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ORIENTING AND GAIN. Each bay tilts in any plane, can be oriented in any direction to give sharpest focus possible. Eliminates awkward or tricky installations. Permits hairline adjustments for utmost gain on both the high and low band stations.

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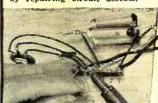
YOU BUILD THIS Radio Circuit early in Course with Soldering Equipment and Radio Parts I send; practice mounting, connecting, soldering Radio parts.



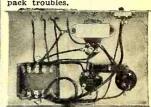
YOU PRACTICE Radio Servicing with this Tester built from parts I send. Also use it to help earn EXTRA MONEY fixing neighbors' Radios.



YOU PRACTICE "FM" Servicing on this Frequency Modulation (FM) Signal Generator, built with parts I supply; learn by repairing circuit defects.



YOU BUILD THIS Vacuum Tube Power Pack, make changes which give you experience, learn how to locate and correct power pack troubles



YOU BUILD THIS A. M. Signal Generator which provides amplitude-modulated signals for many tests and experiments. gives you practical experience.



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COVER PHOTO: High quality amplifiers undergo final laboratory tests at the Burbank plant of Bardwell & McAlister, Inc. Modern design test equipment is required to perform these checks.

(Staff Photo by Arthur E. Haug)

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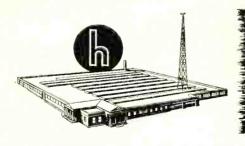


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- Removable calibrated screen for measure of wave amplitude and symmetry of form.
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June, 1948

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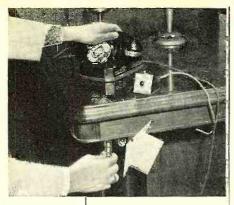
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For the RECORD THE EDITOR

Dell'and and the Company of the Comp

UR daily mail is seldom opened without revealing some very worthwhile and constructive comments from radio servicemen. Each letter is read with care and quite often, one will contain comments of particular interest in pointing out some "sore spot" that the radio serviceman feels can be healed with proper treatment.

The majority of letters are from servicemen that operate their own shops. Many have been in the radio repair business for years and have sold and repaired radios of many makes and models

These men are proud of the reputation they have enjoyed in their community in spite of the bad publicity leveled at their profession. When mechanical or electrical improvements can be made in the sets they sell, they then expect the manufacturer to at least listen to their reasoning and constructive criticism of his product.

We know that many servicemen would welcome an opportunity to be members of an Advisory Board to make recommendations to the set manufacturers, from a practical viewpoint, based on actual "case histories." These men could show, for example, that their selling profit on new sets is often cut simply because Mrs. Jones finds her brand new radio giving trouble and a service call is required.

Radio servicemen are looking for trouble in old sets-that's their bread and butter-but not in brand new ones that eat up their profit.

In analyzing the above mentioned letters it becomes apparent that the greatest criticism is made about methods and assembly techniques, rather than about the component parts in the sets. Loops

wound in cabinets, trick pilot lamps, miscellaneous connections to tuning gangs, plugless speaker cables and plastic covered wiring, these all interfere and take time to disconnect when seeking for trouble in Mrs. Jones' new receiver.

We'll bet that any group of radio service dealers, if given the opportunity, would insist that the sets they sell to their customers be engineered from a practical standpoint—not just on paper. It would be a step in the right direction.

URING the war many radiomen were forced to adopt substitute methods of servicing, due to the lack of proper test equipment, which was either too costly or not available.

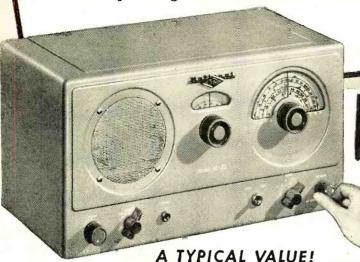
In the past two years there have been many new developments in new test Vacuum tube voltmeters equipment. have left the laboratory stage and now rank with the standard volt-ohm-milliameter in reliability. Signal tracers have been greatly simplified by the elimination of tuned circuits, and have greater versatility.

New signal generators make it possible to do an accurate job of aligning FM and TV receivers. In conjunction with an oscilloscope, the procedure may be made visual, with the result that a far better job may be done.

An audio oscillator in conjunction with an output meter or oscilloscope will enable the serviceman to make a check of audio systems, with resultant better over-all performance. The expenditure for proper test equipment will pay for itself in a short time-in time saved. Equip your shop with the best equipment and give your customers improved service at lower cost. . . . O.R.



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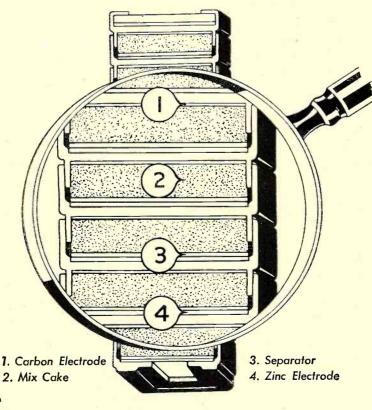
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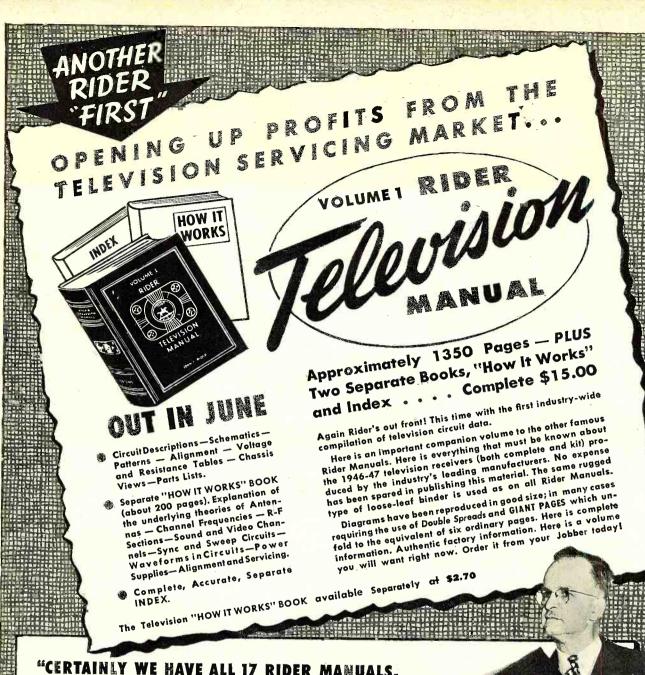
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June, 1948



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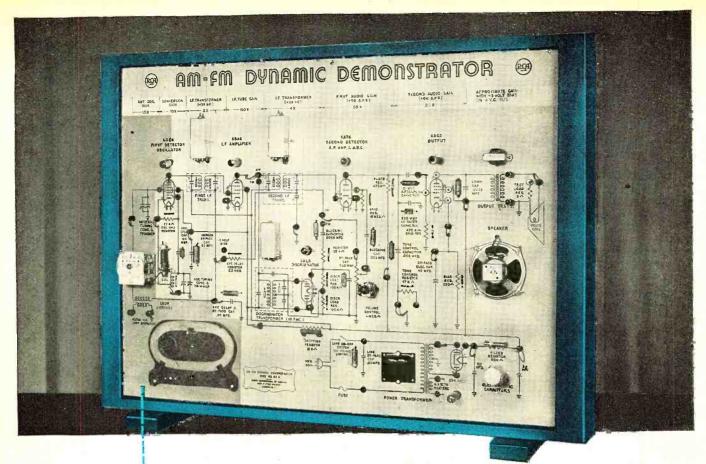
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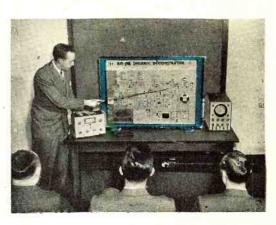
it's a schematic... t teaches radio...it has FM!

Quickly demonstrates radio theory, servicing, and the use of test equipment

It's a schematic of a modern six-tube superheterodyne receiver with the working parts mounted beside the correct symbols. All parts are actually connected and operate!

Circuits separated by different colors—Large color blocks mark each circuit section . . . it's easy to follow the function of each stage in reproducing the signal. Approximate gain data is printed at the top of the panel.

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RCA's Dynamic Demonstrator has helped thousands to learn radio theory. See your RCA Test Equipment Distributor for complete information on this new AM-FM model.

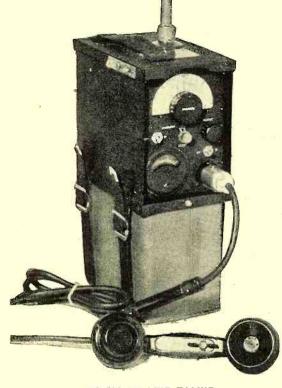


RADIO CORPORATION OF AMERICA
TEST AND MEASURING EQUIPMENT HARRISON, N. J.

TEST AND MEASURING EQUIPMENT

13

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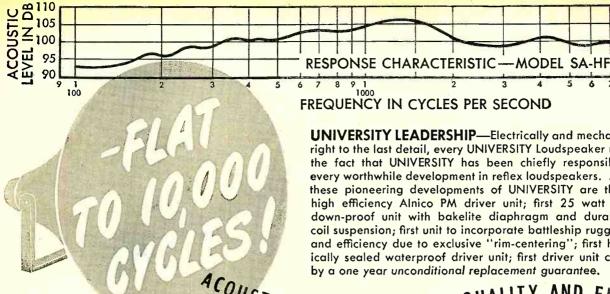
This 8 foot, 3 section mobile antenna is an outstanding value. The elements are made of strong, copper plated steel tubing. The big 4" ceramic insulator reduces wet weather losses to a minimum. A rubber molded spring mounting is also provided. The antenna is terminated at the base with a coaxial fitting for connecting a 72 ohm cable—no moisture problem. Mobile Whip Antenna, complete — only \$5.75 each.

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The Model SA-HF is the product of exhaustive research aimed at developing a driver unit capable of meeting present day high fidelity standards. How well UNIVERSITY engineers succeeded in this undertaking is best indicated by the characteristics of the Model SA-HF. Acoustic response is essentially flat through the entire range of audible frequencies to 10,000 cycles. Conservative continuous power rating is 25 watts. Completely weatherproof and ruggedly constructed for heavy duty, the SA-HF is a high-efficiency unit for every sound requirement.



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June, 1948

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* Presenting latest information on the Radio Industry.

By FRED HAMLIN

Washington Editor, RADIO NEWS

of things here in Washington, facsimile broadcasting to the general public on a commercial or semi-commercial basis will probably be under way. Fax enthusiasts, of course, want it. Some, indeed, go so far as to say that if commercial development is not rapid, "you will have no facsimile service." The quote is from John V. L. Hogan, one of the enthusiasts. Fax, he and others have made quite clear to the Federal Communications Commission, must pay its way soon like any other radio service or be relegated to the ashcan of inventions that failed to find a public. Mr. Hogan, Radio Inventions, and Faximile, Inc., would perish that last thought, and there is every indication that FCC is also in favor of giving facsimile its try at the commercial market. A decision to that effect may be forthcoming between the time this is written and the day you read it.

INTRIGUING HIGHLIGHTS of the FCC hearings on fax late this spring was the testimony which brought out that perhaps the best way to get fax on the airwaves would be to have it share time with FM within the same band. Most of those who testified felt that interruption of FM sound programs for facsimile broadcasts, far from harming FM, might enhance its attraction. Don't run to your FM set and expect to get a copy of the latest flash news, served up by facsimile, as a result of reading this. Mass use of the media is still a long way off, even its best friends admit. But there is every indication that facsimile is about to come out of the baby stage. Could be, given as many years as it took to develop other radio devices, it will be as lusty a feature on the airways as straight sound radio and television. Stronger, say its backers. And sooner than you think.

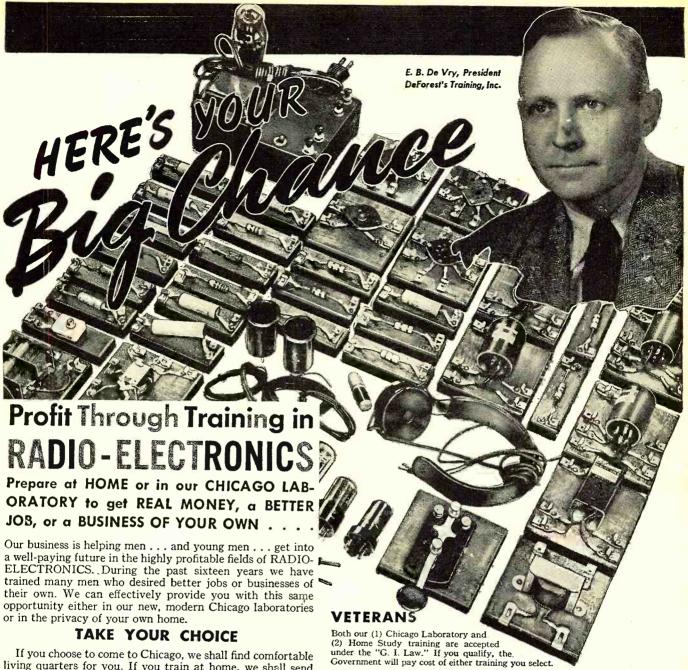
TELEVISION, regardless of the angle from which you look at it, still crowds the news spectrum and from the looks of things will continue to do so for the rest of the year. Straw-in-the-wind items keep cropping up, such as the fact that television set ownership in the New

BEFORE THE SNOW FLIES, from the looks from January to March. This statement is the result of a personal-interview survey of 3500 families in ten counties in New York and New Jersey, Another straw-in-the-wind which continues to surprise the industry and hints of a much larger mass market than was at times anticipated, is that the survey indicates more than 40 per-cent of the video sets are owned by middle and lower-middle income groups. Poorer homes, many without telephones, have a television antenna on the roof.

> RADIO LEADERS are hailing the progress with enthusiasm. "Television is advancing like wildfire this year," said Dr. Ray H. Manson, president of Stromberg-Carlson, recently, "and is destined to be the leading-if not the most importantbroadcast entertainment medium of the year." He adds: "From the standpoint of the manufacturer, television production offers an important plus in this year's operations. Radio broadcasting will continue for many years as the only means of mass entertainment outside of metropolitan areas. However, the large radio-phonograph-television unit is the best buy for most families, and the all-purpose instrument will eventually be considered standard equipment in every living room, for it is an instrument that offers complete home entertainment."

BOND GEDDES echoes these thoughts, and adds some facts and figures, as executive vice-president of the Radio Manufacturers Association, which give you an idea of how video has come up in the world. "In 1947," he points out, "approximately 178,500 TV receivers were produced, according to reports of RMA manufacturers. Industry estimates of 1948 production total 600,000 sets." The production figure this year is already pushing toward the 200,000 mark. The race to reach the receivers with stations is also going strong, Mr. Geddes reports. While there are only some 20-odd commercial TV stations on the air, the Federal Communciations Commission has granted construction permits for 86 additional transmitters and is considering York City area increased 100 per-cent applications for 181 more, he says, Sev-

RADIO NEWS



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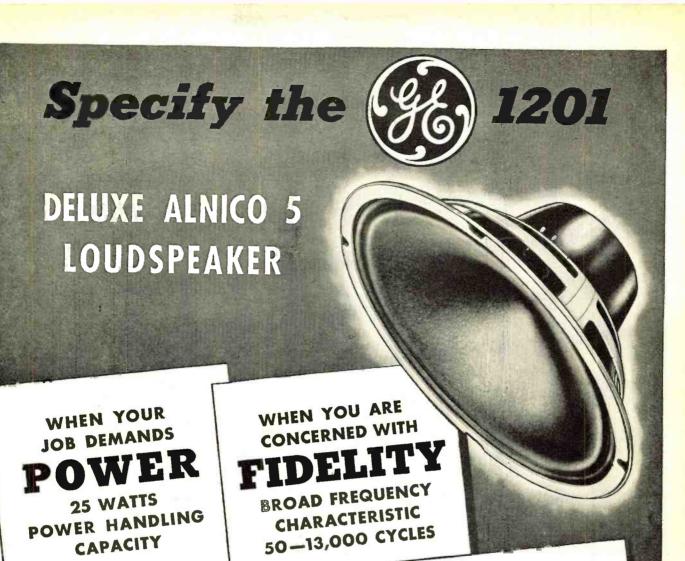


eral recent developments, such as plans for extending coaxial cable circuits, assure the extension of television networks and improvement in progress.

REGULAR RADIO is still very much in the running, however, Mr. Geddes hastens to point out, and he agrees with Dr. Manson that it will be the leading media for some years, "The glamour of television should not mislead anyone," he says, "into believing that radio is on the way out and that he should refrain from buying a needed replacement for his prewar set. Some radio listeners today are buying additional sets so that there will be a radio for every one in the family or a set for every room in their homes." This RMA-inspired campaign, mentioned at other times in this column, is coming along fine. You may recall that a test sales program was set up this spring in Hartford, Connecticut. Radio, newspaper, and direct sales methods were used, and with startling results. RMA reports that for the duration of the campaign, sales in Hartford were two and a half times greater than those in Providence, R. I., chosen because it parallels Hartford in population, market area, and other factors. Now the campaign is being pushed nationwide, and if it proves nothing else, it underlines the findings of the industry's leadersradio is going to be around a long time, and is still as popular as it ever was. television's dramatic spurt regardless.

WE HAVEN'T SAID MUCH for some time about the international situation so far as radio is concerned, so we checked up on it the other day with Wayne Coy, the FCC chairman, and discovered that there's been a lot going on in the field. We learned that this year there will be a total of 15 international radio conferences, all the way from The Hague to Montreal, and that the spirit of friendly international cooperation that pervaded the meetings at the Atlantic City conference (even the Russians played ball, for once) is still in the air in the international field. The conferences this year will work out the details of the broad principles laid down at Atlantic City. But it's a long, hard job, in case you haven't already guessed. Take the Provisional Frequency Board meeting in Geneva. It started in January and probably will be in session for two years. Its job is to produce a draft of the first edition of the new international frequency list as agreed upon at Atlantic City. That list will show the specific assignment of frequencies to specific stations. Drawing it up is a tough job, full of endless detail. The date on which the Atlantic City Radio Regulations will finally become completely effective is September 1, 1949—with luck. But that

(Continued on page 186)



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FM/TV SWEEP SIGNAL GENERATOR. Already America's most popular sweep signal generator. Model 909 is identical to Model 911 above except that it does not include crystal marker oscillators — uses your present AM signal generator to provide variable-frequency marker "pips" when desired. Using any good 'scope and following the clear, concise pictorial instructions, Model 909 makes you master of FM and TV visual alignment . . . the only method guaranteeing fast and perfect i.f. alignment. Thousands already in use by smart service technicians and in the laboratories and factories of FM and TV set manufacturers prove it to be exactly the instrument you have demanded. Convenient portable size matches all Silver LCETI — turns your shop into a modern service laboratory.



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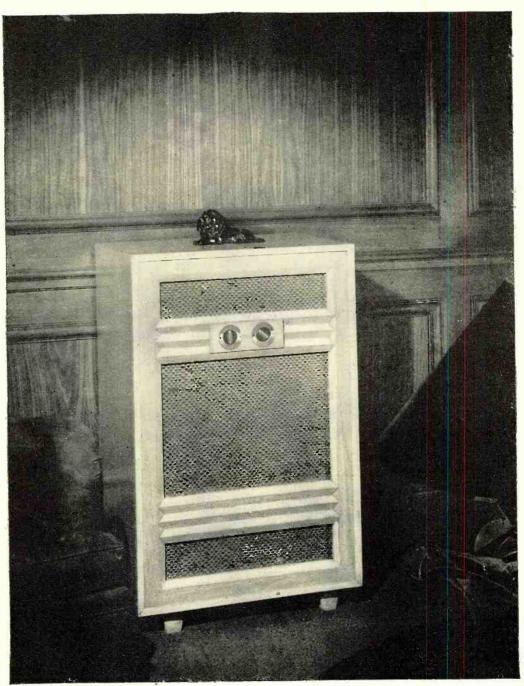
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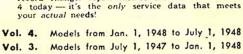
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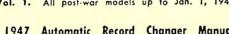
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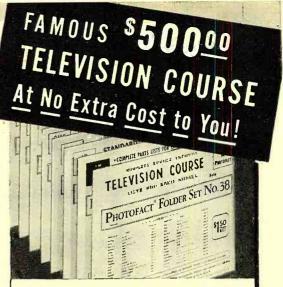
The book that shows you exactly where to replace each tube in 5500 radio receiver models. Covers receivers from 1938 to 1947. Each tube layout is illustrated by a clear, accurate diagram. Saves time - eliminates risky hit-and-miss methods, especially when the customer has removed tubes from the set. A handy pocket-sized 192-page book, indexed for quick reference. You'll use it profitably every single day. Order several copies for your bench and outside calls! ONLY



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HOTOFACT

"The Service that pays for itself over and over again"



NOW RUNNING IN CURRENT PHOTOFACT FOLDER SETS

Here's the first practical, successfully proved Television instruction for the Service Technician! Now - at no extra cost to you - you can prepare for profitable Television servicing without taking time off from your business. If you can service a Superheterodyne, the PHOTOFACT Course will teach you clearly and simply how to service a Television Receiver. Telegrams, letters and 'phone calls by the hundred acclaim the first installment of the \$500 Television Course which appeared in PHOTOFACT Folder Set No. 38. If you haven't started the Course (which is running in current PHOTOFACT Folder issues) - be sure to get PHOTOFACT Sets No. 38, 39 and 40 today! Stay shead of the game with PHOTOFACT!

Don't Miss a Single Installment!

Dial Cord Stringing Guide

The book that shows you the one right way to string a dial cord. Here, for the first time, in one handy pocket-sized book, are all available dial cord diagrams covering over 2300 receivers, 1938 through 1946. Makes dial cord restringing quick and simple. Pays for itself in time saved on a single dial cord repair job. A "must" for every service bench and tool \$1.00 kit. Order today! ONLY

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| Mail This Order Form to HOWARD W. SAMS & CO., INC. 2924 E. Washington St., Indianapolis 7, Indiana |
|--|
| My (check) (money order) for \$enclosed. |
| ☐ Send Photofact Sets38,39,40 |
| through 40) in DeLuxe Binder, 18.39. |
| □ Vol. 3. □ Vol. 2. □ Vol. 1 (\$18.39 each). □ Automatic Record Changer Manual, \$4.95. □ Tube Placement Guide, \$1.25. □ Dial Cord Stringing Guide, \$1.00. |
| Send FREE Photofact Cumulative Index. |
| Name |
| Address |
| C'A. State |

26

RADIO NEWS

Delco PACKAGED now offers DRA-



Most popular models in Delco Home Radio now grouped for best display, quickest turnover!

Here's a great opportunity to pep up your radio sales and step up your radio profits! You can now purchase Delco Home Radios in carefully selected "profit packages"-each with a brilliant new display stand which holds six models.

Pick your package Take your profit

Each Delco is a quality product, backed by three great names: General Motors, Delco and United Motors. And the complete Delco line is so diversified that it attracts a wide range of prospects. Talk to your United Motors' distributor (or write to United Motors Service, General Motors Building, Detroit 26, Michigan) ... select one or more of these new "profit packages" . . . you'll find you're in business to make money!

DELCO RADIO A GEMERAL MOTORS PRODUCT

Delco radios are distributed nationally by United Motors Service. See your United Motors distributor about the Delco Radio line.



DELCO PACKAGE NO. 1502

Twenty-four assorted Delco table model radios, including one combination radio and record player and one display

DELCO PACKAGE NO. 1504

Fifteen assorted Delco console and table model radios and radio-record player combinations and one display stand.

DEALER'S PROFIT \$298.12

Ask about other "Profit Packages" not listed here

June, 1948

HARVEY

FM TRANSLATOR General Electric Model XFM-1



Post-war version of the old G.E. J.F.M-90 Translator which was used and enjoyed by tens of thousands of discriminating radio

Covers 88-108 mc range, dial 12 inches long, uses guillotine tuning for highest efficiency, high stability. Designed for export, has power inputs for 110 to 250 volts, 50/60 cy. Used in conjunction with good audio section or separate amplifier will provide best FM listening you ever heard. In attractive natural walnut cabinet - 1034" high x 1534" wide x 1138" deep, complete with 8 tubes. Tropic-proof construction. Quantity limited, no more available. Get your order in while they lastl

Available only from HARVEY Special price \$49.50 For use with the FM tuner we recommend any of the following:

| Altec-Lansin | g A-323 B Amplifier\$ | 125.00 |
|--------------|---------------------------|--------|
| Altec-Lansin | g 600 Speaker | 45.00 |
| Altec-Lansin | g 603 Speaker | 63.00 |
| Altec-Lansin | g 604 Speaker | 157.50 |
| Crossover fo | r 604 | 30.00 |
| Stephens Tr | u-Sonic P52A Speaker with | |
| crossover | | 123.00 |
| Stephens Tr | u-Sonic P52FR Co-Spiral | |
| | | 48.00 |



RCA 630TS TV Chassis

Complete kit of ports, including all hardware, pre-wired and aligned RCA front end, condensers, resistors, punched chassis, all tubes including kine, complete manual with service notes, all RCA......\$198.50 NOTE: All prices are Net, F.O.B. N.Y.C.

and are subject to change without notice.



