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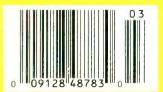
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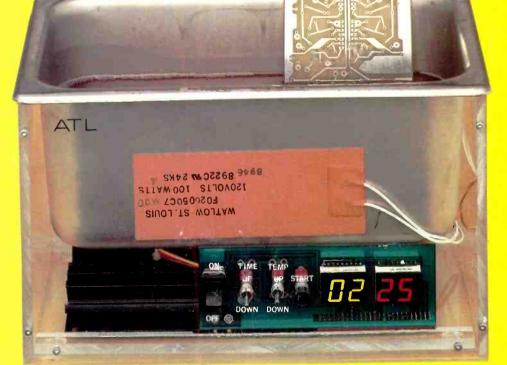
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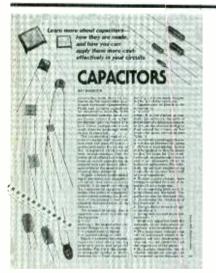
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# ON THE COVER



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# BUILD THIS AUDIO EXPANDER

# **FORCE-SENSING** RESISTORS

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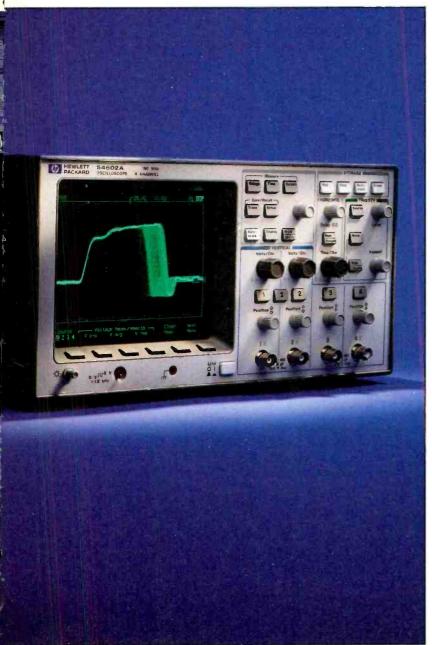




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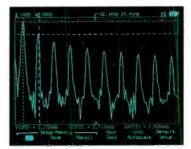
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# WHAT'S NEWS

# A review of the latest happenings in electronics.

# Personal communicator explosion seen

Evidence from a number of sources points to the heating up of the handheld "personal communicator" market. As presently visualized, a personal communicator will be a box that includes the functions of a scratch pad, personal computer, electronic organizer, and, perhaps, a cellular telephone.

It is expected that the user will be able to write messages for storage on a screen with a pen, send those notes elsewhere, call up files of data and phone numbers, and even make phone calls—if the box has an integral cellular phone.

AT&T has been working hard to stake out a position in the communicator market. It has two axes to grind. It would like to sell its cellular communication services in that field, and it is seeking business for its own equipment manufacturing facilities. One way to assure that foothhold is for AT&T to develop the standards that will be accepted by all other manufacturers and communications services providers.

So far, AT&T has forged alliances with several major electronics manufacturers, developed the "Hobbit" microprocessor chip for the units, and has stated its willingness to provide financial backing for suppliers and support software publishers.

Matsushita (Panasonic), NEC. and Toshiba have announced plans to build communicators based on AT&T's Hobbit microprocessor. AT&T is also negotiating a licensing agreement that would allow NEC to manufacture the Hobbit microprocessor. In addition, AT&T expects to sell its own brand of personal communicator, manufactured by Eo Computer, Inc. Mountain View, CA, a joint venture between AT&T, Matsushita, and Marubeni of Japan. It expects to sell the units through its national chain of AT&T Phone Centers.

AT&T is also working with Go Corp., whose PenPoint operating system is incorporated into the Eomade products, to encourage the adoption of the operating system as an industry standard. Its plans include lining up more than a dozen software suppliers to write applications software that is compatible with the PenPoint software.

In another move, AT&T has designed the circuitry for a microminiature disk drive, and it is backing Sundisk, a company that makes a data-storage device for the communicators.

Apple has developed prototypes of a similar unit called the Newton, which it calls a "personal digital assistant" or PDA. Intel is reported to be working with VLSI Technology Inc. to develop a processor for the new units, and Motorola has signed investment and cross-technology agreements with both Apple and Sony.

# **Doubling digital video rate**

The possibility of doubling the amount of digital information that can be transmitted on cable TV channels, without additional video compression, is now a reality. Zenith Electronics of Glenview, IL, has developed vestigial sideband (VSB) digital modulation and transmission technology that makes it possible.

Zenith's 16-level digital transmission system can send two digital HDTV signals on a single 6-MHz cable channel. That doubles the number of digitally compressed standard TV signals on a cable channel, and permits the delivery of as many as 23 movie channels or nine live-video channels. An alternative mix of one HDTV and several standard TV programs is also a possibility.

According to Zenith, radio transmission of digital TV signals results in lower quality TV received signals than cable. Programs transmitted to customers over cable are less likely to be distorted and suffer from interference. Signals in cables have better peak carrier-to-noise ratios and lower levels of interference.

Zenith took advantage of the greater noise-margin of cable transmissions to increase the information-carrying capacity, or data rate, of cable. To increase the amount of digital data delivered through a 6-MHz channel, a cable system must maintain a high signal-to-noise ratio, and must acquire and lock in the carrier, clock, and synchronization information. This is difficult to accomplish with the advanced digital modulation techniques such as 16-and 64-QAM (quadrature amplitude modulation).

By contrast, Zenith's VSB digital modulation and transmission technology, uses auxiliary signals for acquisition and synchronization. The pilot carrier, not feasible in QAM systems, and a data-segment synch signal are both independent of the data.

Zenith's 4-VSB technology obtains a data rate of 21.5 megabytes per second for its "Digital Spectrum Compatible" HDTV (DSC-HDTV) system. The company's newly developed, 16-VSB approach, an extension of the 4-VSB system, yields twice the channel data rate, or 43 megabits per second, with no increase in data compression requirements.

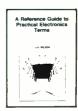
The 16-VSB system obtains signal acquisition even when ghosts and impedance mismatches are present. The system has simple analog-to-digital conversion needs, and it does not requires the more complex adaptive equalizer of the QAM systems. Therefore, 16-VBS is said to offer cost-effective, noise-free TV pictures and digital audio. Moreover, it is said to be compatible with existing computer, telephone, and other digital communications systems.



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March 1993, Electronics Now

# **VIDEO NEWS**

What's new in the fast-changing video industry.

DAVID LACHENBRUCH

• HDTV costs. No matter which of the five proposed HDTV systems is chosen, receiver costs are expected to be about the same. That's the conclusion of a report made to the FCC Advisory Committee on Advanced TV Service, detailing the most complete study of receiver costs made to date. The Specialist Group on Advanced TV Receiver Cost, consisting of representatives of all HDTV system proponents and engineers from receiver-manufacturing companies, found that by 1998 (which was assumed to be the first year of true mass production) the average HDTV receiver with a 34-inch widescreen (16:9) tube could retail for about \$2550 and a 56-inch projection set could sell at around \$3850.

These findings are interesting in view of the fact that the first two widescreen (non-HDTV) sets to be announced for the American market—a 34-inch tube set under the RCA brand and a 50-inch projector by Panasonic—both will carry suggested list prices of \$4999.

The HDTV cost study group found that no proposed HDTV system had a significant cost advantage as far as receivers are concerned. Electronics in 34-inch sets varied from \$216 to \$258 in cost, and for projectors from \$305 to \$374. Cabinet cost of all 34-inch sets was estimated at \$90, and for projectors at \$140. The tube price was put at \$700; projection optics, tubes, screen, and assembly at \$1050. Retail prices were estimated by adding the normal 2.5 multiplier for various markups.

The specialist group threw cold water on those counting on new giant picture-on-the wall displays to replace CRT-based systems. "The cost of future displays with various flat panel technologies and light-valve projectors could not be estimated with any degree of accuracy, because no such displays appear

ready for consumer HDTV at this time," the report stated. "Therefore direct-view CRT and projector technology were assumed to be the most cost-effective displays for the time frame of this analysis."

 8mm/VHS VCR. Something that home videographers have been wishing for is on the way. In Japan, Sony has introduced a dual-deck VCR that can edit from 8mm to VHS and vice versa. Both decks have high-end features such as stereo audio and capability of accommodating high-band recordings (Hi8 and S-VHS), but in standard resolution only. Included are several editing features, including jog/shuttle controls. Presumably frightened by the blustering talk of movie-industry association figures, who claim that dual decks are designed to infringe copyrights, Sony says that it has no plans to export the deck to America, but demand could convince it to change its mind.

Competition could do that as well. Go-Video, which introduced the first VHS-to-VHS dual deck to America, says that it will introduce an 8mm/VHS deck here at midyear. So does Samsung, which makes the dual decks for Go-Video.

• CD-ROM movies. How do you sell a multimedia system when the public doesn't know what multimedia is? Call it a movie machine. That's the formula that will be followed by Denon America, according to its president, Robert Heiblim. People aren't interested in buying something for which they have demonstrated no need and don't understand. Heiblim reasons. Denon is developing a CD-based multimedia system using Intel's Digital Video-Interactive (DVI) system. The most important need is to put regular noninteractive movies on the ROM discs first, according to Heiblim. Consumers know what movies are

and will buy videodisc machines that use little five-inch discs, as long as they are superior to existing laserdiscs, he predicts. When many of these CD movie machines are in place, then interactive programming can be inaugurated.

Denon says that its DVI system soon will have laserdisc quality, which is considers a prerequisite for consumer acceptance. Heiblim says that early multimedia consumer products must be marketed as "VTR's," which stands for "videotape replacements," because consumers won't put their money into unknown devices. He prefers to call Denon's system "something that plays movies and is also interactive."

• Video goggles. Two companies have demonstrated ski-mask-like contraptions that provide personal video pictures using LCD's. Sony displayed its "Visortron" system in Japan, using two small LCD's that are viewed through built-in lens systems. Since each eye views a separate picture, it's possible to display images in true 3-D. Sony says that it's exploring commercial uses for the product.

But another system, "Virtual Vision sport," was about to go into production at our press time. That system is based on the "heads-up" displays used in aircraft, and uses a single LCD and lens-mirror to display a picture that appears to be as large as 60 inches, 8 to 15 feet in front of the viewer. The picture is off to one side, so the user can perform other tasks while watching it.

The five-ounce wrap-around glasses, with a belt-packed TV tuner, battery, and jacks to connect a VCR, camcorder, or TV cable, will go on sale this spring at less than \$900, says its producer, Virtual Vision. An accessory will permit it to pick up wireless signals from the television.

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I have an IBM clone and use it with a monochrome monitor. The system has always been very reliable but recently I've been having trouble with the monitor. I'm not sure what's going on, but the symptoms are that the image flickers randomly. Sometimes it will be perfect for a while and then it will get brighter or darker in random spurts. If I turn the monitor off and then on again, the problem sometimes fixes itself for a while, but it's only a matter of time before the flickering returns. Any ideas?—B. Frish, Los Angeles, CA

You may think of this as a computer problem but any experienced TV person will tell you that this is a simple problem with the clamping circuit on the video input. Most TV's use a combination of diodes and resistors to set the white and black levels to somewhere around a volt or so. Computer monitors do the same.

If you have access to the schematic for the monitor, it should be a fairly simple matter to fix it. All you have to do is locate the relevant part of the circuitry and then take a look at the DC levels with a white and black screen. You'll probably find that one of the diodes is intermittently failing. Changing the bad component is a quick job although it may take a bit of work—with a screwdriver—to get your hands on the component.

If you can't get the schematic for the monitor you can still snoop around with a scope or meter until you locate the clamping circuit. If this is the first time you've ever thought about doing something like this, my advice is to forget about it since there are some real knock-you-down voltages floating around the inside any TV or monitor.

Since the purpose of your letter

seems to be getting your computer working again, the best advice is to buy another monitor. You can get a monochrome monitor for under 80 bucks these days and they even come with warranties. If you don't want to scrap your old monitor, take the guts out of it and turn the case into a fish tank. That's what I did with mine!

# LIMITING LED CURRENT

I'm building a circuit that has several LED's as indicators to let me know how the circuit is performing. Quite often more than one LED is on at a time, and since the circuit is battery powered, it causes a real power drain. All the LED's have one leg in common so I have no way to control individual brightness. Isn't there some simple circuit that will regulate and limit the current used by the LED's, no matter how many are lit?—W. Meredith, Elkins, WV

I'm not really clear about why you can't use separate resistors on the LED's to individually limit the currents, but there is another way to solve the problem. The 78XX-series of voltage regulators have been around for a long time and are even available in special low-power configurations. If I had your problem I'd use whichever regulator was suitable and wire it as shown in Fig. 1.

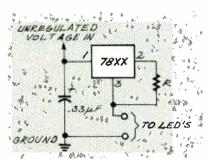


FIG. 1—THE 78XX-SERIES of voltage regulators can be used in a configuration like this to limit current rather than voltage

You should tailor the value of the capacitor to the number of spikes on the line but, in general, the  $0.33~\mu F$  capacitor shown in the schematic should work well.

When you set up the regulator as shown, it works as a current regulator rather than a voltage regulator. The output current draw will be the regulated voltage divided by R. The only thing to watch out for is that you don't try to draw more current through the regulator than what it's rated for. But since you only want to drive a handful of LED's, I don't think you'll have any problems.

### **ONLY HALF-WAY THERE**

I have a laser printer that I'm trying to use for printing graphics. The problem is that I can't seem to print more than half a page—the picture is incomplete and the bottom half of the paper is always blank. What's going on?—A. McChord, Ames, IO

Laser printers produce terrific output, but it's amazing that, while so many people use them, so few really understand how they work. The major constraint in printing graphics with a laser printer is the amount of memory it has, and that seems to be your problem as well.

Copy machines and laser printers are very similar. The former uses an optical image as the source of its output and the latter uses an electronic image in memory for the source. If you want to print with 300-dpi (dot per inch) resolution, your printer will need enough memory to "take note" of the image. If there's not enough memory, the printer will print the page when it runs out of memory—which, in your case, is about halfway through the image.

You have two choices to solve the problem. The first is to add memory to the printer, and you'll need at least one and a half megabytes of RAM to do a 300-dpi full-page

Continued on page 86

12

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# LETTERS

Write to Letters, Electronics Now, 500-B Bi-County Blvd., Farmingdale, NY 11735

# INRUSH CURRENT LIMITER CORRECTIONS

There are two problems with the "Inrush Current Limiter" (*Electronics Now*, December 1992).

First, in Fig. 6 on page 49, the emitter of Q2 and the high end of R5 should be connected to the plus end of C2 (about 24 volts DC). As shown, the Darlington transistor, Q2, and possibly the relay, RY1 (24-volt DC coil) would burn out.

Second, the circuit is too complicated and overdesigned. I designed a much simpler circuit, shown here in Fig. 1 (a) and (b). The relay RY1 will not activate until the resistance of the NTC thermistor R<sub>T</sub> drops low enough for the voltage across RY1 to reach about 80 volts (or whatever the activating voltage for the relay used might be). Resistor R1 might be added to slow down the action by effectively boosting the needed voltage.

Find the maximum resistance (of R1) with which the relay will activate when connected directly to 120 volts AC, and then use a resistor of about half that value. That resistor should be shorted out by another set of contacts of RY1. The effectiveness of the circuit can be seen by finding values of fuses at the just-blow threshold (or just not-blow) when the circuit is used and not used ( $R_T$  shorted out).

I cannot think of an instance when a delay of one second (or more), as stated in the article, would be needed. (If the capacitors in the power supplies need one second to recharge after a spike in the loading current, I would say that the circuit is in peril, and a major redesign of the power supply is needed.) Therefore, the circuit shown here should do the same job nicely.

PTER PESKA

Taylor, MI

In addition to responding to Mr. Peska's comments, I would like to point out several errors that ap-

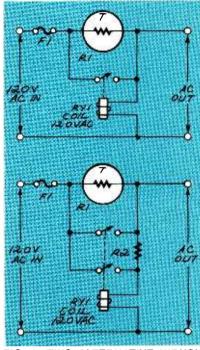


FIG. 1—TWO ALTERNATIVE INRUSH current-limiting circuits.

peared in the article. There is, indeed, an error in Fig. 6 on page 49. The emitter of Q2 and the high end of R5 should be connected to the positive end of C2 (i.e., the positive 24-volt supply). The parts placement diagram, Fig. 7, is correct.

In response to Mr. Peska's comment that the circuit is "too complicated," I'd like to point out that the circuit was designed with a line-derived regulated power supply for several reasons. The main reason to combine such a power supply and timer circuitry was to illustrate the concept of a transformerless linederived, regulated power supply.

This circuit is popular in such commercial products as remote-controlled lamp/appliance controllers. Other advantages of the circuit are that it is independent of the load connected to it, and it features a predictable and easily adjustable time delay. Finally, the circuit is not that "complicated" in the first

place: It does not consist of many components, and it is easy to construct. I agree that Mr. Peska's circuit is much simpler and will work, but my project was designed for the reasons stated in the article.

My response to Mr. Peska's comment that a delay of more than one second is unnecessary is that the circuit allows for a wide range of delays by appropriate selection of a fixed resistor or by the use of a variable resistor. Delays of one second or less are easily obtained by choosing a suitable resistance (simply reduce the value of R4). Again, the wide range of time delays possible was given in Table 1 to illustrate the versatility of the circuit.

In the parts placement diagram (Fig. 7), resistor R8 should be labeled MOV1, R9 should be labeled R8, and R10 should be labeled R9 (there is no R10 in the circuit).

In the first sentence of the last paragraph on page 48, the sentence containing the phrase "shorts out thermistor R9" should read "shorts out thermistor R8."—Douglas Wirth

## **AUDIO UPDATE COMPLAINT**

Larry Klein's November Audio Update contains gross errors and unwarranted assumptions, and it is insulting to audiophiles and readers. For example: The "Hafler test" shown in Fig. 1 has a fatal error in that the amplifier is not evenly loaded. Changes in an amplifier's load usually alter the response of the system significantly, and this change would be included in the null speaker signal.

Klein assumes that a better amplifier will make a better system; this is not necessarily so. The equipment surrounding an amplifier will interact with the amplifier for better or worse, and this makes it difficult to judge an amplifier accurately without considering the related equipment. For this reason, respon-

sible reviewers list the equipment used with the unit under test.

Klein also ignores the fact that audiophiles have a wide range of music preferences that influence equipment purchasing decisions. I argue that one can objectively evaluate equipment, but must include other factors such as performance expectation and personal musical preference.

Klein fails to recognize that sophisticated listening skills take time and effort to develop into a useful tool for evaluating high-end audio equipment. I find his attitude typical of those whose hearing is undeveloped and whose experience seems to be the result of confiding in salesmen, listening to rumors, and "wannabe" experts. Klein's incompetence is so complete that he probably would even claim that CD's sound better than records, contrary to what is obvious.

Address withheld by request

Mr. Duncan's long letter (heavily condensed for space reasons) contains several technical and philosophical confusions—aside from being stupid and insulting. To start:

The Hafler circuit shown in Fig. 1 of my article connects the "null" speaker so it can compare only the input and output of the right channel, which is loaded with a conventional speaker. The resistance loading on the left channel output simply provides the input signal for the right channel.

If I understand Mr. Duncan correctly, he believes that it's more important to match the complementary defects of amplifiers and other equipment than to seek the best performance from each. Since welldesigned power amplifiers-which were the subject of my article—are essentially audibly perfect within their power ratings, Mr. Duncan's mix-and-match approach is chasing a wild goose up a blind alley. Incidentally, the only "responsible" highend reviewers that I know about write for The Audio Critic, mentioned last month.

As to my inexperience in critical listening, I became an avid audiophile in the early 1950's when hifi equipment first became available in the U.S. For five years I worked as

a technician for an electronics kit manufacturer, where I made tests, did repairs, and handled the technical correspondence on my employer's kits that included hi-fi kits. In the evenings and on weekends I "moonlighted" as a freelance hi-fi serviceman.

After being a technical editor at Popular Electronics for two years and a similar magazine for another two years, I became the technical editor of Stereo Review, where I was in charge of its equipment-testing program for about 20 years. During that time I auditioned countless products in my home and office listening room.

Moreover, I was invited to visit the test laboratories and factories of audio equipment manufacturers in England, Germany, Japan, Denmark, Hungary, Austria, Canada, and the U.S. during that 20-year period. At all those locations I was asked to evaluate the sound of their products (mostly loudspeakers), and I frequently was able to validate my responses against objective test data.

I do not "confide" in salesmen, rumor[monger]s, and "wannabes." However, I know many product engineers and audio researchers—and guess what—most of them agree with me that, in general, CD's do sound better than LP's—if only for their superior signal-to-noise ratio.

It's always good to hear from a fan.—Larry Klein

# AN AUDIO/VIDEO-PHILE

I recently discovered *Electronics* Now, checked out every back issue from my public library branch, and spent many rewarding hours reading each one from cover to cover. I can't follow everything yet, but I expect that will come with time.

On a general note, I enjoyed Larry Klein's debunking of some of those outrageous claims from audiophiles. I now have an authority to quote when I say that I cannot discern any significant difference between my \$5000 equipment and the \$20,000 worth of equipment that is supposedly being installed in average 18 ×15-foot American living rooms.

I haven't seen one subjective aucontinued on page 70

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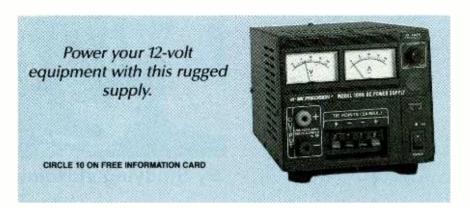
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# EQUIPMENT REPORTS

# B+K Precision Model 1686 DC Power Supply



hether powering a prototype circuit or providing power for equipment being serviced, the bench-top DC power supply is an essential tool for anyone in the electronics industry. It's also essential for any anyone who plays an active role as an electronics hobbyist. B + K Precision (6470 W. Cortland St., Chicago, IL 60635) has recently introduced the *Model 1626*, a supply that is ideal for powering equipment rated at 12 volts.

The 1686 can deliver an output from 3 volts to 14 volts DC with a maximum current of 12 amperes. That high current rating is sufficient to power most car stereo systems, even those with high-power amplifiers. Most mobile amateur radio equipment, as well as CB transceivers, marine radios, and other high-current automotive accessories can be powered safely from the 1686.

The maximum output current available from the power supply is proportional to the output voltage. When the supply is set to deliver 13.8 volts—which is the operating voltage for most equipment nominally rated at 12 volts—the 1686 can deliver 12 amperes continuously to the load. That drops to 10 amperes at 12 volts, 4.5 amperes at 5 volts, and 2.5 amperes at 3 volts.

At all voltage settings, the specified load regulation is less than 0.8% That is, regardless of the load

at the output terminals, the supply's output voltage will deviate less than 0.8% from its initial setting. The line regulation of the supply is also rated at 0.8% from 108–132 volts AC. That means that regardless of the change in the line voltage to which the supply is connected, the output voltage will deviate less than 0.8%. The ripple and noise is specified at less than 10 millivolts rms. Overload current limiting provides protection against excessive overload or short-circuit output.

The 1686 is housed in a black metal cabinet that measures about  $5\frac{1}{2} \times 6 \times 12$  inches; it weighs just over 12 pounds. The front panel features a pair of easy-to-read analog meters along the top edge, one for voltage and the other for current—that provide an indication of what the supply us doing at a glance. To the right of the meters is a rotary knob that controls the output voltage. The bottom half of the panel contains two sets of output connectors, a power switch, and two LED indicators.

The main voltage-output is provided on a set of binding posts. Two sets of spring-loaded terminals—much like the kind commonly found on audio speakers—are provided for connecting low-current loads. The tie points can supply a maximum of 2 amperes. Above the power toggle switch is an LED that serves as a power-on indicator. Above that is an LED that indicates

that the supply is in an overload condition and has reduced its output voltage.

The rear panel contains a fuse holder and a small fan. The fan, which helps to keep the supply compact by reducing the size of the heatsinks needed, does not run constantly. Rather, it is controlled by a thermostat, and comes on only when the internal temperature of the supply is too high for safe operation.

The outputs of the supply are isolated from the chassis and earth grounds, which is essential for flexibility in connections. If required, for example, the positive output can be connected to ground for powering positive-ground automotive equipment.

The isolated outputs also allow multiple supples to be connected together in series or parallel for powering equipment that has higher voltage and current requirements. For example, connecting two supplies in parallel will provide a continuous source of 24 amperes, while connecting two supplies in series will provide an adjustable 6 to 28-volt power supply.

The model 1686 can operate from either 120-volt or 230-volt AC power lines with frequencies of 50 or 60 hertz. A slide switch on the bottom of the chassis permits easy selection.

We found the operation of the model 1686 to be quite straight-forward. The manual supplied with the supply was more than adequate, and we were happy to find that calibration instructions were included there.

B+K Precision has priced its model 1686 at \$199. We think that the supply is ideal for service shops that regularly repair mobile equipment, as well as for retailers who need to power equipment on display. Of course, radio amateurs will also appreciate the 12-ampere continuous duty rating.

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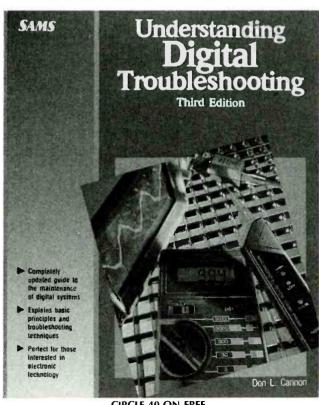
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WAVETEK INSTRUMENTS DIVISION 9045 Balboa Ave., San Diego, CA 92123

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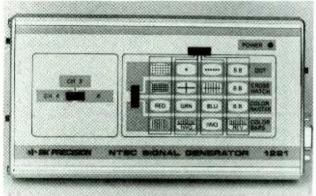


# NEW PRODUCTS

Use the Free Information Card for more details on these products.

HANDHELD NTSC COLOR GENERATOR. A television/ video signal generator small enough to fit into a field-service kit is now available from B+K Precision. The Model 1221, said to offer the same capabilities usually found only in bench models, generates 14 patterns of stable video signals for testing, servicing, and adjustment of TV's and other video equipment.

The generator's patterns include standard NTSC color bars (with and without IWQ), full-field IWQ, split-field color bars with reverse bars and red. green, blue, and black rasters. It also offers six convergence patterns. For monochrome tests, the chroma can be turned off to display the luminance level only. A 1-kHz subcarrier audio tone can also can be switched on or off.



CIRCLE 16 ON FREE INFORMATION CARD

Generator outputs include composite video. IF (45.75 MHz, crystal-controlled), and CH3 and CH4 (crystal-controlled). For AC adapter or an external testing CGA computer 12-volt DC to 18-volt DC monitors, a 9-pin D-type connector provides an RGB output. The user can select either interlaced or progressive scan, TTL or low-level (analog level) for RGB outputs.

housed in a rugged, lightweight aluminum case that acts as an RF shield. It can be powered by the included source.

The Model 1221 NTSC color signal generator is priced at \$369.

**B** + **K** Precision Chicago, IL 60635 Phone: 312-889-1448 The Model 1221 is Fax: 312-794-9740

printer interface, and display backlighting.

The price of the ScopeMeter Model 93 is \$1350, the Model 95 is \$1650, and Model 97 is \$1950. Upgrades of earlier ScopeMeter's are \$155.

John Fluke Mfg. Co., Inc. P.O. Box 9090 Everett. WA 98206 Phone: 800-44-FLUKE

# SCOPEMETER. Fluke's upgraded ScopeMeter combines a 50-MHz, 25megasamples per second dual-channel digital storage oscilloscope with a digital multimeter. It has been given a Version 4

**UPGRADED 90 SERIES** 

software upgrade. This ScopeMeter includes a lot of new features intended to improve its flexibility and "user friendliness." They include percent duty-cycle measurements for pulse-width modulated signals in control circuits, 30-ohm range, and 0.01-ohm resolution

for tracing elusive shorts. Other new features include a "time stamp" to mark the occurance of minimum and maximum values, waveform inversion on both channels for easier calculations, and increased frequency-counter resolution.

The upgrade also includes circuitry that returns the instrument to previous settings when changing between the meter mode and the scope mode. Additional record functions are included, and there is continuous meter-mode display of voltage, frequency, and duty cycle. A smart

trigger algorithm allows hands-off duty-cycle measurements of pulse-width modulated motor-control waveforms.

The three ScopeMeters (Models 93, 95, and 97) offer oscilloscope and digital multimeter functions. They all include such features as autoset, waveform and setup memory, combined display of meter results and waveforms, and convenient menus. The Model 97 also features a built-in signal generator, a component tester, and remote control through an optically isolated RS-232 interface,



Foil-shielding tapes are now available from 3M in convenient kits. Each kit contains 3M's full line of shielding tapes organized in a compact dispenser box. The Scotch brand tapes are intended for reliable point-to-point electrical contact. Examples of applications include EMI/RFI shielding, grounding, and electrostatic-charge draining.

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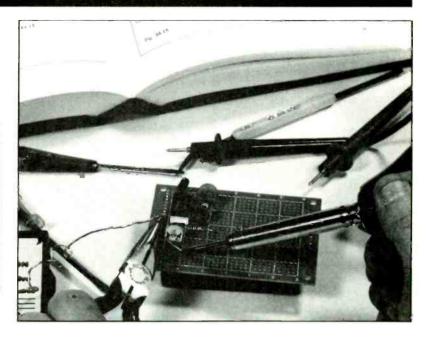




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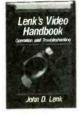




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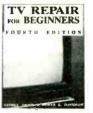


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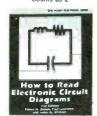
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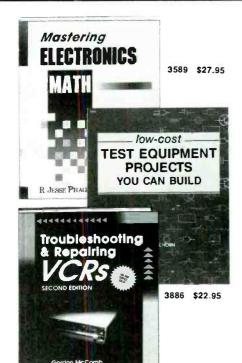
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four-yard-long rolls include one each of: 1170 (aluminum), 1181 (copper), 1182 (double-coated copper), 1183 (tin-alloy-coated copper), 1194 (copper), 1245 (embossed copper), 1267 (embossed aluminum), and 1345 (embossed tin-alloycoated copper). Replacement rolls are available from the same source as the kits.

The kit simplifies the task of finding the right tape when it is needed. The  $4 \times 4 \times 7.5$ -inch container **Phone:** 602-244-4597 is labeled with useful tech- Fax: 602-244-4597 nical and applications information about the tapes: product number, backing, adhesive type and thickness, adhesion, resistance, and shielding effectiveness.

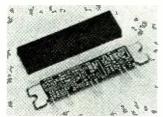
**3M Electrical Specialties** Division **Building 130-3N-56** 6801 River Place Blvd. Austin. TX 78726-9000 Phone: 1-800-328-1368.

900-MHz RADIO POWER MODULE. Motorola has introduced 7.5-volt RF power modules that operate in the 806-940-MHz frequency range with an input power of 1 milliwatt and an output power of 4 watts. The MHW804 Series is intended for cellular telephone, trunking, or other two-way radio systems.

The series includes two modules that differ only in operating frequency band. Both are packaged in cases less than 1/2--inch wide. According to

Motorola, the modules are exceptionally stable, rugged, low in harmonics, and have wide dynamic ranges.

The MHW804-1 operates in the 800 to 870-MHz range, and the MHW-

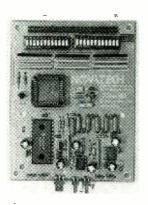


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804-2 operates in the 896 to 940-MHz range. The MHW804-1 is priced at \$50.82 and the MHW-804-2 is priced at \$52.36 in 1 to 399 quantities.

Motorola, Inc.—E114 5005 East McDowell Road Phoenix, AZ 85008

DIRECT DIGITAL SYN-THESIZER KIT. This direct digital synthesizer from Novatech can produce output signals up to 12 MHz. The DDS-3 direct digital synthesizer kit can be programmed to produce sine and TTL/CMOS-compatible signals from 2 Hz to 12 MHz in 2 Hz steps. Its output frequency is set with a 23-bit binary word introduced by DIP switch or ribbon cable.



**CIRCLE 20 ON FREE** INFORMATION CARD

The synthesizer's output amplitude is 1.4 volts peakto-peak into an open circuit. Fast switching of the output frequencies can be obtained because the transition time for changing frequencies is less than 250 nanoseconds. Spectral purity is specified as better than -90-dBc phase noise at 1-kHz offset, -45-dBc spurious, and -40-dBc harmonic.

Stability is specified as better than 10 ppm. The DDS-3 is powered by  $\pm$  5volt DC power. The kit includes a  $3.5 \times 4.5$ -inch printed circuit board and all necessary parts.

The DDS-3 kit is priced at \$119.95 plus \$5 for shipping and handling.

Novatech Instruments, Inc. 1530 Eastlake Ave. E., Suite 303 Seattle, WA 98102

Phone: 206-328-6902 Fax: 206-328-6904

CELLULAR NOTEBOOK

LINK. A prominent Finnish electronics manufacturer has introduced its Cellular Notebook Link, Nokia designed the link for use with Compaq notebook computers equipped with the SpeedPAQ 144 modem



**CIRCLE 21 ON FREE INFORMATION CARD** 

and Nokia 121 cellular phones. The link permits data and fax transmissions to be sent and received over a cellular network.

The interface is a coiled cable with a quick-release data cradle that holds the phone while it is in the fax/ data mode. That design eliminates the separate interface box required in most mobile data installations. The link needs no external battery because the interface is powered by the phone's battery and the computer's internal power source.

When used with the Compag SpeedPAQ 144 modem, the Cellular Notebook Link transmits data at 4800 bits per second. However, if the data is compressed. Nokia says the data throughput will exceed 11,000 bps. Fax transmissions are sent and received at 9600 bps.

Nokia Mobile Phones, Inc. 2300 Tall Pines Drive P.O. Box 2930 Largo, FL 34649-2930

Phone: 813-536-5553 Fax: 813-530-7245

STANDBY POWER SUP-PLIES. Perma Power Electronics is offering a series of standby power systems for backing up computers and peripherals if power fails. WatchDOS supplies can be used with any DOSbased computer or network, but cannot be used with Windows or memorymanagement software. Each system includes a "Hibernate" software utility program.



