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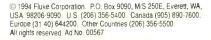
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Vol. 65 No. 9

ON THE COVER

C O

35 MODEM COMMUNICATIONS STANDARDS

There's no doubt that we're livnig in the Information Age, thanks in part to the proliferation of low-cost personal computers, which provide wide-spread, easy access via telephone to on-line networks. Because the U.S. tele-

phone system is analog, a modem is required to translate the digital output of the computer into sounds that can be sent over the phone lines, and to convert those audio signals back into digital information on the



SEPTEMBER

other end. Since their introduction, modems have been continuously evolving as their speed and data-handling capacity increase. It's been a challenge to create standards quickly enough to keep up with the changes. Modems operating under global standards are the integral ingredient in worldwide comptuer communications. This article provides an overview of modem technology, specifications, terminology, and the latest standards.

BUILD THIS

43 TELEPHONE LINE GRABBER

Use this listening circuit to intercept phone

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conversations or monitor room activiities form a remote telephone.— Robert lannini

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This microcontroller-based music-training system allows children to play and enjoy music before they are old enough for formal training. — James E. Tarchinski

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Generate variable-duration output pulses with selectable polarity and a wide range of time intervals, using this inexpensive tool. — *Dev Palmer*

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MORSE CODE TUTOR This BASIC program can teach you Morse code, or help you brush up on your skills. — James E. Tarchinski



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WHAT'S NEWS

Quantum-cascade laser developed

A new kind of semiconductor laser diode, called a quantum cascade (QC) laser, has been developed by AT&T Bell Laboratories. Its developers say that it is the first laser diode that can be made to emit at different wavelengths by varying the thickness of its semiconductor material layers rather than the composition of those layers.

The first QC laser developed emitted at a wavelength of 4.25 microns in the mid-infrared region. But its developers say that QC lasers can be made to emit over a range from 2 microns (the near-end of the mid-infrared region) to 100 microns (well into the far-infrared region). The operation of the QC laser diode differs radically from that of the conventional semiconductor laser.

Applications for the QC laser are expected in communications and in scientific instruments for such work as material analysis, spectroscopy, and environmental monitoring.

Conventional semiconductor lasers operate in the near-infrared to visible light regions (about 0.6 to 1.5 microns). Negative and positive charges (electrons and holes) are injected into their active layers where they annihilate each other, releasing energy as photons.

The energy of these photons and their corresponding wavelengths are determined by the bandgap of the laser's active-layer material. The bandgap is the energy difference between a band of energy levels occupied by the injected electrons (conduction band) and a lower band occupied by the injected holes (valence band). The emission wavelength of a semiconductor laser can be altered only by altering the composition of its semiconductor layers because the bandgap is a fundamental material property.

By contrast, the QC laser is a unipolar semiconductor laser; only one type of charge (e.g., electrons) is needed to make it lase. Electrons jump between two well defined energy levels (quantum wells) and the energy of the emitted photons is equal to the differences between those levels.

The photon energy, determined by the wavelength of the emitted light, is controlled by the thickness of the quantum wells and the height of the energy barriers that confine the electrons to those active regions (quantum confinement). Because the wavelength is determined by quantum effects, the laser can be custom made to operate over a wide wavelength region by altering the thickness but not the composition of its semiconductor layers.

The gain of QC lasers is expected to be much less sensitive to temperature changes than conventional semiconductor lasers. Its emission linewidth is intrinsically narrower, and its frequency response differs from that of other semiconductor lasers.

The development of the QC laser was made possible by recent advances in the understanding of semiconductor band-structures—the relationships between the material's electronic and optical properties and new material deposition techniques. The laser's layers are formed by molecular beam epitaxy (MBE), a method in which atoms are "spray painted" on a substrate, one layer at a time.

The multilayer material, including its quantum-well active regions, consists of alternate layers of nanometer-thick aluminum-indium arsenide and gallium-indium arsenide grown by MBE on an indium-phosphide substrate.

More smart batteries

Another program to develop "smart" batteries has been announced, this one by Energizer Power Systems, a subsidiary of Eveready Battery Co. and National Semiconductor. The joint effort



SMART BATTERIES would be able to determine the proper amount of recharging and the length of battery run-time that remains.

seeks to simplify the charging of rechargeable batteries and provide means for determining the status of that charge for portable computers.

Energizer Power Management brand products will have integrated circuitry within the battery that will monitor battery condition and control battery-charging rate.

By eliminating possible overcharging, which can reduce battery life, Energizer Power Systems says it is possible to increase their charge capacity. The circuitry in the "smart" battery will permit users of the host equipment to determine the status of the charge at any time.

The two companies seek to develop better nickel-metal hydroxide (Ni-MH) and nickel-cadmium (NiCd) batteries. While the initial target is the notebook-computer market, they are planning to apply the concept to mobile communications, power tools, and other battery-powered equipment.

IBM boosts memory capacity

Scientists at IBM's Almaden Research Center in San Jose, Califor-*Continued on page 10*

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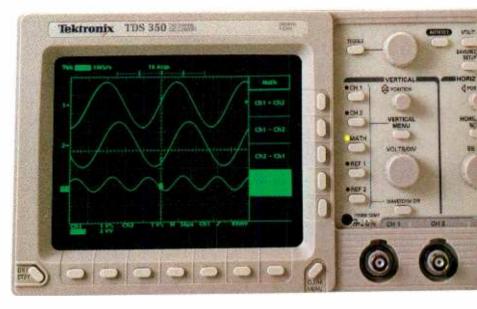
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VIDEO NEWS

What's new in the fast-changing video industry.

DAVID LACHENBRUCH

• Modular TV sets? General Instrument Corporation, a major manufacturer of cable TV equipment, thinks TV should go the way of audio. It plans to enter the televisionset business with modular components, so buyers can choose their features—such as picture-in-picture, type of remote control, screen proportions, and sound systemand build their own custom TVs, GI argues that this will make television sets obsolescence-proof; when one part of the set goes out of date. it's not necessary to discard the whole thing, but just the affected module. Working with Motorola, GI is putting together a package of basic signal-processing components in a box, which it calls 'Joey''-after the Australian kangaroo, which carries its young in a modular way, so to speak. Buyers can then plug in the type of display, sound system, or remote control, depending on their wants and needs.

Gl and Motorola say they don't want an exclusive on the system, and they are inviting television manufacturers to join in to make and self compatible components. Joey would be prepared for the future, and it would accommodate a wide variety of inputs, including descramblers for pay cable, decompression devices for digital signals, multimedia modules, and such interactive equipment as printers and keyboards. GI estimates that the first Joeys could go on the market in a year or less at a retail price of \$300 to \$500.

"Wait a minute," responds the TV industry, visibly unimpressed. TV manufacturers point out that the bucket of dumb components would be selling for the approximate price of a complete 25- to 27-inch set, and it wouldn't even include the two most expensive components— the picture tube and the cabinet. Motorola concedes that prices

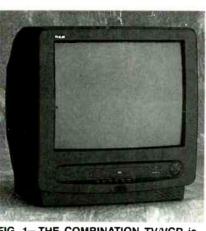


FIG. 1—THE COMBINATION TV/VCR is this year's hottest consumer-electronics product. This might indicate that the U.S. is not ready for modular TV.

would have to come down sharply, but TV manufacturers counter that Joey would be impractical at any price, noting that consumers like to buy complete sets they can plug in and play. That, they say, is the most economical way to manufacture and sell TVs. They also note that the public has trouble with plug-ins, asserting that many consumers can't figure out how to connect a VCR to their TV.

TV manufacturers also point out that the trend has been in the opposite direction-the combination TV and VCR is the hottest product of this year. They also point to experience in the past with modular TV. Sony's Profeel was a high-performance TV set whose monitor was sold separately from the tuner and the audio system. It failed in the market because consumers couldn't understand why they should pay more for a set with no tuner and no sound than one with both features-regardless of quality. Joey's fate is still up in the air.

Movie on five-inch disc.

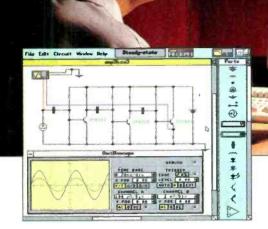
Industry interest is intensifying in the concept of a full-length movie on a 5-inch optical disc, spearheaded by Philips. JVC announced that it

has developed a system that will record more than 135 minutes of high-quality video on a single disc. It uses the MPEG-2 protocol that provides better than laserdisc quality. JVC said its accomplishment was based on "variable-bit-rate" technology. Existing high-density technology for digital video discs based on conventional red lasers can deliver about four times the capacity of a standard CD, but it would still fall at least 50% short of accommodating a full-length movie, which would require six gigabytes of capacity. JVC said that its variable-bit-rate system provides the six gigabytes by using a "high transmission rate for pictures with a lot of information and low transmission rate for those with little information." JVC pointed out that a fixed transmission rate makes inefficient use of disc capacity because that rate is dictated by the requirements of "pictures with the greatest amount of information."

A high official of Sony Corporation of America said that moves to record a full movie on a five-inch disc are in the "right direction." Sony, which is co-holder of the basic CD patents with Philips, is in discussions with other manufacturers throughout the world on standards for the next generation of high-density video disc, said John Briesch, president of Sony Consumer Products. JVC has also pledged to work toward standardization of a new Digital Video Disc (DVD) format.

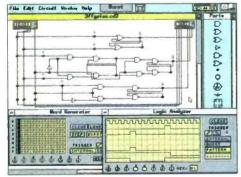
• Electronic game delivery. It has been predicted so often that it's hard to believe that it actually is being done—or at least tested. Since audio and video cassettes as well as video games are merely electronic impulses recorded on various media, why is it necessary to deliver them to stores by such antiquated methods as mail or *Continued on page 80*

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BATTERY BACKUP

I am building a circuit that stores operating data which configures the circuit in CMOS memory. I'd like to use nickelcadmium cells to provide power to the memory when the device is turned off. I need some way to charge the batteries when the device is turned on and then power the CMOS memory only when it's turned off. Can you give me a simple circuit that can do this?—N. Herbert, New London, CT

Charging nickel-cadmium batteries isn't complicated. They should be trickle charged because there's no guarantee as to how long the batteries will be kept under charge. A charge rate that is too high will more than likely damage the batteries.

The circuit you're looking for can be small because you don't need a lot of power to maintain the data in memory. Most CMOS static memory is guaranteed to retain data with current drain that's in the microampere range. This means that the batteries you need to do the job should be button cells or some other form that has a rating under 50 milliampere-hours.

The circuit shown in Fig. 1 performs two functions: It provides for both battery charging and directing battery power when the device you've built is turned off. When the device is turned on, power is available to charge the battery, so D2 is reverse biased and current flows into the batteries through current limiter resistor R1.

When you turn the device off, D2 is forward-biased, and battery power is available. Steering diode D1 keeps the battery from powering anything other than the CMOS memory. You can install almost any diode you want for D2 (even a small 1N914) since the power needed to maintain the memory is so low you'll have difficulty measuring it.

Because the battery can be left to charge for an extended period of time, you'll have to choose a value for R1 that will limit the charging current to one tenth of the battery's ampere-hour capacity. This can be calculated by: R1 = $((V_{CIRCUIT} -$

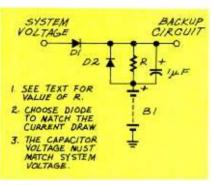


FIG. 1—THIS CIRCUIT CHARGES the battery and controls battery power when the device is turned off.

 $(0.6V + V_{BATTERY}))/I_{CHARGE}$ Note that you have to subtract the 0.6-volt diode drop and battery voltage from the supply voltage. The capacitor in the circuit acts as a sponge to swallow any voltage glitches and also to provide a few seconds of power if you want to change batteries.

MYSTERY IMPEDANCE

I'm trying to measure the impedance of my stereo speakers with no luck. When I put a multimeter across the speaker terminals, I get a reading of less than one ohm. I know there's a difference between impedance and resistance, but I'm not sure what the difference is. Can you explain it to me?—F. Benfish, Scoop, NY

The difference between impedance and resistance is similar to the difference between AC and DC. The resistance exhibited by a particular component remains constant only as long as the materials that determine its resistance remain constant.

The easiest way to understand what this means is to study a capacitor, although it might seem unusual to talk about the resistance of a capacitor. When you apply a DC voltage across the terminals of a capacitor, it initially displays no resistance but, as the field increases, its resistance increases until current flow through the capacitor stops. At that point the capacitor has "infinite" resistance.

The resistance of a circuit element is just the DC component of its impedance. But, as circuit parameters change, the AC component of the impedance will change as well. Those circuit factors include such things as current flow, inductance, and frequency. A speaker's impedance is also affected by environmental factors such as air pressure and temperature, and by the coil that moves the cone in and out of the speaker.

If you want to measure the impedance of your loudspeaker system, put a variable resistor in series with the amplifier and the loudspeaker. By convention, loudspeaker impedance is usually measured at a frequency of 400 hertz, so you'll want an audio function generator or an audio test CD to supply a 400-hertz signal to the amplifier.

Measure the voltage drop separately across both the variable resistor and the speaker, and adjust the resistor until both voltage drops are equal. Then remove the variable resistor from the circuit and measure its value. The value of the resistor will be equal to the speaker's impedance in ohms.

A speaker presents its rated impedance over only a small range of frequencies. You might want to repeat the measurements at different frequencies and chart the results on graph paper.That way you can obtain a graph of how the impedance varies.

VCR HARD-DRIVE BACKUP

I recently exchanged the hard drive on my computer for a new one with a 210-megabyte capacity. I used to back up my old 30megabyte hard drive with floppy disks, but this is impractical with my new drive. I remember reading about circuit cards that would let me back up a hard drive with my VCR. I've been searching for a system like this but I haven't been able to find one. Can you help?—L. Buxbaum, Boston, MA

Hard drive technology is changing rapidly. In the last few years their quality has gone up and their prices have gone down dramatically. The reliability of modern hard drives has lulled a lot of people into carelessness about backing them up. When hard disk drives crashed all the time, backing them up was a necessity, but today some people regard data backup as an option. Big mistake.

I remember seeing the same ads for VCR-hard drive backup systems, but they disappeared as tape backup became standardized, more available, and more affordable. The problem with all VCR backup systems is that there was never an established standard for writing the data on the videotape. By the time the QIC-40 tape-drive standard became widely accepted, VCR backup technology had all but disappeared.

As things stand now, you can buy a 250-megabyte (with compression) tape backup drive for less than \$150. Tape drives cost about half of what they did a few years ago, and they're also significantly less than the cost of those earlier VCR systems you asked about. In addition, standard formats such as QIC-40 and QIC-80 allow tapes to be read on another tape drive in another computer. This not only gives you an easy way to move masses of data from one computer to another but, if your computer goes up in smoke, there will always be a way to restore your data on another machine. This just wouldn't be possible with a nonstandard or, worse yet, proprietary backup scheme.

I agree with you that backing up over 200 megabytes to a bunch of

floppies is about as inviting as a root canal. If you want to back up the data reliably, consider purchasing a standard tape drive. If it makes you feel any better, you might consider the fact that you can buy both a 200-megabyte hard drive and a tape drive today for about half of what you would have paid for the hard drive alone just a few years ago—now that's progress! Ω





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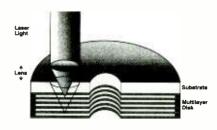
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WHAT'S NEWS

continued from page 4

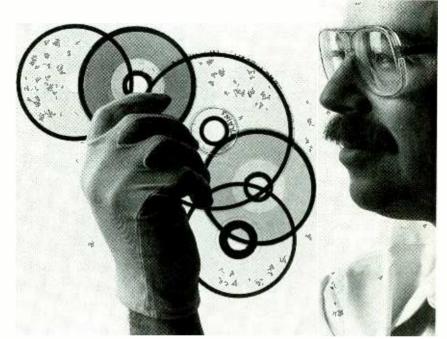
nia, have recently announced advancements that increase the data storage capacity of two different media—conventional magnetic harddisk drives and CD-ROM drives.

IBM's new hard-disk formatting technique allows it to pack 28% more data into its latest line of magnetic hard-disk drives for laptop computers. IBM's new No-ID sec-



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IBM'S MULTILAYER OPTICAL DISKS, made by sandwiching together as many as ten partially transparent, partially reflective layers, can hold up to ten times the data of today's optical disks.



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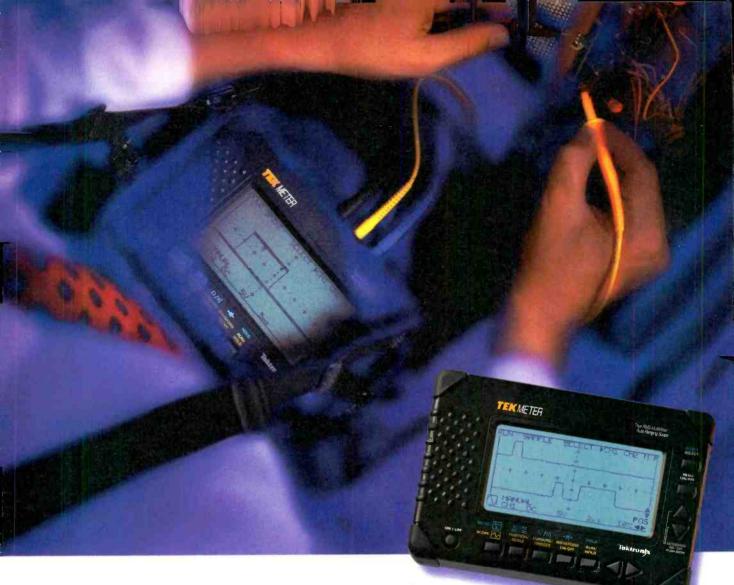
tor format is credited with permitting 270 megabytes to be crammed onto each 2.5-inch diameter disk of an 810 megabyte three-disk drive.

The No-ID sector format increases data-storage capacity by removing all of the disk-sector identification (ID) information that normally precedes every block of data on a disk. Their functions are now handled electronically, freeing up about 10 to 15% of the disk area for storing more user data.

When applied to IBM's magnetoresistive (MR) recording head, the No-ID format also permits the data tracks to be positioned closer together, providing additional capacity gain. The new format is said to permit faster and more reliable datareading and writing. The Almaden Research Center has also demonstrated a new multilevel optical disk that it says will expand the storage capacity of CDs for playing back audio as well as CD-ROMs for playing back computer audio and video data.

In existing CD storage drives, a fine laser beam is focused on a rotating reflecting disk. All data are stored on the disk as annular rings of tiny pits formed by a powerful "write" laser. The pits cause variations in the brightness of the reflected beam from a "read" laser which are converted into digitally coded strings of 1's and 0's.

In the new IBM system, a stack of transparent but reflective disks replaces a single reflective disk. A *Continued on page 80*



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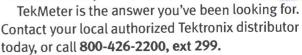


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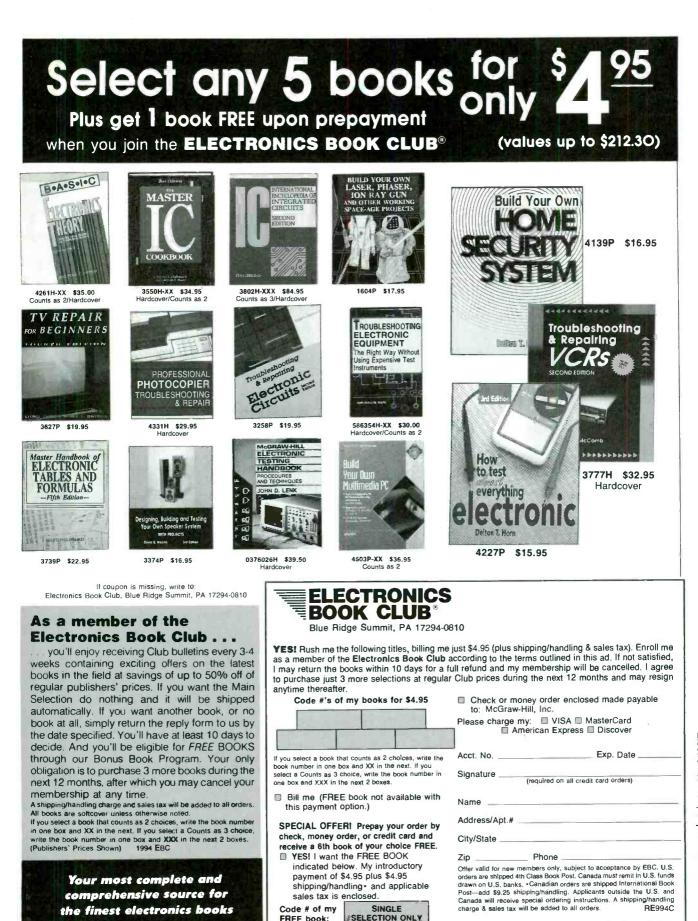
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LETTERS

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MISSING TABLE

The table referenced in the last paragraph of "Computer Connections" in the July issue of Electronics Now was inadvertently omitted. We've included it here, and apologize for any inconvenience caused to our readers by its omission.—Editor tween the pad at the base of Q4 (its center lead) and the ground pad to the left.

Also in the parts-placement diagram, R21 shown between potentiometer R18 and Q5 should be shown as C42; R21 is not used in the circuit.—Editor.

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| Database | Access, Foxpro | (Paradox) | Approach | |
| Email | MS Mail | WordPerfect Office | cc:Mail | |
| Enterprise Glue | MS Office and Visual Basic for Application | WordPerfect Office | Notes | 10 |

TABLE 1—PRODUCT LINEUPS

ATV CORRECTIONS

There are a few corrections to our ATV story that ran in the July and August 1994 issues of Electronics Now. All corrections pertain to the 5-watt transmitter. To begin with, R24 was missing from the Parts List. It should be included there as a 1K, ½-watt resistor.

While it might not have been clear from the parts-placement diagram, reverse-polarity protection diode D4 has only one lead (its cathode) soldered to the PC board. Power is applied to the anode end of the diode, which is not soldered to the board.

In the parts-placement diagram, R30 should be shown as R31. The "real" R30 should be installed be-

REGENERATIVE RECEIVER RESPONSE

I am responding to Mr. Bialkowski's letter (*Electronics Now*, June 1994) expressing his concerns about the use of regenerative receivers.

The demise of regenerative receivers had many causes, but I suspect that the main reason was the availability of low-cost, factory made receivers. As the depression ended,people no longer had to build their own receivers to save money because they were able to buy them. With progress in receiver design, manufacturers chose to make and sell superheterodyne sets, which were easier to tune to the desired stations. On the subject of radio-frequency interference, my article, "The Lost Art of Regeneration" (*Electronics Now*, March 1994) clearly stated that unbuffered detectors should not be allowed to oscillate. Also, Mr. Bialkowski's comparison of the emissions from old-fashioned, tubetype regenerative receivers that dissipated several watts of power with modern versions powered from a 9volt battery that dissipate only a few milliwatts is grossly unfair to the older units.

Strictly speaking, any receiver with an oscillator will radiate some RF energy. The important point is the level of that emission. Many direct conversion receivers in common use today have free-running local oscillators that are buffered only by the mixer stage (often an NE602). Radiation from that kind of receiver can easily equal or exceed that of a regenerative circuit buffered by an RF stage. Nevertheless, the radiation from both types of receiver is likely to be well below the limits imposed by FCC rules, Part 15.

Finally, the term "Autodyne" commonly referred to a regenerative detector operated in an oscillating condition. The tuning was adjusted to zero beat with AM signals, or slightly off zero, which produced an audible tone for the reception of CW. CHARLES KITCHIN *Wilmington, MA*

RELAY RAVES

I thoroughly enjoyed the article, "All About Relays" (*Electronics Now*, June 1994). Not only was it an excellent refresher course, it also provided valuable general-purpose information in a simple and thorough manner.

I hope you will consider running these "how do they work" articles on a regular basis—perhaps "All About Transformers," "All About Transistors," etc. I am convinced

16

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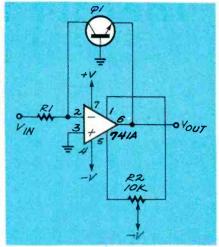


FIG. 1 A LINEAR TO LOG amplifier.

that many of your readers would enjoy this type of article as much as I would. DAVID JENKINS *Austin, TX*

Some recent subjects in this series by Ray Marston have included field-effect transistors (March to May, 1993), bipolar transistors (September to November 1993), oscillators (December 1993), audio amplifiers (March 1994), and power amplifiers (April 1993) —Editor

LINEAR-TO-LOG CONVERTER

I am writing to comment on a circuit that was published in the Q&A column (*Electronics Now, June 1994).* A. Blumenthal asked for a simple circuit that would convert linear functions to log functions. However, the circuit shown in Fig. 2 in Q&A will not work as a linear-to-log amplifier because the 741 operational amplifier inputs are reversed.

That configuration of log amplifier shown is known as a *transdiode log converter*. There are other versions that are not true logging circuits, but they closely approximate the function. The logger shown in Fig. 1 has a range of about 5 decades (100 dB). Its basic function is based on its characteristic of V_O that will be V_{BE}. The V_{BE} of a silicon transistor for

- $V_{CE} = 0$ volts is as follows: $V_{BE} = 2.3 \text{kT/q} \ln (l_c/l_o)$ where
- k = Boltzmann's constant (1.38 \times 10⁻²³ J/K)
- T = absolute temperature (Kelvin)
- q = charge on an electron (1.6 \times
- 10⁻¹⁹ coulomb)
- I_{C} = collector current
- I_{O} = reverse saturation current

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At 27°C, kT/g is equal to 26 mV, which produces:

 $V_{BE} = 60 \text{ mV} \log_{10} (I_c/I_o).$

Thus, for each decade increase in I_C, V_{BE} will increase 60 millivolts. This circuit is an excellent logger. but its 60-millivolt per decade output is inconvenient for most applications where 1 volt per decade is the standard.

R. JEFFREY PERRYMAN Rural Hall, NC

SOFTWARE DOCUMENTATION CHECKS

I thoroughly enjoyed Robert Grossblatt's Drawing Board column on removing software documentation checks (Electronics Now. September 1993). I'm sure you will get some negative feedback regarding that column. Most likely someone will condemn Mr. Grossblatt for encouraging software piracy, or something equally foolish. Anyone who reads the column and runs to their local pirate BBS bragging about his newly learned skill is incredibly lame.

It would have taken me at least twice as long to learn assembly language without the help of a disassembler. Reverse engineering software can also be an incredibly enlightening brain-twister when the software company has seen fit to include an anti-debugger code in its release. The column was not without its

share of inaccuracies, however, Mr. Grossblatt mentions the IRET instructions as "return from subroutine." Actually, IRET means "return from Interrupt Service Routine (ISR)." The complementary instruction to CALL is RET. RETF is also used for returning from far CALLs (those that call code in another 64K segment).

The difference is as follows. When a CALL is executed, it puts the address of the instruction of the next instruction on the stack. That is equivalent to a PUSH IP instruction. When an RET is executed, it restores the word at the top of the stack to the IP register. The effect is to return control to the statement after the CALL. An IRET, however, is for use with the INT instruction. The specifics of ISRs are a book in themselves, so I will not delve into them here. Suffice it to say that the INT instruction pushes both the contents of the FLAGS register and the return address onto the stack. The IRET complements those actions. If an IRET was to be used to return from a CALL, whatever word happened to be at the top of the stack would be transferred to the FLAGS register, destroying the state of the register.

Thank you for providing some very interesting reading. I will be interested to see what other readers have to say about the column. CHRIS McCANN Gilberts. IL

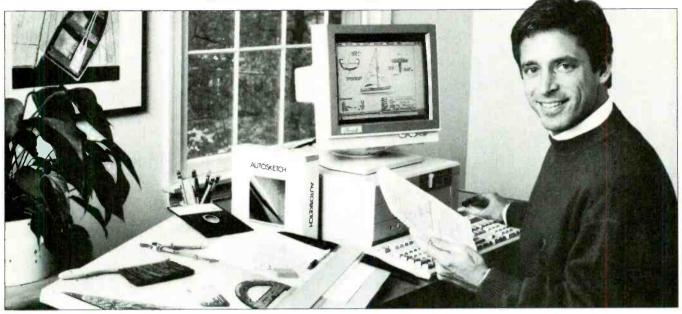
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September 1994, Electronics Now 21

EQUIPMENT REPORTS

B+K Precision LCR Bridge

n experienced electronic technician is known by the quality and capability of the test instruments he keeps. That should not be surprising. After years of trying out different kinds of test equipment, you can expect that he'll end up with the tools that make his job easier, save time, and pay for themselves in as short a time as possible.

Consider the normally odious task of sorting and matching components. This can be very time consuming work if all you have is a basic digital multimeter and you must observe and make a mental note of the value of every part you test. And, of course, you must stay alert enough to reject any parts that don't meet the required tolerances.

Fortunately, a new handheld LCR bridge from B+K Precision (Maxtec International Corporation), 6470 W. Cortland Street, Chicago, IL 60635, 312-889-1448) offers many functions that make sorting and matching components a breeze—it is priced at \$275.

The B+K Precision Model 878 LCR bridge measures inductance, capacitance, and resistance with a basic accuracy of 0.7 %. The meter is packaged in a rugged plastic case and weighs less than a pound. There's a built-in stand on the back of the case, as well as two extremely "grippy," ribbed, rubber feet.

The feet are shaped to keep the meter from sliding, whether or not the stand is in use. Believe it or not, simple product details like no-skid feet make a meter a lot more userfriendly. (If you've ever had a test instrument that kept sliding off the test bench whenever you pulled on its test leads, you know what that means.)

Portability is a nice feature, especially when you are out of range of an AC outlet. But a disadvantage of most handheld instruments is that they can be powered only by a batMeasure, sort and match inductors, capacitors, and resistors quickly and easily with B+K's new Model 878 LCR Bridge.



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tery which periodically must be replaced at extra cost. Out in the field, the Model 878 can be powered by a 9-volt battery, but in the shop you can plug it into the AC line.

Because the meter has features that make bench tasks like sorting easy, it is quite likely that it will be used often on the test bench. That's why B + K thoughtfully added a 9volt DC adapter that plugs into an AC outlet and a jack on the side of the meter. This eliminates the need to consume battery power whenever an AC outlet is handy.

An automatic power-down feature conserves the batteries in case you forget to turn off the meter. However, that power-down feature can be disabled.

The Model 878 features autoranging, but the ranges can be set manually, if necessary. The four-digit liquid crystal display presents values to 9999 in each range, and a dual-display feature permits the simultaneous display of either inductance and Q or capacitance and the dissipation factor (D).

The display will also indicate when battery voltage is low and when the meter should be calibrated. Calibration, which zeros out test-lead capacitance, inductance, and resistance, is as simple as pressing a CAL button.

The meter can measure capacitance from 0.1 picofarad to 10 millifarads, resistance from 0.001 ohm to 10 megohms, and inductance from 0.1 microhenry to 10,000 henries at either 120 hertz or 1 kilohertz. The 1-kilohertz test signal is normally used to test inductors that will be operating at the higher frequencies found in audio, video, and RF circuits.

The 120-hertz signal is better suited for testing inductors for use in lower-frequency circuits such as power supply filter chokes. A pushbutton on the meter's front panel selects either the 120-hertz or the 1kilohertz signal.

Inductors are normally tested in the series equivalent mode. The series mode provides the most accurate Q readings for low-Q inductors. For measuring iron-core inductors that operate at higher frequencies, a parallel equivalent mode can be selected.

Two wide slots on the meter's front panel accept the leads of most components, and a pair of short test leads with alligator clips can test any components whose leads don't fit in the slots.

Sorting features

The meter includes a Max/Min/ Avg mode that can be selected before testing a new batch of components. Then, as each new component in the batch is tested, the meter recalculates a new average for the batch and records those minimum and maximum readings as *Continued on page 64*

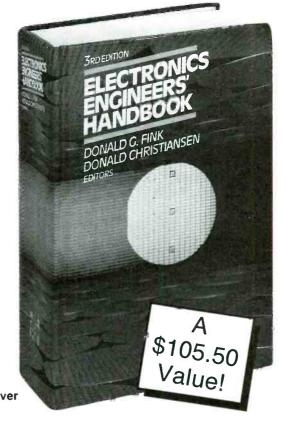
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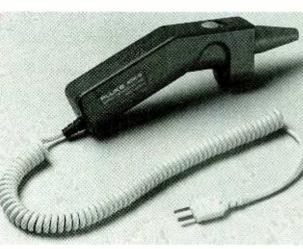
Publisher's price shown. ©1994 EEBC

NEW PRODUCTS

Use the Free Information Card for more details on these products.

NON-CONTACT TEMPERA-TURE PROBE. The Fluke 80PK-IR handheld temperature probe is intended for use with Fluke digital thermometers that accept Type-K miniature thermocouples. The probe receives infrared emissions from the source whose temperature is to be measured making it a non-contact instrument. It is suitable for factory maintenance, heating, ventilation and air conditioning installation and repair, and electrical power transmission applications.

makes the probe suitable for taking temperatures of be made by direct contact methods because they are electrically alive, in motion. inaccessible, or will be contaminated by contacts with attached sensors.



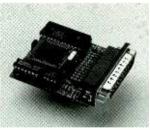
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The probe, which con-Non-contact operation nects directly to a digital thermometer, can be held in one hand, leaving the heat sources that cannot other hand free for adjusting instrument settings. Readings are taken by pointing the probe at the heat source to be measured. The probe has a temperature reading accuracy of 3% and a temperature range of 0° F to 500° F (-18°C to 260° C).

The 80PK-IR infrared. non-contact temperature probe is priced at \$259. Fluke Corporation P.O. Box 9090 Everett, WA 98206 Phone: 800-87-FLUKE Fax: 206-356-5116

port, and a +5-volt regulator. Its EEPROM offers concurrent read/write operation which the device can read while data is being written to it. A BASIC interpreter includes several utilities such as frequency measurement, real time clock/calendar. and hex file loading. The BASIC programs can be interactively edited, and any stored program is automatically executed on power up.

Each of the Xplor-32's 12 digital I/O lines includes a socket that permits solderless connections for external components such as resistors, capacitors, or transistors. All external connections are made through a single 25-pin Dtype subminiature I/O connector.



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A companion ST-25 interface module accesses Xplor-32 signal lines. Screw-type terminals on all I/O lines include a powersupply jack, a 9-pin D-subminiature connector for PC-compatible serial ports, and an X-10 powerline interface jack.

The Xplor-32 is priced at \$59.95. A package including the Xplor-32, ST-25, PC serial interface cable, a 9volt power supply, an ap-

PEN-STYLE MULTIMETER.

The SI1000 pen-style digital multimeter from Shoreline Instruments can display 11 measurement ranges including AC and DC volts, AC current, and resistance. It includes a diode tester and an audible continuity checker. Range can be set with a slide switch.

The multimeter, with a 2000-count liquid crystal display, measures $9\frac{}{8}\times1\frac{}{4}\times1$ inches and weighs four ounces. It can be held like a pen, or gripped in the palm with the display facing upwards. The DMM has a twist-on

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alligator clip that attaches to its ground probe to permit the user to connect it to the circuit and make measurements with only one hand.

The SI1000 pen-style

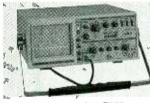
digital multimeter is priced at \$39.95. Shoreline Electronics, Inc. P.O. Box 378 Moffett Field, CA Phone: 408-987-7733 Fax: 408-987-7735

PERSONAL DIGITAL CON-TROLLER BOARD. The Xplor-32 personal digital controller board from Blue Earth Research is intended for embedded control, monitoring limits, and datalogging.

The board, which measures 2.15×2.2 inches, includes an Intel 80C32 microcontroller, a Xicor 8kilobyte EEPROM, a serial

plications disk, and a user's manual sells for \$99.95. **Blue Earth Research** 165 West Lind Court Mankato, MN 56001 Phone: 507-387-4001 Fax: 507-387-4008

UPGRADED 100-MHZ SCOPE. The Model 2190A, 100 MHz, three-channel, six-trace oscilloscope from B+K Precision has more user-friendly controls and a lower price than its predecessor. Maximum sensitivity is given as 1 millivolt per division, and accuracy is specified as better than 3%. Rise time is less than 3.5 nanoseconds.



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Operating modes are CH1, CH2, ADD, DUAL and TRIPLE. Sweep speed is adjustable from 50 nanoseconds per division to 0.5 seconds per division in 22 calibrated steps with fine adjustment. Trigger modes are AUTO, NORM, TV-V, and TV-H. Trigger coupling can be AC, highfrequency reject, low-frequency reject, or DC. Variable hold-off permits the observation of stabilized complex pulse trains.

The Model 2190A has two timebase generators that allow any part of the waveform to be expanded. The signal-delay line permits viewing the leading edge of high-frequency signals and pulses with short rise times. X and Y inputs are provided for horizontal and vertical deflection, while a Z-axis input allows intensity modulation. The six-inch CRT has an illuminated fluorescent graticule that permits waveforms to show up clearly when they are photographed.

The Model 2190A oscilloscope, complete with instruction manual and probes is priced at \$1599. $\mathbf{B} + \mathbf{K}$ Precision

6470 West Cortland Street Chicago, IL 60635 Phone: 312-889-1448

TEMPERATURE-INDICATING

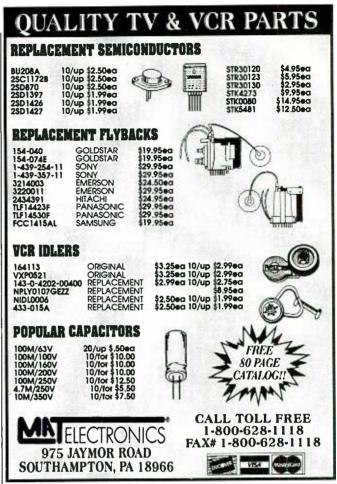
LABELS. A CelsiClock temperature indicating label from Solder Absorbing Technology is a small, clock-shaped, stick-on label that accurately and irreversibly indicates the maximum temperature reached by any device to which it is attached.

Each label measures %16 inch in diameter and contains five temperature-sensitive circles arranged like the numbers on a clock's face. Yellow digits within each circle indicate that circle's temperature rating. If the temperature rating of any circle is exceeded, that circle turns from clear to black—permanently.

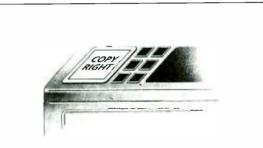
The yellow digits become highly visible when the background turns black. Each of the five circles on the labels has a different temperature rating, accurate to $\pm 1\%$. The labels are available in eight temperature groups covering 40°C to 260°C (105°F to 500°F).



The manufacturer states that CelsiClocks can be applied to power semiconductor devices and micro-



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processors, and are suitable for use on any part or surface where temperature measurement by other means is impractical, dangerous, or expensive.

CelsiClock temperatureindicating labels are priced from \$0.95 to \$1.35 each in packages of ten or at \$0.82 each in a roll of 1000. **Solder Absorbing Tech**-

nology, Inc. 144 Oakland Street Springfield, MA 01108

Springfield, MA 01108 Phone: 800-628-8862 Fax: 413-788-0490

DIGITAL MULTIMETER. The DM28XT handheld, battery-portable digital multimeter from Wavetek can measure and display temperature, capacitance and signal or line frequency in addition to making all of the standard electrical measurements.

It can measures AC voltage to 750 volts, DC voltage to 1000 volts, and both AC and DC current to 10 amperes. It can also measure resistance to 2000 megohms. The DMM includes a diode test circuit and an audible continuity tester.

Temperature can be measured in either Fahrenheit or Centigrade units up to 2000°F (1300°C), and it can measure capacitance up to 2000 microfarads. It can also measure signal or line frequency up to 2 kHz.

The DM28XT includes a liquid-crystal display and a pair of safety test leads. Both current jacks are fused to protect the user and meter from excessive current. Safety features include an audible warning beeper that sounds if a test lead is in the current jack while the meter is set for a voltage measurement.

The *DM28XT* DMM package including a battery, a pair of test leads with insulated probe tips, a



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spare fuse, a beaded Type-K thermocouple probe, a pair of threaded alligator clips, and an operator's manual is priced at \$139.95.

Wavetek Corporation 9145 Balboa Avenue San Diego, CA 92123 Phone: 619-279-2955

MINIATURE GPS ANTENNA.

An AMG Series antenna module for Global Positioning Systems (GPS) from Toko America includes an antenna element, a twopole bandpass filter, and a low-noise gallium arsenide amplifier and cable.

The antenna is tuned to $1575.42 \text{ MHz} \pm 1.023 \text{ MHz}$ for GPS receivers, and it operates on 4 to 5.25 volts. Antenna gain is 4 dBi typical at a 90° angle of elevation, and -4 dBi at 0°.



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The axial ratio is 3 dB maximum at 90°. Typical power gain of its low-noise amplifier is 26 dB, and it draws a maximum of only 25 milliamperes from a 4 to 5.25volt supply. The module is housed in a $38 \times 38 \times 16$ mm package. The cable can be customized on request. The module is offered with or without a radome

An AMG Series GPS antenna module is priced at \$150.

Toko America, Inc.

1250 Feehanville Drive Mt. Prospect, IL 60056-6023 Phone: 708-297-0070 708-699-7864

TRIPLE-OUTPUT CLOCK GENERATORS. The W42C25 single-VCO clock generator from IC Works has three simultaneous clock outputs. It is packaged to take up a minimum amout of space on board-level computers with either Intel X86, Pentium, or RISC microprocessors.



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An included phase-locked loop is said to reduce phase jitter for reference. and it provides two synthesized frequencies. The reference output provides a fixed frequency that matches the frequency of the input frequency or clock. The two synthesized outputs can vary between 2 and 120 MHz, with as many as eight selectable, preprogrammed frequencies stored in an on-chip ROM.

The generator is available in industry-standard, 14-pin, 150-mil-wide plastic SOIC packages and in a 14-pin, 300-mil-wide plastic DIP packages. It can replace high-speed oscillators in computers or other circuits with X86 microprocessors or those that require multiple clock generators.

At 5 volts, typical supply current to the W42C25 is 10 milliamperes. The device is packaged in 14-pin SOIC and 14-pin DIP packages.

In quantities of 1000 or more, the W42C25 is priced at \$1.80 each. IC Works Inc. 3725 North First Street San Jose, CA 95134 Phone: 408-922-0202 Fax: 408-922-0833

SWITCHING MODE DC/DC CONVERTER. The HDB49-C-40 50-watt, switching mode, DC/DC converter from Total Power International has +5.6 and +12volt as well as -12-volt and -5.2-volt outputs. Rated for a maximum of 50 watts, it is adjustable within $\pm 10\%$.

The converter's input voltage is from 35 to 60 volts DC, but is typically 48 volts DC. Load and cross regulation is specified at $\pm 1\%$ on all output terminals. Noise and ripple is 1% peak-to-peak. The converter includes overvoltage, overload, and short-circuit protection.



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The HDB49-C-40 DC/ DC converter is priced at \$99 in hundreds. Total Power International, Inc.