103 West 43rd St., New York 18, N. Y.

Within the

W. W. JABLON has been elected a Vice-President of the Esbey Manufacturing

Company, Inc. of New York. He will head the jobbing and special products division of the company. The iobber division markets a line of replacement chassis and tuners through



distributors and mail order houses while the special products division manufactures various kinds of electronic equipment on subcontract for other companies.

Mr. Jablon, who was previously connected with The Hammarlund Mfg. Co., Inc. is a Director of Radio Parts and Electronic Equipment Shows, Inc.

BENDIX RADIO DIVISION of Bendix Aviation Corporation, has announced the recent appointment of Vincent C. Judd, to the new position of manager of automobile radio sales. Mr. Judd will have offices at Bendix Aviation Corporation's Research Laboratory, 4855 Fourth, Detroit, Michigan.

Mr. Judd, formerly a major in the Signal Corps, was stationed in Detroit during the war as liaison officer with automotive manufacturers. His work was with automobile manufacturers for radio installation provisions and electrical noise suppression on tanks, jeeps, staff cars, and other types of mobile radio applications. After leaving the Armed Forces, Mr. Judd joined the sales engineering staff of Bendix Radio Division. Before joining the Army, he was a member of the company's engineering department.

JOHN F. McALLISTER was recently appointed Designing Engineer of the Specialty

Division of General Electric Company at Electronics Park. In this capacity he will be responsible for the design of the division's products for radio servicemen, precision testing



units, and other electronic application developments.

Mr. McAllister is a graduate of the University of Pennsylvania and holds a degree in physics and engineering. He joined General Electric in 1939 and was assigned to the Test Department. Mr. McAllister spent four years studying and teaching in the company's Advanced Engineering Courses dealing with radio wave propagation, circuits, radar techniques, and new electronic engineering activities.

During that time he was assigned to research work on a number of government equipment projects, including work with the V-2 rocket. In 1947 he returned to Syracuse and was appointed section leader of service test and precision test equipment, a post he relinquished to take his present position.

LEWIS GORDON has been appointed Director of the International Sales Divi-

sion of Sylvania Electric Products Inc. Previously Mr. Gordon was assistant to the Vice President of Sales He has been a sales executive with Sylvania Electric since he joined the com-



pany in 1931 as Manager of New York district sales when he opened the first New York City office. He has been manager of national domestic accounts in lighting sales for many years.

A Harvard graduate, Mr. Gordon will make his new headquarters at Sylvania Electric's International Sales Division office, 50 Broadway, New York City.

SUPREME, INCORPORATED, has acquired the manufacturing rights, facilities, and assets of the Supreme Instruments Corporation. The new corporation is composed of executives, representatives, and key employees of the old company.

The transfer of property and rights includes all patents, engineering developments and trade-marks. Supreme, Incorporated, will continue to sell test equipment and meters under the name "Supreme." All guarantees of equipment previously sold by Supreme Instruments Corporation will be fulfilled by the new company.

Until completion of their new air conditioned plant they will continue to occupy the quarters of the old company.

WHIPPLE JACOBS, president of the Belden Manufacturing Company, has been named chairman of the Electrical Engineering and Physics division of the Development Program campaign of Illinois Institute of Technology.

When constructed, the \$800,000 Elec-

No More
Guessworn
with

OHMITE

Little Devil

COMPOSITION





You never have to guess about the resistance and wattage of any Little Devil resistor. Every unit is not only color-coded, but individually marked for quick, positive identification.

Ohmite Little Devils are rugged and dependable. Millions of these tiny, molded composition resistors have been used in critical war equipment and in leading laboratories. They meet Joint Army-Navy Specification JAN-R-11, including salt water immersion cycling and high humidity tests. Little Devils can be used to their full wattage ratings of 70° C (158° F) ambient temperature. They dissipate heat rapidly, have a low noise level, and low voltage

Ratings for maximum continuous RMS voltage drop are high ... 350 volts for the ½-watt unit, 500 volts for the 1-watt unit, and 1000 volts for the 2-watt unit. Ohmite Little Devils are light, compact, easy to install. They're available from stock in Standard RMA values from 10 ohms to 22 megohms, in ½, 1, and 2-watt sizes. Values as low as 2.7 ohms in the 1-watt size only. Tol. $\pm 10\%$. Also $\pm 5\%$ in $\frac{1}{2}$ and 1-watt sizes.

Ask for them BY NAME from your Distributor

SEND FOR BULLETIN 135

Gives complete data and list of RMA values. Includes dimensional drawings and handy color code. Write for it, today.

MANUFACTURING OHMITE 4885 FLOURNOY STREET, CHICAGO 44, ILL.

Be Right with OHMITE

RHEOSTATS . RESISTORS . TAP SWITCHES . CHOKES . ATTENUATORS

June, 1948



from this NEW, IMPROVED



ear MAGNETIC PHONO PICK-UP

HIGH FIDELITY



\$ Profit and Exquisite Record Reproduction...

JOBBERS ... SERVICEMEN ... turn service calls into profitable sales with ease. This new LEAR Reluctance Pick-Up transforms "flat" old-fashioned sound into full-toned modern reproduction!

This new, improved High-Fidelity Reluctance Pick-Up is LEAR engineered to excel in quality of performance . . . and priced for your profit. Replaces millions of old style crystal pick-ups now in use! Jewel stylus eliminates needle changing - holds surface noise to a bare minimum. It performs a miracle of modernization — assures full tonal beauty of sound wherever installed.

List this "hot" seller in your catalog! Service men who feature the new LEAR Magnetic Pick-up will pick up extra profits every day! Cash-in now-write for complete discount price list today!

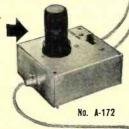
To complete your LEAR Sound Service: New, Improved LEAR PRE-AMPLIFIER, List Price-\$9.90

To provide additional amplification with use of MP-103 LEAR Magnetic Pick-up. Can be connected directly to old crystal cartridge input. High voltage and filament wires provided for connection into existing equipment. Two-position switch permits high-fidelity response to finest quality recordings.

No. PA-103 (not shown here)—LEAR Tone Arm Assembly with MP-103 Magnetic Variable Reluctance Pick-Up Car-tridge, List Price \$15.50.

Designed for high-fidelity reproduction of 10" and 12" recordings Spring counter-balance provides "feather touch" operation—only 17 grams stylus pressure on record. This reduces record wear to a minimum. Handsomely finished in brown metallic.

Factory Representatives - Distributors: A few choice territories are still available for these and other fine LEAR Electronic Products. Write today giving full details.





110 Ionia Ave. N. W. Grand Rapids 2, Mich

trical Engineering and Physics building, will stand on the site of the present Main building built in 1891, It will contain specialized laboratories for basic electrical circuits and electrical machinery, nuclear physics, radio and television, a physics demonstration museum, and an integrated physics library.

Mr. Jacobs, a trustee of Illinois Tech since 1943, is also a director of the Chicago Association of Commerce and Industry, and a vice-president of the National Electrical Manufacturers Asso-

GEORGE COHEN was recently appointed General Manager of the parts sales and

service departments for Emerson Radio and Phonograph Corporation. His departments service all Emerson products and control the sale of parts, tubes, and accessories for all of the com-



pany's radios, phono-radios, and television sets.

Prior to his promotion Mr. Cohen served as Emerson Radio's General Manager in the War Assets Administration Division handling the disposal of surplus electronic properties. During the war he served as Manager of the company's equipment engineering department.

J. M. BAXTER has been named sales representative for the Jensen Manufacturing Company's line of acoustic equipment in the states of Indiana and Kentucky.

Mr. Baxter has been in radio since 1929 when he joined the original Capehart organization as an engineer on p.a. and sound equipment. He served as chief engineer for the Capehart Corporation until 1939 at which time he was placed in charge of record changer development by Farnsworth Television & Radio Corporation.

He recently resigned his position with Farnsworth to organize his own sales representative firm.

NATIONAL BUREAU OF STANDARDS has announced three new appointments. William B. Haliday has joined the staff of the Electron Tube Laboratory and will be engineer in charge of model tube construction. During the war and until his recent appointment he was a radio engineer with the Naval Research Lab-

Also joining the Electron Tube Laboratory will be Russell E. Dorrell, an electronics engineer. Mr. Dorrell will aid in the development and standardization of test methods and equipment for evaluating tube performance.

The third appointment was that of Paul V. Horton, to the Engineering Elec-(Continued on page 128)

RADIO NEWS

TELEVISION ASSEMBLY CO.

INTRODUCES THE

Champion Models

DUMONT INPUTUNER

The Dumont Inputuner tunes continuously from 44 to 216 megacycles without a break, covers all 13 channels as well as FM, amateur, and aviation channels. For ease and convenience of operation no band switching of any kind is required when tuning from channel to channel with the inputuner system. Just one simple operation to reach any desired station.

Assemble the Champion model of your choice, 10" flat surface screen picture, 51 sq. in. picture, 12" screen picture with 75 sq. in. picture or the 15" screen picture with 120 sq. in. picture.

All Champion Models are complete with all tubes and components including the CR Tube.

10" FLAT SURFACE

DEALERS NET

12" SCREEN PICTURE

\$ 303.10

DEALERS NET

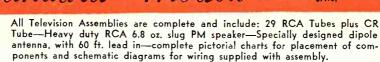
15" SCREEN PICTURE

\$ 393.10

DEALERS NET

tandard Models

NOW AVAILABLE WITH THE STANDARD MODELS— FM RADIO AT A SLIGHT ADDITIONAL COST OF 57.95.



Superior performance is obtained with a new IF Video & Sound IF Strip (Pat. Pend.) aligned, wired, pretuned, tubed and tested. All circuits are contained on one chassis ready to use with the front end unit supplied. This front end will handle 13 channels and is aligned and tested, mounted on a separate chassis. Merely connect B plus filament and output IF leads to the television chassis. It is not necessary to make any RF alignments. These units utilize a clipper circuit which filters out ignition noises.

10" FLAT SURFACE

12" SCREEN PICTURE

15" SCREEN PICTURE

\$ 229.50

\$ 759 50

\$ 349 50

DEALERS NET

DEALERS NET

DEALERS NET

TERMS: 10%
DEPOSIT WITH
ORDER. BALANCE
EXPRESS COLLECT.

Guaranteed

All Television Assemblies are guaranteed to operate to your satisfaction when simple directions are followed.



540 BUSHWICK AVE. BR●●KLYN 6, N. Y.



Precision . .

The ease and grace of a figure skater is a manifestation of infinite skill and precision. The delicate mechanisms that make the RADIART VIBRATOR outstanding represent precision manufacture at its best. The skillful engineering . . . the finest quality materials would be of little value without the precision manufacture that makes a working body of material and design. This is the RADIART VIBRATOR . . . another of the reasons for its superiority. This is why Radiart is preferred everywhere by servicemen who know vibrators.

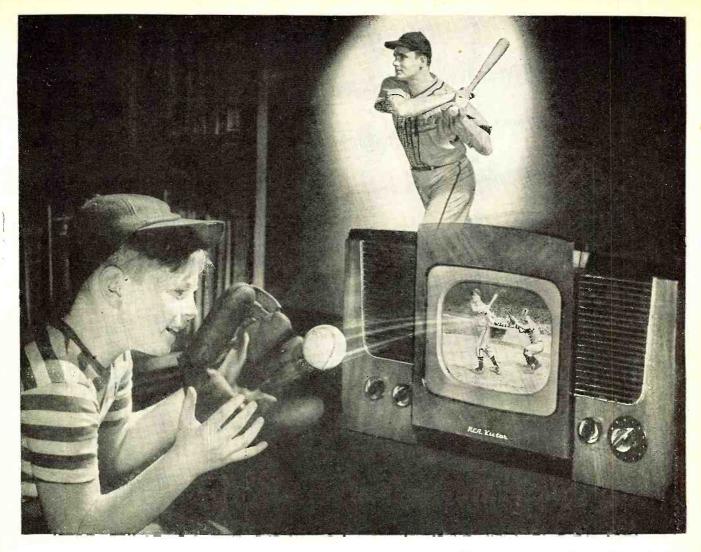




The Radiart Corp.

CLEVELAND 2, OHIO

EXPORT: SCHEEL INTERNATIONAL, INC.



An entire season of baseball action-from Opening Day to World Series-is yours with RCA Victor television.

You're right in the game - with Television

• Comes the shout "Play Ball!" and there you are . . . right on top of every play.

Through television developments in RCA Laboratories, all the action is yours – the crack of bat against ball – fast infield plays – even sidelights in bull pen, dugout, grandstand and bleachers.

At the ball park, RCA Image Orthicon television cameras — rivalling the

human eye in sensitivity—get all the action in day or night games. Shifts from over-all views of the field, to "close-ups," of individual players are swift and revealing...

And at the receiving end — your RCA Victor "Eye Witness" home television set gives you brighter, clearer pictures. You can see the ball that the batter misses, or you can watch his home run smash sail over the distant fence.

Today, because of the original and continuing work of RCA scientists, millions can enjoy sports, entertainment, educational and news events, on television. Research at RCA Laboratories—always a "step ahead"—enters every instrument marked RCA or RCA Victor.

When in Radio City, New York, be sure to see the radio, television and electronic wonders at RCA Exhibition Hall, 36 West 49th St. Free admission. Radio Corporation of America, RCA Building, Radio City, New York 20, N. Y.



RADIO CORPORATION of AMERICA

RADIO SERVICEMEN!

9 PRIZES FOR 18 IDEAS

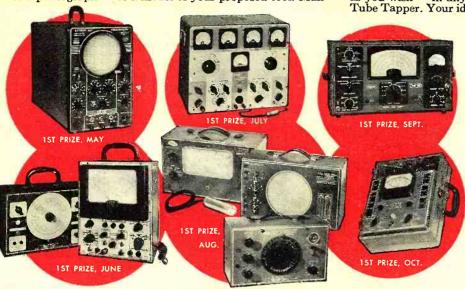
HERE'S HOW EASY IT IS TO WIN

Right now, you may have a winning idea at work in your shop. An idea for a simple service tool which makes your work easier, faster, more profitable. Hytron wants to help make such needed tools available to all servicemen—at cost. You can cash in on your idea easily — and also help the other fellow.

Simply obtain an official entry blank from your Hytron jobber — or write us. Answer a few simple questions on blank. Then include a sketch with constructional details or write us. Answer a few simple questions on the or a photograph — or a model of your proposed tool. Mail

to Hytron Contest Editor. The tool should be simple, practicable, durable, compact, easy and economical to manufacture. Examples: Hytron Tube Tapper and Miniature Pin Straightener.

That's all there is to it. Nothing to buy. Nothing difficult. No fancy writing. And could you use one of those beautiful deluxe test equipments — or one of those crisp new Savings Bonds! Check the easy rules. Get an official entry blank today for full details on how to win. Send in as many entries as you wish — in any or all six contests. Everyone wins a Tube Tapper. Your idea may hit the jackpot. Let's go!



HERE ARE SOME EXAMPLES



Hytron's Tube Tapper and Miniature Pin Straightenershow youthe kindoftoolwanted.Check off the qualities. Simple? Yes. Practicable? Usable time-savers. Durable? Built to last. Compact? Carry them in your pock. et. Easy and economical to manufacture? Adapted to mass production. Tube Tapper a nickel; Pin Straightener 49¢ — both under 50¢. Tools associated with tubes preferred. but other original service tools also acceptable.

HERE ARE THE PRIZES

First Prizes

DuMont Type 274 Five-Inch Oscillograph. MAY

Radio City Products Model 665-A, the "Billionaire", V-T Volt-Ohm-Capacity Meter, Insulation Tester; and Model 705-A Signal Generator. JUNE

JULY Hickok Model 156A Indicating Traceometer.

McMurdo Silver Model 900A "Vomax" Electronic Volt-Ohm-Milliammeter; Model 904 Condenser/Resistor Tester; and Model 905A "Sparx" Dynamic Signal Tracer/Test Speaker. AUG.

SEPT. Jackson Model 641 Universal Signal Generator.

OCT. Weston Model 769 High Frequency Electronic Analyzer.

Second Prize - Each Month Third Prize - Each Month \$50 U. S. Savings Bond \$25 U. S. Savings Bond

Grand Prize

\$200 U.S. Savings Bond — to contestant whose idea is judged to be best of the 6 winning monthly first prizes.

HERE ARE THE EASY RULES

. Any bona fide radio serviceman who repairs radios for the general public and who lives in continental United States is eligible for these contests, except em-ployees of Hytron, their advertising agencies, and their families.

HOW ... Get official entry blank from your Hytron jobber, or write us. Describe on blank your idea for a shop tool for radio servicemen. Include sketch and constructional details — a photo — or model. Make your proposed tool simple, practicable, durable, compact, easy and economical to manufacture (preferably to sell without profit at 50¢ or less) — like the Tube Tapper or Miniature Pin Straightener.

WHERE Mail to CONTEST EDITOR

WHERE ... Mail to CONTEST EDITOR. HYTRON RADIO & ELECTRONICS CORP., SALEM, MASS.

CORP. SALEM, MASS.

WHEN ... There are six monthly contests.
Opening and closing dates for each contest
are the first and last days of each of the
months from May through October, 1948.
inclusive. The postmark date determines
month of entry. Entries for final month's
contest must be postmarked before midnight. October 31, 1948, and received by
November 15th. At judges' discretion, unsuccessful entries in any month's contest
may be re-considered among following
months' entries. You may submit as many
different ideas as you wish in any or all six
monthly contests. Use separate blank for
each entry. each entry.

PRIZES ... See special listing of prizes.

PRIZES ... See special listing of prizes.

JUDGES ... Entries will be judged on originality. simplicity. practicability, durability. compactness, and ease and economy of manufacture. Judges will be: Sanford Cowan. Editor & Publisher of Radio Service Dealer; W. W. MacDonald. Managing Editor of Electronics; Oliver Read. Chief Editor of Radio News; Joseph Roche, Editor of Radio Maintenance; J. L. Stoutenburgh. Executive Editor of Radio & Television Retailing; Lewis Winner, Chief Editor of Service.

Chief Editor of Service.

Judges' decisions final. Duplicate prizes in case of ties. No entries returned. Entries become property of Hytron, who may, at its option and by special arrangement with the entrant, pay the cost of a patent application (if the tool is patentable) with the understanding that Hytron is to have a non-exclusive license to manufacture, distribute, and sell the tool without royalties. Contests subject to all Federal and State regulations. Winners will be announced in radio service trade papers shortly after close of final contest. Prize winner list available approximately one month after available approximately one month after close of last contest.

SPECIALISTS IN RADIO RECEIVING TUBES SINCE 1921



ELECTRONICS CORP.

MAIN OFFICE: SALEM, MASSACHUSETTS



RADIO NEWS



These "sound jurors" record their preferences as they listen over test circuits.

rial by "Sound Jury"



The engineer in the foreground talks over the test circuits which the other engineer sets up on a "circuit simulator."

AFTER Bell Laboratories engineers have designed a new talking circuit, they measure its characteristics by oscilloscopes and meters.

But a talker and a listener are part of every telephone call, and to satisfy them is the primary Bell System aim.

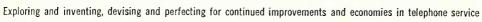
So, before the circuit is put into

operation, a "sound jury" listens in. An actual performance test is set up with the trained ears of the jurors to supplement the meters.

As syllables, words, and sentences come in over the telephones, pencils are busy over score sheets, recording the judgment of the listeners on behalf of you and millions of other telephone users.

Targets of the transmission engineer are: your easy understanding of the talker, the naturalness of his voice, and your all-around satisfaction. To score high is one of the feats of Bell System engineering.

BELL TELEPHONE LABORATORIES

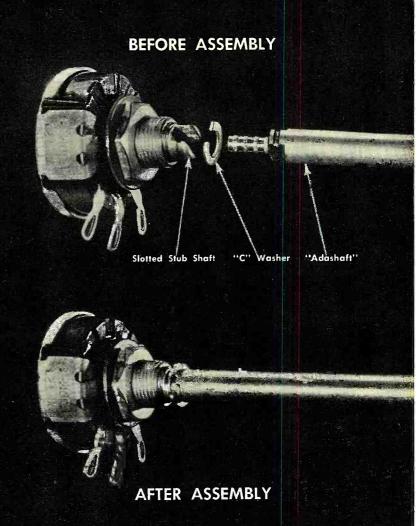




Centra ab Announces an

See how EASILY and QUICKLY "Adashaft" Radiohms can be assembled!

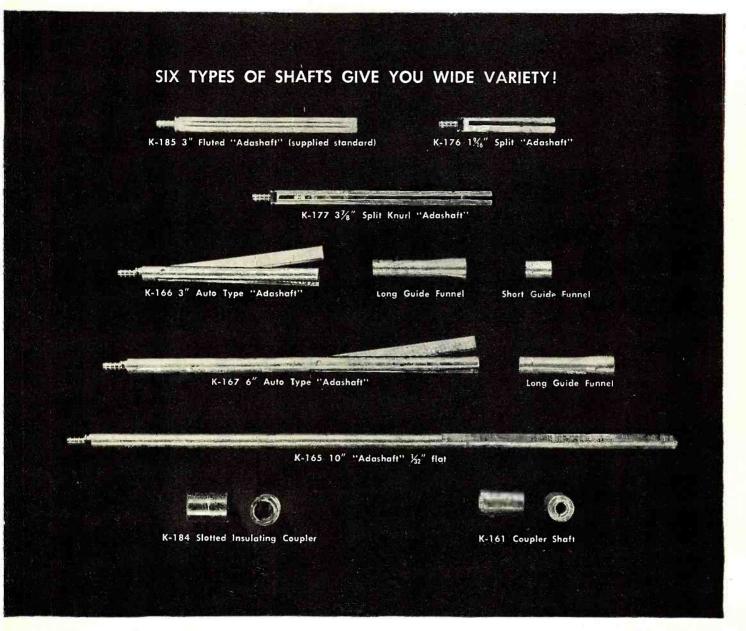
No Wiggle, no wobble, no slip when you use Centralab's "Adashaft" Radiohm. Just insert shaft pilot in hole provided in control stub shaft, and slip "C" washer into place. Quick as a wink, control and shaft become an integral unit, ready for smooth, trouble-free operation. Notice the wide selection of shaft types which Centralab offers you for every kind of set from large radiophonograph combinations to small automobile receivers. Shafts are rugged-built to withstand hard usage, yet easy to cut to lengths required. *Trademark registered



Where line switches are required, use CRL attachable Switch Covers!

Available in five types for "R" Radiohms, 4 types for "M" Radiohms, 1 type for "E" Radiohms. Minimum life of 50,000 mechanical and electrical operations. Underwriters approved. Contact carrier is propelled by full-floating, compression type spring, provides easy, positive action. Rated at 3 amp. 125 volts; 1 amp., 250 volts.

Improved "Adashaft" Radiohm



See how "Adashaft" Radiohms cut down overhead on service and repairs!

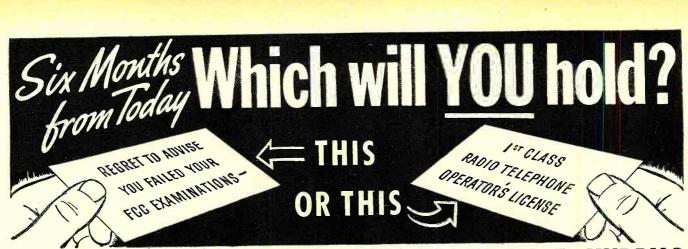
Now, YOU CAN HAVE a small stock of controls on hand, yet be prepared to handle almost any kind of control replacement problem for your customers! Yes, that's what Centralab "Adashaft" Radiohms give you, and that's why more and more radio service dealers are using them to speed up service and cut down inventory.