**CIRCLE 22 ON FREE** INFORMATION CARD

When AC-line power fails, the software detects a signal from the backup power supply, transfers conventional, expanded, and extended memory and

The 400-VA Model DPS-4001 is priced at \$299 and the 600-VA Model DPS-600L, for single personal-use 386 computers, has price of \$375. The 800-VA Model DPS-800L, for office 386 and 486 computer systems, has a price of \$489

Perma Power Electronics, Inc.

5601 West Howard Avenue in a briefcase. Niles, IL 60714 Phone: 708-647-9414 Fax: 312-763-8330

CW TRANSCEIVER. This 5watt, 20-meter CW transceiver covers the 14.000to 14.075-MHz band, MFJ Enterprises' MFJ-9020



### **CIRCLE 23 ON FREE** INFORMATION CARD

compact transceiver measures only 2.25  $\times$  6  $\times$  6.5 inches. It has a sharp, 8pole crystal filter, 500-Hz bandwidth, and Vernier tuning. The tranceiver has a 5-watt transmitter, a superheterodyne receiver, audioderived AGC, CW sidetone, and a built-in speaker with an earphone jack. The MFJ-9020 is powered from 12 to 15 volts DC, and it fits

The price of the MFJ-9020 CW transceiver is \$179.95.

MFJ Enterprises, Inc. P.O. Box 494 Mississippi State, MS

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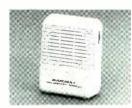
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# ULTRASONIC CLEANER



# Build a professional-quality ultrasonic cleaner and keep hardto-clean connectors, parts, and tools spic and span.

### REINHARD METZ

ULTRASONIC CLEANING HAS BEEN commonplace in commerce and industry for years, particularly for cleaning small, convoluted parts that would be a difficult or impossible to clean otherwise. Items that are routinely cleaned ultrasonically include machine parts, standard and microminiature tools and connectors.

Factory-made ultrasonic cleaners are still too expensive for the average consumer and hobbyist. But with the drawings, photos, and text in this article, you can build your own ultrasonic cleaner. You have options in building this ultrasonic cleaner. You can build the complete system with microprocessor-based time and temperature controls, or you can build only the basic model with on-off controls. You'll be surprised at the low-cost of the parts, regardless of the option you choose. The basic specifications for the ultrasonic cleaner are given in Table 1.

Only non-toxic, non-flammable solutions will be needed to do effective cleaning with this ultrasonic cleaner. You'll be able to clean many different kinds of household or shop objects that are hard to clean-or, in the past, have just been too much trouble to clean well with conventional methods. Those objects include jewelry, kitchen utensils, circuit boards, bicycle and auto parts, and tools. What is more, you can do all your ultrasonic cleaning indoors—you don't have to go into your garage or backyard to keep noxious fumes out of your house.

# Ultrasonic cleaning

The basis for ultrasonic cleaning is a bubbling action in a fluid called *cavitation*—millions of tiny bubbles forming and collapsing within the cleaning solution do the scouring. You have probably seen the cartoons of thousands of cleaning bubbles at work on the TV com-

mercials for bathroom cleaners. The big difference here is that with our cleaner, the bubbles are created ultrasonically by piezoelectric transducers, not by the solution itself.

The disk-shaped piezoelectric transducers are bonded to the underside of the cleaning pan. The dimensions of these barium-titanate ceramic disks change continuously in response to high-frequency signals applied across their sensitive surfaces. These transducers are similar to those used

# TABLE 1 LEADING SPECIFICATIONS FOR THE ULTRASONIC CLEANER

Transducers piezoelectric
Operating frequency
Cleaning pan capacity
Microcontroller
Timing range\*
Solution temperature
w/heater\*

Power requirement

piezoelectric
40 to 60 kHz
3/4 gallon
Intel 8751
1 to 99 min.
25 to 99°C
Power requirement
117-V AC, 60 Hz

\*Optional feature

33

in marine depth finders.

The compression and expansion of the crystalline transducers is coupled mechanically through the bottom of the pan to create the cavitation bubbles in any cleaning solution that you use. (For a complete description of the piezoelectric effect, refer to page 46 of the January 1993 *Electronics Now*).

If the cleaning solution that you select is a recognized solvent for the contaminants that you expect to find on the parts to be cleaned (for example, oil or grease), the ultrasonic cleaner will enhance the cleaning action of that solution.

# Description of the cleaner.

The ultrasonic cleaner has three main parts: a stainless steel pan with two transducers attached, a large circuit board containing the power oscillator and time-and temperature-control circuitry, and a small switch/display circuit board containing the control switches and LED displays.

The large circuit board (approximately 5 ×8 inches) is shown in Fig. 1. The left side of the board is occupied by the power transistor amplifier for the oscillator and its heat sink. The oscillator, made up of components on the board, supplies a 40- to 60-kHz, 1000-volt sinewave to the piezoelectric transducers. The large objects in the center of the board are the two transformers—one standard and one special. The microcontroller and other IC's are located on the right side of the board.

All of the switches are located on the smaller (approximately 2 ×5-inch) PC board shown in Fig. 2. They include, from the left, the on-off power switch, the time up-down toggle switch, the temp up-down switch and the start pushbutton. The green two-digit, seven-segment display on the left indicates time, and red one to its right indicates temperature.

Figure 3 shows the stainless steel cleaner pan upside down with the two piezoelectric ceramic transducers (white disks) bonded to a stainless steel plate

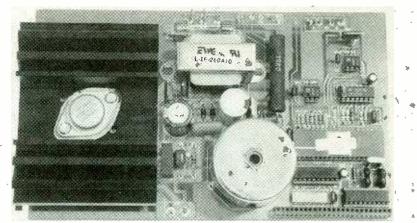


Fig. 1—CIRCUIT BOARD CONTAINING power oscillator and microcontroller-based time and temperature control circuitry.

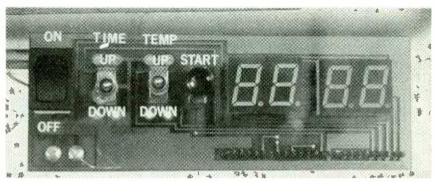


FIG. 2—CIRCUIT BOARD CONTAINING the manual operating control switches and LED time and temperature digital displays

which, in turn, is bonded to the pan bottom. The plate transmits the vibrations from the transducers more uniformly through the bottom of the pan to the cleaning solution, and it helps to protect the brittle transducers from damage that might be caused by objects accidentally dropped into the pan.

The ultrasonic cleaner will work very well without the time and temperature circuitry, but building them should be interesting, and they will add value to the cleaner. The controls will be especially useful if you plan to heat the cleaning fluid, and want to set time limits for the cleaning action on specific objects. Moreover, the controls will shut the unit off automatically.

Both time and temperature are programmable—time from from 1 to 99 minutes, and temperature from 25° to 99° C. The time and temperature functions are controlled by an Intel 8-bit CMOS 8751 microcontroller, which you can program or purchase already programmed.

### Driver circuit

Refer to the right side of the two-page schematic diagram Fig. 4. The amplifier in the transducer oscillator driver is a Hitachi 2SC1922 bipolar power transistor, Q1. The oscillator tank circuit is formed by the inductance the secondary winding of transformer T1 and the effective capacitance of transducers RES1 and RES2. Bridge rectifier BR1 and capacitor Č1 form a 160-volt DC power suppy operated from the 120-volt, 60-Hz line. Resistor R1 provides the base bias for Q1, through the feedback winding of T1.

As Q1 turns on, current flows through the primary of T1, which generates an opposing voltage in its feedback winding, tending to turn Q1 off again. At the parallel-resonant frequency of the tank circuit, made up of the secondary of T1, RES1 and RES2, the phase shift between the base and collector of Q1 is exactly 180°, which is necessary for circuit oscillation. The winding ratios of T1 determine the

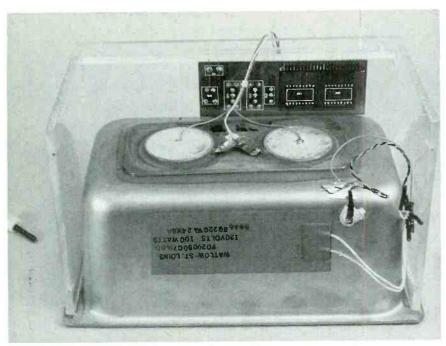
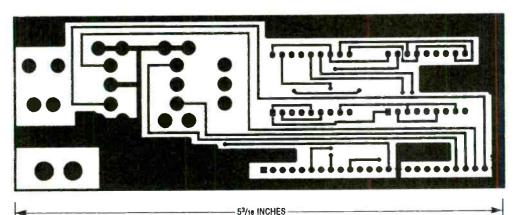
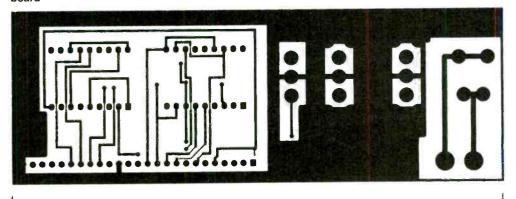


FIG. 3—VIEW OF INVERTED CLEANER PAN with two piezoelectric transducers mounted on it. The back of the control/display board is shown in the background.



THE FOIL PATTERN FOR THE FRONT (component) side of the switch/display circuit board



53/16 INCHES

THE FOIL PATTERN FOR THE REVERSE (solder) side of the switch/display circuit board.

output voltage, and thus the voltage applied to the two transducers.

The input supply voltage is 160 volts DC, and the turns ratio is about 5 to 1, so the output voltage is about 1000 volts peak-to-peak. In addition, the DC startup current provided by RI and C2 is the AC drive current for Q1. Resistor R2 and capacitor C3 supress spurious oscillations at frequencies other than the tank's primary resonant frequency.

As the drive voltage across the transducers swings through the 1000-volt peaks, the transducers expand and contract across their thickness dimensions, and their vibrations are coupled through the pan walls to the cleaning solution.

## Time and temperature control

The CMOS8751 microcontroller, IC1, is the key component of both time and temperature controls. It responds to input from the START button, TIME UP-DOWN switch, TEMP UP-DOWN switch, and the

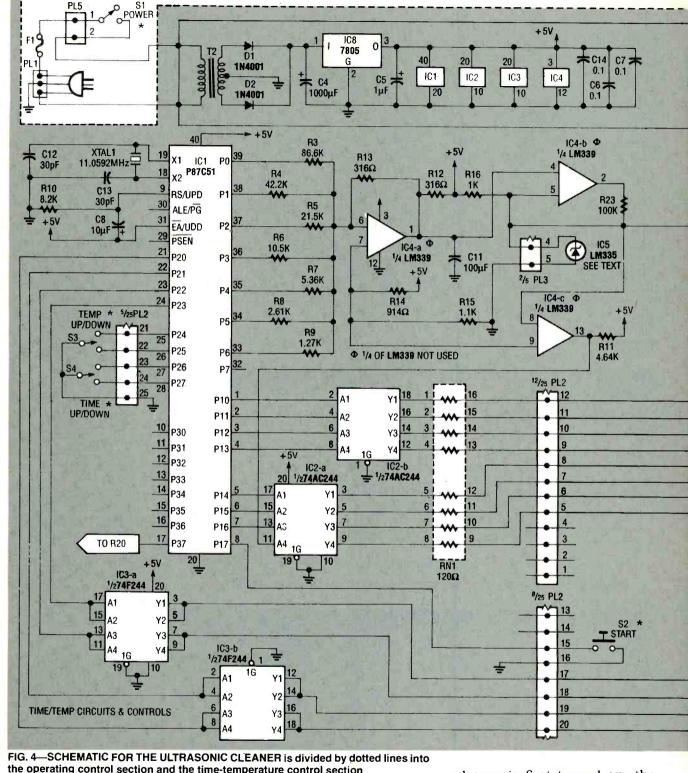
temperature-sensor circuit. It provides the drive signals for the two-digit time and two-digit temperature LED displays, the transducer power Triac Q2, and the heater Triac Q3.

An assembly-code listing for the Intel 8751 firmware is available from the address given in the Parts List or from the R-E BBS (516-293-3000; 1200/ 2400 baud 8, N, I). The program consists of a loop. whose time corresponds to the multiplex rate of the LED displays. Each time the loop is traversed, one of the four digits is enabled; the loop rate is sufficient to eliminate display flicker. Within the loop, inputs are checked and various time, temperature, and display variables are The updated. switches provide direct input through

Electronics

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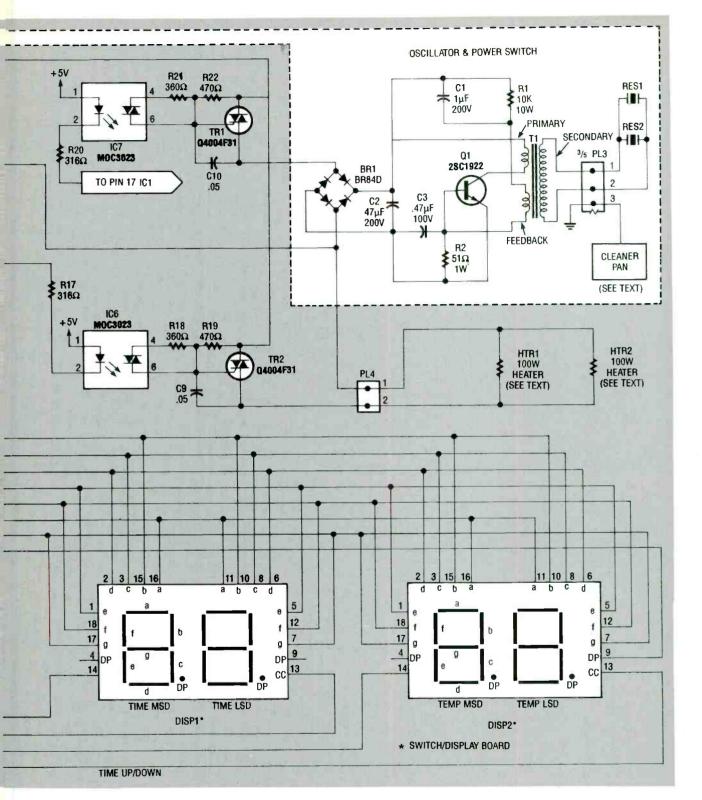


the operating control section and the time-temperature control section

the I/O port.

Temperature is registered in binary format, and it is converted from a digital to an analog signal by resistor string R3 through R9 and IC4-a. This analog signal is then compared with the pan temperature signal from IC5 by IC4-b. When solution temperature falls below the selected threshold, IC6 turns on to energize Q3, which provides current to pan heaters HTR1 and HTR2. When the cleaner is first turned on, the temperature is automatically reset to 25 degrees C. Whenever heat is on, the decimal point of the temperature display LED is turned on.

The timer circuit or function depends on the internal timing capabilities of the 8751, IC1.



When the START button is pressed, Q2 is energized, powering the transducers. The internally registered time is decremented and displayed, and when zero time is reached. Q2 is turned off and the original time is reset. When the cleaner is turned on, the time is set auto-

matically to 5 minutes, but this setting can be adjusted up or down.

Finally, multiplexed segment and digit drive is provided to the displays by IC2, IC3, and current is limited by the eight 120-ohm resistors in network RN1. Power for the control section is

provided by T2, D1, D2, and 5-volt regulator IC8. Further details of the firmware operation can be found by reading the code comments.

# Circuit board assembly

Refer to Fig. 4, the two-page schematic for the complete ul-

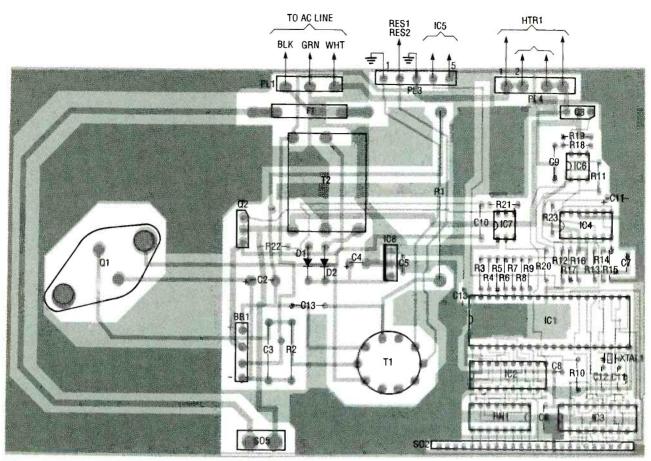


FIG. 5—PARTS PLACEMENT DIAGRAM for large circuit board.



FIG.6—PARTS PLACEMENT DIAGRAM for switch/display circuit board.

trasonic cleaner. A boundary on the schematic separates the oscillator and power switch circuit from the time and temperature circuits and controls. This permits you to distinguish between the basic circuitry needed to operate the cleaner and the time and temperature control circuitry.

Note that both circuit boards are two-sided. Foils for the parts placement and solder sides of both boards are included here. Making these boards might prove to be a challenge if you have not had much experience fabricating printed circuit boards of this complexity. Therefore, both boards complete with solder masks and through-hole plating are offered in the Parts List.

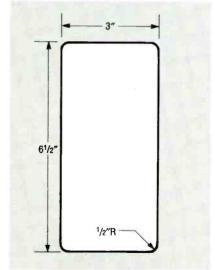


FIG. 7—OUTLINE FOR THE TRANS-DUCER MOUNTING PLATE to be cut from 0.063-inch stainless steel plate.

Refer to Fig. 5, the parts placement diagram for the large board circuit board. The order of component placement on this circuit board is not critical—whether or not you plan to include the time/temperature circuitry and control switches.

The only component on that board not available as a standard catalog item is transformer T1. You can purchase transformer T1 from the same source given in the Parts List or you can wind your own if you choose to do so.

If you choose to wind your own transformer T1, it will be necessary for you to obtain a ferrite core and Litz wire. The core in the prototype is a Ferroxcube 4229-PA275 ferrite core obtainable from Philips Components Discrete Products, Saugerties, NY 12477. The primary winding has 20 turns of 21 strand/36 AWG Litz wire and the secondary has 99 turns of the same wire. Feedback is obtained with 3½ turns of No. 22 AWG wire.

Be sure to double check the values of all the components as you insert them. Power transistor Q1 is positioned on top of the heatsink as shown in Fig. 1, and both parts are fastened to the board with screws at the same time. Insulate Q1 from the

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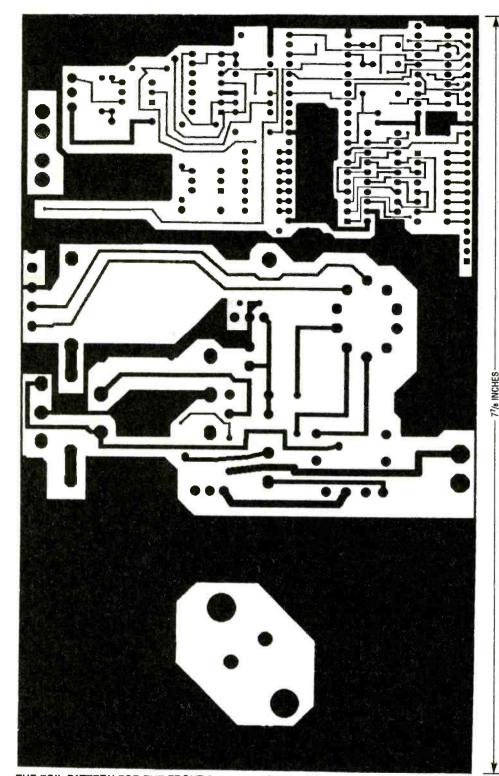






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heatsink with a mica insulator coated liberally with heatsink grease. After mounting Q1, check its isolation with a meter to be sure that it really is insulated from the other components or conductors.

Mount transformer T1 by the lugs on its frame and connect

its wires individually as indicated in Fig. 4. If you plan to build the cleaner without the time and temperature controls, the positions for those components will remain open. The precision temperature sensor, LM355, (IC5) will be epoxied on the bottom of the stainless steel pan.

and be connected to the board by a twisted pair of wires at

Sockets are recommended for all DIP-style IC's (IC1, IC2, IC3, IC4, IC6, IC7), particularly the microcontroller. IC1. Insert all resistors, capacitors, plugs (three-pin plug, PL1; five-pin plug, PL3; and fourpin plug, PL4), sockets (25-pin socket SO2 and two-pin socket SO5, resistor network, rectifier bridge, Triacs and diodes. Solder all leads and trim excess lead lengths. Examine the circuit board closely to be sure there are no accidental solder bridges or cold joints.

Refer to the parts positioning diagram, Fig. 6, and insert the three switches (S1-S3). the sockets for the two dual-digit, segmented LED displays, DISP1 and DISP2, and the right-angle, 25-pin header PL2. Solder all leads and trim excess. Again, check for inadvertent solder bridges or cold solder joints before inserting the dis-

plays.

# Transducer plate and tank

Start the assembly of the tank and transducers by cutting out a  $+3 \times 6\frac{1}{2}$ 

inch rectangle from 0.062-inch stainless steel plate as shown in Fig. 7. Round the corners to 1/2inch radiuses, deburr all edges, and sand or grind both sides so the plate will lie flush against the bottom of the stainless steel

Next, prepare both trans-

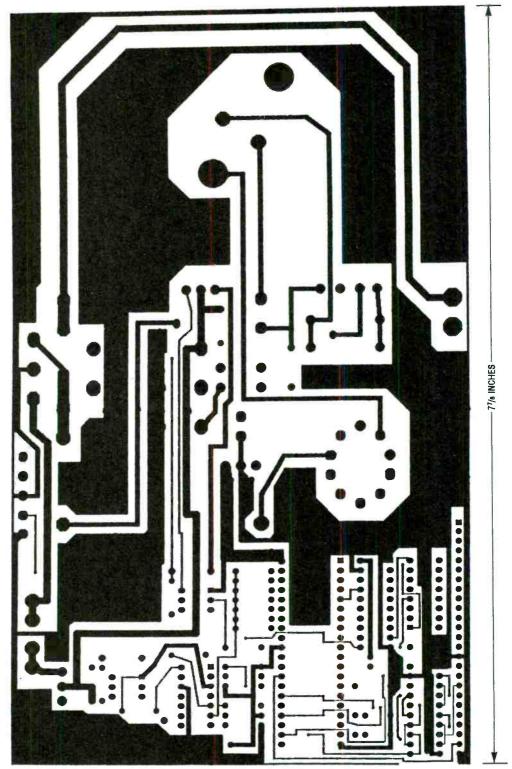
ducers, RES1 and RES2, for wire attachment by cleaning their surfaces with alcohol or other suitable solvent. Strip about 1/4inch of insulation from both ends of a pair of 24 to 26 AWG multistrand hookup wires approximately 12 inches long for transducer connection. Flatten the wires by fanning out their stranded ends, and tin the strands with leadtin solder.

Carefully solder the fanned out strands of one wire to the centers of each transducer as rapidly as possible to prevent overheating and damaging the ceramic transducer. Then solder a copper wire, approximately 3 inches long to connect the reverse sides of the transducers, observing the same precautions about soldering.

Note: the transducers are polarized, and both must have the same polarity on top and on the bottom. If this is not observed, the opposing vibrations of each transducer will cancel the effect of the other one.

After the wires are soldered to the transducers, the next step is to bond the transducers to the rectangular transducer mount-

ing plate. Refer to Figs. 3 and 8 to see how the transducers are positioned on the plate. Mix the two parts of a high quality, slow-setting epoxy and apply a film of it to the plate. Position the transducers on the plate, and while applying slight pressure, rotate them slightly so that



THE FOIL PATTERN FOR THE REVERSE (solder) side of the main circuit board

some epoxy underneath the transducers is squeezed out to form a bead of epoxy around the edges of the transducers where they contact the plate.

When the epoxy holding the transducers has set, apply epoxy to the transducer plate assembly and cement it to the

bottom of the tank, also as shown in Figs. 3 and 8. If you intend to include the optional temperature control, adhere the two heating elements, HTR1 and HTR2, to the sides of the pan (one is shown in Fig. 3.) Solder or crimp sleeves to the ends of the heater wires. Solder a

twisted pair of hook-up wire approximately 12 inches long to the LM335 temperature transducer (IC5) and solder or crimp sleeves to the other ends of the four wires. Epoxy temperature sensor IC5 to the bottom of the pan as shown in Fig. 8. Mark the wires to identify their polar-

Final wiring and assembly

There are no requirements for the ultrasonic cleaner case. You can make one by assembling a box from 1/4-inch sheet plastic or you can purchase a small  $6 \times 6$ ×9-inch plastic storage bin from your neighborhood hardware or houseware store. The bin will work very well as a protective case.

Pass the bare ends of the three-wire line cord terminated with a three-prong plug through the grommeted hole in the case. Strip the ends of the wires for soldered or crimped sleeves to connect them to three-pronged plug PL1, observing the ground wire. The on-off switch on the switch-display board will perform the switching function when the small board is plugged into the large board through plug PL5.

Install fuse F1 in its holder, and place the large circuit board in the case. Connect the transducer, heater, and temperature transducer wires by pressing their terminating sleeves over the header pins as shown in Fig. 8. Plug the switch/display board into the sockets SO2 and SO5. Carefully check all component values and placement, and all wiring against the schematic, Fig. 4, before carrying out the test and checkout procedures. Make any corrections necessary.

Before operating the ultrasonic cleaner, check to be sure that the pan is grounded to the line cord ground and the primary of transformer T1 is isolated from its secondary and tank circuit.

#### Test and checkout procedure

Temporarily support the tank next to the circuit board. Fill the pan at least half full with water. Caution—Never operate the

#### **PARTS LIST**

All resistors are 1/4-watt, metalized film, 5 % unless otherwise stated.

R1-10,000 ohms, wirewound, 10 watt

R2-51 ohms, wirewound, 1 watt

R3-86,600 ohms

R4-42,200 ohms R5-21,500 ohms

R6-10,500 ohms

R7-5300 ohms

R8-2610 ohms

R9-1270 ohms

R10-8200 ohms

R11-4640 ohms

R12, R13-316 ohms

R14-914 ohms

R15-1100 ohms

R16-1000 ohms

R17, R20-316 ohms

R18, R21-360 ohms

R19, R22-470 ohms

Capacitors

C1-1µF, 200 volt, polyester film

C2-47µF, 200 volt, polyester film

C3-0.47 µF, 100 volt, polyester film C4-1000 µF, 15 volt, aluminum elec-

trolytic

C5-1µF, 15 volts, aluminum electrolytic C6, C7, C14-0.1µF, polyester film C8-10 µF, 15 volts, aluminum elec-

C9, C10-0.05 µF, polyester film

C11-100muF, 15 volt, aluminum elec-

trolytic C12, C13-30 pF

Semiconductors

IC1-87C51 CMOS microcontroller with EPROM, Intel or equiv.

IC2-74AC244PC octal bus driver, noninverting, National or equiv.

IC3-74F244 octal bus driver, non-inverting, National or equiv.

IC4-LM339 quad comparator, National

or equiv. IC5—LM335 temperature transducer, National or equiv.

IC6, IC7-GE3023 optoisolator, Harris

or equiv. IC8-LM340TS (7805) voltage regulator, 1A, Motorola or equiv.

Q1-2SC1922 power transistor, Hitachi or equiv.

Q2, Q3-triac, Teccor Q4004F31 or equiv.

D1, D2-1N4001 silicon diode

DISP1—LN526GA 7-segment LED display, Panasonic or equiv.

DISP2—LN526RA 7-segment LED display, Panasonic or equiv.

BR1-BR840, full wave rectifier bridge, Diodes Inc. or equiv.

RN1-eight 120 ohm resistor network, CTS9043 or equiv.

cleaner unless the pan is at least half full of liquid. Apply power, and turn on the cleaner. You should hear a hissing sound from the pan and you should be able to feel the vibrations with your fingertips on Other component

F1-fuse, 6 ampere, standard HTR1, HTR2-100 watts, 120 volts,

Watlow FO20050C7 or equivalent

S1-switch, rocker, panel-mounted S2-switch, miniature toggle, momentary SPST, panel-mounted

S3, S4-switch, miniature toggle, momentary SPDT, panel-mounted

XTAL1-11.0592 MHz crystal holder T1-transformer, custom wound (see text)

T2-transformer, EWC Inc. EL-16-260A10 or equiv.

P1-three-pin header

P2-25-pin right-angle header

P3-five-pin header

P4-four-pin header

P5-two-pin header

SO2-25-pin socket

SO2-2-pin socket

RES1, RES2-piezoelectric transducers, ceramic, 2-inch, Vernitron

56786 PZT-4 or equiv.

Miscellaneous: large and small circuit boards, stainless steel tank (6% × 41/4 × 4 inches, Polarware No.E904 or equiv.), Anodized aluminum heat sink,  $(4 \times 3 \times 2 \text{ inches})$ , transducer mounting plate (see text), mica insulator for a bipolar power transistor, thermal conductive grease, sockets for IC1, IC2, IC3, IC4, IC5, IC6, IC7, three-wire power cord with 3-prong plug, line cord grommet, fuse holder, case (see text), hookup wire, wire sockets, epoxy, solder.

Note: The following parts are available from A&T Labs, P.O. Box 4884, Wheaton, IL 60187:

 Kit of parts for the ultrasonic cleaner without time and temperature controls/displays or case, \$169.00

· Kit of all parts for the complete ultrasonic cleaner including programmed 8751 microcontroller except case, \$249.00

 Double-sided printed circuit boards-large, \$25.00; small, \$9.00

 Programmed Intel 8751 microcontroller, \$29.00

 Custom-wound transformer T1, \$69.00

 Ceramic piezoelectric transducers RES1 and RES2, \$32.00

 Stainless steel cleaner pan, \$19.00 Add 6% shipping and handling on all orders paid for by check or money order. Add 10% shipping and handling on all COD orders (U.S. only) via UPS. Illinois residents add 6.75% state sales tax. For all correspondence please include a stamped, self-addressed envelope.

the edge of the pan. If you do not hear or feel these operating indications, check for the presence of the primary 160 volts at C1, and +5 volts at C5.

When testing, remember that the primary circuit is connected

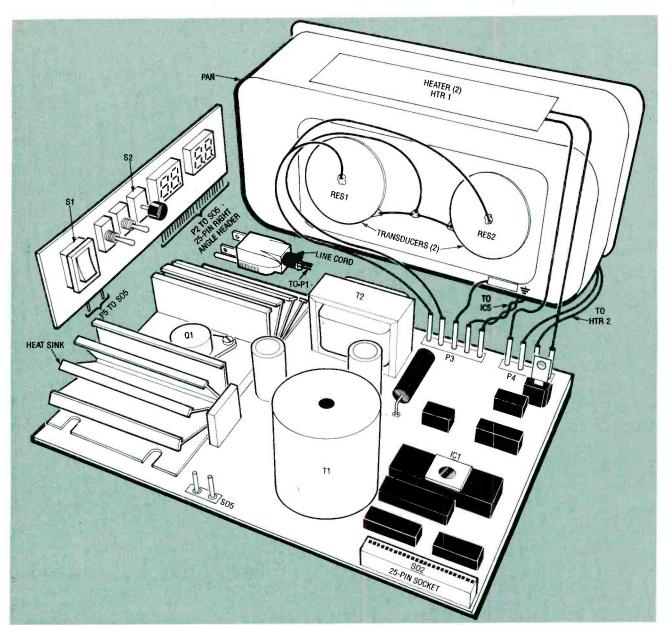


FIG. 8—EXPLODED VIEW showing wiring connections between the main circuit board to the piezoelectric transducers, pan heaters, and temperature sensors mounted on the pan.

to the 120-volt power line, so exercise caution to avoid electric shock. Also, the voltage applied to the transducers is about 1000 volts. If the unit fails to function at turn-on, check for the presence of 11 MHz at pin 18 of the microcontroller IC1, and look for changes in the time and temperature display LED's. At turn-on, those digital displays should readout 5 and 25, respectively.

Although the design frequency should be close to optimal, further adjustment could improve efficiency. Perform any additional tuning by turning the

slug core of transformer T1. Adjust it gradually until you are able to observe maximum turbulence in the cleaning fluid. One way to determine a maximum is by adding a drop of food coloring to the water, and adjusting for maximum dispersion rate of the color in solution.

#### Cleaner operation

You can purchase cleaning fluids from hardware, auto parts, and grocery stores, but you can also easily mix your own. You might want to experiment with cleaning mixtures. A general rule of thumb is that

any cleaning solution that works satisfactorily in cleaning objects by hand methods will also work in the ultrasonic cleaner. Liquid detergent in water, for example, is a good general cleaner, while ammonia in water works well for jewelry. Carburetor cleaner cleans carburetors and other automotive, bicycle or machine parts that are coated with oily or greasy contaminants.

Before cleaning any object in the ultrasonic cleaner, it is a good idea to remove as much surface dirt and grime as possible manually with paper towels, brushes, or cotton rags to minimize the contamination entering the cleaning solution. The

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cleaner is most effective in cleaning hard-to-reach recessed areas. Place the parts to be cleaned in the pan filled with the cleaning solution, and turn on the cleaner. Experiment with various objects to determine their optimum cleaning time.

If the cleaning solution is to be heated, turn the main power on first to allow the solution to reach its set temperature. Time and temperature values are set by pushing the up/down buttons.

#### **Precautions**

The cleaner operates from 120-volt line power and there are liquids present; together these pose an added electric shock hazard if proper grounding is not maintained. Moreover, some cleaning solutions and their vapors can be toxic. Other precautions are:

• The use of flammable cleaning fluids is not recommended. If they are used, exercise all reasonable precautions by moving the cleaner out of doors and never leave it unattended while the fluid is in the pan. Be sure to return all toxic fluids to a safe storage container when cleaning is complete. Never use gasoline as a cleaning fluid!

• Never put your hands into the cleaning solution when the cleaner is on. The intense vibrations can drive particulates into your skin, and the ultrasonic energy could damage body tissues.

• Minimize any time spent close to the operating cleaner because the high-frequency 40-kHz oscillations can cause headaches and might lead to hearing impairment although they are not audible.

• Be sure that the pan is at least half filled with solution during all cleaning operations.