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careers for more than 80 years. Regardless of your previous experience, you can succeed with NRI, too. Experience First-Hand the Intricate **Electronics Inside Today's Computers** You then go on to build a state-of-the-art 486sx/25 MHz Intel-based computer from the keyboard up. You install the power supply, 3.5" floppy drive,

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"No doubt, the excellent back-up of your staff was a significant factor in my swift completion of my microcomputer repair training. Their helpfulness, either by phone or by letter, was nothing short of amazing." J. Preusker, Angston, SA, Australia

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NEW LITERATURE

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Software Development: A How to Digitize Video; by Legal Guide; by Stephen Fishman. Nolo Press, 950 Parker Street, Berkeley, CA 94710: Phone: 510-549-1976; Fax: 510-548-5902; \$44.95, including diskette.

This book, written by a lawyer, provides the guidance that software developers need to protect their intellectual property and be able to profit from it. In addition to offering candid insights on the effectiveness of software patents and trade-secret law, it



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gives the criteria for determining if a certain program is patentable.

Fishman's legal guide explains the strengths and weaknesses of copyrights, trademarks, trade secrets, and patent protection in lay language with a bare minimum of "legalese." It offers advice on the most appropriate protection for intellectual property.

The book also explains how to draft employment, nondisclosure, custom software-publishing, and consulting agreements. Other topics are how to obtain permission to use materials in multimedia projects and how to avoid infringing on the legal rights of others.

Nels Johnson with Fred Gault and Mark Florence. John Wiley & Sons, Inc., 605 Third Avenue, New York, NY 10158-0012; Phone: 1-800-CALL-WILEY; \$39.95 including CD-ROM disc.

This hands-on guide book will inform and guide the reader who wants to learn how to digitize video signals. It will be of value for those with little or no programming or video experience as well as professionals in the field. The text applies to Macintosh as well as IBM or compatible personal computers.

The authors recognize that handling video clips can be tricky because they require special treatment to accommodate their large memory requirements. They want to be sure the reader obtains the best possible playback on screen.



The book explains how to digitize existing videotapes, laserdiscs, and other analog media to create on-screen presentations. It also takes the reader step-by-step from the selection and installation of hardware and software through each phase of video preparation, capture, conversion, storage,

editing, and playback. It even explains the conversion of digital movies back to analog videotape.

The enclosed CD-ROM disk contains OuickTime videos that can be played on computers with Windows (version 3.1) and Macintosh (System 7) computers. The disk's sample movies demonstrate how the choice of window dimensions and frame and audio-sampling rates yields differences in video quality. The disk also includes samples of professionally produced desktop videos.

Behind the Front Panel: The **Design & Development of** 1920's Radios; by David Rutland. Wren Publishers. P. O. Box 1084, Philomath, OR 97370; Phone: 503-929-4498; \$18.95.

This book takes the reader back in radio history to discuss the radio pioneers and their crystal and tube circuit designs that were the cutting edge technology of the day. It explains how the early radios were made and how and why they worked.

Rutland describes vacuum-tube sets made in the 1920's. He has gathered historical information on the products of more than 25 radio manufacturers who were active during that time. The book begins with descriptions of simple crystal radio receivers and goes on to discuss various vacuum-tube regenerative detectors and amplifiers. It ends with a discussion of the superheterodyne circuit still in use.



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The operation of each circuit is explained with the help of simple circuit diagrams and many illustrations. Such venerable devices as tubes, variometers, and variocouplers are described. Circuit diagrams come to life when related to the efforts of the many pioneers who saw the future in reliable, effective radio communications.

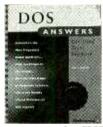
You'll gain insights into the important contributions of such 19th-century scientists as Faraday, Maxwell, and Hertz and see how their work influenced the developments of radio inventors and engineers including Edison, Fleming, DeForest, and Armstrong.

DOS Answers: Certified Tech Support; by Mary Campbell. **Osborne McGraw-Hill, 2600** Tenth Street, Berkeley, CA 94710: Phone: 510-549-6600: Fax: 510-549-6603: \$16.95.

Readers with personal computers that run the DOS operating system will effectively gain 24-hour technical support if they buy this book. It is based on the answers to the most common questions about computers obtained from

Corporate Software Inc., a computer consulting firm that answers 200,000 similar questions on the subject every month.

Every aspect of DOS. from hard-disk setup to updating a previous release is covered in this book. It will help readers perform such tasks as troubleshooting memory and solving file and directory problems, and it explains command syntax and error messages. The book advises on techniques for



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customizing DOS to maximize PC performance. Important topics explained include the DOS Shell, and DoubleSpace batch files.

Opening with a listing of "The Top Ten Tech Errors," the book answers the most common questions on such subjects as setup, file and disk management, utilities, memory, configuration, interoperability, networking, and error messages. An extensive table of contents in question format helps readers find answers in a hurry. Examples are: How can I see if I have any hidden files, and what does the FCBS command in CONFIG. SYS mean?

1994 RF Device Data Book (DL110/D Rev 5). Motorola Inc., Literature Distribution Center, P. O. Box 20924; Phoenix, AZ 85063; Tel:



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800-441-2447; Fax: 602-994-6430; free.

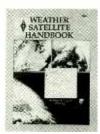
This revised data book presents technical data on Motorola's RF product line. The product families include bipolar, LDMOS, MOSFET RF power, and gallium-arsenide devices packaged in different ceramic and plastic surfacemount cases.

Sufficient information is given on discrete components, hybrid modules, and integrated circuits to permit readers to make the correct selection of Motorola device to meet their specific RF circuit reauirements.

Weather Satellite Handbook: 5th Edition; by Dr. Ralph E. Taggart, WB8DQT. The American Radio Relay League, 225 Main Street, Newington, CT 06111; Phone: 203-666-1541: Fax: 203-665-7531: \$20.00.

This is the fifth edition of a book on weather satellites that was first published in 1976. It introduces the reader to the hobby of receiving weather satellite transmissions directly or indirectly from U.S.and foreign spacecraft-both polar-orbiting and geostationary. Their transmissions can be viewed on a personal computer screen as cloud photographs, and





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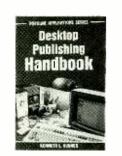
the images can be stored in digital format or reproduced by computer printer or still photography.

This edition has been updated to include information on recent changes and additions to the fleets of satellites that are now operational and whose signals that can be received by amateurs with the proper antenna, receiver, computer, and image reproduction equipment.

The book explains the different kinds of weather satellites now in orbit, how they transmit, their frequencies, and their modes of operation. It also discusses the kinds of images that can be received, and explains how and where to buy or build weather satellite receivers and antennas.

Desktop Publishing Handbook; by Kenneth L. Hughes. Wordware Publishing, Inc., 1506 Capital Avenue, Plano, TX 75074; Phone: 214-423-0090; \$12.95.

This book gives an overview of desktop publishing on IBM and compatible personal computers. Well illustrated, it includes a



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detailed coverage of such subjects as page layout and typography. It offers facts and figures on hardware and guidance on the selection of available applications software to help you get results fast.

Chapters in the book cover the history of desktop publishing, the different kinds of publications, applications programs, and different kinds of personal computers. Video subsystems, input devices, printers and printing, and presentation graphics are discussed.

Third-Party Support Reference Guide: Partnering for Success. Microchip Technology Inc., 2355 West Chandler Blvd., Chandler, AZ 85224-6199; Phone: 602-786-7200; Fax: 602-899-9210.

This 90-page handbook identifies and lists suppliers of software development support, compatible products, and design support for Microchip Technology products. The lists include:



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• 37 third-party software development support suppliers for the company's microcontrollers, application-specific standard products, and memory products.

• Companies that offer programmers, emulators, assemblers, simulators, linkers, compilers, and related accessories.

1994 Supplement C. Jensen Tools Inc., 7815 South 46th Street, Phoenix, AZ

85044-5399; Phone: 800-426-1194; Fax: 602-438-1690; free.

This 68-page catalog lists the latest additions to Jensen's line of personal computer and workstation service products, test equipment, and diagnostics products. Their manufacturers include Wavetek, Datatran, Microhouse, Landmark, Fluke, and Tektronix.



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The new listings include Jensen's universal crimp tool and its 13-piece PC repair kit, Fluke's model 650 Cablemeter, and Tektronix diagnostic tools. Other new products offered are wire and cable connectors, LAN connectivity devices, PC reference guides, soldering and desoldering tools, and ESD-control products.

1994 TEST ACCESSORIES CATALOG. ITT Pomona, 1500 East Ninth Street, Pomona, CA 91766-3835; Phone: 909-469-2900; Fax: 909-629-3317; free.

ITT Pomona has introduced more than 100 new products in its 36-page catalog of test-equipment accessories. Products offered include probes meeting the IEC1010 safety standard and those for oscilloscopes, logic-analyzer accessories, multimeter test leads, and test cable assemblies.



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Other new products described include test clips and adapters for the latest Intel and Motorola microprocessors and microcontrollers, and laboratory power supplies.

1994 Military/Aerospace Reference Manual; Analog Devices Literature Center, 70 Shawmut Road, Canton, MA 02021; Phone: 617-937-1428; Fax: 617-821-4273; free.

This 1,408-page catalog from Analog Devices focuses on products for analog, mixed-signal, and digital signal processing circuitry that are qualified to military and aerospace standards and specifications. Data sheets, selection guides, background information and detailed packaging and ordering information are included.



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Divided into 21 sections, the manual is organized by function. Separate sections present information on such subjects as SMD/ JAN cross references, RADTEST data service and radiation information, and space-qualification. Ω **GET THE LATEST ADVANCES IN ELECTRONICS**

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Electronics Now, September 1994

Modem Communications Standards

Serial communications standards have made worldwide computer communications possible. Here's a look at the latest standards.

STEPHEN J. BIGELOW

WE HAVE NOW BECOME AN "INFORmation society." Low-cost, highspeed personal computersnow in almost every office, school, and home-allow just about everyone to tap into a variety of national information networks. National information networks such as CompuServe and America Online are now serving millions of users. The Internet, a worldwide network of computer networks, is growing at a rate of about 15% per month. There are now more than 40,000 small, private computer bulletin board systems (BBS) within the U.S.

Personal computers, for the most part, are not equipped to connect directly to the national and global information networks. Instead, they must be connected through the public telephone system. However, because the U.S. telephone system is an analog system, computers require a modem (modulator/ demodulator) to translate (or modulate) their digital output into audible sounds that can be sent by telephone lines to a remote location. Those audio signals must then be converted (or demodulated) back into digital information to be "understood" by another computer. This basic concept is illustrated by Fig. 1.

Modems are certainly not new peripherals. They were used with the earliest personal computers. Like PCs themselve modems have evolved through continuous advances in electronics so that they now can pass ever greater volumes of data over a telephone system whose characteristics have barely changed in 100 years.

A result of this constant improvement is a long list of modem specifications with such names as V.32 and V.42bis. This article will give you a basic understanding of modems, their specifications, and it will help help you to understand some of the confusing jargon associated with the latest modems.

The se

he se proach Compaters normally process 16- or 32-bit words of digital information on their internal data buses. Even the computer's parallel printer port offers a data path that is 8 bits wide. However, there is only one transmitting wire in a telephone line. Modems must break down each digital word into a sequence of audio signals, and send each signal in turn along the tele-

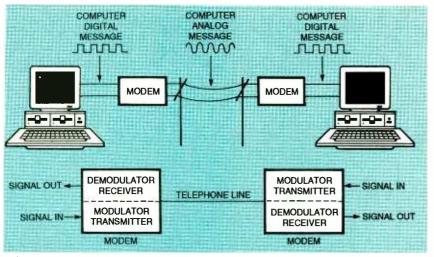


FIG. 1—A MODEM CONVERTS DIGITAL SIGNALS from a computer to analog signals that can be transmitted over telephone lines.

phone wire. An 8-bit data word is sent as eight 1-bit signals.

Most modems for PC communication are asynchronus or unsynchronized. (Synchronous modems are more expensive because they require complex circuitry to keep the receiving modem operating in phase with the transmitting modem for the duration of the transmission.) Because two communicating modems are operating asynchronously, the receiving machine must know when a stream of data is being sent, where each stream of data starts and ends, and whether the stream is correct or not. To accomplish this feat, extra bits are added to the data to organize it into a standard sequence known as a data frame.

A typical serial data frame consists of four parts as shown in Figure 2: the start bit, the data bits, the parity bit, and the stop bit(s). In its idle state, when no data is being sent, a serial-communications signal normally resides in a logic-1 state. The first logic-0 transition is always interpreted as a start bit. The start bit indicates to the receiving modem when the frame's subsequent bits will arrive. It is essential, however, that both modems be operating at the same transfer speed for the transmitted data to be interpreted correctly.

Data bits follow the start bit. There might be from five to eight data bits in the frame. However, 7- or 8-bit data frames are most common for PC communications. As examples, CompuServe data frames have seven data bits, and most BBS facilities (including the *Electronics Now BBS*) are configured for 8-bit data frames. For successful communications, both modems must be set to expect the same number of data bits.

A parity bit might be added to the frame to aid in error detecting. However, because parity checking is ineffective for detecting more than one incorrect bit in a data word, parity is often deactivated (or set to 'none') through communication 'software. When activated, parity is either even or odd.

With even parity, the parity bit will be set (made logic 1) if the number of 1's in the data word is even. With odd parity, the parity bit will be set (made logic 1) if the number of 1's in the data word is odd. The receiving modem calculates parity for the data word and compares it with the received parity bit. If a discrepancy occurs, an error is flagged.

One or two stop bits must be

added to conclude the data frame. One stop bit is typical for most setups since a second stop bit would be redundant. Stop bits are always logic 1's, which leave the system in the idle state to await the next data frame. Both modems must be set to expect the same number of stop bits.

When you want to connect a computer to a BBS or information service, you must configure your system for the correct dataframe format. The most popular frame format is eight data bits, no parity bit, and one stop bit (commonly written 8,N,1). Another popular format is seven data bits, even parity, and one stop bit (7,E,1).

Port Connections and Signals

The translation from parallel data words to a serial data stream takes place within the computer's serial port circuit in an IC known as a universal asynchronous receiver/transmitter (or UART). Logic 1's and O's are converted into bipolar signals. Logic 1's are translated to -5 to -15-volt levels (mark), and logic 0's are tralated to +5to +15-volt levels (space). Those bipolar signals are supplied to the TX (transmit) pin of a standard serial communications port as shown in Fig. 3. Those physical connections are also called RS-232C ports. In Europe, the RS-232C standard is called V.24.

An external modem connected to the serial port modulates the bipolar TX signal into an audio signal which is sent over the telephone line. Audio signals received by the modem and demodulated into bipolar signals are returned to the serial port's RX (receive) pin. An internal modem—that is, a plug-in unit installed inside a

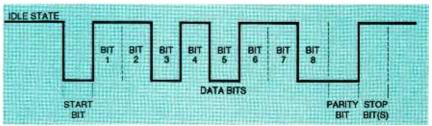


FIGURE 2—A TYPICAL DATA FRAME. This frame is formatted with one start bit, eight data bits, a parity bit, and one stop bit.

computer—contains a serial port on its circuit board. (You might have to disable a serial port in the computer to prevent hardware conflicts with the internal modem's serial port circuit.) For most serial port connections, only TX, RX, and ground wires are needed to establish a working port.

Communications software

Communications software supplies a "front end" for the control of a modem. It helps to remove some of the complexities associated with modem configuration, modem control codes.

One type of communications software is designed for communications with a specific online service. WinCIM, for example, is the Windows version of the CompuServe Information Manager, which is designed specifically to make it easier to "navigate" the CompuServe information service. Such specialpurpose software is outside the scope of this article.

Other communications software is designed for generalpurpose communication. Some popular examples include Procomm Plus, Qmodem, and Crosstalk.

All communications software must be able to operate in two distinct modes: the command mode, and the terminal mode. In the command mode, any commands issued control either the communications software, the host computer, or the modem connected to it. In the terminal mode, any commands issued are sent directly to the modem, or they are sent through the modem and to the remote computer to which it is connected.

Typical instructions that might be issued in the command mode include retrieving a telephone number from a data log, setting the proper communications protocol, dialing a number, and saving any data that is received in a disk file.

In the terminal mode, all keyboard (or disk) input is sent directly to the modem. If the modem is offline or not connected to a remote computer,

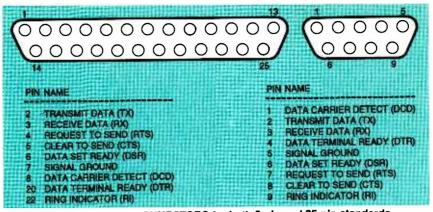


FIGURE 3 - SERIAL PORT CONNECTORS for both 9-pin and 25-pin standards.

the input is recognized as modem commands. If the modem is online and has an active connection to a remote computer, all input is sent through the modem to the remote computer unless certain special control characters precede the data.

The difference between the command mode (in which commands are acted on locally) and terminal mode (in which commands affect the remote computer) is probably the most confusing aspect of modem communications for students and computer beginners.

One common mistake made by newcomers, for example, is to initiate a file transfer in terminal mode without issuing a corresponding command in the command mode. The first command is required to tell the remote computer to send a file. The second is necessary to instruct the host computer to receive it and store it on disk.

Flow control.

To control the flow of data between two modems, software codes (such as XON and XOFF) are passed between them. Communications software interprets such codes and controls modem operation accordingly.

However, the flow of data between a computer and modem is not always controlled by software codes. Instead, additional signal lines in an RS-232 port allow for hardware flow control (or handshaking). The request to send (RTS) line tells a modem to prepare to receive data from the computer. Once the modem is ready to send, it will return a clear to send (CTS) signal to the computer. RTS and CTS signals act together to handle data transfer.

When the computer is ready for operation (but not necessarily ready to send data), it asserts its data terminal ready (DTR) signal. DTR must remain active throughout the entire connection time. The modem sends a data set ready (DSR) signal to the computer after the modem has been activated, and has finished any self-tests or preparation for connection. The DTR and DSR signals establish the connection between modem and computer, but they do not control the flow of data between the two.

If a telephone ring signal is detected at the modem, a ring indicator (RI) signal is sent to the computer. When the modem subsequently picks up the ringing line and detects the presence of carrier, a data carrier detect (DCD) signal is passed to the computer. Ring and carrier detect signals invoke the PC's communication software to receive communication (such as fax messages) from a distant modem.

Modulating the Signals

A modem transmits data by generating a carrier that is then modulated. Several different methods of signal modulation have been developed through the years to improve the efficiency of data transfers. As you might expect, two modems must be capable of the same modulation scheme for successful communications.

Two modems that are commu- 37

nicating with each other must generate different carrier frequencies. Each communication standard defines the transmitting and receiving carrier frequency. For example, for 300baud communication, one modem must have a carrier center frequency of 1170 Hz, and the second must have a center frequency of 2125 Hz. By convention, the modem initiating the call, or the originate-mode modem, has the lower carrier frequency. The modem receiving the call, or the answer-mode modem, has the higher carrier frequency.

In the early days of modem communication, each transition of the audio carrier signal represented a single bit. Each transition is known as a baud, so the baud rate equaled the transmission rate in bits-persecond or bps. Unlike those early modems, modern modem schemes allow two, three, four, or more bits to be encoded into every audio signal transition (or baud). This means that modem throughput now equals two, three, or four times the baud rate being carried on the telephone line.

For example, a modem operating at 2400 baud (2400 audio signal transitions per second) can carry 4800 bps if two bits are encoded onto every baud. The same 2400 baud modem can carry 9600 bps if 4 bits are encoded onto every baud. Today, the modem's baud rate rarely matches the modem's bit rate in bps. If the modem were operating at 4800 baud with 3-bit encoding, it would be transmitting 14,400 bps (14.4 kbps), and so on.

The concept of encoding is different from data compression: Encoding transfers all original data bits from one system to another, while data compression replaces repeating sequences of bits with much shorter bit sequences (known as symbols or tokens). Encoding schemes and data compression are described in more detail later in this article.

Modulation Schemes

All waveforms have three

MODEM GLOSSARY

Answer mode—The operating state of a modem that is expecting a call from another computer. (The modem is in its originate mode when calling another computer.) The modem transmits at the defined high frequency of the communications channel, and receives at the defined low frequency.

Asynchronous data transmission— Data transmission between computers in which each data group contains its own start and stop bits to indicate the beginning and end of each character, and there is no control over the time between characters.

AT Command Set—The set of industrystandard commands for the control of a modem. Each command line must start with the two-character attention code AT (or at).

Attention code—A two-character sequence (AT or at) that signals a modem that one or more modem commands are to follow.

Auto answer—A feature that enables a modem to answer the phone automatically after a preset number of rings.

Auto dial—A modem feature that allows it to automatically dial a telephone number.

Auto-reliable mode—A feature that allows two modems to "negotiate" with each other to determine whether they can use error control and data compression during a transmission.

Baud rate—The number of audio transitions transmitted by the modem each second. This usually not the same as the bit rate (or bits-per-second) rate, because a given baud may have more than one bit encoded into it.

Bits-per-second (bps)—The speed at which a modem sends or receives information. For example, a modem that operates at 2400 bits per second can transfer 2400 binary digits each second.

Buffer—In a modem, a storage location in an internal RAM where data is temporarily stored until the modem can process the data.

Carrier—The continuous base signal generated by a modem. The modem modulates this signal (alters its frequency or phase) to encode the data bits to be transmitted.

CCITT—International Telegraph and Telephone Consultative Committee. See ITU.

basic characteristics: amplitude, frequency, and phase. Each of those characteristics can be adjusted to represent a bit.

Frequency-shift keying (FSK)

Clear to Send (CTS)—An RS-232C signal that tells the computer it can start sending information.

Command mode—One of two operating modes for a modem, also called local mode. In its command mode, a modem interprets any information it receives from the local computer as modem commands. It tries to perform the commands sent to it, and it returns result codes indicating the results of the commands.

Communications software—A program that provides an interface for the control of a modem's functions. Examples of communications programs are Smartcom, Procomm, and Crosstalk.

Configuration profile—The present operating characteristics of a modem, stored in the modem's S-registers. Whenever a modem command is issued to change one of the operational characteristics (such as setting the volume control or turning the speaker on or off), the modem changes the values in the Sregisters to reflect the changes.

Data Carrier Detect (DCD)—An RS-232C signal that indicates when the modem is receiving a carrier signal from a remote modem.

Data Set Ready (DSR)—An RS-232C signal that tells the computer that the modem is connected to the telephone line.

Data Terminal Ready (DTR)—An RS-232C signal that tells the modem that the local computer is ready for data transmission.

Duplex—See definitions half duplex and full duplex.

Escape sequence—A sequence of three characters (normally +) that switch a modem from the on-line mode to the command mode without breaking the telephone connection.

File transfer protocol—An errorchecking protocol for file transfers (such as KERMIT, XMODEM, or YMODEM). The protocol monitors information sent with each block of data. If the received data doesn't match the information used to check the quality of data, the system notifies the sender that an error has occurred and asks for a retransmission.

Flow control—The mechanism that regulates the flow of data between two devices. Modems typically have two methods of flow control: software flow control (XON/XOFF) and hardware flow control (CTS/RTS).

is similar to frequency modulation (FM) where only the frequency of a carrier is changed, and it is one of the oldest modulation schemes still in use. FSK sends a logic 1 as one particular LAPM (link access procedure for modems)—An error control protocol specified by CCITT V.42. LAPM provides error control when one modem is communicating with another modem that supports LAPM.

Line noise—Random signal disturbances that can occur over telephone lines. Noise can disrupt communications and corrupt the transmitted data.

Loopback test—A diagnostic test in which characters that are sent to the modem are immediately sent back from the modem so the computer can compare the characters sent with the characters received.

MNP (Microcom networking protocol)—Provides error control and data compression when one modem is communicating with another modem that supports MNP. (MNP classes 1 through 4 are specified by CCITT V.42 as a backup error-control scheme for LAPM.)

Nonvolatile memory (NVRAM)—Solid-state random-access memory that retains the information stored in it even if its power is removed. NVRAM in modems stores configuration information.

On-line mode—One of the two operating modes of the modem, also called data mode. (The other is command mode). In on-line mode, the modem interprets all information sent to it as data, not commands. The only exception is the escape sequence (normally +), which returns the modem to command mode without breaking the connection. The modem is placed in on-line mode when it makes a connection with a remote modem, or when a command is entered to return to a previously established connection.

Originate mode—The state of a modem that is initiating a call to another computer. (The modem is in its answer mode when expecting a call from another computer.) The modem transmits at the defined low frequency of the communications channel, and it receives at the defined high frequency.

Parity—A data-encoding scheme used in computers for checking the validity of transmitted data. This scheme adds an extra bit to each data word, which the transmitting computer selects based on the type of parity the computers agree to use (odd or even). The receiving computer checks each character and flags a parity error if any character has the incorrect number of bits set.

frequency (usually 1750 Hz), and a logic 0 is sent as another discrete frequency (often 1080 Hz). Frequencies are typically sent at 300 baud, and each baud can carry one bit, so FSK **Protocol**—A set of rules that governs how data is transmitted. To communicate successfully, two computers must use the same protocol.

Request to Send (RTS)—An RS-232C signal that requests that the modem send data. It initiates all data transmission between the computer (or terminal) and the modem. RTS is answered by a Clear to Send (CTS) signal.

Result codes The message sent by a modem after it receives a command.

RS-232C—A standardized system for connecting a device to the serial port of a computer or terminal. It is the recommended standard of the Electronic Industries Association (EIA) for exchanging information between data terminal equipment (such as computers) and data communications equipment (such as modems).

S-registers—NVRAM in a modem that stores the current configuration profile (operating characteristics).

Serial port—The circuits and connector that permit a computer to communicate with serial devices such as printers, modems, plotters, and mice. It is also called a COM or communications port.

Start/stop bits—The bits that identify the beginning and end of an data frame in asynchronous data transmission.

Throughput—The total useful information processed or communicated over a specified amount of time. Data compression increases the throughput of a modem by allowing it to send more information in the same number of bits.

Tone dialing—One of two methods for dialing the telephone. With tone dialing, the modem sends standard Touch Tones. Tone dialing is also called dualtone multi-frequency (DTMF) dialing.

XON/XOFF—A protocol for controlling the flow of data between a modem and its host computer and between two modems (also called software flow control). If the modem receiving data needs time to process the data or perform some other task, it sends an XOFF signal to the sending modem. The sending modem then waits until it receives an XON signal before sending more data. A <CTRL>-S character is usually interpreted as the XOFF command, while XON is usually either a <CTRO>-Q or any character following <CTRL>-S.

can send 300 bps. This early technique resulted in the classical "baud equals bps" confusion which still exists today.

Phase-shift keying (PSK) is a close cousin of FSK, but the

phase timing of a carrier wave is altered while the carrier's frequency stays the same. A logic 1 or logic 0 is represented by the alteration of the carrier's phase. Because phase can be shifted in several precise increments (for example, 0, 90, 180, and 270 degrees), PSK can encode one, two, three, or more bits bit per baud. A 1200-baud modem using PSK can transmit 2400 bps over an 1800-Hz carrier. PSK in conjunction with FSK can encode even more bits per baud.

In quadrature-amplitude modulation (QAM), both the phase and amplitude of the wave are modulated to encode up to six bits onto every baud, although only four bits are usually reserved for data. Most QAM modems have a 1700-Hz or 1800-Hz carrier and a base rate of 2400 baud, so they can carry up to 9600 bps.

Trellis-coded quadrature-amplitude modulation (TCQAM or TCM) also generates an 1800-Hz carrier at a 2400-baud base rate, but it uses the full 6-bit encoding capability of QAM to provide a rate of 14400 bps. TCM is now the most popular modulation scheme for highperformance modems because data can be checked on-the-fly with high reliability.

Signaling Standards

Most of the present computer communications standards have been developed through international cooperation by the ITU or International Telecommunications Union (formally the CCITT). The ITU sets data communication standards for the world. Its members include the major modem manufacturers, common telecommunication carriers, and government officials.

ITU specifications are characterized by the letter V. The V simply means standard (something like the RS in RS-232). The number following denotes the particular standard. Some standards also add the term "bis" which indicates the second version of a particular standard. You might also see the term "terbo" which is the third

4

V.1—A very early standard that defines binary digits as space/mark line conditions and voltage levels.

V.2—Limits the audio power levels of modems used on phone lines.

V.4-Describes the data frame.

V.5—Describes the standard synchronous signaling rates for dialup lines.

 $\pmb{\textbf{V.6-}}\xspace$ Describes the standard synchronous signaling rates for leased lines.

V.7—Provides a list of modern terms in English, Spanish, and French.

V.10—Describes unbalanced highspeed electrical interface characteristics (RS-423)

V.11—Describes balanced high-speed electrical characteristics (RS-422)

V.14—Explains the standard procedure for asynchronous to synchronous conversion.

V.15—Describes the requirements and designs for telephone acoustic couplers. This is rarely used today because most telephone equipment is modular and can be plugged into telephone adapters directly rather than be loosely coupled to the telephone handset.

V.17—Describes an application-specific modulation scheme for Group 3 fax which provides two-wire, half-duplex, trellis-coded transmission at 7200, 9600, 12000, and 14400 bps. Despite its low number, this is a recently introduced standard.

V.19—Describes early DTMF modems for low-speed parallel transmission. This standard is essentially obsolete.

V.21—Provides the specifications for 300 bps FSK serial modems (based on BELL103).

V.22—Provides the specifications for 1200 bps (600 baud) PSK modems (based upon BELL212A).

V.22bis—Describes 2400 bps modems operating at 600 baud with QAM.

V.23—Describes the operation of an unusual FM modem operating at 1200/75 bps. The host transmits at 1200 bps and receives at 75 bps, while the remote modem transmits at 75 bps and receives at 1200 bps. In Europe, V.23 supports some videotext applications.

V.24—This is known as EIA RS-232C in the U.S. V.24 defines only the functions of the serial port circuits. EIA-232E (the

version of a standard.

The Bell System largely dictated North American telecommunications standards before it was broken up into AT&T and

TABLE 1-ITU STANDARDS

current version) also defines electrical characteristics and connectors.

V.25—Defines automatic answering equipment and parallel automatic dialing. It also defines the answer tone that modems send.

V.25bis—Defines serial automatic calling and answering, which is the ITU (CCITT) equivalent of AT commands. This is the current ITU standard for modem control by computers via serial interface. The Hayes AT command set is used primarily in the US.

V.26—Defines a 2400-bps, PSK, fullduplex modem operating at 1200 baud.

V.26bis—Defines a 2400-bps, PSK, half-duplex modem operating at 1200 baud.

V.26terbo—Defines a switchable 2400/1200-bps, PSK, full-duplex modem operating at 1200 baud.

V.27— Defines a 4800-bps, PSK modem operating at 1600 baud.

V.27bis—Defines a more advanced 4800/2400-bps, PSK modem operating at 1600/1200 baud.

V.27terbo—Defines a 4800/2400-bps, PSK modem commonly used in halfduplex mode at 1600/1200 baud to handle Group 3 fax rather than computer modems.

V.28—Defines the electrical characteristics and connections for V.24 (RS-232). Where the RS-232 specification defines all necessary parameters, the ITU breaks the specifications down into two separate documents.

V.29—Defines a 9600/7200/4800-bps, PSK/QAM modem operating at 2400 baud. This type of modem often implements Group 3 fax rather than computer communications.

V.32—Defines the first of the truly modern modems as a 9600/4800-bps, QAM, full-duplex modem operating at 2400 baud. This standard also incorporates trellis coding and echo cancellation to produce a stable, reliable, high-speed modem.

V.32bis—A fairly new standard extending the V.32 specification to define a 4800/7200/9600/12000/14400 bps TC-QAM full-duplex modem operating at 2400 baud. Trellis coding, automatic transfer rate negotiation, and echo cancellation make this type of modem one of the most popular and least expensive for general PC communication.

seven regional telephone operating companies in 1984. Before that time, two major standards had been developed that set the stage for future V.32terbo—Continues to extend the V.32 specification by adding advanced techniques to implement a 14400/16800/19200-bps, TCQAM, fullduplex modem operating at 2400 baud. Unlike V.32bis, V.32terbo is not widely popular because of the high cost of compatible components.

V.32fast—The informal name for a standard that the ITU has not yet completed. When finished, a V.32fast modem will probably replace V.32bis with speeds up to 28,800 bps. It is anticipated that this will be the last analog protocol, eventually giving way to all-digital protocols as local telephone systems become entirely digital. It is expected that V.32fast will be renamed V.34 on completion and acceptance.

V.33—Defines a specialized 14400-bps, TCQAM, full-duplex modem operating at 2400 baud.

V.34—The ratified version of V.32fast. It provides for data speeds up to 128 kbps with transmission rates as high as 3429 baud.

V.36—Defines a specialized 48000-bps "group" modem that is rarely used commercially. This type of modem requires several conventional telephone lines.

V.42—Defines a two-stage process of detection and negotiation for LAPM error control.

V.42bis—Extends the V.42 standard to include data compression.

V.50—Sets standard telephony limits for modem transmission guality.

V.51—Outlines required maintenance of international data circuits.

V.52—Describes apparatus for measuring data transmission distortion and error rates.

V.53—Outlines impairment limits for data circuits.

V.54—Describes loop-test devices for modem testing.

V.55—Describes impulse-noise measuring equipment for line testing.

V.56—Outlines the comparative testing of modems.

V.57—Describes the comprehensive test equipment required for high-speed data transmission.

V.100—Describes the interconnection techniques between PDNs (public data networks) and PSTNs (public switched telephone networks).

modem development.

BELL103 was the first widely accepted modem standard simple FSK modulation at 300 baud. This is the only standard in which the data rate matches the baud rate. It is interesting to note that many modems today still support BELL103 as the lowest common denominator when all other modulation techniques fail.

BELL212A was a second widely accepted modem standard in North America based on PSK modulation at 600 baud to transmit 1200 bps. Many European countries ignored BELL212A in favor of the similar (but not entirely identical) European standard called V.22.

ITU Standards

After the Bell System breakup, AT&T no longer wielded enough clout to dictate standards in North America-and certainly not to the international community which had developed serious computing interests. At this time, the ITU gained prominence and acceptance in the U.S. All U.S. modems have been built to ITU standards ever since. Table 1 provides a comprehensive description of ITU standards. Although not all of the listed standards relate specifically to modems, all are related to communications. Table 1 will help you to understand the broad specifications that are required to fully characterize the communications environment.

MNP Standards

The Microcom networking protocol (MNP) is a complete hierarchy of standards developed during the mid 1980s. They were designed to work with other modem technologies to provide error correction and data compression. Originally developed by Microcom, Inc., the protocol is now in the public domain.

MNP provides error control and data compression when one modem is communicating with another modem that supports MNP. MNP class 4 is specified by ITU V.42 as a backup error control scheme for LAPM in the event that V.24 cannot be invoked. Out of nine MNP levels, most modern modems support the first five. Each MNP class has all the features of the pre-

| ູ່ 📜 🕺 🕇 | ABLE 2-MODEM | STANDARDS COMP | ARISON CI | |
|--|--|--|------------------------------|--|
| Standard | Data Rate (bps) | Modulation Technique | Baud Rate (baud) | |
| Bell 103 Bell 212A V.17 V.21 V.22bis V.23 V.26 V.26bis V.26terbo V.27 V.27bis V.27terbo V.29 V.32 V.32bis V.32terbo V.32fast V.33 V.36 V.37 | 300 1200 7200-14400 300 2400 1200/75 2400 2400/120 4800 PSK 4800/2400 9600/7200/4800 9600/4800 4800-14400 14400-19200 to 28800 14400 48000 72000 | FSK PSK QAM FSK QAM FM PSK (full-duplex_ PSK (half-duplex) PSK (full-duplex) PSK 1600/1200 PSK PSK/QAM QAM TCQAM TCQAM TCQAM TCQAM TCQAM Group-line modem Group-line modem | 1200 1200 1200 1600 | (Bell 103) (Bell 212A)) & 450/390 (Group 3 fax) (Group 3 fax) |

vious class plus its own.

MNP class 1 (block mode): Data is sent in one direction at a time. It is about 70% as fast as data transmissions with no error correction. This level is now virtually obsolete.

MNP class 2 (stream mode): Data is sent in both directions at the same time. That results in a speed about 84% as fast as data transmissions with no error correction.

MNP class 3: The sending modem strips the start and stop bits from a data block before sending it. The receiving modem then adds start and stop bits before passing the data to the receiving computer. It is about 8% faster than data transmissions with no error correction.

MNP class 4: A protocol (with some data compression) that checks telephone connection quality and uses adaptive packet assembly. On a noisefree line, the modem sends larger blocks of data. If the line is noisy, the modem sends smaller blocks of data so that less data must be resent in the event of an error.

MNP class 5: Provides data compression by detecting redundant data and recoding it to fewer bits, thus increasing effective data throughput. A receiving modem decompresses the data before passing it to the receiving computer. MNP5 can speed data transmissions by as much as a factor of two compared with protocols having no data compression or error correction scheme.

MNP class 6: Universal link negotiation allows modems to obtain maximum performance from a line. The modems start at low speeds, then move to higher speeds until the best speed that both modems can work at is found.

MNP class 7: It offers a more powerful data compression process (Huffman encoding) then MNP5. MNP7 modems can increase the data throughput by as much as a factor of three.

MNP class 8: There is no MNP8 at this time.

MNP class 9: It reduces the data overhead encountered with each data packet. MNP9 also improves error correction performance because only the erroneous data must be re-sent instead of re-sending the entire data packet.

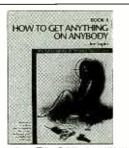
MNP class 10: It includes a set of protocols known as *adverse channel enhancements* to help modems overcome poor telephone connections by adjusting data packet size and transmission speed until the most reliable transmission is established.

Electronics, mini-ADS



CRYSTAL-CONTROLLED! 5 MINUTE AS-SEMBLY! MONEYBACK GUARANTEE! Attach 3 wires and hear every whisper up to 2 miles away on any programmable scanner or VHF surveillance receiver. Pre-tested surface mount module uses standard 9V battery for 100mW output! Includes battery box and crystal for 140MHZ. Custom frequencies available for Law Enforcement. Model VX-100 only \$79.95 + 2.00 S&H. VISA, MC, MO. COD add \$5.00. DECO INDUSTRIES, BOX 607, BEDFORD HILLS, NY 10507. 914-232-3878.

CIRCLE 127 ON FREE INFORMATION CARD



BOOK II HOW TO GET ANYTHING ON ANYBODY—Lee Lapin! ©utting edge audio/ video surveillance, read computers, bypass passwords, see in the dark, obtain unlisted phone numbers, intercept cellular calls, pagers, and faxes, trace and track anybody, surveillance proof any room, tap any phone, WHEW! "Really scary stuff"—CNN. \$34.95 + \$5.00 shipping, INTELLIGENCE INCOR-PORATED, 2228 EI Camino Real, #349-2, San Mateo, CA 94103. 1-800-805-5544 orders only.

CIRCLE 184 ON FREE INFORMATION CARD



AAFFORDABLE LABORATORY POWER SUPPLIES. Direct keyboard data entry for Voltage and current settings—or slew up/ down to sweep outputs. DC enable/disable control. Large LED readouts. RS232 is standard. Program Voltage with your PC and read back the current. Free communications software provided. Models from 12.5V to 125V; 75 Watts. \$429.00–\$449. MC, VISA, and AMEX are OK. KEPCO INC., Dept. MXS-87, Flushing, NY 11352. 718-461-7000; FAX: 718-767-1102.

CIRCLE 190 ON FREE INFORMATION CARD

Data Compression Standards

Most data sent between modems contains some repetitive or redundant information. If the redundant information is replaced by a small "token" during transmission, the data can be compressed.

Data compression has become an important technique that allows modems to increase their data throughput without increasing the baud or bit rate. Data compression can occur only when the two communicating modems support the same compression protocol.

MNP class 5: This standard includes data-compression algorithms that provide up to 2:1 data compression. In effect, MNP5 can give a 2400-bps modem an effective data throughput of as much as 4800 bps; it can give 9600-bps system as much as 19,200 bps.

MNP class 7: Huffman encoding provides a data-compression ratio of up to 3:1. Although it is more efficient than MNP5, not all modems are compatible with it. MNP7 is still generally slower than the ITU's V.42bis.

V.42bis: This standad is a Lempel-Ziv-based data compression scheme for use in conjunction with V.42 LAPM (error correction). V.42bis can compress data by as much as 4:1 (depending on the file sent). Thus, a 9600-baud modem can transmit data at up to 38,400 bps using V.42bis. A 14.4 kbps modem can transmit up to a startling 57,600 bps.

Error Control/Correction Standards

Modem error correction is the ability of some modems to detect data errors that might have occurred in transit between modems, then automatically resend the faulty data until a correct copy is received. As with modulation standards, both modems must be using the same error correction standard to operate together. However, there are few error correction standards, and most modem manufacturers adhere closely to the few that are available.

MNP class 4 is a Microcom error correction protocol (with

some data compression) that checks the quality of the telephone connection and adjusts information in the headers of data blocks using a technique called adaptive packet assembly. If the telephone line is relatively noise-free, the modem sends larger blocks of data to increase throughput. If the telephone line is noisy, the modem sends smaller blocks of data so that less data will have to be resent. This means more successful transmissions on the first try. Because it is about 20% faster than data transmissions using no error correction at all, most modems are now MNP4 compatible.

V.42 is the only ITU error correcting procedure for modems that includes the V.22, V.22bis, V.26ter, V.32, and V.32bis protocols. The standard is also defined as the link access procedure for modems (LAPM) protocol. ITU V.42 is considered very efficient, and is about 20% faster than MNP4. If a V.42 connection can't be established between modems, V.42 automatically provides fallback to MNP4 error correction.

Fax modems

A fax modem is a modem that is capable of sending and receiving faxes as well as data. Virtually all fax modems are compatible with the ITU Group 3 standard. The basic operating principles are similar for modems and fax modems. The data that is transmitted, however, represents picture elements or *pels* instead of pure data.

Communications software that is designed to work with fax modems makes it possible to fax documents created in a word processor without the interim step of printing. Faxes that are received can be converted into a text file (rather than graphic image) with character-recognition software.

Computer communication has come a long way in the last decade. From their humble beginnings of 300 bps, today's modems can effectively and reliably pass the equivalent of 57,600 bps using error correction and data compression. Ω WARNING: The publisher makes no representations as to the legality of constructing and/or using the Telemike telephone security device referred to in this article. The construction and/or use of the device described in this article may violate federal and/or state law. Readers are advised to obtain independent advice as to the propriety of its construction and the use thereof, based upon their individual circumstances and iurisdictions.

TELEPHONE LINE GRABBER

This listening circuit can be called from a remote phone so you can intercept phone conversations or monitor room activities

TELEMIKE IS A TELEPHONE CIRCUIT that, when located in a room miles away, permits you to listen in on the activities that are taking place in that room. It also permits you to listen to or interrupt a conversation on a separate phone line located wherever Telemike can gain access to it.