Centralab "Adashaft" Radiohms are availa-

ble in all sizes for all Model "M" volume control applications. See for yourself how they can streamline your service operations. Ask your jobber about them, or write direct for further information.



Division of GLOBE-UNION INC., Milwaukee



WANT YOUR FCC COMMERCIAL LICENSE IN A Use Cire Training and Coaching Service—and Get Your "Ticket" in a Few Short Weeks!

Thousands of new jobs are opening up—FM, Television, Mobile Communication Systems—These are only a few of the radio fields which require licensed radio technicians and operators.

Your FCC Ticket Is Recognized in ALL Radio Fields as Proof of Your Technical Ability.

More than ever before an FCC Commercial Operator License is a sure passport to many of the better paying jobs in this New World of Electronics.

"I have taken the first class phone Thave taken the first class phone license examination and received my first class ticket last Saturday May 31. In closing I must say yours is an excellent radio course, and I really appreciate your help and the fine service you have rendered me." Student #2876N12

HUNDREDS OF SATISFIED, "I passed the FCC examination in radiotelephone 2nd class, at Detroit June 3rd, and I want to thank you for your ready assistance as my instructor on Section I of Nilson's Master Course."

Student #2779N12

Get your license without delay-Let Cleveland Institute prepare you to pass FCC license examinations, and hold the jobs which a license entitles you to, with CIRE streamlined, post-war methods of coaching and training.

Employers frequently give preference to the license holder, even though a license is not required for the job. Hold an FCC "ticket" and the job is yours!

SUCCESSFUL STUDENTS "I have had my 1st class radio-telephone license since March of this year, and plan to continue with your course since I find it a great help in studying transmit-ters."

Student #2779N12

After sending in Lesson E I took After sending in Lesson E I work
the commercial operator's license
examination for 2nd class radiotelephone, and passed O.K. I received the license last week."
Student #2772N1



I can show YOU W TO PASS FCC COMMERCIAL EXAMS

If you've had any pactical radio experience—amateur, Army, Navy, radio servicing or other, my time proven plan can help you, too, on the road to success. Fill out the coupon below and mail it. I'll send you, FREE, the entire story. Edw. H. Guilford Vice President BULEIN FCC adds FM and television to the First Class License Exam. Effective July 1, 1948, to get a First Class ticket, you will be examined in Frequency Modulation and Television, too.

CIRE training and coaching makes it EASY to get your FCC ticket

> EVEN WITH THE NEW EXAM



CLEVELAND INSTITUTE OF RADIO ELECTRONICS

RN-6 Terminal Tower, Cleveland 13, Ohio

I want to know how I can get my FCC ticket in a few short weeks. Send me your FREE booklet, "How to Pass FCC license Examinations" (does not cover exams for Amateur License) as well as a sample FCC-type exam and Catalog A, describing opportunities in Radio-Electronics.

| NAME | |
|---------|-----------|
| ADDRESS | |
| CITY | ZONESTATE |

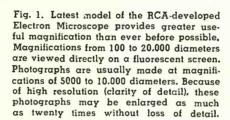
NO OBLIGATION - NO SALESMEN

38



By TOM GOOTÉE

A practical explanation of the Electron Microscope, and the use of electrons to obtain magnification.



Today, this improved electronic instrument provides much higher resolving power (better clarity) and much greater useful magnifications than have heretofore been possible. Any degree of magnification, from less than 100 times to more than 20.

000 times, can be obtained directly and viewed on a small fluorescent screen.

Magnified images can also be recorded on a photographic plate. These photographs, known as *electron micrographs*, are usually made at magnifications of 500 to 10,000 diameters. Then, because of their high degree of resolution (or clarity), these photographs can be enlarged as much as 20 times, thus providing, when necessary, total useful magnifications as great as 100,000 diameters!

Basic Principle

Although a massive and seemingly complex instrument (Fig. 1), the principle of the Electron Microscope is relatively simple and in many ways similar to the ordinary optical or light microscope. This similarity is shown (Fig. 3) by a comparison of the basic

components of the two types of magnifying systems.

Essentially, the light microscope consists of a source of illumination, a condenser lens to concentrate the light in a beam on the object or specimen being examined, an objective lens controlling the focus and quality of a magnified image, and a projector lens for further magnification to produce a final image.

In the Electron Microscope, these optical elements are replaced by electronic elements. (See Fig. 3.) A high-speed electron beam is used instead of a light beam, and the electrons are controlled and focused by means of magnetic coils or magnetic-field lenses—replacing the solid, glass, optical lenses.

The source of illumination is an electron gun, consisting of a filament and cathode, and a specially shaped anode or plate. Electrons emitted by the heated filament are attracted at a furious rate toward the anode, due to the high positive potential of the anode, 50,000 volts, with respect to the cathode. There is a small hole in the center of the anode, however, and most of the electrons shoot through this opening at a tremendous velocity.

Almost immediately, the electrons are concentrated in a beam by the magnetic-field action of the condenser lens. This doughnut-shaped coil bends the paths of the electrons, and directs the resultant high-intensity beam on the object to be examined.

The usual microscope slide is much too thick to be penetrated by the electron beam. For this reason, the

AN has always searched for knowledge of the infinitely small. Until a few years ago, however, he was unable to penetrate deeply into the unknown and unexplored universe that he knew existed but could not see.

Optical or light microscopes—in use since the Seventeenth Century—provide only a partial solution. They have their rightful place in science, but their power is limited, because their operation depends on light waves. They cannot see particles much smaller than the wavelength of light, thus, their greatest magnification—about 2000 diameters, or 2000 times—is only a teasing, long-distance glimpse of the infinitesimal.

It remained for scientists and engineers, working in the field of *electron optics*, to develop a new and revolutionary magnifying device — the *Electron Microscope*—the most powerful microscope in existence.

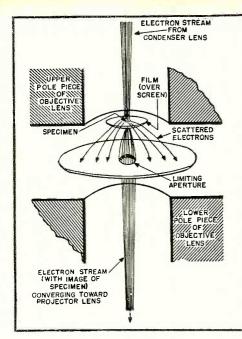


Fig. 2. Simplified action of the electron beam striking the specimen. The specimen is held by means of a thin supporting film on a wire screen in the magnetic field of the objective lens so that the specimen is "illuminated" by the electron beam. Electrons are influenced or deflected according to the varying densities of the specimen. Denser areas result, in greater "scattering" of electrons; less dense areas produce less "scattering." In this way, the high velocity beam is "modulated" according to the shape and density of the specimen, and an image of varying but sharp contrasts is obtained. Widely "scattered" electrons are unwanted, and are removed from the electronic axis as shown. Only the main, usable portion of the electron beambearing the image of the specimen—is allowed to pass through the limiting aperture. The beam is then focused and magnified by the objective lens.

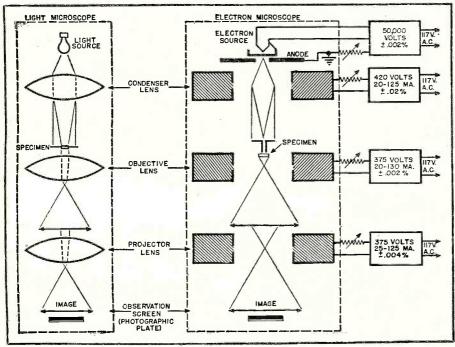
object or specimen is placed on a very thin supporting film or membrane, which is only a few millionths of an inch in thickness and is effectively transparent to the electron beam. The film is made of collodion and is strong enough to support most types of specimens, but for greater rigidity the film is placed over a 200-mesh screen about 1/4-inch in diameter.

When the specimen is bombarded by the high-velocity beam, the path

of each electron is affected in varying degree (Fig. 2) according to the density or composition of the specimen at the point of contact. Portions of a specimen having great density, such as metallic oxides, cause wide "scattering" or abrupt dispersal of all electrons striking such areas. Portions of less density cause less "scattering" of electrons, in proportion to the density of the area where electrons strike.

In this way, a specimen is "illu-

Fig. 3. Electron Microscope is similar in basic principle to the ordinary optical or light microscope. Essentially, the light microscope (left) consists of a source of illumination, a condenser lens concentrating the light in a beam on the specimen or subject under observation, an objective lens controlling the focus of the image, a projector lens for further magnification for microphotography, and an observation screen. In the Electron Microscope (right), optical elements are replaced by electronic elements; the beam of light is replaced by a beam of high speed electrons, and the solid optical lenses are replaced by magnetic field lenses created by energizing magnetic coils. Electronic action takes place in a vacuum within a high, cylindrical metal column. Current for controlling each lens and the electron accelerating voltage is obtained from separate, regulated power supplies.



minated" by the electron beam. Electrons which are widely "scattered" are of no importance, and are eliminated by means of a limiting aperture. The electrons which pass through the aperture, however, bear an image corresponding to the varying density of the specimen under observation.

The small unit (film on screen) containing the specimen is held in proper place by means of a T-shaped specimen holder (Fig. 6) resembling a small, brass cartridge. The specimen holder is mounted in the magnetic field of the objective lens. The electron beam is brought to a focus by the magnetic-field action of this coil, to form an enlarged image.

A part of the area of this magnified image is selected for further, final magnification. Electrons forming this part of the image are allowed to enter the magnetic field of a third coil, known as the projector lens. The electrons are brought to a focus, producing a greatly magnified final image.

Since the electron beam is invisible to the human eye, a fluorescent observation screen is placed in such a way that the beam falling upon it produces a visible image. The screen is enclosed by the viewing chamber of the microscope, but three glass windows in the chamber permit simultaneous observation of the final image by several persons. The front window of the viewing chamber is also equipped with a 2-power glasslens magnifier to aid the operator in focusing images.

Photographs of the final image can be made by allowing the electron beam to fall directly upon a conven-

tional photographic plate.

Control of Operation

Efficiency of this electronic action depends to a great extent on precision control of all factors which influence, or which might influence, the electron beam. This is accomplished in a number of ways.

The physical appearance of the essential electronic components (Fig. 6) illustrates their relative size and (simplified) arrangement inside the main column of the microscope.

The electron gun has an adjustment for raising or lowering the filament heater with respect to the cathode, controlling, to a certain extent, the intensity of the electron beam. Two thumb screws near the base provide angular or "tilt" adjustment of the assembly and two other screws move the gun laterally at right angles to the axis of the column, thus directing the electron beam so that it coincides exactly with the tiny aperture of the condenser lens (Fig. 6).

The magnetic field of the condenser lens regulates the intensity of the beam striking the specimen, and this action is controlled by the amount of current flowing through the coil.

Focusing of the electron beam is accomplished by the magnetic field of the objective lens, producing an en-

larged image. This focusing action is controlled by the amount of current flowing through the coil with no physical change of lens or coil position necessary.

Similarly, no change of lens or coil is required for final magnification, because the electron beam is focused by the magnetic field of the projector lens and, again, this action is controlled by the amount of current flowing

through the coil.

Each of the three magnetic lenses contains a pole piece designed for the particular electronic function. Pole pieces for the condenser and objective lenses are fixed. In the case of the projector lens, however, four distinct adjustments of the pole piece provide four broad ranges of magnification. A gap of 364-inch between the two parts of the pole piece offers a magnification range from 7500 to about 22,000 diameters as the projector lens current is raised from minimum to maximum. When the gap is 1%4-inch, the magnification range is from 4000 to 11,000 diameters. If only the top half of the pole piece is used, the range is from 700 to 4000 diameters. If no pole piece is used with the projector lens, the magnification range is from about 75 to 750 diameters, with distortion usually apparent in the lower part of this range. Within any of these four broad ranges of magnification, there are ten distinct values or steps of magnification, according to the amount of current applied to the coil of the projector lens. Any specified amount or degree of final magnification is obtained by selecting a suitable, fixed, and stable value of energizing current for the magnetic coil.

Only the essential components (Fig. 6) can be allowed to influence the high-velocity electrons passing from the electron gun to the photographic plate. Stray magnetic fields, vibration noises, and all disturbing factors and extraneous effects must be eliminated. For this reason, all of the essential components associated with electronic magnification are enclosed in a single, rigid, well-shielded, cylindrical column (Fig. 4) rising above the control panel.

Since electrons are influenced and scattered by air, the path of the electron beam must be essentially void of air. For this reason, the large, cylindrical, metal column is evacuated by means of suitable pumping apparatus. The state of the vacuum within the column is controlled by a single hand crank, which actuates certain valves operating an oil-diffusion pump (Fig. 4) and a mechanical force-pump. A high vacuum is obtained in a relatively short time. After insertion of a specimen, within 60 seconds the column can be evacuated sufficiently for normal use of the microscope. An interlock prevents application of the filament voltage before the required vacuum is obtained.

In operation, the ability of the magnetic lens system to produce an enlarged image depends upon two important factors; the value of current energizing each of the three coils, and the velocity of the electron beam. To obtain clear and detailed photographs of highly magnified images, these two factors must be constant during the time of exposure. For this reason, separate power supplies are used to provide extremely well-regulated current for each of the three coils. These power supplies are located in the middle and lower cubicles of the cabinet behind the

microscope column and operating panel.

Since the velocity of the electron stream is determined by the potential difference between cathode and anode of the electron gun, this important accelerating potential (50,000 volts) must be maintained with an exceptionally high degree of constancy. This is accomplished by a novel high-voltage power supply (Fig. 5) contained on a single, separate chassis located in the upper cubicle of the power cabinet. Input r.f. oscillations, stabilized at 75 kc., are rectified by three type 8013-A diodes arranged in parallel, providing a stabilized and filtered output. So well-regulated is the output, 50,000 volts up to 1 milliampere, that it is constant to within less than one volt. Styrene con-

Fig. 5. Power supply furnishing an extremely stable, well-regulated accelerating voltage for the electron beam of the mi-croscope. Output of 50,000 volts, up to 1 milliampere, is constant to within less than one volt. Styrene condensers play an important role in this unit. All connecting elements, shields, and tube sockets are of metal and are gold plated.

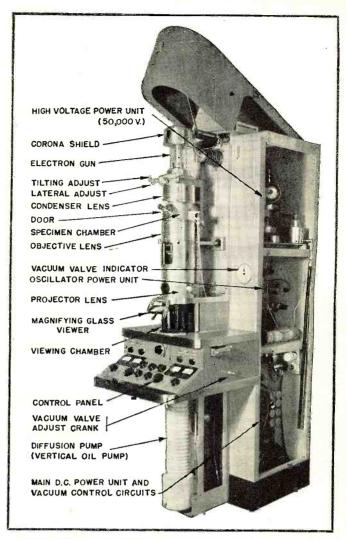
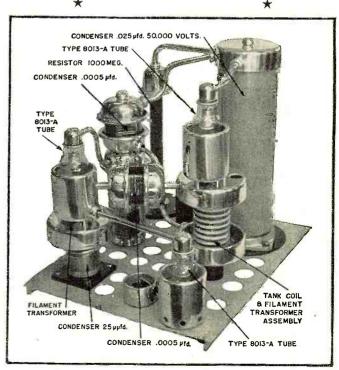
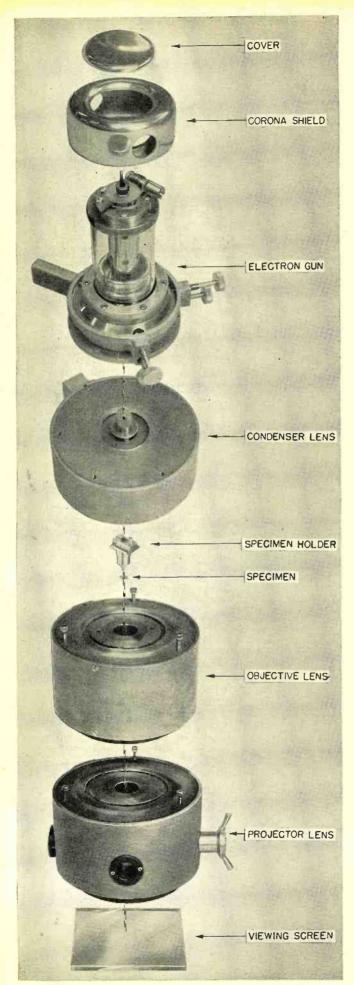


Fig. 4. Complete Electron Microscope, with metal covers removed to show location of all important electronic elements, power supplies, vacuum equipment, control panel, and other major components. Compare this with the simplified arrangement of essential electronic elements as shown in the diagram, Fig. 6.





densers are used; and connecting elements, shields, and tube sockets are metal, and gold plated!

A total of 25 vacuum tubes, power oscillators, rectifiers, and regulators, are used in the three power units contained in the cabinet of the microscope.

Resolution

The complete Electron Microscope (Fig. 4) is considerably more complicated than the ordinary light microscope. Yet in some ways the operation of the Electron Microscope is much simpler and far more convenient. Both types of magnifying devices have certain limitations with respect to one another, but the chief difference between the two types is the higher resolving power and much greater useful magnification of the Electron Microscope.

Ordinary optical or light microscopes are quite adequate for taking photographs at magnifications of 1000 or 2000 diameters. However, an attempt at further enlargement by photography would reveal no new information; the resultant pictures would merely be larger and considerably less clear. This condition exists because the original photographs do not have sufficient resolution (clarity of detail) to permit magnification greater than 1000 to 2000 diameters. In other words, the resolving power of a light microscope is limited.

In the visible range, light waves have lengths between .0004 and .0008 of a millimeter. These wavelengths are relatively long when compared with the size of the particle or object to be viewed; and it is impossible to detect objects or details very much smaller than the wavelengths of the type of "illumination" used. For this reason, the resolving power of a light microscope is limited by the wavelength of its source of illumination, i.e., light.

High-velocity electrons used in the Electron Microscope, however, have a wavelength about 1/100,000 that of visible light. Thus, image resolution with the Electron Microscope is far greater than that obtainable with the light microscope.

Resolution is defined as the ability to distinguish between separate parts or sections of an image.

As a practical example, the average human eye cannot resolve two dots on a piece of paper unless they are at least .2 millimeter apart. One millimeter equals 1000 microns; but even the micron is too big to measure the infinitesimal field of vision of the Electron Microscope. The Angstrom unit is used; and 1 micron is equal to 10,000 Angstrom units.

Stated another way, the average human eye cannot resolve or distinguish detail that is smaller than about 2,000,000 Angstrom units. The Electron Microscope, however, has a maximum resolution of better than 100 Angstrom units!

In everyday terms, this means that particles smaller than a millionth of an inch can be seen clearly and distinctly by the Electron Microscope.

(Continued on page 102)

Fig. 6. Essential components of the Electron Microscope, which originate and control the high-speed stream of electrons. The electron gun consists of a heated cathode and "open" plate, and is the source of the electron beam. Velocity of electrons is maintained constant by the potential difference (50,000 v.) between cathode and anode. Downward direction of electron emission is controlled by tilting and lateral adjustments of the electron gun assembly. Density of the electron beam, just prior to its application to the specimen under observation, is controlled by the magnetic field of the condenser lens. Passing through the specimen holder, the electron beam "illuminates" the prepared specimen. Electrons are affected or influenced according to the varying density of the specimen area being illuminated. Some electrons are scattered out of the field completely: those that continue their journey bear an image of varying density. Focusing of the electron beam is accomplished by adjusting the amount of current flowing in the coil composing the objective lens, with all distances between electronic elements remaining fixed. The amount of final magnification of the image is determined by the amount of current flowing in the coil of the projector lens: and again no physical movement or change of lenses is necessary to vary the amount of magnification. Final image is obtained when the electron beam strikes an observation screen or photographic plate.

An Open Letter to the Radio MANUFACTURER

By A. C. W. SAUNDERS Saunders Radio & Elec. School

Servicemen make excellent goodwill ambassadors-you can help them by heeding these suggestions.

HE engineer designs a radio receiving circuit employing mathematics and techniques of radio physics.

The radio service technician approaches the maintenance of a radio receiver with a knowledge of test instruments, technical skill, and patience.

In design, the circuit is engineered to give the utmost in performance. This is considered in the blueprint and mathematical stage. For "eye appeal", to aid sales promotion, the receiver is dressed up with a handsome dial and cabinet as befits the American home.

In making the prototype of a receiver the mechanical design of the chassis and the parts layout is tailored to fit a production schedule and minimum manufacturing cost considerations. The latter, of course, is economically sound. However, in the arrangement of component parts very little consideration, if any, is given to future repair problems.

We can support this statement with an example from a recent servicing report which showed where a manufacturer located an i.f. transformer too near the rectifier tube. This caused frequency drift. The hours spent in tracking down the source of the trouble were most discouraging. Space does not permit listing the many errors, from the service standpoint, in design and layout of component parts. To mention a few examples will serve to illustrate the point of this article.

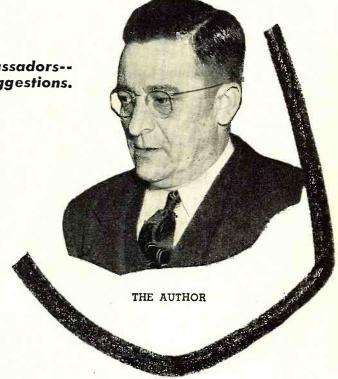
The object of this "open letter" is to point out that suggestions from experienced radio servicemen can be of great value to the industry as a whole and will result in giving the general public better and quicker service.

The most profitable service is quick service. For the radio repairman time consumed in getting to the root of a trouble is wasted time. An example of this is in the case of the i.f. transformer versus the rectifying tube. The record shows four hours of troubleshooting. It took only 2 minutes to place a piece of asbestos as a heat shield around the i.f. can.

The Radio Service Industry now has 27 years of knowledge and experience. The time has come when the repairman in the field should be given a chance to offer constructive suggestions on receiver layout which, if adopted, would enable him to give better service and face less criticism. It is only natural to feel that such an exchange of views between them would be of mutual benefit to both manufacturers and servicemen.

I venture, on behalf of the radio service fraternity, to make the following simple suggestions for consideration.

The tube socket pin connections are important test points in diagnosis. In most cases these contact points are obscured and difficult to reach. They are invariably hidden by a conglomeration of component parts and wiring networks. It becomes a practical impossibility to apply a signal tracing probe, or for that matter, a voltmeter test prod without first removing a number of component parts. When this has been done,



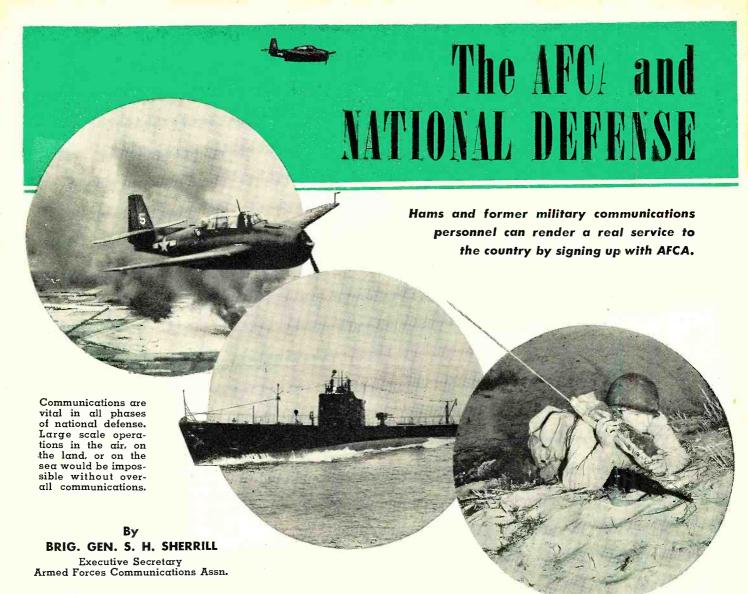
frequently the test is of no value. For example, the output transformer in a popular model receiver completely covered three tube sockets and the connecting wires of the transformer were inaccessible for tracing or test. Cases of this kind are numerous.

The reproduction of the above mentioned receiver was unexcelled, but disturbed by intermittent operation. The cause was eventually found to be a tone control condenser buried under an array of component parts. These parts had to be removed before the condenser was accessible for test and observation. The record shows: time consumed in removing parts—30 minutes; diagnosis—5 minutes; replacing parts removed—30 minutes. This amounted to one hour wasted due to inaccessibility of the defective unit at the plate of the output tube. It is suggested that the tube socket terminal connections be at all times accessible for making tests.

A competent radio repair technician (most of us are that) is one who spares the soldering iron and systematically performs a test in tracking down trouble. If given the opportunity he is able to diagnose an electrical defect in a ten tube receiver in ten minutes while his soldering iron is still cold. His system is as follows:

- He first inspects the underneath wiring of the chassis for obvious defects such as poor connections and loose parts. This is a must for every receiver. He does this first before applying power.
- 2. He then checks tubes. Sometimes he has to rig up a derrick to get the tubes out of tough locations.
- 3. He then tests "A", "B", and "C" voltages, and signal traces, if necessary.
- 4. Then he aligns the set, if necessary.