- Place any objects to be cleaned carefully in the pan with tongs, and take care not to drop any heavy object in the pan that could damage the fragile transducers.
- The use of chlorofluorocarbon (CFC) solvents, commonly used to remove solder paste from circuit boards, is not recommended because of their threat to the environment.  $\Omega$

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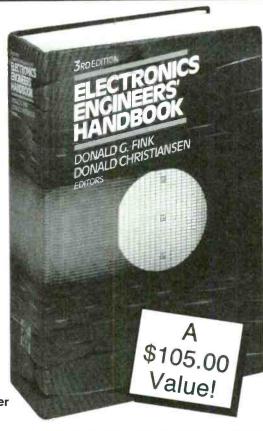
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#### **RAY MARSTON**

FIELD-EFFECT TRANSISTORS (FET'S) are unipolar rather than bipolar devices, and this gives them certain properties that are superior to those of bipolar transistors. Unlike the bipolar transistor, whose current depends on the movement of both electrons and holes, FET operation depends on only one of those charge carriers. Freed from the time delays that occur when those charge carrier recombine, FET's offer faster switching speed and higher cutoff frequencies.

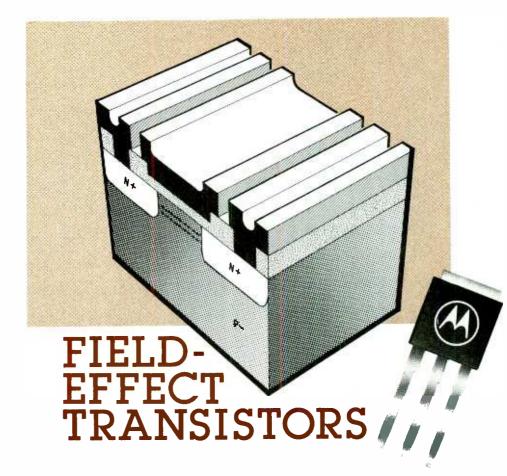
Other advantages of the FET include:

- Voltage rather than current operation.
- Extremely high input impedance in the off state.
- Virtually constant current with respect to voltage at specific bias levels.
- Current change that is inversely rather than directly proportional to temperature.

Despite these advantages, the FET has not replaced the bipolar the bipolar transistor in all applications, but it has encouraged new generations of small-signal and general purpose and RF MOSFET's as well as general purpose and RF MOSFET power transistors. Moreover, the latest digital logic families are based on FET technologies. The basic FET is a simple, three-terminal, voltagecontrolled device with characteristics that are similar to those of vacuum-tube pentodes. Thus, the FET is considered to be the solid-state equivalent of a pentode.

The two major classes of FET's are the junction FET (JFET) and metal-oxide-semiconductor FET (MOSFET), formerly called an insulated-gate FET (IGFET). FET's are further divided into N-channel, P-channel, depletion-mode and enhancement-mode devices. MOSFET's with N-doped channels are called NMOS, and those with P-doped channels are referred to as PMOS.

The three electrodes in all FET's are the source, drain, and qate, analogous to the emitter,



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collector, and base of the bipolar transistor. Both JFET's and MOSFET's are available as discrete transistors. Some MOSFET's have dual gates and are intended for use as radiofrequency mixers.

This article explains how Pchannel and N-channel MOSFET's are combined to form the popular complementary-MOS (CMOS) digital logic families. CMOS technology has made possible very large scale integrated (VLSI) memories, microprocessors and dedicated circuits that contain more than one million transistors and still have very low power requirements.

Most small-signal FET's today

are fabricated with planar geometry in which all electrodes are accessible from the top of the device. The active regions are defined on the wafer or substrate by successive masking, etching, and deposition or ionimplantation steps. But power MOSFET's now being fabricated with vertical structures are actually capable of handling much higher current in smaller areas of silicon.

#### Junction FET's

The simplest FET, the JFET, is illustrated by the cross-section view of Fig. 1-a. It is made by selectively implanting or diffusing ions into the wafer or substrate. An N-type region is

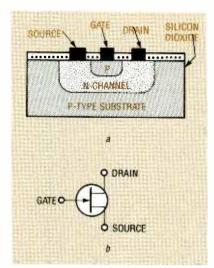


FIG. 1—N-CHANNEL PLANAR JFET showing diffused or implanted channel and gate regions (a), and schematic symbol (b).

defined on the P-type substrate by photolithographic methods, and N-type ions are implanted to form the N-channel. Later in the manufacturing process, following further masking, oxidedeposition and etching steps, Ptype ions are implanted or diffused into the N-channel to form the P-type gate.

Aluminum source and drain terminals are formed directly on the N-channel and an aluminum gate terminal is formed on the P-type gate. The symmetrical construction of the JFET permits the drain and source to be interchanged, if necessary.

If a positive voltage is applied at the drain of the N-channel JFET shown in Fig. 1-a, and a negative voltage is applied at the source with the gate terminal open, a drain current flows. When the gate is biased negative with respect to the source, the PN junction is reverse biased, and a depletion region, devoid of current carriers, is formed.

Because the N-channel is more lightly doped than the P-type gate material, the depletion region penetrates into the N-channel. This region, depleted of charge carriers, behaves like an insulator. The depletion region narrows the N-channel and increases its resistance. If the gate bias is made even more negative, drain current is cut off

completely.

The gate-bias voltage that cuts off the drain current is called the *pinchoff* or *gate-cut-off* voltage. However, as the bias becomes positive, the depletion region recedes, the channel resistance is reduced, and drain current increases. Thus, the JFET gate actually controls JFET current.

The schematic symbol for the N-channel JFET is shown in Fig. 1-b. As in other schematic symbols for solid-state devices, the arrowhead (representing the direction of conventional

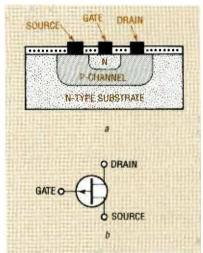


FIG. 2—P-CHANNEL PLANAR JFET showing diffused or implanted channel and gate regions (a), and schematic symbol (b).

current flow) points from P-doped material to N-doped material. In the N-channel JFET symbol, the arrowhead points from the P-type gate toward the N-type channel.

A section view of a P-channel JFET is shown in Fig. 2-a. The channel of the device is P-type material, and the gate is N-type. If a positive voltage is applied to the source, conventional current flows from the source to the drain. To reverse bias the junction between the N-type gate and the P-type channel, the gate must be made positive with respect to the channel. The biasing voltages of a P-channel JFET are opposite to those of the N-channel JFET.

The schematic symbol for the P-channel JFET is shown in Fig. 2-b. The arrowhead also points from P-type material to N-type material. In this instance, it points from the P-type channel to the N-type gate region. The characteristics of the P-channel JFET are similar to those of the N-channel device, except that the voltage and current polarities are reversed.

Both N-type and P-type JFET's operate in the *depletion* mode; that is, they conduct with zero bias on their gates. Figure 3 shows a typical family of *drain characteristics* for an N-channel JFET. As the gate-to-

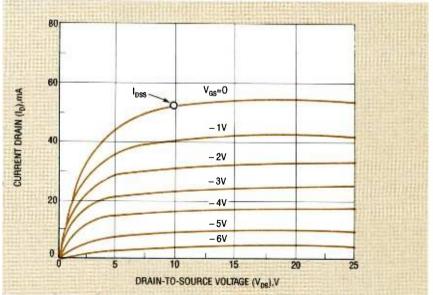


FIG. 3—DRAIN CHARACTERISTICS FOR AN N-CHANNEL JFET. The family of gate curves has its origin at zero drain-to-source volts, and the gate bias values show voltage control.

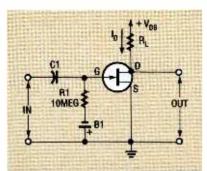


FIG. 4—N-CHANNEL JFET COMMONsource amplifier is analogous to a bipolar common-emitter amplifier.

source voltage is made increasingly negative, the depletion region is increased, and drain current decreases. As a result, pinchoff voltage occurs at a lower value of  $V_{\rm DS}$ . Curves for different values of gate-to-source bias,  $V_{\rm GS}$ , are plotted in the figure because the FET is a voltage-operated device.

#### JFET circuits

When an N-channel JFET is connected to a V<sub>DS</sub> supply as shown in Fig. 4, a drain current, I<sub>D</sub>, flows in the device. The magnitude of I<sub>D</sub> can be controlled by a gate-to-source bias voltage, V<sub>GS</sub>. Similarly, when a P-channel JFET is connected to a negative drain voltage, a drain current, I<sub>D</sub>, flows in the device. The value of  $I_D$  is maximum when  $V_{GS}$  equals zero, and it is reduced (to bring the JFET into a linear operating region) by applying a reverse bias to the gate terminal of the device (negative bias in a N-channel device, positive bias in a P-type).

In Fig. 3, the value of  $V_{\rm GS}$  to reduce  $I_{\rm D}$  to zero, the gate-to-source pinchoff voltage  $V_{\rm P}$  is about -7 volts. The value of  $I_{\rm D}$  when  $V_{\rm GS}$  equals zero (called  $I_{\rm DSS}$  or drain saturation current for zero bias) is about 52 milliamperes for the device shown in the figure.

The gate-to-source junction of the JFET has the characteristics of a silicon diode. When reverse biased (to bring it into its linear operating region), gate leakage currents (I<sub>GSS</sub>) are measured in thousandths of a microammpere at room temperature. Actual gate signal currents are only a fraction of a

that, and the input impedance to the gate is typically 1000 megohms at low frequencies. The gate junction is effectively shunted by a capacitance of a few picofarads, so input impedance falls as input frequency is increased.

If the gate-to-source junction of the JFET is forward biased, it conducts like a normal silicon diode, and if it is severely reverse biased it avalanches like a Zener diode. Neither of those conditions will harm a JFET if its gate currents are limited to those specified.

Referring to the N-channel JFET drain characteristics in Fig. 3, it can be seen that, for each value of  $V_{\rm GS}$ , drain current  $I_{\rm D}$  rises linearly from zero as the

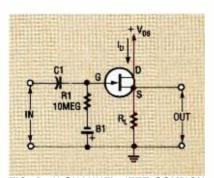


FIG. 5—N-CHANNEL JFET COMMONdrain (source-follower) amplifier is analogous to a bipolar emitter-follower amplifier.

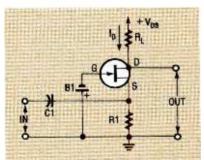


FIG. 6—N-CHANNEL JFET COMMONgate amplifier is analogous to a bipolar common-base amplifier.

drain-to-source voltage ( $V_{\rm DS}$ ) is increased from zero to a value at which a *knee* occurs on each curve. Moreover,  $I_{\rm D}$  remains virtually constant as  $V_{\rm DS}$  is increased beyond where the knee occurs.

Thus, when  $V_{\rm DS}$  for any of the family of  $V_{\rm GS}$  curves is below its knee value, the drain-to-source

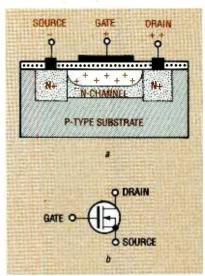


FIG. 7—N-CHANNEL, DEPLETION-mode MOSFET with negative gate bias (a), and schematic symbol (b).

pins of the JFET act like a voltage-variable resistor with its value determined by  $V_{\rm GS}$ . The drain-to-source resistance,  $R_{\rm DS}$ , can be varied from several hundred ohms at  $V_{\rm GS}$  = zero to thousands of megohms at pinchoff. That characteristic permits the JFET to be used in a circuit as a voltage-controlled switch.

From the drain characteristic curve of Fig. 3, it can be seen that when  $V_{\rm DS}$  is above the knee value, the  $I_{\rm D}$  value is dictated primarily by the  $V_{\rm GS}$  value, and is virtually independent of the  $V_{\rm DS}$  value. This characteristic permits the JFET to function as a voltage-controlled current generator.

The gain of a JFET is specified as a transconductance,  $g_m$ , the rate of change of drain current with respect to gate voltage. A  $g_m$  of 5 milliamperes per volt indicates that a variation of one volt on the gate produces a change of 5 milliamperes  $I_D$ . The units of this measurement are in inverse ohms or mhos. You will find that JFET data sheets usually specify  $g_m$  in millimhos or micromhos.

The N-channel JFET in Fig. 4 is organized as a common-source amplifier, analogous to a bipolar NPN common-emitter amplifier. In typical applications, the JFET is biased into its linear region and organized

as a voltage-to-voltage converter or amplifier. As shown in Fig. 4, a load resistor of suitable value,  $R_L$ , should be placed in series with the JFET's drain-to-source current.

Another common JFET configuration is the common drain or source-follower configuration shown in Fig. 5. That configuration is analogous to the bipolar emitter-follower configuration. Yet another possible JFET configuration is the common-gate configuration shown in Figure 6. That configuration is analogous to a bipolar common-base configuration.

#### MOSFET's explained

The metal-oxide FET or MOSFET was developed as an improvement on the JFET, and it has become the most important form of FET. Figure 7-a illustrates an N-channel depletion-mode MOSFET with a negative gate bias. The gate of this MOSFET is fully insulated from the adjacent channel. This is the most important distinction between an N-type depletion-mode MOSFET and an Ntype JFET, which is manufactured with a doped gate region directly under and in contact with the gate.

The surface of the silicon Ptype wafer is first coated with a layer of silicon dioxide (SiO<sub>2</sub>), and the source and drain windows are masked and etched to expose the P-type substrate. Ndopants are heavily diffused or implanted into those two regions. Another window is masked and etched over the channel, and it is given a lighter concentration of N dopant. In subsequent steps, the channel is recoated with an insulating oxide, and the metal source, drain, and gate terminals are deposited.

When the drain is positive with respect to the source, a drain current will flow, even with zero gate voltage. However, if the gate is made negative with respect to the substrate, positive charge carriers (holes) induced in the N-channel will combine with the electrons and cause channel resistance to increase. With increasing nega-

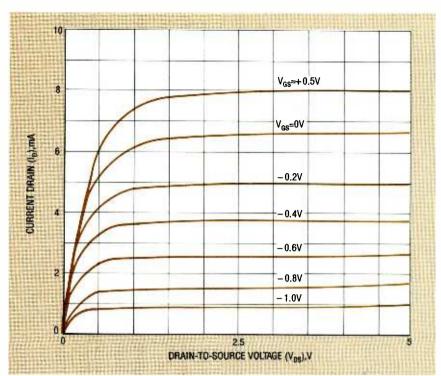


FIG. 8—DRAIN CURVES FOR N-CHANNEL DEPLETION-MODE MOSFET showing the effects of positive and negative bias

tive bias, the pinchoff voltage will be reached, and drain current will cease. However, if the gate is made positive with respect to the substrate, additional electrons are induced, and the channel current then increases.

The schematic symbol for the N-type depeletion-mode MOSFET is shown in Fig. 7-b. The path or channel between the source and drain is shown as a solid bar. The symbol for the P-channel depletion-mode MOSFET is identical to the N-type, except that the arrow points outwards.

Figure 8 is a drain-to-source characteristic curve for an N-channel depletion-mode MOSFET. It can be seen that the current drain,  $I_D$ , is inversely proportional to the magnitude of the negative gate voltages,  $V_{GS}$ . Compare Fig. 8 with Fig. 3 for the N-channel JFET to see their similarities.

Planar enhancement-mode MOSFET's are made by the same methods as planar depletion-mode MOSFET's. However, the N-channel enhancement-mode MOSFET shown in Fig. 9 does not have the N-doped drain-to-source channel through the P-type substrate of

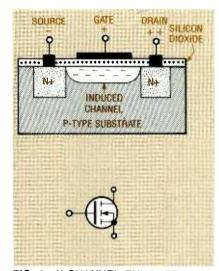


FIG. 9—N-CHANNEL ENHANCEMENTmode MOSFET with positive grid bias (a), and schematic symbol (b).

the N-channel depletion-mode MOSFET. Therefore, there is no conduction between drain and source at zero gate bias.

To turn an enhancement-mode MOSFET on, positive gate bias is needed. As the gate voltage is increased, more electrons are induced into the channel. They cannot flow across the oxide layer to the gate, so they accumulate at the substrate surface below the gate oxide. When a sufficient number of

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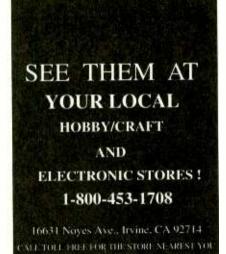
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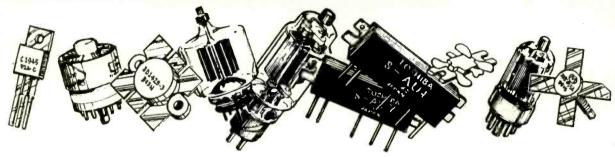
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Here's a great booster for any 2 meter or 220 MHz hand-held unit.
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20, 30, 40, 80M

IN RECEIVERS

#### HAM RECEIVERS **ORP TRANSMITTERS**

#### 20, 30, 40, 80M **CW TRANSMITTERS**



# Build you own man ham station. Sensitive all-mode off. (IV \$35 receivers use direct conversion design was \$160.25 as featured in \$25 and ARRL handbass Very sensitive variance of use of the Sensitive variance E-Z KEY CMOS KEYER

send perfect CW within an hour of receiving this kitl Easy-to-build kit has sidetone oscillator, speed control and keys most any transmitter. Runs for months on a 9V battery, 28-page manual gives ideas on making your own key for extra savings. Add our matching case set for complete station look

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March 1993,

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Fluke 70 II Fluke 73 11 \$87 75 II \$125 Fluke Fluke 77 11 \$145 79 II Fluke \$165

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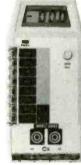
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3 1/2 digit display 10 MΩ impedance

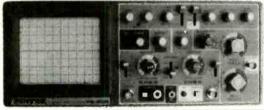
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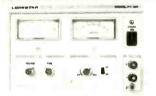
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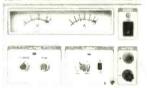
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Switchable between digital and analog 2 K word per channel storage Sampling rate: 10 M sample /sec 8 bit vertical resolution (25 Lerels/div) Expanded Timebase 10ms/div - 0.5 s/div Refresh, Roll, Save all, Save CH2, Pre-Trig Plotter Control



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0-30 VDC , 0-3A output 0.02% + 2mV line regulation 0.02% + 3mV load regulation 1 mVrms noise and ripple Short circuit and overload protected



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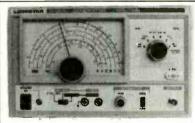
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0.2 Hz - 2 MHz in 7 ranges Sine, square, triangle, pulse and ramp

Output: 5mV-20Vp-p 1% distortion, DC offset ± 10V VCF: 0-10V control frequency to 1000:1

FUNCTION GEN./COUNTER



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100 kHz-150MHz sinewave in 6 ranges

Output 100mVrms to 35 MHz Internal 1kHz, External 50Hz-20kHz modulation



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FG-2100A



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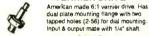
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"For many years we have been using CAIG's liquid and spray products in the lab for service and repair of connectors, switches and potentiometers. I also use their paste products on my boat to prevent corrosion from salt water and air ... fine products for a variety of applications".

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"Corrosion problems on very sensitive connectors have been an annoying problem for us. We have tried many products without success until we tried CAIG's DeoxIT. DeoxIT is the only product R. V., Xerox Corporation that has worked perfectly. We highly recommend it".

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Effectively cleans, polishes and eliminates static electricity on optical viewing surfaces. OpticALL is also recommended as a general purpose antistatic cleaner on plastic, glass and metal surfaces.

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Neutralizes static build-up caused by friction & low humidity conditions.

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ment and parts. Removes oil, grease, dirt and contaminants including rosin flux from PCBs, components and metal parts. Biodegradable.

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Oscilloscope: Mil Spec AN/USM-281A, 8 x 10 CM display, 100 MHz response which accepts standard 1800 series Plug-Ins. Includes Vertical Plug In: 1801A (PL-1186), frequency BW 50 MHz, maximum sensitivity 5mV/DIV. Horizontal Plug-In: 1821A (PL-1187), triggering to 100 MHz, minimum sweeptime 100 NS/DIV, has delayed sweep capacity. Price: \$250.00

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Frequency: 80, 40, 20, 15, 10 meters 3.4 to 5.0 MHZ, 6.5 to 9.5 MHZ 9.5 to 16 MHZ, 16 to 22 MHZ, 22-30 MHZ Mode: SSD or CW

Power Out: 1000 W PEP, 1000W CW Drive: 70-100 watts full output Harmonic Distortion: -40 dBc 2nd - 30 dBc 3rd

Output Independance: 5052 VSWR <2:1 Power Requirements: 1200 watts CW 300 watts SSB no modulation 550 watts SSB speech modulation Voltage 115V or 230V 50-60HZ

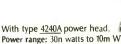
Wt: 38 lbs. Size: 1434" × 734"H × 14"D Price: \$895.00



#### **TEKTRONIX SOLID STATE PORTABLE 491 SPECTRUM ANALYZER**

Frequency 10MHZ—2 GHZ with internal mixers, 1.5GH to 40GHZ with plug-in mixers for use to 12.4GHZ. Dispersion 1KHZ/div, to 10MHZ/div. Coupled Resolution: 1KHZ to 100KHZ. Display Flatness: over 100MHZ dispersion to 12.5GHZ ≤3dB above 12.5GHZ, ≤6dB. Incidental FM: ≤300HZ. Frequency Stability: (after warm up) ±10KHZ with line variation ±5.0KHZ/°c with ±100KHZ, KHZ dispersion. ±20.0KHZ/°c with ±200KHZ, MHZ dispersion. Internal 1MHZ phase lock Input Impedance 5052. Max Input Power: -30dBm (linear range), + 15dBm (mixer limit), I.F. Attenuator: 51dB in 1d steps. I.F. Gain: >50dB. Display: Log, ≤40dB, Linear, ≤26dB, Square Law, ≤13dB. Sweeptime: 10 micro seconds to .5 Sec./div. CRT is 8×10 divisions (.8cm/div.). Power Requirements: 90K136 VAC or 180 to 272 VAC, 48 to 440 HZ, 55 watts. Size: 73/ns"H×127/ns"W×1911/ns"D. Weight: 30 lbs. Price: \$1400.00





Frequency Range: 0.01 to 18 GHz VSWR: 1.5 from 0.01 to 0.015 GHZ 1.35 from 0.015 to 10 GHZ 1.6 from 10 GHZ to 18 GHZ

Connector: Type N

Meter Size: 4.5 inches

Accuracy: ±1% of full scale on all ranges Built in 10 KHZ calibration signal. Power Requirements: 115V/230V, 50-1000HZ @ 5 watts.

(-45 to + 10 dBm).

Size:  $6.1^{\circ}H \times 5.1^{\circ}W \times 11.3^{\circ}D$ .

Weight: 7 lbs.

Price: \$350.00



#### **ANRITSU ML422B**

Anritsu ML422B Programmable Selective Level Meter. Has synthesized frequency tuning (rotary dial on keypad entry). Automatic tone search for unknown signals, swept frequency, keypad data entry for amplitude and frequency limits, IEEE488 computer control capability. Frequency range: 50HZ to 30MHZ (8 digit LED readout). Stability:  $\leq \pm 5 \times 10 - 7/0$  to  $45^{\circ}$ C, ≤ ±1 x 10 - 6/year. Bandwidths: Wideband, 48khz, 3.1khz and 20hz (-3dB). Amplitude Range: -120dBM to +30dBM depending on bandwidth setting (5 digit readout and meter). Amplitude Accuracy: ±0.15dB to ±1.5dB depending on level range and frequency setting. Input Impedence: 75 ohms terminated unbalanced or 10Kohm unterminated balanced. 75, 124, 135, or 600 ohms terminated balanced. 1.5Kohm and 20Kohm unterminated balanced. Distortion: Input ≤ ±10dBM, single tone, 2nd and 3rd Order ≤ -70dBc from 1Khz to 12mhz. 1.F. Rejection: ≤ -70dBM @ 56.6mHz, ≤ -80dB elsewhere. Image Rejection: ≤ -80dB. Phase Jitter: ≤0.5° p-p, 0.1° resolution. Power: 115V, 3.15A, 60hz AC. Size: 16¹¾6°W×7¾8°H ×19¾°D. Price: \$\$6,500.00 Wt: 45 lb.



#### COLLINS KWM—2A TRANSCEIVER

Frequency Range: 3.4 to 30 MHZ except 5.0 to 6.5MHZ. Unit Cover: 80, 40, 20, 15 and 10 meter. Amature bands. Modes: SSB, CW or RRTY. Sensitivity: 0.5 uv for 10 db S + N/N. Selectivity: 2.1 KHZ, 6db down; 4.2 MHZ, 60 db. Image Rejection: ≤40db. Power Output: 3.4 to 15 MHZ 100 watts PEP, 50 ohms; 15 to 25 MHZ, 90 watts PEP, 50 ohms; 25 to 30 MHZ 80 watts PEP, 50 ohms. Plate Input: 175 watts PEP on SSB; 160 watts CW Size: 14.75" × 7.75"H × Price: \$795.00 14"D. Weight: 18 lbs., 3 oz.



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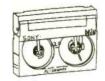
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TR-600B		30 lbs	black	1 1/2"	.50	\$4.00	\$30.00	l i
TR-800	8"	50 lbs	neutral	1 3/4"	.60	\$5.00	\$40.00	
TR-800B		50 lbs	black	1 3/4"	.70	\$6.00	\$50.00	
TR-1100	11"	50 lbs	neutral	3*	.70	\$6.00	\$50.00	
TR-1100		50 lbs	black	3*	.80	\$7.00	\$60.00	
TR-1500	15"	50 lbs	neutral	4"	\$1.00	\$8.00	\$70.00	
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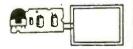
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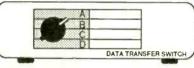
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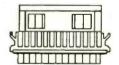


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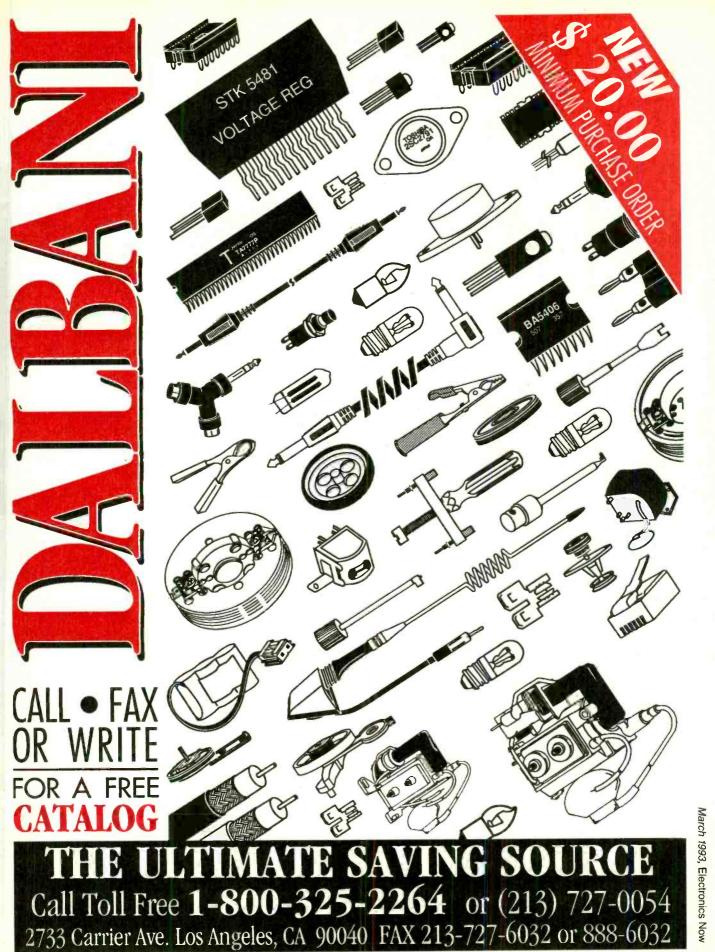


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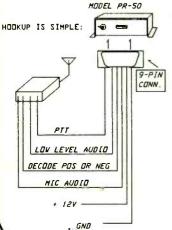
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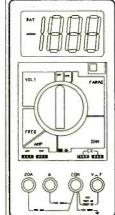
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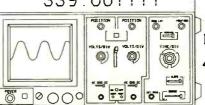
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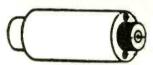
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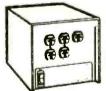
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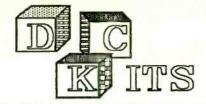
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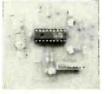
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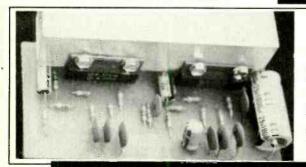
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Optional Holster

\$69.00

#### w/Bargraph Auto & Manual

4000 Count

- 3-3/4 Digit
- · 40 Seg. Bargraph
- Data Hold
- Min / Max
- Frequency Test
- Relative &
- Memory Diode
- Continuity
- Auto Power Off Optional Holster

**DM80** Reg. \$49.



#### **Credit Card Size** w/Bargraph

- 3200 Count
- 32 Seg. Bargraph Auto & Manual
- Auto Power Off
- DCV, ACV, Q
- Data Hold Continuity
- Beeper Plastic Case Included



**DM90** 

Reg. \$59.

#### **Pencil Type** w/Logic

- \$34.00 3-1/2 Digit
  - Auto & Manual Ranging
  - DCV, ACV, ACA, DCA, Ω
  - Logic CMOS/TTL
  - Data Hold
  - Diode

  - Continuity Beeper Case Included



# • 3-1/2 Digit

DM20T

- 20 Ranges / 6 **Functions** DCV, ACV, DCA, Ω
- Dlode Auto Polarity
- Temperature w/ Optional Probe



#### **DM30S**

**Auto Ranging** w/Memory Mode Reg. \$59.

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- 3-1/2 Digit
- Data Hold Memory Mode
- Diode
- Continuity Beeper
- Low Battery Mark Case Included

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Irvine, CA 92718

HP-9060,60MHz Rea. \$29. \$15.00

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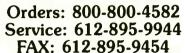
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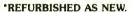
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Ball and socket type grill guides for attaching speaker grill to cabinet. To use, simply drill the appropriate size holes in cabinet and grill frame. 12 pair per package.

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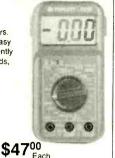


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#### Triplett DMM

The Triplett model 2202 digital multimeter is a full function DMM with built-in transistor and battery testers. Large, easy to read LCD display. Rotary switch for easy one hand function selection. The test leads conveniently attach to meter so they are always in reach. Test leads, manual, and carrying case included.

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#RJ-390-140

Pyle 15" Poly Woofer

15" poly woofer with a 60 oz. magnet and 2" voice coil. Mineral filled poly cone with poly foam surround. Poly cone provides proper internal

damping to help control cone motion at high power excursion. Power handling: 100 watts RMS, 145 watts max. VAS= 10.9 cu ft., QTS=.53, fs= 30 Hz. Frequency response: 20-3,000 Hz. SPL= 98 dB1W/1M. Impedance: 4 ohm Net weight: 9-1/2 lbs.

#RJ-292-070

#RJ-293-090

poly foam surround for

frequency sound that is

distortion. 2" voice coll,

smooth, tight, and low in

power handling: 85 watts

Pyle 10" Poly Woofer

Long throw poly woofer with

superb low bass. Mineral

filled poly cone assures low

\$6480 Each

#### **Pickering Headphones**

We made a special ouyout directly from the manufacturer on these super quality personal headphones. 1" dynamic high velocity element with strontium

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#### 10", Thruster Car Woofer

Heavy duty car woofer capable of handling 175 watts max (125 RMS). 4 ohm impedance. Polymerized paper cone with red poly foam surround. Resonant paper constituting polymers and summer separation. Resolution frequency: 26 Hz. VAS= 5.89, QMS= 4.6, QES= .27, QTS= .26. Frequency response: 30-2,000 Hz. Magnet weight: 38 oz, 2" voice coil. SPL= 92 dB 1W/1M. Net weight: 6 lbs.



#### **Deluxe In-Wall Speakers**

Perfect surround speakers. Customize your media room with these super quality, in-wall speaker pairs. Full size 6-1/2" woofer. Heavy duty 1" soft dome tweeter. Built-in crossover Fits any standard 2 x 4 or larger wall. Retrofit design allows easy installation in new or existing

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#RJ-300-036

\$29995

\$99<sup>95</sup>

## Right Angle

1/4" Phone Plua (Mono)



#RJ-099-020

65¢

#### **Honeycomb Tweeter**

Unique tweeter with a square diaphragm of honeycomb material.

Diaphragm is 1"

square. Excellent dispersion. 13/16" voice coil. Frequency response: 2,000-20,000 Hz. Impedance: 8 ohm. Power handling: 25 watts RMS, 40 watts maximum. 4" x 3-1/4". Limited availability. Net weight: 1 lb.

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\$870 Fach

#### High Voltage Cap Kit



This 85 piece kit contains a selection of 250. 350, and 450 volt electrolytic capacitors. 5 pieces each of 1, 2.2, 3.3, 4.7, 6.8, 10, 22uf and 2 pieces each of 33, and 47uf, 250V radial caps. 5 pieces each of 1, 2.2, 3.3, 4.7, 10uf and 2 pieces each of 22, 33uf, 350V radial caps. 5 pieces each of 1, 2.2, 4.7uf and 2 pieces of 10ut, 450V radial caps. Over \$62.00 wholesale cost if purchased individually. Net weight: 1 lb.

#RJ-020-950

\$49<sup>95</sup>

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Standard radio and TV speaker. 16 ohm impedance. 3 watts maximum power handling. Limited availability

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95¢

bass driver. Low 25 Hz resonant frequency. Weather resistant polymerized paper cone with red poly foam surround and two color printed dust cap. Power handling capability is 250 watts (170 watts RMS). 2" high temp voice coil with rear vented pole piece. 4 ohm impedance, 50 oz. magnet. Frequency response: 23-2,000 Hz, VAS= 19.04, QMS= 3.96, QES= .21, QTS= .20, SPL= 97.85 dB 1W/1M. Net weight: 11 lbs.

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Per Linear Yard 36" x 54"



#### The Loudspeaker Design Cookbook IV

RMS, 130 watts max. fs= 43 Hz. Frequency

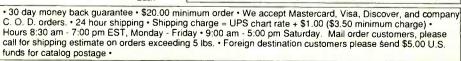
response: 25-3,000 Hz. SPL= 95 dB 1W/1M

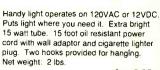
Impedance: 4 ohm. 40 oz. magnet. VAS=1.8 cu ft., QTS= .34, QMS= 10.92, QES= .35.