Telemike contains a sensitive microphone which is activated

ROBERT IANNNINI

by calling the telephone number assigned to the outlet where it is plugged in and entering a code. It also contains circuitry that will permit it to access a telephone on a separate line terminating in the same room or even at the place where the phone line enters the home or building. Sequential pressing of the pound (#) key cycles the circuit to the next mode, that of intercepting a second telephone line and the third mode that resets the circuit after it has been in either of its listening modes. The "called to" telephone can

The "called to" telephone can be miles away, in the same home or building as Telemike, or anywhere Telemike can gain ac-

cess to the "called from " number. The Telemike circuit can be located anywhere in the room where the "called to" phone jack is located or at the entry point of the phone line conspicuous or inconspicuous.

Figure 1 gives the number of times the pound (#) key must be pressed in sequence to initiate Telemike's two operating modes. It also shows the third key pressing needed in sequence to terminate the first two modes so the "called to phone" is not left "off hook."

In the listen mode 1, you can listen to conversations, music, security alarms, the sound of essential building service machinery, or even the sounds of intruders. To make use of the intercept phone conversation mode 2, you must have access to its phone wires or jack for plugging in the second plug from Telemike. The circuit forms a "bridge" between the two lines. Then by keying the pound (#) key twice, you will be on line with both parties of the intercepted phone line.

If you own your own business or vacation cottage that is located some distance from your home, or if you are away from your own home, an installed Telemike will let you find out if a security alarm is sounding, an essential heater or pump is working, or if unwanted persons are present in the room. It could also be useful in unobtrusive monitoring of a bed-ridden patient or child, a teenagers rock and roll party or a romantic adventure in progress.

The intercept phone conversation mode will permit you to interrupt a call in progress to announce a call waiting, emergency, or some other event from wherever you are located—in the house or miles away.

Adaptation required

Telemike was designed to be compatible with the AT&T Corporation's ESS electronic switching system. Consequently, there might be differences in its performance if it is installed in a telephone operating system based on a different design.

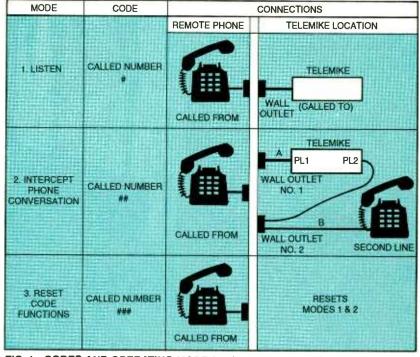


FIG. 1—CODES AND OPERATING MODE for the Telemike telephone line monitor.

This article does not provide details for packaging the Telemike circuitry. However, the circuit can be housed in any suitable metal or plastic project case with provision for mounting the on-off switch on the outside, a battery pack inside, and openings for the phone cords.

Circuit function

Refer to the schematic Fig. 2. Six volts DC is applied to the circuit by switching S1 on. With this voltage applied, the 555 timer IC3 momentarily holds a high and resets NAND gate IC4a to zero, "priming" the circuit.

To initiate the *listen* mode 1, call the number of the "called to" telephone line that is connected to plug PL1. A negative ring signal triggers 555 timer IC1, causing transistor Q1 to conduct. That sends current through the coil of reed relay RY1 and closes its contacts, connecting transformer T1 to the telephone line.

A tone signal initiated by pressing the pound (#) key of the "called from" phone immediately after you have keyed in the "called to" telephone initiates a response after Telemike has been primed. The tone is decoded by dual-tone multiple frequency DTMF filter/decoder MC145436 IC2. It is a silicongate CMOS LSI IC containing the filter and decoder for the detection of a pair of tones conforming to the DTMF standard.

The output of IC1 indexes the CD4017 decade counter IC5 to the logic 1-state, latching transistor Q1 ON. This response then turns on the 741 operational amplifier IC6.

Any sounds in the room where Telemike is located are picked up by microphone MIC1, amplified, and fed back through transformer T2 to transformer T1 from which they are sent over the phone lines. A person listening on the "called from" phone can then hear any sounds or voice within the range of the microphone. This is the *listen* mode.

The Telemike circuit can be switched to the *intercept phone conversation* mode by pressing the pound (#) key a second time. This sequence connects the "called from" phone through the to the second phone line through plug PL2 of Telemike. This permits any conversation on the second line to be interrupted or monitored from the "called from" phone.

A second pressing of the pound (#) key causes decade counter IC5 to index its count to mode 2. That sets pin 4 high which holds Q2 in a conducting state, energizing relay RY2 and closing its contacts. This connects transformer T1 to plug PL2, the connection to the "called to" phone.

Any audible signals at plug PL2 are now connected by the telephone line at plug PL1, allowing you at the "called from" phone to interrupt a conversation on that line or just listen. Complete DC isolation between the two telephones connected to plugs PL1 and PL2 is achieved by the isolated contacts of relay RY1.

The third reset code functions mode is achieved by pressing the pound (#) of the "called from" phone a third time. This indexes decade counter IC4 and turns off Q2 and all other functions, restoring normal telephone operation. Diode D14, connected across RY1's coil, clips the inductive pulse that occurs when relay RY2 is turned off. *Caution*: the "terminate function" must be keyed in before hanging up the "called from" phone or the "called to" telephone might remain offhook. The telephone company will terminate service if it is not corrected within a reasonable length of time.

If you fail to rest Telemike properly before hanging up the "called from" phone, you must reset the circuit manually by going to it and turning it off and on again. This is an obvious inconvenience if you are miles away from the "called to" telephone or its jack.

To make the most effective use of all of the three modes of Telemike, you should subscribe to a dedicated telephone line. (about \$15 per month in most locations).

It is important that *initial access time* be selected properly if you intend to use only a single line. This will be discussed later in this article.

Circuit construction

Refer to the schematic Fig. 2 and the parts placement diagram Fig. 3. The components of the prototype circuit were wired point-to-point on a rectangular piece of perforated board measuring $6\frac{1}{4} \times 4\frac{1}{2}$

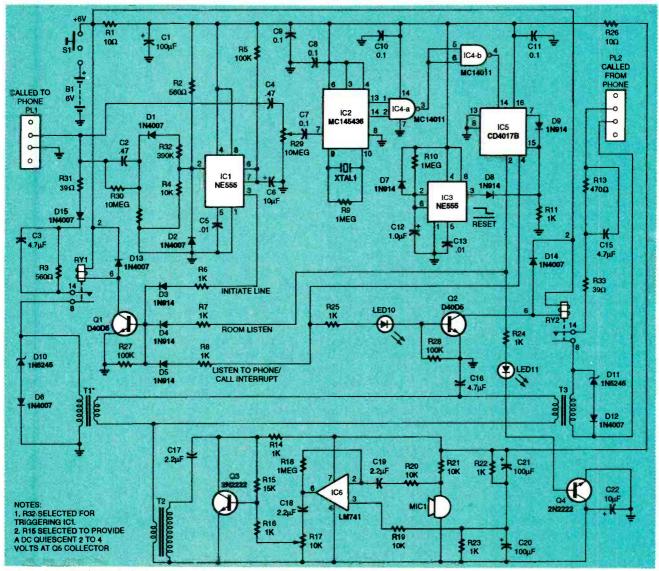


FIG. 2—SCHEMATIC FOR TELEMIKE. All of the integrated circuits and reed relays are inserted in DIP sockets.

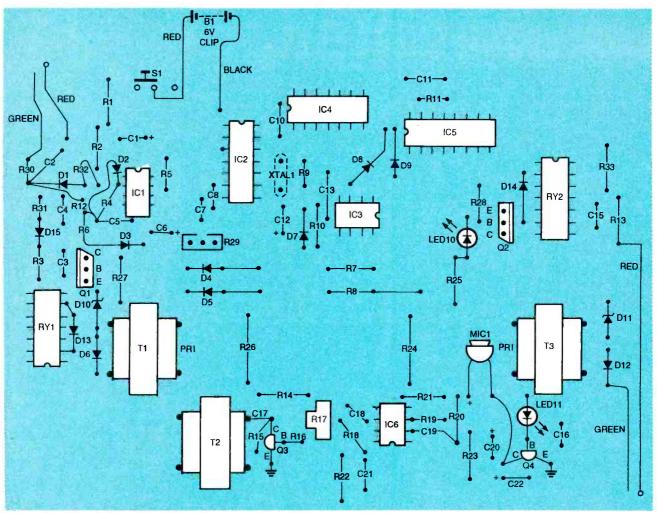


FIG. 3—PARTS PLACEMENT DIAGRAM. The entire circuit fits on a $5\% \times 4$ -inch perforated circuit board. The components are interconnected by point-to-point wiring and power and ground bus wires. Switch S1 can be mounted off the board.

inches with 0.42-inch prepunched holes in a standard 0.1-inch grid.

The component positioning shown in Fig. 3 generally follows that shown in Fig. 2. The component spacing was selected to minimize the length of interconnecting wires without unnecessarily cramping the space between components. This would make the soldering operation more difficult. There are no critical component relationships in this circuit that dictate either close spacing of specific components or isolation between them.

If you want to construct the circuit on a smaller board to fit in a smaller case, you can reduce the spacing between components. However, it is recommended that component orientation remain the same. Identify all components and set them out on a table as shown in Fig. 3. Start by positioning the seven IC sockets (for ICs and reed relays) on the board with the approximate spacing shown in Fig. 3. Place a drop of fast-drying glue under each socket to hold it in position on the board.

The circuit has three identical isolation/impedance-matching transformers T1, T2, and T3. They are rated for a primary impedance of 600 ohms and a secondary impedance of 1200 ohms at 1000 Hz. Measure the DC resistance of the windings with an ohmmeter to verify the continuity of the windings, and confirm the markings for the primary and secondary sides.

The 600-ohm secondary turns should have an approximate DC resistance of 50 ohms, and the 1200-ohm primary turns should have a DC resistance of about 75 ohms.

Insert the transformers in the board in the correct orientation, being careful not to stress the pins because that might break the winding connections, destroying the transformer.

Start inserting all passive components from left to right across the board in small clusters, noting the polarity and orientation of all diodes and polarized capacitors. (Suggestion: position some of the resistors vertically to conserve circuit board space.)

Temporarily fold the leads of all inserted components back flush with the solder side of the board so they will not fall out when the board is handled. Do not trim the leads at this time. Certain component leads will connect with adjacent component leads as part of the complete circuit.

Solder the leads of the components that have been inserted in small groups before proceeding with the next group. Form the power and ground buses from bare copper wire, and solder them as shown in Fig. 3.

Solder in the clip for the fourcell battery pack, with the red wire to plus (+) and black wire to negative (-).

Strip back the jacketing from both ends of the telephone cords to expose the multicolored wires. Strip back the insulation from the red and green wires and solder them to the proper locations on the circuit board, as shown in Fig. 3. The red wires go to the ground bus and the green wires go to the input points. Trim off the other

PARTS LIST

- All resistors are ¼-watt, 10%, unless otherwise specified.
- R1, R26-10 ohms R2, R4, R19, R20, R21-10,000
- ohms
- R3-100 ohms
- R5, R12, R27, R28-100,000 ohms
- R6, R7, R8, R11, R14, R16, R22, R23, R24, R25-1000 ohms
- R9, R10, R18-1 megohm
- R13-470 ohms
- R15-15,000 ohms
- R17, R29-10 kilohms trimmer potentiometer, PCB mount
- R30-10 megohms
- R31, R33-39 ohms
- R32-390,000 ohms
- Capacitors
- C1, C20, C21-100 µF, 25 volts, aluminum electrolytic, radial
- C2-0.47 µF, 100 volts, polyester
- C3, C15, C16-4.7µF, 100 volts, non-polarized aluminum electrolytic
- C4-0.47 µF, 50 volts, film
- C5, C13—0.01 μF ceramic disk C6, C22—10 μF 25 volts, aluminum electrolytic, radial lead
- C14-deleted
- C7, C8, C9, C10, C11-0.1µF, 25volts, ceramic disk
- C12-1 µF, 25 volts, aluminum electrolytic, radial leaded
- C17, C18, C19-2.2 µF, 25 volts, non-polarized, aluminum electrolytic, radial leaded

Semiconductors

- D1, D2, D6, D12, D13, D14, D15-1N4007 silicon rectifier diode
- D3, D4, D5, D7, D8, D9-1N914silicon signal diode
- D10, D11-1N5245, 16 volts, Zener
- LED10, LED11—light-emitting diodes, red, T-13/4 (optional, see text)
- IC1, IC3-NE555N, Philips or eauiv.
- IC2-MC145436P, dual-tone multiple frequency receiver, Motorola or equiv.
- IC4-MC14011BCP, NAND gate, Harris or equiv.

- IC5-CD4017B decode counter, Harris or equiv.
- IC6-LM741CN operational amplifier, DIP package, National or equiv.
- Q1, Q2-D40D5, NPN power transistor, TO-220 package, Harris or equiv.
- Q3, Q4-2N2222 NPN transistor Other components
- MIC1-microphone, omnidirectional, electret, 20 to 15,000 Hz, Radio Shack 270-090 or equiv.
- PL1, PL2-RJ-11 modular telephone plugs
- RY1, RY2-relay, 1 form A SPST NO DIP reed, Mouser D31A310
- S1-slide switch, SPST, Radio Shack 275-401 or equiv.
- T1, T2, T3-transformer, audio, isolation, interstage, 1200 ohm primary, 600 ohm, Mouser TLO22 or equiv.
- XTAL1-crystal, 3.579 kHz, metal, radial-leaded case, MTRON ot equiv.
- Miscellaneous—perforated circuit board; project case (see text); three 8-pin DIP sockets; two 14pin DIP sockets; one 16-pin DIP socket; holder for four AA power cells; four alkaline AA power cells; solid, tinned copper wire (22 AWG), insulated hookup wire (22 AWG), two lengths of telephone cord; 12-volt battery clip; cable ties; solder.
- Note: The following items are available from information Unlimited, P.O. Box 716, Amherst, NH 03031; phone 603-673-4730, Fax 603-672-5406:
 - Complete kit including perforated board, all active and passive components, and telephone cords and plugs.--\$99.50
- Include \$5.00 for shipping and handling. Allow two to four weeks for delivery.

two black and yellow wires flush with the ends of the cord jacket. Assemble the RJ-11 plugs PL1 and PL2 to the other ends of the telephone cords and crimp them in position.

Verify that all diodes, polarized capacitors and transformers have been inserted correctly with their correct orientation and polarities observed. Examine all soldered joints to be sure they are clean and shiny, and that there are no inadvertent solder bridges. Resolder any "cold" solder joints that appear as dull gray, irregular solder bonds. Trim any leads that overlap or form inadvertent short circuits.

Insert the two reed relays, RY1 and RY2, in their sockets. Insert the ICs only as directed in the circuit test procedures.

Circuit test

Measure the continuity between the following points and the circuit board ground bus.: IC1—pin 1; IC2—pin 8; IC3— pin 1; IC4—pin 7; IC5—pins 8 and 13; IC6-pin 4; emitters of transistors Q1, Q2, Q3, and Q4; T1 secondary.

Connect the four AA cells which form the 6-volt DC battery pack to the battery clip. Verify that 6 volts appears between the following test points and the ground bus with a voltmeter. (The current drawn should be 0.1 to 0.2 milliamperes):

IC1—pins 4 and 8; IC2—pins 3, 4 and 6; IC3—pins 4 and 8; IC4—pin 14; IC5—pin 16; IC6 pin 7, collectors of transistors Q1 and Q2.

Plug PL1 into a telephone jack connected to a "test" telephone. (It might be necessary to obtain a modular duplex jack such as Radio Shack's 279 386.)

Insert both the 555 timer IC1 and transistor Q1 in their sockets. Connect one lead of a voltmeter set on the 10-volt DC scale to the collector of Q1, and verify a reading of 6 volts.

Short-circuit plug P1 and observe the voltmeter scale to see if the voltage momentarily drops to near zero. Resistor R32 is specified as 390 kilohms, but it might be necessary to substitute a lower value for reliable

triggering of IC1 via pin 2. However, make that substitution in gradual increments because if the value is too low, the reed contacts of RY 1 will chatter and the circuit will not work.

Switch off the 6 volts with switch S1, insert the DTMF decoder IC1 in its socket, and set trimmer potentiometer R29 to its midrange. Restore power with S1.

Verify that a logic high appears on pins 13 and 14 each time the pound (#) key is pressed on the connected test telephone to verify the operation of decoder IC2.

Switch off the 6 volts with S1 and insert NAND gate IC4. Restore power and verify a logic low on pin 3 each time the pound (#) key is depressed. Measure the inverted signal at pin 4 to perform this test.

Switch off the 6 volts with S1, and insert the second 555 timer IC3. Verify that there is a momentary 5 volts on pin 3 each time power is restored with S1.

Switch off the 6 volts with S1, and insert the decade counter IC5. Restore power and verify that pins 2 and 4 are at logic low and pins 3 and 15 are at logic high.

Press the pound (#) key and verify that pins 2 and 4 of IC5 show alternating logic levels, each repeating every third keying step. These tests verify the proper operation of the logic, reset digital processing, and function counter.

Switch off the 6 volts with S1, insert op-amp IC6, set trimmer potentiometer R17 to midscale, and turn on the power. Press the pound (#) key on the test telephone and listen for any sounds picked up by the microphone to verify the operation of the *listen* mode.

Connect the leads of a voltmeter to the collector pin of Q2 and ground to verify the presence of 6 volts. Press the pound (#) key of the test telephone, and observe that the voltmeter shows a momentary dip to zero. This energizes relay RY2 for the *intercept phone conversation* mode.

Press the pound (#) key of the test telephone and observe a log-

ic high on pin 3 of IC5. This verifies the operation of the *reset code functions* mode. Pins 2 and 4 of IC5 should be at a logic low.

If all of these tests have been passed successfully, the correct functioning of all Telemike controls has been verified.

The following procedure requires two separate telephone lines in the room where the testing is performed. Line A and line B.

Plug the RJ-11 phone plug PL1 into the outlet jack of Line B. (A telephone need not be connected to this jack.) Set a voltmeter on the 100-volt DC scale and connect it to measure 50 volts across the red ring and green tip telephone wires, and look for the expected 50 volts. Switch on S1 and verify that there is no change in the 50-volt reading on the voltmeter other than a momentary drop. Repeat this step making the measurements at the plug.

Pick up the handset from the Line A test phone and key in the number of the Line B phone. It is important that you press the pound key immediately to access the line during its receptive interval. You should be able to hear low-level sounds in the room where Telemike is located clearly. Turn on a radio in the same room if you want a steady audio signal source.

Press the pound (#) key a second time, putting Telemike in its intercept phone conversation mode (non functioning at this time), and then key it a third time to reset the Telemike.

Intercept function

The next test requires a third telephone line (the one to be intercepted).

Plug PL2 into the jack of the third telephone line in the room so you can intercept and monitor any conversations on that line. Switch on S1 and verify that 50 volts DC appears across both ring and tip wires.

Call the Line B phone from the test Line A phone, and access the second phone line by pressing the pound key (#) twice. You should hear a dial tone from the second phone line indicating that you have gained access. This tone indicates that you have intercepted the line and will be able to hear any conversation on it.

Make arrangements for two other persons to converse over the second phone line, and then call the "called to" number and key the pound sign twice to listen in on an actual call in progress. When you are ready to quit this mode, be sure to press the pound key again to reset Telemike.

Note: The audio level on the intercepted conversation might be weak in this mode, forcing you to listen very carefully. If you intend to interrupt a conversation with a message, you might have to speak loudly to be heard.

Telephone compatibility

Not all telephones have the same encoding signal output levels. This could cause circuit unreliability when accessing a second telephone line. If that occurs, you might be able to correct the problem by setting trimmer potentiometer R29 on the Telemike.

Dedicated line

Consider leasing of a dedicated line to Telemike as part of a permanent installation. This will eliminate possible ring signal "sneak through" and the critical timing of the 555 IC1 for allowing access control. Nevertheless, it would still permit all incoming calls to be completed and would have no effect on outgoing calls.

Timer values

The initial access time established by the time constant of resistor R5 and capacitor C6 can be set in most systems to permit a normal incoming telephone call to be made. If this time is too long, and an "off-toon" hook condition is created that will disable the connection. If it is too short, the encoding tones might not pass. This condition should not interfere with outgoing calls. In most cases, the longer time constant will assure encoding control. Ω

Encourage young children to learn to play the piano or organ with this microcontroller-based training system.

JAMES E. TARCHINSKI

MUSIC BRINGS PLEASURE TO ALL OF us and adds to the quality of our lives. While most of us just listen to music, others play musical instruments for pleasure or profit. Parents, relatives, and friends of young children might want them to learn to play and enjoy music at an early ageeven before they are old enough to profit from formal training in an instrument. Micro-Conductor overcomes this problem. This electronic trainer makes it possible for children to play simple tunes on a piano or organ without formal training.

Fifteen LED lamps on an indicator panel light up in the proper sequence under microcomputer control to prompt youngsters to press the associated keys to play nine familiar tunes. The tempo of the music can be regulated from slow to fast as children catch on, and a LED display identifies the tune being played.

The attraction of Micro-Conductor for children aged 4 to 6 is instant satisfaction. With a little practice in following blinking lights with their fingers, children—even those with short attention spans—are rewarded with the sounds of music. Moreover, Micro-Conductor should discourage children from randomly hammering on the keys of the family piano and driving even the most permissive parents to distraction.

The cable-connected indicator panel is placed just above the keyboard, and the circuit board is placed out of the way on top of the organ or piano, as shown in Fig.1. Power for Micro-Conductor is obtained from an AC-to-DC adaptor that plugs into a wall outlet (saving you the expense of a lot of replacement batteries).

Micro-Conductor can be built from readily available components, and its microcontroller is programmed with nine tunes and musical scales. Moreover, it's a great starter project if you've never built a computercontrolled system. Pre-programmed chips are available from the source given in the Parts List if you prefer not to program the microcontroller.

Circuit operation

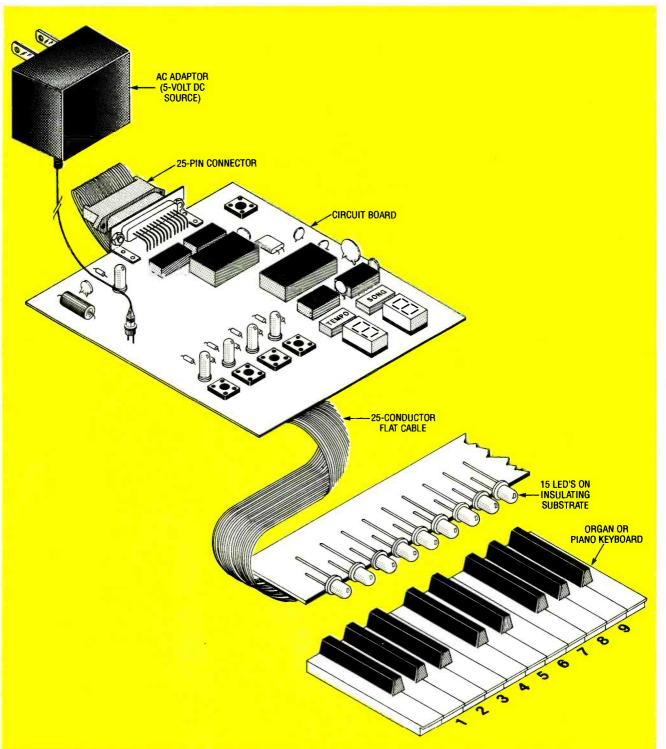
Figure 2 is the schematic for Micro-Conductor. The heart of the system is a Motorola MC68705P3 microcontroller which contains random-access memory (RAM) and field-programmable read-only memory (EPROM). Most of the chip's 28 pins perform input/output functions. Reprogrammable EPROM makes it easy to modify the operation of the trainer and add new songs when the first set has been overplayed.

The nine pieces and musical scales, numbered 0 to 9 and listed in Table 1, are programmed into the microcontroller. Number 9, scales, is the default tune when the unit is first powered up. The number of the tune being played is displayed on seven-segment LED display DISP2. It can be increased by pressing switch S3 or decreased by pressing switch S4. Whenever those switches are pressed, the circuit zeros an internal counter so that the new song begins to play on its first note.

To accommodate children of different ages and abilities, ten different tempos have been included: zero is the slowest and nine is the fastest, with the second value assigned to default. DISP1, another seven-segment LED display, shows the tempo selected. Tempo can be increased by pressing switch S1 and decreased by pressing S2. Unlike tune number, however, tempo can be changed at any time without restarting the piece being played.

Micro-Conductor's controls





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FIG. 1—MICRO-CONDUCTOR SYSTEM INCLUDES (top to bottom) outlet-mounted ACto-DC adaptor, circuit board with microcontroller, function displays and switches, and a flat-cable connected indicator panel that is placed above the right keys on the piano or organ keyboard.

are simple enough to permit youngsters to operate the system by themselves. The four LED lamps on the PC board (LED1 to LED4) are not a required for the operation of the circuit, but were included to make software debugging easier. Microcontroller IC1's Port B (PB0 to PB7) controls input switches S1 to S4 and those four board-mounted LED's. Software (ORGAN5.S05) illuminates each of those LED's whenever the related pushbutton is pressed. IC1's Port C (PC0 to PC3) does most of the work of Micro-Conductor although it only has only four of the 20 input/output pins. Port'C drives IC2, a 74154 four-to-16-line demultiplexer. In response to the 4-bit input from IC1, IC2 drives the 15 LED's (LED6 to LED20) in the cableconnected indicator panel shown in Fig. 1.

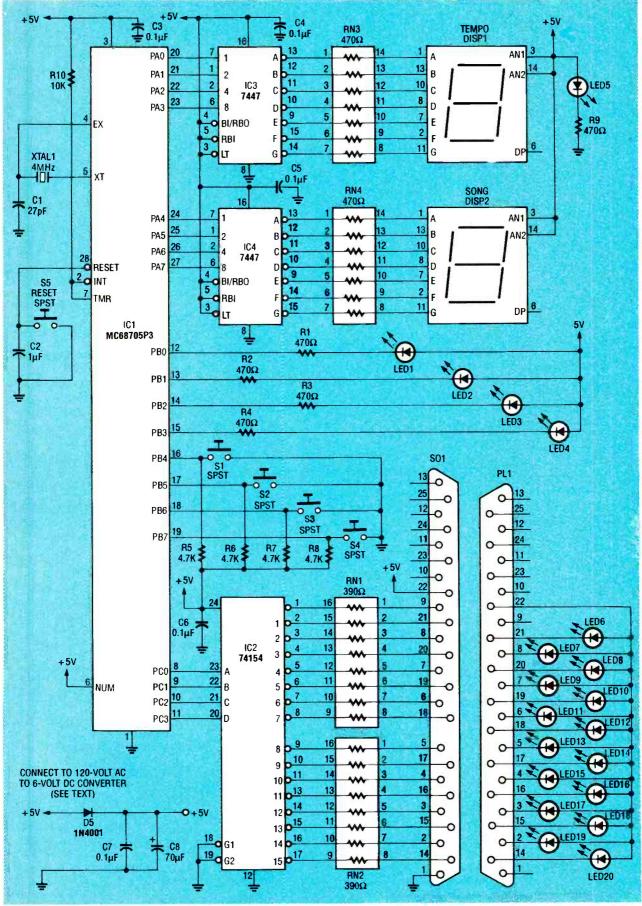


FIG. 2—SCHEMATIC FOR MICROCONTROLLER and indicator panel.

TABLE 1-SONG TITLES

- 0 Three Blind Mice
- 1 This Old Man
- 2 Twinkle-Twinkle Little Star
- 3 London Bridge
- 4 Mary Had A Little Lamb
- 5 Rock-A-Bye Baby
- 6 Yankee Doodle
- 7 Pat-A-Cake
- 8 Hickory-Dickory Dock
- 9 Scales

There is no connection on pin 9 of connector PL1 for IC2's output 0 (pin 1). This permits a delay note, a binary code of %0000 on the input lines of IC2 that can turn off all the indicator panel's LED's. That delay note occurs between tunes and is imbedded within them.

Because IC2's outputs run on negative logic, the 15 LED's on the indicator panel are all tied through current-limiting resistors to +5 volts. When the voltage on the outputs of IC2 go to their low value, the connected LED's are illuminated. Figure 3 shows how the LED's are matched with the organ or piano keys. As shown, Middle C on the keyboard is related to LED9. Figure 3 also shows the four-bit single hexidecimal character code programmed into microcontroller IC1 that is associated with each key.

Control circuit construction

The foil pattern for Micro-Conductor's PC board is included in this article. Referring to the schematic Fig. 2 and the parts placement diagram Fig. 4, insert all resistors, resistor networks, capacitors, switches, and LED's I to 5 in the PC board and solder them. Trim all excess leads close to the board.

Bend both leads of crystal case XTAL1 at right angles approximately ½-inch from the bottom of the case and insert them in the holes as shown on Fig. 4. Then bend about a 4inch length of tinned copper wire in a "U-"shape with its ends ½-inch apart. Insert those ends over the crystal case into the holes on both sides of the metalized shield patch on the underside of the board. Twist the ends

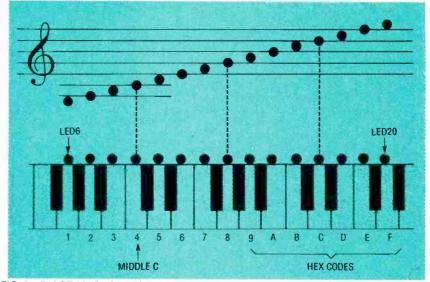


FIG. 3—DIAGRAM SHOWING LOCATION OF LED LAMPS in the indicator unit over the piano or organ keyboard. Hex codes permit coding additional tunes in the microcontroller.

of the wire together to pull the case snugly against the top surface of the board. Solder both the crystal case leads and wire strap ends where they exit the board and trim excess wire lengths.

Insert the 25 pins of the rightangle D-type socket commector SO1 into the matching holes of

PARTS LIST

- All resistors are ¼-watt, 5 %
- R1-R4, R9-470 ohms
- R5-R8-4700 ohms
- R10-10,000 ohms
- RN1, RN2—390 ohms, eight-resistor DIP (CTS 8916 or equivalent)
- RN3, RN43—470 ohms, seven-resistor DIP (CTS 8825 or equivalent)

Capacitors

- C1-27 pF, 16-volt disc
- C2-1 µF, 16-volt disc
- C3-C7-0.1 µF, 16-volt disc
- C8-470 µF, 10-volt electrolytic
- Semiconductors
- IC1—MC68705P3, microcontroller (Motorola)
- IC2-74154N, 4-to-16 line demultiplexer
- IC3–IC4—7447AN, 7-segment LED display drivers
- LED1-LED21-red light-emitting diodes, 13/4
- DISP1, DISP2—7-segment, common-anode LED displays in standard 14-pin DIP packages Other components
- XTAL1—4MHz quartz crystal, HC-18 case, (ECS, Digi-Key X006 or equivalent)
- S1–S5–SPST momentary pushbutton switch, PC-mount, (Panasonic P8034S or equivalent)
- SO1-25-pin, type-D connector

with right-angle mounting brackets (Amphenol 177 or equivalent)

- PL1—25-pin, type-D connector, MTIDC
- Miscellaneous: Micro-Conductor PC board, 28-pin DIP socket for IC1, 24-pin DIP socket for IC2, two 16-pin DIP sockets for IC3 and IC4, length of 25-conductor 0.050-inch, 7 × 36 28 AWG flat cable (see text), AC-to-DC adapter, 120-volts AC outlet mounted, 6/7.5 volts DC, 700 mA, (Radio Shack No. 273-1655 or equivalent), DC jack (Radio Shack No. 274-1563 or equivalent), 4 PC board rubber feet with adhesive backing, strip of wood or plastic (see text), tinned copper wire, solder.
- Note: The following parts and software are available from James Tarchinski, P.O. Box 080133, Rochester, MI 48308-0133
 - Pre-programmed MC68705P3 microcontroller—\$17.00
 - Programmed 5½-inch disk formatted for MS-DOS compatible computers containing all files— \$8.00
- Please include \$2.00 for shipping and handling. Michigan residents must add 5% sales tax.

the PC board and seat the connector flush with the edge of the board. Fasten the connector to the PC board with one of two methods. Drill two holes through the board using one of the two holes on each bracket as a template. (Be sure that you do not drill into a conductive trace on board underside.) Fasten the brackets with nuts and bolts, solder the conductors and trim excess lengths. Alternatively, place drops of epoxy or a suitable cement in the bracket holes to bond the brackets to the board after the leads are soldered and trimmed.

A socket is reqired for IC1 so that the microcontroller can be removed for reprogramming. While not mandatory, sockets are recommended for IC2 to IC4. Position the sockets, solder them, and trim excess leads.

The prototype has a jack for the coaxial plug from the AC-to-DC adaptor wired to the PC board with short lengths of insulated wire. However, you can cut off the plug, strip the wire ends, insert them in the holes, and solder them directly to the board as shown in Fig. 4. You can also drill a hole in the PC board and mount the jack directly on the board. (Be sure to observe the polarities for both adaptor plug and PC board.) Solder the connecting wires between board and jack, and trim excess lengths. Tape or pot the exposed jack terminals with RTV compound to insulate them.

Place the adhesive-backed rubber feet on the four corners of the underside of the PC board to elevate it board above any conductive surface that could short exposed traces and soldered joints. Insert the integrated circuits IC1 to IC4 in their sockets, taking all precautions to prevent IC damage from electrostatic discharge.

You can improve the appearance of the system and provide better protection for the circuitry by enclosing the circuit board in a suitable plastic or wood case. Its inside dimensions should accommodate the circuit board and allow adequete vertical clearance. How-

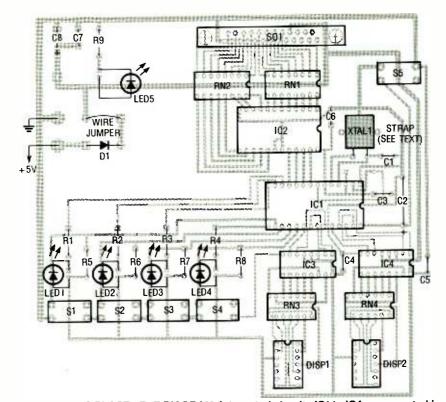


FIG. 4—PARTS PLACEMENT DIAGRAM. Integrated circuits IC1 to IC4 are mounted in sockets. Note wire clamping crystal XTAL1 case to board. A DC jack can be mounted in a drilled hole on the board (not shown).

ever, if you elect this option you will need additional parts *not* listed in the Parts List. Also, the construction procedure given so far must be changed to allow for this alternative.

If you want to put the circuit board in a case, first drill holes at the four corners of the board for standoffs before doing any component assembly. Mount the LED displays on right-angle connectors and cut windows for them in the side walls of the case at the right locations. Also cut openings for the D-type connectors and drill a hole for the DC jack on a side wall. Mount

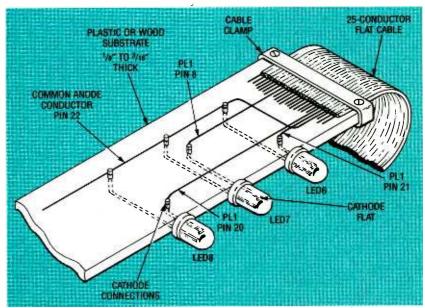


FIG. 5—DETAILS FOR BUILDING THE INDICATOR PANEL. LED leads are bent and inserted in drilled holes in wood or plastic strip and soldered connections are made as shown. Protect exposed conductors with tape or covers (not shown).

switches S1 to S5 on the front panel and wire them to the circuit board with lengths of hookup wire long enough to permit the board to be removed from the case. (You might want to replace them with switches more suitable for case mounting.)

When the board is complete but before inserting the IC's, fasten it to the bottom of the case with screws and standoffs—plastic or metal tubes about ¹/₂-inch long.

Indicator panel construction

Determine a satisfactory length for the 25-conductor flat cable (up to three feet) and cut one end square. Insert and seat that end in the slot of connector PL1 (with mass-termination, insulation-displacement contacts). Position the connector and cable in a vise and, holding both cable and connector firmly together, slowly close the vise to drive the row of contacts uniformly into the cable to form secure bonds with each of the conductors.

Referring to Fig. 5, select a suitable strip of wood or plastic from 1/8 to 3/16-inch thick, about 2 inches wide and up to 20 inches long. Determine the actual length by referring to Fig. 3. Add the center line distances between 15 keys on your piano or organ's keyboard, and allow about 2 inches on each end. Measure in about 2 inches from one end to allow for clamping the cable to the strip, and mark the center line locations for each of the 15 LED's (LED6 to LED20) to be mounted.

Carefully bend all LED leads at right angles (as shown in dotted lines on Fig. 5) to account for the thickness of the insulating strip selected. The bent ends of each LED should equal the strip thickness plus about $\frac{1}{16}$ inch to act as exposed solder terminals when the LED's are seated. (Note that LED cathode leads are shorter than anode leads and are closest to the packages' flat surfaces.)

With a handheld pin drill and bit slightly smaller than the diameter of the LED leads, drill two rows of 15 holes in the strip for the leads as shown in Fig. 5, observing the proper spacing and alignment. Insert the bent sections of the LED Leads into the holes and press the LED's down gently so their leads are flush with the surface of the strip. The terminals should project above the surface of the reverse side. (The leads should fit snugly in the holes so the LED's will not fall out when the strip is handled.)

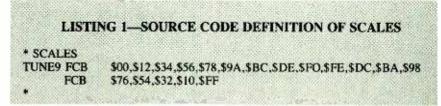
Reverse the strip and position it as shown in Fig. 5. Allow enough cable length for conductors to reach the last LED in the series, and clamp the cable to the strip as shown. The clamp can be an aluminum or copper strap wrapped around the strip and squeezed in a vise or fastened with screws near the edges of the strip.

With the cable securely clamped to the indicator strip, separate the conductors carefully and trim excess wire.

Locate the indicator unit on an insulating surface so that no leads are shorted, and check all connections both visually and with a continuity meter to be sure that the LED's are connected in the specified order. Repair any errors and replace any faulty LED's. Protect the exposed conductors of the unit. They can be covered with vinyl electric tape or, for a more professional appearance, covers. Cut matching covers from suitable sheet plastic and drill holes along their lengths to permit them to fastened to both sides of the strip with nuts and bolts, forming a protective sandwich.

Microcontroller software

Due to limited space, only part of the assembly language program has been reprinted here. The complete program is



with a razor knife back to about 1/8 inch from the clamp. Referring to the schematic Fig. 2, cut off the open-circuited conductors 13, 25, 12, 24, 11, 23, 10, 9, and 1 close to the clamp. Find conductor 22 and cut it off near the anode terminal of LED6, allowing about 1/2 inch for stripping and wrapping bare wire around the exposed LED posts.

Wrap one end of a 20-inch length of tinned-copper wire around the LED6 anode post, and continue wrapping all exposed anode posts to LED20 to form a common conductor. Solder all anode connections and trim excess wire. Now, starting with the cathode post of LED6, cut and strip conductors 21 to 14 as shown in Fig. 2, making allowance for increasing length. Also allow enough slack on each conductor to minimize overlapping and permit it to be pressed close to the surface of the strip. Wrap one turn of the stripped wire ends around each cathode post, solder the connections

available on the Electronics Now BBS (516-293-2283, V.32, V. 42bis). Download file ORGAN5.ZIP, an archived file that must be "decompressed" with the PKUNZIP utility, which is also available on the system. (Note that the Electronics Now BBS is always free of charge.)

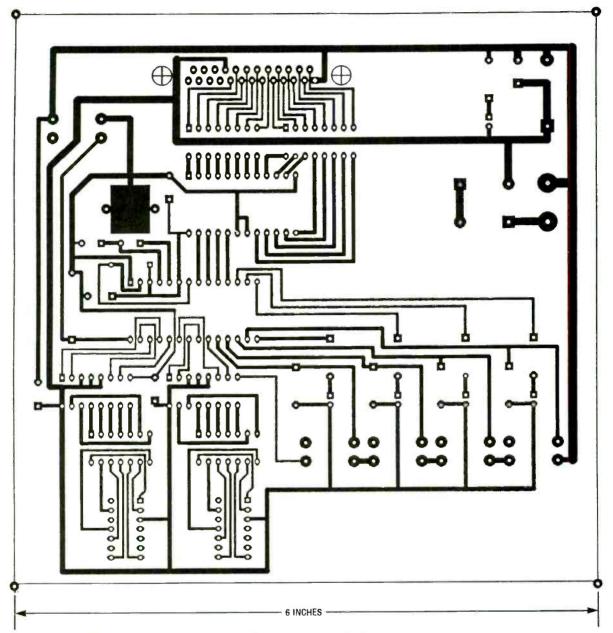
The four files of software are: ORGAN5.S05—Source code file for the software.

ORGAN5.LST—Output listing file generated by the assembler. ORGAN5.P05—Motorola S-record listing of the code that can be sent directly to a PROM programmer.

README.TXT—An ASCII file containing any important lastminute advisory notices.

To program microcontroller IC1 from your PC, follow the manufacturer's procedure. An article entitled 68705 Microcontroller by Thomas Henry, Sept. 1989 R-E includes that procedure.

The assembly language code for Micro-Conductor is in five



BOTTOM FOIL (SOLDER SIDE) for micro-conductor PC board, shown half size.

sections. The first contains all housekeeping functions for the program (e.g. title and version information, RAM variable assignments, general constant equate statements, and definitions of both the processor's mask option register and vector table).

Next, there is code section headed *Initialization*. When the microcontroller detects the end of a reset condition (i.e. when power is first applied), it starts to execute the START label, which is at the beginning of the initialization block. This section of code performs the following duties: Initialization of all I/O portsClearing of the entire RAM

memory to a value of \$00
Initialization of the registers for creating a regular interrupt frequency

• Setting of initial values for several RAM variables

When the microcontroller completes initialization, it switches to the main execution loop labeled MAIN in the source code. That loop handles all Port A and B I/O functions except enabling the 15 indicator unit LED's.

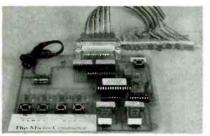
The first function of the MAIN loop is to read the state of the four input switches S1 to S4. After the inputs are debounced via software, the program checks each switch state in sequence. If a specific switch is pressed, either the song variable or the TEMPO variable are incremented or decremented by one. After changing either of these variables, the software automatically checks to prevent a user's attempt to call for a variable beyond the microcontroller's permitted range.

The last block of code in the MAIN section updates the LED displays DISP1 and DISP2. The four bits of the SONF variable are rotated over into most significant nibble within the ac-

cumulator and ored with the four significant bits of the SPEED counter. The resulting byte is then available at Port A (PA0 to PA7) of the microcontroller for the LED driver IC's (IC3 and IC4) and display module to indicate tempo and song number.

The fourth section of code in the file source begins with the label TM—INT, which marks the start of the timer interrupt routine. At regular intervals of about 31 milliseconds, the microcontroller stops executing the MAIN program loop and runs the code between the TM—INT and RTM—INT labels. That section of code controls the 15 indicator LED's (LED6 to LED15) connected IC1's Port C.