 (Continued on page 141)



SHOULD like, at the beginning of this article, to examine in rather general terms the military situation of the United States from the point of view of Industry's part in it. This can be done by quoting General Eisenhower and General Collins in their most recent utterances. They are, therefore, the

thoughts of military leaders to whom all information on these matters is available.

You know, after the first World War,

the public settled back and said: "Well, we have won this one. Thank God, we will never have another one of these. We are through with this business of war. We don't want to hear any more about it. That is the job of the Army and the Navy. That is what we pay them for. Let them worry about it." So everyone settled back and the Army and

one settled back and the Army and Navy attempted to do what they could with no support or interest from most Americans and their representatives.

Washington feels very keenly that we must not let that condition develop again because the problems of national security are far too profound, and their ramifications are too great, frankly, to

trust them to the military services alone. We are confident that any war of the future—as never before—will be total and will touch whole populations to a degree hard for us in the United States even to imagine. Certainly, we know from the last two world wars that they were not fought solely by people in uniform. And even the greatest proportion of people who fought it in uniform, were civilians a few short months or years before the pay-off.

We have finally learned that national defense is not the exclusive property and concern of men in uniform, but is the responsibility as well of labor, management, agriculture, industry, and every group that goes to make up the national life. We also have gained a clearer appreciation than ever before of the value of the time factor in the security problem. The layman, equally with the professional, has correctly interpreted the events and developments of our century to mean that no matter how vast may be a nation's latent or potential power, it will be helpless to defend itself if. unprepared, it is suddenly subjected to attack by a modern military machine.

Many did believe that, in 1948, major security projects have slight chance of passage because this is an election year. But now—since March—the people and their representatives in Congress are at last awake to the danger of apathy in military preparedness.

Our unique industrial economy-universally accepted as a major factor in the Allied victory—is stronger than ever before. Foremost among many technical advances, we have achieved atomic fission. Alone among the industrial powers, our production plant suffered no physical damage during World War II; in fact, we amplified our productivity and developed new techniques that vastly increase our economic efficiency. Consequently, our productive capacity now exceeds, by a greater margin than ever before, our essential domestic consumption, and this differential is a highly indicative yardstick of a nation's defensive potential.

Generally speaking, another war would be fought with weapons devel-

oped before its onset. Except in rare instances, weapons whose development is initiated after outbreak of war have little effect on its outcome because of the time lag between birth of the idea and the attainment of volume production. We must do everything possible now to assure ourselves that we will fight another war with weapons more advanced than those of an enemy. In particular, we must concentrate on designing ground army equipment that will be air-transportable; airborne troops must be given relatively the same supporting fire power that was available to infantry divisions in the last war. And aircraft of maximum speed and firepower must be developed-with the latest in communication and photographic equipment.

Planning for American security, however, is based ultimately on our industrial economy. This is the primary field of the Munitions Board and the National Security Resources Boardagencies established in recognition of the fact that, if numbers were the sole yardstick of military capacity, we could not expect victory over a more numerous foe. General Marshall observed at the end of World War II that we were able to mount successful offensive operations all over the world despite a strategic inferiority in numbers of troops, because the United States industrial establishment vastly exceeded that of the combined enemy. Superiority in the air and on the sea, in ground mobility and fire power, based on industrial output. gave our combat forces superiority at the points chosen for attack. In the future, military readiness must include industrial readiness; and industrial mobilization must be an integral part of detense mobilization. Effective organization, and the enabling legislation required, merit a priority in our security planning.

Joint effort by government agencies, the Armed Forces, industry, and labor can assure us the quick conversion of the nation's industrial establishment to war effort should an emergency demand it. For this, as for political and military planning, we have the lessons of two world wars to guide us.

The major defects of past industrial mobilization have been; inexperience of civilian plant operators in producing purely military items, inefficient allocation of material due to competition between the services and between them and private enterprise, and delays caused by retooling, and by shortage of skilled manpower in some areas while a surplus existed in others. The fundamental defect, however, was the lack, during peacetime years, of coordinated preparation by the industrial and military establishments for the future effort that would be demanded of them jointly.

All of the foregoing indicates that there is a greater need now than ever before for closer cooperation between the military and civilians. Ordnance saw a need for a link between them back in 1919, 29 years ago, and Army Ordnance Association was formed. Over the intervening years that Association has grown in size and ability to assist the Armed Forces; so much so that the Chief of Army Ordnance recently stated: "Since World War II, the Association has carried on a splendid fight for national awarenes of the dangers of apathy in armament matters. Perhaps no other group within or without the Government strove so consistently and for so many years for the right to give industry educational orders. Certainly no other civilian group has done so much in promoting what I call the Science-Industry-Ordnance Fraternity.

"In conference with the Army Ordnance Association, it has been decided that, henceforth, the Ordnance Department will keep industry informed through the Association. The Association will thus be the liaison to tell manufacturers our plans for production, the problems we have for them to solve, ways in which cooperation and coordination may be made more effectual. Five active committees of the Associationon artillery, fire control, gauges, smallarms ammunition, and small armshave already sat in conference with us a number of times, and put much effort into solving of our mutual problems. Members of these committees are key industrialists, and when they speak for the companies of which they are executives, their attack on problems is direct and followed by action."

Industrial engineering of the sort these men carry on is vital. Recognition of this fact is seen in the present aim of the Army-Navy Munitions Board to develop an industrial mobilization plan that is larger, more all-embracing than any attempted before in peacetime. Some phases of the plan have already been activated, while top military and industrial experts are working out others.

And that brings me to Armed Forces Communications Association, the reasons for its formation and what it has done and hopes to accomplish. Just recently, the Munitions Board in a directive outlining to the military planners the procedure to follow in the alloca-

(Continued on Page 188)

Naval radiomen, such as these shown operating a "walkie-talkie", can again fill a vital role in national preparedness.

June, 1948

New Manda in RACRIVER DESIGN

W. WILLIAM HENSLER

Staff Eng., Howard W. Sams & Co., Inc.

T THE late war's end, there was a shortage of all consumer items. Included in this shortage were home radio receivers. This condition resulted from radio receiver manufacturers engaging in other work, thus causing a stoppage of new receiver production as well as contributing to a shortage of replacement and repair parts. After replacement parts and tubes became available many receivers could not be put in operation economically, and there was an obvious need for radio receiver manufacturers to produce new equipment quickly. The O. P. A. regulations constantly hampered the radio industry, necessitating many compromises in components and parts. The radio industry was one of the first to convert to peacetime activities, and incidentally, has been one of the first to fill the needs of the market. As proof of this prompt action, it has been estimated that 15 million receivers were manufactured in 1946 and about 18 million in 1947. One of the reasons for this quick recovery to near-peak production was the fact that many of the first postwar models were identical chassis to the last prewar models. This made it possible to use the same production tools, design engineering, alignment and test procedures, and thus quickly produce a product.

In a few cases some manufacturers were able to design and perfect new equipment superior to their prewar product. The apparent successes in this field are the new FM receivers, which are designed to cover both the old and new frequency bands. Prewar, of course, the FM frequency assignment was 42-50 megacycles and some manufacturers had produced receivers operating in this band. By the end of the war, the FCC had allocated a new band of frequencies, ranging from 88 to 108 megacycles, for

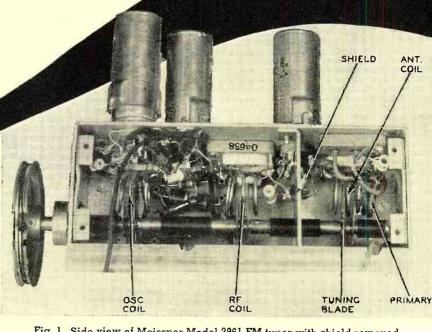


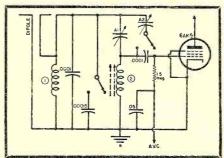
Fig. 1. Side view of Meissner Model 2961 FM tuner with shield removed.

Part 1. The first of a series of articles covering special design features encountered in new postwar receivers. This article deals with the construction and operation of several types of FM-AM tuner units.

FM broadcasting. Although many new techniques had been developed during the war for operation at these frequencies, there are several different tuning systems being used at the present time. This article will consider these FM input and tuning systems.

There are, at present, six distinct types of FM tuning systems being employed by radio receiver manufacturers. While some of them are more or less conventional types, it is well to point out that the requirements for an FM tuning system are somewhat different from the requirements for a standard AM tuner. First, the system must be mechanically rugged. Any tendency of the system to "give" will cause poor

Fig. 2. Schematic of the input circuit of the G.E. "guillotine" FM tuner.



calibration, misalignment, and tuning backlash—all faults which are amplified many times over the same difficulties in AM systems in the broadcast band. If the design engineer has solved the problem of producing a mechanically stable tuning system, he must then solve the problem of the most satisfactory method for injecting the FM signal from the antenna into the tuning system itself.

Capacity Tuned

This tuning system does not vary too greatly from the conventional design that has been used in AM receivers, the main difference being in the size of the tuning condenser and the coil. The tuning condenser usually has three plates and the coil consists of from three to six turns of wire which is usually silverplated to give a higher "Q." Some of these coils have adjustable powdered iron slugs which may be adjusted for proper tracking.

There are two methods of coupling the antenna to the antenna coil. One is the conventional circuit using an antenna coil having a primary and secondary. The other provides for connection of the antenna to a tap on the antenna coil at the proper impedance point. The tapped coil method is especially effective where an unbalanced in-

put system is used. The low side of the antenna coil is already grounded so that the shield of the unbalanced line may be grounded to the chassis. The ungrounded side of the line is connected to the tap on the antenna coil. Thus, with only one tap, the antenna impedance has been matched and a gain is realized due to the autotransformer action in the antenna coil. The other system, however, is more often used due to the more popular use of the balanced "300 ohm" line. The primary usually consists of two turns of wire, either wound inside the antenna coil or interwound at the low end of the antenna coil. The center of the primary is connected to the chassis, or more frequently is bypassed to chassis to give antenna iso-

Most of these input systems couple to the grid of the first tube. There is another type of coupling being used. This method uses a grounded grid amplifier. Arvin and Westinghouse have introduced models using this type of amplifier. The FM signal is coupled to a coil or choke which is in the cathode circuit of the tube. The grid is grounded, or, in this case, is bypassed to ground so that a.v.c. voltage may be applied to the tube. A schematic of this circuit is shown in Fig. 3. The tube current, which flows through the cathode coil (7), reduces the effective "Q" of the coil and broadens the passband of the circuit. The grounded grid acts as a shield between the input and the output circuits. This type system requires no tuning condenser for the input circuit. The output is coupled from the plate to the grid of the next stage which is connected as a cathode follower.

Because the input capacity of a cathode follower is very low, the input resistance of the tube is correspondingly high. Note that the cathode connection

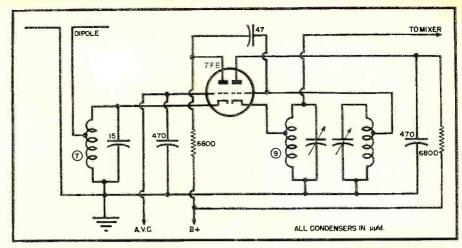


Fig. 3. Schematic diagram of the input circuit of Arvin and Westinghouse FM receivers which use the grounded-grid radio-frequency amplifier.

is tapped down on the cathode coil (9) so that some gain may be realized from the stage.

The FM and AM sections of the tuning condenser are usually combined into a single unit. This eliminates the need for coupling the two units together for tuning. To prevent excessive r.f. currents in the chassis, some manufacturers isolate the frame of the tuning condenser from the chassis and then ground each section with a large braided strap. This strap is returned to the chassis near the associated tuned circuit, thus reducing chassis paths in series with the tuned circuit.

The most popular type oscillator used in the condenser-tuned circuits is the "hot cathode" type. This is probably due to the ease with which the coil can be tapped. Since the oscillator coil is connected to the chassis, the heater terminal of the oscillator tube to be grounded may be connected to the cathode. A heater choke is connected in series with the other heater lead. This places the heater above r.f. ground and reduces the

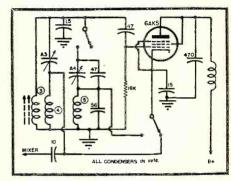


Fig. 4. Circuit of the oscillator portion of the G.E. "guillotine" FM-AM tuner showing the bandswitching arrangement used.

shunting effect of the heater-to-cathode capacity.

Those sets not using separate oscillators usually use the 6SB7-Y or 6BE6 as mixers. The use of a dual-triode is becoming more popular. *Motorola, Westinghouse, Crosley,* and *Philco* are a few of the companies who are using this type of converter almost exclusively. In this

(Continued on page 170)

Fig. 5. Top view of the G.E. "guillotine" tuner.

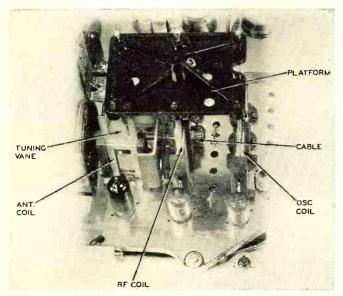
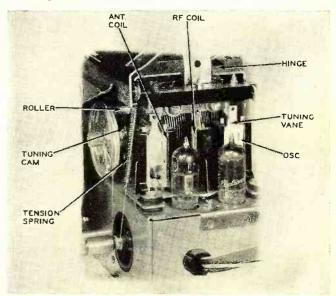


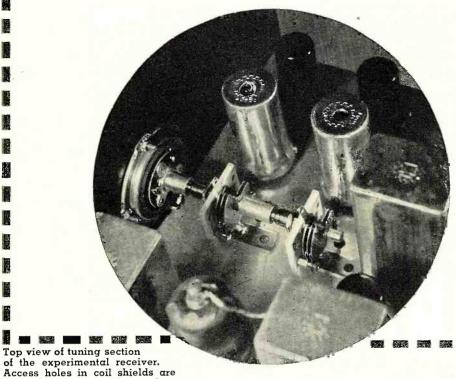
Fig. 6. Another version of the "guillotine" tuner.



June, 1948

A New Approach To GANG TUNING

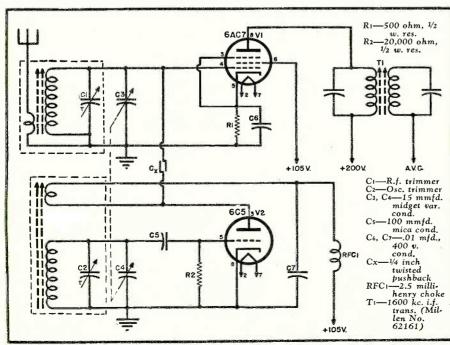
By NEWTON G. NOELL, W9BMS



Simple method for designing ganged tuned circuit for home-built sets, using permeability tuned coils.

for adjusting the padder condensers.

Fig. 1. Typical application of slug-tuned coils in a superheterodyne receiver.



T is a well-known fact that few amateurs attempt building the receivers they use, a possible exception to this being the simple regenerative jobs most of us used to learn the code and get started on the air. Reasons for this are many and varied, but the most important is undoubtedly the difficulty in using ganged tuning while retaining good tracking characteristics. It is the author's conviction, however, that the introduction of shielded, permeability tuned, plug-in coil forms should be a definite incentive to build our own receivers. They are tailormade for the job!

Little design information has been published on the use of permeability tuned coils. Therefore, it is the purpose of this article to set forth a relatively simple method of designing ganged tuning circuits using *Millen* 74001 coil forms, and to describe briefly a receiver that was built experimentally in the development and proof of the author's ideas.

Correct tracking in a superhet receiver is accomplished by designing the local oscillator and r.f. tank circuits so that the local oscillator always tunes to a frequency equal to the signal frequency plus or minus the intermediate frequency. This may be done easily by using a high ratio of fixed to variable capacity across the tuned circuits, providing the frequency band to be covered is relatively narrow. The one drawback, that of pruning the inductance to the exact value, can be eliminated by using permeability tuned coils. If the fixed capacity across each tuned circuit, in the form of small zero or negative drift ceramic types, is mounted inside the coil shields, the advantages to the amateur designer are easily seen.

Determination of the values of L and C to use is accomplished through the use of LC constants and a little simple mathematics.

The LC constant for any one given frequency is $K=25330/f^2$, where f is in megacycles, C in micromicrofarads, and L in microhenrys. Thus, to cover a given band of frequencies:

 $K_1/L-K_2/L=C$ variable

Solving for L:

 $L = (K_1 - K_2) / Cvariable$

Knowing L, the padder value is:

 $Cpad = K_2/L$ —Cinput—Cmin.—Cstray

Where:

 K_1 is the LC constant for the low end of the band

 K_2 is the LC constant for the high end of the hand

L is the desired inductance

C variable is (C max—C min) of the tuning condenser

C input is the r.f. input capacity of the mixer tube or the oscillator tube, as the case may be

C stray is the distributed capacity of (Continued on page 172)



Conversion of SCR-274N RECEIVERS

By C. W. ROESCHKE, W5MLX

Simple methods for converting receivers of the 274 series and extending their ranges.

7 HE receivers of the SCR-274 series results desired. As the receivers are supincluding the ARC-5 Navy version, offer the advantage of excellent construction combined with good performance. Little conversion is required to adapt these receivers to either a.c. or mobile operation, and inasmuch as the per unit cost is low, several may be purchased and used as auxiliary or standby units.

These receivers are supplied in four frequency ranges which may be readily identified by the model number. The BC-453 covers the range of 190 to 550 kc., the BC-946 covers 520 to 1500 kc., while the BC-454 covers from 3.0 to 6.0 mc. The range from 6.0 to 9.1 mc. is covered by the BC-455. These receivers all have the same general appearance and construction, and the only essential difference lies in the i.f. frequencies and frequency ranges. The circuit shown in Fig. 4 is typical of all the receivers in this series. Minor differences are in the tuning capacities and the values of a few parts.

There are several methods of conversion that may be used, depending on the

plied for 28 volt d.c. operation, if batteries or a power supply are available to furnish this voltage and the receiver is equipped with the original dynamotor, no changes at all are necessary. However, it is doubtful if many users will care to operate the receivers under this condition.

Fig. 1. A converted unit with a built-in speaker located at the rear of chassis.

The tube lineup of the receivers consists of a 12SK7 r.f. stage, a 12K8 oscillator-mixer, two 12SK7's as i.f. amplifiers, a 12SR7 as a combined second detector and b.f.o., and a 12A6 output stage. The heaters of the tubes are wired in series in pairs, permitting use on a 24 to 28 volt heater supply.

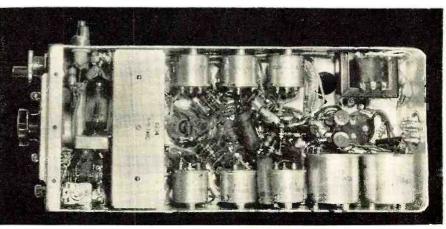
If a 24 to 28 volt transformer, capable of furnishing one-half ampere is available, the filament circuit need not be rewired. Recently there have been several transformers of this type advertised. There are also combination transformers available which are capable of furnishing the necessary plate voltage.

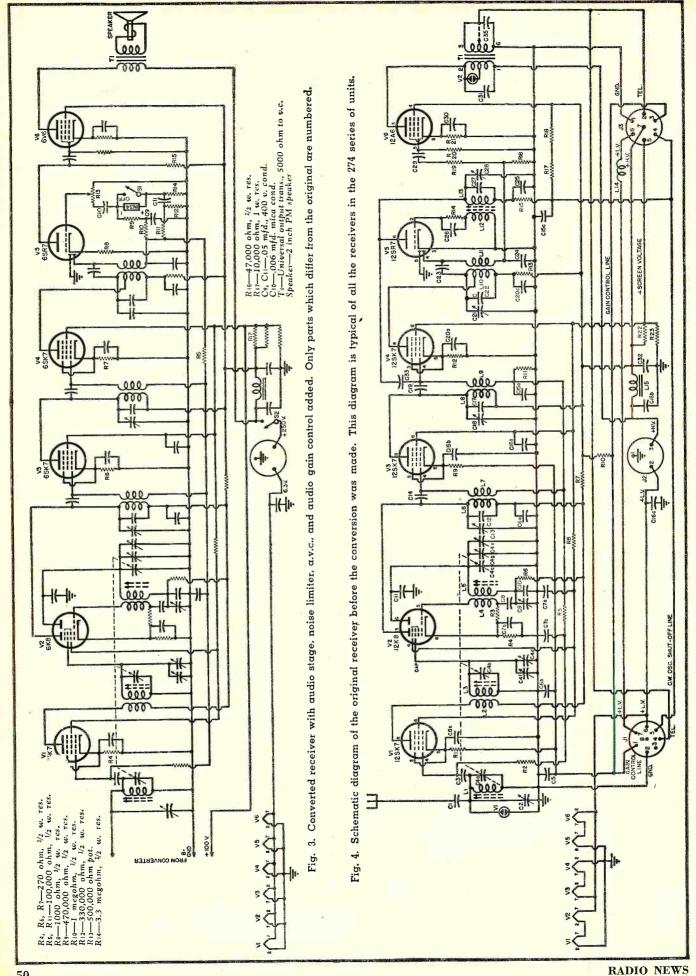
In the event that it is desired to use a transformer of the standard type, it will be necessary to rewire the heaters so that the heaters are all in parallel.

The first step in this conversion is the removal of the bottom plate, easily accomplished by the removal of the screws holding it in place. The tubular condensers and other components mounted along the sides of the chassis should also be removed and allowed to hang over the sides of the chassis. The leads to these components should not be removed, as they will be replaced when the conversion is complete. The heater wiring may be easily traced by following the diagrams in Figs. 3 and 4. One terminal of each heater should be grounded, and a common lead run to the other heater terminals.

When the heater rewiring has been completed, the next step is the inclusion of a gain control. This is best installed in the small adapter socket panel, held in place by four screws. This panel should be removed and disassembled, retaining only the panel portion. The hole presently occupied by the knob should be enlarged to 3/8 inch diameter to take a standard gain control. Two $\frac{1}{2}$ inch holes are drilled on either side to accommodate the b.f.o. and standby

Fig. 2. Bottom view of a converted receiver with the ten meter converter added. The 6J6 converter tube may be seen mounted between the coil box and front panel.





switches. The gain control is connected between terminals 1 and 2 on the receptacle located just behind the control panel.

A 50,000 ohm wirewound control is the value found most satisfactory in this position. The control selected should have a taper designed for control of cathode bias. The b.f.o. on-off switch is connected between terminals 5 and 2 on the control plug. The standby switch is connected from terminal 7 and terminal 2, and serves to ground the center terminal of the power transformer secondary shown in Fig. 7.

The audio output of the receivers is rather low, but is sufficient to drive a small speaker or a pair of headphones. A phone jack may be mounted on the side of the chassis, and connected to terminal 4 of the control plug. The frame of the jack should be grounded to the chassis.

Normally the receivers are supplied with the output transformer connected for high impedance (8000 ohm) output. A tap on the output transformer permits the matching of 600 ohm loads. With the majority of headphones in use, the high impedance tap is the proper one, and the connections of the output transformer should be examined to see which connections are used.

Parts list for diagram, Fig. 4.

R1, R4, R9-620 ohm res. R2, R20-2 megohm res. R1, R4, R9—620 ohm res.
R2, R20—2 megohm res.
R3—51.000 ohm res.
R5—150,000 ohm res.
R1*—150,000 ohm res.
R1, R3, R13—200 ohm res.
R10—360,000 ohm res.
R11, R19—100,000 ohm res.
R12—510 ohm res.
R14*—100,000 ohm res.
R14*—100,000 ohm res.
R15*—5100 ohm res.
R16*—817*—51,000 ohm res.
R19—510,000 ohm res.
R22, R23—7000 ohm res.
R22, R33—7000 ohm res.
C1—85 mmfd. cond.
C2—15 mmfd. cond.
C3—100 mmfd. per sec. (in BC-455)
C4—147 mmfd. per sec. (in BC-454) C4-147 mmfd. per sec. (in BC-454) C5-3 mfd. cond. C6-.05/.05/.05 mfd. cond. C7-.05/.05./.05 mfd. cond. C8, C24—200 mmfd. cond. C9—40 mmfd. cond. C10*—240 mmfd. cond. -3 mmfd. cond. C12, C14, C17, C19, C22, C23—180 mmfd. cond. C13, C18, C21—17 mmfd. cond. C13—05/.05/.05 mfd. cond. C16—22/.22/.22 mfd. cond. C25, C31—.001 mfd. cond. C26*—100 mmfd. cond. C27*-185 mmfd. cond. C28—34 mmfd. cond. C29—.006 mfd. cond. C30—15 mfd. cond. C35—750 mmfd. cond. L1—Ant. input L2, L3—R.f. amp. L4, L5—R.f. osc. L6, L7—In first i.f. L8, L9—In second i.f. L10, L11—In third i.f. L12, L13—C.w. osc. L14—112 microhenry r.f. choke L15—3 henry a.f. choke Ti-Output trans. Vi, V2-Neon tubes Output trans. *Indicates values that vary with the receiver. Those shown apply to receiver B-455-B (6.9.1 mc.) only. Additional circuit elements which may be required in other radio receivers are not shown in this schematic.