This book describes the "science" of loudspeaker design, however applying it is an "art". Using the information in this book will yield hundreds of possible variations in speaker design, with some subtle and not-sosubtle differences. 1991 copyright, fourth edition. Author: Vance Dickason. 154 pages paperback.

#RJ-500-035

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Fluorescent Work Light

#RJ-360-490

5-1/4\* paper cone

post mounted

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# 5-1/4", 2-Way Pioneer

woofer with a 1 polymer tweeter 4 ohm impedance. Response: 100-20,000 Hz. Power

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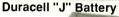
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#### Mini Super Tweeter

Super paper cone tweeter with silver mylar dust cap. Impedance: 8 ohm. Power handling capability: 2 watts RMS. 9-1/16" voice coil. 1-1/2" diameter cone with mounting tabs. Mounting holes: 1-7/8" on center Limited availability

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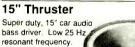
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Fisher Price battery charger. 120VAC input. 12VDC, 9.6W (800mA) output. 6 ft. cord with special connector. Limited availability



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Convenient assortment of clips, washers. springs, and screws. 10 pieces each of 4 sizes of "E" clips, 10 pieces of 2 sizes of



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Special rubber compound quickly and easily seals speakers into cabinets. Eliminates vibration and air leaks. Sold in 1/4" x 36" strips.



Strips are self-adhesive so they stick easily to speaker frame. Limited quantity

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#RJ-210-200

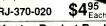
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Economical 30 watt iron with replaceable tip. Blue plastic handle. 120VAC. A quality fron at a reasonable price. Display packaged. \$490 Fact

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Soldering Stand Convenient weighted soldering iron stand with cleaning sponge

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**Kester Pocket Pack** 

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8 Position Dip Switch

**Camcorder Battery** 

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Weight: 1-1/2 lb.

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almost anything. Great for

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Thousands of uses.

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simply drill a hole,

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#RJ-260-295

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Velcro Type Fasteners

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**Pressfit Speaker Terminal** 

3.5 Amp DC Power Supply

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Regulated 13.8VDC, 3.5 amp continuous,

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Add 6 feet to your mini headphones. Gives the user added mobility when listening to personal cassette players.

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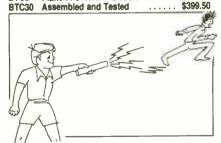
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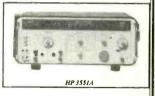


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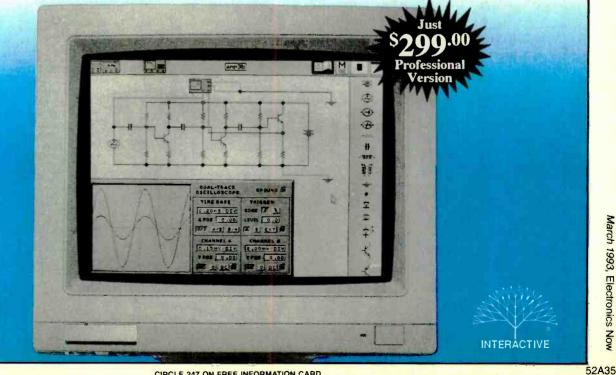
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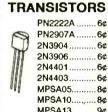


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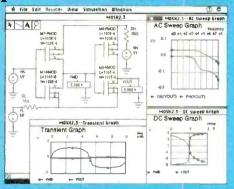
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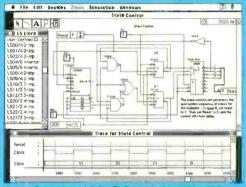
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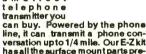


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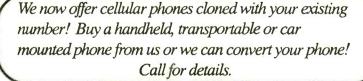
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74150	1.29	74L5123	0.39	74532	0.35
74151	0.39	74L5125	0.39	745157	0.49
74153	D.59	7415126	0.39	745163	0.59
74154	1.35	7415138	0.39	745188	1.75
74157	0.45	7415139	0.39	745287	1.69
74161	0.45	74L5151	0.39	745288	1.69
74163	0.49	7415153	0.39	745373	0.69
74174	0.59	7415154	1.15	745374	0.69
74175	0.59	74L5155	0.49	745387	1.75
74191	0.85	74L5157	0.39	745571	2.95
74221	0.45	74L5163	0.49	745573	2.45

#### **VOLTAGE REGULATORS**

PART #	PRICE	PART#	PRICE	PART#	PRICE
UA78540	1.35	7815K	1.39	7915T	0.45
78L05	0.39	7824T	0.45	7915K	1.49
7805T	0.45	7824K	1.39	7924T	0.45
7805K	1.39	79L05	0.39	7924K	1.49
78M05C	0.49	7905T	0.45	LM317T	0.57
7806T	0.45	7905K	1.49	LM323K	3.25
7808T	0.45	7906T	0.45	LM337K	2.95
78112	0.39	7908T	0.45	LM337T	0.87
78121	0.45	79L12	0.39	LM338K	4.95
7812K	1.39	7912T	0.45	LM350K	3.60
78L15	0.39	7912K	1.69	LM350T	2.85
7815T	0.45	79L15	0.39	LM723	0.49

#### NEC V-20 AND V-30 SERIES

The NEC V-20/30 can improve perfo to 30%! Pin compatible with the

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	Low	power	<b>CMOS</b>	design
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8088.				
ns	PART#	PRICE		
n	V20-8	7.95		
	V20-10	9.95		
	V30	0.05		

#### LINEAR

PART#	PRICE	PART#	PRICE	PART#	PRICE
MAX232	3.95	LM358	0.49	NE602AN	1.95
LM301	0.39	LM380	0.95	LM709	0.79
LM307	0.49	LM380N-B	1.49	LM741	0.29
LM308	0.69	LM393	0.49	LM747	0.59
LM309K	1.49	LM555	0.29	LM1458	0.39
LM311	0.49	LM556	0.49	LM1488	0:49
LM317K	1.85	NE558	0.75	LM1489	0.49
LM318	0.99	LM565	1.49	LM1881	5.75
LM324	0.35	LM566	1.25	LM3900	0.49
LM339	0.49	LM567	0.69	LM3909	1,49

#### LIGHT EMITTING DIODES

PART #	DESCRIPTION	PRICE
MAN72	7-SEGMENT .3" COMMON ANODE LED	0.99
MAN74	7-SEGMENT .3" COMMON CATHODE LED	0.99
LED-JR	JUMBO T1-3/4 RED LED	0.10
LED-JG	JUMBO T1-3/4 GREEN LED	0.14
LED-JY	JUMBO T1-3/4 YELLOW LED	0.14

#### **EPROMS**

				•		
PART#	SIZE	SPEED	Vpp	PINS	PRICE	
2732A-250	4096x8	250ns	217	24	3.95	
2764A-450	8192x8	450ns	12.5V	28	3.95	
2764A-250	8192x8	250ns	12.5V	28	3.95	
2764A-200	8192x8	200ns	12.5V	28	4.49	
27128A-200	16384x8	200ns	12.5V	28	4.95	
27256-250	32768x8	250ns	12.5V	28	4.95	
27C256-250	32768x8	250ns	12.5V	28	5.95	
27(512-150	65536x8	150ns	12.5V	28	6.75	
27C101-200	131072x8	200ns	12.5V	32	7.95	
27C101-150	131072x8	150ns	12.50	32	8.25	

#### STATIC RAM

717114	****					71701
PART#	SIZE	SPEED	PINS	CMOS	LP	PRICE
HM6116-2	2048x8	120ns	24	Y	N	2.95
HM6116LP-2	2048x8	120ms	24	Y	Y	3.95
HM6264LP-10	8192x8	100ms	28	Y	Y	5.95
HM62256LP-12	32768x8	120ms	28	Y	Y	5.95
HM62256LP-10	32768x8	100ms	28	Y	Y	6.95
HM62832-20	32768x8	20ms	28/.3"	Y	Y	13.95
HM62832-15	32768x8	15ns	28/.3"	Y	Y	16.95
HM628128LP-10	131072x8	100as	32	Y	Y	22.95
HM628128LP-85	131072x8	85ms	32	Y	Y	24.95

#### PALS

	•						
PART#	SPEED	PINS	IN	OUT	1/0'5	FUNCTIONS	PRICE
1618	35ns	20	10	2	6	AND-OR INV	2.25
16R4	35ms	20	8	4	4	AND-OR INV	2.25
1686	35ns	20	8	6	2	AND-OR INV	2.25
20L8	40ns	24	14	2	6	AND-OR INV	2.25
20R4A	25ms	24	12	4	2	AND-OR INV	2.45
20R6	40ms	24	12	6	2	AND-OR INV	2.25
20R8	40ns	24	12	8		AND-OR INV	2.25
20X8	50ns	24	10	8	2	AND-OR-XOR INV	2.95
20L10	40ms	24	10	12	2	AND-OR-INV	2.95

#### GAIS

PART#	SPEED	PINS	REPLACES	IN	OUT	PRICE
16V8	35ns	20	10L8 TO 16RP8	8	8	1.95
16V8-15	15ms	20	10L8 TO 16RP8	8	8	2.25
20V8	35ms	24/.3"	14L8 TO 16RP8	20	8	2.95
20V8-15	15ms	24/.3"	1418 TO 16RP8	20	8	3.45
22V10	35ms	24/.3"	PGM OUTPUTS	22	10	6.95
22V10-15	15ms	24/.3"	PGM OUTPUTS	22	10	13.95

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PART #	PRICE	PART #	PRICE	PART #	PRICE
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80C32	10.95	8749H	9.95	8087-2	129.95
8155	2.85	8751H	29.95	8087-1	169.95
8251A	2.89	87C51	39.95	80287-XL	89.95
8253-5	2.75	8755A	14.95	80387-SXP	79.95
8255-5	2.69	8088-1	7.95	80387-DXP	89.95
82C55-5.	3.95	R80286-16	34.95	80487-5X	389.95
8257-5	3.49	80386-33	299.95	ODP486-5X2	0449.95

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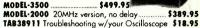
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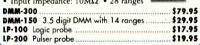
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R/A PC SOLDER	MALE FEMALE	DBxxPR DBxxSR	.49 .55	.69 .75	.79 .85	2.27 2.49	Ξ
W/W TYPE	MALE FEMALE	DBxxPWW DBxxSWW	1.69 2.76	2.56 4.27	3.89 6.84	5.60 9.95	=
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R/A W/W HEADER	IDHXXWR	3.28	4.22	4.45	4.80	7.30		
HEADER SOCKET	1D5xx	.65	.75	.75	1.19	1.19		
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ST-351A	Seagate	42Mb	28ms	3.5" IDE	\$199
CP-30084	Conner	84Mb	19ms	3.5" IDE	5239
ST-3096A	Seagate	88Mb	16ms	3.5" IDE	\$259
CP-30104	Conner	120Mb	19ms	3.5" IDE	5319
ST-3144A	Seagate	131Mb	16ms	3.5" IDE	5319
CP-3204F	Conner	212Mb	16ms	5.25" IDE	\$479



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41256-60	256K x 1	60ns	DIP	2.39
414256-80	256K x 4	80ns	DIP	5.49
1MB-80	1M x 1	80ns	DIP	4.99
1MB-60	IM x 1	60ns	DIP	5.49
41256A9B-80	256K x 9	80ns	SIMM	14.95
41256A9B-60	256K x 9	60ns	SIMM	16.95
421000A9B-80	1M x 9	80ns	SIMM	39.95
421000A9B-60	1M x 9	60ns	SIMM	45.95
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Each co-pi software g			i manual, fetime warra	nty.	Гę
PART #	SPEED	PRICE	PART#	SPEED	PRICE
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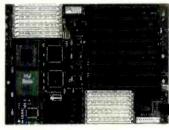
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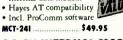
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Maxtor7120	0/72401DE//SCS1\$29	6/426//\$316/596
Micropolis 3	30/860 MBIDE//SCSI/ESDI	Call
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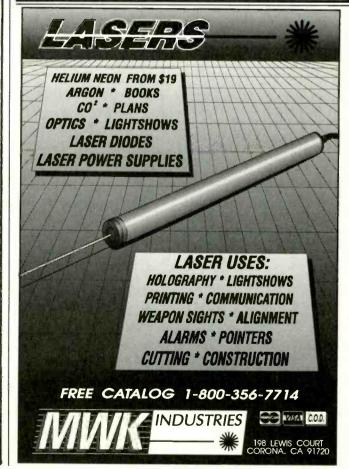
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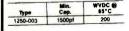
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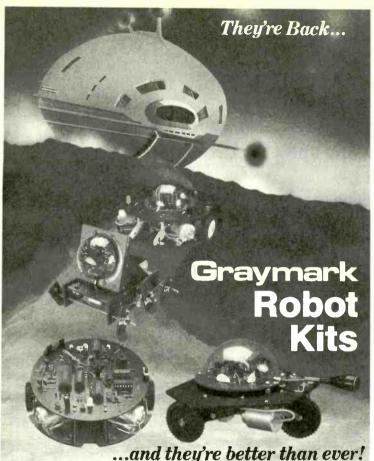
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Sine, Square, Triangle, Pulse, Ramp, .2 to 2MHz, Freq Counter .1-10MHz WE WILL NOT BE UNDERSOLD

UPS SHIPPING: 48 STATES 5%

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Model Y-01 \$48.95

Teaches basics of robotics. Arm grabs & releases, lifts & lowers. & pivots from side to side

#### AM/FM Transistor Radio Kit with Training Course

Model AM/FM 108

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14 Transistors ◆ 5 Diodes Easy to build because schematic is printed right on the PCB

Makes a great school project Model AM 550 AM Only \$17.95

#### Learn to Build and Program Computers with this kit



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Starting from scratch you build a complete system. Our Micro-Master trainer teaches you to write into RAMs, ROMs and run a 8085 microprocessor, which uses similar machine language as IBM PC.

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Full Function 34 Ranges, Includes Capacitance, Transistor/Diode Testing 20Amp AC/DC, Extra Large Display

#### **Multi-Function Counter**

Elenco F-1200 1.2GHz



\$229

Measures Frequency, Period, Totalizer 8 LED digits, Crysral Oven Oscillator 5ppm Accuracy

#### XK-500 Digital / Analog Trainer

A complete mini-lab for building, testing, prototyping analog and digital circuits Elenco's Digital/Analog Trainer is specially designed for school projects, with 5 built-in power supplies. Includes a function generator with continously variable, sine, triangular, square wave forms. All power supplies are regulated and protected against shorts.

#### Power Supplies

- Variable Power Supply +1.25 to 20VDC @ .5 Amp
- (+1.25 to 15VDC @ 1 Amp) -1.25 to -20VDC @ .5 Amp (-1.25 to -15VDC @ 1 Amp)
- +12VDC @ 1 Amp -12VDC @ 1 Amp +5VDC @ 1 Amp

- 30VAC Center tapped @ 15VAC at 1 Amp

#### Analog - Section

- Function Generator Sine
- Triangular, Square wave forms Frequency adjustable in five
- ranges from 1 to 100KHz Fine frequency adjust
- Amplitude adjust DC offset Modulation FM-AM

#### Digital - Section

- Eight data swiches
   Two no bounce loo
- Two no bounce logic switches 8 LED readouts TTL buffered
- Clock frequency 1 to 100KHz Clock amplitude 5VPP square wave

2 breadboards, each contain: 840 tie points (total 1,680)



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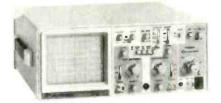
- 1mV Sensitivity
- Dual Time Base
- Illuminated Internal Gradicule

DS-203 20MHz. 10MS/s **Digital Storage Oscilloscope** 

\$775

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- Plotter Output
- 8 Bit Vert. Resolution
- 2048 Pts Hor, Resolu-
- Much More

## B+K 2120



20MHz \$395 Model 2125 \$539.95 2 Channel **Delayed Sweep** 

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Model 1541B

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- 749.95
- Video sync separators Z axis input
- Single sweep
- V mode-displays two signals unrelated in frequency

#### **60MHz DUAL-TRACE**

**Model 2160** 

- 1mV/div sensitivity
- 949.95
- Sweep to 5 ns/div
- Dual time base
  - Signal delay line
    - V mode-displays two signals unrelated in frequency
    - Component tester

#### 100MHz THREE-TRACE

**Model 2190** 

- 1,395.95 TmV/division sensitivity
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  - Signal delay line
  - 19kV accelerating voltage

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Model 2522

- 20MHz analog bandwidth
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  - 2k memory per channel
    - 20MHz equivalent time sampling

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Hitaahi Compost Carios Co	2000

Tiltacili Compact Octics	Coopes
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V-665A - 60MHz,DT, w/cursor	\$1,325
V-1060 - 100MHz, Dual Trace	\$1,375
V-1065A - 100MHz, DT, w/cursor	\$1,649
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RSO's feature; roll mode, averaging, save memory, smoothing, interpolation, pretriggering, cursor measurements.

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	,
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VC-6025A - 50MHz, 20MS/s	\$2,350
VC-6045A - 100MHz, 40MS/s	Call
VC-6145 - 100MHz, 100MS/s	Call

#### **Logic Analysers**



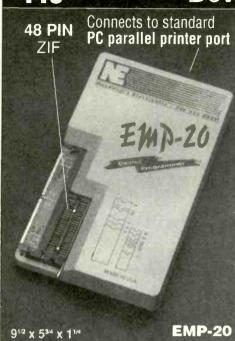
- 32 channels (VC-3120) or 48 channels (VC-3130)
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#### 5" SUPER SURWOOFFRS

(Pincussion Mount) Heavy duty in a very compact size! Features 1 1/4 aluminum voice coil, massive 20 ounce ceramic magnet, 4 ohm impedance, 50 watt RMS (75 watt peak) power. Response to 400 HZ vented backplate, air suspension edge and dust screen.



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GUITAR, STEREO AND AUTO APPLICATIONS

	SIZE	RATING	VC	ICE	MAGNET	STOCK#	PRICE
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	12°dia	100W 200W	2	4Ω	30 oz	63217	\$35.00
	15°dia	150W 300W	2 1/2"	βΩ	56 oz	63218	\$59.00
	°15°dia	200W 400W	3°	βΩ	95 oz	63219	\$100.00
	* massive cast frame-this is our most powerful speaker						



Consists of a 10" 16 ounce magnet, cloth roll. air suspension, 8 ohm woofer, a 3" square tweeter and a press fit quick connect terminal with 75 watt crossover. These were made by Pioneer for a custom manufacturer. You make your own enclosure and save a bundle. All 3 components for one low price!

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#### MISC. SMALL SPEAKERS

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	2 5/8	$4\Omega$	3	G2851	1.50	
	2 1/2	8Ω	.2	G939	1.29	
	2 1/4	32Ω	.25	G3215	.89	
	1 3/4	32Ω	.15	G3214	\$1.00	
	SIZE	IMP	WATT	STOCK	PRICE	
_						_



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G2555 \$1.00

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G2554 10/\$1.00 100/\$9.00 1000/\$70



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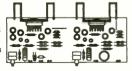
Bright xenon tube for making strobe lights. Size: 1.5"

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Two seperate high ower amps on one PC board put out an incredible 20 watts RMS each, Features low distortion circuitry. Great

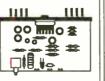


stereo booster amp for your car sound system. Use with any speakers capable of handling at least 20 watts. Operates on 12VDC. Size of board: 6"x2.25"

C6442 \$19.95

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High power amp for various booster applications. Kit features short and open circuit protection and very low distortion (1% or less). Has red LED "on" indicator and will boost any tuner, radio, cassette or CD player to room filling volume! Operates from 12 VDC. Size of board:3.75"x2.1". Complete with parts, PC board and instructions.



SKILL LEVEL 2 C6444 \$14.95 parts, PC board and instructions

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Similar to the 20W+20W stereo amp only this one puts out 10 Watts RMS to each channel. Features one level control that sets level in both channels and red LED "on" indicator. Use this amp with your speakers to boost portable tape players, radios or CD players to room filling volume. Operates from 12VDC. Size of board: 3.75"x2.25". Complete with all



SKILL LEVEL 2 C6443 \$16.95

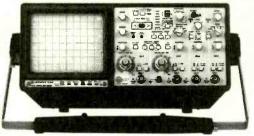
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52A55

March 1993, , Electronics

# HITACHI

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	frequency counter.		
	RS-232 w/HPGL support	2695.00	QUOTES!
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	MHz equivalent sampling, 4K		
	Mem, frequency counter,		CALL
	RS-232 w/HPGL support	3295.00	
VC-6145	4 Ch, 100 MHz, 100 MS/s (1		FOR
	ch), 4KW Mem, frequency		
	counter, RS-232 w/HPGL support	4395.00	PRICE
VC-6155	2 Ch, 100 MHz, 100 MS/s (2		
	Ch), 4 KW Mem, frequency	2005 00	QUOTES!
	counter, RS-232 w/HPGL support	3995.00	





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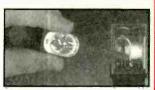
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2MHz FUNCTION GENERATOR

Features a 4-digit frequency counter display.
Operates at 120/220/240VAC 50/60Hz. Complete

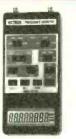
with power card, one cable BNC to insulated clips,

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Microprocessor-based counter measures frequency from 10 Hz to 1.25GHz and period from 0.1µs to 100ms. Includes data hold, min/ max/average readings and relative frequency measurements. Complete with 4 AA batteries, manual and 1-year warranty.



Reg. \$9500 Model RCDS1 **Tool Case** 

Req. \$298.00 Model R53-CDS1 Tool Kit

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BK PRECISION

manual and 1-year warranty.

Z3011B



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#### **PROGRAMMABLE DIGITAL TIMER**

Provides up to 6 on and 6 off settings per week with a minimum switch time as low as 1 minute. Plugs into 3-prong

110VAC outlet and has battery backup (AAA battery incl) to prevent programs from being cleared during power failure. Rated at 15amps. UL listed.



#### DOUBLE-SIDED CORDURA® CASE

One side has 45 pouches to hold your tools, the other side has a built in clipboard to hold a legal size pad of paper, a document pouch and 3 pockets to hold small items. The case also features 3 pockets on the outside of the case.

#### SERVICE SPECIALIST TOOL KIT

56 piece tool kit includes the case above plus commonly needed nutdrivers, hex drivers, screw drivers, pliers, cutters, wrenches, crimping tool, wire stripper, soldering tools and more (DMM is not incl.)

**\$409**.00 Reg. \$499.00

(1) HITACHI

OSCILLOSCOPE



Reg. \$45.00 Model ZSP100

## X1, X10 SWTICHABLE OSCILLOSCOPE PROBE

Monolithic probe features a 100 MHz bandwidth, a 3.5ns risetime, a wide compensation range (10pF to 60pF), a break-resistant center conductor and a sharp heavy-duty tip. Complete with spring hook, BNC adapter, IC and insulating tip and trimming tool. Cable length is 1.5 meters.

Reg. \$42.00 Model ZP200



#### X10 OSCILLOSCOPE PROBE

200MHz monolithic probe provides superior performance with a risetime of less than 1.5ns and a sharp pulse response. Complete with sprung hook, trimmer tool, 6" ground line, BNC adapter, IC and isolating tip. Cable length is 1.2 meters.

**\$39**.00

Model Z16420

# **ESD FIELD**

**20MHz DUAL CHANNEL** 

operator's manual and 3-year warranty.

Panel layout is color-coded to identify functions

easily. Sensitivity 1m/div. Complete with probes,

Kit includes a blue static-dissipative vinyl work surface (18"x22"x0.30") with two female snap fasteners, a common-point grounding cord (15'), one adjustable wrist strap with a 1 megohm resistor, a 6' cord and a 7"x13" storage case.

Model Z815 **BK PRECISION** HAND-HELD **PARTS TESTER** 

This 2000 count, 31/2 digit LCD display meter tests capacitance (20mF), resistance (20MΩ),

transistor hFE, SCRs, diodes, LEDs and batteries. Comes with 9V battery, manual, test leads and 1-year warranty.

**\$24**\_00 Model ZPB1

#### AUDIBLE CONTINUITY **TESTER**



Tester gives a clear audible sound on point-to-point continuity and is suitable for Go/No-Go test for wires, cables, LEDs, switches, diodes, transistors, etc. Complete with test probes and detachable alligator clips. Operates on 9v battery (not incl.).

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- 3-year warranty

Full-function, auto-ranging DMM with 4 digit, 10,000 count resolution measures DC voltage and current, resistance and true RMS AC voltage and current. It features a continuity beeper, diode test, an Auto Min-Max mode, a relative mode and a probe hold mode. Comes complete with manual, test leads, battery(9V). and protective holster.



Reg. \$80.00

\$299.00

Regular \$365.00 R22-IM5 117 Pc. Tool Kit



\$109.00

Reg.\$139.00 Model R380912 Reg.\$159.00 Model R38091F

### DCA/ACA **CLAMP METER**

Functions as 3 1/2 Digit DMM

Transformer jaws measure up to 400A AC/DC and a peak-hold function provides recall of AC or DC current surges. As a DMM it measures AC voltage, DC voltage, AC/DC current and resistance. The meter has the following ranges: ACV: 750V; DCV: 200mV, 200V; DCA/ACA: 200A,400A; Resistance; 2000 ohms Resolution down to 0.1 mV, 0.1A and 10 hm. Comes complete with test leads, battery, carrying case and 1-year warranty. Model R38091F also has a built-in temperature function, 0-1400°F.



## THE PROFESSIONAL'S TOOL CASE

- · Case top has built-in document holder
- Case bottom is partitioned into 3 areas
- Two removable pallets hold over 60 tools

A handsome black case to organize and transport your valuable tools and instruments. This is the same quality case used by thousands of professional field engineers. Case is made of high impact polypropylene, and has snap-action key locks and a padded handle. Size: 17 1/2" x 12 1/2" x 5".

#### 117-PC. PROFESSIONAL FIELD SERVICE KIT

The complete kit comes with the tool case described above and a complete selection of quality, brand-name tools including Diamond, Xcelite and Weller. The kit includes screwdrivers, pliers, tweezers, cutters, wrenches, alignment tools, hex driver blades and a crimping tool, wire stripper, soldering iron & supplies, socket set, penlight, inspection mirror, hammer and more.

Lifetime Guarantee: Any tool that fails under normal use will be replaced free of charge.

\$149.00 Reg. \$183.20 Model ZC2093



#### SERVICE VACUUM CLEANER

Features a powerful 2.2 peak HP motor, easy change double-layer filter bag, shoulder strap and built in handle. Toner-safe. Complete with a 6' Tuflex hose, dusting brush, crevice tool and brush, tube adapter, snorkel tube and small dusting brush. 12"x11"x5". 8 lbs



**\$99.**00 Reg. \$128.65 Model RWTCPS

#### TEMPERATURE CONTROLLED **SOLDERING SYSTEM**

Widely used in industry. It maintains a constant tip temperature of 700°F. Grounded tip protects components from voltage spikes. Comes with power unit, iron, stand, sponge and 700°F tip.

\$49\_00 Reg. \$58.30 Model ZP1KB **BUTANE POWERED** 

SOLDERING TOOL

With cordless convenience this 4-in-1soldering tool converts from

a solderingiron to blow torch, hot blower or hot knife. Butane gas powered. Complete with tips, sponge, iron stand and carrying case.



\$49.<sup>95</sup> Model Z7201F

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Measures 0° to 159°F, has a hi-lo limit setting, an accuracy of ±1° and a built in clock function. ABS covered probe is suitable for air/immersion applications, 1.5V battery incl. 4oz.





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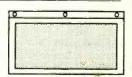
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NOT FOR BEGINNERS!

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w/Data. Your Choice: \$2.95 ea. or 8 for \$14.95

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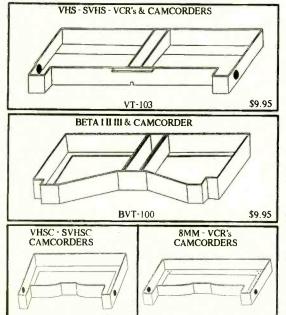
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HOW TO:

- Clean Video Heads pg 3 pg 5 \* Check tape end sensors Renew drive wheels pg 4
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Electronics Now, March 1993

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Just what you needed to finish that home television station...this Channel 2 modulator by Telemet! These used units accept a



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- E. Nine-digit, eight decimal point numeric LCD with solderable connection strip. No funny solders graded! 57 bigs digits and a solder beganning to the tion strip. No funny sockets needed! .5" high digits, overall size of display.75"x3". Pinout included. HSC#13518 \$1.95 ea. or 10/\$15.00
- F. Miniature Toggle Switch SPDT 125VAC 6A or 250VAC 3A Standard type on-on switch, solder eyelet terminals. Any hobbyist should have at least a handful in his parts bin! Now you can afford it... HSC# SW104
- G. High Value Capacitor -- .047 Farad (yes, that's <u>Farad</u>) at 5.5V in a package only .5" dia. and .3" tall. Good for CMOS memory back-up, etc. Made by Sohio. HSC# 10771 \$.29 ea. or 10/\$2.49
- H Leviton 6608 touch-activated dimmer control -- Make any meta surface or contact dim an incandescent lamp (up to 150W) simply by touching it! UL Recognized 120VAC dimmer module has three ns: line, load and touch contact. Think of the applications .5" x 1.5" x 2.75" HSC# 13037











# Perestroika Fallout... Soviet Science Collector's Items!

History on the march! Empires crumbling! Eager young scientists being trained for the new world order! We took advantage of the changing world scene to bring you History on the march! Empires crumbling! Eager young scientists being trained for the new world order! We took advantage of the changing world scene to bring you these unique items that are also great values. Russian (formerly Soviet) microscopes! The manual calls them training microscopes, we would probably call them student-ments, atthough they are not toys. They are both biological (illuminated from below via mirror) microscopes, for transparent specimens. The one on the left is of metal construction, has two objective lenses (8x, 20x) and three eyepieces (7x, 10x, 15x). A recent volume purchase allows us to lower the price to \$59.00. The one on the right is made of plastic, with itxed lenses giving 60x overall magnification. The optical assembly will store in its own base, giving a lightweight, compact (5° x 9° x 15°) package parfect for carrying in a backpack for field trips. It comes with two specimen jars, tweezers, slides, etc. that also store in the base. The quality and workmanship on both units are surprisingly good, given the stories we've heard of Soviet labor woes. Now you can own a piece of history, or just an inexpensive, decent microscope. \$59.00 HSC# 13065



# For your IBM-Comaptible computer...

1. Replacement Fan - Is your computer working fine, but just noisy? You would be surprised at how much dust gets sucked through the power supply. This gums up the bearings of the fan, which then starts to howl. Don't replace the power supply, just change out the fant Brand new 12 VDC .20A fans, 3 1/8" square body with mounting holes on 2 13/16" centers. HSC# 13712 \$9.95

2. Western Digital 16-Bit (AT) Hard/Floppy Controller with SIO, PIO ports -Save slots, save money! WD1003S-WA4 controller will handle two MFM hard drives at 2:1 interleave, two floppy drives (up to 1.44 MB) and also gives you Serial and Parallel Ports. Drive cables included, no manual but installation is typical procedure for AT's. HSC# 13659 \$19.95

# Attention: Robot Builders & Hobbyists!

A. Just inl: 12VDC two-speed reversible motors, perfect for your own personal R2-D2's locomotion! These motors are 3" dia. x 4.5" long with a .5" long shaft. They will provide up to 30 oz.-in. of torque at 2700 RPM, unloaded speed is closer to 5000 RPM. Depending on load they draw anywhere from 5 to 9 amps. The .31" (5/16") dia. shaft is cut with gear teeth, but you could still put a pulley or gear with a set-screw on it. Generous 33" long leads are color-coded for easy hook-up. Connection diagram and torque curve chart provided. These motors are new, but slightly dusty. HSC# 13617 \$7.95 ea.



B. 12VDC SPDT Relay -- Just the thing for controlling the above motor (in fact, they are both left-overs from a camper-jack system). C.P. Clare GP3R211ND1000 relay is rated at 10 amps, uses solderless quickconnect tabs, and has handy mounting ears. HSC# 13618 \$4.95 ea.

C. Heavy duty Coil-cords -- Two types available. Makes connections to moving fixtures easy! Rugged SJO insulation, slightly dusty These are not easy to find, and only limited quantities are available! HSC# 13620 20AWG, 5 cond., 5' stretches to 24' \$5.95 HSC# 13621 18AWG, 4 cond., 4' stretches to 25' \$7.95

D. Stepper Motors -- Two types, both 12VDC, sorry, no docs on either one yet... we'd appreciate info if you have it!



At left, Howard Ind. Model 1-19-4200, 3.6° per step, 1.75" x 1.75" x 1.75" HSC #13036 \$7.50 At right, Minebea Co. "Astrosyn" Model 23LM-C331-03, 1.8° per step. 2.25" x 2.25" x 3" with bracket (not shown) HSC #13594 \$4.95



# Solar Stuff for the Sunshine-Savant!

Check out these great items that work on free energy! Go solar & save!

1) Solar Battery Charger -- Small unit (2.5" x 4.5" x 1.5") has hinged lid with solar cell array for optimum sun angle. Can charge two AA or C Ni-Cd batteries (not included). LED indicates optimum charge rate. HSC#80050 \$12.95 2) Solar Rechargeable Flashlight -- perfect for camping, emergencies... Never needs batteries! 2.5" x 1.25" x 3" fits in purse, backpack. HSC#80048 \$11.95 3) 4-Power Radio -- Good-sounding AM/FM radio has solar panel for daytime use, or its internal dynamo can be cranked to charge internal energy source for up to a half-hour of listening time! Also runs off regular AA batteries or DC Adapter (neither included). Great for emergencies, power outages, camping, etc. 3" x 6" x 1.5" You may never buy batteries again! HSC#80051 \$29.95 4) Solar Education Kit -- includes small solar cell (1.75" x 3" x .25"), booklet, small DC motor, fan blade, spinner disks, stickers, etc. Good for child's school or science fair project. HSC #80017 \$9.95 5) Solar Musical Keychain -- plays melody in bright sunlight, also has LED



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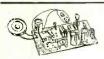
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need to know about recycling.

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E A

Electronics Now, March 1993



### RADAR SIGNAL DETECTOR

If you think that a sensitive radar detector is a complicated piece of equipment, take a look at this new kit. This simple, yet effective, detector circuit can be built in less than an hour and can be tuned to respond to signals between 50MHz to 500GHz. It's a fun kit to build and play with. A cigarette lighter plug is included. Size 1"x'4" operates on 9 to 15v DC.