If enough time (dependent on the TEMPO setting) has elapsed since the keyboard LED's were last updated, the software either turns off any lighted LED or turns on the next one in the



AUTHOR'S PROTOTYPE of the Micro-Conductor.

song due to the value of the NOTE variable. Because IC1 lacks an addressing mode that can handle 16-bit offsets, each tune must tested in sequence.

The last section of code in the source file is the song data. After an appropriate "TUNEx" label, form constant byte (FCB) pseudo instructions insert the notes of the songs into the file. This data is encrypted with the coding system shown in Fig. 3. To conserve PROM, two notes (requiring only four bits each) are placed in every byte of the FCB statements.

Note that there are two special codes in each of the ten songs. Every song begins with a \$00 code, which allows time for a child to move his fingers back to the keyboard before the song is displayed. Similarly, every song ends with a ?? code, indicating to the software that last song being played is finished. See Listing 1 for a section of the project's source code that defines the Scales tune.

When both components of Micro-Conductor have been built and plugged together, it is ready for a test run. Plug in the wall-adaptor and start the included program.

Micro-Conductor will give children a pleasant introduction to formal music instruction. The child will soon learn the relation between the keys and the musical scale and, it is hoped, take an early interest formal music instruction. **R-E**

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NEW LIFE FOR **OLD SCOPES**

Find out how you can give new life to an old oscilloscope.

MICHAEL A. COVINGTON

AN OSCILLOSCOPE IS ONE OF THE most useful test instruments, but also one of the most expensive. A new scope costs \$400 or more, but used scopes in lessthan-perfect condition sell for under \$50. Most industrial users don't want to keep a scope that's showing signs of age. If you learn to troubleshoot oscilloscopes, someone else's loss can be your gain.



Where to find them

Before you can fix up an old scope you've got to find one. The best sources of cast-off scopes are ham radio swap meets, or hamfests. You can find out more about such gatherings by contacting your local amateur radio club for information. The prices at hamfests are really low. This year I bought a Tektronix 541 (originally \$1400) for \$25 and a Heath IO-14 (originally \$400) for \$10-both with minor, but fixable defects.

Last year I did even better. I saw a dilapidated Heath IO-12 under a table marked "free," and the owner immediately insisted I take It off his hands. Admittedly, it had no knobs or tubes, but tubes at a hamfest cost only 25 cents each, so it didn't take long to get it working.

You can also find secondhand scopes in classified ads, but the prices are likely to be higher-\$100 to \$200-although the equipment is usually in better condition. Also, ask at factories and repair shops to see if they are planning to sell off any old or used equipment.

Types of old scopes

There used to be two kinds of scopes; "utility" and "wideband." Nowadays, both have been replaced by calibrated triggeredsweep lab scopes, but the older ones are still worth having.

Utility scopes are designed for audio work and sweep generator alignment; their upper frequency limit is a few hundred kHz. Those scopes were used by the first generation of TV repairmen in the 1950's. Popular models in-





clude the Eico 400 and 425; the Heath OM-1, OM-2, OM-3, OL-1, IO-10, and IO-21; the RCA WO-56, WO-57, and WO-88; and the Radio Shack 22-086. (Yes. even Radio Shack used to sell oscilloscopes!)

When color TV arrived, so did wideband scopes—a utility scope can't show the 3.58-MHz color burst on a video signal. Most wideband scopes are good at least to 5 MHz, and some go down to DC. Heath models O-10, O-11, O-12, and IO-12 are progressive refinements of a classic model. 57 Other wideband scopes include the Eico 435 and 460, and the RCA WO-33, WO-78, WO-79, and WO-91.

In the late 1960's, lab-grade scopes began to replace the cheaper kinds. A lab scope is calibrated on both axes—volts per centimeter vertically and microseconds per centimeter horizontally. In practice, that means that lab scopes have a triggered sweep—they will hold the waveform steady at any sweep speed, whereas with conventional scopes, you have to synchronize the sweep with the signal.

The Heath IO-14 and Knight 83YZ945 were among the first affordable lab scopes. Affluent industrial and government organizations used Tektronix lab scopes, which had been around since the early 1950's. Tektronix spared no expense to provide the best performance. Model 545 had about 75 tubes, including a broadband amplifier with 16 matched 6CB6's, and accepted interchangeable plug-in vertical preamps. Components were silver-soldered to ceramic strips, as shown in Fig. 1. So many of the parts in a Tek scope are custommade that the best way to get replacements is to find another cast-off Tektronix.

Beware of low-frequency lab scopes designed for precision audio work; they aren't useful above audio frequencies. The Hewlett-Packard 130 shows up fairly often at hamfests. So do the lowfrequency preamps for Tektronix and Knight lab scopes.

Initial checkout

Electronics Now, September 1994

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The most expensive parts of a scope are the CRT and the power transformer. If they're bad, it usually doesn't pay to fix the scope, unless you can salvage parts from another one just like



FURTHER INFORMATION

Heath oscilloscope manuals are still available from Heath Company, Benton Harbor, MI 49022; Tel: 616-982-3571. Old Tektronix manuals are available on microfiche from Tektronix, Beaverton, OR 97005. You may be able to borrow Tektronix manuals from a nearby government or industrial lab or the electronic repair shop at a university. RCA manuals can be obtained through RCA distributors. The circuit of the RCA WO-33A was published in the 1963 RCA Receiving Tube Manual.

A gold mine of information is in the Encyclopedia on Cathode-Ray Oscilloscopes, by Rider and Uslan (New York: Rider, 1959). It contains schematics of dozens of scopes, along with advice on troubleshooting. Your local public library may be able to get this for you on an interlibrary loan.

Two books that will help you understand oscilloscope circuitry are *Electronics for Scientists*, by Malmstadt, Enke, and Toren (W. A. Benjamin, N.Y., 1963), and *Typical Oscilloscope Circuitry* (Tektronix, Beaverton, OR, 1961).

Over the years, Radio-Electronics has published many articles about oscilloscopes. The ones I particularly recommend are:

 "All About Oscilloscopes," Charles Gilmore, June–September 1975.

 "How to Use Triggered Scopes," Larry Allen, August 1969.

• "Scope × 100," (Wideband Modifications) Tom Jaski, November 1965.

 "How to Wideband Your Scope," Barry Turner, August 1965.

 "Modifying Heath Scope," Edward J. Och, August 1962.

Finally, you can get the basic specifications of an old scope by finding the manufacturer's ad for it. Tektronix advertised regularly in *Proceedings of the IRE*; other manufacturers advertised in **Radio-Electronics** and Electronics World.

it. So the first check is simply to plug in the scope and try to get a spot or trace on the screen. If you can, the CRT and transformer are good.

If you can't get a spot or trace, don't give up. A blown fuse may have cut off power, or a bad tube may have deflected the beam all the way off the screen. Also, note that triggered-sweep scopes don't display a trace unless there's a waveform at the input and the trigger level is set properly. Most of them have an "auto" position that makes the trace visible even without an input.

The trace on an old utility or service scope won't be very bright. If you can see it indoors, it's probably as bright as the manufacturer intended; lab scopes are much brighter. You can improve contrast by putting a piece of green plastic over the white screen of the CRT, or sometimes by replacing the original green filter with a lighter one.

Warning

High voltage can kill! Before working on a scope, disconnect power and discharge all electrolytics. When making internal adjustments with power applied, use extreme caution. Stand on a dry, insulated floor and keep one hand in your pocket. Do not wear grounded wrist straps or other devices designed to protect lowvoltage IC's.

The most lethal voltage in a scope is probably the 400-volt B+ supply, which can deliver several hundred milliamps. The CRT accelerating voltage is 1500–6000 volts, but is at a much lower current.

Solder, switches, and tubes

Assuming the scope shows signs of life, the next step is to fix bad connections. Many hamfest bargain scopes were built from kits and suffer from cold solder joints. Intermittent, flaky behavior with unknown causes is what often leads the owners to unload a scope. On top of that, the owner usually lets the scope gather dust for a few years in his attic or chicken coop before disposing of it.

The cold solder joints are easy to fix—just melt every joint again, adding solder where necessary. Use a 100-watt soldering iron, not the 15-watt type used for solid state work. We're dealing with 1950's technology, and proper soldering takes power.

The sojourn in the chicken coop really dirties the controls. Solvent squirted from a can will usually fix potentiometers, but rotary switches may need something more potent, like wire brushing. I use miniature brushes that are designed for the Dremel Moto-Tool but will fit an ordinary cordless drill. It takes a lot of brushing to get all the metal clean.

Also, make sure the contacts are properly positioned—they should move visibly as the metal

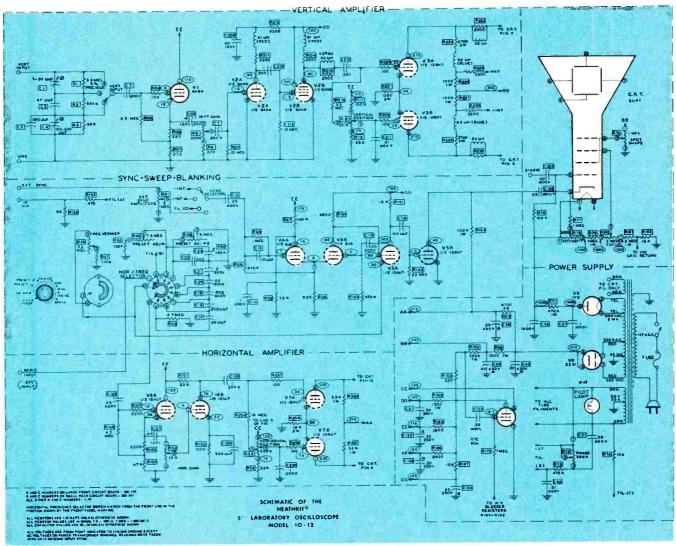


FIG. 2—THIS IS THE SCHEMATIC OF THE Heath IO-12, a popular wideband oscilloscope with recurrent (synchronized, not triggered) sweep.

slides under them. If necessary, you can bend a contact back, clean it with fine sandpaper, and then bend it back into position, but that's tricky. An ohmmeter can tell you whether you've gotten the switch good and clean. Take comfort in the fact that dirty switches and controls usually get cleaner when used regularly.

The next step is to test the tubes. Be warned that tubes in scopes are more critical than in other equipment; matched pairs or selected tubes may be required in some places. If you don't have a tube tester, look for tubes that don't light and try swapping tubes of the same type to see if there is a change in performance. Quite often, a bad tube is all that's wrong.

Oddly enough, if a tube goes bad in a Tektronix vertical amplifier, you may not notice it; the circuit is direct-coupled at low frequencies and the only effect a dead tube has is to decrease bandwidth.

Circuit analysis

Figure 2 shows the circuit of the Heath IO-12, a typical wideband scope. Most troubles are easy to localize because each function of the scope corresponds to a particular circuit vertical and horizontal amplifiers, sync, sweep, and so forth.

Most failures occur in the power-supply. Look for open or leaky filter capacitors and burned-out resistors. Reduced voltages and excessive ripple may indicate that a selenium rectifier has increased in resistance; you can wire a silicon diode in parallel with it, and all the current will go through the silicon. Remember, too, that you can replace a rectifier tube with silicon diodes.

Lab scopes have regulated supplies in which a 150-volt reference voltage controls all the regulators. If the reference voltage is even slightly off, many other circuits will malfunction. You can correct slight errors with "150-volt adjust" potentiometer.

Lower-cost scopes get their high voltage from the power transformer. Lab scopes, however, use a separate 60- to 100kHz oscillator, high-frequency transformer, and voltage multiplier. Loss of high voltage is often caused by a shorted high-voltage capacitor. In a Tektronix scope, you can check for that by disconnecting capacitors, one by one, until the filaments of the high voltage rectifiers light up.

If the power supply is okay but you can't center the trace on the **59** screen, look for a bad tube in a push-pull amplifier, and note that more expensive scopes have push-pull stages throughout their vertical and horizontal sections, not just at the output.

Horizontal sweep is seldom perfectly linear. The earliest scopes used an 884 or 2D21 thyratron tube—essentially a neonlamp blinker with a grid—and generated a poor-quality sawtooth. Later models used dual triods but still weren't perfect, as shown in Fig. 3. Severe nonlinearity, however, may indicate a bad tube or leaky capacitor.

Hum

Many scopes show a noticeable 60- or 120-Hz ripple superimposed on every trace, due to power-supply trouble. To check, try bridging each filter capacitor with a known good one, test all tubes associated with voltage regulation, and check that rectifiers are okay. Hum of that type is normally 120 Hz.

In cheaper scopes, a 60-Hz ripple is caused by the magnetic field of the power transformer, and is considered normal. More expensive scopes have a mu-metal shield around the CRT to block magnetic hum. In tube-type equipment, hum is never totally absent, but its amplitude should be one millimeter of screen deflection or less.

Hum can also come from poor grounding. Mechanical contact between pieces of metal does not always make a good electrical connection, especially if the scope is old. I cured the hum in my Heath IO-14 (Fig. 4) by adding solder lugs to ground PC boards to the chassis, and a grounding strap, made of copper braid, for the vertical attenuator.

Another source of hum is heater-to-cathode leakage in a tube. Regardless of the cause, you can detect where hum is entering the system by removing tubes stage by stage until the hum stops.

Adjustments

Every scope has an astigmatism control to ensure that the beam spot is round, not oval. In some Heath models, that's on the inside (Fig. 5), but it's a good idea to adjust it. Bear in mind that it

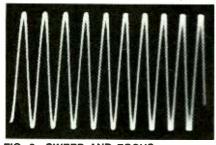


FIG. 3—SWEEP AND FOCUS are somewhat uneven on cheaper scopes; you just have to live with it.

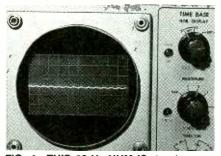


FIG. 4—THIS 60-Hz HUM IS due to poor grounding of the input stage, and can be cured by adding a copper strap.

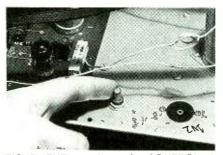


FIG. 5—THE ASTIGMATISM CONTROL of the Heath IO-12 is inside; you may want to make it more accessible.



FIG. 6—IF THE TRACE IS TILTED, mark its position on the screen with a grease pencil, then turn the power off, loosen screws, and rotate the CRT.

interacts with focus and intensity controls.

Most lab scopes have one or more vertical balance controls to keep the trace from moving up and down as you switch from range to range, or from "normal" to "invert." Those controls are well worth adjusting. There may also be internal adjustments to center the trace. Try them to see what they do.

Adjustments that affect frequency response, however, should be approached with great caution. Tektronix lab scopes have numerous adjustment points that shouldn't be touched without the manufacturer's manual. It's easier to make things worse than to make them better.

Calibration adjustments aren't as tricky, providing you have test signals of known voltage and frequency. Remember, anything which changes the high voltage will affect the calibration by altering the stiffness of the electron beam.

If the trace is tilted, rotate the CRT (Fig. 6). To do so safely, remove the green filter and mark the trace position on the screen with a grease pencil. Turn the power off, discharge all capacitors, and then align the tube using the grease pencil mark.

Probes and compensation

One adjustment you must make is the vertical input compensation. Do that with the probe that you're actually going to use in high-frequency circuits. Good probes are designed to reduce capacitive loading on the circuit under test.

Figure 7 shows the circuit of a typical low-capacitance probe. On the $\times 1$ setting, the 10K resistor keeps the cable capacitance from loading the circuit under test, but high-frequency response is poor. On the $\times 10$ setting, the 9-megohm resistor forms a voltage divider with the 1-megohm impedance of the scope. The 9-megohm resistor is bypassed with a small capacitor so that more signal can get through at high frequencies.

To adjust compensation, first set the probe to "direct" (\times 1) or temporarily set it aside and connect the scope directly to a good square-wave source, such as the circuit in Fig. 8. Adjust the trimmer capacitors in the vertical input circuit so the top of the square-wave is flat. There may be as many as a dozen trimmers, each for a different range. Set the probe to 10:1 and adjust the capacitor on the probe itself.

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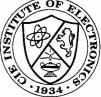
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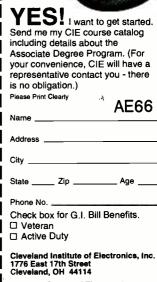


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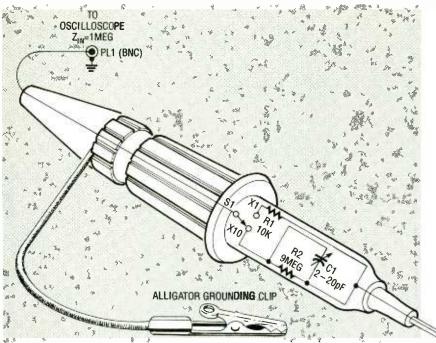
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-THIS IS A CIRCUIT OF A TYPICAL low-capacitance probe. FIG. 7

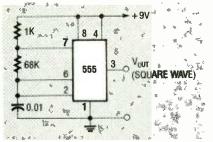


FIG. 8-A SIMPLE 1-kHz SQUARE-WAVE oscillator for testing compensation.

Some scopes have an input impedance of other than 1 megohm-the modern standardand with them, 10:1 probes don't give 10:1 attenuation. For exam ple, a 10:1 probe is actually 3:1 when connected to the 3.3megohm input stage of a Heath IO-12. The probe does its job; the attenuation is just different from what you might expect.

Improvements

You can go beyond fixing the scope and actually improve it in several ways. By replacing rectifier tubes with silicon diodes, and getting rid of filaments, the power transformer will have less of a load to drive, reducing the chance of overheating. You may even want to add a cooling fan. To get one, ask a computer dealer to give you a junked power-supply with a 120-volt fan in it. And how about a really long power cord, or BNC connectors on the inputs,



FIG. 9—REPLACING THE binding post with a BNC connector makes it easier to attach modern probes.

as shown in Fig. 9?

If you're more adventurous, you can improve the circuit design. Many ideas for doing that were published in Radio-Electronics in the early 1960's (see under FURTHER INFORMA-TION). You can increase the bandwidth by adding peaking coils, eliminate hum by using DC on filaments, improve the sync by adding an amplifier stage, or design triggered sweep.

Finally, there's still hope for a scope that's beyond economic repair, but still shows a trace. It can be converted into some other kind of instrument, such as a modulation scope (see the ARRL Handbook), component tester, or transistor curve-tracer. R-E

EQUIPMENT REPORT

continued from page 22

well. At the end of the test, minimum, maximum, and average values for the entire batch of components can be recalled.

A Relative mode makes it easy to separate components whose values measure higher or lower than a reference component. A reference component is inserted in the test sockets, and its value is stored in memory. Then, new component measurements show up as either plus or minus with respect to the reference value.

Electronic components are normally rated with a tolerance figure which indicates how much a given part can vary from its nominal value. Tolerance is given as a percentage of the value marked on the unit. For example, a 100-ohm resistor with a tolerance of 10% should have a true resistance value between 90 and 110 ohms. However, as any experienced technician can tell you, that's not always the case.

The B+K Model 878 includes a Tolerance mode that lets you pick out parts from a batch that don't fall within a given tolerance. To use this feature, you select a tolerance of 1%, 5%, or 10%, and the value of a reference component is stored in memory.

A beeper will sound when a part that doesn't meet the tolerance is tested. These out-of-spec parts can then be discarded, put aside for less-demanding applications, or sent back to the manufacturer for replacement.

To sum up, the B + K Model 878 LCR bridge is really a handy test instrument for anyone seriously involved in electronics. Its features that aid in component sorting make the meter a perfect quality-control tool for checking components before they are installed on a production line.

It's reasonable to expect that the Model 878 will quickly pay for itself by culling out those pesky out-oftolerance components. The 878 will save the cost of lost production and labor needed to find and replace them. This looks like \$275 well spent. Ω



Generate weird sounds with our sound-effect generator based on a light-controlled, tone-burst oscillator.

JOHN CANIVAN

SOUND EFFECTS MEAN BIG BUSIness nowadays, from those intended to enhance home videos to silly ones for your phone-answering machine. In the past we've run articles on how to build very sophisticated—and expensive—sound generators, but this time we present a simple novelty sound-effect generator that's sure to give you and your children hours of fun.

The generator contains two photo cells that control a toneburst oscillator circuit; tone is controlled by one photo cell and the burst interval is controlled by the other. All you have to do is wave your hands above the photo cells to generate all kinds of sounds.

Circuit theory

The tone-burst oscillator circuit uses a 556 timer IC and positive feedback to create the strange sounds. The 556 chip contains two completely independent 555's and, in our application, the output of one 555 controls the interval of oscillation—or the burst time—of the other. Figure 1 shows the pinouts of both the 555 and the 556, and the equivalent circuit of a 555. Positive feedback, which controls the frequency and duty cycle of the 555 timer, is obtained from the charging and discharging voltage across capacitor C through resistors R_A and R_B . During oscillation, voltage across the capacitor changes from $\frac{1}{3} V_{CC}$ to $\frac{2}{3} V_{CC}$, and back again.

The time it takes for the voltage on C to drop from $\frac{2}{3}$ V_{CC} to $\frac{1}{3}$ V_{CC} is known as the discharge time (t_D). When $\frac{1}{3}$ V_{CC} is reached, the 555's flip-flop resets and allows C to charge across R_A and R_B. The time it takes C to charge to $\frac{2}{3}$ V_{CC} is known as the charge time (t_C). When that level of charge is reached, the 555's flip-flop sets and causes C to discharge across R_B, and then the cycle begins again.

Figure 2 shows the complete circuit for our light-controlled tone-burst oscillator. You'll notice that two light-dependent resistors, or photocells, are used: R8 and R9. A photocell is basically a resistor whose value depends on the amount of light to which it is exposed. Its resistance is inversely proportional to the intensity of that light. In bright light, the resistance of a typical photo-cell can drop to 100 ohms, while in darkness its resistance can easily exceed 500 kilohms.

If we use a photocell to replace R_B (in Fig. 1), those minimum and maximum resistance values (100 ohms and 500K) can be used to calculate the range of frequencies that can be generated by the 555:

Cycle time = $0.7(R_A + R_B)C + (0.7 \times R_B \times C)$

If R_B is very small, the cycle time equals $1.4 \times R_B \times C$. If C is 0.1 μ F, the maximum cycle time equals 700 milliseconds to give a frequency of 0.7 hertz, and the minimum cycle time equals 0.2 milliseconds for a frequency of 5000 hertz.

The power supply for this project should be capable of supplying between 5 and 15 volts DC, and it should be able to provide at least 1 amp at 5 volts. The output should never

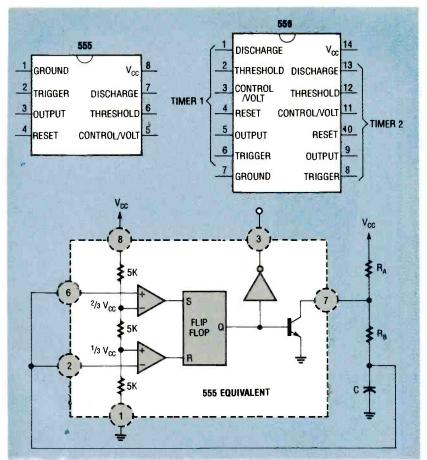


FIG. 1—PINOUTS OF THE 555 AND THE 556, and the equivalent circuit of the 555 timer.

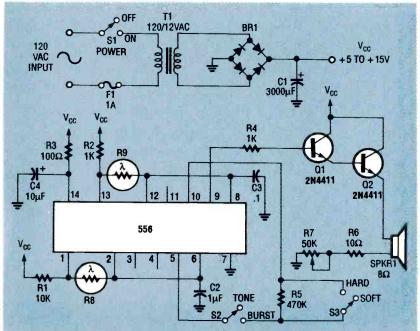


FIG. 2—LIGHT-CONTROLLED TONE-BURST OSCILLATOR. Two light-dependent resistors (R8 and R9) are used to create unusual sound effects.

exceed 15 volts under no-load conditions or else you risk damaging the circuit.

Construction

This project is very easy to build with any acceptable con-

pes, schematic, and detailed

plans for the cabinet, send \$5 to John Canivan, 20 Tyler Ave., W Sayville, NY 11796

PARTS LIST

All resistors are 1/4-watt, 5%, un-

R7-50,000 ohms, 1-watt potenti-

R9, R9-photo cells (values are not

C1-3000uF, 25 volts, electrolytic

Q1, Q2-2N4411 NPN power tran-

BR1-50 PIV 1.5-amp bridge rec-

T1-120/12VAC 1-amp power trans-

Miscellaneous: perforated construction board, enclosure, 14-pin DIP socket, line cord, wire, hard-

Note: For complete operating instructions, set of sound reci-

less otherwise noted.

R1-10,000 ohms

R3-100 ohms

ometer

critical) Capacitors

sistor

tifier

former

ware, etc.

R2, R4-1000 ohms

R5-470,000 ohms

R6-10 ohms, 1/2-watt

C2—1 μ F, 50 volts, Mylar C3—0.1 μ F, 50 volts, polyester C4—10 μ F, 50 volts, electrolytic

Semiconductors

IC1-556 dual timer

Other components F1—1-amp fuse and holder S1–S3—SPST switch

SPKR1-8-ohm speaker

struction technique. The author mounted the components on a piece of perforated construction board and wired them point-to-point. The board, speaker, transformer, switches, and photocells were then installed in a homemade wood cabinet, as shown in Fig. 3. It's best to mount the photocells at least a foot away from each other so that one hand can control frequency while the other hand controls the burst interval. This avoids having motion from one hand interfere with the other hand.

Operation

The circuit should be used in room that has plenty of overhead light, because the frequency and burst intervals are

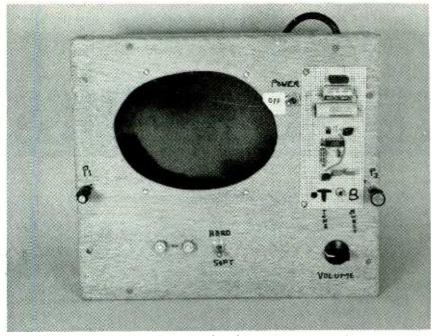


FIG. 3—THE AUTHOR MOUNTED THE COMPONENTS on a piece of perforated construction board and used point-to-point wiring. Everything was then installed in a home-made wood cabinet.

controlled by light intensity. The tone burst feature can be modified by opening and closing S3. That either makes a direct connection between the output of the burst timer and the reset of the tone oscillator, or replaces the direct connection with resistor R5 for a completely different sound effect. By opening S2, the burst feature is eliminated, and the pure tones which result can be controlled by hovering one hand above R9.

Remember that the amount of light striking photocells R8 and R9 is critical for proper circuit operation. Since the sensitivity of photo cells can vary, you should adjust the light to the range of frequencies desired. If the adjustment is not sufficient, you can adjust the range of available frequencies by changing the value of timer capacitors C2 and C3.

Sound recipes

The following is a list of different sounds you can make and instructions on how to make them:

• Police siren—Set TONE/BURST switch S2 on tone and raise and lower your right hand between 1 and 3 inches above R9, once every second.

• Old car starting—Set TONE/

BURST switch S2 on burst and set HARD/SOFT switch S3 to hard. Place your right and left hands over the photocells and raise your left hand (or whichever hand is over R8) slowly.

• Airplane starting—Set TONE/ BURST switch S2 on tone and place your right hand on photocell R9 and raise it slowly. Stop at 2 inches.

• UFO landing—Set TONE/BUR-ST switch S2 on burst and set HARD/SOFT switch S3 on hard. Raise your hands above your head and lower them slowly onto the photocells.

Birds chirping—Set TONE/ BURST switch S2 on burst and set the HARD/SOFT switch S3 on hard. Place left hand 2 inches above photocell R8. Spread the fingers of your right hand and wave them across photocell R9 at a distance of about 2 inches.
Ghosts moaning—Set TONE/ BURST switch S2 on tone and set the HARD/SOFT switch on soft. Flutter your right hand above the photocell R9 while raising it up and down between 1 and 3

 Frankenstein—Set TONE/BUR-ST switch S2 on burst and set HARD/SOFT switch S3 on soft.

HARD/SOFT switch S3 on soft. Raise your hands above your head and lower them slowly until you touch the photocells. Raise your left hand about 3 inches and then lower it to within 1 inch of the switch. At the same time, raise your right hand 3 inches. Repeat the process.

• Radiation warning—Set TONE/BURST switch S2 on burst and set HARD/SOFT switch S3 to hard. Cup your right hand 1 inch above photocell R9 and then cup your left hand about 2 inches above photo-cell R8.

• Foghorn—Set TONE/BURST switch S2 on burst and set HARD/SOFT switch S3 to hard. Place your right hand on photocell R9. Place your left hand on photocell R8.

• Smoke detector—Set TONE/ BURST switch S2 on burst and set HARD/SOFT switch S3 to hard. Place your right hand 3 inches above R9, and place your left hand 1 inch from R8.

The light-controlled tone-burst oscillator is basically a musical instrument, and the quality of sound depends on the skill and creativity of the musician. If you've ever been searching for a circuit that can create special sound effects, then this project is right up your alley. **R-E**

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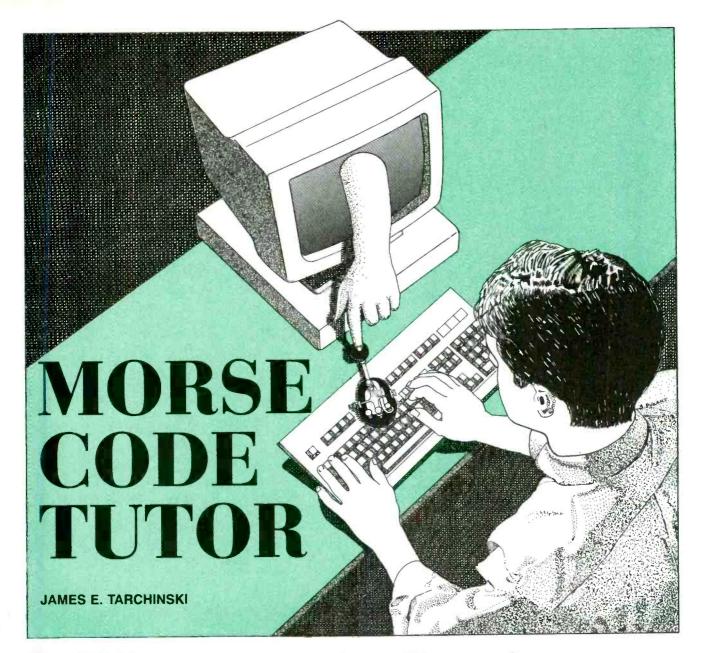
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This BASIC program can teach you Morse code or help sharpen your skills if you already know it.

WHEN TV WAS FIRST INTRODUCED. many thought it was the beginning of the end for radio—why would people want audio when they could have both audio and video? Forty years later, however, radio is still alive and well, thank you.

In this era of global communication, where voice and video signals are carried by wires, radio waves, and fiber optics, you might wonder about the usefulness of Morse code. In fact, it too is alive and well.

Many new shortwave listeners (SWLers) do not know Morse code, hence much activity in the SW bands goes uncomprehended. Even experienced SWLers have a tendency to let their code translation skills lapse over the years, making it difficult to understand MC in real time. Although the Federal Communications Commission (FCC) eliminated the Morse code test from the Technician-class amateur-radio license (**Radio Electronics**, April '91), anyone applying for more advanced license grades must still pass a Morse code test.

We have a solution to both problems: a BASIC-language program that teaches Morse code and runs on any PC or compatible. The program is simple enough to modify for other computers as well.

The Morse code program drills you in a "flash-card" manner by "beeping" and displaying an encoded character on the screen. It then waits for you to press the corresponding key. The program **69** also displays the number of correct and incorrect responses, making it easy to track your learning progress.

The program is presented in its entirety in Listing 1. You can type it in and save it to disk, or download file MCPP.BAS from the RE-BBS (516-293-2283, 1200/2400, 8N1 or 7E1).

Using the program

Run MCODE and the program should ask you to enter a random-number seed. Enter any number in the given range (-32768-32767) and the program will proceed. (The number you enter is used to initialize the computer's random-number generator so that you'll get a different series of characters each time you run the program.) A sign-on screen appears, as shown in Fig. 1; press any key to continue. Then the main menu appears, as shown in Fig. 2.

The menu allows you to choose one of four predefined sets of characters for practice, to define your own set, or exit the program. Set 1 consists of the letters A–Z; set 2, the digits 0–9; set 3, nine common punctuation marks; and set 4, all 45 letters, digits, and punctuation marks.

Table 1 shows the Morse code representation of all characters used in the program. Each section of the table corresponds to a menu item. As you may know, each Morse code character is represented by several short and long sounds (dits and dahs, respectively). In the table and on the screen, dits are represented by asterisks and dahs by dashes.

You can create your own custom character set. If you're just starting to learn Morse code, you can begin by concentrating on just a few characters, the vowels, for example, and gradually add more characters as your skills improve.

If you choose the "User definable" mode, the program allows you to enter 2–46 characters. All characters must be listed in Table 1; if one isn't, the program will crash.

After you select a mode of operation, the screen clears and enters quiz mode. The program displays an encoded character near the center of the screen and LISTING 1-MORSE CODE PRACTICE CODE

```
1000 CLEAR : DIM A$(46), B$(46): SCREEN 0, 0, 0, 0
1010 COLOR 10, 0, 0: KEY OFF: WIDTH 80: RANDOMIZE: CLS
1020 SPD = 5 'Set default sound speed: 1=slow, 20=fast
   1000 CLEAR :
   1030
  1040 PRINT *****
1050 PRINT ***
   1060 PRINT ***
                                                                      MCPP.BAS: The Morse Code Practice Program
                 PRINT ***
   1070
                                                                                                                                                                                                                                     . . .
   1080 PRINT ***
                                                                                       (c) 1988 by James E. Tarchinski
                                                                                                                                                                                                                                    * * *
   1090 PRINT ***
   1100 PRINT
  1110 COLOR 11
1120 PRINT
  1130 PRINT
1140 PRINT
  1120 PRINT " This program is designed to help you learn the Morse Code"
1140 PRINT "representation of characters. You will be given the"
1150 PRINT "opportunity to select which of five modes of operation you"
1160 PRINT "would like to utilize."
  1100 PRINT "Would like to utilize."

1170 PRINT

1180 PRINT " If you wish to change the mode of operation, or if you wish"

1190 PRINT "to exit the program, just press the 'Esc' while in Quiz Mode"

1200 PRINT "the program will return to the mode selection menu."

1210 PRINT
               PRINT
PRINT
  1220
                                           The following keys are also active in Quiz Mode:"
  1230 COLOR
1240 PRINT
1250 PRINT
                COLOR 14
                                                 F1 = Change sound speed ( 1=slow, 20=fast, default='; SPD; *)*
F2 = Toggle sound on/off*
F3 = Toggle display on/off*
F4 = Display Morse Code reference screen*
                                  .
   1260
                PRINT
  1270
1280
                PRINT "
   1290
                GOSUB 2580 'Press any key to continue subroutine
  1300
1310
  1320
                1330
  1340 KEY 1, "[": KEY 2, "]": KEY 3, "
1350 FOR I = 5 TO 10: KEY I, "": NEXT
                                                                                                             "(": KEY 4, ")"

      1360
      Image: Start St
  1410
  1420 GOSUB 2380 'Set default sound speed
1430 PT.FLG = 1: PL.FLG = 1
   1440
  1450
  1470
 1480 WIDTH 80: CLS : COLOR 10
1490 PRINT
  1500 PRINT "-=-=- MODE SELECTION MENU -=-=-=*
 1510 PRINT
1520 PRINT "Which mode would you like to use?"
1530 PRINT 'I. Alpha characters"
1540 PRINT ' 2. Numbers"
1550 PRINT ' 3. Punctuation"
 1550 PRINT * 3. Functuation*
1560 PRINT * 4. All of the above*
1570 PRINT * 5. User definable*
1580 PRINT * 6. EXIT PROGRAM*
1590 INPUT *Your choice (1-6): *, IN$: M = ABS(VAL(IN$))
 1600 PRINT
 1610 IF M > 6 OR M < 1 THEN PRINT "PLEASE ENTER A VALID NUMBER!": GOTO 1490
 1620
 1630 CLS : CT = 0: WG = 0: IF M = 6 THEN END
 1640
1650
 1660
               1670
1670 IF M = 1 THEN MIN = 1: MAX = 26

1690 IF M = 2 THEN MIN = 27: MAX = 36

1700 IF M = 3 THEN MIN = 37: MAX = 46

1710 IF M = 4 THEN MIN = 1: MAX = 46

1720 IF M <> 5 THEN 1880
1720 IF M <> 5 THEN 1880

1730 '

1740 PRINT "Enter the characters to be used:"

1750 LINE INPUT ">> "; C$

1750 MIN = 1: MAX = LEN(C$)

1770 IF MAX < 2 OR MAX > 46 THEN BEEP: GOTO 1490

1780 '

1790 J2$ = ""
 1790 J25 = --

1800 FOR I = 1 TO MAX

1810 J1$ = MID$(C$, I, 1)

1820 IF J1$ >= "a" AND J1$ <= "z" THEN J1$ = CHR$(ASC(J1$) - 32)

1830 J2$ = J2$ + J1$
1840 NEXT
1850 CS = J2S
  1860
1870 '
1880 '************ QUIZ USER ********************************
 1890
1900 KY = INT(RND(1) * (MAX - MIN + 1) + MIN): IF KY = KY.OLD THEN 1900
1910 KY.OLD = KY
1920
```

```
1930 WIDTH 40: COLOR 15
1940 CLS : PRINT "Correct: Incorrect: "
1950 LOCATE 1, 10: PRINT CT: LOCATE 1, 33: PRINT WG
1960 '
1960
1970 PT$ = A$(KY): CT$ = B$(KY)
1980 IF M <> 5 THEN 2030
1990 FOR I = 1 TO 46
2000
            IF B$(I) = MID$(C$, KY, 1) THEN PT$ = A$(I): CT$ = B$(I): I = 46
2010 2020
           NEXT I
        .
2030 PLY$ =
2040 FOR I = 1 TO LEN(PT$)
           IF MID$ (PT$, I, 1) = "-" THEN PLY$ = PLY$ + DASH$ ELSE PLY$ = PLY$ +
2050
DOTS
2060
           PLYS = PLYS + PS1S
2070 NEXT
2080
2080
2090 LOCATE 15, 16: PRINT STRING$(8, 32)
2100 LC = INT(20 - LEN(PT$) / 2)
2110 IF PT.FLG = 1 THEN LOCATE 15, LC: PRINT PT$: LOCATE 20, 1
2120 IF PL.FLG = 1 THEN PLAY PLY$ + PS2$
2130
2130 '

2140 IN$ = INKEY$: IF IN$ = '' THEN 2140

2150 IF IN$ = CHR$(27) THEN 1480

2160 IF IN$ = CHR$(13) THEN 2120

2170 IF IN$ = '[' THEN GOSUB 2280: GOTO 1930

2180 IF IN$ = ']' THEN PL.FLG = 1 - PL.FLG: GOTO 2140

2190 IF IN$ = '[' THEN PT.FLG = 1 - PT.FLG: GOTO 2090

2200 IF IN$ = ']' THEN GOSUB 2450: GOTO 1930

2210 '
2130
2210 '
2220 IF IN$ >= "a" AND IN$ <= "z" THEN IN$ = CHR$(ASC(IN$) - 32)
2230
2240 IF IN$ = CT$ THEN CT = CT + 1: GOTO 1880
2250 WG = WG + 1: LOCATE 1, 33: PRINT WG; : GOTO 2140
2260
2270
2280
2290
        290 '
2300 WIDTH 80: COLOR 10: CLS
2310 PRINT
2320 PRINT *Current Sound Speed is'; SPD; * (1=slow and 20=fast).*
2330 INPUT *New value (RETURN = no change): *, IN$
2340 IF IN$ = ** THEN 2420
2350 J = ABS(VAL(IN$))
2360 IF J < 1 OR J > 20 THEN PRINT *ENTER A NUMBER FROM 1 TO 20!*: GOTO 2310
2370 SPD = J
2380 DASH5 = *A* + $TR$(SPD)
2390 DOT$ = *A* + $TR$(3 * SPD)
2400 Ps1$ = *P* + STR$(3 * SPD)
2410 PS2$ = *P* + STR$(SPD)
2410 PS2$ = *P* + STR$(SPD)
2420 RETURN
2430 2440
       2450 2460
2460 CLS : COLOR 11
2470 CLS : COLOR 11
2480 PRINT * == MORSE CODE REFERENCE SCREEN ==*
2490 J = 1: K = 1
2500 FOR I = 1 TO 46
2510 LOCATE J + 3, K: PRINT B$(I); * *; A$(I)
2520 J = J + 1: IF J > 16 THEN J = 1: K = K + 13
2520 NFT J
2510 FOR 1 = 1
2510 LOCATE J
2520 J = J +
2530 NEXT I
2540 GOSUB 2580
2550 RETURN
2560
2570
2580
        2590
       1.
2600 LOCATE 24, 1: COLOR 15: PRINT "Press any key to continue...";
2610 IN$ = INKEY$: IF IN$ <> "" THEN GOTO 2610
2620 IN$ = INKEY$: IF IN$ = "" THEN GOTO 2620
2630 RETURN
2640 '
2650
2660 2670
       : 'I-P
                                                                                                  : 'Q-X
: '0-
                                                                                                 : 15.
2750 ' APOST. COMMA
2770 DATA *----**,*--**-
                                       HYPHEN PERIOD
                                                                       SLASH
2780 ·
2790 ·
2790 ' COLON
2800 DATA "---**
                        N SEMI-C QUEST-M UNDER-L PERENTH.
2810
2820 DATA 39,44,45,46,47,58,59,63,95,40
2840 'END OF PROGRAM
```

"plays" the Morse code representation on the PC's speaker. Next the program waits for you to press a key corresponding to the encoded character. If you choose incorrectly, you get another chance. If you guess correctly, a new encoded character is displayed. In either case, the program displays the number of right and wrong answers in the status line at the top of the screen.

You have several other options during quiz mode. You may return to the menu at any time by pressing Esc. In addition (referring back to Fig. 1), you can toggle sound on and off by pressing F2, and video on and off by pressing F3. (Of course, if you turn both sound and video off, it's going to be difficult to practice!) You can also press F4 to display a table of Morse codes. In addition, you can press F1 to vary the rate at which characters are played. The lower the number, the slower the playback speed. One other key is active: if you press Enter, the program will replay the current character.

Program description

The program consists of nine distinct sections: five major code sections, three subroutines, and one data section.

The first code section (lines 1000–1310) performs initialization chores and displays the sign-on screen.

The next section (1320–1450) initializes function key labels and reads encoding data into arrays A\$ and B\$. The A\$ array contains the encoded character data, and the B\$ array contains the ASCII equivalents.

The third section (1460-1650) displays the Mode Selection Menu and gets user input. If the user chooses item 6, the program simply ends at that point, otherwise processing continues with the next section.

