a pulse-stretching technique should be used. In Fig. 2, feed back transistor Q_3 and network R_1 , R_2 , C are added for this purpose.

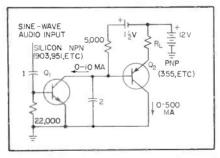


FIG. 1—Relay operates on c-w audio input

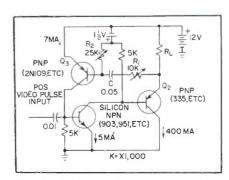


FIG. 2—Pulse-stretching technique adapts circuit for pulsed-video input

The rising edge of an input positive pulse turns on Q_1 , Q_2 and Q_3 , in that order, and the regeneration around the loop speeds up the action. The transistors remain turned on full until the charge on C is dissipated causing a sharp fall in the transistor currents.

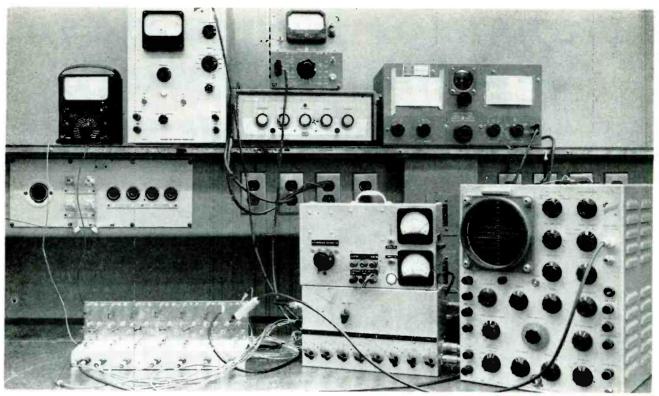
The width of the square wave produced across R_L may be controlled by varying either R_1 or R_2 . The duty cycle is adjusted to be as high as possible (up to 70 percent on time can be obtained) at the lowest pulse repetition frequency used; for higher repetition frequencies the relay will simply count down.

Switching Efficiency

Since the transistors are acting as switches in Fig. 2, efficiencies are higher than in the circuit of Fig. 1. For example, with 12 v on the collector of Q_2 and 50 percent duty cycle, a 10.5-v squarewave is developed across a 15-ohm load, with an average emitter current of 340 ma. Average d-c output power developed across R_L is then 3.6 w.

The efficiency of Q_2 is nearly 90 percent and is independent of signal level since the transistor is either full on or shut off.

A pulse amplitude of 1 v is sufficient to trigger the relay. A 6-v d-c relay may again be used in place of R_L . When zero-bias silicon transistors were used, total idling current was less than 5 μ a, but useful d-c power was limited to 0.5 w with the transistors available.



Complete test setup shows the digital-analog converter at the lower left with dynamic input simulator and power supply next to it

Digital-Analog Converter

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ELECTRONIC DIGITAL computers use digital systems throughout their arithmetic units, but the outputs required are often of an analog form. The digital-analog conversion is sometimes done in an electromechanical form as in shaft position servos.

Transistors were used in preference to vacuum tubes in the equipment to be described because of their reliability, low power consumption and small size. The converter is required to convert seven bits of binary information to 128 analog steps in amplitude of a 400-cps sinewave and convert an additional binary bit to requisite phase information.

These functions must be performed within a 4 millisecond sampling period, occurring at an average repetition rate of 20 cps. Input information is received in

parallel form from a shift register and must be stored in the digital-analog converter between sampling period. A binary ZERO is represented by a -30 volt signal at the respective input terminal, a ONE by zero volts. The converter output works into a high-impedance load and a full-scale output of 20 volts peak to peak must be supplied. The equipment must operate over a temperature range from -50 C to +85 C.

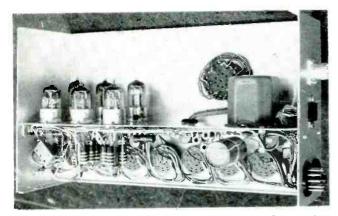
Gates

The circuit diagram of the complete digital-analog coverter is shown in Fig. 1. To keep the current drain on the gate pulse signal within the permissible limits, a gate pulse current amplifier, common to all eight bit-converters, was used. Its current gain is in excess of that required to keep the drain

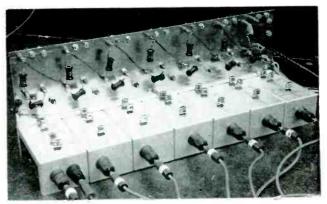
on the gate-pulse source within the permitted limits. Diodes $D_{\mathfrak{s}}$ and $D_{\mathfrak{s}}$ provide correct d-c levels for the a-c coupled gate pulse.

Seven bit-converters have identical circuitry. Transistor Q_7 plus associated circuitry constitute a sample gate circuit. It is connected as a common-emitter amplifier and is normally cut off by its -16 v bias battery. If a ZERO (-30 v) is read into the gate from register connection X_1 the gate transistor is kept cut off even if the positive gate pulse arrives.

The gate pulse is also connected to the collector side of the gate transistor through a 33,000-ohm resistor and will appear at the gate circuit output with an amplitude of about 8 volts if transistor Q_{τ} is not conducting. Thus a ZERO read into the register results in a positive output pulse from the gate



Dynamic input simulator contains 400-cps oscillator, 25-cps gating circuit and output cathode followers to drive bit converters



Rear view of converter unit showing modular construction Left module also contains the gate-drive amplifier

CUMMARY — When high-speed or environment rule out mechanical converters, purely electronic units must be employed. This transistorized converter changes eight binary bits, received in parallel from a shift register, to 128 steps in amplitude of a 400-cps sine wave. One binary bit is used to obtain phase information. Operation is performed within a 4-millisecond sampling period occurring at an average rate of 20 cps

Provides Storage

circuit. If a ONE (0 v) is read into the gate circuit from the register, Q_{τ} still remains cut off in the absence of the gate signal. In the presence of the gate signal the

Table I-Resistance Matrix Outputs

E_{1}	Digital E ₂	Input E ₃	$\begin{array}{c} \textbf{Analog Output} \\ \textbf{E}_{0} \end{array}$
0	0	0	0
1	0	0	1/8
()	1,	0	1/4
1	1	0	3/8
0	0	1	1/2
1	0	1	5/8
0	1	1	3/4
1	. 1	1	7/8

transistor is driven into saturation.

The collector circuit thus becomes a low-resistance path to ground. Since the collector voltage between gate pulses is about +8 volts, there will be an 8-volt negative pulse at the output of the gate circuit for the duration of the gate signal. To avoid accumulative charging of the 1- μ f coupling capacitor and thereby losing the correct 8-volt collector potential between pulses, it is necessary to have a time separation between subsequent pulses that is long compared to the pulse duration.

An alternative gate circuit, which can operate at higher word rates, is illustrated in the phase reversal unit. The gate circuit output for a ZERO input is a positive, differentiated pulse fed to the base of $Q_{\rm II}$ of the storage flip-flop, driving it into conduction. The base circuit of gate

transistor Q_{10} is the same as in the previous gate circuits and Q_{10} will therefore remain cut off with a ZERO at the register input.

The collector side of Q_{10} is connected in parallel with the second flip-flop transistor Q_{12} . If a ONE is read from the register, gate transistor Q_{10} is driven into conduction, bringing the collector voltage of Q_{12} down thus setting the flip-flop so Q_{11} is cut off and Q_{12} conducts. The differentiated pulse, which tends to set the flip-flop in the opposite direction, is swamped out because of its shorter duration.

Storage

To obtain reliable operation of the diode switches, several milliamperes must be drawn from the storage flip-flops. Because of the 20-volt peak to peak maximum analog output signal required, the tran-

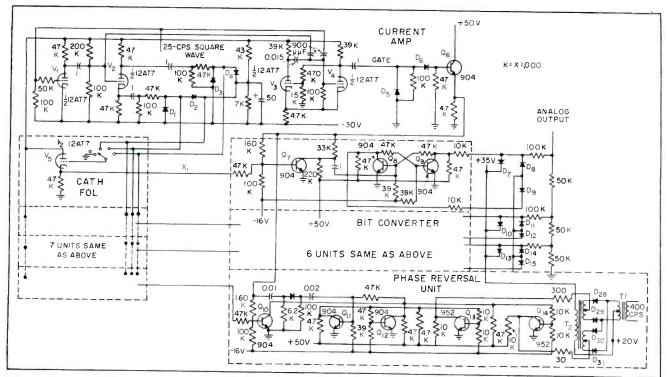


FIG. 1—Complete digital-analog converter. Electron-tube circuits check operation of transistorized converter and supply gate signal

sistors must be operated at collector voltages of up to 40 volts. The flip-flops will operate reliably using transistors with a current gain of 15. Test conditions for this gain were $V_c = 50$ volts, $I_c = 2$ ma and an ambient temperature of -55 C.

In the simple Eccles-Jordan circuit of Fig. 1, $(Q_8 Q_9)$ the collector voltage swing is approximately 4 to 45 volts. To maintain the lower of these limits a low collector saturation resistance is required.

As has been mentioned previously, a ZERO read from the register will result in a positive output pulse from the gate circuit. The positive pulse from the gate circuit drives Q_s into saturation, while $Q_{\mathfrak{p}}$ is cut off. Thus a ZERO from the register results in a voltage of +45 volts on the collector of $Q_{\mathfrak{p}}$ and a voltage of +4 volts on the collector of $Q_{\mathfrak{p}}$. A ONE read from the register reverses the voltages.

Solution of the mesh equations

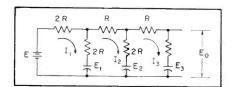


FIG. 2—Resistance matrix used to solve mesh equations to determine parameters of output circuit

for the resistance matrix of Fig. 2 provides the following equation for its output voltage:

If $E_{\circ} = 0$ and E_{1} , E_{2} and E_{3} are assigned the values of either 0 or 1, inserting all possible combinations of these values results in the outputs shown in Table I.

Thus, if a correct resistance ratio is maintained throughout the matrix, the output will be a true analog of the digital reference voltages. A zero for E_1 , E_2 or E_3 means a short circuit to ground, not an open circuit!

The resistance matrix described above is expanded to seven digital inputs and provided with the necessary diode switches as shown in Fig. 1. The switching diodes providing single pole-double throw action for the first binary bit are D_{τ} and $D_{\rm s}$. If the voltage on the collector of Q_0 is +45 volts, current will flow from this point through the 10,000-ohm resistor and D_{τ} to the +35-volt line, providing a lowimpedance path between the resistance matrix tie-in resistor (100,000 ohm) and the +35-voltline, which is heavily bypassed and thus on ground potential for the 400-cps reference voltage.

The voltage at the tie point of D_8

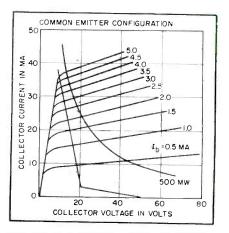


FIG. 3—Characteristic curves of transistors used as phase-reversal switches show broken load lines over which transistors are operated

and $D_{\rm e}$ is +20 volts with 20-volt peak to peak of the 400-cps voltage superimposed. Thus the highest instantaneous voltage at this point will be +30 volts and the lowest instantaneous voltage will be +10 volts. The d-c voltage at the tie point of $D_{\rm r}$ and $D_{\rm s}$ is slightly over 35 volts and $D_{\rm s}$ is therefore cutoff during the entire reference voltage swing.

If a ONE is read from the register, the voltage at the collector of Q_{\bullet} is about +4 volts. Thus current is flowing from the tie point of D_{\bullet} and D_{\bullet} , through D_{\bullet} and the 10,000-ohm

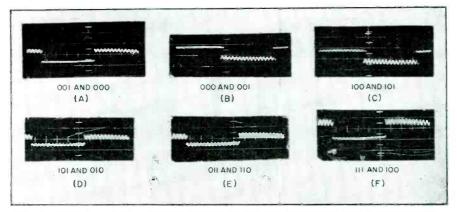


FIG. 4—Typical converter output waveshapes for the repetitious binary inputs shown

resistor to the collector of Q_b . Diode D_s will never cut off during the entire period of the reference voltage.

Since the impedance of the conducting diode D_s is small compared to the 10,000-ohm resistor, practically all of the reference voltage will appear at the tie-in point of the resistance matrix. The voltage at the tie point of D_{τ} and D_s never goes above +30 volts. Thus D_{τ} remains cut off during the entire reference-voltage swing.

The two load extremes on the reference source will be no-load (all converters ZERO) and a load of about 1,250 ohms (all converters ONE).

To keep reference-voltage fluctuations as a result of these varying loads to a minimum, a load compensation circuit is included in each bit converter. In the first bit converter it consists of diode $D_{\rm o}$ and the 10,000-ohm resistor connecting it to the collector of $Q_{\rm s}$. This collector is at a low potential whenever the collector of $Q_{\rm o}$ is at a high potential and vice versa. Thus either $D_{\rm s}$ or $D_{\rm o}$ will be conducting at all times, and the variation in load of the reference signal source will be greatly reduced.

Phase-Reversal Unit

In the phase-reversal operation either one of the diode pairs D_{2s} , D_{20} or D_{80} , D_{81} is biased in the conducting direction, while the other pair is cut off. The plate side of all four diodes is maintained at a d-c potential of +20 volts from the +20-volt battery through the center tap on the secondary winding of T_1 . The center tap on one of the primary windings of T_2 must be kept at a more positive potential to keep

the corresponding diodes cut off. The center tap on the other primary winding of T_2 is at a lower d-c potential, maintaining conduction through the corresponding diodes.

Since the primary windings on T_2 are connected to oppose each other, transferring the reference signal input from one of these windings to the other will shift the phase of the reference signal output voltage by 180 degrees. The d-c drawn through the forward-biased diodes must be equal to at least the peak a-c necessary to produce the required output voltage.

After quite a bit of experimentation, a diode bias current of 15 ma and a transformer T_2 with an open-circuit shunt inductance of four henrys were used. The transistors driving the phase-reversal switches Q_{18} and Q_{14} are operated along a broken load line as shown in Fig. 3. As long as the collector voltage exceeds +20 volts, the transistors operate with a 10,000-ohm load resistor connected between collector and the +50 volt supply. As the collector voltage becomes less than +20 volts, the diode pair starts to conduct and the 300ohm resistor connecting the collector to the center tap on T_2 becomes the decisive part of the load. This keeps the transistor from exceeding its dissipation rating during any part of the operating cycle.

The electron-tube circuits of Fig. 1 constitute the test equipment used to check the operation of the digital to analog converter. All necessary signals are obtained from a 25-cps square wave input to provide the digital-analog converter with a repetitious series of two 8-bit binary numbers. The two numbers

can be preselected by appropriate settings of the bit selector switches in the test equipment. The test equipment also provides the gate pulse.

The outputs available from the register connections for corresponding settings of the bit selector switches are: bit selector switch in zero poition, O volts; bit selector switch in ONE position, +30 volts; bit selector switch is ZERO -ONE position, O volts for positive half cycle of 25-cps input pulse and +30 volts for negative half cycle of input pulse; bit selector in ONE -ZERO position, +30 volts for positive half cycle of 25-cps input pulse and O volts for negative half cycle of input pulse. Voltages are with reference to the simulator chassis.

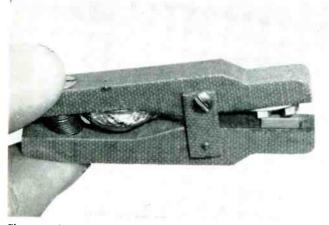
Input Signals

The input simulator must be kept at a -30 volt potential with reference to the digital-analog converter chassis. The 25-cps input pulses of negative polarity are amplified and limited in amplitude by V_1 . Tube V_2 is a phase splitter and the outputs available at plate and cathode are 180 degrees out of phase. Phase splitter outputs are limited to 0 volts and +35 volts by the diodes D_1 , D_2 and D_3 , D_4 respectively. These voltages are fed to the appropriate bit selector switch positions, in each block.

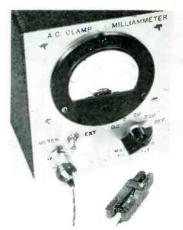
Tubes V_s and V_{\star} constitute a monostable multivibrator with a 4-millisecond pulse time. In its stable state, V_{\star} is conducting; V_s cut off. A positive trigger pulse at the grid of V_{\star} will turn this tube off and consequently turn on V_s maintaining this state until the 0.015 μ f coupling capacitor is charged. The pulse at the plate of V_{\star} is roughly rectangular and has a 4-millisecond duration.

There must be a gate pulse for every half cycle of the 25 cps input voltage to obtain a reading of subsequent words and thus, a positive trigger pulse must be derived from positive and negative slopes of the input pulse. This is done by obtaining a differentiated pulse before and after the first amplifier stage.

Figure 4 shows the output of the digital-analog converter when driven by the input simulator.







Complete microammeter with clamp

UMMARY — Small toroidal current transformer clamped around unknown current measures 0 to 200-microampere range over frequency band of 50 cps to 100 kc with negligible reaction upon measured circuits. Feedback to tertiary winding supplies frequency correction to transistor amplifier

Clamp-On Microammeter

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DIRECT-CURRENT METERS that measure minute currents without interrupting the circuit have been described in the literature. The clamp-type transistor microammeter to be described was developed to demonstrate the practicality of similar a-c instruments.

This meter uses a small current transformer which can be clamped about the unknown current. An amplifier increases the electrical out-

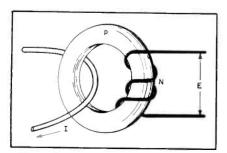


FIG. 1—Secondary winding and unknown current interlace closed magnetic core

put of the transformer to operate an indicating meter or a cro.

Theory of Operation

An unknown sinusoidal current of I amperes surrounded by a closed magnetic core with a secondary winding of N turns is shown in Fig. 1. The amplitude of the induced secondary voltage is

$$E = \omega N P I \tag{1}$$

where P is the core permeance in webers per ampere-turn.

If the secondary is connected to the input terminals of a zero inputimpedance current amplifier as shown in Fig. 2, the input current will be

$$I_s = (I/N)/[1 + (f_c/f)^2]^{1/2}$$
 (2)

where $f_{\circ}=R_{\circ}/(2\pi L)$, R_{\circ} is the effective a-c resistance of the secondary and L is its self-inductance. The output current of the amplifier

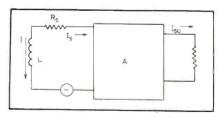


FIG. 2—Equivalent circuit of transformer probe and preamplifier

is substantially independent of f in the range where $f>>f_c$. When the transformer's physical dimensions are small, f_c may be several kc.

The method of effectively reducing f_{\circ} for this instrument is to supply negative feedback from the amplifier output to a tertiary winding on the core. When this is done, the output current of the amplifier becomes $I_{*\circ} = (I/N)/[1 + (f_{\circ}/N)]$

$$I_{se} = (I/N)/[1 + (f_c/Af)^2]^{1/2}$$
 (4) and f_c is reduced by amplifier current gain A .

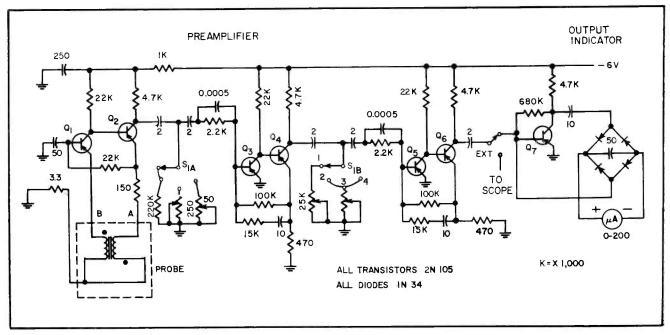


FIG. 3—Clamp-type transistor microammeter has four full-scale ranges from 200 $\mu\alpha$ to 200 ma

Measures A-C Current

Preamplifier Q_1 Q_2 in Fig. 3 supplies frequency correction for the pickup transformer whose signal winding terminates at B. The feedback winding terminates at A.

Output Indicator

The 200-microampere output indicator is driven by Q_{τ} through a full-wave bridge rectifier; 100-percent negative feedback is used around Q_{τ} to improve the rectifier linearity. The ratio of d-c output to a-c input of Q_{τ} is therefore slightly less than unity and an input of about 220 microamperes a-c deflects the meter full scale.

If the transformer secondary winding consists of 250 turns, the output current of preamplifier Q_1 Q_2 will be about 0.8 microamperes a-c for an unknown current of I = 200microamperes. Consequently, a current amplification of 220/0.8 = 280 is needed between the preamplifier output and the input to Q_7 . Feedback pairs Q_3 Q_4 and Q_5 Q_6 furnish gain of 20 per pair. Adjustable

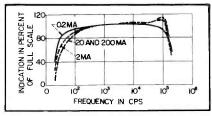


FIG. 4-Frequency response curves for four ranges of operation of transistor microammeter

shunt attenuators permit calibration of each current range.

The transformer probe consists of a silicon iron core of 0.014-in. laminations with 15-in, outside dimensions and a thickness of 1 in. The stack of C-shaped laminations fixed in the lower jaw of the clamp

is wound with two 250-turn windings of number 44 wire. The I-sloped stack in the upper jaw is mounted on a pivot so it will seat properly on the rising legs of the C.

The response of the completed microammeter is shown in Fig. 4. The most sensitive current range, 200 microamperes full scale, is useful in the frequency range from 50 cps to 100 kc. The internally generated noise is about 20 μ s.

This work was done at NBS as part of a research program sponsored jointly by the ONR, the AFOSR, and the AEC.

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CUMMARY — Anticipated performance is seldom achieved in passive filter circuits whose design is based solely on theoretical considerations. Distributed capacitance due to component proximity and encapsulating materials, temperature effects and impedance mismatch radically skew the results. Such pitfalls can be readily avoided, providing they are anticipated in advance and allowance made for them in the design

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Design and Manufacture

ore and more engineers are finding it necessary to design filters in their everyday circuit requirements. Design formulas for various L-C filters are available in adundant quantities in design and texts and handbooks. But as many engineers have found, the practical application of the theory is not only difficult, but to the uninitiated the construction of a suitable filter defies all attempts.

The techniques described in this article apply particularly to L-C filters using toroidal inductances although many of them can be applied to other filters of the L-C or R-C type. Whether the filter is of high-pass, low-pass, bandpass or band-rejection configuration, the design and test procedure should follow the same pattern. First the operating frequency is determined. Next, the input and output impedances are chosen to meet circuit requirements.

For correct operation, the theoretically calculated impedances and resonant frequencies must be ob-

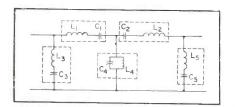


FIG. 1—Typical filter configuration. Circuits to be resonated separtely are enclosed in dashed-line boxes

tained in the practical configuration. To accomplish this, the resonant frequencies of all circuits within the filter must be accurately attained and each L-C combination resonated as either a series or parallel circuit, as determined by its use in the filter.

The L-C combinations to be separately tuned in a simple lowpass filter are shown in Fig. 1. To tune these circuits, a signal generator, vacuum-tube voltmeter and a frequency indicator unit are required. To prevent loading of parallel resonant circuits a 100 K resistor is placed in series with the signal generator output lead. Series resonant circuits would be heavily loaded by this resistor so it is not used while tuning them. At radio or very high audio frequencies a resistor will be needed in series with the input to the vtvm.

Filter Testing

The test circuit is shown in Fig. 2. The input voltage to the circuit should never exceed 1 v rms as toroids exhibit hysteresis and saturation effects. With voltages above 1 v rms the inductance change is great enough to cause circuit detuning. At 2 v rms most toroids will change inductance about -7 percent over the value measured at 1 v rms. Below 1 rms the inductance change is negligible for most practical filter applications. In the case of "wedding-ring" size toroids, however,

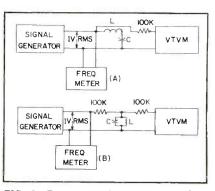


FIG. 2—Test setups for resonating filter sections. For series-resonant circuit (A) adjust L-C combination for null on vtvm. For parallel-tuned circuit (B) adjust for peak on meter

the signal level should be held to a maximum of 0.5 v rms.

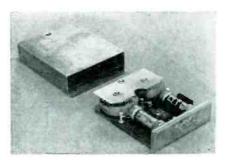
In some cases it may be found that it is not possible to resonate the L-C combination to the desired frequency. The cause is the relatively high distributed capacitance in the toroid. Each toroid will therefore have its own parallel resonant frequency.

There are two steps to be taken in avoiding this pitfall. First, always design for the lowest impedance filter that will satisfy the circuit requirements. In any type of L-C filter the inductance is directly proportional to the filter impedance. Thus lower inductances mean higher self-resonant frequencies.

Second, after designing the filter, check with the manufacturer to



Each filter section is tuned separately



Prototype ready for hermetic sealing



Production filter used in tone detector

of Practical Filter Circuits

verify that the toroid self-resonant frequency is higher than that of the circuit in which it is to be used.

Packaging

In the past it has been common practice to haywire the filter together on the bench, and after carefully laying it into a suitable container, it is encapsulated with wax, plastic or rubber compound. Invariably the encapsulated filter fails to show the same electrical characteristics which it exhibited during the bench test. The higher the operational frequency the greater the divergence between the two sets of characteristics.

The discrepancy occurs because of the dielectric effect of the encapsulating compound on the inductors and capacitors. The greatest effect occurs when the compound enters the center hole of the toroids. Wrapping the filter in fish paper before encapsulation reduces the dielectric effects somewhat but does not add to the mechanical rigidity and over-all filter reliability.

The entire filter should be assembled on a phenolic board. Capacitors are soldered between parallel bus wires. Toroids may be mounted either singly or in multiple units by means of machine screws through the holes. The toroids may be laid against each other with no measurable effect upon the electrical characteristics.

For vibration it is recommended that ½-in. thick cork washers be used to separate the torids. A round phenolic washer may be used under the head of the screw to hold the entire assembly in place. The completed filter assembly, securely mounted and wired on the board, may be installed in the container without resorting to en-

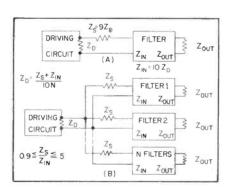


FIG. 3—Driving circuit design for single (A) and multiple (B) filter connections. The higher the raatio $Z_s/Z_{(n)}$, the better the isolation will be between filters

capsulation. Thus the response curve will remain unchanged.

At higher audio frequencies, say 10 kc and up, capacitors should not be near the container walls if they are metal. The proximity factor is even greater as the filter impedance increases since the capacitance is inversely proportional to the impedance. Since both higher frequency and higher impedance create

lower values of capacitance, the added capacitance caused by the container walls creates a greater detuning effect upon the filter.

Physical Size

The most effective method of reducing filter size is to resonate the toroid to a fixed value of capacitance. Varying the capacitance involves the use of a pack of capacitors for each value required in the filter. Capacitor packs use volume quickly, so a filter should be designed around standard capacitance values.

The higher the impedance of the filter, the lower will be the capacitance values and hence the smaller the volume. Toroid sizes remain the same over extremely wide ranges of inductance.

Choose the smallest physical toroid size with sufficient Q for the requirements. Once the configuration and adjacent-frequencies attenuation are established, reduce the toroid size until another filter section is needed to attain the required attenuation. Then use the next larger size toroid.

When mounting toroids, the idea may occur of running a screw through opposite sides of the filter container, and stringing the toroids on the screw. This produces a non-operative filter when the container is metal. The effect is that of a shorted turn which reduces the Q

of the toroid to a very low value and causes considerable detuning of the circuit.

Temperature Compensation

The average temperature coefficient of toroids is -180 ppm/deg C. Temperature compensating capacitors are available in low capacitances which make high frequency filter compensation feasible. For use at audio frequencies, however, it is not possible to find large values of positive or negative coefficient capacitors.

One arrangement has worked excellently. It consists of using a combination of C or D characteristic silver mica capacitors in conjunction with metallized paper capacitors. The ratio of silver mica to metallized paper capacitance should be 5/1. This combination works exceptionally well between 0 C and +90 C. Over this range, the maximum drift of filter center frequency is 0.1 percent. Between -20 C and +90 C the total frequency shift is 0.3 percent.

The C and D characteristic silver micas are usually between ± 70 ppm/deg. C. The metallized paper capacitors have a high positive temperature coefficient from +30 C up, essentially zero coefficient from 0 C to +30 C, and are highly negative from 0 C down.

Circuit Impedance

Of primary importance to proper filter operation are both input and output impedance matching. Many a filter has exhibited different response properties in the circuit from those noted in the test setup. Generally this stems from improper input impedance circuitry. Output matching is easily accomplished by shunting the proper value of resistance across the output of the filter which usually operates into the grid circuit of the following stage.

For years it has been common practice to drive filters from cathode followers with the cathode-follower output impedance designed to match that of the filter input. But at critical band-edge or cutoff frequencies the filter impedance usually changes radically, causing the input voltage to rise and fall accordingly. This distorts the actual

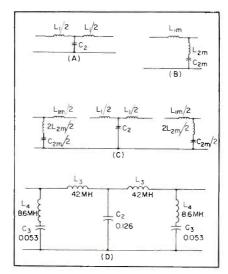


FIG. 4—Development of low-pass filter configuration, beginning with center section designed constant-k (A) plus end section which is m-derived (B). Mid-section and two half-sections are combined for configuration at (D)

filter response characteristic curve.

The simplest means for alleviating this condition is to use a driving-circuit impedance not greater than one-tenth that of the filter input impedance. Matching is accomplished by using a series resistor to make up the impedance differential, in this case nine times the driving circuit value. Reduced gain is made up by one amplifier stage. The correct procedure is shown in Fig. 3. It should be noted that the higher the Q of the filter components, the more closely the measured characteristics will match the theoretical ones. Low voltage levels will aid this two ways. Overloading or saturation of the toroid will not occur and leakage in capacitors is reduced to an inconsequential level thereby raising the capacitor equivalent resistance. For this reason, 200-working-volts d-c low-Q metallized paper capacitors may be used in filter circuits. even though this type of capacitor is noted for its comparatively high leakage.

Temperature and Aging Effects

Tests have proven that toroids will change characteristics when exposed to moist air. This was especially true of the wax impregnated types, although plastic encapsulated toroids show a very pronounced improvement. Where long

period drift (time measured in years) must be kept to 0.03 percent or less, however, the best precaution is to seal the container hermetically after installation of the filter.

Bandpass filters having a center frequency of 3,100 cps and built in this manner showed not 1 cps of bandpass shift or change in width after a period of two years. In most cases it is wise to cycle the filter from room temperature to 90 C before hermetically sealing the unit.

Design Examples

To best illustrate the preceding comments on filter design, two examples are given. For the first case, a low-pass filter with matching end-sections will be designed. The second example will be that of a simple bandpass filter.

For a low-pass filter, assume the following requirements:

Attenuation: 30 db down at 2.5 F_a ; 0.5 db down at F_a

Cutoff frequency: $F_e = 3,000$ cps Impedance: R = 600 ohms

Special Requirements: Z_{IN} and Z_{OVT} should be equal (600 ohms). End sections will be m-derived since L-C attenuation will be about 18 db/octave. At 2.5 F_c attenuation therefore would theoretically be 27 db. In practice it will be about 24 db.

Cutoff Frequency

Experience has shown that attenuation at the design cutoff frequency is usually 3 db. Thus to meet the requirement of 0.5 db down at F_o move the design F_o out to $(1.4 \times 3,000 \text{ cps})$. The 1.4 multiplier is an empirically determined factor.

The filter will be designed with a single constant-K center section

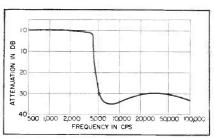


FIG. 5—Frequency response curve of low-pass filter circuit of Fig. 4D

as shown in Fig. 4A. Then

$$L_1 = R/\pi F_c$$

= 600/(3.14 × 4,200) = 0.046 h
 $L_1/2 = 23$ mh
 $C_2 = 1/\pi F_c R$
= 1/(3.14 × 4,200 × 600)
= 0.126 μ f

End Sections

The m-derived end sections are required when a specific frequency or frequencies require additional attenuation beyond that normally supplied by the constant-K section. Additional constant-K sections would supply increased attenuation beyond cutoff but would also cause excess attenuation at the cutoff frequency F_c .

In this filter, one-half an end section is placed on either side of the filter, making it symmetrical. Some volume and components could be saved by using only half an end section but the attenuation of the critical m-suppressed frequency ($F_{\infty}=2.5\ F_{\circ}=7,500\ {\rm cps}$) would be reduced by approximately 6 db. Then

$$m = \sqrt{1 - (F_c/F_{\infty})^2}$$

= $\sqrt{1 - (4,200/7,600)^2} = 0.83$

The full *m*-derived end section is shown in Fig. 4B wherein

$$L_{1m} = mL_1 = 0.83 \times 0.046 = 38 \text{ mh}$$

 $L_{2m} = (1 - m)^2/4m(L_1) = 4.3 \text{ mh}$
 $C_{2m} = mC_2 = 0.83 \times 0.126 = 0.105 \mu\text{f}$

In dividing the m-derived end section into two parts it is necessary to halve the values of L_{1m} and C_{2m} and double the value of L_{2m} . Combining Fig. 4A and 4B with the half end sections the filter as shown in Fig. 4C is obtained.

Practical Operation

The final filter configuration with the various components combined to give the most compact arrangement is shown in Fig. 4D. To obtain correct filter operation, $L_{\rm s}C_{\rm s}$ will resonate at

$$F_{c^1}=1/(\pi\,\sqrt{L_3C_2)}=2,\!200~{
m cps}$$
 and L_4C_3 will resonate at

$$F = 1/(\pi \sqrt{L_4 C_3}) = 7,500 \text{ cps.}$$

With the components resonated as indicated, the filter will exhibit an impedance of $600 \text{ ohms} \pm 20 \text{ percent from zero to } 3,000 \text{ cps.}$ The response will be 0.5 db down at 3,000 cps, 3 db down at 4,200 cps and 35 db down at 7,500 cps. The response curve is plotted in Fig. 5.

Care should be taken to see that the physical layout does not allow capacitive coupling between the input and output circuits. Proximity to the sides of the metal case is a common cause of input-output cou-

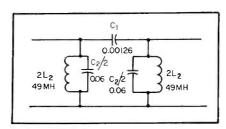


FIG. 6—A double-tuned bandpass filter in π form with capacitative coupling

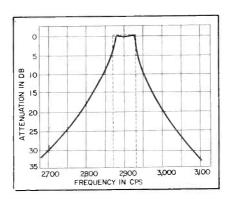


FIG. 7—Frequency response curve of bandpass filter circuit of Fig. 6. Broken line shows ideal pass band

pling, thus causing the low-pass effect to be nullified at higher frequencies. Many a low-pass filter designed for cutoff in the audio frequencies has looked like a direct wire connection at 50 or 100 kc.

If this particular low-pass filter were to be connected in parallel with other filters, it should be noted that at 7,500 cps the m-derived end sections are practically short circuits. Assume that another filter designed to pass frequencies between 7,000 and 9,000 cps were parallel across the input circuit of the low-pass filter. The output of the band-pass filter would be essentially zero for signals around 7,500 cps. For this reason, the two filters would require series input resistors and low impedance driving circuits for isolation.

For a band-pass filter, assume the following requirements:

Attenuation: 3 db down, 60 cps band pass; 28 db down, 200 cps either side of F_{\bullet}

Center frequency: $F_c = 2.9$ kc.

Bandwidth: 60 cps (2,870 to 2.930)

Impedance: 30,000 ohms

Special Requirements: Miniaturize if possible. Must be temperature compensated between $-20~\mathrm{C}$ and $+80~\mathrm{C}$.

Band-Pass Design

The filter configuration used as a first attempt will be a simple capacitance-coupled, double-tuned π circuit as shown in Fig. 6. Then

$$C_1 = \frac{(F_1 + F_2)}{(4\pi F_1 F_2 R)} = 0.00183 \ \mu {\rm f}$$

wherein

 F_1 is 2,870 cps, F_2 is 2,930 cps and

R is 30,000 ohms.

In addition,

$$C_2 = F_1/[\pi F_2(F_2 - F_1)R] = 0.173~\mu {
m f}$$
 $C_2/2 = 0.087~\mu {
m f}$
 $L_2 = R(F_2 - F_1)/(4\pi F_1 F_2) = 0.017~{
m h}$
 $2L_2 = 34~{
m mh}$

Since the filter must be temperature compensated the combination of silver mica and metalized paper capacitors may be tried. As practically all the drift with temperature would be in the tuned circuits and not in C_1 , only the $C_2/2$ values will be temperature-compensated. If a 0.01- μ f metalized paper and two 0.025- μ f silver micas (total 0.06 μ f) are used the capacitor packs are small, keeping the filter size to a minimum.

Assuming that a filter impedance higher than 30,000 ohms may be tolerated (in some cases this is very desirable), the C_2 formula may be solved for R by substituting 0.06 μ f for $C_2/2$ or 0.12 μ f for C_2 . Thus we have

 $R = 2,870/(3.14 \times 2,930 \times 60 \times 0.12 \times 10^{-6})$ = 43,400 ohms

Solving for C_1 and $2L_2$ using this new value of impedance:

$$C_1 = 0.00126 \ \mu \text{f}$$

 $2L_2 = 49 \ \text{mh}$

Results in Manufacture

A production model of this filter shows less than 0.2 percent drift between -20 C and +90 C. Between 0 C and +90 C the drift is 0.1 percent or less. The response curve of this filter is shown in Fig. 7. The 3 db bandwidth in production is 60 cps ± 1 cps, and the attenuation at ± 200 cps of center frequency is 30 db or better.

of monostable multivibrator. This prevents erratic operation when circuit is used in a television sync generator. Since both transistors are off during timing cycle, circuit is relatively insensitive to transistor variations and operates reliably from -50 to +70 C for input frequencies from 250 cps to one mc

By A. I. ARONSON and C. F. CHONG*

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Monovibrator Has

GENERATION of accurate television line and frame frequency rates, a function common to all sync generators, is generally done by starting with a stable high-frequency crystal oscillator and counting down in proper multiples to the desired frequencies. Frequency division is often accomplished with multivibrator circuits.

Monostable Multivibrator

In one such circuit a monostable multivibrator uses the complementary symmetry property of transistors and is shown in Fig. 1. Transistors Q_1 and Q_2 are biased on. With an applied negative trigger, Q_1 is turned off, causing the voltage at A to go to slightly less than V_1 . Since the voltage across C_1 cannot change instantaneously, it appears also at point B, the base of Q_2 , turn-

ing Q_2 off. Capacitor C_1 discharges towards V_2 through R_2 and R_5 .

When the voltage at B goes negative, Q_2 starts conducting and turns Q_1 on. Capacitor C_1 now discharges through a path comprising the saturation resistance of Q_1 and the input resistance of Q_2 . After C_1 is fully discharged, Q_1 and Q_2 are on and ready for another input trigger to start the circuit recycling. Frequency division is accomplished by controlling the length of time Q_1 and Q_2 are off so that a specified number of input triggers can be accepted without causing circuit action.

Advantages

Use of complementary transistors in place of similar conductivity transistors provides a higher charge-to-discharge ratio of the timing capacitor. In addition both transistors are off during the timing cycle thereby reducing the effects of transistor variations on timing accuracy.

Charge-Discharge Ratio

High charge-to-discharge ratio is desirable because unreliable operation can occur if an input trigger is coincident with the discharge of C_1 .

In a conventional monostable circuit^{1, 2} the timing capacitor discharges through a collector load resistor of one transistor and the input resistance of the other while in the present circuit the capacitor discharges through the saturation resistance of one transistor and an input resistance of the other. Since

*Now with Remington Rand Univac, Phila., Pa.

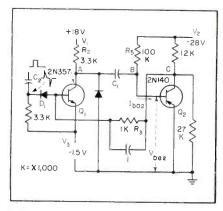


FIG. 1—Monostable multivibrator circuit uses complementary-symmetry facility of transistors to decrease recovery time

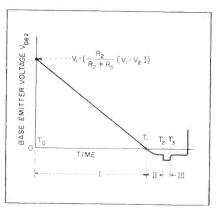


FIG. 2—Base-emitter recovery voltage of Q_2 sketched for three intervals of timing cycles. Intervals II and III are expanded

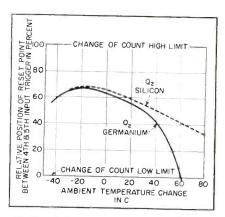
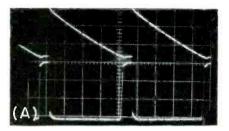
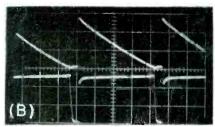


FIG. 3—Shift in reset point, T_e of Fig. 2. A shift to 0 or 100 percent indicates a miscount of 4 or 6 respectively





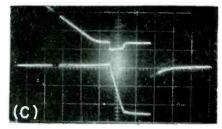


FIG. 4—Oscillograms of a l-kc input signal for frequency-divider circuis. Waveforms (A) show base-emitter voltage V_{bc2} (top) and collector voltage (bottom) of Q_2 with scale v=5v/divider and h=1 ms/divider, while (B) shows base-emitter voltage, V_{bc2} (top) and collector voltage (bottom) of Q_1 with scale v=5v/divider and h=1 ms/divider and (C) shows waveform (B) on expanded scale

Fast Recovery Time

the sum of the latter resistances is low, an increase of five or more in charge-to-discharge ratio can be obtained with this circuit.

Figure 2 is a diagram of the recovery voltage $V_{\rm be2}$ on the base of Q_2 for three intervals of the timing cycle. When $T>T_1$ and $V_{\rm be2}$ crosses zero, Q_2 begins to conduct. Charging of C_1 is controlled by the base-emitter diode of Q_2 . Interval III is the discharge time of C_1 . Interval II and III each represent about 2 percent of the total recovery time.

The duration from the starting trigger to the time V_{be2} equals zero corresponding to interval I in Fig. 2 is given by

$$T_1 = (R_2 + R_5) C_1$$

$$ln \left\{ \begin{array}{c} V_2 - I_{bo2} R_5 - V_1 + A \\ V_2 - I_{bo2} R_5 \end{array} \right\}.$$
Where
$$A = [R_2/(R_2 + R_5)] (V_1 - V_2)$$

Values of C_1 and C_2 are a function of the operating frequency and the

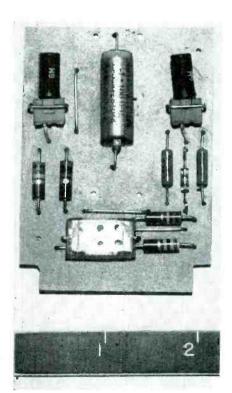
Circuit Reliability

desired time constants.

When both transistors are off, the timing is controlled at room temperature, primarily by passive elements. At elevated temperatures, however, the reverse saturation current I_{bo2} of the pnp unit approximately doubles for each 7 C of temperature rise.

The voltage drop across R_5 caused by current I_{bo2} is high enough at high temperatures to influence the charge time of C_1 . Reducing the effects of I_{bo2} by decreasing R_5 is undesirable because this also decreases the charge-to-discharge ratio of the circuit.

Use of a silicon transistor for Q_2 gives a 100-to-1 reduction in I_{bo2} and is the best means of reducing temperature effects on circuit recovery time. Improvement in circuit reliability using a silicon transistor for Q_2 is illustrated in Fig. 3. This curve shows the percentage



Monostable circuit constructed on a printed wiring plug-in board

shift in the reset point, T_z of Fig. 2, of the circuit used as a divide-by-five counter as a function of temperature. A shift to either zero or 100 percent indicates a miscount to four or six respectively. For moderate temperature ranges a germanium transistor for Q_z will be satisfactory.

Resistor R_s helps reduce the input trigger power required to turn Q_1 off by limiting the base current in Q_1 . The collector diode prevents Q_1 from going into saturation reducing further the trigger power required.

Application

A sync generator can be built using this circuit which occupies 54 cu in. and weighs one pound. It requires 0.7 w of power.

The frequency divider circuit operates reliably with input trigger from 250 cps to one mc. Various waveforms for a 1-kc input signal are shown in Fig. 4A and B. The voltage at the base of Q_2 is enlarged in Fig. 4C to indicate the change in the recovery-voltage waveform due to the input diode of Q_2 .

The circuit operates reliably with input triggers from 0.2 to 20 v.

Credit is due Dr. H. J. Woll for the circuit proposal and for his encouragement during the development.

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Charts Simplify Passive

By DONALD R. J. WHITE*

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CUMMARY — Universal design data permit design of Butterworth and Tchebycheff filters of prescribed steady-state insertion-loss characteristics. Design of band-pass prototypes of lumped-element configuration is given

Table I—Realizability of Band-Pass Filter Prototypes

	neunzability of band-rass rifler Prototypes
Band- Pass	$f_0 = 1 \text{ kc} \qquad \qquad f_0 = 10 \text{ kc}$
Filter Type	$Q_L = 5 Q_L = 20 Q_L = 100 Q_L = 5 Q_L = 20 Q_L = 100$
	50 500 10K
3 A 3B 3C 3D 3E 3F 3G	I P P I I I I I I I M R P I M P<
3 H	I M P I I P I I M M P P I P P I M P
Band- Pass	$f_0 = 100 \text{ kc}$ $f_0 = 1 \text{ mc}$
Filter Type	$Q_L = 5$ $Q_L = 20$ $Q_L = 100$ $Q_L = 5$ $Q_L = 20$ $Q_L = 100$
	50 500 10K
3A B3 3C 3D 3E 3F 3G 3H	P R R P P I M M I P R P P P I M P I P R R P P I M M I P R P P P I M M I P R P P R P P P I M M I P R P P P I M M I P R P P R P P R R P R R R R R R R R R R R R R R R R R R R
Band- Pass	$f_0 = 10 \text{ mc}$ $f_0 = 100 \text{ mc}$
Filter Type	$Q_L = 5 \mid Q_L = 20 \mid Q_L = 100 Q_L = 5 Q_L = 20 Q_L = 100$
	50 500 16K 50 500 10K
3A 3B 3C 3D 3E 3F 3G 3H	M P M I P I I I I I I I I I I I I I I I I I I I I
1 μh]≦	$\begin{array}{lll} \text{ealizable (R):} & \text{Marginally practical (M):} \\ \text{$L \leq 100 \text{ mh}$} & 0.05 \ \mu\text{h} \leq L \leq 30 \text{ h} \\ \text{$C \leq 0.1 \ \mu\text{f}$} & 0.3 \ \mu\mu\text{f} \leq C \leq 5 \ \mu\text{f} \end{array}$
Practical (
300 cps $3 \text{ ke } \leq 1$ $30 \text{ ke } \leq 300 \text{ ke } \leq 3 \text{ nic } \leq 1$	

for band-pass filters having either a Butterworth or Tchebycheff response with lumped-element, lossless L-C components is presented. By following the prescribed method, filters can be designed with minimum time and motion.

Filter Specifications

In designing band-pass filters the following information should be determined:

- (1) Center frequency f_o
- (2) Either the pass-band width B or the loaded Q-factor Q_L
- (3) Either the 60-db bandwidth B_{00} or skirt selectivity S_n in db per bandwidth
- (4) Allowable pass-band ripple variation ϵ in db
- (5) Input-output impedance level R in ohms
- (6) Maximum acceptable midband insertion loss in db
- (7) Quality factor Q_o of L-C components

Width of the pass band is measured between the 3-db cut-off frequency points. For Tchebycheff functions, these points correspond to the ripple variation. Items 3 and 4 establish the number of stages necessary for realizing the desired rejection just outside the pass band. The maximum-flat Butterworth response has no ripple in the pass band. However, the Tchebycheff or overcoupled response has an equal ripple variation in the pass band but offers additional skirt selectivity. Tchebycheff response use may result in fewer tuned stages.

^{*} Now with American Machine and Foundry Co.

L-C Filter Design

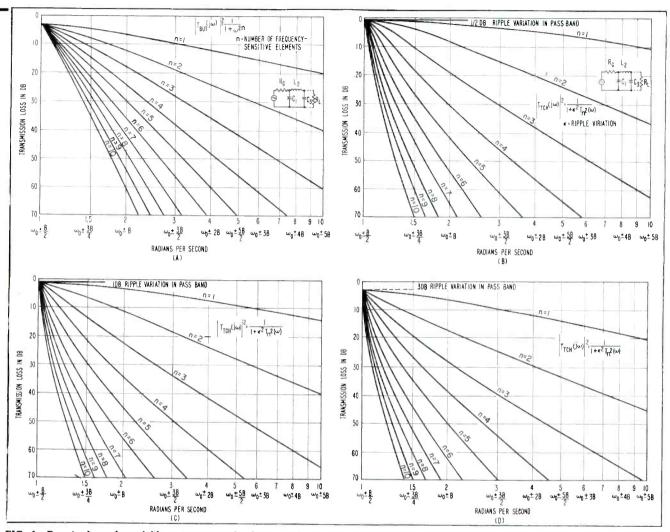


FIG. 1—Required number of filter stages can be found with the aid of transmission loss against frequency graphs for a Butterworth function (A) and for Tchebycheff functions with different ripple variations (B), (C) and (D)

Item 5 is restricted to approximately equal input and output impedances. Finally, item 7 establishes the compatability between the physically realizable specifications 1 through 6.

Design Procedure

When items 2, 3 and 4 are specified the required number of filter stages may readily be found by using Fig. 1A through 1D. Conversely, these graphs are useful in establishing different skirt selectivities in terms of an allowable or fixed number of stages. Although the graphs correspond to the low-pass prototype, they are equally useful for their band-pass, band-rejection or high-pass analogs.

When item 6 is selected, when Q_o of the coils and capacitors is known, and when the number of stages n is computed, the actual insertion loss may be found from the graph of Fig. 2. If the insertion loss found in Fig. 2 exceeds the maximum acceptable loss indicated by item 6, one or more specifications must be compromised.

Filter Selection

Figures 3A through 3H are prototype band-pass filters which provide essentially the same response. The most applicable is selected. Figure 3A, 3B, and 3C have identical responses and are derived directly without approximation from the same low-pass prototype.

Since the component values may be difficult to realize, Fig. 3D through 3H offer substitute forms. The prototype most easily realized or applicable should be selected.

Table I has been prepared using each of the eight prototype bandpass filters. Frequency, loaded Q factor and impedance level are the variables. With this table the recommended filter types for each application can be readily determined.

Components

The value of the capacitors, inductors and resistors are shown in Fig. 3A through 3H for low-pass Butterworth or Tchebycheff elements. These latter elements are

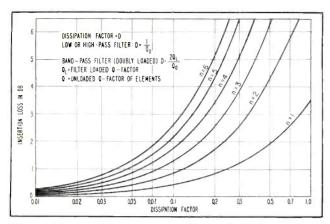
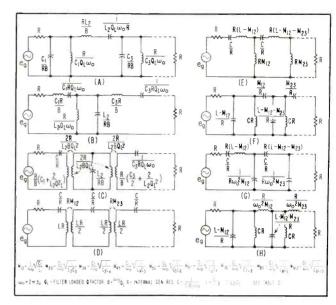


FIG. 2—Filter insertion loss may be found where dissipation factor and number of storage elements are known

FIG. 3—Since the eight illustrated prototypes have the same response, selection of the proper filter depends upon realizability and applicability of the configuration



listed in Table II for the Butterworth function and for the Tchebycheff functions with $\frac{1}{2}$, 1, 2 and 3 db ripple variation.

A maximally-flat, band-pass filter

with a center frequency of 100 kc, a 3-db bandwidth of 10 kc and therefore $Q_L=10$ is required. It should provide at least a 25-db rejection at 100 ± 15 kc where db/B

Table II-Element Values of Low-Pass Prototypes

n	Туре	db Ripple	$\bar{C_i}$	L_2	C_3	\mathbf{L}_{1}	\mathbf{C}_{\S}	\mathbf{L}_6	R_{θ} R_{L}
1	But Tch Tch Tch Tch	0 0.5 1 2 3	2 0.699 1.018 1.530 1.995						1 1 1 1 1 1 1 1 1 1
2	But Tch Tch Tch Tch	0 0 5 1 2 3	1.414 1.403 1.822 2.488 3.101	1.414 0.707 0.685 0.608 0.534					1 1 1 1.984 1 2.661 1 4.120 1 5.800
3	But Tch Tch Tch	0 0.5 1 2 3	1 1.596 2.024 2.711 3.349	2 1.097 0.994 0.833 0.712	1 1.596 2.024 2.711 3.349				1 1 1 1 1 1 1 1 1 1
4	But Tch Tch Tch Tch	0 0.5 1 2 3	0.765 1.670 2.099 2.793 3.439	1.850 1.193 1.064 0.881 0.748	1.850 2.366 2.831 3.606 4.347	0.765 0.842 0.789 0.682 0.592			1 1 1 1.984 1 2.661 1 4.120 1 5.800
5	But Tch Tch Tch Tch	0 0.5 1 2 3	0.618 1.706 2.135 2.831 3.482	1.620 1.230 1.091 0.899 0.762	2 2,541 3,001 3,783 4,538	1.620 1.230 1.091 0.899 0.762	0.618 1.706 2.135 2.831 3.482		1 1 1 1 1 1 1 1 1 1
6	But Tch Tch Tch Tch	0 0.5 1 2 3	0.517 1.725 2.155 2.852 3.505	1.410 1.218 1.104 0.907 0.769	1.930 2.606 3.063 3.847 4.606	1.930 1.314 1.152 0.939 0.793	1.410 2.476 2.937 3.715 4.464	0.517 0.870 0.810 0.696 0.603	1 1 1 1.984 1 2.661 1 4.120 1 5.800

C in farads, L in henrys, R in ohms, n=number of frequency-sensitive elements, $\omega=radians/second$ and $\varepsilon=ripple$ variation

measured as shown in Fig. 4A approximates 22 db/bandwidth. Maximum allowable insertion loss should be 3 db and the filter should work into and out of a 100-ohm impedance level. The coil quality factors Q_o may be expected to be about 100 and the Q_o of the capacitors about 800. The Q_o of the capacitors thus may be neglected.

Prototypes

Table I indicates that virtually all band-pass prototypes having these specifications are readily realizable.

The total number of stages required to realize the specified skirt selectivity is found in Fig. 1A to be about 2.7. Three stages will be used since only integers are possible. Figure 2 shows that the 3-stage filter would be 2.5 db based expected insertion loss for this

Using the band-pass prototype of Fig. 3A and Table II, the eleon Q_L/Q_o ratio of 0.10 or D=0.2. ment values are

$$C_1{}' = C_3{}^1 = C_1/(2\pi BR) = 0.16~\mu f, \\ L_1{}' = L_3{}^1 = L_2~R/2\pi~B = 16~\mu~h, \\ C_2{}' = 1/(2\pi~f_o~Q_L~RL_2) = 800~\mu\mu f ~\rm{and} \\ L_2{}' = R/(2\pi~f_o~Q_L~C_1) = 3.2~mh.$$

The resulting band-pass filter is shown in Fig. 5B.

Physical Realization

Since the dynamic range of the required capacitors and coils is $L_1C_2Q_L^2=200$, which makes physical realization inconvenient, the prototype network of Fig. 3D is

chosen. The resulting band-pass network is shown in Fig. 5A. Element values are now easily realized and are of the same order of magnitude. Frequency response of each network is shown in Fig. 5C.

As another example a 30 mc band-pass filter is required to give a maximum slope rejection per stage for which a 3 db pass-band ripple variation will be allowed. This suggests Tchebycheff response. Apart from this ripple, an additional 2-db midband insertion loss is permitted.

Selectivity

Skirt selectivity must be at least 60 db per bandwidth and the 3-db bandwidth must be 6 mc. Therefore $Q_{\scriptscriptstyle L}=30/6=5$. The $Q_{\scriptscriptstyle o}$ factors of the coils used are 200. The desired impedance level is 50 ohms.

The required number of stages obtained from Fig. 1D is 5. Figure 2 shows that the minimum insertion loss resulting from these nonlossless inductors is 1.3 db. The prototype of Fig. 3F is chosen from

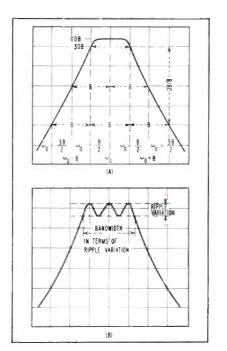


FIG. 4—Decibel/bandwidth concept of a Butterworth function is measured one bandwidth from the -3-db point of the response curve (A). Bandwidth of Tchebycheff response is measured along trough of ripple variation (B). Techniques described are usable for filter design from about 300 cps to about 500 mc using either Tchebycheff or Butterworth

Table I because of the practical realizability and the resulting filter together with its frequency response is shown in Fig. 6.

Thus, by using modern synthesis techniques a desired class of steadystate, band-pass filter responses can be obtained.

The author thanks J. H. Mills, Jr. for his work on the band-pass prototypes and table of recommended prototypes, C. L. Ranck for his work on the synthesis of the Butterworth and Tchebycheff lowpass prototypes and A. Feiner.

This work was performed under RADC contract No. AF 30(602)-

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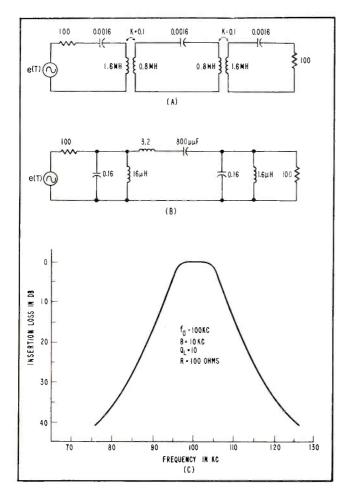
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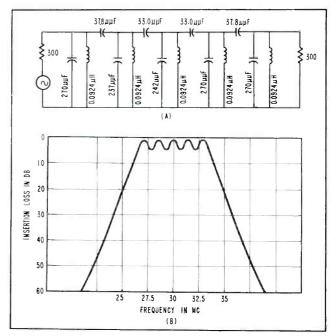
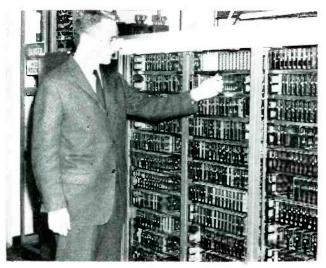
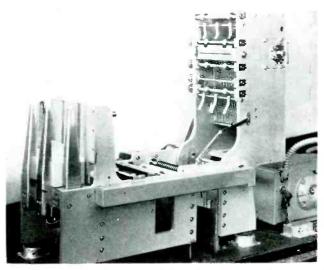


FIG. 6—Tchebycheff band-pass filter (A) was designed in second example with the aid of universal design data and has indicated frequency response (B)

FIG. 5-Although both prototypes have the same steady state frequency response (C), band-pass filter (A) is more easily realizable than filter (B)



Electronic circuits for transcribing card punch are packaged on plug-in assemblies and housed in racks shown



Cards in punch mechansim feed from left to right. Punches and solenoids are housed in hinged portion shown in open position

Puncher Transcribes

By JAMES E. PALMER, JAMES J. O'DONNELL and CHARLES H. PROPSTER Jr.*

> Commercial Electronic Product Division Radio Corporation of America Camden, New Jersey

UMMARY — Transistor circuits consisting of two-input resistor gates, flip-flops and other delay circuits are combined in plug-in assemblies to provide logical and driving operations for card puncher that produces business machine cards at the rate of 150 a minute. Each card is checked by reading completed card and comparing its output with original input

Large DIGITAL DATA processing systems are often required to produce accounting machine cards punched with information in a business machine code. These cards may be used as permanent records, to communicate with other data processing facilities or as output documents in the form of bills or checks.

The transistorized transcribing card punch to be described is used with the Bizmac computing system. It converts large volumes of data stored on magnetic tape into punched accounting machine cards at the rate of 150 cards per minute and provides many accuracy con-

trol features to assure correct data punching. Transistor circuits are used throughout.

Functional Description

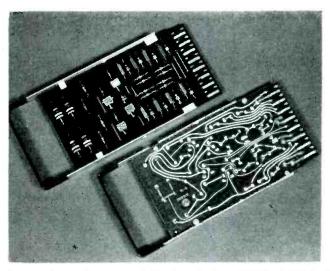
The input to the transcribing card punch is received from a magnetic tape reader in seven-bit binary-coded decimal alpha-numeric code. Character rates of 10 to 30 kc are acceptable but the unit requires that the magnetic tape messages be of fixed field format. All characters appearing on tape which do not have business-machine code equivalents are interpreted as blank columns on the cards, except for certain control

symbols such as start message, end message and item separator which are deleted completely.

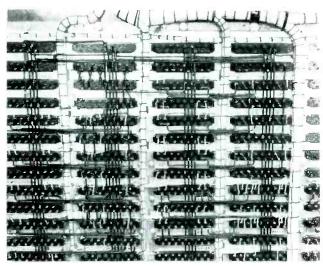
A plugboard permits rearrangement of data and insertion of special characters. Generally an entire message is punched into one card and the characters of the message may be rearranged in any sequence.

In all modes of operation the system checks itself by reading the cards after they have been punched and comparing them with the tape message from which they were punched. Parity check on input information provides further ac-

^{*} Formerly with RCA



Universal gate, inverter and flip-flop plug-in assembly holds four of the basic elements shown in Fig. 3



Wiring in prototype model of transcribing card punch shows s'mplicity and neatness resulting from use of cabled wiring

Computer Output

curacy control. Errors stop card punching. The erroneous card is separated from the correct ones and the tape is backed up, coming to rest just ahead of the message which was punched in error.

Logical Operation

A block diagram of the transcribing card punch is shown in Fig. 1. The temporary storage conthree sectors tains that switched cyclically around read-in, punching and checking circuits. Three messages are in process at any one time. Simultaneously one is read in, a second is punched and a third is checked. Operation will be described by following one message through a complete machine cycle.

During the read-in cycle the temporary storage is cleared and connected to the tape reader. A full card cycle of 40 millisec is allotted for this purpose although read-in needs only part of that time. At the end of this cycle, the temporary storage sector containing the message just read in is switched to the punching circuits.

During the punch cycle, information is read from temporary

storage into the coder to convert to business machine code. The output of the coder feeds a 12-channel electronic commutator synchronized with the card advance.

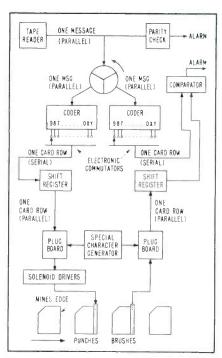


FIG. 1—Block diagram of transcribing card punch shows method whereby stored information is first used to produce punched cards and then used to check them

The cards enter the system nines edge first and travel in a direction parallel to their shorter axes. They are moved intermittently past a punching station and punched one row at a time.

The commutator selects the output channel from the coder corresponding to the row to be punched. This card-row is sent serially to the shift register which converts the information from serial to parallel form. Eighty bits are read out simultaneously through the plugboard to a register which drives the 80 punch magnets that punch one card row. The card is advanced to the next row and the process repeated. After 11 reptitions, one card is completely punched and is then transported to the checking station located exactly one card space away from the punching station.

During the check cycle the card is read, one row at a time, by 80 brushes and the information sent through the plugboard into a second shift register. This shift register converts parallel information to serial forms. Its output is sent into a single-channel comparator.