KIT RSD-1 \$12.95

### STROBE LIGHT

If you need an attention getter, or warning light, you need the strobe light kit. Use it for emergency light for autos, for model planes or radio towers. Even use it on your bicycle. Operates on 6 or 12v DC and has a variable strobe rate.

KIT ST-1 \$8.95

### DIGITAL THERMOMETER

Have you ever wanted to tell temperature changes fast & accurately? The DT-1 klt will turn your digital volt meter into an accurate digital thermometer with .1 degree resolution. It gives you a 250 degree window with a range from -40F to 300F degrees. It has a remote sensor .25" sq. that can be mounted many feet from the meter if need be.

KIT DT-1 \$8.95



### BLINKEY LIGHTS

Want to attract attention? These kits are perfect for decorating name tags, lighting up your hat, or flashing lights for your model trains. Some people use them to simulate a burg-lar alarm for autos. Put it in a box, set it on your dash and it looks like the real thing. Each kit contains two LEDs that alternates flashing. Operates on a 9v battery. Size .5"x.5"

KIT RB-2 \$3.45

# CAPACITANCE METER

This easy to build kit will turn your digital volt meter into a CAPACITOR METER. Turn that junk box of unmarked capacitors into a fortune. Measures capacitors from (2pF to 2.2uF. Operates on a 9v battery. Size 1.75"2"

KIT CA-2 \$12.95

### WIRELESS FM MIKE

Small but mighty .8"x1"
PCB, will really stomp
out a signal well over 400
yds. This is a buffered
wireless mike that operates on 80 to 120 MHz
FM. Comes complete
with a microphone, and
9V battery connector.
Operates on 6 to 12v DC.
KIT WM-1 \$12.95



### SUPER SNOOPER-BIG EAR

Use this BIG EAR amplifier to listen through walls, hear conversations across the room. Beef up the sensitivity with a parabolic reflector and hear blocks away. Due to the size, the BIG EAR can be hidden about anywhere. Use the earphones from a pocket transistor radio to listen. Makes an ultra-sensitive intercom. Can also be used as a general purpose 1.5W amp. We supply a mini-microphone in the kit. You can also use any 8 to 45 ohm speaker. Operates on 6 to 12v DC. Size 1"x1.75"

KIT AA-1 \$10.95



### **AC LINE MONITOR**

This is something every computer user, photographer, or anyone that must maintain a safe usable AC line voltage should have handy. Monitor the voltage of your motor home's 110v AC generator inside the motor home. Every technician's bench needs this item. The AC line monitor will Indicate, with multi-color LEDs, what voltage is being distributed to your equipment at that particular outlet.

KIT LM-110 \$10.95



### 12V BATTERY MONITOR

Have you ever been in your car, boat, or camper—you try to start your motor but the battery is dead? The BATTERY MONITOR kit uses the cigarette lighter plug outlet to monitor the true battery voltage. Multicolor LEDs indicate the voltage in 1v steps from 11v to 15v, green means great, yellow is good, and red — call the tow truck or get out the oars. Size 1.2"x1.75"

KIT LM-12 \$5.95



### PHONE BUG

Small but mighty, so small it fits anywhere. Telephone line powered, never needs batteries. Transmits both sides of a phone conversation loud and clear, wireless, to any FM radio at great distances away. Variable tunes 70MHz to 130MHz. It can also be used to make any phone a speaker phone. Size .55"x1",

KIT TEL-B1 \$10.95



PHONE RECORDING SWITCH

This telephone line powered switch is small enough to install anywhere only .9"x.6". Every time someone picks up the phone the tape recorder will record both sides of the conversation automatically. Use it in your office to record all phone conversations so you don't lose that important address you wrote on the back of an envelope.

KIT TEL-SW 1 \$10.95

### **BUSY PHONE LIGHT**

Add this little kit to any or all of your phones. When any extensions are in use the LED will light. Uses a 9v battery. P.C. Board 1"x'yz". Complete with etched & drilled PCB, all parts and schematics.

KIT TEL-LIT-1\$9.95



### VOICE ACTIVATED SWITCH

This vox can be used to operate a lape recorder, ham radio, CB radio. Use it to turn on an alarm. The output can operate a load up to 100ma. It will operate a relay, lights, motor, or LEDs. What could you do with a sound activiated switch? Size 1.5"x1.25"

KIT VOX-1 \$6.95

### LIE DETECTOR

This kit can be great fun at parties. Lie and an audible tone will change, the more you lie the more the tone changes. When you lie your palms & forehead sweat. This kit allows you to measure these changes. Only a very slight amount of change will cause the tone to increase in frequency. Operates on 6 to 12v DC. Size

KIT LD-1

# LASER KITS

Laser Switching Power Supply Kit, input 12V DC .75-1.25A. Output 2 to 3 KV at 3-4.5 MA, trigger voltage of approx. 8-10 KV. Complete with 6.25" x 2.25" printed circuit board, schematic and all the parts.

LPS-1 ......\$59.95

1MW Laser Tube, NEW Mini He-Ne 1.125" dia. x 5.75" long, perfect for experimenters and laser projects. Works great with above power supply LPS-1.

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Mirror and Motor Kit—This unique kit allows you to project Lissajous patterns on walls and ceiling. Change the pattern by changing the speed of the motors. Comes complete with 2 motors, front surface mirrors, motor brackets, rheostat control to control #1 motor, and high power resistors to use on #2 motor.

MM-2.....\$19.95

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Laser Power Supply Kit LSP-1 1MW Laser Tube L1MW-1 Mirror and Motor Kit MM-2

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Electronics Now, March 1993

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# Scanner & Shortwave

AOR AR1000XLT \$449.00 AM Broadcast to Microwave 1000 Channels



500KHz to 1300MHz coverage programmable hand held. Ten scan banks, ten search banks. Lockout on search and scan. AM plus narrow and broadcast FM. Priority, hold, delay and selectable search increment of 5 to 995 KHz. Permanent memory. 4 AA ni-cads and wall plus eig charger included along with belt clip, case, ant. & earphone. Size: 6 7/8 x 1 3/4 x 2 1/2. Wt 12 oz. Fax fact document # 205.

AR2500 \$449.00 2016 Channels 1 to 1300MHz Computer Control



62 Scan Banks, 16 Search Banks, 35 Channels per second. Computer control for logging and spectrum display. AM, NFM, WFM, & BFO for Priority bank, delay/hold and CW/SSB. selectable search increments. Permanent memory. DC or AC with adaptors. Mtng Brkt & Antenna included. Size: 2 1/4H x 5 5/8W x 6 1/2D. Wt. 11b. Fax fact # 305

AR3000 \$1195.00 400 Channels 100KHz to 2036MHz



Extreme coverage, excellent sensitivity, plus processor controlled band pass filtering and attenuation to eliminate interference. Top rated receiver in its class, offers AM, NFM Wide FM, LSB, USB, CW modes. RS232 control. Lockout in search. 4 priority channels. Delay & hold & Freescan modes. AC/DC pwr cord and whip ant. included. Size: 3 1/7H x 5 2/5W x 7 7/8D. Wt 2lbs., 10oz. Fax fact document #105.

Free Stuff

Demo disk of SCS (scanner control system) software for AR 3000 & AR2500. Call toll free to order. Also, Free with AR2500: Control software, a \$49.95 value. Allocation chart of all voice frequencies. Dial Fax Facts for doc. #999.

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# Mobile Scanners

Bearcat 760XLTM \$249.95 100 Channel 800 MHz



Five banks of 20 channels each. Covers 29-54, 118-174, 406-512 and 806-954MHz (with cell lock). Features scan, search, delay, priority, memory backup, lockout, service search, & keylock. Includes AC/DC cords, mtng brkt, antenna. Size: 4 3/8 x 6 15/16 x 1 5/8. Wt: 4.5lbs. Fax fact document #550.

Bearcat 590XLTX \$199.95 100 Channel 11 Band



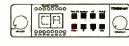
Five banks of 20 channels each. Covers 29-54. 118-174, and 406-512MHz. Features scan, search, delay, priority, memory backup, lockout, service search, & keylock. Includes AC/DC cords, mtng brkt, antenna. Size: 7 3/8 x 6 15/16 x 1 5/8. Wt: 4.1lbs. Fax fact document #570.

Bearcat 560XLTZ \$99.95 16 Channel 10 Band



Compact, digital programmable unit covers 29-54, 136-174, and 406-512MHz. Features scan, WX search, delay, priority, memory backup, lockout, review,& auto delay. Includes AC/DC cords, mtng brkt, antenna. Size: 7 3/8 x 2 1/2 x 1 5/8. Wt: 2.51bs. Fax fact document #560.

Trident TR-2C \$69.95



### Scan/CB. Optional laser/wide radar

Scans pre-programmed by state channels in low, high, UHF & T bands. Weather, 40 ch. CB receive plus mobile relay. Size: 5 5/8 x 4 7/8 x 1 3/4. Wt: 1.5lbs. Fax fact document #580.

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174, 406-512 and 830-950 MHz (no cell lock). Features scan, search, delay, priority, permanent memory, lockout, backlite, & keylock. Includes AC/DC adaptor, belt clip, antennas. Size: 5 3/4H x 2W x 1 1/2D. Wt: 12oz.. Fax fact document #650.

# Bearcat 200XLTN \$229.95 200 Channels 800 MHz

Ten scan banks plus search. Covers 29-54, 118-174, 406-512 and 806 956MHz (with cell lock). Features scan, search, delay, 10 priorities, mem backup, lockout, WX search, & keylock. Includes NiCad & Chrgr. Size: 1 3/8 x 2 11/16 x 7 1/2. Wt. 32 oz. Fax Facts # 450

Bearcat 100XLTN Now \$159.95 100 Channels, Keyboard Programmable. Similar to 200XLTN above without 800MHz. Fax facts #460

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Bearcat 55XLTR Now \$99.95! 10 Channels Keyboard Programmable. 10 Band with LCD. Requires 5AA's . Fax facts #480

# Table Top Scanners

Bearcat 855XLTE Now \$179.95! 50 Channels Keyboard Programmable with 800MHz. LCD

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WX search, review, memory backup. Fax facts #670. Bearcat 172XLM Only \$124.95 16 Channels with 10 bands. Track tuned, LED display, priority,

WX search, review, memory backup. Fax facts #680.

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March 1993, Electronics Now

Connect Muscle Wires ™ to a battery or other power source and watch them contract in length up to five percent! Remove power, and they relax and are ready for millions more cycles. Create direct linear action without heavy gears, coils, or motors. Use Muscle Wires in robots, models, planes, railroads — anywhere you need small, strong all-electric motion.

### What Are Muscle Wires?

Muscle Wires are highly processed strands of a nickel-titanium alloy called *nitinol*. At room temperature they are easily stretched by up to 5% of their length. When conducting an electric current they return to their original "unstretched" shape with a force thousands of times their weight.

### How strong are Muscle Wires?

The force a wire pulls with varies with size, from 35 to 330 grams. For more strength, use several wires in parallel.

### How fast can Muscle Wires activate?

They contract as fast as they are heated – as quickly as 1/1000 of a second. To relax, the wire must cool again. Rates of many cycles per second are possible with active cooling.

### Flexinol Muscle Wire Specifications

Wire Diameter	50 µm	100 µm	150 µm
Resistance	510 $\Omega/m$	150 $\Omega/m$	$50 \Omega/m$
Contract Force	35 yrams	150 grams	330 grams
Typical Current	50 mA	180 mA	400 mA

### How much power do Muscle Wires need?

Power varies with wire diameter, length, and surrounding conditions. Once the wire has fully shortened, power should be reduced to prevent overheating.

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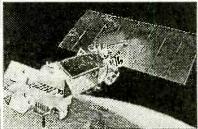
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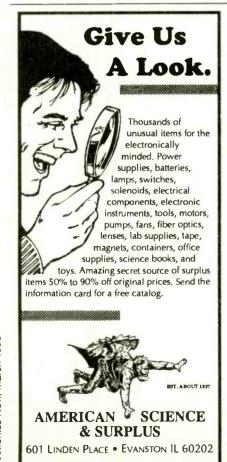
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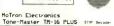
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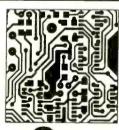
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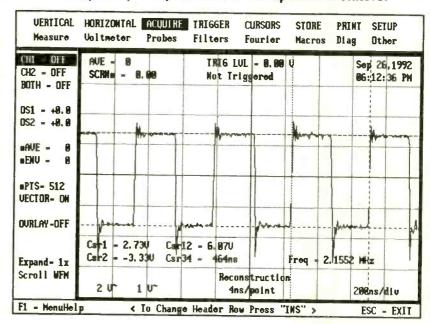
These boards have completely independent vertical channels, each with their own 25 or 40 megasample /sec 8-Bit A/D converter, 8K/32K static ram, and 10 vertical gain settings (in 1,2,5 steps) standard. This gives you the same high performance whether you are using one channel by itself or multiple channels simultaneously - not a common feature amoung other addons. Also, in addition to 27 timebase settings (in 1,2,5 steps), there is a user programmable mode for sweeps as slow as 1 year/div.

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TIME BASE RANGE **
MAXIMUM TIME RESOLUTION
VERTICAL RESOLUTION
MEMORY (Standard)***

- = Available 4th Qtr 92
- \*\* = Screen display can zoom up to 10X
- \*\*\* = 32K option available

8K words	8K words	8K words	8K words
250 рв	400 ps	400 ps B-Bit A/D)	l ns
20ns-2 sec/div	50ns-2 sec/div	50ns-2 sec/div	50ns-2 sec/div
40 Ms/sec	25 Ms/sec 2 (+ 1 exter	25Ms/sec nal trigger/enable)	25 Ms/sec
10 MHz	6.2 MHz	6.2 MHz	6.2 MHz
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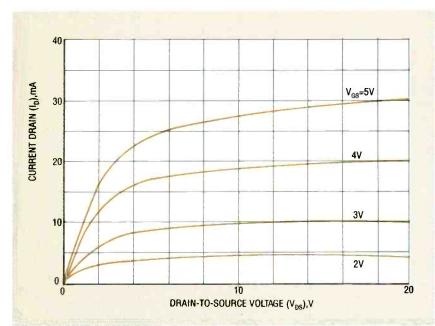


FIG. 10—DRAIN CURVES FOR AN N-CHANNEL, enhancement-mode MOSFET showing the effects of increasingly positive gate bias.

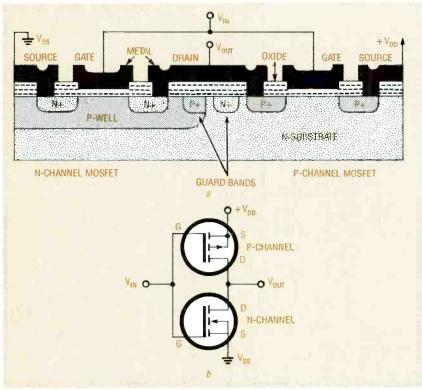


FIG. 11—CMOS INVERTER (NOT) GATE FORMED FROM N-CHANNEL AND P-channel enhancement-mode MOSFET's with power, ground, input, and output connections as shown in (a), and schematic (b).

electrons has accumulated, the P-type substrate material is converted into an N-channel, and drain-to-source conduction occurs. The magnitude of the drain current depends on the channel resistance, but it is controlled by the gate voltage.

The schematic symbol for an

N-type enhancement-mode MOSFET is shown in Fig. 9-b. In this symbol, the gate does not make direct contact with the channel. The arrowhead points from the P-type substrate toward the (induced) N-type channel, shown as a line broken into three sections to indicate an in-

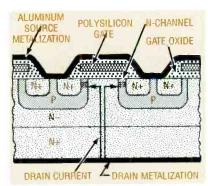


FIG. 12—SECTION VIEW OF AN N-channel DMOS power MOSFET showing its vertical structure and vertical current flow.

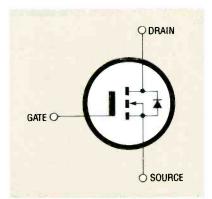


FIG. 13—SCHEMATIC SYMBOL FOR A DMOS power MOSFET including a drain-source diode.

### termittent channel.

Current flow in the channels of both kinds of enhancement mode MOSFET's is proportional to the voltage on their gates.  $V_{GS}$ . This can be seen for an N-type enhancement-mode MOSFET by examining the family of gate voltage ( $V_{GS}$ ) curves in Fig. 10. Current drain,  $l_D$ , is directly proportional to the positive value of gate voltage.

A P-channel enhancementmode MOSFET is made the same way as the N-channel enhancement device except that Ptype drain and source regions are diffused into an N-type substrate. The symbol for a P-type enhancement-mode MOSFET is the same as the one shown in Fig. 9-b except that the direction of the arrow is reversed. In the case of a P-type enhancement-mode MOSFET, the drain current is directly proportional to the negative values of its grid voltage.

The high gate impedance of all MOSFET's makes them susceptible to damage from even low-energy electrostatic discharge (ESD). For this reason many discrete MOSFET's and IC's based on MOSFET's are protected with on-chip Zener diode circuits.

# **CMOS** logic devices

An enhancement-mode MOSFET can act as a switch when it is turned on or off by a voltage applied to the gate electrode: N-channel MOSFET's are switched with positive gate voltage, and P-channel MOSFET's are switched with negative gate voltage. These are known as complementary responses, and they form the basis for complementary MOS or CMOS digital logic families.

Figure 11-a is a section view of a complementary pair of MOSFET's on a common substrate, the basic topography for all CMOS gates. The common substrate that is used for this pair is an N-doped silicon wafer. To make an N-channel MOSFET on an N-doped substrate, it is necessary to diffuse or implant a P-doped well in the substrate. The smaller N-type wells can then be formed in this P-doped region.

Because the substrate is N-doped, fewer steps are required to form the P-channel FET. The P- and N-doped guard bands isolate and insulate the individual transistors in this integrated circuit to prevent mutual interference. (Although not illustrated here, these guard bands are actually N- or P-doped rings formed around the complete FET below the oxide layer in this CMOS technology.

The two transistors in the section view, Fig. 11-a, can be connected to form a CMOS logic inverter, the simplest of digital logic circuits. This is accomplished by connecting the gates together to form an input  $(V_{IN})$  terminal, and taking the output  $(V_{OUT})$  from the common drain. The source on the left side of the diagram,  $V_{SS}$ , is grounded, while the source on the right side is connected to the positive supply,  $V_{DD}$ .

Those connections are shown schematically in Fig. 11-b. How does the inverter work? Consid-

er the P-channel device to be the driver and the N-channel device to be the load. Recall that an N-channel enhancement-mode MOSFET conducts with a positive gate voltage, while a P-channel, enhancement-mode MOSFET conducts with a negative gate voltage.

When the voltage input to the inverter is low (logic 0), the gate voltage of the P-channel device is negative, equal to the supply voltage  $V_{\rm DD}$ . As a result, the P-channel MOSFET is switched on, and there is a low impedance path from the output to  $V_{\rm DD}$ . Because the N-channel is off (gate voltage is zero), there is

CMOS unit is extremely low. These properties of N- and P-type enhancement-mode FET's combined to form CMOS gates provide many advantages:

• Extremely low power consumption.

• Wide power supply voltage range.

• High DC noise margin

• High input impedance

• Wide operating temperature range.

The diagram in Fig. 11-a illustrates standard CMOS metalgate technology (74C/4000), but there are many other CMOS technologies including the high-speed silicon-gate HC,

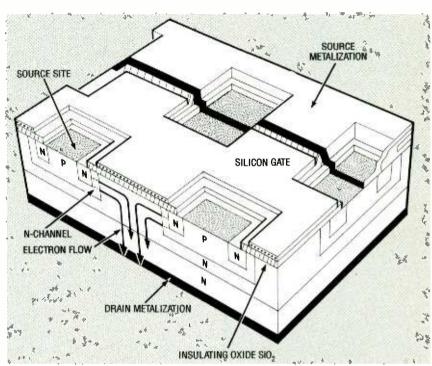


FIG. 14—CUTAWAY OF AN N-CHANNEL DMOS power MOSFET showing the arrangement of multiple cells in parallel.

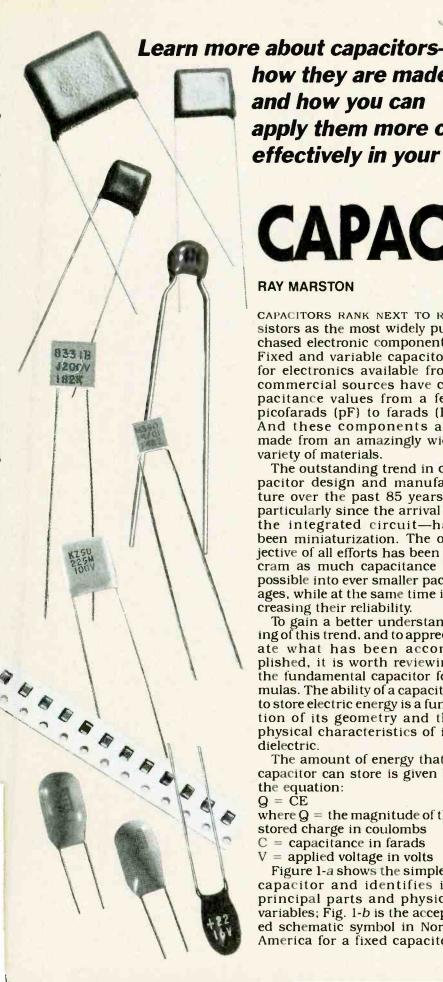
a very high impedance path from the output to ground. Therefore, the output voltage rises to  $V_{\rm DD}$ .

When the input voltage is high (logic 1), the situation is reversed. The P-channel FET is cut off, and the N-channel FET is on, so the output voltage falls to zero. Therefore, the circuit is a logic inverter: a low input results in a high output, and vice versa.

In either logic state one FET is on while the other is off. Because one FET is always turned off, the quiescent current of the HCT, and FACT families. Another digital logic technology called BiCMOS takes advantage of the lower power consumption and higher integration density of CMOS, and the higher speed and superior drive capability of bipolar transistors.

# Power MOSFET's

Power MOSFET's exhibit the properties of small-signal MOSFET's such as high-input impedance and voltage control, and they have drains, sources and gates, but they are designed continued on page 89



how they are made, and how you can apply them more costeffectively in your circuits

# CAPACITORS

**RAY MARSTON** 

CAPACITORS RANK NEXT TO REsistors as the most widely purchased electronic components. Fixed and variable capacitors for electronics available from commercial sources have capacitance values from a few picofarads (pF) to farads (F). And these components are made from an amazingly wide variety of materials.

The outstanding trend in capacitor design and manufacture over the past 85 years particularly since the arrival of the integrated circuit—has been miniaturization. The objective of all efforts has been to cram as much capacitance as possible into ever smaller packages, while at the same time increasing their reliability.

To gain a better understanding of this trend, and to appreciate what has been accomplished, it is worth reviewing the fundamental capacitor formulas. The ability of a capacitor to store electric energy is a function of its geometry and the physical characteristics of its dielectric.

The amount of energy that a capacitor can store is given by the equation:

Q = CEwhere Q =the magnitude of the stored charge in coulombs C = capacitance in farads

V = applied voltage in volts

Figure 1-a shows the simplest capacitor and identifies its principal parts and physical variables; Fig. 1-b is the accepted schematic symbol in North America for a fixed capacitor.

and Fig. 1-c is the accepted symbol for a variable capacitor.

Capacitance in farads is determined by:

C = kA/d

where k is the dielectric constant (permitivity), the ratio of the ability of a dielectric material to store electrostatic energy to that stored by a vacuum between the same electrodes (see Table 1).

A = directly opposing plate area d = distance between the plates

Different multiplying factors can be applied to this equation so that the value for C is in microfarads or picofarads when A and d are measured either in inches or millimeters. Nevertheless, important engineering tradeoffs can be seen from both of these equations:

 To store a given charge, more voltage is needed for a small capacitor than a large one.

- If the opposing plate area. A, is held constant, the value of capacitance can be increased by: a. Decreasing the thickness of the dielectric, h.
- b. Using a dielectric with a higher constant, k.
- c. Doing both (a) and (b) simultaneously.

While not apparent from the formulas, other facts about capacitors to be considered are:

- The maximum voltage that can be impressed across a capacitor, without destroying it, depends on the dielectric and the separation of the plates.
- For a given dielectric, the allowable maximum voltage can be increased as the distance be-

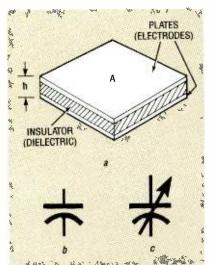


FIG. 1—A BASIC PARALLEL-PLATE capacitor has parallel metal plates or electrodes separated by a dielectric that can be air or a solid insulator.

tween the plates is increased.

The volumetric efficiency of capacitors has been improved within the constraints mentioned. How this has been done will be explained in the discussion of each of the most common capacitor manufacturing technologies.

Advanced circuit manufacturing methods have increased demand for miniature chip capacitors for hybrid circuits and surface mounting. New plastic film and ceramic dielectrics now offer a wider range of operating characteristics than was available ten years ago; metalizing has reduced capacitor weight and size by eliminating metal foil from many film capacitors now being produced.

The quality and reliability of electrolytic capacitors has been improved with more effective methods for etching foils, the introduction of better electrolytes, and improved sealing. Solid-electrolyte tantalum capacitors made as dipped radial or chip units are becoming more popular. Capacitors made from mica and glass have faded away to become specialty items, with their former functions largely performed by multilayer ceramic capacitors. Moreover, ceramic disk caps are rarely specified in new designs; they have been replaced by smaller, easier-to-place ceramic tubular capacitors.

The fabrication of increasing numbers of capacitors within very large scale integrated circuits such as microprocessors and digital signal processors has not reduced sales of discrete capacitors; in fact, the sales of certain kinds of capacitors have increased because of the proliferation of IC's. Moreover, capacitors are necessary in the external circuitry for the dedication of such multifunction linear IC's as compandor and modulation chips. Thin- and thick-film capacitors are being formed on ceramic substrates for networks and hybrid circuits that operate well into the microwave band.

Variable capacitors, still used primarily in radio-frequency circuits, are also being made from improved plastics and ceramics, a departure from their traditional dielectrics of air, glass, and ceramic, to reduce their size, extend their capacitance range, and cut cost.

# Capacitor terms

Capacitors are widely specified with a glossary of widely accepted technical terms. A knowledge of these terms will be helpful to anyone who specifies or uses capacitors.

Capacitance. The basic unit for capacitance is the farad, but most capacitors for electronics applications need capacitance values that are only small fractions of a farad: microfarad (µF—one-millionth of a farad) and picofarad (pF—one-millionth of one-millionth of a farad).

Ambient temperature. The ac-

tual value of a capacitor de-TABLE 1 DIELECTRIC CONSTANTS COMMON CAPACITOR MATERIALS

0800MIII MIAI C	HIALO		
Dielectric	, <b>k</b> .	- # _	>
Vacuum * *	* \$\frac{1}{2} \cdot 1 \cdot 1.	`y %	21.1
Air	1.00	06	۰
Polystyrene	2.5	* '	
Polyester	ે 3		٤.,
Mica	, 5	*	3.,,
Aluminum oxide	* 7 🦠		
Tantalum oxide	25		
Ceramic (low k)	ુ <sup>ત્ર</sup> 10 ું	8.	*
Ceramic (high k)	100-	-10,0	00

pends on the temperature of its environment, known as ambient temperature. Percent capacitance change, a function of temperature, is referred to room temperature, 25°C.

Capacitive tolerance is the variation in capacitance value of the capacitor expressed as a percentage of its value at room temperature, 25°C, which is referred to as the nominal value. Temperature coefficient (TC) is the change in a capacitor's capacitance per degree change in temperature, expressed in parts per million per degree Celsius (ppm/°C). The coefficient can be positive, negative, or zero. The letter P indicates that the coefficient is positive: N if negative. The designation NPO identifies a zero-temperature coefficient. Rated working voltage is the maximum permissible operating voltage at which a capacitor can be continuously operated at maximum rated voltage (without derating). This rating must be specified as AC or DC because they are not usually equal.

Surge voltage is the maximum instantaneous voltage to which the capacitor should be subjected; exceeding that voltage will cause the capacitor's breakdown. Surge voltage is higher than working voltage.

DC leakage is the small amount of direct current that flows in a capacitor at a specified voltage. Caused by the presence of free charge carriers within the dielectric, it is the reason why a charge cannot be stored indefinitely in a capacitor; eventually it leaks off.

Insulation resistance (IR) is the resistance of the dielectric. High resistance results in low leakage current. This variable is inversely related to ambient temperature.

Capacitive reactance  $(X_C)$  of a capacitor is inversely related to the product of capacitance and frequency in accordance with:  $X_C = 0.159/f \times C$ 

where 0.159 is a conversion constant

 $X_C$  = capacitave reactance (ohms)

f = frequency (hertz)C = capacitance (farads) Equivalent series resistance (ESR), expressed in ohms, is the sum of all internal resistance values of a capacitor. These include lead resistance, terminal losses, and dissipation in the dielectric. ESR increases with frequency.

Impedance (Z) of a capacitor is the total opposition it offers to the flow of alternating current at a given frequency:

$$Z = \sqrt{X_C^2 + (ESR)^2}$$

where Z = impedance (ohms)  $X_C^2 = capacitive$  reactance (ohms)

ESR = equivalent series resistance (ohms)

Capacitive impedance is inversely proportional to frequency and temperature; ideally, it equals capacitive reactance.

Dissipation factor (DF) of a capacitor is the ratio of energy dissipated to energy stored in the dielectric. DF is a figure of merit for the quality of a capacitor.

$$DF = ESR/X_C \times 100\%$$

Ideally capacitors have low values of DF over wide temperature ranges.

Q or Quality factor is the ratio of energy dissipated to energy stored, so it is the reciprocal of dissipation factor at low frequencies.

$$Q' = 1/DF = X_C/ESR$$

The highest quality capacitors have high Q's.

Ripple current is the result of a periodic AC voltage wave superimposed on the DC voltage applied to the capacitor. Ripple current flowing through the ESR of a capacitor can generate heat, raising the temperature of the capacitor.

Volumetric efficiency is a measure of relative capacitance per unit volume. One capacitor has a higher volumetric efficiency than another capacitor of the same size (volumetric dimensions) if it is able to store more charge, or has a higher capacitance rating.

# Capacitor applications

Capacitors have many different applications in electronic circuits:

- Blocking—limiting the flow of direct current or low frequency alternating current without significantly affecting the flow of high-frequency AC.
- Bypassing—providing a lowimpedance path around a circuit component to permit the flow of alternating current
- Coupling/decoupling—coupling or decoupling alternating signals between circuits and systems.
- Energy storage—storing electric energy for later release to power a device or circuit.
- Filtering—removing the DC component from a signal.
- Smoothing—reducing the ripple on an input signal
- Timing—providing capacitance value in timing circuits.
- Tuning—providing capacitance value for tuning in a tank circuit.

# **Fixed capacitors**

Figure 2 is a diagram showing how fixed capacitors are classified as *electrostatic* and *electrolytic*. Electrostatic capacitors are so named because an electrostatic charge is stored between opposing plates. They are named for the dielectrics between their plates. This can be air or a vacuum or such solid

materials as plastic film, ceramic, mica, and glass.

Electrostatic capacitors are further classified by packaging method: leaded or non-leaded (chip); radial or axial leaded; molded, conformally coated, or dipped in an encapsulant, typically epoxy. A film capacitor can be further classified by the specification of its plastic film such as polyester or polycarbonate.

Electrolytic capacitors are made of metals, normally either aluminum or tantalum, that form extremely thin anodic oxide layers of high-dielectric constant and good electrical characteristics during electrolytic processing. These capacitors are classified by the metal from which their anodes are made—aluminum or tantalum—and capacitor configuration: wet foil, wet slug, or dry slug (solid electrolyte).

# Film capacitors

Film capacitors are made with thin dielectric plastic films such as polyester (Mylar), polycarbonate, polystyrene and polypropylene that is 0.06 mil (1.5 micrometers) to over 0.8 mil (20 micrometers) thick. The electrodes of film capacitors can be metal foil (film/foil) or metal directly deposited on the film (metalized). Film/foil capacitors are made of dielectric film sandwiched between tin or alumi-

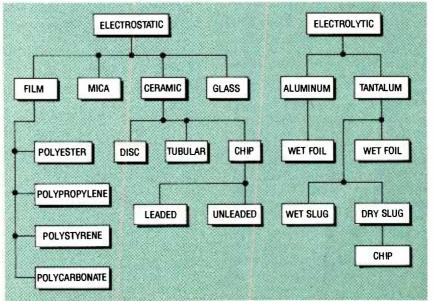


FIG. 2—POPULAR FIXED CAPACITORS are organized as electrostatic and electrolytic, and identified by their dielectric and package style.

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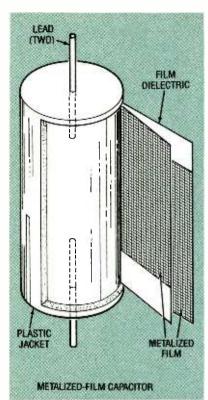


FIG. 3—VIEW OF PLASTIC-FILM capacitor shows how metalized: film dielectric (with leads connected) is rolled into a cylinder and jacketed with molded or conformally coated plastic.

num foil plates (about 0.25-mil thick). They are most widely specified for energy storage, pulse discharge, and arc suppression applications.

The plates of metalized capacitors are very thin vacuum-deposited layers of aluminum or zinc, which permits these capacitors to be smaller and lighter than film/foil capacitors with the same capacitance ratings. These capacitors can be made as shown in Fig. 3, or the metalized film can be cut into rectangles and stacked. The stacks are then leaded and molded in a protective encapsulant package.

Self-healing is a very important feature of metalized-film capacitors. A localized dielectric breakdown caused by a transient overvoltage will not necessarily cause capacitor failure because the metalized film around the fault evaporates without shorting the adjacent metalized plates. This response isolates the fault and effectively restores the electrical properties of the capacitor.

Both film/foil and metalized-film capacitors are made with axial or radial leads in a variety of case sizes. They can be hermetically sealed in tubular or rectangular metal cases, or encapsulated by molding or conformally coating with epoxy.