Section four (1660–1870) sets up the range of characters to be practiced, and section five (1880–2270) quizzes the user. Section five actually outputs the Morse code characters to screen and speaker, collects user responses, and tabulates them. It also handles operation of the four function keys.

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*× MCPP.BAS: -The Morse Code Practice Program ×¥ ¥X (c) 1988 by James E. Tarchinski ** **

This program is designed to help you learn the Morse Code epresentation of characters. You will be given the ppportunity to select which of five modes of operation you ould like to utilize.

If you wish to change the mode of operation, or if you wish to exit the program, just press the 'Esc' while in Quiz Mode the program will return to the mode selection menu.

The following keys are also active in Quiz Mode: F1 = Change sound speed (1=slow, 20=fast, default= 5) F2 = Toggle sound on/off F3 = Toggle display on/off F4 = Display Morse Code reference screen

ress any key to continue...

FIG. 1—THE MORSE CODE PRACTICE PROGRAM signs on like this, showing keys that are active in Quiz Mode. The program is written in GWBASIC and runs on any PC compatible.

TABLE 1-MORSE CODE

| | Letters | | Numbers | Punctuation |
|--|---|--|---|---|
| A * B*** C -*-* D -** E * F *** G* H **** I ** | K -*- L *-** M N -* O P ** Q*- R *-* S *** T - | U ** V *** W * X -** Y -* Z** | 1 * 2 ** 3 *** 4 **** 5 ***** 6 -**** 7 *** 8 ** 9 ** 0 * | ,**- , *-*-* ; **** ; -*-*-* ; -*-*-* / -****-* / -**-** (-**- ***-* |

| -=-=- | - MODE SELECTION MENU |
|--------|---|
| | mode would you like to use? Ilpha characters |
| | lunbers |
| 3. F | unctuation |
| 4. f | ll of the above |
| | lser definable |
| 6.E | XIT PROGRAM |
| Your c | thoice (1-6): |

FIG. 2-THE MAIN MENU allows you to choose one of several practice sets, define your own, or exit the program.

Customization

You may wish to modify the program operation, including default speed, and whether sound and display are on or off. To modify the default speed, assign the desired value to variable SPD in line 1020, being sure that the new value is between one and twenty. To disable the display, all you have to do is set PT.FLG equal to zero in line 1430. To disable the sound, all you have to do is set PL.FLG equal to zero in line 1430.

One intriguing enhancement would be to add the ability to "play" real text and allow you to try to decipher it in real time. But that's an exercise for the reader.

| Oh. by the way: $-* - *$ | |
|-----------------------------|---|
| | |
| ** - **** - **** * ** *-* - | |
| — —* *—* *— — — *—*—*— | Ω |



The inexpensive Minute Marker can generate variableduration output pulses with selectable polarity and a wide range of time intervals.

MANY HOBBY PROJECTS REQUIRE the timing of intervals between a fraction of a second and a minute. This article describes the Minute Marker, a simple device that uses low-voltage 60-hertz AC from a power-supply transformer for synchronization. It provides a variable-duration output pulse with selectable polarity and a wide range of time intervals.

Figure 1 shows a block diagram of the Minute Marker. The power supply generates the required 5-volts DC for the circuit, and also provides a 60hertz signal for the clock generator, which generates a 60-hertz square wave. The square wave is fed to the decoder, which counts cycles and decodes the desired time interval. The output pulse generator, as you probably guessed, generates the output pulse.

Figure 2 shows the schematic of the Minute Marker. The output of transformer T1 is 12.6volts AC at 60 hertz, which is rectified by D1 and regulated by IC4, an LM7805 regulator, to provide 5-volts DC for the circuit. The unrectified AC is bandpass-filtered by R1, R2, R5, C1, and C2. Resistors R2 and R5 also form a DC-voltage divider which biases the input of Schmitt trigger IC3-a to 2.5 volts. The Schmitt trigger generates a 60-hertz square wave,

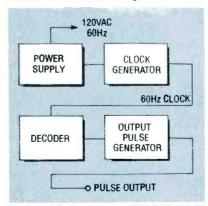


FIG. 1—MINUTE MARKER BLOCK DI-AGRAM. A 60-hertz square wave is generated from a 60-hertz signal, which is then used to decode desired time intervals. which is fed to the input of IC1, a CD404012-stage binary counter.

The outputs of the counter are decoded a 4081 quad AND gate (IC2), and the decoded output is fed back to the reset input of the counter, which resets the counter when the desired count is reached. Table 1 shows some useful time intervals that can be decoded with four decoder outputs or less; the desired outputs are simply AND-ed together. (The schematic in Fig. 2 is shown with the decoder outputs wired for a one-minute interval.)

The pulse from IC2-d is inverted by Schmitt trigger IC3-d, and passed along to the output pulse generator. The output pulse is generated by two Schmitt triggers cross-connected as an RS flip-flop (IC3-b and IC3-c). The output of the flip-flop is fed to R3, R4, and C3, whose values set the output pulse duration. The output pulse duration (T) can be approximated by the formula T =

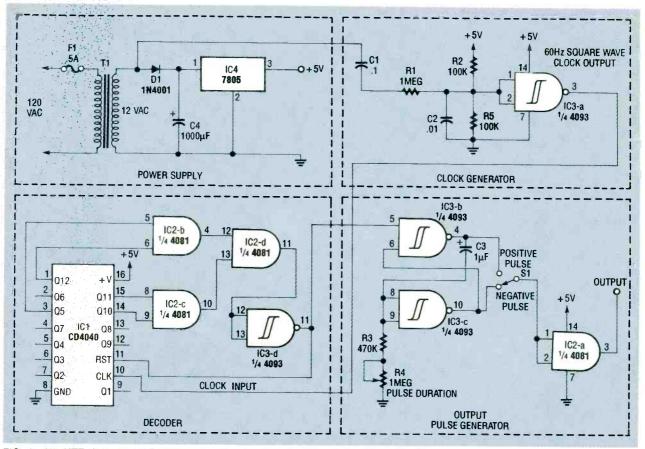


FIG. 2-MINUTE MARKER SCHEMATIC. 12.6-volts AC, at 60 hertz, is rectified and regulated to 5-volts DC for the circuit. Unrectified AC is fed into a Schmitt trigger, which generates a 60-hertz square wave. The square wave is fed to a CD404012-stage binary counter, which decodes time intervals.

PARTS LIST

All resistors are 1/4-watt. 5% R1-1 megohm R2, R5-100,000 ohms R3-470,000 ohms R4-1 megohm, potentiometer Capacitors C1-0.1 µF, ceramic C2-0.01 µF, ceramic C3-1.0 µF, electrolytic

- C4-1000 µF, electrolytic
- Semiconductors
- IC1-CD4040 12-stage binary
- counter IC2-CD4081 quad two-input AND
- gate IC3-CD4093 quad two-input
- NAND Schmitt trigger IC4—LM7805 5-volt regulator
- D1-1N4001 diode
- Other components
- F1-0.5-amp fuse
- T1-120/12.6 VAC transformer
- S1-SPDT switch
- Miscellaneous: Project case, perforated construction board, wire wrap, solder, etc

TABLE 1-TIME INTERVALS

| Interval Seconds | Number of 60-Hz Cycles | Decoded Outputs |
|---------------------|---------------------------|-------------------|
| 0.1 | 6 | Q2, Q3 |
| 1.0 | 60 | Q3, Q4, Q5, Q6 |
| 10.0 | 600 | Q4, Q5, Q7, Q10 |
| 60.0 | 3600 | Q5, Q10, Q11, Q12 |

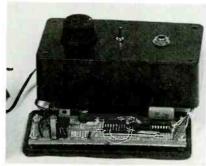


FIG. 3-COMPLETED PROTOTYPE. This circuit can generate timing intervals between a fraction of a second and a minute.

 $1.2 \times C3 \times (R3 + R4)$. A positiveor negative-going pulse is selected by S1, and buffered by the remaining AND gate (IC2-a).

Building the marker

Construction is not critical, but be careful when working with AC voltages. The circuit can be built on perforated construction board using point-topoint wiring. The selected time interval can be hard-wired to IC2, or you can use a DIP switch or header to make changing the time interval easy. The outputpulse duration and polarity can be left adjustable, or the polarity can be fixed, and R3 and R4 can be replaced with a single resistor to suit a specific application. Figure 3 shows the author's completed prototype installed in a common plastic hobby case. Ω

Cold-fusion update, a \$39 laser pointer, video driver circuits, computer I/O boards, and transmission line use.

DON LANCASTER

always like to look for unusual or controversial topics—mostly because they are there, I guess. In past issues, I have looked into such genuine scientific wonders as sonoluminescence, aerogels, magnetic refrigeration, and solitons, and at such pseudoscience subjects as perpetual motion, UFO resources, and dowsing. Today, there's one topic that seems neither fish nor fowl. So I guess its time to ask...

What ever happened to cold fusion?

The answer to this one depends on whom you ask. So, I will give you several current points of view and let you draw your own conclusions. You will find a summary in Fig. 1.

Many thousands of individuals and hundreds of firms worldwide tried the cold-fusion experiments. But after some early excitement, most of them were unable to reproduce the results claimed.

At the very least, cold fusion is now clearly in chaotic disarray. Several leading scientific journals refused to publish anything on cold fusion. Prevailing opinions are widespread that cold fusion is simply *pathological science* in which most researchers see anything they want to. Just like that *polywater* fiasco a few decades back.

It is another example of what research insiders call the *Utah Effect*. Clearly, a lot of people learned the hard way that calorimetry is a very precise science—one that involves a lot more than glancing sideways at a thermometer.

Your best starting place for obtaining information on cold-fusion is a critical summary review in the January 7, 1994 *Science* on pages 105 and 106. Of the five major books on this topic, the latest and the best appears to be *Bad Science: The Short Life and Weird Times of Cold* Fusion by Gary Taubes.

On the other hand, the cold fusion research continues—mostly by highly vocal mavericks who are well out of the scientific mainstream; they are often discredited out of hand by *Big Science* establishment people. At times unfairly and unreasonably. Further developments in this work is likely to show up in *Cold Fusion Times* or in *Cold Fusion Magazine*.

My own view is this: Yes, there seem to be real circumstances in which excess heat *appears* to result from lab experiments. But, no, I have not seen so much as one credible shred of evidence that a new atomic process is responsible.

I think that the excess heat created in most cold-fusion experiments is caused by bad labwork. Several mundane explanations should eventually crop up for the others. None is likely to lead to a new or useful energy source.

For instance, a little noted paper cropped up in *Science* smack in the middle of the cold-fusion fiasco. A Bell Labs researcher figured out how to make a fuel cell that *premixes* the gasses. This is now thoroughly verifiable, but was previously thought impossible. His work looks amazingly similar to the cold fusion setups that the researchers are now using.

Transmission line review

At DC, audio, and other low frequencies, you can usually assume that a signal identical to the one you send into one end of a wire will ar rive at the other end instantaneously. Cables are used primarily for their shielding effects.

Video and RF users do not have this luxury. Instead, they must use *transmission lines*. In a transmission line, a signal is sent from one end of a cable so it can arrive somewhere else sometime later. If you are not *very* careful with your transmission lines, you can end up with reflections, echoes, or standing waves. At best, these effects can badly distort the signal you are trying to transmit, or change the signal size and waste delivered power. At worst, they can literally destroy a high-power transmitter.

When do you need to worry about transmission lines? In addition to radio and video uses, they also become important in networks, in SCSI communication, and even in routing address and data lines on high-speed computers.

The rule is this: Use transmission lines if the distance from the signal input to the output exceeds one tenth of a wavelength at the highest frequency of interest. Another rule: Electrical signals travel about a foot per nanosecond in free space, or about eight inches per nanosecond in most wires.

Let's say you have a lossless coaxial cable that is so long that you don't have to worry about what is coming out at the far end. A cable is an example of a *distributed* network, where all the inductance and the capacitance will change in small increments. The *lumped* or *discrete* model of Fig. 2 describes it.

But you can't just analyze this model as a plain old network. Instead, you must apply the differential equations of a propagating wave. When you use this advanced math to calculate the input impedance of your cable network, you'll find an amazing result. You end up with an input impedance that looks like a pure resistor of constant value, over all frequencies. This is called the characteristic impedance of the cable. As far as the source is concerned, it looks and behaves just like a real resistor-as long as our uniform cable is so long that no energy ever returns from the far end.

The characteristic impedance of free space is 377 ohms. All cables have values lower than this. Twin lead has a value of 300 ohms. Cable TV and most video cables have a Z of 72 ohms. Hams and broad-casters typically use 50-ohm cables. Lower impedances are pre-ferable for higher powers.

Since any infinitely long length of cable looks like a resistor, we can replace any portion of it with a real resistor. This is known as properly *terminating* a cable. One rule is that all cables must be properly terminated in a resistor whose value equals its characteristic impedance! Another rule is: always use cables in a series daisy chain, going from unit to unit, with only the farthest unit terminated. Never connect cables in parallel or in any star arrangement unless each one has its own distribution amplifier.

What happens if you forget to terminate a cable? Assume you have an ultra-short cable and you purposely short circuit its far end. The

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input still looks like a short circuit. The signal goes to the end, bounces off the short circuit and returns, almost immediately.

Things get interesting in a big hurry if the cable is longer. The *time delay* of the cable causes a *phase shift* in the return signal. If you have a cable exactly one-half wavelength long, the short circuit returns to the input as a very *high* impedance. Looking at things another way, the incoming signal and the returning signal cancel each other out.

You can also prove that, in a cable exactly one quarter wavelength long, the end short circuit will appear at the input as the characteristic impedance. Thus, any dead short circuit one quarter wavelength away will appear as a properly terminated cable—but only for one specific frequency.

The same statement applies for an open termination, except that an open circuit will appear as a short a half wavelength away and appear as the characteristic impedance a quarter wavelength away.

You can't have a true open termination on any cable in the real world. In fact, *any* mismatch in a cable termination will reflect some energy and create *standing waves* along the cable. The strength of these standing waves is described by the *voltage standing wave ratio*, or VSWR. The ideal VSWR value is 1.0, meaning the line has no standing waves.

A higher VSWR limits the power that can be delivered to the load. It also causes excessive voltages and currents along the cable. At worst, it can make the input look like a short circuit and overload the source---or even destroy the transmitter. A mismatched antenna will result in a high VSWR.

So, if your main goal is delivering a signal to a load, you must terminate the cables properly. On the other hand, you can purposely exploit shorted cables as very high Q circuit elements. Cables that are shorter than a quarter wavelength look like inductors. Cables that are longer than a quarter wavelength, but less than half a wavelength, look like capacitors. A half-wavelength cable looks like an open circuit, and the cycle repeats for longer distances.

Purposely mismatched endshorted cable stubs can be used for tuning, impedance matching, trapping, and filtering. At higher frequencies, you can obtain those

I/O INTERFACE CARD RESOURCES

Aptix

2890 N First Street San Jose, CA 95134 (408) 428-6200

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1381 Saratoga Street Minden, NV 89423 (702) 267-2704

Blue Earth

 165 West Lind Court Mankato, MN 56001
 (507) 387-4001

Circuit Cellar

4 Park Street Ste 20 Vernon, CT 06066 (203) 875-2751

ComputerBoards

125 High St Mansfield, MA 02048 (508) 261-1123

Data Translation

- 100 Locke Drive
- Mariboro, MA 01752 (617) 481-3700

Industrial Computer Source PO Box 23058 San Diego, CA 92193

(800) 523-2320

Intelligent Instrumentation 1141 W Grant Road, MS131 Tucson, AZ 85705 (602) 623-9801

, IOtech

25971 Cannon Road Cleveland, OH 44146 (216) 439-4091

Keithley

440 Myles Standish Blvd Taunton, MA 02780 (800) 348-0033

»National Instruments

6504 Bridge Point Parkway Austin, TX 78730 (800) 433-3488

PAIA Electronics 3200 Teakwood Lane Edmond, OK 73013

(405) 340-6300

3805 Atherton Rd Rocklin, CA 95765 (916) 624-8333

Pro-Log Corp

.

590 - 487

2555 Garden Road Monterey, CA 93940

(408) 372-4593

values from a *Smith Chart* available on *GEnie* PSRT as file #367 SMITHCHT.PS.

Video Op-amps

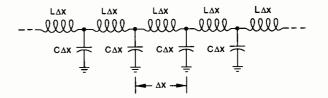
Most video cables require proper termination. The rule is that five or more feet for high-quality videocable and twelve or more feet for TVquality signals *must* be properly terminated at the far end of the cable and *only* at the far end. Once again, video cables *must* be daisy-chained unless each has its own distribution amplifier. Midpoints on the cable string must *not* be terminated. Usually a "high-Z" switch on your monitor (or whatever) gives you this choice.

What driver impedance should you use on your cable? If the far end is terminated properly and there are no standing waves, there will be nothing to reflect from the near end. Theoretically you could drive your cable from any impedance source. If you are delivering high power to a radio transmitter, for example, your obvious choice is to make the source driver impedance as *low* as possible to maximize efficiency.

Much of today's video is distributed by a different scheme called *back termination* (see Fig. 3). With back termination, the cable is driven through of a series resistance equal to the characteristic impedance. This further helps to cancel any reflections, and also provides the optimum maximum power transfer. As a side benefit, back termination also protects the driver against shorted cables.

But, there is a minor "gotcha" with back termination. Half the power is consumed in the input resistor. And, because of the voltage divider, you get only one-half the

Any long and lossless transmission line (or coaxial cable) forms an example of a distributed network, made up of many tiny series inductors of L Henrys per unit length and shunt capacitors of C Farads per unit length...



You cannot simply analyze this as a low pass network; instead you have to take a tiny piece from the middle and ask what happens as a wave passes through it. Doing this leads to a messy differential equation. In the solution, the design factor $\sqrt{L/C}$ pops up in several places.

Specifically, the velocity of the wave turns out to be $1/\sqrt{L/C}$ meters per second and the impedance of the rest of the cable will turn out to be exactly $\sqrt{L/C}$ Ohms. A *constant* resistance that is *independent* of frequency.

This magic resistance value is called the *characteristic impedance* of the cable. To a source driver, a very long or otherwise properly terminated cable will appear the same as a physical resistor of equivalent value.

For cables to work properly:

- (1) All cables MUST be terminated in their characteristic impedance at their far end.
- (2) Cables must NEVER be used in parallal or in a "star" configuration. Unless they have separate drivers.
- (3) Cables may be daisy chained from one point to another. But they must NEVER have mid-line terminations.

FIG. 2—Some transmission line and coaxial cable fundamentals.

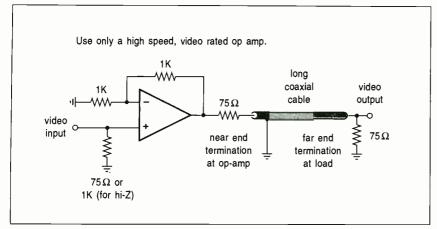


FIG. 3—"Back termination" is a popular method for driving video cables. It is shortcircuit proof and minimizes reflections, but an amplifier with a gain of at least +2 is needed. Any unterminated outputs could be badly overloaded..

NAMES AND NUMBERS

Analog Devices PO Box 9106 Norwood, MA 02062 (617) 329-4700

Burr-Brown

6730 S Tucson Blvd Tucson, AZ 85706 (602) 746-1111

C Users Group

1601 W 23rd St Ste 200 Lawrence, KS 66046 (913) 841-1631

Fire Engineering PO Box 1289 Tulsa, OK 74101 (918) 835-3161

Firefighters Bookstore

18281 Gothard No.105 Huntington Beach, CA 92648 (800) 727-3327

GEnie

401 N Washington St Rockville, MD 20850 (800) 638-9636

Hewlett-Packard PO Box 10301

Palo Alto, CA 94303 (415) 857-1501

Linear Technology 1630 McCarthy Blvd Milpitas, CA 95035 (408) 432-1900

Maxim 120 San Gabriel Drive Supparalo, CA 94096

Sunnyvale, CA 94086 (800) 998-8800

signal level at the far end of the cable. To overcome this, you should set up a video distribution amplifier

S AND NUMBERS

Metrologic Coles Road \$AK Route 42 Blackwood, NJ 08012 (800) ID-METRO

Motorola

5005 E McDowell Road Phoenix, AZ 85008 (800) 521-6274

National Semiconductor 2900 Semiconductor Road Santa Clara, CA 95052 (800) 272-9959

RF Micro Devices 7341-D West Friendly Ave Greensboro, NC 27410 (910) 855-8085

Science 1333 H Stree

1333 H Street NW Washington, DC 20005 (202) 326-6400

Siemens Componants 2191 Laurelwood Boad

2191 Laurelwood Road Santa Clara, CA 95054 (408) 980-4500

Small Parts

PO Box 4650 Miami Lakes FL, 33014 (305) 557-8222

ST Publications

407 Gilbert Avenue Cincinnati, OH 45202 (513) 421-2050

Synergetics

PO Box 809 Thatcher, AZ 85552 (602) 428-4073

with a gain of +2 or higher. The amplifier *doubles* the signal level. The back termination resistor cuts

the signal back down to size. When using back termination, you also must be sure you terminate the far end of the cable. Otherwise, your video levels will be far too high, and might overload your equipment.

Video distribution amplifiers are common these days. *Radio Shack* offers several off-the-shelf models. But it is tricky to make one that works without a negative power supply.

Suitable video driver chips are now available from *Maxim*, *National*, *Burr-Brown*, *Linear Technology*, and *Analog Devices*, among others. My favorite is *Maxim*, which gives away lots of free samples.

National also has some samples available of its new LM6181 highperformance video op-amp. This one uses current, rather than voltage feedback, to give you a 50megahertz back-terminated bandwidth plus a 2000-volt-per-microsecond slew rate. A demonstration circuit board is also offered (see Fig. 4). This one is also an excellent plug-and-go video driver. It also lets you evaluate competing op-amps. Both the chip and the evaluation board are available free to qualified persons. National's technical support is provided via (800) 272-9959.

"Forgotten Lore" contest

Let's have a different kind of contest this month, one that's especially good for old timers. Just tell us about some long forgotten electronics lore—tips and techniques that fell through the crack somewhere along the way, but still remain useful.

For instance, there's not too much point in reminding people that they can service a classic record changer outside of its case by setting it on three quart-size ginger-ale bottles. But these three tips still are very useful: (1) A tiny amount of beeswax on a screwdriver tip makes a very useful screwholder; (2) One single thread from a pad of No.000 steel wool might replace the superexpensive and hard-to-find low-amperage fuses for protecting microammeters; and (3) A neon test light still makes a great "hot chassis" tester. Just hold one tester lead and touch the other one to the suspect area. If the lamp lights dimly, you

have located a hot chassis and a severe shock hazard.

There will be a dozen of the usual *Incredible Secret Money Machine II* books going to the better entries, with an all-expense-paid (FOB Thatcher, AZ) *tinaja quest* for two going to the very best of all. Be sure to send all of your *written* entries to me at *Synergetics*, rather than to Electronics Now editorial.

A \$39 laser pointer

I've been waiting several years for the price of laser pointers and their solid-state laser diodes to drop. It seems that *Metrologic* has turned the corner with a complete and ready-to-use 3-milliwatt laser pointer for \$39 (Model ML-211). At long last, no-nonsense lasers for hacking are available at low cost in quantity.

The spot size is about a half inch at thirty feet. Presumably the beam could be further collimated with external lenses. The 675-nanometer red light is visible in bright daylight. Feedback stabilization permits maximum safe output. Battery life is eight hours continuous with a pair of alkaline AAA cells, and much longer with lithium cells. A safety slider on the pocket clip prevents unintended use.

My only complaints are that the delivery was very slow and that the batteries wobble in the case. This is bound to cause damage when the unit bounces around for months in, say, a toolbox or glove compartment. A strip of cloth cures this.

Yes, you can do all the usual "red string" laser stuff. But forget about holography. First, there isn't enough power. And second, the light beam almost certainly operates in the higher-order optic modes, so the light isn't totally coherent. Monochromatic yes, coherent no.

The brightness of the laser pointer should be more than enough for most uses. But as a fireman, I was disappointed by its fireground performance. It turns out that a freshly burned black is black indeed, and it simply does not reflect light. One possible solution would be a pushbutton higher-power mode.

A dozen experiments are described in a pamphlet supplied with the pointer. Obviously, you can

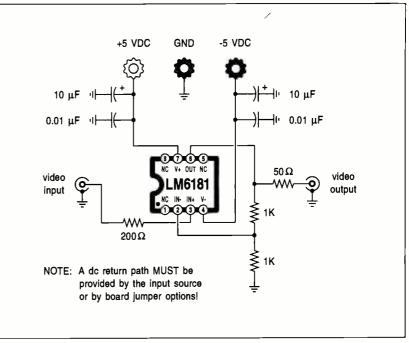


FIG. 4—National Semiconductor's high-speed op-amp evaluation board can be used as-is as a superb video cable driver. It is also very handy for op-amp testing.

strap this onto a level or bounce it off a mirrored loudspeaker. My favorite is annoying cats. It drives them bonkers in a darkened room.

Computer I/O interface

A lot of construction projects published in this magazine are those that plug into your PC or other computer and give you real-world I/O. Two other good sources for computer interfaces include John Bell Electronics and Circuit Cellar.

There are also many commercial I/O card offerings. There are cards that do data acquisition, A/D or D/A conversion, signal conditioning, and power interfacing. While these cards are expensive, they are plug-and-go and usually include warranties, technical help, and software.

For this month's resource side-

| â | NEED HELP? |
|------|---|
| | ne or write your Hardware ker questions to: |
| 4 · | Don Lancaster Synergetics Box 809-EN Thatcher, AZ 85552 |
| | (602) 428-4073 |
| (800 | fast PSRT access, modem)) 638-8369, then an HHH. n XTX99005,SCRIPT. |

bar, I've gathered together the names of a few of the major players in the industrial PC I/O arena. Most of them offer fat and free catalogs that include useful application notes and other technical information.

New tech lit

From Siemens, there's a new Hall Effect Integrated Circuits Data Package on automotive applications. And from RF Micro Devices, there's a new RF and Wireless Comm data book.

Motorola has two free directories: a Technical Literature Guide and Applications Literature Guide.

There's a new catalog from *Small Parts.* It's an essential source for everything your hardware store never heard of, besides being the greatest hacker robotics store in the world. Small Parts also custom shapes metal and plastic.

There are two other special interest bookstores: *The Working Library* by *ST Publications* on screen printing, sign painting, graphic layout, neon, and pinstriping, and the *Firefighter's Bookstore* on fire science books and videos. Of the dozens of firefighting trade journals, I like *Fire Engineering* the best.

Hundreds of C language publicdomain software programs are now offered by the C User's Group.

Hewlett-Packard has just started shipping out its new LaserJet 4M+ printer. At a first glance, this one looks like a routine upgrade with a few minor improvements. It includes genuine Adobe PostScript Level II, a bolt-on-duplexer, enhanced 600 DPI resolution, 12 pages per minute, refillable cartridges, all service manuals available, efficient memory, multiple trays that can hold nearly a thousand pages, and stunning new photo grays. All at an \$1800 street price.

All of a sudden, this is the machine that will *completely* blow away ink-based black-and-white jiffy printing. At least for 5000 or fewer copies, this new printer gives higher quality at lower cost than ink printing. The photo grays must be seen to be believed. There are 120 gray levels at 106 spots per inch.

A major threshold clearly has been crossed with this machineone that opens up an incredible number of new hardware hacking opportunities. A new era has clearly been defined in which you could publish your own top-quality books from home, right off your own kitchen table.

The only negative on the 4M + isits appalling lack of a supporting hard disk. But such a serious omission almost certainly will soon be fixed. You can temporarily work around this omission by the sneaky use of full-page PostScript forms. Additional information and support on this incredible new machine is on GEnie PSRT and in my Book-ondemand Resource Kit.

For most hardware hackers most of the time, any patent involvement is absolutely certain to result in a net loss of time, energy, money, and sanity. Thoroughly tested real-world alternatives appear in my Case Against Patents package, which also includes my Incredible Secret Money Machine II as a bonus book. See my nearby Synergetics ad for detail.

A reminder that ten free hours of GEnie use are still available, per our "Need Help" box. As usual, most of the resources I've mentioned appear in the Names & Numbers and Computer I/O Resources sidebars. Be sure to check here before calling our no-charge technical helpline. $\hat{\Omega}$

WHAT'S NEWS

continued from page 10

movable lens on the drive's laser can be focused to "read" only one disk at a time while ignoring the others in the stack. This ability to focus the beam permits IBM to stack up to 10 layers in a single disk assembly. However, the writing format is the same as that on single disk CDs. The concept is shown in the figure.

IBM researchers say that a 10layer disk will store about 6.5-million bytes of data, the equivalent of more than a million pages of printed text. The disks are made by stacking disks on top of each other and bonding them together with spacers that provide a gap between each layer. Data can be stored on the surface of any disk within the stack. The surface to be read or written to is selected by moving the optical disk drive's focusing lens up and down.

The maximum number of disks in a stack is limited by the power of the laser, the transparency of the layers, and cost of manufacturing the assembly. Writable disks will have fewer layers because the writing process requires that the disk material absorb some of the laser light. IBM has demonstrated two-, four-, and six-layer read-only disks and two- and four-layer write-once disks.

The IBM scientists do not think that commercial manufacture of drives based on multilayer CDs will be challenging. They say that today's CD drives have movable lenses that can compensate for any warpage in the disks that are spinning under them. However, modifications on existing CD players would be required before the drives can accommodate multilevel disks.

On the other hand, they say that drives built specifically for the stacked CDs will be compatible with and able to play existing single-disk CDs. It could take IBM two years to bring out a commercial version of the multilevel system.

Meanwhile, other companies are working on other methods for increasing the capacity of CD-ROM drives. Philips, for example, is working on a method that will allow disks to hold four to seven times more data than existing disks. Ω

VIDEO NEWS

continued from page 6

trucks? All of the schemes for electronic delivery and inventorying have fallen apart in the past. Now, one is actually in progress.

It took a major power in retailing-Blockbuster Video-to get the tests moving. Sega is participating in those tests, which initially will deliver electronic games to the Blockbuster stores.

Some 10 to 15 Blockbuster stores will participate in the test, which should last two to four months. Although details haven't been announced, a full library of cartridge games might be transmitted and stored on a local server. Each title could be downloaded by the customer in as little as 20 seconds from the in-store server.

Although the system initially would be aimed at supplying rental customers with the latest "hot" video games, it might also be applied to sales of games. Under one scenario, a customer could buy a reprogrammable cartridge for slightly more than a standard one and have it rewritten later with the next hot game for less than it would cost to buy a whole new game cartridge. The same system will be tested for music cassettes, but that test has been delayed because of copyright problems.

 Japan studies digital **HDTV.** Although the revelation several months ago that Japan might abandon its analog, high-definition TV system caused a hysterical reaction, NHK, the Japan Broadcasting Company, has announced a study group on digital HDTV without causing any riots, or even adverse comments. NHK softened the blow by saying that it would be well into the 21st century before digital HDTV could be implemented. They want to wait for simple and inexpensive consumer converters to become available.

At the same time, NHK's research lab announced it would have a 50-inch, thin, color-plasma display ready for public demonstrations in time for the Nagano Olympics in 1998. Ω

- special project

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Are you interested in helping us make this magazine as good for you as it can be? Then be one of the first to join the 1994 *Electronics Now Reader Council.* Twice a year you'll be asked to complete a detailed questionnaire. It will tell us about the things in this magazine that are important to you and give us the information we need to make this your best possible reading.

If you would like to be considered for this special *Electronics Now* project, take a few minutes to answer the questions on this page and return it to us.

While we cannot accept everyone, we will randomly select our participants, giving each one of you an equal chance of being selected.

Please mail the completed questionnaire no later than November 30, 1994, to:

Total Recall Research Group Box 4079 Farmingdale, NY 11735-9622

Thank you, and I am looking forward to hearing from you!

Larry Steckler, Editor-in-Chief

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- 10. If you were the editor, would
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Longer Shorter More build it Less build it More how to Less how to

- 11. What articles would you publish?
- 12. What new columns would you add?
- 13. What else would you change? Use a separate sheet for your comments. Please give as much detail as possible.

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September 1994, Electronics Now

AUDIO UPDATE

The joys of audio clipping

here's a kind of clipping that I, not my amplifier, have been engaged in for several years. I refer to my compulsion to cut out and put aside news items of audio interest for reference or possible use in this column. Unfortunately, in my filing system, any given clipping might end up on top of or behind a bookcase, on a coffee table, on the floor of my office, or-courtesy of the cleaning lady-in a wastepaper basket. The problem is brought on not by my sloth and lack of organization-although these factors could play a role—but by the sheer influx of printed matter coming my way. (Reader mail frequently is not answered for the same reason, or for lack of a stamped, self-addressed envelope, and for that | apologize.)

I am sometimes tempted by a Monty Python suggestion for coping with paper floods: Get a goat. The animal's digestive system would provide an ecologically correct disposal solution to the paper influx and, coincidentally, a ready source of fertilizer for my wife's herb garden. In any case, a 24-hour search of my premises has turned up the following comment-worthy items of interest.

Akihabara angst

In my half dozen or so trips to Japan starting in 1972, I visited a wonderful melange of shrines, electronics factories, temples, parks, retail establishments, and cultural centers. My two favorite places, to which I returned whenever possible, were the Zen temples in Kyoto and the electronics shops in the Akihabara district in Tokyo. Food for the mind and hobby.

As an adolescent, I haunted the Cortlandt Street electronics area in downtown Manhattan. Dozens of radio-parts stores that sold new, used, and surplus equipment filled the narrow streets where the World Trade Center's dual towers now



FIG. 1—AN AKIHABARA PARTS counter display.

stand. The Akihabara is everything Cortlandt Street ever was—and far more! During the years when the dollar was worth two or three times in yen what it is today, I could barely restrain myself. Since my position at *Stereo Review* provided all the conventional audio equipment I could use, I loaded up with watches, tools, electrical fixtures, electronic parts, and audio accessories not available in the U.S.

But it wasn't just the bargains, it was the ambiance of the place that turned me on. Dozens of audio, appliance, and hardware discount stores competed with hundreds of little arcade stalls, each displaying tastefully arranged selections of switches, resistors, capacitors, jacks, plugs, semiconductors, and so forth. It was a hobbyist's dream, even if the counter displays frequently resembled gigantic electronic sushi platters.

The international section of *The New York Times* reported that early witnessing is evolution, rather than extinction. But for purely sentimental reasons, I would hate to see the old-fashioned Akihabara area go the way of Cortlandt Street.

LARRY KLEIN

Mental Mozart

My musical tastes have always been somewhat eclectic and, in a sense, dated. As far as popular music is concerned, I seem to be stuck in the Sixties along with The Doors, Jefferson Airplane, Cream, and Moody Blues. My classical tastes go even further back, with a heavy concentration on Baroque in general, plus Beethoven and Mozart. Modern music, of any persuasion, seldom tickles my fancy.

For several reasons I was fascinated by a recent item in the science section of *The New York Times* about a series of experiments conducted on 36 students at the University of California at Irvine. It turned out that listening to 10 minutes of Mozart's piano music significantly raised the scores on IQ tests of spatial reasoning. Tests given immediately after the Mozart listening sessions showed an average improvement of 9 points over scores achieved when the same students listened to a 10-minute relaxation tape. (Fundamentalist audiophiles might be concerned about whether the music was in digital or analog format, but I have no relevant information other than that the piece was Mozart's "Sonata for Two Pianos in D Major" performed by Perahia and Lupu.) Interestingly, the Mozartian magic seemed to work whether or not the students even liked the music.

Aside from the doctorates of the researchers, several factors seem to raise this study above the Weird-Science category. For one thing, their working hypothesis seems reasonable. Researcher Dr. Frances H. Rauscher explained that the experiments are testing a neurobiological model of brain function that postulates certain neural firing patterns in the brain. Those patterns might be common in certain activities-chess, mathematics, and listening to certain kinds of music. Mozart was picked because the complex, highly structured, and non-repetitive character of his compositions might stimulate neural pathways important to cognition. Further testing is planned to evaluate the effects of rock and contemporary minimalist music.

I'm surprised that no one seems to have thought of testing the potential positive effects of pulse trains generated by a random-number function-generator. Perhaps it should have been mentioned earlier, but any IQ improvement that occurs is only temporary. You can cancel your trip to the CD dealer if you were looking for a permanent Mozartian mental fix. Sorry about that!

Inner-ear outage

As if we don't have enough eardamaging sound levels in our environment, a new source of hearing problems has been discovered. The new causal agency is not the old villain, long- or short-term acoustic overload, but rather the result of physical-impact damage to the mechanisms of the inner ear. Couch potatoes have nothing to worry about, but those who are aerobically obsessed and regularly bounce about in local gyms, or who are involved with long-distance running or other jarring activities, could end up with persistent dizziness, unsteadiness, vertigo, motion sickness, ringing, or "fullness" in their ears-and last, but not least, high-frequency hearing loss.

How do all these difficulties come about? According to Dr. Michael I. Weintraub, a clinical professor of neurology at New York Medical College, repeated jarring tends to loosen the tiny granules called otoliths found in two chambers of the inner ear. They are part of a sensing system that provides data to the brain about the body's spatial orientation-which is why inner-ear infections sometimes cause dizziness. When the otoliths are shocked out of place by a blow to the heador continuous high-impact aerobics-they send confused positional signals to the brain, resulting in one or more of the symptoms described above.

Dr. Weintraub estimates that perhaps 20% to 25% of those who are aerobically involved might end up with otolith-impairment symptoms. He also found that 67% of those with such symptoms also had tinnitus (ringing) or a "full" or muffled sensation in their ears. In addition, over 80% of the instructors and 60% of their students had high-frequency hearing loss. I asked Dr. Weintraub about the nature of the HF loss, and he said that it was actually a notch at about 6 kHz, which is typical of hearing damage brought on by exposure to continuous high sound levels. He suspects that the problem is not the high impacts per se but rather the volume of the music typically played during classes. It seems that if your otoliths don't get you, your cochlea's hair cells will.

The good news that not everyone is susceptible to otolith impact is offset by the fact that the problems can take years to develop. The cumulative damage factor is insidious in that significant inner-ear damage can occur before the symptoms become bothersome and perhaps even become irreversible.

What does it mean philosophically when the pursuit of good health might make you deaf and/or dizzy? I don't know, but I think I'm going to lie down now.

S NEW BOOKS for the Project Builder



I

BP350—ELECTRONIC BOARD GAMES .. \$6.00 Twenty novel electronic board games that you can build from the plans in this book. Whether you are interested in motor racing, searching for buried treasure on a desert island or for gold in Fort Knox, spinning the

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From installing a TV or FM antenna to setting up a multi-antenna array for shortwave listening or amateur radio, this book explains the basics of VHF and UHF antenna operation and installation. The

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DRAWING BOARD

A different tachometer design approach.

ROBERT GROSSBLATT

f you've been following this series on building a tachometer and have breadboarded the PLLbased design, you probably have found that it's difficult, if not impossible, to find loop-filter component values that will generate reliable tachometer performance from idle to red line. Most commercial tachometers based on this design have circuitry to automatically switch the loop components as the engine rpm crosses one or more boundary values. If you're determined to use a PLL-based design, you'll probably have to do something similar.

Working out the details of a switching circuit based on engine rpm isn't the kind of thing you can do between breakfast and lunch. Before you do it, follow along here for a while as I go through the alternate design I described before. The hardware might be a bit more complex, but it's much less susceptible to bobble (fluctuation of the digits) than the PLL-based tachometer.

The basic approach to the design is shown in the block diagram of Fig. 1. The fundamental operating principles are simple. The number of high voltage pulses coming from the coil are counted for a precise time period. Then that number (sparks per precise time period) is used to calculate the rate in revolutions per minute. The traditional drawback of a design like this is that by multiplying the spark rate, you also multiply the differences between each successive sample This causes an unacceptable amount of bobble in the final display.

This problem can't be ignored, and there are three basic ways to solve it. The optimum solution depends how the circuit is going to be used. In no particular order, the ways around the problem are:

1. Increase the sampling period.

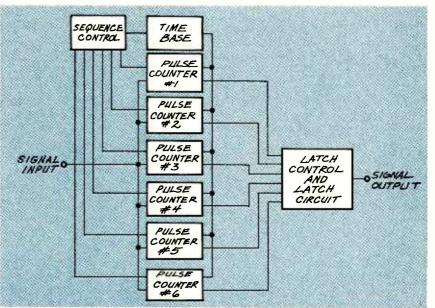


FIG. 1—BASIC TACHOMETER DESIGN. The number of high-voltage pulses coming from the coll for a precise time period is used to calculate the rate in revolutions per minute.

2. Limit the allowable variation between successive samples.

3. Increase the number of samples in the sampling period.

By increasing the sampling period, you're enlarging the statistical universe and, as you would expect, this will smooth the differences between successive samples. If you increased the sampling to a minute, you would be measuring rpm directly. The downside of doing this is, as you probably realize, the display update will be terrible-it would change only once a minute. Since the tachometer should supply meaningful information in real time, any update rate greater than one second is unacceptable.

Limiting the allowable variations between successive samples is a reasonable way to eliminate display bobble while still keeping the update rate at a reasonable interval. This is the kind of thing that is usually done in microprocessor-based designs because it's pretty simple to implement with a couple of lines of code in the software that drives the circuit. While it's possible to do the same thing in a hardware-only circuit, the design considerations are more complex.

If the number of samples per basic counting period is large enough, you can do some gross smoothing by ignoring a couple of the least significant bits. In the case of a tachometer, even an eight-cylinder engine produces only 200 sparks per second at the coil at 3000 rpm, so there's not much room for dropping low-order bits from the count. You really need more than eight bits of data to be able to get away with something like this.

If there's some way to do it, increasing the number of samples per sampling period is the best way to enlarge the statistical universe but, sad to say, short of adding a cylinder or two your engine, there's not much you can do to increase the number of sparks. The pulses from the center-coil pole of the distributor provide as rapid a spark rate as you can get.

So now that each of the three potential solutions has been ruled out for one reason or another, let's come up with another solution.

The statistical sample can be increased without shortening the update rate by using more than one counter to total up the number of samples. That's the basic idea behind the block diagram shown in Fig. 1. Each counter (I've shown six of them, but you can use as few or as many as you like) is fed with the conditioned coil input and it keeps track of the number of pulses. At the end of the update period, the count in one of the counters is sent to the section of the circuit that calculates engine rpm. Immediately after reading the number stored in the counter, the counter is cleared and it starts totaling the coil pulses again.

At the end of the next update period, the same operation is done with the next counter in sequence. This whole operation is controlled by a sequencing circuit that accesses each counter in turn and also opens and closes the latch that holds the spark count for processing before it reaches the circuit for display.

This design approach eliminates the problems stemming from too small a sample. It also permits a short update period so that the information from the tachometer is meaningful. The tachometer will base it's calculation on the last several seconds of engine rpm. If the circuit has an update period of a half a second, and the counters keep a running count of the last three seconds worth of engine pulses, whenever the display is updated, the circuit will drop the oldest half-second pulse count and add the next one. In this way, the display will always show the average rpm from the last three seconds of the engine's activity.