Meanwhile, the temporary stor-

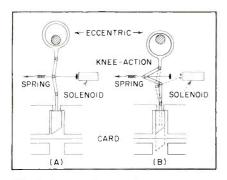


FIG. 2—Knee-action punch mechanism is shown at top of punch stroke (A). Solid lines in (B) show condition when no punching is done while dotted lines indicate condition for punching

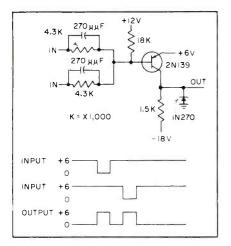


FIG. 3—Universal gate, inverter and flip-flop circuit. Response to various inputs is shown below

age sector containing the original information has been switched from the punching circuits to the checking circuits. The information in the temporary storage is translated by a second coder and another 12-channel commutator selects and routes the appropriate channel to the comparator where a check is made against the information read back from the brushes.

Punch Mechanism

Figure 2 illustrates the knee-action punch mechanism. Eighty such mechanisms are arranged side by side permitting an entire row to be punched.

At the beginning of each punch cycle, the solenoid armature is driven into the solenoid by the mechanical motion of the knee. In this position the solenoid, if energized, moves no mechanical mass. To punch it prevents the knee from bending during the downward stroke of the eccentric. This re-

quires relatively little force at a time when the solenoid is capable of exerting its maximum force; that is, when the armature air gap is smallest.

Transistorized Circuits

The basic circuit chosen to meet the logic requirements of the trancribing card punch is shown in simplified form in Fig. 3. This two-input resistor gate provides not cally the gating function, but also signal amplification and standardization. If either input is lowered to ground potential, the transistor conducts raising the output to +6volts. For negative going signals, defined as logical ONES, the element acts like an or gate followed by an inverter. If a single input is used, the element functions as a simple power amplifier-inverter.

When both inputs are at +6 volts, the output will be at ground potential. Thus, the AND function preceded by inversion is obtained.

Typical delays of $0.2~\mu sec$ per stage are obtained when these elements are cascaded. The output resistor of each element can absorb 10 ma from the stages it drives and 1.6 ma are required by each gate input. Hence, up to six gate inputs may be driven by each element.

The 18,000-ohm resistor supplies leakage currents when the transistor is not conducting. The necessary flip-flop or storage function is provided by cross-connecting two of the basic elements.

An accurate time delay or pulseforming one-shot multivibrator is shown simplified in Fig. 4A. Application of a negative-going pulse to the input terminal triggers Q_i into conduction causing its collector to swing from ground level to +6volts. This 6-volt swing is coupled through capacitor C which is initially charged to +6 volts. This raises the base potential of Q_2 to about +12 volts and cuts off the transistor. The base potential then begins an exponential decay toward ground. When the base of Q_2 reaches the vicinity of +6 volts, Q2 begins to conduct. The voltage swing required for the transition from cutoff to saturation is a few tenths of a volt and this transition is assisted by the gain of Q_2 and the feedback through Q_1 . Thus, the time required to turn on Q_a is a small fraction of the total one-shot duration. Therefore, wide variation in transistor characteristics can be tolerated without compromising circuit performance. Only in the case of short duration one-shots, where transistor storage effects become important, does variation of transistor parameters become appreciable. The standard pulse width of this system is 3 µsec. Similarly, transistor saturation voltages and diode-voltage drops have little effect as they are small compared to the 6 volts through which the timedetermining capacitor must discharge.

Figure 4B shows that supply voltage variations have little effect on circuit operation. If the ± 6 volt

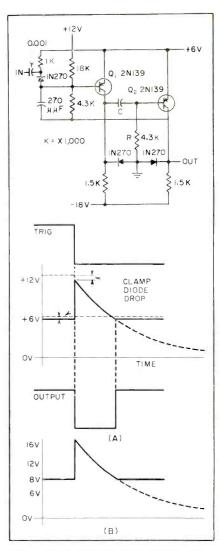


FIG. 4—Time delay or pulse-forming oneshot multivibrator (A). Waveforms show base voltage of $Q_{\rm c}$ as a function of time with correct supply voltage. Effect of increasing supply voltage is shown in (B)

supply should rise to +8V then C would be initially charged to +8V also. When Q_1 turns on in response to a trigger, its collector swings through 8 volts and the base of Q_2 moves to +16V. The decay takes place as before but starts from a much higher voltage. However, the base of Q_2 must only drop to +8 volts before Q_2 begins to conduct. This is half way between its starting point and ground just as in the case of a +6 volt supply. Hence, the duration of the output pulse remains the same.

Shift Register

The two-cell shift-register in Fig. 5 has provision for parallel input, gated-parallel output, serial input, serial output and reset; thereby making a single circuit universally applicable to all shift register requirements.

Each flip-flop cell is set by the application of a ONE (ground level) to its parallel input terminal, and reset at once by the application of a ONE to the reset terminal. Shifting is accomplished by the application of a ZERO (+6 volts) to the advance terminal. This advance signal must endure for at least 5 μ sec and must be separated from the previous advance signal by at least 25 μ sec.

The gated-parallel output is derived from a diode gate consisting of D_5 and D_6 or D_7 and D_8 which allows a one to be presented at the output terminals of all cells which are set whenever a ONE is applied to the gate terminal. Conversely, ZEROS will be presented at the output terminals of all cells which are reset at the time of the gate signal.

Shift-register operation may be explained by assuming Q_1 and Q_3 are conducting and both transistor pairs contain ZEROS. The first cell, consisting of Q_1 , Q_2 and associated circuitry, is set by the application of a ONE to the first parallel input terminal labeled P_{1-A} . This causes Q_2 to conduct turning Q_1 off. The first cell now contains a ONE and the collector of Q_1 is at ground level while the collector of Q_2 is at +6 volts.

The advance terminal is held at ground level externally and 6 volts appears across the series combination of R_3 and C_3 charging C_5 to

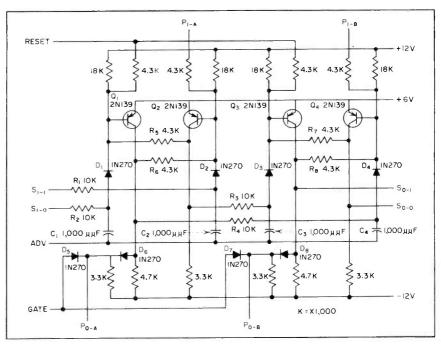


FIG. 5—Universal shift register is made up of a number of cells in cascade. Circuits are packaged four cells per plug-in unit

+6 volts. No voltage is applied cell. If S_{t-0} is at ground level and across R_t and C_t as the collector of S_{t-1} at +6 volts prior to the application of the advance signal, then

After C_3 has been charged the shift register is ready to receive an advance signal. When the advance terminal is raised to +6 volts, the anode of diode D_3 is raised to about +12 volts by the voltage doubling effect of the charge on C_3 . This biases D_3 in the forward direction and allows the charge stored in C_3 to flow into the base of Q_3 turning it off. Flip-flop action turns on Q_4 and the second cell of the shift register now contains a ONE.

The levels impressed on the serial input terminals S_{1-1} and S_{1-0} determine the charge on C_1 and C_2 and therefore determine the effect of the advance signal on the first

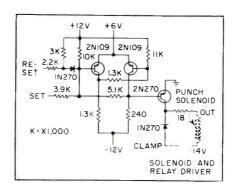


FIG. 6—Punch-solenoid driver uses medium-power transistors to supply required driving currents

 S_{1-1} at +6 volts prior to the application of the advance signal, then the first cell is switched to the reset or ZERO state through D_2 . If S_{1-1} is at ground level and $S_{\text{\tiny I-O}}$ at +6volts, the first cell does not change state in response to the advance signal since it already contains a ONE. The shift-register output is fed through the plugboard to a punch-solenoid driver. Four-hundred ma at 14 volts are required by the punch solenoids at a 20 percent duty cycle. As shown in Fig. 6 this power can be supplied by medium power transistors.

A flip-flop is included as part of the package to provide storage and to serve as a preamplifier for the output transistor. The flip-flop is set by a ONE and reset by a ZERO. In addition to reducing the required driving current for reset this feature allows the circuit to be used as a simple current amplifier, without storage action, by connecting the set and reset terminals together and driving them both with a one. Although the output transistor is required to supply large currents, it is still operated safely as the transistor is saturated to minimize internal dissipation.

Credit is due K. L. Chien, C. T. Cole, H. H. Cremer, N. C. Florio and R. F. Boy for their aid.

CUMMARY — Use of solid-state rectifiers and high-current regulator tubes eliminates power transformer and reduces size and cost of power supplies. Units have regulation better than 1 percent, ripple of 0.01 percent and stacking factor of about 150-ma capacity per inch of rack space

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Compact Supplies Have

R ACK AFTER RACK of electronic equipment, filled more than half way with power supplies is a common sight in laboratories. This condition prompted the development of regulated units that are smaller, lighter and more economical through the use of solid-state rectifiers and high current regulator tubes.

Transformer Elimination

Elimination of the power transformer, the largest single component, requires that the d-c ground be connected to one side of the line and that voltage multipliers be used to achieve the desired output. Since laboratory a-c supplies generally have one wire grounded and a third wire connected to the conduit for safety, the power system ground may usually be used for the d-c ground. Where this is not possible or a negative output voltage is needed, the unit is merely plugged into an isolation transformer.

Chief objections to the voltage multiplier are excessive regulation and ripple. In a regulated supply this increases the required gain of the regulator.

However, the regulation is better for a low impedance a-c line than for a transformer power source. Small voltage drops across silicon or germanium rectifiers further decrease the regulation required. Finally, regulation is dependent on the capacitance as illustrated in

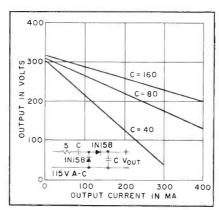


FIG. 1—Graph of dependence of voltage-doubler regulation upon capacitance

Fig. 1, and can be minimized by using the largest capacitors consistent with the peak-current rating of the rectifiers.

Elimination of the choke removes

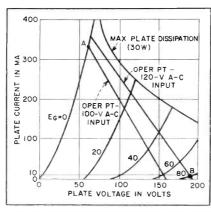


FIG. 2—Operating point loci for 100 and 120-v a-c inputs are superimposed upon plate characteristics of the Chatham 6336

the second largest expensive component and increases the regulator burden.

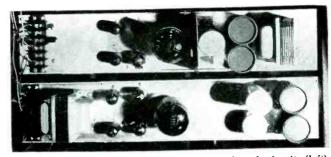
The Regulator Tube

Since power supplies are generally used for fixed output voltages, high perveance triodes are preferred. At the lowest line voltage, the tube must be able to supply the required output current without positive bias. At the highest line voltage, the tube must be capable of dissipating the power due to passing full load current and the negative bias required to reduce the output current to zero should be no more than about one-half the output voltage. This permits the use of a two-stage d-c feedback amplifier without a separate power supply.

The Chatham 6336, which has a μ of 2.7, makes the design feasible. Its high power dissipation allows the use of a single triode section in a 250-ma, 150-v power supply, thus eliminating tube paralleling difficulties.

Figure 2 shows the plate characteristics of the 6336 with the operating point loci for 100 and 120-v a-c input for a 150-v d-c supply. Point A indicates the maximum output current at the lower line voltage and point B is the required bias for zero output current. The amplifier current is 10 ma. For 250-ma output, the operating points shown skirt zero bias and maximum plate dissipation by a sufficient mar-





Since compact units use only one of two sections of a regulator tube, two supplies can conveniently be constructed as dual units (left). Each unit fitted on a $3\frac{1}{2}$ -in. panel and mounted in a rack, can be either of the same type or 150 and 250-v supplies. Unit at upper right has a heat reflector between the capacitors and the 6336 to reduce heating effects caused by component proximity

Wide-Range Regulation

gin to accommodate tube and line voltage variations. These variations make operation at 300-ma output unreliable.

Circuit

Figure 3 is the circuit for a 150-v, 250-ma unit. The 250-v, 150-ma units which use a voltage tripler are similar. Both types have been in 40-hour per week service for over a year with good reliability. Their regulation is 1 v and the ripple is 15 mv peak-to-peak.

Since each supply uses only one of the two sections of the regulator tube, it is most economical to construct two such supplies together. They can both be the same type or one can be 150 v and the other 250 v. No difficulty is experienced in fitting all components on a single 3 1/2-in. panel. The B— is connected to the grounded side of the line through an 8-amp fuse and to the safety ground through a 2.5-ohm resistor. The fuse will blow and a neon bulb will light if the plug is put into an incorrectly wired receptacle. The resistor ensures that current is drawn from the line and not the safety ground.

A 5-ohm resistor limits the surge current in the rectifiers to 25 amp when the unit is first turned on. Its high power rating is due to the

high rms a-c current drawn. A conventional two-stage triode ampilifier is used.

Voltage adjustment made with a potentiometer across the 5651 reference tube is a superior alternative to varying the cathode resistor of the first triode as much less power is dissipated in the control.

Reducing Heat Effects

Separation of the heat-sensitive parts, such as electrolytic capacitors as far from the regulators as possible is advisable. Heat reflectors made of shiny metal have proved effective. Free air circulation should be provided.

Performance

For best operation or the highest output, the a-c input may be adjusted to the prevailing line voltage by connecting the secondary of the filament transformer in series (buck or boost) with the high side of the line.

The same general design has been used in a 2.5-amp supply, variable from 50 to 119 v in one-volt steps by a tap-switch control and a precision voltage divider. This supply uses eight 6394 tubes in parallel with series-strung filaments, thus eliminating the filament transformer. It is used to apply precise voltages to a 300-w lamp.

The author thanks J. M. Heyning, G. T. Inouye and C. F. Knapp for their help.

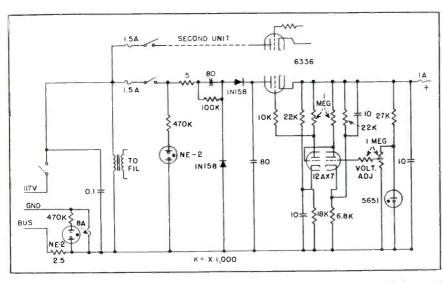


FIG. 3—Regulated 150-v. 250-ma power supply design eliminates expensive chokes and power transformers. The 5-ohm resistor limits surge current in rectifiers

Graphic Construction

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Crystal frequencies are plotted against channel frequencies to produce a direct-reading chart that reveals whether a proposed intermediate frequency in a given narrow-band f-m receiver will present spurious responses due to harmonics generated by the local oscillator. Suitable intermediate frequencies are immediately spotted for single, double and triple conversion superheterodyne receivers

HERE is a quick graphical method of determining whether a proposed i-f will be suitable for use in a given receiver.

The operating frequency of the lowest i-f to be used in the receiver is chosen so that the required selectivity can be obtained. The lower this is, the greater the ease with which a strict selectivity curve or shape factor can be realized. However, too low a frequency necessitates relatively larger components in the tuned circuits and creates a selectivity burden in the preceding stages.

If the preceding stage is an r-f amplifier, it will generally be difficult to attenuate the image which will appear at a frequency two times the i-f away from the carrier. The image is always on the same side of the carrier as the injection. Thus too low an i-f yields poor image rejection while permitting excellent selectivity.

Using a high i-f improves the image rejection but makes it more difficult to achieve special selectivities or shape factors, such as those required for f-m communications where selectivity curves like that shown in Fig. 1 are desirable.

Double Conversion

If the stage preceding the low i-f is another i-f of higher frequency, the receiver is then a double-conversion superheterodyne. This higher i-f further increases the percentage spacing between the direct image and the carrier. The direct image is twice the high i-f away from the carrier, thus simplifying the front-end r-f selectivity circuitry.

A first i-f (the highest used in the receiver) which is too low makes it difficult to acquire good direct image rejection. The high i-f is also required to attenuate the indirect image which is twice the low i-f away from the high i-f. Thus, the lower the frequency of the high i-f the more easily the indirect image is rejected.

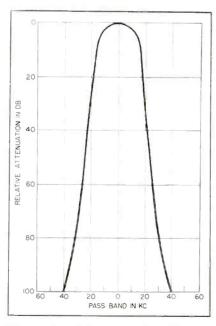


FIG. 1—Selectivity curve desirable for f-m communication

Conversely a high i-f which is too high permits the r-f tuned circuitry to eliminate readily the direct image, but the resultant selectivity in the high i-f is inadequate to suppress the indirect image unless a great number of tuned circuits is used in the high i-f. See Fig. 2.

Receivers having severe selectivity requirement are usually of the double-conversion type and used chiefly for bands up to 174 mc. To have sufficient image rejection when higher frequency bands are used, the 2nd i-f ends up at a

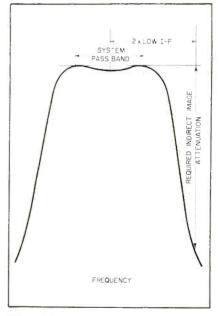


FIG. 2—Selectivity curve of high i-f is inadaquate to suppress indirect image

Finds Clear I-F

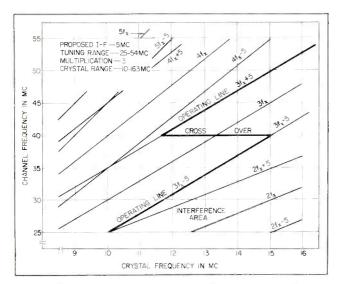


FIG. 3—Crystal frequencies are plotted against operating frequencies. The lines represent operating frequencies that are integers of 2, 3, 4 and 5 times the crystal frequency. For this example, a high i-f of 5 mc is proposed and the Nt_x plus-and-minus 5 lines are drawn parallel to the Nt_x lines. Here spurious responses are spotted at about 25 mc

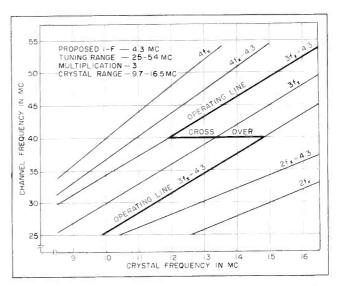


FIG. 4—In this graph, a proposed i-f of 4.3 mc is plotted, identical to the procedure used in Fig. 3. None of the $N f_x$ lines intersect within this range and a choice of 4.3 mc results in a receiver that is free of spurious responses. The ideal situation is to choose a high i-f that will result in a graph on which there are no intersecting lines in the operating range

rather high value. This makes adequate adjacent channel selectivity difficult.

The easiest solution is to add a 3rd i-f (of a lower frequency) to gain the necessary selectivity.

A chart of commonly-used intermediate frequencies is shown in Table I. A starting i-f is chosen from this table. The choice of an i-f then dictates the fixed frequency or frequencies of the conversion oscillators. If the first conversion oscillator is of the fundamental type which enables channel frequency trimming, then frequency multipliers are sometimes incorporated to produce the required injection frequency. The use of overtone crystals will sometimes eliminate the need for the multipliers, but overtone crystals do not lend themselves readily to triming techniques.

The presence of these oscillator frequencies and their harmonics can mix with frequencies other than the desired signal and produce a signal at the first i-f. Such a condition results in spurious response which the graphical method spots. Rationalized or normalized ordinates are avoided for the sake

of simplicity and a direct-reading scale results.

Construction

The graphical layout is drawn on linear-by-linear paper.

- 1. Choose the i-f frequencies from Table I.
- 2. On the vertical axis, lay off the frequency range to be tuned.
- 3. On the horizontal axis lay off the actual crystal frequency range of the first local oscillator.
- 4. By observation determine integers that, when multiplied by the values of actual crystal frequencies on the horizontal axis, yield numbers which fall within the limits of the vertical axis. For each integer draw a line which represents N times the frequency of the crystal.
- 5. Add two parallel lines to each of the Nf_x lines, displaced above and below the Nf_x line by a vertical axis frequency equal to the first i-f.
- 6. One of the lines drawn in step 5 will be the operating line. If the injection frequency is always on one side of the carrier, the operating line will be continuous. If the injection frequency is both above and below the signal frequency to minimize crystal spread,

a crossover line is drawn parallel to the horizontal axis at the crossover frequency on the vertical axis. This crossover line connects the two operating lines, one above the integer line, the other below it. Darken the operating lines for clarification.

Suppose a crystal-controlled receiver is required that will tune from 25 to 54 mc. All spurious responses and images must be 100 db down from a sensitivity of 0.3 μ v. The bandpass is to be \pm 15 kc wide at the 6-db points and \pm 40 kc wide at the 100-db points. Fundamental crystals are used with a multiplication of 3. Injection will be on the low side above 40 mc and on the high side below.

The graph in Fig. 3 for this example is drawn following the steps given in the preceding section.

1. Selectivity dictates the use of a low i-f between 260 and 1,600 kc. A good compromise is 455 kc. The high i-f must permit 100-db attenuation at twice its value away from the carrier. A 5.0-mc value is a good first choice, allowing the front-end circuitry to attenuate signals 10 mc off channel by 100 db. (Continued on page 172)

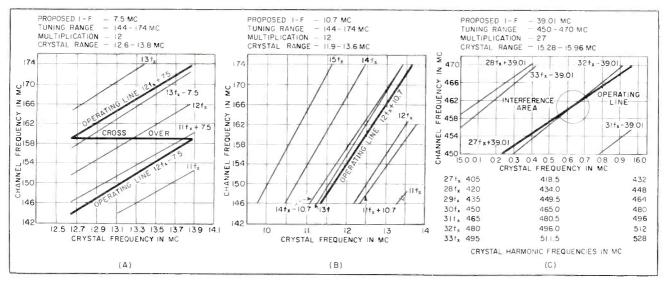


FIG. 5—Graphic plots showing various frequency ranges and i-f c'.oices. Note that plots (B) and (C) do not make use of the crossover techniques

- 2. Operating frequencies of 25 to 54 mc are laid off along the vertical axis.
- 3. Crystal frequencies of 10 to 16.3 mc are laid off along the horizontal axis.
- 4. Integers of 2, 3 and 4, when multiplied by values laid off on the X axis, fall in between values laid off on the Y axis. Draw lines $2f_x$, $3f_x$, and $4f_x$.
- 5. Another line 5 mc above the $2f_x$ line is drawn parallel to it. A line 5 mc below can be neglected since it will fall out of range. Similarly lines 5 mc above and below are drawn parallel to the $3f_x$ line. Draw lines $4f_x + 5$ and $4f_x 5$.
- 6. On the 40 mc horizontal line, darken the portion connecting the $3f_x + 5$ and the $3f_x 5$ lines. This is the crossover. Darken the upper portion of the $3f_x + 5$ and lower portion of $3f_x 5$ lines. These are the operating lines.

The graph now indicates an intersection of the $2f_x + 5$ line and the operating line occurring at approximately 25 mc. For example suppose the desired channel fre-

quency was 26.11 mc. The crystal frequency yielding 26.11 mc would be $\frac{1}{3}(26.11+5)$ or 10.37 mc. The second harmonic of 10.37 mc is 20.74 mc. Two signals can mix with the 20.74-mc frequency and produce a 5.0 mc i-f. They are 25.74 mc and 15.74 mc.

Front-End Attenuation

A 15.74-mc signal is easily attenuated in the front-end tuned circuits, but a 25.74-me signal is only 370 kc away from the desired 26.11 mc signal. The front-end circuitry cannot be expected to attenuate such close signals, and this choice of i-f therefore results in a spurious response for each channel operating in this interference range. If the selectivity of the front end plus the selectivity of the oscillator multiplier circuits is around 2 mc for 100 db, spurious responses will be obtained when operating on channels between 25 me and 28.5 mc.

The ideal situation is to end up with a graph on which there are no lines intersecting the operating range. From Fig. 4 it is apparent

that if the $3f_x - 5$ line is moved closer to the $3f_x$ line by 0.5 mc at 25 mc, the $2f_x + 5$ line would automatically move 0.5 mc closer to the $2f_x$ line, thus separating the $3f_x - 5$ line from the $2f_x + 5$ line by about 1 mc at the point where they formerly intersected.

This means changing the high i-f from 5.0 to 4.5 mc. In doing so the crystal frequencies will also change slightly, making exact values difficult to judge.

Upon obtaining a clear i-f it is wise to log all the harmonics of the second (and third, if used) conversion oscillator frequencies that occur within the operating range of the receiver.

Clear Frequencies

A second choice of 4.3 mc is next investigated. The identical procedure is followed in Fig. 4. Here the 4.3-mc graph is free of spurious responses due to harmonics, a good choice for the receiver. In Fig. 5A, 5B and 5C examples of various frequency ranges and i-f choices are given. Their eighth to twentieth harmonics may fall within the pass band of the receiver on certain channels.

Frequency Check

The remedy is to replace the second or third oscillator with a crystal that injects on the other side of the i-f. The harmonics of these alternate crystals should be computed to be sure that any alternate crystal harmonics do not fall on the same channel.

Table I—Commonly Used Frequencies in Kc

Conversion	1st I-f in Ke	2nd I-f in Me	3rd I-f in Me
Single	50, 262, 290, 455, 1,500, 1,600, 2,200		
Double	262, 290, 455, 456, 1,500, 2,200		2.2, 3.2, 4.3, 4.5, 6, 10.7, 21.5
Triple	290, 455	4,3, 5, 6, 10.7	15, 39.01, 41.25

Servo Analysis Charts

By ERWIN BISER and SAMUEL ADLER

Mathemetician

Engineer-in-Charg

Servo System Engineering Activity Signal Corps Engineering Laboratories Fort Monmouth, New Jersey

or closed-loop response curves of servo systems. When both amplitude and phase angle are known for either open or closed-loop operation, corresponding parameters for the opposite condition are given

DESIGNING SERVO SYSTEMS usually involves compounding the elements and computing the open-loop performance. Ascertaining system performance in its applied form requires conversion of the open-loop performance to the closed-loop patterns or the inverse. The servo conversion charts enable a designer to convert amplitude and phase information for a specific frequency from one form to the other with little effort and practically no calculation.

Transfer Function

This conversion can also be of value in determining the proper compensation devices for particular servo systems. The transformation formulas from which the conversion charts were made are limited to systems with unity feedback.

It is frequently impossible to obtain the open-loop performance directly from a test on the system. The open-loop transfer function is represented by the ratio of the output angle θ_e to the error angle θ_e . But since θ_e is such a small quantity in sensitive servo systems, it is difficult to extract the true signal from

noise, quadrature and harmonics. The designer therefore utilizes the closed-loop transfer function $\theta_{\theta}/\theta_{t} = KG/(1 + KG)$.

Open to Closed Loop

To utilize the servo conversion charts the amplitude and phase angle for a specific frequency must be known. For example an open-loop control system with a transfer function $KG(j\omega) = 5/[j\omega (0.6 j\omega + 1)]$ $(0.1 j\omega + 1)$ will have as an output when the frequency ω is 2 radians per sec, an amplitude A of 1.6 and a phase angle a of -151 deg. To determine the closed-loop response reference is made to Fig. 1A, wherein the abscissa represents the open-loop amplitude A while the ordinate represents the closed-loop amplitude B.

Method

First locate the curve representing a phase angle a of -150 deg, the nearest value on the chart to the -151 deg given. The line A=1.6 intersects this phase-angle curve on the vertical scale at the value B=1.88, which is the amplitude of the loop when closed.

To obtain the phase angle of the closed loop performance the chart of Fig. 1C is used. The line A=1.6 intersects the open-loop phase angle curve a=-150 deg. The corresponding value of the phase angle of the closed loop b is then read on the vertical scale as -35 deg.

Closed to Open Loop

The servo conversion charts are equally effective in converting the closed-loop to the open-loop performance. A closed-loop transfer function of $KG/1+KG)=5/[j\omega\ (0.6\ j\omega+1)\ (0.1\ j\omega+1)+5]$ will result in an output when the frequency ω is 3 radians per sec, of an amplitude B of 2.62 and a phase angle b of -134 deg. To transform to the open-loop characteristics for these particular values reference is made to the chart of Fig. 2A.

The line B=2.62 intersects the closed-loop phase-angle curves -130 and -140 deg. By interpolation the corresponding value of the open-loop amplitude A for b=-134 deg is read on the vertical scale as 0.77.

To obtain the phase angle of the open loop the chart of Fig.

(Continued on page 174)

Servo Analysis Charts (continued from page 173)_

2D is used.

On the abscissa the closed-loop amplitude B=2.62 is located. This line intersects the closed-loop phase angle curves. Again by interpolation for b=-134 deg the corresponding open-

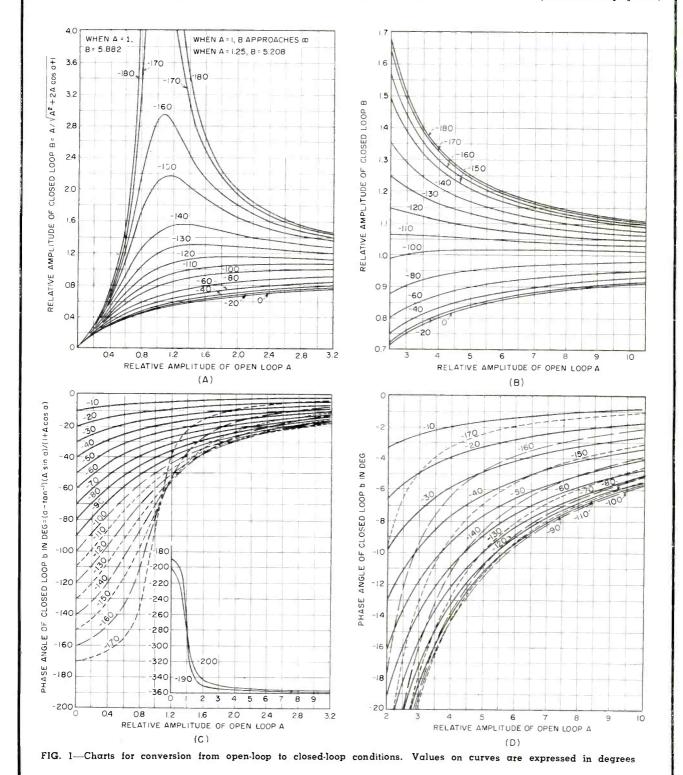
loop phase angle a is read on the vertical scale as -168 deg.

Summarizing

To summarize, the charts of Fig. 1A and 1B are used to obtain the closed-loop amplitude B

when the open-loop amplitude A and phase angle a are known. The charts of Fig. 1C and 1D are used to obtain the closed-loop phase angle b when A and a are known.

(Continued on page 176)



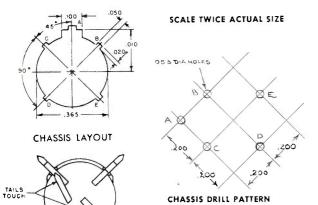
174





STAND-OFF Type Universal Transistor Socket. Shown four times actual size

UNIVERSAL TRANSISTOR SOCKETS



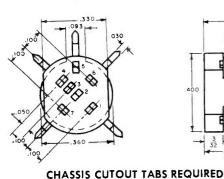
New Universal Transistor Sockets for use with the ten transistor bases illustrated and the five base types shown. Casting is mica-filled phenolic (MFE).

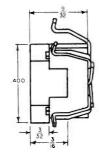
Contacts are beryllium copper, gold plated. Contacts may be used with either one or two sided 1/16" p. w. boards. Table at lower left lists the chassis cutout tabs required for the various base types.



STAND-OFF TYPE UNIVERSAL TRANSISTOR SOCKET

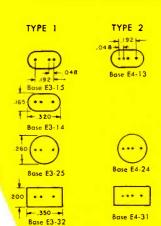
"CINCH components for printed circuitry", 24 page catalog, available on request.







TRANSISTOR BASES FOR THE NEW UNIVERSAL TRANSISTOR SOCKETS







FOR THE VARIOUS BASE TYPES

Part No.	Transistor Base Types	Chassis Cutout Tabs Used	Contact Positions Used
46T24443	All	A, B, C, D, E	All
46T24444	1 & 3	C, D, E	1, 3, 4, 7
46T24445	2 & 3	B, C, D, E	1, 2, 3, 4, 7
46T24446	3	C, D, E	1, 4, 7
46T24447	4	A, B, C, D, E	1, 4, 5, 6, 7
46T24448	5	B, D, E	1, 6, 7
46T24419	1 & 3	C, D, E	1, 3, 4, 7

In positions where contacts are not required, cavity for contact is also omitted except in position 5, on sockets 46T24444, 24445, 24446, and 24448.

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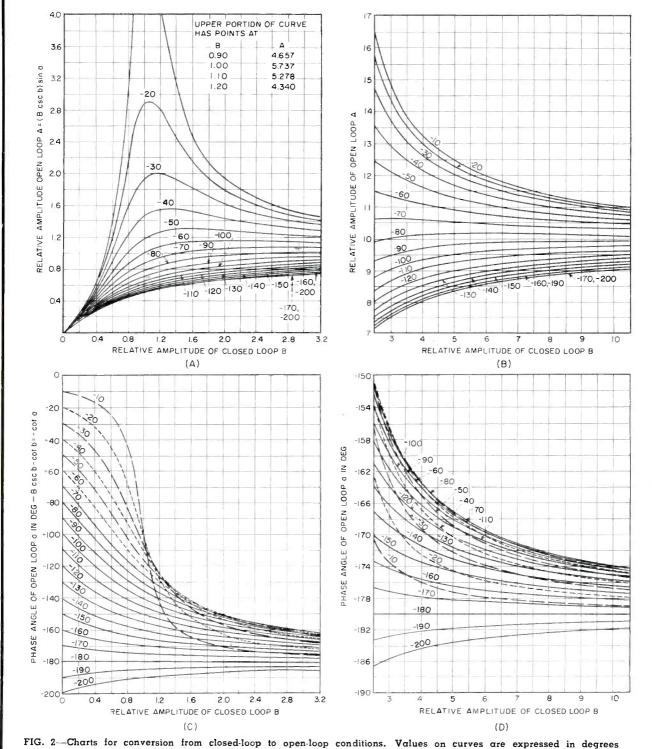
Servo Analysis Charts (continued from page 174).

The charts of Fig. 2A and 2B are used to obtain the open-loop amplitude A when the closed-loop amplitude B and phase angle b are known. The charts of Fig. 2C and 2D are used to obtain the open-loop phase angle a when B and b are known.

To plot a representative closedloop or open-loop response curve usually requires eight or ten frequency checks. This results in calculations involving many terms some of which may be in error. Use of these servo charts should not only eliminate the possibility of these errors, but also provide a quick means of improving system performance.

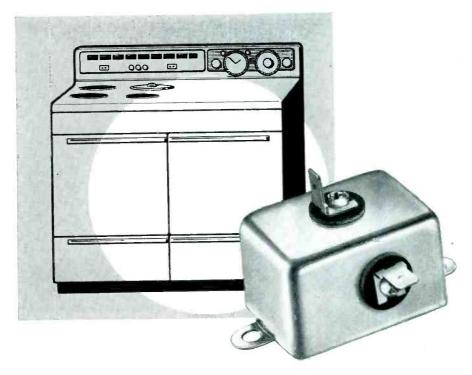
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A major appliance manufacturer recently had need for an economical buzzer-type alarm to act as a high-temperature signal on an oven.

The manufacturer turned to Mallory—pioneer in the automobile vibrator industry—for aid in designing this electromechanical device. The idea sounded challenging . . . so, we put our quarter-century of vibrator experience to work.

Literally overnight, we came up with a simple, practical design which we're now economically producing . . . and we have a new and satisfied customer.

Maybe you, too, have need for components that might be considered "buzzin' cousins" to a vibrator . . . not only in the home appliance field, but perhaps for industrial products. If so, there's a wealth of experience and engineering ability in Mallory's Vibrator Division that can help solve problems you may have in electromagnetic or electromechanical devices. Let's talk it over!

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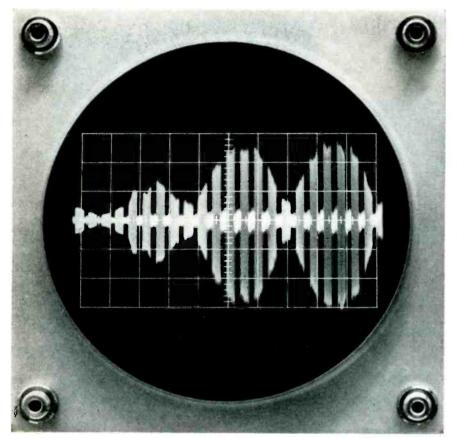
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Electrons At Work



Variations in amplitude of satellite's pulses are accounted for by sphere's rotation once every six seconds

Sputnik's Beep Baffles Scientists

WHAT DOES IT MEAN, if anything? Not only scientists but the general public as well are deeply concerned with the significance of the well publicized radio transmissions of Sputnik I.

Although there is considerable disagreement about whether coded data is contained in the satellite's transmissions, scientists and engineers in this country are gathering data feverishly. Electronic engineers at Tektronix in Portland, Oregon have made photographs of oscilloscope presentations of the beep, along with other measurements.

The signal shown in the photograph was received on a frequency of 20.005 megacycles. Height of the oscilloscope is directly proportional to signal strength, and the total horizontal sweep is equivalent to 10

seconds. The received signal was beat against an oscillator to produce a difference signal of 1.8 kilocycles.

This signal was received on Oct. 4 at 10:16 pm Pacific Standard Time. The beeps lasted for a period of 0.27 second and the pause was 0.19 second, a rate of 2.17 pulses per second. The ratio of on to off time changed from 27 to 18 by the morning of Oct. 6 to 18 to 23 and by that night to 18 to 22.

Of course, after that there were periods of sticking on one or the other transmission frequency for long periods of time.

The hypothesis that the satellite rotates once every six seconds is used to account for the three-second periods during which the pulses vary in intensity in half sinusoidal patterns.

Conductor Size and Spacing for Printed Circuits

By L. N. MERSON Philadelphia, Pa.

CONDUCTOR SIZE is determined by the desired current-carrying capacity of the wire. For circular copper wire, the general practice is to allow 300 to 400 circular mils per ampere for normal ventilation and space conditions, and 500 to 600 mils per amp for small poorly ventilated enclosures. The following formulas were developed for calculating the width of strap conductors as used in printed circuits, so as to obtain the same cross-sectional area.

For normal conditions: width in inches = amps/thickness \times (235 to 315) \times 10⁻⁸ or

For close quarters: width in inches = amps/thickness \times (390 to 470) \times 10⁻⁶ or, in terms of foil weight in ounces per square foot (1 oz = 0.00135 inches thick): amps/oz \times (11/64 to 15/64) for normal conditions or amps/oz \times (19/64 to 22/64) for close quarters.

Table 1 shows the nominal widths per ampere for 1 and 2-oz copper foil

A ½ in. wide strap of 2-oz copper foil is approximately equivalent to No. 24 copper wire.

Strap conductors have considerably more surface area than the equivalent circular wire. A 3 in. strap of 2-oz copper foil (1 amp capacity) has about 4 times the surface area of the equivalent size of circular wire, and therefore 4 times the r-f current capacity due to skin effect. This larger area

Table I—Nominal Width of Printed Circuit Conductors

	1-oz copper	2-oz copper
Normal Conditions	3/16 in./ amp	3/32 in./ amp
Close Quarters	5/16 in./ emp	5/32 in./





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- 0.005% resolution with 10 turn voltage control.
- Continuously variably output voltage without switching.
- External overload and short circuit protection included.
- Either positive or negative can be grounded.
- Units can be series connected.
- Suitable for square wave pulsed loading.
- Power requirements: 105-125 volts, 50-400 cycle.
- Terminations on front and rear of unit.
- High efficiency.
- Low heat dissipation.
- Compact, light weight.
- Color: grey hammer tone.
- Suitable for bench or rack use.
- Voltmeter and ammeter provided.

VOLTAGE REGULATED POWER SUPPLIES

				-			
Model	Output Volts	Output Amps.	Outp Imped Ohr DC- 1 KC	ance	R	ack Mour H	it D
SC-32-0.5	0-32	0-0.5	0.02	0.2	19"	31/2"	11"
SC-32-1	0-32	0-1	0.01	0.1	19"	31/2"	11"
SC-32-1.5	0-32	0-1.5	0.01	0.1	19"	31/2"	11"
2SC-32-1.5	0-32	0-1.5	0.01	0.1	19"	7"	11"
DUAL OUTPUT	0-32	0-1.5	0.01	0.1	15	,	**
SC-32-2.5	0-32	0-2.5	0.01	0.1	19"	31/2"	11"
SC-32-5	0-32	0-5	0.005	0.05	19"	51/4"	13"
SC-32-10	0-32	0-10	0.001	0.01	19"	83/4"	13"
SC-32-15	0-32	0-15	0.001	0.01	19"	101/2"	13"
2SC-100-0.2	0-100	0-0.2	0.1	1.0	19"	51/4"	11"
DUAL OUTPUT	0-100	0-0.2	0.1	1.0	19"	574	11
SC-150-1	0-150	0-1	0.05	0.5	19"	51/4"	13"
SC-300-1	0-300	0-1	0.1	1.0	19"	83/4"	13"
SC-300-1	0-300	0-1	0.1	1.0	19"	83/4"	13"

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Model SC-32-0.5 SC-32-1 SC-32-1.5 SC-32-2.5 also results in more efficient heat dissipation, so that probably much higher current densities can be tolerated, and strap widths can be less than values calculated allowing 300 circular mils per ampere.

A la-in. wide conductor of 2-oz copper foil can carry up to 20 amps or more without rupturing, at least under good ventilation conditions. The formulas therefore contain a high safety factor.

Table 2 shows the overload current values for various conductor sizes. These are maximum values for current surges and are not to be exceeded at any time. Normal operating currents should be closer to the values indicated in the preceding table.

► Solder Bridging—A spacing between conductors of at least ½ in. is recommended if dip-soldering or

similar techniques are to be used, since closely spaced conductors present an opportunity for short circuits due to solder bridging across the gap. Although the use of soldering fluxes reduces this danger to some extent, this minimum spacing should be maintained.

breakdown becomes very critical at high altitudes. At sea level and 25 C the breakdown voltage for a gap with sharp edges is 1,000 volts for a ½ in. separation. However, at 50,000 feet and 60 C the same gap will have a breakdown voltage as low as 100 volts. Using a safety factor of 2, a good rule would be to allow ¼ in. separation per 100 volts for equipment which may be used at altitudes up to 50,000 feet. A further safety factor results

Table II—Overload Current and Resistance for Printed Wiring

Width	Amperes	Ohms/in
1/4 in.	23	0.002
1/8 in.	15	0.004
1/16 in.	10	0.008
1/32 in.	5	0.016
2-oz coppe	r	
1/4 in.	35	0.0009
1/8 in.	20	0.0018
1/16 in.	15	0.0035
1/32 in.	8	0.007

from the fact that the printed edges do not form needle gaps, which is the condition for which these values are calculated. At ground level this factor can be increased 10 to 1.

Engineers Work in Altitude Simulator

ENGINEERS are working at simulated altitudes of 95 miles in Beverly Hills, Calif. The altitudes are created in a high-vacuum laboratory designed by Litton Industries under Air Force sponsorship.

Two large pumps used to evacuate the chamber are believed to be capable of reducing pressure to the equivalent of 136 miles altitude. So far, a simulated altitude of 110 miles has been obtained, although

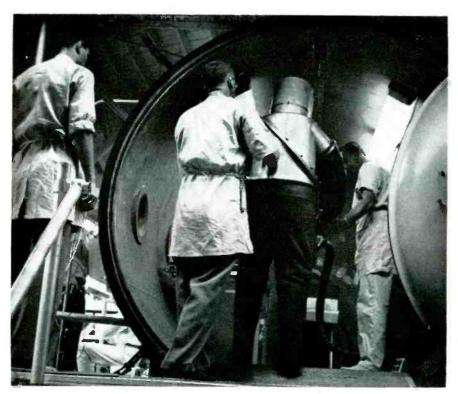
no one was in the chamber during the test. Space suits worn by personnel in the 15-foot long cylinder subject the engineers to the pressure equivalent of 27,000 feet.

The walls of the tank are made of half-inch hot-rolled steel. Port-holes enable observers to see the engineer inside. A physician watches instruments that continuously monitor blood pressure, respiration, temperature.

A major application of the highvacuum environment is in the design of vacuum tubes. Normally adjustments are made to the elements of a tube, then the air is evacuated and the envelope sealed. After tests are made, the seal must be broken and new adjustments made or another tube with the new parameters used. The process can take months or, if new samples are used each time, it can be expensive.

In the vacuum chamber, adjustments can be made and the tube can be tested immediately since it is already operating in a vacuum. It has been found that an engineer can work in this atmosphere for as long as four hours.

Another major area in which the chamber will be used involves highaltitude weapons systems. Lubri-



Space-suited engineer enters chamber capable of simulating altitudes of 136 miles

PROBLEM:

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In a submarine, every inch of space is required to perform several functions. In some cases, a battle station must also serve as living quarters for the ship's personnel. Such was the case of the recently launched third atomic-powered submarine, the U.S.S. Skate. It was found necessary to place sleeping berths in the forward torpedo room. In the event of an enemy contact, berths must be repositioned quickly, to allow space for the vital workings of the torpedo room and silently, to avoid detection by enemy sonar. Grant Slides were chosen by the Electric Boat Division of General Dynamics for this essential job and they perform it well. In addition to operating quickly and silently, the slide used had to be sturdy enough to support a sailor...again the Grant Slide specified proved the perfect answer for this important application.

Grant No. 380 Slides recommended for loads up to 500 lbs./pair

Courtesy U.S. Navy Electric Boat Division of General Dynamics Corporation

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The Front Cover

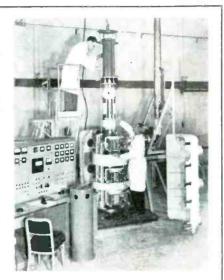
THE KLYSTRON being lowered into a test tank delivers up to 1,000,000 watts peak r-f power. Average power is 100,000 watts. The 700-pound X626 klystron is 10 feet 5 inches long.

The high-power tube is expected to increase the effectiveness of some types of radar and, in linear accelerator operation, to offer new advantages in the processing of food, chemicals, plastics and petroleum.

The X626 was designed and developed by Eitel-McCullough for Continental Electronics Mfg. under sponsorship of the Rome Air Development Center. Eitel had to provide special laboratory equipment for production, aging and testing of the new klystrons.

The lab is equipped with a special high-voltage power supply divided into two sections. One section can deliver 120,000 volts at 2 amperes, the other, 120,000 volts at 4 amperes. The two sections are housed together and can be connected in series to furnish 240,000 volts. Output can be continuously varied between 15,000 and 240,000 volts.

All test operations involving high voltage are controlled from the remote test console shown in the left of the photograph. The console enables engineers to control and adjust the power supply, tune klystrons being tested through a series of servomechanisms and monitor all test



data. A key interlock system is designed to ensure that all personnel are clear of high-voltage equipment before power can be turned on.

Several test tanks with a combined capacity of 10,000 gallons of oil are used for testing and operating the klystrons. The electron gun of the tube extends below floor level into the insulating and cooling oil in the tanks.

Output of the tube is fed into a dummy water load (extending up at the right of the klystron) to dissipate the r-f energy. Over two tons of lead shielding is used to protect personnel from x-rays. The cylinder in front of the test console is part of the shielding.

The facility includes a two-ton electric hoist for handling the klystrons.



Engineer adjusts tube minus envelope in high-vacuum chamber

cants, known to vaporize at high altitudes, will be studied.

Electronics plays a part in monitoring the evacuated tank. An electron gun fires a stream of electrons inside the chamber. The stream is hardly visible because of the lack of air. If a leak occurs, however, the electron stream ionizes the gas causing a glow.

An electronic production technique is used to check the space suit each time it is used. Helium is pumped into the suit with the suit in the chamber. A Consolidated Electrodynamics leak detector in the chamber detects escaping gas.

Extend Output With Regulated Flip Flop

By R. W. HOFHEIMER

Lincoln Laboratory
Massachusetts Institute of Technology
Lexington, Mass.

NEED FOR a bistable multivibrator circuit capable of producing an output having a wide voltage swing at a relatively large current occasioned the development of the regulated flip-flop shown in Fig. 1. This circuit is suitable if only one output is required instead of the two complementary outputs available from conventional flip-flops.

► Advantages — Primary characteristics of the regulated flip-flop are the accuracy and stability of its output. This is achieved in conventional flip-flops by using clamping circuits. The inherent difficulty encountered with clamping techniques is that when the output amplitude is increased the output impedance is correspondingly reduced thereby defeating the initial purpose of the circuit.

Stability of the output voltage produced by a regulated flip-flop with varying loads depends, to a great extent, upon the open-loop gain of the amplifier. Since gains of 1,000 or more are readily obtainable, a high degree of regulation is provided. The amplitude swing of the output is approximately 100 volts.

▶ Operation—The regulated flipflop shown in Fig. 1 includes a conventional direct coupled, feedback stabilized amplifier. Considering only the amplifier portion of the circuit, the output voltage can be determined as follows:

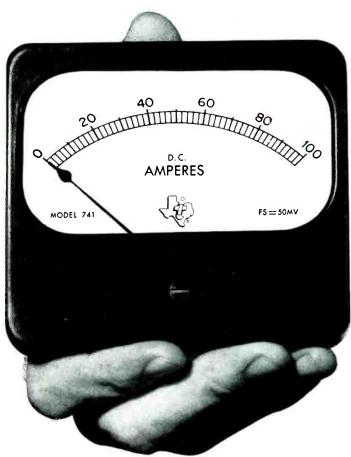
$$\frac{E_{\text{out}} - E_G}{R_1} = \frac{E_G - E_{CC}}{R_2}$$

$$E_{\text{out}} = \frac{R_1}{R_2} (E_G - E_{CC}) + E_G \tag{1}$$

where $E_{\text{out}} = \text{output voltage}$; $E_{g} = \text{grid bias}$; and $E_{gg} = \text{bias supply voltage}$.

When means are provided for applying inputs consisting of successive trigger voltages having opposite polarities, the amplifier is converted into a bistable d-c amplifier. This is accomplished through the switching circuit made up of

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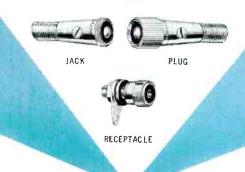


TEXAS INSTRUMENTS

actual size of the new



miniature microphone connectors



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Part No.	Description	Length	AMPHENOL Connector
75-1	Plug	111/64"	75-MC1F
75-2	Jack	1^a	75-MC1M
75-3	Receptacle	5/8"	75-PC1M

Simple to connect, reliable in operation, AMPHENOL'S miniature microphone connectors are ready now for your use. For additional information, please write.

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crystal diodes D_1 and D_2 . The output voltage for positive input pulses can be determined by Eq. (1) and for negative input pulses can be determined as follows:

$$\frac{E_{\text{out}} - E_{G}}{R_{1}} = \frac{E_{G} - E_{CC}}{R_{2}R_{3}}
R_{2} + R_{3}$$

$$E_{\text{out}} = \frac{R_{1}(R_{2} + R_{3})}{R_{2}R_{2}} (E_{G} - E_{CC}) + E_{G}$$
(2)

Introduction of positive feedback through crystal diode D_s from the output stage to the input stage converts the bistable d-c amplifier into a regulated flip-flop. The amplifier will now maintain itself in

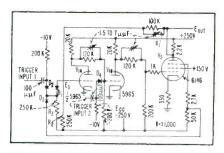


FIG. 1-Regulated Flip-Flop Circuit

either of the two states. A second trigger input through crystal diode D_4 is incorporated in the final design to provide means for resetting the flip-flop.

Equations (1) and (2) demonstrate that the stability of the output voltage depends on the constancy of R_1 , R_2 , R_3 , and E_{cc} and on the amount of drift exhibited by E_g in the first stage.

Infrared Camera

AN INFRARED CAMERA capable of giving temperature indications directly from a photograph has re-

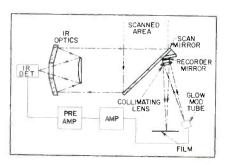
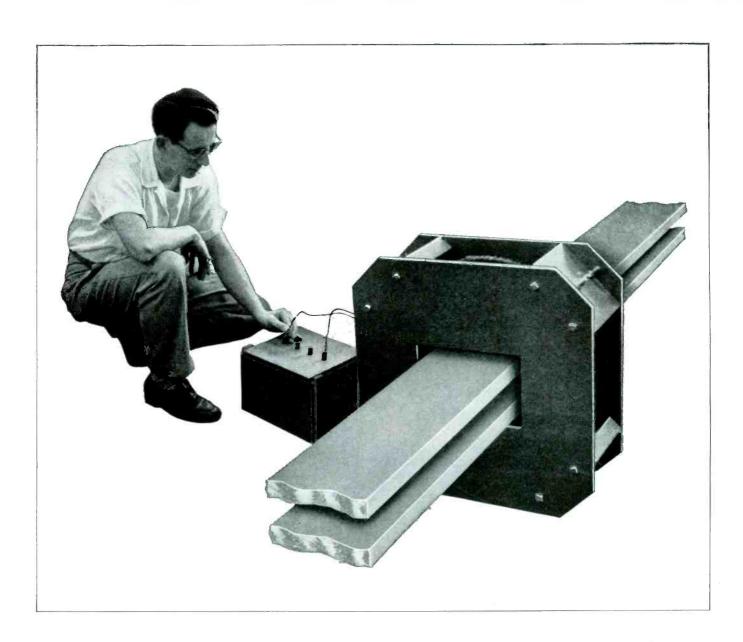


FIG. 1—Arrangement of infrared scanning system developed for photography



Now... measure 200 to 10,000 amperes with isolated meters—CONTROL's Standard Transductors

CONTROL transductors have made obsolete the use of shunts for metering or recording heavy d-c loads. Now, for the first time, a standard line of transductors—nine units ranging from the 200-amp to the 10,000-amp size—make it possible for the systems engineer to measure high bus currents without direct electrical connections into the circuit.

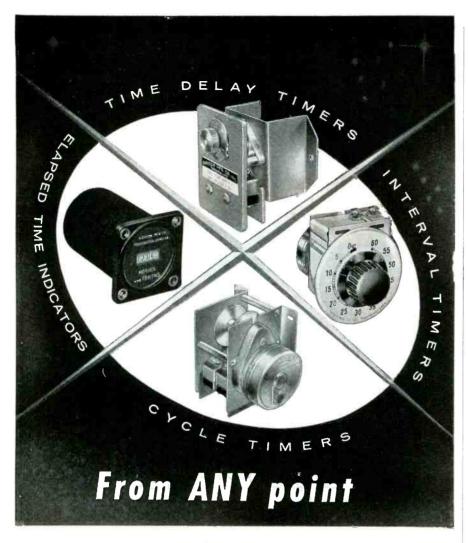
CONTROL transductors are saturable reactors, through which the bus or cable passes. Output is linearly proportional to the bus current, with an accuracy to \pm 1% of full scale reading. Supply voltage variations of \pm 10% will not affect this accuracy.

In addition to eliminating the need for breaking into the circuit for connections, the CONTROL transductor has another major advantage over the shunt-millivoltmeter. The transductor will deliver relatively large amounts of power to permit such things as overload relaying and to permit a feedback signal for a magnetic amplifier.

No longer need you be dependent upon "what's available" or a special design. Catalog T-10 gives you a standard range of transductor sizes to meet vour every need. For full details . . . CONTROL, Dept. E-43, Butler, Pa.

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A SUBSIDIARY OF GENERAL TIME CORPORATION

HAYDON Manufacturing Company, Inc. 2436 ELM STREET, TORRINGTON, CONN.



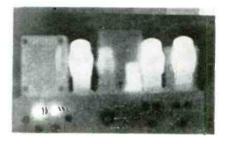
Temperature photo of man with pipe. Gray scale at top compares to temperatures of (1 to r) 75.2 F, 77.4 F, 79.5 F, 83 F and 86.5 F

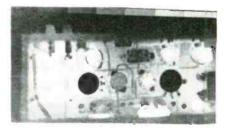
cently been developed. Using a thermistor and mirror scanning system, the device detects a temperature differential of 0.02 C in the scanned area. The field of scan is 20 deg horizontal and 10 deg vertical containing 30,000 resolution elements.

► Gray Scale — Temperatures of points in the photograph can be determined from a calibrated gray scale produced on the film during photography.

The system is shown in Fig. 1. The point scanned by a mirror is reflected through an optical system to a flake thermistor infrared detector.

The output of the thermistor is then used to modulate a glow modulator tube. The light from the tube is focussed on a mirror attached to the rear of the scanning





Infrared photograph of electronic chassis. Tubes are clearly outlined and transformer at left is hotter than rest of chassis

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Compensated for ambient temperature changes from -55° to $+70^{\circ}$ C. Heaters consume approximately 2 W. and may be operated continuously. The units are rugged, explosion-proof, longlived, and-inexpensive!

TYPES: Standard Radio Octal, and 9-Pin Miniature . . . List Price, \$4.00. Standard Delays

AMPERITE

REGULATO

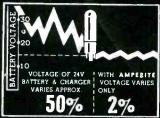
der-voltage or under-current protection. PROBLEM? Send for Bulletin No. TR-81

Also - Amperite Differential Re-

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Hermetically sealed, they are not affected by changes in altitude, ambient temperature (—55° to $+90^\circ$ C.), or humidity . . . Rugged, light, compact, most inexpensive List Price, \$3.00. Write for 4-page Technical Bulletin No. AB-51

MPERITE CO. Inc., 561 Broadway, New York 12, N. Y.

Telephone: CAnal 6-1446 In Canada: Atlas Radio Corp., Ltd., 50 Wingold Ave., Toronto 10 ELECTRONS AT WORK

mirror and moving in synchronism with it. The mirror motion scans the glow modulator tube output across the film to make the photograph.

Typical infrared patterns taken with this equipment are shown in the photographs.

Scanning time for a complete photo can be as short as 1.9 minutes for a 10 by 10 degree field. Depending on resolution required, scan time can be up to 17 minutes.

Phototubes Count Buses

A SYSTEM under development in London uses a photoelectric scanning system to keep track of buses as they pass check points. As described by McGraw-Hill World News, a box containing a light source and phototube is mounted on a lamp post or wall at selected points along the bus route. When a bus passes, a tape on the side of the bus reflects the light from the source back to the phototube in a coded series.

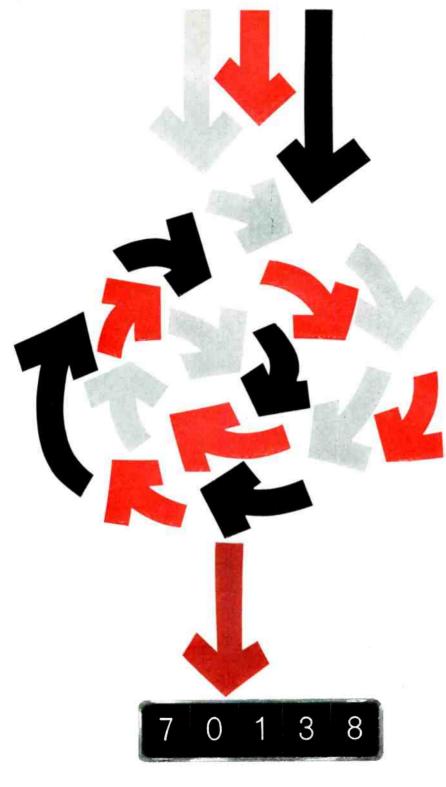
The phototube output is amplified and fed to the central control room where the bus number and location are flashed on a panel for checking.

Solar Powered Electric **Fence Charger**

By G. W. ISAACS Associate Professor
Agricultural Engineering Department
Purdue University
Urbana, Ill.

SILICON SOLAR CELLS are supplying energy to operate an electric fence charger in experiments at the Purdue University Agricultural Experiment station. Electric fence chargers now common on farms are powered either by connection to electric mains or by dry or storage batteries.

Connection to power mains may be impractical for fence chargers used in remote areas. Replacing of dry batteries or the recharging of storage batteries is a nuisance job sometimes forgotten by the farmer until the livestock



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251-57

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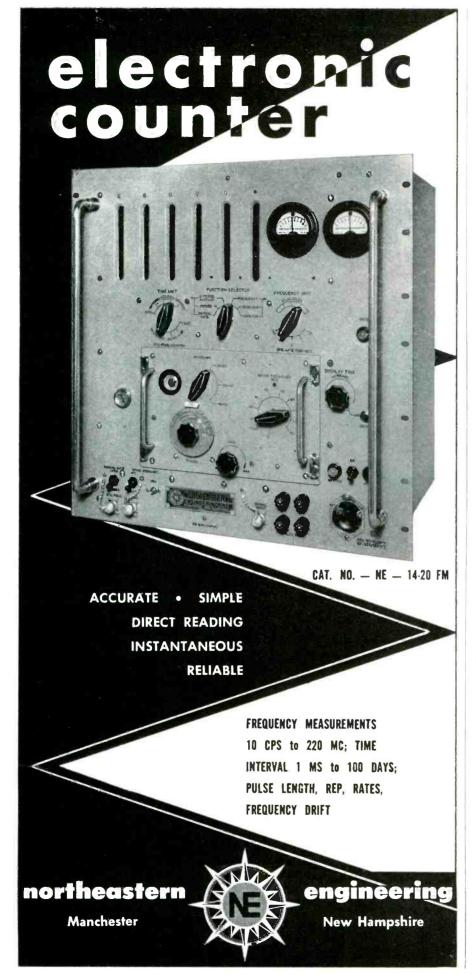
DEVICES & INDICATORS ...

DIGITAC, INC.

420 South Beverly Drive
Beverly Hills, California
an affiliate of Bill Jack Scientific
Instrument Co. and

Otto Nemeth

189



have jumped the fence because the batteries were discharged.

In the experimental application, silicon solar cells convert solar energy to electrical energy which is used to maintain the charge of a storage battery. The storage battery operates the fence charger on a 24-hour basis, whether or not the sun is shining. It is interesting to note that the solar cells will not operate the fence charger alone, even in bright sunlight, since the current required by the charger flows



Solar cells mounted on battery case supply power for electric fence

in brief peaks of high instantaneous value and spaced about one second apart. The solar cells alone cannot supply the high instantaneous current demand, but can maintain a charge on the storage battery which can supply the peak demand.

► Circuit—The solar cells are connected across the battery. Measurements with an integrating microammeter showed that the equivalent of 30 milliamperes of continuous current at six volts is required by the fence charger, a commercial model. Forty-eight silicon solar cells are located in a glass-enclosed frame atop the fence charger as shown in the photograph. Three groups of 16 series-connected silicon cells are connected in parallel. The storage capacity of the storage battery is sufficient for at least ten days operation of the fence charger without sunlight. Both lead-acid and nickel-cadmium storage cells have been used. The latter is probably more desirable, since it is less af-

Extended Life and High Stability at 1256

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616G-617G-SUBMINIATURE MYLAR* Dielectric CAPACITORS

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This ruggedly designed capacitor is a standout for stability after thousands of hours at 125°C... field tested under the severest military conditions.

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A superior capacitor element rated for accelerated life testing twice that applied to conventional metal enclosed tubulars.

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Formed Mylar insulators prevent leakage to the case and contribute to the high IR which characterizes these designs.

*PuPont's trademark for polyester film.



