



ENGINEERING EXHIBIT APPLICATION FOR CONSTRUCTION PERMIT

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

710 kHz 50 kW-U DA-2

December 15, 1986



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A. D. RING & ASSOCIATES, P.C.

WASHINGTON, D.C.

Section V-A		AM Broadcast Engineering D	Data
Name of Applicant Ma	ambisa Broa	dcasting Corporation	<u> </u>
Purpose of Authoriza		☐ Construct a new station	
		☐ To make changes in one	of the following:
Antenna system (inclined height by addition of	uding increase in FM or TV antenna)	☐ Main studio location poir	nt outside the city limits and not at transmitter site.
☐ Station location to a	different city or town	☐ Transmitter location	
☐ Hours of operation		☐ Power	☐ Frequency
☐ From DA to Non-DA		☐ From Non-DA to DA	□ Trequency
😡 Other (summarize brie	efly the nature of the	changes proposed) Delete on	e monitored madia .
	*		e monitored radial bearing. Dur monitored radial bearin
2. Facilities requested: Frequency			
requency	kH	Iz Hours of Opera	tion <u>Unlimited</u> Power
			Night Day 50 kw 50 kw
3. Station location:	State	City o	
	Florida	Mi	iami
North Latitude Antenna System (include)		58 07 " West Long	80 ° 22 ′ 44 "
		Non-Directional ☐ Day ☐ Nig	yht
Estimated Efficiency:		mV/m/kW/ at one Kilometer.	
If antenna is either top le (include apparent electric	oaded or sectionalized ical height).	d, describe fully in attached Exhibit No.	 -
		Directional	
Day only (DA-D)		K) Difference	
Night only (DA-N)		Different constants or po	ower day and night (DA-2)
	er day and night (DA-	 ☑ Different constants or po □ Different constants or po 	ower day and night (DA-2) ower night and critical hours (DA-3)
Night only (DA-N) Same constants and power		☐ Different constants or po	ower day and night (DA-2) ower night and critical hours (DA-3) . s Rules for each Directional Antenna pattern
Night only (DA-N) Same constants and power	g data in accordance w	☐ Different constants or po	ower night and critical hours (DA-3) s Rules for each Directional Antenna pattern
Night only (DA-N) Same constants and power mit complete engineering posed. * De of feed circuits (excitate)	g data in accordance w tion):	with Section 73.150 of the Commission's Series feed Shun	ower night and critical hours (DA-3) , s Rules for each Directional Antenna pattern nt feed

AM Broadcast Engineering Data

	ssociate	d isolation circuits.	ach as Exhibit No furthe	er details and dimensions, including any other antennas mounted on tower an
o	Attach as	s Exhibit No <u>.*</u> a pl erpoise. Show number	at of the transmitter site showing and dimensions of ground radia	g boundary lines, roads, railroads, other obstructions, and the ground system als or, if a counterpoise is used, show heights and dimensions.
6. T	ransmitt	ter location: *	State	County
			City or Town	Street Address (or other identification)
7. If at	the stud	dio will not be within l Exhibit No*ju	ooundaries of the principal comr sstification pursuant to Section	munity to be served and if the studio is not at the transmitter location, 73.1125 of the Commission's Rules.
th	e propos	sed site, and locations	of the proposed 1000 mV/m cor	cographs taken in clear weather at appropriate altitudes and angles to permit must be marked so as to show compass directions, exact boundary lines of intour for both day and night operation. Photographs taken in eight different table in lieu of the aerial photographs if the data referred to can be clearly
). Alí	ocation	Studies:		
	having r 5 mV/m	easonable scales, show	ring the 1000, 25, 2 and the 5 md proposed operations. On the	having reasonable scales, showing the 1000, 25, 5, 2 and normally protected perations. For nighttime operation, attach as Exhibit No map(s), V/m contours. (RSS nighttime interference-free contour if it is greater than map(s) showing the 25 mV/m, 5mV/m and interference-free contours, clearly cense and the business and residential areas therein.
B.		daytime operation, at scale reproduction the tinent area to show the		ocation study utilizing Figure M-3 of the Commission's Rules or an accurate trength measurement data where available, a full scale exhibit of the entire
	(a)	Normally protected	and the interfering contours for	the proposed operation along all azimuths.
	(ь)	Normally protected hibited overlap would of prohibited overlap	- reserved seem as more existing	ting stations and other proposed stations in pertinent arcs with which pro- stations and other proposals which require study to clearly show absense
	(c)	The 0.1 mV/m groun Section 73.187 of th	dwave-contour in pertinent arcs e Commission's Rules when ope	s of Class 1 stations and appropriate studies to establish compliance with ration is proposed on a U.S. Class 1 channel.
	(d)			
		and operating or prop	er location of each station or proposed facilities.	oposal requiring investigation, with identifying call letters, file numbers,

AM Broadcast Engineering Data

В.	(2)	(2) For daytime operation, attach as Exhibit No	* a tabulation of the following:	
		(a) Azimuths along which the groundwave con required by B(1).	ntours were calculated for all stations or proposals shown on allocation study exhib	oits
		(b) Inverse distance field strength used along a	zimuth.	
		(c) Basis for ground conductivity utilized along must be either submitted or be properly ide	g azimuths specified in (2)(a). If field strength measurements are used, the measur entified as to location in Commission files.	ements
C. F	-or	For nighttime operation, attach as Exhibit No*	, allocation data including the following:	
(1)	 Proposed nighttime limitation to other existing other proposals and existing stations which requ 	or proposed stations with which objectionable interference would result, as well a uire study to clearly show absence of objectionable interference.	s those
(:	2)	 All existing or proposed nighttime limitations w facilities investigated under C(1) above. 	which enter into the nighttime R.S.S. limitation of each of the existing or proposed	
(:	3)	 All existing and proposed limitations which con- limitations which must be studied before being e 	tribute to the R.S.S. nighttime limitation of the proposed operation, together with excluded.	those
(4	4) ,	 A detailed interference study plotted upon an agent existing or proposed facilities along bearing other 	ppropriate scale map if a question exists with respect to nighttime interference to der than on a direct line toward the facility considered.	other
(5	5) -	5) The detailed basis for each nighttime limitation (calculated under C(1), (2), (3) and (4) above.	
10. I	s th	s the population within the 1 V/m contour less that the 25 mV/m contour?	n 300 persons or less than 1.0 percent of the population within 图 YES	
1. A	\tta hov	Attach as Exhibit No* a map (7.5 minute U.S howing the following information:	5. Geographic Survey topographic quadrangles if available) of the proposed antenn	a location
A	. F	A. Proposed transmitter location accurately plotted	with the latitude and longitude lines clearly marked and showing a scale of statut	e miles.
			in elevations in the vicinity of the antenna, indicating the location thereof.	
C	. T	Transmitter location and call signs of all non-broa government receiving stations in the general vicin	adcast radio stations (except amateur and citizens band), established commercial a ity which may be adversely affected by the proposed operation.	nd ·
. D.			M and TV broadcast stations within 2 miles of the proposed antenna location.	
۲ C)n	On File- No change from au	uthorized operation	

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April 1985

12.	Environmental Statement, See Part	Subpart 1 of the Commission's Rules.	
	Would a Commission grant of your	Dilication be a major action as defined by Section 1.1305 of the Commission's Rules.	⊠ NO
	If Yes, submit as Exhibit No.	ne required statement in accordance with Section 1.1311 of the Commission's Rules.	
	If No, - explain briefly.		
	No change fr	authorized operation	
			_
	I certify that I represent the	licant in the capacity indicated below and that I have examined the foregoing statement of	
techr	nical information and that it is true to	e best of my knowledge and belief.	
		Karl D. Lahm	
_ [December 15, 1986	Rame Name	
(Date)	Signature (Check appropriate box below)	
	ICT OF	1140 19th Street, N.W., Suite 500	
	STARL D.	Address (Include ZIP Code)	
	No. 80	\\rightarrow\rightarro	
	1*1 -	(202) 222 6700	
	POLESSIONAL	Telephone No. (Include Area Code)	
	SSIONAL	MG.	
От	echnical Director	Registered Professional Engineer	
□ c	hief Operator	☐ Technical Consultant	
□ o	ther (specify)		

World Radio History

ENGINEERING EXHIBIT APPLICATION FOR CONSTRUCTION PERMIT

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

710 KHZ 50 KW-U DA-2

ENGINEERING STATEMENT

Mambisa Broadcasting Corporation (MBC), licensee of AM broadcast station WAQI, Miami, Florida hereby proposes changes in the assigned monitored radial bearings pertaining to its directional antenna systems. Specifically, deletion of the requirement for monitoring in one direction and a change in bearing for four directions are requested. Grant of the instant application will permit final action on the complete proof of performance for the WAOI directional arrays, which is being submitted simultaneously.

Monitored Direction Deletion

It is requested that the requirement to monitor the radial bearing 92 degrees True be deleted. This bearing corresponds to the center of the secondary lobe of the nighttime radiation pattern and is directed straight out into the Atlantic Ocean. No cochannel station is located in this direction or between it and the adjacent monitored radial bearings, 20.5 and 120 degrees True.

Changed Radial Bearings

For daytime operation, WAQI must monitor the 220 degree True radial bearing. The actual radiation pattern minimum is located one degree away, at 221 degrees True. The actual minimum bearing was used in the current Proof of Performance. Consequently, it

is requested that the 220 degree assignment be changed to 221 degrees.

For nighttime operation, WAQI is required to monitor the radial bearings 330, 340, and 350 degrees True. None of these direction corresponds to a theoretical or augmented pattern inflection point (minimum or maximum). They do not define the outer boundaries of a protected cochannel station's contour.

As best as can be determined, the basis for the assignment of these radials was that the 330 degree radial passes just outside the protected 0.5 millivolt per meter (mV/m) skywave service contour of cochannel Class I-B station WOR, New York, the 340 degree radial corresponds to the bearing of tower lines 1-2-3 and 4-5-6, and the 350 degree bearing corresponds to one of the ideal minima caused by the wide-spaced tower pairs of this parallelogram array, the symmetrical mate of the 120 degree monitored bearing. Figure 1 illustrates the placement of these bearings with respect to the WOR protected skywave service area. Of the entire 52 degree sector of protection to WOR, these bearings span only 19 degrees.

Near the WAQI transmitter site, these three directions pass over largely uninhabited, inaccessable swampland. The original 1965 Proof of Performance utilized close-in measurements taken on a "swamp buggy" for these radials. The 1975 proof of performance included measurements taken within a moving helicopter for these bearings. The Commission's engineering records for this facility demonstrate that accurate measurement and analysis of field strength levels in these directions is exceptionally difficult.

The relevant pattern inflection azimuths throughout the span of protection to the skywave service area of WOR are 333, 0.5, and 20.5 degrees True. The 333 degree bearing corresponds to an tiny minor lobe, while the 0.5 and 20.5 degree bearings correspond to pattern nulls. Furthermore, the 0.5 degree bearing

corresponds to the minimum radiation point of the augmented standard pattern. Sufficient measuring locations are accessible by road on the 0.5 and 20.5 degree bearings, eliminating the need for airborne measurements in those directions.

The 333 degree radial passes through the southwestern tip of the WOR protected skywave service area. The 0.5 degree radial passes through the middle of that area. The 20.5 degree radial passes through the southeastern boundary of the WOR protected service area (along the North Carolina Capes) and through the eastern section of Long Island, where WOR provides groundwave service. The relationship of these bearings to the WOR skywave service contour is illustrated by Figure 2. They span 50 degrees of the 52 degree sector of protection toward WOR. Consequently, it is believed that monitoring of these three pattern inflection bearings inherently affords better monitoring of the protection afforded to the WOR service area.

WOR, in pleadings objected to the partial proof of performance for this facility filed September 10, 1985, has expressed its concerns over the sufficiency of the existing radial bearing assignments. Attachment I is a copy of a letter to the undersigned from WOR's engineering consultant attesting to WOR's support of monitoring the 333, 0.5, and 20.5 degree bearings in lieu of the 330, 340, and 350 degree bearings.

It is requested that the 330, 340, and 350 degree monitored bearing assignments be changed to 333, 0.5, and 20.5 degrees, respectively. The latter assignment set better defines the groundwave and skywave protected service areas of cochannel Class I-B station WOR. Those bearings correspond to theoretical pattern inflections (the criterion currently used by the Commission staff in assigning monitored directions), as well as the augmented pattern minimum radiation direction. Sufficient ground locations, accessible by road, are available on two of the three directions, facilitating accurate array adjustment and proof of performance measurements.

Conclusion

The monitored radial bearing changes requested herein will not adversely affect any station or authorization. In fact, their adoption will better assure establishment of adequate protection to Class I-B station WOR, while permitting MBC to perform field strength measurements in a more convenient and accurate manner.

December 15, 1986

A. D. RING & ASSOCIATES, P. C.

Karl D. Lahm, P.E.

Registration Number 8049

District of Columbia

SMITH AND POWSTENKO

BROADCASTING AND TELECOMMUNICATIONS CONSULTANTS

WASHINGTON, D. C. 20036

NEIL M. SMITH
GEORGE A. POWSTENKO
JEANNE F. SMITH
KEVIN T. FISHER

August 6, 1986

Mr. Karl D. Lahm A. D. RING & ASSOCIATES, P.C. Suite 500 1140 Nineteenth Street, N.W. Washington, D. C. 20036



Dear Karl:

On behalf of RKO General, Inc., licensee of WOR, New York, New York, this is to advise you that WOR agrees with your plan for WAQI, Miami, Florida, as described in your letter of July 3.

WOR is a Class I-B station on 710 kHz, and WAQI operates as a Class II station on that channel. At present, WAQI is required to measure and monitor three radials toward the WOR secondary service area: 330° T, 340° T, and 350° T. Under your proposal, WAQI would instead measure and monitor at 333° T, 0.5° T, and 20.5° T. I believe that your proposal would better assure the protection of WOR while minimizing measurement difficulties for WAQI.

If I can be of assistance in your dealings with the Commission on this matter, please let me know.

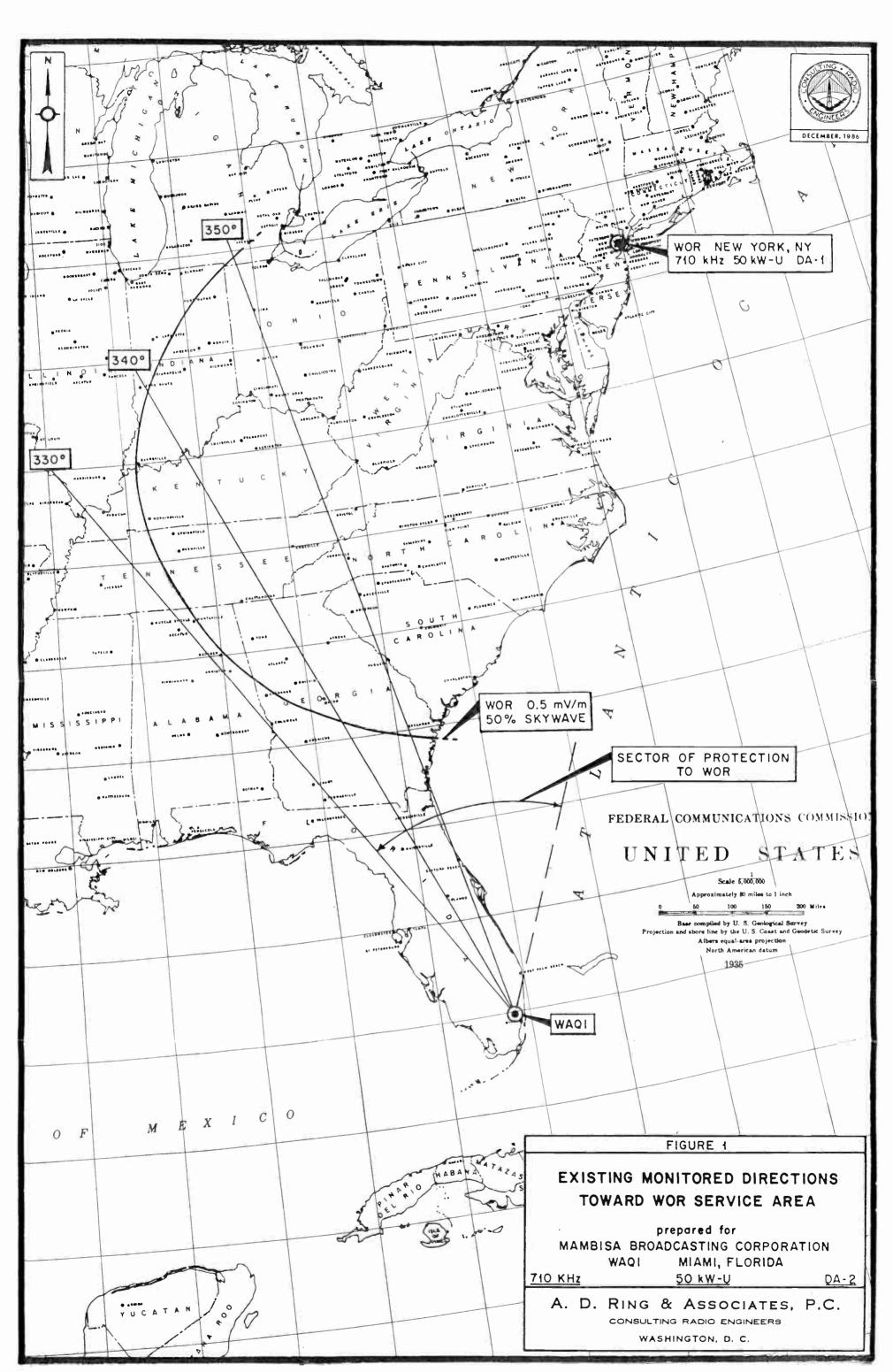
Best regards,

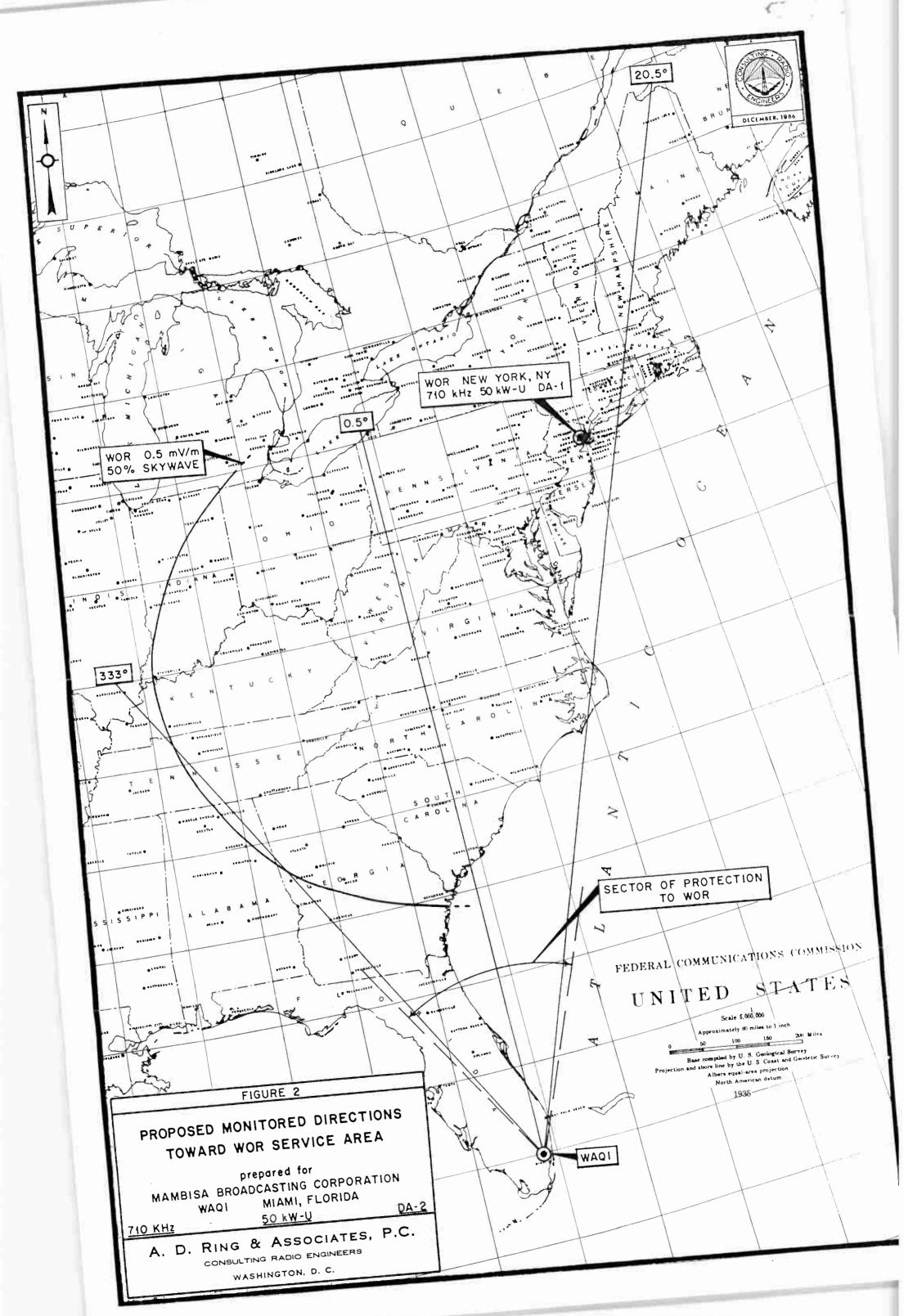
Neil M. Smith

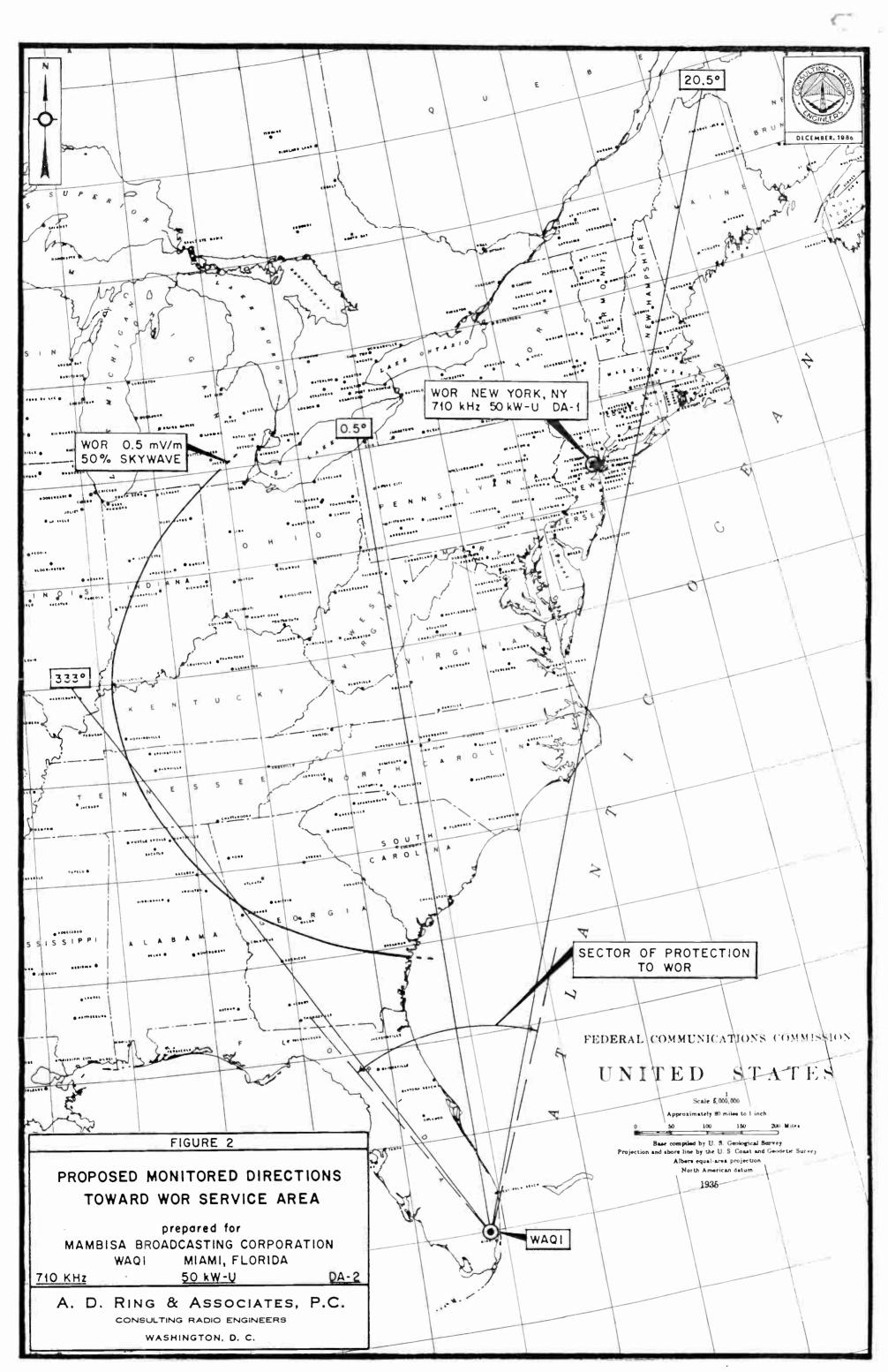
NMS/dee

cc: Mr. George J. Capalbo

Mr. Paul Stewart







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ENGINEERING EXHIBIT APPLICATION FOR MODIFICATION OF LICENSE COMPLETE PROOF OF PERFORMANCE

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

710 kHz 50 kW-U DA-2

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Engineering Exhibit Summary

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

710 kHz 50 kW-U DA-2

WAQI has completed replacement of its seven antenna towers. Complete proof of performance data is set forth herein establishing that the WAQI directional antenna system has been adjusted to comply with the radiation requirements of the authorized standard radiation pattern. A companion application for construction permit is being filed simultaneously to request reassignment of monitored radial bearings to those employed in the instant proof of performance, which correspond to theoretical pattern minima and maxima and address concerns raised by cochannel station WOR, New York, N.Y. Grant of the instant application would not constitute a "major environmental action" as defined by Section 1.1305(d) of the Commission's rules.

Name of Applicant Mamb	oisa Broadca	sting C	orpo	 oration				
PURPOSE OF AUTHORIZATION	APPLIED FOR: (check	one)						
	Station L	icense			er Iter I-9	ns		
	Direct me	asurement of	power	1,	2, 6,	7, 8 and 10		
1. Facilities authorized in constru	uction permit			y				
Call Sign Fi	le No. of Construction F	Permit	Frequ	uency	Hou	rs of operation	Pow	ver in kilowatts
IM D(1)	Application : Concurrently		7:	LO.	ט	·	Night 50	Day 50
2. Station location								
State				City or tow	n			
Florida				Mi	ami			
3. Transmitter location *								
State	County			City or tow	n		State address (or other iden	
4. Main Studio location *			1				1	
State	County			City or tow	n		Number and	Street
5. Remote control point location	(only if authorized) *							
State	,			City or tow	'n		Street addres	=
6. Operating constants:						-		
RF common point or antenna of power in amperes	current without modulation	on for night		RF commo		or antenna current	without modulat	tion for day
Actual measured antenna or of at operating frequency	common point resistance	e (in ohms)		Actual mea		antenna or commo	n point <i>reactance</i>	e (in ohms)
Night 50	Day 50			Night	0	Kanay	Day ()	
Antenna monitor indication for	or directional operation		1					
Tower	Phase readin	g in degrees		Ante	enna b	ase current	current	
	Night	Day		Night		Day	Night *	
	+ 113.5	0.0		26.5		38.7	0.528	1.00
2-SW	$\frac{0.0}{109.5}$	+ 13.0		$\frac{20.3}{11.3}$. 4.	10.2	0.428	0.33
<u>3-5 Night 7-NW Da</u> 4-N	- 169.0	N/A	$\overline{}$	9.4		N/A	0.346	N/A
	+ 78.0	N/A		17.5	1.11	N/A	0.651	N/A
6-E	- 38.0	N/A	,	8.55		N/A	0.317	N/A
Manufacturer and type of ant	enna monitor: ac Instrumen	•	9 (2		t tari	1 4		Direct Reading
7. Description of antenna system			1	04) 5/1	4. W.T	, , , , , , , , , , , , , , , , , , ,	5/N 133	
(If directional antenna is used Height figures should not incl	the information reques	sted below sh	ould be	given for ea	ch eler	nent of the array. I	Use separate she	ets if necessary.
Uniforn Cross al	eight in feet of complet pove base insulator, or a rounded. *			Overall height in feet above ground (without obstruction lighting) * If antenna is either top loaded or set tionalized, describe fully in Exhibit No. — STL receive antenna at 330 ft.				scribe fully in Exhibit TL receive at 330 ft.
Excitation			X Se	eries			ltower #	Shunt

: I

^{*} On File, No Change

North talliuride West incorporate The processors of the change in antenna or common point resistance. Replacement of all towers, installation of STL receive antenna or in the permit? None West incorporate West incorporate (a) Manufacture's name of each cakinated instrument used and manufacture's name of each cakinated instrumen	eographic coordinate to									
The page of the change in antenna or common point resistance. Replacement of all towers, installation of STL receive antenna or to find the permit? None Name None Name None Name None Name None Name Name Name None Name										
Antenna resistance measurement Attach as Exhibit No. Engla sketch of the details and dimensions of ground system. Attach as Exhibit No. Engla showing clearly all components of coupling circuits, point of resistance measurements, location of antenna ammeter, connection to and characteristics of all tower lighting location circuits, statisty by the antenna, including other antennas, and associated circuits. (c) Full description of method used to make measurements. (g) The graph drawn of 10 to 12 readings in a band 50 to 60 kilohetz with the operating frequency near the center. In what respect, if any, does the apparatus constructed differ from that described in the application for construction permit or in the permit? None Give reasons for the change in antenna or common point resistance. Replacement of all towers, installation of STL receive antenna on to struct to the best of my knowledge and belief. Replacement the applicant in the capacity indicated below and that I have examined the foregoing statement of technical information and struct to the best of my knowledge and belief. Replacement 17, 1986 Name Karl D. Lahm (Please Pant or Type) Signature Check appropriative to be bowl 1140 19th Street, N. W. Address Unclude Area Code) Technical Director Chief Operator Technical Director	North latitude	4)	*	٧٠ُ٧	est longit	ude	υ			**
Attach as Exhibit No. English following: (a1) Qualifications of persons taking measurements. (b1) Schematic diagram showing clearly all components of coupling circuits, point of resistance measurements, location of an armonic control of the change in an armonic control of the coupling circuits, point of resistance measurements, location of an armonic patient of any other influence, lines, etc. connected to an armonic patient of the coupling circuits, and any other influence, lines, etc. connected to an armonic patient of the coupling of the antiquency and sex-oclated original (f). Table of complete data taken. (c) Full description of method used to make measurements. (d) The graph drawn of 10 to 12 readings in a band 50 to 60 kilohertz with the operating frequency near the center. (a) The graph drawn of 10 to 12 readings in a band 50 to 60 kilohertz with the operating frequency near the center. (a) The graph drawn of 10 to 12 readings in a band 50 to 60 kilohertz with the operating frequency near the center. (b) The graph drawn of 10 to 12 readings in a band 50 to 60 kilohertz with the operating frequency near the center. (c) The graph drawn of 10 to 12 readings in a band 50 to 60 kilohertz with the operating frequency near the center. (d) The graph drawn of 10 to 12 readings in a band 50 to 60 kilohertz with the operating frequency near the center. (e) The graph drawn of 10 to 12 readings in a band 50 to 60 kilohertz with the operating frequency near the center. (g) The graph drawn of 10 to 12 readings in a band 50 to 60 kilohertz with the operating frequency near the center. (g) The graph drawn of 10 to 12 readings in a band 50 to 60 kilohertz with the operating frequency near the center. (g) The graph drawn of 10 to 12 readings in a band 50 to 60 kilohertz with the operating frequency near the center. (g) The graph drawn of 10 to 12 readings in a band 50 to 60 kilohertz with the operating frequency near the center. (g) The graph drawn of 10 to 12 readings in a band 50 to 60 kilohertz with the	not fully described abov in circuits. Also, if nece	e, attach as Exhibitessary for a compl	NoEng further deta ete description attach	als and dimensions as Exhibit No.E.T.	including Iga sketo	any other a	ntenna mount tails and dime	ed on towe	er and ass ground s	sociated isol ystem.
(d) Manufacturer's name of each calibrated instrument used and manufacturer's rated accuracy. (b) Schematic diagram showing plant all components of coupling circuits, point of resistance measurements. Location of antenna summeter, connection to and characteristics of all those righting solition fricings, salid dianis, and any other fixtures, lines, etc. connected to or supported by the antenna, including other antennas, and associated circuits. (c) Full description of method used to make measurements. (d) Date, accuracy, and by whom each instrument was last calibra dianis, and any other fixtures, lines, etc. connected to or supported by the antenna, including other antennas, and associated circuits. (d) Table of complete data taken. (e) The graph drawn of 10 to 12 readings in a band 50 to 60 kilohertz with the operating frequency near the center. In what respect, if any, does the apparatus constructed differ from that described in the application for construction permit or in the permit? None Give reasons for the change in antenna or common point resistance. Replacement of all towers, installation of STL receive antenna on to struct to the change in antenna or common point resistance. Replacement of all towers, installation of STL receive antenna on to struct to the best of my knowledge and belief. (202) 223–6700 Signature OF CO No. 8043 No. 8043 No. 8043 Registered Professional Engineer (Chief Operator Karl D. Lahm (Please Print or Type) Washington, D.C. 20036										
to Schematic diagram showing clearly all components of coupling circuits, point of resistance measurements, location of antenna ammeter, connection to and characteristics of all tower lighting isolation circuits, static drains, and any other fixtures, lines, etc. connected to or supported by the antenna, including other antennas, and associated circuits. (c) Full description of method used to make measurements. (g) The graph drawn of 10 to 12 readings in a band 50 to 60 kilohertz with the operating frequency near the center. In what respect, if any, does the apparatus constructed differ from that described in the application for construction permit or in the permit? None Give reasons for the change in antenna or common point resistance. Replacement of all towers, installation of STL receive antenna on to #5 complete readjustment of antenna system. Partity that represent the applicant in the capacity indicated below and that I have examined the foregoing statement of technical information and its true to the best of my knowledge and belief. Name Karl D. Lahm (Please Point or Type) Signature Check approbriate box below: No. 8043 No. 8043 Registered Professional Engineer K Technical Consultant	Attach as Exhibit No.	Eng. the following	:							
point of resistance measurements, location of antenna ammeter, connection to and characteristics of all tower lighting isolation crucius, static drains, and any other fixtures, lines, etc. connected to or supported by the antenna, including other antennas, and associated circuits. (c) Full description of method used to make measurements. (g) The graph drawn of 10 to 12 readings in a band 50 to 60 kilohertz with the operating frequency near the center. In what respect, if any, does the apparatus constructed differ from that described in the application for construction permit or in the permit? None Give reasons for the change in antenna or common point resistance. Replacement of all towers, installation of STL receive antenna on to 45, complete readjustment of antenna system. Perily that I represent the applicant in the capacity indicated below and that I have examined the foregoing statement of technical information and its true to the best of my knowledge and belief. Name Karl D. Lahm (Please Print or Type) Signature Of Columbia Director Registered Professional Engineer K Technical Director	(a) Qualifications of	persons taking me	asurements.	(d)				rated instru	iment use	ed and manu
to Full description of method used to make measurements. (g) The graph drawn of 10 to 12 readings in a band 50 to 60 kilohertz with the operating frequency near the center. In what respect, if any, does the apparatus constructed differ from that described in the application for construction permit or in the permit? None Give reasons for the change in antenna or common point resistance. Replacement of all towers, installation of STL receive antenna on to #5, complete readjustment of antenna system. ertify that I represent the applicant in the capacity indicated below and that I have examined the foregoing statement of technical information and struct to the best of my knowledge and belief. Name Karl D. Lahm (Please Print or Type) Signature OF COLUMN Address (Include 2IP Code) Washington, D.C. 20036 Technical Director Technical Director Technical Consultant	point of resistance nection to and cha	e measurements, lo tracteristics of all to	ocation of antenna amover lighting isolation cir	meter, con- (e) rcuits, static	Date, ad	ccuracy, and	I by whom ea	ach instrum	nent was	last calibrat
In what respect, if any, does the apparatus constructed differ from that described in the application for construction permit or in the permit? None Give reasons for the change in antenna or common point resistance. Replacement of all towers, installation of STL receive antenna on to #5, complete readjustment of antenna system. errify that I represent the applicant in the capacity indicated below and that I have examined the foregoing statement of technical information and struct to the best of my knowledge and belief. Name Karl D. Lahm (Please Print or Type) Signature Check appropriate box below) 1140 19th Street, N.W. Address (Include ZIP Code) Washington, D.C. 20036 Technical Director Chief Operator Technical Director					Table of	complete o	lata taken.			
Give reasons for the change in antenna or common point resistance. Replacement of all towers, installation of STL receive antenna on to #5, complete readjustment of antenna system. errify that I represent the applicant in the capacity indicated below and that I have examined the foregoing statement of technical information and is true to the best of my knowledge and belief. Name Karl D. Lahm (Please Print or Type)	(c) Full description of	f method used to	make measurements.	(g)						60 kilohertz v
(202) 223-6700 Jephone No. (Include Area Code) Signature (Check appropriate box below) 1140 19th Street, N.W. Address (Include ZIP Code) Washington, D.C. 20036 No. 8049 Technical Director Chief Operator X Technical Consultant	None			nom mai describe	ed in the	аррисатіон і	or construction	on permit o	or in the	permit?
Signature Check appropriate box below Check appropriate box below 1140 19th Street, N.W. Address (Include ZIP Code) Washington, D.C. 20036 Washington, D.C. 20036 Chief Operator Technical Consultant	. Give reasons for the congestion Replaces #5, compertify that I represent the	nent of all olete reade	or common point res ll towers, ljustment o	istance. installat f antenna	ion c	of STL	receiv	e ant	enna	on to
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Technical Director Registered Professional Engineer Chief Operator Technical Consultant	Give reasons for the or Replacen #5, compertify that I represent the strue to the best of manager December 1 (202) 223-67	e applicant in the y knowledge and to 1986	or common point res	istance. installat f antenna ow and that I have	ion c syst e examine	of STL tem. d the forego Karl I (Ple	receive ing statement of Lahm asse Print or in eck appropria	t of technic	enna cal inform	on to
Technical Director Chief Operator Technical Director Registered Professional Engineer Technical Consultant	Give reasons for the or Replacen #5, compertify that I represent the strue to the best of manager of the December 1 (202) 223-67	e applicant in the y knowledge and to 1986	or common point res	istance. installat f antenna ow and that I have	ion c syst e examine	of STL tem. d the forego Karl I (Ple	receive ing statement in the state of the st	re ant	enna cal inform wowl	on to
Chief Operator	Give reasons for the or Replacen #5, compertify that I represent the strue to the best of manager of the December 1 (202) 223-67	e applicant in the y knowledge and to 1986	or common point res Il towers, Ijustment o capacity indicated beloelief.	installat f antenna ow and that I have No. LAHAM 8049	ion c syst e examine	of STL cem. d the forego Karl I (Ple	receive on statement of the state of the sta	re ant t of technic Type) Techox belovet, ZIP Code)	enna cal inform	on to
Other (specify)	Give reasons for the or Replacen #5, compertify that I represent the strue to the best of more than the December 1 (202) 223-67 Rephone No. (Include A	e applicant in the y knowledge and to 1986	or common point res Il towers, Ijustment o capacity indicated beloelief. RICT O KARL I	installate f antenna ow and that I have Na Side Side Side Side Side Side Side Side	ion of systematics and systematics are second and systematics are second as a systematic and systematics are systematically as a systematical systematics are systematically as a systematical systematic systematic systematics are systematically as a systematic systematic systematics are systematically as a systematic systematic systematics.	of STL cem. d the forego Karl I (Ple	receive ing statement of Lahm ase Print or 1 leck appropria	t of technic	enna cal inform	on to
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ENGINEERING STATEMENT