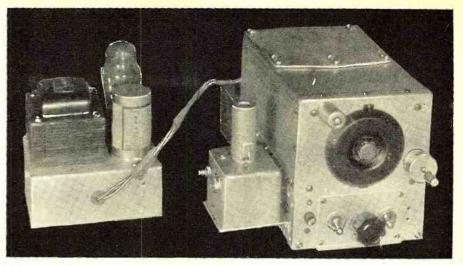


Fig. 5. A converted receiver with a.c. power supply and "outboard" converter.

With the alterations listed to this point, the receiver is ready for service, with the proper source of power. A satisfactory a.c. supply is shown in Fig. 7. The use of the resistor R_1 in place of the normal filter choke serves a dual purpose. It serves to drop the output voltage to the proper value of 250 volts

and, in addition, contributes materially to the filtering action. The 5.0 and 6.3 volt windings of the power transformer are connected in series, to give a total voltage of approximately 12 volts under the load of the receiver. Care should be taken to see that the voltages in the

(Continued on page 162)

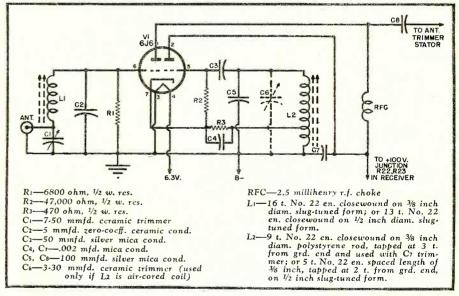
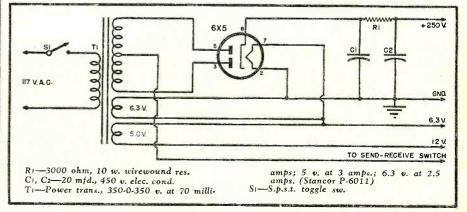
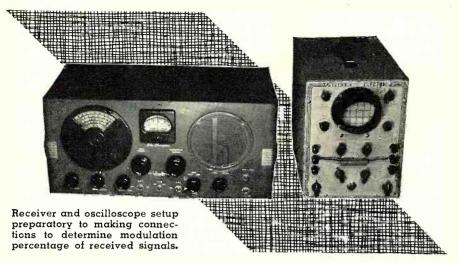


Fig. 6. Schematic of the converter section used with the 274 series receivers.

Fig. 7. An a.c. power supply suitable for powering any of the 274-N receivers.



Measuring Modulation Percentage of AM SIGNALS



By RUFUS P. TURNER, WIAY

Properly connected to a receiver, a scope will give modulation patterns for received signals.

T IS well-known that per-cent modulation reports given by most hams received signals usually are worthless. To be sure, extremes such as overmodulation and undermodulation may be detected, but the ear is not a dependable instrument and should not be the basis of numerical reports. No serious operator is overly disturbed by an ear report rating his modulation as

HORIZONTAL DEFLECTING PLATE MODULATED VERTICAL DEFLECTING PLATE

Fig. 1. Connections for producing "circulmodulation patterns on the screen.

such-and-such definite percentage. Indeed, it is amazing to note the various degrees of overmodulation which commonly are recognized by top amateur phone operators as flat 100 per-cent.

From time to time, readers have shown interest in securing a quantitative scheme for more accurately reporting the modulation percentage of received signals. The viewpoint has been that a simple modulation indicator would rank with the S-meter in furnishing useful information regarding received signals.

Oscilloscopic Method

ested in measuring the modulation percentage of received signals has at his disposal an interesting oscilloscopic method. A number of amateurs already use the oscilloscope to check transmitter modulation and can shift the instru-

The operator who is seriously inter-

concerning this method has not appeared in the radio magazines for several years and undoubtedly some amateurs will learn about it for the first time from this article.

ment easily to the receiver. Information

Fig. 1 shows the basic connections employed. The amplitude-modulated r.f. signal is applied to the horizontal and vertical deflecting plates of the cathoderay tube through a phasing network comprised of condenser C and resistor R. The horizontal and vertical amplifiers of the oscilloscope are not used. The "DIRECT" inputs are employed in this application.

Action of the RC combination produces a circular or elliptical pattern on the oscilloscope screen. If the reactance of the condenser is equal to resistance R, the pattern is a circle (See Fig. 3A). For all other ratios of reactance to resistance, an ellipse appears. (See Fig. 3).

When the carrier is unmodulated, the ellipse or circle is formed by a reasonably thin line. A pattern of this type is shown in Fig. 4A. When modulation is applied to the carrier, however, this line swells outwardly and inwardly to produce a "doughnut", as in Fig. 4B, or a disc as in Figs. 4C and D. When modulation is removed, the pattern flips back to a thin-lined ellipse or circle.

Fig. 4B shows how modulation percentages up to 100 may be determined from measurements made from the center of the pattern (point A) along any radius through the pattern. These dimensions may be measured with a scale or ruler, dividers, or by means of the oscilloscope screen graduations. Anything less than 100 per-cent modulation will produce a doughnut, such as shown in Figure 4B-that is, there will be a central dark or open area. At 100 percent modulation, this center hole will just close completely. This unmistakable pattern is shown in Figure 4C. When the signal is overmodulated, the pattern will close up, but a bright button also will appear at its center, as shown in Figure 4D. The diameter and brilliance of this button is somewhat proportional to the amount of overmodulation, however there is no simple way of determining how much higher than 100 the percentage is. It is both interesting and useful to watch these patterns form as the received signal "talks up."

Fig. 2 shows how the oscilloscope must be connected to the receiver to (Continued on page 181)

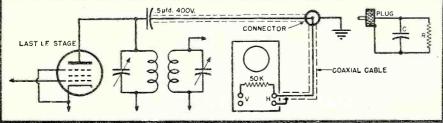


Fig. 2. Complete connections between oscilloscope and receiver. At right is a "constant alignment" replacement plug to be inserted when the cable and oscilloscope are disconnected from the receiver.

ersatile SUBSTITUTION



Front panel view of a commerciallybuilt radio servicing and test unit.

By SIDNEY S. FLEISHMAN

Test-Craft Instrument Co.

Operation and construction data on a commercial test unit designed to facilitate radio servicing.

THE radio serviceman, a skilled diagnostician, like the doctor, must have the proper equipment to fulfill his obligations to his trade or profession. Efficient diagnosis of "ailing" radio receivers requires good diagnostic equipment. With the proper equipment, the serviceman eliminates all guesswork, thus tending to reduce loss of time and labor.

The increased complexity of the radio servicing profession because of recent developments in new circuits and other electronic equipment has established the fact that no radio engineer, serviceman, or hobbyist can be without the proper laboratory or service equipment.

An efficient aid to the radio serviceman is the novel instrument briefly outlined here. Basically a universal type of test speaker, this instrument also incorporates a resistance-capacity decade, leakage tester, continuity tester, output meter, voice coil, and field substitution. Because of its versatility, this instrument establishes the use of the fundamental test of substitution, the pros and cons of which have long since been thoroughly discussed. Receiver components, when under instrument tests, often appear to be in perfect condition, however, when substitution is made, they prove to be otherwise. Primarily designed as an auxiliary instrument, this unit used in conjunction with other instruments facilitates service work.

This instrument, designed around a specially engineered universal transformer, affords proper matching of load impedances up to 25,000 ohms. Both dynamic and permanent magnet types of speakers can be tested equally well. It affords replacement or substitution of any type of speaker, thereby eliminating the need for removing a speaker from the customer's home. Various load

impedances are listed on a chart which is a permanent part of the front panel.

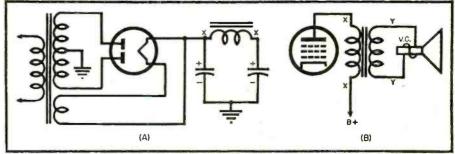
Upon suspecting an open field, the serviceman need only open the field circuit and by means of the tip jacks (marked "Field" on the front panel of the instrument) can easily and rapidly select any substitute field impedance from 500 to 2500 ohms. See Fig. 1A.

If an output transformer is suspected of being defective, it is only necessary to open the primary of the defective transformer and connect the leads from the jacks marked "Input" across the plate and the "B+" of the output tube at points X. Fig. 1B. The proper selection of the input, by means of the three input jacks 1, 2, or 3, is entirely dependent upon the load and the resistance of the output tube and the circuit in question. The selection of the substitute output transformer impedance and the input jacks is made by means of the front panel chart.

If the voice coil is suspected of being defective, substitution can be made easily and readily. The leads of the voice coil are first opened and connection is made at points Y by means of the test leads connected to the tip jacks marked "V.C." across the secondary of the output transformer of the receiver being tested. Fig. 1B.

The resistance substitution decade of this instrument incorporates six standard resistors. These resistors are those (Continued on page 183)

Fig. 1. (A) Method for checking open field coil in a speaker. (B) Means for testing an output transformer (instrument inserted at points X) and method for testing a defective voice coil with tester being inserted at points Y on the diagram.





By McMURDO SILVER McMurdo Silver Co., Inc.

A description of a new, super-selective i.f. channel for use with your present receiver.

OR the amateur or the short-wave listener who has never been troubled by noise, heterodyne interference, or the inability to bring in every station clearly, this article will have no interest. Since it is doubtful that such a person exists, it is probable that the unit described will be of some interest to most readers.

The 100 kc., super-selective i.f. amplifier to be described may be connected to any broadcast or communications-type receiver which employs any intermediate frequency between 450 and 500 kc. Since 455 kc. has been adopted almost universally as the standard for receivers manufactured in recent years this i.f. amplifier may be added to practically any receiver.

When added, it will yield a small increase in sensitivity. Most important however, it will give the receiver a gain in selectivity, and a reduction in noise and interference of approximately four times.

Sharpness of tuning in any superheterodyne receiver is a function of the number, quality, and degree of primary-to-secondary coupling of the tuned circuits in the i.f. amplifier and of the in-

termediate frequency employed. Most receivers incorporate one or two i.f. stages having from four to six i.f. tuned circuits operating at 455 kc. The most expensive receivers may use three i.f. stages having a total of eight tuned i.f. circuits. For a given coil " Q_i " selectivity may be increased by a factor of approximately 4.55 times if the i.f. were lowered to 100 kc.

An alternative for improving receiver selectivity is by means of the widely-used i.f. crystal filter. For 100 cycle selectivity desired in c.w. telegraph reception this is satisfactory—except for the complexity of operation of the crystal filter. This is usually so great that many amateurs, even though they could use such selectivity, actually operate their receivers with the crystal filter switched out as it is too bothersome to operate.

For speech and broadcast reception the crystal filter has never proved satisfactory. Any attempt to "broaden" its selectivity curve usually results in a still sharply peaked nose to the selectivity curve coupled with curve skirts widening too fast for good selectivity but not fast enough to avoid serious distortion of signal quality. To make the general

situation just a bit worse, amateurs who have written of their experiences along this line have commented that the mania for "high fidelity" reception has caused receiver manufacturers to lessen rather than increase the selectivity of their newer receivers.

Ever since there has been an interference problem in radio reception engineers have recognized that the ideal selectivity curve would be drawn in the shape of a perfect rectangle—just wide enough to give passband width adequate for desired quality of reception yet high enough to insure rejection of nearby stations.

Articles appearing in the October and December, 1947, and the January, 1948, issues of "QST" have proposed methods of increasing receiver selectivity toward this ideal. The principle involved was to heterodyne, by a local oscillator, the usual 455 kc. receiver i.f. to a lower frequency at which greater selectivity could be obtained. This may be accomplished by a simple "outboard" i.f. amplifier added to an existing receiver.

The lower the new "outboard" intermediate frequency chosen, the greater the selectivity obtainable. Also the lower the "outboard" i.f. chosen, the greater the probability of image interference due to a signal at twice this new i.f. getting through the basic receiver i.f. amplifier. For reasons of cost, bulk, complexity and such possible new i.f. image interference vs. desired selectivity, 100 kc. appears to be a logical choice. By methods possible today really excellent "Q's"

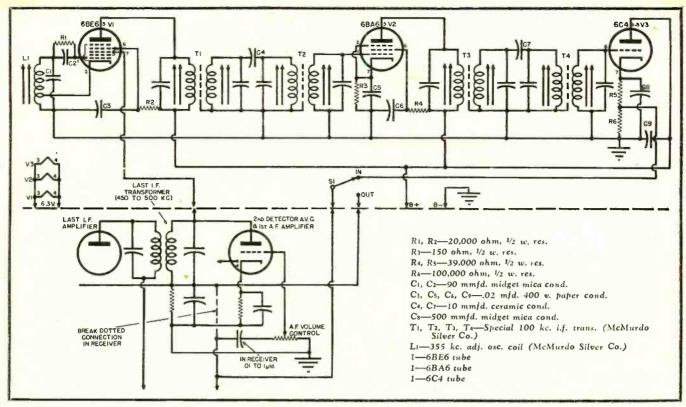


Fig. 2. Schematic diagram of the "805" converter and i.f. channel. The unit is used in place of the regular receiver i.f. channel to provide increased selectivity. The "805" is shown at top while a typical receiver i.f. is shown below.

may be obtained at 100 kc.—so much so as to yield the close-to-ideal selectivity curve of Fig. 4 for four specially designed 100 kc. i.f. transformers.

At first glance it might seem that any receiver exhibiting the sharpness of tuning of Fig. 4 would cut sidebands to a point where speech would be rendered almost unintelligible. It is only 2.4 kc. wide at its "2 times down" point, falling off with close to theoretically perfect steepness to a width of only 7.2 kc. at 10,000 times down. Fortunately, a long recognized but seldom used fact sets such thinking to naught. In any amplitude modulated broadcast or amateur phone transmission there exists the carrier frequency plus two sidebands carrying the modulating intelligence. One sideband lies below the carrier frequency and one above it. Both contain the identical audio modulation. To any engineer it is obvious that we need receive but one of these two sidebands for good signal intelligibility.

If we now look at Fig. 4 in terms of using its super-selectivity to accept but one of the two transmitted sidebands, we see that the audio frequency range is not one-half of 2.4 kc. but instead is 0 to 2400 cycles. Such a frequency range is probably as good, maybe even a bit better, from a fidelity standpoint than that provided by many of the broadcast receivers in use today.

We may, at will, tune in either sideband of a desired station. By so doing we will eliminate entirely the noise, heterodyne squeals, and station interference affecting the other sideband. Thus, we have a two-to-one improvement in selectivity. However, our conventional double sideband receiver will probably have a selectivity curve nose 8 to 12 kc. broad, with skirts falling so slowly as to be unable to reject interference lying 10 to 20 kc. away on either side of the desired signal in the event of reasonably strong interference.

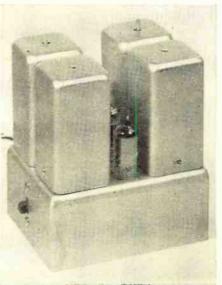
If we credit the average receiver with much more selectivity than will ever ordinarily be found, that is, with a curve nose which is only 10 kc. wide at "2 times down," then it is self-evident that

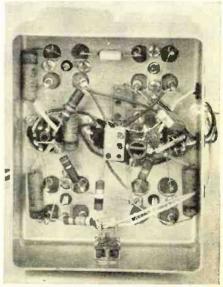
selectivity, such as is shown in Fig. 4, will give a four-times improvement. In actual practice the increase in effective selectivity is much greater due to the new ability to reject all interference on one side of the signal or the other.

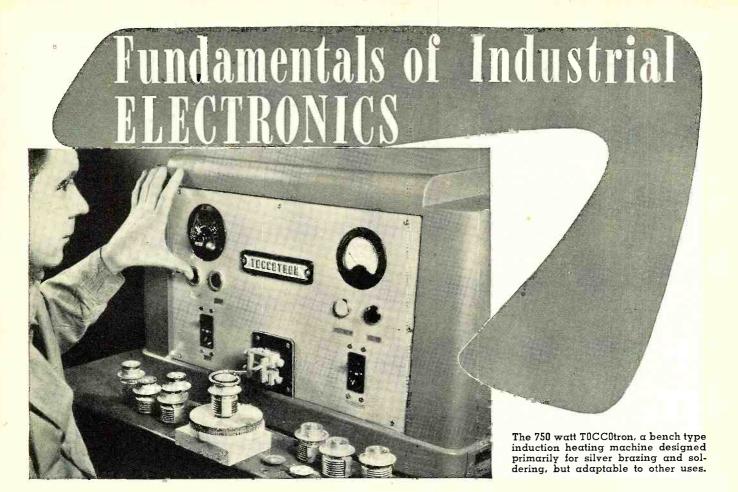
Figs. 1 and 3 show how we may go about getting this "new look" in truly steep-sided curve skirts. We may get it "in a box" as seen in these photographs or it may be built into an new or existing receiver in accordance with the circuit of Fig. 2. The important thing is that the circuit may be added to almost

(Continued on page 137)

Fig. 3. Top and under-chassis views show simplicity of the unit's construction.







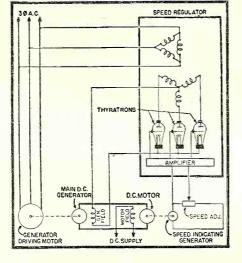
By ROBERT ENDALL

Servicemen—here is a source of income which has been largely overlooked but can prove lucrative.

T THE present time it is difficult for the independent radio service dealer to predict the future progress of the radio service industry. Competition is increasing in the home radiophonograph service field, while the need for service is decreasing with the appearance of new sets on the market. Some television receiver manufacturers are now offering installation and factory service, for an additional fee, as part of the purchase of their television receivers. Another possibility which may develop is that FM receivers, black-andwhite, and color television receiverswhich are much more complex and critical than AM receivers and require the use of advanced testing equipment and technical knowledge-may be serviced mainly through large centralized service organizations, if not by one manufacturer. Any of these eventualities would leave the independent radio service dealer out of the picture to some extent.

It is impossible at present to forecast whether any of the above possibilities will materialize, and what will be their effect upon the industry if they do. To a large extent this will depend upon the quality and adequacy of the services supplied by the independent radio dealer. For his own best interests, therefore, as well as for the interests of the entire in-

Fig. 1. An electronic motor speed control system consisting of a d.c. motor driven by a motor-generator set whose field is energized by the electronic regulator.



dustry it is imperative that he keep his technical progress and equipment abreast of the latest developments in electronic design and manufacture. Instead of allowing himself to be restricted to the relatively narrow prewar fields of home and automobile radio sales and service, he should attempt instead to expand the field of application of the services which he can supply.

One phase of the electronic industry which can potentially become a major phase of the radio service industry in the reasonably near future is the installation, maintenance, and repair of industrial electronic equipment. The fields of application of electronic controls in industry are increasing at a tremendously rapid pace, now that their value has been demonstrated by their many wartime applications. Proof of the importance and potentialities of industrial electronics is given in the recent statement of the Federal Communications Commission that the dollar volume of r.f. heating equipment alone at the present time is equal to the total value of production of all communications equipment.

A number of considerations arise in the service of industrial electronic equipment which make it quite different in certain respects from servicing other radio and electronic devices, and which make the services of the independent radio repairman particularly valuable.

When a failure is encountered in an electronic control device installed in a factory production setup, immediate location and repair of the defective item is of the utmost importance, since many thousands of dollars worth of time, labor, and materials may be lost by unnecessarily prolonged delays in the resumption of production. In addition, preventive maintenance and periodic inspection of equipment perform the extremely valuable function of detecting potential breakdowns of equipment and correcting the defects before they can interrupt production. These factors may open the field of industrial electronic servicing to the local independent radio repairman, since the owner of a manufacturing plant can always count on having preventive maintenance and emergency repair service available on immediate notice, and is at the same time spared the expense of employing his own maintenance department for electronic control equipment.

In many communities, the radio service dealer who has established his competence often tends to take on the position of a sort of independent radio and electronic consultant, to design and build numerous electronic devices which his customers may desire for various purposes. In the past, such equipment has consisted mainly of custom-built radio receivers and phonographs, and gadgets such as automatic garage door openers, burglar alarms and photoelectric exposure timers. In some cases, however, they have been of a much more complex nature such as custombuilt test equipment for industrial concerns. There is every possibility that this tendency may extend to the field of industrial electronic controls, particularly in their installation and maintenance. With an intelligent and conscientious approach on the part of independent repairmen, this should become a major field for the future utilization of their services. However, the great responsibility involved in such service cannot be too strongly emphasized, and the service dealer who plans to engage in industrial service work must be prepared to accept fully this responsibility.

This article is written to present an introduction and brief review of the basic principles of industrial electronics, for the benefit of the radio repairman who would like to prepare himself for future work on industrial electronic control equipment.

Major Applications

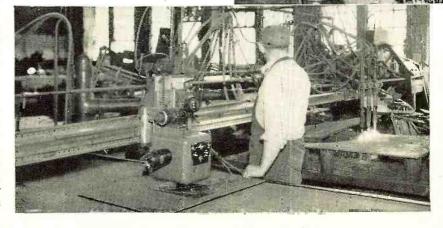
In many applications the introduction of electronic principles has made it a relatively simple matter to perform functions which would otherwise be impossible, while many other industrial problems have been solved better and more cheaply by mechanical or other electrical means. Electron tube devices

An example of a photoelectric relay setup to count objects passing on a conveyer. The objects interrupt a beam of light thus actuating the relay unit. Electronic motor drive used in testing airplane propeller governors. Continuous and accurate control of speed is possible with this electronic control.

Electronic metal detector inspecting plastic blanks to eliminate any piece containing metal particles before the material is subjected to processing.

Photoelectric color register control for multicolor gravure press.

Photoelectric scanning head with gas-cutting control mounted on gascutting machine. The photoelectric scanning head follows the pattern.



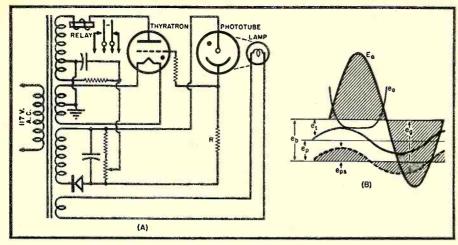


Fig. 2. (A) Basic circuit for an a.c. operated photoelectric relay. (B) Voltage relations of the basic circuit shown in (A).

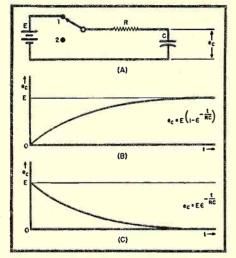
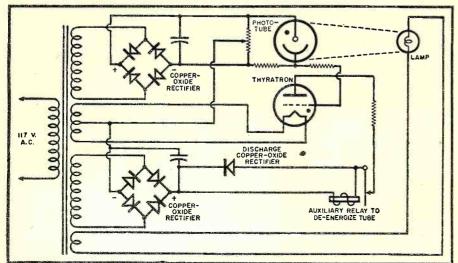


Fig. 3. (A) Circuit for determining voltage across a condenser in a single series RC circuit. (B) Voltage across condenser charging and, (C) discharging.

have proved of value to industry in such applications as process control, as safeguard and alarm devices, and for electrical, mechanical and optical measurements. A few of the many important types of electronic controls, and some of their major applications, will be described briefly to give an indication of their great present and potential value to industry:

- (1) Photoelectric controls, which were the earliest application of electronics in industrial control, are still among the most widely used and among the most important applications of electronics in industry. They are useful for actuating systems in response to a change of color, shade, density, shape, or position of any component of the system, without mechanically touching the controlling object. There are several types of applications:
 - (a) Where only a simple on-and-off relay effect is desired, for instance as limit switches to control manufacturing operations, or for the stoppage of machinery when a light beam is affected, as by a break in a printing press paper roll.
 - (b) Where a varying light input intensity produces a variable regulating effect, as in process regulating equipment.