Long Term Stability—Extensive testing indicates capacitance change is less than 1% after 5000 hours operation at rated voltage and 125°C

Life Test—500 hours at 125°C and 125% of rated voltage

Insulation Resistance—See curve below for typical performance

Temperature Immersion—Meet requirements of MIL-C-25A for 125°C (Characteristic K)

Mechanical Properties—Meet all requirements of MIL-C-25A

Capacitance Change with Temp.—See curve below for typical performance

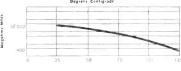
616-G (One Lead Grounded to Case)

Cap. In . Mfd.	50V	150V	400 V
.001	173 x 11/4	.173 x ½6	233 x 11,
.047	.312 x 11/6 .400 x 3/4	.312 x 11/6 .400 x 15/6	

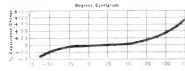
617-G (Both Leads Insulated From Case)

50V	150V	400V
	.173 x 3/4 .193 x 3/4 .233 x 3/4 .312 x 7/4 .400 x 11/4	.312 x 1/4 .400 x 11/4

Insulation Resistance vs. Temp



Capacitance Change vs. Temp



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GOOD-ALL CAPACITORS NOW AVAILABLE AT YOUR LOCAL DISTRIBUTOR.

(continued)

GAS-FILLED CONDENSERS



Lapp's experience of 18 years of design and manufacture of gas-filled condensers is back of this precision-made unit and its promise of years of trouble-free duty. It is small in size and low in loss,

offers high voltage and current ratings, high frequency limits, safety, puncture-proof operation and constant capacitance under temperature variation.

The entire electrical and mechanical assembly of the Lapp gas-filled condenser is supported by a top aluminum ring, the steel tank serving only as a support for this ring and as a leak-proof gas container. High-potential plates are carried on a rigid center stud which is supported by a top ceramic bowl. Grounded rotor plates are carried on ball bearings nearly the full tank diameter. This construction provides a grounded tuning shaft on variable models and makes possible efficient and complete water cooling for high current operation.

Models in four tank diameters, 7" to 18", are available, in variable or fixed capacitances, for duty up to 30,000mmf; in current ratings to 400 amps at 1mc; operating voltages to 80Kv peak. Write for Bulletin 302, with complete description and characteristics data. Lapp Insulator Co., Inc., Radio Specialties Division, 137 Sumner Street, Le Roy, N. Y.



fected by periods of overcharging.

More efficient use could be made of the solar cells if they could be automatically disconnected from the circuit when the sun is not shining and they are not charging the storage battery. If they are not disconnected, the solar cells draw current from the battery at a very significant rate when the sun is not shining. A reverse current relay similar in operation to that used on automotive electric systems could be used, but it would have to be rather sensitive, costly and would require some energy to operate.

An arrangement currently being evaluated uses a thermostat in series with the solar cells. The thermostat is set just above the highest expected night-time temperature so that it opens the circuit at night and on most cloudy days. When the sun strikes the thermostat, it closes the circuit and allows the solar cells to charge the storage battery. The thermostat is painted black for maximum solar energy absorption and enclosed under glass to protect it from the cooling effect of the wind. A transistor diode is also being considered for this application.

Meter Shows Current Drift from Nominal

By DAVID T. GEISER

Sprague Electric North Adams, Mass.

CURRENT stability is often difficult to measure because variations are usually small compared to the steady value and even smaller in comparison with the full-scale value of the ammeter that must be used

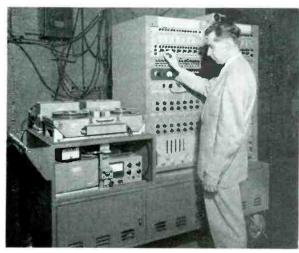
However, measurements of small variations in current are important in constant-current applications such as transistor test power supplies and timing circuits, as well as any place where changes in electrical power or rate of energy transfer are significant.

The circuit described was built to monitor deviations in current in test and control circuits. This is

How a tape recorder on wheels does multiple duty

Complete make-ready at test cells in less than an hour

Here is a whole "dynamic-data recording facility" that can be rolled into place as easily as coffee and doughnuts. It is the familiar pushcart — but in this case glorified into a versatile system of roving instrumentation.



Ampex 800 Mobile Tape Recorder and other equipment mounted together on a dolly at General Electric's Small Aircraft Engine Department.

42 TAPE TRACKS CAN CONVERGE ON A SINGLE TEST

For its own use, the Small Aircraft Engine Department of General Electric developed this dolly-mounted tape system to circulate among a number of test cells. Each dolly carries an Ampex 814, fourteen-track recorder, and all related calibrating, amplifying and monitoring equipment. Three are shared among the many engine test cells . . . or all can be used at once on the same test, making 14, 28 or 42 tape tracks available on any engine run as needed.

INTERCONNECTED EQUIPMENT SAVES TIME

During lengthy engine setups, there is no tape recording equipment tied up at the test cell. When the engine is ready, the recording equipment is connected in less than an hour. Everything on the dolly is permanently interconnected, hence only external hookup need be made. Formerly, when this instrumentation was brought in in pieces, it was an all day job.

Data recorded on this mobile system include turbine-blade stresses, vibrations, control responses and dynamic temperatures and pressures. Data frequencies range up to 3000 cycles per second. By slow playback, magnetic tape brings these

down within the limits of direct-writing instruments of only 100-cycle response. The dynamic information gained in this way has greatly aided the development of small turbo shaft engines of remarkable power-to-weight ratio. One of these, General Electric's T58, produces 1024 horsepower from only 325 pounds of engine weight (including a 75 pound reduction gear).

A CHOICE OF RECORDERS FOR MOBILE USE

The Ampex 814 is extremely compact. The 14-track recorder occupies only three cubic feet and weighs only 140 pounds. It also has factory-furnished shock mounting and is of exceptionally rugged structure.

Though Ampex's FR-100 and FR-1100 laboratory tape recorders are much larger, they too can be mounted on dollies or trailers. They record and reproduce, have more modes of tape travel, and require only 117-volt, 60-cycle power

All of these Ampex recorders have interchangeable plug-in amplifiers and a wide choice of tape speeds. These features accommodate the changing requirements that are likely in moving from test to test.



Mobility of another size an Ampex FR-100 recorder (left foreground) in a large instrumentation trailer designed by General Electric's Missile and Ordnance Systems Department for firing range use. FR-100s are sometimes used on small dollies too.

A new brochure on the Ampex 800 Mobile and Airborne Recorder has just been published. May we send you a copy? Literature is also available on other models, and recommendations can be made on specific applications. For any of these requests, write Dept. E-12.

MAGNETIC TAPE APPLICATIONS BY AMPEX

ONE OF A SERIES



Series FR-100



Series 800 Mobile and Airborne



Model FR-200 Digital



SeriessFL-1,00 stoopsRetorders



Series FR-1100



FIRST IN MAGNETIC TAPE INSTRUMENTATION

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with an FM TELEMETRY Transmitter

Sensitized for human reactions, this dummy helps collect human factor data for development of ejection seats for supersonic jet aircraft. The full-scale rocket sled tests are one phase of the industry-wide program to develop a safe standardized pilot escape system for the Air Force.

The Model 3021 Transmitter used in these tests is a rugged subminiaturized unit designed for high shock impact and extreme environments.

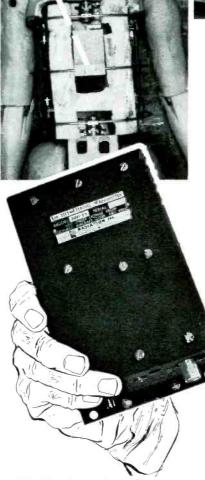
Frequency - :

- 215-235 mc

Power Output - Weight -

2 watts
 1.7 pounds

Write for complete data and prices to P.O. Box 37, Melbourne, Florida



Personnel Inquiries Invited.



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Meter shows current deviations 100 microamperes either side of nominal current in circuit being monitored

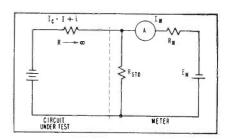


FIG. 1—Only deviations from nominal current (I) pass through meter

done by effectively subtracting the nominal current from the actual current and indicating the difference directly on a meter.

In Fig. 1, I_{\circ} is actual current in a source of nearly constant current, I is the steady portion and i the deviation.

For zero milliammeter indication,

$$I_c = I$$
 and $E_m = IR_{\rm std}$

By superposition

By superposition
$$I_m = \frac{(I+i)\frac{R_{\rm std}R_m}{R_{\rm std}+R_m}}{R_m} - \frac{IR_{\rm std}}{R_{\rm std}+R_m}$$

$$= \frac{(I+i)R_{\rm std}}{R_{\rm std}+R_m} - \frac{IR_{\rm std}}{R_{\rm std}+dR_m}$$

$$= \frac{iR_{\rm std}}{R_{\rm std}+R_m}$$

where E_m is voltage across meter, R_{std} is resistance standard and R_m is meter resistance.

This shows that the meter indication is proportional only to the variable part of the metered current.

▶ Design — The meter voltage source, E_m , should be a constant-impedance supply with adjustable output voltage. In the illustrated model dry cell batteries are used and voltage is varied with a constant-impedance attenuator. Enough se-

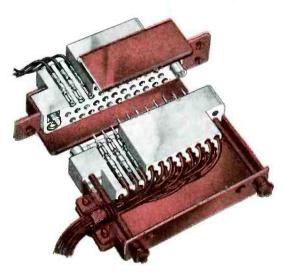
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MEETS MIL-C-8384A Specifications. Also physically interchangeable and will mate with ordinary connectors having similar contact arrangements.



EVALUATION UNITS available from stock—*Order now*. For complete information, write today for BULLETIN CEC 4004-X10.



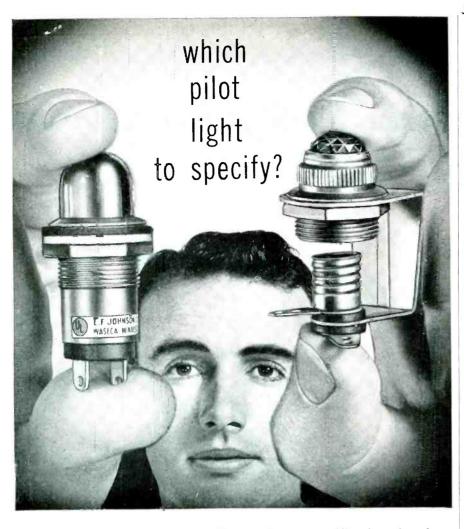
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Available types include: continuous indication neon types; models for high and low voltage incandescent bulbs; standard or wide angle glass and lucite jewels in clear, red, green, amber, blue or opal. Specials, including those meeting military specifications are also available in production quantities.



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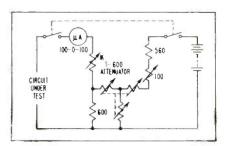


FIG. 2—Using a 45-volt battery in this circuit, steady currents from one to 50 ma can be balanced so that deviation current can be measured

ries resistance is used with the battery to equal attenuator impedance, and the attenuator is accurately terminated. This gives a variable voltage source with very close to 300-ohms internal impedance at small cost.

A current-deviation range of ± 1 ma was desired. For a 200-ohm $R_{\rm std}$, the meter resistance, $R_{\rm m}$, should be 1,800 ohms, using a 100-0-100 microammeter. The 300-ohm voltage source and 1,000-ohm meter required 500 ohms more, which is supplied by a variable resistor.

Operation with a 45-volt battery permits balancing out steady currents of one to fifty milliamperes with the circuit shown in Figure 2. Somewhat greater ease of balance is obtained by using a tapped battery and selecting voltages that permit balance in the low-attenuation portion of the T attenuator.

Accuracy measured is approximately three percent of full-scale deviation, 3 microamperes in this case, over the full range of steady current. Recalibration has not been found necessary after the battery and meter resistors have been adjusted.

A momentary on-off-on switch is recommended for ease of instrument use.

VHF Rheostat

By W. B. WRIGLEY and T. R. SCOTT, JR.

Engineering Experiment Station Georgia Institute of Technology Atlanta, Georgia

EXTENSION of the frequency rangeof crystal impedance meters to very high frequencies has emphasized the need for low-phase-angle vhf rheostats. The resistors presently



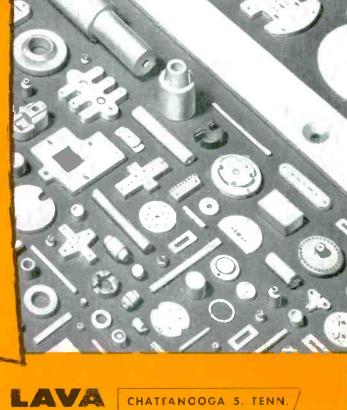
Rugged PLSIMAD® ALUMINA CERAMICS

may be the answer!

For exacting applications, your chances are better with AlSiMag pecause more special-characteristic Aluminas are available here than from any other source. You beneft from extra "know-how" ... years of experience in producing simple and complicated Alumina parts in a broad range of shapes and sizes ... plus equipmen for rapid delivery in any quartity. Precision tolerances. Prototypes pefore tooling, if was like.

Advantages like these give you greater freedom: Ten: le strengths up to 25,000 lbs./sq. in. Compressive strengths up to 420,000 lbs./sq. in. Flexural strengths up to 62,000 lbs./sq in. Superior electrical characteristics, Eafe operation at continuous temperatures up to 2952° F. Loss factors as ow as .C074 at 10,000 MC.

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Franklin AII Electronic Digital Voltmeter

5 COMPLETE READINGS/SEC - ACCURACY 0.1% Full Scale

MODEL 310 A DIGITAL VOLTMETER WITH MODEL 318 AMPLIFIER

Accuracy: Plus one count, minus nothing. (0.1% of full scale.)

Range: X1, 0.1 V to 120.0 V.
X10, 0.01 V to 12.00 V.
X100, 0.001 V to 1.200 V.
X1000, (318 A Amp. only) 0.0001 V to
0.1200 V.

Input, Impedance to Amplifier: 318, 1 megohm. 318 A, 100 K ohms.

Speed: Adjustable from 5 complete readings per second down. (310 A Digitizer alone: from 60 complete readings per second down.)

Reading modes: Manual—triggered by push button. Automatic—self triggering at 10 readings per second.

External—by relay closure.

External trigger—reads on applications of 20 volts minimum pulse with 5 volts per microsecond rise time.

Outputs: Visual—4 illuminated decimal digits.
(First digit : zero or one.)

Stair case code—a nine is approximately 55 volts; a zero is approximately 130 volts. Time gate—linearly proportional to input voltage (100 microseconds per volt.)

The Model 310 A is the voltmeter you've been looking for to provide you with reliable readings without periodic factory adjustments. It is designed, built and proven for making reliable production line and laboratory precision voltage measurements from 0.0001 volts DC to 120.0 volts DC in four ranges.

This versatile all electronic digitizer can also be used as an analog to digital conversion element in data reduction systems and for measuring strain, pressure, temperature, and motion.

The 310 A with 318 amplifier will connect directly to the new Hewlett Packard Model 560 A Printer giving *Five Complete* Readings per sec.

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FOR ADDITIONAL INFORMATION WRITE TO DEPT.310

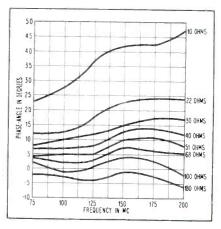


Franklin Electronics, Inc.

BRIDGEPORT, PA.

Electronic & Nuclear Development & Manufacturing used as substitution elements in CI meters are unsatisfactory because of the reactive effects that may introduce appreciable error in frequency and resistance measurements. In addition, the use of fixed resistors requires interpolation between successive resistances for most crystal parameter measurements.

To overcome the limitations of fixed resistors, a series of vhf rheostats has been developed that minimize the reactive effects and being continuously variable eliminate the



[FIG. 1—Characteristic curves of a commercial resistor

necessity of interpolation. With these rheostats, satisfactory CI meter operation has been obtained up to 200 mc, indicating suitability for other similar vhf applications.

The acceptable phase-angle tolerance for resistors used in the CI meter was established in terms of the Q and the frequency tolerance of the crystal unit to be measured. substitution resistance method of determining the equivalent electrical parameters of a quartz crystal, various resistors are substituted for the crystal in an oscillator until a resistor is obtained that gives the same frequency of oscillation and the same oscillator grid current as the crystal.

Under these conditions, the crystal and resistor appears essentially the same to the oscillator. Since the resistor may have a non-zero phase-angle, the crystal will also be operating at a phase-angle other than zero. The maximum phase-



for combination navigation and automatic pilot systems in airliners • for inertial guidance systems in guided missiles • for inertial navigation systems in military aircraft



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ALL THE DETAILS? Write for data file 124A.

Beckman Helipot

Newport Beach, California A division of Beckman Instruments, Inc. Engineering representatives in principal cities angle that can be tolerated before unacceptable errors are introduced may be determined from the expression for the phase-angle of the impedance of a series resonant circuit.

For an assumed crystal Q of 10,000 and an established frequency tolerance of 0.001 percent, resistors or rheostats exhibiting phaseangles of $\pm\,11$ deg or less may be considered satisfactory as substitution elements for quartz crystals in CI meters.

Of the resistors tested, the commercial units for which curves are shown in Fig. 1 exhibited the most satisfactory phase-angle characteristics. However, at low resistance values, the need for some form of reactive compensation is apparent since the phase-angles exceed 11 deg. Even though the low resistance values could be compensated, the necessity of interpolation further limits satisfactory utilization of fixed resistors. Consequently, efforts were directed toward the development of a suitable variable resistor

The phase-angle characteristics of resistors are primarily deter-

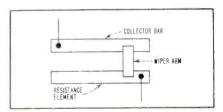


FIG. 2—Method of maintaining constant path 14.191k.

mined by the stray inductive and capacitive reactances associated with the resistive element. In variable units, the additional problem of varying reactance is encount-

In any satisfactory low-phaseangle variable unit it is desirable that these reactances be minimized and furthermore be maintained constant throughout the resistance range. A constant electrical path length is required if the effect of varying inductance with resistance setting is to be overcome. Figure 2 shows a method of maintaining a constant electrical path length.

An experimental model vhf rheo-

RIGHT



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Engineering representatives in principal cities

MICRO-BEARING **ABSTRACTS**

hu A N DANIFIS President New Hampshire Ball Bearings, Inc.

DYNAMIC AND STATIC LOAD RATINGS

Load ratings of MICRO bearings are based on standards established by the Anti-Friction Bearing Manufacturers Association and are the result of ex-

tensive tests.

The "life" of an individual bearing is defined as the number of revolutions the bearing makes before the first evidence of fatigue develops. Fatigue, in turn, is a function of bearing load and although other factors, such as contamination and high temperature, affect the life of a bearing, it is assumed that clean bearings running at normal temperatures are being considered.

It is not possible to predict the life of any individual bearing. The problem, therefore, is best approached by a consideration of empirically derived dispersion curves which provide a means of determining bearing life on a probability basis. That is, they per-mit the average life of a given group of bearings to be accurately specified.

For purposes of standardization, the "rating life" of a group of apparently identical ball bearings is defined as the number of revolutions that 90% of the group will complete or exceed before the first evidence of fatigue develops. This figure is approximately one-fifth of the average life.

. If two groups of similar bearings are run under different loads F_1 and F_2 within normal operating range of loading and rpm, their lives L1 and L2 are inversely proportional to the cubes of the loads, i.e., The BASIC LOAD RAT-ING C is that radial load which a group of apparently identical bearings can endure for a rating life of one million revolutions, with stationary load and rotating inner ring. Within normal operating ranges, rating life for any load is a constant number of revolutions, so the following relationship, a restatement of the inverse cube pro-portion, may be used to compute rating life when basic load rating and applied radial load are known:

$$L = \left(\frac{C}{P}\right)^3$$

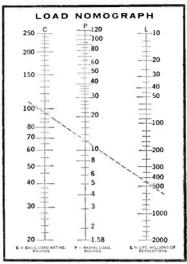
L=rating life in millions of revolutions where, C=basic load rating in pounds P=applied radial load in pounds

The nomograph illustrated permits the quick evaluation of any one of the three quantities when the other two are known. For example, if the C rating of a given bearing is 95 pounds, and the bearing is loaded radially with

Flanged Plain







12 pounds, P, a straight edge crossing these two values in their respective columns shows that the bearing could be expected to have a life, L, of 450 million revolutions.

"EQUIVALENT LOAD"

Bearings whose loads are primarily radial are usually also subjected to axial forces. When the axial component of the load is greater than a negligible value, this combined radial and thrust load may be expressed in terms of a simple radial load in order that the basic load rating C may be calculated. This simple radial load is known as the "equivalent load", which is that constant stationary radial load which, if applied to a rotating inner ring, would give the same life as that which the bearing will attain under the ac-

tual conditions of load and rotation.

A formula for determining "equivalent load" and a more comprehensive discussion of static and dynamic loads is found in our design handbook.

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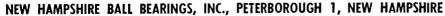


Plain and Shielded

Flanged and Shielded







District Offices: Pasadena, Calif., Park Ridge, Ill., and Great Neck, N. Y.

stat incorporating the features mentioned above is shown in Fig. 3. Basically, the rheostat consists of a resistance element, a collector bar, and a wiper arm. The metal film resistance element was fabricated by sputtering a nickel film on a glass base. The collector bar is solid copper.



FIG. 3-Experimental vhf rheostat

The resistance element and collector, spaced approximately &-in. apart, are attached to the base of the holder. The wiper arm, made of spring bronze, is attached to the carriage, which is positioned to the desired resistance setting by the leadscrew.

Except for minor difficulties the vhf rheostats have been satisfactory as experimental models. Several units were troublesome because of deterioration of the nickel resistance film, which is sensitive to corrosion. Metals of the platinum family, which are less sensitive to corrosion, have been used as substitutes for nickel. Osmium, a member of this family, is extremely hard and appears to be adherent to glass.

Satisfactory operation has been obtained with several units using osmium. Erratic operation was also caused by the rigidity of the wiper arm and imperfections in the surface of the glass. Improvements have been realized through modification of the wiper arm by slotting each finger. This makes a more flexible unit that follows small imperfections in the surfaces of the resistance and collector elements. Several resistance elements using etched glass as a base for the metal film appeared to give improved operation.

Although the vhf rheostat is com-



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Automatic Ranges...0.0001 to 999.9 volts covered in four ranges.

Accuracy...0.01% or 1 digit, whichever is larger.

Counting Rate...30 counts per second, providing average balance (reading) time of 1 second, maximum balance time of less than 2 seconds.

Reference Voltage...Chopper-stabilized supply, referenced to an unsaturated mercury-cadmium standard cell.

Input Impedance...10 megohms, all ranges.

Output...Visual display, plus print control.

Automatic print impulse when meter assumes balance.

No accessories required to drive parallel input printers.

Input...115 volt, 60 cycle, single phase, approximately 75VA.

Dimensions...Control unit, $5\frac{1}{4}$ " high x 19" wide x 16" deep. Readout display, $3\frac{1}{2}$ " high x 19" wide x 9" deep.

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FIJ. 4—Measured and calculated phase angles of whi rheostat

parable to fixed resistors, resistance values below approximately 100 ohms require some form of reactance compensation to reduce the phase-angle to less than 11 deg for CI meter applications.

From data collected it seems reasonable to assume that, for low resistance values, the rheostat may be equivalent to a variable resistance in series with a constant inductance. Figure 4 compares measured and calculated values. A value of 0.013 microhenrys fits the actual vhf rheostat data very closely. Series compensation of the rheostat was accomplished with fixed capacitors.

Since the vhf rheostat may be used in circuits in which both terminals are above ground, it is appropriate to determine some indication as to the magnitude of the distributed capacitance existing between the rheostat and the ground plans upon which it may be

Table I—T-Network Equivalent Distributed Capacitance Rheostat and Ground

	B = 100 ohms B	R = 60 ohms
Fre-	Com-	Com-
quency	pensated	pensated
în mc	$C = 500 \mu f$	$C = 91 \mu f$
75	2.66	2.85
100	2.45	2.56
125	2.44	2.83
150	2.62	2.77
175	2.63	2.88
200	2.83	2.98

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Input Impedance:	0.5 megohm and 50 mmf.
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Stability:	Short Term: 1 part in 1,000,000
	Long Term: 5 parts per million per week
Time Bases:	0.001 to 10 seconds in 1 millisecond steps
	0.0001 to 1 second in 0.1 millisecond steps
	(0.0001 to 10 sec. in 0.1 millisec. steps,
	0.001 to 100 sec. in 1 millisec. steps optional)
Read-Out:	Direct. Four digits. (Five digits optional)
Display Time:	Automatic: Continuously variable, 0.1 to 10 sec.
	Manual: Until reset
Power Requirements:	117 volts ± 10%, 50-60 cycles, 250 wotts (50-400 cycles optional)
Dimensions:	17" W x 83/4" H x 131/2" D
Weight:	35 lbs. net.
Finish:	Panel: Light grey baked enamel
	Case: Dark grey baked enamel
	Data Subject to Change Without Notice

*Model FL Flow Pickup: Courtesy-Wough Engineering Co., Van Nuys, Calif.

Computer-Measurements Corporation

5528 Vineland Avenue, North Hollywood, Calif. Dept. 78-P

mounted. Measurements and subsequent calculations of this capacitance were performed on several of the compensated rheostats with various resistance settings and over the frequency range of 75 to 200 mc. Representative results of these measurements are shown in Table I.

In general, the phase-angles of all the open-circuit measurements were close to 90 deg. Therefore, except for extremely high frequencies, the reactance of C is very large when compared to R.

The development from which this report was abstracted was supported by the Signal Corps Engineering Laboratories under Contract No. DA-36-039-sc-56730.

Sweep Testing Thyratron Characteristics

By J. G. WEISSMAN

Sylvania Electric Products, Inc. Kew Gardens, N. Y.

A CONVENIENT method for determining the firing characteristics of thyratrons is shown in Fig. 1. Direct measurement of thyratron critical grid voltage and indication of surge voltage and peak currents is obtained as well as any anomalies

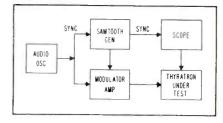


FIG. 1—Setup for sweep testing thyratron firing characteristics with which critical grid and surge voltages and peak and pre-breakdown currents can be determined

that may exist, such as pre-break-down currents.

► Concept—The method, in brief, consists of modulating a low-frequency sine-wave carrier with a sawtooth wave. The resulting output wave, shown in Fig. 2, provides sine waves ranging linearly in amplitude from zero to some pre-set

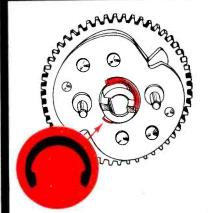
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Waldes Truarc Rings speed assembly, facilitate maintenance, improve performance of new automatic calculator



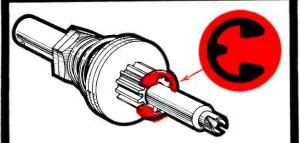
THE NEW MARCHANT DECI . MAGIC

automatic-decimals calculator made by Marchant Calculators, Inc., Oakland, California.



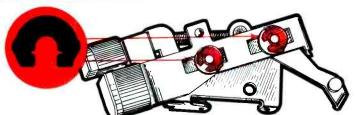
CRESCENT RING SPEEDS ASSEMBLY, DISASSEMBLY

Main clutch utilizes radiallyinstalled series 5103 crescent ring for rapid assembly and disassembly. Ring's low protruding shoulder provides necessary clearance between ring and the two studs. The main clutch operates each time a Deci-Magic control key is depressed.



E-RING SECURES PARTS AGAINST SPRING

THRUST. Slip clutch assembly uses Truarc series 5133 E-ring to hold parts on shaft. Functioning of the assembly is dependent upon the ring's ability to withstand thrust exerted by the heavy barrel spring.



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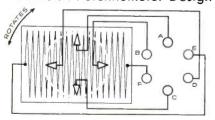
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*Described in full in Radiation Laboratory Handbook, Vol. 17.

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PRECISION POTENTIOMETER DIVISION

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peak value. This signal, when applied to the grid of a thyratron already biased back to prevent selffiring, will cause the tube to fire when the net value of the negative d-c bias and the positive-going peak of the applied carrier is equal to the strike voltage of that particular tube. By observing the plate wave-

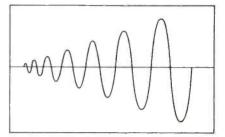


FIG. 2—Triggering waveform applied to thyratron under test

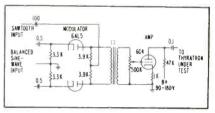


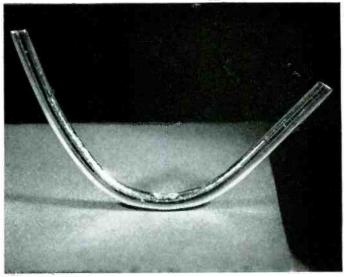
FIG. 3—Modulator-amplifier circuit. Modulates low-frequency sine-wave carrier with sawtooth wave to produce the triggering waveform shown in Fig. 2

forms on an oscilloscope whose horizontal sweep has been calibrated in terms of net grid voltage, the grid firing voltage can be read directly.

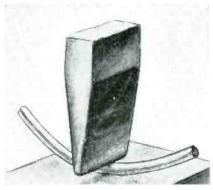
► Circuits—A balanced carrier frequency, as provided by the audio oscillator, is fed into a 6AL5 balanced diode modulator and 6C4 amplifier shown in Fig. 3. A sawtooth voltage source providing approximately 5-v. peak output will be sufficient for most modulation requirements. Some crossover distortion about the zero axis may be evident but this will not affect accuracy of the system.

The choice of carrier frequency is governed primarily by the ionization and deionization times of the particular thyratron. Frequencies lower than 500 cps are suitable for most thyratrons. A 400-cps carrier modulated by an 8-cps sawtooth is a convenient combination providing 50 positive-going peaks per sweep period. If this sweep is spread over the 10-centimeter use-

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Wire bonded to germanium by thermo-compression technique (enlarged). Wires only 1/10 the breadth of a human hair have been successfully anchored to germanium wafers only three hairs thick. The bond may be an ohmic contact or rectifying contact by adding suitable impurities to the wire and the semiconductor.



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At Bell Labs Howard Christensen and Orson Anderson discuss their discovery of new bonding principle with Peter Andreatch, Jr., who collaborated in the studies.

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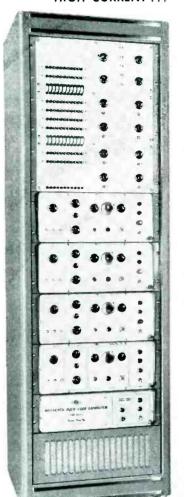
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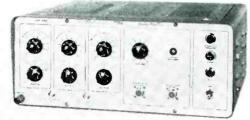
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ful face length of a standard 5-inch oscilloscope, calibration is simplified.

A typical thyratron test circuit is shown in Fig. 4. The circuit constants shown would be applicable for testing a Type 5643 tube. The externally applied grid bias of -5 volts is sufficient to prevent the tube from self-firing with the 1-megohm grid resistor. The high value of plate load resistor is required to extinguish the tube once it has fired. The exact value of this plate-dropping resistor will depend on the plate supply voltage being used.

A convenient oscilloscope calibration is shown in Fig. 5A. Here the maximum peak-to-peak value of the input signal from the modulator-amplifier has been set to 10 volts, (5-v positive and 5-v negative about

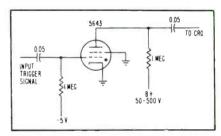
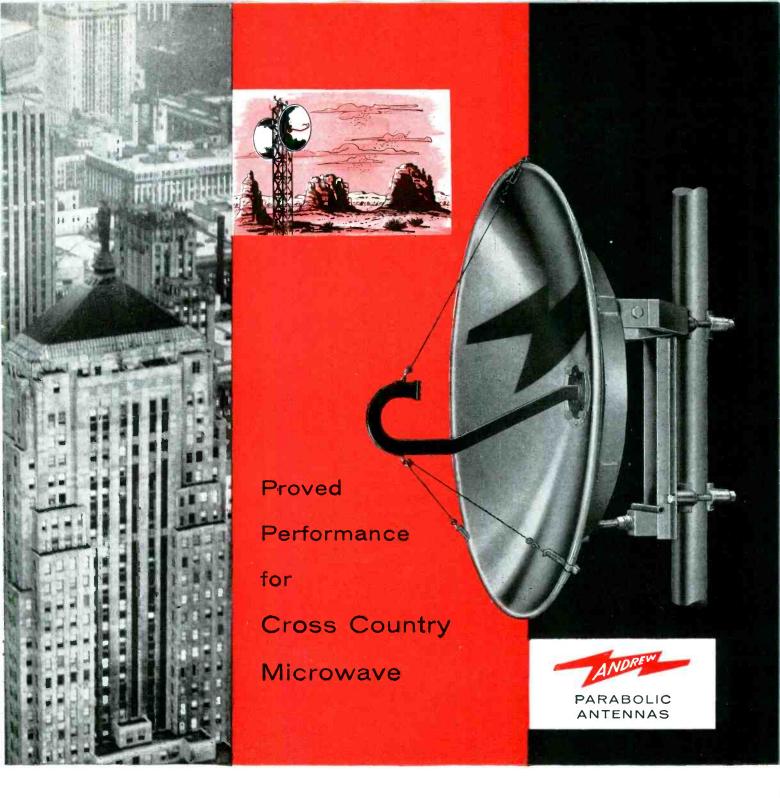


FIG. 4—Typical thyratron test circuit for type 5643 subminiature thyratron

the zero axis). Thus, the positivegoing peaks of the sine-wave carrier will vary from 0 to +5 volts during each sweep of the modulating sawtooth wave. The actual voltage appearing at the grid of the tube at any instant will be the sum of the externally applied -5 volts d-c bias and the value of the positive-going peak of the carrier at that instant. Thus, the net voltage actually appearing at the control grid will be varying from -5 volts to 0 volts for each sweep period and the time axis of the oscilloscope can be calibrated in terms of net grid voltage.

When this net value of grid voltage reaches the strike voltage of the tube, for example, -2.2 volts, the tube will fire and draw plate current. Plate voltage will then drop, because of the high value of plate load resistor, causing the tube to extinguish. The next positive-going peak of the applied input sig-



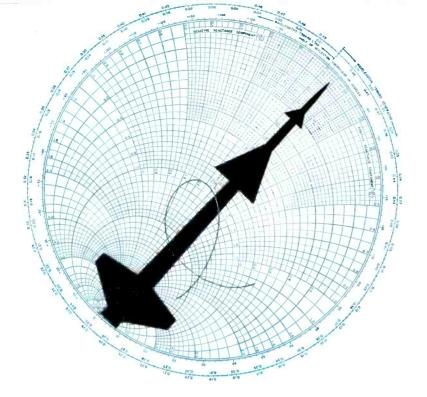
This busy metropolitan area is the termination of over 1000 miles of microwave systems, providing reliable communications across town and country for the Western Union Telegraph Company Andrew's experience in research, development and manufacturing is the reason why the dependable performance of an Andrew PS8-37, eight-foot Parabolic antenna was selected for this installation.

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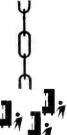
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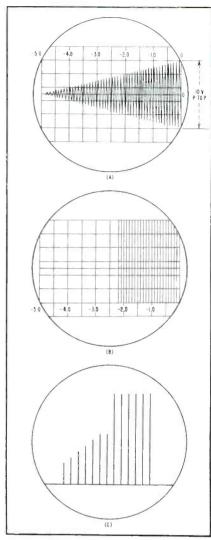
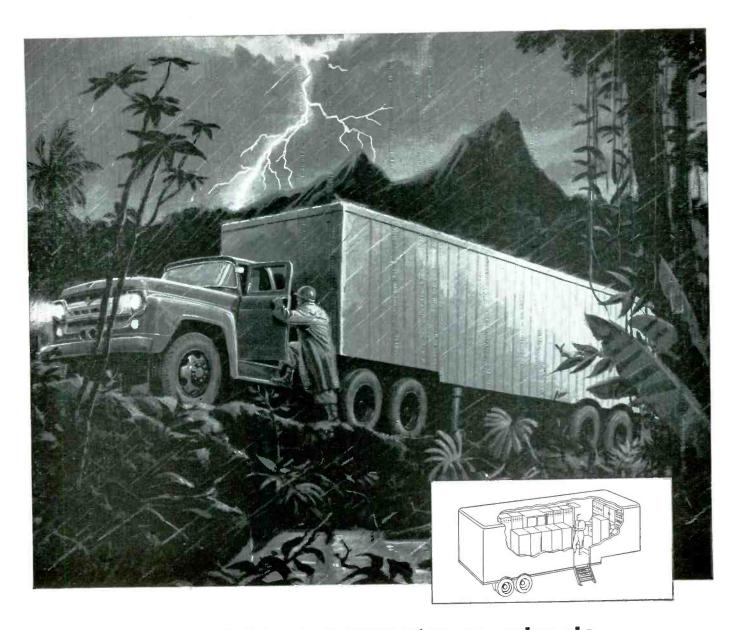


FIG. 5-Waveshapes obtained on oscilloscope during sweep testing of thyratron characteristics. Scope is shown calibrated for measuring strike voltage when input triggering signal (A) to the thyratron is set at 10 volts, peak-to-peak. Strike voltage (B) is -2.2 v. Pre-breakdown currents, indicating incomplete firing (C) can also be determined

nal will again cause the tube to fire and then extinguish. The plate waveform will appear as shown in Fig. 5B. Since the horizontal sweep of the oscilloscope is still calibrated in terms of net grid voltage, the position of the first plate voltage pulse indicates the strike voltage of the particular tube.

From the amplitude of the plate pulse such quantities as surge voltage and peak currents can be determined. The existence of appreciable pre-breakdown currents indicating incomplete firing will be evident if a display such as shown in Fig. 5C is obtained.



Rugged and right—a computer on wheels MOBIDIC'S getting ready to roll anywhere

Today's demands for fast handling of information and split-second decisions have made computers an integral part of many fixed-based operations. But why not provide these same advantages to army headquarters in the field—where speed is more important than ever before?

This is the problem the U. S. Army Signal Engineering Laboratories and Sylvania are solving together by the development of Mobidic—a general purpose mobile digital computer designed to handle the Army's data processing problems in the field and ruggedized to travel over the roughest terrain through the

most difficult temperature extremes.

Mounted in a 26-foot trailer, and ready to roll at any time, Mobidic will be available wherever decisions are made, to receive and process information from forward and rear locations, to provide up-to-the-second information to administrative and tactical staffs. Hundreds of details such as unit strengths, firepower, supply and vehicle availability, and field intelligence will become readily available to decision-making staff officers through Mobidic.

MOBIDIC's list of skills includes processing of logistical and intelligence in-

formation as well as analytical and real-time computation.

MOBIDIC is another example of Sylvania's integrated approach to systems engineering and close cooperation with the Armed Services. From concept to production, Sylvania's engineering talents and manufacturing facilities are ready for any challenge. If your project requires this kind of capability, Sylvania engineers will be glad to discuss it with you. For information on the capabilities of Sylvania's Electronic Systems Division, write for free booklet titled, "A Digest of Specific Capabilities."

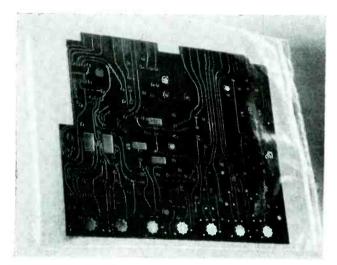


Sylvania Electric Products Inc. Electronic Systems Division 100 First Avenue, Waltham, Massachusetts

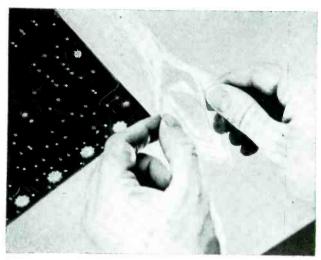
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Production Techniques

Transparent Polyethylene Bags Protect Printed Circuits



Printed wiring board can be inspected while in bag yet is protected from moisture, dirt and scratches during handling



Special pressure-grip closure for bags is sealed by thumb pressure but can easily be opened as shown

To PROTECT delicate printed circuits used in advanced electronic devices from shipping and handling damage, Photocircuits Corp. is packaging them in specially designed film bags made of Bakelite polyethylene. The polyethylene film bags, which are furnished with a

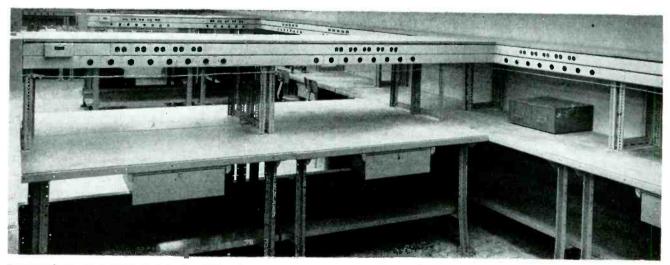
special dustproof and waterproof pressure closure, protect the parts from scarring during stacking and shipment yet permit visual inspection. They also keep out moisture and dirt during storage.

Standard bag sizes as made by Kennedy Car Liner and Bag Company, Inc., Shelbyville, Ind. are 3 by 6 inches and 8 by 11 inches, using 0.004 inch film. The special closure (supplied by Flexgrip, Inc.) seals with thumb pressure and can be easily opened when the part is needed. The bags are reusable.

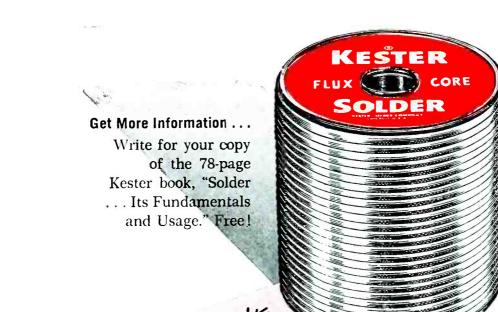
Lab Benches Have Outlets For Three Power Services

Power requirements for lab benches are solved at GE's Advanced Electronics Center in Ithaca, N. Y. by designing each bench as a self-contained and independent unit that can be taken

down, relocated and set up in a minimum of time. Wiring is an integral part of each bench, so mov-



Engineer-designed benches have power outlets arranged in convenient raceways. Square duct at left on bench holds power leads going up to main duct on ceiling



1 16 513 de 18 51 de

KESTERSOLDER

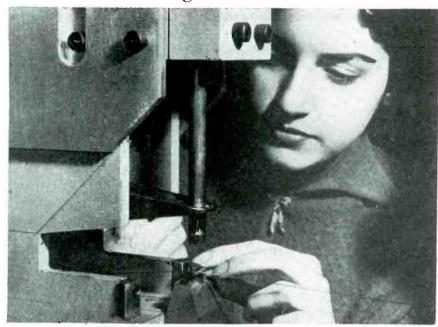
4204 Wrightwood Avenue • Chicago 39, Illinois Newark 5, New Jersey • Brantford, Canada ing merely involves reconnecting to power sources.

Necessary versatility is achieved with multiple runs of Wiremold 3000, a raceway system. The benches have the outlets mounted above the work surface in two runs to provide three standard voltages, with a fourth being added where necessary.

The top run has 115-v single-phase, three-wire service with grounded receptacles, controlled by a 20-amp circuit breaker. The bottom row has 400-cps, three-phase, 220-v service on four-prong receptacles, alternating in the same raceway with 28-v d-c receptacles. Two 30-amp breakers mounted on the end panel of the bench control these two services.

Power is brought from the outside to a power room on each floor. From there it is carried through metal ducts to distribution panels in each laboratory. From the panels, square ducts take it to the benches where it is carried through Wiremold to the outlets. Constancy of power to the center section of each bench is regulated by a Variac. The side sections are on line voltage.

Ultrasonic Welding Joins Foil to Wires



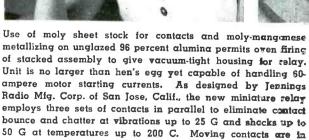
Joining aluminum foil to copper foil with ultrasonic welding unit at General Engineering Labs of American Machine and Foundry Co.

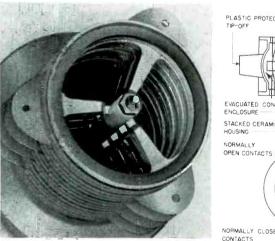
SOLID STATE BONDS with deformations only a fraction of those of pressure welding, usually without heat, can now be achieved reliably with ultrasonic welding. Since there is no current passing through the joint, there is no

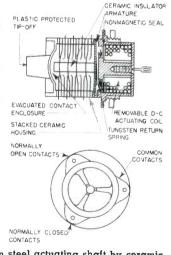
arcing, spitting or sputtering. Extremely thin electrical conductors of foil dimensions can be joined to members of similar or much heavier thicknesses, as well as to wire of the same or different composition. In many cases in-

Design of the Month: CERAMIC VACUUM RELAY









center of relay, insulated from steel actuating shaft by ceramic bushings. At bottom of shaft is iron armature, actuated through nonmagnetic seal by coil outside vacuum chamber. Coil is anchored by one screw, permitting easy replacement. Inherently clean contact surfaces in high vacuum also provide positive insurance of dry-circuit conductivity, so that contact resistance is low for microampere currents even after years of shelf life as required in stockpile missiles. Plastic cap covers razor-sharp edge of exhaust tip-off

New Sperry Reflex Oscillator Klystron



COVERS A BAND

Low-Voltage Test Oscillator Spans 21% of Center Frequency

Featuring complete coverage of the frequency range from 8.5 to 10.5 kmc, the new SRX-92 reflex oscillator klystron is designed for use as a local oscillator in microwave receivers and spectrum analyzers, as a signal source in radar test equipment, or as a low-power bench oscillator.

Low-voltage operation, low hysteresis and high thermal stability are other important advantages of this new klystron, which delivers a minimum output power of 20 mw over a minimum bandwidth of 35 mc. In addition, it offers single-screw tuning over the entire frequency range, with integral cavity and tuner.

Sperry has packaged all these key features in a klystron that combines low cost and small size—it weighs only 4½ ounces. For detailed information on the SRX-92 and other Sperry klystron tubes, write or phone the nearest Sperry district office.



DIVISION OF SPERRY RAND CORPORATION

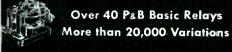
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structure provides at least twice the contact pressure found in relays of comparable size. This extra force accounts for the extremely high shock and vibration resistance shown in the specifications.

SL LATCHING TYPE - Unique magnetic latch assures positioning of armature and exceptional pressure. A 1 watt, 3 ms. pulse to either coil transfers contacts. Transfer time is only 0.5 ms. Coils are designed for continuous duty. Has the same exceptional shock and vibration characteristics as the SC.

POTTER & BRUMFIELD, INC., PRINCETON, INDIANA/SUBSIDIARY OF AMERICAN MACHINE & FOUNDRY COMPANY







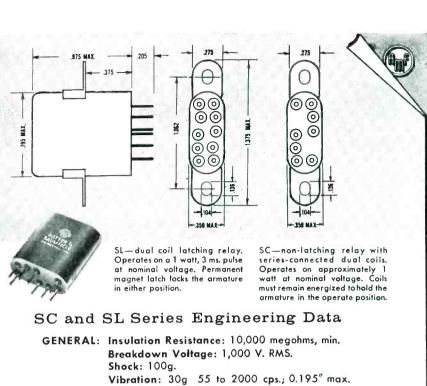












excursions from 10-55 cps.

Temperature Range: -65° C. to $+125^{\circ}$ C.

Weight: 17.5 grams (5/8 oz.).

Operate Time: 3 MS, max, with 550 ohm coil @ 24 V. DC. (SL: 630 ohm coil at 24 V. DC).

Transfer Time: 0.5 MS max.

Terminals: (1) Plug-in for microminiature recep-

tacle of printed circuit board.

(2) Hook end solder for one #20 AWG wire.

Enclosure: Hermetically sealed.

CONTACTS: Arrangement: 2 Form C.

Material: Gold flashed palladium.

Load: 2 amps @ 28 V. DC, resistive; 1 amp

@ 115 V. AC, resistive.

Pressure: SC-13 grams min.; SL-16 grams min,

COIL: Power: Approx. 1.0 watt at Nominal Voltage.

Resistance: SL-40 to 1400 ohms; SC-35 to

1250 ohms.

Duty: Continuous.

MOUNTINGS: Bracket, stud and plug-in.

P&B STANDARD RELAYS ARE AVAILABLE AT YOUR LOCAL ELECTRONIC, ELECTRICAL AND REFRIGERATION DISTRIBUTORS

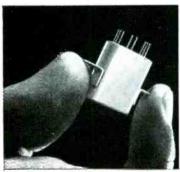
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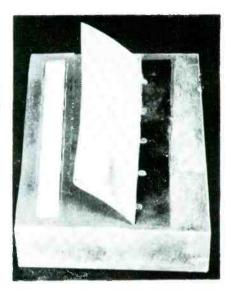


Potter & Brumfield, Inc., Princeton, Indiana Attn: T. B. White, Brig. Gen. USMC (Ret.) Special Projects Engineer

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See our catalog in Sweet's Product Design File



Aluminum foil only 0.001 in. is here ultrasonically welded to 1-in. aluminum plate

sulated sheet or foil can be welded without prestripping. Also, it is of use in joining foil or fine wire of copper or aluminum to wire, sheet, tube or plate material.

► Welding Foil Coils—One of the principal factors that has restricted the acceptance of foil for coils is the problem of making sound connection between the aluminum and the copper leads. Aluminum is difficult to solder, and resistance welding will often burn through the foil. Ultrasonic welding is one of the most promising methods here.

Aluminum foil as thin as 0.00015 in. can be welded readily to wire, other foil or other members. Relative thickness of the parts being joined is no problem; 1-mil foil can easily be welded to a 1-inch aluminum plate. The strength of ultrasonic welds in aluminum compares favorably with that of other methods, including high-pressure Ultrasonic welds cause no crystal growth, hence there are no brittle bonds to give early failure from fatigue.

▶ Power Needed — Another desirable feature of ultrasonic welding is the lower power requirement. For example, to join two pieces of re-in. aluminum sheet by resistance welding would require a machine of about 75-kva capacity. An ultrasonic machine using 31 to 4 kva will do the same job. The



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Unique Balanced-Armature Relays meet all requirements of the most exacting operating environments — shock, acceleration, vibration and high temperatures.

In the Leach Balanced-Armature Relay, shock and vibration forces cannot move the relay armature. This eliminates faulty operation of contacts during extreme vibration and acceleration.

These Leach Relays meet or exceed requirements of MIL-R-5757, MIL-R-6106, MIL-E-5272. Typical ratings include: vibration, 20 G's to 500 cps (higher ratings available); shock and acceleration, more than 50 G's; temperature, -50° to +125°C; life, 50,000 continuous operations minimum at rated load; available 28 vac, 115 vac, 400 cps operation. At right is Leach 9226, 1.49x1.49x 1.68 inches.



Leach has gained a unique reputation for creating reliable relays, *custom-tailored* to solve specific circuitry problems. Write for your copy of the Leach Balanced Armature Relay Catalog.



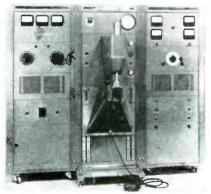


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latter can be plugged into almost any standard 220-v factory power line and is semiportable. The welding head can be 50 to 100 ft from the electronic apparatus. By contrast, the resistance welder requires special heavy bus bar installation and will be a relatively cumbersome unit to move to a new location.

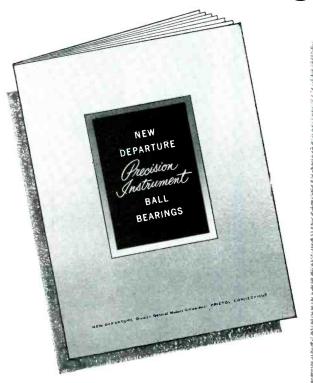
- ▶ Welding Procedure Ultrasonic welds are made by clamping the pieces to be joined with a force of from 10 to 400 lb, and simultaneously introducing vibratory energy at the point of pressure. This high-frequency mechanical energy passes into the metal parts, breaking up the interface between them. In a brief interval, generally under 2 sec, a solid-state metallurgical bond is produced with external deformations that are usually less than 5 percent.
- ► Transducer The ultrasonic transducer usually consists of a stack of nickel laminations wound with insulated wire. Nickel as supplied by International Nickel Co. gives the largest possible magnetostrictive effect of any commercially available material. Also, it affords a rugged construction that is durable, resistant to elevated temperatures and corrosion, and readily fabricated. Nickel is particularly useful at high power levels.
- ► Generators—Alternating current is supplied to the transducer by a



Ultrasonic unit for spot-welding applications, powered by 2,000 r-f watt ultrasonic generator made by Sonobond Corp., West Chester, Pa. Its rugged laminatednickel-stack transducer will handle aluminum up to 0.050 in. thick



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Inch and Metric Series Equivalents

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To meet the requirements for lighter, smaller and more powerful auxiliary gasoline-engine-driven generators for both rotary and fixed wing aircraft, Homelite has designed and built several special units.

Typical of these new Homelite generators is the Model 34D28 shown above.

Weighing only 67 pounds...almost half the weight of previous auxiliaries with comparable power...this Homelite develops 70 amperes at 28.5 volts DC and is capable of starting 700 h.p. aircraft engines either directly or with a small battery floated on the line.

Requiring less than 3 cubic feet of storage space, this unit is equipped for push button or manual starting and starts without preheating in temperatures as low as minus 40 degrees Fahrenheit.

Meeting specifications for lightweight, powerful generators... for both military and commercial applications... is the specialty of the house with Homelite. We've been doing it for close to half a century.

No matter how new, how different or how tough your requirements . . .

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Chain Saws

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power oscillator at the design frequency of the transducer and coupling system. Depending upon the characteristics of the system, this will generally range from 4 to 60



Portable Aeroprojects Sonoweld unit being used for welding thin materials such as foil and fine wire. Power supply at rear is 300 r-f watt ultrasonic generator operating from 117-y a-c line

kc. Units delivering up to 4 kw are in everyday laboratory use and even heavier equipment is in development.

A light-weight and extremely portable ultrasonic welding unit is now available for welding thin materials, such as foil and fine wire. It is powered by a 300-watt ultrasonic generator which operates from a 117-v a-c line and will handle thicknesses up to 0.012 in. of aluminum or up to 0.005 in. of copper.

Soldering Aluminum Without Fluxing

SIMPLE AND EFFECTIVE techniques for soldering aluminum and its alloys as well as galvanized metals have been developed by G. M. Bouton and P. R. White, metallurgists at Bell Telephone Laboratories. These techniques employ an inexpensive and stable zinc-base alloy as a preferred solder. No flux or vigorous abrasion is necessary. Joints in aluminum made by these methods are stronger than commercial aluminum itself. The tech-

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supervisory control systems





Westinghouse VISICODE supervisory control systems employ "all-relay" terminal equipment developed to provide remote control and supervision of unattended substations of electric utility systems, hydroelectric generating stations, water supply systems, gas and petroleum pipelines and similar applications.

Quoting Westinghouse Descriptive Bulletin 32-450, "Standard telephone-type relays are used because of their extreme simplicity and maximum dependability. The reliability of this relay is demonstrated by the fact that the original installation, made by Westinghouse in 1921 using this relay, is still in continuous service."

The key to any "all-relay" system is the reliability of the basic relay component. For the ultimate in dependability, Westinghouse uses North relays!

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After heating uncleaned aluminum with ordinary torch, just a wiping stroke with stick of new zinc-base alloy solder is enough to give perfect tinning



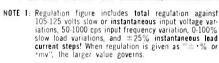
Bright central area is new zinc-base solder (magnified about 15 times) on sheet of commercial-grade aluminum. Around central spot is dark area in which solder has crept under oxide layer and alloyed with alumium surface

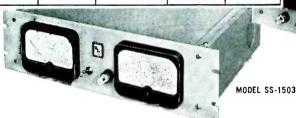
nique is most effective for joints where the surfaces are accessible for manipulation with the solder stick, such as butt and T joints.

Long-term stability of the soldered joint is assured by rigid exclusion of deleterious elements such as lead, tin, bismuth and cadmium from the zinc-base alloy to prevent integranular corrosion. About 0.05 percent of magnesium may be added to enhance its stability, and from 2 to 8 percent of

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MODEL	OUTF	·UT	RIPPLE	REGULATION (SEE NOTE 1)	INTERNAL IMPEDANCE DC - 100KC	PANEL HEIGHT (SEE NOTE 2)	DELIVERY	PRICE (INCLUDING METERS)
	VOLTS	AMPS	RMS Millivolts		OHMS	INCHES	DAYS	
SS-7-15	0-7	0-15	1.0	±0.1% or 3 MV	0.005	31/2	75	\$ 880
SS-10-10	0-10	0-10	1.0	±0.1% or 5 MV	0.02	31/2	75	700
SS-32-3	0-32	0-3	1.0	$\pm 0.1\%$ or 10 MV	0.10	51/4	45	600
SS-32-10	0-32	0-10	1.0	$\pm 0.1\%$ or 10 MV	0.04	83/4	45	790
SS-32-20	0-32	0-20	1.0	$\pm 0.1\%$ or $10~\text{MV}$	0.02	121/4	45	1100
SS-1003	50-100	0-1.5	1.0	±0.1%	0.03	51/4	30	490
SS-1503	100-150	0-1.5	1.0	±0.1%	0.06	51/4	10	520
SS-1603	0-160	0-1.5	1.0	$\pm 0.1\%$ or 20 MV	0.50	7	15	600
SS-2003	150-200	0-1.5	1.5	±0.1%	0.10	7	30	630
SS-2503	200-250	0-1.5	1.5	±0.1%	0.15	83/4	45	720
SS-3003	250-300	0-1.5	2.0	±0.1%	0.20	101/2	60	850
SS-1505	100-150	0-3	2.0	±0.2%	0.04	101/2	75	950
SS-1605	0-160	0-3	2.0	±0.2%	0.30	121/4	75	1050





quote on custom requirements.

MODEL SS-32-3

MODEL SS-1603

The enthusiastic reception which greeted our Solid State fully transistorized power supplies encouraged us to expand our stock line, incorporating the most popular of the custom designs of the last 2 years. All designs incorporate our unique short-circuit-proof (not merely short-circuit-protected) power-transistor circuit.

If power supply size, weight, efficiency, and reliability are

important to you . . . you need N J E Solid State! We

have developed several hundred special designs (series

and shunt regulator configurations) and are prepared to

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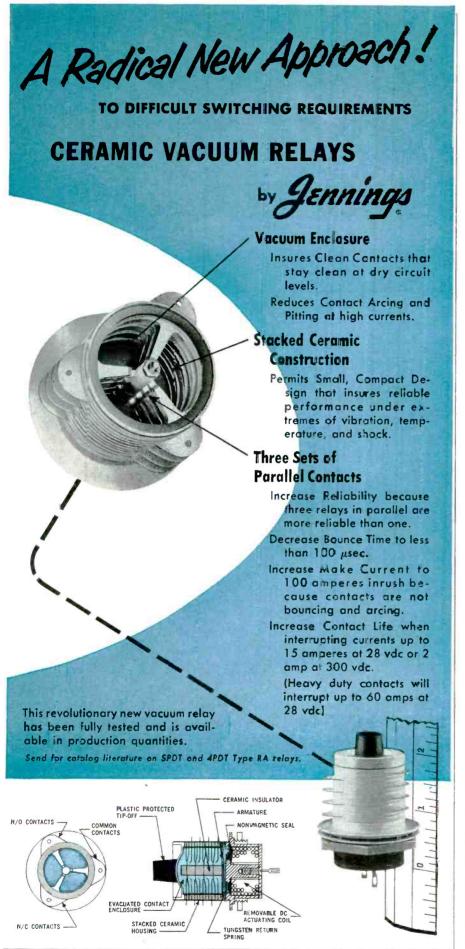
CORPORATION

Electronic Development & Manufacturing

343 CARNEGIE AVENUE KENILWORTH, NEW JERSEY

Nje

COMPETENT ENGINEERING REPRESENTATION EVERYWHERE



aluminum may be included. A commercial version of this alloy is New Jersey Zinc's Horse Head Zamac 3, available from Henning Bros. & Smith, 91 Scott Ave., Brooklyn, N. Y.

In soldering aluminum it is not necessary to remove rolling mill oils or the surface oxide from the area to be wetted. A single stroke of the solder stick across the heated aluminum surface will cause the solder to penetrate the oxide and wet the aluminum. The normally tenacious oxide film is lifted off much like paint peeling from wet wood. This raised oxide coating may then be wiped aside.

Surfaces thus wet can be joined by bringing them together while hot and adding more solder. Heat may be applied electrically or by means of torches burning common fuels. This soldering technique is equally effective for joining galvanized surfaces without a

Hot Air Jet Tests Individual Components

By LLOYD WARE and JOHN FALLON Sanders Associates, Inc. Nashua, New Hampshire

EFFECT OF HIGH TEMPERATURES on the performance of individual components is easily determined even when components are assembled in close proximity to one another, by using a fine jet of hot air as the heat



After copper tubing is wound around soldering iron, tinfoil is wrapped around to conserve heat

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HIGH QUALITY DIODES AND TRANSISTORS MUST HAVE CONSISTENTLY HIGH QUALITY WELDS

Raytheon subminiature

<u>precision welding systems</u>

provide extremely uniform

production—from the 1st to

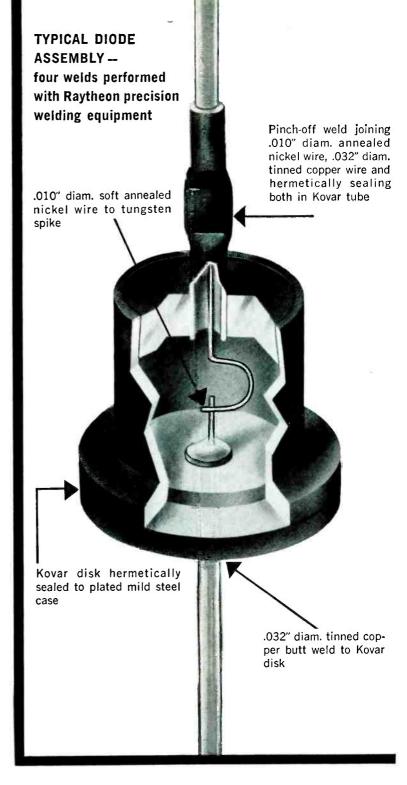
the 1,000,000th unit.

The four difficult welds shown here are being performed with Raytheon precision welding equipment at the rate of 25,000 units a day by the diode division of a major electronics manufacturer.* In addition to joining the components of these diodes, the welding also seals them hermetically. Statistical sampling of production runs consistently meets JETEC specifications for high quality welds.

Raytheon AC and DC power supplies, controls, welding heads and transformers have been proved in applications where high speed, low cost, precision welding is required. Millions of tubes, transistors, diodes, relays, instruments, capacitors and resistors have been produced with Raytheon welders—designed and produced by *electronic* engineers for use in electronic manufacture.

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*Name on request



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Commercial Equipment Division

Waltham 54, Mass.

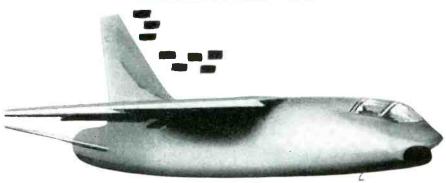
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Raytheon production equipment for the electronic industry — AC and DC welding equipment . Automatic welding systems . Magnetizers . Ultrasonic Impact Grinders

for quick look at telemetered signals jet fighter builder uses





ELECTROGRAPHS installed in the ground station provide an immediate record of 24 simultaneous air-to-ground telemetered flight parameters. Progress of the flight test is followed with virtually no delay, thus minimizing costly reruns and permitting program changes during the test sequence. The Model 420 ELECTROGRAPH is the ONLY photographic recorder suitable for truly "quicklook" applications. High contrast records visible to the abserver may be produced within ½-second after receipt of the excitation



signal . . . NO other photographic oscillograph approaches this performance. When the "quick-look" must be quick, specify the ELECTROGRAPH.