The circuit details for a tachometer like this are not really very difficult. The design is complex, but the basic elements are things that we've done together many times

CL-A VCC 57-A EN-A 5 QI-A 6 DZ-A 02-B 7 @2-A 8 D3-A 9 03-A 10 D4-A 11 Q4-A 12 CL-B GND 16 CLOCK(A) Vcc ENABLE(A) RESET(B) QO(A) 03(B) QI(A) QUE 520 Q2(A) QI(B 6 Q3(A) OO(B) 7 RESET(A) ENABLE(B) 8 GND CLOCKB) 16 Q5 Vcc 01 RESE7 00 CLOCK 02 ENABLE 06 CASCADE 09 Ø7 7 Q3 8 08 GND

FIG. 2—TO BE READY FOR NEXT MONTH, obtain some 4520 binary counters, 4508 octal latches, 4017 decade counters, and 4049 hex inverters.

before. Remember that you must break complex circuitry down to

bite-sized pieces and then work out the details of each piece. I think Chairman Mao once said something like that.

Before we continue, you must clearly understand how the tachometer calculates its data. Because the output of the circuit is a combination of time and counts, there are two ways to make the measurement. The first is to measure the time period per pulse, and the second is to do the opposite---measure pulses per time period.

The first case requires an accurate clock that runs at a frequency significantly higher than the frequency of the pulses coming from the engine. The circuitry should count the clock pulses per engine pulse and then use the resulting number to calculate the engine rpm. This is the preferred approach for tachometers that have to work with fairly low-frequency input clocks such as heart-rate monitors.

That method doesn't offer any advantage, and it makes calculating the rpm unnecessarily difficult. The final number produced by a circuit like this would be minutes per revolution, and we would have to design circuitry to take the reciprocal of that number to give us the number of revolutions per minute.

The second measuring scheme (the one I'll show here) not only makes the math simpler, but the circuitry simpler as well. There's always more than one way to design a circuit, but it's always best to keep things as simple as possible.

The circuit we're going to build is based on standard counters, latches, and other bits of logical glue, so you won't have any trouble getting the parts. And although I'll be using specific components, you'll be able to substitute similar ones that you might already have.

Because there will be several engine pulse counters running in parallel, the best way to start it is to get one counter working and then add the other counters afterwards. If you want to be ready for next month, get yourself some 4520 binary counters, 4508 octal latches, 4017 decade counters, and also some 4049 hex inverters. The pinouts for those ICs (excluding the inverters) are shown in Fig. 2. Ω

85

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COMPUTER CONNECTIONS

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JEFF HOLTZMAN

ool computer products stand out. They're noticed and remembered. Even after they are no longer available, their legacy lives on, endowing future generations with their most important characteristics. These products are landmarks.

To get on my cool-product list, which stretches back to the late '70's, a product did not necessarily have to be the first available in its category, although some were. In fact, most products on my list are not initial releases, but version 3.0 or later. Every product in the list either defined a new category, or refined and perfected an existing category. Many are not current versions, because the version cited represents what is, in my opinion, the best tradeoff between architecture, ease of use, and feature set. Often, subsequent versions had added features, but did not update the architecture, so overall product integration suffered, often leading to needlessly complex interfaces or generally software.

I've broken my list down into four categories: hardware, DOS software, Windows software, and areas that still lack cool products.

Cool hardware

IBM's PC, PC-XT (with a hard disk and hierarchical directory structure), and PC-AT (with an 80286 CPU and 16-bit expansion bus): IBM defined the first three generations of PCs, and forever changed the way that business is done and, in many ways, the way we live.

Intel's 386 and 486 microprocessors: IBM lost the initiative when Intel released the 386, so the microprocessor itself, rather than any particular computer brand, characterized the next generations of personal computers.

Radio Shack Model 100: Introduced around 1984, this was the first laptop computer. It had a full size keyboard, an eight-line \times 40character LCD, and a 300-bps modem. Built-in software programmed in ROM included a telecommunications program, a word processor, and BASIC. As much as 32 kilobytes of RAM could be installed. A ROM socket and even an expansion-bus connector were provided for future upgrades. I have many fond memories of writing software for the machine, developing hardware for the expansion bus, and simply writing while on the go. Its biggest limitation was its small display. Nonetheless, the Model 100 defined the notebook computer.

Steve Ciarcia's \$50 acoustic-coupled 300-bps modem kit: Byte magazine published plans for this kit around 1983. It worked, was reliable, and, most important, it was affordable. It introduced legions of personal computer users to telecommunications.

Hayes 2400 bps SmartModem: At the time, the transition from 300 to 2400 bps (with a short detour through 1200 bps) seemed to take forever. But once it happened, Hayes defined a modem standard that still stands. In the subsequent move to 9600 bps and beyond, Hayes no longer enjoyed the stature it once had. Nonetheless, the phrase "Hayes-compatible" carries a marketing cachet reserved for a rarefied few.

IBM's 256-color video graphics array (VGA) and multicolor graphics aray (MCGA): IBM introduced the 256-color mode with its PS/2 Models 25, 30, 50, and 60 in April 1987. The jump from EGA's 16 colors was simply breathtaking (even with the loss of resolution). Hercules' monochrome video adapters deserves a runners-up award for bringing affordable bit-mapped graphics to the rest of us, at a time when color capability was much more expensive. Super-VGA (SVGA) video has continually evolved since 1987, so that I cannot single out any product that stands head and shoulders above the rest.

Hewlett-Packard's LaserJet Series II: Quality, expandability, de-

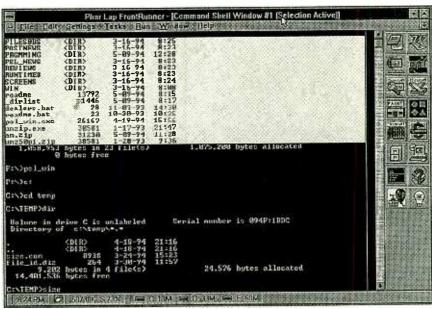


FIG. 1—FRONT RUNNER is a new Program Manager replacement that effectively marries the DOS command-line interpreter with the Windows GUI. You can launch DOS and Windows programs from the command line, peruse a scroll-back buffer, and put your favorite icons on the toolbar.

pendability, and affordability characterize this laser printer. I wish that mine would die so I could buy a newer model—but it won't. 'Nuff said.

NEC Multisync Monitors: In the absence of timing-signal standards from the video-card manufacturers, NEC put the smarts in the monitor, thereby creating a subindustry and a raft of competitors.

Cool software

MicroPro WordStar 3.3: From the late 70's to the early 80's, WordStar was king of the word-processing heap. Extensively customizable, with a powerful, logical, but less-than intuitive interface, its presence is still felt in software development environments from Microsoft and Borland, and text editors from many vendors. The DOS EDIT program (i.e., QBasic) even implements a subset of the old WordStar commands. In WordStar's heyday, WYSIWYG (what you see is what you get) meant accurate on-screen line and page breaks, in monospaced typewriter-style fonts. We've come a long way since then, but true WYSIWYG still eludes even the best high-end systems.

Turbo Pascal 3.0: Turbo Pascal 1.0 for CP/M put a company called Borland on the map in 1983. It simultaneously defined a new software category, what we now call the integrated development environment (IDE). I still use TP3 for quick and dirty programming tasks.

Lotus 1-2-3 2.01: Throughout the mid 1980's, Lotus 1-2-3 was what defined spreadsheet software. It was often used to test machine compatibility and performance. I suspect that few users of today's megaprograms need more than the functionality contained in 2.01.

SideKick 1.5: Another Borland product, SideKick defined the terminate and stay resident (TSR) program, both technically and from the user point of view. Techniques pioneered by SideKick created a huge market for DOS add-ins-at least until Windows 3.0 came along.

386Max: The first 386 memory manager, 386MAX taught the industry about the difference (to the processor) between physical and logical memory. In the process 386MAX extended (prolonged?) the life of DOS by giving PC users software control over the physical memory allocation.

LapLink III; Throughout the 1980's, networking was expensive and difficult. Floppy disks provided a way to transfer data, but that process was slow and error-prone. Traveling Software (which got its start by developing products for the Model 100) recognized a need and moved swiftly to fulfill it. Version 3 of LapLink allowed files to be transfered by serial or parallel ports. It was the first to provide over-the-wire "self-cloning," so the software had to be installed on only one computer. All of that functionality was packed in a 60-kilobyte executable file. I still prefer LapLink III to later versions because of its compactness and efficiency.

Derive: High-end symbolic math programs demand big, fast machines, but Derive from Soft Warehouse always ran comfortably on very low end hardware. Derive has a huge following in the high school and college math markets. Moreover, several textbooks have been written that use Derive for student exercises in algebra, graphics, and beginning calculus.

4DOS: I've always thought that MS-DOS's COMMAND.COM is a brain-damaged command-line interpreter. JPSoft's shareware replacement moves light-years beyond COMMAND.COM. It provides batch-file compiling, file-list processing, and a whole lot more.

The Semware Editor (TSE):This text editor emerged as a follow-on to the highly successful shareware program, Qedit. TSE is a text-editing engine that can be customized extensively; it comes with user interfaces that emulate Brief, Word-Star, and WordPerfect, and you can customize it to your heart's content. TSE includes a compiler that lets you build user interfaces and custom features with a Pascal-like language.

Lantastic: In the DOS networking category, Artisoft's Lantastic stood peerless (so to speak) in its balance between power, ease of use, and conformance to industry standards. Alas, the product might be in danger because of the assault from Microsoft Windows for WorkGroups and Chicago, which contain built-in, low-functionality, peer-to-peer networking.

Norton Utilities: To many people, the Norton Utilities means one thing: undeleting files. But Norton Utilities has always included numerous useful file and disk utilities, batch file enhancers, and more.

Cool Windows software

Microsoft Windows 3.1: This is a tentative choice. When Chicago is released and market tested, I think it will probably overtake Windows 3.1. But it could possibly lose it to OS/2 or some other 32-bit operating system. Until then, 3.1 stands as the paradigm of the graphical user interface (GUI). The Macintosh GUI was first, and probably better, but Windows captured the market.

Aldus PageMaker 3.0: This version ran under Windows 286 and Windows 386, and could subsequently be patched to run under successor versions 3.0 and 3.1. PM3 set new standards in smooth-operating controls, intuitive page-design metaphor, and WYSIWYG screen displays. PM3 features that once defined the high end in desktop publishing now come standard in sub-\$100 packages.

Visio 2.0: Created by the original developers of PageMaker, Visio single-handedly defined a new product category and brought unprecedented graphics power to non-professional computer users.

Adobe Type Manager 2.5: One of the biggest differences between Windows 3.0 and Windows 3.1 was the addition of the TrueType font system. Prior to TrueType, dealing with fonts under Windows was a nightmare—unless you used Type Manager, which was introduced on the PC for Windows 3.0. Adobe Type Manager is still *the* solution for quality font display and printing. With the current market glut of poor-quality TrueType fonts, good ones are hard to find. It's hard to go wrong with ATM (PostScript) fonts.

Microsoft Word: Throughout the past decade, Microsoft has never sat on its laurels. Instead, the company has steadily improved its name-sake word processor with each successive release, starting originally in DOS, and eventually moving to Win-

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dows 3.0. From its introduction, Word's document model followed publishing-industry standards now adopted by all major competitors, not proprietary page-description metaphors. Word for Windows 6.0 (really the third Windows version) is the latest and, in my opinion, best so far. For anyone who views document development as a form of engineering rather than typing, Word is the only choice.

Visual Basic: Another Microsoft product. Visual Basic defined a new technique. Visual Programming. As with Word, it's hard to single out a particular version as superior, because the overall product concept is so radically different. Visual Basic created a new industry: add-on tools, called VBXs (for Visual Basic Extensions). The purpose of this type of environment is to give the programmer a chance to focus on what the user needs rather than the details of how the programmer must implement them. The product's overwhelming success indicates the validity of the concept.

Quicken for Windows: All in all, I consider personal-finance tools to be a pretty boring category. However, one program stands so far above the others that there is no comparison. Quicken for Windows

offers 95% of the functionality of the competition, wrapped in a user interface that is far better. Like Page-Maker 3.0, Quicken's user interface can teach designers in any software category about the meaning of the terms usability and user-friendly.

Categories lacking cool products

There are several product categories that, I believe, still lack defining products. Among these I include Windows file managers, Windows command-line interpreters, modem communications, and CD-ROMbased database packages.

Each of those categories has its share of pretty good products, some of which show tremendous promise. For example, a relative newcomer in the Windows command-line interpreter category, FrontRunner (by PharLap Software), might make my next list.

On the other hand, the whole telecommunications category is still a complete and total mess. The steps that are required to straighten it out goes far beyond what the computer industry can supply by itself. Standard interfaces and protocols for interacting with the proliferating service providers are desperately needed, but they are nowhere in sight.

CD-ROM suffers from similar problems. Every product out there has a different user interface and database format. Certain products, such as Microsoft's BookShelf (reference works) and Encarta (encyclopedia) deserve special mention as ground-breakers, but not as examples of perfection.

Conclusions

That's my list. Undoubtedly I have forgotten a few things, and neglected others. In the future I'll present reader responses and updates to the list. In the meantime, I welcome any comments you might have (email: jkh+atacm.org). Ω



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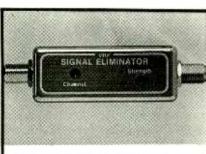
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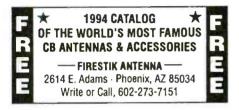
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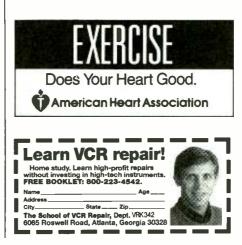
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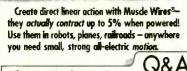
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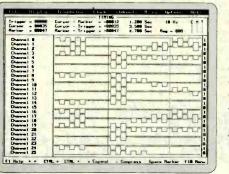
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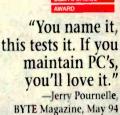


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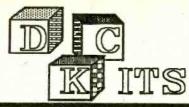
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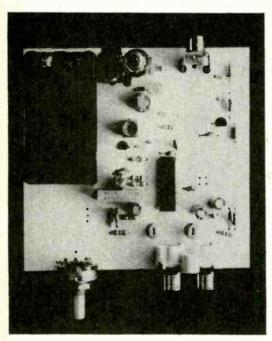


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500KHz to 1300MHz coverage in a programmable hand held. Ten scan banks, ten search banks. Lockout on search and scan. AM plus narrow and broadcast FM. Priority, hold,

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TRIDENT TR4500 \$449 **2016 Channels** 1 to 1300MHz Computer Control 62 Scan Banks, 16



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Most Economical receiver in its class, offers AM, NFM Wide FM. modes. 5KHz increments. Delay &

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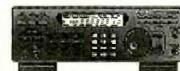
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Three new Bearcat units offer expanded coverage and more memory than before. The 890 offers 200 channels, base/mobile operation, VFO tuning, service search, weather alert, search and store, and more. The 2500 hand held has 400 channels, fast scan and more. The Bearcat 8500 has 500 channels in 20 banks, VFO, auto store, alpha numeric display, 10 priority channels, aux tape output jacks, and coverage to 1.3 Gigahertz.

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TRIDENT TR2C Police & CB \$69.95 Scans police pre-



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Hand Held Scanners

Bearcat 200XLTN \$209.95 200 Channels 800 MHz Ten scan banks plus search. Covers29-54, 118-174, 406-512 and 806-956MHz (with cell lock). Featuresscan, search, delay, 10 priorities, mem backup, lockout, WX search, keylock. Includes NiCad & Chrgr. Size: 1 3/8 x 2 11/16 x 7 1/2. Bearcat 120XLTJ 100Ch H/L/U..... \$149.95

Bearcat 150XLT 100Ch H/L/U/8 \$199.95 Bearcat 220XLTJ 200 Ch H/L/U/8 \$249.95

Coverage of above hand helds is: 29-54, 136-174, 406-512, and 800MHz band as indicated. Fax facts #475 Table Top Scanners

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DESCRIPTION CAT NO ET10EN Etch Tank System

PRICE \$48.00



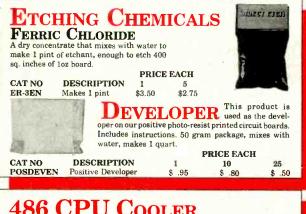
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| Singl | e-Sided, 1oz. Copper Foil on Fi | berglass \$ | Substrate | | | |
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| GS101EN | 100mm x 150mm/3.91" x 5.91" | \$ 3.90 | \$2.98 | \$2.60 | | |
| GS114EN | 114mm x 185mm/4.49" x 7.28" | 4.80 | 3.49 | 3.20 | | |
| GS152EN | 150mm x 250mm/5.91" x 9.84" | 8.69 | 5.98 | 5.78 | | |
| GS153EN | 150mm x 300mm/5.91" x 11.81" | 10.20 | 7.20 | 6.80 | | |
| Doub | le-Sided, loz. Copper Foil on F | iberglass | Substrate | • | | |
| | | PR | ICE EAC | H | | |
| CAT NO | DESCRIPTION | 1 | 10 | 50 | | |
| GD101EN | 100mm x 150mm/3.91" x 5.91" | \$ 5.07 | \$3.68 | \$3.38 | | |
| GD114EN | 114mm x 185mm/4.49" x 7.28" | 5.95 | 4.29 | 3.99 | | |
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| GD153EN | 150mm x 300mm/5.91" x 11.81" | 11.95 | 8.69 | 8.30 | | |
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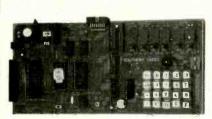


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Use our FaxBack Automated Document Retrieval System, Dial 1-800-662-5426 (602-834-1005 in AZ) and select document #5025 on your push-button phone. You'll receive an article reprint from Australia's "Silicon Chip" magazine, reviewing the Southern Cross SBC. This is a free service available 24-hours a day. Don't forget to have your FAX# handy.



THE SOUTHERN CROSS

A Single Board Z-80-Based Computer

Here is a single board computer designed especially for the 1990's generation of students. With a series of add-on boards, smart sockets, fully commented monitor & an intelligent EPROM emulator, it can teach many aspects of microprocessor & micro-controller techniques of programming.

The Southern Cross SBC is designed to teach beginners modern code development techniques as well as assembly language. Start with machine language using the on-board

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Simple, but powerful monitor program fully annotated. Learn to use parts of it in your own programs by 'system calls' & using a 'header file'

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SC6EN Assembled

SC5EN Kit



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Three Digit Panel Meter and Counter Module

Basic low cost counter. Twa or more counter modules may be plugged together with 6pin sockets & harness provided. Uses a single-unit 3-digit LED display. Built around the 14553 & 14551 chips. Box & battery pravided. The separate COUNTER MODULE shows how to use the Kit as a caunter. Has COUNT & RESET switches with debounce circuit built in ta eliminate prablems from noisy switches. 9V battery operation. CATNO PRICE KIT IEN

\$19.95

Introduction to a Power Supply

Batteries soon become an expensive way to power your electronic kit and electranic games. This is a basic pawer supply using twa 7805 regulators. Input up to 20V AC from a transformer or power pack. Twa regulated outputs—fixed 5V, the other variable. Box provided. Good introduction to electronics. CATNO PRICE

KIT 4EN \$12.77

Introduction to LM3909. **Continuity Tester & Long Life** Flasher

Most ICs operate in the 4V to 40V range. The LM3909 from National Semiconductor changed this. Two PCBs supplied. A 1.5V D cell will flash an LED for over two years. Use as an imitation car alarm. A second PCB connects the chip as a 1.5V continuity tester. Seven pages of documentation provided from National Semiconductor. PRICE CATNO KIT 11EN \$9.95

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Can be adjusted to turn on your tape recorder through its REMOTE plug. Has feedback and delay circuit for robust operation. Very sensitive. Proven circuit. Needs 6V plug pack for most stable operation. CATNO PRICE

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KIT 24EN

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General Purpose 4-1/2 Digit **Frequency Counter with LCD**

General Purpose 4-1/2 Digit Counter uses Harris 7224 IC, Full instructions INCLUDING the 7224 data sheet is included. All pins from the 7224 are brought out for easy access. Directly drives an LCD (provided). This project is a building block that you can use as part of a larger project. The LCD section can be cut away and connected by a flat ribbon cable. The Kit has its own 5V regulated supply on board for the 7224, allowing a relatively wide range of voltage inputs from +6V to 10V. The Harris 7224 counts up to 15MHz, guaranteed, 25MHz typical.

| CAT NO | PRICE |
|--|---------------------------------|
| KIT 36EN | \$42.00 |
| the second secon | the second second second second |

Intro to Microcontrollers

Learn ta program microcontrollers without going to technical college. This Kit introduces the Motorola 68HC705K1, an 8 bit, 16-pin microcontroller released in 1992. The Kit is a down counter from 60 ar 90 secands with beeps every 10 seconds. All the software code is supplied and fully explained. See how easy it is to change the time and beep settings by simple changes in the software program. You can judge for yourself haw using micro-controllers is a huge advance aver using logic ICs. On/off switch and pulldown resistars an Input lines are all built into the K1 and are under software control. 9V battery pawered.

All the information about haw to continue learning to pragram these "computers-ana-chip" is supplied. The tools to program the K1 are available at very low cost (under \$200) from Matorola. The K1 is the simplest 8-bit microcontraller available. CATN

| KII JOEN | 400.70 |
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| KIT 38EN | \$38.95 |
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Laboratory source of acoustical shock waves. Blow holes in metal, produce cold" steam, atomize liquids. Many deaning uses for PC boards, jewelry, coins, small parts, etc.



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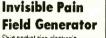
ULB1 Plans.....\$10.00 ULB1K Kit/Plans....\$69.50

100,000V Intimidator / Shock Wand Module Build an electrical device that is affective up to 20 feet. May be

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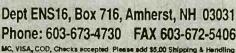


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Shoots flaming ball - two shot capacity Great for special effects and remote fire starting. CAUTION REQUIRED! FIREBALL Plans (Dangerous Product).....\$10.00









TV & FM Joker / Jammer

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High brightness red HeNe laser visible for miles. Produce your own light show! Projects a visible beam of red lite clearly visible in most circumstances. Can be used to intimidate by projection of a red dot on target subject. Also may be used to "listen in" using our laser window bounce method #LLIS1 below. Easy to build module makes A working visible laser!

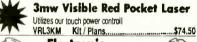
LAS1KM Kit w/1mw Laser Tube, Class II. LAS3KM Kit w/2.5mw Laser Tube, Class IIIA



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Allows you to hear sounds from an area via a lite beam reflected from a window or other similar objects. System uses our ready-to-use LATR1 Laser Terminator gun site as the transmitter. The receiver section is supplied as an easy-to-build kit, including our cushioned HS10

| headsets. | LLIST2 Plans |
|-----------|---|
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Intended for parties and entertainment but must be used with caution. includes valuable text book reference and plans. EH2 Plans and Text Book \$19.50





Electronics Now, September 1994

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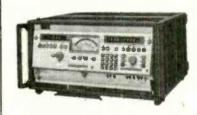
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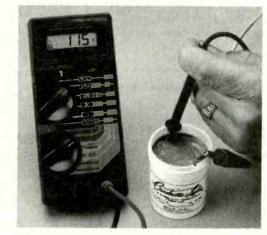
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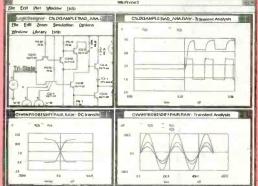
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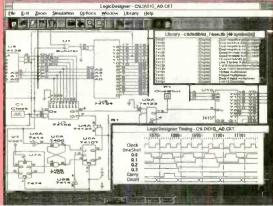
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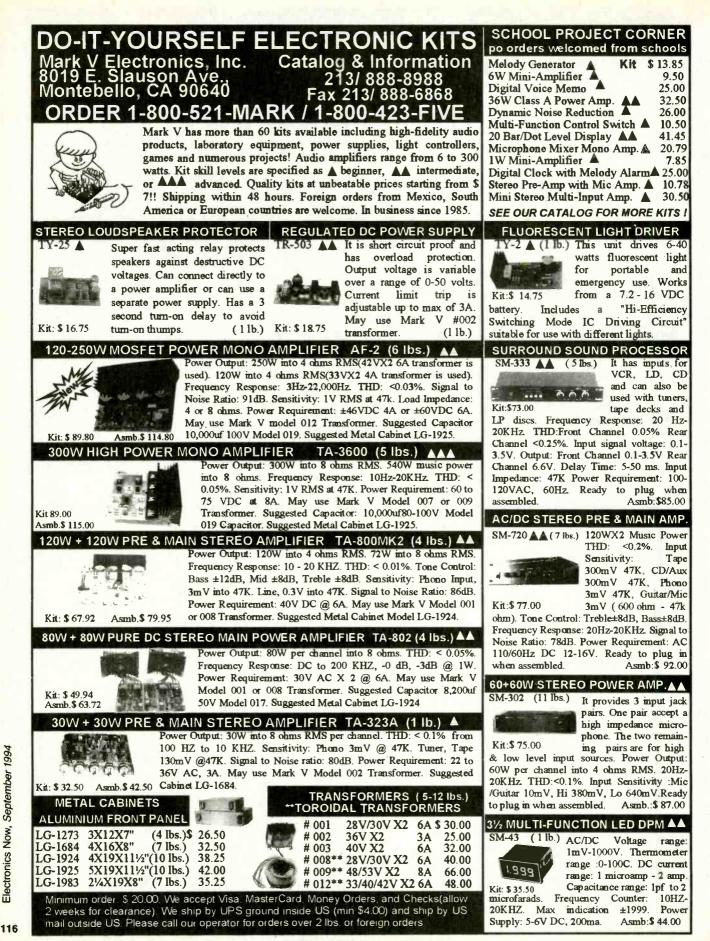
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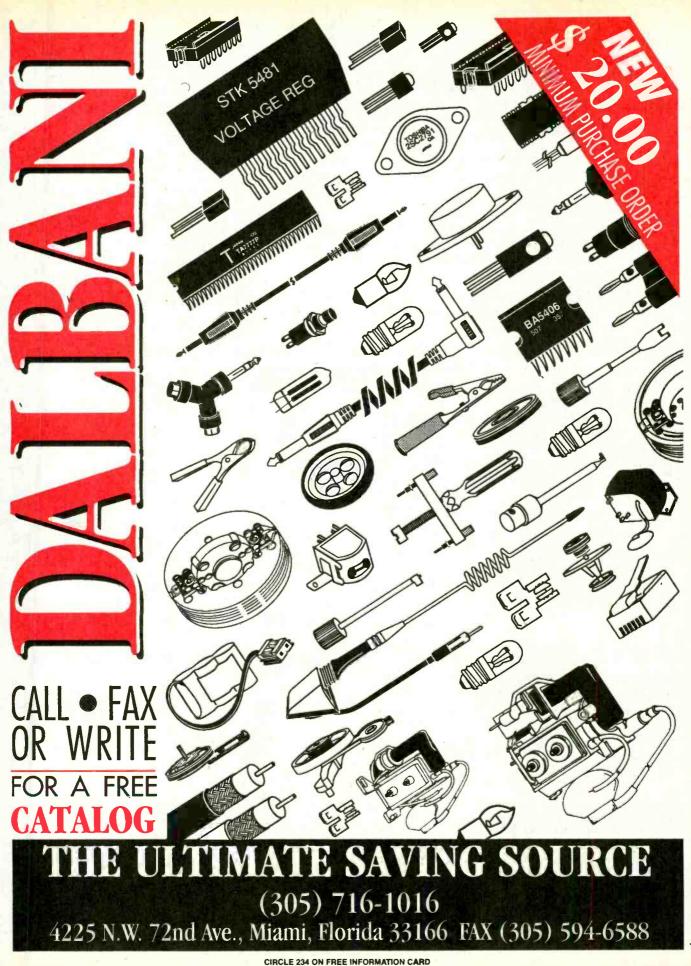
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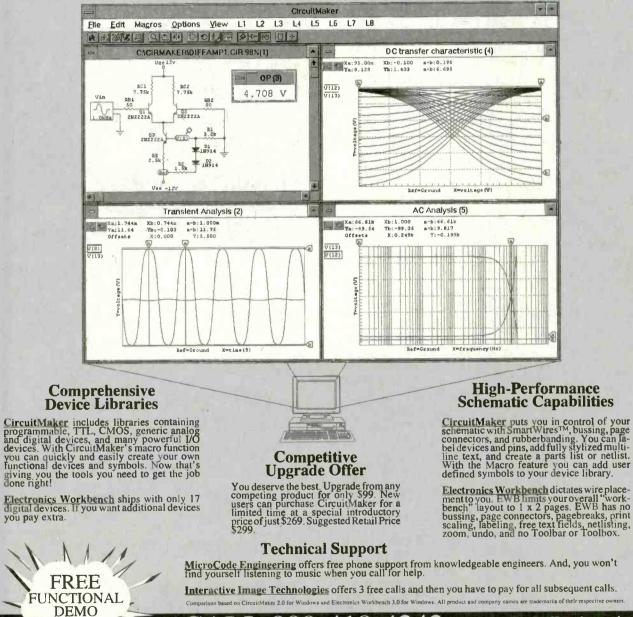
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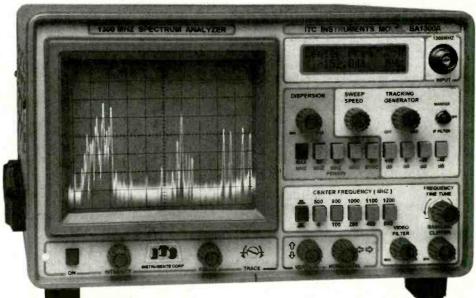
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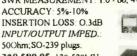


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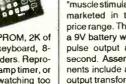
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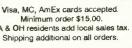
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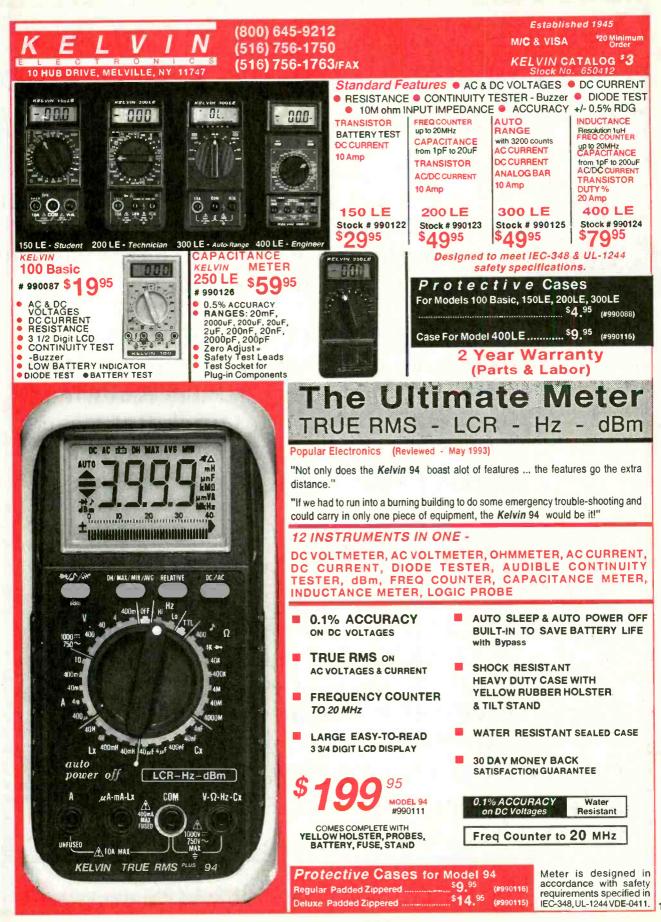
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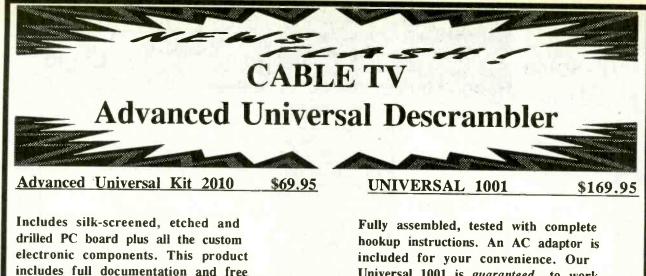
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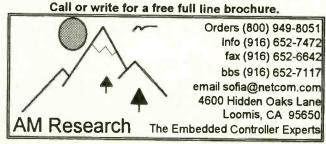
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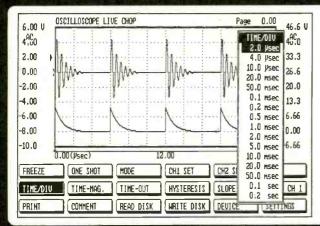
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LOW COST: HANDYPROBE

Connect the HANDYPROBE to the parallel printer port of the PC and start the software. Measuring can be carried out at once. The HANDYPROBE does not need external power supply. Some technical specifications:

0.5 ... 400 volt software select input range; 100,000 samples/sec.; one input channel; 8 bits resolution (overall accuracy 2%). A complete software program consisting of a digital storage oscilloscope, spectrum analyzer, voltmeter and a transient recorder is provided. HANDYPROBE is very suitable for servicing and educational purposes.

MULTIFUNCTIONAL: TP5008

The TP5008 is an interface card that provides an analog output in addition to two input channels. This output in combination with the two inputs may be used for the setting up of a complete control loop. The output may also be used as a function generator. The TP5008 has a resolution of 8 bits and a sampling rate

of 200,000 samples/sec (200 KHz). The input range may be set to 0.5 ... 20 volt full scale deflection. The output range covers 1.25 or 2.5 volt. The TP5008 is fitted with BNC connectors and is delivered complete with a user manual and software. Separately available are 1:1-1:10 probes and 1:100 oscilloscope probes. **CONWAY Engineering, Inc.** distributes the complete range of computer controlled measuring instruments of TiePie engineering. Connecting these instruments to a PC (MS-DOS 3.0 or higher) results in a number of comprehensive test

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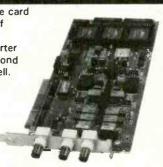
The HANDYSCOPE is connected to the parallel printer port. This makes it possible to carry out measurements with a laptop or notebook PC. Due to its high resolution (12 bits), the HANDYSCOPE is a very accurate unit. The measuring time is 100,000 samples/sec. Either of the two channels can be set independently over a range of 0.5 ... 20 volt (with a 1:10 probe up to 200 volt). The advanced software enables many measurements to be carried out. Two probes (switchable 1:1-1:10) are provided. The HANDYSCOPE is constructed as a small table model with two BNC

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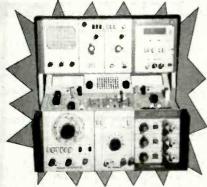
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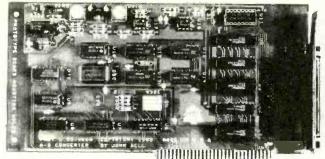
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| -R392 RECEIVER .5-30MHz | |
| - T195 100w COMPANION XMTR TO 392 | |
| RACAL RA6793A RECIVER (like new) | \$3000.00 |
| TRANSWORLD TW-100 PORTABLE TRANS | |
| SYNTHESIZED, AUTO TUNE, 100WATTS | \$2295.0 |
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| -COLLINS 30L-1 POWER AMP | \$ 355.00 |
| TRANSWORLD TW1500 1-Kw BROADBAND | AMP - |
| w/POWER SUPPLY | \$2500.0 |
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| ·COLLINS 516-F2 PWR SUPPLY(USED) | |
| -HARRIS RF280 HF/TACTICAL TRANSCEIVI | |
| -LEXEL MOD 75 HIGH POWER ARGON LAS | ER\$1500.0 |

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IBM Compatible - Input voltage 0 to 2 volts (0.00048 volts per count). Conversion time <1ms. Accuracy is better than +/- 2 counts. Linearity is better than +/- 1%. Part #93-326A \$149.95. Also a 50 MHz sample rate with 8 bit conversion. \$179.95 This board has one 8 bit TTL input port and one 8 bit TTL output port and comes with a diskette with BASIC programs for Data logging, Low Frequency Oscilloscope, Temperature measurement using a Radio Shack Thermistor, and Voltage measurement.

I also have a Parallel I/O board using 2 8255s (48 I/O Lines), Relay Output board, Opto Isolated Input board, 8748 Controller and more. Circle my number on the FREE INFORMATION CARD to get more info on my other interface boards.