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

710 kHz 50 kW-U DA-2

WAQI has completed replacement of its seven antenna towers, reconfiguration of its antenna monitor sampling system, and readjustment of its directional antenna system. Since the most recent (1975) complete proof of performance was based largely on measurements taken in a moving helicopter, it is understood that the Commission staff will not accept a partial proof of performance in this instance, as would otherwise be the case. Data set forth herein establishes new nominal operating parameters, monitor point locations, and monitor point field strengths. Various pertinent facts regarding the equipment installation are also stated.

Antenna Monitor and Sampling System

The WAQI antenna monitor sampling system consists of Delta Electronics toroidal current transformers sampling the base current of each tower, connected to the Potomac Instruments AM-19(204)/PMA-19 antenna monitor by Andrew FHJ-2-50 phase stabilized coaxial transmission line. The lengths of these lines were measured on site and found to be within one degree of equal length, with the exception of the line to tower #7, which is used only during daytime operation. All lines are subjected to identical environmental conditions. The limited seasonal temperature changes of South Florida assure that the phase change of the tower #7

sampling line attributable to its unequal length remains below 0.5 degrees. This sampling system meets the requirements of the former provisions of Section 73.68 of the Commission's rules.

Table I sets forth complete antenna monitor indication data for both operating modes. For nighttime operation, it is recommended that the deviation indications (digital) and attenuator settings of the PMA-19 Precision Monitor Adaptor (PMA) be considered the most accurate representation of the sample current amplitudes. The PMA direct phase readings should be employed. PMA direct ratio readings are supplied also. For nighttime operation, the AM-19 (analog) monitor indications should not be relied upon.

Adjustment of the Directional Antenna Systems

Tower replacement commenced at WAQI during January of 1986. The nighttime directional antenna system was initially set up by Leonard A. Spragg, P.E. to produce within-limits field strengths at monitor points during March. The daytime system was operating well within limits at that time, with greater than theoretical suppression observed. Adjustment of the daytime directional antenna commenced in May, with ground proof of performance measurements completed in June. Airborne measurements for the daytime system were conducted in August. Tower #7, unused during nighttime operation, was detuned, as detailed in Appendix i. After receipt of equipment which would allow determination of low WAQI field strength in the presence of equal or greater Cuban interference in late August, nighttime antenna system adjustments commenced. adjustments and measurements, which were hampered by equipment failures partially caused by lightning damage, were completed in November, 1986.

Nondirectional Operation

All field strength measurements reported herein for nondirectional operation were obtained with tower #1 (W) excited. All other towers were detuned by adjusting a terminating coil at each tower base to obtain a current minimum at one-third the height of each tower.

Nondirectional measurements used in conjunction with the analysis of directional data were taken during the same season as the corresponding directional data. Since several months separated the gathering of daytime and nighttime data, duplicated nondirectional measurements are reported herein. Appendix ii presents a comparison of May/June and October/November nondirectional data for typical radials. Close-in nondirectional measurements used only to determine the nondirectional inverse distance field strength at one mile were not repeated, since conductivity changes would not materially affect the results thereof. Since, for each pattern, the nondirectional reference data is contemporaneous and the data of Appendix ii establishes negligible seasonal conductivity changes, it is believed that the data provided meets the Commission's requirements.

Directional Antenna Performance Data

Table I sets forth theoretical and present adjustment operating parameter data, for both antenna monitor and base current indications. Differences between theoretical and present adjustment values are attributable to the fact that the base feed current, which is sampled, consists of both radiation and tower base capacitance current components.

The nondirectional tower antenna base input resistance was measured. The directional common point resistances were adjusted to match the transmitter. Resistances measured are set forth in Table I. Information concerning methods and results is being provided to the station for retention in its files. Analyzed inverse distance field strengths are summarized in Table II. All inverse distance values are below the limits established by the WAQI authorized standard radiation patterns, as shown.

Measured radiation patterns for nondirectional, daytime directional, and nightiime directional operation are included as Figures 1, 2, and 3. RMS values were computed by polar planimeter measurement of the area contained within the pattern and computation of the equivalent nondirectional radius. Results were checked by numerical integration of the measured field strengths. The measured daytime pattern RMS is 93 percent of the standard pattern RMS, while the nighttime pattern RMS is 92 percent of the standard pattern value, indicating that substantial operating efficiency continues to exist.

Monitor Points

Field strength measurement data obtained throughout the adjustment and measurement cycle was analyzed to determine how well various potential monitor points tracked the field strength analyzed for the radial as a whole. The monitor points chosen herein exhibit the best historical performance, as well as reliable accessibility, for all points available between one and four miles from the transmitter site. For the 20.5 degree radial, the monitor point is located 4.35 miles from the transmitter site, due to the lack of road access to more than one point between two and four miles. Figure 4 shows the monitor point locations and routings to those points from the transmitter site. Photographs and descriptions of each point are included as Figures 5-A through 5-I.

Contemporary photographs and descriptions have been provided for all points, regardless of whether or not they not been changed.

Change of the requirement to monitor the daytime radial bearing 220 degrees True to 221 degrees (the actual location of a radiation minimum) and the nighttime radial bearings 330, 340, and 350 degrees True has been requested in a companion application for construction permit. After discussions with the consulting engineer for RKO General, Inc., licensee of cochannel class I-B station WOR, New York, N.Y., it was agreed to change these radial bearings to 333, 0.5, and 20.5 degrees True, which correspond to theoretical pattern inflection bearings and span a much broader arc of the WOR protected service area, better assuring establishment of interference protection to WOR than do the present radial bearing assignments.

The aforementioned Application for Construction Permit also requests deletion of the requirement to monitor the radial bearing 92 degrees True. This direction corresponds to a strong secondary lobe and is directed into the Atlantic Ocean, toward no cochannel stations. It is believed that monitoring of this direction serves no useful purpose. Consequently, no monitor point description has been provided.

Field Strength Measurements

Field strength measurements were conducted to establish the performance of the directional antenna system in accordance with the standards of Section 73.151 of the Commission's rules. For the daytime pattern, nine radial bearings were selected, corresponding to the pattern minima (35 and 221 degrees), maxima (141 and 308 degrees), -3 dB points (92.5 and 190 degrees), -6 dB point (71 degrees) and intermediate bearings between the minor lobe and minima (0.5 and 277 degrees). For the nighttime pattern, thirteen radial bearings were used, corresponding to the pattern minima (0.5, 20.5,

and 120 degrees), tiny lobes between minima (308 and 333 degrees), the FCC Fort Lauderdale monitoring station (35 degrees), cochannel stations (235 and 277 degrees), the secondary lobe (92.5 degrees), the main lobe (162 degrees), and -3 dB points (71, 141, and 190 degrees). An Application for Construction Permit is being filed simultaneously requesting reassignment of the monitored radial bearings to those reported herein.

Close-in nondirectional field strength measurement data is detailed by Tables III-A through III-N. Such data was taken by helicopter, using the retractable boom assembly developed by WNOE, New Orleans. Appendix iii describes this airborne measurement procedure in some detail. Additional nondirectional data is set forth with corresponding directional data and the analysis thereof in Tables IV-A through IV-I for daytime operation and Tables V-A through V-M for nighttime operation. Measured nondirectional field strengths are plotted on the graphs of Figures 6-A through 6-N.

Daytime directional data and the numerical analysis thereof is presented by Tables IV-A through IV-I. Measured daytime field strengths are plotted on the graphs of Figures 7-A through 7-I. Where sufficient measurement locations could not be accessed on the ground (along the 190, 221, 277, and 308 degree radials), airborne measurements were conducted, as noted. The airborne measurement locations reported were selected from field-versustime (distance) chart recordings to provide, when combined with the ground locations, a relatively uniform spacing of points versus distance.

Nighttime directional data and the numerical analysis thereof is presented by Tables V-A through V-M. Once again, airborne measurements were required on those radials (190, 235, 277, 308, and 333 degrees) where sufficient points could not be accessed on the ground. The directional field strength in directions of high radiation suppression was of the same order of magnitude as cochannel interference from Cuba. In such directions, airborne

measurements were terminated where the field strength was low enough to result in inaccuracy due to interference. Airborne measurement locations were selected from field-versus-time (distance) chart recordings to result, when combined with ground locations, in a relatively uniform spacing of points versus distance. Nighttime field strength data is illustrated graphically by the plots of Figures 8-A through 8-M. Measurements were made by Timothy Sawyer of this firm and independent subcontractors Charles N. Miller, P.E., Michael Perryman, and Paul L. Whitney, whose qualifications are a matter of record with the Commission, under the direction of the undersigned. The field strength meter types, serial numbers, and calibration dates are:

Manufacturer & Type		<u>Serial</u>	Calibration Dat		
Potomac Instruments	FIM-21	105	March 20, 1986		
Potomac Instruments	FIM-21	524	January 6, 1986		
Potomac Instruments	FIM-41	463	April 3, 1984		
Potomac Instruments	FIM-41	512	March 20, 1986		
Potomac Instruments	FIM-41	659	May 24, 1979		

Meter serial number 463 was calibrated by the manufacturer for use with a remotely located loop antenna and was used exclusively for helicopter measurements. All meters were compared and found to agree within their rated accuracies.

Measurement Point Location

Measurement points were selected to comport with requirements of Section 73.186 of the rules to as great an extent as possible, while at the same time being readily accessible by road. The road structure near WAQI approximates a "one mile grid" structure and several roads have been blocked or their entrances fenced in order

to prevent trash dumping, limiting the number of measurement locations available near the transmitter site. Nondirectional field strength measurements were taken at least 0.4 mile away from the transmitter site and directional measurements were commenced 1.4 miles from the transmitter site for the day pattern and approximately two miles from the transmitter site for the night pattern, in accordance with Section 73.186 specifications. In those few cases where the use of locations within these distances could not be avoided, geometric proximity effects were accounted for in the analysis of measured data. Field strength measurement locations are illustrated by the maps of Figures 9-A through 9-V.

Measurement Analysis

Nondirectional measurements were analyzed by the graphic analysis technique described in Section 73.186(a)(3) of the rules. Graph 6 of Section 73.184(f) was used in the determination of unattenuated field strength at one mile and the effective ground conductivities. Field strengths so determined were plotted for each radial bearing measured, yielding a measured nondirectional RMS of 950 millivolts per meter at one mile.

The unattenuated field strength at one mile for directional operation was analyzed using the directional to nondirectional logarithmic ratio method. Geometric proximity effects were evaluated for each radial. Where use of proximity correlations changed the analyzed field strength by more than five percent, they were employed, as detailed in Tables V-A through V-M. Proximity effect estimation and correlation was applied using the undersigned's Quadrature Method, as described by Appendix v.

Environmental Considerations

Section 1.1305(d) of the Commission's rules provides that grant of any application would be considered a "major environmental action" if the exposure of workers or the public results in an exposure to levels radio frequency radiation in excess of the "Radio Frequency Protection Guides" recommended in standard ANSI C95.1-1982 of the American National Standards Institute (ANSI). To protect its facilities from vandalism and the public from injury or excessive radiation exposure, WAOI has installed chain-link fences across the access roads to the transmitter site.

A Radiation exposure survey was conducted at the WAQI transmitter site using a Holaday Industries HI-3002 Microwave Energy Meter. The survey revealed that the public is not exposed to excessive energy and that workers are exposed to levels above the ANSI standard within equipment shelters at the tower bases. Station personnel need to access the area within the shelters during station operation only for the purpose of reading the antenna base current meters. This action takes less than one minute and is required not more than weekly, which is predicted to result in an average exposure in compliance with the ANSI standard.

STL Antenna Installation

An STL receiving antenna was installed at tower #5 (NE). Figure 10 illustrates the vertical plan of that tower. The STL coaxial cable is isolated across the tower base by means of an isocupler.

Conclusion

The data detailed herein demonstrates that, in accordance with the Commission's rules, the present adjustment of the WAQI nighttime directional antenna system complies with the radiation limitations of the authorized standard radiation pattern. Revised operating specifications may be issued based on the data set forth herein.

December 17, 1986

A. D. RING & ASSOCIATES, P.C.

Timothy Z. Sawyer

Karl D. Lahm, P. E.

District of Columbia #8049 State of California #E010307

TABLE I

Antenna System Operating Parameter Data

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

Operating Power Parameter	ondirectional	Daytime DA	Nighttime DA
	Tower #1	Common Point	Common Point
Antenna input resistance (ohms	23.2	50.0	50.0
Antenna current (amps)		32.4	32.4
Antenna input power (kilowatts		52.6	52.6

<u>Daytime</u> Directional

Tower Number	Theo. Field Ratio	Ind.* Sample <u>Ratio</u>	Theo. Field Phase (deg)	Ind.* Sample Phase (deg)	Antenna Base Current (amps)	Base Current <u>Ratio</u>
1 - W	1.000	1.00	0	0	38.7	1.000
2 - S W	0.333	0.33	-134	-141	12.4	0.320
7 - N W	0.333	0.26	+174	+13	10.2	0.264

Nighttime Directional

Tower Number	Theo. Field Ratio	Direct Sample Ratio **	PMA-19 Atten. Reading	Monitor O Dev. Ratio	Theo. Field Phase (deg)	Ind.** Sample Phase (deg)	Antenna Base Current (amps)	Base Current <u>Ratio</u>
1 - W	0.504	0.528	11.49	0.527	+112.0	+113.5	14.1	0.532
2 - S W	1.000	1.000	6.05	1.000	0.0	0.0	26.5	1.000
3 - S	0.504	0.428	14.28	0.424	-112.0	-109.5	11.3	0.426
4 - N	0.327	0.346	17.48	0.346	-173.0	-169.0	9.4	0.355
5 - N E	0.650	0.651	9.37	0.646	+75.0	+78.0	17.5	0.660
6 - E	0.327	0.317	18.99	0.319	-37.0	-38.0	8.55	0.323

^{*} As indicated on Potomac Instruments AM-19(204) antenna monitor, serial number 1023

^{**} As indicated on Potomac Instruments PMA-19 precision monitor, serial number 133

TABLE II

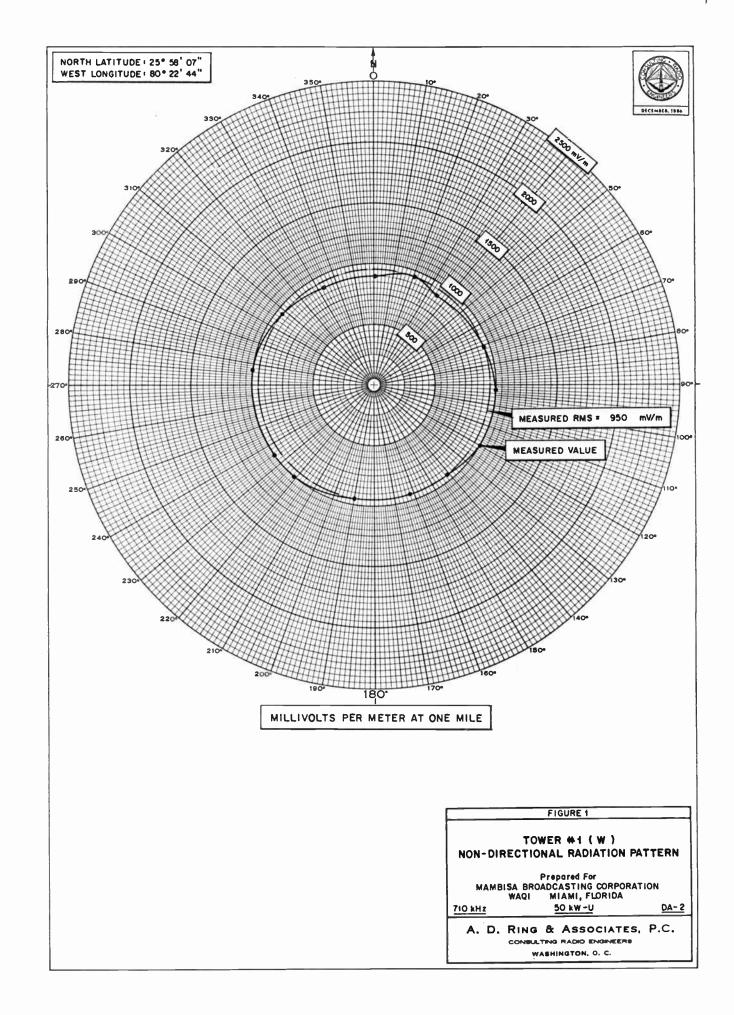
ANALYZED FIELD STRENGTH SUMMARY

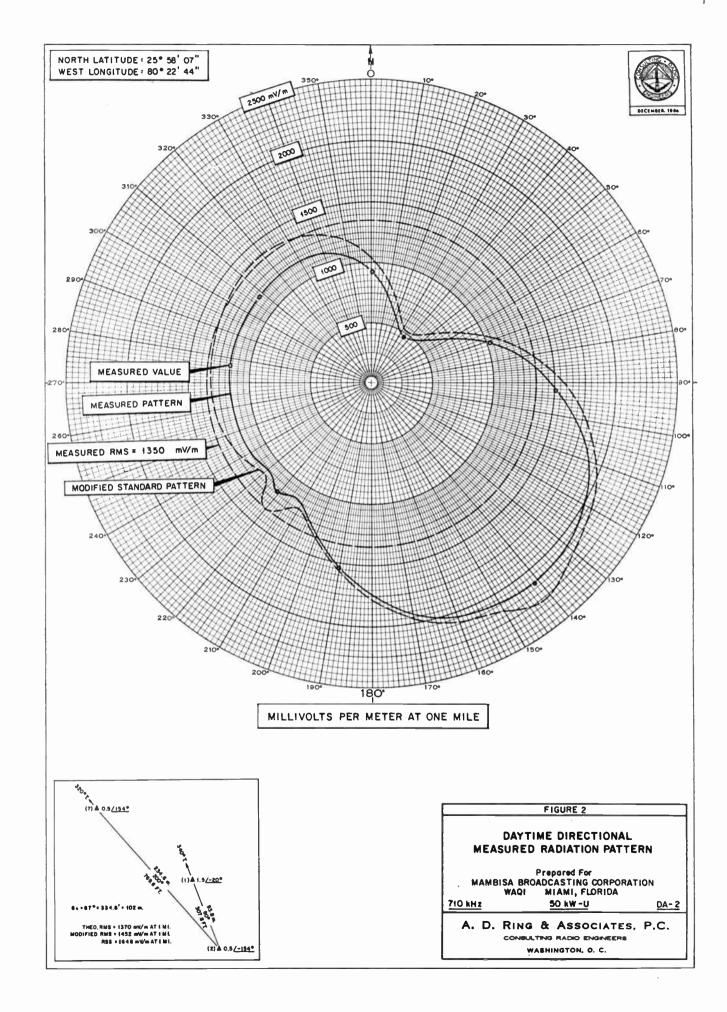
prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

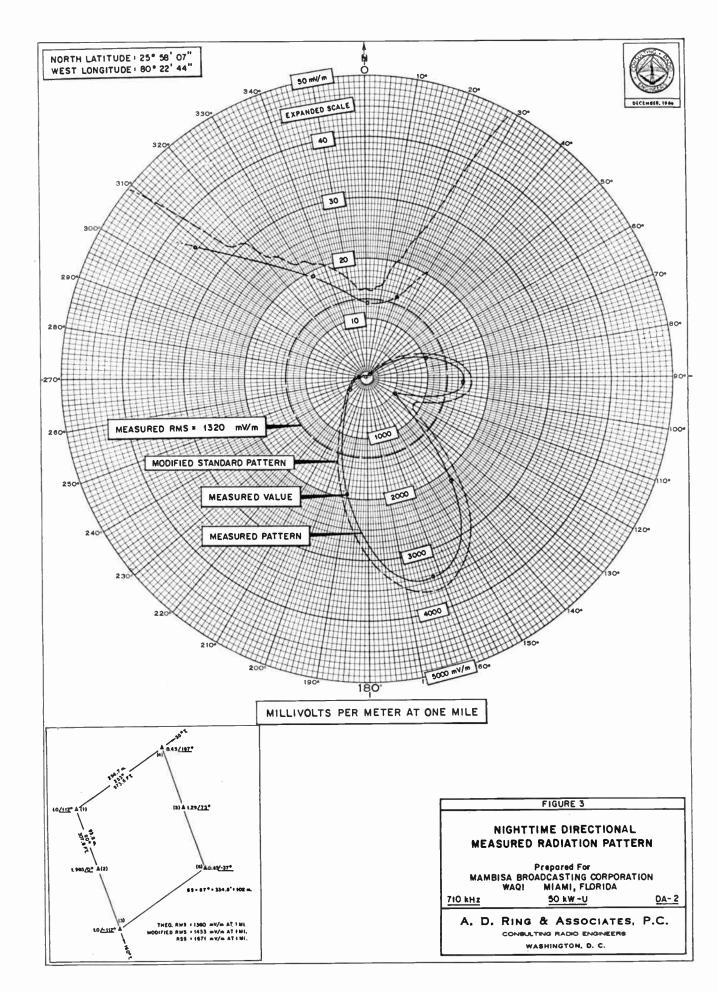
UNATTENUATED FIELD STRENGTH AT ONE MILE

Radial Bearing	Nondirectional 25 kW Tower #1	Daytime Directional Analyzed Authorized		Nighttime Analyzed	Directiona Authorize		
(deg)	(m V / m)	(m V / m)		(m V / m)	(mV/m)	- ((mV/m)
0.5 20.5	900 950	928		1030	12.6 14.4	*	15.0 25.1
3 5 7 1	900 950	468 1025	*	524 1096	81.3 1010		122 1196
92.5 120	1000 1000	1510		1628	1600 522	*	1718 894
141 162	950 950	2120		2260	2180 3430		2533 3665
190 221	950 1000	1550 1190	*	1570 1348	1930		2197
235 277	1000 1000	1170	*	1379	339 125	*	450 195
308 333	950 900	1160		1355	35.4 19.1	*	50.0 21.7
RMS	950	1350		1452	1320		1433

^{*} Monitored direction







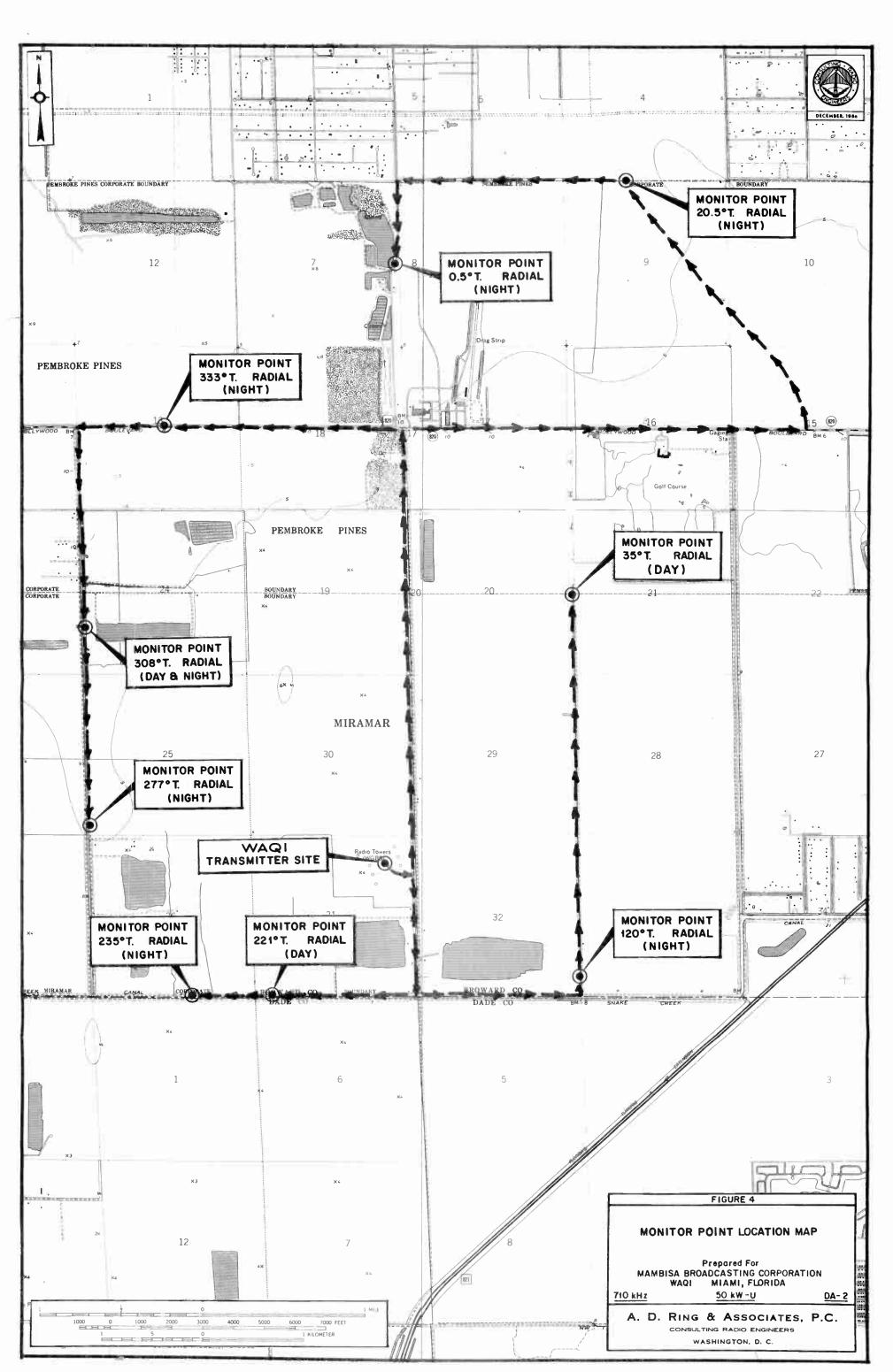


FIGURE 5-A

MONITOR POINT DESCRIPTION

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida



Nighttime 0.5 Degree Monitor Point

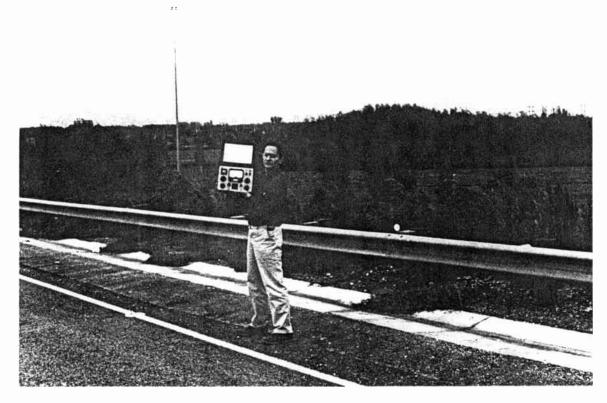
From the transmitter driveway, proceed north on NW 172nd Avenue for a distance of 2.75 miles (4.4 km.) to Hollywood Blvd (Pines Blvd). Turn right on Hollywood Blvd. (Pines Blvd.) and proceed east for a distance of 2.45 miles (3.9 km.) to the junction with Interstate I-75 North. Turn left onto I-75 North and proceed north for a distance of 2.0 miles (3.2 km.) to the West Sheridan Street exit. Proceed west on Sheridan Street for a distance of 1.6 miles (2.6 km.) to the intersecton with 172nd Avenue. Turn left (enter road to gravel pits) and proceed south for a distance of 0.5 miles (0.8 km.). The point is located at the spot on the west side of the road marked by a painted orange steel stake.

Radial Point Number 13
Distance from transmitter 2.65 miles (4.3 km)
Measured Field Strength 3.05 mV/m
Computed Permissible Field Strength 3.63 mV/m

FIGURE 5-B

MONITOR POINT DESCRIPTION

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida



Nighttime 20.5 Degree Monitor Point

From the transmitter driveway, proceed north on NW 172nd Avenue for a distance of 2.75 miles (4.4 km.) to Hollywood Blvd (Pines Blvd). Turn right on Hollywood Blvd. (Pines Blvd.) and proceed east for a distance of 2.45 miles (3.9 km.) to the junction with Interstate I-75 North. Turn left onto I-75 North and proceed north for a distance of 2.0 miles (3.2 km.) to the West Sheridan Street exit. Proceed west on Sheridan Street for a distance of 0.1 miles (0.2 km.) to the west side of the I-75 overpass. The point is located at the spot on north side of the road marked by a painted orange steel stake.

Radial Point Number 12
Distance from Transmitter 4.45 miles (7.2 km)
Measured Field Strength 2.2 mV/m
Computed Permissible Field Strength 4.1 mV/m

FIGURE 5-C

MONITOR POINT DESCRIPTION

prepared for Mambisa Broadcasting Corporation WAOI Miami, Florida



Daytime 35 Degree Monitor Point

From the transmitter site, proceed south on 172nd Avenue for a distance of 0.75 miles (1.2 km.) to the intersection with Honey Hill Road. Turn left and proceed east on Honey Hill Road for a distance of 1.0 miles (1.6 km.). Turn left on SW 160th Avenue (west side of canal and proceed north for a distance of 2.5 miles (4.0 km.). The point is located on the west side of the road, marked by a painted steel stake.

Radial Point Number 10
Distance from transmitter 2.03 miles (3.3 km)
Measured Field Strength 198 mV/m
Computed Permissible Field Strength 222 mv/m

FIGURE 5-D

MONITOR POINT DESCRIPTION

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida



Nighttime 120 Degree Monitor Point

From the transmitter site, proceed south on 172nd Avenue for a distance of 0.75 miles (1.2 km.) to the intersection with Honey Hill Road. Turn left and proceed east on Honey Hill Road for a distance of 1.0 miles (1.6 km.). Turn left on SW 160th Avenue (west side of canal and proceed north for a distance of 0.1 miles (0.2 km.). The point is located on the west side of the road, marked by a painted steel stake.

Radial Point Number 6
Distance from transmitter 1.37 miles (2.2 km)
Measured Field Strength 248 mV/m
Computed Permissible Field Strength 425 mV/m

FIGURE 5-E

MONITOR POINT DESCRIPTION

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida



Daytime 221 Degree Monitor Point

From the transmitter site, proceed south on 172nd Avenue for a distance of 0.75 miles (1.2 km.) to the intersection with Honey Hill Road. Turn right and proceed west on Honey Hill Road for a distance of 0.92 miles (1.5 km.). The point is located on the south side of the road, marked by a painted steel stake.