As in flight test use, most "quick-look" applications require a high degree of record readability. The high contrast of ELECTROGRAPH recordings is UNEXCELLED with the result that record readability is maximum. The black traces and timing lines embossed on light-colored, non-glare emulsion offer the optimum condition for ease of data reduction.

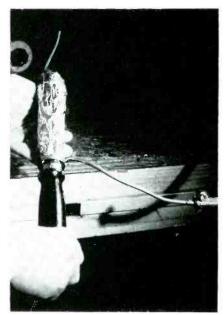
For additional details on this 24-channel recording oscillograph, you are invited to write, wire or call for bulletin CGC-311.

Century Electronics & Instruments, Inc.

1333 No. Utica, Tulsa, Oklahoma

source. This can readily be improvised from a 100-watt soldering iron, a sheet of tinfoil, about 7 feet of 3/16-inch copper tubing and a pneumatic air hose of approximately 3/16-inch inside diameter.

► Construction—First, mark off a distance of 2 to 3 inches from one end of the copper tubing and, starting at the tip of the soldering iron, wind the remainder of the tubing tightly around the iron's heating element. This will leave about 8 inches of excess tubing near the handle of the iron. Insert the free end of this excess tubing into the

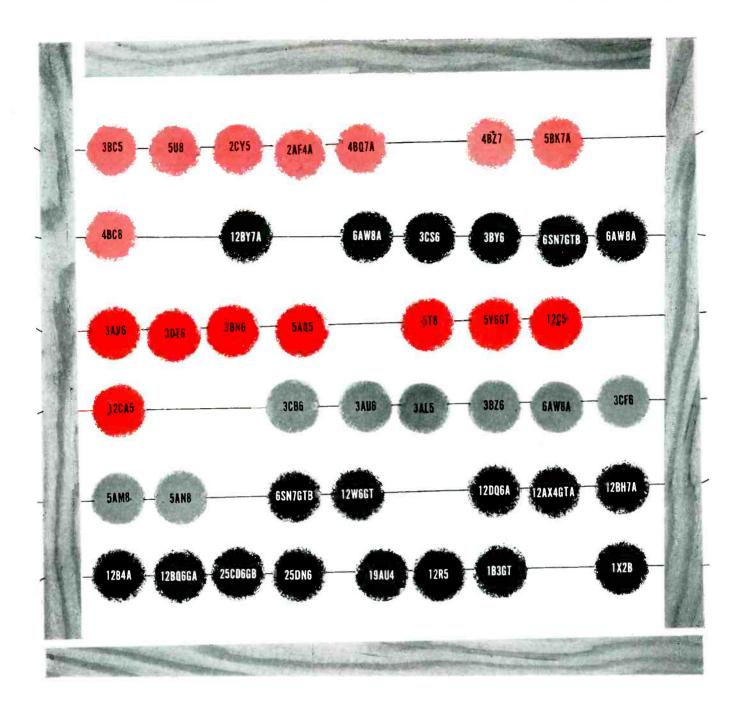


Iron ready for use, with tubing connected to compressed air line

air hose and secure the connection with a hose clamp. Since virtually no heat is transmitted at this point, there is little danger of the hose's being damaged.

Having coiled the tubing around the iron's heating element, wrap this section of the iron tightly with tinfoil to help retain the heat. The iron can now be plugged in and the air supply turned on to give a fine and easily controlled jet of hot air which can be focussed on individual components for pin-point heating.

► Use—Air temperature can be regulated by varying the heat in the iron with a Variac or large rheostat. Heating area can be controlled by adjusting the air flow with a



ANYWAY YOU ADD IT...IT'S TUNG-SOL FOR SERIES-STRING TV TUBES

Advanced designs in heater and cathode structures, which made possible controlled warm-up time, established Tung-Sol as the pioneer producer of 600 ma series-string heater tubes for TV

Tung-Sol, while continuing to add to this select circle of most widely used 600 ma types, further expanded its series-string line to include 450 and 300 ma tubes for sets requiring fewer tubes.

At present Tung-Sol supplies a complement of nearly 200 of these tubes to the initial equipment manufacturers and the replacement field . . . a

solid indication not only of the success of the series-string principle, but also of Tung-Sol's unfailing ability to meet the strictest performance requirements and production schedules.



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with

Model 316 VOLTMETER



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PRICE: \$290

SPECIFICATIONS

FREQUENCY RANGE 0.05 cps to 30KC down to 0.01 cps with corrections

VOLTAGE RANGE 0.02 to 200V peak to peak lowest reading corresponds to 7.07 my rms of a sine wave

ACCURACY 3% throughout ranges and for any point on meter scale IMPEDANCE 10 megohm by any average acceptance of 30 must

OPERATION Unaffected by line variation 100 to 130V, 50 cycle, 45 watt

FEATURES

- Pointer "flutter" is almost unnoticeable down to 0.05cps, while at 0.01cps the variation will be small compared to the sweep observed when employing the tedious technique of measuring infrasonic waves with a dc voltmeter.
- A reset switch is available for discharging "memory" circuits in order to conduct a rapid series of measurements.
- The reading stabilizes in little more than 1 period of the wave.
- Meter has a single logarithmic voltage scale and a linear decibel scale.
- Accessories are available for range extension up to 20,000 volts and down to 140 microvolts.

For further information on this and other Ballantine instruments write for our new catalog.

Ballantine Laboratories, Inc.

100 Fanny Road, Boonton, New Jersey



Using hot air jet to heat small coil deep down in chassis

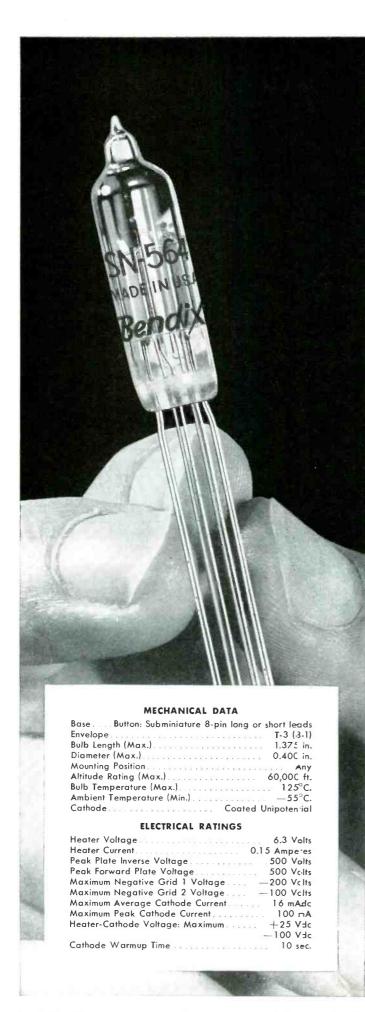
valve or by moving the air outlet toward or away from the component under observation. Component temperatures have been raised as high as 90° C using these simple techniques.

► Calibration—Initial and final temperatures of the component under observation can be determined in either of two ways, depending on the degree of refinement required. When only approximations are necessary, assume room ambient as the starting temperature and use a thermometer to measure the temperature rise. Holding the thermometer in the air blast at a fixed distance from the jet, wait until the temperature of the thermometer is stabilized, then note the temperature and the time required. If the component subsequently heated is of approximately the same size as the thermometer bulb and the distance from the air source is about the same, the component's temperature will rise to approximately the same level during an equivalent heating interval.

When the component is substantially larger than the bulb of the thermometer, more time is needed to rise its temperature an equivalent amount if the same air blast and distance are used; this, of course, may be approximated.

To make precise measurements of component temperatures, attach a thermocouple bridge to each component as it is being heated.

► Cooling—After a component has



Now available— subminiature xenon tetrode thyratron

RETMA 5643



Improved Type TD-17

APPLICATIONS: Counters, grid control rectifiers, gyro erection systems, missile systems, automatic flight control systems, and other control circuits requiring utmost degree of reliability.

ADVANTAGES: Freedom from early failure . . . long service life . . . uniform operating characteristics . . . ability to withstand severe shock and vibration.

FEATURES: Advanced mechanical and electrical design plus 100% microscopic inspection during manufacture . . . special heater-cathode construction minimizes shorts , . . 24-hour run-in tests under typical overload conditions.

The TD-17 is but one of many electron tubes designed and built by Bendix Red Bank for special-purpose applications. For full information on the TD-17, or on other tubes for other uses, write RED BANK DIVISION, BENDIX AVIATION CORPORATION, EATONTOWN, NEW JERSEY.

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Canadian Distributor:
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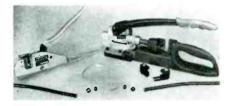
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been heated, its temperature must be lowered to room ambient before the next component is heated; otherwise, equipment performance will be influenced by the temperature variation in more than one component. A blast of cool air from a separate air line, after readings have been observed and recorded, will lower a component's temperature in

Splicing Multiconductor Shielded Cable

A NEW METHOD of splicing single and multi-conductor shielded cables, developed by Burndy Corp. of Norwalk, Conn., uses standard inexpensive parts to make compact, flexible, high-conductivity splices with



STEP 1-Crimping tools, compression connectors, ferrules and splicing braid used in making one complete splice in shielded cable shown in foreground



STEP 2-Removing insulation from cable



STEP 3-Placing inner ferrule over shield



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- HIGH PEAK INVERSE VOLTAGE 120V.
- FAST REVERSE RECOVERY 80K ohms in .3 µsec.*
- HIGH OPERATING TEMPERATURE 175° C.

 *When switching from 5 mA to 40V. RL = 2K. CL = 10 $\mu\mu$ f.

RATINGS

Maximum inverse working voltage: 100V. Average forward current: 200 mA. Maximum power dissipation: 200 mW. Latest achievement of the GI team of semiconductor specialists is this universal silicon diode 1N658. Radio Receptor's newly developed process combines in skillfully balanced proportion every desirable characteristic you've sought in silicon diodes. Result is a fully reliable component that does a better job in almost every standard application.

In addition to the 1N658, Radio Receptor offers to the industry a full range of RETMA subminiature silicon diode types to meet other applications. Full information is available upon request to Se tion E-12.

RRco. 1N658 is available now in production quantities for immediate delivery from our factory. Small quantities for testing and evaluation can be purchased from any authorized RRco. distributor and orders sent direct to Radio Receptor will be handled promptly.

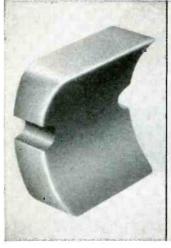


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RADIO RECEPTOR COMPANY, INC.

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General Electric permanent magnet outperforms wire-wound field in D-C tachometer generator

Improved Alnico 6 magnet increases reliability and accuracy over wide ambient temperature range.

Instruments can determine rotational speeds from 100 to 5000 rpm with an error of less than .05% — despite ambient temperatures of 20° to 50° C. Problem is that these instruments are only as accurate as the tachometer generators that supply their power.

Conventional generators use copper windings. This means they are dependent on external — and often varying — power sources. They are adversely affected by wide temperature changes. And, they are costly to repair when windings burn out.

The 46-frame D-C generator, above, gets around these difficulties by using a G-E Alnico 6 permanent magnet. Here's why:

- 1. The G-E Alnico magnet does not depend on outside excitation.
- **2.** It supplies reliably constant power.
- Exposure to varying ambient temperatures does not affect the magnet's power or dependability.
- External regulating equipment

 needed with wire-wound fields
 is eliminated by the use of Alnico magnets.
- 5. Unlike copper windings, permanent magnets never wear out.

These advantages, in themselves, were enough to make the magnet-powered generator a success.

However, with conventional Alnico 6, plastic-steel was needed between the "as-cast" surfaces of the magnet and the machined parts of the generator to cut eddy current losses, and to shield the flux. This added to the time and cost of producing the generator; made it almost impossible to disassemble for normal servicing and maintenance.

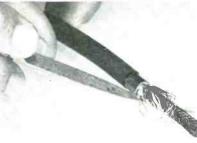
So G-E magnet engineers increased the coercive force of the Alnico 6 magnet by about 7%. The need for the plastic-steel "mud" was eliminated . . . and so were the difficulties of assembly and disassembly.

This generator is just one of the many applications where G-E magnets can outperform wire-wound fields for accuracy and reliability. And the work of G-E Magnet Engineers in improving Alnico 6 is just one of the many services they offer to designers and manufacturers of electrical products.

For more information about G-E magnet engineering services, or for your copy of the new G-E Magnet Design Manual, write: Magnetic Materials Section of General Electric Company, 7806 N. Neff St., Edmore, Michigan.

PRODUCTION TECHNIQUES

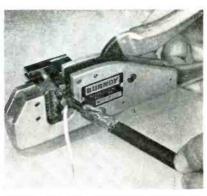
(continued)



STEP 4—Combing out excess shield length after positioning ferrule



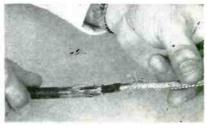
STEP 5—Strands of shield are folded back over ferrule and held in place with Scotch tape, after which inner conductors are stripped as shown in preparation for insertion in Insulink connectors



STEP 6—Insulink connector is inserted between jaws of crimping tool up to stop at rear, stripped conductor is inserted, and tool handles are closed



STEP 7-Cable with crimped links



STEP 8—Length of splicing braid is opened with pencil and pushed over links as shown

electrical and physical properties comparable to those of the cable.

Inner conductors are splices with small compression connectors. Shields are joined with a section of

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MODEL 1329

Simpson WIDE-VUE

panel instruments



MODEL 1227

MODEL 1327

....

a new concept
in styling and visibility

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The clean, graceful lines of "Wide-Vue" panel instruments add two plus values to your equipment designs. First, style—ultra-modern beauty that blends with today's streamlined panels. Second, functionalism—longer scales with wide-angle readability. The $2\frac{1}{2}$ " size, for example, has the same scale length as a conventional $3\frac{1}{2}$ " meter. Wide-Vue's durable cover is formed in one piece from clear plastic, and can be supplied with black or color (custom-built units only) finishes. DC, AC, and AC rectifier types in $2\frac{1}{2}$ ", $3\frac{1}{2}$ ", and $4\frac{1}{2}$ " sizes.

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0-1 DC MILLIAMPERES



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PUT) 10, 20, 8, 100 volte PMS

FREQUENCY (FIXED) -250 cps. to 15,000 cps. VOLTAGE (OUTPUT) $-10,\,30$ & 100 volts RMS, all with floating center-tapped output. DISTORTION -0.1% maximum harmonic content, 0.05% maximum AC hum, 0.01% maximum noise. CALIBRATION ACCURACY $-\pm0.02\%$ under usual lab ambient conditions*, checked against station WWV as a primary standard. FREQUENCY STABILITY $-\pm0.5\%$ maximum, under usual lab ambient conditions*, $\pm0.02\%$ maximum per ±10 volts variation in line voltage, $\pm0.05\%$ maximum, zero to full load. AMPLITUDE STABILITY $-\pm0.1\%$ maximum under usual lab ambient conditions*, $\pm0.02\%$ maximum, per ±10 volts variation in line voltage, $\pm0.2\%$ maximum, zero to full load.

Special models operating from other prime power sources, with higher power capacities and at other frequencies supplied to your specs in cabinet or rack styles. Write today!

*Lab ambient, 10°C to 40°C.

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Special Products Division of International Electronic Research Corporation, Burbank, California



STEP 9—Outer Hyrings are slipped over



STEP 10—Shield and splicing braid are crimped between Hyrings



STEP 11—Half of splice after removal of excess braid, shield and tape



STEP 12—Pushing splicing braid back to expose links in preparation for insertion of stripped conductors of other cable. Note staggering of splices



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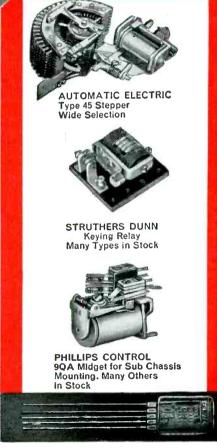
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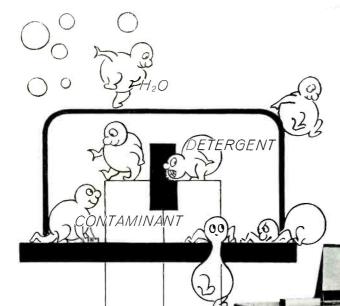
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transistor
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diode
failures
BEFORE
they
happen

Reliability of many electronic circuits has been seriously hampered due to leaking transistors . . . even though these units were carefully checked before installation. The reason often lies in the testing methods. For example, the bomb test not only has low sensitivity and other inherent inaccuracies, but also exposes the unit to chemicals which can cause latent field failure. RADIFLO leak detection eliminates these problems; is positive, fast, inexpensive and non-destructive to the sealed unit.



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ADVANTAGES OF USING RADIFLO

- 1. Test units after they are completely sealed.
- 2. Grade transistors nondestructively by leak
- Test in production quantities for less than 1c each.
- 4. Test production quantities to a sensitivity of 10-11 cc/sec.
 - 5. RADIFLO can be completely automated to eliminate error and reduce cost.

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Parts to be tested for leaks are placed in a container and subjected, under pressure, to an inert, non-toxic, radioactive gas. They are then air washed and the amount of the gas which penetrated the transistor or other sealed unit is accurately measured to determine leak rates as small as 1 cc per 5000 years. Testing of parts may be done quickly and in quantity to prevent production delays. RADIFLO may also be used directly on the production line for **automatic** acceptance or rejection of parts whose leak rate exceeds pre-determined limits.

When transistors are checked for leaks by the RADIFLO method, their reliability and performance are effectively insured. Write for bulletin No. 7071.1

RADIFLO parts testing service available at American Electronics plant.

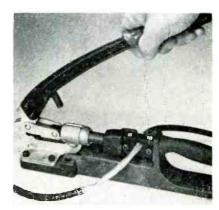


AMERICAN ELECTRONICS, INC.

655 W. Washington Blvd., Los Angeles, California



STEP 13—Completing splice of second inner conductor



STEP 14—Completing crimping of shield over splicing cable



STEP 15—Crimping length of vinyl tubing over splicing braid to insulate and waterseal splice



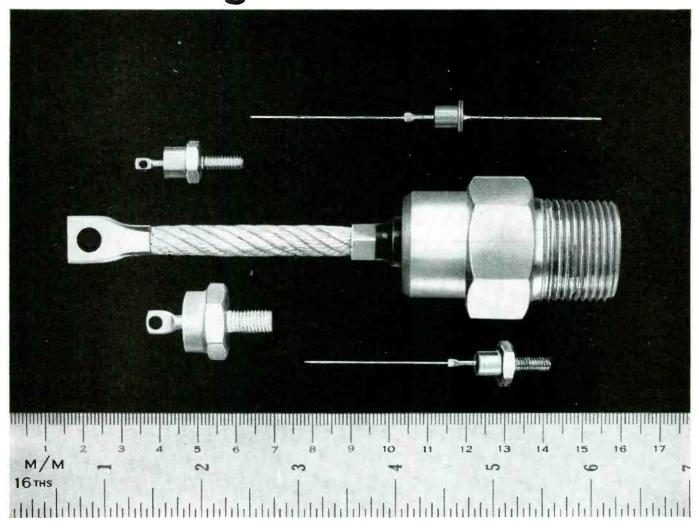
STEP 16—Testing splice for water sealing at pressure of 700 psi

splicing braid, each end of which is crimped to the shield with ferrules. For insulation or water protection, the entire splice can be sealed with vinyl tubing to withstand hydrostatic pressures in excess of 600 psi.

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Number	PIV (Max.)	Peak Reverse Current (Max.)	Maximum Current at 150°C Case	Thermal Drop Junction to Case
302	50-600 V	20 Ma	35 Amps.	1°C Per Watt
303	50-600 V	10 Ma	18 Amps.	1.5°C Per Watt
304	50-600 V	10 Ma	12 Amps.	2°C Per Watt
322	50-500 V	40 Ma	110 Amps.	.3°C Per Watt
LOW P	OWER			
305	50-800 V	1.5 Ma	1.6 Amps.	5°C Per Watt
320	50-800 V	1.5 Ma	1.6 Amps.	5°C Per Watt

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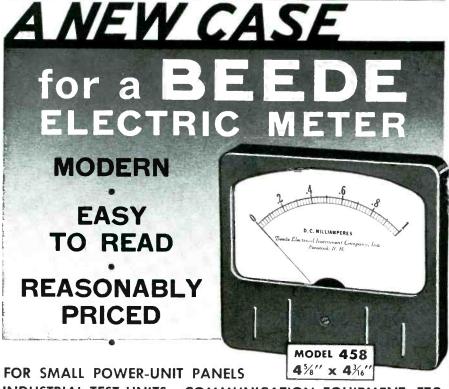
Standard units are now available — or we can fabricate to your specifications. Write us for quotes. Orders filled promptly.



Insuline CORPORATION OF AMERICA Division of Van Norman Industries

186 Granite St., Manchester, N. H.

CIRCLE 134 READERS SERVICE CARD



INDUSTRIAL TEST UNITS—COMMUNICATION EQUIPMENT, ETC.

LONG LASTING AND ACCURATE TO THE DOT

BEEDE ELECTRICAL INSTRUMENT CO., INC.
PENACOOK, N. H.



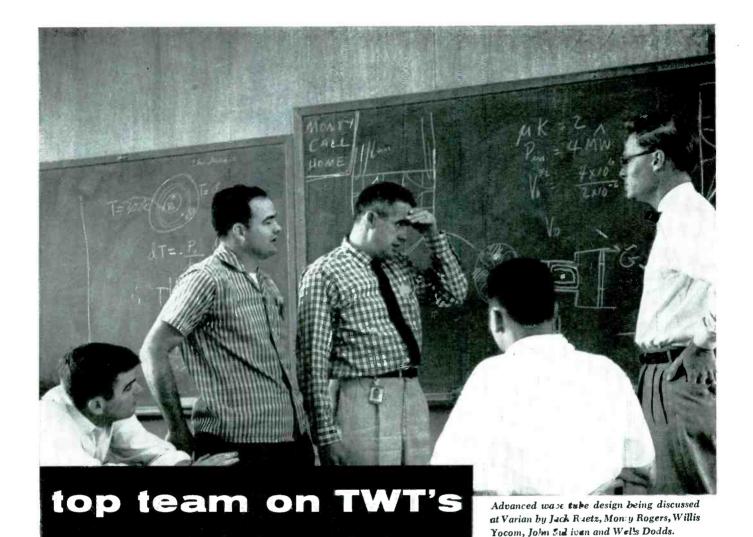
Absence of corners simplifies loading of lower deck of cart when bringing supplies up to assembly line

one dozen standard bread-pan containers for small parts. The lower platform holds larger components or large containers.

For easier loading and handling there are no corner posts, while the top and bottom corners are rounded for safety against personnel injury. Heavy steel cross-rods provide low-friction loading surfaces for bulky or heavy containers. Constructed of strong tubular steel, nickel-plated for durability, the carts are fitted with four ball-bearing swivel casters for extreme maneuverability. Manufacturer is McClintock Mfg. Co., 802 West Whittier Blvd., Whittier, Calif.

Epoxy Adhesive Kit

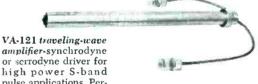
PACKAGING of a new Hysol epoxy adhesive and hardener in separate toothpaste-type collapsible tubes eliminates on-the-job weighing and proportioning of these ingredients



Traveling-wave tubes, as any of the men above will tell you, are slated for an important place in the world of electronics. And these men, backed by Varian know-how, are out to assure the fullest possible realization of the wave tube's promising future.

With one of the industry's most competent wave tube development groups, Varian is geared to meet a wide range of difficult challenges in its field . . . applying to newer systems problems the same know-how and teamwork that just a few years ago established Varian's leadership in klystrons.

Many new ideas and applications are on the way, to back up the success of tubes like the VA-121 and VA-161 shown here. The entire Varian wave tube team is ready to go to work for you, to shape up a wave tube application or come up with the answers you've been looking for. Write or call your Varian representative or Varian's Application Engineering Department.



amplifier-synchrodyne or serrodyne driver for high power S-band pulse applications. Performs to detailed specifications of phase and amplitude stability to meet the stringent requirements of phase-coherent MTI radar systems.

VA-161 backward wave oscillator for use in tunable radar local oscillator, countermeasure and bench and test applications. In the frequency range from 8.2 to 12.4 kMc.



25-40 watts 30 db min. .01 max. 2250 volts +27 volts Grid Pulse Voltage

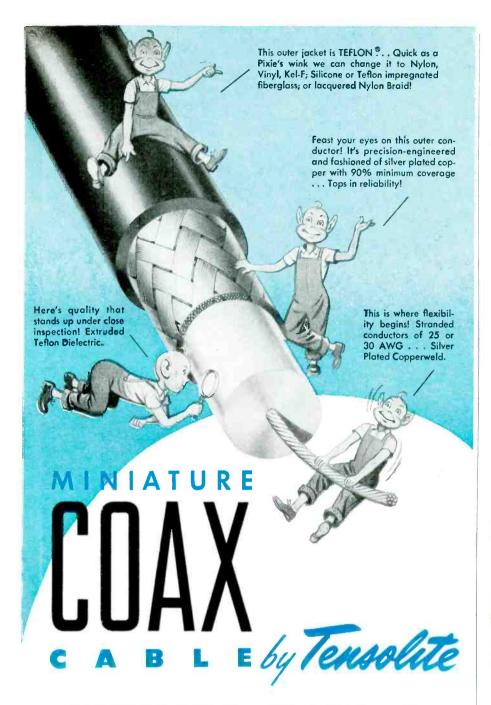


Power Output 30 to 120 mW Anode Voltage 150 to 600 volts Permanent Magnet Size: 41/8 x 5 x 61/2 inches Weight: Approx. 6 lbs.

THE MARK OF LEADERSHIP



KLYSTRONS, TRAVELING WAVE TUBES, BACKWARD WAVE OSCILLATORS, LINEAR ACCELERATORS, MICROWAVE SYSTEM COMPONENTS, R. F. SPECTROMETERS, MAGNETS, MAGNETOMETERS, STALOS, POWER AMPLIFIERS, GRAPHIC RECORDERS, RESEARCH AND DEVELOPMENT SERVICES



Here is a "Pixie Eye View" of Tensolite's new miniature Coaxial Cable . . . and here are the answers to some of the questions you will ask:

TEMPERATURE RANGE: From -90° to $+250^{\circ}$ C , . . depending on jacket used. Teflon jackets approved for entire temperature range listed.

IMPEDANCE VALUES: 50, 70, 75, 93 and 95 OHMS available from TENSOLITE as standard constructions.

TO MILITARY SPECIFICATIONS: MIL-C-8721 (with KEL-F jacket); RG-178, RG-179 and RG-180. MIL-C-17B (with TEFLON jacket); RG-187/U, RG-188/U, RG-195/U and RG-196/U.

COLOR CODED JACKETS: In standard colors and striped combinations.

AND FOR YOUR CUSTOM REQUIREMENTS: TENSOLITE Factory and Field Engineers are ready to assist you in the Design, Development and Production of any miniature Coaxial Cables for specific or unusual applications. Simply write or call TENSOUTE for complete descriptive literature and samples.

OD DUPONT

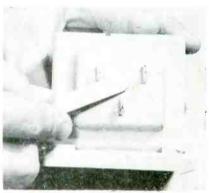




Squeezing from far end of tube insures even pressure, giving uniform thickness of each bead when dispensing resin and hardener in preparation for mixing



Wood blade serves equally well for mixing and applying epoxy adhesive



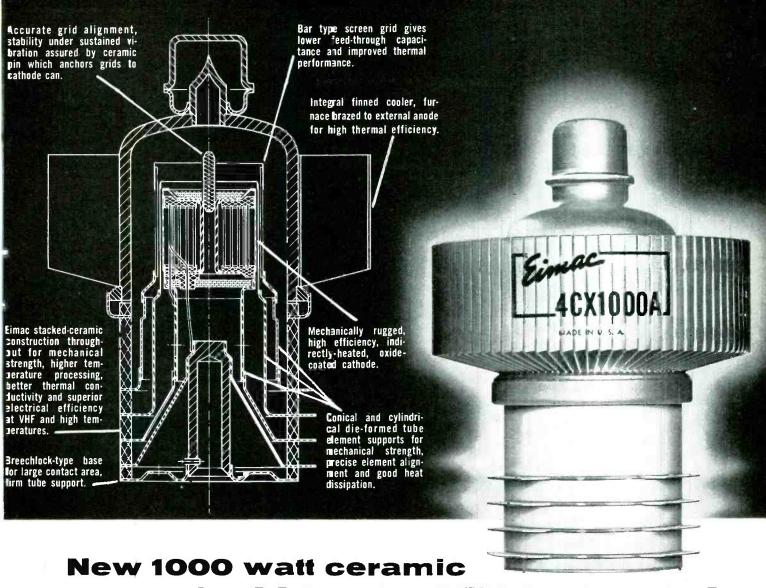
Filling void in encapsulated transformer

when a small quantity of the epoxy is needed for repair of an electronic component.

Any discardable flat surface, such as wood, cardboard or paper, can be used as a palette for mixing. The ingredients are squeezed from the tubes in parallel beads of equal ength, then mixed with a spatula or a wood tongue depressor. The same tool can be used for applying the adhesive.

At room temperature, the adhesive will harden in about 1 hour and cure completely in 24 hours. At 140 F, easily achieved with heat lamps, hardening takes only ½ hour and a complete cure 1½ hours.

The ability of the Bakelite epoxy



tetrode for SSB...the EIMAC 4CX1000A

Eimac fills another important transmitting need with this air-cooled, ceramic-metal, one-kilowatt tetrode . . . the 4CX1000A. Specifically designed for single side band operation the 4CX1000A is a low-voltage, high-current Class AB₁ RF or AF linear amplifier tube, exhibiting high power gain and exceptionally low distortion characteristics. The 4CX1000A achieves its maximum rated output power with zero grid drive, thus minimizing driver stage design problems and eliminating one source of distortion.

Eimac stacked ceramic design gives the 4CX1000A excellent immunity to damage by mechanical and thermal shock. Electrical stability is assured by internal ceramic support of the tube elements and clean internal

design. Ideal for applications where space is at a premium, this mechanically-rugged, electrically-reliable thousand watt tetrode measures less than 5 inches high and 3½ inches in diameter. High temperature processing, made possible by Eimac ceramic-metal design, produces an extremely clean tube. This ideal environment assures long life for the efficient oxide-coated cathode.

Efficient, trouble-free socketing and cooling is provided for the 4CX1000A by the new SK-800 Air System Socket and SK-806 Chimney.

Write our Application Engineering Department for a brochure and data sheet describing this important new tube in detail.

EITEL-McCULLOUGH, INC.

SAN BRUNO - CALIFORNIA

Eimac First for quality, dependability and performance



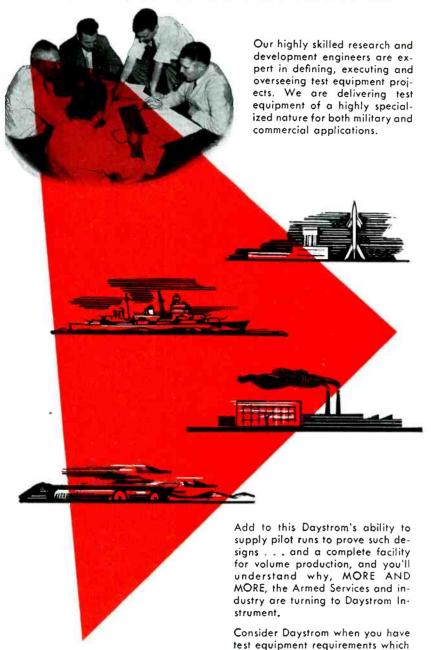
MAXIMUM RATINGS (Per Tube)

TYPICAL OPERATION SINGLE-TONE SSB

DC Plate Current 1.0 Amps

DAYSTROM INSTRUMENT WILL DESIGN AND BUILD YOUR SPECIAL TEST EQUIPMENT

We Have the Engineers and Facilities For RESEARCH, DEVELOPMENT and PRODUCTION





DAYSTROM INSTRUMENT

ards.

must meet the most critical stand-

Division of Daystrom Inc.

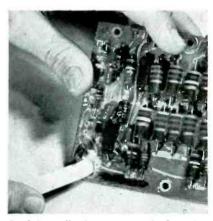
Archbaid, Pennsylvania



Sealing component in ceramic housing



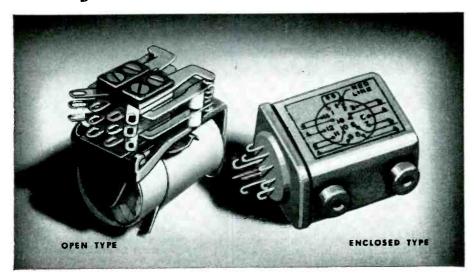
Filling holes in plastic molds. After adhesive is cured, repair can be sanded, smoothed and buffed to gloss finish



Applying adhesive over repaired portion of printed wiring board to restore protective moisture-sealing coat. For broken board, small patch of glass cloth would be used over surface to improve mechanical strength of bond

resin to wet and adhere to both metallic and nonmetallic surfaces makes this kit practically universal in application in the electronic field. The only requirement is that the surfaces to be filled or joined are completely clean and dry. It can thus be used for filling cavities in plastic or metal objects, repairing flaws in encapsulated compon-

R-B-M Miniature Multipole Relays of Proven Reliability



Light weight, Small Size Open and Hermetically Sealed Types for Electronic and Communication Application

APPLICATION: R-B-M Miniature Multipole Relays are used where the prime factors in switching electronic circuits are small size, light weight and reliability. These proven designs are produced for switching low power circuits, low capacitance circuits and power circuits. 125° C insulation now available on some versions. Coils can also be designed for plate circuit.

CONSTRUCTION:

Magnet Frame—Four sizes available on open type relays and three sizes on hermetically sealed type.

Contacts—Cross-bar palladium welded to nickel silver springs or button contacts on Beryllium copper springs.

Terminals and Mountings—Glass headers provided with either solder or plug-in type terminals with many various types of mountings available. Octal type plug-in headers can be provided on the HL enclosure. Plug-in terminals to fit either 9 or 14 pin standard sockets. Maximum of 14 pins for solder connections.

TYPICAL SPECIFICATIONS*

Open	Maximum Coil Resistance (OHMS)	Minimum Power Requirements Per pole at 25° C(WATTS)	Maximum Contact Form With rated current at 32 V.D.C. or 115 V.A.C. (non-inductive load)	Maximum Coil Watts	Enclosed
SM	9,000	.2	.2 4 PDT 5 Amps. or 3 Amps. 6 PST 3 Amps.		HSM
SMD-2	9,000	1,0	SPNO Parallel Contacts Make 80 Amps. Break 20 Amps. at 32 V.D.C.	3.75	HSMD-2
sc	18,500	.16	4 PDT 5 Amps. or 3 Amps. 6 PST 3 Amps.	4.5	HPSC
SA	18,500	.14	4 PDT 5 Amps. ar 3 Amps. 6 PST 3 Amps.	4.5	HLSA
SM-RF	9,000	.2	SPNO, SPDT, DPNC, SPNC, DPNO	3.75	HSM-RF HLSM-RF
SAD-2	18,500	1,0	SPNO Parallel Contacts. Make 80 Amps. Break 20 Amps. at 32 V.D.C.	4.5	HLSAD-2

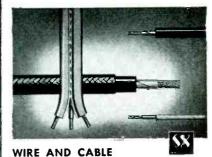
*Other ratings and specifications available.

For additional information write for Bulletin No. 1050

RBM DIVISION

Manufacturers of Magnetic LOGANSPORT, INDIANA
Controls and Devices





A full "Extra Test" line of lead, appliance, automotive and refrigeration wires, plus submersible pump cable and 200° C. Sil-X insulations are examples of the versatility of "Essex Engineering".

Wire and Cable Division Fort Wayne, Ind.



MINIATURE RELAYS

The Type MS Miniature Sensitive Relay is ideal for any application requiring a compoct, highly reliable single pole D. C. device, where a low cost solution is required because of volume usage and competitive problems. Request Bulletin No. MS-1.

R-B-M "Control" Division Logansport, Ind.



COILED CORDS

The "spring" in Coiled Cords automatically synchronizes with moving components that are electrically powered. There are no looping, tangling cords in the way... because Coiled Cords extend and retract as needed. Write for new literoture.

Cords Limited Division DeKalb, 111.





by R. George Roesch

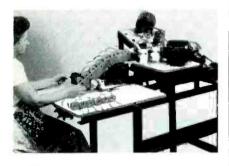
Eliminate Manual Operations for Uniformity

The efficiency of many manual wire-processing operations may now appear to be perfect for the specific jobs for which they are used. The actual efficiency, however, is limited by the manual operations. It is impossible for anyone to do something time after time, exactly the same way. Honest human effort can result in some errors.

Mechanized Wire Processing

One logical way of attaining practical quality control of wire processing—has proved to be mechanized Wire Processing Equipment developed for the specific job.

Assuming uniformity of product up to the Wire Processing Equipment, such mechanical processing can result in uniform high quality every time.



A typical example is this mechanized wire cutter and stripper designed for shunt coils wound with AWG No. 30 Formvar-insulated wire. Except for hand loading, the operation is completely automatic, at the rate of 1,620 coils per hour with one operator.

If you have a production wireprocessing job, we would like to discuss it with you.

THE ERASER CO., INC. 1068 S. Clinton St., Syracuse 4, N. Y.

REPRESENTATIVES:

There are still a few choice territories open, offering unusual opportunities for service and profit. Write R. George Roesch.

ents, resealing printed wiring boards after replacement of a component, and repair of broken ceramic, glass, aluminum, ferrous metal and wood pieces as well as most plastics and most types of hard rubber. The two-tube kit as marketed by Houghton Labs., Inc., Olean, N. Y. is particularly useful where only a very small amount of adhesive is needed at a time.

Hard Anodizing Gives Insulation on Aluminum

USE OF HARD ANODIZING for insulating an aluminum chassis permits direct mounting of power transistors or power rectifiers to utilize the full heat-sink ability of the chassis, while providing required insulation. Dielectric tests at 500 volts indicate a resistance of several thousand megohms, which is more than adequate for existing or proposed power circuitry.

The new hard anodizing process, developed by Hughes Aircraft Co.

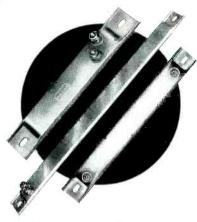


Finished aluminum chassis which has been hard-anodized to give insulating surface. Bare metal is left exposed in strips on sides for grounding purposes

in conjunction with Anachrome Corp., South Gate, Calif., is an adaptation of the versatile Hardas process which is applicable to any aluminum alloy chassis. Dimensional changes are minute, because the insulation is provided by a thin film of aluminum oxide formed on the surface by chemical action.

The self-insulating chassis eliminates the need for mica washers or other heat-blocking insulators between transistor and chassis when isolation is required. The resulting near-maximum transfer of heat to the chassis greatly increases the efficiency of transistor and rectifier circuits.

When to specify **VULCAN ELECTRIC** STRIP HEATERS



- When application is for: Contact heating of dies, platens, molds, or any items with flat surfaces to which elements may be clamped. Also air heating source for ovens, air ducts,
- 2. When specifications call for: Seamless one-piece sheath; rugged non-oxidizing terminal posts; steel sheath for sheath temperatures to 750°F; Chromalloy sheath for sheath temperatures to 1200°F; 8" 421/2" lengths (or longer); 150 to 1500 watts (or higher).
- 3. When you have "hot" problems: Vulcan Engineers are ready to supply special heating units — engineered to your needs.

VULCAN ELECTRIC BAND HEATERS



Constructed basically like the strip heaters, Vulcan Electric Band Heaters are designed for clamping around tanks, pipes, injection heads, etc. Standard width is $1\frac{1}{2}$ "; inside diameters from 6" to 15" (special smaller or larger sizes available). Semi or full circular bands. Equipped with mounting tabs or clamping bands.

Write for free catalog



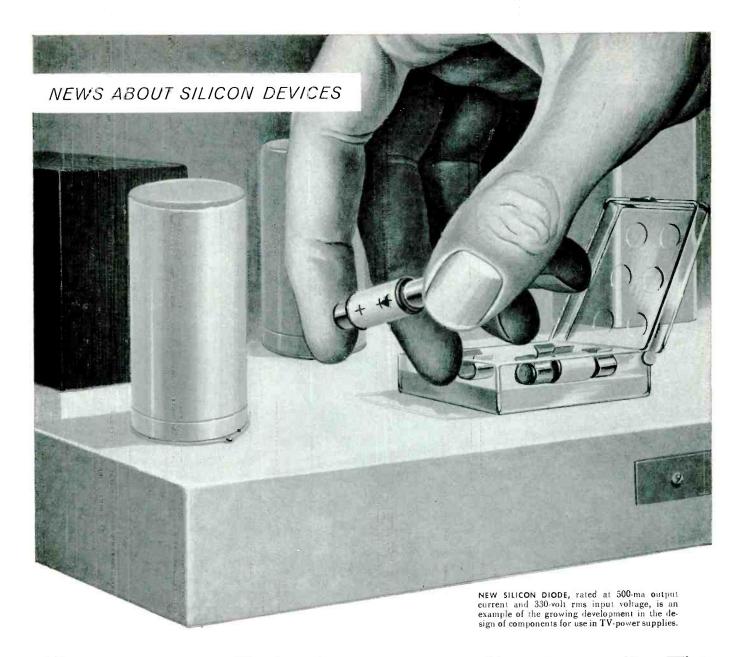
ELECTRIC COMPANY

DANVERS 10, MASS.

Cartridge • Strip • Tubular • Immersion Electric Soldering and Branding Irons Solder and Glue Pots

CIRCLE 142 READERS SERVICE CARD

December 1, 1957 - ELECTRONICS



Now...more efficient power supplies for radio-TV made possible with Du Pont Hyperpure Silicon

Actual test results as reported by various manufacturers indicate important advantages of silicon diodes and rectifiers. One TV manufacturer, for example, operated samples of silicon rectifiers under load continuously for 5,000 hours—with no noticeable drop in output voltage. Another manufacturer reports no voltage change after 500 hours in 95% humidity.

Silicon-equipped sets are relatively free of a decline in B+ voltage. Silicon diodes are up to 99% efficient in units operated at 60 cps—reverse leakage is as low as a few microamperes. Both rectifiers and transistors of silicon have temperature ratings far higher than those of other semiconducting materials... can operate continuously at -65° to 200°C.

Note to device manufacturers: You can produce silicon transistors, rectifiers and diodes of the highest quality with Du Pont Hyperpure Silicon. It's now available in three grades for maximum efficiency and ease of use . . . having a purity range of 3 to 11 atoms of boron per billion. Technical information is available on crystal growing from Du Pont . . . pioneer producer of semiconductor-grade silicon.



NEW BOOKLET ON DUPONT HYPERPURE SILICON

You'll find our new, illustrated booklet about Hyperpure Silicon helpful and interesting—it describes the manufacture, properties and uses of Du Pont Hyperpure Silicon. For your copy write to: E. I. du Pont de Nemours & Co. (Inc.), Silicon N-2496-E-12, Wilmington 98, Dela. (This offer is limited to U.S. and Canada.)

PIGMENTS DEPARTMENT



BETTER THINGS FOR BETTER LIVING ...THROUGH CHEMISTRY

93 New Products and Latest Manufacturers' Bulletins Are Reviewed . . . Control, Testing and Measuring Equipment Described and Illustrated . . . Recent Tubes and Components Are Covered

POWER SUPPLY

completely transistorized

MANDREL INDUSTRIAL INSTRUMENTS, Division of Mandrel Industries, 5134 Glenmont Drive, Houston, Texas. The PV-2 inverter is a completely transistorized power supply designed to operate 50 or 60 cps synchronous motors from a 12 v d-c source. It is tuning fork controlled and capable of operating motors rated up to 140 va input.

Output waveform is a modified square wave ideally suited for



driving synchronous motors. The output voltage frequency is accurate to 0.01 percent and stable to 0.01 percent. Its magnitude is adjustable in steps to yield 115 v rms of the 50 or 60 cps component of the modified square wave output. Input current varies from 2 amperes no load to approximately 12 amperes full load. The input voltage may vary from 10.5 to 13.0 v with no deleterious effect.

Complete warm-up time is 30 sec. Overall size is $7\frac{1}{2}$ in. by $6\frac{3}{4}$ in. Price is \$750. Circle 401 on Reader Service Card.

MINIATURE CAPACITOR

flat or round



ASTRON CORP., 255 Grant Ave., East Newark, N. J. A new miniature Mylar dielectric capacitor is now available in production quantities. The new capacitors, type XPR and XPF, are designed for applications requiring minimum size, high insulation resistance and exceptional capacitance sta-

bility. A Mylar polyester outer wrap affords good protection against moisture, its ends being sealed with a plastic thermosetting resin. Voltage rating is 150 v at 85 C, 100 v at 125 C.

Reliable performance is achieved over the entire operating temperature range of -55 C to +125 C. The new series is available in flat and round construction. Circle 402 on Reader Service Card.

TINY RESISTORS

carbon film types

MEPCO, INC., Morristown, N. J., has announced microminiature carbon film resistors. Resistance range is 5 ohms to 100,000 ohms. Wattage is 0.1 w at 70 C. Type C-1H is sealed in a ceramic case for protection against humidity and damage in installation. It meets requirements of MIL-R-10509B, characteristic B. Length is $\frac{3}{2}$ in. and diameter $\frac{3}{2}$ in. Type C1 is resin



coated. Resistor is not damaged when potted in epoxy resins. It meets requirements of MIL-R-10509B, characteristic X. Length is 15 in. and diameter 16 in. Circle 403 on Reader Service Card.

AUDIO OSCILLATOR with wide frequency range

WAVEFORMS, INC., 333 Sixth Ave., New York 14, N. Y., has developed



It takes a lot of doing to produce the exact same thing over and over again hundreds of thousands of times—without slipping up on a thousandth of an inch, watt, or milligram. This insistence on *uniformity* has helped build our reputation as the world's most Consistently Dependable producer of CAPACITORS. Continuously uniform production is a science—one that we've painstakingly pursued since 1910.

Typical of the "countless" C-D electrolytics used by major equipment manufacturers the world over are:

WEC" MINIATURIZED CERAMIC CASED TUEULARS For crampedspace applications in hearing aids, transistorized devices, and remote control assemblies. Less than ¼ "D., only ¾ "L. "NL" ULTRA-SMALL Hermetically sealed aluminum cased electrolytics, built for compactness, ruggedness, low leakage, long shelf and in-use life.

TANTALUM 3 tubular types, all with low power-factor, moisture-impervious hermetic seal, long service and especially long shelf life. "TX" with sintered anode; "TAN" miniature foil type; sub-miniature, low-voltage wire anode type "NT".

TYPE "UP" Made in the smallest tubular aluminum cans possible for any given capacity and voltage combination. In single, dual, triple and quadruple capacity combinations.

Write for catalog to Cornell-Dubilier Electric Corporation, South Plainfield, New Jersey.



CORNELL-DUBILIER CAPACITORS



SOUTH PLRIMFIELD, N. J.; NEW BEDFORD, WORCESTER & CAMBRIDGE MASS.; PROVIDENCE & MORE VALLEY, R. S.; INDIANAPOLIS, IND.; SANFORD, FUQUAY BERINGE & VARIAS, N. C.; VENICE, CALIFA & SUBL: THE RABBAPIT CORP., CLEVELAND, OHIO; CORNELL-DUBILIER ELECTRIC INTERNATIONAL, N. T. the 401A general purpose audio oscillator. The instrument features extended range (10 cps-100 kc), high output (20 v or $\frac{1}{2}$ w), purity of signal ($\frac{1}{4}$ percent distortion for all conditions) and a flex-

ible attenuator system.

The unit utilizes a new oscillator circuit to achieve low distortion and freedom from switching and tuning transients. This new oscillator circuit, together with

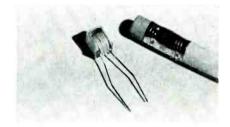
novel output amplifier circuitry, provides overall instrument performance heretofore available only in instruments of greater complexity and costs. Circle 404 on Reader Service Card.

SELENIUM DIODE

for computer applications

BRADLEY LABORATORIES, INC., New Haven, Conn., is producing a new selenium diode, designed especially for computer applications.

First use of the unit, designated SP1M4H867, was as a replacement for a germanium diode in which considerable difficulty was en-



countered because of random surges of pulses. One of the inherent advantages of selenium is its ability to withstand overload.

Specifications of the selenium diode are: 50 ma intermittent duty, 12 milliseconds on; 5 ma continuous duty; and peak inverse voltage of 150 v. Clip-type housing measures 4 in. by % in. by % in. Circle 405 on Reader Service Card.

VANE TRANSDUCER

local angle of attack type



G. M. GIANNINI & Co., INC., 918 East Green St., Pasadena 1, Calif. A new local angle of attack transducer that conforms to MIL-T-25627 (USAF) has been added to the company's line of vane transducers. This unit, model 2562, provides accurate angle of attack information at all speeds and altitudes throughout a wide operational range.

This instrument consists of a heated, split-wedge vane, geared

to two output synchros. Damping is maintained at 0.5 of critical by a uniquely simple viscous-type damping mechanism. Recovery time for 63 percent of a step input at 110 knots is only 0.075 sec, and sensitivity is 0.2 deg from 90 knots to 125 knots and 0.1 deg from 125 knots to Mach 3.0.

Specifically designed to meet or exceed the requirements of MIL-T-25627, this transducer is ideal for operational or flight-test applications requiring accurate angle of attack or side slip information. Circle 406 on Reader Service Card.

D-C MILLIVOLTMETER

and d-c amplifier

INDUSTRIAL CONTROL Co., 805 Albin Ave., Lindenhurst, L. I., N. Y. The 216A is an extremely sensitive, direct reading, d-c millivoltmeter and d-c amplifier. It features a zero center indication with ±1 mv d-c full scale, and a zero point so stable that no zeroing control is provided. Maximum amplifier gain is 1,000, input impedance 2 megohms, and full scale sensitivities range from 1 mv to 10 v d-c in 9 overlapping ranges.

The 216A is designed for rack-mounting, is ruggedized for military usage and is built to MIL-T-945A. Panel dimensions are 19 by



8 in. and depth behind the panel is 8 in.

The unit has been designed especially for military ground support equipment. It is also recommended

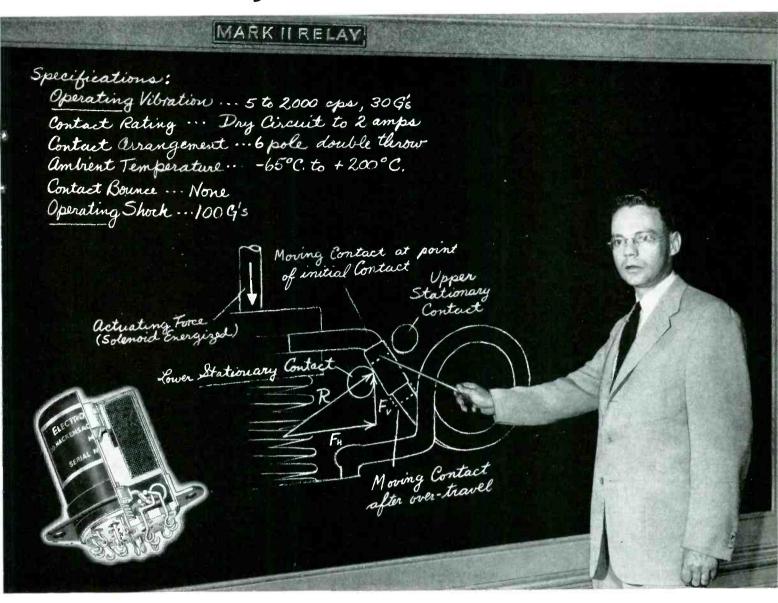
wherever a rugged, reliable and sensitive millivoltmeter and amplifier are required. Circle 407 on Reader Service Card.

COUNTER

has two predeterminations

PRESIN Co., 12128 W. Pico Blvd., Los Angeles 64, Calif. Specifically designed for winding tapped coils, the model U280Z has two predeterminations, each independently settable to a total of 99,999, one for the tap and one for the final with knockoff by spdt switches. The counters add and subtract to

Now in production revolutionary WEDGE ACTION RELAY!



MARK II RELAY provides ULTRA-RELIABILITY under the most extreme environmental and operating conditions.

NOVEL WEDGE ACTION SWITCHING provides positive contact in both energized and de-energized conditions.

Contact pressure constantly increases during over-travel.

Wedge Action now supersedes "Wiping Action".

- Removes contaminants from contact surfaces.
- Reduces resistance to micro-level currents.
- Renders relay extremely resistant to shock and vibration.

BRIEF DESCRIPTION: Six pole, Double-throw, Miniature unit. Hermetically sealed, Meets—and *exceeds*—specifications MIL-R-5757C and MIL-R-25018.

From an organization of recognized authority in advanced instrument design—Electro Tec—comes, not merely another new relay, but a *completely new concept* in ultra-precision relay operation.

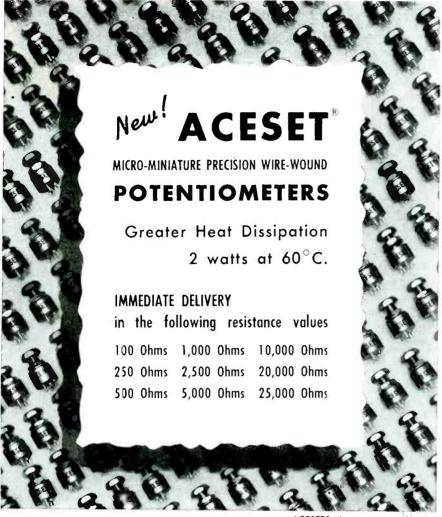
This new Mark II Wedge Action relay—now in production—offers designers of ultra-reliable electronic equipment immediate and outstandingly high performance, amply proven under the most extreme environmental and operational conditions. Designers should write—or wire for additional information.

Products of Precision Craftsmanship

ELECTRO TEC CORP.

South Hackensack, N. J.





ACESETS shown approx. 1/2 size

Now you can select from nine different resistance values and improve the accuracy and dependability of your circuit performance. ACESET precision, wire-wound, micro-miniature potentiometers offer greater stability under temperature cycling through the use of 20 ppm temperature coefficient wire. Improved performance at lower costs have been achieved by mass producing to standard specifications. Shipments are guaranteed within 24 hours of receipt of order. Call, wire or teletype Dept. F at Ace Electronics Associates, Inc., 99 Dover Street, Somerville, Mass. SOmerset 6-5130. TWX SMVL 181

MECHANICAL SPECIFICATIONS

One piece precision-machined metal case Passivated stainless steel shaft
Self-contained locking device
Panel anti-rotation pin
Mechanical rotation: 330° nominal
Size: 1/2" diameter x 5/16" body length

ELECTRICAL SPECIFICATIONS

Heat Dissipation: 2 watts at 60°C.

Voltage breakdown: 1,000 VDC

Electrical Angle: 325° nominal

Temperature coefficient of wire: 20 ppm

Resistance tolerance: ±10%

Linearity: \pm 5 %



ACEPOT®

ACETRIM*

ACEOHM®

*TRADEMARK APPLIED FOR ACESET®

a maximum speed of 5,000 rpm. The double presetting is quickly and easily accomplished by means of grip wheels under the hinged cover. Both predeterminations are simultaneously reset to zero for repeat cycling by quick lever or automatically by motor.

The counter is available with optional 8-digit key reset totalizer, or for electrical counting for base and panel mounting. Among other applications for the counters are processes requiring a warning or deceleration signal. Circle 408 on Reader Service Card.



ALL-METAL MOUNTING

for airborne equipment

ROBINSON AVIATION, INC., Teterboro Air Terminal, Teterboro, N. J., has developed a low frequency all-metal unit mounting to mount airborne resolvers, computers and radar search equipment. The natural frequency of model 1459 is between 5 and 9 cps for vibration protection. Vibration isolation response at 30 cps, for example, is as high as 90 percent and improves at higher frequencies. Met-L-Flex resilient elements incorporated in the design provide the environmental control of shock impacts and superimposed vibratory forces. These mountings possess a high percentage of inherent damping for longer equipment life under severe conditions.

Model 1459 is designed to ac-



Now-the first 155°C (Class F) polyester film-coated magnet wire designed to meet new AIEE requirements

Another Anaconda first! Anatherm—a new polyester film-coated magnet wire—fully tested for use at "hottest-spot" temperatures up to 155°C. With this new higher level of thermal stability, Anaconda Anatherm is the first film-coated wire to meet the newly adopted AIEE 155°C (Class F) rating!

Greater thermal stability—plus excellent abrasion-resistance characteristics, chemical stability and dielectric strength—makes Anatherm ideally suited for manufacturers seeking maximum performance and reliability from smaller and smaller equipment operating at higher and higher temperatures.

As a polyester magnet wire, Anatherm can be used equally successfully at any hottest-spot temperature over the range of 105°C to 155°C.

Available in single and heavy film thickness in AWG sizes from 15 through 25.



FREE TECHNICAL BULLETIN on Anatherm Magnet Wire is available. Simply write: Anaconda Wire & Cable Company, 25 Broadway, New York 4, New York.



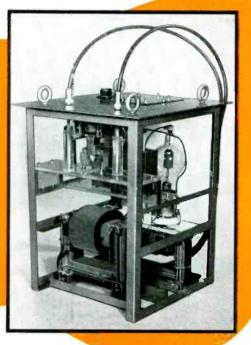
ASK THE MAN FROM ANACONDA®

ABOUT ANATHERM MAGNET WIRE

CIRCLE 167 READERS SERVICE CARD

VOLTAGE QUALITY RELIABILITY

50 KV DC SUPPLY



Typical of the Del high voltage oil insulated power supplies, this 50 KV unit was developed specifically for laboratory and industrial use by engineers with long experience in the high voltage field.

Controls with special features to suit your requirements can be furnished on short term delivery.

Other supplies up to 200 KV, 20 KVA, in air, oil or solid insulating media, with vacuum tube or semi-conductor rectifiers.

For additional information write to:

SPECIFICATIONS

ELECTRICAL:

INPUT: 110/220 volts, 50/60 cycles.
OUTPUT: 0-50KV DC @ 5 or 7 MA.
POLARITY: Either positive or negative
high with one terminal at ground potential, or center ground.
CIRCUIT: Full wave voltage doubler.
RECTIFIERS: Vacuum tubes or selenium,
RIPPLE: 0.4% per MA.
INSULATING MEDIUM: Special high

INSULATING MEDIUM: Special high grade insulating oil to insure freedom from electrical noise.

SAFETY FEATURE: Stored energy automatically discharged from capacitors on removal of input power.

PHYSICAL:

SIZE: 16½" x 16½" x 22½" high.
FINISH: Gray hammertone enamel.
HOUSING: Heavy gauge steel oil tight
tank with four eye bolts for lifting.
CONNECTORS:

Input — AN-3102-22-18P fastened to tank.

Output — Shielded polyethylene cables.

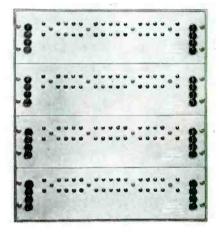


DEL ELECTRONICS CORPORATION
521 HOMESTEAD AVENUE MOUNT VERNON, N. Y. OWERS 9-3232

WE DESIGN AND MANUFACTURE A VARIETY OF HIGH VOLTAGE, LOW CAPACITY FILAMENT TRANSFORMERS, REACTORS AND OTHER SPECIAL PURPOSE TRANSFORMERS.

commodate loads of 16 to 23 lb per mounting. They are used in multiple units to mount airborne components requiring shock and vibration protection as set forth in military specification MIL-C-172B. Modifications for lighter or heavier load ratings may be designed upon request.

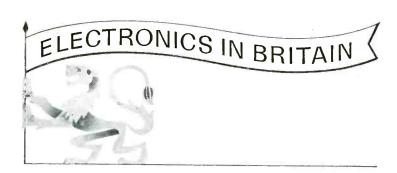
Installation requires only one 4-20 UNC-2B bolt to attach the equipment to the mounting. Mounting to the airframe is facilitated by four 0.196 diameter holes per mounting. Self-locking devices and choice of thread size are available. Circle 409 on Reader Service Card.



LONG DELAY LINE has 100 external taps

EPSCO INC., 588 Commonwealth Ave., Boston 15, Mass., has manufactured a lumped constant delay line to meet the specific requirements of an auto-correlation application—complex input waveforms are to be delayed from 0 to 100 milliseconds, without any deterioration of the shape of the waveforms resulting when the maximum delay is used. The delay line has 100 external taps, permitting the delay to be selected in one-millisecond increments.

The 100-millisec line consists of four identical 0 to 25 millisec tapped delay lines in cascade. Each of these separate delay lines contains 25 sections of m-derived LC networks utilizing high-Q toroidal inductances and ultrastable capacitors. The precise matching of all these LC networks makes possible the successful cascading of



British 25W high fidelity output tube



builds Sound Reputation

Other Mullard hi-fi audio tubes

EF86

Low noise, low hum, low microphony

input tube

ECC83

High μ double triode

EL84

Medium power output pentode-

17 watts in push-pull

EZ81

Full wave, noval base, rectifier-

350V at 150mA

GZ34

Full wave rectifier-

450V at 250mA.

Principal Ratings

Heater 6.3V, 1.5A

Max, plate voltage 800V

Max. plate dissipation 25W

Max. screen voltage 500V

Max. screen dissipation 8W

Max. cathode current 150mA

Base

Octal 8-pin.

Second to none. This claim has been made for many products but none deserves it more than the Mullard EL34 (6CA7) high fidelity output tube. The exceptionally high efficiency of this tube has led to its adoption by the majority of equipment manufacturers in Britain, as well as an ever increasing number in America and Canada.

The facts speak for themselves. In push-pull ultralinear operation (distributed load), two EL34 tubes under self-bias conditions will give over 40W output at a low level of distortion. Distortion may be further reduced to a very low value when negative feedback is applied

The EL34 when used as a pentode is capable of supplying still higher power output. Under fixed-bias class B conditions, 100W is obtainable from a pair of EL34 tubes in push-pull.

A further significant feature of this tube is its high transconductance value of 11,000 µmhos, resulting in high power sensitivity and low drive requirements.

Full details of the complete range of Mullard hifidelity audio tubes may be obtained from either of the distributing companies mentioned.

ELECTRONIC TUBES used throughout the world

Supplies available from:

in the U.S.A.

International Electronics Corporation.

Dept. E12, 81, Spring Street, N.Y. 12, New York, U.S.A

in Canada

Rogers Majestic Electronics Limited, Dept. IL, 11-19 Brentcliffe Road, Toronto 17,

Ontario, Canada.

MULLARD OVERSEAS LTD., MULLARD HOUSE, TORRINGTON PLACE, LONDON, ENGLAND

Mullard is the Trade Mark of Mullard Limited and is registered in most of the principal countries of the world.