Fig. 4. Schematic diagram of a lock-in type of photoelectric relay.



(c) Where a selective effect is desired, as in sorting or grading of objects according to some characteristic such as color or size.

By careful design of the optical system so that the variation in light depends only upon the particular characteristic which it is desired to detect, the phototube can serve as a practical substitute for the human eye in many industrial applications.

The simplest and earliest type of industrial photoelectric device is the photoelectric relay, which responds to the presence or interruption of the light beam with an on-off action. It has many applications in making automatic such functions as production counting, conveyor control, door control, lighting control, and many others known only to the individual users. It is possible also to make use of the simple photoelectric relay in connection with optical and mechanical systems of special design to perform many other functions such as automatic weighing control, printing controls, pin-hole detection, grading and sorting, improved safety controls for many types of dangerous machinery, and many other similar applications.

In addition to the on-off photoelectric relay, the continuously variable response of the phototube to a variable light input may be used as the basis for regulating many types of industrial processes where continuously variable control is required. Photoelectric equipment has been applied to perform a variable regulating function in a large number of industrial operations because the phototube satisfies two great needs characteristic of most regulated processes: (a) a means for quick analysis, and (b) a means for quick response control. Many of the more important industrial photoelectric applications fall under this classification of process regulators. Equipment for this type of application includes; chemical process regulators, loop regulators on paper coating or steel strip mills, register regulation for printing machines and for packaging operations, temperature regulation, and controls for other industrial processes.

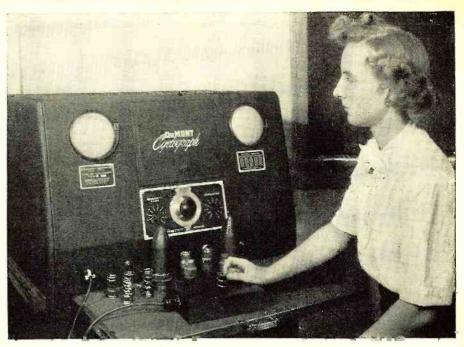
(2) In many industrial applications, the timing or duration of different processes is of great importance in determining the quality of the final product. Electronic timing circuits may be used to control manufacturing operations which are performed in a definite time sequence in which all the time intervals. may be of fairly long duration, as well as processes in which one of the time intervals is so short that it cannot possibly be controlled with any degree of success by any other method. Some of the applications of automatic timing and sequencing devices in the first category include injection molding processes, heat treating cycles, honing machine

operations, photographic printing, intermittent testing, and sequencing of a large variety of industrial operations. Applications in the second category include the precise measurement of time intervals, and the extremely important field of resistance welding control.

(3) The growing industrial need for simple and accurate control of adjustable-speed motors operated on alternating current has largely been solved by the application of electronic techniques. The use of the electronic circuit for motor control has made it possible to obtain the adjustable-speed characteristics of the shunt-wound d.c. motor while taking advantage of the almost universal availability of a.c. power, and at the same time attain a much greater stability and accuracy of control than when the same motor is operated in a d.c. system. The electronic method of motor control has innumerable industrial applications in the operation of all types of machine tools, and wherever else smooth stepless adjustment is required over a wide range of motor speeds.

(4) Accurate measurement and control of temperature is another of the major needs of industry where the application of electronic principles has been of great help. At some stage in their preparation, almost all products pass through one or more processes in which temperature is an important factor. Very often the choice of method and instruments to keep the temperature within set limits may have a considerable bearing on product cost and quality, on continuity of production, and on the life of plant equipment.

The electronic temperature control circuit converts the output of the temperature-measuring element into energy which regulates the action of the furnace or refrigerator, or whatever other type of temperature controlling mechanism is used. The characteristics of electronic circuits are so well suited to the field of temperature control that they have already become the standard method of control in a constantly increasing number of processes. In metallurgical processes and research, where the accurate control and regulation of temperature are especially important and the range to be covered is very wide, a large variety of electronic instruments have been developed to maintain constant temperatures or to vary temperature automatically according to a predetermined time schedule. Controls for high temperatures have been widely used in the production of steel and various iron and steel products, for control of cement kilns, and in the control of furnaces for the manufacture of many other types of products. Electronic controls have also been used in many systems where control of room temperature and refrigerating systems is re-



The DuMont Cyclograph for testing materials by means of magnetic induction.

quired. Refrigeration applications are numerous in oil refining processes, in metal tempering and surface hardening, in rubber processing, and in many other well-known industrial processes. Control of room temperature is one of the requirements of air-conditioning in the paper, textile, and food industries.

(5) The use of electronic circuits to generate power has demonstrated its value in the field of high-frequency heating. Heating of non-conducting objects by dielectric losses, and of conducting objects by induction, from a high-power radio-frequency oscillator have so completely been shown to be superior to other methods in a wide variety of applications that they have become an accepted industrial technique. This method has been especially useful in such fields as vacuum tube production, in the molding and heat-treating of all types of small metal parts, and have enabled such processing to be done much more quickly and conveniently than by older methods.

(6) In industrial operations it is ex-

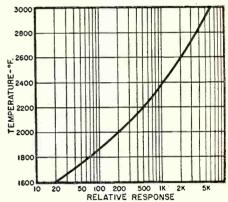
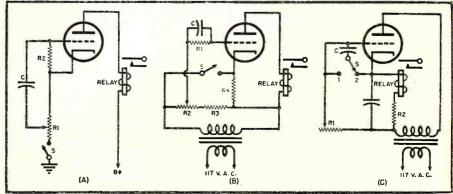


Fig. 5. Typical curve showing phototube response to a black-body radiation.

tremely desirable to be able to stop or position valves, transmission, hydraulic equipment, fire doors, etc., from a conveniently located remote point. One of the important characteristics of electronic equipment in this connection is the ease and simplicity with which signal levels and amplitude of response are

(Continued on page 109)

Fig. 6. Schematic diagrams showing three basic electronic timing relays.



F VACUUM TUBE VOLTMETER

By R. H. KRUEGER

This general-purpose v.t.v.m. is compact in size and versatile in operation. It has a high input impedance, is battery-operated, provides for a.c.-d.c. measurements, and incorporates a polarity-reversing switch.



HE vacuum tube voltmeter described in this article features - small size, reasonably long battery life, and a voltage scale which is linear on all ranges. This instrument has proved handy when working on battery radios out in the field where no a.c. mains are available. Due to its small size and portability it has also been found useful around the service shop.

The meter used is a 0-150 microampere, $2\frac{1}{2}$ inch, round unit, although any other meter with a microamprange of 0-100 or 0-200 may be used. If other than a 0-150 microammeter is used, resistors R_{12} and R_{15} (Fig. 2) will have to be changed. If the microammeter is a 0-200 type, it is recommended that resistors R_{12} and R_{15} be of the order of 35,000 ohms. This, in turn, will increase the "B" battery drain a little but not enough to shorten the battery life appreciably.

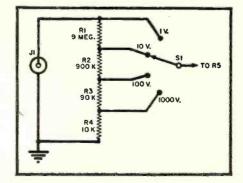
The instrument is entirely self-contained and uses standard sized No. 950 Eveready flashlight batteries and a small "portable" size 45-volt "B" battery, such as the Burgess XX30. Voltage ranges of 0-1.5, 0-15, 0-150, and 0-1500 are covered by the unit. The accuracy of the instrument is very nearly that of the meter and is entirely dependent upon the accuracy of the input resistors, R_1 , R_2 , R_3 , and R_4 . R_{16} is an isolating resistor located in the probe and need not be very accurate. A 3 megohm resistor, R_s , was inserted between the grid of the input tube and the range selector switch to help stabilize the circuit. The grid of this tube was bypassed to ground through a 500 μμfd. condenser.

The circuit is a cathode follower balanced bridge and uses four 3S4 tubes connected as triodes. Each tube has

its own filament battery and as none of the filaments is common a separate filament switch was used for each tube. Two wafers of a four-wafer switch were used for the "A" battery switch which consists of 2-pole, 4-position switches mounted on each wafer. These are located at the front part of the switch. The third wafer is the "B" battery switch and breaks the positive lead. These switches are wired so that they are "on" in all positions except the "off" position. Wafer number four is located at the rear of the switch and serves to reverse the polarity of the meter, which in turn reverses the polarity of the test leads. This makes a total of four positions for the switch, namely, "off," "negative," "positive," and "a.c." If the meter should indicate "positive" when the selector switch is in the "negative" position, the leads at the microammeter should be reversed to correct the reading.

There are nine fixed resistors and

Fig. 1. Alternative input circuit that may be used should dial scale be calibrated in divisions of 1, 10, 100 or 1000, full-scale.



one potentiometer in the bridge circuit proper. None of these resistors is critical in value as long as they are matched in pairs. Resistors to be matched are: R_8 and R_{11} , R_9 and R_{10} , R_6 and R_7 , and R_{12} and R_{15} . About two per-cent accuracy in matching the pairs is close enough for proper balance of the bridge circuit. No trouble was encountered in matching tubes for the bridge balance, nor was any trouble encountered in selecting tube V1 (Fig. 2) to give no grid current and consequently no deflection of the meter when the test leads were shorted. When the range switch is moved through the different ranges no resetting of the zero adjustment will be required. Reversing the position of the tubes may be necessary in order to obtain bridge balance, but a little experimenting with different tubes in different positions should bring about a balance when the "zero-adjust" potentiometer is set at approximately center position.

Although the input circuit uses a probe with a 1 megohm resistor, this has little detuning effect on the circuit under measurement. The probe was constructed using a standard test prod, a 1 megohm resistor, a piece of shielded, single-wire microphone cable, and a connector. The resistor was placed as close to the tip of the test prod as possible and the shielding run close to the resistor. This type of construction produces no meter deflection when the probe is handled.

The input voltage divider, or range switch, was chosen to give voltage readings of 1.5, 15, 150, and 1500 volts.

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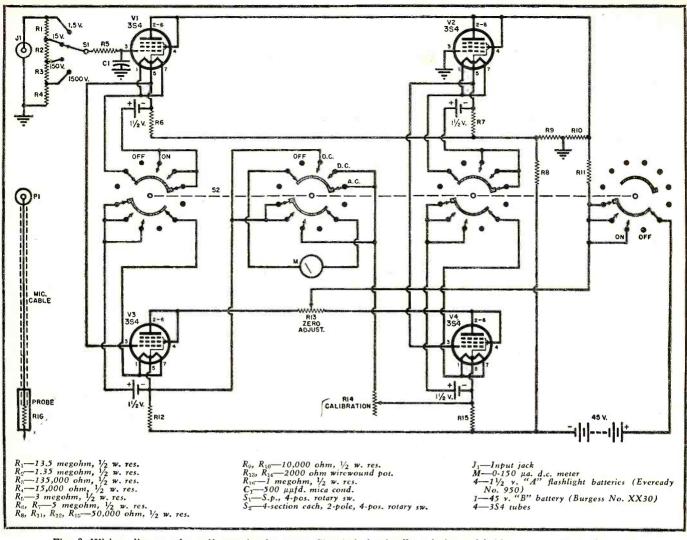
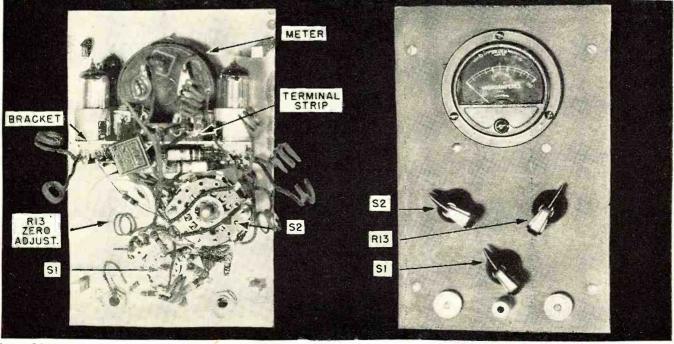


Fig. 2. Wiring diagram for self-contained v.t.v.m. Circuit is basically a balanced-bridge type cathode follower.

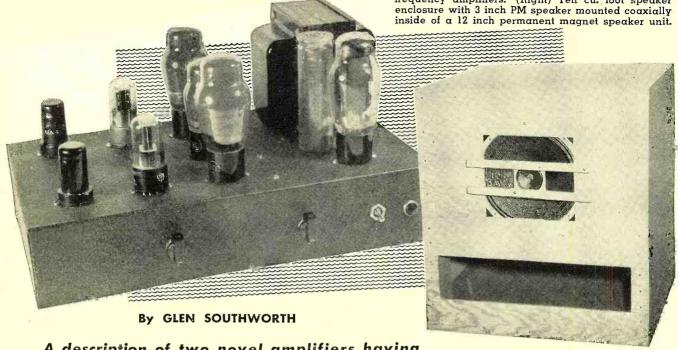
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Front and rear views of the home-built v.t.v.m. One of the input jacks, shown at the bottom of the front panel, is not connected in the circuit. It is simply used to balance the appearance of the panel.



Vide Range Phonograph System

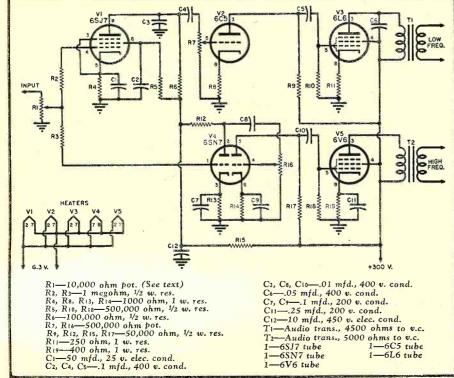
(Left) Chassis with power supply and high and low frequency amplifiers. (Right) Ten cu. foot speaker enclosure with 3 inch PM speaker mounted coaxially



A description of two novel amplifiers having separate low and high frequency sound channels.

NTEREST in high fidelity radios and phonographs has grown markedly since the end of the war, and today an increasing number of sets with high power amplifiers and coaxial speakers amplifiers, speakers, and associated are being placed on the market, while equipment are currently available. Unfor those who wish to assemble their fortunately, ready made equipment is own system several lines of high quality

Fig. 1. Schematic of simplified amplifier with a maximum power output of 6 watts for the low frequency stage and 4 watts for the high frequency stage.



priced considerably higher than the average music lover can afford. By using circuits designed to compensate for the deficiencies in commercial grade components, wide range reproduction may be enjoyed at a reasonable cost.

The system described in this article employs two separate amplifiers, one for the range between twenty and one thousand cycles, and the other for the range between one thousand and twenty thousand cycles. The advantages of this arrangement are numerous.

Absolutely linear response does not mean maximum listening enjoyment in most cases, as the hearing characteristics of different individuals vary widely, high frequency cut-off being from six to twenty thousand c.p.s. Generally, as people grow older their sensitivity to high frequencies decreases and they may derive greater enjoyment from a well accentuated treble. On the other hand, many people enjoy accentuated bass response, and with the use of two separate amplifiers and their associated tone networks, a very wide range of frequency response may be obtained.

Intermodulation distortion is probably one of the chief reasons that many people do not like highs in reproduced music. As a reproducing system is nearly always reproducing complex waves, harmonic distortion may not be particularly objectionable as it merely alters the relationship of the fundamental and harmonics somewhat, giving a somewhat different timbre to the music and sometimes is deliberately introduced to give the listener a sense of "liveness." Intermodulation distortion is noise generated by the modulation of one audio frequency by another to produce spurious "sidebands" which are of an unmusical character and which may make high notes sound screechy or sound like speaker rattle. In conventional amplifiers, intermodulation distortion is related to harmonic distortion as they are both produced by nonlinearities. When large amplitude bass frequencies are passed through the same amplifier with relatively small amplitude high frequencies, severe intermodulation distortion may result from the tubes being driven onto a nonlinear portion of the plate curve, which gives, according to one researcher, approximately four per-cent intermodulation distortion for every one per-cent of harmonic distortion.

The use of two separate amplifiers means that intermodulation distortion can be effectively reduced by separating the large amplitude bass impulses from the lower amplitude high frequencies at the input, thus preventing their interaction

Conventional coaxial and multiple speaker systems are of two main kinds, those with a mechanical crossover systems such as found in "dia-cone" type coaxial speakers, and those with an electrical crossover system of the LC type usually fed from a five hundred ohm line. A dual amplifier system does away with the need for either of these. The high frequency unit drives a high frequency radiator which may be a conventional three or four inch PM speaker, while the low frequency unit drives a twelve or fifteen inch speaker. It should be noted that two twelve inch speakers will approximately equal the radiating area of a seventeen inch speaker and four, a twenty-four inch speaker, though may be inferior from the standpoint of resonant frequency and transient response.

Selecting a speaker with a low resonant frequency is desirable to prevent boom in reproduction, and it is best to pick a fairly heavy diaphragm to keep the speaker from cracking up at high volume levels.

Frequency runs made on small three, four, and five inch PM speakers showed that acoustic output could be obtained to above sixteen thousand c.p.s., and that the speakers were capable of radiating considerable amounts of power above one thousand c.p.s., though the power handling capabilities are limited and care must be taken to attenuate

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June, 1948

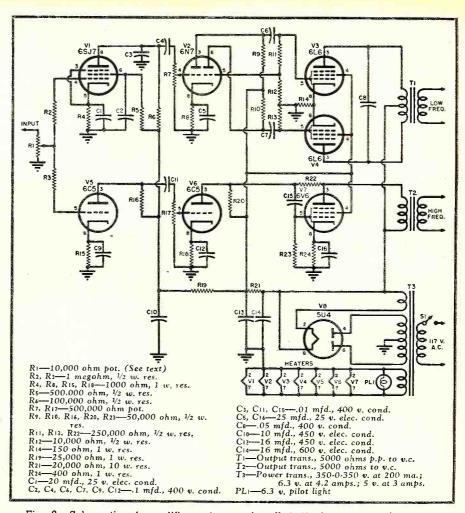
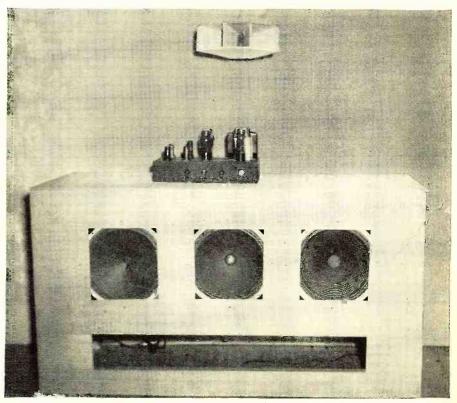
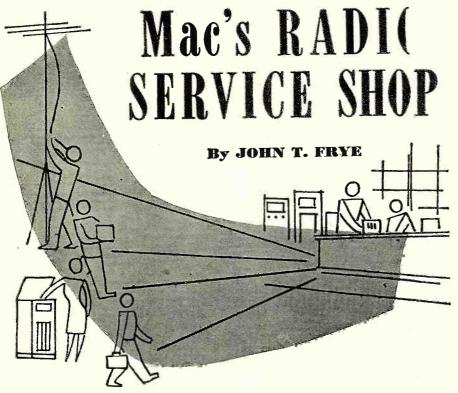


Fig. 2. Schematic of amplifier using push-pull 6L6's for the low frequency power amplifier, and a single 6V6 for the high frequency power amplifier. Values given are for a crossover frequency of approximately 1000 cycles per second.

A more elaborate 25 cu. foot enclosure housing three 12 inch speakers. The tweeter is coupled to small plywood horn mounted above low frequency enclosure.





BARNEY HAS A BIRTHDAY

ISS PERKINS, precisely at two minutes to nine, stepped inside Mac's Radio Service Shop ready to start another day as its very efficient office force. Before the door could close behind her she was pounced upon by a red-headed demon and swung dizzily about the office while the demon sang very lustily and slightly off-key, "Oh, waltz me around again, Matilda!"

"Barney Jameson, you let me go!" she gasped. "Let me down this instant!"

After one last wild swing, Barney obediently deposited her on her desk, her hat tilted rakishly over one eye, and her horn-rimmed spectacles far down on her sharp little nose.

"What on earth is the matter with you?" she demanded, her hands fluttering about trying to repair the damage.

"It's my birthday, Matilda—I mean, Miss Perkins," Barney explained with such a dazzling smile that she could not resist smiling back just a little.

"And that, when you remember that our assistant is a wild young Irishman, should explain everything," Mac said with a chuckle from where he had been watching in the open door of the service department. "Well, my young bucko, you come on back here. I have a birthday present for you."

Winking and leering wickedly over his shoulder at Miss Perkins, Barney made a dash and slid through the door into the service department.

"Where it is? Where's the present?" he demanded.

"Right there," Mac replied, waving at the service bench. "Starting today,

you are going to do some trouble-shooting."

"Honest, Boss?" Barney asked happily. "You mean you are really going to let me show you how much I have learned out of those books I've been beating my brains out on?"

"How much or how little," Mac said dryly. "First, though, I want to brief you a little on procedure. To begin with, there is the matter of testing tubes. The roller chart on the checker shows you how to set each control for a particular tube. Always set up the controls and then double-check the settings before you stick a tube in the testor."

"That's to keep from burning out a filament, I presume," Barney said airily.

"You presume right, and another thing toward the same end is to arrange the tubes to be checked in this tray so that those with the lowest filament voltages are on the left and the filament voltages are progressively higher as you go toward the right. For instance, you might have a couple of 6SS7's, a 12SA7, a 12SQ7, a 35Z5 and a 50L6 laid out in that order. If you checked from left to right, you would run no danger of putting a tube in the tester with too high a filamentvoltage setting, for every change necessary in this control is toward a higher setting."

"Check and double-check," Barney said, making a circle out of his thumb and forefinger.

"Don't forget to adjust the line voltage on the checker, either," Mac admonished. "Do it with a tube plugged in."

"Do I have to check the line-voltage for each tube?"

"Ordinarily, no. Adjust it with the first tube in the checker and let it alone for the rest; however, when testing a tube with a heavy filament current, such as an 83, you may have to boost it up a little."

"I've got it," Barney stated. "If the hand goes into the green, I stick the tube back in the set; if it stays in the red, I throw the tube away; and if it stops in that little orange space, I toss a coin to see whether I throw the tube away or use it."

"It's not quite that simple," Mac said with a grin. "In the first place, you check all the elements for shorts by throwing these switches and watching the neon lamp. While making this test, you keep tapping the tube with this little rubber hammer; and don't let me catch you hitting it as though you were trying to drive a tent-stake," he warned, trying to scowl fiercely.

"Okay, Boss, okay!" Barney replied, holding his arms up as though warding off an expected blow. "I'll see you don't catch me."

"Don't just strike the tubes on top. Tap them first on one side and then on the other," Mac went on. "Don't neglect to check each section of multipurpose tubes separately."

"What do I do with those that read 'doubtful'?" Barney asked.

"I usually leave that up to the customer. Of course, if a new tube makes a noticeable difference, I replace the old one; but often this is not the case. Usually, though, the customer will tell you to discard the doubtful ones."

"And now let's talk about the service bench," Mac went on. "For the present, you will not use the scope, the signal tracer, or the vacuum-tube voltmeter. Those belong in the high school of radio servicing, and you are still in the grades. The signal generator and the multimeter there are your trouble-shooting weapons, and they are capable of telling you a lot more about what is wrong with a radio than you will be able to understand."

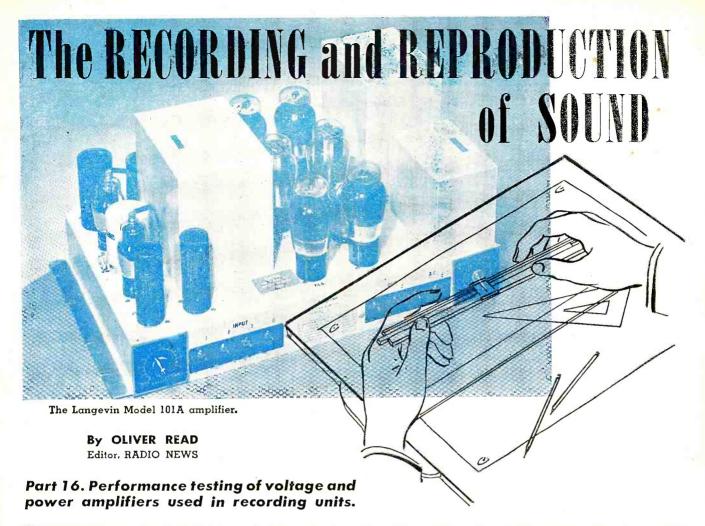
"Such cruel, cutting words—and on my birthday, too!" Barney muttered darkly.