Radial Point Number

Distance from transmitter

Measured Field Strength

Computed Permissible Field Strength

1.04 miles (1.7 km)

1100 mV/m

1250 mV/m

FIGURE 5-F

MONITOR POINT DESCRIPTION

prepared for Mambisa Broadcasting Corporation WAOI Miami, Florida



Nighttime 235 Degree Monitor Point

From the transmitter site, proceed south on 172nd Avenue for a distance of 0.75 miles (1.2 km.) to the intersection with Honey Hill Road. Turn right and proceed west on Honey Hill Road for a distance of 1.35 miles (2.2 km.). The point is located on the south side of the road, marked by a painted steel stake.

Radial Point Number 7
Distance from transmitter 1.41 miles (2.3 km)
Measured Field Strength 268 mV/m
Computed Permissible Field Strength 356 mV/m

FIGURE 5-G

MONITOR POINT DESCRIPTION

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida



Nighttime 277 Degree Monitoring Point

From the transmitter driveway, proceed north on NW 172nd Avenue for a distance of 2.75 miles (4.4 km.) to Hollywood Blvd (Pines Blvd). Turn left on Hollywood Blvd. (Pines Blvd.) and proceed west for a distance of 1.98 miles (3.2 km.) to the junction with SW 196th Street. Turn left and proceed south on SW 196th Street (east side of canal) for a distance of 2.46 miles (4.0 km.) The point is located at the spot on the west side of the road, marked by a painted orange steel stake.

Radial Point Number 8
Distance from transmitter 1.82 miles (2.9 km)
Measured Field Strength 71 mV/m
Computed Permissible Field Strength 111 mV/m

FIGURE 5-H

MONITOR POINT DESCRIPTION

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida



308 Degree Monitor Point

From the transmitter driveway, proceed north on NW 172nd Avenue for a distance of 2.75 miles (4.4 km.) to Hollywood Blvd (Pines Blvd). Turn left on Hollywood Blvd. (Pines Rlvd.) and proceed west for a distance of 1.98 miles (3.2 km.) to the junction with SW 196th Street. Turn left and proceed south on SW 196th Street (east side of canal) for a distance of 1.25 miles (2.0 km.) The point is located at the spot on the west side of the road, marked by a painted orange steel stake.

Radial Point Number 11
Distance from transmitter 2.35 miles (3.8 km)
Day Measured Field Strength 510 mV/m
Computed Permissible Field Strength 595 mV/m
Night Measured Field Strength 10 mV/m
Computed Permissible Field Strength 14.1 mV/m

FIGURE 5-I

MONITOR POINT DESCRIPTION

prepared for Mambisa Broadcast Corporation WAOI Miami, Florida



Nighttime 333 Degree Monitor Point

From the transmitter driveway, proceed north on NW 172nd Avenue for a distance of 2.75 miles (4.4 km.) to Hollywood Blvd (Pines Blvd). Turn left on Hollywood Blvd. (Pines Blvd.) and proceed west for a distance of 1.45 mi. (2.3 km.). The point is located at this spot on the north side of the road and is marked by a painted orange steel stake.

Radial Point Number 13
Distance from transmitter 3.03 miles (4.9 km)
Measured Field Strength 9.1 mV/m
Computed Permissible Field Strength 10.3 mV/m

TABLE III-A

CLOSE-IN NON-DIRECTIONAL MEASURED FIELD STRENGTH DATA

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

0.5 Degrees True

Distan Tower #1(W) (Mi.)	<u>Array</u> <u>Center</u>	Time (EST)	Field Strength (mV/m)
0.56	0.55	*	1500
0.82	0.82	*	860
0.96	0.96	*	750
1.09	1.09	*	660
1.23	1.23	*	600
1.37	1.37	*	560
1.51	1.51	* *	520
1.64	1.64	*	470
1.78	1.78	*	440
1.91	1.91	*	400
	Tower #1(W) (Mi.) 0.56 0.82 0.96 1.09 1.23 1.37 1.51 1.64 1.78	#1(W) Center (Mi.) 0.56 0.55 0.82 0.82 0.96 0.96 1.09 1.09 1.23 1.23 1.37 1.37 1.51 1.51 1.64 1.64 1.78 1.78	Tower Array #1(W) Center (EST) 0.56 0.55 * 0.82 0.82 * 0.96 0.96 * 1.09 1.09 * 1.23 1.23 * 1.37 1.37 * 1.51 1.51 * 1.64 1.64 * 1.78 1.78 *

^{*} Non-directional airborne measurements were taken between 1158-1201 EST on December 2, 1986.

TABLE III-B

CLOSE-IN NON-DIRECTIONAL MEASURED FIELD STRENGTH DATA

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

20.5 Degrees True

Point <u>Number</u>	Distan Tower #1(W) (Mi.)	Array Center	Time (EST)	Field Strength (mV/m)
1	0.67	0.63	*	1850
2	0.83	0.79	*	1600
3	0.98	0.94	*	1450
4	1.28	1.25	*	930
5	1.41	1.38	*	815
6	1.53	1.50	*	730
7	1.66	1.63	*	640
8	1.78	1.75	*	585
9	1.92	1.89	*	500
10	2.06	2.03	*	440

^{*} Non-directional airborne measurements were taken between 1210-1214 EST on December 2, 1986.

TABLE III-C

CLOSE-IN NON-DIRECTIONAL MEASURED FIELD STRENGTH DATA

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

Point	<u>Distan</u> Tower	ce from Array		
Number	#1(W) (Mi.)	Center	Time (EST)	Field Strength (mV/m)
1	0.67	0.61	*	980
2	0.81	0.75	*	840
3	0.95	0.89	*	760
4	1.09	1.03	*	670
5	1.23	1.17	*	610
6	1.50	1.45	*	540
7	1.65	1.60	*	465
8	1.79	1.74	*	420
9	1.94	1.89	*	390

^{*} Non-directional airborne measurements were taken between 1220-1223 EST on December 2, 1986.

TABLE III-D

CLOSE-IN NON-DIRECTIONAL MEASURED FIELD STRENGTH DATA

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

	Distan	ce from		
Point	Tower	Array		
Number	#1(W)	Center	Time	Field Strength
	(Mi.)		(EST)	(mV/m)
1	0.87	0.78	*	950
2	1.02	0.93	*	780
3	1.18	1.09	*	660
4	1.33	1.24	#1025	620
5	1.46	1.37	*	520
6	1.59	1.50	*	480
7	1.72	1.63	*	440
8	1.85	1.76	*	410
9	1.98	1.89	*	380
10	2.11	2.02	*	360

^{*} Non-directional airborne measurements were taken between 1242-1245 EST on December 2, 1986.

[#] Ground measured point, measured on October 29, 1986 at 1025 EST.

TABLE III-E

CLOSE-IN NON-DIRECTIONAL MEASURED FIELD STRENGTH DATA

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

92.5 Degrees True

Point Number	Distan Tower #1(W) (Mi.)	Array Center	Time (EST)	Field Strength (mV/m)
1	0.63	0.54	*	1500
2	0.85	0.76	*	860
3	0.96	0.86	*	745
4	1.28	1.19	#1450	618
5	1.38	1.29	#1452	585
6	1.48	1.39	#1454	525
7	1.59	1.50	#1458	545
8	1.77	1.68	*	540
9	1.94	1.85	*	500
10	2.11	2.02	*	460

^{*} Non-directional airborne measurements were taken between 1255-1258 EST on December 2, 1986.

[#] Ground measured points, measured on October 24, 1986 EDT.

TABLE III-F

CLOSE-IN NON-DIRECTIONAL MEASURED FIELD STRENGTH DATA

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

	<u>Distan</u>	ce from		
Point	Tower	Array		
Number	#1(W)	Center	Time	Field Strength
	(Mi.)		(EST)	(m V / m)
1	0.60	0.52	*	1500
2	0.88	0.80	*	860
3	1.03	0.95	*	750
4	1.17	1.09	*	670
5	1.31	1.23	*	600
6	1.45	1.37	#1344	650
7	1.55	1.47	*	470
8	1.65	1.57	#1346	495
9	1.82	1.74	*	370
10	1.98	1.90	*	350

^{*} Non-directional airborne measurements were taken between 1322-1325 EST on December 2, 1986.

[#] Ground measured points, measured on October 20, 1986 EDT.

TABLE III-G

CLOSE-IN NON-DIRECTIONAL MEASURED FIELD STRENGTH DATA

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

Point <u>Number</u>	Distan Tower #1(W) (Mi.)	Array Center	Time (EST)	Field Strength (mV/m)
1	0.58	0.51	*	1500
2	0.75	0.68	*	890
3	0.92	0.86	*	690
4	1.01	0.95	*	610
5	1.08	1.02	#0944	740
6	1.38	1.32	*	460
7	1.52	1.46	*	430
8	1.66	1.66	*	400
9	1.76	1.70	*	380
10	1.94	1.88	*	370

^{*} Non-directional airborne measurements were taken between 1310-1313 EST on December 2, 1986.

[#] Ground measured point, measured on October 28, 1986 EST.

TABLE III-H

CLOSE-IN NON-DIRECTIONAL MEASURED FIELD STRENGTH DATA

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

Point	<u>Distan</u> Tower	ce from Array		
Number	#1 (W) (Mi.)	Center	Time (EST)	Field Strength (mV/m)
1	0.56	0.52	*	1600
2	0.66	0.62	*	1400
3	0.76	0.72	*	990
4	0.86	0.82	#1132	1000
5	1.00	0.96	*	760
6	1.13	1.09	*	670
7	1.26	1.23	*	580
8	1.39	1.36	*	520
9	1.66	1.63	*	440
10	1.93	1.90	*	380

^{*} Non-directional airborne measurements were taken between 1340-1343 EST on December 2, 1986.

[#] Ground measured point, measured on December 1, 1986 EST.

TABLE III-I

CLOSE-IN NON-DIRECTIONAL MEASURED FIELD STRENGTH DATA

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

Point Number	Distan Tower #1(W) (Mi.)	Array Center	Time (EST)	Field Strength (mV/m)
1	0.50	0.51	*	1750
2	0.60	0.61	*	1500
3	0.79	0.80	#1130	1120
4	0.84	0.85	#1113	1120
5	0.96	0.97	*	760
6	1.08	1.09	*	690
7	1.21	1.22	*	610
8	1.33	1.34	*	550
9	1.58	1.59	*	470
10	1.82	1.83	*	410

^{*} Non-directional airborne measurements were taken between 1355-1358 EST on December 2, 1986.

[#] Ground measured points, measured on December 1, 1986.

TABLE III-J

CLOSE-IN NON-DIRECTIONAL MEASURED FIELD STRENGTH DATA

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

	<u>Di</u> stan	ce from		
Point	Tower	Array		
Number	#1(W)	Center	Time	Field Strength
	(Mi.)		(EST)	(m V / m)
1	0.48	0.54	*	1650
2	0.75	0.81	*	950
3	0.89	0.95	*	840
4	1.04	1.08	#1218	880
5	1.05	1.13	#1355	660
6	1.22	1.28	*	610
7	1.36	1.42	*	530
8	1.49	1.55	*	470
9	1.62	1.68	*	440
10	1.74	1.80	*	410

^{*} Non-directional airborne measurements were taken between 1418-1421 EST on December 2, 1986.

[#] Ground measured point, measured on October 28, 1986 EST.

TABLE III-K

CLOSE-IN NON-DIRECTIONAL MEASURED FIELD STRENGTH DATA

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

Point Number	Distan Tower #1(W) (Mi.)	Ce from Array Center	Time (EST)	Field Strength (mV/m)
1	0.52	0.59	*	1600
2	0.62	0.70	*	1500
3	0.85	0.93	*	880
4	0.97	1.05	*	780
5	1.09	1.17	*	680
6	1.21	1.29	*	620
7	1.33	1.41	#1438	690
8	1.36	1.46	#1508	630
9	1.56	1.64	*	470
10	1.74	1.82	*	440

^{*} Non-directional airborne measurements were taken between 1418-1421 EST on December 2, 1986.

[#] Ground measured point, measured on October 24, 1986 EDT.

TABLE III-L

CLOSE-IN NON-DIRECTIONAL MEASURED FIELD STRENGTH DATA

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

		ce from		
Point	Tower	Array		
Number	#1(W)	Center	Time	Field Strength
	(Mi.)		(EST)	(mV/m)
1	0.53	0.63	*	1600
2	0.73	0.83	*	1000
3	0.86	0.96	*	850
4	0.98	1.08	*	750
5	1.11	1.21	*	670
6	1.23	1.33	*	600
7	1.43	1.53	#0950	610
8	1.72	1.82	#0952	555
9	1.77	1.87	#0957	480
10	1.89	1.99	*	420

^{*} Non-directional airborne measurements were taken between 1455-1458 EST on December 2, 1986.

[#] Ground measured point, measured on Dewcember 1,1986.

TABLE III-M

CLOSE-IN NON-DIRECTIONAL MEASURED FIELD STRENGTH DATA

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

Point <u>Number</u>	Distand Tower #1(W) (Mi.)	Array Center	Time (EST)	Field Strength (mV/m)
1	0.77	0.84	*	1000
2	0.87	0.95	*	900
3	0.98	1.06	*	830
4	1.15	1.23	*	690
5	1.31	1.39	*	600
6	1.47	1.55	*	530
7	1.63	1.71	*	470
8	1.79	1.87	*	430
9	1.95	2.03	*	390
10	2.11	2.19	*	370

^{*} Non-directional airborne measurements were taken between 1510-1513 EST on December 2, 1986.

TABLE III-N

CLOSE-IN NON-DIRECTIONAL MEASURED FIELD STRENGTH DATA

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

Point Number	Distan Tower #1(W) (Mi.)	Array Center	Time (EST)	Field Strength (mV/m)
1	0.62	0.66	*	1400
2	0.79	0.83	*	950
3	1.28	1.32	*	630
4	1.35	1.39	*	600
5	1.42	1.46	*	570
6	1.49	1.53	*	540
7	1.56	1.60	*	510
8	1.70	1.74	*	470
9	1.84	1.88	*	440
10	2.01	2.05	*	400

^{*} Non-directional airborne measurements were taken between 1510-1513 EST on December 2, 1986.

TABLE IV-A

DAYTIME DIRECTIONAL MEASURED FIELD STRENGTH DATA AND NUMERICAL ANALYSIS

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

0.5 Degrees True

			Measure	d Field		
Point	Distance	Time	Non-DA	Time	D A - D	Log Ratio
Number	(Mi)	(EDT)	(m V / m)	(EST)	(m V / m)	(DA/ND)
11	2.18	*1510	390	1228	405	0.0164
12	2.48	*1517	325	1145	325	0.0000
13	2.65	*1514	312	1148	285	-0.0393
14	3.03	*1512	273	1206	265	-0.0129
15	3.68	*1451	222	1157	235	0.0247
16	4.16	*1449	187	1159	282	0.1784
17	4.42	*1447	170	1201	278	0.2136
18	4.66	*1445	148	1203	131	-0.0530
19	5.18	*1441	145	1205	132	-0.0408
20	5.69	*1438	125	1208	118	-0.0250
21	6.18	*1435	112	1209	106	-0.0239
22	6.43	*1433	110	1210	105	-0.0202
23	8.10	1458	91.0	1217	85.0	-0.0296
24	8.60	1505	84.0	1214	81.0	-0.0158
25	9.50	1521	79.0	1223	64.0	-0.0914
26	9.90	1509	81.0	1226	92.0	0.0553
27	10.10	1516	66.0	1229	82.0	0.0943
28	10.75	*1416	62.0	1232	62.0	0.0000
29	11.02	*1407	61.0	1234	64.0	0.0209

Average Log Ratio: 0.0132

Antilog: 1.031

Nondirectional Analyzed Field Strength (mV/m): 900 Directional Analyzed Field Strength (mV/m): 928

Nondirectional measurements taken October 21, 1986

* Nondirectional measurements taken October 22, 1986
Directional measurements taken November 30, 1986

TABLE IV-B

DAYTIME DIRECTIONAL MEASURED FIELD STRENGTH DATA AND NUMERICAL ANALYSIS

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

35.0 Degrees True

			Measure	d Field		
Point	Distance	Time	Non-DA	Time	DA-D	Log Ratio
Number	(Mi)	(EDT)	(m V / m)	(EDT)	(mV/m)	(DA/ND)
10 (MI	•	1301	380	1449	198	-0.2831
11	3.26	1324	225	1454	123	-0.2623
12	5.12	1403	142	1505	72.0	-0.2950
13	5.72	1411	118	1509	59.0	-0.3010
14	6.34	1415	115	1511	58.0	-0.2973
15	6.58	1418	96.0	1513	51.0	-0.2747
16	7.03	1426	94.0	1517	49.0	-0.2829
17	7.85	1439	103	1522	50.0	-0.3139
18	8.50	1453	84.0	1528	43.0	-0.2908
19	9.02	1500	76.0	1532	39.0	-0.2897
20	9.52	1510	71.0	1544	36.0	-0.2950
21	10.50	1524	64.0	1552	34.5	-0.2684
22	11.43	1530	59.0	1556	31.5	-0.2725
23	12.47	1552	54.0	1608	27.5	-0.2931
24	13.40	1601	46.0	1615	24.0	-0.2825
25	14.70	1609	43.5	1622	20.5	-0.3267
26	15.56	1623	41.0	1632	21.0	-0.2906
27	16.47	1628	40.0	1655	22.0	-0.2596
28	17.65	1640	34.5	1703	18.5	-0.2706
29	18.90	1651	26.8	1710	15.0	-0.2520
30	19.80	1715	28.0	1732	15.5	-0.2568

Average Log Ratio: -0.2837

Antilog: .5203

Nondirectional Analyzed Field Strength (mV/m): 900 Directional Analyzed Field Strength (mV/m): 468

Nondirectional measurements taken on May 22, 1986 Directional measurements taken on June 1, 1986

TABLE IV-C

DAYTIME DIRECTIONAL MEASURED FIELD STRENGTH DATA AND NUMERICAL ANALYSIS

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

71.0 Degrees True

			Measure	d Field		
Point	Distance	Time	Non-DA	Time	D A – D	Log Ratio
Number	(Mi)	(EDT)	(m V / m)	(EDT)	(m V / m)	(DA/ND)
11	2.28	0944	320	1145	345	0.0327
12	4.37	1005	185	1207	193	0.0184
13	5.20	1011	142	1209	150	0.0238
14	6.48	1020	128	1214	125	-0.0103
15	6.98	1027	120	1558	138	0.0607
16	7.50	1116	97.0	1552	110	0.0546
17	8.54	1122	59.0	1547	72.0	0.0865
18	9.08	1130	86.0	1543	97.0	0.0523
19	9.60	1135	83.0	1539	92.0	0.0447
20	10.30	1142	70.0	1535	72.0	0.0122
21	11.16	1149	68.0	1527	74.0	0.0367
22	11.97	1202	57.0	1523	61.0	0.0295
23	13.00	1209	55.0	1517	60.0	0.0378
24	14.00	1224	35.5	1511	36.5	0.0121
25	15.04	1240	39.5	1500	41.5	0.0215
26	15.95	1249	45.0	1456	48.5	0.0325
27	17.30	1301	35.0	1442	36.5	0.0182

Average Log Ratio: 0.0332

Antilog: 1.079

Nondirectional Analyzed Field Strength (mV/m): 950 Directional Analyzed Field Strength (mV/m): 1025

Nondirectional measurements taken May 25, 1986 Directional measurements taken June 2, 1986

TABLE IV-D

DAYTIME DIRECTIONAL MEASURED FIELD STRENGTH DATA AND NUMERICAL ANALYSIS

prepared for Mambisa Broadcasting Corporation Miami, Florida WAOI

92.5 Degrees True

			Measure	d Field		
Point	Distance	Time	Non-DA	Time	D A – D	Log Ratio
Number	(Mi)	(EDT)	(m V / m)	(EDT)	(m V / m)	(DA/ND)
7	1.50	*1703	540	1129	860	0.2021
11	2.19	1347	350	1151	550	0.1963
12	2.55	1352	325	1154	490	0.1783
13	2.89	1356	263	1158	420	0.2033
14	6.20	1411	133	1221	200	0.1772
15	6.90	1425	125	1227	185	0.1703
16	7.20	1420	115	1230	169	0.1672
17	7.70	1430	120	1233	180	0.1761
18	8.20	1439	95.0	1238	143	0.1776
19	8.72	1446	84.0	1244	128	0.1829
20	9.35	1513	73.0	1305	115	0.1974
21	10.24	1520	79.0	1310	120	0.1816
22	10.76	1526	51.0	1318	74.0	0.1617
23	11.87	1611	41.5	1326	63.0	0.1813
24	13.10	1619	40.0	1342	63.0	0.1973
25	14.07	1633	31.5	1355	42.5	0.1301
26	14.70	1650	44.0	1402	64.0	0.1627
27	16.06	1729	21.0	1422	30.5	0.1621

Average Log Ratio: 0.1781

1.507 Antilog:

Nondirectional Analyzed Field Strength (mV/m): 1000 Directional Analyzed Field Strength (mV/m): 1507

Rounded to: 1510

Nondirectional measurements taken May 23, 1986 Nondirectional measurements taken May 24, 1986 Directional measurements taken June 2, 1986

TABLE IV-E

DAYTIME DIRECTIONAL MEASURED FIELD STRENGTH DATA AND NUMERICAL ANALYSIS

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

141.0 Degrees True

			Measured	Field		
Point	Distance	Time	Non-DA	Time	DA-D	Log Ratio
Number	(Mi)	(EDT)	(m V / m)	(EDT)	(m V / m)	(DA/ND)
11	2.15	0955	389	1000	898	0.3633
12	3.60	1030	231	1030	578	0.3983
13	4.02	1039	208	1035	450	0.3351
14	4.92	1056	198	1044	428	0.3348
15	5.33	1110	167	1048	360	0.3336
16	5.82	1126	138	1055	310	0.3515
17	6.40	1143	131	1103	285	0.3376
18	6.98	1154	108	1109	245	0.3557
19	7.40	1206	117	1114	249	0.3280
20	8.70	1225	88.5	1123	203	0.3606
21	9.65	1239	89.0	1131	203	0.3581
22	11.00	1257	71.5	1140	162	0.3552
23	12.16	1309	62.0	1149	145	0.3690
24	13.60	1325	41.5	1157	92.0	0.3457
25	15.35	1343	54.0	1215	126	0.3680
26	16.90	1404	36.5	1224	78.0	0.3298
27	18.40	1428	37.7	1239	77.5	0.3130
28	19.70	1444	29.5	1249	62.5	0.3261

Average Log Ratio: 0.3480

Antilog: 2.228

Nondirectional Analyzed Field Strength (mV/m): 950
Directional Analyzed Field Strength (mV/m): 2117

Rounded to: 2120

Nondirectional measurements taken May 25, 1986 Directional measurements taken June 2, 1986

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

190.0 Degrees True

Point Number	Distance (Mi)	Time (EDT)	Non-DA (mV/m)	Time (EDT)	DA-D (mV/m)	Log Ratio (DA/ND)
11	2.88	1506	310 310	1023	512 500	0.2179
12	3.93	1521	181 250	1018	298 310	0.2165
13	4.50	##0937	170 190	1013	293 280	0.2364
14*	5.15		140		260	0.2688
15*	6.95		130		180	0.1413
16*	7.94		120		150	0.0969
17*	8.95		75.0		150	0.3010
18	11.00	1743	67.5 76.0	1506	106 110	0.1960
19*	12.00		59.0		100	0.2291
20*	13.02		56.0		90.0	0.2061
21	13.90	#1708	27.5 27.0	1423	46.5 76.0	0.2281
22	14.52	#1718	45.5 55.0	1415	72.0 71.0	0.1993
23	15.77	#1734	36.2 49.0		60.5 60.0	0.2230
24	16.80	#1746	34.0 37.0	1408	56.0 57.0	0.2167
25	17.82	#1759	34.0 38.0	1402	55.0 54.0	0.2089
26*	18.85		30.0		48.0	0.2041
27	19.90	#1806	26.0 33.0	1344	44.0 44.0	0.2285

Average Log Ratio: 0.2120

Antilog: 1.629

Nondirectional Analyzed Field Strength (mV/m): 950 Directional Analyzed Field Strength (mV/m): 1548

Rounded to: 1550

(See page 2 for footnotes)

- Nondirectional measurements taken May 23, 1986
- # Nondirectional measurements taken May 24, 1986
- ## Nondirectional measurements taken May 25, 1986 Directional measurements taken June 2, 1986
 - * Airborne measurement
- ** Airborne measurement above ground point, not included in average Nondirectional airborne measurements taken 1547-1609 EDT on August 2, 1986
 - Directional airborne measurements taken 1615-1635 EDT on August 1, 1986

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

221.0 Degrees True

Point Number	Distance (Mi)	Time (EDT)	Non-DA (mV/m)	Time (EDT)	D A - D (m V / m)	Log Ratio (DA/ND)
4	1.04	1218	880 1200	1210	1100	0.0969
5	1.10	1355	660 980	1324	990 800	0.1761
11* 12*	2.25 2.50		420 350		600 520	0.1549 0.1719
13	2.75	1423	290 320	1550	385 440	0.1231
14	3.03	1406	260 290	1601	330 360	0.1035
15	3.40	#1058	235 270	1612	275 320	0.0683 **
16	3.75	#1051	258 250	1620	280 280	0.0355
17	3.92	1341	223 220	1541	230 250	0.0134
18*	4.50		200		230	0.0607
19* 20*	5.00 5.50		180 160		200 180	0.0458 0.0512
21* 22*	6.00 6.50		150 120		160 150	0.0280
23	7.00	#1048	110 110	1425	132 140	0.0969 0.0792 **
24* 25*	8.00 9.00		100 98.0		100 100	0.0000 0.0088
26 27*	10.05 11.00	1440	73.0 68.0	1436	88.0 72.0	0.0812 0.0248
28	19.00	1615	33.0	1453	40.0	0.0835

Average Log Ratio: 0.0746

Antilog: 1.187

Nondirectional Analyzed Field Strength (mV/m): 1000 Directional Analyzed Field Strength (mV/m): 1187

Rounded to: 1190

(See page 2 for footnotes)

- Nondirectional measurements taken October 28, 1986 # Nondirectional measurements taken December 1, 1986 Directional measurements taken November 4, 1986
- * Airborne measurement
- ** Airborne measurement above ground point, not included in average Nondirectional airborne measurements taken 1714-1735 EDT on August 2, 1986
 Directional airborne measurements taken 1655-1716 EDT on August 1, 1986

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

277.0 Degrees True

		Measured Field					
Point Number	Distance (Mi)	Time (EDT)	Non-DA (mV/m)	Time (EDT)	DA-D (mV/m)	Log Ratio (DA/ND)	
7	1.53	0950	610 500	1530	750 720	0.0897	
8	1.82	0952	555 420	1528	670 630	0.0818	
9	1.87	0957	480 410	1525	600 600	0.0969	
11*	2.37		350		520	0.1719	
12	2.87	1012	305 300	1515	370 360	0.0839	
13	3.34	1043	258 220	1434	312 325	0.0825	
14	3.39	1040	250 210	1432	300 260	0.0792	
15* 16	3.67 3.95	1211	200 232 170	1455	230 295 220	0.0607 0.1043	
17* 18* 19*	4.43 4.90 5.38		160 150 140		160 170 160	0.0000 0.0545 0.0580	
20	5.85	1039	155 120	1300	178 180	0.0601	
21* 22* 23*	6.44 7.02 7.60		110 110 100		140 130 120	0.1047 0.0726 0.0792	
24	8.18	1310	100 100	1320	127 95.0	0.1038	
25*	8.84		99.0		90.0	-0.0414	
26	9.50	1256	79.0 90.0	1329	112 80.0	0.1516	

			Measi	ured Fi	ield		
Point	Distance	Time	Non-D/	4	Time	D A - D	Log Ratio
Number	(Mi)	(EDT)	(m V / m) ((EDT)	(m V / m)	(DA/ND)
27*	10.60		84	. 0		75.0	-0.0492
28*	11.32		70.	. 0		67.0	-0.0190
				A۱	verage	Log Ratio	: 0.0679
						Antilog	: 1.169
	Nondire	ctional	Analyzed	Field	Stren	gth (mV/m)	: 1000
	Dire	ctional	Analyzed	Field	Stren	gth (mV/m)	: 1169
			·			Rounded to	: 1170

Nondirectional and directional measurements taken December 1, 1986

^{*} Airborne measurement

^{**} Airborne measurement above ground point, not included in average Nondirectional airborne measurements taken 1111-1103 EDT on August 3, 1986

Directional airborne measurements taken 0929-0950 EDT on August 2, 1986

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

308.0 Degrees True

			Measured Field				
Point Number	Distance (Mi)	Time (EDT)	Non-DA (mV/m)	Time (EDT)	DA-D (mV/m)	Log Ratio (DA/ND)	
11	2.35	1027	380 370	1343	510 520	0.1278	
12* 13*	2.79 3.22		320 270		440 400	0.1383 0.1707	
14	3.68	1004	225 210	1348	300 320	0.1249	
15*	3.99		210		320	0.1829	
16	4.29	1046	203 200	1353	262 250	0.1108	
17	4.35	1036	195 180	1351	248 240	0.1044	
18	4.55	1050	165 180	1358	225 230	0.1347	
19	4.80	1053	160 170	1359	220 190	0.1383	
20	5.10	1201	158 160	1449	213 160	0.1297	
21*	5.66		150		130	-0.0621	
22* 23*	6.21 6.77		140 120		110 110	-0.1047 -0.0378	
24	7.32	1242	100 100	1347	143 100	0.1553	
25* 26	7.89 8.46	1234	95.0 89.0	1339	100 120	0.0223 0.1298	
27*	9.03		87.0 84.0		98.0 93.0	0.0442	
28 * 29	9.60 19.90	1410	80.0 37.0 39.0	1435	88.0 48.0 59.0	0.0414 0.1130 **	

Average Log Ratio: 0.0876

Antilog: 1.223

Nondirectional Analyzed Field Strength (mV/m): 950 Directional Analyzed Field Strength (mV/m): 1162

(See page 2 for footnotes)

TABLE IV-I

Page 2 of 2

Nondirectional and directional measurements taken on December 1, 1986

^{*} Airborne measurement

^{**} Airborne measurement above ground point, not included in average Nondirectional airborne measurements taken 1156-1218 EDT on August 2, 1986
Directional airborne measurements taken 1020-1059 EDT on August 2, 1986

TABLE V-A

NIGHTTIME DIRECTIONAL MEASURED FIELD STRENGTH DATA AND NUMERICAL ANALYSIS

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

0.5 Degrees True

				red Field		
Point	Distance	Time	Non-DA	Time	D A - N	Log Ratio
Number	(Mi)	(EDT	') (mV/m)	(EST)	(m V / m)	(DA/ND)
11	2.18	** 15		1154	4.90	-1.9009
12	2.48	** 15	17 325	1140	3.20	-2.0067
13(M	P) 2.65	** 15	312	1146	3.05	-2.0099
14	3.03	** 15	12 273	1204	3.00	-1.9590
15	3.68	** 14	51 222	1222	2.85	-1.8915
16	4.16	** 14	49 187	1228	1.60	-2.0677
17	4.42	** 14	47 170	1230	1.50	-2.0544
18	4.66	** 14	45 148	1233	1.65	-1.9528
19	5.18	** 14		1236	1.30	-2.0474
20	5.69	** 14		1241	1.20	-2.0177
21	6.18	** 14		1245	2.75	-1.6099
22	6.43	** 14		1250	2.25	-1.6892
23	8.10	* 14			0.92	-1.9953
24	8.60	* 15			0.84	-2.0000
25	9.50	* 15			0.62	-2.1052
26	9.90	* 15			1.80	-1.6532
27	10.10	* 15			2.90	-1.3571
28	10.75	** 14			2.40	-1.4122
29	11.02	** 14			1.90	-1.5066

Average Log Ratio: -1.8546

Antilog: .0140

Nondirectional Analyzed Field Strength (mV/m): 900
Directional Analyzed Field Strength (mV/m): 12.6

^{*} Nondirectional measurements taken October 21, 1986

^{**} Nondirectional measurements taken October 22, 1986 Directional measurements taken November 24, 1986

NIGHTTIME DIRECTIONAL MEASURED FIELD STRENGTH DATA AND NUMERICAL ANALYSIS

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

20.5 Degrees True

			Measured	i Field		Quadrature Method	
Point Number	Distance (Mi)	Time (EDT)	Non-DA (mV/m)	Time (EST)	DA-N (mV/m)	Correction Factor	Log Ratio (DA/ND)
11	2.85	1420	308	1448	1.90	0.687	0 2707
12(M		1425	205	1433	2.20		-2.3727
13	4.57	1427	200			0.827	-2.0519
14	5.52	1432	162	1414	3.20	0.834	-1.8750
15	5.88	1434		1428	0.90	0.876	-2.3127
16			128	1425	0.72	0.888	-2.3013
	6.58	1437	130	1422	1.70	0.908	-1.9256
17	6.93	1439	125	1418	0.82	0.915	-2.2215
18	7.70	1447	102	1252	1.90	0.930	-1.7614
19	8.74	1451	62.0	1247	1.40	0.944	-1.6714
20	9.80	1455	75.0	1241	1.10	0.954	-1.8541
21	10.75	1505	61.0	1303	1.00	0.961	-1.8025
22	11.40	1509	60.0	1308	1.10	0.965	-1.7520
23	12.45	1514	55.0	1313	0.80	0.970	-1.8504
24	14.20	1521	41.0	1319	1.00	0.977	
25	15.42	1528	42.5	1325	1.60	0.980	-1.6230
26	17.16	1534	32.5	1331	1.10		-1.4330
27	17.72	1538	30.0	1334		0.984	-1.4776
28	18.68	1543	27.0		0.92	0.984	-1.5202
29	19.40	1546		1339	0.76	0.986	-1.5566
30	19.96		25.8	1343	0.78	0.987	-1.5252
J 0	17.70	1550	25.5	1346	0.82	0.988	-1.4981

Average Proximity Corrected Log Ratio: -1.8193

Antilog: .0152 Nondirectional Analyzed Field Strength (mV/m): 950 Directional Analyzed Field Strength (mV/m): 14.4

Nondirectional measurements taken October 22, 1986 Directional measurements taken November 23, 1986