MEV 51



Hunt R. C. E. is a proprietary etchant, formulated to etch printed circuits fast and to speed up production. It offers these 6 big advantages:

- 1. 15% increase in etching speed
- 2. Fast action over entire circuit
- 3. Uniformly smooth etching
- 4. Easily removed by washing
- 5. Substantial increase in capacity
- 6. Freedom from fumes

HUNT S.C.E. (Solder Circuit Etch) FOR SOLDER-PLATED CIRCUIT BOARDS

This ready-prepared product is designed to etch solder-plated circuit boards more easily, more effectively than it has ever been done before. You'll find that Hunt S. C. E..

- 1. Etches rapidly at room temperatures
- 2. Has a high capacity for copper
- 3. Never attacks the circuit
- 4. Has guaranteed uniformity, and is of the highest quality because of rigid laboratory control

Hunt S. C. E. is essentially an oxidizing solution with the capacity to keep the oxidized copper permanently in solution. Although many acids will etch copper, S. C. E. solution has the peculiar property of not attacking the solder . . . but giving fast, odorless etching of the copper.

Write to nearest Hunt Branch for:

Technical Bulletin No. 1.—
"The Etching of Copper by Hunt
R. C. E. Solution"

Technical Bulletin No. 3—"the Etching of Solder Plated Circuit Boards by Hunt S. C. E. Solution"

HUNT R.C.E. SOLUTION

145 lb. rubber drums 600 lb. poly drums HUNT S.C.E. SOLUTION

125 lb. carboys 530 lb. poly drums



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the four units—in fact, there is no reason why more than four such units could not be cascaded, thus creating an even longer delay line.

A significant design feature of the 25-millisec lines is that their input and output sections are externally disconnectable, which means the lines can be cascaded or used separately without any internal wiring modifications. Circle 410 on Reader Service Card.



SUBMINIATURE SWITCH

toggle-actuated

UNIMAX SWITCH DIVISION, The W. L. Maxson Corp., Ives Road, Wallingford, Conn. Designed to give the advantage of single-hole panel mounting and a toggle actuator mechanism, together with subminiature size, the new USMB-1 snap-acting switch fits into back-of-panel space only 2 5/23 in. by §in. Connection terminals at the rear of the switch housing handle wires up to No. 18.

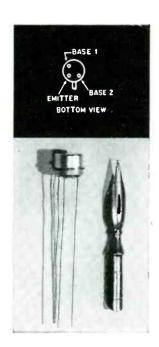
The toggle actuator can be furnished with any USM series basic switch. The USM series are rated at $2\frac{1}{2}$ amperes, 30 v d-c, inductive; 4 amperes 30 v d-c, resistive; and 5 amperes 125/250 v a-c. Data sheet USM-2 gives complete information. Circle 411 on Reader Service Card.

RECTIFIERS

miniaturized, copper oxide

BRADLEY LABORATORIES, New Haven, Conn. A new line of miniaturized copper oxide instrument rectifiers is announced under the series designations of CX1A4F and CX5A4F.

Advantages are negligible error with temperature variations, long

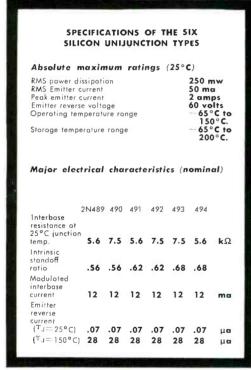


G-E Unijunction Silicon Transistor

NOW FULLY CHARACTERIZED AND PROVED FOR USE IN SIMPLIFYING CIRCUITRY

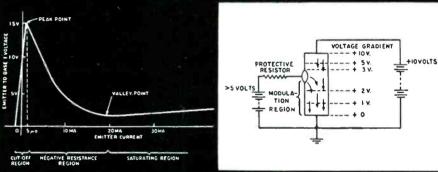
The unique advantage of the unijunction transistor lies in its open-circuit-stable negative resistance characteristics. The unijunction is the nearest solid state equivalent to the grid-controlled thyratron and is very sensitive to voltage levels. It is primarily useful in switching and oscillator applications. Not only will one unijunction do the job of two transistors (and with less circuitry) but the circuit will be more stable over a wide temperature range.

Technical data and application ideas are available to help you in studying the unijunction—the first device other than the transistor itself to reach commercial success. The six unijunction types can be obtained from most G-E Distributors, or write General Electric Company, Semiconductor Products Dept., Section \$25127, Electronics Park, Syracuse, New York.



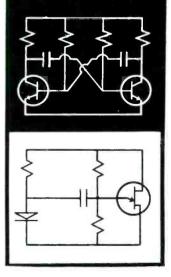
Progress Is Our Most Important Product





The unijunction consists of an "N" type silicon bar mounted between two ohmic base contacts, with a "P" type emitter near base 2. When the emitter is forward biased, emitter current flows, lowering the resistivity of the bar between emitter and base. Inherent regeneration results in a negative emitter to base 1 impedance. As the emitter current increases past the valley of the curve, the conditions for inherent regeneration cease to exist. The peak point of the curve shows the beginning of the negative resistance region.

Among the many simplified circuits possible with the uniquaction (cutting transistor requirements in half) are a frequency divider, matrix switching circuit, low level d-c current-sensing circuit, temperature control element, phase and/or amplitude sensitive switch. The conventional multivibrator circuit (above right) requires even more circuitry than is shown if it is to be as stable as the comparable unijunction circuit shown below. A relaxation oscillator usually takes 4 resistors, 2 transistors and a capacitor. A single unijunction, a resistor and capacitor will do the equivalent job.



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peripheral
equipment
for
digital
computers

NEW speed ... NEW versatility... NEW reliability! The Potter Model 906, using transistors, offers years-ahead design and performance for every tape handling, function.

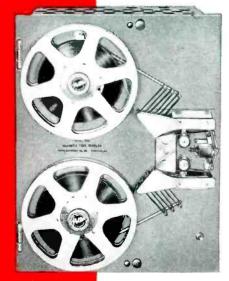
FEATURES

- Completely transistorized
- Up to 150 ips
- As many as 4 speeds forward and reverse
- Rewind or search at 400 ips
- · Vacuum loop buffer
- 3 millisecond starts.
- 1.5 millisecond stops
- Tape widths to 11/4"
- Up to 47 channels
- All functions remotely controllable
- Capable of continuous cycling at any frequency from 0 to 200 cps without flutter
- In-line threading, end of tape sensing, and tape break protection

Other Potter products include Transistorized Frequency Time Counters, Magnetic Tape Handlers, Perforated Tape Readers, High Speed Printers, Record-Playback Amplifiers and Record-Playback Heads.

WRITE, WIRE OR PHONE FOR SPECIFICATIONS ON THE MODEL 906

906



TRANSISTORIZED MAGNETIC TAPE HANDLER



POTTER INSTRUMENT COMPANY, INC.

SUNNYSIDE BOULEVARD, PLAINVIEW, N.Y.

OVERBROOK 1-3200

NEW PRODUCTS

(continued)



life, retention of electrical characteristics under vibration and high resistance to momentary overload. Designed for general meter and instrument application, the series also meet the specifications for VU meters.

Units consist of 4 cells in a full-wave bridge circuit. They are rated up to 2 ma d-c and 6 v a-c input, and supplied with 3-in. leads. Various types of mountings are provided to meet assembly requirements. Overall dimensions without mounting are \$\frac{1}{4}\$ in. by \$\frac{3}{16}\$ in. Units are moisture and fungus-resistant. Circle 412 on Reader Service Card.



ULTRASONIC CLEANER self-contained unit

Branson Ultrasonic Corp., 40 Brown House Road, Stamford, Conn., has available a self-contained ultrasonic cleaner in a single cabinet. Including a heater, temperature control, filtration and recirculation system in addition to the ultrasonic generating equipment, model R-50 is nonetheless

the mighty nine

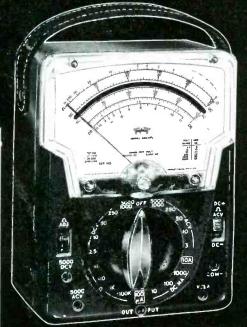


TWO NEW VOLT-OHM-MILLIAMMETERS

Now the Triplett Mighty Nine Has Expanded to A Line of 11 VOMs Tailored to Meet Your Preference, Purse or Purpose. Only Triplett Offers So Complete A Variety.

With the new 630-PL and 630-APL you get these important new features:

- Voltage scales for those who want ranges reading by 10's (2.5-10-50-250-1000-5000).
- Instant-vision, wider spread scales; streamlined case, handsome modern design.



New Triplett Model 630-APL

- · D.C. Polarity Reversing Switch.
- £ to 500,000 Cycles per second frequency response in A.C. measurements.
- 5000 ohms per volt sensitivity in A.C. ranges; 20,000 chms per volt D.C.

Both new testers — with the popular continued Models 630 and 630-A—offer these proved Triplett advantages:

- One switch will select any range; minimizes chance of incorrect settings and burnouts.
- Reads from .1 ohm (4.4 ohm center scale) to 100 megohms; four ranges.
- Molded circuit panel for instant component replacement.
- \bullet Models 630-APL and 630-A feature ½% resistors for greater accuracy; long mirrored scales to eliminate parallax in reading.
- Banana-type leads for low contact resistance at jacks.

! Want it?



Triplett Models 630 and 630-A read volts 0-3-12-60-300-1200-6000); or Triplett New Models 630-PL and 630-APL reading 2.5-10-50-250-1000-5000.

Choose your preference in range reading.

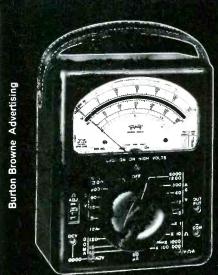
MODEL 630-PL... Dealer Net \$44.50 MODEL 630-APL. Dealer Net \$54.50 MODEL 630 Dealer Net \$44.50 MODEL 630-A..., Dealer Net \$54.50

Only Triplett offers 11 VOM's — a line complete enough to give you exactly what you want.



Triplett Electrical Instrument Co. Bluffton, Ohio

53 Years of Experience



Triplett Model 630-A





Triplett Model 630



















There will be more TANTALUM CAPACITORS for 1958 Deliveries

\$ 1957...our Golden Anniversary Year...draws to a close, we look back on a year of important achievements in our continuing efforts to serve our customers better.

In the past year, we produced more tantalum—delivered more tantalum capacitors than ever before. But still the demand for more and more tantalum continues to grow.

To keep pace with this ever increasing demand, we have made the largest capital expenditures in Fansteel history for new buildings, new research laboratories, new equipment. Only a few short weeks ago, a new tantalum-columbium plant on a 113-acre tract near Muskogee, Oklahoma, started producing metal powders and ingots.

It is interesting to note that we constructed more building space in 1957 alone than the entire Company owned in 1941.

Looking ahead to 1958, we anticipate a 100% increase in capacitor grade tantalum production.

Capacitor production facilities at the Fansteel North Chicago Plant have also been increased, all of which promises production enough to meet all normal demands for tantalum capacitors.

We sincerely regret that in the past, because of the demand, it has been necessary for us to operate under self-imposed allocation procedures. However, we are confidently looking forward to serving you in 1958 with the usual Fansteel promptness in deliveries. Even now, our enlarged and improved facilities are beginning to achieve this.

Sincerely,

Fruit N. Dieggs

President

FANSTEEL METALLURGICAL CORPORATION

NORTH CHICAGO, ILLINOIS, U.S.A.

small enough to be moved about easily. Overall dimensions are 22 by 19 by 37 in. high. Piping, pump and filter are of stainless steel with Teflon gaskets, making the unit suitable for alkaline solutions, solvents and mild acids.

The size of the tank itself is 6 by 16 by 11 in. deep, with a total working volume of 5 gallons. The transducers mounted to the bottom have a rated input of 250 r-f watt average (1 kw peak), which they convert into mechanical vibrations at 38 kc. This high-speed agitation causes cavitation in the liquid, providing a gentle but thorough scrubbing action. Even insoluble soils may be removed in minutes—sometimes seconds—and little operator attention is necessary. Circle 413 on Reader Service Card.



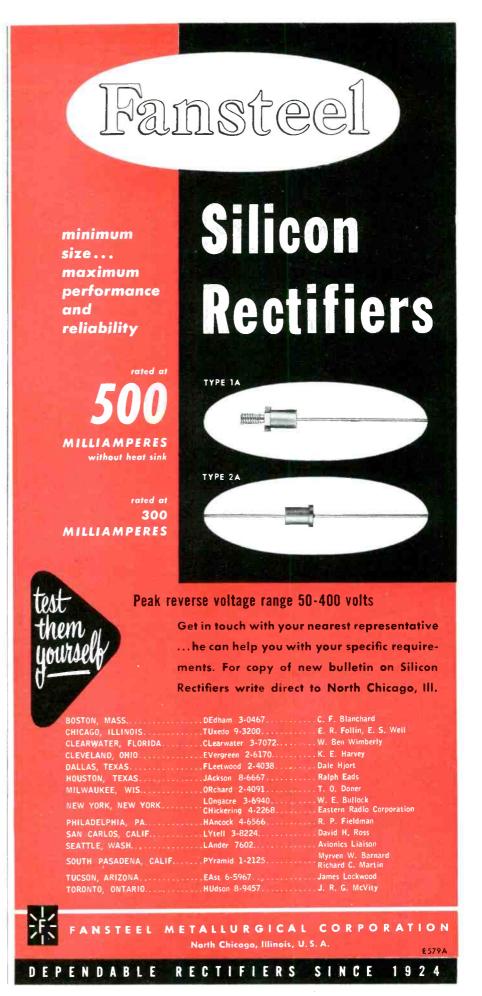
ROTARY JOINT

for microwave uses

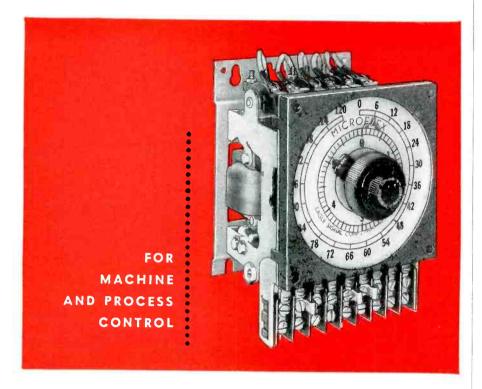
MICROWAVE ASSOCIATES, INC., Burlington, Mass. A new Ku-band rotary joint is available for use in radar and other microwave applications which require relative rotation between two waveguide members.

The MA-651 rotary joint will handle r-f peak powers close to the maximum power capability of RG-91/U waveguide. The unit may be pressurized up to 60 psig for increased r-f power handling capability. UG-419/U military standard choke flanges are used. Teflon seals keep out moisture and allow operation of the rotary joint in severe environmental conditions.

The rotary joint is fabricated from brass. Overall height from center lines of waveguide input



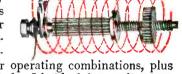
EAGLE Microflex Reset Timer



Accurate to 1 part in 1200

Time settings of pinpoint accuracy are a reality, thanks to the Microflex double dial. It takes one complete turn of the inner dial to advance the outer dial just one division. That's a 20-to-1 ratio, made possible by the patented Microflex threaded axle and pinion (see sketch). Examples of resultant accuracies are $\pm 1/60$ of a second on a 20-second dial, and \pm 1/10 of a second on a 120 second dial.

The Microflex Reset Timer is driven by a heavy-duty industrial synchronous motor. Contacts are tripped closed or open after a preset time interval. Start-



ing and resetting are electrically controlled. Microflex offers over 150 timer operating combinations, plus a wide range of long or short time periods. It's ideal for applications like molding presses, dielectric heating, automatic mixing, die casting machines, machine tools and rubber curing.

Write for free Bulletin 110.

EAGLE TIMERS SAVE TIME . . . SAVE MONEY SIGNAL CORPORATION Industrial Timers Division MOLINE, ILLINOIS

MAIL COUPON TODAY

EAGLE SIGNAL CORPORATION Industrial Timers Division, Dept. E-1257 MOLINE, ILLINOIS

Please send Bulletin 110 containing complete data on Microflex Reset Timers.

NAME AND TITLE	
COMPANY	
ADDRESS	

STATE

arms is 2.640 in. Maximum diameter is 315 in. All surfaces are silver plated. External noncontacting surfaces are painted with blue-gray lacquer. Other high power rotary joints are available in the 35 kmc frequency range. Circle 414 on Reader Service Card.



VOLTAGE DIVIDER

100:1 step-down ratio

BOONTON ELECTRONICS CORP., 738 Speedwell Ave., Morris Plains, N. J., has developed model 91-7A voltage divider adapter for use with the model 91-B r-f voltmeter to extend its voltage range and raise its input resistance. Model 91-7A is a capacitance divider with a step-down ratio of 100:1 thus converting the 0.001 to 3 v range of the 91-B voltmeter to 0.1 to 300 v. Frequency range of the divider is 500 kc to 500 mc, with self-resonance at 900 mc.

Outstanding feature is its extremely high shunt resistance approaching 100 megohms at low frequencies and in the order of one megohm at 100 mc. Shunt capacitance is 2.5 µµf. Another important feature is that the fullwave square law region of the 91-B voltmeter is thus extended permitting rms response to approximately 10 v. Circle 415 on Reader Service Card.

DELAY LINES

lumped constant type

VALOR ELECTRONICS Co., 13214 Crenshaw Blvd., Gardena, Calif. A recently introduced group of delay lines using subminiature toroidal inductors and disk capacitors in a lumped constant con-



How to keep informed on the



AT YOUR FINGER TIPS, issue after issue, is one of your richest veins of job information — advertising. You might call it the "with what" type — which dovetails the "how" of the editorial pages. Easy to read, talking your language, geared specifically to the betterment of your business, this is the kind of practical data which may well help you do a job quicker, better — save your company money.

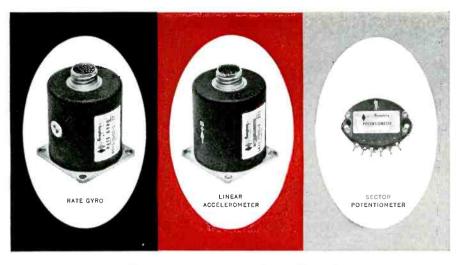
Each advertiser is obviously doing his level best to give you helpful information. By showing, through the advertising pages, how his product or service can benefit *you* and *your* company, he is taking *his* most efficient way toward a sale.

Add up all the advertisers and you've got a gold mine of current, on-the-job information. Yours for the reading are a wealth of data and facts on the very latest in products, services, tools . . . product developments, materials, processes, methods.

You, too, have a big stake in the advertising pages. Read them regularly, carefully to keep job-informed on the "with what" part of your business.



McGRAW-HILL PUBLICATIONS



Advanced Instrumentation by Humphrey

New production inertial sensing instruments for extra precision and reliability

Among the outstanding features of Humphrey's new inertial sensing instruments are: dry helium filled, hermetically sealed steel cases; standardized mountings for rate gyro and linear accelerometer; and choice of regular AN connector or new pigmy connector,

RATE GYRO is of new simplified design, with light-weight efficient motor, accurate troublefree damping, and choice of inductive or potentiometer pick-off.

LINEAR ACCELEROMETER is of dual contra-rotating mass design. It has practically zero sensitivity to cross acceleration and angular acceleration; ± symmetrical or asymmetrical ranges (0 to 1G) to (0 to 100G).

sector potentiometer is designed for precision angle measurement in minimum space. Of all-metal construction, it is used extensively in aircraft instrumentation. Resistance element is tapped with three extra connections to provide greater circuit flexibility. Suitable for angles up to 70°. Standard units suitable for operations to 350°F.

FOR COMPLETE SYSTEMS, SPECIFY HUMPHREY GYROSCOPES, ACCELEROMETERS, POTENTIOMETERS



OF THE PARTY OF TH

figuration make available all the superior features of lumped constant delay lines in a package size even smaller than distributed constant delay lines. Delay lines are available with from 50 to 10,000 ohm characteristic impedance, 0.1 to 10 μ sec delay, and up to 0.01 μ sec rise time.

Features of these lines include low distortion, low insertion loss and control of characteristic impedance and delay to as tight as 1 percent. Frequency and phase compensation for optimum pulse response across the pass band of the delay line is accomplished by a novel application of m-derived filter techniques.

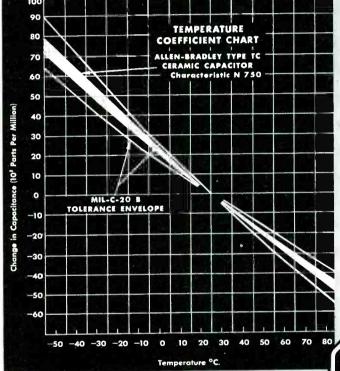
Typical delay line examples are: the 2.5C9-3/10 packaged in a \S in, metal tube one inch long having glass-to-metal end seals. This is a $\frac{1}{4}$ - μ sec delay line having a rise time of 0.07 μ sec and a characteristic impedance of 1,000 ohms. The 5C8-7/15 is a $\frac{1}{2}$ - μ sec delay line having a rise time of 0.07 μ sec and a characteristic impedance of 500 ohms and is packaged in a \S in diameter tube 3 in long. Circle 416 on Reader Service Card.



RADAR DUPLEXER for use in the KA-band

MICROWAVE ASSOCIATES, INC., of Burlingham, Mass., has developed a standard lightweight branch guide high power duplexer for pulsed radar applications in the 35,000 mc band. It is designed for

FOR SUPREME ACCURACY IN Try ALLEN-BRADLEY



You can obtain greater precision with Allen-Bradley temperature compensating capacitors . . . much more accurate than conventional units . . . more accurate than the requirements of MIL or RETMA specifications.

Allen-Bradley is able to assure this accuracy by producing its own ceramic bodies. Years of experimentation, thousands of tests, and meticulous compounding enable Allen-Bradley to provide the exact characteristics you require. The accompanying temperature coefficient curve—typical of all Allen-Bradley temperature compensating capacitors—illustrates how precisely these characteristics are maintained.

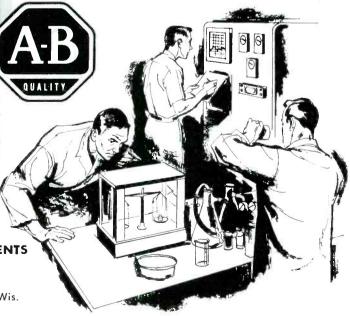
Allen-Bradley temperature compensating capacitors are available from 2.0 to 510 mmf with eleven different temperature characteristics from P-100 to N-1500 in tolerances of $\pm 5\%$, 10%, and 20%. Use these quality ceramic capacitors—they cost no more—and they will give you a more stable product.

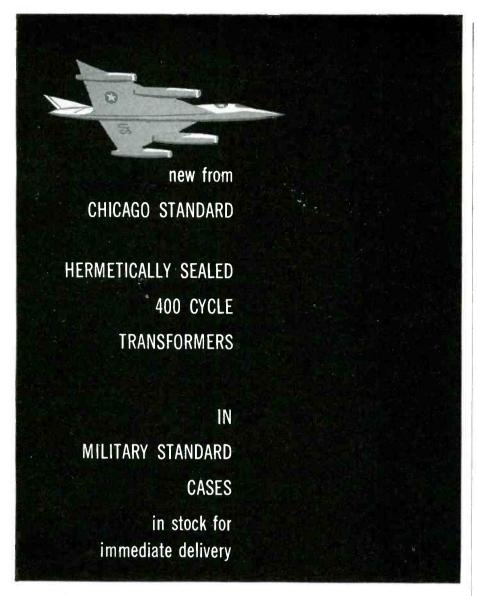
In modern laboratories, Allen-Bradley physicists conduct exacting tests on ceramic disc capacitors. The data accumulated from many thousands of tests—both electrical and physical—enables Allen-Bradley to produce ceramic disc bodies with *exact* temperature compensating characteristics.

ALLEN-BRADLEY

RADIO, ELECTRONIC, AND TELEVISION COMPONENTS

Allen-Bradley Co., 110 W. Greenfield Ave., Milwaukee 4, Wis. In Canada: Allen-Bradley Canada Ltd., Galt, Ont.





POWER TRANSFORMERS—TF4SX03* (plate and filament)
FILTER REACTORS—TF4SX03*
FILAMENT TRANSFORMERS—TF4SX01*

These transformers are designed and built in accordance with MIL-T-27A, Grade 4, Class S (85°C. ambient, 45°C. rise), operating temperature and life expectancy X (10,000 hours, minimum). Maximum operating altitude 70,000 feet. Schematics permanently silk-screened on one-piece drawn steel case.

For complete details on these new stock transformers write for the new Chicago Catalog CT3-57.



(indicate letter designations that vary with case size.)

CHICAGO STANDARD TRANSFORMER CORPORATION

3502 Addison Street • Chicago 18, Illinois
Export Sales: Roburn Agencies, Inc. 431 Greenwich St., New York 13, N.Y.

use with the 5790 TR tube and ATR-5791 (or higher power equivalents) in RG-96/U radar systems.

In a typical radar application the waveguide output flange of a pulsed magnetron such as the MA-207 is connected to the duplexer input flange by means of a magnetron-to-UG-599/U-adaptor (MA-550C). Magnetron output power is coupled to the antenna system transmission line by the UG-600/U output flange of the duplexer.

The duplexer, in conjunction with TR-5790 and ATR-5791, performs the switching operation from transmission to reception necessary in radar applications. Radar echo signals are detected in a balanced mixer (such as the MA-531) connected to the output flange of the TR-5790. Circle 417 on Reader Service Card.



TRANSDUCER with plug-in assembly

AUTOMATIC TIMING & CONTROLS, INC., King of Prussia, Pa., has developed a special transducer featuring a plug-in terminal for lead wires. The terminal assembly is mounted on the outside of the unit's stainless steel shell.

Exceptionally low null voltage of 20 mv rms (maximum) makes possible a sensitivity of 0.49 mv per 0.001 in. displacement per v input at 2,500 cps. Input is $12\frac{1}{2}$ v, 2,500 cps single ended and grounded; impedance is greater than 2,500 ohms. Output is 6.1 v per 1 in. displacement at rated excitation; impedance is less than 700 ohms. Range is ± 0.63 in. Phase angle is less than 20 deg between ± 0.01 in. and ± 0.05 in. less than 16 deg between ± 0.05 in. and ± 0.5 in.

This design was developed to re-



All business is specialized

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Here's a smart business man. He spends his time where every sitzmark parks a prospect at his feet. It's simple sense: He specializes... and it pays!

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Simplifying HF Power Measurement

Model 67 TERMALINE DIRECT-READING R-F WATTMETER

30 mc to 500 mc (to 1000 mc if specified)

50 ohms

Triple Range 0-25 watts

0-100 "

0-500

Type N Input Connector (Adaptor for PL-259 supplied)

Model 67 is a larger type Wattmeter than the well-known AN-ME-11/U (our Model 611) R-F Wattmeter. Specifically designed for fixed station transmitters to 500 watts output, it may be used nicely on low range for mobile gear. Provided with an aluminum cased, shockmounted meter, Model 67 is as simple to use as a DC voltmeter. Now in general use throughout the industry, TERMALINE Wattmeters may be depended upon for fast, accurate and repeatable power readings



NON-RADIATING

... Accuracy - 5%

RUGGED CONSTRUCTION

... Size — 17" x 9" x 6"
Wght. — 30 pounds



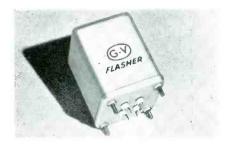
ELECTRONIC CORP. 1800 EAST 381th ST., CLEVELAND 14, OHIO TERMALINE Coaxial Line Instruments

VAN GROOS COMPANY Sherman Oaks, Call.

CIRCLE 185 READERS SERVICE CARD

Metallurgists.. Specialists in Small Wire. BASE METAL WIRES . . . Very small diameter - for filaments, thermocouples, resistance units. PRECIOUS METAL WIRES . . . Produced in Platinum, Gold, alloys and pure metals — small diameter ... Platinum alloy resistance wires. COATED WIRES . . . Comprising an extensive range of electroplated grid wires...Enamel insulated wires for precision resistors, potentiometers. ANODIZED ALUMINUM WIRE . . . Insulation at 800°F . . . Precision drawn to close resistance in the smaller sizes Write for List of Products Since 1901 Serving Industry-for Over 56 Years SIGMUND COHN CORP. 121 SOUTH COLUMBUS AVE., MOUNT VERNON, N. Y.

place a precision pot as a feedback element in the circuitry of a hydraulic servo missile vane control system. Circle 418 on Reader Service Card.



HEAVY DUTY FLASHER for aircraft and industry

G-V CONTROLS INC., Hollywood Plaza, East Orange, N. J., has available a flasher designed for long life with loads up to 2 amperes at 120 v a-c or 32 v d-c. The type BF unit combines two thermal relays and one magnetic relay, all hermetically sealed, in a circuit in which the load current is handled by the magnetic relay. The thermal relays govern the "on" and "off" portions of the flashing cycle, which is therefore unaffected by load current or load contact erosion.

The unit is suitable for aeronautical use and for industrial service. The flasher is compensated for ambient temperature variation from -65 C to +125 C. It will withstand aircraft vibration and shock requirements. It is contained in a case $2\frac{1}{16}$ in. by $2\frac{1}{16}$ in. by $3\frac{1}{16}$ in. high, and weighs 9 oz. Output contacts are spdt and are isolated from input circuit. Circle 419 on Reader Service Card.

TWIN POWER TRIODE

for heavy-duty use

TUNG-SOL ELECTRIC INC., 95 Eighth Ave., Newark 4, N. J., has developed the type 6528 twin power triode. A high current, medium mu twin triode developed specifically for series regulator service in d-c power supply units, the 6528 has been designed with high reliability features. Rugged construction has been included within

the unit in order to satisfy the most stringent requirements of heavy-duty military and commercial applications.

The 6528 was designed for use when unusual output characteristics, high reliability or long life are requirements. It makes possible a circuit having fewer components and resulting in a more efficient power supply unit. Circle 420 on Reader Service Card.



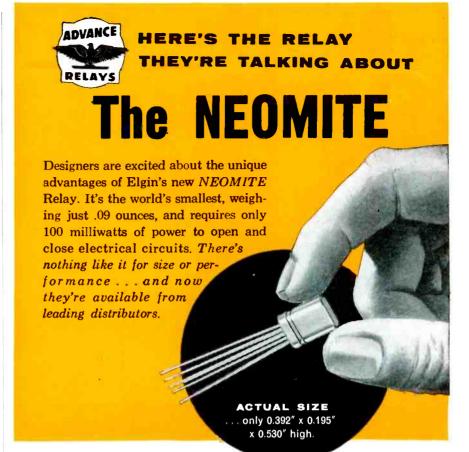
SOLID STATE BATTERY

delivers high current drains

PATTERSON, MOOS DIVISION of Universal Winding Co., Inc., 90-28 Van Wyck Expressway, Jamaica 18, N. Y., has developed a miniature, h-v solid state battery that is capable of delivering higher current drains for longer periods of time than other comparable batteries.

Called the Dynox 95, the first model of the new battery is 11 in. long, & in. in diameter, and has a potential of 95 v in 0.14 cu in. It can supply a steady current of 1×10^{-9} amperes for 176,000 hours at 70 F with only a 10-percent voltage drop, or a flash current of 20 µa. Also, it can be stored for 20 years without losing its power.

Other characteristics include resistance to extreme shock or vibration, performance at extreme temperature ranges, including the ability to operate after temperature cycling between -100 and



SPECIFICATIONS

Relay Type	NMIC 50	NMIC 200	NMIC 500	NMIC 1K	NMIC 2K
D. C. Coil Resistance (± 10% @ 20°C)	50 Ohms	200 Ohms	500 Ohms	1000 Ohms	2000 Ohms
Coil Voltage Pickup	3-5 V.D.C. 44 MA Max.	6-10 V.D.C. 22 MA Max.	9-15 V.D.C. 14 MA Max	12-21 V.D.C. 10 MA Max.	18-30 V.D.C. 7 MA Max.

Duty: Continuous Dropout: 30 to 60% of pickup Contact Rating: .25 AMP at 28 V.D.C. resistive load

Operation Time: 4 milliseconds max. @ rated voltage

Dielectric Strength: Sea level: 500 V RMS. High altitude: 500 V RMS

Shock: Shock test: 50 G. without damage

Vibration: 10 G to 500 cps Contact Arrangement: SPDT Form C

Ambient Temperature Range: -55°C to +85°C

Life: 1,000,000 operations at rated load Contact Resistance: .05 Ohms

YOU'LL FIND WHAT YOU WANT IN ADVANCE RELAY











. . . it's the most complete line of relays to meet almost every need. And they're available from stock at leading distributors all over the country. Write today for catalog information.



ELECTRONICS DIVISION

ELGIN NATIONAL WATCH COMPANY Elgin, Illinois



LESS THAN 0.07% AVERAGE CHANGE AFTER 1000 HOUR EXTREME HUMIDITY TEST

ERIE "PAC" ... THE ONLY MODULE THAT INCORPORATES PRECISION RESISTOR **ELEMENTS IN** ITS BASIC DESIGN

Through the employment of ½ watt precision film resistors, ERIE has added to its line of "PAC" modules and greatly widened the field of effective "PAC" applications.

"PAC" Pre-Assembled Components

have proven immensely popular with manufacturers of home and auto radios, TV sets, electronic organs, and

other equipment.

The new "PAC" units incorporating deposited carbon resistors, are highly resistant to humidity, and offer high reliability for precision military and industrial applications. They have been thoroughly proven in severe humidity tests in which they with-stood 1,000 hour exposure with an average change of less than 0.07% and maximum change of 0.19%.

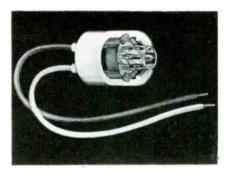
Samples will be submitted for your

own trial tests and applications.



170 F. It is hermetically sealed.

The battery has a functional place in modern electronics systems where miniaturization and reliability of performance in extreme environments are required. These applications include power sources in missiles, avionics, alarm systems, instrumentation—such as computers-and telemetering as well as capacitor charging applications. Circle 421 on Reader Service Card.



MAGNETRON CONNECTOR

for space saving design

JETTRON PRODUCTS, Route No. 10, Hanover, N. J. An improved magnetron input connector has the normally exposed metal parts encased in silicone to permit space saving in the power supply design. This assembly will fit any of the following magnetrons: 4J50, 4J52A, 6551 and 6865.

The heater-cathode contact is made of heat treated beryllium copper, heavily silver plated and has eight contact springs making contact with the tube. The heater contact is floating in a silicone rubber insulator which prevents undue strain on the tube input end. All internal connections are made with a high temperature alloy solder and friction contacts have been eliminated. The lead wires are insulated with Silastic 80 so that the connector may be operated at very high temperatures without failure.

Catalog No. 9000-C has a 4,000 μμf minimum capacitor built into the connector. Catalog No. 9000 is made without the capacitor, and is identical in outline dimensions. The body of the connector is 14 in. long and 13g in. in diameter. A red lead identifies the heater connection and a white lead identifies the heater-cathode connection. The standard lead length is 12 in. with in. stripped and tinned. Circle 422 on Reader Service Card.



CRYSTAL OSCILLATORS

are transistorized

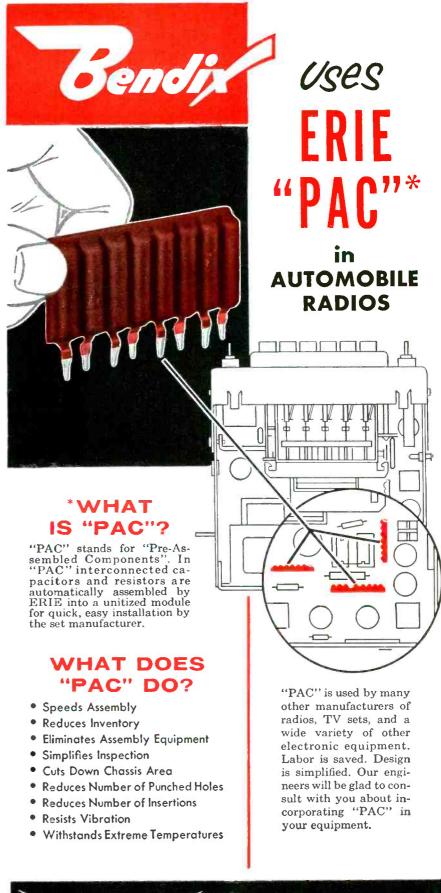
REEVES-HOFFMAN DIVISION of Dynamics Corp. of America, Carlisle, Pa. New crystal-controlled oscillators, available over a frequency range of 4 kc to 250 kc, are transistorized for compactness. Length (seated) is 5½ in.; diameter 13 in. These ruggedly built oscillators are capable of surviving shock of 100 g's and withstanding vibration of from 5 to 55 cycles at 0.030-in. total excursion. Output power is 600 µw. Frequency stability is ± 0.015 percent over an ambient temperature range of from -40 C to +60 C. Over the same range of operating temperature, output level stability is ± 2 db from the 25 C level. The oscillators are mounted in a plug-in octal base. Circle 423 on Reader Service Card.



POWER RESISTOR

miniature precision type

MEPCO, INC., Morristown, N. J. Type P-1 is a new addition to the line of precision power resistors







YOUR BEST BUY

It is made of the highest quality acid-free kraft paper and the finest electrical-grade resins obtainable.

The processing cycles allow ample time for proper curing, ensuring uniformity and good machinability.

It is available in the diameters, wall thicknesses and lengths you may require.

It is subjected to a thorough and rigid inspection.

This know-how and careful workmanship are the result of many years' experience.

You can depend upon prompt, reliable service at all times.

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ABRASIVE DIVISION OF CLEVELAND, OHIO Cleveland Container Canada, Ltd., Prescott and Toronto, Ont.

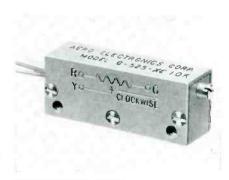
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NEW YORK AREA: R. T. MURRAY, 604 CENTRAL AVE., EAST ORANGE, N. J. NEW ENGLAND: R. S. PETTIGREW & CO., 62 LA SALLE RD., WEST HARTFORD, CONN. CHICAGO AREA: PLASTIC TUBING SALES, 5215 N. RAVENSWOOD AVE., CHICAGO

WEST COAST:

IRV. M. COCHRANE CO., 408 S. ALVARADO ST., LOS ANGELES

manufactured by the company. It meets the requirement of MIL-R-26C, style RW 59, characteristic G. One percent is the standard tolerance but it is also available in tolerances down to 0.1 percent on special order. The resistor is rated at 2.5 w at 70 C derate to zero at 275C. Temperature coefficient is 0.002 percent per deg C; length, ½ in.; diameter, ¼ in. Circle 424 on Reader Service Card.



TRIMMING POT sealed miniature type

ELECTRONICS CORP., 2311 West Burbank Blvd., Burbank, Calif., is in production on a sealed miniature trimming potentiometer which withstands severe environmental conditions. The unit has a metal body and cover, both "U" shaped, with the cover precision fitted to the body for protection against humidity, splashing and dust. For further protection, the unit is epoxy sealed around the cover and around the leads where they emerge from the case, and a silicone O-ring is placed behind the leadscrew opening. This construction is designed to meet pertinent Mil Specs with reference to humidity requirements.

Built for critical applications, the unit is unusually rigid, and resistant to twisting, impact and breakage. Designated Aero-Pot G-720 series, it is adjustable throughout 32 turns by a screwdriver in a slotted shaft.

Case dimensions are 11 in. long, in, high, in, wide. Weight is 4 oz. Resistance range is from 100 ohms to 100,000 ohms in one case size. Resolution, depending on resistance is 0.2 to 2 percent. Linearity is 1 percent. Temperature range is -55 C to +175 C. Units

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are supplied with Teflon insulated wire leads or plug-in terminals. Circle 425 on Reader Service Card.



TEST GAGES readings up to 15,000 lb

MARTIN-DECKER CORP., 3431 Cherry Ave., Long Beach 7, Calif., has developed a new series of precision test gages. An improved technique in the manufacture of the Bourdon tube, coupled with an advanced design movement, makes possible a 360 deg calibration. A 12 in. 360 deg calibrated gage provides the same readability obtained in a 16 in. 270 deg dial.

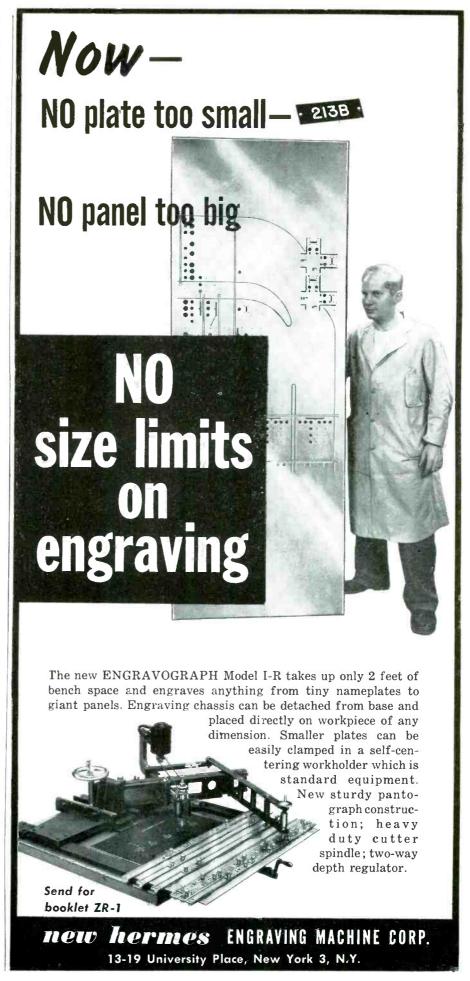
Test gage performance has been improved to permit readings up to 15,000 lb. Guaranteed production calibration is 0.15 percent full scale accuracy. Flush, wall, or stem mount is available. Sizes range from 60 psi to 15,000 psi. Circle 426 on Reader Service Card.



PRECISION POTS

two new types

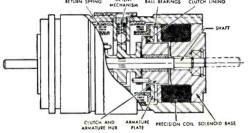
INTERNATIONAL RESISTANCE Co., 401 North Broad St., Philadelphia





The Syncramental Motor accurately translates pulses to incremental shaft position for conversion of digital information to analogous shaft displacements. Compact, long-life power can rotate potentiometers, counters, rotary switches, control mechanisms.

A special magnetic clutch mechanism, rather than ratchets, indexes the shaft. Clutch and detent mechanism are mounted between two LEDEX Rotary Solenoids whose armature plates face each other. Clutch rotates with one or the other of the energized armatures, to which it has been



magnetically attracted, causing shaft rotation. Solenoid de-energizing returns the armature to original position, but clutch and shaft are held in displaced position by the detent.

PERFORMANCE:
Angular increment per pulse—36° (either direction). Detent accuracy—±1/2° under no load conditions. Maximum stepping rate—15 per second. Load capacity—up to 2 lb. in. starting torque at 20°C. Life expectancy—2 million steps in either direction.

ENVIRONMENTAL CONDITIONS:

ENVIRONMENTAL CONDITIONS:

Temperature—minus 55°C. to 120°C. Altitude—up to 90,000 ft. Meets applicable requirements of MILE-5272A.

ments of MIL-E-52/2A.

SIZE, MOUNTINGS:
Dimensions—1.500" dia. x 2.525" long. Weight—13 oz. Mountings—standard Servo.

White today for complete data ...

G.H. Leland



123 WEBSTER STREET, DAYTON, OHIO IN CANADA: Marsland Engineering Ltd., Kitchener, Ontario IN EUROPE: NSF Ltd., 31-32 Alfred Place, London, England 8, Pa., has added two new precision potentiometers, types HA-100 and HA-105 to its product line. Available in 5 and 10-turn types, these units feature very short case lengths— $\frac{1}{16}$ in. on 5-turn model and $1\frac{1}{16}$ in. on 10-turn. Encased in grade XX laminated phenolic with a polished natural finish, the units can be furnished with flexible silver plated terminals riveted to case, or with rigid turret-type terminals. Standard linearity is ± 0.5 percent.

Type HA-100, rated at 2 w, features rotation of 3,600 deg, -0 deg +4 deg. Standard resistance values are from 2,500 to 75,000 ohms. Type HA-105 is rated at 1.5 w and has rotation of 1,800 deg, -0 deg +4 deg. Standard resistance values are 1,000 to 25,000 ohms. Circle 427 on Reader Service Card.



MINIATURE R-F TUBE

with internal shield

AMPEREX ELECTRONIC CORP., 230 Duffy Ave., Hicksville, L. I., N. Y., has available the new ECC85/ 6AQ8, a miniature, high-mu, high transconductance twin triode. It has been specifically designed for use in a-m and f-m receivers as a grounded-grid or groundedcathode r-f amplifier and as a selfoscillating frequency converter or cascode amplifier. Through the use of an internal shield, separating both triode sections, the ECC85/6AQ8 reduces oscillator radiations from the antenna of the receiver to an extent not obtainable with previously available

twin-triodes. Higher transconductance permits increased front-end gain and lower noise. Circle 428 on Reader Service Card.



INDUCTION MOTOR

60-cycle unit

EASTERN AIR DEVICES, INC., 385 Central Ave., Dover, N. H. A new, 60-cycle induction motor has been announced for fan and blower drive or general purpose induction drive motor applications. A one-inch diameter unit, it operates off the 115 v, 60-cycle line directly—without the use of step down transformers or dropping resistors.

With a stall torque of 0.7 oz in. and a running torque of 0.4 oz in., the new motor can get more air from bigger fans than other components of its type. High starting torque means especially good reliability at low temperatures where bearing friction becomes important.

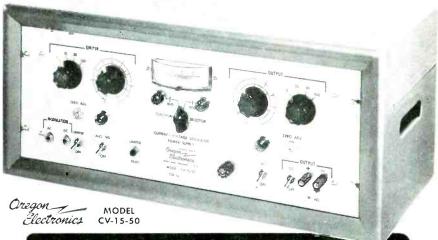
As an example of its power-capacity, the new unit can drive a 3-in. fan blade at 3,200 rpm, or a 4-in. fan blade at 2,700 rpm with only 6 w input. Circle 429 on Reader Service Card.

CLUTCHES

and clutch brakes

STERLING PRECISION CORP., 34-17 Lawrence St., Flushing 54, N. Y. A group of reverse acting electromagnetic clutches and clutch brakes have been added to the company's line of precision servo components. These units differ from the conventional types in that the input and output shafts





for TRANSISTOR ENGINEERING

For the first time you can have a power supply that will protect transistors from overload... both voltage and current! Set for maximum voltage on the limiter control and the output power will be interrupted before the limit is exceeded. (An audible or visual alarm can also be used). When used for regulated voltage supply, the system becomes a current limiting circuit.

SPECIFICATIONS

INPUT: Nominal 117V, 50-60 cycles.

OUTPUT: Voltage regulated ranges—0-5; 0-15; 0-50; 0-150 volts and Current regulated ranges of 0-15; 0-50; 0-150; 0-500 milliamperes. Output floating or either positive or negative grounded.

REGULATION: Voltage—better than 0.05%. Current—better than 0.2%.

RIPPLE: Voltage—Less than 2mv peak-peak. Current—Less than 2mv peak-peak across 100 ohm load.

LIMITER: Provides visual and audible alarm or visual and cutout as selected.

Same ranges as output. Adjustable by means of panel control.

MODULATION & EXTENDED CONTROL: Plugging jacks provide for external

MODULATION & EXTENDED CONTROL: Plugging jacks provide for external modulation or adjustment of current regulated output and extended or remote adjustment of voltage output.

METER: Dual range 5-15 and multipliers.

PANEL: Anodized aluminum—natural or satin black. Standard rack width, 7" high.

CABINET: Heavy gauge steel tinished in silver grey smooth baked enamel.



Write for complete information

2105 S. E. SIXTH AVE. PORTLAND 14, OREGON BElmont 6-9292

MANUFACTURERS OF SPECIAL ELECTRONIC EQUIPMENT

COLOR TV Shadow Masks

—A development of BUCKBEE MEARS through close cooperation with TV industry engineers. Containing 400,000 close tolerance holes (.010" ± .0005").

Now produced in quantity on our especially designed continuous etching machines.



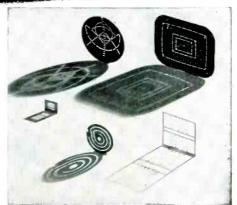
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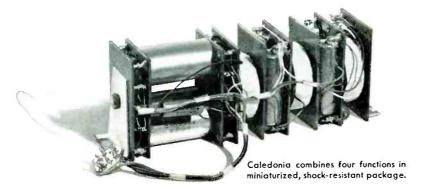
ETCHED AND ELECTRO-FORMED PRECISION PARTS

-- Electric shaver combs, metal reticles for optical instruments, fine tube mesh and code discs.

These are but a few of the variety of parts that can be quickly produced to precise tolerances by our specific problem and specifications to our engineers.



CIRCLE 194 READERS SERVICE CARD



Electronics today is partly packaging

PROBLEM: Design a small (50 cubic in.) and light (3¾ lbs.) unit that contains: 1. a positive d.c. pulse selector

- 2. a negative d.c. pulse selector
- 3. a high level 60 cps band pass filter
- 4, a 400 cps detector circuit
- (all with tight tolerances, naturally).

Design it to operate within the usual military environmental conditions, including high vibration and shock.

SOLUTION: We assembled the components shishkabob style. Then mounted the

kabob in a metal case filled with an epoxy foam compound to hold the parts in a firm cushion.

TIME ELAPSED: From original assignment, through design to volume production—two months.

If such quick, dependable assistance in design and production can make your work more effective, we'll be glad to hear from you. We offer experience, good production facilities, and a recognized quality record.

CALEDONIA

ELECTRONICS AND TRANSFORMER CORPORATION

Dept. E-12, Caledonia, N.Y. • In Canada: Hackbusch Electronics, Ltd., 23 Primrose Ave., Toronto 4, Ont.



are coupled when the coil is deenergized. Energization of the coil uncouples the shafts and applies the brake to the output shaft if a brake is required. This mode of operation results in conservation of power in many applications. Coupling faces may be supplied flat or with crown teeth resulting in a wide range of torque transmission abilities. Braking surfaces are flat and are rated 8 oz in. minimum torque. Circle 430 on Reader Service Card.

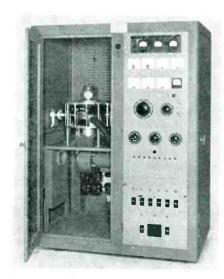


TEST-POINT JACKS are micro-miniaturized

SEALECTRO CORP., 610 Fayette Ave., Mamaroneck, N. Y. Types SKT-13 and SKT-14 are approximately one-third and one-half, respectively, the 0.637 in. overall length of the SKT-10 miniature test-point jack.

Taking a 0.040 in. pin, the SKT-13 measures only 0.203 in. overall length including turret lug, by 0.140 in. straight-sided bushing diameter. The SKT-14, taking a 0.060 in. pin, measures 0.345 in. overall length including lug, by 0.148 in. bushing diameter.

Both types feature machined beryllium-copper contact members with gold flash over silver-plate finish. The ideal Teflon insulation provides a voltage rating of 750 rms and flashover of 3,000 at sea level, or 1,300 at 50,000 ft, in a temperature range of -65 to +200 C. The SKT-14 is readily, quickly and permanently press-fitted in drilled or punched metal-chassis holes up to 0.140 in. chassis thickness, by means of a simple insertion tool available from Sealectro, used with drillpress or arbor type equipment. They come in a choice of eight RETMA code colors. Circle 431 on Reader Service Card.



TRANSMITTER

1-kw klystron unit

LEVINTHAL ELECTRONIC PRODUCTS, INC., Stanford Industrial Park, Palo Alto, Calif. Model 74T transmitter produces 1 kw of c-w power over the band 1,700 to 2,400 mc. It utilizes an Eimac 3K2500SG klystron with a power gain of 25 db.

The transmitter consists of a beam-power supply, focus-electrode supply, klystron-filament supply, three focus-magnet supplies, and all required controls, meters, interlocks, indicators and so forth to comprise a complete system. The unit is packaged in a single cabinet with connections available for input and output r-f and a-c power.

Incidental f-m is below 5 cps. With proper modulation of the r-f drive, the unit is capable of a-m, f-m, fsk, or ssb modulation. The equipment requires about 10 kva of power from a 208-v, 3-phase.

DECADE RESISTANCES



DECADE BOX ... with precision wirewound resistors mounted on steatite-insulated switches. TEN resistors per decade ... giving better than 0.1% accuracy above 10 ohms.

- 4				lotai	
-1	Type	Dials	Ohm Steps	Resistance—Ohms	Price
- 1	817	3	0.01	11.1	\$60.00
	818	3	0.1	111	51.00
۲	820 821	3	1,1	1,110	56.00
Ħ	822	3	10 100	11,100	60.00
	823	1 7	1.000	111,000 1,110,000	63.00 77.00
ı	824	33333333	10,000	11,100,000	120.00
	817-A	4	0.01	111.1	75.00
	819	4 4 4	0.1	1,111	71.00
7	825	4	.1	11,110	77.00
1	826 827	4	10	111,100	79.00
-	828	4	100 1,000	1,111,000 11,110,000	92.00
ŀ		_			139.00
-	8285 829	5	0.1	11,111	94.00
1	830	5	10	111,110 1,111,100	101.00 113.00
-]	831	5 5 5	100	11,111,000	155.00
ı	817-C	6	0.01	11.111.1	105.00
1	8315	6 6 6	0.1	111.111	109.00
1	832	6	1	1,111,110	121.00
L	833	6	10	11,111,100	169.00



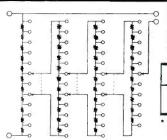
UNMOUNTED DECADE

Туре*	Dials	Ohm Steps	Total Resistance—Ohms	Price
435	1	0.1	_1	\$12.00
436	1	1	10	13.25
437	1	10	100	13.25
438	1	100	1.000	15.00
439	1	1,000	10,000	16.00
440	1 1	10,000	100,000	18.50
441	1 1	100,000	1,000,000	32.50
442	1	1,000,000	10,000,000	60.00

* Knob (#M-25594) not included. Available at additional cost.

Shallcross

DECADE Voltage dividers



. . . same quality construction as in Decade Resistances. Choice of Kelvin-Varley or conventional potentiometer circuits.

KELVIN-VARLEY CIRCUIT

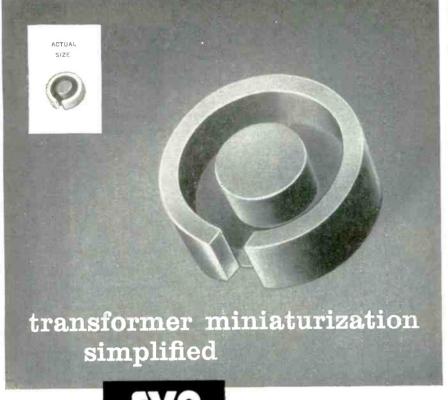
Туре	Dials *	Input Resistance (Accuracy ±0.05%)	Price
8350	4	10.000	\$140.00
8349	4	50.000	145.00
8348	4	100,000	150.00

* RESOLUTION—Any ratio between 0.0000 and 1.0000 in steps of 0.0001.

POTENTIOMETER CIRCUIT

₩₩₩a -₩₩₩a -₩₩₩a	Туре	Dials	Ohm Steps	Total Resistance (Accuracy ±0.1%)	Price
	837 835 836	4 4 4	0.1 1.0 10.0	1,000 10,000 100,000	\$126.00 139.00 146.00
-mmy mmy mmy	849 848	5	0.1 1.0	10,000 100,000	165.00 176.00

SHALLCROSS MANUFACTURING COMPANY, 522 Pusey Avenue, Collingdale, Pa.

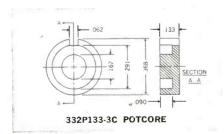


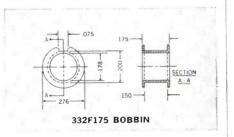
with



micro-miniature potcores

Made of Ferroxcube 3C material, the No. 332P133-3C potcore by FXC is less than 3/8" in diameter and successfully eliminates pulse transformer problems created by limitations in weight and space. The coils for this potcore are wound on a specially designed nylon bobbin. The shape of the potcore, combined with the high-permeability material surrounding the windings, gives excellent shielding and effectively minimizes stray fields. The potcores can be placed close together or even stacked, with negligible coupling between coils.





Requests for literature and engineering samples should be made on your company letterhead and addressed to:

Applications Engineering Department
FERROXCUBE CORPORATION OF AMERICA
(A subsidiary of North American Philips Co., Inc.)
50 South Bridge Street, Saugerties, New York

4-wire, 60-cps source. Circle 432 on Reader Service Card.



CONVERTERmatches ER-90 X-Y plotter

MANDREL INDUSTRIAL INSTRUMENTS, Division of Mandrel Industries Inc., P. O. Box 13243, Houston, Texas, is now marketing a polar Cartesian coordinate converter priced at \$390. Model ER-95 converter was designed specifically to match the ER-90 X-Y plotter. It is applicable, however, anywhere conversion from polar to Cartesian coordinates is required. Conversion is achieved by a sine-cosine pot linked to a nullseeking servo. The value of "R" impressed across the pot is therefore resolved into its quadrature components according to the position of the pot, this position being determined by the θ input. Speed of pot positioning is 360 deg per sec and θ sensitivity is 0.5 mv d-c per deg. Power required by the self contained power supply is 50 w at 115 v, 60 cps. Overall size is 6 in. by 7 in. by 19 in. and the unit may be either rack mounted or used as a bench instrument. Circle 433 on Reader Service Card.



ELECTROLYTICS

tantalum foil type

OHMITE MFG. Co., 3653 Howard St., Skokie, Ill., has developed a line of high quality, tantalum foil, electrolytic capacitors, and is producing these in limited quantities for engineering evaluation and use. Carrying the trade designation "Tan-O-Mite", a designation which also applies to Ohmite's tantalum wire units, the series TF capacitor features the extraordinary shelf and operating life, stability and greater capacitance per unit volume that is characteristic of tantalum metal units. Wide operating temperature range (-55 C to +85 C) is another feature of these capacitors.

Supplied in sealed metal cases in three sizes the Series TF units collectively offer a capacitance range of 0.25 to 140 μ f. Working voltages up to 150 v are available.

Polar Tan-O-Mite capacitors are provided for d-c application where reversals of potential do not occur, and non-polar units where reversals do occur or for a-c applications of limited voltage. Circle 434 on Reader Service Card.



TRANSDUCER

nals by filtering.

operates from —90 F to +275 F G. L. COLLINS CORP., 2820 E. Hullett St., Long Beach 5, Calif. New design of a telemetering position transducer provides a frequency change of 4.0 percent in the associated oscillator circuit with each inch of shaft movement. The new unit forms the inductive portion of a Hartley type oscillator employing a single triode tube. Output signals of up to 10 transducers can be mixed and transmitted on a single channel to a remote receiver which will separate the signals.

The unit operates with a center frequency from 900 cps to 6,000 cps. Frequency change is linear within 1 percent over a stroke of 3.2 in. and frequency drift with



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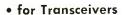
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- for Receivers
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Compact, lightweight units specifically designed to convert battery voltage DC to high voltage DC in two-way radios, public address amplifiers, or wherever conventional power supplies are used. UAC units are rugged, vibrationresistant converters that outlast vibrator power supplies by thousands of hours. No moving parts . . . No wear . . . No tear . . . No arching.

SPECIFICATIONS					
TRANSCEIVER SUPPLY	RECEIVER SUPPLY				
INPUT: 12 VDC*	12 VDÇ or 13.6 VDC*				
OUTPUTS: 450 VDC @ 255 MA	250 VDC @ 130 MA				
275 VDC @ 150 MA — 55 VDC @ 5 MA	290 VDC @ 130 MA				
TEMPERATURE RANGE: — 55°C to +71°C	−55°C ta +71°C				
EFFICIENCY: 85%	85%				
SIZE: 31/2"x5"x3"	23/4"x23/4"x23/6"				
WEIGHT: 31/2 lbs.	8 oz.				
LIST PRICE: \$85	\$45				
*For Railroad Applications Same Specifications with	s: n 64 to 72 VDC Input at				





additional cost.





Dept. E127

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Westbury, L. I., N. Y.

Cable Address: UNIVATOMS

temperature is less than 0.1 percent per 100 F. Harmonic content is less than 1 percent. The new transducer has an operating temperature range of -90 F to +275F, is 6.5 in. long and weighs 8.2 oz. Circle 435 on Reader Service Card.



DIGITAL INSTRUMENTS

feature in-line readouts

ZINN INSTRUMENTS, P. O. Box 733, Lomita, Calif., has announced a complete line of digital instruments including digital voltmeters, ohmmeters, frequency meters and ratiometers. All units feature in-line readouts, small size, twoway tracking if desired, and plug-in packaging of all tubes and stepping switches.

The unit illustrated is a threedigit volt-ohmmeter with an accuracy of one digit on d-c volts and ohms, and 1 percent on a-c volts. Overall size is 3½ in. by 19 in. by 11 in. Some four digit models fit into this same package with an accuracy up to 0.01 percent. Circle 436 on Reader Service Card.



INDICATOR

shows elapsed time

DEJUR-AMSCO Corp., 45-01 Northern Blvd., Long Island City 1,

N. Y., has available the series HD-656 sealed elapsed time indicator. This $2\frac{1}{2}$ in diameter meter is enclosed in a housing which meets military specifications, and has five, easy-to-read digit counters that register 1/10 minute or 1/10 hour increments to 9,999.9, or hour steps to 99,999. It provides a check on operating times of machine tool, electronic and similar equipment to insure proper maintenance and replacement at desired intervals.

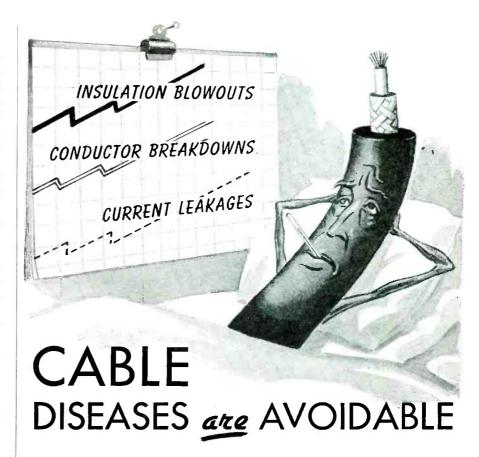
The unit is equipped with a self-starting synchronous motor for 110-125 v, 60 cycles a-c, and capable of operating continuously from -55 C to +85 C. Sealed housing is a combination of sturdy drawn steel case and die cast aluminum mounting flange. Sealed solder lugs are also standard.

Complete specifications and outline drawing are available. Circle 437 on Reader Service Card.