Film capacitors are most widely specified for capacitance values from 500 picofarads to 10 microfarads. (Refer to Table 2.) Their working voltages typically range from 50 volts DC to 630 volts DC—although they can have higher ratings. Capacitance tolerance is typically from  $\pm 1\%$  to  $\pm 10\%$ 

### Film dielectrics

The four most widely used film dielectrics are:

- Polyester (tradenamed Mylar) capacitors are the most popular general-purpose film capacitors. This film permits high volumetric efficiency, low leakage, and a moderate temperature coefficient. Some film/foil and metalized units can operate to 125°C at 50% of rated voltage. Metalized-polyester units can perform blocking, coupling, decoupling, bypass, and filtering.
   Polycarbonate capacitors
- Polycarbonate capacitors have operating temperatures from -55°C to as high as +125°C with proper voltage derating.

Capacitive tolererances can be as low as  $\pm 5\%$ . This dielectric film offers high insulation resistance and stability.

- Polystyrene capacitors have characteristics that are similar to those of polypropylene, but they have lower volumetric efficiency. They have capacitive tolerances as low as 1%. Film/foil units are widely used in inductive-capacitive filters.
- Polypropylene capacitors have higher volumetric efficiency than polyester capacitors. Except for AC rating, their characteristics are similar to those made from polystyrene. They have tolerances as low as ±2%. These capacitors are specified where precision, reliability, and low losses are important: e.g. tuning, filtering, and timing.

# Ceramic capacitors

There are three ceramic capacitor styles: single-layer disc, single-layer tubular, and monolithic multilayer. There are three principal classes of ceramic dielectric based on their k rating: Class I, II, and III. Low-k materials have linear characteristics, and their properties are independent of frequency over their normal range. They are suitable for resonant-circuit or filter

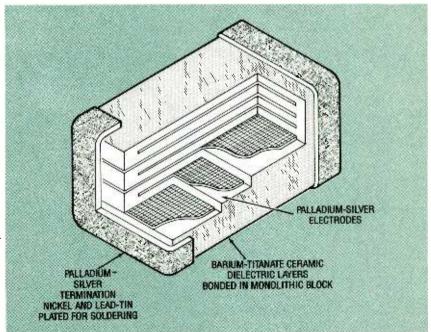


FIG. 4—CUTAWAY VIEW OF A CERAMIC MULTILAYER CHIP capacitor shows noblemetal electrodes deposited on thin layers of ceramic dielectric which are then pressed and fired to form a monolithic unit.

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characteristics. High-K ceramics have very high effective dielectric constants. They are suitable for coupling and de-

coupling applications.

 Disc ceramic capacitors are made by metalizing both surfaces of a thin low-k (Class III) ceramic disc with silver-based ink to form the electrodes, firing the disk, and soldering on radial leads. They are jacketed by dipping in phenolic resin or epoxy. These capacitors are being replaced by tubular ceramic units made of the same materials that save circuit board space and permit automatic parts placement.

 Tubular ceramic capacitors are made by coating the inner and outer surfaces of Class III ceramic tubes with silver-based thin-film ink, firing, and attaching leads to the tube before jacketing it by epoxy dipping.

 Monolithic multilayer ceramic (MLC) capacitors are made by screening thin-film, precious metal-based conductive ink on thin layers of "green" or unfired layers of higher k (Class II and III) ceramics. The screened layers are then stacked (up to 40 layers), compressed, and fired to form monolithic capacitors, as shown in Fig. 4.

If the MLC capacitor is to be a chip capacitor for a hybrid circuit or surface-mounting, conductive-metal terminations are plated on its ends, as shown in Fig. 4. The terminals of surfacemount chips are further plated with lead-tin alloy to improve the terminal-to-pad solder

Demand for MLC chips has risen with the worldwide growth of surface mounting. Chip MLC's will withstand the molten- solder temperatures encountered in reflow and wave soldering. They are available in standard sizes to fit the grasping tools in automated pick and place machines. The most common sizes are  $0.08 \times 0.05$  inch (0805),  $0.125 \times 0.063$  inch (1206), and  $0.05 \times 0.225$  inch (2225).

Cylindrical leadless capacitors are also made for surface mounting. These capacitors

TABLE 2 CHARACTERISTICS OF POPULAR FIXED CAPACITORS

Туре	Capacitance Range	Working Voltage	Maximum Operating Temp. (C)	Tolerance (Percent)
Electrostatic				
Film				
Polyester (Mylar)		No. 11 61 LLD		
Film/foil	0.001—1.0	80-200 VDC	+ 125*	±5—±10
Metalized	0.001—10.0	60—630 VDC	+ 125*	±5—±10
Polycarbonate				-1
Metalized	0.01—10	100—630 VDC	+125*	$\pm 5 - \pm 10$
Polystyrene				
Film/foil	47 pF-0.039	63—630 VDC	+ 85	±1±5
Polypropylene				
Film/foil	47 pF-0.022	63—630 VDC	+ 85	±2-±5
Metalized	0.001-3.3	250-100 VDC	+ 85	±5-±10
Ceramic				
Multilayer	10 pF56	200 VDC	+ 125	±5-±10
Disc	.75 pF—2.2	50—6 KVDC	+ 125	±5-±10
Mica	1 pF-0.1	50,000	+150	±.25-±5
Glass	10 pF—0.15	6000	+ 125	±1-±20
Electrolytic				
Aluminum	1.0—1 MEG	5-450	+ 105	-10-+100
Tantalum				
Wet slug	1.7—2400	6-630	+ 125	±5-±20
Wet foil	.12-3500	3-300	+125	±5-±20
Solid slug	0.0023-1000	6-100	+ 125	+5-±20

With derating

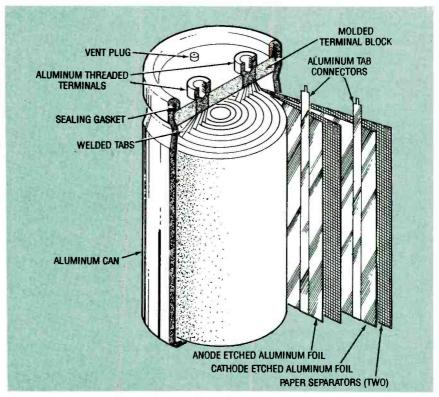


FIG. 5—VIEW OF AN ALUMINUM ELECTROLYTIC CAPACITOR shows how the cathode (porous paper spacer filled with liquid electrolyte) is sandwiched between the oxidized aluminum anode foil and cathode connection foil, rolled into cylinder, and then sealed in an aluminum can.

have metalized-band contacts on the ends of their epoxycoated bodies for soldering to lands of surface-mount circuit boards.

For conventional throughhole mounting, axial or radial leads are attached, and the chip is jacketed by dipping or molding in epoxy. MLC capacitors are specified for bypassing noise to ground, timing, and frequency selection.

### Ceramic dielectrics

Ceramic dielectric materials are classified by dielectric constant *k* as Class I, Class II and Class III:

- Class I dielectrics are made by mixing magnesium titanate (for a positive temperature coefficient) with calcium titanate (for a negative coefficient) to form a dielectric material with low k values, and properties essentially independent of frequency. They exhibit ultrastable temperature coefficients of ±30 ppm/°C over the temperature range of -55° to +125°C. Class I includes NPO (negative, positive, zero), also known as COG and BY.
- Class II dielectrics are high-k materials (called ferroelectrics) based on barium titanate. With the addition of barium stanate, barium zirconate, or magnesium titanate, their dielectric constants can be lowered from values as high as 8000 for increased temperature stability. These dielectrics include general purpose X7R (BX) and Z5U (BZ).
- Class III dielectrics were developed primarily for ceramic disc capacitors because they permit high volumetric efficiency. But this introduces a tradeoff between high leakage resistance and low dissipation factor. Class III capacitors have low working voltages.

### Other electrostatic capacitors

The dielectric in a *mica* capacitor is mica, a natural mineral that is chemically inert and very stable. The capacitor is generally made as a "sandwich" of alternating layers of tin-lead foil plates and mica. These capacitors can operate at tempera-

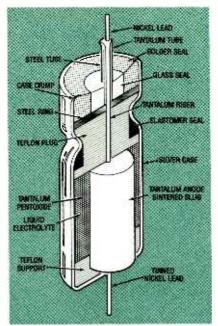


FIG. 6—CUTAWAY VIEW OF WET-SLUG tantalum capacitor shows tantalum slug filled with wet-electrolyte sealed in a silver case.

ture up to  $+150^{\circ}$ C. Silvered mica capacitors offer greater mechanical stability and more uniform characteristics. They are made by screening and firing a thin layer of silver on the surface of the mica to form the plates.

Glass capacitors are made by stacking alternate layers of thin glass dielectric in a sandwich structure similar to that of the mica capacitor. They are specified where temperature stability is a requirement.

## **Electrolytic capacitors**

The dielectrics of aluminum and tantalum electrolytic capacitors are oxides formed by electrochemical reaction with those metals. There are three styles of electrolytic capacitor: wet foil, wet slug, and dry or solid slug. Aluminum electrolytic capacitors are wet foil units, but tantalum capacitors are also available as wet-slug and solid slug units. They can be *polarized* or *nonpolarized*.

All electrolytic capacitors exhibit high capacitance per unit volume (high volumetric efficiency). An aluminum electrolytic capacitor can store four, five or more times the charge of an equivalent-size film capacitor, and a tantalum capacitor

can store three times as much charge as an equivalent aluminum capacitor.

However, aluminum electrolytic capacitors have higher DC leakage and lower insulation resistance than electrostatic capacitors. Moreover, they have higher power losses because of their higher equivalent series resistance (ESR).

The anodes of aluminum electrolytic capacitors are made from high-purity aluminum foil that has been electrochemically etched to increase its effective surface area. A thin aluminum-oxide-dielectric layer, about 0.01 micron, is then grown on the etched foil in another electrochemical process. The enlarged surface area of the etched foil provides a far larger dielectric surface than would be possible with unetched foil.

A porous paper spacer filled with a liquid electrolyte is sand-wiched between the etched and oxidized anode foil and another aluminum cathode foil. The liquid electrolyte is the actual cathode, but the cathode foil is in contact with the liquid electrolyte and is needed to complete the electrical circuit.

After attaching a series of connecting tabs to the foils, the "sandwich" is rolled, as shown in Fig. 5, and inserted in an alu-

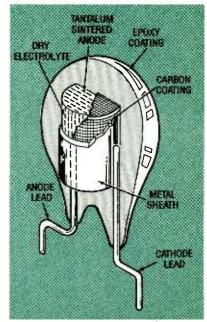


FIG. 7—CUTAWAY VIEW OF A SOLID tantalum capacitor jacketed by dipping in epoxy.

minum can, which is then sealed. However, the sealed can has an overpressure vent.

Direct current must flow in only one direction in a polarized electrolytic capacitor. Even short-term current reversal could destroy the oxide dielectric and short-circuit the capacitor. A "+" mark on the case identifies its positive terminal.

Aluminum electrolytic capacitors are made with radial or axial leads, and some styles for switchmode power supplies have spring-metal terminals that snap into circuit board holes. An external plastic sleeve permits off-ground applications for the capacitor.

Nonpolarized aluminum electrolytic caps are essentially two polarized capacitors back-to-back with their cathode terminals connected. The anode terminals make the external circuit connection, while the cathode terminals are isolated by an insulator. Both foils are anodized to form oxide barriers, and they share a common electrolyte-filled porous spacer.

A nonpolarized capacitor has half the capacitance of a comparably sized polarized capacitor with the same voltage rating. Although not as efficient as polarized capacitors, the nonpolarized units are used for AC motor starting and other AC control applications.

### **Tantalum capacitors**

Tantalum electrolytic capacitors are available in three forms: wet-foil, wet slug, and dry slug. Wet-foil tantalum capacitors are made in about the same way as aluminum electolytics. As a group, tantalum capacitors exhibit higher volumetric efficiency, more stable characteristics, higher operating temperature ranges, and longer shelf lives than aluminum capacitors. However, they cost more and have lower voltage ratings.

Both wet and dry slug tantalums are made from porous pellets of tantalum. The anode slug is formed by pressing tantalum powder and a binder in a mold, and firing it in a vacuum furnace (sintering) to bond the powder and drive off the binder.

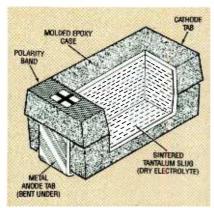


FIG. 8—CUTAWAY VIEW OF A SOLID tantalum capacitor chip for surface mounting applications.

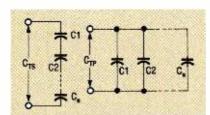


FIG. 9—CONNECTING CAPACITORS in series yields a total capacitance that is less than that of the lowest-value unit (a), but connecting them in parallel yields a total capacitance equal to the sum of all unit values.

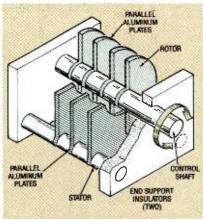


FIG. 10—SIMPLIFIED DRAWING of a tuning capacitor shows a concept that is used in many variable capacitors.

The tantalum oxide dielectric is electrochemically formed in the porous pellet.

Figure 6 is a cutaway view of a wet-slug tantalum capacitor with an acid electrolyte. Its volumetric efficiency about three times that of a comparably sized foil unit. Moreover, wet-foil tantalums are the most reliable of all capacitors.

The high cost of wet-foil and wet-slug tantalums makes

them too expensive for most consumer and industrial applications. However, those high-reliability capacitors are widely specified for military electronics and avionics. Military specifications MIL-C-3965 and MIL-C-39006 govern the procurement of military-style wet-foil and solid-slug units.

The solid-anode or dry-slug unit, shown in Fig. 7, is the most popular and economical tantalum capacitor. It has a thin film of manganese dioxide chemically deposited on its tantalum dioxide dielectric to act as a second electrode. Solid-slug capacitors can be sealed in metal cases, or protected by dipping in epoxy as shown in Fig. 7. The solid-slug units have the longest life and lowest leakage of any tantalum caps. Chip capacitors for surface mounting, as shown in Fig. 8, are made by the same process.

# Capacitor identification.

Today the capacitor's nominal value (and sometimes its tolerance) are printed on its body where space permits. Values such as 47 and 68 are typically in microfarads, while values such as 120 or 4700 are usually in picofarads. A capacitor might also be marked with its working voltage: for example, 63 V or 100 V.

Some capacitors are still marked with colored bands based on the EIA system used for identifying resistors. The colors of the bands are read from left to right. A black band represents zero, brown represents one, and red, orange, yellow, green, blue, and violet represent the digits two to seven, in that order. Grey represents eight, and white represents nine. As in resistor coding, a gold band denotes a capacitive tolerance of 5%, while a silver band denotes 10%

You might encounter capacitors with obsolete coding schemes in old radios or TV's or at surplus sales. Some of those codes are based on colored dots, spots or "hashmarks." It is wise to consult a radio engineering handbook or data reference book published before 1970 if

you want to find out how to interpret those codes if you plan to use them in your circuits and are in doubt about their ratings.

# Connecting capactors

Figure 9 illustrates capacitors connected in series and parallel. The formula for calculating the effective value of two capacitors in series is:

 $C_{TS} = C1 \times C2/C1 + C2$ For two or more capacitors in series it is:

 $C_{TS} = 1/1/C1 + 1/C2 + 1/C3 + 1/C3$ 

For capacitors in parallel the formula is:

 $X_{TP} = C1 + C2 + C3 + C_n$ 

# Variable capacitors

For many years the most prominent variable capacitors were those used to tune radio receivers, transmitters, and oscillators. However, in the latest transistorized equipment they have been largely superseded by varactors or voltage variable capacitors. These are silicon or gallium arsenide PN junction diodes that make use of the variation of junction capacitance with reverse bias. Nevertheless, the design concept embodied in the tuning capacitor lives on in a wide range of miniature, PC board-mounted variable capacitors for many different tuning applications.

Figure 10 is a simplified sketch of an air-dielectric tuning capacitor. Its capacitance value can be changed by rotating its control shaft so that the movable set of metal plates (rotor) meshes in different positions with respect to the fixed set (stator). Its capacitance value is greatest when the rotor is fully meshed with the stator.

The rotor plates of tuning capacitors can be shaped so that, with shaft rotation, capacitance variation is linear or nonlinear. For example, it might follow a nonlinear logarithmic or square law function. Two or more tuning capacitors can be ganged together so that they vary in unison, simultaneously tuning separate circuits to different frequencies.

Trimmer capacitors are "set and forget" variable capacitors made for infrequent adjustment. Many different types are available for commercial and industrial applications. Vane types are miniaturized versions of the tuning capacitor shown in Fig. 10, except that layers of solid dielectric, typically plastic, are inserted between the rotor and stator plates.

Vane-type trimmers with body diameters of less than a half inch are made for PC-board mounting. They have plastic cases and dielectrics of polypropylene, polyethylene, polycarbonate, or PTFE films. These trimmers are made for screwdriver and/or key adjustment.

There are also simpler trimmer capacitors that permit more limited capacitance variation for high-frequency tuning applications.



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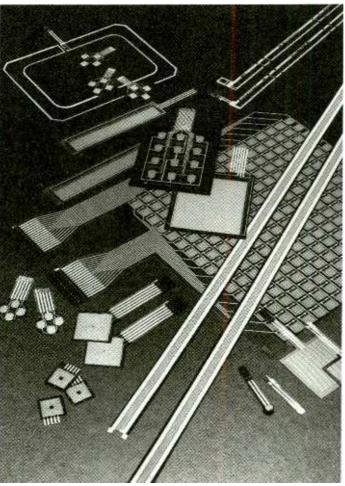
# FORCE-SENSING RESISTORS

ONE OF THE MANY modern sensor technologies is really keeping engineers and hobbyists quite busy designing circuits. Billed as the ultimate switch technology, the Force Sensing Resistor (FSR) is a tactile sensor that discerns variations in applied force. The harder you press this thick-film device, the more its resistance decreases. The FSR was first developed for musicians who wanted their electronic pianos to play louder when the keys were pressed harder. FSR's are temperature, chemical, and moisture resistant, and they are insensitive to vibration and electromagnetic interference. FSR's contain no moving parts to wear out, and can withstand

over ten million operations. Figure 1 shows some of the dif-

ferent types of FSR's.

FSR's are as thin as business cards, and can be designed to sense forces as light as a fingertip or as heavy as a truck. They can also sense variations in applied pressure and alter their response accordingly. In addition, the sensor's actuation threshold can be adjusted using simple electronics. Applications for FSR's are virtually unlimited, as you can see from Table 1. The FSR is ideally suited to keypads, computer input devices, touch switches, alarm sensors, limit switches, electronic keyboards, digitizers, and pressure sen-



Force-sensing resistors open up lots of new applications for electronics.

T.L. PETRUZZELLIS

sors.

An FSR device typically exhibits three decades of dynamic resistance change with respect to force and it can operate at much lower currents than most

other sensors. The FSR can also be used to construct a linear potentiometer which can monitor the position of a force as well as the amount of applied force. A threelayer XYZ-type FSR device can be constructed that will give an X-Y coordinate position indication with a 0.005-inch resolution, as well as provide the force (Z) measurement. The XYZ pad is ideal for such applications as a graphic pad, pen stylus tablet, or mouse-type device for computer input. The FSR sensors can also be configured into many different types of switch arrays, with sizes up to  $22 \times 32$ inches, at much lower cost than many other force

In the past, there were two principle types of force sensors: piezopolymers and ceramic strain gauges. The fast rise times and high sensitivities of the piezopolymers cause a lot of unwanted acoustic and vibration pickup. Piezopolymer sensors often require more complex interfacing than the FSR devices. FSR sensors are not as accurate for precise absolute measurement, but they are much more rugged and cost considerably less than straingauge sensors.

The construction of an FSR is a sandwich of two polymer films or sheets. A conductive pattern is deposited on one of the polymer sheets as a pattern of inter-

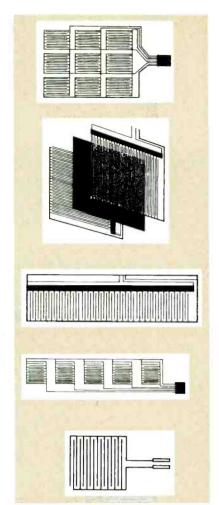


FIG. 1—FORCE-SENSING RESISTORS contain no moving parts to wear out and then can withstand over ten million operations

digiting electrodes as shown in Fig. 2. The electrode pattern often looks like a comb, with the teeth and spacing typically being less than one millimeter. Next, a proprietary polymer is deposited on the other sheet. The sheets are then faced together so that the conducting fingers are shunted by the polymer.

The output resistance of the FSR is typically around one megohm with no external force applied. A force-versus-resistance graph is shown in Fig. 3. The graph displays the log/log characteristics of an FSR where the resistance varies from one megohm to around 50 kilohms, depending on the applied force in grams (g). (We know that a gram isn't really a force, but let's just think of it that way for the moment.) Figure 4 shows a

### **TABLE 1—FSR APPLICATIONS**

Graphic pads
Cursor keys
Mouse devices
Pen stylus tablets
Pressure sensors
Piano keyboards
Toner-level sensors
Foot pedals
Gait-analysis sensors
Artificial-limb force sensors
Dental-byte sensors
IV drip pressure sensor
Bed weight distribution sensor
Security tiles/alarm sensors
Load cells

Suspension sensors
Accelerometers
Water-level sensors
Panel switches
Digital tuning controls
Joysticks
Game controllers
Steering wheels
Gas pedals
Robotic touch sensors
Industrial keyboards
Deadman safety switches
Smart brake pedals
Oil-pressure sensors
Limit switches

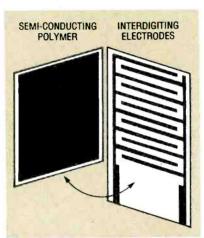


FIG. 2—AN FSR IS MADE OF two polymer films or sheets. A conductive pattern is deposited on one of the polymer sheets, and a proprietary polymer is deposited on the other sheet.

force-versus-conductance graph in which a simple linear response is shown from a force of zero grams. A key element in the design of an FSR is the fineness of the pitch of the conducting fingers. The force-versus-resistance relationship is strongly affected by sensor and actuator size, shape, and materials.

# Linear potentiometer FSR's

When force-sensing resistors are used to make a linear potentiometer (an FSR-LP), the device can be used to sense both position and applied force. Figure 5 depicts the layered construction of an FSR-LP. When wiring an FSR-LP, a voltage is

applied between the hot lead and ground. When a force is applied to the force-sensing layer, the wiper contacts are shunted through that layer to one of the conducting fingers of the resistance strip. The voltage from the wiper is then proportional to the distance along the strip. To sense a force, a resistance measurement is made between the wiper terminal and either the hot or ground lead. Two alternative FSR-LP connection diagrams are shown in Fig. 6.

Force and position measurements are not entirely independent; however, the position measurement can be made unambiguously if the measuring device draws a negligible amount of current (less than 1 microampere) so that there is no voltage drop across the wiper resistance. Therefore, an LF411 or similar op-amp-with a low V<sub>OS</sub> and l<sub>BIAS</sub>—is recommended when interfacing to an FSR-LP. Because the contact between the wiper and the resistor is momentary, some kind of sampleand-hold device must be used to interface an FSR; quite often a capacitor between the wiper contact and ground is sufficient to accomplish this.

Force measurements are less ambiguous, and very good approximate measurements can be obtained by shorting the two fixed resistor ends (hot and ground) together, and measuring the resistance between the

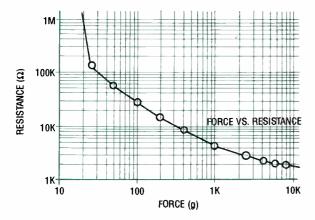


FIG. 3—FORCE-VERSUS-RESISTANCE. The resistance varies from one megohm to around 50 kilohms, depending on the applied force.

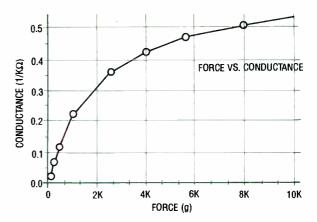


FIG. 4—FORCE-VERSUS-CONDUCTANCE. The linear response is shown from a force of zero grams to 10,000 grams, or 10 kilograms.

combined leads and the wiper. If the force is applied at the middle of the potentiometer, the device will have an additional resistance of one half of the total fixed resistance, because the resulting middle contact parallels the two halves of the fixed resistor. If, on the other hand, force is applied to either end of the FSR-LP's active area, the fixed resistance is essentially shorted out. That problem can be overcome by making the FSR resistance high compared to the potentiometer resistance, therefore making a low-current position measurement a must. The slight force-measurement error can also be subtracted out with a simple analog circuit or, given a position measurement, compensated for in software if a microprocessor is used with the system.

The positional resolution of a force and position sensing resistor (FPSR) depends on the width of the applied force, distribution, and the fineness of the conductive fingers, which is typically in the 10–100 micrometer range.

### **FSR-LP XYZ**

An XYZ pad or tablet is constructed by placing two FSR-LP's back-to-back and perpendicular to each other. An XYZ pad can measure the position of a force on an X-Y coordinate plane, as well as the applied force (Z). Figure 7 shows the layered construction of an XYZ pad. Note that an unambiguous

position can be measured only for a single applied force; multiple force contacts will cause false readings. That is not a problem for graphics pads, mouse devices, or pen stylus tablets, but the XYZ pad cannot be used for complex pattern recognition. Position accuracy of an XYZ pad based on FSR-LP's is typically about 1 percent.

A true force sensor will give a constant reading at a constant force, independent of the area over which the force is applied, or its distribution. If a constant force is applied to a true pressure sensor, the reading will be inversely proportional to the area of the applied force. An FSR has a function that is between a force and pressure sensor. A typical FSR will display the resistance of the square root of the area of the applied force. That holds true when the force footprint is smaller than the FSR's active area, and large compared to the spacing between the conductive electrodes or fingers. Because of the sensitivity of the FSR's resistance to the area and distribution of force, the force footprint must be held constant in position and distribution. An elastomeric or rubber overlay placed over the sensor can solve that problem. The FSR can be used as a pressure sensor when the applied force is large compared to the FSR's active area.

FSR devices are designed to be easily interfaced with a wide variety of circuitry. A simple

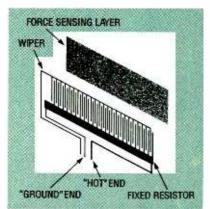


FIG. 5—FSR-LP'S CAN SENSE both position and applied force. This is the layered construction of an FSR-LP.

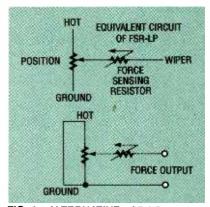


FIG. 6—ALTERNATIVE FSR-LP connection diagrams.

analog interface is shown in Fig. 8. A basic requirement for interfacing an FSR is to ensure that the current through the device does not exceed 1 mA/cm<sup>2</sup> of the activation footprint. The voltage measurement across the FSR is then related to the applied force, and increased pressure results in increased

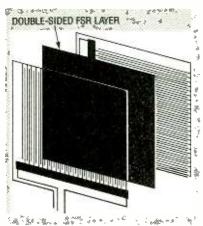


FIG. 7—AN XYZ PAD IS TWO FSR-LP's back-to-back and perpendicular to each other.

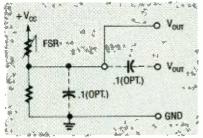


FIG. 8—FSR ANALOG INTERFACE. Increased pressure results in increased voltage output.

voltage output. Precision measurements, however, are a somewhat more difficult because of the shape of the power law curve. For higher precision measurements, it is usually wise to go into the digital domain as soon as possible, so that the log/log characteristics of the device can be translated into more linear results.

If your design calls for measurement of impact (i.e. a data keyboard), then the FSR can be placed in a voltage divider, and the divider can be capacitively coupled to the succeeding stages. That would eliminate offset problems due to a preload condition. The interface shown in Fig. 9 is useful where a higher current or a lower source impedance is necessary. The opamp can be used either as a unity-gain buffer, or it can be configured to amplify the FSR's output. Offsets can be trimmed by the 500-ohm potentiometer. Gain is set by the ratio of the resistors R<sub>F</sub> and R<sub>S</sub>. Suggested op-amps for that circuit are the

LF351/353 or the TL071/72 series of low bias-current devices. The low bias currents of those op-amps reduces the possible input offsets, due to the high source impedances of the FSR.

Figure 10 shows a force-to-frequency converter. In that circuit, an oscillator is constructed with the FSR as a feedback element around a Schmitt trigger integrated circuit. At zero pressure, the FSR is an open circuit. Depending on the last stage of trigger, the

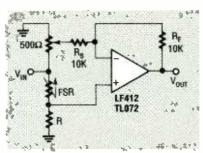


FIG. 9—THIS INTERFACE is useful when higher current or lower source impedance is necessary.

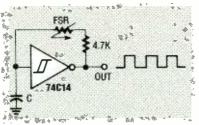


FIG. 10—FORCE-TO-FREQUENCY CON-VERTER. An oscillator is constructed with the FSR as a feedback element around a Schmitt trigger.

output remains constant-either high or low. When pressure is applied to the FSR, the oscillator starts, and its frequency increases with increasing force applied to the FSR. Resistor R1 limits the current through the sensor. Bypassing R1 with a capacitor will cause the curve to be steeper at higher forces. Connecting a large-value resistor in parallel with the capacitor (C), quenches any tendency for the circuit to oscillate at low applied forces. When using the circuit with CMOS or TTL, a digital process can be controlled by counting leading or trailing edges of the oscillator output.

Industry-standard connectors, such as pin- or com-



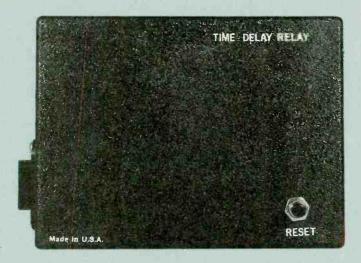
FIG.11—THIS PHOTOGRAPH shows some of the many different shapes and sizes of available force-sensitive resistors. The ruler in the lower right-hand corner gives you an idea of their size.

pression-types, can interface the FSR devices. Conductive adhesives are also commonly used to attach leads to FSR devices. Do not attempt to solder wire leads directly to the polymer sensor, because direct heat will destroy the device.

The force-sensing resistors require a backing for activation accuracy, as mentioned previously. The most unpredictable aspect of the FSR's force/resistance characteristic is the pressure range under 100 grams/ cm<sup>2</sup>. If you are going to measure small forces with your FSR, you can preload the FSR with a 100-200 gram/cm<sup>2</sup> load and measure the resistance changes. Elastomer or plastic overlays can be used to enhance the FSR's response characteristics by evenly spreading the actuator's force.

FSR sensors are available in many sizes, configurations, and shapes, and custom devices can be designed by the manufacturer. For more information on FSR technology, write on your company letterhead to Interlink Electronics, 1110 Mark Ave., Carpinteria, CA 93013. An evaluation/prototype kit is also available for \$79.95.





# TIME DELAY RELAY

**JAMES MELTON** 

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**OUR TIME-DELAY RELAY WILL DRIVE** up to a 3-ampere AC load for a specified period of time, and then shut the load off automatically. It can turn electrical appliances and lights off after a time interval ranging from just a few seconds all the way up to about an hour.

One of the many possible jobs for the relay is the control of indoor Christmas lights-just push a button and the lights will stay on for a few hours, and then automatically turn off. Outdoor Christmas lights, although a considerably larger load, can also be controlled by one of these relays.

The author has several different antennas that are connected to amateur radio equipment in his garage. As a precaution, the feedlines to the radios are routed through mechanical relays that keep them grounded when not powered, and they are connected to the radios only when the reset switch on the time-delay relay is pushed. Several hours later, if he has been called away from the radios (and forgotten that they were on), the relay drops out, and the antennas will have been automatically grounded.

One of these units can even be used with a coffee maker. Quite often coffee makers are left on overnight or over the weekend: the owner returns to find a ruined coffee pot-and a very hot one at that. A time-delay relay in the burner circuit will solve that problem. Simply set the timer to stay on for 2 hours, and if it's not reset, it will allow the coffee pot to cool off.

Operation

The circuit, shown in Fig. 1, is based on a 4060 CMOS 14stage binary counter with an on-board oscillator driver. The basic frequency is set by the values of R1, R2, and C1, and it's

roughly 1/R1×C1. Resistor R2 should be about 10 times the value of R1. The values shown generate an approximate 4.5hertz frequency, which is then divided down by IC1. Divided outputs are available ranging from divide-by-4 to divideby-16384 (see Fig. 1).

The chosen output is tied to the base of Q1 through currentlimiting resistor R4, and to the base of Q2 through R3. Transistor Q1 is the hold transistor for the timing circuit, and transistor Q2 turns on the solid-

state relay.

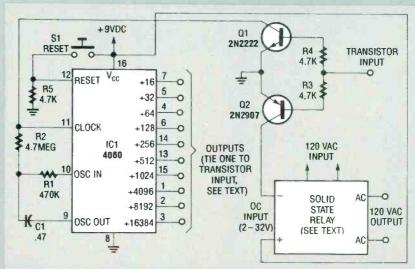


FIG. 1—THE CIRCUIT is based on a 4060 CMOS 14-stage binary counter that controls a solid-state relay.

When you push reset button S1, all of ICI's outputs go low (including the one you have tied to the transistor input). Transistor Q1, an NPN unit, shuts off and its collector, which is tied to timing resistor R2, presents no load to the timing circuit. Transistor Q2, a PNP unit, turns on when a low is applied to its base, thus turning on the solid-state relay.

When the chosen output of IC1 goes high, Q1 turns on, grounding the clock input to IC1, stopping any further counting until S1 is pushed again. At the same time, Q2 shuts off, which turns off the solid-state relay, thus cutting off power to the load.

# Construction

The author built his pro-

# PARTS LIST

All resistors are 1/4-watt, 5%.

R1-470,000 ohms

R2—4.7 megohms

R3-R5-4700 ohms

Capacitors

C1-0.47 µF, 25 volts, tantalum

Semiconductors

IC1-4040 CMOS timer/divider

Q1-2N2222 NPN transistor

Q2-2N2907 PNP transistor

S1—Normally-open pushbutton switch

Miscellaneous: Solid-state relay (sized for the application you have in mind), perforated construction board, wire, solder, AC linecord, project case.