COMPUTED UNATTENUATED NEAR FIELD STRENGTHS

		Computed Un	attenuated	Radiation
Point	Distance	Theoretical	Measured	Standard
Number	(miles)	(m V / m)	(mV/m)	(mV/m)
1	0.67	90.1	92.4	102
2 3 4	0.83	58.9	61.2	68.9
3	0.98	42.3	44.6	51.3
	1.28	24.9	27.1	32.7
5 6 7 8	1.41	20.5	22.7	28.0
6	1.53	17.5	19.6	24.6
7	1.66	14.8	17.0	21.7
8	1.78	12.9	15.0	19.6
9	1.92	11.1	13.2	17.5
10	2.06	9.66	11.7	15.9
11	2.85	5.06	6.97	10.3
12	4.45	2.09	3.71	6.06
13	4.57	1.98	3.58	5.88
14	5.52	1.36	2.82	4.77
15	5.88	1.20	2.61	4.46
16	6.58	0.96	2.28	3.95
17	6.93	0.87	2.15	3.74
18	7.70	0.70	1.91	3.35
19	8.74	0.55	1.65	2.93
20	9.80	0.44	1.46	2.61
21	10.75	0.37	1.32	2.37
22	11.40	0.32	1.24	2.23
23	12.45	0.28	1.13	2.04
24	14.20	0.21	0.98	1.78
25	15.42	0.18	0.90	1.64
26	17.16	0.15	0.81	1.47
27	17.72	0.14	0.78	1.43
28	18.68	0.12	0.74	1.35
29	19.40	0.12	0.71	1.30
30	19.96	0.11	0.69	1.26

TABLE V-C

NIGHTTIME DIRECTIONAL MEASURED FIELD STRENGTH DATA AND NUMERICAL ANALYSIS

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

35.0 Degrees True

			Measure	d Field		
Point	Distance	Time	Non-DA	Time	DA-N	Log Ratio
Number	(Mi)	(EDT)	(m V / m)	(EST)	(m V / m)	(DA/ND)
10	2.03	*1320	395	1109	28.5	-1.1418
11	3.26	*1438	250	1137	21.0	-1.0757
12	5.12	*1451	150	1147	13.5	-1.0458
13	5.72	*1455	115	1149	9.50	-1.0830
14	6.34	*1500	121	1152	7.20	-1.2255
15	6.58	*1505	102	1155	7.80	-1.1165
16	7.03	*1513	92.0	1157	8.50	-1.0344
17	7.85	*1520	98.0	1201	7.20	-1.1339
18	8.50	*1526	86.0	1208	5.60	-1.1863
19	9.02	*1548	80.0	1213	8.10	-0.9946
20	9.52	*1553	68.0	1219	7.50	-0.9574
21	10.50	*1559	66.0	1229	8.50	-0.8901
22	11.43	*1605	61.5	1234	7.30	-0.9256
23	12.47	*1610	49.0	1301	6.30	-0.8909
24	13.40	*1615	50.0	1321	6.70	-0.8729
25	14.70	*1621	45.0	1327	4.30	-1.0197
26	15.56	*1636	42.0	1336	3.00	-1.1461
27	16.47	**1443	38.0	1341	4.20	-0.9565
28	17.65	**1449	35.0	1352	3.20	-1.0389
29	18.90	**1456	27.0	1400	2.20	-1.0889
30	19.80	**1519	28.0	1420	2.20	-1.1047

Average Log Ratio: -1.0442

Antilog: .0903

Nondirectional Analyzed Field Strength (mV/m): 900 Directional Analyzed Field Strength (mV/m): 81.3

 ^{*} Nondirectional measurements taken October 24, 1986
 ** Nondirectional measurements taken October 25, 1986
 Directional measurements taken November 25, 1986

TABLE V-D

NIGHTTIME DIRECTIONAL MEASURED FIELD STRENGTH DATA AND NUMERICAL ANALYSIS

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

71.0 Degrees True

			Measure	d Field		
Point	Distance	Time	Non-DA	Time	D A – N	Log Ratio
Number	(Mi)	(EDT)	(m V / m)	(EST)	(m V / m)	(DA/ND)
11	2.28	1300	327	1128	420	0.1087
12	4.37	1337	180	1136	215	0.0772
13	5.20	1345	145	1139	185	0.1058
14	6.48	1351	132	1143	132	0.0000
15	6.98	1358	121	1147	117	-0.0146
16	7.50	1404	109	1151	107	-0.0080
17	8.54	1409	51.0	1155	63.0	0.0918
18	9.08	1413	92.0	1200	95.0	0.0139
19	9.60	1415	91.0	1205	89.0	-0.0097
20	10.30	1419	66.0	1208	69.0	0.0193
21	11.16	1425	59.0	1218	68.0	0.0617
22	11.97	1436	61.0	1222	59.0	-0.0145
23	13.00	1443	54.0	1226	54.0	0.0000
24	14.00	1450	39.5	1231	39.5	0.0000
25	15.04	1459	42.0	1238	40.0	-0.0212
26	15.95	1506	41.5	1244	49.0	0.0721
27	17.30	1513	38.0	1253	35.0	-0.0357
						0 0000

Average Log Ratio: 0.0263

Antilog: 1.062

Nondirectional Analyzed Field Strength (mV/m): 950 Directional Analyzed Field Strength (mV/m): 1009

Rounded to: 1010

Nondirectional measurements taken October 25, 1986 Directional measurements taken November 26, 1986

TABLE V-E

NIGHTTIME DIRECTIONAL MEASURED FIELD STRENGTH DATA AND NUMERICAL ANALYSIS

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

92.5 Degrees True

			Measure	d Field		
Point	Distance	Time	Non-DA	Time	D A – N	Log Ratio
Number	(Mi)	(EDT)	(m V / m)	(EST)	(m V / m)	(DA/ND)
11	2.19	*1524	365	1501	630	0.2370
12	2.55	*1526	312	1459	515	0.2177
13	2.89	*1530	275	1455	450	0.2139
14	6.20	*1614	105	1440	220	0.3212
15	6.90	**1358	115	1434	185	0.2065
16	7.20	**1402	110	1431	163	0.1708
17	7.70	**1406	121	1428	198	0.2139
18	8.20	**1412	98.0	1423	148	0.1790
19	8.72	**1416	90.0	1422	132	0.1663
20	9.35	**1434	72.0	1406	110	0.1841
21	10.24	**1440	82.0	1358	115	0.1469
22	10.76	**1445	55.0	1353	96.0	0.2419
23	11.87	**1453	40.5	1349	62.0	0.1849
24	13.10	**1511	44.0	1345	68.0	0.1891
25	14.07	**1517	28.5	1331	53.0	0.2694
26	14.70	**1525	38.0	1320	57.0	0.1761
27	16.06	**1535	27.0	1308	38.0	0.1484

Average Log Ratio: 0.2039

Antilog: 1.599

Nondirectional Analyzed Field Strength (mV/m): 1000 Directional Analyzed Field Strength (mV/m): 1599

Rounded to: 1600

Nondirectional measurements taken October 24, 1986
 Nondirectional measurements taken October 25, 1986
 Directional measurements taken November 26, 1986

TABLE V-F

NIGHTTIME DIRECTIONAL MEASURED FIELD STRENGTH DATA AND NUMERICAL ANALYSIS

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

120.0 Degrees True

			Measure	d Field		
Point	Distance	Time	Non-DA	Time	D A – N	Log Ratio
Number	(Mi)	(EDT)	(m V / m)	(EST)	(m V / m)	(DA/ND)
	\ 1 27	1044		1000		
6 (MP		1344	650	1329	248	-0.4185
11	3.60	1410	208	1346	98.0	-0.3268
12	4.78	1416	175	1350	100	-0.2430
13	4.93	1431	162	1402	88.0	-0.2650
14	6.10	1440	118	1409	66.0	-0.2523
15	6.45	1446	128	1412	63.0	-0.3079
16	7.03	1453	115	1416	64.0	-0.2545
17	7.33	1457	112	1418	61.0	-0.2639
18	8.60	1509	82.0	1425	44.0	-0.2704
19	9.15	1516	86.0	1431	41.0	-0.3217
20	9.70	1522	79.0	1435	39.5	-0.3010
21	10.25	1537	61.0	1442	33.0	-0.2668
22	10.86	1540	60.0	1445	28.5	-0.3233
23	11.60	1548	54.0	1449	27.5	-0.2931
24	12.59	1553	62.0	1455	26.0	-0.3774
25	13.25	1602	45.5	1500	23.5	-0.2869
26	13.80	1608	52.0	1504	25.5	-0.3095
27	14.35	1613	53.0	1508	24.5	-0.3351
28	14.83	1618	45.5	1510	24.0	-0.2778
29	15.87	1627	38.5	1518	23.0	-0.2237
30	16.50	1633	51.0	1520	28.5	-0.2527
31	17.70	1647	29.5	1524	23.5	-0.0988
32	18.50	1659	48.5	1530	28.5	-0.2309

Average Log Ratio: -0.2827

Antilog: .5216

Nondirectional Analyzed Field Strength (mV/m): 1000 Directional Analyzed Field Strength (mV/m): 522

Nondirectional measurements taken October 20, 1986 Directional measurements taken November 24, 1986

TABLE V-G

NIGHTTIME DIRECTIONAL MEASURED FIELD STRENGTH DATA AND NUMERICAL ANALYSIS

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

141 Degrees True

			Measure			
Point	Distance	Time	Non-DA	Time	D A - N	Log Ratio
Number	(Mi)	(EST)	(m V / m)	(EST)	(m V / m)	(DA/ND)
11	2.15	*0959	385	1041	808	0.3220
12	3.60	1000	230	1058	540	0.3707
13	4.02	1008	210	1102	545	0.4142
14	4.92	1020	195	1108	530	0.4342
15	5.33	1035	165	1112	410	0.3953
16	5.82	1044	135	1118	350	0.4137
17	6.40	1052	130	1126	325	0.3979
18	6.98	1056	110	1130	225	0.3108
19	7.40	1100	115	1134	220	0.2817
20	8.70	1115	86.0	1144	225	0.4177
21	9.65	1122	88.0	1155	208	0.3736
22	11.00	1130	72.0	1202	192	0.4260
23	12.16	1135	60.0	1210	132	0.3424
24	13.60	1145	43.5	1217	71.0	0.2128
25	15.35	1155	55.0	1226	132	0.3802
26	16.90	1158	37.0	1239	82.0	0.3456
27	18.40	1205	36.5	1251	83.0	0.3568
28	19.70	1210	30.5	1259	62.0	0.3081

Average Log Ratio: 0.3613

Antilog: 2.298

Nondirectional Analyzed Field Strength (mV/m): 950 Directional Analyzed Field Strength (mV/m): 2183

Rounded to: 2180

Nondirectional measurements taken October 29, 1986

* Nondirectional measurements taken October 28, 1986
Directional measurements taken November 29, 1986

TABLE V-H

NIGHTTIME DIRECTIONAL MEASURED FIELD STRENGTH DATA AND NUMERICAL ANALYSIS

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

162.0 Degrees True

			Measure	d Field		
Point	Distance	Time	Non-DA	Time	D A - N	Log Ratio
Number	(Mi)	(EST)	(m V / m)	(EST)	(m V / m)	(DA/ND)
11	2.94	*1011	315	1518	1100	0.5431
12	5.05	1353	168	1456	640	0.5809
13	5.58	1343	155	1503	520	0.5257
14	6.10	1331	104	1442	440	0.6264
15	7.22	1322	98.0	1436	355	0.5590
16	9.20	1310	78.0	1429	282	0.5582
17	9.90	1300	76.0	1425	258	0.5308
18	10.27	1250	85.0	1421	300	0.5477
19	11.05	1241	73.0	1410	235	0.5077
20	12.40	1228	58.0	1405	214	0.5670
21	13.00	1220	57.0	1401	200	0.5452
22	14.25	1210	46.5	1355	175	0.5756
23	15.12	1205	52.0	1349	188	0.5582
24	16.08	1153	32.0	1343	135	0.6252
25	17.13	1146	36.0	1337	125	0.5406
26	18.19	1137	24.0	1332	89.0	0.5692
27	19.08	1131	36.5	1326	118	0.5096
28	19.87	1124	24.5	1322	92.0	0.5746

Average Log Ratio: 0.5580

Antilog: 3.614

Nondirectional Analyzed Field Strength (mV/m): 950 Directional Analyzed Field Strength (mV/m): 3434

Rounded to: 3430

Nondirectiona measurements taken October 28, 1986

* Nondirectional measurements taken December 1, 1986
Directional measurements taken November 29, 1986

NIGHTTIME DIRECTIONAL MEASURED FIELD STRENGTH DATA AND NUMERICAL ANALYSIS

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

190 Degrees True

			Measure	d Field		
	Distance	Time	Non-DA	Time		Log Ratio
Number	(Mi)	(EST)	(m V / m)	(EST)	(m V / m)	(DA/ND)
11	2.88	1513	330	0958	660	0.3010
			290		530	**
12	3.93	1523	190	0955	375	0.2953
			210		430	**
13	4.50	1533	185	0951	360	0.2891
			180		320	**
14*	5.15		150		280	0.2711
	6.95		110		210	0.2808
16*	7.94		94.0		190	0.3056
17*	8.95		77.0		165	0.3310
18	11.00	1626	67.0	1059	143	0.3293
			58.0		140	**
19*	12.00		53.0		120	0.3549
	13.02		44.0		95.0	0.3343
21	13.90	#0946	27.5	1041	56.0	0.3089
			47.0		92.0	**
22	14.52	#0951	44.5	1037	85.0	0.2811
			42.0		78.0	**
23	15.77	#1127	38.0	1119	78.0	0.3123
			38.0		76.0	**
24	16.80	#1019	33.0	1124	72.0	0.3388
			33.0		65.0	**
25	17.82	#1030	32.0	1129	69.0	0.3337
			29.0		56.0	**
26*	18.85		30.0		55.0	0.2632
27	19.90	#1046	28.0	1134	55.0	0.2932
			26.0		50.0	**

Average Log Ratio: 0.3073

Antilog:

2.029

Nondirectional Analyzed Field Strength (mV/m): 950 Directional Analyzed Field Strength (mV/m): 1927

Rounded to: 1930

Nondirectional measurements taken October 27, 1986 except for those marked #, taken on October 28, 1986
Directional measurements taken November 30, 1986

* Airborne measurement

** Airborne measurement above ground point, not included in average

Nondirectional airborne measurements taken 0930-0940 EST on December 4, 1986

Directional airborne measurements taken 0900-0914 EST on December 3, 1986

NIGHTTIME DIRECTIONAL MEASURED FIELD STRENGTH DATA AND NUMERICAL ANALYSIS

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

235 Degrees True

			Measure	d Field		Quadrature Method	
Point	Distance	Time	Non-DA	Time	DA-N	Correction	log Datio
Number	(Mi)	(EDT)	(mV/m)	(EST)	(mV/m)	Factor	Log Ratio (DA/ND)
7 (MP)	1.41	1438	690	1022	268	0.707	
, , , , ,	1.41	1430	540	1022	200	0.797	-0.5094 **
8	1.46	1508	630	1146	262	0.803	-0.4765
			520			0.000	**
11*	2.32		380		200	0.868	-0.3404
12*	2.75		320		170	0.886	-0.3271
13*	2.97		280		160	0.894	-0.2917
14	3.18	1518	278	1216	100	0.900	-0.4896
			150		260		**
15	3.37	1524	235	1219	95.0	0.906	-0.4364
			250		73.0		**
16	3.66*		240		74.0	0.913	-0.5507
17	3.95	1533	223	1223	92.0	0.918	-0.4214
			220		78.0		**
18	4.05	1540	260	1228	89.0	0.920	-0.5016
			210		74.0	*****	**
19	4.32*		170		65.0	0.925	-0.4514
20	4.58*		160		43.0	0.929	-0.6026
21	4.84*		160		45.0	0.933	-0.5812
22	5.10	1559	143	1239	48.0	0.936	-0.5029
			160		41.0		**
23	5.30	1602	135	1237	47.0	0.938	-0.4859
			140		45.0		**
24	5.72	1618	125	1243	41.5	0.943	-0.5046
			120		36.0		**
25	6.50	1614	86.0	1324	30.5	0.949	-0.4729
			120		30.0	0.515	**
26*	7.28		95.0		31.0	0.954	-0.5066

Average Proximity Corrected Log Ratio: -0.4696

Antilog: .3391

Nondirectional Analyzed Field Strength (mV/m): 1000 Directional Analyzed Field Strength (mV/m): 339

		Computed Ur	nattenuated	Radiation
Point	Distance	Theoretical	Measured	Standard
Number	(miles)	(m V / m)	(mV/m)	(mV/m)
1	0.52	1414	1363	1526
2	0.62	1091	1045	1183
3	0.85	702	663	768
4	0.97	588	552	646
5	1.09	505	472	556
2 3 4 5 6 7	1.21	441	411	487
7	1.41	364	337	404
8	1.46	349	322	387
9	1.56	322	296	357
10	1.74	282	258	314
11	2.32	201	182	225
12	2.75	165	149	186
13	2.97	151	136	170
14	3.18	140	126	158
15	3.37	131	118	148
16	3.66	120	107	135
17	3.95	110	98.2	124
18	4.05	107	95.5	121
19	4.32	99.8	88.9	113
20	4.58	93.6	83.3	106
21	4.84	88.2	78.3	%100.0
22	5.10	83.3	73.9	94.5
23	5.30	79.9	70.9	90.7
24	5.72	73.7	65.2	83.7
25	6.50	64.3	56.8	73.1
26	7.28	57.0	50.2	64.9

Nondirectional measurements taken on October 24, 1986
Directional measurements taken on November 29, 1986
Nondirectional airborne measurements taken 1010-1031 EST on December 4, 1986
Directional airborne measurements taken 1005-1020 EST on December 3, 1986

 ^{*} Airborne measurement

^{**} Airborne measurement above ground point, not included in average

NIGHTTIME DIRECTIONAL MEASURED FIELD STRENGTH DATA AND NUMERICAL ANALYSIS

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

277 Degrees True

			Measure			
	Distance	Time	Non-DA	Time	D A – N	Log Ratio
Number	(Mi)	(EST)	(m V / m)	(EST)	(m V / m)	(DA/ND)
7	1 52					
7	1.53	0950	610	#0949	62.0	-0.9929
0 / М1) 1 00	0050	520	1507		**
O (M i	9) 1.82	0952	555	1507	71.0	-0.8930
0	1 07	0057	460			**
9	1.87	0957	480	1503	59.5	-0.9067
11+	0 07		450			**
11*	2.37	1010	380		72.0	-0.7225
12	2.87	1012	305	#1513	37.5	-0.9103
1.0	2 24	1010	310		46.0	**
13	3.34	1043	258	1447	28.5	-0.9568
1.4	2 22		270		33.0	**
14	3.39	1040	250	1442	29.0	-0.9355
15+	2 67		260		32.0	**
15*	3.67		250		28.0	-0.9508
16	3.95	1211	232	##1115	23.0	-1.0038
174	4 40		230		27.0	**
17*	4.43		200		28.0	-0.8539
18*	4.90		180		24.0	-0.8751
19*	5.38		170		26.0	-0.8155
20	5.85	1039	155	##1020	16.5	-0.9728
014			150		16.0	**
21*	6.44		130		18.0	-0.8587
22*	7.02		120		18.0	-0.8239
23*	7.60	1010	100		14.0	-0.8539
24	8.18	1310	100	1348	12.2	-0.9136
05+	0.04		88.0		12.0	**
25*	8.84	1050	78.0		11.0	-0.8507
26	9.50	1256	79.0	1411	11.7	-0.8294
			73.0		7.30	**

Measured Field							
Point Number	Distance (Mi)	Time (EST)	Non-DA (mV/m)	Time (EST)	DA-N (mV/m)	Log Ratio (DA/ND)	
27* 28*	10.60 11.32		79.0 69.0		7.10 7.50	-1.0464 -0.9638	
	Nondirec Direc	tional tional	Analyzed Fiel Analyzed Fiel	d Streng	Log Ratio: Antilog: gth (mV/m): gth (mV/m):	.1255 1000	

Nondirectional measurements taken December 1, 1986 Directional measurements taken November 30, 1986

[#] Directional measurements taken December 1, 1986

^{##} Directional measurements taken November 29, 1986 Nondirectional airborne measurements taken 1038-1056 EST on December 4, 1986 Directional airborne measurements taken 1045-1050 EST on

December 3, 1986 * Airborne measurement

^{**} Airborne measurement above ground point, not included in average

NIGHTTIME DIRECTIONAL MEASURED FIELD STRENGTH DATA AND NUMERICAL ANALYSIS

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

308 Degrees True

Measured Field						
Point	Distance	Time	Non-DA	Time	DA-N	Log Ratio
Number	(Mi)	(EST)	(m V / m)	(EST)	(mV/m)	(DA/ND)
11/M	P) 2.35					
11(11	r) 2.35	1027	380	1349	10.0	-1.5798
12*	2.79		320		12.0	**
13*	3.22		260		13.5	-1.2846
14	3.68	1004	210		6.90	-1.4834
14	3.00	1004	225	#1010	3.20	-1.8470
15*	3.99		109		4.70	**
16	4.29	1046	180	1250	3.30	-1.7368
- 0	1 • 2 3	1040	203 170	1358	5.20	-1.5915
17	4.35	1036	195	1256	4.90	**
	1.55	1030	160	1356	4.80	-1.6088
18	4.55	1050		1400	5.90	**
	1.55	1030	165 160	1402	6.00	-1.4393
19	4.80	1053	160	1404	6.60	**
	1.00	1033	150	1404	5.60	-1.4559
20	5.10	1201	158	# 1 O 4 O	5.00	**
	••••	1201	130	#1040	5.90	-1.4278
21	5.66		110		3.70	**
22*	6.21		100		5.70	-1.2855
23*	6.77		92.0		7.70	-1.1135
24*	7.32		100		6.40	-1.1576
			89.0		6.80	-1.1675 **
25*	7.89		86.0		3.80	
26	8.46	1234	89.0	1457	3.40 4.30	-1.4030
			75.0	1437	2.70	-1.3159 **
27*	9.03		72.0		1.90	-1.5786
28*	9.60		65.0		2.30	-1.4512
29*	19.90	1410	37.0	1534	2.30	-1.4512
			J J	1334	2.50	-1.5003

Average Log Ratio: -1.4281

Antilog: .0373

Nondirectional Analyzed Field Strength (mV/m): 950 Directional Analyzed Field Strength (mV/m): 35.4

TABLE V-L

Page 2 of 2

Nondirectional measurements taken December 1, 1986
Directional measurements taken November 23, 1986
Directional measurements taken November 24, 1986
Nondirectional airborne measurements taken 1110-1133 EST on December 4, 1986
Directional airborne measurements taken 1138-1200 EST on December 3, 1986

* Airborne measurement** Airbotne measurement above ground point, not included in average

NIGHTTIME DIRECTIONAL MEASURED FIELD STRENGTH DATA AND NUMERICAL ANALYSIS

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

333 Degrees True

Measured Field						
	Distance	Time	Non-DA	Time	DA-N	Log Ratio
Number	(Mi)	(EST)	(m V / m)	(EST)	(m V / m)	(DA/ND)
11*	2.38		320		8.70	-1.5656
_	2.71		260		9.90	-1.4193
) 3.03	1032	310	#0950	9.10	-1.5323
- · , · · ·	,	1002	235	#0330	7.10	-1.3323
14*	3.36		200		4.75	-1.6243
15*	3.68		180		5.10	-1.5477
16*	4.00		160		3.70	-1.6359
17	4.32	1100	183	1415	2.80	-1.8153
			160		3.35	**
18	4.75	1102	180	1412	1.60	-2.0512
	_		150		2.60	**
19*	5.28		130		2.00	-1.8129
20*	5.81		110		1.70	-1.8109
21*	6.34		110		2.30	-1.6797
22	6.86	1119	92.5	##1426	1.60	-1.7620
0.0			90.0		2.40	**
23	6.98	1116	71.0		1.90	-1.8970
2.4	7 10	1.600	86.0		1.75	**
24	7.15	1622	96.0	1423	1.85	-1.7151
25	7 70	1.00	81.0		1.80	**
23	7.70	1625	94.0	1430	2.15	-1.6407
26*	8.35		81.5		1.10	**
27	9.00	1515	73.0	"1040	2.80	-1.4162
21	9.00	1515	79.0 67.0	#1048	1.30	-1.7837 **
28*	11.24	1531	63.0	#1205	1.55	
29*	13.70	1653	49.0	#1205 #1528	0.90 2.70	-1.8451
		1000	79.0	#1360	2.70	-1.2588

Average Log Ratio: -1.6742 Antilog: .0212

900

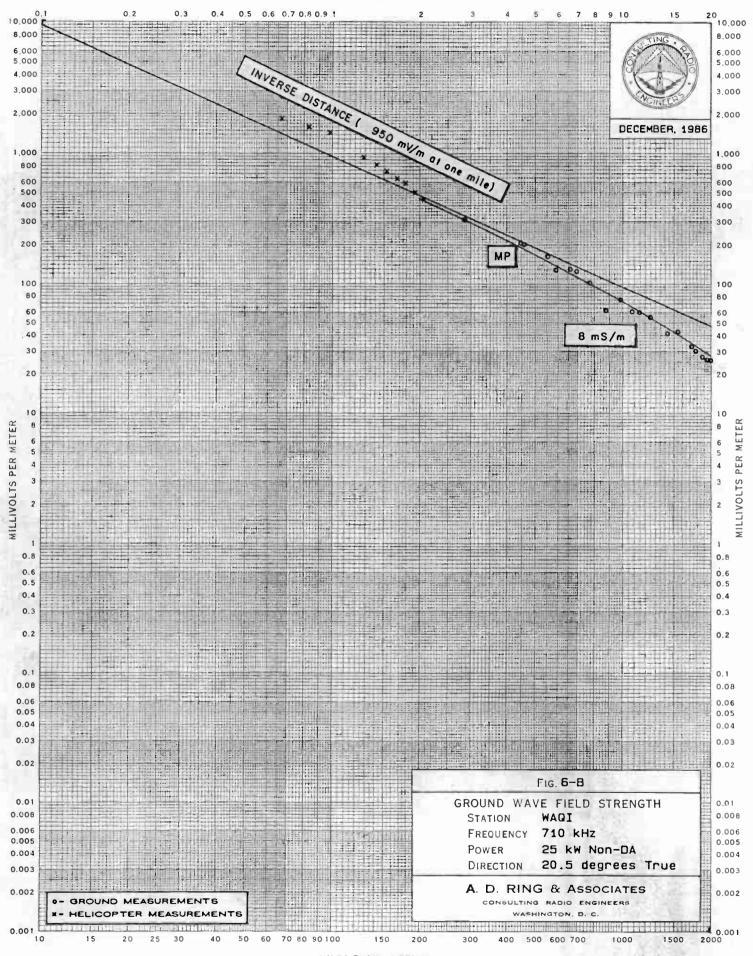
Nondirectional Analyzed Field Strength (mV/m): Directional Analyzed Field Strength (mV/m):

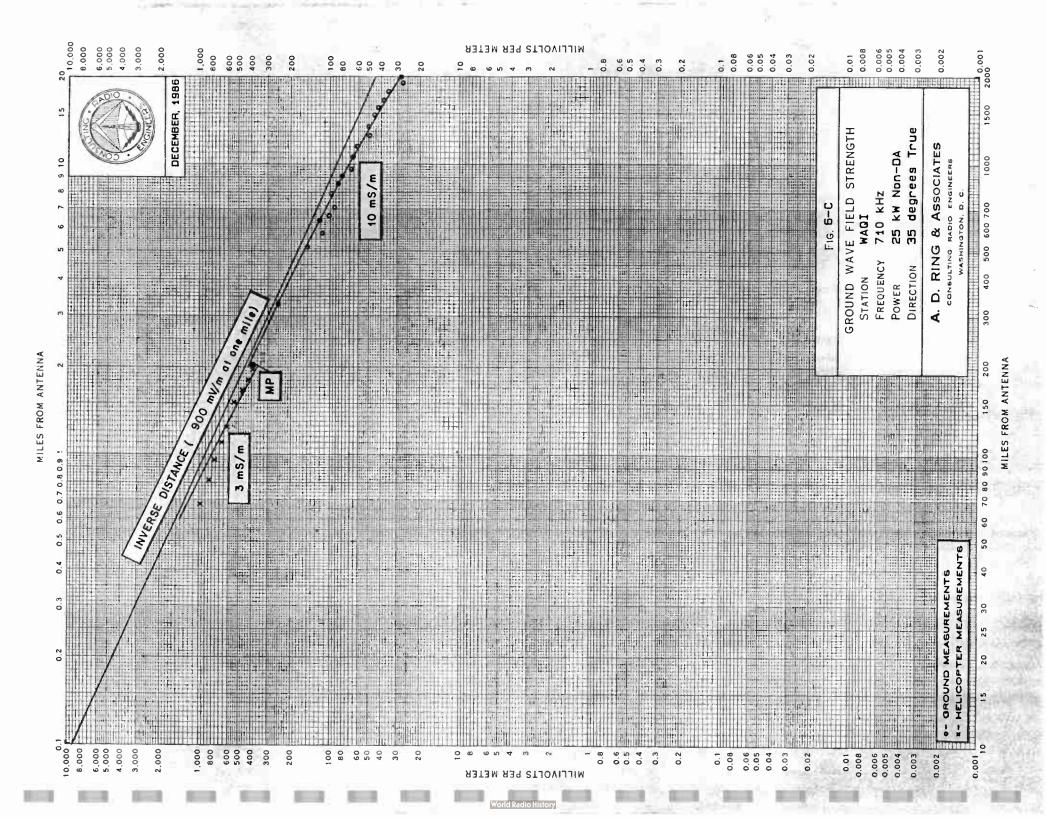
Nondirectional measurements taken December 1, 1986 Directional measurements taken November 23, 1986

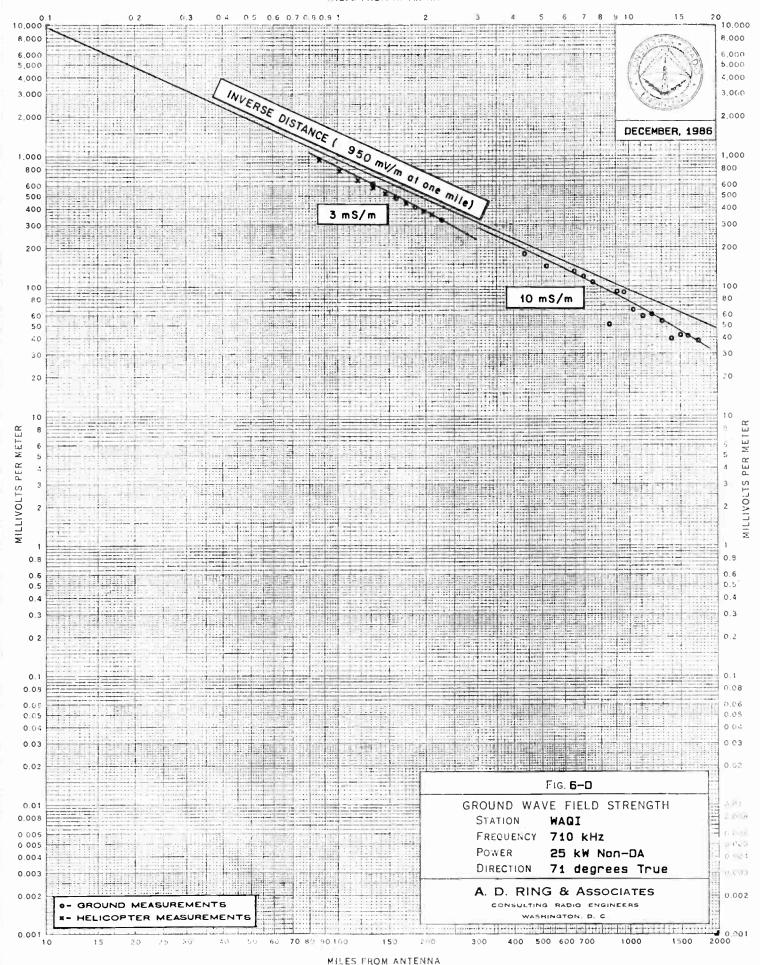
- # Directional measurements taken November 24, 1986
 ## Directional measurements taken November 30, 1986 Nondirectional airborne measurements taken 1145-1203 EST on December 4, 1986 Directional airborne measurements taken 1330-1402 EST on
- December 3, 1986 Airborne measurement
- ** Airborne measurement above ground point, not included in average