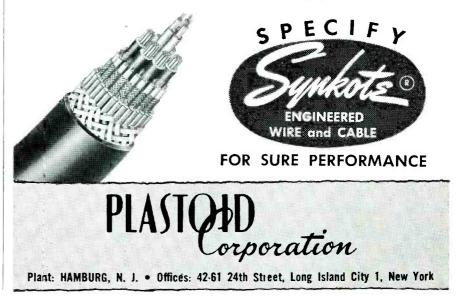
PRECISION POT linear or nonlinear

WATERS MFG., INC., Boston Post Road, Wayland, Mass. Resistance values from ½ ohm to 500,000 ohms with standard linearity of 0.5 percent are available in the modern WP1-5 precision potentiometer. Linearities to 0.1 percent are possible as well as top conformity for nonlinear designs. The potentiometer is contained in an anodized aluminum case 15 in. in diameter and 132 in. deep behind the panel. Turret type terminals mounted on a fungusproof insulating strip of high-impact Epon-glass laminate are provided for circuit connection. Servo or 3-hole mounting are

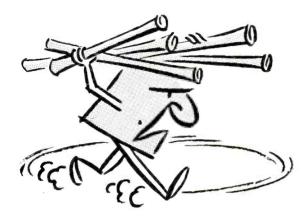


Synkote engineered and constructed cables are free of these ills. Long life, quality and performance are assured by ample insulation thicknesses, proper compounding, uniform and adequate conductors and constant continuity testing.

Whether it be a few or a hundred conductors, whether they be braided, wrapped, foiled, striped or jacketed you will find our engineers have the know-how requisite to the production of faultless high-quality multi-conductor cable to meet the most exacting specifications.



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can develop and make your miniature assemblies

When your designs require miniature or sub-miniature assemblies in volume, Waltham facilities are the answer to your problems. At Waltham you'll find the specialized tools—many made in our own shops to meet specific needs—and the highly skilled people with long experience in operating them.

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The same ingenuity that gave the new Waltham Vertical Gyro its superior performance characteristics can be applied to resolving the production problems facing you.

A Waltham engineer is well qualified to talk to you about mechanical or electromechanical assemblies. Ask him to call on you—or send us your drawings and specifications.

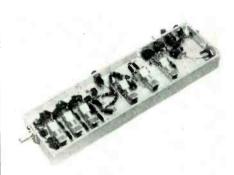
WALTHAM PRECISION INSTRUMENT COMPANY
FORMERLY WALTHAM WATCH COMPANY

WALTHAM 54, MASSACHUSETTS

PRECISION HAS BEEN OUR BUSINESS SINCE 1850

standard; bushing mount is also available, in a case 35 in. deep.

Shaft diameter for both models is ½ in. Standard resistances are 50, 100, 200, 500, 1,000, 2,000, 5,000, 10,000, 20,000, 25,000, 40,000 50,000 and 100,000 ohms; ranges beyond these are furnished on special order. A data sheet is available. Circle 438 on Reader Service Card.



I-F AMPLIFIER

afc unit

LEL, INC., 380 Oak St., Copiague, L. I., N. Y., has added a new subminiature afc unit to their line of missile and radar amplifiers. This unit, designed for use in a 0.1 µsec pulse system, contains in one chassis all the elements required for afc purposes such as the i-f amplifier, diode phantastron, and an internal control for manual tuning of the LO. A sweep frequency of 3 cps and a sweep output of 45 v at an adjustable level of 115 to 195 v is also provided. Overall dimensions are 111 in. by 3½ in. by 1 in., including controls. Circle 439 on Reader Service Card.

DUAL CHANNEL ANALYZER

counts at 200,000 per sec

Franklin Electronics, Inc., Dept. 421, Bridgeport, Pa., has introduced a new dual channel pulse height analyzer which provides 200,000 counts per sec in the range of 3 to 140 v. Model 405 makes possible studies of the amplitude distribution of voltage pulses within its specified range. Providing for both integral and differ-

ential spectrum analysis, it also enables studies of energy distribution of nuclear particles when used with a linear amplifier or scaler.

Model 405 contains two completely isolated single channel pulse height discriminators operated from a regulated power supply. Pulse height zero drift is only 0.05 v per week with regulated voltage. Slit width (window) is 0 to 10 v. Dead time is 1.0 µsec. Circle 440 on Reader Service Card.



PRECISION POTS in 5 and 10-turn models

INTERNATIONAL RESISTANCE Co., 401 North Broad St., Philadelphia 8, Pa., has added two new precision potentiometers, types HC-100 and HC-105, to the product line of its St. Petersburg, Fla.

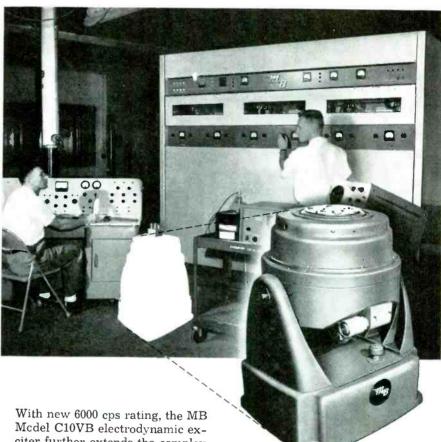
subsidiary, Circuit Instruments, Inc.

Available in 5 and 10-turn models, these units feature side terminals, shorter internal lead length and lower end resistance. Encased in grade XX laminated phenolic with a black mirror finish, they are a slim 1 in. in diameter. Standard linearity is ± 0.5 percent.

Type HC-100 features 3,600 deg, -0 deg +4 deg rotation and is rated at 4 w. Its weight is 2.3 oz and standard resistance values range from 500 to 100,000 ohms. Type HC-105, which weighs only 1.8 oz, has a rotation of 1,800 deg, -0 deg, +4 deg and is rated at 3 w. Standard resistance values are from 250 to 50,000 ohms. Bul-

6000 cps

-a new high in frequency from a high force vibration exciter system



Mith new 6000 cps rating, the MB Mcdel C10VB electrodynamic exciter further extends the complex motion testing range . . . yet delivers 1750 pounds force for sinusoidal testing with an MB Model T666 15 KVA amplifier (36,000 watt plate dissipation).

This is versatile equipment. With an MB T666 amplifier and TEMC control cabinet, it has the "muscle" to subject electronic products and other critical components to accelerations up to 58 "g". Adding an MB T88 Complex Motion Console equips it for duplicating the actual "noise" or random motion of the environment. This system is designed with an eye to future needs.

What's more, the exciter works in environmental test chambers.

so that vibration can be combined with heat, cold, altitude. This not only saves test time, but gives more realistic data on performance as well.

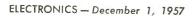
MB C10VB Exciters have UNIMODE rocker suspension (pat. pend.) which assures linear motion and a uniform spring rate over the total stroke of 1-inch (double amplitude).

Users of MB test equipment have at their call a nationwide field service organization of vibration specialists to help on application problems. Send for full data on the complete line MB Shakers.

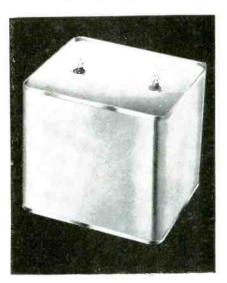
MB manufacturing company

A DIVISION OF TEXTRON INC.

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HEADQUARTERS FOR PRODUCTS TO ISOLATE ... EXCITE ... AND MEASURE VIBRATION



letin A-5A is available. Circle 441 on Reader Service Card.



TEFLON CAPACITORS

values from 0.001 to 10 μf

DEARBORN ELECTRONIC LABORATO-RIES, 1421 North Wells St., Chicago 10, Ill., has available a comprehensive line of Teflon capacitors. This dielectric is noted for its exceptional electrical properties from -55 to +200 C. Minimum insulation resistance is one million megohm-microfarads at 25 C and 1,000 at 200 C. Capacitance change over the entire temperature range is less than 4 percent. Dielectric absorption is second only to polystyrene. Dissipation factor reaches a maximum of about 0.2 percent at 200 C. Capacitance values from 0.001 to 10 μf are available in hermetically sealed metal tubes or drawn rectangular cans. Standard voltages are 200, 400 and 600. Circle 442 on Reader Service Card.

BROADBAND ABSORBER

reflection cut down

B. F. GOODRICH SPONGE PRODUCTS DIVISION, Shelton, Conn. A 10-to-1 decrease in reflection of its standard 12CM broadband microwave absorbent material for simulating free space conditions indoors has been announced by the company.

The material is now available with a maximum of 0.1-percent reflection above 8,400 mc. This de-



(continued)

crease in reflection at X-band, where most missile guidance and fire control systems operate, is designed to allow more accurate testing of such systems in indoor freespace chambers.

Other absorbers are available with a maximum of 0.1-percent reflection at lower microwave frequencies. Maximum reflection of the standard 12CM broadband absorber remains less than 1 percent from 2,500 to 8,400mc and less than 1 per cent over the same frequency range for a selected 12CM material. Circle 443 on Reader Service Card.

NPN TRANSISTORS

four new types

GENERAL TRANSISTOR CORP., Jamaica, N. Y., has available four new germanium alloyed junction transistors, types 2N444, 2N445, 2N446 and 2N447. Of the *npn* variety, these transistors are especially useful for small signal amplifier and high speed switching applications. The four units offer alpha cutoff frequencies ranging from 0.5 to 9.0 mc and small signal current gain ranges from 15 to 125.

This brings to sixty-nine, the number of different transistors commercially available from the company. Circle 444 on Reader Service Card.

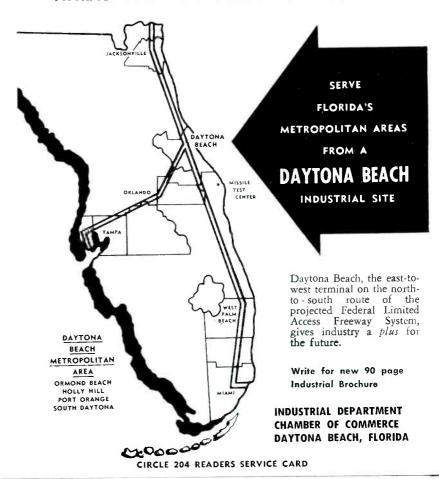


CRYSTAL FILTER

features miniature design

BLACKHAWK ENGINEERING, 1912 Woodruff Ave., Janesville, Wisc. Selectivity of the order attained by several cascaded double-tuned i-f stages in the 200-500 kc range

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permitting heavier Rhodium electroplate than ever before possible. The photograph shows a film of Rhodium plate, produced with RHODEX, from which the basis metal was dissolved. Note the continuous unimpaired surface. We tried this experiment with leading competitive Rhodium formulations — the plate fell to pieces at a touch of the pencil. No special "know-how" — you can duplicate this demonstration in your own laboratory, with RHODEX. No cracking, no peeling...even in thickness exceeding one thousandth of an inch. Send for details.

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has been attained in a miniature crystal filter.

Double conversion is no longer required in many communications receiver designs, since both image frequency rejection and adjacent channel selectivity may now be provided, utilizing a single i-f of 3 mc. It provides better than equivalent performance with fewer tubes.

The unit is hermetically sealed. hence environmental stability is assured. Since the response curve is crystal-controlled no tedious i-f alignment is required. Filters are also available to custom requirements in the 3 to 15 mc range. Circle 445 on Reader Service Card.

PULSE GENERATOR

wide-range unit

BURROUGHS CORP., Electronic Instruments Division, 1209 Vine St., Philadelphia 7, Pa., has announced a new wide-range pulse generator, the type 1006.

The unit produces a stable source of pulses in eight overlapping frequency ranges up to 4.5 mc. Its output may be a continuous train of pulses controlled by selecting one of the eight frequency ranges or a single pulse controlled by pressing a pushbutton on the front panel. The output pulse is either a positive or negative half sine-wave of 0.1 µsec duration whose amplitude is variable from 8 to 30 v. Circle 446 on Reader Service Card.



SUBMINIATURE SWITCH

with overtravel plunger

UNIMAX SWITCH, Division The W. L. Maxson Corp., Ives Road, Wallingford, Conn. Designed to provide the advantages of panel (continued)

mounting plus over-travel plunger actuator, along with the small size of a subminiature switch, the USMJ-1 switch mounts in a ½-in. hole and fits into back-of-panel area only \$\frac{3}{2}\$ in. long by \$\frac{3}{2}\$ in. wide. Solder-lug terminals, located on the rear of the switch, handle wires up to No. 18.

This actuator can be furnished with any basic USM Unimax switch. The type USMJ-1 is designed to meet commercial standards. The type USM3J-1 is designed for high-temperature applications—up to 275 F. Type USM5J-1 is designed to meet Military Specification MIL-S-6743.

Electrical ratings are $2\frac{1}{2}$ amperes 30 v d-c, inductive; 4 amperes 30 v d-c, resistive; 5 amperes 125/250 v a-c. Circle 447 on Reader Service Card.



PRECISION POT

miniature, single-turn

SPECTROL ELECTRONICS DIVISION OF CARRIER CORP., 1704 South Del Mar Ave., San Gabriel, Calif., announces an improved version of their standard $\frac{\pi}{2}$ in. diameter, single-turn model 700.

With high-quality toroidal coils, the 700 is now available with resistance values up to 125,000 ohms and ±0.2 percent linearity. This precise miniature incorporates, with its increased range, all aluminum construction—up to 6 sections ganged on a single shaft—with class 5 ball bearings at both ends—first pot section 0.687 in. long and each additional cup only 0.500 in. in length.

All terminals are glass insulated, steel sheathed, gold plated and permanently locked-in. Nine additional terminals are available

DIRECTIONAL COUPLERS

VSWR and RF POWER MEASURING EQUIPMENT

New Products included in new Catalog No. 12 create the most extensive line available.

Ę	RF POWE	R and VSW	R INSTRUMENTS	
1	Model No.	Frequency Range (mcs)	Power Range Incident & Reflected (watts)	RF Connectors and Impedance
\	261** 262 263 702N 703N ♣705N ♣706N 711N ♣722N ♣723N ♣40588 445A9	0.5 - 225 0.5 - 225 28 - 2000 20 - 2000 20 - 2000 28 - 2000 1000 - 3000 1000 - 3000 28 - 2000 28 - 2000 28 - 2000 20 - 2000	0 - 1000 (relative) 0 - 1000 (relative) 0 - 10; 100; 1000 0 - 4 0 - 12 0 - 120 0 - 30; 75; 300 0 - 4 0 - 12 0 - 4000 0 - 12,000 0 - 12,000	Type 83-1R 52 ohms Indicator only Type N* 52 ohms Type N 52

	DC, OUTP	UT DIRECTI	ONAL COUPLERS	
J	Model No.	Frequency Range (mcs.)	Power Range Incident & Reflected (watts)	RF Connectors and Impedance
	576N1 576N3 ▲576N4 576N6 ▲592N	42 - 2000 20 - 2000 46 - 2000 28 - 2000 1000 - 3000	1.2 0 - 12 0 - 40 0 - 400 0 - 4	Type N* 52 ohms Type N* 52 ohms Type N* 52 ohms Type N* 52 ohms Type N 52 ohms
\	▲593N 402B8 442A9 442A10	1000 - 3000 28 - 2000 28 - 2000 20 - 2000	0 - 12 0 - 4 ,000 0 - 12,000 0 - 40,000	Type N 52 ohms 15% Flange 51.5 ohms 31% Flange 50.0 ohms 31% Flange 50.0 ohms

	RF OUTP	UT DIRECTIO	NAL COUPLERS	
J	Model No.	Frequency Range (mcs.)	Coupling Attenuation	RF Connectors and Impedance
1	313N3 313N4 313N5 313N6 442A40	300 - 2000 120 - 2000 60 - 2000 30 - 2000 200 - 1000	30 db 40 db 50 db 60 db 40 db	Type N* 52 ohms 31/4" Flange 50.0 ohms

	ABSORPT	ION TYPE RF	WATTMETERS	
/	Model No.	Frequency Range (mcs.)	Power Range (watts)	RF Connectors and Impedance
	621N 624N 625C5 651N 611A7	1 to over 1000 1 to over 1000 50 - 1000 25 - 1000 50 - 1000	0 - 120 milliwatts 0 - 4 0 - 120 0 - 25; 100; 500 0 - 1200	Type N* 52 ohms Type N* 52 ohms Type C 50 ohms Type N 52 ohms 31/4" Flange 50 ohms

	OIZA	44 - 1000	1 0-8000	378 Hange 30 onns
<i>5</i>	RF LOAD	RESISTORS		
	Model No.	Frequency Range (mcs.)	RF Power Dissipation (watts)	RF Connectors and Impedance
	633N 635N 636N	3000 3000 3000	50 (air cooled) 200 " " 600 " "	Type N* 52 ohms Type N* 52 ohms Type N* 52 ohms Type N* 52 ohms
	636A	2000	600 " "	31/8" Flange 50.0 ohms

Т	CALORIM	ETRIC TYP	E Primary Standard of RF Power	
J	Model No.	Frequency Range (mcs.)	Power Range (watts)	RF Connectors and Impedance
	641N	0 - 3000	0 - 3: 10: 30: 100: 300	Type N 52 ohms

▲New products

*Also available with UHF, C, and HN Connectors.

**Coupler Unit Only for use with 262 Indicator.



M. C. JONES ELECTRONICS CO., Inc.
BRISTOL, CONNECTICUT

INSTRUMENT AND COMPONENT

SALES REPRESENTATIVES

High quality manufacturer of electronic test instruments, associated equipment and components seeks energetic sales representatives, particularly in the following areas:

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- Florida

Preference will be given to conscientious and enthusiastic organizations with good contacts and ability to interpret market requirements. We back up your efforts with strong merchandising and liberal commissions.

Write us your qualifications and present commitments.

TRANSITRON inc.

Division of Van Norman Industries, Inc. 186 Granite Street, Manchester, N. H. Attn: Director of Sales and Marketing



CIRCLE 209 READERS SERVICE CARD

HIGH VOLTAGE



MODEL LAB-60 RF TYPE

Continuously Variable 0-60 KV DC Regulated Power Supply

Current output 1 ma. at 60 KV 2 ma may be drawn from 50 KV to 0. Supplied with either positive polarity output. Regulation stability-1% at 1 ma 21% wide x 22% high x 18' deep.

.\$695.00 Net LAB-60 Complete with meter. LAB-60 PN Reversible pol: polarity model of above \$745.00 Net

MODEL 457 41/2 KV POW SUPP

Utilizes two as a paralle feeding a IX2 tube. For a voltage of DC at 1 mi the low volt.

MODEL 2040 40 KV DC Power Supply

In constant use in laboratories and industrial plants throughout the world for condenser charging, electrostatic spraying and stress testing, etc. Available with either positive or negative 40 KV output. Volt-



esting, etc. Available 9 40 KV output. Voltage range of approx. 15 to 40 KV. The 15 to 40 KV variance in voltage is controlled through a knob on the front panel. If required for TV use, a voltage output of approximation of the controlled of the controlled from the controlled output of approximation of the controlled output output of the controlled output of the controlled output of the controlled output out quired for Tv use, a voltage output of approx. 4 to 6 KV is available through a tap. Voltages supplied through a 4 ft. HV Safety Cable, 19½" wide x 12¾" high x 13" deep.

Specify desired polarity when ordering....\$150.00 Net With HV meter installed in front panel.\$50 additional

the require. at 50 By verial from 1 KV. Dimensions: 55%. Dimensions: 55%. Dimensions: 55%. Dimensions: 55%. Dight x 5" deep x 41%" wide. In completely enclosed metal housing (not shown). Less low voltage DC supply \$32.50 Net 2G-30—Continuously Variable of DC Power Supply 1 focus range of 4 to spot tube

MODEL RG-30—Continuously Variable 15-30 KV Regulated DC Power Supply with regulated focus incorporates a voltage tap in the range of 4 to KV for use with 5WP15, 5TP4 and flying spot tubes than .5% at 1 milliampere. In wide use for color milliampere. In wide use for color tube development work, transcription recording systems. Also available with focus and convergence voltage taps for RCA Tri-Color tubes at slight additional cost. This model can be adjusted for 40 KV output at .5 milliampere for new tubes.

19½" wide x 12¼" high x 13" deep\$295 Net With meter installed on front panel\$345 Net COMPLETE LINE OF HIGH VOLTAGE COILS-

-Send for complete catalog E

TELEVISION

3029 WEBSTER AVENUE N. Y. 67, N.Y. Kingsbridge 7-0306

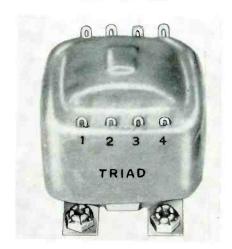
per section—taps at nearly any angle of the coil, and tap-welded to a single turn of the resistance wire. Circle 448 on Reader Service Card.

DIGITIZER

a multipurpose unit

FRANKLIN ELECTRONICS. INC. Bridgeport, Pa., has developed a new all-electronic digital voltmeter for making precision voltage measurements from 0 to 120 v d-c. Called the model 310 A, this multipurpose digitizer is ideal for laboratory and production measuring. It can also be used as the essential analog to digital conversion element in data reduction systems.

This low-cost instrument provides accuracy of 0.1 percent of full scale and readings at a rate of 60 per sec-automatically or on command. Measurements are displayed on the front panel via 4 clearly illuminated decimal digits (000.0 to 120.0). Coded outputs of each significant figure in the visual readout provide a signal source to operate matrices, punched or categorizing equipment. Circle 449 on Reader Service Card.



TRANSFORMERS

with long life expectancy

TRIAD TRANSFORMER CORP., 4055 Redwood Ave., Venice, Calif., announced recently that most of its transformer types can now be supplied in versions designed to exceed the requirements of MIL-T-27A specification, Class S. This specification covers transformers and inductors with life expectancies of greater than 10,000 hours, and operating conditions from -50 C to 130 C.

These new 130 C transformers cost only slightly greater than Class R (105C) types. They are also available to customer specification on special order. Circle 450 on Reader Service Card.

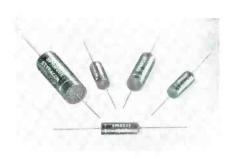
LIMIT SWITCHES preadjustable, snap-action

TECHNOLOGY INSTRUMENT CORP. OF CALIFORNIA, 7229 Atoll Ave., North Hollywood, Calif., has available a conveniently packaged pair of rugged snap-action limit switches for attachment to a 1-in. pot.

Outstanding features of the switch are its range of angles from 0 to 360 deg and the fact that the switch can be preadjusted to actuate over this range of angles. Also of interest is the operating torque at switch action points of 3.5 in. oz (max) and running torque of 0.5 in. oz (max).

The switch action is extremely compact, requiring approximately ½ in. additional length and on a 1-in. potentiometer gang.

Fully illustrated material and complete information covering mechanical and electrical specifications are available. Circle 451 on Reader Service Card.



CAPACITORS

polystyrene film type

SPRAGUE ELECTRIC Co., North Adams, Mass., has announced the type 194P Styracon capacitors. They use an especially processed polystyrene film for their dielectric. They are protected against moisture as well as mechanical



he's working for you

THIS FELLOW IS TRAINED IN YOUR BUSINESS. His main duty is to travel the country — and world — penetrating the plants, laboratories and management councils... reporting back to you every significant innovation in technology, selling tactics, management strategy. He functions as your all-seeing, all-hearing, all-reporting business communications system.

THE MAN WE MEAN IS A COMPOSITE of the editorial staff of this magazine. For, obviously, no one individual could ever accomplish such a vast business news job. It's the result of many qualified men of diversified and specialized talents.

AND, THERE'S ANOTHER SIDE TO THIS "COMPOSITE MAN," another complete news service which complements the editorial section of this magazine—the advertising pages. It's been said that in a business publication the editorial pages tell "how they do it"—"they" being all the industry's front line of innovators and improvers—and the advertising pages tell "with what." Each issue unfolds an industrial exposition before you—giving a ready panorama of up-to-date tools, materials, equipment.

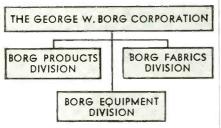
SUCH A "MAN" IS ON YOUR PAYROLL. Be sure to "listen" regularly and carefully to the practical business information he gathers.



McGRAW-HILL PUBLICATIONS

NEW PRODUCTS (continued)

George W. Borg, who founded this corporation, is the "Mr. Clutch" who started with Borg & Beck. He then helped organize the Borg-Warner Corporation of which he became president. Later he served as chairman of the board until he resigned to devote his full attention to The George W. Borg Corporation.



The George W. Borg Corporation is comprised of three divisions

- Borg Products Division Manufactures automotive clocks.
- Borg Fabrics Division Manufactures deep-pile fabrics best known of this line is the fashionable "Borgana" fabric.

• Borg Equipment Division Manufactures Micropots (precision potentiometers), Microdials (precision turn-counting dials), instrument motors, frequency standards, aircraft navigational instruments and components for systems.



HOW BORG EQUIPMENT DIVISION CAN HELP YOU .

Borg's background of experience will save you time and money by helping you solve design and production problems of electronic components. Whether you are faced with a special problem or interested in a standard component, call Borg Equipment Division for an economically sound solution. Write today for catalog BED-A56.



BORG EQUIPMENT DIVISION

THE GEORGE W. BORG CORPORATION JANESVILLE, WISCONSIN

CIRCLE 211 READERS SERVICE CARD

damage in installation by prephenolic molded mineral-filled shells with resin end seals, thus overcoming poor field experience with wrapped-type designs.

The extremely high Q, minimum dielectric absorption, and high insulation resistance of type 194P capacitors make them most suitable for applications in tuned circuits, timing and integrating circuits, and in inter-stage coupling networks in high quality amplifiers. Because they approach an ideal capacitor in their electrical characteristics, they also make good working standards for school and college electronics laboratories. Circle 452 on Reader Service Card.

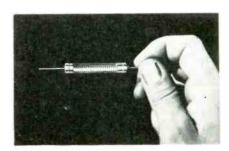




ENCODER

all-electronic converter

AVION DIVISION ACF INDUSTRIES, INC., 800 North Pitt St., Alexandria, Va., has introduced the new type 525 encoder (analog to digital converter). It is an allelectronic converter designed to provide precise and dependable conversion of analog input data to digital output voltages. Particular emphasis is placed upon accuracy and resolution. Dependable operation is maintained over a wide range of environmental conditions. The 525 encoder makes possible the use of versatile, noisefree digital transmission and computing techniques to a greater degree of accuracy than heretofore possible. When used in combination with a model 1002 decoder, it becomes possible to solve problems in telemetering, analog computation, digital computation, pcm, and many other data processing applications. Circle 453 on Reader Service Card.



METAL FILM RESISTOR cannot burn up, short out

THE DAVEN Co., Livingston, N. J., has available the Davohm series 850 hermetically sealed metal film resistors, specifically designed to negate the possibilities of shorting out or burning up. There are no organic compounds in the resistor which might carbonize. The series 850 are extensively used in critical applications where severe line overloads might burn up conventional resistors or cause them to short out and overload other components. Typical present applications include fuel gages in jet planes and line terminations in telemetering circuits.

This series offer the lowest noise level available, low ohmic values, excellent high frequency characteristics, a wide temperature range and complete hermetic sealing in smallest size. Circle 454 on Reader Service Card.

MOLDED CHOKE COILS

with radial leads

DELEVAN ELECTRONICS, East Aurora, N. Y., has introduced a complete series of 42 radial lead coils. Inductance values range from 0.47 to $10,000 \mu h$. All other values are exactingly defined for easy engineering evaluation. Each coil is hermetically encapsulated in molded alkyd plastic making it possible for all coils to easily conform to MIL-C-15305A specifications

There is a "Flat" base molded in the body of each coil at the lead exit to permit snug and secure placement of coils on printed circuit boards. The radial leads are suitable for either automation equipment or hand insertion. Leads are spaced at 0.100 in. increments for customer's convenience.

The 42 radial lead coils range in size from 0.235 in diameter and 0.625 in length to 0.500 in diameter and 0.825 in length with 5 different mold sizes available. Circle 455 on Reader Service Card.

TOGGLE SWITCHES single and double pole

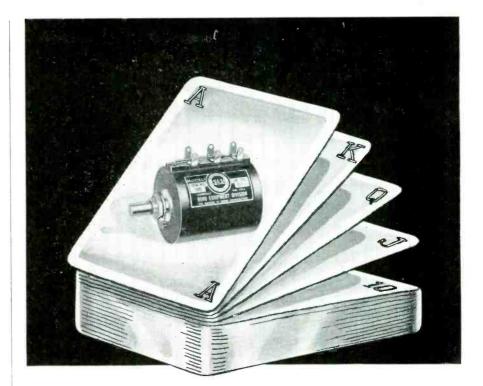
ALLIED CONTROL Co., INC., 2 East End Ave., New York 21, N. Y., has added to its line of components a group of subminiature toggle switches formerly manufactured by Miniature Switch Corp. This line of switches is especially suited for use in printed circuits, transistorized and other miniaturized electronic equipment for the Military.

The body of the single pole type measures 0.520 by 0.270 by 0.320; the double pole type, 0.520 by 0.520 by 0.320. Dielectric is 1,000 v rms; vibration is 10 g 10-500 cps. They meet shock specifications MIL-S-901 (type C). Circle 456 on Reader Service Card.

TEFLON WIRE

has improved color coding

Wirecraft Products, Inc., 10 Lake St., West Brookfield, Mass. Improved color coding of Teflon tape insulated wire can now be obtained by new techniques developed for spirally wrapping two different colored strips on white or colored backgrounds. The two different colored strips of two different widths are so applied that the background color is always visible between them. The first stripe is applied twice the width of the second stripe and the background



SELECT THE ACE OF COMPETITIVE POTENTIOMETERS . . .

Borg 1100 Series Micropots!

Now! Mass-produce your precision equipment products with price advantages in your competitive markets! Borg 1100 Series MICROPOTS give you quality potentiometers at a competitive price. Cut down high production costs that are "stacking the deck" against you. Write for the name of your nearest Borg Jobber or "Tech-Rep" today!

1100 SERIES MICROPOT ADVANTAGES . . .

- 1. Lug-type terminals or coded flexible leads 9" long.
- Optional rear shaft extension on single and ganged assemblies.
- 3. Precision, interchangeable parts give permanent accuracy.
- 4. Engineered for easy installation . . . long-lasting service.
- 5. Interchangeable Borg MICROPOTS permit maximum flexibility.
- 6. Two bearing supports . . . $1\frac{1}{2}$ " maximum between bearings.
- 7. Simplicity of construction . . . fewer parts minimize servicing.
- 8. Production quantities available.

Write for complete engineering data — Catalog BED-A56

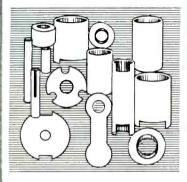
BORG EQUIPMENT DIVISION THE GEORGE W. BORG CORPORATION

JANESVILLE, WISCONSIN





- NIEMAND BROS. have the ANSWERS!



Many manufacturers have found the answers to problems of reducing unit costs and speeding up production by using Niemand Bros. Paper Tubular Products.

They're practical—buy them in the quantities you need in the materials you want—high dielectric kraft, fish paper, foils, special protective coated and laminated papers and Mylar*. Printed or plain, they're made in diameters from .093" to 2" and up.

And, also available from Niemand Bros. are precision drawn paper or Mylar* caps in diameters from .141" to 2", as well as die cut washers and custom parts.

*DuPont's reg. trade mark for its polyester film. Send for complete details. lucks for Exectrical Application RAvenswood 8,-0909

CIRCLE 213 READERS SERVICE CARD

spacing between the stripes is controlled to give maximum legibility.

Spiral stripes are wrapped as an integral part of the insulation and are clear and vivid in color, nonfading, and permanent under all conditions.

The background between the last stripe of one group and the first stripe of the next is always wider than the background color between the stripes. This improved striping method makes each wire more readily distinguishable even in the most complicated circuitry where the reverse use of the same color combinations cannot always be avoided. Circle 457 on Reader Service Card.



R-F AMPLIFIERS for tv signal distribution

WESTBURY ELECTRONICS, INC., 300 Shames Drive, Westbury, N. Y., has announced the addition of two new r-f amplifiers to their line of tv distribution system equipment. Both units feature high gain, low noise input, excellent linearity of response providing clear, snowfree tv pictures of high quality for a large number of tv receivers from a single antenna. They are available in two models: ABB-3 channels 2 to 6, or the all band model ABB-4 (illustrated) for channels 2 through 13. Circle 458 on Readers Service Card.

TRANSMITTER is fully transistorized

GENERAL ELECTRIC Co., Syracuse, N. Y. A new carrier-current transmitter, fully transistorized for improved performance, is now being furnished. Designated as type CT-50B, the new unit supersedes

GE's type CT-20 transmitter. which has been widely used to transmit frequency-shift signals for impulse and frequency telemetering, automatic dispatching, remote station supervisory control and transferred tripping.

The new transmitter is crystalcontrolled and can be operated on any specified frequency from 30 to 200 kc. The operating frequency is stabilized because the two oscillators used have similar temperature - stability characteristics. Circle 459 on Reader Service Card



D-C POWER SUPPLIES in 16 basic models

BETA ELECTRIC DIVISION OF SOREN-SEN & Co., INC., 333 E. 103 St., New York 29, N. Y., is now offering a new line of rack-mounting h-v d-c power supplies, the series 1000. Available in 16 basic models with outputs from 0-1 to 0-50 ky at from 2 to 500 ma, the series 1000 features rugged construction, moderate price, conservative design, complete self-protection, and minimum operational hazards.

Typical of the series is the model 1050-5. This unit has a range of 0-50 kv at 0-5 ma, 1 percent ripple, 6 ma fixed overload, 40 percent regulation, and 420 va input at 117 v. It has a 21 in.-high panel and weighs 125 lb (with oil). The 1050-5 is also available in a more elaborate version for research and development work. In the latter version it has fine control of h-v output to approximately 0.03 percent of maximum, triple range load current and output voltage meters with scale ratios approximately 1:3:10, zero start normal with bypass button for sudden application of high voltage, and an

overload relay with trip adjustable from 20 to 120 percent of rated current. Circle 460 on Reader Service Card.

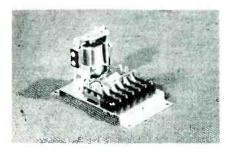


POWER SUPPLY

for many applications

ALFRED ELECTRONICS, 897 Commercial St., Palo Alto, Calif., announces the new 175 to 3,500 v at 0 to 25 ma precision power supply, model 218A. Voltage is adjusted with a 10 turn pot and is resettable to $\pm \frac{1}{2}$ percent. Line regulation is 0.003 percent and 0 to full load regulation is 0.006 percent of full scale. Extreme long and short term stability is provided; the drift specification is 0.1 v or 0.01 percent (whichever is greater) per hour and 0.02 percent for eight hours. Ripple voltage is less than 20 mv peak to peak. Also available with similar voltage and operating characteristics are 50 ma, 100 ma and 150 ma supplies.

The supplies are flexible high voltage sources for a variety of measurements involving: ionization counters, klystrons, traveling wave tubes, backward wave oscillator tubes and photomultiplier tubes. Circle 461 on Reader Service Card.



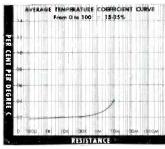
RELAY SUBASSEMBLY powered by magnetic pickup

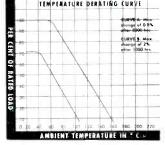
ELECTRO PRODUCTS LABORATORIES, INC., 4500 N. Ravenswood Ave., Chicago 40, Ill., announces a new,

IMMEDIATE DELIVERY

(Small Quantity)

PRECISION CARBON DEPOSITED RESISTORS





Temperature coefficient characteristics for ALPT-1 watt resistor

Derating curve for ALPT-1 watt

STANDARD RESISTORS $\pm1\%$ TOLERANCE IN 10% RMA VALUES FROM 10 OHMS TO 2.7 MEGOHMS

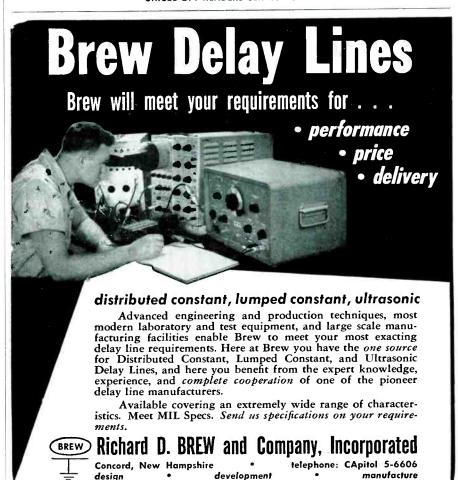
APST-1/2 WATT, APXT-1/2 WATT AND APCT-1 WATT SALES OFFICES AND DISTRIBUTORS

Factory Delivery, other than stock values: 1/10, 1/5, 1/4, 1/2, 1, 2 and 5 Watt

ALLIES' PRODUCTS CORPORATION
P. O. Box 188, Kendall Branch, Miami, Florida

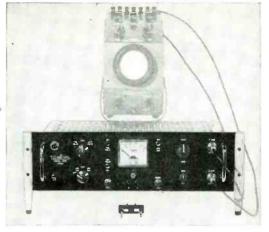
BROCHURE SUPPLIED UPON REQUEST.

CIRCLE 214 READERS SERVICE CARD



ANNOUNCING

TESTER by TECHNITROL



This moderate-price instrument provides an invaluable means for the rapid, accurate checking of semiconductor diodes for instability and irregularities. The dynamic curve, far more revealing than static testing, is quickly apparent on a scope screen, and is readily adapted to volume testing. In addition, the easy portability of this 16-pound instrument makes it ideal for field work as well as bench or rack installation.

Designed for use with a D.C.-coupled oscilloscope, the Technitrol Diode Tester provides for a variety of back and forward voltages, as well as independently-controlled ranges for back and forward currents.

CALIBRATED RANGES:



CIRCLE 216 READERS SERVICE CARD

FCHNITROL ENGINEERING COMPANY 1952 E. Allegheny Ave., Phila. 34, Pa

RIBBONS · STRIPS

★ PURE TUNGSTEN

★ MOLYBDENUM

★ THORIATED TUNGSTEN
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ULTRA THIN SIZES

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TOLERANCES CLOSER THAN COMMERCIAL STANDARDS by

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Note: for highly engineered applications—strips of TUNGSTEN and some other metals can be supplied

ROLLED DOWN TO .0003 THICKNESS

- Finish: Roll Finish-Black or Cleaned
- Ribbons may be supplied in Mg. weights if required

For HIGHLY ENGINEERED APPLICATIONS

DEVELOPED AND MANUFACTURED BY

H.CROSS CO. 15 BEEKMAN ST., N. Y. 38, N. Y. WOrth 2-2044
COrtland 7-0470

compact relay subassembly designed as a safety device for machine tool builders. The device, model 3420, operates as an over or under speed control.

The relay requires no external source of power other than that generated by a power type magnetic pickup. The pickup consists of a magnet with a coil of wire surrounding it, and acts as a miniature generator when placed near the teeth of a gear.

A typical application would be a 12 tooth 8 pitch ferrous gear with the power type pickup mounted at 0.005 in. spacing. At a peripheral speed of 250 in. per sec, the speed control relay would close with the power generated.

Critical speed for the relay is set by adjusting spacing between the magnetic pickup and actuating metal. The over/under speed control relay is spdt with contacts rated at 5 amperes noninductive load. Circle 462 on Reader Service Card.



TRANSISTOR TESTER for lab and routine inspection

STRAND ENGINEERING Co., 1354 N. Main St., Ann Arbor, Mich., announces an instrument for rapid evaluation and testing of *npn* and *pmp* power transistors at their normal operating power. Model 102 power transistor tester is designed both for laboratory use and for routine inspection by shop personnel. It measures (1) collector current for zero emitter current at base-collector voltages from 0 to 75 v; (2) large signal current gain at collector currents up to 2.0 amperes, collector voltages from 0 to

PROTECT

ELIMINATE HOT SPOTS

0

VENTILATED

MIL Spec Quality

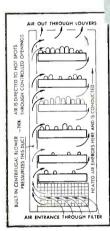
Complete Package Modular Construction

> **Fully Controlled** built-in Cross-ventilation System

Cool Exactly Where Needed

Cool Heat Load of 2-3 KW Input

Proven in 4 Years' Operation in Government Laboratories



MODEL FC1-24V-681/4H Dolly Optional STANDARD UNITS: 19" to 24" Panels 18" to 36" Deep

Matching Consoles Available

OTHERS TO YOUR

NOTE: Adjustable air-flow pattern to your exact needs is effected by snap-in closures—no 'chimney' effect

- Available in cabinets or consoles -with 12-gauge or 3/6" steel frame · Adjustable interior rails afford ready mounting for chassis slides
- Front and rear doors with glass panels or cutouts . Paint finish to customer requirements

Write for Complete Data: Series FC/E

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CIRCLE 218 READERS SERVICE CARD ELECTRONICS - December 1, 1957

NEW PRODUCTS

28 v and base currents up to 50 ma; (3) small signal current gain in the grounded emitter connection at any chosen operating point; and (4) collector-base breakdown voltage.

(continued)

Measurements may be made over a wide range of operating conditions, with minimum heating, and the controls are arranged for quick, simple setup. Three fiveway binding posts permit connecting transistors of all types; and adapters can be furnished for plug-in connection. Circle 463 on Reader Service Card.



VANE PUMP CARTRIDGE

for electronic drive

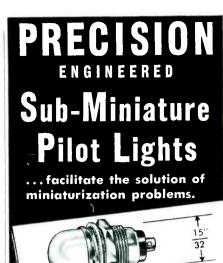
VICKERS INC., Detroit 32, Mich. To meet small-space, low-weight specifications for electronic applications, the company has announced the miniaturization of the vane type pump cartridge. It weighs only 2.5 oz and will deliver 1.04 gpm at 1,000 psi and 10,000 rpm. It has an output of 0.06 hp, and is less than 11 in. in diameter.

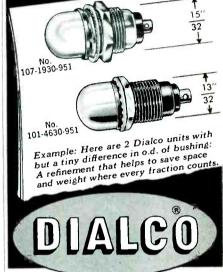
The cartridge is available either singly or stacked for incorporation into user's housing or Vickers will furnish suitable housings. Suggested uses are: small radar drives, small computer drives and cooling for electronic chassis or missile skin. Circle 464 on Reader Service Card.

RELAY TESTER

priced at \$195

ZEUS ENGINEERING Co., INC., 635 South Kenmore Ave., Los Angeles 6, Calif. Simple relay tester, model 15B, is designed for instantaneous go, no-go test for single pole to 6 pdt relays. Coil excitation is





Un your next miniaturization project, consult DIALCO for the Pilot Lights. You will quickly find the proper unit for use with either tiny Incandescent bulbs $(T-1)^3/4$; or with sub-miniature Neon bulbs (NE-2D).

TWO-TERMINAL units are fully insulated. SINGLE-TERMINAL units are for use on grounded circuits. Also DIMMING or NON-DIMMING sub-miniatures for every

requirement. Meet all applicable Military Specifications. Samples for design purposes on request at once - no charge. (actual size)

No. 134-3830-375-9 No. 101-3830-951

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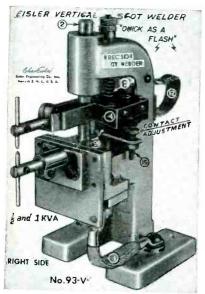
Dialight Corp., 58 Stewart Ave., Brooklyn 37, N. Y.			
☐ Send brochures on Sub-Min. Pilot Lights ☐ Brochures on other Dialco Pilot Lights			
Name			
Position			
Company			
Address			

CIRCLE 219 READERS SERVICE CARD

EISLER VERTICAL SPOT WELDERS

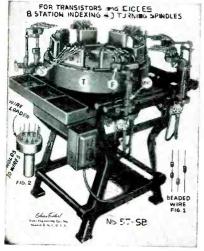
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TRANSISTOR DIODE MACHINERY AUTOMATIC OR SEMI-AUTOMATIC



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CIRCLE 220 READERS SERVICE CARD

NEW PRODUCTS





variable from 6 to 150 v. A set of lights indicates opens, shorts, or intermittent contact operation. The tester has five different connector types and adapters are available to permit plug-in of solder-terminal relays. Circle 465 on Reader Service Card.



TEMPERATURE PROBE conforms to MIL-P-25726

G. M. GIANNINI & Co., INC., 918 East Green St., Pasadena 1, Calif. Model 49137 total temperature probe conforms to MIL-P-25726. It utilizes a resistive sensing element to accurately measure stagnation temperature over the range of -70 C to $\frac{1}{4}$ 350 C and at speeds to Mach 1.5.

The pure platinum wire sensing element designed for this instrument is encased in a thin ceramic blanket deposited on a thin-walled cylinder. This ceramic cover effectively seals the element, and protects it from damage by particles entering the chamber. Resistance of the element is 50 ohms at 0 C (temperature coefficient = 0.003 ohm/ohm/deg C from 0 to

...IF YOU NEED

POWER SUPPLIES Call TRANSVAL

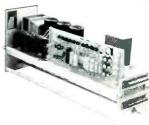
VErmont 9-2301, Culver City, California For Data on TRANSISTORIZED Power Supplies that gives you these advantages:

- \bigstar PROTECTED from overload and short-circuit
- ★ DESIGNED to meet YOUR exact specifications
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HIGH VOLTAGE POWER SUPPLY

Output voltage to 1050 volts (±5V). Regulation 0.5% with nominal load and input from 109 to 121 volts. Size: 5" x 4" x 4½"; 3½ lbs.





ULTRA STABLE POWER SUPPLY

Stability of one millivolt over entire output range of 0. to 4 amps at 10 volts. Other voltages with the same stability may also be obtained.

MULTIPLE HIGH VOLTAGE POWER SUPPLY

Designed for multiple voltage control ranging from -150 volts at 600 ma, to +300 volts at 250 ma. Up to 6 different voltages per drawer. Can be made to ANY specification.



TRANSVAL engineers have set new standards for high stability, light weight power supplies based on advanced techniques of applying transistors. The units shown above are only a few of the many developed by Transval that meet specifications never before considered practical for transistorized power supplies. Among the leading builders of missiles, rockets, and piloted aircraft using Transval transistorized power supplies are Douglas, North American, Northrop, Hughes, Beckman, Norden Ketay, and Canadian Applied Research Ltd.

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Specialists in Transistorized Power Supplies

CIRCLE 221 READERS SERVICE CARD

December 1, 1957 — ELECTRONICS

100 C), response time is 1.5 sec maximum, and the recovery factor is 0.99 + 0.01.

Specifically developed to meet the requirements of MIL-P-25726, this lightweight temperature probe is ideal for any operational or flight test application requiring accurate and rapid measurement of adiabatic temperatures. Circle 466 on Reader Service Card.



TIME CODE GENERATOR for girborne use

ELECTRONIC ENGINEERING CO. OF CALIFORNIA, 1601 E. Chestnut Ave., Santa Ana, Calif., is producing an airborne time code generator, employing transistor-driven, magnetic cores. The compact, light-weight unit is designed for missile and aircraft instrumentation.

The 1½ cu-ft unit supplies a 16-bit, 24-hr binary code to hours, minutes and seconds. Signals generated by the equipment are suitable for recording timing marks or time codes on magnetic tape, oscillographs, or to energize neon lights for indicating time code on the edge of motion picture film in optical instrumentation equipment.

The binary code readout is once per sec at a 100 pps rate. Time can be read directly to 0.01 sec and interpolated to 0.001 sec. In addition to binary code, continuous pulse trains of 100 pps, 10 pps, 5 pps and 1 pps are produced. The basic signal source for the airborne time code generator is a







HOPKINS HY-THERM CAPACITORS are hermetically sealed in metal containers with highest quality compression type end seals. They are 100% inspected for leaks and because of the quality construction and use of the finest materials they are without peer in their field. Each HY-THERM capacitor will meet and exceed the applicable military specifications and satisfy the most stringent quality control and reliability programs.



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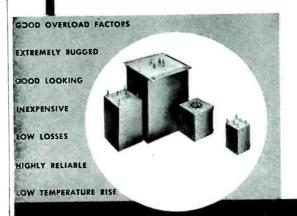
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PERMANENTIZED TRANSFORMERS

custom built to your specifications



New formula developed by Electro makes possible reduced size and more rugged construction in resin-potted transformers. New porting material welds core, coil, case, and terminals, with permanent bonding to case. Built to withstand 170° C. May be qualified under MIL-T-27A, grades 1, 2, 4, or 5 in class R, S, or T, as well as commercial specifications.

ELECTRO ENGINEERING WORKS, INC.

401 Preda St., San Leandro, Calif. • In Metropolitan Oakland area





√ 2 Simple Designs provide many circuits **√** Rugged Metal Housing √ Completely Enclosed



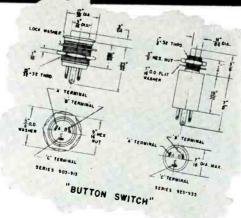
Series 903 (Red Push Button) Series 913 (Black Push Button) for behind name! Push Button) for behind panel

(Black Fush Dutton) to mounting.

Series 923 (Red) Series 933 (Black) mounts from front of panel.

Rated at 250 mils, non-inductive load, A.C., 30 watts maximum. See drawing

Write for catalog \$-57A



Also Available "TINI-SWITCHES"

An open subminiature design.



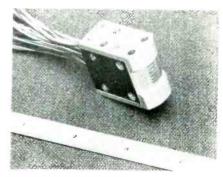
1336 N. Halsted St. Chicago 22, III.

Canadian Rep: Atlas Radio Corp., Ltd., 50 Wingold Ave., Toronto, Canada.

temperature controlled crystal with a long term accuracy of 1 part in 10°. Weight of the unit is 20 lb. The unit will operate up to an altitude of 70,000 ft and from temperatures of -40 C to +80 C.

Input power of the unit is 25 w, which is supplied from standard aircraft-type sources. Magnetic cores, silicon transistors and silicon diodes are used throughout the generator; no vacuum tubes are employed.

The generator can also be supplied without the camera neon lamp driver unit which trims its size to 1 cu ft. Circle 467 on Reader Service Card.



MAGNETIC HEAD new design for missiles

DATA STORAGE DEVICES Co., 7828 Burnet Ave., Van Nuys, Calif. The 7-channel magnetic tape recording head recently developed can be directly connected to thermocouples to record without the use of amplifiers, using only 20 μw . Since the complete system is carried aboard a missile, the head has been designed to withstand high shock and vibration forces as well as high temperature and thermal shock. Other features of this small lightweight, aluminum head, include gap alignment scatter under 1/10 mil, mounting base machined to within 90 deg \pm 15 sec of the gap line and tape guides integral with the head.

The precision features of this head are typical of a complete line of magnetic heads manufactured by the company including drum heads, digital tape heads capable of 2,000 bits per channel per in. with 100 percent resolution, video heads to 4.5 mc, and heads for all types of analog and binaural audio



Tough

Insulate and anchor the power supply cord to your housing...

no need for grommets, wire knots or costly labor.









Send for samples to fit your wire, today!

HEYMAN
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KENILWORTH 2, NEW JERSEY



HEY MAN! ...SAY HEYMAN

CIRCLE 226 READERS SERVICE CARD ELECTRONICS — December 1, 1957

recording. Circle 468 on Reader Service Card.



CONNECTOR

for printed circuits

DEJUR-AMSCO CORP., 45-10 Northern Blvd., Long Island City 1, N. Y., has produced a printed circuit connector with patented polarizing screwlocks.

These right angle construction precision connectors are designed for printed board or printed cable applications, and meet airframe requirements for vibration and high altitude. Contact spacing is based on 0.100 grid in accordance with latest EIA printed circuit specifications.

Series 683 connectors are available in 11 or 33 contacts. Standard molding compound is mineral filled Melamine (MIL-P-14E, type MME)—others on request. In addition to the regular solder cup for No. 20 Awg wire, receptacles can also be supplied with taper pin termination for solderless wiring. Circle 469 on Reader Service Card.



ROTARY SWITCH with adjustable stop

THE DAVEN Co., Livingston, N. J., has available a new rotary switch with adjustable stop. It is ideal



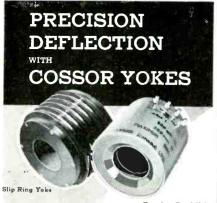
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CIRCLE 227 READERS SERVICE CARD



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 - PRECISION MECHANICAL DESIGN ACCURATE PRODUCTION METHODS

Custom Built to the most Exacting Specifications

by Cossor Engineers In Mumetal Cores for Optimum Geometry In Ferrite Cores for Speed and Sensitivity

In Non-magnetic Cores for Perfection of Response

Any of Cossor's Three Core Types can be made in single or double axis with single or push-pull windings, and encapsulated for fixed or slip ring (rotating) use.

Normal characteristics of yokes for 1-1/2 in. neck tubes are:

Positional accuracy - the spot position will conform to the yoke current co-ordinates within 0.25% of tube diameter. For deflection angles less than ±25° better accuracy can easily be achieved.

Memory .

0.5% max. without overswing: 0.1% or less with controlled overswing

Complete encapsulation in epoxy (stycast) or silicone resins is standard for all Cossor deflection yokes, and is done with special moulding tools ensuring accurate alignment of the yoke axis. When slip rings are added, solid silver rings are mounted in encapsulating resin. The finished slip ring yoke is precision turned to centre bore, and can include bearing mounting surfaces with dimensional tolerances approaching those associable with high quality metal parts.

Settling Time (Micro sec.)

120 VInductance in Henries

Sensitivity degrees/ milliamperes =



COMPONENTS DIVISION

CANADA LIMITED

301 Windsor St., Halifax, N. S. 8230 Mayrand St., Montreal, Que. 648A Yonge St., Toronto, Ont. Corporation House, 160 Laurier West, Ottawa, Ont.

CIRCLE 228 READERS SERVICE CARD

for flexibility in all types of circuit experimentation, laboratory work, breadboard setups, and in circuitry where the exact number of switch positions might be changed at a later date. This unit will have a maximum of either 24 positions with 15 deg spacing or 32 positions with 111 deg spacing. One, two, three and four-pole units are available in this design.

Features are: sturdy, dependable construction; large silver alloy contacts and slip rings; temper-proof, knee action silver alloy rotor blades; accurately machined dielectric; and gold flashed turret-type terminals for ease of soldering.

The switches are constructed to meet and exceed applicable military specifications on humidity. moisture, environment, temperature cycling, contact resistance, life, vibration and shock. They will meet and exceed applicable paragraphs of MIL-S-3786, MIL-E-5272, and MIL-T-945A

Continuous current carrying capacity (not make or break) is 15 amperes. Switches are smooth operating, positive action, rotary selector type. Switch contact resistance remains extremely uniform and is on the order of 0.003 ohm. Capacitance between switch contacts, and between switch contacts and return slip rings, varies from $0.4~\mu\mu f$ to $2.5~\mu\mu f$ depending on the switch. Breakdown voltage between contacts and slip ring is 3,000 v. Circle 470 on Reader Service Card.



MAGNETIC FLOWMETER free of obstruction

FISCHER & PORTER Co., 292 Jacksonville Road, Hatboro, Pa., an-



This Man Has

 $\mathbf{E}.\mathbf{Q}$

YNII?

F. B. Gunter is Manager of Communications Equipment Engineering at Westinghouse-Baltimore. His E.Q. (Exceptional Qualifications) include a B.S.E.E.; four years in the Army and Air Force in ground and airborne radar; 13 years of design and management experience in communications equipment; senior member in I.R.E. and A.I.E.; two patents and a series of papers on carrier and microwave equipment design and application. Today, Frank Gunter and men with similar E.Q.'s are spearheading Westinghouse-Baltimore's advance into the new dimensions of the electronic age.

IF YOU HAVE THE E.Q. to work alongside the men of the Westinghouse-Baltimore team, we suggest that you drop us a letter about yourself. WRITE TO: Dr. J. A. Medwin, Westinghouse Electric Corporation, Dept. 738, P. O. Box 738, Baltimore 3, Maryland.

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BALTIMORE

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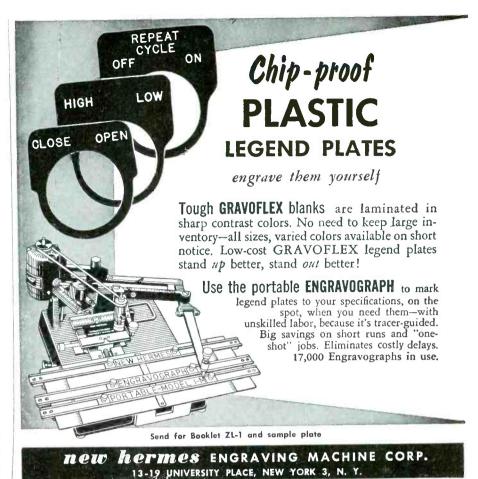
An Engineer's Company nounces the development of an obstructionless flowmeter based on magnetic principles. 10D1416A is unaffected by extreme operating conditions and measure with a high degree of accuracy even the most difficult fluids, including slurries or those of a corrosive nature. Pressure drop through the meter body is eliminated since the unit is completely free of any obstruction to flow.

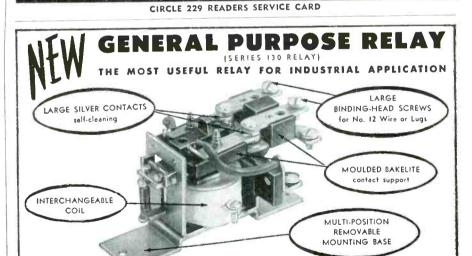
Features of the meter and its specially designed readout equipment are as follows: (1) A manual adjustment to set any flow at full scale. (2) Utilization of full receiver range with maximum flow value as low as that equivalent to 1 ft per sec. (3) Entire system is independent of power line variations over a wide range of voltage and frequency. (4) Fluid conductivity requirements have been minimized. (5) Meter can be substituted directly in existing pneumatic flow control or ratio control systems. (6) Low power consumption. Circle 471 on Reader Service Card.



RELAY SOCKET for close mounting

THE HART MFG. Co., Hartford, Conn., has developed a new socket designed for close mounting of its recently announced Diamond H series W general purpose relays. The socket makes it possible to wire a complete chassis or assem-





SO VERSATILE RELAY 15

SPECIFICATIONS

CONTACTS

Single-and-double pole Single-and-double throw

Aux, DT contacts available

RATINGS

20 amp. at 115 V 60 Cy. AC or 24 V DC

U.L. Approved

COILS

AC & DC to 230 V (Interchangeable)

Power—2 watts

Metal strap or bakelite. Base can be rotated 90 degrees either direction for mounting convenience.

MOUNTING BASE

DIMENSIONS Base-1" x 3 1/8" Request complete data on Series 130 Relay.

SIGNA LONG BRANCH, N. J. RELAYS



scription. Unusually Complete Tool Room • Press Shop . Hydrogen Annealing, Machining and Polishing Operations · Glass-to-Metal Hermetic Sealing. Production of completed parts ready for assembly in your own plant.

A complete service in our plant means prompt service to your plant.

Call on us for free consultation and quotations.

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Over 3,000 high precision tools and

dies available to reduce your initial

CIRCLE 231 READERS SERVICE CARD

TELEPHONE AND TELEGRAPH EQUIPMENT

Radio Engineering Products is currently producing a number of types of equipment, electrically and mechanically interchangeable with standard Bell System apparatus.

CARRIER-TELEPHONE EQUIPMENT

C5 Carrier-Telephone Terminal (J68756). A kit for adding a fourth toll-grade channel to existing C systems is available. • C1 Carrier-Telephone Repeater (J68757) • 121A C Carrier Line Filter • H Carrier Line Filter (X66217C).

CARRIER-TELEGRAPH EQUIPMENT

40C1 Carrier-Telegraph Channel Terminal (J70047C) • 140A1 Carrier Supply (J70036A1, etc.) • 40AC1 Carrier-Telegraph Terminal.

VOICE-FREQUENCY EQUIPMENT

V1 Telephone Repeater (J68368F) • Power Supply (J68638A1) • V1 Amplifiers (J68635E2 and J68635A2) • V3 Amplifier (J68649A) • V-F Ringers (J68602, etc.) • Four Wire Terminating Set (J68625G1) • 1C Volume Limiter (J68736C).

D-C TELEGRAPH EQUIPMENT

16B1 Telegraph Repeater (J70037B) • 10E1 Telegraph Repeater (J70021A) • 128B2 Teletypewriter Subscriber Set (J70027A).

TEST EQUIPMENT

2A Toll Test Unit (X63699A) • 12B, 13A, 30A (J64030A) and 32A (J64032A) Transmission Measuring Sets • 111A2 Relay Test Panel (J66118E) • 118C2 Telegraph Transmission Measuring Set (J70069K) • 163A2 Test Unit (J70045B) • 163Č1 Test Unit (J70045D).

COMPONENTS AND ACCESSORIES

255A and 209FG Polar Relays • Repeating and Retard Coils, several types • 184. 185, 230A and 230B Jack Mountings.

RADIO ENGINEERING PRODUCTS 1080 UNIVERSITY ST., MONTREAL TELEPHONE CABLES University 6-6887 RADENPRO, MONTREÅL

bly before plugging in the spadeterminal relays. If necessary, units may be replaced instantly without rewiring. Socket leads may be connected to a panel or terminal board for easy rearrangement of sequencing.

Measuring only $1\frac{1}{2}$ in. by $1\frac{1}{2}$ in. by 17 in., series W relays are available with standard ratings up to 25 amperes resistive at 115-230 v a-c; 1 hp, 125 v, 2 hp, 250 v a-c, with d-c and other higher ratings obtainable to meet special requirements. Circle 472 on Reader Service Card.



POWER SUPPLIES

use selenium rectifiers

FILM CAPACITORS, INC., 3400 Park Ave., New York 56, N. Y. A line of hermetically-sealed oil-filled power supplies of the full wave voltage doubler type featuring a 5-kv unit has been announced.

Model PS5-S obtains extra long life as a rugged and reliable power supply through the use of selenium rectifiers. This, in conjunction with plastic film h-v capacitors, provides for a compact unit that is small in size and able to meet most military shock and vibration specifications.

The unit delivers 5,000 v d-c at 5.0 ma from a 117 v a-c, 60 cps source. The output voltage may be varied from 0-5,000 v at rated load by varying the input voltage. Ripple is 1.5 percent rms maximum at rated load, less for smaller values of load. This unit can also be used for 400 cps operation if desired, with no change in output specifications except the ripple, which will be very much reduced.

The base of the unit measures only 33 in. by 4% in. and is 6 in. high. Overall height including the solder sealed terminals is $7\frac{1}{8}$ in. Container is CP70 style and utilizes standard CP70 mounting brackets. Circle 473 on Reader Service Card.

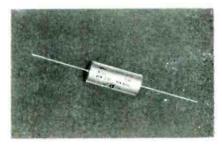


VIDEO AMPLIFIER

is rack-mounted

INSTRUMENTS FOR INDUSTRY, INC., 150 Glen Cove Road, Mineola, N. Y., has added a rack-mounted model 395 super-video amplifier to its line of standard amplifiers. It features a very high gain over a wide bandwidth.

Specifications are: bandpass, 1 ke to 50 me; gain, 70 db; input impedance, 90 ohms; output impedance, 90 ohms; output voltage capability, more than 1 v rms; noise figure, 15 db; gain control, provided on front panel; rise time. 10 millimicroseconds; and tube complement, 24-6AK5's and 1-5R4-GY. Circle 474 on Reader Service Card.



DIELECTRIC CAPACITOR stable, reliable, rugged

DIAMOND ELECTRONICS CORP., 64 White St., New York 13, N. Y., has



Meeting the ever-increasing standards of perfection established by the electronics industry is a challenge admirably met by Zell's highly skilled engineers. They are able to exercise unusually rigid quality controls because all production operations are carried out in Zell's own completely equipped, ultra modern plant,

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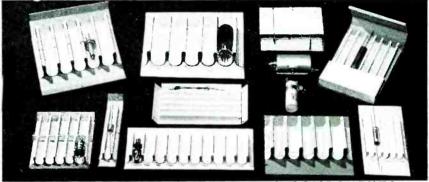
Complete tool room facilities, 65 Power Presses (to 50 tons).