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| TEK 7A13 100 MHz Differential Comparator | \$450.00 |
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| TEK 7853A 100 MHz Dual Time Base | \$200.00 |
| TEK SC502 15 MHz Dual Trace O'scope, TM500 | \$375.00 |
| TEK 475 200 MHz Dual Channel O'scope | \$750.00 |
| TEK 7704A 250 MHz 4-slot frame | \$300.00 |
| TEK 7904 500 MHz 4-slot frame | \$450.00 |
| TEK 7904 System w/7A24,7A26,7B80,7B85 | \$1,000.00 |
| TEK 7A24 400 MHz Dual Trace Amplifier | \$450.00 |
| TEK 7A26 200 MHz Dual Trace Amplifier | \$250.00 |
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| TEK 7A29-OPT.04 | \$1,150.00 |
| 1 GHz Amplifier, variable delay | |
| TEK 7B10 1 GHz Time Base | \$500.00 |
| TEK7B15 1 GHz Delaying Time Base | \$600.00 |
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| TEK 7S14 1 GHz Dual Channel Sampling Unit | \$700.00 |
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| TEK P6046 100 MHz 1X/10X Diff. Probe | \$750.00 |
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| HP 3312A 13 MHz Function Generator | \$800.00 |
| TEK DD501 Digital Delay Generator | 8075 00 |
| TEKFG502 11 MHz Function Generator | \$325,00 |
| WAVETEK 164 30 MHz | \$850.00 |
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| HP 8015A-opt002 50 MHz | \$700.00 |
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| HP 8080A 1 GHz Dual Channel Pulse Gen | \$1,400.00 |
| HP 8082A 250 MHz Pulse Generator | \$1,400.00 |
| TEK PG502 250 MHz Pulse Generator, Tr<1nS | \$700.00 |
| HP 8165A Prog. | \$2,600.00 |
| Signal Source,1 mHz-50 MHz | |
| TEK AWG5105 Arbitrary Waveform Generator | \$3,000.00 |
| TEKFG5010 20 MHz | \$1,200.00 |
| Programmable Function Gen | |
| TEKPFG5505 Prog. 12 MHz | \$1,275.00 |
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| INDER MOT & COMPONENT TERT | HP 8444A-opt059 Tracking \$1,500.00 | NARDA 769-20 20 dB Attenuator. \$250.00 |
| IMPEDANCE & COMPONENT TEST | Generator, 0.5-1500 MHz | 150 W,DC-6 GHz |
| | HP 8552B IF Section \$750.00 | WEINSCHEL 1515 Power Divider. \$125.00 |
| HP 4800A Vector Impedance Meter \$550.00 | HP 8553B RF Section, 1 kHz-110 MHz | DC-18 GHz, SMA |
| BOONTON 62AD 1 MHz Ind. Meter, 2-2000 uH \$700.00 | HP 8554B RF Section, 0.1-1250 MHz \$800.00 | NUMBER OF THE OWNER AND A DESCRIPTION OF THE OWNER AND A DESCRIPTION OF THE OWNER AND A DESCRIPTION OF THE OWNER |
| BOONTON 72B 1 MHz Cap. Meter, 1-3000 pF \$500.00 | HP 8555A RF Section, 0.01-18 GHz | MISCELLANEOUS |
| HP 4328A-001 Milliohmeter, 0.001-100 ohms \$1,350.00 | TEKTR503 Tracking Generator, \$1,750.00 | |
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| Synth Sig /Swp. Gen., 18-40 GHz | •••• |
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| HP 86222A RF Plug-in, 10-2400 MHz | \$1,500.00 |
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| HP 86240A RF Plug-in, 2.0-8.4 GHz | |
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| WILTRON 6617-opt.03 Prog. | \$3,300.00 |
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| BOONTON 42B/41-4B Power Meter, | \$475.00 |
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| 1 MHZ-12.4 GHZ BOONTON 42B/41-4E Power Meter, | \$650.00 |
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| HP Q8486A WR22 Power Sensor, | \$1,500.00 |
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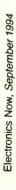
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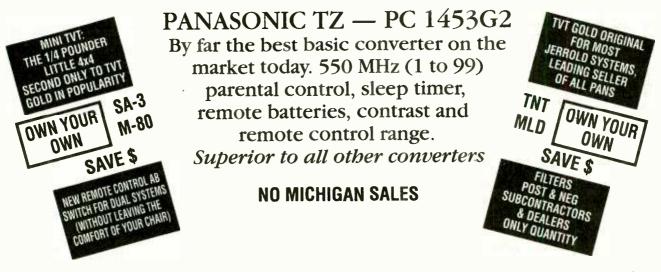
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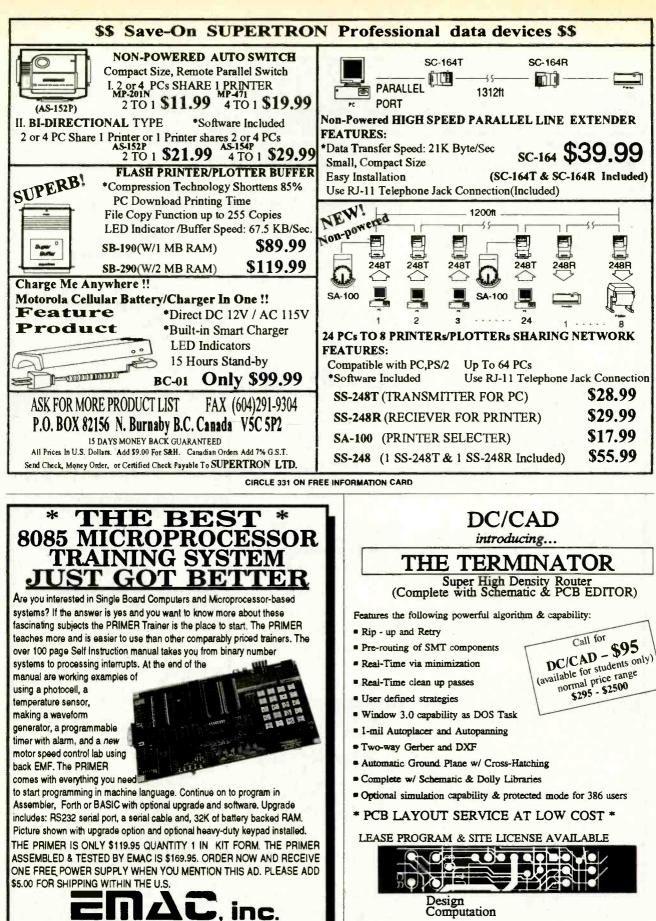
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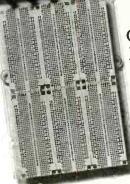
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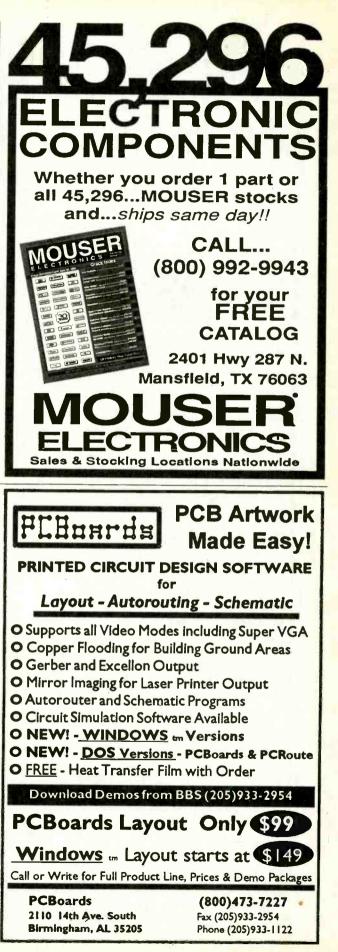
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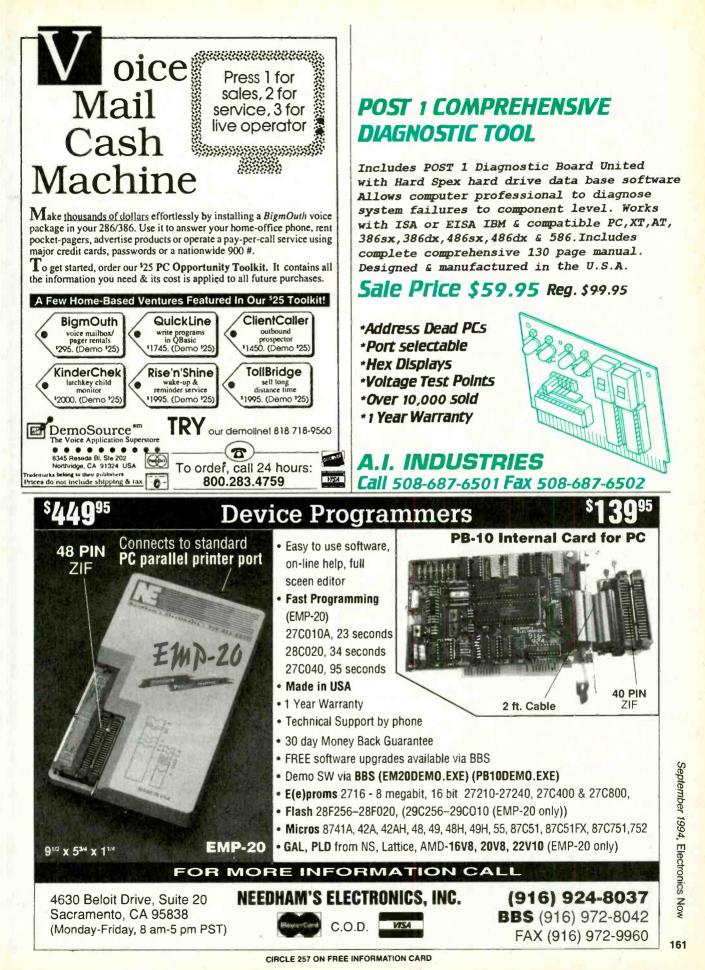
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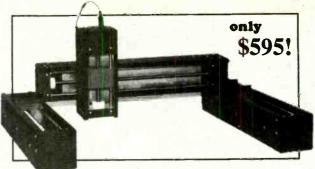
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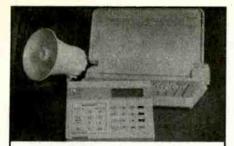
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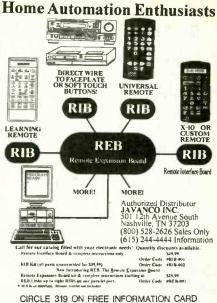
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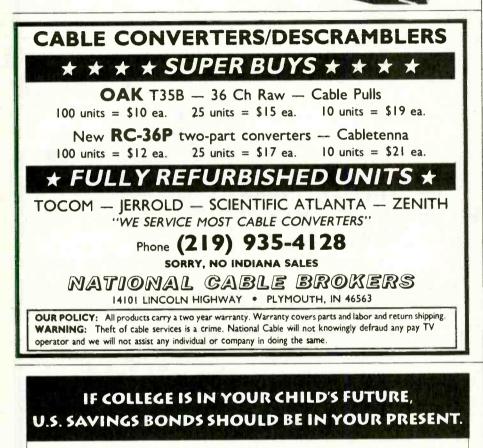
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| 3312A, DISTORTION ANALYZER. 800.00 331A, DISTORTION ANALYZER. 225.00 3400, RMS VOLTMETER. 300.00 3403C, TRMS DMM, 3.5 DIGIT, 16H2-10kHz. 450.00 3403C, TRMS DMM, 3.5 DIGIT, 16H2-10kHz. 450.00 3403C, TRMS DMM, 3.5 DIGIT, 16H2-10kHz. 450.00 3437A, HIGH SPEED SYSTEM DMM,1000 R/SEC HPIB. 350.00 3440/3444A, DIGITAL MULTIMETER. 75.00 3455A, 6-1/2 DIGITAL MULTIMETER. 700.00 3467A, LOGGING MULTIMETER, 4.5. 1000.00 3469B, MULTIMETER, DIGITAL/ANALOG READOUT. 275.00 3551B, TRANSMISSION & NOISE MEASUREMENT SET. 200.00 3581C, SELECTIVE VOLTMETER, 15H2-50 kHz. 1200.00 3881A, WAVE ANALYZER, 15 H2-50 kHz. 1500.00 3881A, SELECTIVE VOLTMETER, 02H2-25.6Hz. 5000.00 3884B, SELECTIVE LEVEL METER. 1000.00 3702A, IF/BB RECEIVER. 2000.00 400E, AC VOLTMETER. 55.00 4115E, SWR METER. 150.00 412, POWER METER. 150.00 413E, SWR METER. 150.00 431A, POWER METER. 150.00 431A, POWER METER. 150.00 431A, POWER ME |
| 331A, DISTORTION ANALYZER. 225.00 3400, RMS VOLTMETER. 300.00 3403C, TRMS DMM, 3.5 DIGIT, 1.6Hz-10kHz. 450.00 3406A, BROADBAND SAMPLING VOLTMETER. 800.00 3437A, HIGH SPEED SYSTEM DMM,1000 R/SEC HPIB 350.00 3447A, HIGH SPEED SYSTEM DMM,1000 R/SEC HPIB 350.00 3440/3444A, DIGITAL MULTIMETER. 75.00 3455A, 6-1/2 DIGITAL MULTIMETER, 4.5 1000.00 3467A, LOGGING MULTIMETER, 14.5 1000.00 3490A, DMM, 5 DIGIT 275.00 3490A, DMM, 5 DIGIT 275.00 355B, TRANSMISSION & NOISE MEASUREMENT SET 200.00 3581C, SELECTIVE VOLTMETER, 15 HZ-50 kHZ 1500.00 3582A, SPECTRUM ANALYZER, 02Hz-25.6HZ 5000.00 3584B, SELECTIVE LEVEL METER 1000.00 3702A, IF/BB RECEIVER 2000.00 400E, AC VOLTMETER 150.00 410C, VOLTMETER 150.00 4119, DC NULL METER 150.00 4121, POWER METER 150.00 4131, POWER METER 100.00 4312, POWER METER 100.00 4314, POWER METER 100.00 4315, POWER METER 100.00 |
| 3400, RMS VOLTMETER. 300.00 3403C, TRMS DMM, 3.5 DIGIT, 1.6Hz-10kHz 450.00 3403C, TRMS DMM, 3.5 DIGIT, 1.6Hz-10kHz 450.00 3403C, TRMS DMM, 3.5 DIGIT, 1.6Hz-10kHz 800.00 3437A, HIGH SPEED SYSTEM DMM,1000 R/SEC HPIB. 350.00 3440/3444A, DIGITAL MULTIMETER. 75.00 3455A, 6-1/2 DIGITAL MULTIMETER, 4.5 1000.00 3467A, LOGGING MULTIMETER, DIGITAL/ANALOG READOUT. 275.00 3459B, MULTIMETER, DIGITAL/ANALOG READOUT. 275.00 355B, TRANSMISSION & NOISE MEASUREMENT SET 200.00 3581A, WAVE ANALYZER, 15 Hz-50 kHz 1200.00 3581C, SELECTIVE VOLTMETER, 15HZ-50KHZ 1500.00 3586B, SELECTIVE LEVEL METER 1000.00 3702A, IF/BB RECEIVER 2000.00 400E, AC VOLTMETER. 55.00 410C, VOLTMETER. 150.00 413E, SWR METER. 150.00 413E, SWR METER. 150.00 413E, POWER METER. 150.00 413I, POWER METER. 150.00 431B, POWER METER. 150.00 432A/478A, PWR MTR, 0.01-10 GHz, -20 dBm TO +10 dBm. 300.00 435A,8481B, PWR MTR W/SENSOR. 1 mW-25 W, 0.01-18 GHz1325.00 436 |
| 343/A, HIGH SPEED SYSTEM DMM,1000 R/SEC HPIB. 350.00 3440/3444A, DIGITAL MULTIMETER. .75.00 3455A, 6-1/2 DIGITAL MULTIMETER. .700.00 3467A, LOGGING MULTIMETER, 4.5. .1000.00 3467A, LOGGING MULTIMETER, 4.5. .1000.00 3467A, LOGGING MULTIMETER, AS .1000.00 3490A, DMM, 5 DIGIT .275.00 3555B, TRANSMISSION & NOISE MEASUREMENT SET .200.00 3581A, WAVE ANALYZER, 15 Hz-50 KHZ .1200.00 3582A, SPECTRUM ANALYZER, 02Hz-25.6Hz .5000.00 3586B, SELECTIVE VOLTMETER, 15HZ-50 KHZ .1500.00 3702A, IF/BB RECEIVER .0200.00 400C, VOLTMETER .1512.50KHZ .1000.00 .702A, IF/BB RECEIVER .2000.00 .7586B, SELECTIVE LEVEL METER .100.00 .75.00 410C, VOLTMETER .150.00 410C, VOLTMETER .150.00 4115E, SWR METER .150.00 4131B, POWER METER .150.00 431C, POWER METER .100.00 432A/478A, PWR MTR, 0.01-10 GHz, -20 dBm TO +10 dBm |
| 343/A, HIGH SPEED SYSTEM DMM,1000 R/SEC HPIB. 350.00 3440/3444A, DIGITAL MULTIMETER. .75.00 3455A, 6-1/2 DIGITAL MULTIMETER. .700.00 3467A, LOGGING MULTIMETER, 4.5. .1000.00 3467A, LOGGING MULTIMETER, 4.5. .1000.00 3467A, LOGGING MULTIMETER, AS .1000.00 3490A, DMM, 5 DIGIT .275.00 3555B, TRANSMISSION & NOISE MEASUREMENT SET .200.00 3581A, WAVE ANALYZER, 15 Hz-50 KHZ .1200.00 3582A, SPECTRUM ANALYZER, 02Hz-25.6Hz .5000.00 3586B, SELECTIVE VOLTMETER, 15HZ-50 KHZ .1500.00 3702A, IF/BB RECEIVER .0200.00 400C, VOLTMETER .1512.50KHZ .1000.00 .702A, IF/BB RECEIVER .2000.00 .7586B, SELECTIVE LEVEL METER .100.00 .75.00 410C, VOLTMETER .150.00 410C, VOLTMETER .150.00 4115E, SWR METER .150.00 4131B, POWER METER .150.00 431C, POWER METER .100.00 432A/478A, PWR MTR, 0.01-10 GHz, -20 dBm TO +10 dBm |
| 3440/3444A, DIGITAL MULTIMETER. .75.00 3455A, 6-1/2 DIGITAL MULTIMETER. .700.00 345A, 6-1/2 DIGITAL MULTIMETER. .700.00 345A, 6-1/2 DIGITAL MULTIMETER. .700.00 3469B, MULTIMETER, DIGITAL/ANALOG READOUT. .275.00 3490A, DMM, 5 DIGIT .275.00 355B, TRANSMISSION & NOISE MEASUREMENT SET .200.00 3581A, WAVE ANALYZER, 15 Hz-50 kHz .1500.00 3582A, SPECTRUM ANALYZER, 02Hz-25.6Hz .5000.00 3586B, SELECTIVE VOLTMETER, 15HZ-50KHZ .1500.00 3702A, IF/BB RECEIVER .0000.00 400E, AC VOLTMETER .55.00 410C, VOLTMETER .150.00 415E, SWR METER .150.00 410C, VOLTMETER .75.00 431B, POWER METER .150.00 432A/478A, PWR MTR, 0.01-10 GHz, -20 dBm TO +10 dBm .300.00 435A/8481B, PWR MTR W/SENSOR. 1 mW-25 W, 0.01-18 GHz1325.00 .436A/03.002 DIGITAL PM w/ HPIB .5900.00 436A/03.002 DIGITAL PM /SENSOR .1500.00 .436A/03.002 DIGITAL PM w/ HPIB .5000.00 436A/03.002 DIGITAL PM /SENSOR .1500.00 .436A/03.002 DIGITAL PM SENSOR .550.00 436A/03.002 DIGITAL PM SENSOR .550.00 </td |
| 340/A, LOGGING MULTIMETER, 4.5. 1000.00 349B, MULTIMETER, DIGITAL/ANALOG READOUT |
| 34504, DMM, 3 DIGHT |
| 34504, DMM, 3 DIGHT |
| 3581A, WAVE ANALYZER, 15 Hz-50 kHz 1200.00 3581C, SELECTIVE VOLTMETER, 15HZ-50 KHZ 1560.00 3582A, SPECTRUM ANALYZER, 02Hz-25.6Hz 5000.00 3586B, SELECTIVE LEVEL METER 1000.00 3702A, IF/BB RECEIVER 2000.00 400E, AC VOLTMETER 55.00 410C, VOLTMETER 150.00 419, DC NULL METER 150.00 419, DC NULL METER 75.00 431, POWER METER 150.00 431, POWER METER 150.00 431C, POWER METER 100.00 432A/478A, PWR MTR, 0.01-10 GHz, -20 dBm TO +10 dBm 300.00 435A, POWER METER 450.00 436A/03./002 DIGITAL PM w/ HPIB \$900.00 436A/03./002 DIGITAL PM w/ HPIB \$900.00 436A/4841B, PWR MTR V/SENSOR 1 mW-25 W, 0.01-18 GHz. 1325.00 436A/03.00.00 436A/4841B, PWR MTR W/SENSOR 1 mW-25 W, 0.01-18 GHz. 1325.00 436A/03.00.00 436/8484 DIGITAL PM/SENSOR \$1500.00 436/8484 DIGITAL PM/SENSOR \$150.00 436/8484 DIGITAL PM/SENSOR \$150.00 436/8484 DIGITAL PM/SENSOR \$150.00 436/8484 DIGITAL PM/SENSOR \$150.00 4510, AMPLIFIER, TWT 2 |
| 3561C, SELECTIVE VOLTMETER, 15HZ-50KHZ 1500.00 3582A, SPECTRUM ANALYZER, 02Hz-25.6Hz 5000.00 3586B, SELECTIVE LEVEL METER 1000.00 3702A, IF/BB RECEIVER 2000.00 400E, AC VOLTMETER 2000.00 400E, AC VOLTMETER 55.00 410C, VOLTMETER 150.00 415E, SWR METER 150.00 419, DC NULL METER 75.00 431, POWER METER 100.00 431C, POWER METER 100.00 432A/478A, PWR MTR, 0.01-10 GHz, -20 dBm TO +10 dBm 300.00 435A, POWER METER 450.00 436A/03./002 DIGITAL PM w/ HPIB \$900.00 436/8484 DIGITAL PM/SENSOR \$1500.00 436/A03./002 DIGITAL PM w/ HPIB \$900.00 436A/03./002 DIGITAL PM w/ HPIB \$900.00 436/A03, TRANS TEST SET, AC & BATT, PWR 200.00 491C, AMPLIFIER, TWT 24GHZ, 1W 30DB GAIN 200.00 4915A,003, TRANS TEST SET, AC & BATT, PWR 1250.00 5044A, SIGNATURE ANALYZER w/ PROBES 250.00 5245L, SOMHz FREQUENCY COUNTER 75.00 5246L, FREQUENCY COUNTER 75.00 5246L, FREQUENCY COUNTER 350.00 |
| 3380B, SELECTIVE LEVEL METER. 1000.00 3702A, IF/BB RECEIVER. 2000.00 400E, AC VOLTMETER. 2000.00 410C, VOLTMETER. 55.00 410C, VOLTMETER. 150.00 415E, SWR METER. 150.00 419, DC NULL METER. 75.00 431, POWER METER. 75.00 431B, POWER METER. 100.00 431C, POWER METER. 100.00 432A/478A, PWR MTR, 0.01-10 GHz, -20 dBm TO +10 dBm. 300.00 435A, POWER METER. 150.00 435A, POWER METER. 150.00 436A/03, /002 DIGITAL PM w/ HPIB. \$900.00 436/8484 DIGITAL PM/SENSOR. \$150.00 4310, AMPLIFIER. 200.00 435A/03, TRANS TEST SET, AC & BATT. PWR. 250.00 5044, SIGNATURE ANALYZER w/ PROBES. 250.00 52451, 50MHz FREQUENCY COUNTER. 7 |
| 3702A, IF/BB RECEIVER. 2000.00 400E, AC VOLTMETER. 55.00 410C, VOLTMETER. 150.00 415E, SWR METER. 150.00 419, DC NULL METER. 150.00 431, POWER METER. 75.00 431B, POWER METER. 75.00 431B, POWER METER. 100.00 432A/478A, PWR MTR, 0.01-10 GHz, -20 dBm TO + 10 dBm. 300.00 435A, POWER METER. 450.00 436A/03./002 DIGITAL PM w/ HPIB. \$900.00 436/A/8481B, PWR MTR W/SENSOR. 1 mW-25 W, 0.01-18 GHz1325.00 436/A/03./002 DIGITAL PM w/ HPIB. 4360.048484 DIGITAL PM/SENSOR. \$1500.00 436/A/8481 DIGITAL PM/SENSOR. \$1500.00 436/A/03./002 DIGITAL PM w/ HPIB. \$900.00 436/A/8484 DIGITAL PM/SENSOR. \$1500.00 436/A/03.002 DIGITAL PM w/ HPIB. \$900.00 436/A/3484 DIGITAL PM/SENSOR. \$1500.00 436/A/8484 DIGITAL PM/SENSOR. \$1500.00 436/A/8484 DIGITAL PM/SENSOR. \$1500.00 436/A/303.002 DIGITAL PM w/ HPIB. \$200.00 436/A/8484 DIGITAL PM/SENSOR. \$1500.00 436/A/31A, VECTOR IMPEDANCE METER, 5 Hz-500 kHz. \$50.00 |
| 410C, VOLTMETER. 150.00 413E, SWR METER. 150.00 419, DC NULL METER. 75.00 431, POWER METER. 75.00 431B, POWER METER. 100.00 431C, POWER METER. 100.00 431C, POWER METER. 100.00 431A, POWER METER. 150.00 432A/478A, PWR MTR, 0.01-10 GHz, -20 dBm TO + 10 dBm 300.00 435A, POWER METER 450.00 435A/8481B, PWR MTR W/SENSOR. 1 mW-25 W, 0.01-18 GHz. 1325.00 436A/03.002 DIGITAL PM w/ HPIB. \$900.00 436/8484 DIGITAL PM/SENSOR. \$1500.00 4310, AWPLIFIER. \$150.00 4310, AWPLIFIER. \$150.00 450.00 \$000.00 4510, AMPLIFIER. \$150.00 5044, SIGNATURE ANALYZER w/ PROBES. \$250.00 52451, SOMHz FREQUENCY COUNTER. \$50.00 |
| 410C, VOLTMETER. 150.00 413E, SWR METER. 150.00 419, DC NULL METER. 75.00 431, POWER METER. 75.00 431B, POWER METER. 100.00 431C, POWER METER. 100.00 431C, POWER METER. 100.00 431A, POWER METER. 150.00 432A/478A, PWR MTR, 0.01-10 GHz, -20 dBm TO + 10 dBm 300.00 435A, POWER METER 450.00 435A/8481B, PWR MTR W/SENSOR. 1 mW-25 W, 0.01-18 GHz. 1325.00 436A/03.002 DIGITAL PM w/ HPIB. \$900.00 436/8484 DIGITAL PM/SENSOR. \$1500.00 4310, AWPLIFIER. \$150.00 4310, AWPLIFIER. \$150.00 450.00 \$000.00 4510, AMPLIFIER. \$150.00 5044, SIGNATURE ANALYZER w/ PROBES. \$250.00 52451, SOMHz FREQUENCY COUNTER. \$50.00 |
| 419, DC NULL METER. 75.00 431, POWER METER. 75.00 431B, POWER METER. 100.00 431C. POWER METER. 100.00 432A/478A, PWR METR. 150.00 432A/478A, PWR METR. 100.00 435A, POWER METER. 450.00 435A, POWER METER. 450.00 435A, POWER METER. 450.00 436A/03./002 DIGITAL PM w/ HPIB. \$900.00 436A/03./002 DIGITAL PM w/ HPIB. \$900.00 436/8484 DIGITAL PM/SENSOR. \$1500.00 436/A4801A, VECTOR IMPEDANCE METER, 5 Hz-500 kHz. 550.00 491C, AMPLIFIER, TWT 24GHZ, 1W 30DB GAIN. 2000.00 4935A/003, TRANS TEST SET, AC & BATT. PWR. 1250.00 5044A, SIGNATURE ANALYZER w/ PROBES. 250.00 5245L, 50MHz FREQUENCY COUNTER. 75.00 5246L, FREQUENCY COUNTER. 75.00 5233B, FREQUENCY CONVERTER, 18GHz. 350.00 53002A, UNIVERSAL COUNTER. 500HZ 150.00 |
| 431, POWER METER. .75.00 431B, POWER METER. .100.00 431C, POWER METER. .100.00 432A/478A, PWR MTR, 0.01-10 GHz, -20 dBm TO + 10 dBm. .300.00 435A, POWER METER. .450.00 435A, POWER METER. .450.00 436A/03./002 DIGITAL PM w/ HPIB. .5900.00 436A/03./002 DIGITAL PM w/ HPIB. .5900.00 436A/03./002 DIGITAL PM/SENSOR. \$1500.00 436A/03./002 DIGITAL PM/SENSOR. \$1500.00 436A/03./002 DIGITAL PM/SENSOR. \$1500.00 436A/03, 002 DIGITAL PM/SENSOR. \$1500.00 436A/03, 002 DIGITAL PM/SENSOR. \$1500.00 491C, AMPLIFIER, TWT 2.4GHZ, 1W 30DB GAIN .200.00 4935A/003, TRANS TEST SET, AC & BATT PWR. .1250.00 504A, SIGNATURE ANALYZER w/ PROBES. .250.00 5245L, 50MHz FREQUENCY COUNTER. .75.00 5246L, FREQUENCY COUNTER. .75.00 5233B, FREQUENCY CONVERTER, 18GHz. .350.00 5300B/5305B, MEASURING SYSTEM. .450.00 5302A, UNIVERSAL COUNTER. .50MHZ .50MHZ |
| 431B, POWER METER. 100.00 431C, POWER METER. 150.00 432A/478A, PWR MTR, 0.01-10 GHz, -20 dBm TO +10 dBm. 300.00 435A, POWER METER. 450.00 435A, POWER METER. 450.00 435A, POWER METER. 450.00 435A, POWER METER. 450.00 435A/8481B, PWR MTR W/SENSOR. 1 mW-25 W, 0.01-18 GHz. 1325.00 436A/03, /002 DIGITAL PM w/ HPIB. \$900.00 436/8484 DIGITAL PM/SENSOR. \$1500.00 441A, AMPLIFIER. 200.00 4800A/4801A, VECTOR IMPEDANCE METER, 5 Hz-500 kHz. 550.00 491C, AMPLIFIER, TWT 24GHZ, 1W 30DB GAIN. 2000.00 4935A/003, TRANS TEST SET, AC & BATT. PWR. 1250.00 5004A, SIGNATURE ANALYZER w/ PROBES. 250.00 5245L, 50MHz FREQUENCY COUNTER. 75.00 5246L, FREQUENCY CONVERTER, 18GHz. 350.00 5300B/5305B, MEASURING SYSTEM. 450.00 5302A, UNIVERSAL COUNTER, 50MHZ 150.00 |
| 435A, POWEK METER. .450.00 435A, 8481B, PWR MTR W/SENSOR. 1 mW-25 W, 0.01-18 GHz1325.00 436A/03./002 DIGITAL PM w/ HPIB. .5000.00 436/8484 DIGITAL PM/SENSOR .11500.00 436/8484 DIGITAL PM/SENSOR .11500.00 436/8484 DIGITAL PM/SENSOR .11500.00 436/8484 DIGITAL PM/SENSOR .11500.00 461A, AMPLIFIER. .200.00 4800A/4801A, VECTOR IMPEDANCE METER, 5 Hz-500 kHz .550.00 491C, AMPLIFIER, TWT 24GHZ, 1W 30DB GAIN .2000.00 4935A/003, TRANS TEST SET, AC & BATT PWR. .1250.00 5004A, SIGNATURE ANALYZER w/ PROBES. .250.00 5245L, 50MHz FREQUENCY COUNTER. .75.00 5246L, FREQUENCY COUNTER. .75.00 5233B, FREQUENCY CONVERTER, 18GHz .350.00 5300B/5305B, MEASURING SYSTEM. .450.00 5302A, UNIVERSAL COUNTER, 50MHZ .150.00 |
| 435A, POWEK METER. .450.00 435A, 8481B, PWR MTR W/SENSOR. 1 mW-25 W, 0.01-18 GHz1325.00 436A/03./002 DIGITAL PM w/ HPIB. .5000.00 436/8484 DIGITAL PM/SENSOR .11500.00 436/8484 DIGITAL PM/SENSOR .11500.00 436/8484 DIGITAL PM/SENSOR .11500.00 436/8484 DIGITAL PM/SENSOR .11500.00 461A, AMPLIFIER. .200.00 4800A/4801A, VECTOR IMPEDANCE METER, 5 Hz-500 kHz .550.00 491C, AMPLIFIER, TWT 24GHZ, 1W 30DB GAIN .2000.00 4935A/003, TRANS TEST SET, AC & BATT PWR. .1250.00 5004A, SIGNATURE ANALYZER w/ PROBES. .250.00 5245L, 50MHz FREQUENCY COUNTER. .75.00 5246L, FREQUENCY COUNTER. .75.00 5233B, FREQUENCY CONVERTER, 18GHz .350.00 5300B/5305B, MEASURING SYSTEM. .450.00 5302A, UNIVERSAL COUNTER, 50MHZ .150.00 |
| 4800A/4801A, VECTOR IMPEDANCE METER, 5 Hz-500 kHz550.00 491C, AMPLIFIER, TWT. 24GHZ, 1W 30DB GAIN |
| 4800A/4801A, VECTOR IMPEDANCE METER, 5 Hz-500 kHz550.00 491C, AMPLIFIER, TWT. 24GHZ, 1W 30DB GAIN |
| 4800A/4801A, VECTOR IMPEDANCE METER, 5 Hz-500 kHz550.00 491C, AMPLIFIER, TWT. 24GHZ, 1W 30DB GAIN |
| 4800A/4801A, VECTOR IMPEDANCE METER, 5 Hz-500 kHz550.00 491C, AMPLIFIER, TWT. 24GHZ, 1W 30DB GAIN |
| 4935A/003, TRANS TEST SET, AC & BATT. PWR |
| 5245L, 50MHz FREQUENCY COUNTER |
| 5240L, FREQUENCY COUNTER. .75.00 5253B, FREQUENCY CONVERTER, 18GHz. .350.00 5300B/5305B, MEASURING SYSTEM. .450.00 5302A, UNIVERSAL COUNTER, 50MHZ 150.00 |
| 5253B, FREQUENCY CONVERTER, 18GHz |
| 3302A, UNIVERSAL COUNTER, SOMHZ |
| 5302A, UNIVERSAL COUNTER, SOMHZ |
| |
| 5312A, HP-1B INTERFACE 100.00 5314A, 100 MHz/100 nS UNIVERSAL COUNTER, PORTABLE 250.00 |
| 5314A, 100 MHz/100 nS UNIVERSAL COUNTER, PORTABLE250.00 |
| 5315A, UNIVERSAL COUNTER. 500.00 5326C, UNIVERSAL COUNTER. 50MHz. 100.00 |
| 3328A. IIMEK/COUNTER. SOOMHZ DUAL CHANNEL 250.00 |
| 59500A, MULTIPROGRAMMER INTERFACE 500 00 |
| 6110A, 3000V AT 6mA DUAL POLARITY POWER SUPPLY275.00 6111A, PRECISION POWER SUPPLY, 0-20V, 0-1A275.00 |
| 6130B, BIPOLAR DIGITAL PROG. POWER SUPPLY, +/-500A600.00 |
| 6130B, BIPOLAR DIGITAL PROG. POWER SUPPLY, +/-500A600.00 6131B, CVCC, PROG., +/-100@5A |
| 6200B, 40V/20V AT 0.3A/0.6A CVCC POWER SUPPLY 200.00 |
| 6200B, 40V/20V AT 0.3A/0.6A CVCC POWER SUPPLY 200.00 6201, 0-20V, 0-1.3A, THREE UNITS 175.00 |
| E 6201, 0-20V, 0-1.3A, THREE UNITS |
| 6264B, 20V AT 20A CVCC POWER SUPPLY |
| 6282A, 10V AT 10A CVCC POWER SUPPLY 275.00 |
| 6 6284A, 0-20V DC AT 3A DC POWER SUPPLY |
| 6291A, 40V AT 5A CVCC POWER SUPPLY |
| 6439B, 0-60V DC AT 15A DC |
| 6448B, 600V AT 1.5A CVCC POWER SUPPLY |
| 652A, AUDIO OSCILLATOR, 10Hz-10MHz. 275.00 6824A, POWER SUPPLY/AMPLIFIER, 50V 1A. 300.00 |
| 6940B. MULTIPROGRAMMER 500.00 |
| 6942A, MULTIPROGRAMMER |
| 174 775D, DUAL DIRECTIONAL COUPLER, 450-950MHZ250.00 |

| CASE AND THE STOLEN, 2-12.4 CHZ. | 133.00 |
|---|---------|
| 8405A, VECTOR VOLTMETER, 1-1000 MHz | 600.00 |
| 8407A, NETWORK ANALYZER, 0.1-110 MHz. | 300.00 |
| 0411, ILANN FREQ CONV. UPI (18. ().11-18.0GHZ | 725.00 |
| 8411A, FREO CONV for 8410, 110MHz-12.4GHz | 500.00 |
| 8411A/018, FREQ CONV for 8410, 110MHz-18GHz | 725 00 |
| 8412A, PHASE MAG. DISPLAY for 8410 | 400.00 |
| | |
| 8414A, POLAR DISPLAY | |
| 8418A, AUX. DISPLAY HOLDER. | 200.00 |
| 8443A, TRACKING GEN/COUNTER, LED DISPLAY | 700.00 |
| 8444A, TRACKING GENERATOR, 0.5-1300 MHz | 800.00 |
| 8445B, AUTOMATIC PRESELECTOR | 700.00 |
| 8447A, AMPLIFIER, 0.1-400 MHz. | 300.00 |
| 8552A, IF SECTION. | 500.00 |
| 8413A, PHASE GAIN INDICATOR for 8410 8414A, POLAR DISPLAY. 8418A, AUX. DISPLAY HOLDER. 8443A, TRACKING GEN/COUNTER, LED DISPLAY 8443A, TRACKING GENERATOR, 0.5-1300 MHz. 8445B, AUTOMATIC PRESELECTOR. 8447A, AMPLIFIER, 0.1-400 MHz. 8552A, IF SECTION. 8552B, IF SECTION. 0-110 MHz | 750.00 |
| 8553B, RF SECTION, 0-110 MHz | 500.00 |
| 8553B, RF SECTION, 0-110 MHz | |
| 8554B, RF SECTION, 0.1-1250 MHz | 800.00 |
| 8554B, RF SECTION, 0.1-1250 MHz. 8555A, RF SECTION, 10 MHz-18 GHz. 8556A, LF SECTION, 20 Hz-300 kHz. | 800.00 |
| 8556A, LF SECTION, 20 Hz-300 kHz | 500.00 |
| 85B, COMPUTER | 350.00 |
| 85B, COMPUTER. 8614A, SIGNAL GENERATOR, 0.8-2.4 GHz. | 375.00 |
| 8620A/8621A, SWEEP OSC. SYSTEM 0.1-4.2 GHz | 600.00 |
| 8620A/8621A, SWEEP OSC. SYSTEM 0.1-4.2 GHz. 8620C/011, SWEEP OSCILLATOR MAINFRAME, HPIB | 550.00 |
| 86222A, RF PLUG-IN, 0.1-2.4GHZ | 400.00 |
| 86222B, RF PLUG-IN, 0.1-2.4GHZ | 1700.00 |
| 00222B/002, KF PLUG-IN, 0.01-2.4 GHz | 1800.00 |
| 86230B, RF PLUG IN, 1.8-4.2 GHz | 400.00 |
| 80240B, 2-8.4GHZ PLUG | 200 00 |
| 86241A/001, RF PLUG IN, 3.2-6.5 GHz | 400.00 |
| 86245A, RF PLUG-IN, 59-12.4GHZ. 86245A, RF PLUG-IN, 12.4-18GHZ. 86260A, RF PLUG-IN, 12.4-18GHZ. 8640B, SIGNAL GENERATOR, 0.5-512 MHz, AM/FM | 250.00 |
| 80200A, RF PLUG-IN, 12.4-18GHZ | 800.00 |
| 8040B, SIGNAL GENERATOR, 0.5-512 MHz, AM/FM | 1400.00 |
| 000JD, SIGNAL GENERATOR, 2.3-6.5 GH7. | 4000.00 |
| 8740A/H18, TRANSMISSION TEST UNIT, DC-18 GHz | 100.00 |
| 8742A, REFLECTION TEST SET | 500.00 |
| 8745A, S-PARAMETER TEST SET, 0.1-2.0GHZ | |
| 9278A. PLOTTER | 125.00 |
| | |

TEKTRONIX

| 10 | | |
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| 0 | 1240, LOGIC ANAL W/ 2 D2 CARDS, 36 CHANNEL | 1000.00 |
| 0 | 1240, LOGIC ANAL W/ 2 D2 CARDS, 36 CHANNEL 1241/D2/D2, LOGIC ANAL, 36 CHAN, 50 MHz, CLR DI | SP 2000.00 |
| 0 | 144. NISC TEST SIGNAL GENERATOR | 700.00 |
| 0 | 147, NISC TEST SIGNAL GENERATOR | \$600.00 |
| 0 | 184. TIME MARK GENERATOR | 50.00 |
| 0 | | |
| 0 | 2215, 60MHz DUAL TRACE O'SCOPE | \$800.00 |
| 0 | 2215, 60MHz DUAL CHANNEL O'SCOPE | \$1200.00 |
| 0 | 2245, 100MHz, CH 34 for DMM MEASURE | \$1700.00 |
| 0 | 2246, 100MHz 100MHz ON SCREEN DMM | \$1900.00 |
| 0 | 2445,150MHZ CURSORS. 2465, 300MHz 4 CHANNEL 0'SCOPE | \$2500.00 |
| 0 | 2465, 300MHz 4 CHANNEL O'SCOPE | \$3500.00 |
| 0 | 434, STORAGE O'SCOPE, 25MHZ | |
| 0 | 434, STORAGE O'SCOPE, 25 MHZ. 465B, 100MHz DUAL VERT./TIME O'SCOPE. 466, 100 MHz VERT./TIME STORAGE O'SCOPE | |
| 0 | 466, 100 MHz VERT./TIME STORAGE O'SCOPE | 1100.00 |
| 0 | 475, 200 MILL DUAL CHANNEL USLUFE | /50.00 |
| 0 | 475A 250MHZ DUAL CHANNEL O'SCOPE | 015 00 |
| 0 | 485, 350 MHz DUAL VERT./TIME O'SCOPE | 900.00 |
| 0 | 485, 350 MHz DUAL VERT /TIME O'SCOPE. 491, SPECTRUM ANALYZER, 10 MHz-12.4 GHz | 950.00 |
| 0 | 492. SPECIKUM ANALYZEK, S0 kHz-21 (iHz | 5950.00 |
| 0 | 528, TELEVISION WAVEFORM MONITOR. | |
| 5 | 5440/D40, 50 MHz THREE SLOT FRAME | |
| 0 | 577/D2, CURVE TRACER 5A22N, DIFFERENTIAL AMPLIFIER | 1505.00 |
| - | SA22N, DIFFERENTIAL AMPLIFIER. | 400.00 |
| 0 | 7623A, MULTIMODE STORAGE O'SCOPE, 100MHz | |
| 0 | 7633, 100 MHz STORAGE, 1000cm/uS WRITING | 600.00 |
| 0 | 7704, ISOMHZ, FOUR SLOT FRAME | 250.00 |
| | 7704, 150MHz, FOUR SLOT FRAME | |
| ĥ | 7834, 400 MHZ STORAGE, 2500 cm/uS WRITING. | |
| 'n | 7034, 400 MILZ SIS, W/(11/A/4/(11/A/6/11/B80/(11/B85 | 1150.00 |
| ň | 7844, 400 MHz DUAL BEAM FRAME | 900.00 |
| 'n | 7904, 500 MHz FOUR SLOT FRAME. | 450.00 |
| 2 | 7904, 500 MHz SYS, W/(1)7A19,(1)7A26.(1)7B80,(1)7B85, 7A13, DIFFERENTIAL COMPARATOR, LED DISPLAY. | 1000.00 |
| 1 | 7A14 CURPENT PROPE AND WEER TOOLSPLAY. | 400.00 |
| 'n | 7A14, CURRENT PROBE AMPLIFIER, 120MHz. | |
| í. | 7A18, 75 MHz DUAL TRACE AMP | 100.00 |
| 'n | 7A19, 600 MHz AMP. 7A24, 400 MHz DUAL TRACE AMP. | 250.00 |
| í | 7A24, 400 MHZ DUAL TRACE AMP. | 450.00 |
| í | 7A26, 200 MHz DUAL TRACE AMP. | 200.00 |
| 5 | 7A29, 16Hz VERT. PLUG. 7A42, 4 CHANNEL LOGIC TRIG. VERT. AMP., 350MH | 800.00 |
| , | 1A42, 4 CHANNEL LUGIC TRIG. VERT. AMP., 350MH | Iz1500.00 |