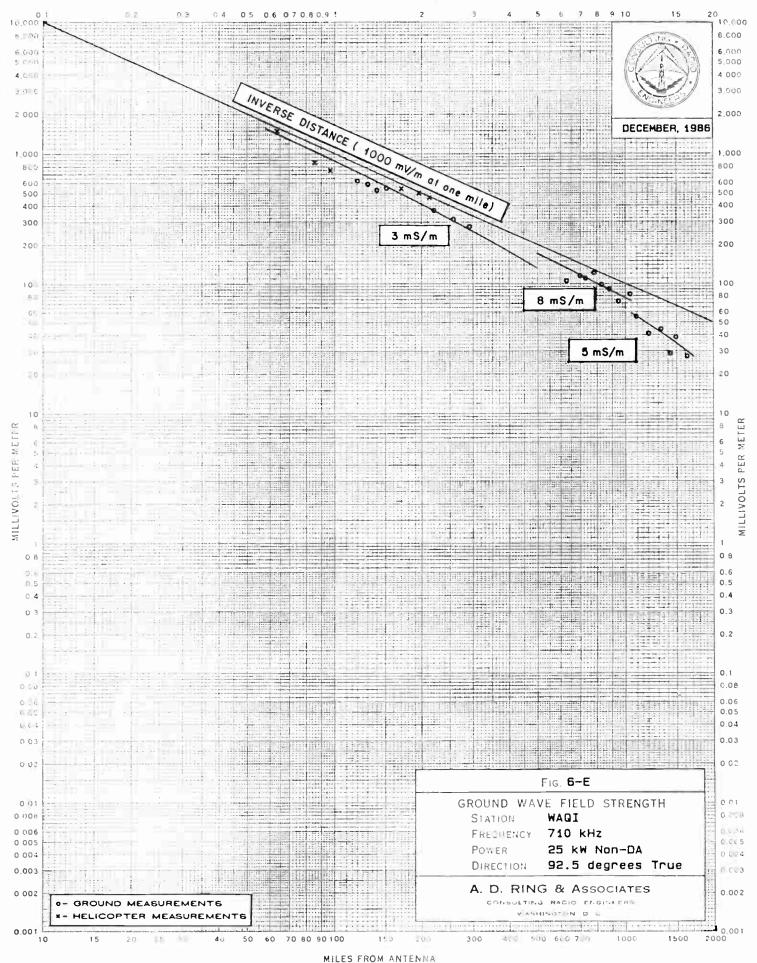
MILES FROM ANTENNA

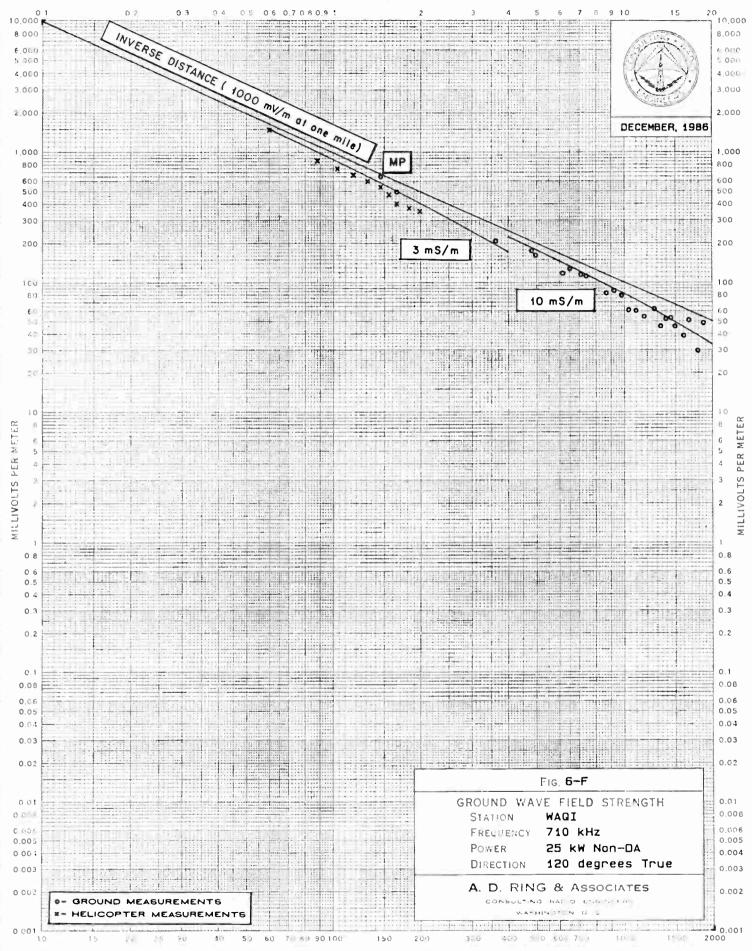
dia History

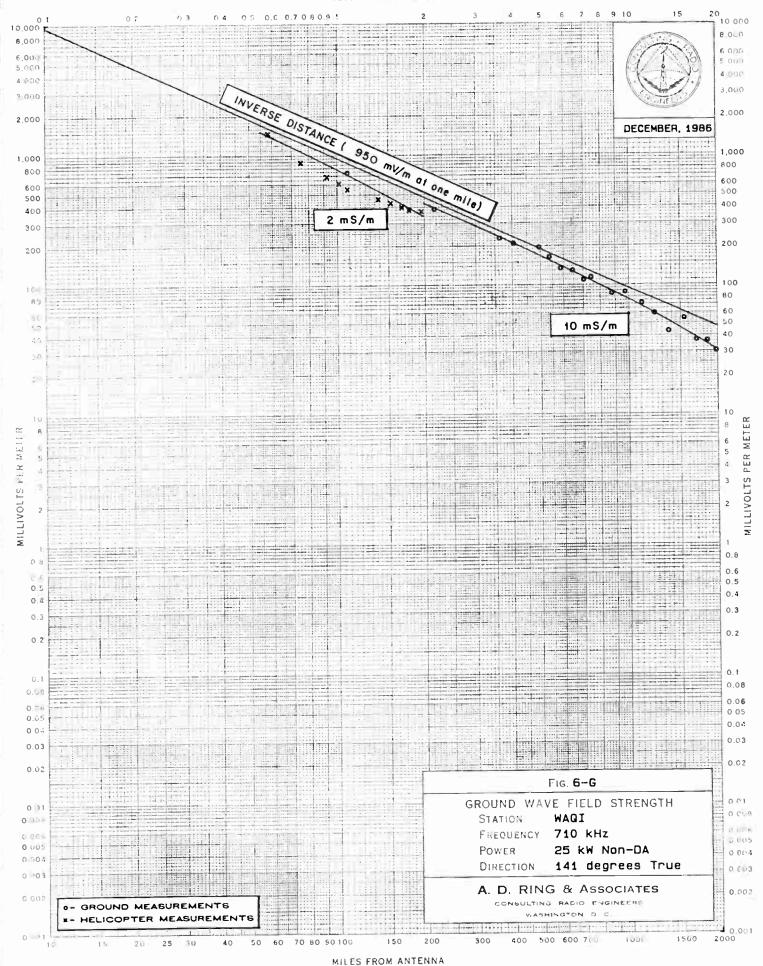


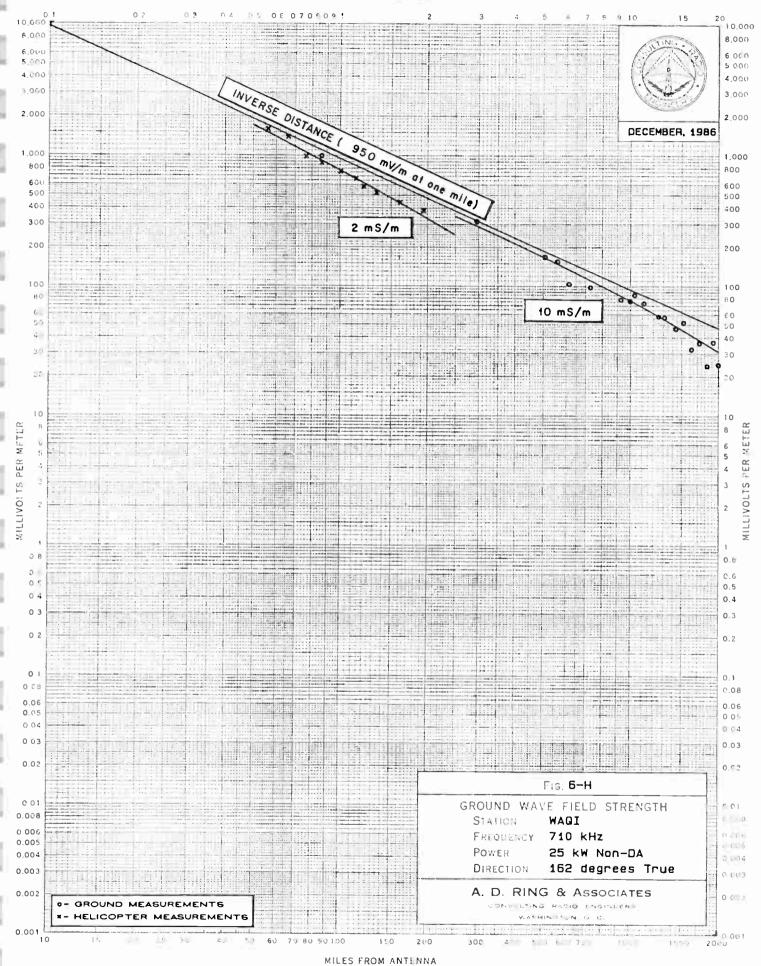


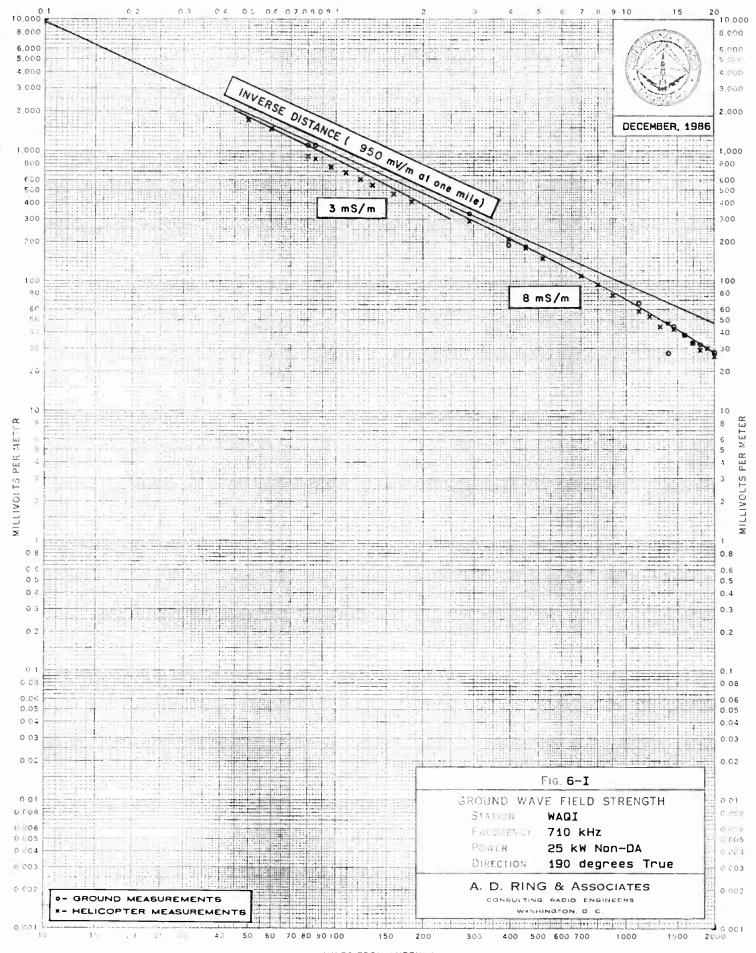


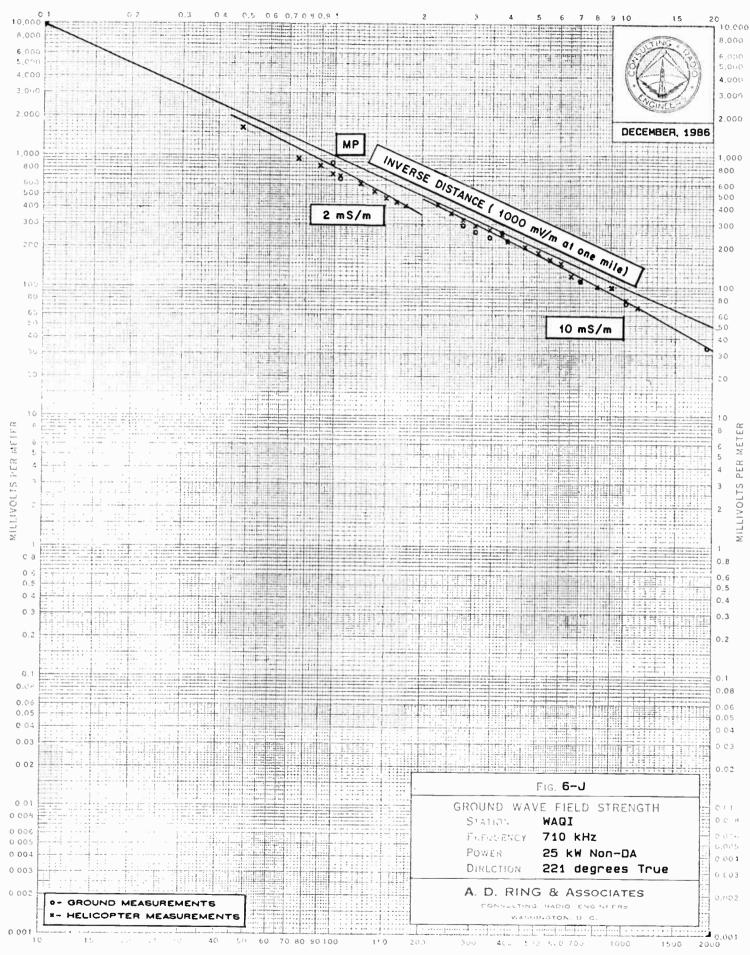


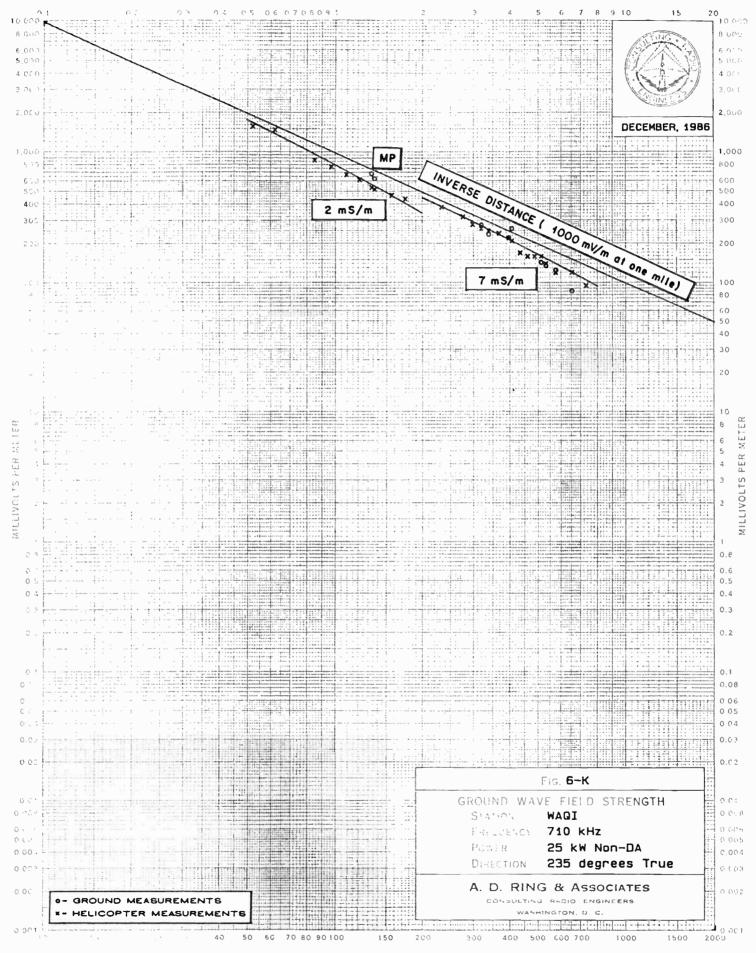


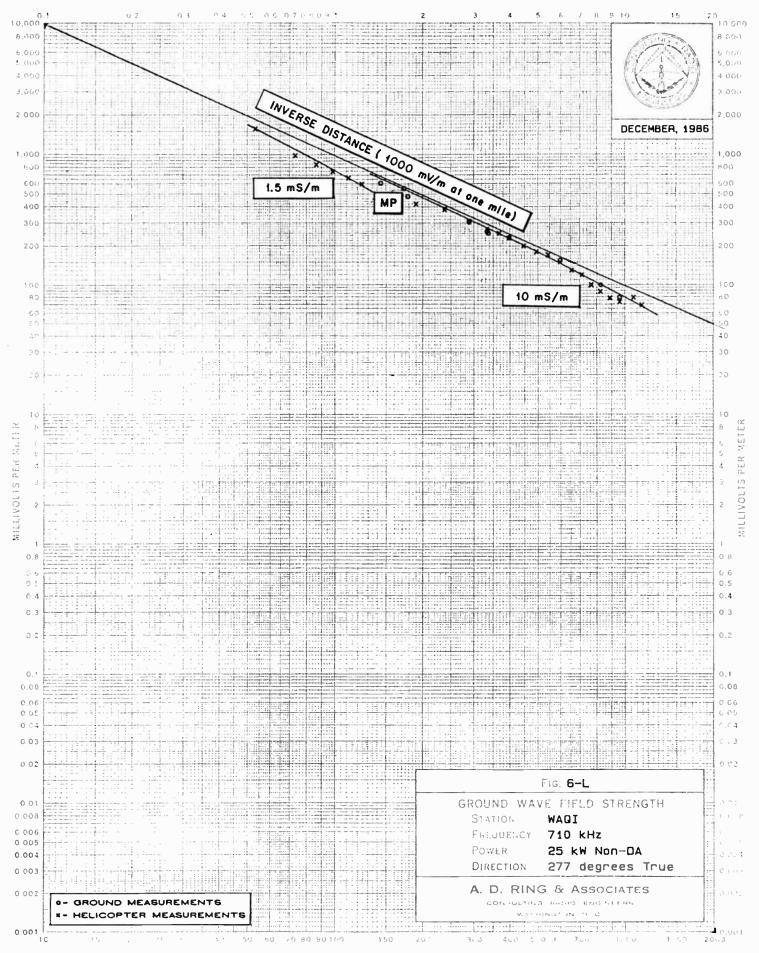


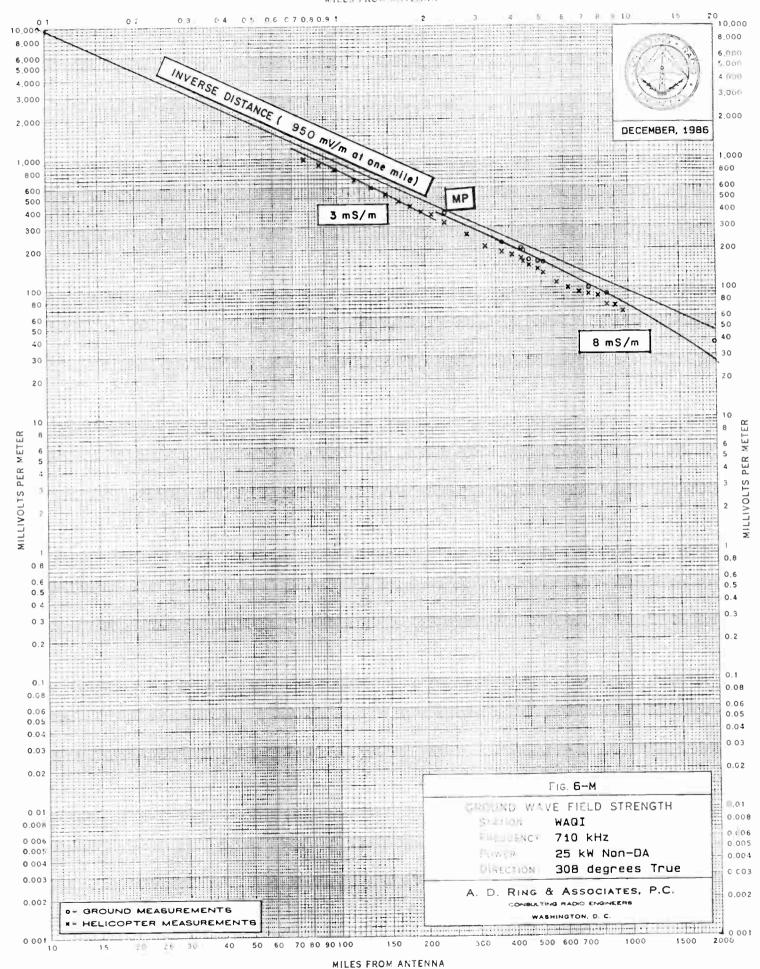


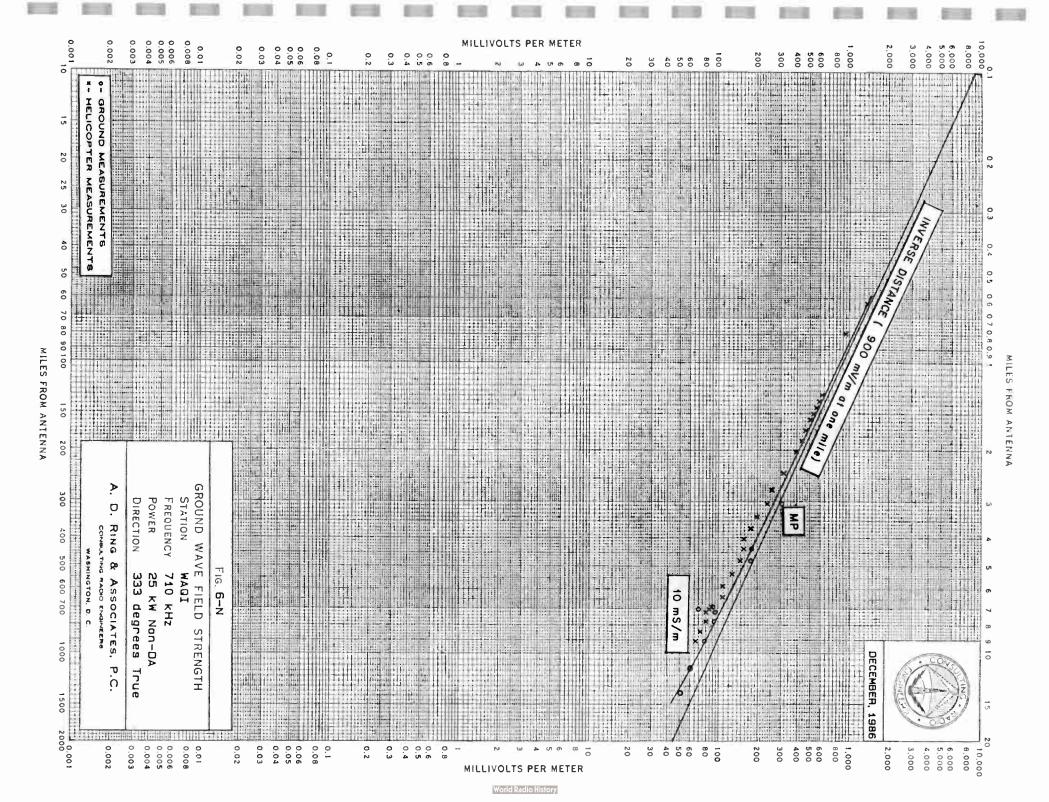


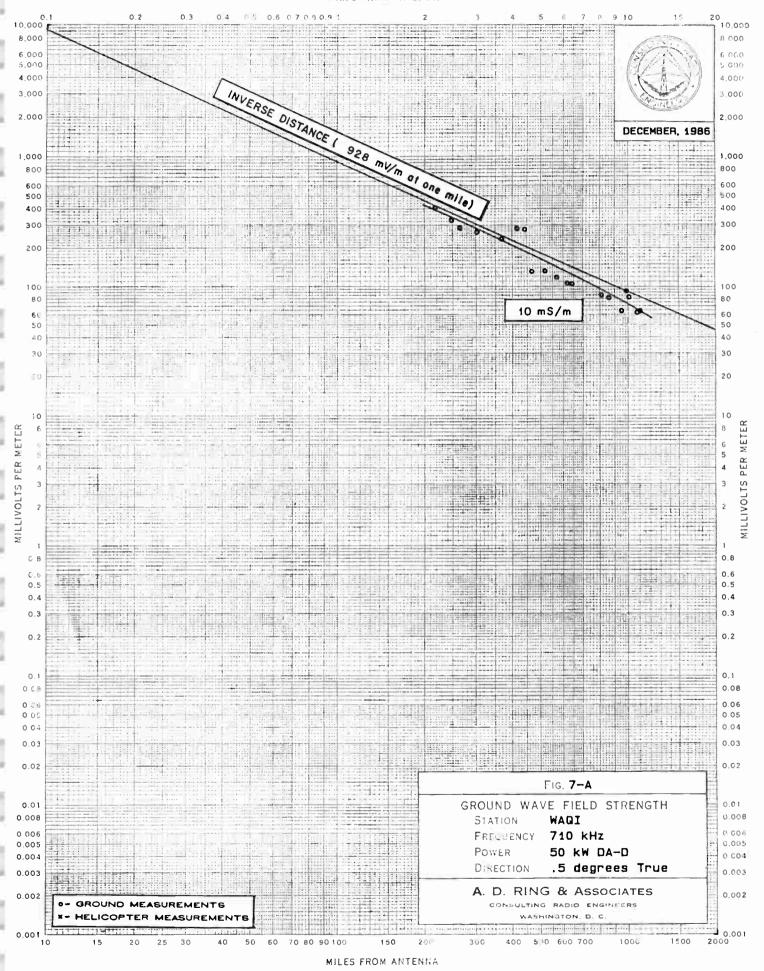


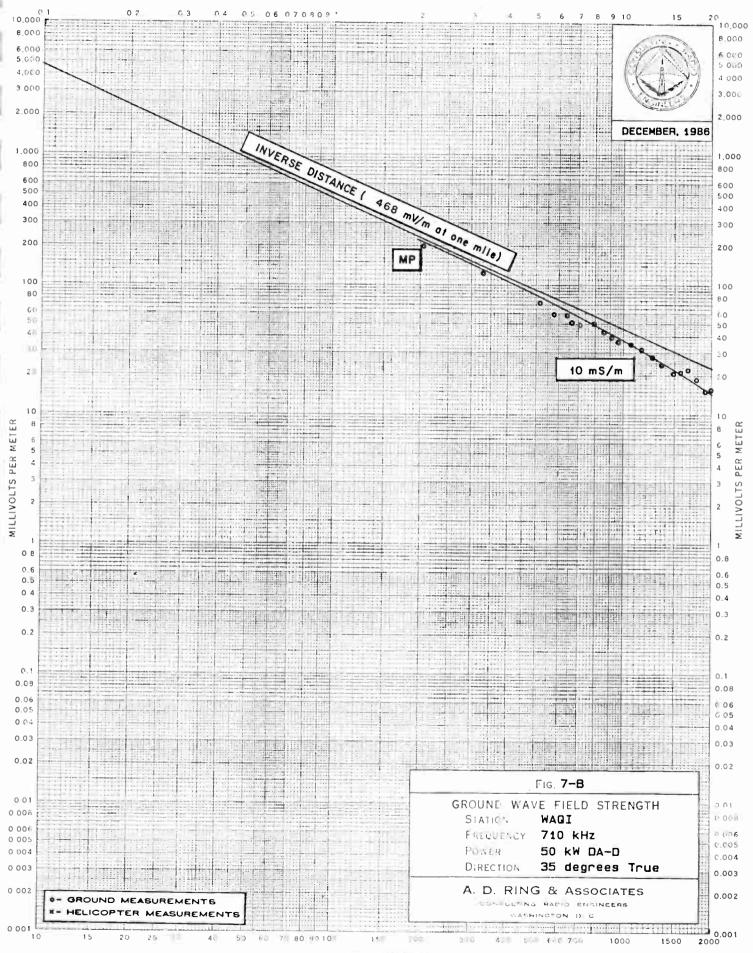


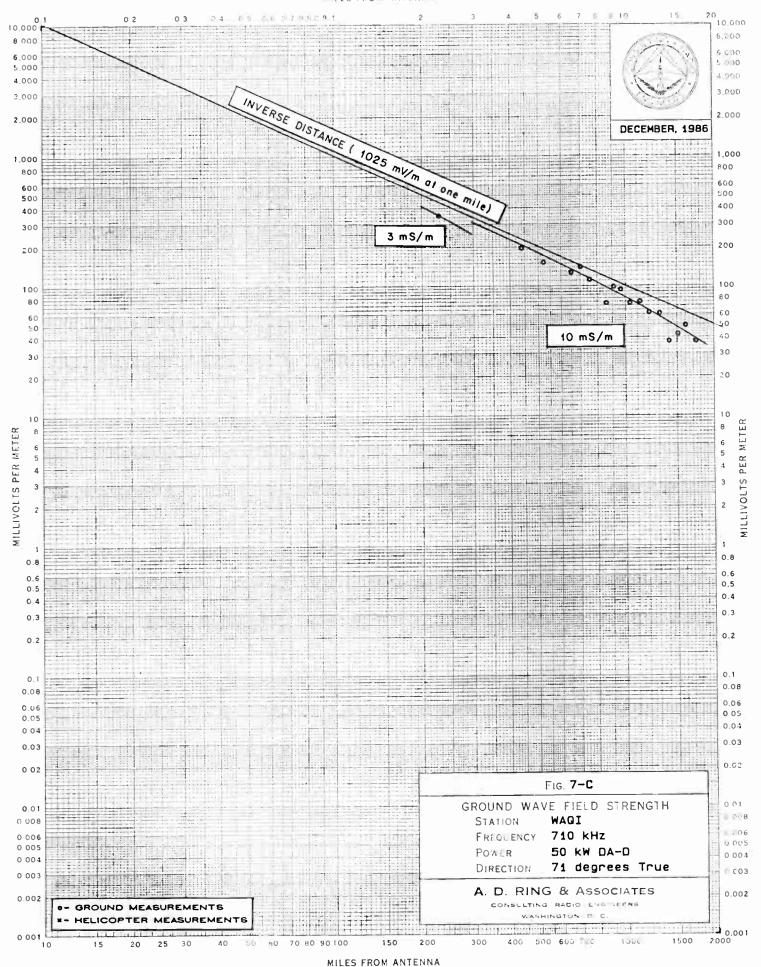


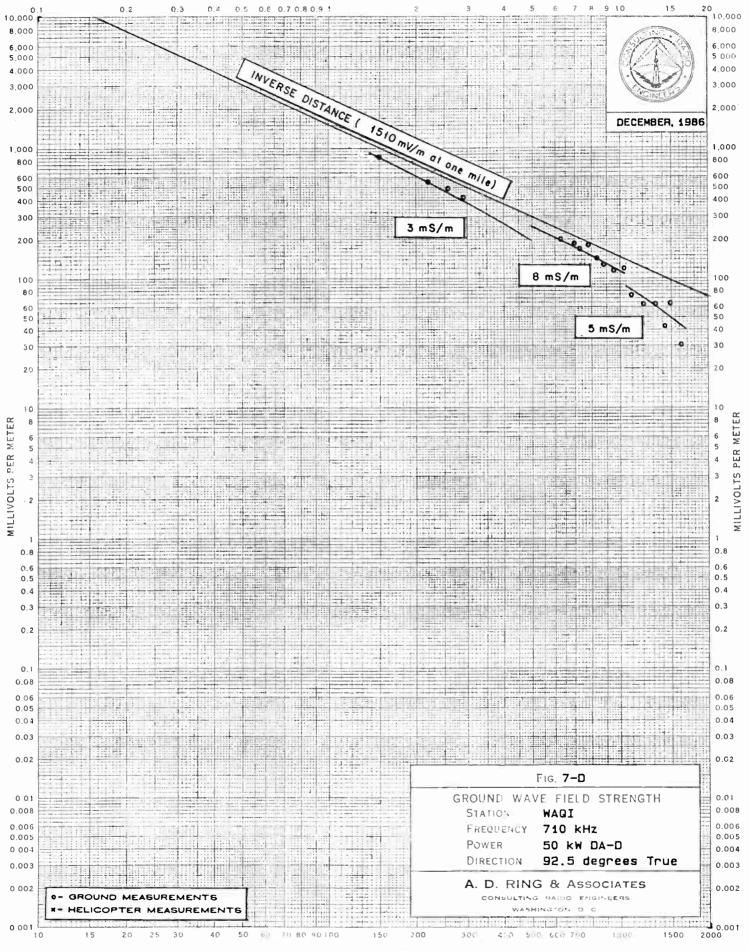


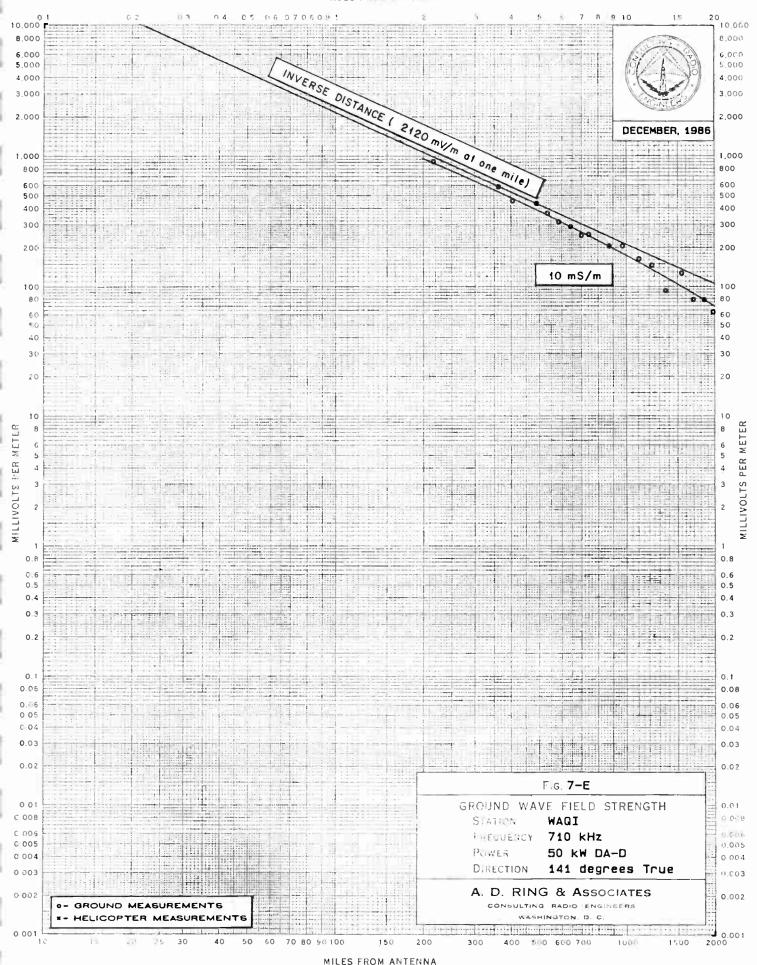


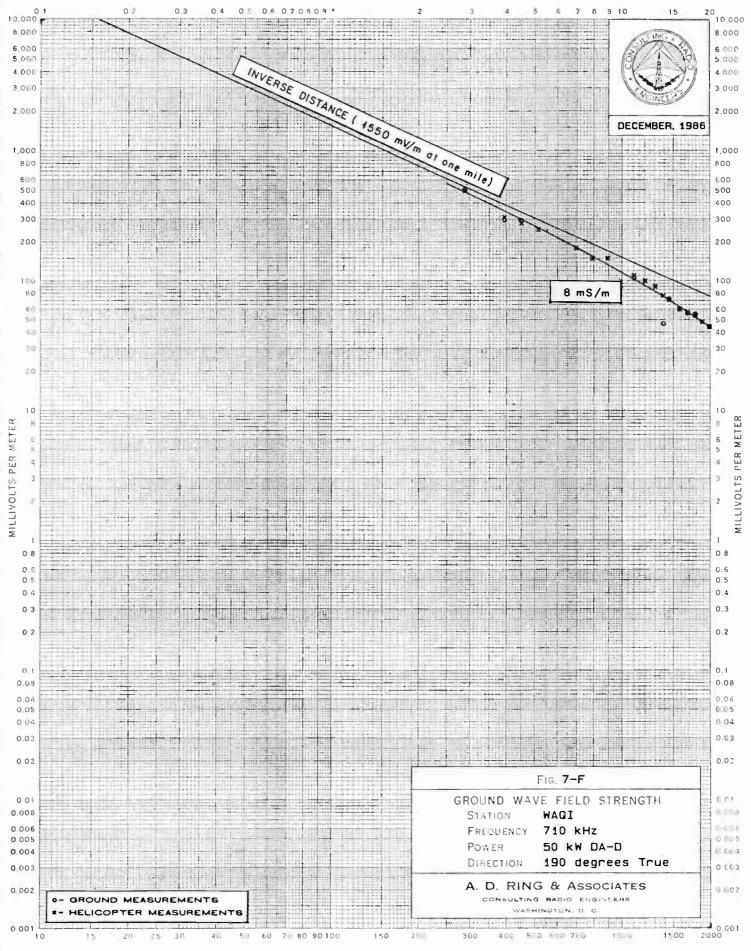


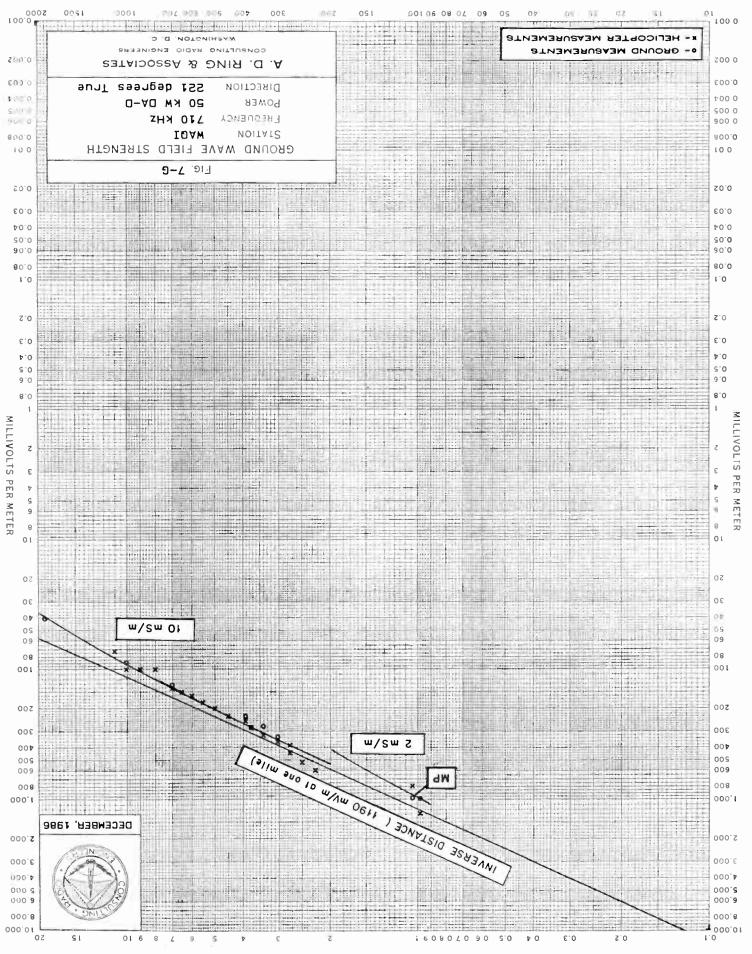


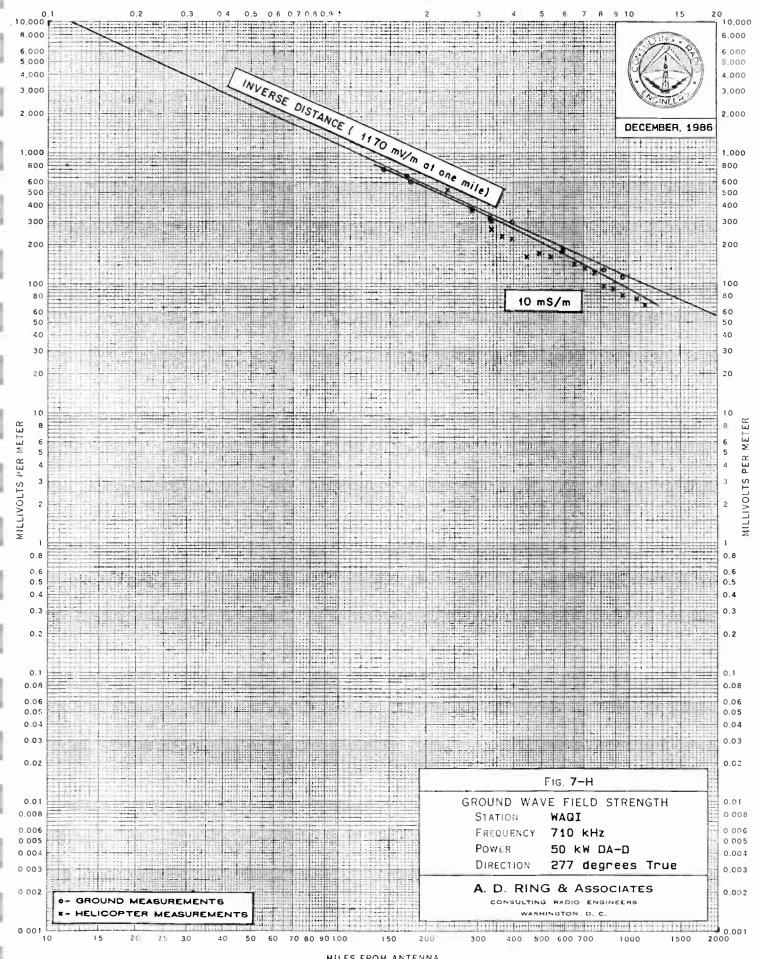