6b Power Presses (to 30 tons).
 Double stage annealing-fusing furnaces.
 Advanced plating facilities for Nickel, Gold, Tin, Cadmium, Copper, Silver, etc.
 Complete glass facilities.
 Mass Spectrometer leak testing.
 ZELL engineers control every process every step of the way, assuring uniform quality and performance.

REPRESENTATIVES: Your Inquiries invited!



CIRCLE 233 READERS SERVICE CARD



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RONDO, a cardboard device, holds and protects inserted objects by the spring-clip action of its fluted partitions. Easy to load and handle. Various sizes and styles have been developed for many parts, such as tubes, resistors, capacitors, diodes, fuses, etc., with diameters from 8 to 26mm and up.

Maximum efficiency and economy are accomplished when the same RONDO device is used throughout production, storage, shipping and display. RONDO is a paper product, sold at paper prices.

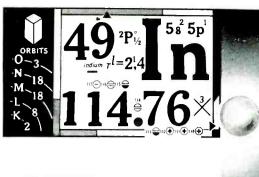
Send for leaflet and suggestions regarding your specific packing need.

RONDO PROCESS AND DESIGNS ARE COVERED BY PATENTS IN ALL MAJOR COUNTRIES

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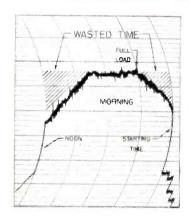
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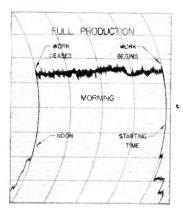
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developed a polystyrene dielectric capacitor with excellent stability, reliability and ruggedness. Stability is within ± 0.1 percent of original value after repeated temperature cycling and under long term load. No capacity drift trend can be detected. New processing and quality control techniques enable 100-percent elimination of border-line components. Short-term life failure is nonexistent and long-term life test results are exceptional.

Lead attachment is accomplished to obtain superior uncased pull strength and uniform contact for minimum noise and power factor. The new method of encasement provides maximum strength to resist severe vibration and shock tests. Circle 475 on Reader Service Card.



WAVE TIMER

is transistorized

RANSOM RESEARCH, 323 West 7th St., San Pedro, Calif. Model WT-1 wave timer measures electrical signals from one event per sec to 500,000 per sec with five-place accuracy. It may be used as an events-per-unit-time meter. Preset count capacity is up to 9,999 and the precision timer range extends up to one sec in increments of $100~\mu sec$.

The wave timer utilizes transistorized plug-in computer elements, thus eliminating all tubes and relays. The instrument consists of a time base, an amplifier, a logic for correctly starting, stopping and recycling the wave timer, a four decade preset counter with no display, and a five decade counter with display.

The instrument is designed to operate with a minimum input

pulse of 5 v or a minimum sine wave signal of 10 v. Input impedance is 10,000 ohms and power requirement is only 20 w. Circle 476 on Reader Service Card.

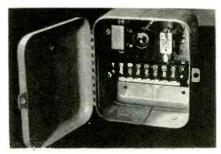


D-C POWER SUPPLY for use with strain gages

VIDEO INSTRUMENTS Co., INC., 2340 Sawtelle Blvd., Los Angeles 64, Calif. Model SR200 is a transistorized, regulated d-c power supply for use with strain gages.

Output voltage is continuously variable from 5 to 12 v at currents up to 200 ma. Output voltage regulation is ± 0.1 percent with line input voltage fluctuations from 95 to 135 v. Line voltage transients within this range will not cause overshoot or ringing nor affect rated ± 0.1 -percent output voltage regulation. The unit may be used on supply voltage frequencies ranging from 50 cps to 400 cps.

The power supply is ruggedly constructed and may be operated in widely varying ambient temperatures. Six units can be mounted in one 19-in. rack panel only $3\frac{1}{2}$ in. high. Net selling price is \$95 each. Circle 477 on Reader Service Card.



PILOT RELAY
uses cold cathode tube

HALEDY ELECTRONICS Co., 57 William St., New York, N. Y., has an-

SPECIALISTS SPECIALISTS

COMPLETE LINE for every Military and Special purpose.

- Yokes for 7/8", 1-1/8", 1-1/2", 2-1/8" neck diameter CR tubes.
- Rotating and fixed coil designs.
- Core material to suit your requirements.

Special test instruments can establish your yoke deflection parameters to an accuracy of $\pm 0.1\%$.



Series alding fleid and parallei (bucking) fleid designs.









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CIRCLE 237 READERS SERVICE CARD

MISSILE TEST DATA TRANSCRIPTION AND ANALYSIS

The transcription, analysis, and evaluation of ballistic missile test data is one of the important aspects of R-W's system engineering and technical direction responsibility for the Air Force Ballistic Missile Program. Utilizing the facilities of R-W's Data Reduction Center, test data are transcribed and reviewed to determine performance characteristics and confidence levels.

The following positions in this rapidly expanding field are currently open on the R-W staff:

Senior analyst to direct mathematicians, engineers, and technical aides in missile test analysis projects and to participate in overall evaluation of missile systems performance. The test information originates from optical, radar, and telemetry instrumentation. Particular emphasis is placed upon electronic analysis of vibration data.

Engineer with wide experience in telemetry operations. The position volves planning and directing the conversion of telemetered data into forms appropriate for the analysis of weapon systems performance. Experience in the design, maintenance, and operation of telemetry data transcription and electronic vibration analysis equipment is desirable.

Engineer experienced in the utilization of missile test data transcription equipment. This position involves the planning of equipment schedules, with various research and industrial organizations, for the conversion of missile test data. A thorough knowledge of the capabilities and limitations of telemetry transcription and electronic vibration analysis equipment is desirable.

Inquiries should be addressed to: Mr. J. H. Armitage

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P.S. We also produce IRN Magnetle Iron powders for the Electronic Core Industry, the Magnetic Tape Recording Industry and others. Write for complete technical information.

CIRCLE 238 READERS SERVICE CARD

nounced an electronic pilot relay capable of controlling large values of current and power with a current flow of 2 millionths of an ampere through the utilization of a special cold cathode tube of almost unlimited life. This minute flow of current now permits delicate mechanisms with extremely light contact pressures to control large electrical currents.

The cold cathode triode tube (TT-1) is designed for use under the most rugged conditions since it has no heater filament and it is assured almost unlimited life. In effect this results in a minute amount of current required to operate; and in instantaneous starting operation (no warm-up). The relay will operate over any input resistance from a dead short to 10 megohms, with leads of unlimited length. It also boasts a current amplification up to $2\frac{1}{2}$ million.

Utilizing a 115 v 60 cycle line source the relay consumes 2 w when in operation. The pilot relay is housed in an 18 gage steel case; and a visible jewel indicator permits visibility for off/on operation even while relay case is locked. Price is \$43.87. Circle 478 on Reader Service Card.



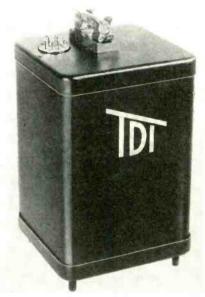
MICROSYNS have a variety of uses

LEAR, INC., 110 Ionia Ave., NW, Grand Rapids 2, Mich., claims manufacture of the smallest self-contained microsyn available. Approximately 1-in. in diameter and 1-in. long, the units have a sensitivity of 500 mv per deg with a

threshold of 0.01 deg at 20 v excitation. Linearity is within 0.5 percent to 7 deg. The subminiature microsyn weighs less than 1.2 oz.

Intended for use wherever there is need for accurate translation of angular displacement into electrical signals, the miniature units may be used in such applications as position-indication of gyros, control follow-up devices, computation, process control, motion and torque amplification.

The company produces the microsyns with pigtail connectors or with color-coded teflon-insulated terminals. Excitation may be 20 v, 400 cps or 25 v, 800 cps. The units use standard Bu Ord mounting and have demonstrated resistance to the most severe environmental conditions. Circle 479 on Reader Service Card.



FILTER reduces generator ripple

TRANSISTOR DEVICES, INC., 730 Boulevard, Kenilworth, N. J., announces a new filter designed primarily for aircraft, mobile and portable installations to reduce the generator ripple electronically 100 to 1 at worst point, and thereby eliminate the need for heavy chokes.

The unit output (20 v adjustable) is regulated to extremely close tolerance of 0 to 0.5 ampere.

Intended for use with 24 to 28 v d-c systems, the 40 cu in. filter

offers an efficiency of 85 percent and weighs only 2 lb. The electronic filter replaces heavy iron cored filters with a fraction of the weight, and is very easily installed. Circle 480 on Reader Service Card.



BASIC SWITCH

features ceramic case

ELECTRO SNAP SWITCH & MFG. Co., 4218 West Lake St., Chicago 24, Ill. The new basic switch S9-4 provides precision tolerances in an ambient temperature range of -100 deg to +900 deg F. The ceramic case contains the company's standard switch mechanism for spdt two circuit electrical control with a probable mechanical life of 750,000 cycles of operation. The staggered screw terminals, made of stainless steel, permit easy wiring. The switch case measures 14 in. long with standard 0.101 diameter mounting holes.

The switch is rated: 5 amperes 125/250 v a-c, 30 v d-c inductive. Circle 481 on Reader Service Card.



ELECTRICAL CONNECTORS

are miniaturized

AMPHENOL ELECTRONICS CORP., Chicago 50, Ill. A complete line of miniature electrical connectors has been announced. Named "minni E", the connectors are described as being the first miniatures fully conforming to the "E"

performance requirements of MIL-C-5015C. Besides being offered in an "E" construction, these connectors are available in potting, cable clamp and jacketed cable types—the potting construction also meets the moisture resistant requirements of MIL-C-5015C. Temperature limits are -67 F to +257 F. Voltage ratings are 500 v rms at sea level and 600 v rms at sea level. Using mated sealed connectors, no derating for altitude is necessary at 70,000 ft.

Features include a springloaded coupling ring, stainless steel bayonet slots and pins, hooded female contacts, unitized rear grommet seal, face seal gaskets and visual full engagement indicator. "Minni E's" are offered in 5 shell sizes and 17 insert arrangements, including coax contacts. Hermetically sealed receptacles are also available.



TIME DELAY RELAY has octal plug adapter

AGA DIVISION, Elastic Stop Nut Corp. of America, Elizabeth, N. J., has developed a new plug-in feature for its basic Agastat time delay relay models. The new octal plug feature adapts the Agastats to products and machines using plug-in components.

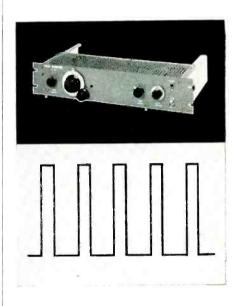
The octal plug is wired internally to the Agastat to allow immediate installation and operation. Two timing adjustments are available, a needle valve and a dial head adjustment. Each is adjustable from 0.1 sec to 15 minutes. There are four timing ranges available in the dial head type,

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brings the precision of digital comparison, measurement, and counting to the test laboratory.

One of a series of special purpose instruments designed for the digital specialist.

high frequency PULSE GENERATOR



The Burroughs Type 1050 Generator produces half sine wave pulses in the 10 mc range. Pulse width may be 30, 40, 50, 60, or 70 millimicroseconds. Pulse amplitude is adjustable from 1 to 30 volts of either polarity.

Further information is available from Dept. C.



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Service Card.

Designed for Application



The No. 90672 ANTENNA BRIDGE

ANTENNA BRIDGE

The Millen 90672 Antenna Bridge is an accurate and sensitive bridge for measuring impedances in the range of 5 to 500 ohms at radio frequencies up to 200 mc. It is entirely different in basic design from previous devices offered for this type service inasmuch as it employs no variable resistors of any sort. The variable element is an especially designed differential variable capacitor capable of high accuracy and permanency of calibration over a wide range of frequencies. A grid dip meter such as the Millen 90651 may be used as the source of RF signal. The bridge may be used as the source of RF signal. The bridge may be used as the source of RF signal. The continuity of the manual continuity of the signal in impedance, antenna resonance, transmission line impedance, standing wave ratio, receiver input impedances. By means of the antenna bridge, an antenna matching unit may be adjusted so as to provide the minimum standing wave ratio on the radiation system at all frequencies.

JAMES MILLEN MFG. CO., INC.

MAIN OFFICE AND FACTORY MALDEN MASSACHUSETTS



and each timing range is color coded for quick identification. Adjustments may be made within these timing ranges.

These time delay relays are

relatively unaffected by wide temperature changes from -65 to +160 F. They can be supplied for continuous a-c duty and for continuous or intermittent d-c service. They are available for a-c operation at all standard voltages from 6 to 550 v, 60 cycles and 25 cycles. For d-c operation, they are made for all standard voltages from 6 to 230 v. Circle 482 on Reader



VIBRATION PICKUP has outstanding linearity

CONSOLIDATED ELECTRODYNAMICS CORP., 300 North Sierra Madre Villa, Pasadena, Calif. A new vibration pickup, designed to the critical standards of laboratory accuracy yet filling all the requirements of operational use, is now available. Type 4-120 was developed for ground and in-flight monitoring of jet engines, but can be used in all h-f, low-amplitude vibration studies under extremes of temperature. The instrument is capable of continuous operation from -65 F to +500 F. It has a frequency range of 40 to 2,000 cps with linearity of ±4 percent of reading (for constant frequency) over the entire range.

Insensitive to transverse vibration, it will produce a signal directly proportional to the velocity as low as the recording equipment will measure. Maximum acceleration without damage is 50 g.

Among other important design features is the use of two magnets. one to control sensitivity and the other to control damping. This makes it possible to adjust the critical damping for specific temperatures up to 400 F. Another feature is a hermetically sealed case. The new unit is 14 by 24 in. and weighs less than 5 oz. Circle 483 on Reader Service Card.



PROGRAM TIMER with plug-in major parts

ELECTRONIC PROCESSES CORP. OF CALIFORNIA, 2190 Folsom St., San Francisco 10, Calif., announces a new electronic program timer which will independently control the sequence and timing of several related operations of a machine or process. Model PT-157 is designed to permit rapid and accurate change of the time settings controlling each operation and eliminates complicated and time consuming cam adjustments.

The unit as shown controls both the on-and-off sequence of six different operations. More operations may be controlled by adding one switching comparator for each additional on-and-off operation. Complete versatility as well as ease of maintenance is provided through the unitized plug-in construction of the major component

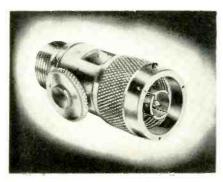
Time cycles up to 5 minutes are available, with accurate settings for each time control made against a calibrated meter. The time setting for any operation may be varied as the cycle is in progress without interrupting the time cycle or the settings of the other operations. Remote start and emergency stop switches are available, and circuit wiring flexibility is provided by a wiring duct. Circle 484 on Reader Service Card.



INDICATOR anticipates bearing failures

LYCOMING DIVISION, Avco Mfg. Corp., Stratford, Conn. A unique precision instrument capable of anticipating bearing failures in rotating machinery has been announced.

The temperature acceleration indicator acts as an electronic "detective" by detecting acceleration of temperature rise in a variety of units. It has applications for aviation, industrial and automotive development fields. Circle 485 on Reader Service Card.



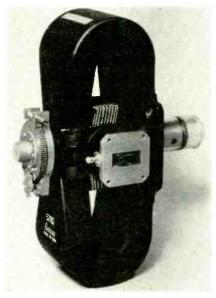
TUNING STUB for use in uhf and shf

Don-Lan Electronics, Inc., 1101 Olympic Blvd., Santa Monica, Calif. An inexpensive subminiature broadband coaxial matching and tuning stub for use in uhf and shf (to 10,500 mc) consists of a compact element furnished with a simple knob which is turned until the desired match is reached, then locked into position.

The unit, called a Widjet, is a 1.6 oz stub which takes the place of bulky telescoping matching stubs or tuning elements now in use. It consists of a variable temperature-compensated capacitor which is incorporated in the connector.

By simplifying problems of tuning, the Widjet allows the use of much less expensive components in coaxial systems. Less precise units which would otherwise produce vswr can easily be tuned out.

The unit is designed for applications in antenna systems of relays, communications, iff, radar and other r-f areas. Male and female type N connectors of the stub allow simple installation in existing systems. The unit meets or exceeds environmental requirements of MIL-E-5272A. Circle 486 on Reader Service Card.



X-BAND MAGNETRON tunable over 8,500-9,600 mc

BOMAC LABORATORIES, INC., Salem Road, Beverly, Mass., has added the 5780 tunable X-band magnetron to its expanding line of microwave oscillator tubes. The 5780 is an integral magnet, aircooled, pulsed type magnetron, which is continuously tunable over a frequency range of 8,500 to 9,600 mc. Being capable of reliable performance at over 300 kw (peak)

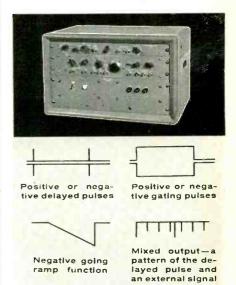
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DELAY GENERATOR produces Accurate

produces Accurate variable time pulses



The Burroughs Delay Generator Type 6010 produces the four types of pulse outputs shown above. Delays can range from 1 to 10,000 µsec. Instrument accuracy is 1%, and jitter is better than 0.02%.

Further information is available from Dept. C.

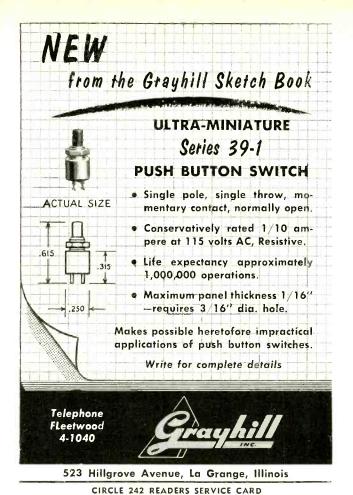
Burroughs

for engineers

BURROUGHS CORPORATION
Electronic Instruments Division

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power output, the 5780 is extremely well adapted for use in short pulse, X-band applications where high power output is desired.

The cathode terminal and mounting plate of the tube are designed to fit the standard fixed-frequency 4J50 mounting socket. The 5780 is 10 in. (maximum) long, 8.250 in. (maximum) wide, and weighs approximately 15½ lb. Circle 487 on Reader Service Card.



TRUE RMS VOLTMETER rugged and compact

CONSOLIDATED ELECTRODYNAMICS CORP., 300 N. Sierra Madre Villa, Pasadena, Calif., has available a stable, highly sensitive electronic voltmeter, designed for measuring a-c voltage in systems where it is imperative to know the true rms magnitude of nonsinusoidal periodic waveforms or noise potentials.

Model 14A features extreme accuracy in combination with rugged, compact construction. Low-current-consuming transistors, space-saving printed wiring, and dependable miniature components have been used to provide a reliable, small (6 by 8 by 6 in.), and lightweight (7½ lb) instrument. It operates on 115-v, 60 cps a-c.

The voltmeter is particularly suitable for use in noise-figure determination and in making noise-level measurements of equipment operating at audio and carrier frequencies. It utilizes a thermomilliammeter, a transistor amplifier, and a coaxial input attenuator to provide full-scale indication for input voltages from 0.5 my to 200 v. Accurate readings from 15 cps to 500 kc are provided. Voltage differences as small as 0.5

percent can be detected on the large meter. Further information appears in CEC Bulletin 7003. Circle 488 on Reader Service Card.



TIME DELAY LINES tubular, semiadjustable

DELTIME, INC., 608 Fayette Ave., Mamaroneck, N. Y., has announced model 107 semiadjustable tubular delay lines. The delay length may be specified by user and is adjustable over a range of 5 µsec. Adjustment is made by turning a sleeve along the threaded body. Intermediate pickoff may be specified as required. Body diameter is 11 in. maximum, while length of tubular casing is dependent upon the delay factor. Construction is suitable for resisting the most strenuous environmental conditions. Literature is available. Circle 489 on Reader Service Card.



POWER SUPPLY for transistor work

Model Rectifier Corp., 1065 Utica Ave., Brooklyn 3, N. Y. The new DV60-2 transistor power supply

features ripple attenuation down to a maximum of 0.05 percent at full rated output. This compact and precision-made unit, designed for developmental and experimental transistor work, delivers 0 to 60 v d-c, at currents up to 1,000 ma. Conservatively rated, it employs no moving parts and features isolated output.

The manufacturer states that one DV60-2 transistor power supply will replace several high-cost power sources, and end annoying battery hook-up problems. The a-c line operated unit employs a continuously variable autotransformer; a full-wave bridge selenium rectifier and a 2-section choke input filter in its simple, trouble-free circuitry. Located up front and easily accessible are protective magnetic circuit breaker; a 2-position voltmeter range switch; a 3-position milliammeter range switch; modern, easy-to-read volt and milliammeters accurate to 2 percent; and 5-way output binding posts.

Measurements are 10\(^3\) in. by 7 in. by 9\(^1\) in. Circle 490 on Reader Service Card.



CAPTIVE FASTENER for use on subassemblies

MORAN Co., 115 Main St., El Segundo, Calif. A new type of captive fastener particularly adapted for use on electronic subassemblies, has been licensed for manufacture and marketing to the Moran Co., by Northrop Aircraft, Inc., developers of the device.

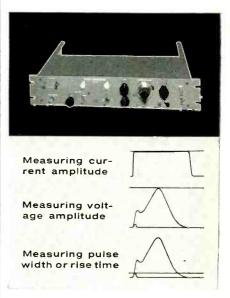
The fastener consists of a swaged-in-place sleeve, a bolt with both a threaded shoulder and shaft, and a small spring. Two threads at the top of the swaged-in-place sleeve accommodate the threaded shoulder of the bolt. Two turns of

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brings the precision of digital comparison, measurement, and counting to the test laboratory.

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PULSE CALIBRATOR measures peak amplitude



Burroughs Type 1810 pulse calibrator permits accurate oscilloscope measurements of voltage amplitude, current amplitude, pulse width or rise time. Over-all instrument accuracy of 1% extends from the millivolt range to 50 volts. Input may be ac, dc, or pulse.

Further information is available from Dept. C.

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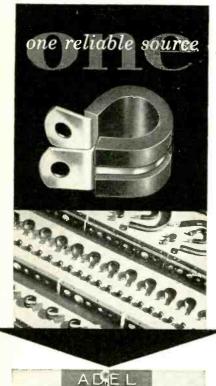
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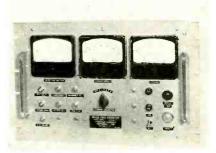
A DE L PRECISION
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Direct inquiries to Huntington Division 1444 Washington Ave., Huntington 4, W. Virginia DISTRICT OFFICES: Burbank • Mineola Dayton • Wichita • Dallas • Toronto the bolt carry it through the threads to become captive within the sleeve, held in place by a small tension spring.

The subassembly may then be tightly fastened to a major assembly by turning the bolt into tapped holes or other mating fasteners until the bolt tightens on a shoulder in the lower part of the sleeve.

Advantages of the new device include elimination of loose fastener parts on the assembly or repair bench and its quick detach features. The bolt has a hexagonal, slotted head permitting use of either screw driver or wrench to attach or detach the subassembly. Circle 491 on Reader Service Card.



PULSE RATE COMPUTER

in new instrumentation line

FAIRCHILD CAMERA AND INSTRUMENT CORP., Robbins Lane, Syosset, L. I., N. Y. Transistorized nuclear reactor control instrumentation can now be obtained for immediate delivery. This instrumentation covers the start-up, intermediate, and power ranges of operation. Various optional combinations and modifications are available, providing custom-flexibility to meet all requirements.

This equipment comes in either:
(a) commercial specification for use in laboratories and commercial power plants, or (b) military specification for use aboard Naval vessels and in Army packaged power plants.

The present design using silicon transistors only, is for operation up to 65 C and 100 percent humidity conditions. Equipment for higher temperatures can be supplied. Complete technical manuals and evaluation reports are available on request. Circle 492 on Reader Service Card.

New Literature

High Reliability Capacitors. The Gudeman Co., 340 W. Huron St., Chicago 10, Ill., has released a catalog, XR-461, on their line of high reliability capacitors. The capacitors discussed are manufactured under strict quality control procedures governing raw material selection and manufacturing conditions. Circle 501 on Reader Service Card.

Switch Catalog. Centralab, a Division of Globe-Union Inc., 900 E. Keefe Ave., Milwaukee, Wisc. A new 35-page manufacturer's switch catalog with complete specifications on rotary, slide, and lever switches is available.

The new catalog provides specifications on the complete line of Centralab switches capable of handling power from 1 kw to 1μ w. Circle 502 on Reader Service Card.

Production Machine. Burg Tool Mfg. Co., Inc., 15001 South Figueroa St., Gardena, Calif., has available literature on the Burgmaster six- and eight-spindle automatic, hydraulic turret drills which feature preselective spindle speeds, preselective feeds and precision depth control. The machines described have many uses in production of electronic assemblies. Circle 503 on Reader Service Card.

Transistor Analyzer. Norden-Ketay Corp., Commerce Road, Stamford, Conn., The four-page bulletin No. 387C describes the BCT-300 transistor curve tracer. Data include a block diagram showing the variety and flexibility of test functions, as well as specifications and photograph showing functionally located operating controls. Circle 504 on Reader Service Card.

Servomechanical Parts. Reeves Instrument Corp., 207 E. 91st St., New York, N. Y., has available a new 32-page comprehensive catalog of servomechanical parts. It describes a complete line of miniature and standard parts for prototype and production servos.

Included are descriptions and specifications for precision gears, mounting plates, shaft hangers.

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Mechanical Specifications: Wt. 60 lbs., 3" OD x 26 ft. boom, taper swaged elements, tapering from 136" OD to 1/2" OD, incorporating stainless steel hardware, "Borg-Warner" Cycolac moldings, 1/4-20 S.S. junction terminals and heavily cadmium plated mounting plate. Wind surface area: 7 sq. ft. Wind load at 100 mpb: 210 lbs.

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TYPE 803

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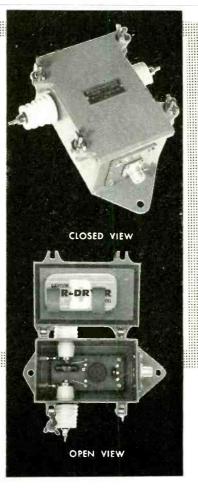
NEMS . CLARKE



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Silver Spring, Maryland

For further information write department AC-1



dial assemblies, couplings, and many other parts for assembling servo systems. Circle 505 on Reader Service Card.

Cradle Folder. Augat Bros. Inc., 33 Perry Ave., Attleboro, Mass. A 16-page booklet illustrates and gives dimensional diagrams and technical specifications for a wide line of cradles that feature heat transfer, and cushion from shock and vibration. It describes cradles for subminiature tubes, resistors, capacitors, transistors, diodes, capacitors, crystals and relays. Circle 506 on Reader Service Card.

Condensed Connector Catalog. U.S. Components, Inc., 456 East 148th St., New York 55, N. Y., has available a condensed verison of its comprehensive catalog of power and electronic circuit connectors, and associated equipment. The short-form catalog illustrates the company's complete line of connectors, and lists key specifications and operating characteristics. The line covered includes subminiature and miniature power and electronic connectors in several configurations; pressurized, waterproof and hermetically-sealed. Also shown are printed circuit connectors and card receptacles. Circle 507 on Reader Service Card.

Microwave Components. Microwave Associates, Inc., Burlington, Mass. A 16-page illustrated booklet covers the company's work in the field of waveguide components, magnetrons, semiconductors, and switching devices. Skills and facilities, production and administrative functions are outlined. Also included are pictures of the staff with their individual backgrounds. Circle 508 on Reader Service Card.

A-F Amplifiers. Cinema Engineering Division of Aerovox, 1100 Chestnut St., Burbank, Calif., has issued a catalog on its audio-frequency amplifiers, a dozen pages with illustrations, charts and diagrams.

The Cinema amplifier line stresses the laboratory type units and was designed essentially for maintenance-free sound systems, scientific laboratories, tape and disk recording equipment, motion picture film recording use and other purposes.

Each model and style described is adapted for individual applications, as well as for large multiple installations. Technically, the items discussed use custom-built transformers, precision wire-wound resistors, and other high quality components to provide constant performance and reliability.

Neither input nor output transformers are included in feedback loops; thus providing complete isolation. A new standardized plug-in chassis assembly further increases flexibility of application. Specifications listed in catalog 16-C are based on normal v-t characteristics. Circle 509 on Reader Service Card.

Preset Electronic Counters. Post Machinery Co., Beverly, Mass. A single-sheet bulletin covers the model PW-5 preset counter designed for accurate reliable industrial preset counting up to 5,000 units per second with direct readout totalizer. Description, features, optional features and specifications are included. Circle 510 on Reader Service Card.

Transistorized Amplifiers. Universal Transistor Products Corp., 143 E. 49th St., New York 17, N. Y. A timely new four-page case history brochure shows how the company solves difficult amplifier problems for diversified segments of the electronics industry.

Among the problems solved as described in the brochure are those of:

- (1) Designing a 20-w amplifier for p-a systems that fits into a 50 cu in. package.
- (2) Designing a transistorized plug-in high-gain audio amplifier that is directly interchangeable with a vacuum-tube unit.

Detailed descriptions and inside photographs of the units designed by Universal to solve these problems appear in the free brochure. Circle 511 on Reader Service Card.

Precision Roller-Lever Basic Switch. Micro Switch, a Division of Minneapolis-Honeywell Regulator Co., Freeport, Ill. Data sheet 127 illustrates and describes a low pretravel, high overtravel, roller-lever actuator basic switch. New uses, contact arrangement, characteristics, electrical rating, list price and discount schedules are included. Circle 512 on Reader Service Card.

Millisecond Operations Recorder. Fischer & Porter Co., Hatboro, Pa. Catalog 30A1400 illustrates and describes a transistorized millisecond operations recorder. Outstanding features and specifications are given. Circle 513 on Reader Service Card.

Semiconductors. Transitron Electronic Corp., Wakefield, Mass. A six-page folder contains illustrations, chief features and specifications for a line of silicon transistors, diodes, rectifiers and regulators, and germanium diodes and transistors. Circle 514 on Reader Service Card.

Controllers. Limit Daytronic Corp., 216 South Main St., Dayton 2, Ohio. A new, 2-color 4-page folder describing models 561 and 562 limit controllers is now available. The folder describes in detail the use of Daytronic limit controllers for automatic control of weight, size, force, thickness, pressure. flow. acceleration. stress, strain or other physical quantities. A number of suggested applications are shown. Specifications of standard models and description of selectable options is given. Circle 515 on Reader Service Card.

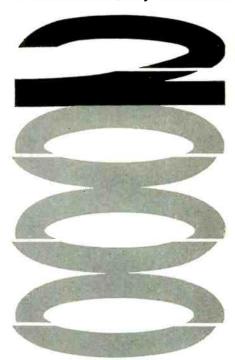
Semiconductor Solder Data. Anchor Metal Co., Inc., 966 Meeker Ave., Brooklyn 22, N. Y. As a service to the electronic and allied industries, the company has made available a handy reference chart for semiconductor soldering applications.

The reference chart offers phase diagrams for the more popular Anchor soldering alloys used in semiconductors. In addition, a list of high-purity elements is included, indicating the purity of each element that is available. Circle 516 on Reader Service Card.

This precision

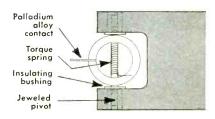


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Johnson, Others Honored By Franklin Institute



J. B. Johnson (left) accepts Longstreth Medal from S. W. Rolph, Franklin Institute president

DR. JOHN BERTRAND JOHNSON, head of the physics department, Thomas A. Edison Laboratory of McGraw-Edison, West Orange, N. J., was recently awarded the Edward Longstreth medal of the Franklin Institute in Philadelphia, Pa.

The honor was bestowed upon Dr. Johnson for his work leading to the understanding, recognition and measurement of noise in conductors caused by heat generated by molecular action. He established the fundamental nature of the noise which occurs in any kind of electrical conductor or resistor. The chief theoretical value of his

experiments is that it makes possible a determination of the lower limit of attainable noise reduction so that the impossible will not be expected of an amplifier.

A pioneer in the study of cathode-ray tubes, Dr. Johnson, who has been associated with the Edison Laboratory since 1952, developed the first sealed-off cathode ray oscillograph tube for general laboratory use.

Others in our field honored at the Medal Day ceremony included: Sir Robert A. Watson-Watt of Toronto. He received an Elliott Cresson Medal for his leadership in the development of radar systems.

A John Price Wetherill Medal went to Warren W. Carpenter of Winter Park, Fla., for important contributions to the technology of modern telephone switching.

William G. Pfann of the metallurgical research department of the Bell Telephone Laboratories, Murray Hill, N. J., received the Francis J. Clamer Medal in recognition of his discovery and application of zone refining metals and other crystalline substances.

Dr. Robert M. Page and Leo C. Young, both of the USNRL, Washington, D. C., were awarded the Stuart Ballantine Medal for their development of the first pulse radar system in the U.S.

Fairchild Enters Semiconductor Field

FAIRCHILD SEMI-CONDUCTORS CORP. has been formed in Palo Alto, Calif., for the development and production of silicon diffused transistors and other semiconductors, we are told by Fairchild Camera and Instrument Corp., the sponsoring organization.

The new company was organized around a group of senior scientists and engineers who have been working together in the development of transistors and other semiconductor devices. With four divisions already associated with missile and satellite instrumentation, semiconductors are expected to enhance Fairchild Camera's advances in that effort.

The research group of the new company will be headed by Dr. Robert Noyce, formerly of the Re-

Proceedings of the IRE

looks into outer space with RADIO ASTRONOMY

rich harvest of new information about the sun and certain solar phenomena, meteors and meteor showers recorded in broad daylight, the galaxy of stars of which our own sun is a part, and other galaxies infinitely distant from us. Regions of the universe invisible to the eye and the photographic plate can now be seen via their measurable radiation at radio wave lengths. New developments in antennas, propagation, low-noise receivers and the ionosphere are occurring because of progress in radio astronomy.

Here is the revolutionary technique which is carrying us to uncharted regions of the universe. Discoveries in this field during the last decade have created another vitally important branch of science.

January 1958 Special Issue

PAPERS BY KARL JANSKY in issues of PROCEEDINGS OF THE IRE during the early 1930's first reported the existence of radio waves emanating from outside the earth's atmosphere . . . now PROCEEDINGS publishes the first full discussion of radio astronomy, its current state and future prospects, written by the leading authorities from all over the world.

Special January Issue Contains Nearly 400 Pages Summarizing All That Is Known About Radio Astronomy

"On Karl Jansky" by C. M. Jansky, Jansky & Bailey.

"Recollections of Early Experiments in Radio Astronomy" by G. Reber, Hawaii.

"Radar Echos From the Moon at a Wave Length of 10 cm" by B. S. Yaplee, et al, N. R. L.

"Excitation of the Hydrogen 21 cm Line" by G. B. Field, Princeton.

"Extra Galactic 21 cm Line Studies" by H. S. Heeschen, Greenbank Nat. Obs., N. H. Dieter, Harvard.

"Radio Stars and the Milky Way at 440 mc" by N. G. Roman & B. Yaplee, N. R. L.

"A High Resolution Radio Telescope for Use at 3.5 M" by B. Y. Mills, et al, Australia.

"The Sydney 19.7 Mc/s Radio Telescope" by C. A. Shain, Australia.

"Radio Telescope Antennas of Large Aperture" by J. D. Kraus, Ohio State.

"An Antenna Array for Studies in Meteor and Radio Astronomy at 13 Meters" by P. B. Gallagher, Stanford U.

"A Wide Band Antenna System for Solar Noise Studies" by H. Jasik, Jasik Labs.

"Radio Interferometry of Discrete Sources" by R. N. Bracewell, Stanford U.

"A Polarimeter in the Microwave Region" by K. Akabane, Tokyo Obs.

"The Cornell Radio Polarimeter" by M. H. Cohen, Cornell.

"10.7 cm Solar Radio Flux Measurements" by W. J. Medd & A. E. Covington, Canadian Res. Council.

"Absorption Techniques as a Tool for 21 cm Research" by A. E. Lilley & E. F. McClain, Yale.

"Lunar Thermal Radiation at 35 KMC" by J. E. Gibson, N. R. L.

"Planetary and Solar Radio Emission at 11 Meters Wavelength" by J. D. Kraus, Ohio State.

MORE THAN 45 ARTICLES IN ALL

Proceedings of the IRE

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☐ Enclosed is company purchase order for the January, 1958 issue on RADIO ASTRONOMY.

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The Institute of Radio Engineers

1 East 79th Street . New York 21, N. Y.

search Division of Philco Corp. President of the new corporation is H. E. Hale, a v-p of Fairchild Controls Corp. and general manager of the Components Division.

Richard Hodgson, executive v-p of Fairchild Camera and Instrument Corp., is chairman of the board.

First products to be offered will be a high speed computer transistor to be followed by transistors which will serve the applications of vhf power oscillators, vhf amplifiers, and very high power applications at lower frequencies.

Autometric Names Operations Analysis Head

HERBERT BOMZER has been apdirector of operations pointed analysis for Autometric Corp. The outfit was organized in May, 1957 as a subsidiary of Paramount Pictures Corp. and is a research and development organization whose main interests are developing equipment and techniques reconnaissance systems, automatic processing and analysis of intelligence data, multicolor presentations, radar simulation equipment and other forms of specialized electronic systems.

Bomzer in his new capacity will

be responsible for analysis and coordination of the company's research and development efforts. He is a former projects supervisor for Ford Instrument Co., where he had been concerned with computer design problems, wave propagation theories, and the design of instruments and techniques used in the fields of reconnaissance and simulation.

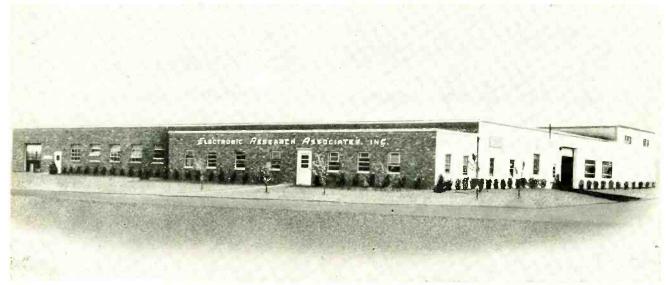
Hardwick, Hindle Inc. Buys George Rattray

GEORGE RATTRAY & Co., INC., Richmond Hill, N. Y., manufacturer of precision potentiometers, an-

nounces that it has become a wholly owned division of Hardwick, Hindle, Inc. of Newark, N. J., a subsidiary of American Seal-Kap Corp. George Rattray, founder of the company, will continue as president

The new association will enable the Rattray Co. to expand their engineering staff and facilities, and will permit completion of the development and manufacture of a full line of precision potentiometers. In addition, both technical and advisory services to customers will be expanded and improved. Rattray & Co. potentiometers will now be marketed throughout the country.

ERA Acquires Enlarged Facilities in Cedar Grove



Electronic Research Associates' enlarged facilities

ELECTRONIC RESEARCH ASSOCIATES, INC., manufacturer of tubeless and semiconductor products, formerly located in Nutley, N. J., announces the acquisition of new and enlarged facilities located in Cedar Grove, N. J.

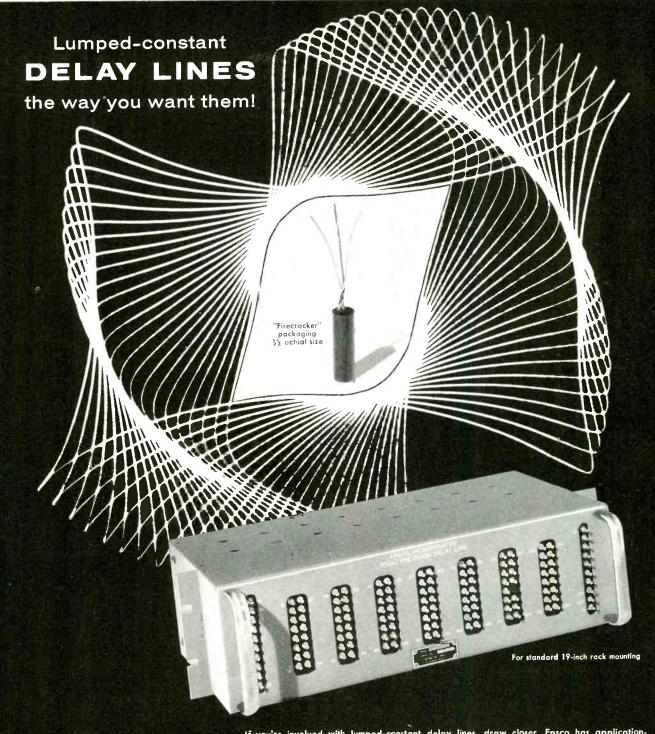
These new facilities represent a several-fold enlargement of floor

area. The new plant will accommodate increased production, engineering and processing facilities for the company's line of semiconductor and transistorized converters, power packs, transistor test equipment, and transistorized apparatus.

The plant facilities are air-con-

ditioned, one-story modern brick construction, and include several acres of additional ground to permit further expansion. Facilities previously located in the Nutley area will be maintained so as to accommodate the company's other manufacturing operations.

(Continued on page 320)



Epsco has met these limits — what are yours?

- Delays from 20 millimicroseconds to 200 milli-seconds or longer, if desired.
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- elay tolerance of 0.1% or 10 millimicroseconds, hichever is greater. haracteristic impedance tolerance of 1% from 0 to 5,000 ohms.
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If you're involved with lumped-constant delay lines, draw closer. Epsco has applicationengineered a wide range of such devices for coding, decoding, telemetering systems, speech synthesis, auto and cross-correlation, trigger delay, pulse forming circuits, etc.

Unique packaging is our meat: just tell us your space, configuration and mounting requirements and performance specifications. If you are concerned with environmental problems, we will test your delay lines for shock, vibration, moisture, altitude, temperature, etc., in Epsco's own in-plant environmental laboratory.

Custom engineering-production of electronic components (shift registers, magnetic logic elements, delay lines, special pulse transformers, etc.) is our specialty. You can count on Epsco's cooperation and conscientious service right down the line. Your inquiry will receive prompt action. Write for Delay Lines Technical Bulletin DL-55.

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DC to 5 MC LAB & TV
5" OSCILLOSCOPE

=450
Factory-wired and tested \$129⁵⁰
Also available as kit \$79⁹⁵

Features DC Amplifiers!

Flat from DC-4.5 mc, usable to 10 mc, VERT, AMPL.; sens. 25 rms mv/in; input Z 3 megs; direct-coupled & push-pull (hruout; K-follower coupling bet, stages; 4-step freqcompensated attenuator up to 1000:1. SWEEP; perfectly linear 10 cps-100 kc (ext. cap. for range to 1 cps); pre-set TV V & H positions auto, sync. ampl. & lim. PLUS; direct or cap. coupling; bal. or unhal, inputs; edge-lit engraved lucite graph screen; dimmer; filter; bezel fits sid. photo equipt, High intensity trace CRT. 0.06 usec rise time. Push-pull hor, ampl., fiat to 100 kc, sens. 0.6 rms mv/in. Built-in volt. callb. Z-axis mod. Sawtooth & 60 cps outputs. Astig. control. Retrace blanking. Phasing control.



NEW TV-FM SWEEP GENERATOR & MARKER

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Factory-wired \$11995
and tested
Also available \$6995
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Entirely electronic sweep circuit (no mechanical devices) with accurately-biased increductor for excellent linearity. Extremely flat RF output; new AGC circuit automatically adjusts osc. for max. output on each band with min. ampl. variations. Exceptional tuning accuracy; edge-lit hairlines eliminate parallax. Swept Osc. Range 3-216 mc in 5 fund. bands, Yariable Marker Range 2-75 mc in 3 fund. bands; 60-225 mc on harmonic band. 4.5 mc Xtal Marker Osc., xtal supplied. Ext. Marker provision. Sweep Width 0-3 mc lowest max. deviation to #-30 mc highest max. dev. 2-way blanking. Narrow range phasing. Attenuators: Marker Size, RF Fine, RF Coarse (4-step decade). Cables: output, 'scope horiz., scope vertical.



COMPLETE with steel cover and handle.

SPEED, ease, unexcelled accuracy & thoroughness. Tests all receiving tubes (and picture tubes with adapter). Composite Indication of Gm, Gp & peak emission. Simultaneous sei of any 1 of 4 combinations of 3 plate voltages, 3 screen voltages, 3 ranges of continuously variable grid voltage (with 5% accurate pot). New series-string voltages; for 600, 450, 300 ma types. Sensitive 200 as meter. 5 ranges meter sensistivity (1% shunts & 5% pot.) 10 SIX-position lever switches; free point connection of each tube pin. 10 push-buttons rapid insert of any tube element in leakage test circuit & speedy sel of individual sections of multi-section tubes in merit tests. Direct-rending of inter-element leakage in ohms. New gear-driven rollchart. Checks n-p-n & p-n-p transistors; separate meter readings of collector leakage current & Beta using internal de power supply. CRA Adapter \$4.50

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PLANTS AND PEOPLE

DuMont Names Divisional G-M



(continued)

Frederick H. Guterman

APPOINTMENT of Frederick H. Guterman as general manager of the Technical Products Division, Allen B. DuMont Laboratories, Inc., has been announced. Prior to joining DuMont, he was assistant vice president, sales and planning, at American Bosch Arma Corp.

Guterman will be responsible for overall sales and marketing of oscilloscopes and associated electronic test equipment, automotive test equipment, industrial tv systems, and two-way mobile radio systems.

Leach Appoints Director Of Engineering

ROBERT R. BEACHLER, Jr., has been appointed director of engineering for the Leach Corp., Los Angeles, Calif.

In addition to guidance and direction of the engineering activities of the Leach Relay and Inet Divisions in the design and production of relays and ground power units for aircraft and missiles, Beachler will be responsible for management of the Special Products Division, the future product development unit of the corporation.

Beachler had been associated with the Engineering Research Laboratory of North American Aviation, Inc., for the past 17

ACME ISONEL WIRE

Plus Acme #150 VARNISH
Equals Class B
Equals MIL-T-27A Class S

Freed Transformer Co., Inc., Brooklyn, N. Y., a leader in engineering and manufacturing of transformers and reactors for the electronics industry, has found in the above equation the solution to the manufacturing and performance problems of Class B (MIL-T-27A, Class S) Commercial and Military units

Acme Isonel Wire is a Class B (MIL-T-27A Class S) wire. However, optimum insulation system performance can only be achieved when this wire is impregnated with a compatible varnish. Acme #150 is that varnish.

Acme #150 Varnish does not require a high temperature cure. It has excellent resistance to oils. Acme #150 Varnish meets all the requirements of specifications MIL-V-1137A, Class CB, Type M for government equipment. In fact, it exceeds the heat resistance requirements of this specification by 50%.

Acme #150 Varnish improves thermal stability, while maintaining dielectric strength when used in Class B (MIL-T-27A Class S) windings.

ACME WIRE CO.

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MAGNET WIRE • COILS
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INSULATING VARNISHES
AND COMPOUNDS



December 1, 1957 — ELECTRONICS

years, successively holding positions of engineer, supervisor, group leader, and director of the laboratory. He has also been active as a consultant in instrumentation and electroacoustics.

Zwerin Assumes IRC Post

INTERNATIONAL RESISTANCE Co., Philadelphia, announces the appointment of Martin I. Zwerin to special representative for market development of new products.

Prior to joining IRC, Zwerin was



Martin I, Zwerin

a staff member of the Curtiss Wright Corp., handling market research and advertising. He was previously associated with Westinghouse Electric International Co. as sales engineer, and with the Philco Corp. as electronics engineer.

GE Enlarges Computer Setup

GENERAL ELECTRIC Co. has started expansion to double size of its computer division plant at Phoenix, Ariz. The work requires an addition of 30,000 sq ft of building at a cost of \$225,000. Target date for completion is Jan. 1.

At the same time the company announced optioning of 160 acres

PART COST CUT 1/2

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Maximum length: 1¾"

Send today
for bulletin.

Many manufacturers have learned that GRC specialized techniques and facilities have cut the cost of tiny components for their products 50% and more compared with production in their own plants. Parts like the slotted gear shaft illustrated are die cast to precise specifications—trimmed, ready for use—in one automatic operation. Consult Gries about cost-cutting components for your products.



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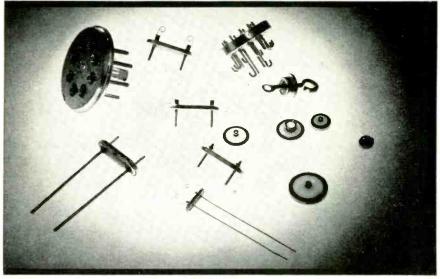
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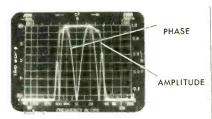
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CURVE TRACER



that conveniently measures both

PHASE & AMPLITUDE

response characteristics

on identical frequency scales.



PANORAMIC'S unique SONIC PHASE & AMPLITUDE RESPONSE ANALYZER

MODEL

A multi-purpose instrument, the PA-1 quickly and conveniently analyzes two important characteristics of audio devices and networks . . . phase shift and amplitude response vs. frequency.



The PA-1 operates with the widely accepted Panoramic Sonic Analyzer LP-1a, a proven performer. angle and amplitude readout appear as single line curves on identical frequency scales . . . either on the screen of the LP-la or on its auxiliary chart recorder, Model RC-3. Selection of the type of analysis is quickly obtained with a front panel control. Overall frequency range is from 20 cps to 22.5 kc.

ADVANTAGES

Amplitude/Frequency Response

- Provides virtually unlimited dynamic range
- Indicates response to fund-amental frequencies only
- Discriminates against hum
- Minimizes the effect of

Phase Angle/Frequency

- As an attenuation curve tracer: measures
 "stop-band" regions in excess of 100 db
 As a swept phase shift curve tracer: reads out
 ordinates on vertical linear scale calibrated to 180°
 full scale . . . or magnifies small phase shifts for detailed study by expanding a fewer number of
 degrees to full scale
 Lag and lead sense determined by an
 internal circuit

The PA-1's many advantages are still further amplified when used in combination with other instruments forming a part of Panoramic's unique response tracing system.

Panoramic's Triangular Wave Generator TW-1 generates a continuously variable linear bidirectional swept frequency enabling the establishment of the proper rate of scan to insure precise measurement of non-transient response characteristics.

Panoramic's Signal Alternator SW-1 presents two signals at alternate intervals making possible the injection of a marker or the comparison of two similar responses. leader Variations are instantly visible.

> Write, wire, phone TODAY for detailed specification bulletin on the PA-1.

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of land in Deer Valley, near the present temporary plant site, as location for a permanent gardentype factory site.

The GE computer division, which headquarters at Phoenix, was recently awarded a \$1½ million annual contract to operate a computer center at the Army ballistics agency in Huntsville, Ala. GE already operates a computer center at Arizona State College, at Tempe. Some of the computation work of the new center will be handled at the Arizona center. Huntsville is the home of Redstone, the Army's missile development center.

RCL Expansion Under Way

RADIATION COUNTER LABORATORIES, INC., Skokie, Ill., has started an expansion program which will double the size of its present plant, Completion of the 64,000 sq ft addition will increase RCL's present production capacity 100 percent.

present trend toward nuclear data processing using instrumentation typified by RCL's 256-Channel Analyzer and the augmented demands for radiation sensing elements has forced the organization to expand to meet the present and also the expected future needs for its equipment.

RCL's gross sales the last two quarters were in excess of a two million dollars per year rate and were the highest in the company's ten year history.

Webcor Makes Test Facilities Available

THE Government Division of Webcor, Inc., Chicago, Ill., plans to make available its extensive environmental and general test facilities to serve the testing needs of industry. In the past, these facilities have been used by Webcor exclusively for its own developmental and contract work. At present, these laboratories are being utilized to test timers, signal generators,

data recorders, guidance systems, direction finders, keyers, and classified Military equipment, as well as Webcor's commercial products.

The laboratory will furnish facilities for testing commercial items in addition to performing tests on qualification acceptance, inspection and quality assurance tests to fulfill requirements of military specifications.

Richard F. Hahn will manage the laboratory facilities in this expanded program.

Control Data Hires A Washington Director

HENRY S. FORREST has been appointed to the position of director of government service engineering and manager of the eastern office, located at Washington, D. C., for Control Data Corp., Minneapolis, Minn.

In his new position, Forrest will maintain liaison with government



Henry S. Forrest

clients in research and development activities of the firm. Control data will be active in the fields of electronic data processing and control, including advanced weapons and guided missile systems, air traffic control, and air defense.

Forrest has been associated for the past 10 years with Sperry Rand's Univac Division as Washington manager for research and development and special systems sales, and with one of its predeces-



This new Speer Packaged Assembly Circuit offers you a wide variety of custom, preassembled units of high-quality components for use in conjunction with printed board applications.

P.A.C. permits the insertion, as a group, of a full range of capacitors and resistors in simple or complex circuitry. Each P.A.C. is based on components of uniform dimensions, %" diameter and %" long. Component availability includes Jeffers tubular ceramic capacitors and Speer fixed composition resistors, providing wide circuit flexibility in a single P.A.C. unit.

ADVANTAGES OF SPEER P.A.C.

- · Simplifies chassis design and assembly
- Reduces printed circuit board area and insertion operations
- Permits easy and low-cost component change-over to accommodate circuit revisions
- Broad choice of characteristics—low capacitance temperature compensating units and high capacitance bypass capacitors mounted in same P.A.C. unit
- Isolation of individually mounted units provides low shunt capacitance across resistors
- Pretested components achieve unusually close tolerance assembly

Learn more about the new Speer P.A.C. For information write to:

JEFFERS ELECTRONICS DIV.

Speer Carbon Co. Du Bois, Pennsylvania





- **★ Up** to 50,000,000 megohms!
- * Test voltage variable 100-600 vdc!
- ★ Uncrowded 4½" meter scale!
- ★ Automatic capacitor discharge!
- * Safe test terminals!
- ★ Only \$365!

Here's the only high resistance megohmmeter selling at \$365 with features not found on instruments selling for twice as much. Measuring range up to 50,000,000 megohms to meet the requirements of recent advances in insulating materials. The t-7 Megohmmeter is housed in a hardwood case with recessed vertical panel and convenient carrying handle.

Industrial Instruments has a wide selection of megohmmeters for both laboratory and high-speed production testing. Choose the model that best suits your needs from this table of specifications.

Model	TEST Voltage	RANGE		POWER	
		Low	High	Consumption	PRICE
L-2A	200 fixed	I meg.	100,000 meg.	40 watts	\$200
L-4A	200 and 500 fixed	1 meg. 2.5 meg.	100,000 meg. 250,000 meg.	52 watts	\$230
L-6B	100 to	1 meg.	100,000 meg	82 watts	\$295
L-7	100 to	1 meg.	5x10'' ahms	75 watts	\$365

*Continuously variable, built-in voltmeter for accurate setting.

Write today for complete catalog of Electrical Test Equipment manufactured by . . .



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sor organizations, Engineering Research Associates, Inc., of St. Paul.

With ERA he served as the Washington representative and in several engineering assignments. Before that, Forrest held electronic engineering posts with the Navy's Bureau of Ships and the Naval Research Laboratory.

Packard-Bell Hires Liaison Engineer



G. M. Russell

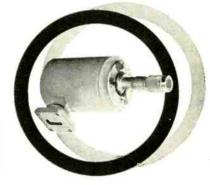
GEORGE M. RUSSELL has joined Packard-Bell Electronics as liaison engineer attached to the Washington, D. C., office.

Russell comes to Packard-Bell from RCA Service Co., Inc., where he was engaged in systems engineering at Patrick Air Force Base, Florida. He formerly was associated with RCA in field engineering attached to the U. S. Embassy in The Hague, Netherlands, and prior to his RCA affiliation he was a field engineer for Phileo Corp.

Electro Data Names Allen

JOHN T. ALLEN has been appointed field engineering supervisor in the Dallas, Tex., district of the Electro

D-B broad band gas-filled cavity wavemeters



Each instrument covers a wide segment of the total range. Only 11 sizes serve from 2.6 KMC to 90 KMC. Accuracy is so high they may be used as secondary standards. Nitrogen filled and sealed for long life and high Q. Bi-metallic structure provides high degree of thermal compensation. Write for literature.



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December 1, 1957 — ELECTRONICS.

Data Div. of Burroughs Corp.

Allen is responsible for installation and servicing in the Dallas area of Electro Data equipment—including the Datatron electronic data processing systems and E101 computers.

He joined Electro Data in June, 1956, after serving as an electronic computer customer engineer and an installation technician.

Elco Acquires Macson Co.

ANOTHER step in the long range expansion program of Elco Corp. was recently reached with the acquisition of Macson Co., Los Angeles, Calif., by Elco's wholly owned subsidiary, Elco Pacific.

With this acquisition Elco is adding a complete line of power connectors to its present line and will also be in a position to give better service to the rapidly growing Pacific industrial area.

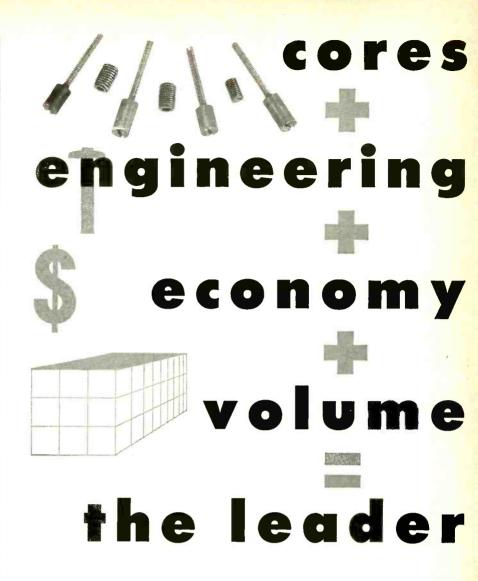
Honer Promoted at G-D Corp.

ROBERT E. HOMER, specialist in electronics and microwave systems for more than a decade, has been appointed chief electronics engineer at Convair (San Diego), a Division of General Dynamics Corp. Honer joined Convair in 1953 as design specialist in charge of the microwave group.

Honer's career has included color to research immediately following World War II with the Zenith Radio Corp. and research and development work as associate professor of research at Georgia Tech. He has had published numerous articles on antennas and microwave.

Hunt Becomes Sales Engineer

APPOINTMENT of J. N. Hunt as Atlanta district sales engineer for the Collins Radio Co., Cedar Rapids, Iowa, was recently announced. He had been an associate field engineer for the company be-





*trademark

Also, custom iron cores to your specifications.

We are proud as the originators of ENGINEERED ECONOMY* IRON CORES that we have been able to reduce the prices of our products so tremendously in the past few years. This has been achieved through constantly increasing volume production, reduction of costs through improved manufacturing techniques and the use of automation. We now have better and more uniform quality than ever before.

Now, you can select from over 19 types of ENGINEERED ECONOMY* IRON CORES where previously we had to produce over a hundred. Fewer varieties enables us to stock more and sell at lower prices. We invite your inquiry.

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Vitreous Enamelled Miniature Capacitors

Values: 18 to 1000 uufd

Tolerances: ±20%, ±10%, ±5% and ±2% (±0.5 uufd at low values) Temperature Coefficient:
Substantially zero — with spread of ±40 parts/million/degree C

Max. Ambient Temperature: 150° Centigrade

Power Factor at 1 mc: better than 0.001

Manufactured in England and Canada

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Welwyn International, Inc.

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fore receiving this assignment.

Hunt was formerly associated with Lockheed Aircraft as a special course instructor in electronic systems. He also served for 10 years as a communication specialist for the Atlanta and West Point railroad and for two years served in the Navy as an electronic systems specialist.

Juaire Named Chief Engineer



Phillip Juaire

BUREAU OF ENGRAVING, INC., Minneapolis, Minn., makers of etched circuits, has appointed Phillip Juaire chief engineer in charge of research and product development of its Industrial Division.

Along with his research and development duties, Juaire is also responsible for operation of the Bureau's control laboratory.

GPE Promotes Garman to V-P

RAYMOND L. GARMAN was recently elected to the office of vice president—engineering and research of General Precision Equipment Corp. He has been technical director of General Precision Laboratory Inc., a GPE subsidiary, since 1945 and has, in addition, held executive positions of increasing responsibil-

TEST YOUR MAGNETIC CIRCUITS



RAWSON FLUXMETER
TYPE 504

The only portable fluxmeter available which returns rapidly to zero when a single button is depressed. Simple and fast in operation. Convenient and light in weight.

Not limited to a single type of measurement. Has universal application for laboratories or production. Measures strength of magnets and electromagnets, permeability and hysteresis loops for iron and steel, total flux lines in circuit, flux lines developed in air gap, etc.

Has a mechanical clamp to protect the pivots and jewels when in transit.

RAWSON ELECTRICAL INSTRUMENT COMPANY

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Specialists in designing and manufacturing of allpurpose fasteners and wire forms. Tooled to produce over 1000 styles in any screw size, material, finish, quantity, to your specifications.

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ELECTRONICS — December 1, 1957

PLANTS AND PEOPLE

(continued)

ity, having recently been elected chairman of the board of GPL, an office which he will continue to hold.

In his new position and as chairman of the engineering plans committee, Garman, with technical representatives from other GPE companies, will have general oversight and direction, at the policy level, of the engineering and research activities of the companies in the GPE group, which extend over a wide area of industrial equipment and controls, motion picture and ty equipment, and components and systems for guidance, control and simulation of missiles and aircraft.

Ace Moves to Larger Quarters

THE Ace Engineering and Machine Co., Inc., Philadelphia, Pa., manufacturers of shielded enclosures recently moved into its newly completed plant at Huntingdon Valley, Pa., a suburb of Philadelphia.

The one-floor air-conditioned offices and plant enclose an area of approximately 18,000 sq ft, and house the executive offices, together with all engineering, design, manufacturing, and testing facilities, under one roof.

Ace Engineering designs and fabricates radio-interference-proof shielded enclosures of copper, bronze, aluminum and galvanized steel screening, as well as sheet metal. The enclosures permit delicate radio frequency tests to be carried out in an area completely free of extraneous radio interference. They are also used to house powerful signal generators and other sources of r-f generation.

National Beryllia Opens New Plant

NATIONAL BERYLLIA CORP., producing high purity, high density beryllium oxide, alumina oxide, zirconia and thoria configurations, announces the opening of a new production plant in Haskell, N. J. Completely retooled with new and larger furnaces, mixing, grinding



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- · fast operate and release time.

You can order XY Deca Switches in a wide variety of off normal and release magnet spring combinations to suit your specific requirements. Compact and light, the switches are 43/4" long, 4" wide, 11/2" high and weigh 201/4 ounces.

Complete technical details are contained in Bulletin T-5001, available on request.



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and extruding equipment, National Beryllia Corp. offers prompt efficient service in the fabrication of precision ceramics for the nuclear energy, rocketry, electronic and metallurgical industries.

Brown Takes Exec Post at ESC

ESC CORP., Palisades Park, N. J., manufacturers of delay lines, has announced appointment of Col. Charles B. Brown as administrative assistant to the president, Morton Fassberg. Brown retired earlier



C. B. Brown

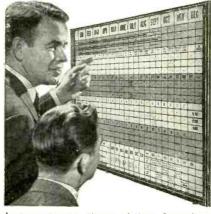
this year, after more than 30 years of military service.