"You will hear a lot worse words if you damage that meter," Mac warned. "Take a good long look at it. Notice how straight that pointer is. See how snugly it hugs zero. Watch how smoothly it swings. Mind that it stays that way."

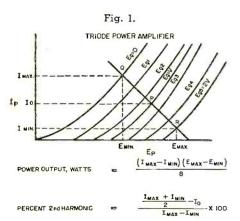
"Do you have any helpful suggestions—as though I didn't know," Barney said sweetly.

"Plenty of 'em. For one thing, while checking receiver voltages in general, stay on the five-hundred-volt range. With that big scale, you can easily read it down to five volts. Most receiver voltages will not go much beyond half-scale, and if you happen to get the polarity reversed—and this should not happen often if you watch what you are doing—you are not likely to bend the pointer."

(Continued on page 126)



MPLIFIERS may be divided into two classifications, i.e., voltage amplifiers and power amplifiers. A voltage amplifier is an amplifier which is intended to deliver a large alternating voltage into a high resistance load. The



power amplifier is designed to deliver appreciable power and may or may not require power to drive the grid circuit.

Amplifiers are also divided according to their method of operation into class A, class AB, class B, and class C amplifiers. In a class A amplifier the plate current is a faithful reproduction of the waveform of the applied grid voltage over a

complete cycle; in a class AB amplifier this is the case for more than 180 degrees but less than 360 degrees; in a class B amplifier for only 180 degrees and in a class C amplifier for less than 180 degrees.

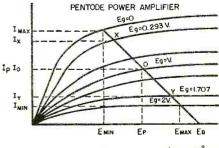
Multi-stage amplifiers generally consist of several stages of voltage amplification followed by one or more stages of power amplification. The total amplification is limited by miscellaneous noises such as thermal agitation and shot effect which occur in the first stage and are amplified along with the signal. When the amplification becomes so great that these noises become a large part of the output, the amplifier becomes useless. Therefore, it is necessary to keep the noise down, especially in the first stage. Operating the units at lower voltages and using special tubes are some of the remedies employed.

In multi-stage design it is important to proportion the stages so that none of the early stages can become overloaded before maximum output is obtained in later stages. Such a condition may occur if the volume control is placed in the second stage and the input device delivers more voltage than the bias of the first stage. Placing the volume control in a later stage will make

the condition worse unless the amplifier is to be used for only one input device of very low output. In general, it is best to put the volume control in the earliest possible stage and to place tubes with low bias and high gain first.

A tube used as a voltage amplifier delivers maximum amplification (equal to mu) if the a.c. load is infinite and the actual plate voltage remains at the rated value. The gain drops with the plate load and with the plate voltage,

Fig. 2.



POWER OUTPUT, WATTS = $\frac{\left[I_{MAX}-I_{MIN}+1.41\left(I_{X}-I_{Y}\right)\right]^{2}R_{P}}{32}$

ERCENT 2nd HARMONIC =
$$\frac{I_{MAX} + I_{MIN} - 2I_{0}}{I_{MAX} - I_{MIN} + 1.41 (I_{X} - I_{Y})} \times 100$$

PERCENT 3rd HARMONIC =
$$\frac{I_{MAX}-I_{MIN}-I.4I\left(I_{X}-I_{Y}\right)}{I_{MAX}-I_{MIN}+I.4I\left(I_{X}-I_{Y}\right)} \times 100$$

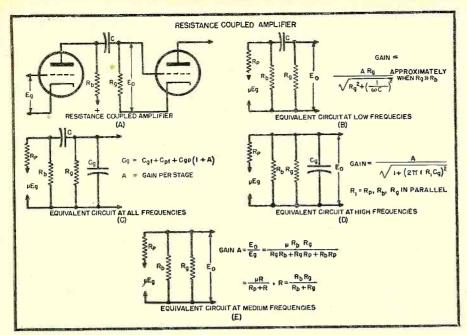


Fig. 3.

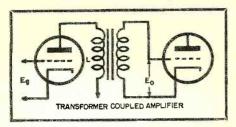


Fig. 4.

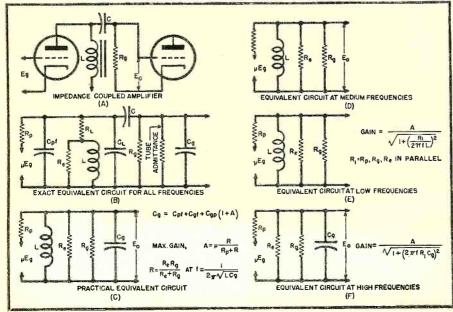
so that the best compromise of plate load and plate voltage must be determined. Other problems, such as parallel capacitance, must be taken into consideration.

The obtainable gain and the maximum output as well as the distortion of any tube can be determined for any load and power supply by a geometrical construction on the plate family of curves

When the a.c. load is different from the d.c. load, a load line should first be drawn corresponding in slope to the d.c. load and starting from the plate voltage point on the X axis. At the chosen operating point the real load line should be

(Ep-Ip curves). When the load has the same a.c. and d.c. resistance, the load line is drawn from the plate supply point on the X axis at a slope equal to 1/R or I/E, taking into consideration the scale of units employed along the coordinate axes. An operating point is then selected, representing the fixed grid bias; variations in plate current and plate voltage for any grid voltage can then be read. The load should be so selected that the intersections of grid voltage lines are regularly spaced.

Fig. 5.



constructed at a slope corresponding to the a.c. load resistance. Maximum output and gain are immediately apparent from the curves.

Power Amplifiers

Maximum undistorted output is obtained from triodes when the load equals 2Rp, for pentodes when the load is approximately 1/5th Rp. The performance as a single-ended class A amplifier can be predicted from the Ep-Ip curves as shown in the example in Fig. 1. Draw the load line through the chosen operating point at the slope corresponding to the a.c. load (the d.c. resistance is usually negligible). For minimum distortion, the segments of the load line, PQ and PR should be equal. When the ratio of their respective lengths is 9:11, the harmonic distortion is five per-cent.

In Fig. 1 maximum power output and harmonic distortion is given in the equations. Fig. 2 gives the same data for pentodes. The gain of amplifiers is often given in decibels. The decibel is a logarithmic unit, expressing the ratio between two magnitudes of power. Mathematically:

db.=10 log
$$(P_1/P_2)$$

where P₁ and P₂ are the output and input power (in watts) respectively of the amplifier.

When the impedance at input and output are equal, the decibel may also be expressed in terms of voltages or currents:

db.=20 log
$$(E_1/E_2)$$

db.=20 log (I_1/I_2)

The decibel is used, in addition, as a unit of loss and gain in networks. Although the decibel is not an absolute unit of power level, it can be used to indicate the power level in decibels above or below an arbitrary "zero level." One of the most frequently employed zero levels is 6 milliwatts. In acoustical measurements a zero level of 10-16 watts per square cm. has been accepted.

Audio Amplifiers

Audio-frequency amplifiers may be divided according to their type of coupling into resistance-coupled amplifiers, transformer-coupled amplifiers, impedance-coupled amplifiers, and directcoupled amplifiers.

The charts of Figs. 3, 4, 5, and 6 show the fundamental circuits. Complete information on the constants for resistance-coupled amplifiers and their performance will be found in tube manuals.

Resistance-coupled amplifiers have the advantage of economy while the frequency response can be made nearly flat. The phase distortion is less than that of other types of coupling except direct coupling. Disadvantages include lower gain than impedance or transformer coupling with the same tubes and power supply and the tendency to "motorboating."

Impedance-coupled amplifiers have a lower voltage drop across the load, thus making the plate voltage higher. The frequency response falls off at the low end as well as at very high frequencies, above the point where parallel resonance occurs. The drop at the low end can be minimized by placing a resistor across the plate choke. If the value of the resistance is 1/3 of the choke reactance at the lowest frequency, or less, the impedance of the combination will not vary more than a few per-cent over the audio range.

At present, transformer-coupled triode amplifiers can be designed to have a frequency characteristic as good as that of a resistance-coupled amplifier. The gain of such amplifiers is not as high as that of the resistance-coupled amplifiers using pentode tubes, and the cost of the transformers is high. When sensitive amplifiers are used and a transformer is at the input, the hum problem is much greater than with RC amplifiers. Well shielded transformers are required and even then critical placing is necessary.

Direct coupling is really a special case of resistance coupling. In such circuits the plate of the first stage is directly connected to the grid of the next, a condition which requires some juggling with power supplies. Since the load between stages is a resistance and the coupling elements per stage are reduced, this type of amplifier can be made to have a better response than most other types. Response at low frequencies is better and delay distortion is less. The main difficulties are the tendency to drift due to temperature changes and the difficulty in designing amplifiers of many stages. It is possible, however, to make an amplifier employing a drift-corrector which makes the system practical for amplification of a.c. signals but not for d.c. Practical circuits for a single-ended amplifier and a push-pull amplifier are shown in Fig. 6,

Feedback

When a portion, B, of the output of an amplifier having a voltage amplification A, is fed back to the input, the gain becomes: A/(1-AB). In this case B is positive for regeneration and negative for degeneration. Non-linear distortion, noise, and hum will be multiplied by the factor: 1/(1-AB).

These equations hold when the feedback voltage is in series with the input signal and there are no additional phase shifts due to reactances.

Fig. 7 shows several ways of arranging the feedback circuit in transformer-coupled and resistance-coupled circuits. There is a phase shift of 180 degrees in each stage which should be taken into consideration; in addition, there is a phase shift in each stage which varies with frequency but is never more than 90 degrees. This fact limits the number

of stages to be bridged by the feedback circuit. When the sum of the shifts amounts to 180 degrees, oscillation starts unless the gain at that point is less than one. For this reason, degeneration is limited, as a rule, to three stages and to about 30 db.

Measuring Distortion in A.F. Amplifiers

The simplest qualitative test for distortion in a class A audio-frequency amplifier stage may be made, as shown in Fig. 8, by applying a signal voltage of proper level to the input and inspecting the circuit for one or all of the following abnormal conditions:

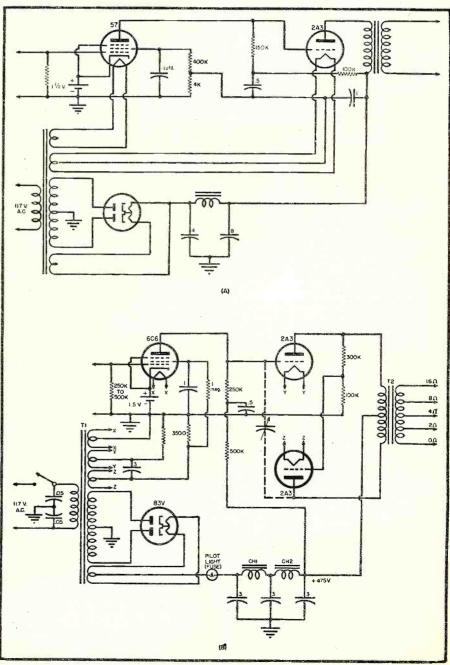
- (a) Presence of d.c. grid current.
- (b) Fluctuation of the d.c. plate current.
- (c) Fluctuation of the d.c. cathode

voltage, if the circuit employs cathode resistor bias.

Each of these indications generally occurs in a positive direction, and each will disappear upon removal of the signal. It must be borne in mind, however, that this method is purely rudimentary in nature and serves only to detect the presence of distortion. One or two of the indications may be absent, depending upon the main cause of the trouble.

The three simple indications are well known and frequently used by servicemen and p. a. testers who have no equipment suitable for making quantitative distortion measurements, but must, in the course of routine testing, localize distortion without reference to the actual per-cent harmonic energy present. (Continued on page 165)

Fig. 6.



REGULATED D.C. SUPPLY Improvements

By W. L. KINSELL

Senior Project Engineer Farnsworth Television & Radio Corp.

> Fig. 1. Special test equipment incorporating the regulated power supply in the bottom panel of the unit.



Theory and construction of a d.c. power supply with improved voltage regulation.

THE MOST common and simplest application of electronic tubes is in the conventional a.c. operated d.c. power supply. It is involved in nearly all electronic apparatus and the information needed for its design is well covered by all general radio engineering texts and handbooks in considerable detail.

When the functioning of equipment requires a stabilized low impedance

source of d.c. power, it is necessary to resort to the use of one of the varieties of electronically regulated d.c. power supply systems that have become so well-known and widely used within the past ten years. Much has been written on the principles involved and detailed instructions on the design of a system to supply any given voltage and current have been outlined. Since this is a subject that is at once relatively simple,

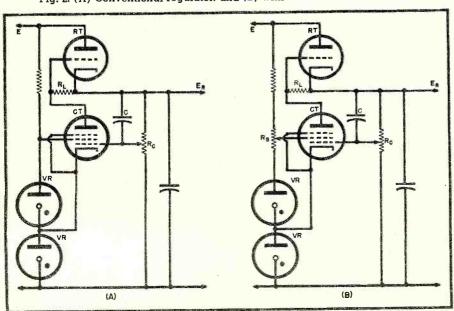
yet not entirely familiar to all individuals who may find themselves interested in or required to use regulated supplies in applications demanding their advantages, a bibliography is presented as an appendix to this paper that will provide the reader with both general and detailed coverage of the subject. RADIO NEWS readers will find M. S. Kay's article in the November 1944 issue to be very informative. Therefore, no space will be used here to cover the theory or describe the several varieties of regulated power supplies in use.

Present Deficiencies

For all applications where today's regulated power supplies fill the bill, no improvements would be necessary. However, as fine as these supplies are, there are already demands for supplies of improved characteristics.

For example, suppose the output voltage of such a system varies one-half of one per-cent as the line voltage fluctuates over short or long periods of time. This degree of stabilization is roughly representative of what may be expected of an average regulated supply. At 300 volts, the variation may approximate one or two volts. As with any performance, though this regulation may be entirely satisfactory for most applications, there is some equipment whose performance is limited solely by the stability of its power supply and there are new designs

Fig. 2. (A) Conventional regulator, and (B) with screen resistor Rs added.



of complex electronic apparatus that might be made successful if power supply stability could be improved. Therefore, we must not assume that the conventional regulated power supply, because it is such an improvement over the unregulated type, is all that it need be. This article will point out a method for bringing about this improvement that does not appear to have been developed previously.

In passing it should be pointed out that the aspect of voltage stabilization that is most annoying may be termed, for lack of a more standard term, "jitter". While it is important for a voltage stabilizer to iron out supply or line voltage drift, it may in some cases be even more important to reduce jitter caused by the line voltage transients that are so bad in some locations. It is quite common to observe the output voltage of a regulated supply jumping erratically twenty-five or fifty millivolts, oftentimes very sharply due to line voltage transients. While this is relatively good stabilization, such an effect can be very undesirable in some cases. The change to be described by this article will effectively reduce this phenomenon to a few per-cent of the usual value.

One of the other power supply characteristics for which this article will indicate improvement is that which is correctly known as "regulation". As the load on a power supply varies, its output voltage will also vary. As in the case of stabilizing the effects of line voltage fluctuations, the variations due to "regulation" when the load changes may run about one-half per-cent over the useful range, or one or two volts when delivering 300 volts. True, this is very small, but some of the complex applications we see in electronic equipment may be more successful and more may be possible if this also can be improved. This article will show the manner in which this may be done.

A slightly different expression for this latter characteristic is "internal impedance". If the output voltage of a supply did not vary as the load changes, it would be equivalent to a battery with zero resistance and we would say that it has zero internal impedance. Consequently the improvement to be described in regulation will reduce the internal impedance of the supply. An average value for a conventional supply may be five or ten ohms, without this further improvement.

One additional characteristic which may be improved by the method given by this article is hum voltage. While the hum on the output of a conventional regulated supply may measure five to ten millivolts and may be insignificant for many applications, it too is capable of improvement by the means to be described. Many occasions arise where ad-

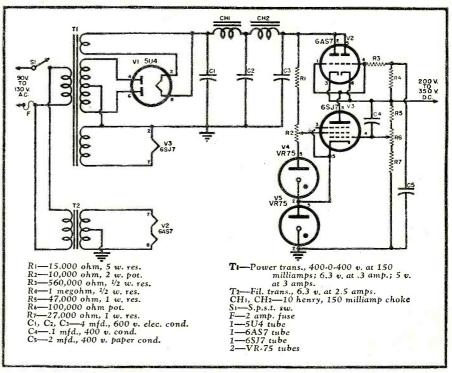


Fig. 3. Circuit diagram of a 100 milliampere regulated power supply.

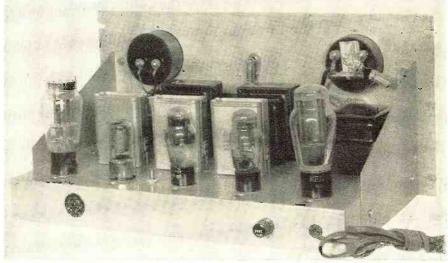
| | STABILI | ZATION | | | | |
|-------------------------|-----------|----------|--------|-------|-------------|--|
| POT SETTING | 0 | 1/4 | 1/2 | 3/4 | Max. | |
| Output Voltage Change | -1.1v | 6v | 0 | + .5v | | |
| (See Text) | -2.5v | -1.8v | -1.3v | 7v | 2v | |
| | REGUL | ATION | | | | |
| POT SETTING | 0 | 1/4 | 1/2 | 3/4 | Max. | |
| Output Voltage Change | -1.v | 75v | 35v | 0 | + .3v 8v | |
| (See Text) | -1.5v | -1.3 v | -1.1 v | -1. v | | |
| I | NTERNAL I | MPEDANCE | S . | | | |
| POT SETTING | 0 | 1/4 | 1/2 | 3/4 | Max | |
| Internal Impedance ohms | 40 | 30 | 14 | 0 | -12 | |

Table I. Performance data on the improved d.c. voltage regulator.

ditional filtering is necessary to reduce hum in circuits carrying low signal levels. The reduction of this hum by the means to be described is just as effective and probably cheaper.

(Continued on page 174)

Fig. 4. Rear view of the power supply chassis of unit shown in Fig. 1.



Conspiled by KENNETH R. BOORD

Monsieur Jean Pipon, head of the English Department of Radio Saigon, French Indo-China, on the March 16, 1947, special broadcast dedicated to readers of this department of RADIO NEWS:

"On a day in the summer of 1928, the Director of the French Radio-Electric Society, in his office in the Boulevard Haussman, Paris, sent for his commercial agent. A customer had just arrived from Saigon, who wanted to buy a 12-kw. short-wave broadcasting station. At that time, only the most important countries had such luxuries. The man must be mad-or, at best, a very poor joker! When inquiries were made, however, it was found that the man, Monsieur Joseph de la Pommeraye, was a 'serious' prospective customer, who, with a group of friends, wished to 'endow' French Indo-China with a powerful radio station. The commercial agent hastened to invite the gentleman to luncheon, and on this occasion learned of the forthcoming creation of the Franco-Indochinese Radio Company.

"Twelve months later, this company purchased a plot of ground at Chi-Hoa, on the outskirts of Saigon, and had buildings constructed there. Two engineers came from France, and also a fine orchestra—certainly the best that Indo-China had ever known, for of the seven musicians engaged, five were first-prize winners from the Paris Conservatory.

"On July 18, 1930, the first Radio Saigon broadcast took place, in the presence of the Governor-General, Monsieur Pasquier. From the very beginning, results were excellent (except within a radius of about 150 miles and in Cambodia). Considerable improvement was achieved by the addition of new aerials.

"Letters came in from the four corners of the globe, so to speak. Listeners everywhere showed their enthusiastic admiration for France's fine effort. In Indo-China, however, the population was not well-equipped to hear the new station's broadcasts. In 1930, there were only 108 radio sets in the entire country, and these were of the loudspeaker type.

"It was suggested that the Administration should have at least one radio

receiver installed in the public hall of every village. But, alas, nothing came of this idea, and what was worse, owing to the heavy expenses incurred, Radio Saigon was obliged to cease its transmissions on April 30, 1932. Letters of disappointment and protest poured in from all over the world. Yet in spite of various press campaigns, "The Voice of France in the Far East,' the name under which Radio Saigon was known to many hundreds of listeners, remained silent.

"In 1938, the matter was taken up in Paris and Indo-China, and these negotiations resulted in the formation of the Indochinese Broadcasting Com-



Pierre Crenesse, internationally famous war correspondent and France's most popular radio commentator, has arrived in New York to take up his new duties as director of the French Broadcasting System in the United States. Among his duties, Mr. Crenesse will have charge of exchange programs between France and the United States. The New York office is already servicing over 200 radio stations.

pany. In January 1939, the transmitting apparatus was taken from Chi-Hoa and was installed in Phu-Tho. The studios were set up temporarily at the Radio-Electric Centre in Saigon itself. In March 1939, French radio specialists arrived on the Air-France plane. Thanks to their valuable help, the first broadcast from the new studio was given at 0700 hours on April 1.

"We carried on under considerable difficulties. There were frequent breakdowns in the technical equipment, which we were still waiting patiently to have renewed, and we were particularly short of gramaphone records. Gradually then,

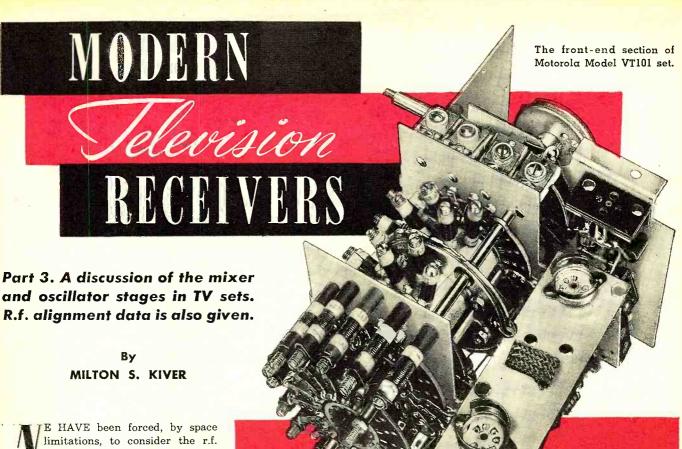
both equipment and recordings began to arrive. Broadcasters became more varied and daily transmissions were given in French, Cochinchinese, Tonkinese, English, Dutch, Cambodian, Chinese, and Siamese. A tremendous mail arrived with every boat; in fact, about 60 percent of the letters received bore foreign stamps.

"Then in September of 1939, war broke out in Europe. Radio Saigon found itself unable to continue as a private enterprise. Government aid was given and the 'Voice of France in the Far East' continued to be heard. Then came June 1940-and the Armistice! All telephonic and telegraphic communications with France were broken, and so Indo-China was unable to receive any firsthand news from France. However, listeners continued to hear three daily news bulletins. But they hardly realized the tremendous amount of work that was involved for the staff of the station and for the Radio Control Service. For a month, the head of this Service could not have had more than two or three hours sleep each night. Surrounded by contradictory reports and telegrams, he was continually listening-in-hoping to find out what was really happening in France. Meanwhile, more technical equipment had arrived and Radio Saigon could now be heard throughout the French Empire.

"When the Japanese first arrived in Indo-China, they were, of course, much concerned with the radio and tried their best to turn the station into a pro-Japanese affair. They somehow managed to 'drag' from a timorous Government rights of control over the station's broadcasts.

"But they met with stubborn Underground opposition—at least from some members of the staff. I could make a long story of my Homeric struggle with their censors and the system of code signals established with other Allied stations—but time does not permit. Everything went along more or less smoothly until March 9, 1945. That was the date of the Japanese 'con de force' which resulted in their overthrowing the French colonial government and taking full power.

(Continued on page 152)



section of the receiver in three separate articles. From the servicing viewpoint, in which we are primarily interested, the r.f. amplifier, oscillator, and mixer should be lumped together in one package and looked upon as a single operating unit. As we progress through the television receiver, we will find other stages which can be combined into distinct units until, at the conclusion, we will have converted the complex television receiver structure into seven distinct packages. Troubleshooting will then devolve into a system whereby we localize each defect to a certain unit and thereafter center our complete attention on this unit until the defect has been found. In this article we conclude the r.f. package with an analysis of mixers and the alignment methods applicable to these stages.

Within the mixer of the television receiver, the received signal and the oscillator voltage both modulate the electron stream to form the desired audio and video i.f. voltages. Most radiomen have long been accustomed to pentagrid converters in this section of an AM receiver. Television sets, however, almost never use these tubes because of the proportionately large amount of noise voltage they generate plus the instability in oscillator frequency. Oscillator operation becomes increasingly critical with frequency and it is best to provide separate tubes for the oscillator and mixer.