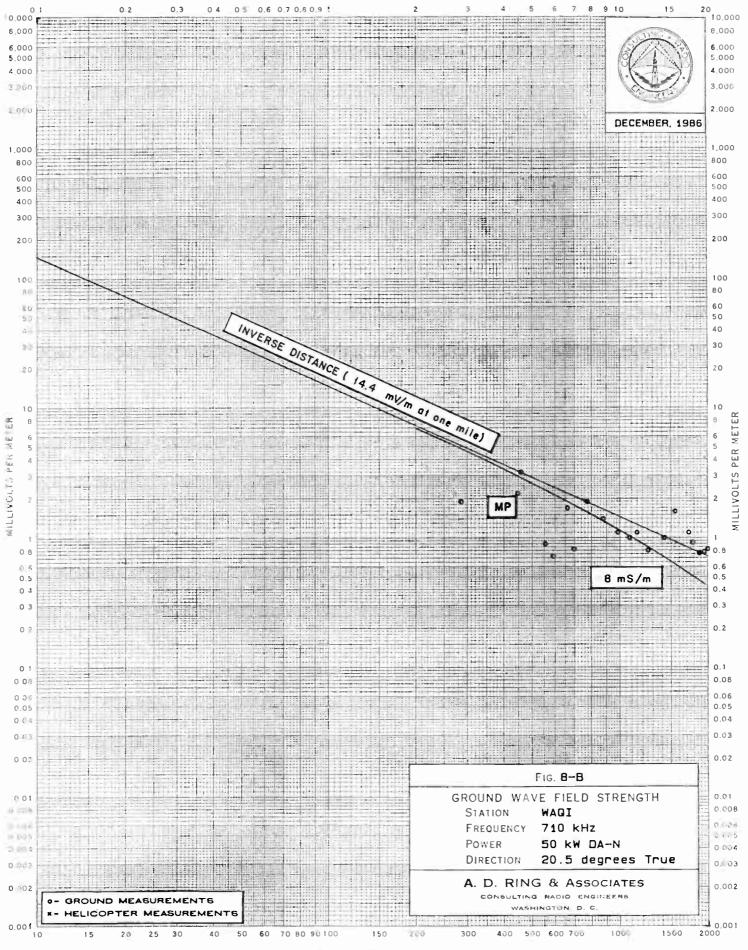


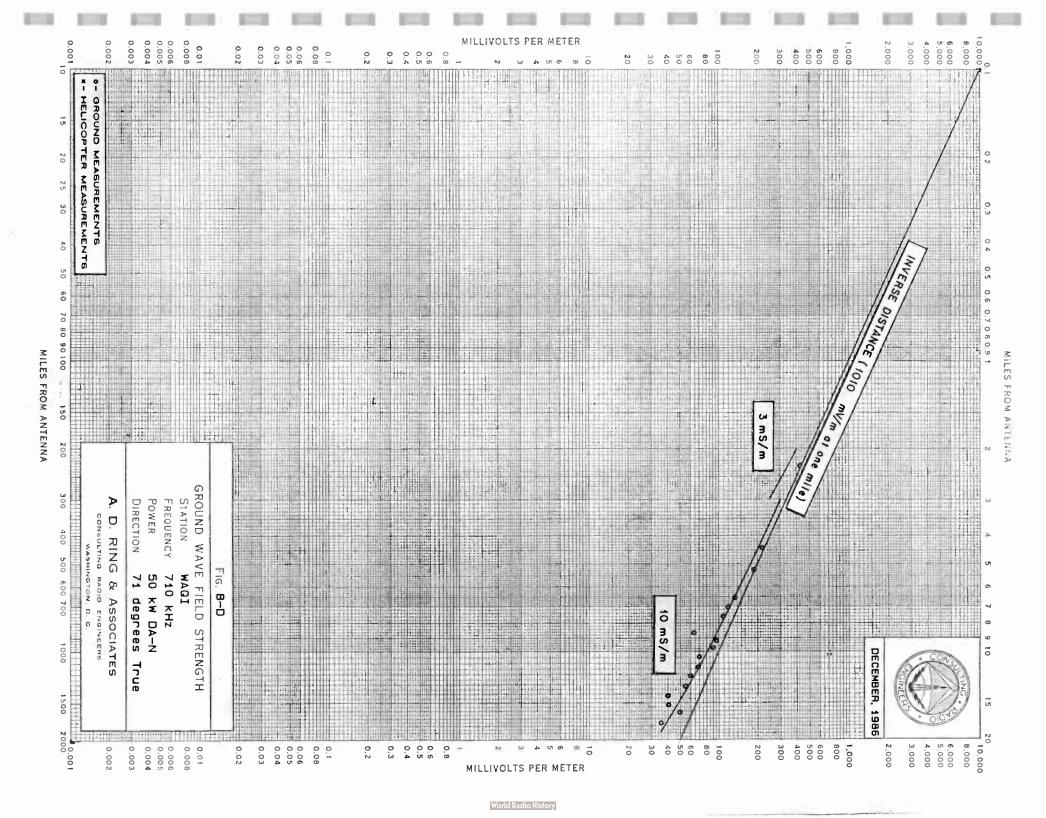




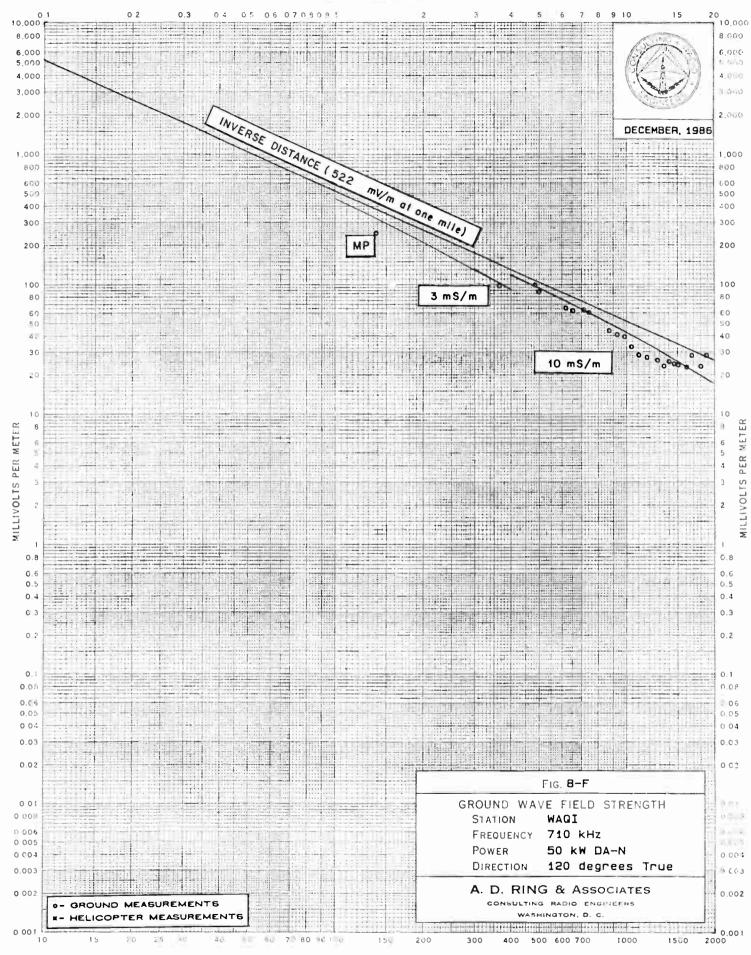
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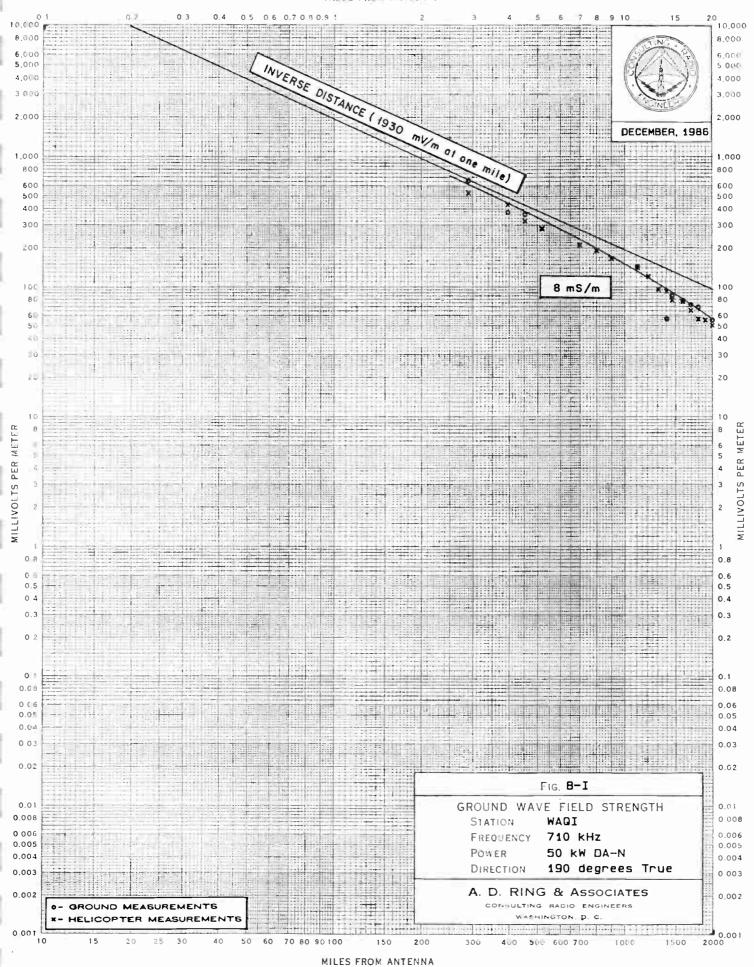
dio History



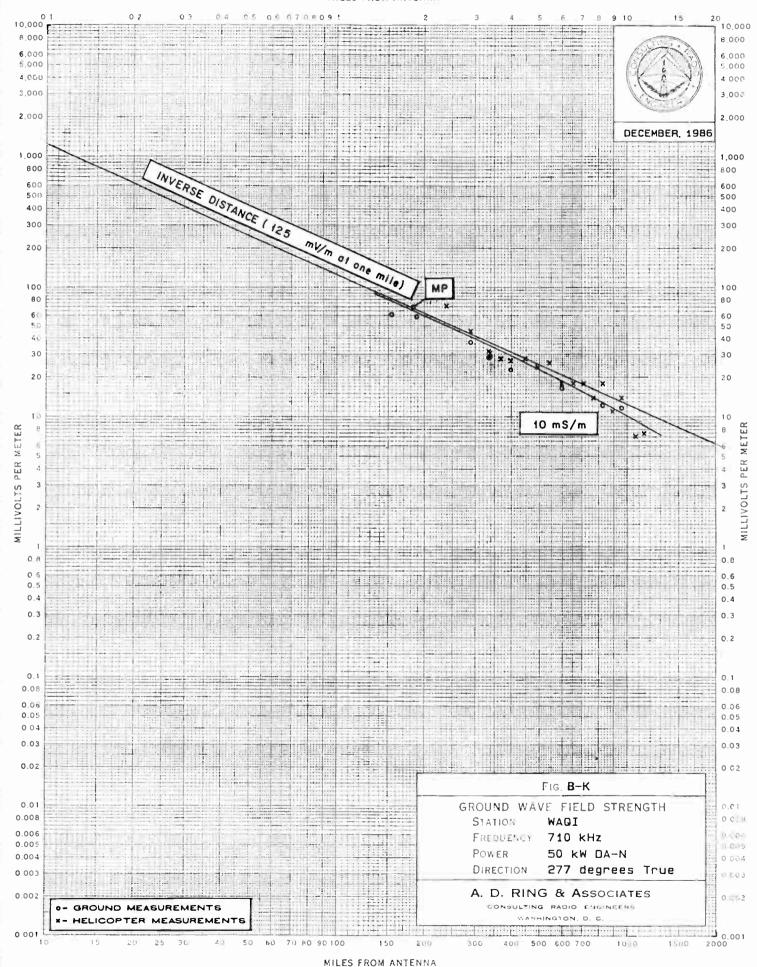


10 0 10 1

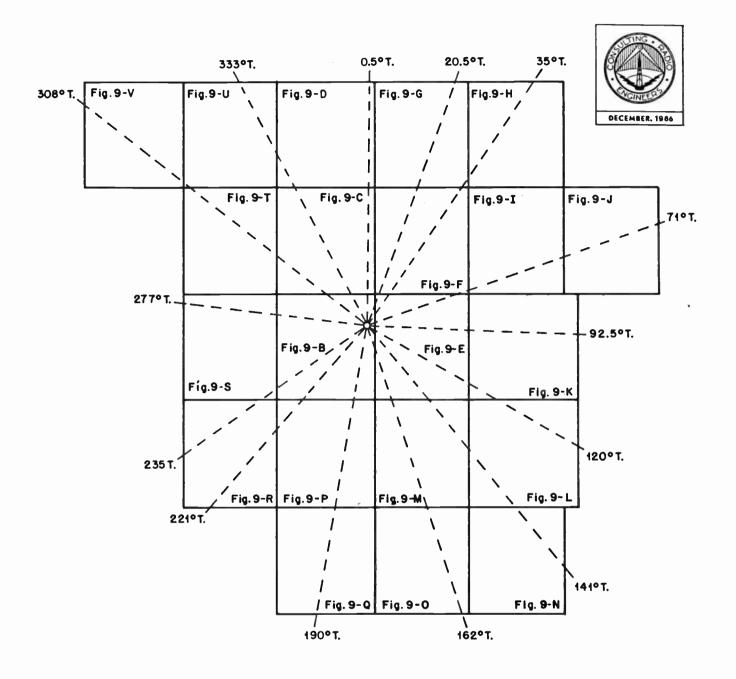




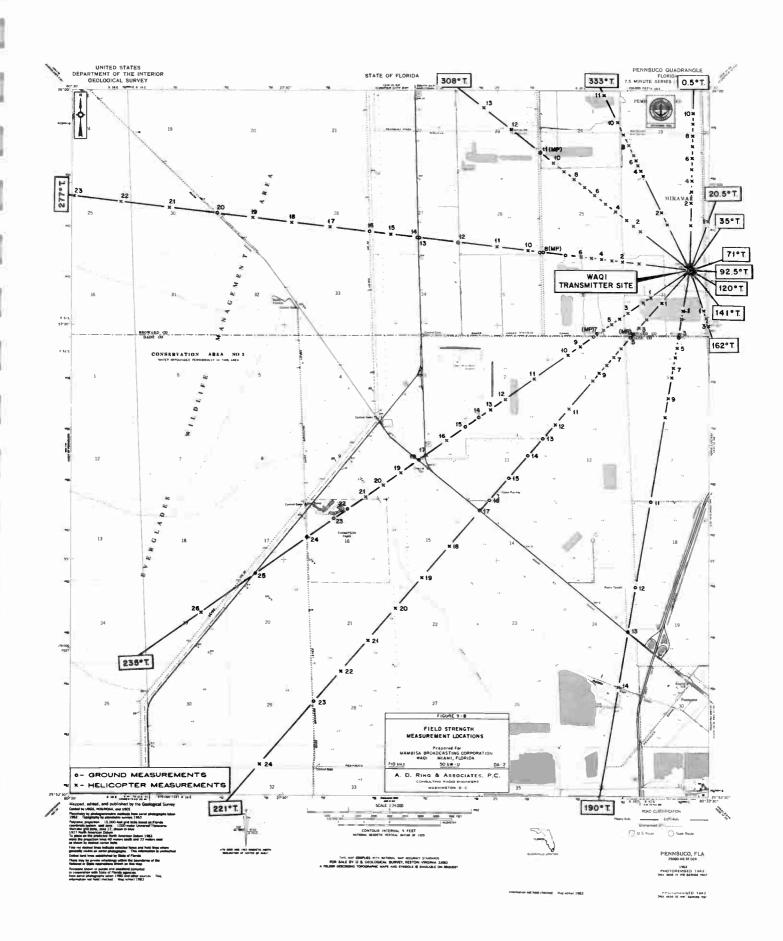
D 1: 11: 1

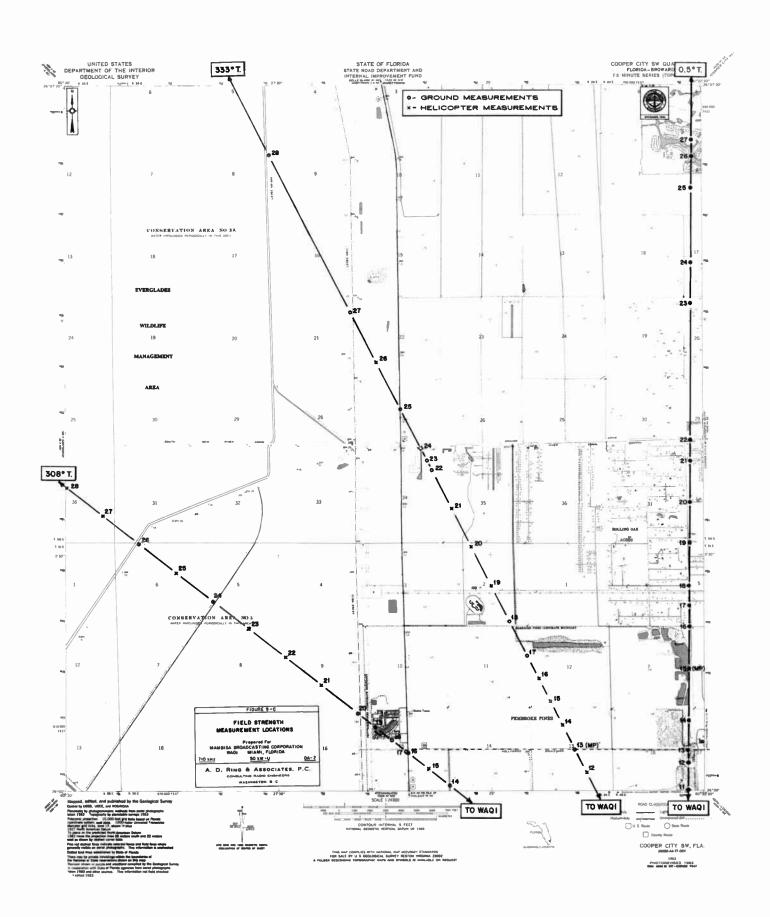


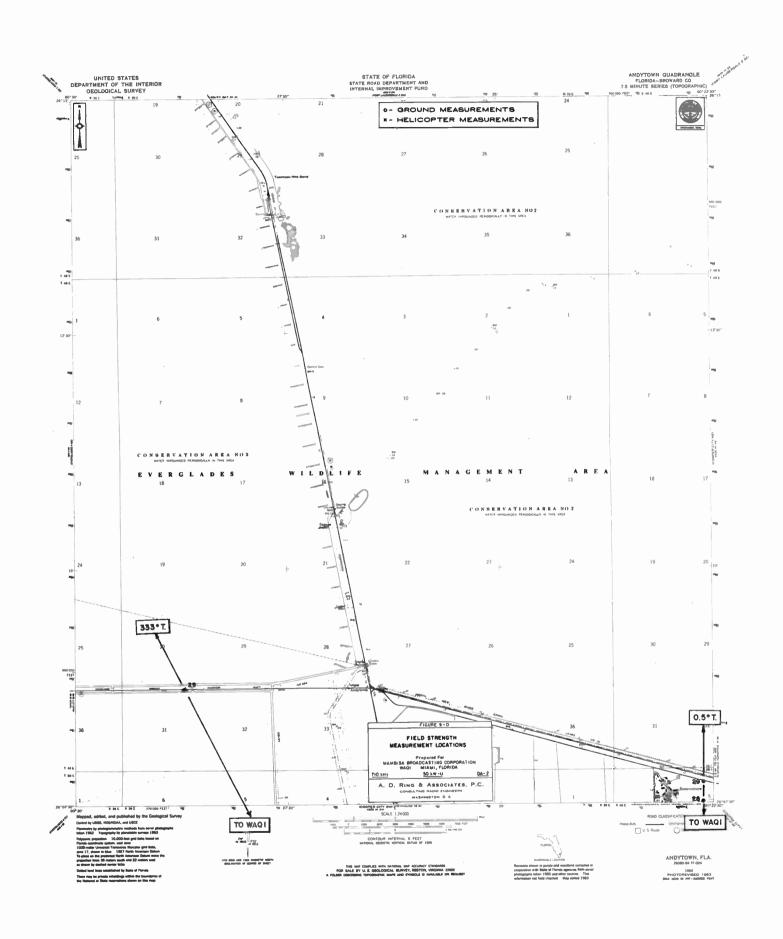
ANDREA MOGE STILL

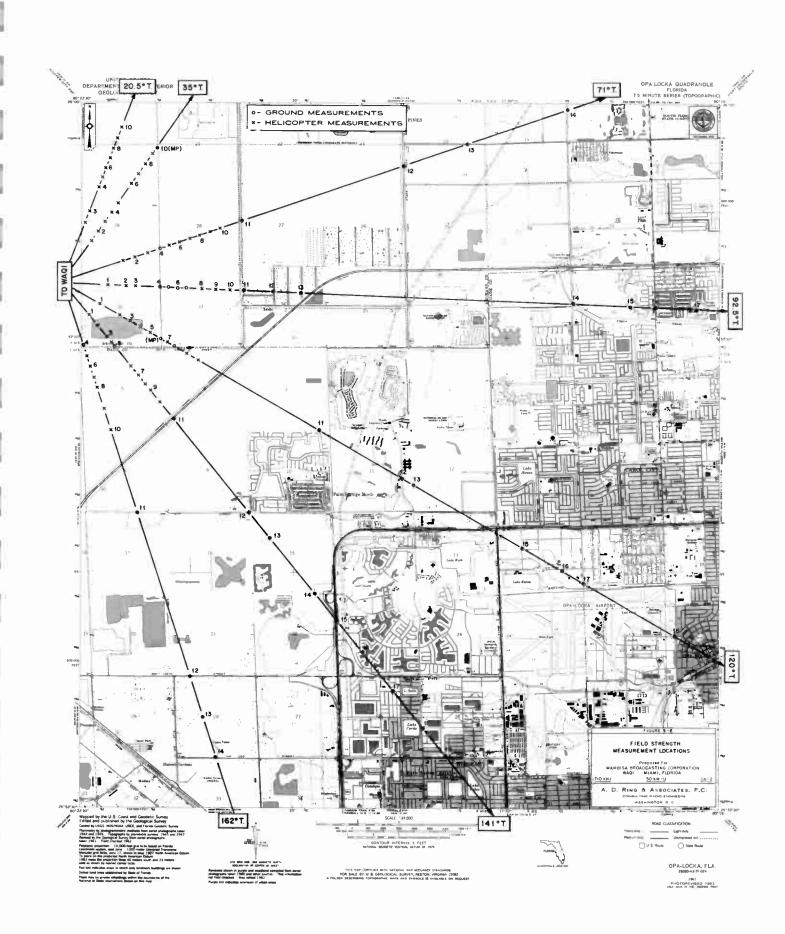


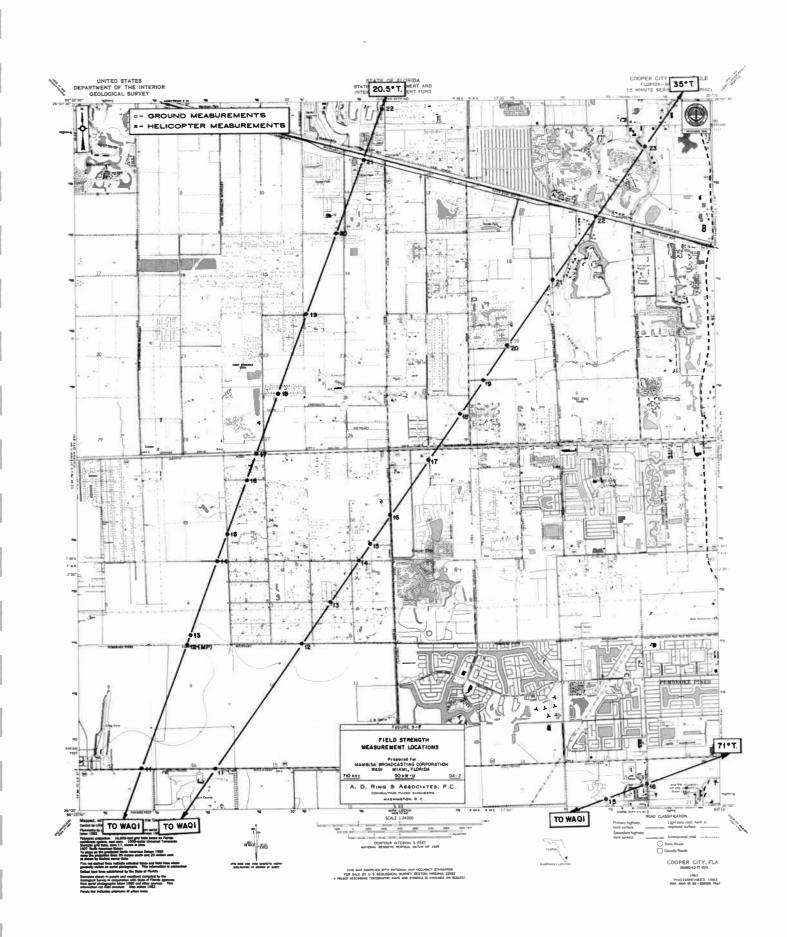
INDEX TO MEASURING LOCATIONS Prepared For MAMBISA BROADCASTING CORPORATION WAQI MIAMI, FLORIDA 710 kHz 50 kW-U DA-2 A. D. RING & ASSOCIATES, P.C. CONSULTING RADIO ENGINEERS WASHINGTON, D. C.