DOVEDE **ELECTR®NICS**

| 7B10, DELAY TIME 2ns/.2s/DELTA TIME 350.00 7B15, DELAY TIME 2ns/.2s. 400.00 7B33A, 100 MHz DUAL TIME BASE 200.00 7B80, 400 MHz DELAYED TIME BASE 200.00 7B85, 400 MHz DELAYED TIME BASE 200.00 7B55, 400 MHz DUAL TIME DELAYING TIME BASE 250.00 7D01, LOGIC ANALYZER PLUG 200.00 7D02/PM111, LOGIC ANALYZER W/6809 POD 450.00 7D13, 21/2 DIGIT DMM 125.00 7D15, 225 MHz UNIVERSAL COUNTER/TIMER 300.00 7D11, DELAY LINE 100.01 711, SAMPLING UNIT 400.00 7S11, SAMPLING UNIT 400.00 7S12/S6/S52/7603, TDR SAMPLING SYSTEM W/S6, S52. 1950.00 7T11, SAMPLING SSO MHz UNIV COUNTER 1350.00 DC5009/01, PROG 135 MHz UNIV COUNTER 1350.00 DC5030, DIGITAL COUNTER PLUG-IN, 100MHz 350.00 DC5034, 125 MHz UNIVERSAL COUNTER 1350.00 DC5034, 125 MHz UNIVERSAL COUNTER 250.00 DC5034, 225 MHz UNIVERSAL COUNTER 250.00 DC504, COUNTER/TIMER, 1Hz-80MHz 185.00 DC5050, 135 MHz UNIVERSAL COUNTER 250.00 DS010, DIGITAL DELAY 75.00 DMS010, PR | | |
|--|---|----------|
| 7B92A, 500 MHz DUAL TIME BASE | 7B10, DELAY TIME 2ns/.2s/DELTA TIME | 350.00 |
| 7B92A, 500 MHz DUAL TIME BASE | 7B15 DELAY TIME 2ns/.2s. | 400.00 |
| 7B92A, 500 MHz DUAL TIME BASE | 7B53A 100 MHZ DUAL TIME BASE | 200.00 |
| 7B92A, 500 MHz DUAL TIME BASE | 7080 400 MH2 DELAYED TIME BASE | 200.00 |
| 7B92A, 500 MHz DUAL TIME BASE | 7885 400 MH2 DELTA TIME DELAYING TIME BASE | 250.00 |
| 7D01, LOGIC ANALYZER PLUG. 200.00 7D02/PM111, LOGIC ANALYZER W/6809 POD. 450.00 7D10, DIGITAL EVENT DELAY. 200.00 7D13, 3-1/2 DIGIT DMM. 125.00 7D15, 225 MHz UNIVERSAL COUNTER/TIMER. 300.00 7D207, PROGRAMMABLE DIGITIZER. 250.00 7M11, DELAY LINE. 150.00 7S11, SAMPLING UNIT. 400.00 7S12/S6/S52/7603, TDR SAMPLING SYSTEM W/S6, S52. 1950.00 7111, SAMPLING SWEEP UNIT. 7M11, OPERATIONAL AMP. 100.00 AM501, OPERATIONAL AMP. 100.00 DC5009/01, PROG 135 MHz UNIV CTR, TCXO. 750.00 DC5010, PROG. 350 MHz UNIV. COUNTER. 1350.00 DC503, DIGITAL COUNTER PLUG-IN, 100MHz. 350.00 DC503, DIGITAL COUNTER PLUG-IN, 100MHz. 350.00 DC504, COUNTER/TIMER, .1Hz-80MHz. 185.00 DC505A, 225 MHz UNIVERSAL COUNTER. 250.00 DM501, DIGITAL DELAY 350.00 DM501, DMM MODULE, 4,5 DIGIT DISPLAY. 275.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DMM. 350.00 DM502, MULTIMETER, 3.5 DIGIT. 225.00 PG504, 40 MHz FUNCTION GENERATOR. 250.00 PG503, 3 MHz FUNCTION GENERATOR. <t< td=""><td>7003, 400 MHZ DELIA TIME BASE</td><td>450.00</td></t<> | 7003, 400 MHZ DELIA TIME BASE | 450.00 |
| 7D201, PROURAMMABLE DIGITIZED. 150.00 7M11, DELAY LINE. 400.00 7S11, SAMPLING UNIT. 400.00 7S12/S6/S52/7603, TDR SAMPLING SYSTEM W/S6, S521950.00 7711, SAMPLING SWEEP UNIT. 7M10, OPERATIONAL AMP. 100.00 0C5009/01, PROG 135 MHz UNIV CTR, TCXO. 750.00 DC5010, PROG. 350 MHz UNIV. COUNTER. 1350.00 DC503, DIGITAL COUNTER PLUG-IN, 100MHz. 350.00 DC503, 125 MHz UNIVERSAL COUNTER. 500.00 DC504, COUNTER/TIMER, .1Hz-80MHz. 85.00 DC5050, 135 MHz UNIVERSAL COUNTER. 250.00 DC509, 135 MHz UNIVERSAL COUNTER. 700.00 DD501, DIGITAL DELAY. 350.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DISPLAY. 275.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DISPLAY. 275.00 DM5010, ROGRAMMABLE 4-1/2 DIGIT DIMM. 350.00 DM502, MULTIMETER, 3.5 DIGIT. 225.00 PG501, 1 MHz FUNCTION GENERATOR. 250.00 PG502, 11 MHz FUNCTION GENERATOR. 250.00 PG503, 3 MHz FUNCTION GENERATOR. 250.00 PG504, 40 MHz FUNCTION GENERATOR. 250.00 PG504, 40 MHz FUNCTION GENERATOR. 250.00 PG501, 50 MHz PUL | TBYZA, SUO WITZ DUAL TIME DISE | 200.00 |
| 7D201, PROURAMMABLE DIGITIZED. 150.00 7M11, DELAY LINE. 400.00 7S11, SAMPLING UNIT. 400.00 7S12/S6/S52/7603, TDR SAMPLING SYSTEM W/S6, S521950.00 7711, SAMPLING SWEEP UNIT. 7M10, OPERATIONAL AMP. 100.00 0C5009/01, PROG 135 MHz UNIV CTR, TCXO. 750.00 DC5010, PROG. 350 MHz UNIV. COUNTER. 1350.00 DC503, DIGITAL COUNTER PLUG-IN, 100MHz. 350.00 DC503, 125 MHz UNIVERSAL COUNTER. 500.00 DC504, COUNTER/TIMER, .1Hz-80MHz. 85.00 DC5050, 135 MHz UNIVERSAL COUNTER. 250.00 DC509, 135 MHz UNIVERSAL COUNTER. 700.00 DD501, DIGITAL DELAY. 350.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DISPLAY. 275.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DISPLAY. 275.00 DM5010, ROGRAMMABLE 4-1/2 DIGIT DIMM. 350.00 DM502, MULTIMETER, 3.5 DIGIT. 225.00 PG501, 1 MHz FUNCTION GENERATOR. 250.00 PG502, 11 MHz FUNCTION GENERATOR. 250.00 PG503, 3 MHz FUNCTION GENERATOR. 250.00 PG504, 40 MHz FUNCTION GENERATOR. 250.00 PG504, 40 MHz FUNCTION GENERATOR. 250.00 PG501, 50 MHz PUL | TOUL LUGIC ANALIZER TECO | 450.00 |
| 7D201, PROURAMMABLE DIGITIZED. 150.00 7M11, DELAY LINE. 400.00 7S11, SAMPLING UNIT. 400.00 7S12/S6/S52/7603, TDR SAMPLING SYSTEM W/S6, S521950.00 7711, SAMPLING SWEEP UNIT. 7M10, OPERATIONAL AMP. 100.00 0C5009/01, PROG 135 MHz UNIV CTR, TCXO. 750.00 DC5010, PROG. 350 MHz UNIV. COUNTER. 1350.00 DC503, DIGITAL COUNTER PLUG-IN, 100MHz. 350.00 DC503, 125 MHz UNIVERSAL COUNTER. 500.00 DC504, COUNTER/TIMER, .1Hz-80MHz. 85.00 DC5050, 135 MHz UNIVERSAL COUNTER. 250.00 DC509, 135 MHz UNIVERSAL COUNTER. 700.00 DD501, DIGITAL DELAY. 350.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DISPLAY. 275.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DISPLAY. 275.00 DM5010, ROGRAMMABLE 4-1/2 DIGIT DIMM. 350.00 DM502, MULTIMETER, 3.5 DIGIT. 225.00 PG501, 1 MHz FUNCTION GENERATOR. 250.00 PG502, 11 MHz FUNCTION GENERATOR. 250.00 PG503, 3 MHz FUNCTION GENERATOR. 250.00 PG504, 40 MHz FUNCTION GENERATOR. 250.00 PG504, 40 MHz FUNCTION GENERATOR. 250.00 PG501, 50 MHz PUL | /DUZ/PMIII, LUGIC ANALIZER W/0009 10D | 200.00 |
| 7D201, PROURAMMABLE DIGITIZED. 150.00 7M11, DELAY LINE. 400.00 7S11, SAMPLING UNIT. 400.00 7S12/S6/S52/7603, TDR SAMPLING SYSTEM W/S6, S521950.00 7711, SAMPLING SWEEP UNIT. 7M10, OPERATIONAL AMP. 100.00 0C5009/01, PROG 135 MHz UNIV CTR, TCXO. 750.00 DC5010, PROG. 350 MHz UNIV. COUNTER. 1350.00 DC503, DIGITAL COUNTER PLUG-IN, 100MHz. 350.00 DC503, 125 MHz UNIVERSAL COUNTER. 500.00 DC504, COUNTER/TIMER, .1Hz-80MHz. 85.00 DC5050, 135 MHz UNIVERSAL COUNTER. 250.00 DC509, 135 MHz UNIVERSAL COUNTER. 700.00 DD501, DIGITAL DELAY. 350.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DISPLAY. 275.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DISPLAY. 275.00 DM5010, ROGRAMMABLE 4-1/2 DIGIT DIMM. 350.00 DM502, MULTIMETER, 3.5 DIGIT. 225.00 PG501, 1 MHz FUNCTION GENERATOR. 250.00 PG502, 11 MHz FUNCTION GENERATOR. 250.00 PG503, 3 MHz FUNCTION GENERATOR. 250.00 PG504, 40 MHz FUNCTION GENERATOR. 250.00 PG504, 40 MHz FUNCTION GENERATOR. 250.00 PG501, 50 MHz PUL | 7D10, DIGITAL EVENT DELAT. | 125.00 |
| 7D201, PROURAMMABLE DIGITIZED. 150.00 7M11, DELAY LINE. 400.00 7S11, SAMPLING UNIT. 400.00 7S12/S6/S52/7603, TDR SAMPLING SYSTEM W/S6, S521950.00 7711, SAMPLING SWEEP UNIT. 7M10, OPERATIONAL AMP. 100.00 0C5009/01, PROG 135 MHz UNIV CTR, TCXO. 750.00 DC5010, PROG. 350 MHz UNIV. COUNTER. 1350.00 DC503, DIGITAL COUNTER PLUG-IN, 100MHz. 350.00 DC503, 125 MHz UNIVERSAL COUNTER. 500.00 DC504, COUNTER/TIMER, .1Hz-80MHz. 85.00 DC5050, 135 MHz UNIVERSAL COUNTER. 250.00 DC509, 135 MHz UNIVERSAL COUNTER. 700.00 DD501, DIGITAL DELAY. 350.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DISPLAY. 275.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DISPLAY. 275.00 DM5010, ROGRAMMABLE 4-1/2 DIGIT DIMM. 350.00 DM502, MULTIMETER, 3.5 DIGIT. 225.00 PG501, 1 MHz FUNCTION GENERATOR. 250.00 PG502, 11 MHz FUNCTION GENERATOR. 250.00 PG503, 3 MHz FUNCTION GENERATOR. 250.00 PG504, 40 MHz FUNCTION GENERATOR. 250.00 PG504, 40 MHz FUNCTION GENERATOR. 250.00 PG501, 50 MHz PUL | 7D13, 3-1/2 DIGIT DMM | 300.00 |
| 7D201, PROURAMMABLE DIGITIZED. 150.00 7M11, DELAY LINE. 400.00 7S11, SAMPLING UNIT. 400.00 7S12/S6/S52/7603, TDR SAMPLING SYSTEM W/S6, S521950.00 7711, SAMPLING SWEEP UNIT. 7M10, OPERATIONAL AMP. 100.00 0C5009/01, PROG 135 MHz UNIV CTR, TCXO. 750.00 DC5010, PROG. 350 MHz UNIV. COUNTER. 1350.00 DC503, DIGITAL COUNTER PLUG-IN, 100MHz. 350.00 DC503, 125 MHz UNIVERSAL COUNTER. 500.00 DC504, COUNTER/TIMER, .1Hz-80MHz. 85.00 DC5050, 135 MHz UNIVERSAL COUNTER. 250.00 DC509, 135 MHz UNIVERSAL COUNTER. 700.00 DD501, DIGITAL DELAY. 350.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DISPLAY. 275.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DISPLAY. 275.00 DM5010, ROGRAMMABLE 4-1/2 DIGIT DIMM. 350.00 DM502, MULTIMETER, 3.5 DIGIT. 225.00 PG501, 1 MHz FUNCTION GENERATOR. 250.00 PG502, 11 MHz FUNCTION GENERATOR. 250.00 PG503, 3 MHz FUNCTION GENERATOR. 250.00 PG504, 40 MHz FUNCTION GENERATOR. 250.00 PG504, 40 MHz FUNCTION GENERATOR. 250.00 PG501, 50 MHz PUL | 7D15, 225 MHz UNIVERSAL COUNTER/ IIMER | 2500.00 |
| AM301, OFERATIONAL ANI | 7D20T, PROGRAMMABLE DIGITIZER | 150.00 |
| AM301, OFERATIONAL ANI | 7M11, DELAY LINE | |
| AM301, OFERATIONAL ANI | 7S11, SAMPLING UNIT | 400.00 |
| AM301, OFERATIONAL ANI | 7S12/S6/S52/7603, TDR SAMPLING SYSTEM W/S6, S52. | |
| AM301, OFERATIONAL ANI | 7T11. SAMPLING SWEEP UNIT. | 900.00 |
| DC5010, PROG. 350 MHz UNIV. COUNTER. 1250.00 DC503, DIGITAL COUNTER PLUG-IN, 100MHz. 350.00 DC503A, 125 MHz UNIVERSAL COUNTER. 500.00 DC504, COUNTER/TIMER, 1Hz-80MHz. 185.00 DC505A, 225 MHz UNIVERSAL COUNTER. 250.00 DC509, 135 MHz UNIVERSAL COUNTER. 700.00 DD501, DIGITAL DELAY. 350.00 DM501, DMM MODULE, 4,5 DIGIT DISPLAY. 275.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DMM. 300.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT. 300.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT. 300.00 DM502, MULTIMETER, 3.5 DIGIT. 225.00 FG501, 1 MHz FUNCTION GENERATOR. 250.00 FG502, 11 MHz FUNCTION GENERATOR. 250.00 FG503, 3 MHz FUNCTION GENERATOR. 250.00 FG504, 40 MHz FUNCTION GENERATOR. 250.00 PG504, 40 MHz FUNCTION GENERATOR. 300.00 PG501, 50 MHz PULSE GEN. 300.00 PG503, 50 MHz PULSE GEN. 300.00 PS5011, 0-20V PRECISION POWER SUPPLY. 150.00 PS5011, 0-20V PRECISION POWER SUPPLY. 150.00 PS5013, DUAL POWER SUPPLY 250.00 R5103N, RACK MOUNT O'SCOPE 200.00 <td>AM501. OPERATIONAL AMP</td> <td>100.00</td> | AM501. OPERATIONAL AMP | 100.00 |
| DC5010, PROG. 350 MHz UNIV. COUNTER. 1250.00 DC503, DIGITAL COUNTER PLUG-IN, 100MHz. 350.00 DC503A, 125 MHz UNIVERSAL COUNTER. 500.00 DC504, COUNTER/TIMER, 1Hz-80MHz. 185.00 DC505A, 225 MHz UNIVERSAL COUNTER. 250.00 DC509, 135 MHz UNIVERSAL COUNTER. 700.00 DD501, DIGITAL DELAY. 350.00 DM501, DMM MODULE, 4,5 DIGIT DISPLAY. 275.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DMM. 300.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT. 300.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT. 300.00 DM502, MULTIMETER, 3.5 DIGIT. 225.00 FG501, 1 MHz FUNCTION GENERATOR. 250.00 FG502, 11 MHz FUNCTION GENERATOR. 250.00 FG503, 3 MHz FUNCTION GENERATOR. 250.00 FG504, 40 MHz FUNCTION GENERATOR. 250.00 PG504, 40 MHz FUNCTION GENERATOR. 300.00 PG501, 50 MHz PULSE GEN. 300.00 PG503, 50 MHz PULSE GEN. 300.00 PS5011, 0-20V PRECISION POWER SUPPLY. 150.00 PS5011, 0-20V PRECISION POWER SUPPLY. 150.00 PS5013, DUAL POWER SUPPLY 250.00 R5103N, RACK MOUNT O'SCOPE 200.00 <td>DC5009/01. PROG 135 MHz UNIV CTR, TCXO</td> <td>750.00</td> | DC5009/01. PROG 135 MHz UNIV CTR, TCXO | 750.00 |
| DC503A, 125 MHz UNIVERSAL COUNTER. 300.00 DC504, COUNTER/TIMER, 1Hz-80MHz. 185.00 DC505A, 225 MHz UNIVERSAL COUNTER. 250.00 DC509, 135 MHz UNIVERSAL COUNTER. 700.00 DD501, DIGITAL DELAY. 350.00 DM501, DMM MODULE, 4,5 DIGIT DISPLAY. 275.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DMM. 350.00 DM5014, MULTIMETER, 4.5 DIGIT. 175.00 DM502 MULTIMETER, 3.5 DIGIT. 225.00 FG501, 1 MHz FUNCTION GENERATOR. 250.00 FG502, 11 MHz FUNCTION GENERATOR. 250.00 FG503, 3 MHz FUNCTION GENERATOR. 250.00 FG504, 40 MHz FUNCTION GENERATOR. 250.00 FG505, 50 MHz FULSE GEN. 300.00 PG504, 50 MHz PULSE GEN. 300.00 PG501, 50 MHz PULSE GEN. 500.00 PS5010, POWER SUPPLY 150.00 PS5011, 0-20V PRECISION POWER SUPPLY 150.00 PS5012, DAL POWER SUPPLY 150.00 PS5013, DAL POWER SUPPLY 250.00 PS5014, 0-20V PRECISION POWER SUPPLY 250.00 PS5013, DAL POWER SUPPLY 250.00 PS5013, DAL POWER SUPPLY 250.00 PS5014, 0-20V PRECISION POWE | DC5010, PROG. 350 MHz UNIV. COUNTER | .1350.00 |
| DC503A, 125 MHz UNIVERSAL COUNTER. 300.00 DC504, COUNTER/TIMER, 1Hz-80MHz. 185.00 DC505A, 225 MHz UNIVERSAL COUNTER. 250.00 DC509, 135 MHz UNIVERSAL COUNTER. 700.00 DD501, DIGITAL DELAY. 350.00 DM501, DMM MODULE, 4,5 DIGIT DISPLAY. 275.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DMM. 350.00 DM5014, MULTIMETER, 4.5 DIGIT. 175.00 DM502 MULTIMETER, 3.5 DIGIT. 225.00 FG501, 1 MHz FUNCTION GENERATOR. 250.00 FG502, 11 MHz FUNCTION GENERATOR. 250.00 FG503, 3 MHz FUNCTION GENERATOR. 250.00 FG504, 40 MHz FUNCTION GENERATOR. 250.00 FG505, 50 MHz FULSE GEN. 300.00 PG504, 50 MHz PULSE GEN. 300.00 PG501, 50 MHz PULSE GEN. 500.00 PS5010, POWER SUPPLY 150.00 PS5011, 0-20V PRECISION POWER SUPPLY 150.00 PS5012, DAL POWER SUPPLY 150.00 PS5013, DAL POWER SUPPLY 250.00 PS5014, 0-20V PRECISION POWER SUPPLY 250.00 PS5013, DAL POWER SUPPLY 250.00 PS5013, DAL POWER SUPPLY 250.00 PS5014, 0-20V PRECISION POWE | DC503 DIGITAL COUNTER PLUG-IN, 100MHz. | 350.00 |
| DC504, COUNTER/TIMER, 1Hz-80MHz. 183.00 DC505A, 225 MHz UNIVERSAL COUNTER. 250.00 DC509, 135 MHz UNIVERSAL COUNTER/TIMER. 700.00 DD501, DIGITAL DELAY. 350.00 DM501, DMM MODULE, 4,5 DIGIT DISPLAY. 275.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DMM. 300.00 DM5010, MULTIMETER, 4.5 DIGIT. 300.00 DM502, MULTIMETER, 3.5 DIGIT. 225.00 PG501, 1 MHz FUNCTION GENERATOR. 250.00 PG502, 11 MHz FUNCTION GENERATOR. 250.00 PG503, 3 MHz FUNCTION GENERATOR. 250.00 PG504, 40 MHz FUNCTION GENERATOR. 250.00 PG504, 50 MHz PULSE GEN. 300.00 PG501, 50 MHz PULSE GEN. 300.00 PG501, 90 WER SUPPLY 100.00 PS501-1, 0-20V PRECISION POWER SUPPLY. 150.00 PS5010, PROGRAMMABLE TRIPLE POWER SUPPLY. 50.00 PS5010, PROGRAMMABLE TRIPLE POWER SUPPLY. 50.00 PS5010, PROGRAMMABLE TRIPLE POWER SUPPLY. 50.00 PS5013, DUAL POWER SUPPLY. 250.00 R5103N, RACK MOUNT O'SCOPE 200.00 SC504, 90 MHz O'SCOPE 475.00 | DCS02A 126 MUS LINIVERSAL COUNTER | |
| DC509, 135 MHz UNIVERSAL COUNTER/TIMER. 700.00 DD501, DIGITAL DELAY. 350.00 DM501, DMM MODULE, 4,5 DIGIT DISPLAY. 275.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DMM. 350.00 DM5014, MULTIMETER, 4.5 DIGIT. 300.00 DM502, MULTIMETER, 3.5 DIGIT. 175.00 DM502A, MULTIMETER, 3.5 DIGIT. 225.00 FG501, 1 MHz FUNCTION GENERATOR. 250.00 FG502, 11 MHz FUNCTION GENERATOR. 250.00 FG503, 3 MHz FUNCTION GENERATOR. 250.00 FG504, 40 MHz FUNCTION GENERATOR. 250.00 FG501, 50 MHz PULSE GEN. 300.00 P6504, 50 MHz PULSE GEN. 300.00 P6505, 50 MHz PULSE GEN. 500.00 P5501, POWER SUPPLY 100.00 P5501, POWER SUPPLY 150.00 P55010, PROGRAMMABLE TRIPLE POWER SUPPLY 150.00 P55013, DUAL POWER SUPPLY 250.00 R5103N, RACK MOUNT O'SCOPE 200.00 SC504, DUAL TRACE O'SCOPE PLUG, 15MHz. 475.00 | DC504 COUNTER/TIMER, 1Hz-80MHz | 185.00 |
| DC509, 135 MHz UNIVERSAL COUNTER/TIMER. 700.00 DD501, DIGITAL DELAY. 350.00 DM501, DMM MODULE, 4,5 DIGIT DISPLAY. 275.00 DM5010, PROGRAMMABLE 4-1/2 DIGIT DMM. 350.00 DM5014, MULTIMETER, 4.5 DIGIT. 300.00 DM502, MULTIMETER, 3.5 DIGIT. 175.00 DM502A, MULTIMETER, 3.5 DIGIT. 225.00 FG501, 1 MHz FUNCTION GENERATOR. 250.00 FG502, 11 MHz FUNCTION GENERATOR. 250.00 FG503, 3 MHz FUNCTION GENERATOR. 250.00 FG504, 40 MHz FUNCTION GENERATOR. 250.00 FG501, 50 MHz PULSE GEN. 300.00 P6504, 50 MHz PULSE GEN. 300.00 P6505, 50 MHz PULSE GEN. 500.00 P5501, POWER SUPPLY 100.00 P5501, POWER SUPPLY 150.00 P55010, PROGRAMMABLE TRIPLE POWER SUPPLY 150.00 P55013, DUAL POWER SUPPLY 250.00 R5103N, RACK MOUNT O'SCOPE 200.00 SC504, DUAL TRACE O'SCOPE PLUG, 15MHz. 475.00 | DC505A 225 MH7 UNIVERSAL COUNTER. | 250.00 |
| DD501, DIGITAL DELAY | DC500 125 MH ₂ UNIVERSAL COUNTER/LIMEK | |
| DM5010, PROGRAMMABLE 4-1/2 DIGIT DMM. 330.00 DM501A, MULTIMETER, 4.5 DIGIT. 300.00 DM502, MULTIMETER, 3.5 DIGIT. 175.00 DM502A, MULTIMETER, 3.5 DIGIT. 225.00 FG501, 1 MHz FUNCTION GENERATOR. 250.00 FG502, 11 MHz FUNCTION GENERATOR. 250.00 FG503, 3 MHz FUNCTION GENERATOR. 250.00 FG504, 40 MHz FUNCTION GENERATOR. 250.00 PG504, 40 MHz FUNCTION GENERATOR. 900.00 P6501, 50 MHz PULSE GEN. 300.00 PG503, 50 MHz PULSE GEN. 300.00 PS501, POWER SUPPLY 100.00 PS501, POWER SUPPLY 150.00 PS5010, PROGRAMMABLE TRIPLE POWER SUPPLY. 750.00 PS5013, DUAL POWER SUPPLY 250.00 R5103N, RACK MOUNT O'SCOPE 200.00 SC504, 90 MHz O'SCOPE PLUG, 15MHz. 475.00 | DDS01 DIGITAL DELAY | 350.00 |
| DM5010, PROGRAMMABLE 4-1/2 DIGIT DMM. 330.00 DM501A, MULTIMETER, 4.5 DIGIT. 300.00 DM502, MULTIMETER, 3.5 DIGIT. 175.00 DM502A, MULTIMETER, 3.5 DIGIT. 225.00 FG501, 1 MHz FUNCTION GENERATOR. 250.00 FG502, 11 MHz FUNCTION GENERATOR. 250.00 FG503, 3 MHz FUNCTION GENERATOR. 250.00 FG504, 40 MHz FUNCTION GENERATOR. 250.00 PG504, 40 MHz FUNCTION GENERATOR. 900.00 P6501, 50 MHz PULSE GEN. 300.00 PG503, 50 MHz PULSE GEN. 300.00 PS501, POWER SUPPLY 100.00 PS501, POWER SUPPLY 150.00 PS5010, PROGRAMMABLE TRIPLE POWER SUPPLY. 750.00 PS5013, DUAL POWER SUPPLY 250.00 R5103N, RACK MOUNT O'SCOPE 200.00 SC504, 90 MHz O'SCOPE PLUG, 15MHz. 475.00 | DMS01 DMM MODULE 45 DIGIT DISPLAY | |
| FG502, 11 MHZ FUNCTION GENERATOR. 250.00 FG503, 3 MHZ FUNCTION GENERATOR. 250.00 FG504, 40 MHZ FUNCTION GENERATOR. 900.00 P6504, 40 MHZ FUNCTION GENERATOR. 900.00 P6505, 1000X 40kV PROBE, AC/DC. 300.00 P6506, 50 MHZ PULSE GEN. 300.00 P5501, POWER SUPPLY 100.00 P5501, 0.20V PRECISION POWER SUPPLY 150.00 P55010, PROGRAMMABLE TRIPLE POWER SUPPLY 750.00 P55030, DUAL POWER SUPPLY 250.00 R5103N, RACK MOUNT O'SCOPE 200.00 SC502, DUAL TRACE O'SCOPE PLUG, 15MHz. 475.00 | DMS010 PROGRAMMARIE 4.1/2 DIGIT DMM | |
| FG502, 11 MHZ FUNCTION GENERATOR. 250.00 FG503, 3 MHZ FUNCTION GENERATOR. 250.00 FG504, 40 MHZ FUNCTION GENERATOR. 900.00 P6504, 40 MHZ FUNCTION GENERATOR. 900.00 P6505, 1000X 40kV PROBE, AC/DC. 300.00 P6506, 50 MHZ PULSE GEN. 300.00 P5501, POWER SUPPLY 100.00 P5501, 0.20V PRECISION POWER SUPPLY 150.00 P55010, PROGRAMMABLE TRIPLE POWER SUPPLY 750.00 P55030, DUAL POWER SUPPLY 250.00 R5103N, RACK MOUNT O'SCOPE 200.00 SC502, DUAL TRACE O'SCOPE PLUG, 15MHz. 475.00 | DMS010, FROORAMMADLE 41/2 DIGIT | |
| FG502, 11 MHZ FUNCTION GENERATOR. 250.00 FG503, 3 MHZ FUNCTION GENERATOR. 250.00 FG504, 40 MHZ FUNCTION GENERATOR. 900.00 P6504, 40 MHZ FUNCTION GENERATOR. 900.00 P6505, 1000X 40kV PROBE, AC/DC. 300.00 P6506, 50 MHZ PULSE GEN. 300.00 P5501, POWER SUPPLY 100.00 P5501, 0.20V PRECISION POWER SUPPLY 150.00 P55010, PROGRAMMABLE TRIPLE POWER SUPPLY 750.00 P55030, DUAL POWER SUPPLY 250.00 R5103N, RACK MOUNT O'SCOPE 200.00 SC502, DUAL TRACE O'SCOPE PLUG, 15MHz. 475.00 | DM502 MULTIMETER 35 DIGIT | 175.00 |
| FG502, 11 MHZ FUNCTION GENERATOR. 250.00 FG503, 3 MHZ FUNCTION GENERATOR. 250.00 FG504, 40 MHZ FUNCTION GENERATOR. 900.00 P6504, 40 MHZ FUNCTION GENERATOR. 900.00 P6505, 1000X 40kV PROBE, AC/DC. 300.00 P6506, 50 MHZ PULSE GEN. 300.00 P5501, POWER SUPPLY 100.00 P5501, 0.20V PRECISION POWER SUPPLY 150.00 P55010, PROGRAMMABLE TRIPLE POWER SUPPLY 750.00 P55030, DUAL POWER SUPPLY 250.00 R5103N, RACK MOUNT O'SCOPE 200.00 SC502, DUAL TRACE O'SCOPE PLUG, 15MHz. 475.00 | DMS02, MULTIMETER 35 DIGIT | 225.00 |
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| PS5010, PROGRAMMABLE TRIFLE FOWER SUTTER PS503A, DUAL POWER SUPPLY | P6015, 1000X 40kV PROBE, AC/DC | 300.00 |
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| | SG502 AUDIO OSCILLATOR. | 300.00 |

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| ANDTELL ML 423D /21 SELECTIVE LEVEL MELEK | |
| DAV PRECISION 1850A FRED COUNTER SIZMER. | |
| BAFCO 920A FREQUENCY RESPONSE ANALYZEK | / 50.00 |
| DIOMATION KD101 D LOGIC ANALYZER | |
| | |
| BLUE MPR-336E-MPI, ENV. CHAMB W/ CIR SRV0CORD BOONTON 92BD, DIG RF MV METER, 10KHz-1.2GHz BOONTON 93A, TRMS VOLTMETER, 10 Hz-20 MHz CLIMET CI-3100, OPTICAL PART. TRANSDUCER DANA 9000, MICROPROCESSING TIMER/COUNTER | 700.00 |
| BOONTON 93A, TRMS VOLTMETER, 10 Hz-20 MHz | 125.00 |
| CLIMET CI-3100, OPTICAL PART. TRANSDUCER | |
| DANA 9000, MICROPROCESSING TIMER/COUNTER | |
| DANA 9000, MICROPROCESSING TIMER/COUNTER. DELTRON SP, CVCC, 10V, 5A, METERED PWR SUP DELTRON SP, 40V, 5A, CVCC METERED PWR SUP E.S.I. SP-2534, 4-1/2 DIGIT LCR METER, GPIB. | 150.00 |
| DELTRON SP, 40V, 5A, CVCC METERED PWR SUP | 1000.00 |
| E.S.I. SP-2534, 4-1/2 DIGIT LCR METER, GPIB. | 2000.00 |
| FIP AST MICKUWAVE PULSE COUNTER. | |
| FLUKE 1722, IEEE 488 CONTROLLER | 175 00 |
| FLUKE 1910A, 125 MHz COUNTER/TIMER. | 250.00 |
| FLUKE 1920A, FREQUENCY COUNTER, 520MHZ | 250.00 |
| FLUKE 1952B, COUNTER/TIMER,TCXO, 2 CHAN. FLUKE 1953A/02, UNIV TIMER/COUNTER 2 CHAN. FLUKE 4265A, BIN PROG PRECISION PWR SUP. FLUKE 6011A, FREQ. SYN. 10MHz-11MHz, 1Hz RES. | 350.00 |
| FLUKE 1953A/02, UNIV TIMER/COUNTER 2 CHARMEN | 250.00 |
| FLUKE 4205A, BIN PROG PRECISION I WR SOT | 2000.00 |
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| FLUKE 750A, REFERENCE DIVIDER. FLUKE 8000A, DMM, 3.5 DIGITS, 5 FUNCTIONS. | 175.00 |
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| FLUKE 845AR, HIGH IMPEDANCE VOLTMETER. | 300.00 |
| FLUE 9600A DMM AS DIGITS FUNCTION | |
| GENERAL MICROWAVE 460B-10, 3 HEADS | |
| CENEDAL MICROWAVE A76 POWER MELER | |
| GUILDLINE 91540, TRANSVOLT 4890 STAND CELLS. | |
| CUILD SIG, DOAL THAT YOUT 4890 STAND CELLS. | |
| HARRISON LAB 6206A, POWER SUPPLY. | |
| | |
| HITACHI V-ISIF, FORT. O'SCOPE HITACHI V-212F, PORT. O'SCOPE HONEYWELL 1858/700, OSCILLOGRAPH | 700.00 |
| HONEYWELL 1858/700 OSCILLOGRAPH | 2000.00 |
| IBM SYSTEM 9000 CONTROLLER. | . 3000.00 |
| INTERSTATE F31 3 MHZ FUNCTION GENERATOR | |
| INTERSTATE F72, 20 MHz PULSE FUNCTION GEN | 450.00 |
| HONEY WELL 1838/100, CONTROLLER. IBM SYSTEM 9000, CONTROLLER. INTERSTATE F31, 3 MHz FUNCTION GENERATOR INTERSTATE F72, 20 MHz PULSE FUNCTION GEN INTERSTATE F23, PULSE GENERATOR | 200.00 |
| | |

| S BRUKER | |
|--|----------------------|
| INTERSTATE P24, PULSE GENERATOR | |
| INTERSTATE P24, PULSE GENERATOR. KAV 1/432D. ATTENUATOR. KAV 30-0, ATTENUATOR. KEITHLEY 225, CURRENT SOURCE. KEITHLEY 230, PROGRAMMABLE VOLTAGE SOURCE | |
| KAV 30-0, ATTENDENT SOURCE | |
| KEITHLEY 260, NANOVOLT SOURCE. | |
| KEITHLEY 261, PICOAMPERE SOURCE. | PIB500.00 |
| KEPCO BOP-72-1.5M, 72V AT 1.5A BP OP AMP/PWR S | UP400.00 |
| KEPCO BOP-72-3M, 72V AT 3A BI OT AMETERED SI KEPCO JQE, 36-3MVP, 36V AT 3A CVCC METERED SI | UP300.00 |
| KEPCO JQE, 100-2.5MVP, 1000 AT 2.5A CVCC MTR 30 KEPCO JOE, 15-6MVP, 15V 6A | |
| KEITHLEY 261, PICOAMPERE SOURCE KEITHLEY 705/2x7158, LOW CUR SCANNING SYS, G KEPCO BOP-72-1.5M, 72V AT 15A BP OP AMP/PWR SUP KEPCO JOE, 36-3MVP, 36V AT 3A CVCC METERED SI KEPCO JOE, 100-2.5MVP, 1000 AT 2.5A CVCC MTR SU KEPCO JOE, 15-6MVP, 15V 6A KEPCO JOE 55-10M, 55V AT 10A CVCC POWER SUPP KIKUSUI 5509, O'SCOPE, 15MHz, 4 CH | LY350.00 |
| KIKUSUI 5509, O'SCOPE, ISMHz, 4 CH KIKUSUI 5513, O'SCOPE KIKUSUI COS6100, 5-CHANNEL 100 MHz O'SCOPE LEADER 480-U71, TV-VIF PLUG IN UNIT LEADER LDM 170, DISTORTION METER. LEADER LMS-3100, TV SOUND METER LEADER LMS-3100, TV SOUND METER | |
| LEADER 480-U71. TV-VIF PLUG IN UNIT | |
| LEADER LDM 170, DISTORTION METER. | |
| LH RESEARCH 137A. PULSE GEN, 125MHz-10Hz MAGNAVOX T-23893 CHART PRINTER. | |
| MARCONI 2304, MOD METER | |
| MARCONI 2337A, AUTOMATIC DISTORTION METER | |
| MARCONI TF2370/TK, SPECTRUM ANAL., 0-1250 ME MAYNARD MAINSTREAM 150, 150MB EXT. TAPE D | RIVE FOR |
| LEADER LMS-3100, TV SOUND METER. LH RESEARCH 137A. PULSE GEN, 125MHz-10Hz. MAGNAVOX T-23893. CHART PRINTER. MARCONI 2304, MOD METER. MARCONI 2337A, AUTOMATIC DISTORTION METE MARCONI TF2300B, AM/FM MOD METER. MARCONI TF2370/TK, SPECTRUM ANAL, 0-1250 MH MAYNARD MAINSTREAM 150. 150MB EXT. TAPE D PS/2, UNUSED & COMPLETE. MEASUREMENTS CORP 80 . SIGNAL GENERATOR. MICRO TECHNICAL INDU 358 THERMO PROBE MICROTEL SG800, SWEEP SIGNAL GEN 1GHz-18GI MILLIVAC 828A. | |
| MICRO TECHNICAL INDU 358 THERMO PROBE | |
| MICROTEL SG800, SWEEP SIGNAL GEN IGHZIGH | |
| MICROTEL SG800, SWEEP SIGNAL GEN TORZIGO MILLIVAC 828A MILLIVAC MV-823B-S1, RF MILLIVOLTMETER, 10 KF 1mV-10V, W/ADAPTERS PHILLIPS 3226, O'SCOPE PHILLIPS 5512, NTSC TV PATTERN GENERATOR PHILLIPS 5512, NTSC TV PATTERN GENERATOR | 1z-1.2 GHz, |
| PHILLIPS 3226, O'SCOPE. | |
| PHILLIPS 5312, NISC TV TATTER OLIVEITER | |
| PHILLIPS PM2434B, AC MILLIVOLIMETER PHILLIPS PM3225. O'SCOPE PHILLIPS PM6302, RCL BRIDGE | |
| PHILLIPS PM6302, RCL BRIDGE PHILLIPS PM6611, UNIVERSAL COUNTER POWER DESIGN 2005A, PREC PWR SRCE, 20V, 500n POWER DESIGN 2K-10, 0-2000V 0-10mA CV PWR SU POWER DESIGN 6050A, UNIV DC SOURCE, TO 60V, POWER DESIGN 6050A, UNIV DC SOURCE, TO 60V, | nA200.00 |
| POWER DESIGN 2K-10, 0-2000V 0-10mA CV PWR SU | P200.00 |
| RACAL-DANA 1250, UNIV SWITCH CONTROLLER. | |
| RACAL-DANA 1230, UNV SWICH CONCESSING D RACAL-DANA SERIES 6000, MICROPROCESSING D RACAL-DANA SERIES 9000, TIMER/COUNTER 9 DI RADIO RESEARCH 41, AM/FM SIGNAL GENERATO | GIT250.00 |
| RADIO RESEARCH 41, AM/FM SIGNAL GENERATO RADIOMETER COPENHAGE SMG1 STEREO GEN | R200.00 |
| RFL INDUSTRIES 829G, AC/DC CAL STANDARD | |
| SLAUGHTER 103-2.5J. 2.5 KVAC HIPOT. | |
| RADIO RESEARCH 41, AM/FM SIGNAL GENERATO RADIO RESEARCH 41, AM/FM SIGNAL GENERATO RADIOMETER COPENHAGE SMG1 STEREO GEN RFL INDUSTRIES 829G, AC/DC CAL STANDARD SHIBASOKU AS9538, MPX TV SOUND SIGNAL GEN SLAUGHTER 103-2.5J. 2.5 KVAC HIPOT SLAUGHTER 103-2.5J. 2.5 KVAC HIPOT SLAUGHTER 205, MEGOHMETER 20,000 MEG ELEC SYSTRON-DONN 6244A/011. 4.5 GHz PORT CNT PPB/MNTH OXCO SYSTRON-DONNER 712-2A/809-A, SPECT ANAL SYSTRON-DONNER 712-2A/809-A, SPECT ANAL SYSTRON-DONNER M107, PREC DCV SRCE, 0-1kV/50 TAUTRON MB-1A, PCM ERROR RATE MEAS RECEI TAUTRON MB-302, BERT REC | TER, W/30 |
| PPB/MNTH OXCO SYSTRON-DONNER 712-2A/809-A, SPECT ANAL | 700.00 |
| SYSTRON-DONNER M107, PREC DCV SRCE, 0-1kV/50 | VER300.00 |
| TAUTRON MB-302, BERT REC. TAUTRON ME-1, PSEUDO RANDOM DATA RATE N | |
| TATTOON ME 202 DATA RATE EXTENDER | |
| D TAUTRON ME-502, DATA GENERATOR TAUTRON MR-502, BATT TRANSMITTER | |
| TAUTRON MS-2, UHF PULSE SOURCE | |
| TEXSCAN 7271. | 500.00 |
| 0 THERMOTRON 012005, TEMP LIMIT CONTROL | |
| A THE THE ALLA DIAN ACIDE VEC 2K 20M OHMS | 75 00 |
| | |
| 0 VU-DATA PS950, w/975, MINI O'SCOPE w/ COUNTE | |
| 0 WAVETEK 1002, SWEEP SIGNAL GENERATOR | |
| A WAVETEV 124 SWEEP GENERATOR | |
| 0 WAVETEK 1402A, VHF SWEEP GENERATOR FOR | USE W/1502, |
| 0 WAVETEK 1701, UHF/VHF SWEEP GENERATOR | 1500.00 FOR250.00 |
| | |
| 0 WAVETEK 1801A, SWEEP GEN, 1-350 MHZ, 15 OHM. 0 WAVETEK 182A, 4 MHZ FUNCTION GENERATOR 0 WAVETEK 184, 5 MHZ SWEEP/FUNCTION GENERA | TOR325.00 |
| WAVETEK 185, 5 MHz LIN/LOG SWEEP/FUNCT GE WAVETEK 2001A, SWEEP/SIGNAL GEN, 1-1400 MHz | N |
| WAVETER 3000, SIGNAL GENERATOR, 1-500MHZ | |
| WESTON ELECTRICAL IN 759 FOOT-LAMB METER | |

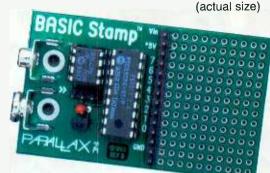


CINCLE 241 ON FREE INFORMATION CARD

BASIC STAMP

Stamp-Sized Computer Runs BASIC

The BASIC Stamp is a small single-board computer that runs BASIC programs. It has 8 I/O lines, which can be used for a variety of digital and analog purposes. The Stamp's BASIC language includes 'amiliar instructions, such as GOTO, FOR...NEXT, and IF...THEN, as well as SBC instructions, such as SERIN, PWM, and BUTTON. Each

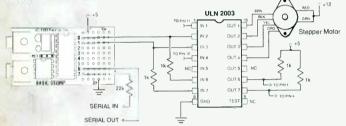


instruction takes 2-3 bytes of the Stamp's 256-byte EEPROM, resulting in a maximum program size of 80-100 instructions. Programs execute at about 2,000 instructions per second.

The BASIC Stamp Programming Package contains everything you need to program Stamps using your PC. The package includes our editor software, programming cable, manual, application notes, and free technical support. The package is available for \$99; Stamps are sold separately for \$39.

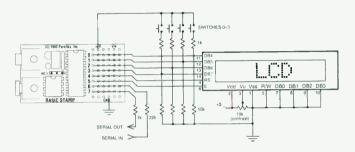
Stepper Motor Controller

This circuit makes the Stamp into a remote stepper motor controller. Using serial communications, the Stamp sends out a request for number of steps and delay between each. When it receives the data, the Stamp steps the motor as directed.



Micro-Terminal

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Models above shown actual size

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|--|---------------|----------------|-----------------|----------------|----------------|-----------------|---------------|----------------|
| tron | | | | | | | | |
| PLASTIC SURFACE-MOUNT | | | ++VAM-3 1.45 | | +VAM-6 1.29 | ++VAM-7 1.75 | | |
| add suffix SM to model no. (ex. MAR-ISM) | MAR-1 1.04 | MAR-2 1.40 | MAR-3 1.50 | MAR-4 1.60 | MAR-6 1.34 | MAR-7 1.80 | MAR-8 1.75 | |
| | MAV-1 1.15 | +MAV-2 1,45 | +MAV-3 1.55 | MAV-4 1.65 | | | | MAV-11 2.15 |
| CERAMIC SURFACE-MOUNT | RAM-1 4.95 | RAM-2 4.95 | RAM-3 4.95 | RAM-4 4.95 | RAM-6 4.95 | RAM-7 4.95 | RAM-8 4.95 | |
| PLASTIC FLAT-PACK | MAV-1 1.10 | +MAV-2 1.40 | +MAV-3 1.50 | +MAV-4 1.60 | | _ | | MAV-11 2.10 |
| | MAR-1 0.99 | MAR-2 1.35 | MAR-3 1.45 | MAR-4 1.55 | MAR-6 1.29 | MAR-7 1.75 | MAR-8 1.70 | |
| Freq.MHz,DC to | 1000 | 2000 | 2000 | 1000 | 2000 | 2000 | 1000 | 1000 |
| Gain, dB at 100MHz | 18.5 | 12.5 | 12.5 | 8.3 | 20 | 13.5 | 32.5 | 12.7 |
| Output Pwr. +dBm | 1.5 | 4.5 | 10.0 | 12.5 | 2.0 | 5.5 | 12.5 | 17.5 |
| NF, dB | 5.5 | 6.5 | 6.0 | 6.5 | 3.0 | 5.0 | 3.3 | 3.6 |
| Notes: + Erequency | range DC | -1500MHz | ++ 6 21 | n 1/2 dB lc | ee than ehr | 214/172 | | |

Notes: + Frequency range DC-1500MHz ++ Gain 1/2 dB less than shown

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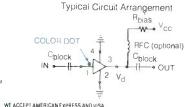
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