Since World War II, he has served as executive officer, Signal Center, Ft. Monmouth, N. J.; Army Coordinator, Joint Communications Electronics Committee of the Joint Chiefs of Staff, Washington, D. C.; Chief, Frankfurt Signal Branch, Signal Division of the European Command. He was also Director of Communications Department, Armored School, Fort Knox, Kentucky.

Dominguez Elected Assistant V-P of IT&T

Jose D. Dominguez, recently appointed executive engineer for the telephone and radio operating department of IT&T Corp. in New

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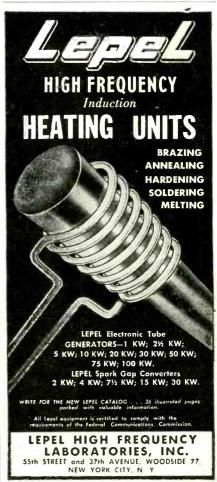
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THE MAN WE MEAN IS A COMPOSITE of the editorial staff of this magazine. For, obviously, no one individual could ever accomplish such a ast business news job. It's the result of many qualified men of diversified and specialized talents.

AND. THERE'S ANOTHER SIDE TO THIS "COMPOSITE MAN," another complete news service which complements the editorial section of this magazine—the advertising pages. It's been said that in a business publication the editorial pages tell "how they do it"—"they" being all the industry's front line of innovators and improvers—and the advertising pages tell "with what." Each issue unfolds an industrial exposition before you—giving a ready panorama of up-to-date tools, materials, equipment.

SUCH A "MAN" IS ON YOUR PAYROLL. Be sure to "listen" regularly and carefully to the practical business information he gather...



McGRAW-HILL PUBLICATIONS

York City, has been elected an assistant vice-president of the corporation.

He has been with the IT&T System for 30 years in various capacities, and was president of its Puerto Rico Telephone Co. from January 1956 to September 1957, during which time the company carried out the largest program of expansion in its history.

Applied Research Changes Name, Moves

THE NAME of Applied Research, Inc., Chicago, Ill., industrial research firm, has been changed to Booz, Allen Applied Research, Inc. The firm's headquarters has been moved to 430 Green Bay Road, Kenilworth, Ill.

Booz, Allen Applied Research, Inc., has facilities at Frederick, Md., and Dayton, Ohio. The firm does research and development work on scientific and technical problems for industrial companies and the government.

The company currently is conducting an extended operations research project for the Army, and is also engaged in work for the Navy and Air Force.

For industrial companies, the firm is working on problems involving automation, electronics, thermodynamics, electronic instrumentation for medical experiments, operations research and nuclear technology.

Company Formed to Serve Computer Industry

A NEW electronic company, Digital Equipment Corp., designed to provide vital testing equipment to the billion-dollar-a-year U.S. computer industry, has been incorporated in Maynard, Mass.

Two recent members of the staff of the Lincoln Laboratory of MIT, both active in the design and application of advanced computers and particularly development of the Semi-Automatic Ground Environment (SAGE) computer systems for the U. S. Air Defense, are or-



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ganizers of the new enterprise. They are Kenneth H. Olsen, president, and Harlan E. Anderson, vice president.

Several factors motivated the establishment of this business. One was the long delays that occur from the time a new idea is developed in a laboratory to its availability in the field. Digital Equipment Corporation hopes to shorten this lag and expects delivery of its first products within 60 days.

Hunter Named To Exec Post



Gould Hunter

CAPTAIN GOULD HUNTER, USN (Ret), has been named administrative assistant to the president and executive vice-president of Eitel-McCullough, Inc., San Bruno, Calif. This position, as assistant to W. W. Eitel and J. A. McCullough, cofounders of the company, is newlycreated because of expansion of the Eimac product line and production facilities.

Hunter, who joined Eitel-McCullough, Inc., in late 1956 as assistant to the vice president, manufacturing, was formerly Commanding Officer of the Navy Electronics Laboratory at San Diego, Calif.

Robinson Joins Walkirt

JAMES ROBINSON has joined the Walkirt Co., Inglewood, Calif., as chief engineer. He will be respons-

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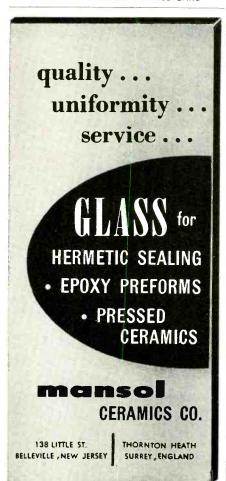
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ible for all new product design, the application of Walkirt products, and most phases of production quality control.

(continued)

Robinson joins the company direct from a four-year association with General Communication Co., Boston, Mass., where he was part of the engineering department's design-development team.

Prior thereto, he was for three years associated with the Canadian Government and concerned with electronic instrumentation on several projects including a geophysical survey project north of the Arctic Circle.

Senseney Takes New Post

IRON FIREMAN MANUFACTURING CO. recently named George Senseney as director of engineering for its electronics division in Portland, Oregon. He will also head research and development activities.

The division manufactures relays, gyroscopes, slip rings and brushes, heating controls and other electronic parts and instruments.

Senseney went to Portland from New York City where he was vicepresident and chief engineer for Rahm instruments after being assistant director of research for Reiber Research Laboratories.

Schneider Joins Magnavox

APPOINTMENT ofStanley Schneider as director of engineering for the Government and Industrial Divisions of The Magnavox Co., Fort Wayne, Ind., has been announced. He comes to Magnavox from the Canadian Westinghouse Co. where he has been employed for the last six years.

Tracerlab Appoints Hansen

S. S. AUCHINCLOSS, president of Tracerlab Inc., Waltham, Mass., recently announced the appointment of Carl Woodrow Hansen as chief

Using **Thermistors**

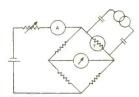
Edited by

FENWAL ELECTRONICS

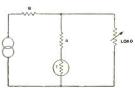
This is the third in a series of news columns devoted to thermistors vice that is super-sensitive to temperature change.

The example in point: power measurement and voltage control.

A bead thermistor can be used to balance a bridge circuit, allowing the thermistor current to be measured and its DC power calculated. This is done with a 2000 Ω bead thermistor in a 200 Ω bridge circuit with a variable resistor in series with the bridge. This will heat the thermistor enough to lower the resistance to 200 Ω and balance the circuit to determine the H.F. power. By applying a source of high frequency power to the thermistor through capacitors this will further heat the thermistor and the bridge will be unbalanced. Then reduce the DC power until the bridge balances again. Calculate the new DC power, and the difference between the two calculations is the H.F. power.



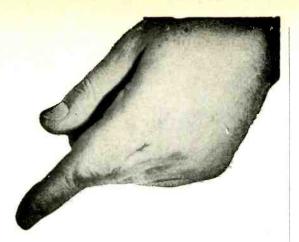
To maintain constant voltage a thermistor with a suitable series resistor can be placed in parallel with a load in a circuit. As the load resistance increases there is a reduced drop across resistor "B." This tends to raise the voltage across the load. The thermistor heats up, reduces its resistance, and more current passes through it and through resistor "B." This brings the voltage across the load back to its original state. Controls like this can maintain as close as 1% voltage regulation over a broad range of load resistance, or any voltage from 1/2 volt to 100 volts can be regulated in this way with suitable circuitry.



Engineers: these and other thermistor applications are discussed in 12-page catalog EMC-1. Write for your copy to FENWAL ELECTRONICS, INC., 211 Mellen St., Framingham, Massachusetts.



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anginear of the Industrial Produ

engineer of the Industrial Products
Division.

Hansen was formerly with the X-ray Division of General Electric Co. in Milwaukee, Wisc., where he was project engineer in the Apparatus Engineering Dept.

General Transistor Names Vice-President



Bernard Jacobs

HERMAN FIALKOV, president of General Transistor Corp., has announced the appointment of Dr. Bernard Jacobs to the newlycreated post of vice-president in charge of research.

A specialist in semiconductor development, Jacobs has performed in this capacity at Federal Telephone and Radio Corp. and Radio Receptor Co. He was previously employed by Sperry Semiconductor Division of Sperry-Rand Corp. as head of material research where he was responsible for the development of basic techniques usable in semiconductor device fabrication.

Instron Builds New Plant

To MEET stepped up demands for its electronic testing equipment, Instron Engineering Corp., Quincy, Mass., is building a new 25,000 sq ft plant in Canton, Mass. The new

plant will be devoted to the design and production of universal testing machines and other electronic test equipment. The building will also house the company's administrative and engineering offices. At present, Instron employs more than 70 peo-

Company Formed to Grow Single Crystals

THE SINGLE CRYSTAL CORP. OF AMERICA was recently formed in Saxonburg, Pa., to grow single crystals of various materials for electronic, optical and nuclear applications.

Besides the production of growing single crystals, Siccoa is also engaged in research on new single crystals, on its own as well as for industry and government. Siccoa is prepared to engage in any problem concerning single crystal growth since it is staffed with physicists in the solid state, nuclear, electronic and chemical fields.

Gramer-Halldorson Gets New Chief Engineer

LARRY STINEMAN has been appointed chief engineer for Gramer-Halldorson Transformer Corp., Chicago, Ill. He recently served several years as chief engineer for Merit Coil and Transformer Corp., prior to which time he was senior engineer for Thordarson-Meissner.

Avien Names Engineering Manager

SEYMOUR RABINOWITZ has joined Avien, Inc., as the company's engineering manager. He was formerly supervising engineer, Atomic Engineering Branch, and chief of product engineering, Picatinny Arsenal, Dover, N. J. He also served on the staff of the Atomic Energy Commission as branch chief in the Special Projects Division, and as electronics engineer on the Technical Advisory Staff of the Commission's New York Office.

In addition to his experience in the field of atomic energy, Rabino-

witz was for a number of years with the Signal Corps serving in a supervisory capacity in several fields including test instrumentation, environmental protection systems, and component engineering. While with the Signal Corps, he was also responsible for the technical administration of one of the Signal Corps' largest radar sys-

Allegany Instrument Hires Perino



P. R. Perino

P. R. PERINO recently joined the staff of Allegany Instrument Co. at Cumberland, Md., as project engineer. He was formerly head of instrument engineering for Aerojet-General Corp. at Sacramento. Calif., and has also headed Proving Ground Instrumentation Phillips Petroleum Company's Rocket Fuels Division at McGregor, Texas.

AES Honors Long

Roy A. Long, research engineer in Stanford Research Institute's engineering research division, has been elected a Fellow in the Audio Engineering Society. Recognition of Long's activities in communications systems was made recently at the annual awards banquet in New York City.



placed between ter minals. Binder head screws and terminals brass, nickel plated. Insulation, molded

and minals--Screw Solder Terminals— Screw Terminal above, Panel with Panel with Terminal be-Solder For every need.

Six series meet every requirement: No. 140, 5-40 screws; No. 141, 6-32 screws; No. 142, 8-32 screws; No. 150, 10-32 screws; No. 151, 12-32 screws; No. 152, 1/4-28 screws.

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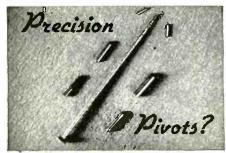
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New Books

Television Engineering Handbook

EDITED BY DONALD G. FINK McGraw-Hill Book Co., Inc., New York, 1957, 1,483 p, \$18.00.

THE "Television Engineering Handbook" is a monumental work which, in 20 chapters written by 33 authors, endeavors to present the factual information which one is usually looking for when he reaches for a handbook.

The opening chapters (written by the editor-in-chief in his usual lucid style) present basic equations, numerical data and constants, definitions, explanation of technical terms and both Governmental and industrial standards pertaining to the radio frequencies, the video frequencies and (to a minor degree) the audio frequencies found in television. Furthermore, just about all the specialized fundamental data a television engineer is likely to need is also presented (common mathematical tables, which are generally available in other handbooks, are omitted).

▶ Optical Aspects—In the next two chapters, well-known authorities present, in satisfying detail, information relative to monochrome and color vision, geometric and physical optics and the colorimetry that is of interest to workers in the television field. The difference between resolution as measured in photography and in television (which often confuses the uninitiated) is also detailed together with discussions of diffuse versus specular densities, photographic film versus television camera speeds and (some 14 chapters later) the relation between f/ and T-stop num-

The theories of color vision and of color matching, which form the foundation for all color television systems are clearly presented, as are explanations of the foremost systems of color specification. Particular emphasis is placed upon the CIE system and its relationship to the NTSC color television

► C-R Devices — Following chap-

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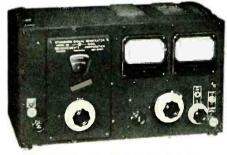
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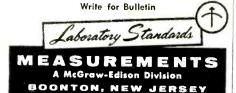
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CIRCLE 283 READERS SERVICE CARD ELECTRONICS — December 1, 1957

ters cover cathode-ray devices, including both display and pickup tubes, and the scanning deflection circuits for monochrome and color picture tubes. A tabular summary of the important characteristics of six camera tubes currently in use (two of them abroad, only) for monochrome and color service in both television and industrial applications will be appreciated by those who have occasion to compare the characteristics of various pickup devices. Similarly, supplementing the descriptions and diagrams, there are summary tables comparing the principal monochrome and color picture tubes.

Another chapter covers the problems of scanning synchronization, synchronizing signal separation and makes passing mention of the decoding of color information synchronizing signal generation. The transmission of monochrome and color information and the nature of the composite video signals and waveforms that must be handled in such transmission are covered very competently and with thoroughness in still other chapters. The encoding of color signals is also covered in considerable detail.

Video frequency, radio-frequency and i-f system components are covered, as is the wideband modulation and demodulation processes and the numerous aspects of wave propagation in the vhf and uhf portions of the spectrum.

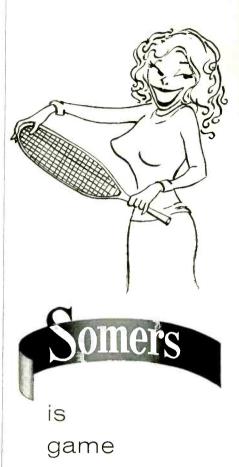
Two chapters are devoted to monochrome and color television receivers, one to television studio and film camera chains and still another to color broadcasting terminal equipment.

An authoritative chapter is devoted to the often forgotten, but very vital television relay systems and network transmission facilities that makes nationwide television possible in this country. Finally, television transmitters, and their associated transmission lines and antennas are described.

The bibliographies which accompany the various chapters vary from meagre to abundant. Where supplied, they will be valuable to workers in the field.

For the most part, the subjects are covered adequately. However,

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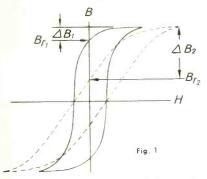


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Advantages of
Air Gap vs. Toroidal
Construction in
Pulse Transformers

As pointed out in previous Pulse Notes, a pulse transformer wound on a core with an accurately controlled air gap performs more satisfactorily in some applications than one wound on a toroidal (gapless) core.

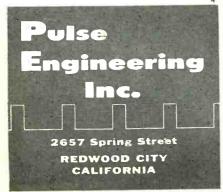


Consider for a moment the two B-H loops in Figure 1. The loop shown in solid lines is for a toroidal sample of a typical magnetic material used in pulse transformers. The dashed loop is for the same material with an air gap included in the magnetic circuit. In the case of the toroid, removing the pulse magnetizing force causes the core flux to return to the value $\text{Br}_1^{\,\star}$. On the next pulse the total flux swing possible is ΔB_1 .

The gapped core, on the other hand, returns to Br, which allows the much greater flux swing $\triangle B_z$. Consideration of the voltagetime integral, ET = NA $_{\!J}$ dB, indicates that a pulse transformer wound on the gapped core passes a pulse of greater area without core saturation than one wound on the gapless or toroidal core.

*This discussion is valid only for cases in which no reverse (resetting) current flows in any of the transformer windings.

For further technical information including diagrams, specifications, and schematic applications of pulse transformers, write for your free copy of our new 12-page catalog.



CIRCLE 285 READERS SERVICE CARD

as is probably unavoidable in an undertaking involving as many authors as does this handbook, there is repetition, as well as gaps and, of course, differences in the clarity, completeness and up-to-dateness of the various chapters.

(continued)

The index, although extensive, omits the listings of some important topics.

► Audio—In common with practically all books on television, (including one by this reviewer) only the absolute minimum of mention is made of the audio signal that is an essential part of a complete television signal. The preoccupation of transmitter and receiver design engineers, of some operating personnel, and even of program producers with obtaining an excellent picture, but with little regard to the sound quality, is truly amazing. Perhaps this book might better have been called a "Video Handbook."

This handbook is a must on the shelves of electronic libraries.—HOWARD A. CHINN, CBS Television, Div. of Columbia Broadcasting System, Inc., N. Y., N. Y.

Introduction to Printed Circuits

By ROBERT L. SWIGGETT John F. Rider Pub., Inc., New York, 1957, 101 p, \$2.70.

ALTHOUGH production engineers will find here no long-sought secret formulas for etching and plating solutions, no magic answers to dipsoldering problems and no completely new printed-circuit techniques, this little paper cover book does constitute an execellent means of becoming acquainted with the complete picture of printed-circuit developments for the past twenty years.

► Major Emphasis—Logically this book deals with the steps involved in converting copper-clad XXXP phenolic laminate into an assembled and soldered circuit, with a chapter on repair procedures thrown in for good measure. Automatic assembly systems are covered without going into the many problems which have beset purchasers



December 1, 1957 — ELECTRONICS

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CIRCLE 288 READERS SERVICE CARD ELECTRONICS - December 1, 1957

NEW BOOKS

of these multi-station machines. Plated circuits receive a more factual coverage, with an excellent discussion of adhesion problems. Lesser used techniques are covered adequately for the reader who seeks quick orientation.-J. M.

(continued)

Thumbnail Reviews

Professional Engineers' Income and Salary Survey. National Society of Professional Engineers, 2029 K St., N. W., Washington, D. C., 1957, 45 p, \$1.00 (paper). Results of 1956 survey of 17 000 registered and survey of 17 000 registered and survey of 18 000 r of 17,000 registered professional engineers in all technical branches.

Audio Amplifier Service Manual, Vol. 9. Howard W. Sams & Co., Indianapolis, Ind., 1957, 240 p, \$3.95. Data on 15 amplifiers, three preamplifiers, 12 tuners and five custom radios produced during 1956.

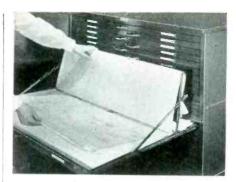
An Introduction to Reactor Physics, 2nd Edition. D. J. Littler and J. F. Raffle, Pergamon Press Inc., New York, 1957. Based on a set of declassified lectures given by the authors to the Reactor School at the Atomic Entered ergy Research Establishment in Har-well, the first part of this book deals with nuclear physics while the last part shows, in detail, the calculations used in evaluating the critical size of a gas-cooled, graphite moderated, natural uranium reactor.

Marine Electrical Practice. By G. O. Watson, Philosophical Library, New York, 1957, 325 p, \$12.00. This book will be primarily of interest to marine engineers who want to learn about the electrical equipment they must operate.

Elements of Color in Professional Motion Pictures. Society of Motion Picture and Television Engineers, New York, 1957, 104 p. Introduction to films, lighting, makeup, processing, printing and other aspects of production of professional color motion pictures.

Ionization and Breakdown in Gases. By F. Llewellyn-Jones, John Wiley & Sons, Inc., New York, 1957, 176 p, \$3.50. Fundamental principles of motions of electrons and ions in gases and physical processes which cause the phenomenon of the electric spark.

Electric Hygrometers—NBS Circular 586. By Arnold Wexler, U. S. Govern-ment Printing Office, Washington 25, D. C., 1957, 21 p, \$20 (paper). Various humidity sensors are classified and discussed in accordance with their basic principles of operation and the simple circuits that are used to measure the resistance of the sensors are presented. Advantages and disadvantages of the various sensors are also covered.



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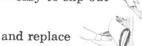
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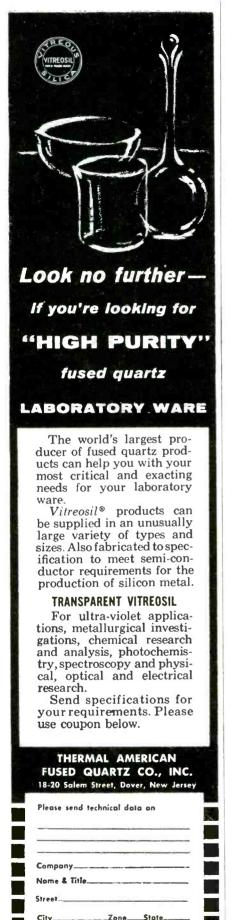
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Letters

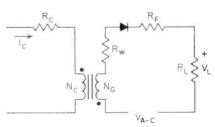
An Oddity of Dots

DEAR SIRS:

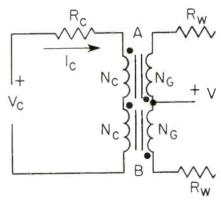
THE second paragraph (of "Core Tester Simplifies Ferro-Amplifier Design," by Roberts and Horstman, Aug. 1 p 150) says in part: "It [a core-test method] consists of using a half-wave rectified current to drive the core flux to saturation once each cycle. A d-c control current reset the flux during the off half-cycle. . . ."

While the description states that the d-c control current resets the flux, it is not certain whether it is in the same or in the opposite direction relative to the rectified saturating current. Normally, of course, the reset current is in the opposite direction.

If the dots are ignored in Fig. 5A,



it could be assumed that the effects of the currents in N_c and N_a are opposite. In Fig. 6A, the + sign



indicates that the arrow in Fig. 5A shows current direction. If the dot had the same meaning as the knot in a coil lead, indicating the start of a winding, where both windings were wound in the same manner, then the currents would have the same saturating effect on the core and there would be no reset.

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goofed, either in redrawing the figures incorrectly or in not noticing the oddity of the dots, or in being fallaciously convinced that all was well.

Is there any intention here of conforming to any convention, and what is the convention?

ALFRED P. STEENSEN
46 Walnut Street
Sharon, Massachusetts

DEAR SIRS:

MR. STEENSEN feels that the article is ambiguous in regard to the polarity of the d-c control current. To clarify this matter in his mind, I would like to say that the polarity dots are in full accord with accepted standards, and are also in accord with the definition outlined by Mr. Steensen.

However, the important point is that in terms of the conventions used in the article a positive control current is of the same polarity as the excitation current, and a negative value of control current is required to cause reset of the flux in the core. This is clearly indicated in Figs. 2 and 4 where an increase in the value of flux change is shown to occur for more negative values of control ampere-turns.

R. W. ROBERTS Magamp Engineering Section Westinghouse Electric Corp. Pittsburgh 30. Penna.

Long Probe, Short Time

DEAR SIRS:

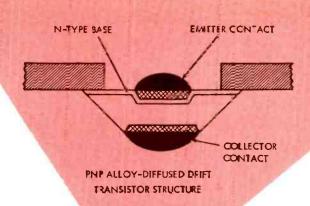
IT HAS come to my attention that there are several errors in the abstract "Long Scope Probes Using Passive Elements" (Sept. 1, p 206). The unit of time should be musec (millimicrosecond, 0.0001 microsecond) when referring to the rise times of the probe systems.

It should be mentioned that the probe rise-times of 16 and 14 millimicroseconds include an oscilloscope rise time of 12 millimicroseconds, so that the probes themselves have rise times of about 10.5 musec for the 227-ft unit and 7.2 musec for the 55-ft unit.

Also, Fig. 1A is not a "typical computer waveform," but merely a very fast and well-shaped voltage step used for testing and adjusting probe systems.

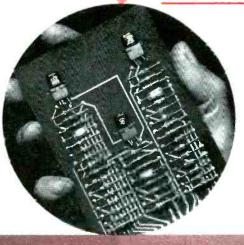
WILLIAM F. SANTELMANN JR. Lincoln Laboratory, MIT Lexington 73, Massachusetts

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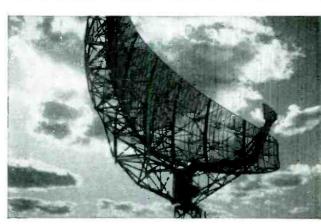
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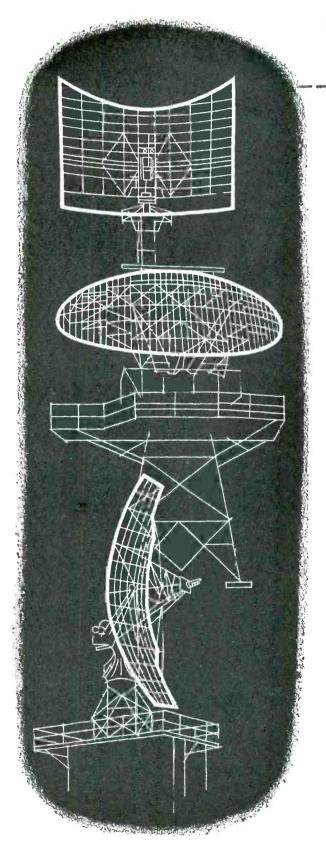
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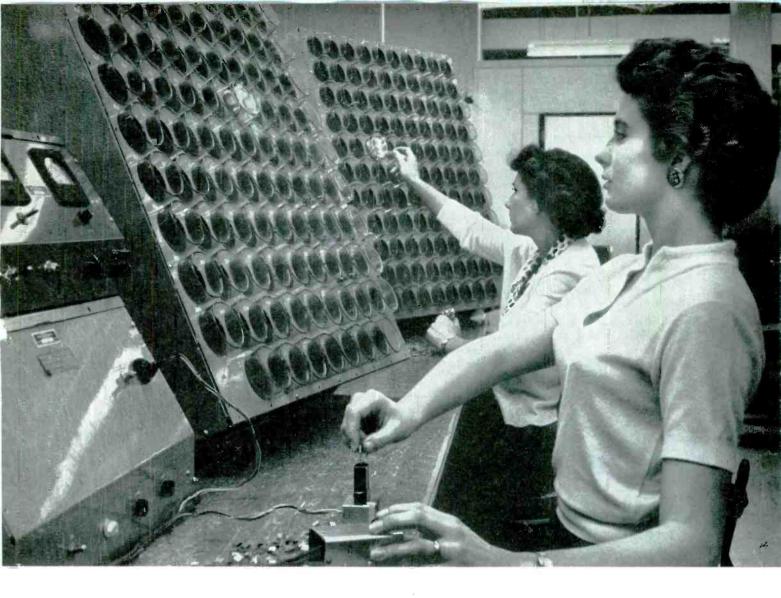
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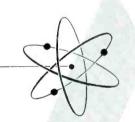
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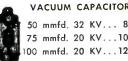
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SHORAN

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AN/SPT-Series

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TDY, MRQ, SPT, SPQ-TPQ-IAN/UPT-TI-T3, T4

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MC, with power supplies for mobile operation.

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Portable 225-398 mc point to point 10 chan. crystal controlled voice and mew radio set. This is a very late radio set used for point to point and ground to air communication. The transmitter output is 8 watts on 10 pre-set crystal controlled channels instantive selected by a band switch. The REC is also crys. controlled on the trans. freq. The set is inclosed in 3 water proof shock proof cabinets that may be set up in a few minutes on location. This equipment is ideal where a reliable radio link easily transported is needed, Power Input Is either 24 VDC 115/230V AC or DC. Complete sets avail. Write

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This is the Standard MIL. F.M. Handi-Talkie With a Range of About I Mile. The Set Operates From Batteries With an Output of .25 Watts, the Set is Self Contained With Its Own Antenna. Weight is Approx. 6 Lbs. The Set is Crystal Controlled and Will operate with PRC, SCR 508, 508 SCR-300 Etc. Quantities Avail.

AN/TRC-1-3-4 100 MC RADIO-RELAY EQUIPMENT

The ANTRC series is a mobile portable set for duplex or simplex radio telephone point to point communication. This set will operate with the CF series carrier systems to provide multi channel operation. The TRC operates on 100 MC with an output of 10 50 watts. The set is orystal controlled. Complete sets avail. Input 110v 60 oyo.

SCR-399-499

Mobile and fixed station high power radio sets; the SCR-399 is mounted in a HO-17 shelter. The SCR-499 is transported in carrying cases to be set up for field operation. Freq. of the sets is 2-18 mo. pwr eutput is 350w. Phone and C.W. 2 communication receivers are provided. Input is 110v 60 cys.

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COMMUNICATIONS EQUIPMENT

X-BAND—RG, 52/U WAVE GUIDE PARABOLOID DISH, 18" diam. Spun Aluminum 8" Focus. For AN/APS-6 3 CM DIPOLE and Feed Assembly (May be used with above dish.) 8 inches long. For AN/APS-6 5 CM DIPOLE and Feed Assembly (May be used with above dish.) 8 inches long. For Station, choke to choke, Has "Built-in" Di-Coupler. 20 DB, with "N" Takeoft". 30" Parabolic Reflector Spun Aluminum dish 10½" Focus 3 CM. DIPOLE FEED, 15" L. for APS-15 10½" focus MITRED ELBOW, Cast aluminum, 1½" x ½" W.G. W.E. Flanges. "E" Plane. 33.50 GM. ANTENNA ASSEMBLY; Uses 17" paraboloid dish, operating from 24 vdc motor. Beam pattern: 5 deg. in both Azimuth and elevation. Sector Scan. over 160 deg. at 35 soans per minute. Elevation Scan. over 160 deg. at 35 soans per minute. Elevation Scan. over 2 deg. Tilt. Over 24 deg. Main Guide is 6" Long, with 90 Deg. "E" Plane bend at one end, and is fitted with Std. UG 39/UG 40 flanges. Coupling figure: 20 db Nominal. \$22.50 Bulkhead Feed-thru Assembly. Pressure Gauge Section with 15 lb. gauge. \$10.00 Directional Coupler, UG 49/U take off 20db. \$15.00 MAGNET AND STABILLIZER CAVITY For 2341 Magneron. 90 degree elbows. "E" Plane 2½" radius. \$8.50 Beacon/receiver unit. Complete with dual klystron mount. TR/ATR section. duplexer. and 30 mo 1F/-X-BAND-RG, 52/U WAVE GUIDE netron \$24.50 90 degree elbows, "E" Plane 2½" radius. \$24.50 90 degree elbows, "E" Plane 2½" radius. \$8.50 Beacon/receiver unit. Complete with dual klystron mount. TR/ATR section. duplexer. and 30 mc IF/-Mixer unit. Originally designed for 9000 mc receiv-ing using 723A/B. New, less tubes. \$22.50

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2J27	\$3.75	4J42	\$22.50	706CY	\$9.75
2J31	\$9.00	5J23	\$18.00	706EY	\$9.75
2J32	\$9.25	5J30	\$4.75		\$2.90
2J38	\$9.00	70013	\$8.75	730A	\$4.75
2.139	\$22.50	780D	\$8.75		

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Mfd. by G. E. for Armed Services 3000-3700 MC. Comes turnished with variable attenuator, coax, adapter cord. Cal. chart and pickup antenna. Has output jack for external meter or other monitor device. Reasonance indicator is 3½, 20 microamp meter. Brand new, in portable wooden carrying case



\$75.00

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PULSE TRANSFORMERS

K-2745 Primary: 3.1/2.8 KV, 50 ohms Z. Secondary: 14/12.6 KV 1025 ohms Z. Pulse length: 0.25/1.0 usec @ 600/600 PPS. Pk Power 200/150 KW. Bifilar: 1.3 Amp. Has "built-in" magnetron well. ...\$32.50 K-2451-A. Primary: 3.1/2.6 KV—50 ohms (line). Secondary 14/11.5 KV—1000 ohms Z. Pulse length: 1 usec @ 600 PPS. Pk. Power Out: 200/130 KW. Bifilar: 1.3 Amp. Fitted with magnetron well. ...\$29.50 K35145—Pulse Inversion: PRI: 5 KV PK. Pulse Negative. Sec: Pos. Pulse, 4 KV: 1 usec. and .001 DUTY RATIO ...\$6.50 541318-1—3 wdgs. Ratio: 1:1:1, 1.0 uln, /wdg. 2.5 ohms DCR ...\$5.50 UTAH X-151T-1: Dual Transformer. 2 Wdgs. per section 1:1 Ratio per sec 13 MH inductance 30 ohms DCR UTAH X-151T-1: Two sections. 3 Wdgs. per section 1:1 Ratio; 3 MH, 6 ohms DCR per Wdg. ...\$5.00 UTAH X-150T-1: Two sections. 3 Wdgs. per section 1:1 Ratio; 3 MH, 6 ohms DCR per Wdg. ...\$5.00 C86G/11; Ratio: 4:1 Pri. 200V, Sec. 53V, 1.0 usec Pulse @ 2000 PPS. 0.016 KVA. ...\$4.50 TR1049 Ratio 21 Pri. 220 MH, 50 Ohms, sec. 0.75 H. DCR 100 Ohms. ...\$6.75

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cy. Output: 135 vdc/10 ma. 90 vdc/5ma; 3 vdc/360
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with model TBX radio gear. \$9.50
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BC 602 Control box for SCR 522 (pushbutton). \$3.75
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WRITE OR WIRE FOR INFORMATION ON OUR COMPLETE LINE OF SURPLUS ELECTRONIC COMPONENTS. ALL PRICES NET F.O.3. PASADENA, CALIFORNIA



2176-E East Colorado St Posadena 8, California RYan 1-7393

INVERTERS *



10042-1-A Bendix
DC Input 14 volts;
output: 115 volts;
400 cycles. 1-phase; 50 watt
2116-2-A Bendix
Output: 115 VAC; 400 cyc; single phase; .4.
amp. Input: 24 VDC, 5 amps.
12117 Bendix
Output: 6 volts; 400 cycles, 6 volt amperes
1 phase. Input: 24 VDC; 1 amp.
12121 Bendix

Output: 6 vol...

1 phase. Input: 24 VDL; 1 a...

12121 Bendix
Input: 24 volt D.C. 18 amp. 12000 r.p.m.
Output: 115 volts, 400 cycle, 3-phase. 250
volt amp, 7 pf.

400 cycle; amps.

12123 Bendix
Output: 115 V; 3 phase; 400 cycle; amps.
.5; Input: 24 VDC; 12 amp.
12126-2-A Bendix
Output: 26 volts; 3 phase; 400 cycle; 10
VA; 6 PF. Input: 27.5 volts DC; 1.25 amps.

12130-3-B Bendix 2130-3-B Bendix Output: 125.5 VAC; 1.5 amps. 400 cycles single phase, 141 VA. Input: 20-30 VDC. 18-12 amps. Voltage and frequency regu-

137 Bendix Output 250 VA, 115 volts, 3 phase, 400 cycle, 1.25 amp., 0.8 pf. Input 27.5 volt DC, 20 amp. \$59.50

DC, 20 amp.
12142-1-A Bendix
Output: 115 volts, 3 phase, 400 cycle, 250
VA. Input: 27.5 VDC, 22 amps. Voltage
and frequency regulated.

12147-1 Pioneer
Output: 115 VAC, 400 cycles; single phase.
Input: 24-30 VDC; 8 amps.
Price \$39.50 each

Price \$39.50 each
778 Bendix
Output: 115 volt, 400 cycle; 190 VA; single phase and 26 volt, 400 cycle, 60 VA, single phase. Input: 24 VDC.
10285 Leland
Output: 115 volts AC; 750 VA, 3 phase, 400 cycle, 90 pf and 26 volts. 50 VA single phase, 400 cycle, 40 pf. Input: 27.5 VDC 60 amps. cont. duty, 6000 rpm. Voltage and frequency regulated.
10339 Leland
Output: 115 volts: 190 VA; single phase;

0339 Leland
Output: 115 volts; 190 VA; single phase;
400 cycle, .90 pf and 26 volts; 60 VA; 400
cycle, .40 pf. Input: 27.5 volts DC, 18
amps. cont. duty, voltage and freq. regulated. \$49.50

10486 Leland Output: 115 VAC; 400 cycles; 3-phase; 175 VA; .80 pf. Input: 27.5 DC; 12.5 amps.; cont. duty. \$70.00

cont. dury. 10563 Leland Output: 115 VAC; 400 cycle; 3-phase; 115 VA; 75 pf. Input: 28.5 VAC; 12 amps. \$35.00

F16 Jack & Heintz Output: 115 volts, 400 cycle, 1 or 3 phase, 250 VA pf. 9. Input: 27.5 volts, 20 amp. Electronic frequency and voltage regulated. \$99.50 each

PE109 Leland Output: 115 VAC, 400 cyc.; single phase; 1.53 amp.; 8000 rpm. Input: 13.5 VDC; 29 \$50.00

1.53 amp.; 8000 rpm. Input: 13.5 VDC; 29 amp. amp. \$50.00 PE218 Leland Output: 115 VAC; single phase pf. 90; 380/500 cycle; 1500 VA. Input: 25-28 VDC; 92 amps.; 8000 rmps.; Exc. Volts 27.5. BRAND NEW \$30.00 MG149F Holtzer-Cabot Output: 26 VAC @ 250 VA; 115 V. @ 500 VA; single phase; 400 cycle. Input: 24 VDC @ 36 amps. \$40.00 MG153 Holtzer-Cabot Input: 24 VDC; 52 amps. Output: 115 volts —400 cycles, 3-phase, 750 VA. Voltage and frequency regulated. \$95.00 AN 3499 Eicor, Class "A" Input: 27.5 volts at 9.2 amps. AC. Output: 115 volts, 400 cycles; 3 phase, 100 voltamp; continuous duty. Price \$39.50 each

PIONEER TORQUE UNITS







\$14940 **TRANSFORMERS**

Mfgd. by Kenyon. Output: 5 volts, 115 amps. Input: 105/125 volts, 60 cycle, single phase. Overall dimensions: 10" x 7" x 6". Approx. wt. 30 lbs. \$15.00

SELSYNS-SYNCHROS



1CT ccnt. Trans. 90/55V 60 cy.
1DG D ff. Gen. 90/90V 60 cy.
1F Syn. Mtr. 115/90V 60 cy.
1G Gea. 115V 60 cy.
1SF Syn. Mtr. 115/90V 400 cy.
2J1F3 Gen. 115/57.5V 400 cy.
2J1F3 Gen. 115/57.5V 400 cy.
2J1F3 Gen. 115/57.5V 400 cy.
2J1F1A Gen. 115/57.5V 400 cy.
2J1F1A Gen. 115/57.5V 400 cy.
2J1H1 Diff. Gen. 57 5V 400 cy.
2J5D1 Cont. Trans. 105/55V 60 cy.
2J5H1 Gen. 115/105V 60 cy.
2J5H1 Gen. 115/105V 60 cy.
2J5H1 Gen. 115/57.5V 400 cy.
2J5H1 Gen. 115/57.5V 400 cy.
5CT Ccnt. Trans. 90/55V 60 cy.
5D Difl. Mtr. 90/90V 60 cy.
5DD Gliff. Gen. 90/90V 60 cy.
5SSM. Gen. 115/90VAC 60 cy.
5SSM. Gen. 115/90VAC 60 cy.
5SSM. Gen. 115/90VAC 60 cy.
5G Syn. Gen. 115/90VAC 60 cy.
6G Syn. Gen. 115/90VAC 60 cy.
82SN. Gen. 115/90VAC 60 cy.
R110-2A Kearfott Cont. Mtr.
115V 400 cy.
R200-A Kearfott Cont. Trans.
26/11.8V 400 cy.
R210-1-A Kearfott Receiver
26/11.8V 400 cy.
R220-T-A Kearfott Receiver
26/11.8V 400 cy.
R235-1A Kearfott Receiver
26/11.8V 400 cy.
R235-1A Kearfott Resolver
26/11.8V 400 cy.
R2406-1 Type 11-4 Rep. 115V 60 cy.
C69406-1 Type 11-2 Rep. 115V 60 cy.
C78248 Syn. Jff. 115V 60 cy.
C78248 Syn. Transm. 115V 60 cy.
C78248 Syn. Transm. 115V 60 cy.
C78248 Syn. Diff. 115V 60 cy.
C78248 Syn. Transm. 115V 60 cy.
C78248 Syn. Transm. 115V 60 cy.
C78248 Syn. Transm. 115V 60 cy.
C78248 Syn. Diff. 115V 60 cy.
C78249 Syn. Diff. 115V 60 cy.
C78240 Syn. Diff. 115V \$37.50 37.50 37.50 37 50 12.50 7.50 10.00 7.50 5.00 7.50 17.50 17.50 17.50 17.50 34.50 34.50 34.50 34.50 34 50 42.50 12.50 25.00 17.50 15.00 20.00 20.00 20.00 20.00 10.00 12.50 5.00 7 50 7.50 7.50 19.50 25.00 19.50 15.00 10.00 20.00 12.50 15.00 ea.

INFRA RED **SNOOPERSCOPE**

High quarry surplus prices. East-man Kodak Infra-Red

SNOUPERSCUPE Receiver, Type B, 7"
long with 5" SCHMIDT
ultra-high-speed Objective Lens
(approx: f 0.5). Elaborate optical system, many coated lenses.
Uses 2 penlight batteries. Govt.
cost approx. \$300. Factory-new.
Shipping wt. 9 lbs. Price \$19.95
Waterproof Snooperscope Carrying
Case avtra Shipping wt 3 lbs

Case, extra. Shipping wt. Price \$3.00 Price \$3.00 Dual purpose U.S.N. floodlight throws strong beam or invisible infra-red rays. With infra-red lens, spare sealed beam lamp, batteries. Ship-ping wt. 23 lbs. Price \$14.95

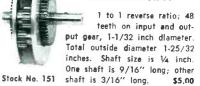


DIFFERENTIAL

Size 2-11/16" long 1-11/16" dia. 1-1 reverse ratio. ¼" shaft on each end; one shaft 25/32" long, one shaft 15/32" long. Input and output gear 1-23/32" dia. 53 teeth.

\$3.50 ea.

SIMPLE DIFFERENTIAL



Stock No. 150

BALL DISC INTEGRATOR

Forward & Reverse 21/4-0-21/4. Input shaft spline gear 12 teeth 9/32" dia. 3/6" long. Output shaft 15/64" dia. x 15/32" long. Control shaft 11/32" x 3/6" long. Cast aluminum construction. Approx. size 3" x 3" x 234".



No. 145 \$17.50 ea.

(All Shafts on Both Ball Bearing Supported)

SMALL DC **MOTORS**

(approx. size overall 334" x 114" dia.:)
5067126 Delco PM, 27 VDC, 125 RPM,
Governor Controlled
5069600 Delco PM 27.5 VDC 125 rpm 12.50
5069230 Delco PM 27.5 VDC 145 rpm 15.00
5068750 Delco 27.5 VDC 10,000 rpm
1x1x2")
5069790 Delco PM, 27.5 VDC 10,000 rpm
1x1x2")
5069790 Delco PM, 27 VDC, 100 RPM,
Governor Controlled
15.00 ea.
5BA10A118 GE 24 VDC 110 rpm 10.00
5BA10A137 GE 27 VDC 250 rpm reversible 10.00
5BA10A37 GE 27 VDC 250 rpm reversible 10.00
5BA10A350, G.E., 12 VDC, 140 R.P.M.
15.00
206-1001 PM Planetary Gear Reduced
Motor with Magnetic Brake. Mfgd. by
Air Equipment 26 volts 600 ma 145
rpm

5BA10FJ33, G.E., 12 VDC, 56 R.P.M.,

| 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | 15.0

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5,000-VR105	.37	100-861	5.00		.50
15,000-OB2	.42	200-851	5.00		
40,000-1U4	.30	2.000-371B	.50	1,000-7AG7	.50
40,000-6.14	.40	2.000-826		500-6SN7WGT	.75
35.000-BA6	.35	2.000-6107/BS212 A	nton	500-REL36	.25
35,000-12AT7	.55	Intergrater	1.00		
10,000-956	.20	2,000-6108/BS213	1.00	10,000-954	.10
1,500-805	2.50	1,000-6109	1.00	10,000-955	.25
10,000-1625	.20	2,000-26D6	.50	10,000-957	.25
40.000-1626	.05	1,500-958A	.20	500-837	.80
10,000-1632	.20	5.000-6SG7GT	.20	20,000-6SD7GT	.17
2,000-1960	.20	40.000-6U7G	10	100-5J26 Magnatron	- 1
2,000-5676	.50	10,000-6J7G		orig case	150.00
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1.000-5841	1.25	5,000-VT67 (30 Specia			
500-CK1026	1.25	5,000-VT25 (10 Specia			
400-533AX	1.25	2.000-2C34			
750-5829WA	2.00	10,000-LN23 Diode			
200-5896	2.50	1.000-WL1B32/532		10,000-9006	.10
100-5647	2.50	800-6J4WA			
1,000-5977	2.00	100-2C43			
500-5AP1	3.00	2,000-RK73		BS6	6.95
1,500-5CP1	3.00	1.000 843		1	

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3,000 Hammerlund Variable Condenser-Transmitting Type, 23 plate,
100 mmfd-v/w BC375, 2,500 volts ins. ceramic\$1.25
1,000 Wallace Tiernan torsional relay, frequency selective for use in
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ciples used permit this relay to be used for most exacting condi-
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Silver Ceramic Trimmers—Jobber Boxed—Types TS2A 1½-4½mmf,
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1,000 Leach relays 115 VAC DTST 30 AMP, #6104\$4.00
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$5,000 500\Omega, 1,000\Omega, 2,000\Omega, 5,000\Omega, 10k, 15k, 20k, 50k \dots 100per M
50,000 Mallory 2 watt W.W. 10,000 ohms, '4"x4" shaft. \$100 per M
50,000 CDI 1/ west on her 1 mag grounding the first of the
50,000 CRL ½ watt carbon, 1 meg screwdriver shaft\$50 per M Write us for prices on your needs—save money
10,000 ea. APC Condensers, screwdriver shaft
25 mmfd—15¢ 50 mmfd 20¢ in 100 lots Electrolytic Condensers—Plug in aluminum cans for octal sockets, size
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40,000 2,000 mfd 15v\$200 per M
Have 2,000,000 ceramic tubular cond.—sizes from 5 mmf, 10, 15, 25, 50,
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\$15.00 per M
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.007, .008, .009, .01\$30.00 per M
1,500 American type TS13 Hanoset telephone phenolic case trans, re-
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5633	4.00	5750	2.20	6073	1.50
5635	4.00	5751	2.00	6080	3.50
5636	2.40	5751WA	3.50	6080WA	6.00
5637	3.08	5763	.90	6096	1.30
5639	5.75	5783	3.75	6098CT	1.90
5641	4.00	5784	4.00	6099	1.40
5643	3.85	5784WA	6.00	6100	2.00
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FC45	4.75	5787	4.75	6101	
5645	3.75	5787WA		6106	8.00
5646		5814	.50	6110	4.75
5647	3.75	5814A	1.50	6111	3.79
5651	1.25	5814WA	3.00	6112	4.00
5651WA	3.25	5829 WA	3.50	6116	45.00
5654/6AK5W		5840	3.00	6130	4.50
	1.25	5840A	4.25	6136/	
5654/6AK5W	1/	5844	1.40	6AU6WA	
6096	2.75	5851	2.50	6147	3.00
5663	.95	5854	1.30	6159	3.00
5670	1.95	5886	1.75	6161	37.50
5670WA	4.00	5894	17.80	6189/12AU7	2.50
5672	1.00	5896	3.00	6201/	
5677	5.00	5898	7.50	12AT7WA	2.50
5678	1.00	5899	3.25	6211	1.00
5687	2.00	5899A	5.75	6263	9.50
5687WA	4.00	5902	4.00	6279/5C22	27.00
5691	4.75	5932	3.00	6280/416B.,	35.00
5692	5.00	5933	1.50	6386	5.00
5696	.75	5963	1.25	6524	11.00
5702WA	3.85	5967	9.50	7193	.20
5703WA	3.85	5969	9.50	8012	1.00
5704	1.20	5977	2.50	9001	.65
5718	1.25	5977A	3.00	9002	.45
5718A	4.00		6.75		.90
5710	1.40	5992		9003	
5719		5995	9.75	9004	.50
5719A	2.75	6000	2.00	9006	.20

	REC1	TIFIERS & R	EGULA	TORS	
OB2	\$.50	3529	\$4.75	371B \$2.5	50
OB2WA	2.25	5R4G Y		575A 10.6	90
OB3	.90	5R4WGY	2.50	6761 48.0	06
OC3	.50	5Y3WGT			65
OC3	2.25	5X3	2.20	N-710/6011 8.5	50
OD3	.50	6-4	.50	836 1.2	20
OD3W	2.25	6-7		872A 1.0	žΟ
SB	2.00	6-11	.50	876	15
SC	1.95	7H4B	.50	878	50
1V	.90	15R	.25	NL1051FG-	
1 Z 2	2.50	100R/8020.	2.75	271/5551 50.0	ю
2C53	9.00	249B	2.58	NL1052/5552/	
2X2	.25	249C	2.50	FG235A 82.0	10
2X2A	.75	250R	3.95	VXR2700. 6.0	oc
3B24	.65	267B	4.95	991	
3B24W	4.25				
3B24WA	7.00	313C	2.25	5560/FG-95 17.0	
	92.50	314A	80.00	5931/5U4WG 4.6	0 (
3B28	4.00	371A	1.00	8013 3.0	10

	SCOPE	TUBES	
2AP1		5CP11	\$7.00
3AP1	1.59	5CP11A	8.50
3CP1	1.75	5FP7A	2.50
3DP1S2	4.75	5JP1	8.75
3FP7	1.00	5JP1A	25.00
3GP1	2.00	5NP1	2.00
3JP1	7.00	7BP1A	15.00
3W2P1		7CP1	4.99
3EP1	1.25	9LP7	10.00
5BP1A	8.50	12DP7	12.00
5BP4	2.25		
5CP1		51UCP11	25.00
5CP1A	7.00	902P1	2,25

EVALENA /WARE	21/20 400 00	7074 /5 40.5
1K015XA/X481	3K30\$90.00	723A/B \$6.50
B,C,D\$40.00	6BL6 24.00	726A 4.7
SRX16 100.00	6BM6 27.50	726C.WE 18.0
2K25 10.00	6BM6A 28.50	726 C. RAY 11.50
2K28 24.09	V45P.O.R.	5611 40.00
2K43100.00	V50 75.00	5721135.0
2K45 25.00	V52P.O.R.	5981/5650. 45.0
2K48 45.00	WL417A 2.00	6116 45.00
2K54 14.00	QK404 48.00	D178461/
2K55 14.00	707B 1.75	419A 48.00

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2J21A \$4.75	4J31\$125.00
2J22 4.50	4J33125.00
2J 26 4.50	4J34 25.00
2J27 4.50	4J42 25.00
2J28 25.00	4J50 90.00
2.129 25.00	4J51 75.00
2J31 12.25	4J52 50.00
2J32 9.50	4J58125.00
2.133 28.50	4J64 40.00
2J34 10.00	5J23 75.00
2J37 28.50	QK60 19.50
2J38 28.50	QK62 19.59
2J42 45.00	QK284 95.00
2J48 24.00	QK366
2J49 32.50	QK367
2,150 32.50	706AY-GY. 9.50
2J51 130.00	720AY/CY, 32.08
2J51A 148.00	728AY/CY. 40.00
2J55 45.00	725A 2.50
2,156 38.00	
2J61 9.95	5586105.00
2.162 4.00	5657100.00
4J21 35.00	5780 150.00
4J26 45.00	6177 75.08

2C43	7.75	446B	.75	8014A 60.00	
	Т	R. AND ATR	. TUBI	s	٦
1B24 1B24A	55.50 12.50	1B40	\$2.00 3.50	BL25/1B27.512.00 532A	

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2D21W80	VT-158 9.0	0 2059W 3.50					
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C5B50	323B 3.4						
EL5B 5.00 5C22 20.00	354A 8.0						
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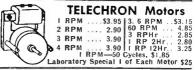
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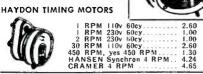
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OC3/VR10550	4J61125.00	FG-10512.50	845 2.50	5750/6BE6W 2.00
OD3/VR150 .50	4X150A 19.75	FG-17215.00	866A 1.25	5751 1,85
EL-C1B 1.00	4X500F	FG-190 2.50	866JR 1.25	5755 8.50
EL-C1K 6.00	5AP1, 2.50	211H 10.00	869B50.00	5763
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1DA480	5BP1A 7.50	244A 2.50	874	5784 4.00
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1B231.00	5C22 25.00	249B 3.00 249C 3.50	885	5796 6.50
1B24 5.00 1B35A 6.50	5CP1	250R 3.50	91317.50	5798 10.00
1B59 10.25	5CP7A 8.50	251A35.00	917 1.35	5800 6.00
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2AP1 2.00	5LP1A	268A 5.00	CK-1006 3.00	5828 6.00
2AP1A 3.00	5LP2A 5.00	271A 7.50	K1051P1 25.00	5829
GL-2B2315.00	5R4GY 1.20	272A 4.00	K1052P2 75.00	5829WA 2.50
2BP1 4.00	5R4WGY 2.75	274A 2.50	1237 3.75	5830/FG4185.00
2C3635.00	5RP1A 9.75	274B	HY-1269 2.50 1274 2.50	5838 7.50 5839 7.50
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2J51175.00	6AL5W 1.00	311A 3.50	5560/FG95 13.50	5932/6L6WGA 3.00
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2K25 12.00	6AS6W 2.50	336A 2.50	5634 5.00	5977 2.50
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3C23 375	12AU7WA 2.50	464A 1.00	5676	6146 4.35
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3C335.00	HK-24G 3.00	GL-678 40.00	5685	6201/12AT7WA. 2.50 6263 9.00
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K802	150	1.25	S	LOW RELEA	SE	F811	4 A	2.00
K803	300	1.25	Сорр	er Slug at He	el End	F812	4A, 1B	2.25
K804	400	1.25	K817	350	2.00	F813	4A, 2B°	2.50
K805	500	1.25				F814	5A	2.25
K806	550	1.50		FRAMES		F815	6A, 2C	3.50
K807	1300	1.50	For Co	st of Relay A	dd Price	F816	10	1.65
K808	2000	2.00		me to Price	of Coil	F817	2C	2.00
K809	4000	2.25			Price	F818	3C	2.50
K810	6500	2.75	Stk#	Contacts	Ea*	F819	4C	3.00
K811	20000	4.50	F801	1 A	1.45	F820	5C	3.50
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			F803	1A, 1C	1.85	F822	Frame†	1.25
	DUAL COILS		F804	1A, 1B, 1C	2.00		•	
K813	380/380	2.00	F805	1A, 1B, 2C	2.50	° Counte	rweight † No	Contacts
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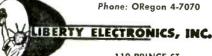
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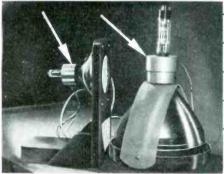
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mc Coy quartz crystal

meet

important requirements

Less than 1/2" wide; please note dimensions below.

WEIGHT ... One twenty-fifth (1/25)

of an ounce.

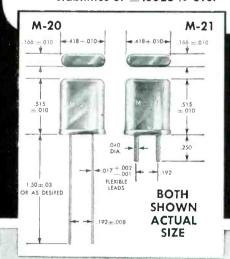
Braio

. Withstands from 10 to 2000 c.p.s.



Withstands from 0 to 30 g.

stabilities of $\pm .0025\%$ over -55° C to $\pm 90^{\circ}$ C possible.



McCoy McMite lightweight quartz crystals extend the limits of electronic design. These little, hermetically sealed units are built rugged to pack regular size performance into minimum space . . . with no sacrifice of stability or dependability! Praduced in frequencies from 3 mc to 125 mc to meet government specifications or made to your own specifications.

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FREED

MIL-T-27A POWER, FILAMENT, PULSE & AUDIO TRANSFORMERS

FOR IMMEDIATE
DELIVERY FROM STOCK

POWER TRAN	ISFORMERS - STANDARD
All primaries	105/115/125 v., 60 c.p.s.

					Filament Filament #1 #2				
Cat. No.	Hi Volt Sec.	ct	Volts	DC Amps	Voit	Amp.	Volt	Amp.	MIL Case Size
MGP1	400/200	V	185	.070	6.3/5	2	6.3	3	HA
MGP2	650	V	260	.070	6.3/5	2	6.3	4	JB
MGP3	650	V	245	,150	6.3	5	5.0	3	KB
MGP4	800	V	318	.175	5.0	3	6.3	8	LB
MGP5	900	V	345	.250	5.0	3	6.3	8	MB
MGP6	700	V	255	.250					KB
MGP7	1100	V	419	.250					LB
MGP8	1600	V	640	.250					NB

FILAMENT TRANSFORMERS-STANDARD All primaries 105/115/125 v., 60 c.p.s.

Cat.	Seco	ndary	Test	MIL	
No.	Volt	Amp	VRMS	Case	
MGF1	2.5	3.0	2,500	EB	
MGF2	2.5	10.0	2,500	GB	
MGF3	5.0	3.0	2,500	FB	
MGF4	5.0	10.0	2,500	НВ	
MGF5	6.3	2.0	2,500	FB	
MGF6	6.3	5.0	2,500	GB	
MGF7	6.3	10.0	2,500	JB	
MGF8	6.3	20.0	2,500	KB	
MGF9	2.5	10.0	10,000	JB	
MGF10	5.0	10.0	10,000	KB	

PULSE TRANSFORMERS

Block'g. Osc.	Int. Coupl'g	Low. Pow. Out.	Pulse Voltage Kilovots	Puise Duration Microseconds	Duty Rate	No. of Wdgs.	Test Volt. KVRN	Char. Imp. Ohm
V	V		0.25/0.25/0.25	0.2-1.0	.004	3	0.7	250
V	V	Ì	0.25/0.25	0.2-1.0	.004	2	0.7	250
V	V		0.5/0.5/0.5	0.2-1.5	.002	3	1.0	250
V	V		0.5/0.5	0.2-1.5	.002	2	1.0	250
V	V		0.5/0.5/0.5	0.5-2.0	.002	3	1.0	500
V	V		0.5/0.5	0.5-2.0	.002	2	1.0	500
V	V	V	0.7/0.7/0.7	0.5-1.5	.002	3	1.5	200
V	V	V	0.7/0.7	0.5-1.5	.002	2	1.5	200
V	V	V	1.0/1.0/1.0	0.7-3.5	.002	3	2.0	200
V	V	V	1.0/1.0	0.7-3.5	.002	2	2.0	
V	V	V	1.0/1.0/1.0	1.0-5.0	.002	3	2.0	500
V	V	V	0.15/0.15/0.3/0.3	0.2-1.0	.004	4	0.7	700
	< < < < < < < < < < < < < < < < < < <	N	Note	Pulse Voltage Vilage Vil		The image The	Section Sec	Section Sec

AUDIO TRANSFORMERS

Frequ. re	sp. 300 to 10000 cps ± 2 08.	All Case Sizes Al							
		Impellance				DC			
Catalog No.	Application	Prim. Ohms	Çt.	Sec. Ohms	27	Prim.	Max. Unbal. MA	Max Level DBM	
MGAI	Single or P.P. Plates — to Single or P.P. Grids	10K	V	90K Split	V	10	10	15	
MGA2	Line to Voice Coil	600 Split		4, 8, 16		0	0	- 33	
MGA3	Line to Single or P.P. Grids	600 Split		135K	V	0	0	+ 15	
MGA4	Line to Line	600 Split		600 Split		0	0	H15	
MGA5	Single Plate to Line	7.6K 4.8T		600 Split		40	40	+33	
MGA6	Single Plate to Voice Coil	7.0K 4.8T		4, 8, 16		40	40	+ 33	
MGA7	Single or P.P. Plates to Line	15K	V	600 Split		10	10	- 33	
MGAB	P.P. Plates to Line	24K	1	600 5plit		10	1	- 30	
MGA9	P.P. Plates to Line	60K	V	600 Split		10	1	+ 27	

Send for further information on these units, or special designs. Also ask for complete laboratory test instrument catalog.

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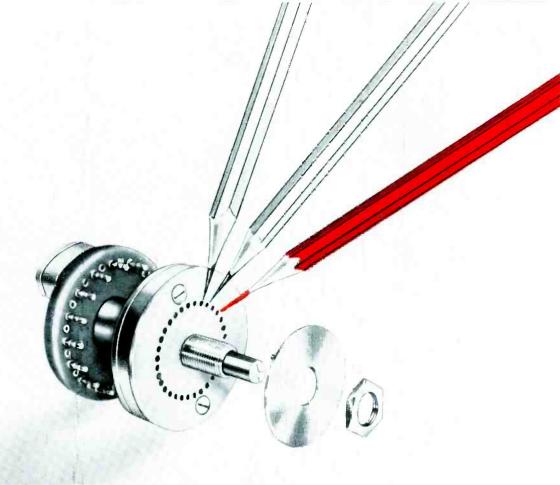
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Stop it

... where you want it!

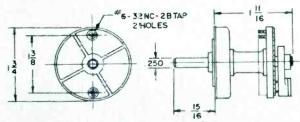
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For flexibility in all types of circuit experimentation, laboratory work, breadboard setups, and in circuitry where the exact number of switch positions might be changed at a later date, the new DAVEN Rotary Switch with an Adjustable Stop is ideal. This unit, as a single pole switch, can have a maximum of either 24 shorting positions with 15° spacing or 32 shorting positions with $11\frac{1}{4}^\circ$ spacing. One, two, three, and four pole units are available in this design.

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KNEE ACTION* silver alloy rotor blades; high grade, accurately machined dielectric; and gold flashed turret-type terminals for ease of soldering.

*Patented

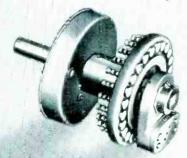


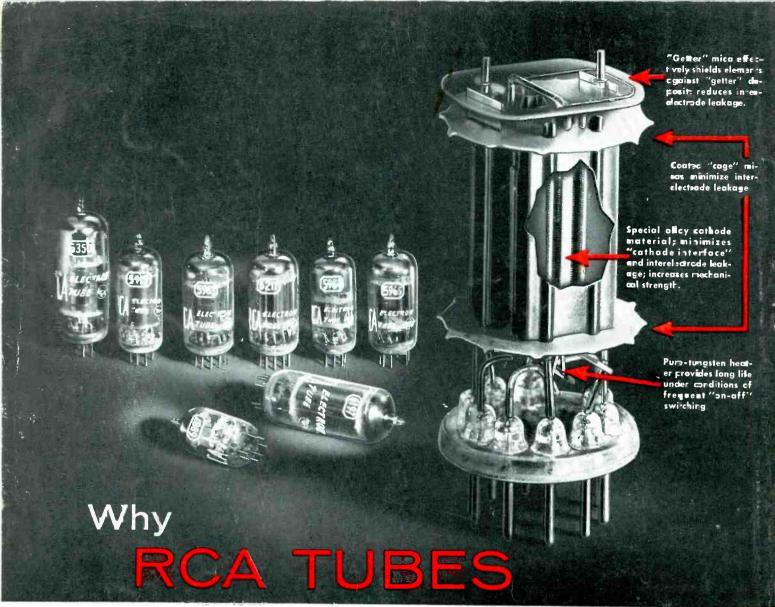
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