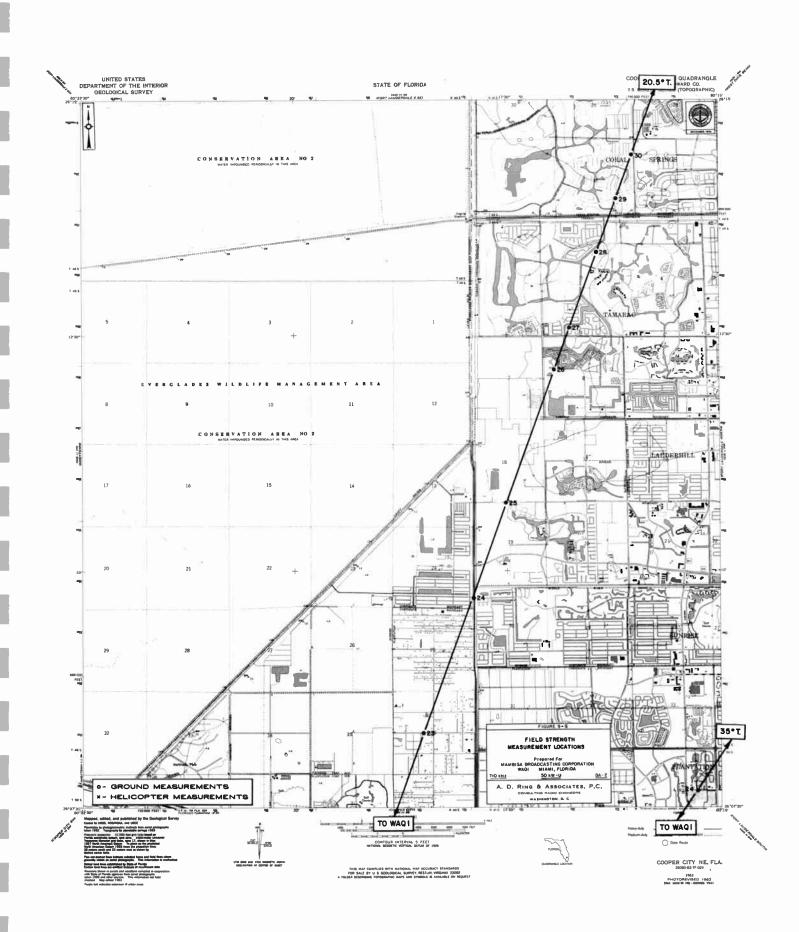


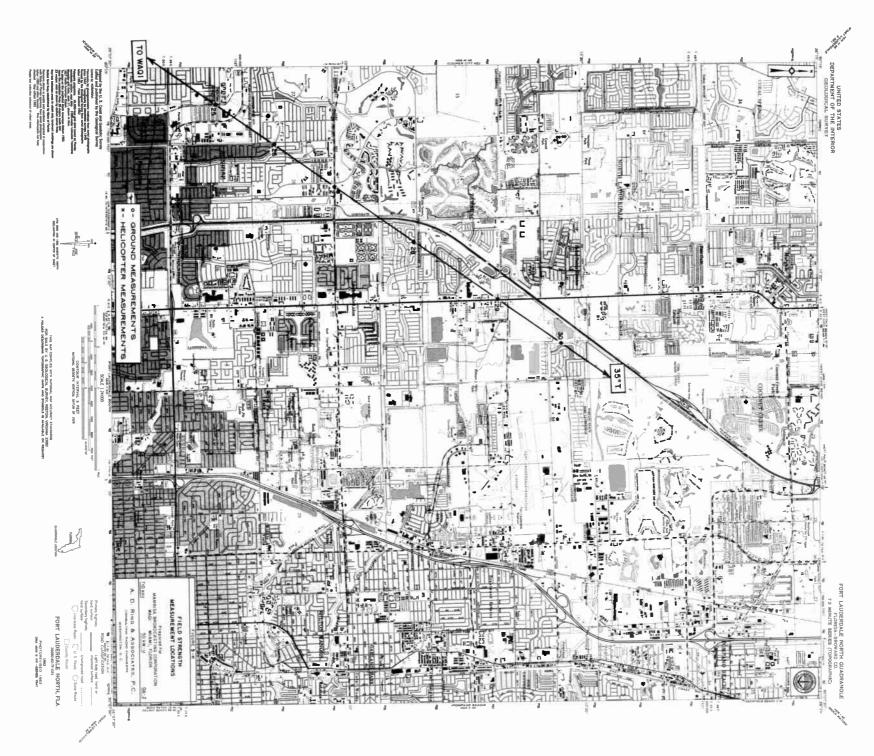




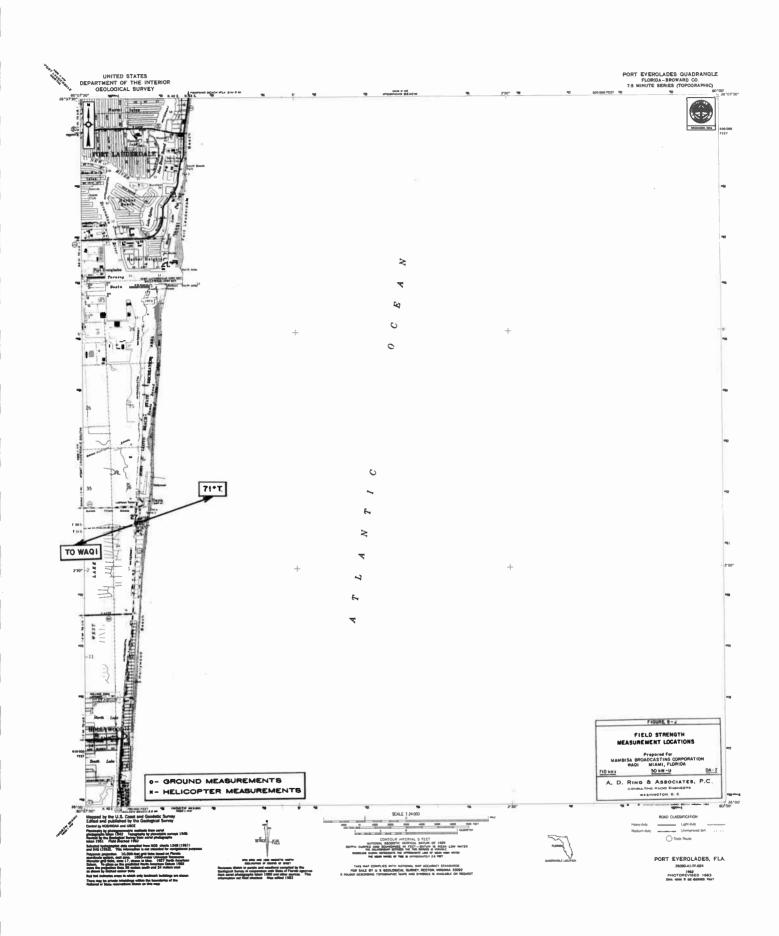


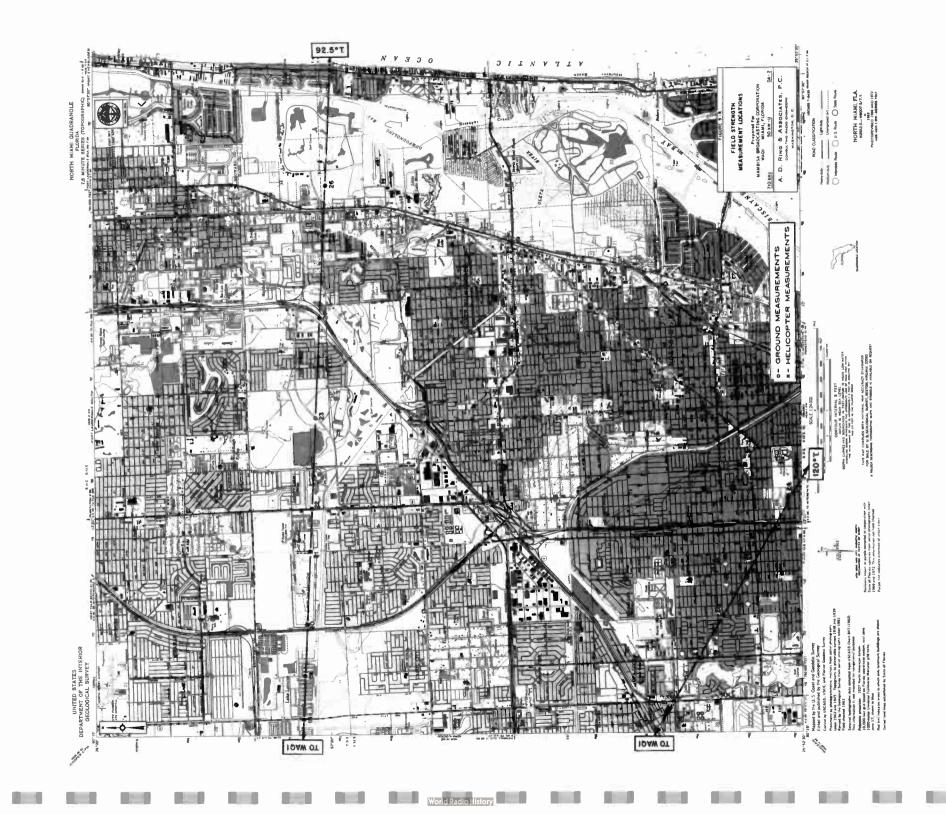


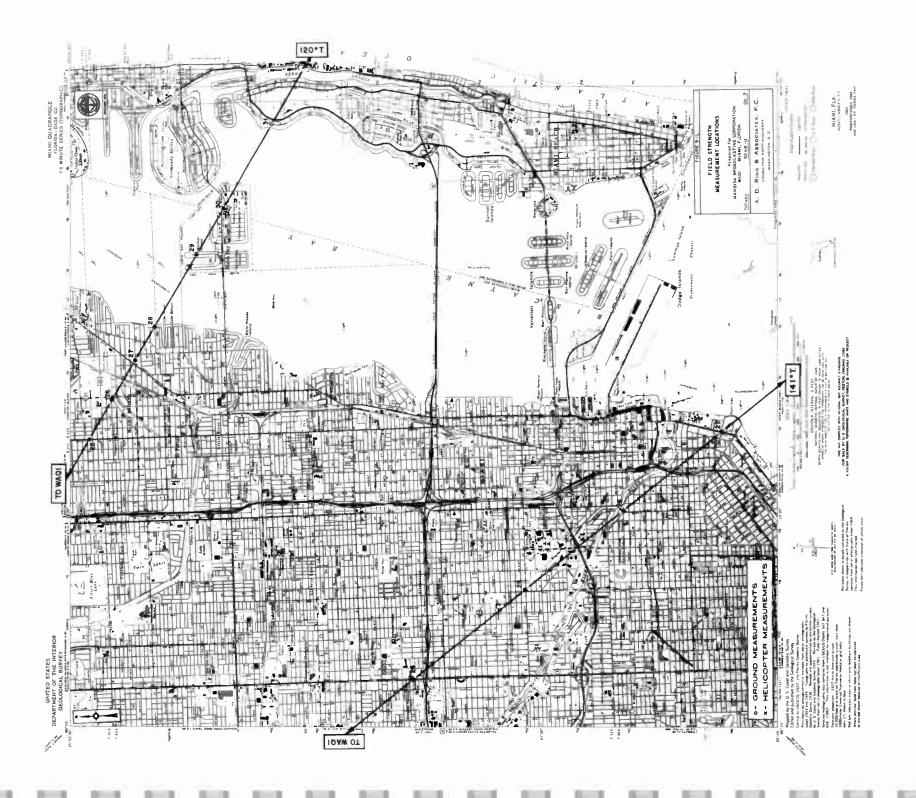


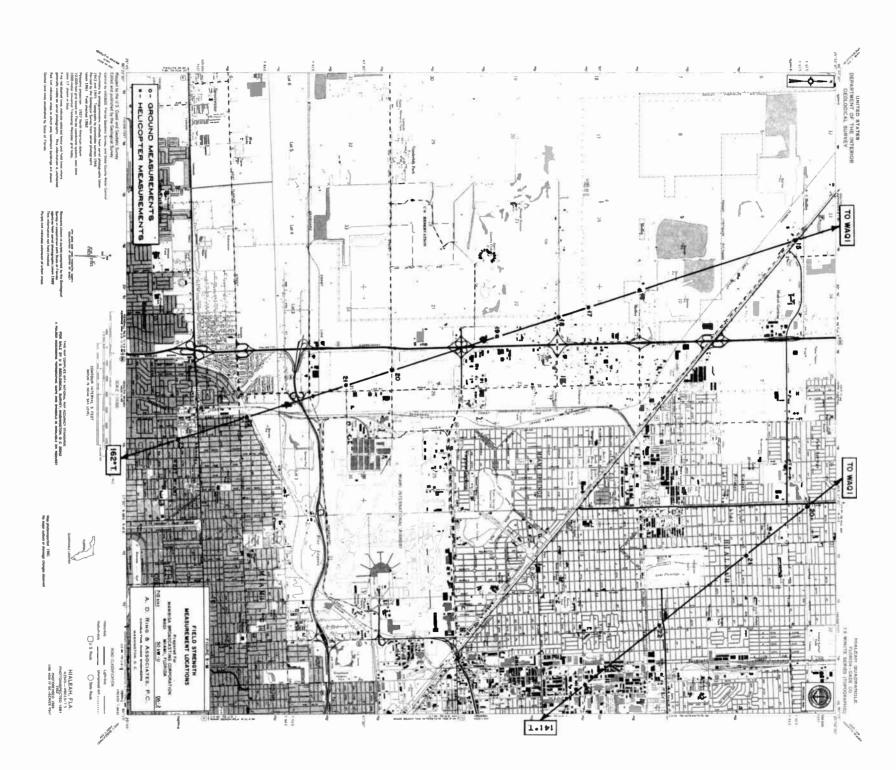


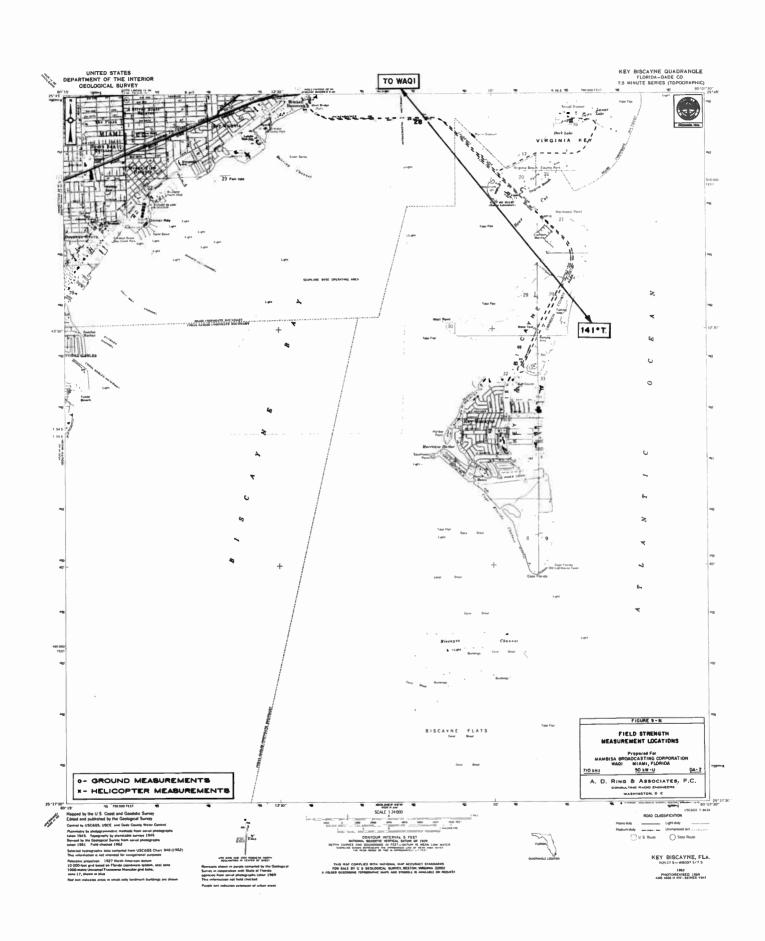






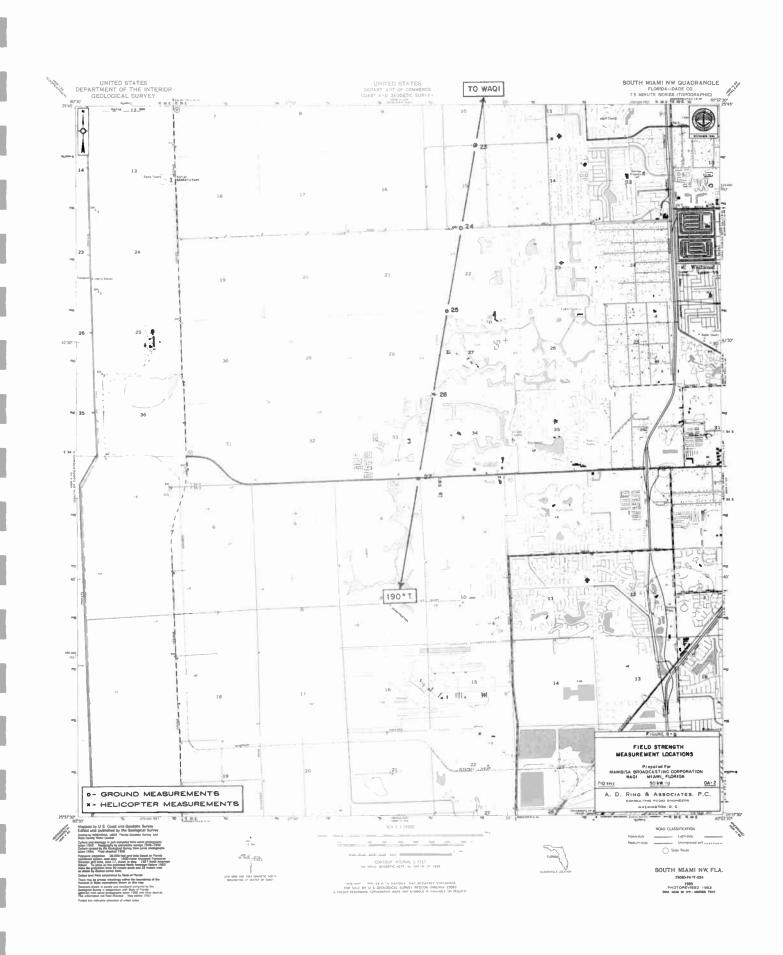


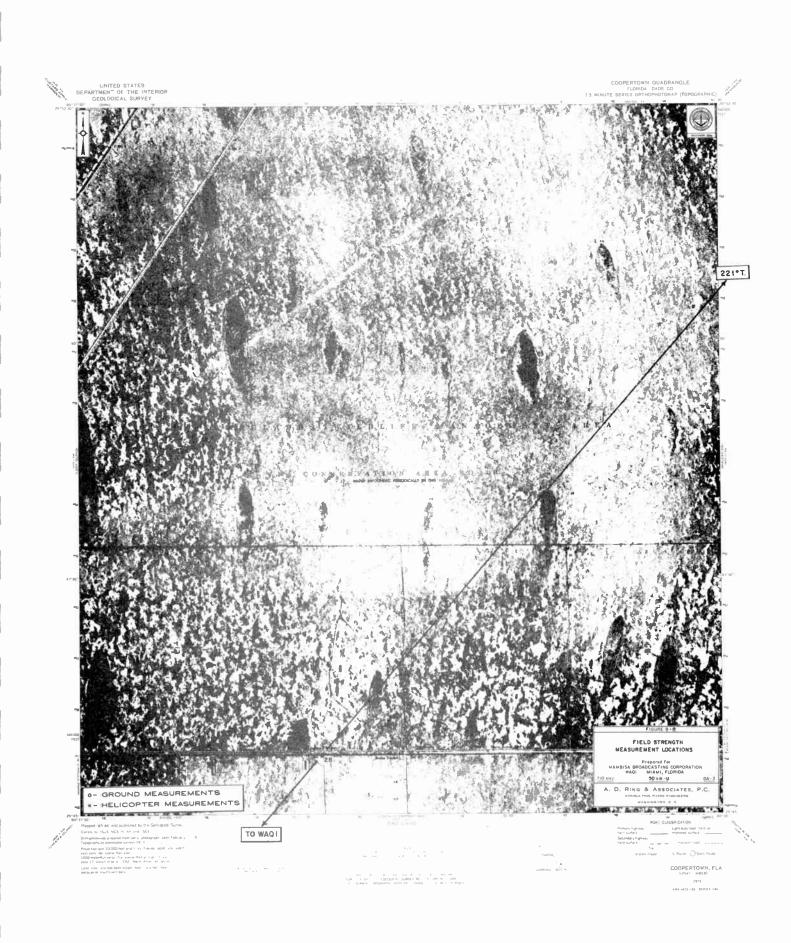


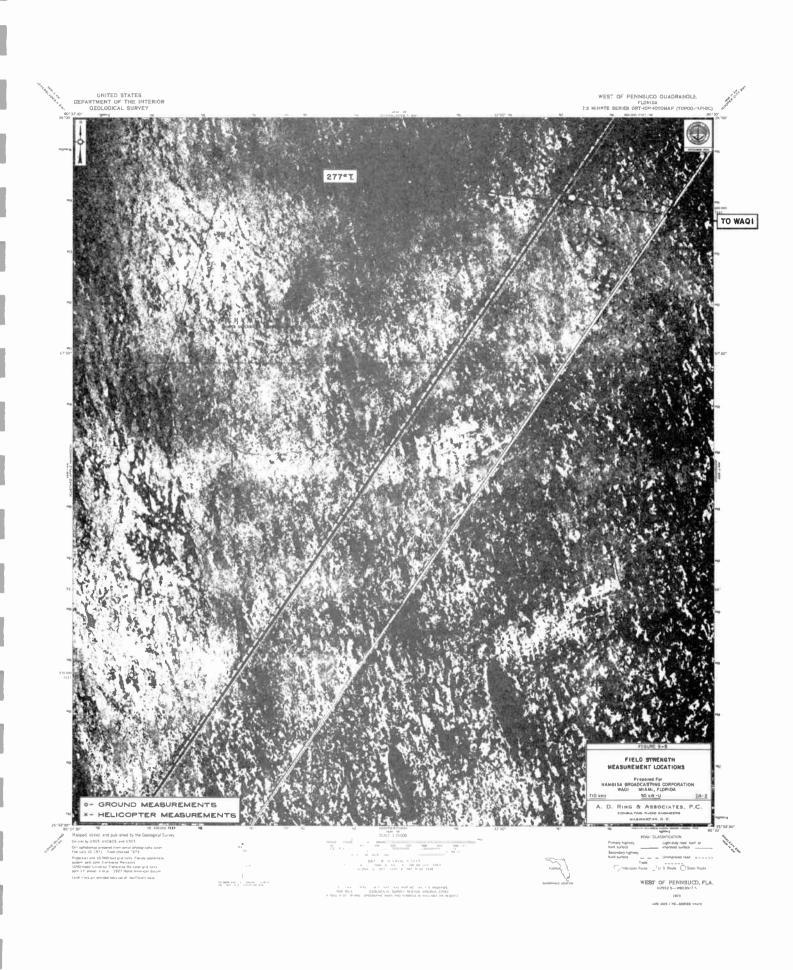


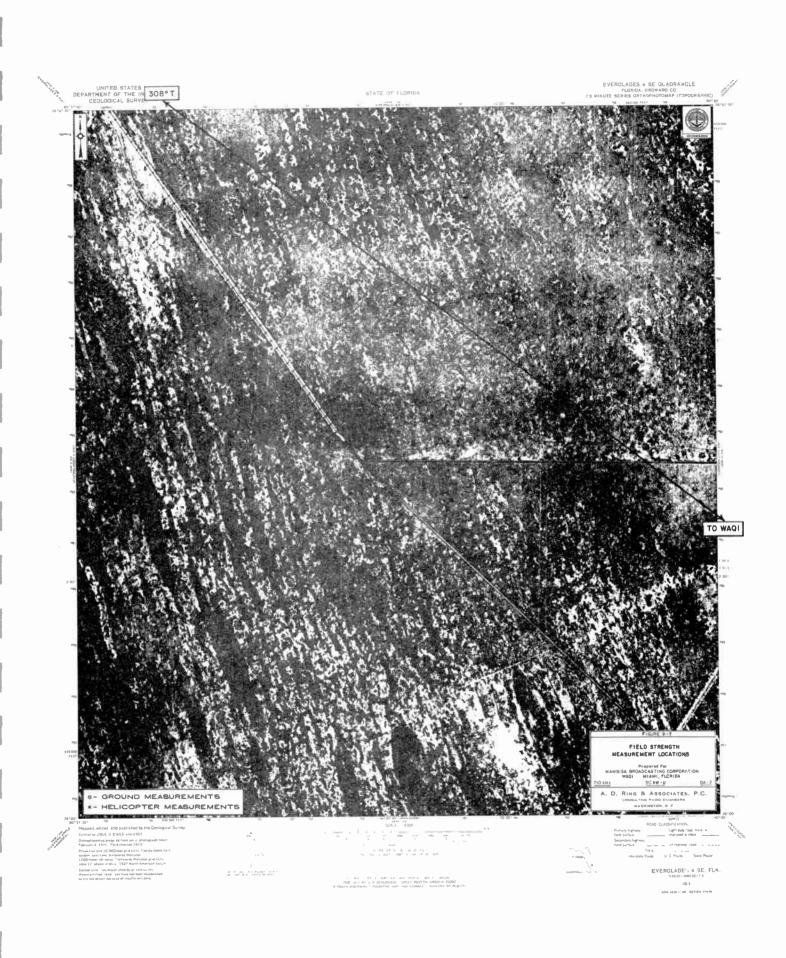




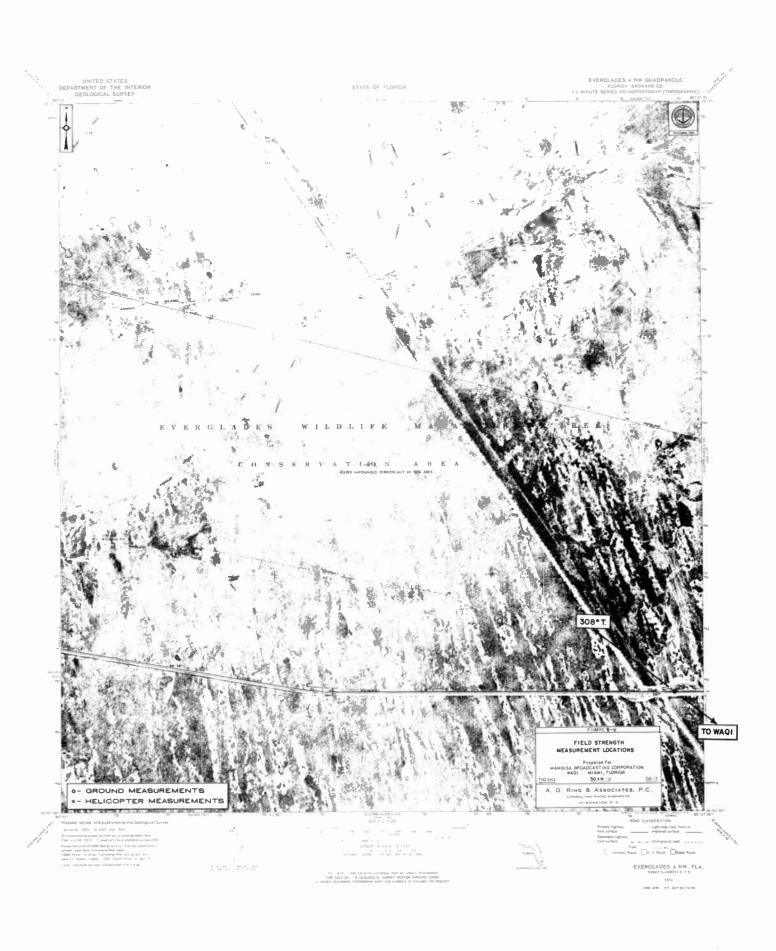






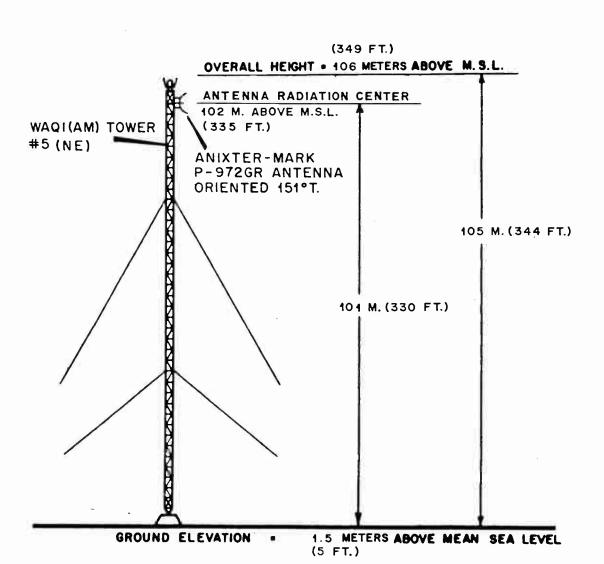






NORTH LATITUDE : 25° 58' 07" WEST LONGITUDE : 80° 22' 44"





NOT DRAWN TO SCALE

FIGURE 10

STL RECEIVE ANTENNA

PREPARED FOR
MAMBISA BROADCASTING CORPORATION
WAQI MIAMI, FLORIDA

A. D. RING & ASSOCIATES, P.C. CONSULTING RADIO ENGINEERS

WASHINGTON, D. C.

APPENDIX i

DETUNING OF UNUSED TOWERS

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

It is well known that unused towers can act as parasitic reradiators, distorting the directional antenna pattern produced by driven radiators. This is especially true for directional arrays exhibiting extremely high radiation suppression, such as the WAQI nighttime antenna system. If unused towers are properly detuned, they will have little impact, if any, on the radiation pattern produced.

Tower #7(NW) is unused during nighttime operation at WAQI. The tower was detuned by adjusting a terminating inductive reactance to produce a current distribution which results in approximately zero radiated field in the horizontal plane. Figure i-1 illustrates the current distribution obtained. The data from which Figure i-1 was plotted is set forth in Table i-I. As expected, a current minimum or "crossover" occurs at approximately one-third the tower height. The current areas above and below the crossover point are approximately equal, resulting in near zero reradiated field in the horizontal plane.

Current distribution measurements were obtained by having a tower rigger ascend the tower, stopping every 10 feet to measure the current using an adapted field strength meter. The Potomac Instruments field strength meters actually measure magnetic field strength, which is directly proportional to current in the immediate vicinity of a conductor, such as a tower. The meter used was fitted with a wooden spacing block to facilitate uniform positioning of the meter with respect a tower leg at each measurement location, resulting in comparable data. The gap in the loop antenna shield was short-circuited in order to desensitize the field strength meter.

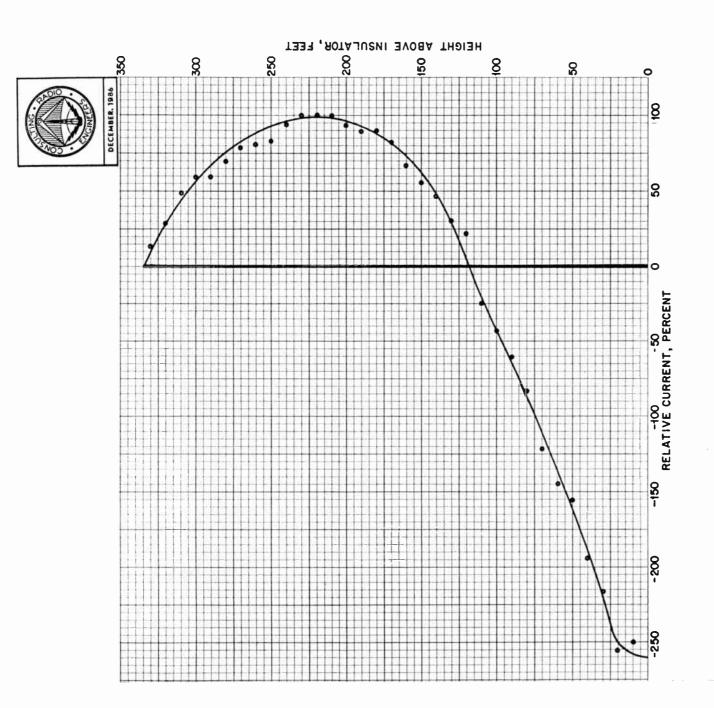
For daytime and nondirectional operational modes, detuning of unused towers was accomplished by monitoring the current at one-third the tower height and adjusting the terminating reactance for a minimum indication. Based on the data obtained for tower #7 and our experience, it is believed that this method is wholly adequate for the daytime directional and nondirectional modes.

TABLE i-I

TOWER #7(NW) CURRENT DISTRIBUTION DATA

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

Height Above	
Base Insulator	Relative Current
(feet)	(percent)
	(percent)
2.6 - 10	250
5, 2 20	256
7,4 -30	217
10.4 40	194
13.0 50	156
15.6	128
18.2 70	106
20.8 80	83
23.4 90	61
100	43
110	25
120	22
130	31
140	47
150	56
160	67
170	83
180	89
190	89
200	
210	94
57,1 220	100
230	100
240	100
250	94
260	83
270	81
280	78
290	69
300	58
310	58
320	49
84 330	29
ν φ 330	14



UNUSED TOWER #7 CURRENT DISTRIBUTION

Prepared For MAMBISA BROADCASTING CORPORATION WAQI MIAMI, FLORIDA 710 KHz 50 kW - U DA- 2

A. D. RING & ASSOCIATES, P.C. CONSULTING RADIO ENGINEERS

WASHINGTON, D. C.

World Radio Histor

APPENDIX ii

EVALUATION OF SEASONAL GROUND CONDUCTIVITY CHANGES

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

Field strength measurements made in conjunction with the WAQI proof of performance were conducted over a period of approximately seven months, from late May until early December. Although contemporaneous directional and nondirectional measurements are available in all cases, precluding seasonal effects (if any) from distorting the numerical (ratio) analysis of measured data, there may remain some question of mixing data taken during different seasons on field strength measurement graphs.

The environmental conditions which lead to significant seasonal ground conductivity changes do not exist in South Florida, where WAQI is located. Foliage conditions are virtually constant throughout the year. Temperature variations are minimal, as indicated by the NOAA publication "Local Climatological Data - Annual Summaries for 1984". The difference between the highest Normal Daily Maximum and lowest Normal Daily Minimum temperatures for Miami, Florida is 30 degrees Fahrenheit. By comparison, the corresponding difference at Washington, D.C. is 60 degrees; the figure for Syracuse, N.Y. is 66 degrees.

Figures ii-1, -2, and -3 and the corresponding Tables ii-I, -II, and -III present a comparison of nondirectional field strength readings obtained along the 35, 141, and 190 degree radials early and late during the project. As can be readily observed, there is no discernable difference in ground conductivity for measurements taken in distinctly different times of the year.

These radial bearings were randomly chosen and are believed to be representative of the situation as a whole. Sufficient ground measurements taken during May and June were not available for westerly radials such as 277 degrees and 308 degrees in order to make a statistically valid comparison. However, the terrain along westerly bearings is swampland similar in nature to that along the 190 degree radial. Similar performance is expected.

Based on the nature of the land and the data shown, it is not believed that any seasonal conductivity changes of any significant sort occur in the vicinity of the WAQI transmitter site. Intermixture of data taken during different parts of the year should cause no distortion of analysis results.