# The relay in action

To use the solid state relay, simply plug the relay into a 120-

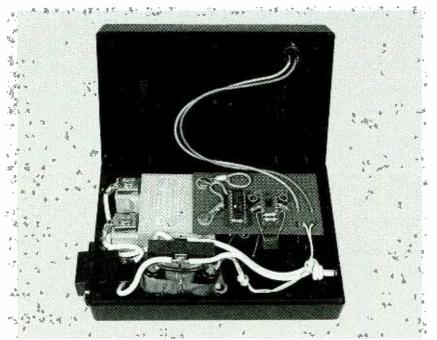


FIG. 2—THE PROTOTYPE RELAY is built on a small piece of perforated construction board mounted on the end of the solid-state relay.

totype relay on a small piece of perforated construction board using point-to-point wiring, and arranged the parts so that the board would mount on the end of the solid state relay (the input terminals are big enough to support the circuit board). Figure 2 shows the inside of the prototype. Note that the author has built in a 9-volt power supply that is not shown in the schematic.

volt outlet, plug an appliance (that draws no more than 3 amperes) into the time-delay relay, and push the reset button. The circuit will begin timing and will shut off at the end of the period you have selected. When you use the time-delay relay to shut off your appliances, you'll not only be adding a safety feature and saving money—you'll also be doing something good for the environment!

# **LETTERS**

continued from page 17

diovisual phenomenon discussed anywhere. During a TV broadcast of a choir singing, my attention would inevitably focus on an individual singer (usually the cute one), and I would swear that I could hear her individual voice against a background of the entire choir.

Sure enough, when the camera zoomed in on her, she sounded exactly as I had earlier perceived she would. If there were several attractive choir members, I would be able to pick out their individual voices too. The cameraman apparently often agrees with my choices, and pans his camera on the photogenic singers during the performance. I can even keep track of their individual voices with closed eyes.

The same phenomenon seems to occur during orchestral performances, where I seem to be able to isolate individual instruments from the whole orchestra.

I cannot think of a way to test this phenomenon scientifically because what comes out of the speaker is a blended waveform. Thus, the perception must be the result of my visual clues together with the audio. I will chicken out with an escape clause: The human brain must be a wondrous organ if it is able to interpret such fine subtleties from a blended signal. But, all the same, I wonder if anyone else shares my illusions, or is there something more to this?

KELVIN MOK Edmonton, Alberta, Canada

### SILICON CHIP

I was recently looking at *Silicon Chip*, an Australian electronics magazine that had lots of interesting projects in it. It would be good if **Electronics Now** could reprint some of these articles for readers in this country.

WILLIE JONES

Valley Stream, NY

Good news for you! The magazine you mentioned, Silicon Chip, will soon be in print in this country. See the ad for it on page 25 of this magazine.  $\Omega$ 

# March 1993, Electronics Nov

# BUILD THIS AUDIO MAN EXPANDER

### PHILL HAUSMAN

IT SEEMS THAT EVERYBODY IS AN audio enthusiast these days. With compact discs, stereo TV, hi-fi video tapes, and laserdiscs cheaply available to the general public, nobody wants to settle for ordinary sound. If you build our audio processor, you won't have to settle for ordinary sound either! Our audio processor, which can be built in one evening, can be installed easily between any audio output source and any audio input source, and it can "supercharge" any mono or stereo audio signal.

Some of the many uses for the audio processor include enhancing the audio output from a stereo system or any scanner, shortwave, CB, or ham radio receiver. Stereo and mono TV sound can also be greatly enhanced; a pseudo-stereo effect can be added to a mono soundtrack, and if stereo audio is already in use, you can add enhanced stereo effects. The processor also has amazing effects on old mono or pre-Dolby cassette and 8-track tapes—it's great for doing restoration of old recordings.

# **Features**

The audio processor provides a complete array of controls that give the user maximum flexibility in adjusting the processor. The unit has switch-selectable stereo sound from a stereo source, spatial (widened) sound from a stereo source, and pseudo-stereo sound from a mono source; LED's indicate which mode is selected.

The unit exhibits very low noise (-64 dB minimum) and low total harmonic distortion (maximum THD is 0.5% at 1000 Hz). The input and output resistance is 100 kilohms, which is the standard line-level resistance. The left and right channels provide a minimum of 60 dB separation, and there's an adjustable input attenuator for



# Enhance stereo and mono audio, for under \$30, with our one-chip audio processor.

each channel, which provides a minimum of 70.0 dB attenuation. There's independent gain adjustment of the left and right channels in the spatial stereo mode, and independent gain adjustment of the left and right channels in the mono pseudostereo mode.

# Theory of operation

The audio processor, whose schematic is shown in Fig. 1, is based on the Signetics/Philips TDA3810N stereo, spatial, pseudo-stereo processor IC. A block diagram of the chip is shown in Fig. 2. The device is essentially a system of internal op-amps used as active filters. The chip contains three op-amp stages, switching circuitry, power-supply regulation circuitry, and LED drivers.

The easiest way to understand how the chip works is to follow the audio signal through the chip for each individual mode.

## Stereo mode

When the stereo mode is selected, the left input signal

passes through input-attenuator R14, and is coupled via C4 to pin 2 of IC1 (the TDA3810N). The right input signal passes through R15 and C3 to pin 17 of IC1. The various active filters within IC1 serve as a unity-gain bandpass filter with a -3 dB low-frequency cutoff occurring at 20 hertz, and the -3 dB high-frequency cutoff occurring well beyond 20,000 hertz.

### Spatial mode

As shown in Fig. 3, when the spatial, or widened, stereo mode is selected, active op-amp circuits selectively remove certain parts of the audio spectrum. The effect is achieved by feeding the audio input to the non-inverting input of an opamp. The inverting input is fed by the output of the internal buffer/amplifier coupled with a cross-channel signal through R2. Both channels operate in the same way. The gain of each channel can be adjusted independently: R3 adjusts the left channel and R1 adjusts the right channel.

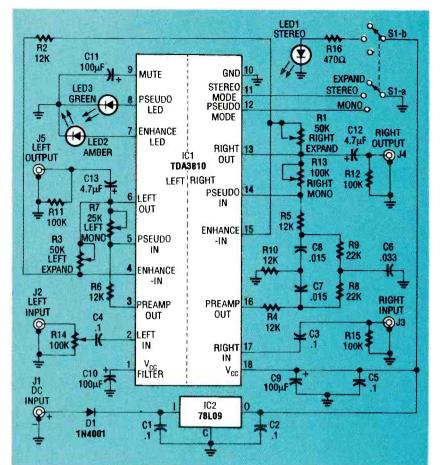


FIG. 1—THE AUDIO PROCESSOR is based on the Signetics/Philips TDA3810N stereo, spatial, pseudo-stereo processor IC.

### **PARTS LIST**

All resistors are 1/4-watt, 5%, unless otherwise noted.

R1, R3—50,000 ohms, panelmount potentiometer R2, R4–R6, R10—12,000 ohms

R7—25,000 ohms, panel-mount potentiometer

R8, R9—22,000 ohms

R11, R12—100,000 ohms

R13-R15—100,000 ohms, panelmount potentiometer

R16-470 ohms

Capacitors

C1–C5–0.1  $\mu$ F, 50 volts, metal film C6–0.033  $\mu$ F, 50 volts, metal film C7, C8–0.015  $\mu$ F, 50 volts, metal film

C9-C11-100 μF, 16 volts, electrolytic

C12, C13—4.7 µF, 35 volts, electrolytic

Semiconductors

IC1—TDA3810N audio processor chip (Philips)

IC2-78L09 9-volt regulator

D1-1N4001 diode

LED1-LED3—light-emitting diodes (use three different colors)

Other components

S1—DP3T panel-mount switch
J1—2.1 mm panel-mount power
jack (optional)

J2-J5-panel-mount RCA jack

Miscellaneous: 18-pin IC socket, metal project case, 12-volt DC wall transformer (100-mA), 6 knobs, PC board, shielded cable, wire, solder, etc.

Note: The following items are available from HESC, PO Box 12649, Fort Wayne, IN 46864-2649:

 A kit of parts including a PC board and all parts that mount on it (does not include potentiometers, project case, or wall transformer)—\$19.95 + \$3.05 S&H

 PC board and TDA3810N— \$14.95 + \$3.05 S&H

• TDA3810N—\$7.00 postage paid

Please allow 6 to 8 weeks for delivery.

# Pseudo stereo mode

As shown in Fig. 4, when the mono pseudo-stereo mode is selected, the processor creates a "stereo" image using the various active filters differently on each channel. The left channel is fed through a flat-response amplifier (200 Hz to 20 kHz) to achieve a constant gain across the audio spectrum. The gain is adjustable via potentiometer R7, which controls feedback. The optimum setting recommended by Philips, the chip manufacturer, is +2.00 dB at 15 kHz; R7 gives an adjustment range of -69.0 dB to +6.0 dBat 15 kHz.

The right channel uses a twin-T notch filter to give the illusion of signal separation, or the pseudo-stereo effect. Between 100 and 1600 hertz, the notch filter attenuates the audio range by -33.0 dB at its lowest point, which occurs at about 450 hertz. The gain is adjustable by R13, which controls feedback. Philips recommends 0 dB at 15,000 Hz, although R13 gives a range of -68.0 dB to +6.0 dB. Figure 5 shows the frequency response of each channel.

Remaining circuitry

The TDA3810 contains a muting circuit with built-in hysteresis (controlled by C11) that prevents the status LED's from flickering when switching from mode to mode. Also included is the mode selection switch (S1-a and -b) and the corresponding status indicators LED1, LED2, and LED3.

The project requires an external power supply of +10.5–24.0 volts DC, which passes through polarity-protection diode D1 to the input of IC2, a 78L09 +9.0 volt DC, 0.1-amp voltage regulator. Capacitors C1 and C2 provide decoupling and anti-oscillation protection for IC2.

## Construction

Most of the parts for the audio processor are available from many electronics distributors. A foil pattern is provided if you want to make your own PC board, or you can use the board available from the source men-

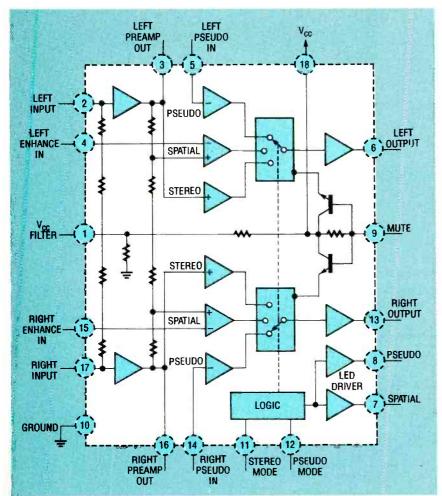


FIG. 2—BLOCK DIAGRAM OF THE TDA3810N. The device contains three op-amp stages, switching circuitry, power-supply regulation circuitry, and LED drivers.

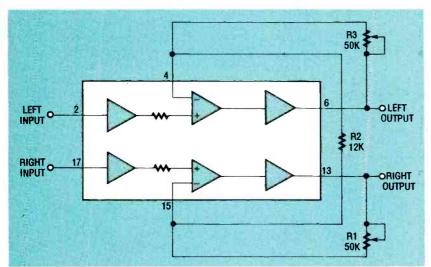


FIG. 3—IN THE SPATIAL STEREO MODE, active op-amp circuits selectively remove certain parts of the audio spectrum.

tioned in the Parts List.

Because this is an audio project, component tolerances and the matching of component values between the left and right channels is important. All re-

sistors should be within 5 percent of the listed value, and it's a good idea to check them. Be sure to use high-quality capacitors, as poor-quality capacitors can adversely effect the overall frequency response of the circuit's processor.

Following the parts-placement diagram in Fig. 6 as a guide, install all resistors and capacitors, paying attention to the polarity of the electrolytics. Also mount diode D1, observing its polarity. Mount the 78L09 voltage regulator (IC2) with the flat side pointing toward the outside edge of the PC board. It's a good idea to use a socket for IC1, and you can install it now and then insert the IC. Observe the proper pin-1 orientation when putting the chip in its socket.

A metal enclosure will provide the best shielding from interference. However, a plastic box will probably be acceptable as well. Prepare the enclosure by laying out the front and rear panels for drilling. After drilling, deburr and clean the enclosure. The author mounted solder posts at each point on the board that must be hard-wired to another component. That made it easy to mount the board, jacks, and controls in the case, and then do the point-topoint wiring. Otherwise, all wires will have to be soldered to the board before mounting it in the enclosure. In either case, mount the completed PC board to the enclosure using appropriate hardware.

If you haven't done so yet. mount all of the potentiometers, jacks J1–J5, the LED's, and switch S1 to the enclosure. Then solder all cables and wires from the board to the jacks and controls. Following Fig. 6, pay careful attention to the places where shielded cable must be used. Hook-up wire can be used for all other connections. When connecting the feedback gaincontrol potentiometers (R1, R3, R7, and R13), wire them so their resistance increases as they are turned clockwise. Figure 7 shows the inside of the completed prototype.

### Testing

When the project is complete, check all components for proper location and polarity, and also check your soldering. Using a DC voltmeter, check for the fol-

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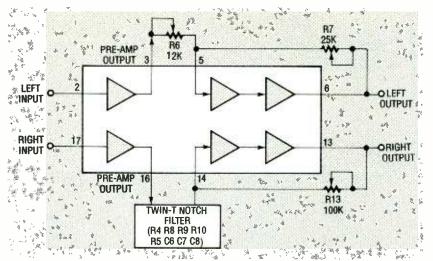


FIG. 4—IN THE MONO PSEUDO-STEREO MODE, the processor creates a "stereo" image using the various active filters in different ways on each channel.

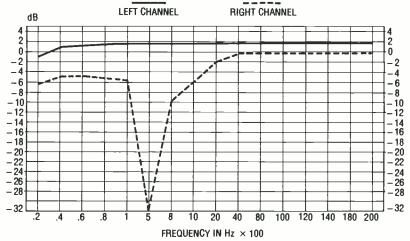


FIG. 5—FREQUENCY RESPONSE of each channel in the mono pseudo-stereo mode.

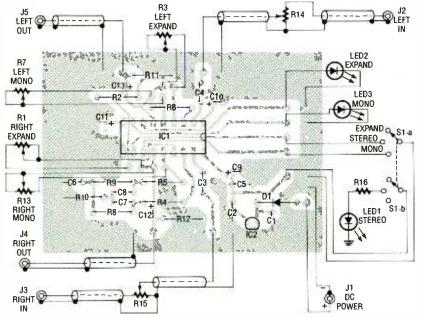


FIG. 6—PARTS-PLACEMENT DIAGRAM. Pay attention to those controls that require shielded cable for connection to the PC board.

lowing voltages after applying power to the circuit:

Power-supply output—10.5–24 VDC

IC2 output—8.55—9.45 VDC

IC1 pin 1-4.2-4.8 VDC

IC1 pin 2—4.2—4.8 VDC

IC1 pin 3—4.2—4.8 VDC

IC1 pin 4—4.2—4.8 VDC

IC1 pin 5—4.2—4.8 VDC

IC1 pin 6—4.2—4.8 VDC IC1 pin 13—4.2—4.8 VDC

IC1 pin 13—4.2—4.8 VDC

IC1 pin 15-4.2-4.8 VDC

IC1 pin 16-4.2-4.8 VDC

IC1 pin 17—4.2—4.8 VDC IC1 pin 18—8.55—9.45 VDC

If all of those voltages are correct, the audio processor is ready to use.

### Installation and use

If the audio processor is placed near a TV set and tends to pick up stray interference, move the processor around on the TV until the interference disappears. Also, be sure to use a well-filtered DC power pack or power supply to eliminate hum from the AC line.

Be sure all input and output cables are shielded, and well grounded to the PC board ground foil. Improper grounding can cause ground loops and other noise problems that are hard to track down. When the processor is to be installed between the Tape In/Tape Out jacks on a stereo system, hook it up the same way as if a tape deck were being installed.

Some stereo TV sets have linelevel output jacks on them. In that case, all you have to do is install the audio processor unit between the TV's output jacks and the stereo's auxiliary or

tuner input jacks.

If the audio processor unit will be installed between a speaker output and an amplifier input, the speaker output level must be reduced to a level that the audio processor can safely handle, which is a maximum of 2 volts rms. Always set the input-attenuator potentiometers to maximum attenuation before applying an input signal to the processor. Connect all mono audio sources to both of the inputs.

continued on page 82

DON LANCASTER

listory often repeats itself, first as a tragedy and then as a farce. It sure amazes me how many hardware hackers and software types refuse to learn from the past.

For instance, over a decade ago, the Apple II community conclusively proved beyond a shadow of a doubt that copy protection does not work. Never did and never will.

Neither do hardware locks or similar add-ons. Yet many IBM-PCcompatible folks are hell-bent on wasting new time, dollars, and energy reproving this fundamental truth to themselves. You will find only three known effects of copy protection: (a) it annoys and inconveniences legitimate users, sending them all to unlocked competitive products; (b) it diverts time and energy that is best spent improving and updating your code; and, of course, (c) any copy protection dramatically increases the number of the bootleg copies of your product that get circulated.

The reason for c is simple. Copy protection always attracts attention to itself, causing scads of ultra-creative people to devote countless hours of time and amounts of energy toward cracking the secrets of your product.

The bottom line is this: Undoing copy protection is fun! Not only is the challenge fun, it is by far the fastest and most cost-effective way to learn machine-language programming. It's also one of the best and the cheapest high-quality learning experiences you will find anywhere ever-and it's a positively superb entertainment value.

For most hardware offerings. even grinding a part number off the key integrated circuit will have the exact opposite of the intended effect: All that does is cause lots of high-energy people to puzzle out what the chip is and where to get one. The universal hacker popularity for that BA1404 stereo FM broadcaster can be directly traced to one firm stupidly grinding off one too many part numbers.

By far the most absurd notion on hardware copy protection that has been resurrected is to ...

### Pot it in epoxy!

I simply can't believe the number of calls and letters I've gotten on this lately. Back in the late 1950's, it was conclusively seen that potting your circuits in epoxy offers no design security whatsoever. In fact, epoxy potting will always have the exact opposite effect.

First, any reasonably good design engineer could select a "black box" approach and carefully look at the inputs and outputs of the circuit. From the circuit's size and cost, and from information in trade journals, data books, distributor's catalogs, and ap notes, an engineer can easily come up with three or four methods to perform the same function—at least one of which will end up far cheaper, better, and more creative than yours.

Second, it's a simple matter to Xray any potted project—free even, if it's a small module and you visit a reasonably curious dentist.

Third, most of the epoxy sources also supply epoxy strippers. These

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dissolve out the potting compound, cheaply, rapidly, and conveniently so it can be quickly washed away.

Fourth, epoxy could have several disruptive effects on your circuits. It changes the heat distribution and the operating temperatures of components. It can subtly detune polystyrene capacitors and its weight shifts mechanical resonances to more destructive frequencies.

Fifth, a very little-known fact: The ferrite RF beads used on typical high-frequency analog circuits must be able to change in size slightly or they will not work properly. The highfrequency energy gets absorbed by magnetostriction that, in turn, converts to heat. Locking ferrite beads in epoxy can alter their response.

Used with care, there are times and places where epoxy potting is an appropriate technique. Especially for water resistance or use in hazardous environments. But epoxy potting for copy protection just does not work.

### **Getting Nichrome wire**

I've gotten several calls and letters recently asking for hacker sources for Nichrome wire. I'll show you some sources and alternatives in just a bit. But please note that Nichrome is a trade name for a resistive alloy from Driver Harris Co. that can be drawn into wire or sputtered on a substrate.

Most often, you'll want all of your electrical or electronic wiring to be very efficient, wasting as little energy and producing as little heat as possible. But there are other times and places when you want to cause a wire to intentionally generate heat or create a specific voltage drop.

Obvious examples include toasters, electric blankets, hot-wire plastic or foam cutters, laminating machines, space heaters, soldering irons, motor starters, thermal re-

lays, refrigerator defrosters, or for dummy transmitter loads. Some non-obvious places for carefully controlled resistance wire include current-meter shunts, and sensors that turn your printer on whenever you power your computer.

Most elements, alloys, and other materials are grouped into four types. Conductors can pass electricity fairly easily and have low resistances. Conductors can include both ordinary wire and resistance wire.

Semiconductors offer a moderately high resistance to electrical currents, with silicon and gallium arsenide being the most obvious examples. Insulators offer very high resistance to electrical current. Rubber, glass, plastics, and ceramics are typical insulators.

Superconductors can offer zero resistance to electrical currents. But most superconductors are complex formulations that work under special conditions at extremely low temperatures. You'll find more on superconductors in the Hardware Hacker II reprints.

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	RESISTIVITY	RESISTIVITY
MATERIAL	measured in	as compared
	$\mu\Omega$ -cm	to copper
	·	
Aluminum	2.8	1.64
Brass	7.0	4.07
Constantan	44.1	25.60
Copper	1.7	1.00
German Silver	33.0	19.18
Gold	2,4	1_42
Invar	81.0	47.00
Iron	10.0	5.81
Lead	22.0	12.79
	4.6	2.67
Magnesium	5.7	3.31
Molybdenum Music wire	11.8	6.86
Music wife	11.8	0.00
Monel	42.0	24.40
Nichrome	150.0	87.20
Nickel	7_8	4.53
Platinum	10.0	5.81
Silver	1.6	0.95
Tantalum	15.5	9.01
Tin	11.5	6.69
Tungsten	5.5	3.20
Zinc	5.7	3.34

FIG. 1—THE RESISTIVITY OF ANY MATERIAL is defined as the face-to-face electrical resistance of a unit cube. Here are several resistivity values for some of the more widely used metals and alloys.

Take a one-centimeter cube of any element, alloy, or material. Next, apply a voltage from full face to the opposite full face. Then measure the current. By Ohm's Law, the ratio of the voltage to current determines the resistance of the cube. But we have a special name for the resistance of a unit cube. This is the resistivity, and is identified p, the Greek letter rho.

The resistance of a wire increases with its length and decreases in proportion to area. The metric resistivity units are ohm-centimeters (ohm-cm). I'll use a wondrously oddball unit of microOhmcentimeters ( $\mu\Omega$ -cm) here so our numbers look nicer.

Resistivity values let us compare materials independent of their actual sizes. Some popular resistivity values are shown in Fig. 1, while Fig. 2 shows you how much resistance you can expect for various wire sizes of selected materials.

The lowest resistivity of common elements or alloys is silver, checking in at 1.6  $\mu\Omega$ -cm. But silver is fairly rare and readily tarnishes, and the

commodity price of silver changes all over the lot. So, silver isn't used too much except for RFI suppression microwave equipment, and exotic military stuff.

Copper, of course, is the universal choice for a conductor. It has a resistivity of a mere 1.7  $\mu\Omega$ -cm only five percent worse than silver.

At first glance, aluminum appears almost as good as copper, having a conductivity only 64 percent worse. In theory, the thicker but cheaper and lighter aluminum conductors could be substituted.

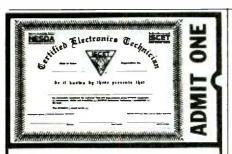
But aluminum has a pair of nasty habits which include electrochemical decomposition and the building up of sapphire-hard (literally!) oxide coatings. Making a solid connection to an aluminum wire is not a trivial task. Several decades ago, a bunch of house trailers burned up after some abortive attempts at trying to perfect aluminum wiring.

Most of the other popular elements and alloys have resistivities that are moderately higher than copper. But a magic alloy of 61 perFigure 2 shows you how much resistance to expect for various wire sizes for each of these materials. A foot of 20-gauge Nichrome wire has a resistance of 0.659 ohms. The same alloy in 30-gauge provides around 6.75 ohms total.

Resistance wire gets measured in ohms per thousand feet. Or you may prefer its equivalent of milliohms per foot. Naturally, resistance wire works just like any other resistor, obeying Ohm's law and the usual  $P=E^2/R$  power relations. A watt of electricity is, of course, a watt of heat. And a BTU of heat equals 17.58 watts. So you can easily calculate the amount of heat. BTU or *British Thermal Unit* is the amount of heat needed to raise the temperature of one pound of water by one degree Fahrenheit.

MATERIAL	10 gauge	20 gauge	30 gauge	40 gauge
			Committee of	
Aluminum	2	17	169	1720
Brass	4	41	419	4260
Constantan	26	260	2640	26,800
Copper	1	10	103	1050
German Silver	19	194	1970	20,100
Gold	1	14	141	1480
Invar	47	477	4850	49,300
Iron	6	59	598	6080
Lead	13	130	1320	13,400
Magnesium	3	27	275	2800
Molybdenum	3	34	341	3470
Music wire	7	70	706	7180
Monel	24	247	2451	25,600
Nichrome	65	659	6750	70,240
Nickel	5	46	467	4750
Platinum	6	59	598	6080
Silver	1	10	98	991
Tantalum	9	91	928	9430
Tin	7	68	688	7002
Tungsten	3	32	330	3350
Zinc	3	33	344	3450
Values in milli	ohms per too	ot ~or~ Ohm	s per 1000	feet,

FIG. 2—SOME TYPICAL RESISTANCE VALUES for different materials and wire gauges.



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Other resistance-wire variables include the tensile strength, the temperature coefficient of resistance, and the temperature coefficient of expansion. The resistance-temperature coefficient gets important fast in such things as meter shunts. The expansion temperature coefficient becomes crucial if the wire passes through some ceramic seal. Should the wire and the ceramic expand at different rates, one or both can self destruct at high temperatures.

The fastest and simplest way to get some Nichrome wire to play with is to gently crush up a surplus power resistor in a vise and unwind the wire. Different sizes offer different lengths and gauges of wire. Resistance wire often ends up at surplus stores at bargain prices, es-

pecially at Fair Radio Sales. American Science and Surplus also offers cheap resistance wire originally intended as refrigerator defroster elements.

One big supplier of new resistance wire is *MWS Wire Industries*. Its equivalent to Nichrome is known as MWS-675. It also offer two dozen other variations. Its MWS-875 provides even higher resistivity with better temperature coefficients for both resistance and expansion. This alloy includes chrome, aluminum, and iron, with traces of carbon and silicon. It is also slightly lighter in weight.

By the way, other trade names for alloys similar to *Nichrome* are *Trophet C, Alloy C, HAI-NiCr60, Chromel C, Nikrothal 6,* and *Electroloy.* 

For this month's contest, just tell me about a new or unusual hacker use for resistance wire. There'll be all of the normal *Incredible Secret Money Machine II* book prizes, along with an all-expense-paid (FOB Thatcher, AZ) tinaja quest for two going to the best submission of all.

As usual, send your written entries to me here at *Synergetics* and not to the **Electronics Now** editorial offices.

### A hacker interface

In several past columns, we have looked at the FCC Part 68 Interfaces. These are required any time you want to put voice, music, caller-ID data, or modem tones on or off of the phone line. The key component needed is just a fancy transformer with a high isolation voltage rating, a very good balance, and the ability to accept DC primary current.

There are lots of dollars, time, and effort needed to get an interface FCC type approved. And it is now illegal to make any connection to the phone line without going through an FCC approved, Part 68 interface. At least in the U.S.

Several firms now offer "pass through" interfaces that you can include within your own circuits to get an instant and automatic type approval. The two major suppliers are now *Cermetek* and *Dallas Semiconductor*. Sadly, their pricing has been too high for most hacker uses.

A startup outfit by the name of *CircuitWerkes* is now offering a new and hacker-friendly Part 68 interface at an acceptable price of \$29.95. And yes, it offers a full type-approval pass through. It's subject to only a few easy rules that involve component spacing, labels, documents, and modifications. Figure 3 shows you the circuit.

A small relay makes the on-hook and the off-hook state connections. To "sieze" or "answer" the line, apply 12 volts DC to the relay, providing 60 milliamperes.

The ring-detector circuit is active only when on-hook. It consists of a optoisolator that responds to the high AC ringing voltage (typically 140 volts at a frequency of 28 to 40 Hertz). The output of the ring detector is an open collector. You'll have to provide both an external pull-up

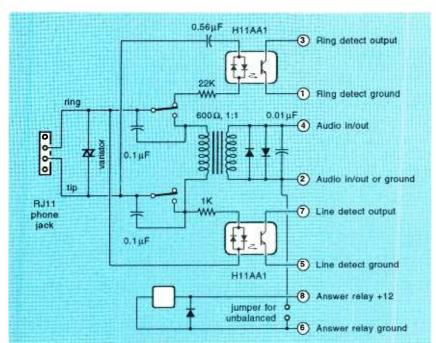


FIG. 3—THE CIRCUITWERKES MPC-2 is an FCC Part-68 telephone interface that offers a "pass through" type approval for your own hacker projects.

resistor and a filter capacitor to ground. Suitable values are 12,000 ohms and 5 microfarads.

The main data path is active both on- and off-hook. This dual feature is needed for a caller-ID compatibility. When you are on-hook, the data path is capacitor-coupled.

When off-hook, the data path is DC-coupled through the transformer primary. A second optoisolator in parallel with the primary acts as a line-current detector. The line current is detected by monitoring the DC *voltage* drop across the primary.

The line-current detection lets you know when your calling party hangs up. The optoisolator also offers open-collector output. A pull-up resistor is also required here.

The main data path is a special transformer with two clipping diodes that limit the maximum applied audio. A jumper option allows you to select a balanced or single-ended 600-ohm source/sink for your audio output.

Typically, your computer will first monitor the ring detector. After a ring, it seizes the line and optionally grabs the caller-ID tones. Then it will send or receive your voice or data. Finally, you can hang up by causing the relay to drop out—either by detecting the absence of line current or by hanging up on purpose.

As a second contest for this month, just tell me about a new or unusual application for a hacker-legal Part 68 interface project.

Much more information on those caller-ID applications appears in a dozen files on my *GEnie* PSRT.

### More semiconductor resources

We will wrap up our continuing listing of the major semiconductor houses in a third and final sidebar.

This month, we will cover *OKI* up through *Zilog*. I've tried to zero in on those suppliers with the greatest hacker interest.

A complete list will appear in the *Hardware Hacker IV* reprints. I've also gathered them together into the ICMFGRS.PS download you'll find on *GEnie* PSRT.

As we have seen before, your best bet here is to request a short-form catalog, the price list, and a literature directory. Be absolutely sure to use professionally sounding phone calls or your own custom PostScript laser letterhead. A ball-point pen on tablet paper flat out won't hack it. Much more on finding and using technical information is in my newly revised *Incredible Secret Money Machine II*.

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Also free on professional request is the new Spread Spectrum Handbook from Stanford Telecomm. This is a dozen pages of ap-notes and useful references, along with bunches of data sheets for the company's high-end digital spread-spectrum chips.

The Scrambling News has detailed insider information on the current TV video scrambling and descrambling methods. It also offers books full of schematics, modifications, and related technical information. A competing newsletter is the Satellite Watch News.

The SRS Encoder is a new monthly newsletter from the Seattle Robotics Society. Lots of regional information on great surplus buys are included here.

Joe Singer's Printer's Devil is a

superb alternative publication on home printing and presswork. "A press in every home; a home in every press." It is published quarterly at a bargain \$10 per year subscription price.

Finally, the New Age Alternatives Discount Catalog is another resource for pseudoscience devices and information. Fascinating reading for sure. This one is offered by Lor'd Industries.

A reminder here: I have reprints available for most of my columns. Both in Book-on-demand published hard copy and on-line at GEnie PSRT. The titles now include my Ask the Guru, Hardware Hacker, the Blatant Opportunist, LaserWriter Secrets, and the new Resource Bin. Check my nearby Synergetics ad for more details.

As usual, I have gathered most of the mentioned resources together into our Names and Numbers and Semiconductor Manufacturer's III sidebars. Also, as usual, you can get technical help, consultant referrals, and lots of off-the-wall networking by calling my helpline.



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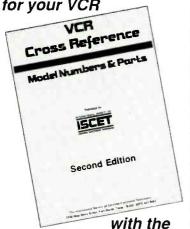
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### **AUDIO EXPANDER**

continued from page 74

In the stereo mode, the only adjustments are the input-attenuator controls (R14 for the left and R15 for the right). For a line-level input, set them for 0 attenuation. Other higher-level sources should be adjusted as desired by the user (without exceeding the 2-volt rms maximum input limit).

In the spatial stereo mode, the

input attenuator controls should be adjusted the same way as in the stereo mode. The spatial controls (R3 for the left and R1 for the right) can then produce very interesting spatial effects. Also, adjusting the input-attenuator controls produces interesting effects due to the cross-channel coupling provided by resistor R2. Experiment with those four controls to determine their optimum settings.

In the mono pseudo-stereo mode, the input-attenuator

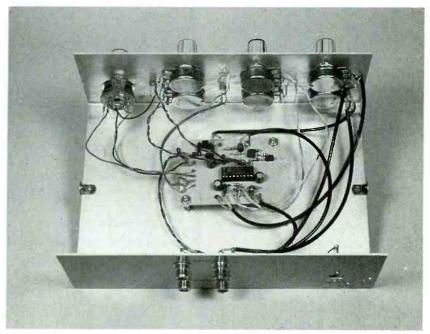
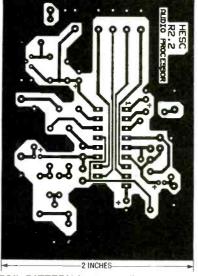


FIG. 7—A METAL ENCLOSURE provides the best shielding from interference. Here's the inside of the completed prototype.



FOIL PATTERN for the audio processor.

controls should be adjusted the same way as in the stereo mode. The pseudo stereo controls (R7 for the left and R13 for the right) should be set as follows: R7 should be set to give a +2.0 dB higher output level versus the right output channel control (R13). For example, set R7 for an output of +2.0 dB, and set R13 for an output of 0 dB. The specific levels are not critical; just keep a 2.0 dB differential between the left and right output channels.

When using a mono input source, the spatial stereo mode will produce some very interesting and useful effects. The input attenuator controls will also have interesting effects.  $\Omega$ 

sales tax to total.

83



INFRARED REMOTE CONTROLS ARE very common these days, thanks to all the video, audio, and VCR equipment on the market that can be controlled with an infrared remote. Remote controls are great when they work properly. However, it's very frustrating when you press a button on the remote control and nothing happens. If you've ever had that problem, then you know what we mean when we say it's frustrating.

It's always hard to know

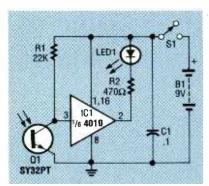


FIG. 1—THE IR TESTER circuit lets you know if the button you press on a remote control is working.