TABLE ii-I

SEASONAL FIELD STRENGTH VARIATION DATA

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

35 Degrees True, Nondirectional

				Field			Field
Point	Distance	Date	Time	Strength	Date	Time	Strength
Number	(Miles)	1986	(EDT)	(m V / m)	1986	(EDT)	(mV/m)
10	2.03	5 - 22	1301	380	10-24	1320	395
11	3.26	11	1324	225	н	1438	250
12	5.12	44	1403	142	н	1451	150
13	5.72	11	1411	118	п	1455	115
14	6.34	16	1415	115	11	1500	121
15	6.58	16	1418	96	11	1505	102
16	7.03	11	1426	94	н	1513	92
17	7.85	11	1439	103	II	1520	98
18	8.50	41	1453	84	н	1526	86
19	9.02	н	1500	76	н	1548	80
20	9.52	11	1510	7 1	11	1553	68
21	10.50	"	1524	64	11	1559	66
22	11.43	н	1530	59	11	1605	61.5
23	12.47	11	1552	54	11	1610	49.0
24	13.40	11	1601	46	11	1615	50.0
25	14.70	11	1609	43.5	16	1621	45.0
26	15.56	11	1623	41.0	**	1636	42.0
27	16.47	н	1628	40.0	10-25	1443	38.0
28	17.65	11	1640	34.5	H	1449	35.0
29	18.90	H	1651	26.8	16	1456	27.0
30	19.80	11	1715	28.0	11	1519	28.0

TABLE ii-II

SEASONAL FIELD STRENGTH VARIATION DATA

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

141 Degrees True, Nondirectional

				Field			Field
Point	Distance	Date	Time	Strength	Date	Time	Strength
Number	(Miles)	1986	(EDT)	(mV/m)	1986	(EDT)	(mV/m)
5	1.02	5-25	0904	742	10-28	0944	740
11	2.15	н	0955	389	11	0959	385
12	3.60	н	1030	231	10-29	1000	230
13	4.02	н	1039	208	н	1008	210
14	4.92	н	1056	198	u	1020	195
15	5.33	11	1110	167	11	1035	165
16	5.82	H	1126	138	н	1044	135
17	6.40	H	1143	131	li .	1052	130
18	6.98	**	1154	108	11	1056	110
19	7.40	11	1206	117	11	1100	115
20	8.70	19	1225	88.5	H	1115	86
21	9.65	ш	1239	89.0	ш	1122	88
22	11.00	11	1257	71.5	n	1130	72
23	12.16	Ħ	1309	62.0	li .	1135	60
24	13.60	11	1325	41.5	11	1145	43.5
25	15.35	u	1343	54.0	11	1155	55.0
26	16.90	81	1404	36.5	u	1158	37.0
27	18.40	11	1428	37.7	и	1205	36.5
28	19.70	II	1444	29.5	44	1210	30.5

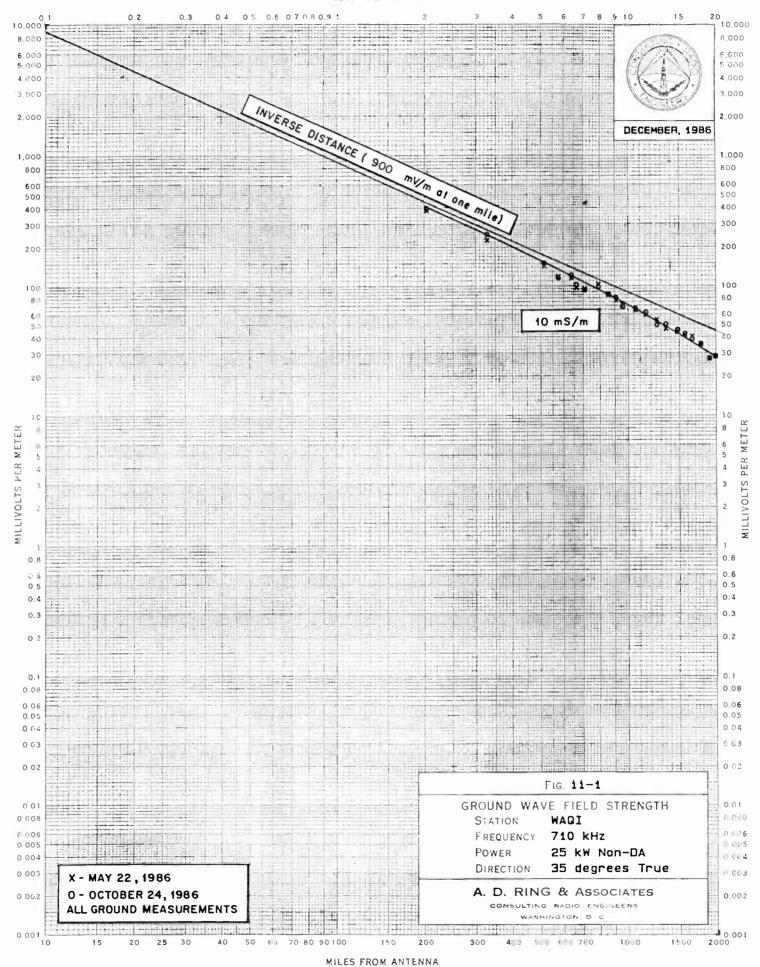
TABLE ii-III

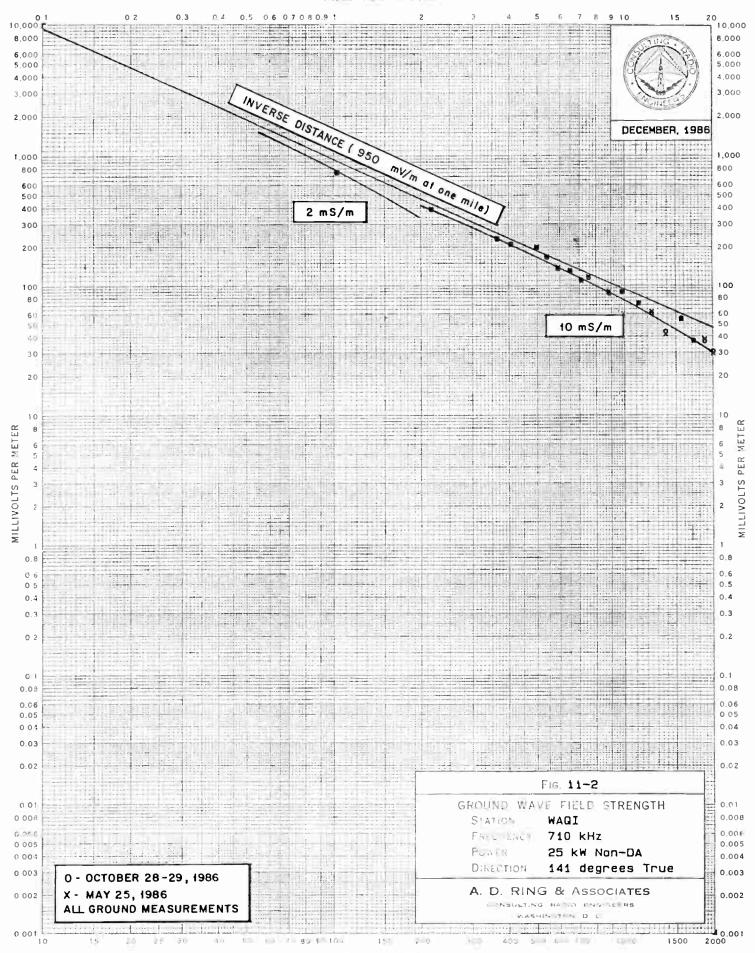
SEASONAL FIELD STRENGTH VARIATION DATA

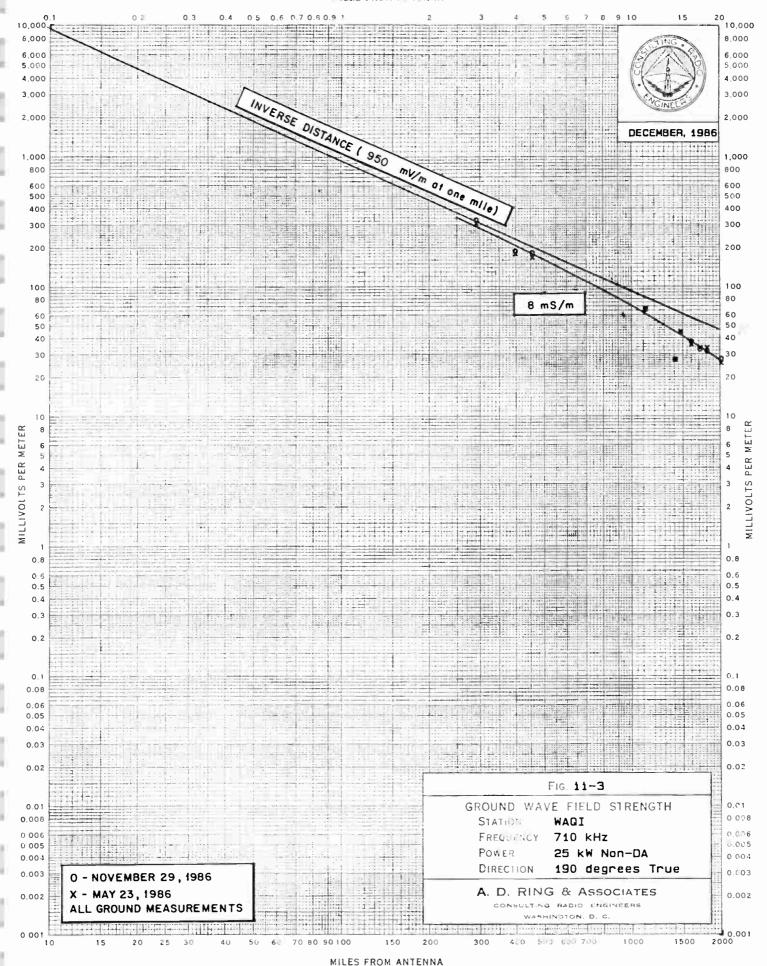
prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

190 Degrees True, Nondirectional

Point Distance Date Time Streng Number (Miles) 1986 (EDT) (mV/m	gth Date Time Str	eld ength V/m)
11 2.88 5-23 1506 310 12 3.93 " 1521 181 13 4.50 5-25 0937 170 18 11.00 5-23 1743 67.5 21 13.90 5-24 1708 27.5 22 14.50 " 1718 45.5 23 15.77 " 1734 36.2 24 16.80 " 1746 34.0 25 17.82 " 1759 34.0 27 19.90 " 1806 26.0	10-28 0946 2 0951 4 1127 3 11019 3 1030 3	0 5







APPENDIX iii

FIELD STRENGTH MEASUREMENTS BY HELICOPTER

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

The WAQI transmitter site is located in marshland near the Florida Everglades. Areas to the south, southwest, west, and northwest of the transmitter site have few roads which may be used to access field strength measurement locations. The area is inhabited by numerous species of unfriendly reptiles, discouraging access by foot. Consequently, a limited number of ground-accessable measuring locations are available. Airborne measurement of field strength using a helicopter was necessary in these directions in order to obtain sufficient measurement data.

Measurement Equipment

Measurements were conducted using a Bell 206B JetRanger II helicopter contracted from Crescent Airways of Pembroke Pines, Florida. The loop antenna of a Potomac Instruments field strength meter was mounted on a retractable boom assembly, which was attached to the landing skids of the helicopter. A cable connected the loop antenna to the meter itself, which was, in turn, connected to an Esterline-Angus model 601C chart recorder. The meter and recorder were located in the rear passenger compartment of the helicopter. The loop, cable, and meter have been calibrated as a system by Potomac Instruments, Inc. Figure iii-l illustrates two views of the boom assembly in the measuring position. The boom is raised when the helicopter is landing. This assembly was originally developed by AM broadcast station WNOE, New Orleans, Louisiana. Further details may be found in the Commission's engineering file for WNOE. The

installation of the assembly on the helicopter was inspected and approved in accordance with the requirements of the Federal Aviation Administration.

<u>Calibration</u> Procedure

The chart recorder was calibrated to duplicate the indications of the field strength meter. Measurements were taken along the 35 degree True radial in order to check the correlation between ground measurements and airborne measurements. The helicopter was flown out the radial at essentially constant speed, with the chart recorder operating at a velocity of 3 inches per minute. As measurement locations established on the ground were passed, tick marks were placed on the chart. The field strength values measured on the ground and read off the recorded chart are presented in Table iii-I.

Airborne readings are compared to nondirectional data taken during May and October. In both cases, excellent correlation was obtained. Figure iii-2 illustrates the comparison of airborne data with the May ground measurements; Figure iii-3 illustrates the comparison with the October measurements.

The nature of the apparatus employed suggests that use of a correlation factor to determine equivalent on-the-ground field strength data is inappropriate. The data of Table iii-1 establishes that minimal differences in readings exist; differences well within the range of instrument and parallax errors. For the measurements conducted in connection with the proof of performance of WNOE, no correlation factor was used. Given the nature of the equipment, the data obtained, and the prior experience, use of a correlation factor is deemed inappropriate for this case.

Measurement Method

For close-in nondirectional field strength measurements, a known starting point was established by reference to landmarks, approximately 2 miles from the transmitter site. The helicopter was flown at a constant speed directly to the nondirectional radiator (tower #1), with the starting, ending, and any intermediate ground reference marked on the recorded chart of field strength versus time.

For complete radial measurements, a combination of visual and electronic navigation was employed. A Texas Instruments TI-9200 Loran C aircraft navigation receiver was used, tuned to the Southeast chain of Loran C stations. The navigation system was initialized as the helicopter sat on the ground near the center of the WAOI antenna array, whose geographic coordinates are known. In flight, the system provides accurate information concerning the distance in nautical miles and bearing with respect to True North from the initial reference point. As a backup, the helicopter's radio Automatic Direction Finder (ADF), tuned to WAQI, was also used.

Two runs were flown for each complete radial and mode of operation, inbound and outbound. As ground measurement points or other identifiable landmarks were passed, tick marks were placed on the recorded chart of field strength versus time. Where no landmarks were available, mileages were marked based on Loran C distance indications. Use of this procedure permits interpretation of distances on the chart with a high degree of confidence and repeatability. Measurements were made as far as periodic landmark availability permitted.

Data Analysis

The field strength versus time charts for each run along each radial were first read for airborne field strengths at ground measurement points. A correlation analysis was then conducted to determine the combination of directional and nondirectional runs that best approximated results obtained on the ground. Those runs were then read in detail.

Intermediate airborne measurement points were selected between ground points by evenly dividing the chart between adjacent ground point tick marks in order to achieve an approximately equal interval of distance (time) between adjacent measurement points, both ground and air. It is believed that this practice of evenly dividing the recorded chart between adjacent ground points largely eliminates errors in point location attributable to variations in helicopter speed.

Personnel

The JetRanger II helicopter was piloted by James Hunter, an employee of Crescent Airways. Timothy Z. Sawyer of this firm, a licensed fixed-wing pilot, served as navigator. The equipment was operated by Lyndon H. Willoughby, its designer, during the August measurement program and by Paul L. Whitney, during the December work.

Conclusion

It is believed that the measurement procedure employed results in as accurate and repeatible field strength measurements as can possibly be obtained in a moving aircraft.





FIGURE iii - 1

LOOP ANTENNA MOUNTING FOR HELICOPTER MEASUREMENTS

Prepared For MAMBISA BROADCASTING CORPORATION WAQI MIAMI, FLORIDA

710 kHz

50 kW -U

DA - 2

A. D. RING & ASSOCIATES, P.C.

CONSULTING RADIO ENGINEERS WASHINGTON, D. C.

World Radio History

TABLE iii-I

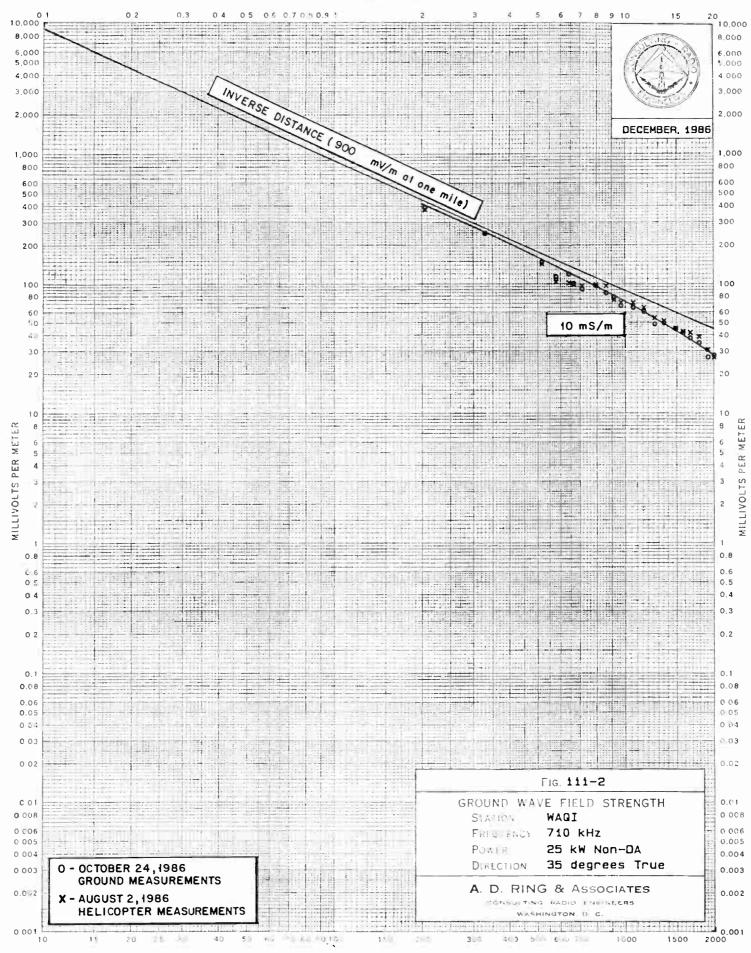
HELICOPTER FIELD STRENGTH MEASUREMENT CALIBRATION DATA

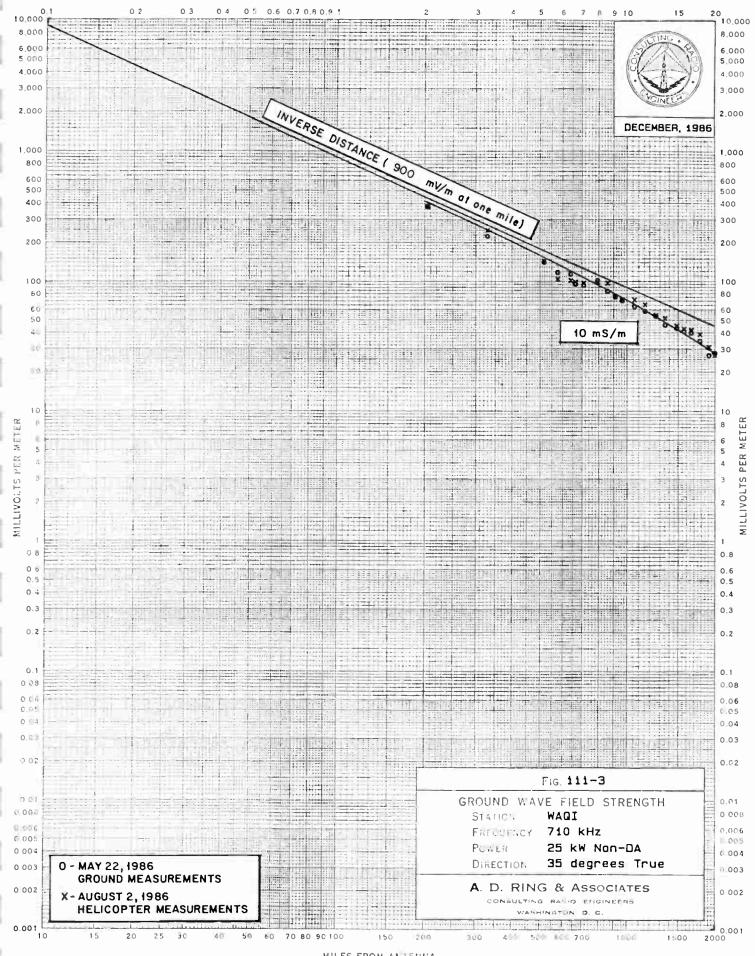
prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

Point Numbe		May Ground (mV/m)	October Ground (mV/m)	August Air (mV/m)	Ratio (Air/May)	Ratio (Air/Oct)
10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	2.03 3.26 5.12 5.72 6.34 6.58 7.03 7.85 8.50 9.02 9.52 10.50 11.43 12.47 13.40 14.70 15.56 16.47 17.65 18.90 19.80	380 225 142 118 115 96.0 94.0 103 84.0 76.0 71.0 64.0 59.0 54.0 46.0 43.5 41.0 40.0 34.5 26.8 28.0	395 250 150 115 121 102 92.0 98.0 86.0 80.0 66.0 61.5 49.0 50.0 45.0 42.0 38.0 35.0 27.0 28.0	380 250 145 105 103 100 98.0 100 98.0 72.0 72.0 66.0 55.0 52.0 45.5 43.0 42.0 39.0 31.0 27.0	1.0000 1.1111 1.0211 0.8898 0.8957 1.0417 1.0426 0.9709 1.1667 1.0000 1.0141 1.1250 1.1186 1.0185 1.1304 1.0460 1.0488 1.0500 1.1304 1.1567 0.9643	0.9620 1.0000 0.9667 0.9130 0.8512 0.9804 1.0652 1.0204 1.1395 0.9500 1.0588 1.0909 1.0732 1.1224 1.0400 1.0111 1.0238 1.1053 1.1143 1.1481 0.9643
			Average	e Ratio:	1.0449	1.0286

See Table ii-I for ground measurement times

Airborne measurements conducted on August 2, 1986 from 1504 to 1523





APPENDIX iv

FIELD STRENGTH MEASUREMENT in the PRESENCE of SIGNIFICANT COCHANNEL INTERFERENCE

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

WAQI is a Spanish language station serving southern Florida on 710 kilohertz. Monitoring reports by the Field Operations Bureau (FOB) of the Federal Communications Commission (FCC) indicate that a cochannel station with an estimated power of 50 kilowatts is operated near Havana, Cuba, some 388 kilometers from the WAQI transmitter site. This Cuban station produces significant field strength, on the order of 0.8 to 1.5 millivolts per meter (mV/m), in the vicinity of the WAQI transmitter site. Consequently, accurate measurements of WAQI field strength below 10 mV/m may be obscured by cochannel interference. Reliable field strength measurement is not possible unless the WAQI signal can be detected and measured separately.

A. Theory of Instrumentation

AM broadcast field strength meters include an envelope detector circuit. Such a circuit approximates a product device. Two signals, differing in frequency, applied to the detector input will result in sum and difference components at the detector output. If the amplitude of one signal is held constant, the sum or difference signal output will be directly proportional to the amplitude of the signal which varies.

If two signals are applied to the detector, one being the desired signal received from a broadcast station and the other a locally generated, constant amplitude signal injected into the receiver circuit by appropriate means, a beat frequency will be

produced, corresponding to the frequency difference between the signals, with its amplitude proportional to that of the received signal. For example, two signals separated in frequency by 20 Hertz will produce a beat of that frequency at the detector output.

Assume that three signals are applied to an envelope detector. The frequencies of these signals are 709.950, 709.980, and 710.000 kilohertz. Audio beat frequencies are produced at 20 (710.000-709.980), 30 (709.980-709.950), and 50 (710.000-709.950) Hertz. If the amplitude of the 709.950 kilohertz signal is held constant, the 30 Hertz product amplitude is directly proportional to the amplitude of the 709.980 kilohertz signal, within the dynamic range of the equipment used. The 30 Hertz component can be easily isolated by means of a narrow, adjustable audio bandpass filter.

In order to accurately measure the WAQI signal in the presence of significant Cuban interference, a frequency relationship similar to that of the foregoing example was established, as illustrated by Figure iii-1. The WAQI carrier frequency set approximately 20 Hertz below that of the Cuban station. A locally generated signal, approximately 30 Hertz below the WAQI carrier frequency, was injected into a field strength meter. The resultant audio output was fed to a narrowband adjustable audio filter and precision detector, the output of which is metered and can feed a chart recorder.

B. Apparatus Configuration

Figure iii-2 is a block diagram illustrating the equipment configuration employed. A Potomac Instruments SD-31 synthesized signal generator was used as the local signal source. Its output was injected into the Potomac Instruments FIM-41 field strength meter (FSM) input through a suitable potentiometer and isolation

resistor. The detector (recorder) output of the field strength meter was connected to a Sine Systems FSV-1 frequency-sensitive audio voltmeter (FSV), which was custom made for this project. Figure iii-3 is a photograph of the instrument system. Each component is firmly bolted to a base plate, in order to eliminate any chance of measurement inconsistency attributable to component physical position.

C. Instrument Linearity

Field strength meter detector linearity was tested on the bench, where it was noted that significant clipping of the audio beat frequency was occurring. Increase in the capacitance of C129 in the field strength meter fully resolved this problem. Once again, calibration was checked against an unmodified meter. No differences were noted.

To test linearity and dynamic range of the apparatus system, two locally generated signals were applied to the Potomac FSM input. These signals were adjusted for a difference in frequency of 30 Hertz. The amplitude of one signal was adjusted for an indication of 7 millivolts (mV) on the FSM. The other signal signal was adjusted to 2.0 mV. The FSV tuning was adjusted for maximum indication and the gain was calibrated to result in an FSV meter reading of 2.0. The amplitude of the second signal was varied in discrete steps from 0.2 to 3.0 mV and the FSV reading recorded. It was found that, up through 2.0 mV, the FSV reading tracked the second signal amplitude within the degree of accuracy to which the meters could be read by the naked eye, i.e., there was virtually no error between second signal amplitude and FSV indication. Above 3.0 mV, significant errors were noted, as predicted by theory.

The same test was repeated for first signal amplitude of 70 mV with second signal range of 2 to 30 mV. Comparable results

were obtained. There were no significant tracking errors noted over the range 0.02 mV to 20 mV, provided that the proper ranges were selected for both the FSM and FSV units and the signal amplitude being measured did not exceed one-third of the constant signal level.

The bandwidth of the Sine Systems FSV-1 unit is quite narrow, approximately 5 percent of the center frequency, precluding errors caused by the addition of undesired beat frequency signals to the signal under measurement. The unit features variable tuning and a readout of the frequency to which it is tuned, facilitating accurate setup and use.

D. Apparatus Calibration

Since the Potomac Instruments FSM was modified by adding an input jack for the local oscillator signal and connecting this jack to the meter input via a high resistance, its calibration was carefully checked against an unmodified meter. All connections were as described above, but the local oscillator was shut off. No difference between modified and unmodified meter indications were noted at several measurement locations and with several different ambient signal levels. Furthermore, the effect of the layout of the three instruments on measured field strengths was determined in a similar manner by comparison to the readings of the FSM standing alone. No differences in readings were noted. Consequently, it is concluded that the FSM modifications made and instrument mounting scheme used have no adverse affect on instrument calibration.

Prior to taking actual field strength measurements, at a measurement location where WAQI field strength was sufficiently greater than the cochannel interfering signal, the instrument system was calibrated. First, the FSM was calibrated in the normal manner with the local oscillator (SD-31) off. The WAQI

field strength was then read. The local oscillator was activated and set for a signal injection level appropriate to the FSM and FSV ranges selected. The FSV calibration was adjusted to match the FSM indication previously obtained.

Measurement Results

The field strength readings obtained by conventional FSM and unconventional FSV measurement are presented for the 0.5 and 20.5 degree nighttime radials by Tables iv-I and iv-II, respectively. The difference in readings obtained is illustrated graphically by Figures iv-4 and iv-5. As can be readily seen, the difference between FSM and FSV indications is minimal for signal strengths exceeding 3 millivolts per meter, becoming more pronounced as signal strength decreases. This is to be expected, since the interfering Cuban station's signal amplitude becomes significant with respect to and, eventually, greater than the WAQI signal amplitude, dominating the reading of the FSM.



FIGURE iv-1

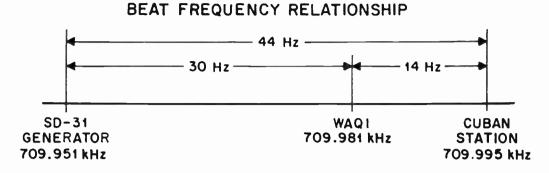


FIGURE iv-2



INSTRUMENT CONFIGURATION

Prepared For DRAWN BY FGA MAMBISA BROADCASTING CORPORATION SCALE: WAQI MIAMI, FLORIDA NONE DEC., 1986 710 kHz 50 kW - U

DA-2

DRAWING NUMBER: NONE

APPROVED BY KDL

WASHINGTON: D. C

A. D. RING & ASSOCIATES

CONSULTING RADIO ENGINEERS





FIGURE iv-3

BEAT FREQUENCY FIELD STRENGTH MEASUREMENT APPARATUS

Prepared For MAMBISA BROADCASTING CORPORATION WAQI MIAMI, FLORIDA

710 kHz

50 kW -U

<u>DA-2</u>

A. D. RING & ASSOCIATES, P.C.

CONSULTING RADIO ENGINEERS

WASHINGTON, D. C.

TABLE iv-I

TOTAL AND INTERFERENCE-FREE FIELD STRENGTH DATA

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

0.5 Degrees True, Nighttime Directional

Data		Total	Field	WAQI	Field
Point	Distance	Time	FSM	Time	FSV
Number	(Miles)	(EST)	(mV/m)	(EST)	(mV/m)
11	2.18	1154	4.90	1156	4.90
12	2.48	1140	3.20	1143	3.20
13	2.65	1146	3.10	1148	3.05
14	3.03	1202	3.10	1204	3.00
15	3.68	1218	3.00	1222	2.85
16	4.16	1225	1.90	1228	1.60
17	4.42	1229	1.80	1230	1.50
18	4.66	1231	2.00	1233	1.65
19	5.18	1234	1.70	1236	1.30
20	5.69	1239	1.35	1241	
21	6.18	1242	2.80	1245	1.20
22	6.43	1247	2.40		2.75
23	8.10	1234		1250	2.25
24	8.60		1.25	1235	0.92
25		1231	1.20	1232	0.84
	9.50	1223	0.72	1224	0.62
26	9.90	1219	1.90	1220	1.80
27	10.10	1215	3.25	1215	2.90
28	10.75	1207	2.60	1208	2.40
29	11.02	1210	2.25	1211	1.90

All measurements conducted on November 24, 1986

TABLE iv-II

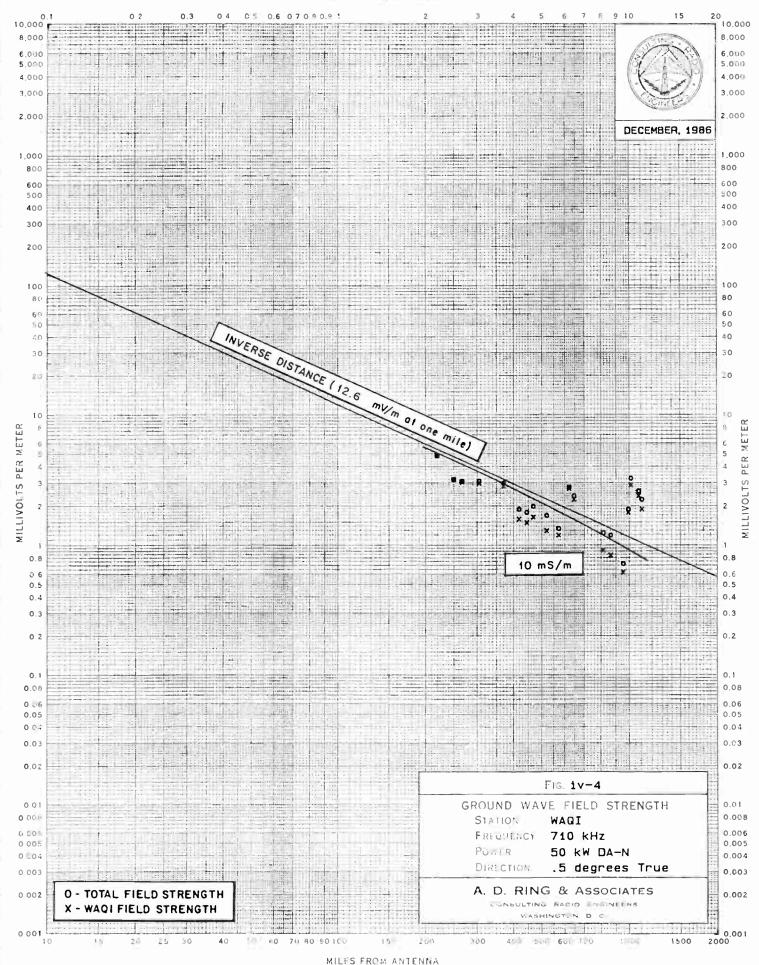
TOTAL AND INTERFERENCE-FREE FIELD STRENGTH DATA

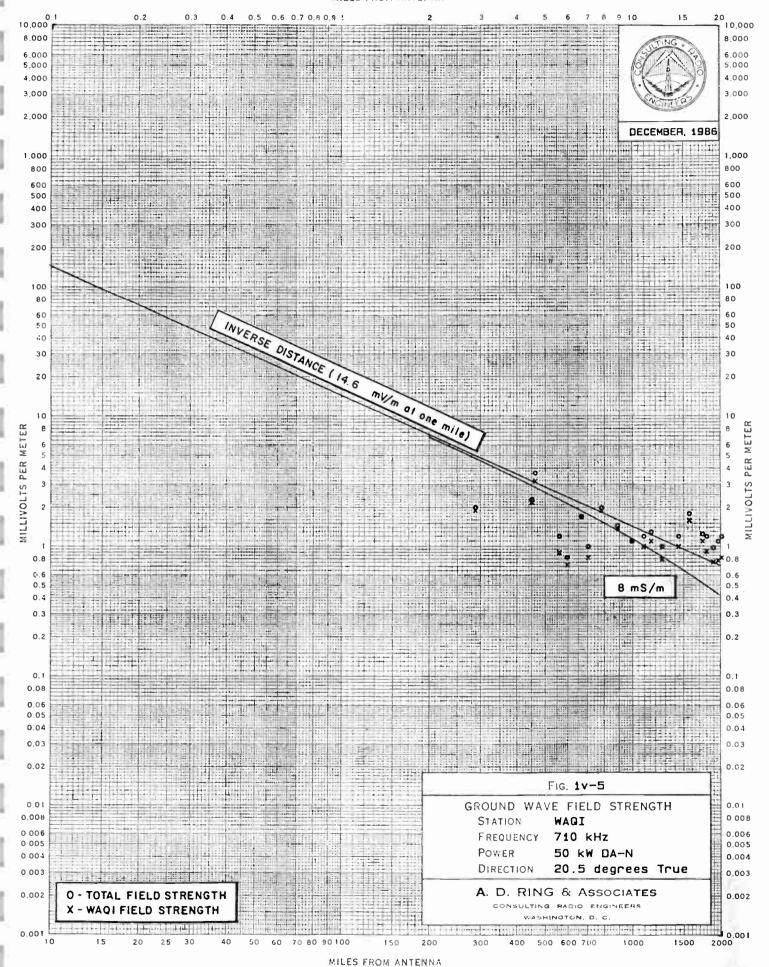
prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

20.5 Degrees True, Nighttime Directional

Point Number	Distance (Miles)	Total Time (EST)	Field FSM (mV/m)	WAQI Time (EST)	Field FSV (mV/m)
11 12 13 14 15 16 17 18 19 20 21 22 23 24	2.85 4.45 4.57 5.52 5.88 6.58 6.93 7.70 8.74 9.80 10.75 11.40 12.45 14.20	1447 1432 1413 1427 1424 1421 1417 1251 1246 1240 1304 1307 1312 1318	2.00 2.30 3.70 1.20 0.82 1.70 1.00 2.00 1.45 1.10 1.20 1.30 1.00 1.20	1448 1433 1414 1428 1425 1422 1418 1252 1247 1241 1303 1308 1313 1319	1.90 2.20 3.20 0.90 0.72 1.70 0.82 1.90 1.40 1.10 0.80 1.00
25 26 27 28 29 30	15.42 17.16 17.72 18.68 19.40 19.96	1324 1330 1333 1338 1342 1345	1.80 1.25 1.20 0.98 1.10 1.20	1325 1331 1334 1339 1343 1346	1.60 1.10 0.92 0.76 0.78 0.82

All measurements conducted on November 23, 1986





APPENDIX v

GEOMETRIC MEASUREMENT DISTORTION (PROXIMITY) CORRELATION METHOD

prepared for Mambisa Broadcasting Corporation WAQI Miami, Florida

It is well known that, for directional arrays with wide interelement spacing, measured field strengths will not always follow an approximate inverse relationship with respect to increasing distance from the transmitter site. This is because the inverse relationship holds only where the bearing from each tower in the array to the measurement point is identical. Where such a relationship does not obtain, the field vectors from each tower will have slightly different relative magnitudes and phases with respect to the assumed ideal, resulting in different computed radiation. This effect is especially significant in directions of high radiation suppression.

Field strength measurements subject to such distorting effects cannot be analyzed by conventional graphical or numerical means. Instead, an approximation of the expected field strength versus distance relationship must be employed to correlate the data obtained with theoretical effects.

For the purpose of conducting numerical analysis of data subjected to proximity effects, the Quadrature Method of proximity correlation (correction) has been devised. This method has been accepted by the Commission in connection with the Applications for License of AM broadcast stations WCAR, Livonia, Michigan (File Number BL-800404AA, as amended October 24, 1985), KHYT, South

Tucson, Arizona (File Number BL-850321AE), and KTNN, Window Rock, Arizona (File Number BL-860221AA). Method theory is set forth in detail in the former two applications and will not be repeated herein. The essential purpose of the Quadrature Method procedure is to apply correlation factors to measured data to permit an "equivalent" inverse distance analysis. WAQI field strength measurements were evaluated for proximity effects using the Quadrature Method.

In this application, the use of the Quadrature Method has been expanded to provide unattenuated and attenuated field strength versus distance curves, correlated to measured data. Consequently, it is possible to construct a field strength versus distance curve for the theoretical, measured, and standard pattern cases to illustrate fit of measured data to these conditions, without modification of the raw field strength data before it is plotted.

The standard pattern equivalent field strength, taking into account proximity effects, can be computed for any location relatively simply. The theoretical "near-field" signal strength for that location is computed, taking into account the complete geometry of the situation. That value is normalized to one kilometer by multiplying it by the distance from the center of the array to the point. The normalized theoretical value obtained is then applied to Equation (2) of Section 73.150(b) and the equation of Section 73.152(c)(2)(ii) of the Rules to find the modified standard field strength, which then can be denormalized by dividing it by the distance to the point. The result is the standard pattern field strength at the point.

The Quadrature Method involves a convergent determination of the quadrature difference between measured and theoretical radiation. This difference value, at one kilometer, can also be combined with the theoretical near-field signal strength to determine the measured unattenuated radiation at the point. The equations describing this procedure are as follows:

$$E_q^2 = E_m^2 - E_{tf}^2$$

where: E_q = Quadrature error magnitude

E_{tf} = Theoretical far-field radiation in measured radial direction, at one kilometer

 E_{m} = Analyzed measured radiation at one kilometer

$$E_{p} = -\frac{1}{d} - E_{tn}^{2} + E_{q}^{2}$$

where: E_{p} = Measured unattenuated radiation at point

E_{tn} = Theoretical near-field radiation at point, normalized to one kilometer

d = Distance from array center to point

Having determined a correlated unattenuated field strength versus distance relationship, the attenuated case can be easily derived by scaling appropriate conductivity attenuation factors to the curves drawn.

If proximity correlation has been properly applied, two conditions will obtain. First, the measured field strength data points will fit the correlated conductivity curves reasonably. Second, the measured unattenuated field strength curve will fall below the curve for the standard pattern case. Tables V-B and V-J and Figure 8-J of the WAQI Proof of Performance illustrate application of this technique to the instant situation.