### **PARTS LIST**

R1-22,000 ohms, I/4-watt, 5% R2-470 ohms, I/4-watt, 5%

C1-0.1 µF, ceramic

IC1-4010 CMOS hex non-inverting buffer

LED-light-emitting diode, any

Q1—SY32PT IR phototransistor or equivalent

B1-9-volt battery

Project case, PC board or perforated construction board, battery clip, wire, solder, etc.

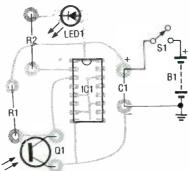
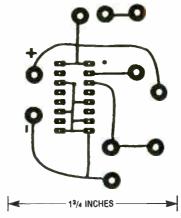


FIG. 2—PARTS-PLACEMENT diagram for the IR tester. Point-to- point wiring can also be used.



FOIL PATTERN for the IR tester circuit.

whether a malfunction is due to the remote control or the device you are trying to control. After all, infrared (IR) is invisible to the human eye, so how do you know if the control is working?

The answer is simple: Build our IR remote-control tester. It will let you know if, when you press the button, the control is emitting an IR signal.

The IR tester circuit is shown in Fig. 1. IR phototransistor Q1 receives the signal from a re-

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mote control and sends it to one gate of a CMOS 4014 non-inverting hex buffer. The output from the buffer drives an LED that flashes the received signal to let you know that the remote control (or at least the one button you pressed) is working and emitting an IR signal.

We've provided a foil pattern to make a PC board for this project, but the circuit can easily be made using point-to-point wiring. Figure 2 shows the partsplacement for the PC board, should you decide to use it. The completed circuit can be installed in any suitable case. Mount the IR phototransistor where it can easily receive the IR signal, and mount the LED where it's easy to see. A 9-volt battery powers the circuit, but you can certainly build an AC-

powered supply if you wish.
Once constructed, the tester will determine if your remote control is causing the problem. Simply point the remote control at the IR phototransistor, and press each button. The LED will flash for proper operation.

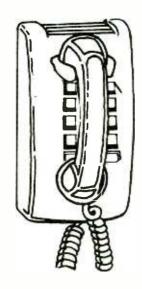
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### AUDIO UPDATE

### The Audio Answerman: Part 1

LARRY KLEIN

ere is another collection of helpful (or at least interesting) audio questions and answers from reader mail and my files.

### **Audio education**

I've been intensely interested in music recording and audio technology ever since my early teens. At this point, I'm seriously considering entry into the audio field in a professional capacity. Where can I get information about my options and the educational requirements?

T.M.

Norwalk, CT

You're in luck. A definitive Directory of Educational Programs has been published by the Education Committee of the Audio Engineering Society (AES) that covers courses ranging from seminars to four-year graduate programs that grant degrees. Institutions, facilities, courses, degrees, and tuition are listed in a convenient format.

As a bonus, there are helpful articles that discuss the variety of job opportunities within the field and ways to approach the education process. The postpaid cost of the directory is \$5 for AES members, \$6 for nonmembers. Delivery is 4 to 6 weeks. Send your check to Audio Engineering Society, 60 E. 42nd St., Room 2520-RE, New York, NY 10165. While you are writing, you might also ask for an AES membership application.

### Flat sound

Recently I told a friend that I built my own speakers from scratch. To my annoyance, he immediately asked, "How flat are they?" Are we getting so wrapped up in specifications that we forget the basic goal—good sound the way we like to hear it? I spent over 50 hours reworking my ported speakers so I could have a lot of bass—the way I like it. Don't

get me wrong; specs and test reports are definitely helpful, but keep in mind that I'm spending money to have sound the way I want to hear it—not as some expert says it should be heard.

P.W.

Rochester, NY

If P.W. had written about choosing the paint color for his living room walls or selecting a blend of coffee-or a wife-I would not argue with the subjectivity of his approach, although my own tastes would probably differ. Everyone has a right to his own tastes—however absurd they might be. I assume you are using "good" in the sense that it satisfies you. However, when the goal is to reproduce a recorded sound, then the system that's doing it must not add any special sound characteristics of its own. If P.W. prefers speakers that readjust the original tonal balance of the program material in a given direction, that's his privilege. But I must point out that his speakers, by definition, are then not providing high-fidelity reproduction. Theoretically, fidelity to some original is what hi-fi is all about.

### Planned obsolescence

I use my audio equipment at least four hours a day, and next year my receiver will be 10 years old. How does wear affect audio equipment, and how long will it be before planned obsolescence sets in? H.S.

Elliston, VA

Congratulations to your receiver on its 10th birthday! Before I answer your question on wear, I'd like to discuss "planned obsolescence," a term that seems to be fading from popular use. Actually, the alleged practice that the term describes never did make much sense; what most people really meant by it was

planned deterioration. In other words, certain parts or components in a device supposedly were designed to have both a short life and a high replacement cost, thereby encouraging the purchase of a new replacement. But it seems to me that the ill will engendered by premature breakdown would cause consumers to avoid the faulty brand when considering a replacement—thus defeating the purpose of the alleged planned obsolescence.

The loudest complaints of planned obsolescence usually occur when a new audio format threatens to render obsolete someone's treasured collection of program material. For example, the industry switched from from 78 rpm's to LP's, LP's to cassettes, and then cassettes to CD's. The obsolescence in those cases was, truthfully, planned to obtain higher fidelity—or in the case of cassettes, greater convenience—for the music collector and listener.

The general public (unlike some of the audio magazines and syndicated columnists) does not automatically extend a warm welcome to every new trend in audio. Witness, for example, the marketplace fiascoes of such components as the "elcassette" and, lately, DAT. I suspect that there are other fiascoes of the digital variety now waiting in the wings.

In regard to your question about wear, solid-state devices, unlike high-power vacuum tubes, do not have an inherently short life. This is not to say that transistors never fail, but rather that their predicted life span extends far beyond that of tubes. Because of minute manufacturing flaws, small-signal transistors (and integrated circuits) can develop leakage over time, and power devices ultimately can flex themselves to death from repeated heat-

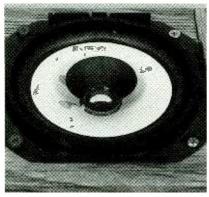
ing and cooling cycles during normal use. Other components, such as electrolytic capacitors, fail over time for a variety of mechanical and electrochemical reasons.

### **Whizzers**

I'm curious about the speakers installed in the lower front-door panels of my car. I removed the grille from one of the speakers and found it to have a single gray 6-inch cone with a separate small white cone cemented to its center. Does the smaller cone serve as a tweeter? D.C.

Lancaster, PA

Sort of, but not really. What you've described is known as a "whizzer," and its purpose is to enhance the high-frequency sound from your speakers. A whizzer is a small, light, and stiff subsidiary cone with an unsupported outer edge that is cemented to the center of the main cone. The area of attachment is directly over the driver's voice coil. The whizzer picks up the higher frequency vibrations from the voice coil, and helps to send them out into the world as sound.



HERE IS A WHIZZER CONE attached to a low-cost speaker.

If carefully designed, a whizzer can provide improved highs from larger, full-range drivers. Obviously, the manufacturing cost of adding a whizzer to a driver is very low compared with the cost of a separate tweeter with its crossover and mounting complications. On the other hand, a separate or coaxially mounted tweeter is able to put out significantly more high-frequency energy—which you could probably use considering the calf-high mounting location of your speakers.

### X-ray problems

Despite the printed reassurances posted at the passenger inspection areas of airports, I've always tried to keep my films and tapes from being X-ray inspected. I recently heard that color TV sets can also produce X-ray radiation. How far away from my TV should I keep my audio and video tapes to be safe, or will it not make a difference? M.O.

Burlington, VT

As far as I can determine, X-rays at the levels used in baggage examination have no effect on tapes or the signals recorded on them. It's true that the stray magnetic fields produced by X-ray equipment and color TV cathode ray tubes might affect a recorded signal, but one expert told me that the tapes would have to be stored inside the operating equipment in close proximity to a transformer or deflection coil before an erasure is likely to occur. However, metal detectors, also used in airports, can be hazardous to the health of your recorded tapes.

### **Parameters**

"Parameter" seems to have become a new catchword among those involved with politics and/or the Pentagon. Is "parametric" derived from the same word, and exactly what does it have to do with equalizer design?

J.H.

Chevy Chase, MD

My copy of Webster's dictionary defines parameter as "A (mathematical) quantity or constant whose value varies with the circumstances. of its application, as the radius line of a group of concentric circles. which varies with the circle under consideration." The adjectival form is "parametric." In other words, a parametric equalizer does not limit you to the specific built-in fixed operating frequencies and bandwidths of a conventional graphic equalizer. Instead, you can assign "arbitrary values" as the equalization needs arise. This can be very handy, for example, when the frequency of the peak that you want to reduce doesn't line up very well with one of the sliders on a standard 1/3-octave graphic equalizer.

### O&A

continued from page 12

graphics image. The second, less expensive alternative is to print at 150-dpi resolution—half the number of dots means half the memory requirements. If you can live with the lower resolution, the latter is a cheap, quick fix for the problem.

There's one more possible answer to your problem but I doubt that it's applicable. It may be that you have enough memory in the printer to do 300-dpi, but you're using the memory to hold downloaded fonts and other things. Remember that memory used for fonts isn't available for graphics. Check your software (and not just the graphics stuff) to see whether this is true or not. If it is, unloading the fonts may free up enough printer memory to permit you to print graphics at the maximum 300-dpi resolution.

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### DRAWING BOARD

### Our descrambler is almost finished.

ROBERT GRUSSBLATT

elieve it or not, there's not a lot more to the design of the basic descrambling circuit than the subject matter we've covered over the past few months. But if you're really interested in video, there's much more for you to learn—the video-scrambling stuff we've been going through is just one small part of the subject. Video is a complex business, and once you get the hang of how signals can be manipulated, you'll find that there's no end to the kind of circuitry you can design. There's also a huge market for it as well. But back to the subject at hand.

When we first started work on the SSAVI descrambler, the block diagram probably looked quite complex. But if you look at Fig. 1, you'll see that most of the work has been done. The most difficult job left for us is to come up with the counter that's needed by the phase-locked loop. It's a job we have to do carefully because the success of the descrambler depends on how well we can maintain the stability of the horizontal-sync signal.

The phase-locked loop in our design is driven by a 504-kHz clock based on an R-C network. That frequency was chosen for two basic reasons: The first is that it's exactly 32 times the NTSC line frequency of 15,750 Hz, and that makes it easy for us to do the division necessary to produce horizontal sync pulses. The second, and somewhat more subtle reason, has to do with the period rather than the frequency.

A 504-kHz clock has a period of 1.98 microseconds. That's interesting because, by using five of the counts, we can get a pulse that has a width of 9.92 microseconds, which is close enough to the NTSC's established standard of 10.7 microseconds for a horizontal

blanking pulse.

Before we go any further, I have to comment on my apparent disregard for precision. I've been using language and design techniques that are loaded with phrases like "close to," "pretty much the same as," "in the ballpark," and so on. Now, I'm as impressed with standards as anyone I know, but numbers have to work in the real world as well as on

amazed at how sloppy the signal really is. The average horizontal frequency might be 15,750 hertz, but there's considerable jitter from line to line in the signal. The same is true for burst, blanking, and all the other components in the line.

Despite these variations in the signal, the picture that shows up on your TV screen is apparently unaffected by them. The difference be

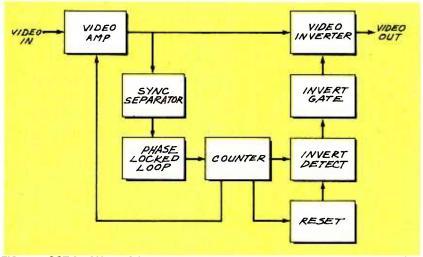


FIG. 1—MOST OF OUR BLOCK DIAGRAM has already been turned into actual circuitry. Now we need a counter for the phase-locked loop.

paper. You have to keep things like cost in mind when you're designing a circuit.

The NTSC standards for a video signal have a precision of several decimal points, and every broadcaster in the country spends a lot of time and effort making sure his signal adheres to that standard. The same is true of TV manufacturers, as well. The theory for standardization is terrific but, as is usually the case, what happens in reality is different. All you have to do to see what I mean is put a scope on the video signal received by your TV set; you'll find an overall similarity to the video standard, but you'll be

tween studio-quality video (the stuff on the monitors in the broadcaster's control room) and received video (the stuff you see on your TV) is minimal.

Keeping all that in mind, let's design the rest of the descrambler.

The next thing we need is a divide-by-32 counter to complete the phase-locked loop section of the circuit. After my discussion of the relative importance of precision, you should understand why the phase-locked loop's oscillator is only RC-based, and not crystal controlled: It's just cheaper and easier.

The divide-by-32 circuit (the "Counter" in Fig. 1) can be built in

several ways; as a matter of fact, we've designed a whole bunch of these things in the past. In order to keep the circuit as simple as possible, we'll use the 4040 binary counter whose pinouts are shown in Fig. 2. This is one of the earliest members of the CMOS family and still one of the best choices for general counting. It's a ripple counter, rather than a synchronous counter, so don't use it for applications where super accuracy is required. Remember that a ripple counter is a bunch of sequential counters, and each internal stage uses the output of the preceding stage as an input. This means that the outputs change in sequential order, and an incorrect count will be present briefly on the pins. Since the problem is caused by the propagation delay of each counter stage, the duration of the incorrect count on the outputs is, by and large, a function of the clock

The 4040's clock input is fed with

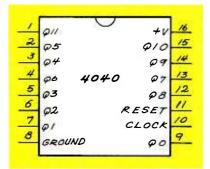


FIG. 2—FOR OUR DIVIDE-BY-32 circuit, we'll use the 4040 binary counter whose pinouts are shown here.

the 504-kHz signal generated by the 4046, and we're using a series of gates to decode the count and provide horizontal blanking and some other timing signals needed for the descrambler. The actual circuit is shown in Fig. 3. You should understand why each of these signals is needed before you start hooking everything up to the back of your TV set. To see what we need from the counter, let's use it to restore horizontal sync and then figure out what else we need to completely unscramble the incoming video.

Getting a horizontal sync clock for the phase-locked loop circuit is simple. All we have to do is pick off

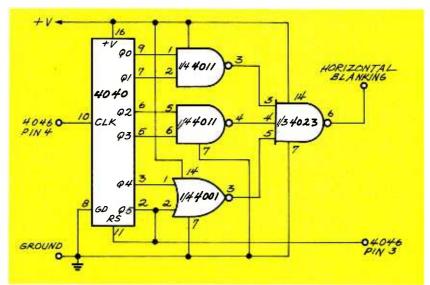


FIG. 3—THE 4040's CLOCK INPUT is fed with the 504-kHz signal generated by the 4046. We're using a series of gates to decode the count and provide horizontal blanking.

the Q4 output. That is a dividedby-32 version of the input clock from the phase-locked loop's 504-kHz oscillator and, as shown, it's fed back to pin 3 of the 4046. Now that the phase-locked loop is provided with a constant reference signal, it will accurately generate sync pulses—even when they're not sent along with the transmitted video.

The remaining problem to deal with is turning off the generated sync pulses during the vertical interval when real transmitted sync is present. (Remember that the video isn't scrambled during the vertical interval.) To do that, we have to count the lines of video as they're received and make sure that transmitted sync is processed for the first 26 lines of each frame. The starting point for the count is the vertical sync signal and, as you recall, we've already isolated the signal. The sync separator we built earlier produces a positive-going version of vertical sync. If we use the rising edge of that signal as the zero point for the counter, we have to count a number of lines to reach the point where the lines of video are carrying picture information and are therefore scrambled.

The two lines in the frame that mark the beginning and end of the transmitted horizontal sync are 260 and 27, respectively. We need a circuit that can count the received lines and let the rest of the descrambler know when to use re-

ceived horizontal sync and when to use the artificial sync generated by the phase-locked loop. The zero point for the counter will be the rising edge of our vertical sync signal. Since that occurs at line 3, we have to decode a count of 24 and 257.

We can use a 4040 to do that job as well. This is the same sort of counter decoding we've done before in this project and others. When the counter reaches 24 we have to enable a gate that will send the phony horizontal sync pulses to the video amplifier at the circuit's input. When we get to a count of 257, the gate has to be disabled to let the real horizontal pulses through to resync the phase-locked loop circuit.

Decoding those two numbers is a pain in the neck since it involves watching nine counter lines. You can do that with a bunch of gates, but a better way is to use an EPROM. The choice is yours although, if you haven't had much experience in this sort of decoding, it's probably a good idea to work out the logic and build the decoder with gates. Otherwise an EPROM is the way to go. Assuming, of course, that you have programming capabilities.

When we get together next time, I'll give you the truth table for the EPROM and we'll finish off the descrambler. All that's left is a couple of flip-flops, a bit of work on the video section, and a way to detect the presence of normal or inverted video. Simple stuff!  $\Omega$ 

### FET'S

continued from page 56

to handle higher currents. As majority-carrier devices that store no charges, they can switch faster than bipolar power transistors.

Figure 12 is a section view of an N-Channel, enhancementmode power MOSFET. Unlike its small-signal counterpart, the latest power MOSFET's are fabricated with vertical rather than planar structures. They are made with the doublediffused (DMOS) process, and they have conductive silicon (polysilicon) gates. The gate of this device is isolated from the source by a layer of insulating silicon oxide.

When a voltage is applied between the gate and source terminals, an electric field is set up within the MOSFET. This field alters the resistance between the drain and source terminals, and it permits conventional current to flow in the drain in response to the applied drain circuit voltage. There are also Pchannel, enhancement-mode power MOSFET's in which conventional current flows in the opposite direction of the Nchannel device. Figure 13 is the schematic symbol for a DMOS enhancement-mode, N-channel power MOSFET.

Figure 14 is an cutaway view of a typical DMOS power MOSFET. It is made up of many cells or transistor elements connected in parallel. Each source cell consists of a closed rectangular or hexagonal channel which separates a source region from the substrate drain body. The cells are formed in an integrated circuit process, and there might be more than a half million cells per square inch of substrate. All of the source cells are connected in parallel by a continouus deposition of aluminum metalization, which forms the grid-like common source terminal.

The DMOS power MOSFET contains an inherent PN junction diode, and its equivalent circuit can be considered as a diode in parallel with the

source-to-drain channel, as shown in the schematic symbol of Fig. 13.

International Rectifier (IR) makes DMOS power MOSFET's that have hexagonally shaped cells, so it calls its products HEXFET's. Motorola Semiconductor also offers DMOS power MOSFET's, but its devices have rectangular rather than hexagonal cells. Motorola named its power MOSFET's TMOS to call attention to the T-shaped current flow that occurs in the cells between the common drain and the channels to the multiple sources.

Power MOSFET's are widely specified for high-frequency switching power supplies (generally those that switch at frequencies above 100 kHz), AC and DC motor speed controls, high-frequency generators for induction heating, ultrasonic generators, audio amplifiers, and amplitude modulation transmitters.

The advantages to using power MOSFET's over power bipolar transistors include:

- Faster switching speeds and lower switching losses.
- Absence of the bipolar's second breakdown
- Wider safe operating area
- Higher input impedance
- High, if not higher, gain
- Faster rise and fall times
- Simple drive circuitry

The principal disadvantages of power MOSFET's are their higher cost and a higher static drain-to-source on-state resistance, which can cause unacceptable power losses in certain switching applications. However, the manufacturers have made progress in reducing those resistance values. DMOS geometry has largely replaced the V-groove or VMOS process that was widely used to fabricate power MOSFET's back in the 1970's.

Radio-frequency power MOSFET's are now available that will operate over the 2 to 200 MHz frequency range. The high power and high gain of these devices makes tham suitable as power amplifiers in solid-state transmitters for FM and TV broadcasting.



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### COMPUTER CONNECTIONS

### The Emerging PC

JEFF HOLTZMAN

992 drew to a close with some of the most exciting developments in the PC industry in years. There is no single overarching product or technology, but lots of little bits and pieces that together point to the emergence of a new class of personal computers with unprecedented power, versatility, and connectivity. Core technologies include powerful and upgradeable CPU's, general-purpose digital signal processors (DSP's), rapid acceptance of local buses and corresponding decrease in the ISA/ EISA/MCA bus wars. Other trends involve accelerated true-color graphics, motion video compression and decompression, drastically reduced power consumption, increased semiconductor and magnetic storage, full-featured operating systems, built-in local-area network connectivity, 100-MHz+ LAN speeds, and wireless cellular networking.

### PC architecture

During the past year, the 486 has quickly surged ahead of the 386 as the platform of choice. Spurred on by competition from Cyrix, AMD. and others, Intel has released a wide variety of 486-based devices, with many more to come. Prime features of all include low power and performance enhancement through clock-doubling-and -tripling, as demonstrated by IBM recentlytechnology. The clock doublers have been well received, even though pricing continues to hover near that of full motherboard upgrades that provide better perfor-

And speaking of Intel, you may think of the company primarily in terms of CPU's, but during the past few years, Intel has stuck its corporate thumbs in numerous pies—and

has come out holding several juicy plums. Of course, there are the CPU's. There is also video-compression technology, exhibited first as the Digital Video Interactive (DVI) boards for digitizing and displaying full-motion video on desktop computers. Part of DVI is Real Time Video (RTV), which Intel has ported from the i750 video processor to the 386/486/Pentium architecture. and now calls Indeo. Indeo is one of the compression algorithms included as part of Microsoft's Video for Windows; Indeo is also being supported by Apple's QuickTime, and by IBM's recently announced Ultimotion. As discussed here in the preceding few months, softwareonly video is gimmicky, but an important first step in computer video.

Then there are network cards; Intel's cards are highly regarded, and are available for extremely competitive prices. Next come faxes and modems. Intel's SatisFAXion 400 is the highest-performing general-purpose modem and fax card combination on the market, although its bundled software leaves something to be desired. And let's not forget about PC integration chip sets, especially the upcoming Peripheral Component Interconnect (PCI) devices that will provide a standard local-bus architecture for 32- and 64-bit microprocessors. PCI-based systems should start appearing about the time you read this.

Of course, PCI is not the only kid on the block; a competing standard is the VL bus, named after the Video Electronics Standards Association's local bus. Both VL bus and PCI provide high-performance links between a CPU and its peripherals (such as network, video, and disk controller cards). In the words of one industry analyst, VL-bus seems to be better supported by expan-

sion-card manufacturers, and PCI by systems developers. Despite the lack of accepted standards, local-bus video is catching on. At last fall's Comdex, the computer industry's leading trade show, numerous video-card manufacturers announced VL-Bus products, including ATI, Cardinal, Genoa, Matrox. VideoLogic, and VidTech. Nonetheless, Intel's influence should not be underestimated. It will probably take 18-24 months for VL bus or PCI to emerge as a clear victor; in the meantime, both will be well supported by many manufacturers. One irony of all this is that the ISA vs. EISA vs. MCA bus war initiated with IBM's April 1987 introduction of the PS/2 line has become moot. The traditional expansion bus will be relegated to mouse, modem, and other low-speed devices.

The emergence of Windows (and to a lesser extent OS/2) has driven video card manufacturers to unprecedented levels of price/performance in just a few short years. Little more than two years ago, high-speed, high-resolution, high-color (24-bit) cards were available only on coprocessor-based boards, with prices beginning around \$1000. Today, you can get "accelerated" video adapters that provide 80% of the performance for 20% of the price of the coprocessed boards.

High-resolution monitors have also fallen in price, but not nearly as much as required. In addition, screen sizes greater than 16 inches invariably mean bulky, heavy, powerhungry devices. The monitor remains the weakest overall component of today's computer system.

One area of potential concern is semiconductor memory. The U.S. Department of Commerce recently instituted import duties on memory chips from several Korean manufac-

urers; street prices have already isen 25–30%. The DoC is expected to make a final ruling in early spring about whether those manufacturers are "dumping" chips below market value. If so, growth of Windows, OS/2, and corresponding applications software will likely slow. On the other hand, IBM and other manufacturers have started shipping 16-Mbit DRAM's on various systems. Clearly, the day of 16-, 64-, and 128-megabyte systems is not far off.

Digital-signal processing is poised to change dramatically the way PC's deal with analog data. Texas Instruments recently introduced a DSP chip and several corresponding boards that provide fax, modem, sound synthesis, speechrecognition, and data-compression capabilities. If this chip were made a standard part of every motherboard, it would eliminate the need for dedicated fax, modem, sound, and compression boards.

### Pervasive networking

It won't be long before every desktop and portable PC, Macintosh, and workstation comes with built-in network capability. Chips & Technologies and Standard Microsystems have joined AMD, Artisoft, and National Semiconductor in the market for low-cost, single-IC Ethernet interfaces. These devices provide a complete network interface in a \$20 package (in lots of 1000 + pieces). Zenith Data Systems was the first to include a built-in Ethernet port, but other manufacturers are following suit.

In the local-area networking arena, Microsoft released Windows for Workgroups (WfW), a version of Windows with built-in peer-to-peer networking. Although not as robust as market leader Lantastic, WfW has built-in scaled-down versions of Microsoft's widely regarded E-mail and group-scheduling applications. The main thing lacking is a DOS client (i.e., it is not possible to attach to a WfW server from a DOSonly machine). However, Microsoft will sell one separately, and may well bundle it with the forthcoming DOS 6.0, which will also include antivirus, disk-compression, and robust backup utilities. That should further squeeze Symantec/Norton and Central Point Software, providers of popular utility programs. WfW will not likely displace large NetWare (or other brand) LAN's. Microsoft appears to be targeting first-time network users and corporate workgroups with traditional client-server systems (e.g. NetWare) that also need peer-to-peer services.

Wireless networking is on the verge of exploding. There was a burst of interest on this subject at Fall Comdex. For example, two leading computer companies (IBM and Apple) have teamed up with several cellular telecommunications providers (McCaw, Ram Mobile Data, Ardis—itself a joint venture between Motorola and IBM-and others) to support Cellular Digital Packet Data, a way of delivering digital data (e.g. E-mail) to one or more recipients anywhere, on demand, and in real time. IBM, Apple, Motorola, and a startup called Eo demonstrated various notebook computers, stylus-input devices, and personal digital assistants (PDA's) performing CDPD activities with attached cellular modems and cellular telephones.

### Portables and printers

More manufacturers are supporting the PCMCIA (Personal Computer Memory Card Industry Association) standard. One vendor has gone so far as to call PCMCIA the ISA bus of the 90's. PCMCIA is not, however, without problems. The technology has gone through several fairly rapid evolutionary stages, PCMCIA 1 and PCMCIA 2, the latter being the current version. PCMCIA 1 was originally designed for memory expansion; but the idea of credit-card-size expansion devices quickly caught on and was expanded. IBM, for example, recently introduced several products called Credit Card Adapters that provide Token Ring and Ethernet connectivity, and 3270 terminal emulation. Other vendors also provide fax and modem adapters.

The technology has evolved more rapidly than the standards, so there is a potential for incompatibilities. To help avoid those problems, Intel developed an enhancement to PCMCIA 2, the Exchangeable Card

Architecture (ExCA), which appears to be catching on. In addition to basic PCMCIA 2 compatibility, ExCA addresses several other issues, including the use of multiple cards in a system, and hot swapping (the ability to insert and remove cards with power on). Caveat emptor if you plan to buy new systems with PCMCIA expansion capabilities.

On the other hand, pen-based computing (as discussed here in the February 1992 issue), has taken off much slower than expected. Originally, the industry expected to see significant activity by the end of 1992, but now it looks as if little will happen before late 1993. However, as one manufacturer puts it, "The timing for our projections was off—not the projections themselves."

Hewlett-Packard has once again created a ground-breaking product: The LaserJet IV. It is a true 600-dots per inch laser printer, with street prices starting around \$1300; for PostScript, add about \$500. You don't have to look twice to see the difference between 300 and 600 DPI, especially when reproducing fine curves and gray-scaled photographs. Another innovation is bidirectional communications, which allows the printer to inform a host computer of such printer faults as paper out and paper jamming.

Compag also broke into the highresolution market last summer with an extremely competitive, large-format laser printer that accepts useful add-ins including a send/receive fax modem. That idea quickly spread to the retrofit market for older Laser-Jet II's and III's, which now have several choices for faxes that interface through font-cartridge slots. Microsoft will shortly introduce a II/III upgrade cartridge of its own. The company claims that this cartridge will print Windows graphics much quicker than with the use of either PostScript or PCL. It will also provide a voice interface that will, for example, inform the user aurally that paper is out.

On the workstation front, DEC recently released seven computers ranging from \$10,000 workstations to \$300,000 mainframes, all based on the long-awaited 64-bit Alpha microprocessor. DEC has also publicly

demonstrated Windows NT running on an EISA-based Alpha PC—that, incidentally, includes a PCI-based local bus. Sun and HP simultaneously announced competitive upgrades to their lines. Sun appears to be going after the high-end PC market, claiming much better Auto-CAD performance than with a 50-MHz 486. Industry feeling is that HP provides the performance edgebut Sun still holds the largest market share, about 34%. IBM has been strangely silent about its wellreceived RS/6000 line throughout these recent scuffles.

### Conclusions

Together, all these developments add up to a new era of power and convenience for personal-computer users. The day is not far off when you will be able to connect to a worldwide network from anywhere, at any time, and obtain any available information. The rate of approach to this goal has increased rapidly during the past year, and the trend is likely to continue. More next time.

### **Product watch**

Figure 1 shows a screen shot of a ground-breaking new Windows database: Microsoft's Access. This is a product made to order for people whose needs exceed the capabilities of typical flat-file databases, but who don't enjoy writing code in dBASE (or whatever), and who, in any case, want a wholly Windows-based solution. To understand Access, imagine uniting a powerful, multilingual, multiuser



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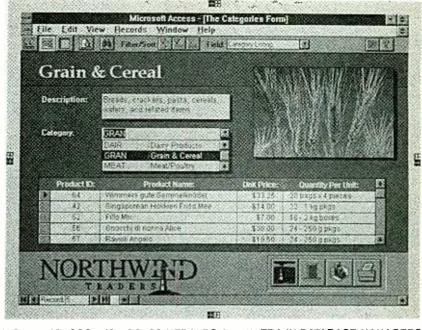


FIG. 1—MICROSOFT'S ACCESS HERALDS A NEW ERA IN DATABASE MANAGERS. This program provides power, ease of use, and ease of learning for Windows users. It spells trouble for Borland's dBASE and Paradox lines, both of which still have no Windows versions.

database engine with a visual development environment like that in Visual Basic, giving it a good dose of object-oriented behavior, and topping it all off with extensive help and tutorial information suitable for occasional database developers.

In addition to its own format, Access can read and write ASCII, Btrieve, dBASE, Excel, and Paradox files in their native formats. Access can also attach to SQL databases (at present, only Microsoft's SQL server, but Oracle support is scheduled soon). Access has extremely intuitive form-, report-, and query-building tools. For example, the form builder lets you draw fields, attach attributes (e.g. color and input validation criteria), and go.

Like Microsoft's other major Windows applications (Word and Excel), Access has just the right balance of power and ease of use. As with the other products, Access makes it easy to get started, and macros and a full development language called Access Basic provide lots of room for growth as your needs evolve. Access supports typical data types (character, date, numeric, logical), as well as binary objects including images, sound, and video.

Access is a fully relational prod-

uct that allows one to create "virtual" tables, called Dynasets, that consist of records concatenated from other tables joined by common fields. Any updates to a Dynaset propagate back into the source tables from which the data came. Access also provides multiuser network access (including WfW support) and record-level locking. Initial pricing was set at about \$100. If you can get a copy at that price, grab it. It's one of the best software deals around.

Home hardware hackers will want to check out Home Automation Laboratories, which publishes a catalog chock-full of information and product listings for devices that control lights and other electrical appliances remotely through special control panels or your PC. Simply reading the catalog can be an education in itself.

If you're looking for special laser printer paper or labels, check out the Paper Direct catalog. It lists numerous specialty items including foils that you can run through your laser printer to add color to presentations, prefolded brochure blanks that go through your laser printer and have business-card cutouts, and lots of other goodies. In both cases, tell 'em we sent you.  $\Omega$ 

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Part	Product		
No.	No.	Description	Pric
3R34761	XC556G	T1 3/4, (green)	\$.16
3R34796	XC556R	T1 3/4, (red)	.12
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No.	No.	Description Price
3R28628	PN2222	TO-92 case\$.12
3R28644	PN2907	TO-92 case
3R35991	1N4004	DO-41 case10
3R38236	2N2222A	TO-18 case25
3R36126	1N4735	DO-41 case
3R38359	2N3904	TO-92 case12
3R36290	1N751	DO-35 case15
3R38421	2N4401	TO-92 case15
3R36038	1N4148	DO-35 case
3R38308	2N3055	TO-3 case





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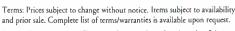
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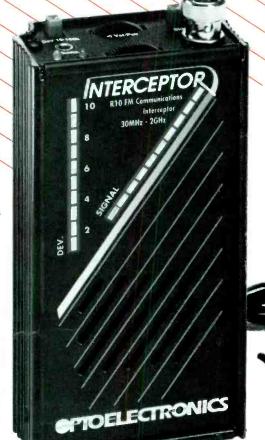
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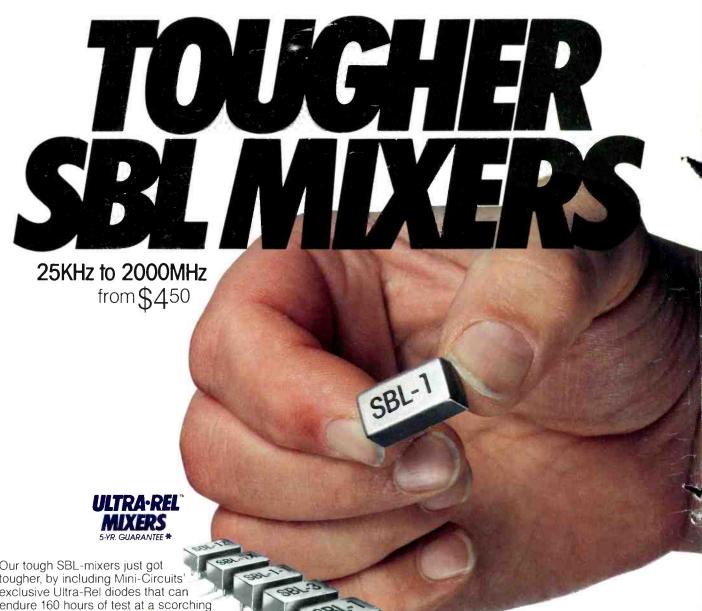
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