Miniature high-frequency triodes and pentodes appear to find equal application as mixers in current television re-June, 1948 ceivers. Incoming signals, at this point in the receiver, are extremely weak and all extraneous noise must be prevented from approaching signal strength. Triodes are superior to pentodes and the latter are superior to pentagrid converters because each element within a tube develops a certain amount of noise. In this respect, diodes would be the best tube of all to use, except that it is felt the amplification provided by triodes and pentodes outweigh whatever reduction in noise would result from the use of a diode.

The signal from the r.f. amplifier is transformer or impedance coupled to the mixer in nearly all circuits. The major exception to this occurs in the RCA quarter-wave transmission-line tuner. Here, a combination of link and capacitive coupling carries the signal over to the mixer tuning line. The oscillator voltage, in all sets, is transferred either by capacitive or inductive coupling. Andrea, DuMont, Industrial Television, Motorola, Belmont, Farnsworth, and United States Television employ capacitive coupling. Representative of this group is the circuit shown in Fig. 1. In all instances, the oscillator voltage is applied to the control grid of the mixer through a small 1-5 mmfd. condenser.

Inductive coupling is employed by RCA, Admiral, Philco, and General Electric. In the RCA tuner (which is also employed by Admiral), a single turn of link coupling is placed between the oscillator and mixer lines. See Part 2. In addition, the physical location of the two units is such as to also provide direct coupling.

The RCA tuning line differs considerably from the conventional circuit and hence merits additional attention. The grids of the twin triode mixer are fed in push-pull by both the signal and the oscillator and the i.f. voltages produced (by the heterodyne action) are in phase on the mixer plates, permitting the two plates to be connected in parallel. Unwanted signals of i.f. frequency that arrive at the converter grid in a push-pull manner are out of phase at the mixer plates. Since the plates are tied together, these signals are cancelled out.

A series-resonant circuit placed between the end of the mixer tuning line and ground prevents i.f. feedback in the mixer by grounding the grids for the i.f. frequency. They also function as a trap to reject all short-wave signals of i.f. frequency which arrive at the mixer grids in a push-push manner. Iron-core screws permit variation of the induc-

tance of selected coils in the quarterwave line for circuit alignment. A 10,000ohm resistor is effective on Channels 1 through 8 to broaden the response to the required 6.0 mc. On Channels 9 through 13, the resistor is unnecessary

because 6.0 mc. represents a smaller percentage of the total frequency and hence is easier to achieve with coils of the same O or less.

In General Electric television receivers, coupling between oscillator, r.f. amplifier, and mixer is accomplished inductively by placing all coils on the same form and in close proximity to each other. See Fig. 2. The plate coil of the r.f. amplifier is adjacent to the grid coil of the mixer. The oscillator coil is placed

> on the opposite side of the mixer grid coil. The oscillator and r.f. amplifier coils are located as far as possible in order to minimize radiation of the oscillator signal through the antenna system. A signal so radiated can have an injurious effect on any nearby television receiver, as indicated by the interference pattern obtained from the screen of a nearby set. See Fig. 4.

> In the particular arrangement employed in Fig. 2, adjustment of the bandwidth response is made by moving the plate coil closer to or farther away from the grid coil. Spreading or squeezing of the plate or grid coil turns, raises or lowers the resonant frequency.

> Philco receivers employ a turret tuner in which the r.f. amplifier input and antenna coils are wound on the same snap-in form. The output of the r.f. amplifier is inpedance coupled to the mixer. The mixer and oscillator coils are wound on a second snap-in form. On Channels 1 through 6, the coupling between oscillator and mixer is inductive; for Channels 7 to 13, capacitive coupling is added in order to obtain a greater transfer of oscillator voltage. The r.f. section of the Philco receiver has been previously shown.

> We have now a fairly comprehensive analysis of the frontend or r.f. section of current television receivers. Servicing techniques applicable to these stages have been covered in the first two articles of this series and little new need be added for the mixer stage. The three stages function as a group and what is true of one will generally apply to all. Of remaining interest is the alignment of these stages.

R.F. Circuit Alignment

Television circuits, in the front-end of the receiver, must be capable of passing a 6.0 mc. range of frequencies. In order to achieve this, overcoupling in the tuned circuits is resorted to and the usual r.f. response curve, then, has the appearance shown in Fig. 3. The over-coupling produces the dip in the center with a peak on either side. The dip should be no greater than 30 per

Table 1. A comparison of present-day television receivers. The chart below includes only those models which are on the market and which have been discussed in the articles thus far. As new models become available, they will be added to chart and adequate explanation of their operation given.

| Manufac- turer | Model No. | Picture Type | | Tube | | Model Type | | Tuning Method | | | | | |
|----------------------------------|--------------|-----------------|-------|---------------|----------------|---------------|---------|------------------|--------------------|----------------------|---------------------|------------------|--|
| | | Direct | Proj. | Size Diam. | Screen Size | Table | Console | Contin- uous | Selector Switch | R.F. Amp. | R.F. Osc. | Mixer | |
| Admiral | 30A14 | X | 0 | 10 | 6 x 8 | | X | | X | 6J6 ⁶ | 6J6 ⁶ | 6J6 ⁶ | |
| | 30A15 | X | | 10 | 6 x 8 | | X | | X | Same | Same as Model 30A14 | | |
| | 30A16 | X | | 10 | 6 x 8 | | X | | X | Same | Same as Model 30A14 | | |
| Andrea | T-VJ12 | X | | 12 | 7½x10 | X | | | X^1 | 6J6 | 6J6 | 6AG5 | |
| | C-VJ12 | X | | 12 | 7½x10 | | X | | X^1 | Same as Model T-VJ12 | | | |
| | CO-VJ12 | X | | 12 | 7⅓x10 | | X | | X1 | Same as Model T-VJ12 | | | |
| Belmont | 21A21 | X | | 7 | 5½x 4¼ | X | | X | | 6AK5 | 6C4 | 6AK | |
| Du Mont | RA-101 | X | | S | ee Note 4 | | X | X | | 6J6 | 6J6 | 6AK5 | |
| | RA-102 | X | | 12 | 7½x10 | | X | X | | 6J6 | 6J6 | 6AK | |
| | RA-103 | X | | 12 | 7½x10 | No | te 5 | X | | 6J6 | 6J6 | 6AK | |
| Farnsworth | GV-260 | X | | 10 | 6 x 8 | X | | | X | 6BA6 | ½-6J6 | 6AG5 | |
| | 801 | X | į, | 10 | 6 x 8 | | X | | X | 6AU6 | ½-7F8 | ½-7F | |
| General Electric | 802 | X | | 10 | 6 x 8 | | X | | X | San | ne as Model | 801 | |
| Industrial Television Inc. | IT3R . | х | | See Note 3 X7 | | | | 6J6 | 6J6 | 6AK | | | |
| Motorola | VT71 | X | | 7 | 4½x 6 | X | | | X | ½-7F8 | ½-7F8 | ½-7F | |
| | VT101 | X | | 10 | 63/8× 81/2 | | X | | X | 6AG5 | ½-6J6 | ½-6J | |
| | 48-1000 | X | Ÿ | 10 | 6 x 8 | X | | | X | 6AG5 | 6J6 | 6AG | |
| Philco | 48-1050 | X | | 10 | 6 x 8 | | X | | X | Same | as Model 4 | 3-1000 | |
| | 48-2500 | | X | . 5 | 15 x20 | | X | | X | 6AG5 | 6J6 | 6AG5 | |
| | 621TS | X | | 7 | 4½x 55/8 | X | | | X | 6J6 | 6J6 | 6J6 | |
| | 630TS | X | | 10 | 63%x 8½ | X | | | X | 6J6 | 6J6 | 6.16 | |
| RCA | 721TS | X | | 10 | 63/8x 81/2 | X | | | X | 6J6 | 6J6 | 6J6 | |
| | 630TCS | X | . 7 | 10 | 63/8x 81/2 | | X | | X | Same as Model 630TS | | | |
| | 721TCS | X | 0 | 10 | 63/8x 81/2 | | X | | X | Same as Model 721TS | | | |
| | 730TV1 | X | | 10 | 63/8x 81/2 | | X | | X | Same as Model 721TS | | | |
| | 730TV2 | X | 12 | 10 | 63/8x 81/2 | | X | | X | Same as Model 721TS | | | |
| | 641TV | X | | 10 | 63/8 x 81/2 | | X | | X | 6J6 | 6J6 | 6J6 | |
| | 8TS30 | X | | 10 | 63/8x 81/2 | X | | | X | Same as Model 630TS | | 30TS | |
| | 648PTK | | X | 5 | 15 x20 | | X | | X | 6J6 | 6J6 | 6J6 | |
| | T-502 | X | | 10 | 6 x 8 | | X | | X | 6AG5 | 6AK5 | 6AK5 | |
| United | T-507 | | X | 5 | 21 x16 | | X | | X^2 | 6AG5 | 6AK5 | 6AK5 | |
| United States Television | T-525 | | X | 5 | 25 x19 | | X | | X^2 | Same | Same as Model T-507 | | |
| | T-530 | | X | 5 | 30 x22½ | | X | | X^2 | Same | Same as Model T-507 | | |
| | T-621 | | X | 5 | 22¼x16¼ | | X | | X^2 | Same as Model T-507 | | | |

¹The Andrea receivers employ a tuner "turret" which is somewhat similar to the Philco tuner except that all 13 channels are wired into position. The r.f., mixer, and oscillator tubes, with their circuit components, are also contained within the copperplated steel case. This reduces reradiation and protects the circuits from external fields.

The r.f. tuning circuits of U.S.T. receivers closely resemble those employed in G.E. receivers. See explanation in Part 1 of this series.

¹Industrial Television receivers are designed solely for commercial use. The picture tube is housed separately and controlled by a control unit located some distance away. Picture sizes can range from 6x8 inches for a 10-inch diameter tube to 12½x17½ inches for a 20-inch diameter tube.

¹The set appears in six different style cabinets: Hampshire, Sherwood, Westminster, Revere, Plymouth, and Devonshire. Differences between models are in the size of the cathode-ray tube. The Hampshire and Westminster use a 20-inch tube; the other four models use a 15-inch diameter tube.

¹This model receiver is available in three types of cabinets, two of which are table models and one is a console.

console.

6Models 30A14, 30A15, and 30A16 employ an r.f. end section which is very similar to the RCA front end

system.

Industrial Television employs the "Inductuner" in an arrangement similar to that found in DuMont receivers

cent of the maximum amplitude of the curve. If the dip exceeds 30 per-cent, the coupling is too tight and should be loosened somewhat. The audio and video carriers are placed within 90 per-cent of the maximum amplitude.

The equipment needed to properly align the r.f. stages include:

- 1. A sweep signal generator with a center-frequency range from 44 to 216 mc. and a maximum sweep of 10 mc.
- An AM signal generator capable of providing frequencies from 44 to 216 mc.
 - 3. An oscilloscope.
 - 4. A vacuum-tube voltmeter.

In the order of receiver alignment, the r.f. stages are the last ones adjusted. However, we are concerned only with these stages at the moment and we will assume that the video i.f. and audio i.f. circuits have already been adjusted. When the analysis reaches these particular sections of the receiver, a full discussion of their alignment procedure will then be given.

The order of alignment within the r.f. section varies with the manufacturer. Some start with the oscillator and then align the r.f. tuning circuits. Others suggest that the process commence at the r.f. circuits, leaving the oscillator for last. In most cases it makes little difference which is taken first, so let us begin with the oscillator.

In every set, the oscillator must be precisely set to each of thirteen frequencies, one for each channel.* There are three possible ways to accomplish this adjustment.

- Apply a signal at the r.f. sound carrier frequency and note the indication at the FM detector output.
- Check the oscillator frequency directly against the known frequency of a separate signal generator, noting the indication on an oscilloscope.
- 3. Using a sweep generator, a marker signal, and an oscilloscope.

Method No. 1

The application of Method No. 1 will depend upon whether the set is using a Foster-Seeley discriminator, a balanced ratio detector, or an unbalanced ratio detector.

a. Foster-Seeley Discriminator. In this type of detector, the output is zero when the signal reaching it is exactly at the i.f. value. Connect an AM signal generator to the antenna terminals of the receiver and set it to the sound carrier frequency of some channel, say 13. This is 215.75 mc. Connect a vacuum-tube voltmeter across the full discriminator output, as shown in Fig 5A. Set the receiver selector switch to channel 13. Now vary the oscillator tu ing adjustment for this channel until the meter reads zero. The voltage polarity will be positive on one side of this zero point June, 1948

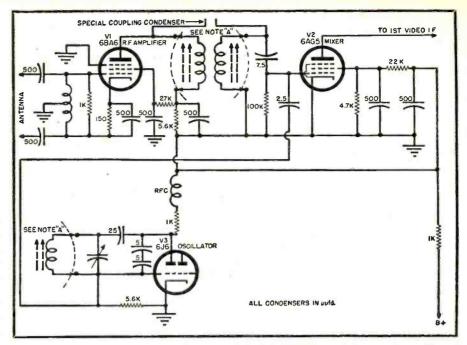


Fig. 1. The r.f. section of the Farnsworth Model GV-260 television receiver. The special coupling condenser consists of two short sections of wire over which has been placed a length of spaghetti. Adjustment is made by varying the distance between the ends of the wires. Note "A". An eight position rotary switch that switches in different coils for each of the available television channels.

and negative on the other. Each channel is adjusted, in turn. Whether we start with Channel 1 or Channel 13 will depend upon the design of the receiver. In RCA sets, for example, we must start with Channel 13 because each lower channel is dependent upon the setting of each higher channel. When the coils are independent of each other (as in most circuits), then the starting channel is immaterial.

b. Balanced Ratio Detector. A balanced ratio detector is shown in Fig 5B. Connect the vacuum-tube voltmeter between point A and ground. Connect the AM signal generator to the antenna terminals of the set and set it for the sound r.f. carrier of the desired channel, again say 13. Place the receiver on the same channel. Now adjust the oscillator coil for this channel until the meter reads zero. The same procedure is followed for all channels. Always be certain that the receiver selector switch is set to the channel being adjusted.

c. Unbalanced Ratio Detector. An unbalanced ratio detector is shown in Fig 5C. Connect a vacuum-tube voltmeter between point B and ground. The AM signal generator is connected to the receiver input terminals, using the same frequencies noted previously. The oscillator tuning adjustments are now set for maximum voltage on the vacuum-tube voltmeter. A similar procedure is followed for each of the thirteen channels.

In each instance, the incoming signal

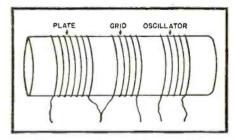


Fig. 2. The plate, oscillator, and mixer grid coils are all placed on a common form in General Electric video receivers.

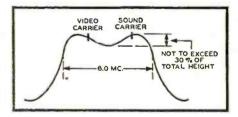
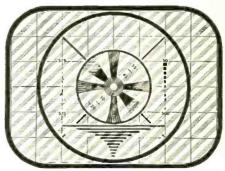


Fig. 3. This is the form of the r.f. response curve for most television receivers. Serviceman should recognize it.

Fig 4. The interference pattern produced on a video screen by other r.f. signals.



^{*}In any one community, the maximum number of assigned channels is seven. However, in order to make the above procedure universally applicable, all channels will be considered.

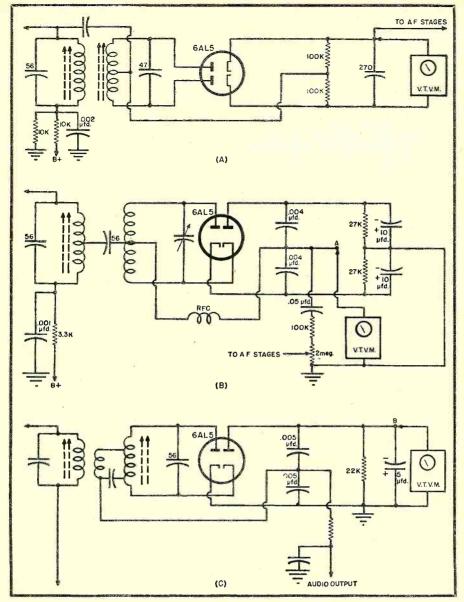


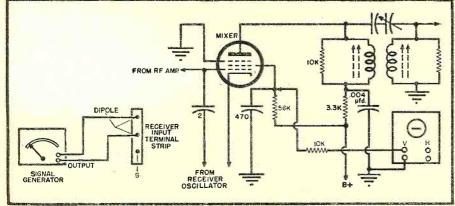
Fig. 5. (A) A Foster-Seeley discriminator as used in RCA television receivers. (B) A balanced ratio detector employed in Philos television receivers. (C) An unbalanced ratio detector similar to those found in Belmont and Motorola Model VT-71 sets.

mixes with the oscillator voltage, producing a difference or i.f. frequency. When the i.f. is at the proper frequency, the indications noted above will be obtained

Method No. 2

For the second method of checking the oscillator frequency, we connect the apparatus as shown in Fig. 6. The oscillator and signal generator voltages beat

Fig. 6. Connecting the test apparatus for Method No. 2 as described in text.



against each other and the beat signal is visible on the oscilloscope screen. The oscillator is adjusted until its frequency is equal to that of the signal generator. When this occurs, the difference beat frequency is zero and only a straight horizontal line is visible on the screen. Note that now the signal generator must be set to the oscillator frequency and not to the sound r.f. carrier frequency, as in Method No. 1. To compute this value, add the sound r.f. carrier frequency plus the sound i.f. Thus, for Channel A, a sound r.f. carrier frequency of 65.75 mc. and a sound i.f. of 21.25 mc. will result in an oscillator frequency of 87 mc. Hence, the calibrating AM generator should be set to 87.00 mc. for this channel. For other channels the value would naturally be dif-

The vertical input terminals of the oscilloscope are shown attached to the junction of the screen bypass condenser and screen dropping resistor. When the mixer is a triode, the oscilloscope should be connected to the junction of the plate dropping resistor and the plate bypass condenser.

Method No. 3

In this third method, we require a sweep signal generator, an AM signal generator and an oscilloscope. Connect the oscilloscope to the grid of the first audio amplifier. (The volume control should be turned completely clockwise, for maximum output.) Connect the sweep and AM signal generators to the input terminals of the receiver. (50mmfd. isolating condensers in the leads of both signal generators.) Set the receiver controls for the desired channel and adjust the sweep generator so that it sweeps across this channel. The AM signal generator is set at the frequency of the sound r.f. carrier for this channel. The response pattern obtained on the screen will appear as shown in Fig. 7. Somewhere along this curve will be a pip, produced by the AM signal generator. The receiver oscillator coil is now adjusted until the pip falls exactly in the center of the linear section of the FM detector curve.

This latter method of alignment is applicable to all television receivers since all FM detectors possess essentially the same S-shaped response curve.

When a "Fine-Tuning" control is available, it is placed at mid-position and kept there throughout the alignment of the r.f. amplifier, mixer, and oscillator stages.

Input and R.F. Circuit Alignment

For the r.f. and mixer tuning circuits, we require a response curve on all channels similar to the one shown in Fig 3. At the higher channels, Nos. 7 through

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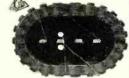
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| | | Osci | llator | R.F. Ampli | R.F. Amplifier & Mixer | | Order of | |
|-----------------------------------|--|-------------------------------------|---|-------------------------------------|--------------------------------|---------------------|--|--|
| Manufac- turer | Model No. | Mfg. Recom- mended Methods | Other Methods Applicable | Mfg. Recom- mended Methods | Other Methods Applicable | Matching Network | Channel Alignment R.F., Osc. and Mixer | |
| | 30A14 | 1a or 2 | 3 | A | В | | | |
| Admiral | 30A15 | | Same as M | fodel 30A1 | 4 | Yes | Channel 13 | |
| | 30A16 | | | | | | | |
| | T-VJ12 | 1b | 2 and 3 | A | В | | | |
| Andrea | C-VJ12 | | 0 | | *** | Yes | Immaterial | |
| | CO-VJ12 | | Same as I | Model T-V | J12 | | | |
| Belmont | 21A21 | 3 | 1c and 2 | В | A | Yes | Note 1 | |
| | RA-101 | R.f. sec | tion of thes | e receiver | s is not to b | e aligned | | |
| Du Mont | RA-102 | In case | of difficulty | the Indu | ctuner assen | nbly is to | | |
| | RA-103 | turer. | | set and re | eturned to | manufac- | | |
| Farnsworth | GV-260 | 1a | 2 and 3 | A | В | None Required | Immaterial | |
| General | 801 | 1a | 2 and 3 | A | В | None | | |
| Electric | 802 | | Same as | Model 801 | | Required | Immaterial | |
| Industrial Television, Inc. | IT3R | In case | R.f. section of these receivers is not to be a by men in the field. In case of difficulty, the Inductuner assemble removed from set and returned to maturer. | | | | | |
| Motorola | VT71 | 2 | 1c and 3 | A | В | Yes | Channel 1 | |
| | VT101 | 1a | 2 and 3 | В | A | Yes | Immaterial | |
| | 48-1000 | 1b | 2 and 3 | В | A | | | |
| Philco | 48-1050 48-2500 | | Same as Mo | odel 48-10 | 00 | None Required | Note 2 | |
| | 621TS | la or 2 | 3 | A | В | | | |
| RCA | 630TS 721TS 630TCS 721TCS 730TV1 730TV2 641TV 8TS30 648PTK | r.f. tun | ll R C A Television reteivers use same f. tuner and all are aligned in the me manner. | | | Yes | Channel 13 | |
| | T-502 | 3 | 1a and 2 | В | A | | | |
| United States Television | T-507 T-525 T-530 T-621 | same typ | nodels listed e of r.f. tun same man | er and all | ntially the are align- | Yes | Immaterial | |

NOTES

The Belmont receiver employs continuous tuning and therefore the r.f., oscillator, and mixer tuning circuit adjustments are similar to those made on low-frequency AM sets where continuous tuning is likewise employed. The six lower television channels are tuned by one set of coils and the upper seven channels by another. For each set, the turn spacing of a coil is adjusted at the low end of that band and a trimmer condenser adjusted at the ligh end to insure tracking over the entire band. The R.F. and mixer circuits of Philco receivers require alignment only on channel 10. Once the two trimmer condenser adjustments have been accurately set, all other channels will automatically fail into proper position.

Table 2. Table shows manufacturers' prefered method of aligning TV receivers.

13, the 6.0 mc. bandpass is easier to achieve and the overcoupling between coils is not so marked. In the Farnsworth Model GV-260 receiver, the recommended response characteristic for Channels 7 through 13 is shown in Fig. 8A. For G.E. receivers, the recommended response curve is shown in Fig 8B. These are variations that will be encountered among the various receivers on the market. During alignment, compare the response curves obtained with those recommended by the manufacturer in his service bulletin. If no curves are given in the bulletin, adjust the circuit until those shown in Fig. 3 are obtained. After the alignment is completed, examine the test pattern received from a local station. All vertical wedges should be visible up to at least 250 or 300 lines. Detail should stand out clearly. If the picture is fuzzy, readjust the input and r.f. coils, watching the test pattern until it is as clear and sharp as possible. An "air-check" should be run on every receiver before it leaves the shop.

In the response curve of Fig. 8B, the high-frequency end is peaked more than the low-frequency end. This is done purposely in this receiver to offset losses suffered by the high-frequency signals when passing through the set.

Alignment of the input and r.f. stages can be achieved by either of two methods, and each is applicable to all television receivers. In Table 2, the manufacturer's preference is indicated together with all applicable methods.

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|---------------------------------|---------------------------------|---------------------------------|---------------------------------|---------------------------------|--------------------------|--|---------------------------------|---------------------------------|--------------------------|---------------------------------|-------------------|
| 413 414 415 416 418 | 422 423 424 425 426 | 430 431 433 434 435 | 438 440 441 442 443 | 446 447 448 451 453 | 459 462 466 468 | 470 472 473 474 475 477 | 481 483 484 485 487 | 491 492 493 494 495 | 498 501 502 503 | 507 508 509 511 512 | 518 519 522 |

I.F. Frequency Standards

| | | ke | |
|---------|---------|---------|-----|
| 450 | 454.166 | 461.111 | FIN |
| 451.388 | 455.556 | 464.815 | |
| 452.777 | 459.259 | 465.277 | |

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| 2125 | 2282 | 2415 | 2557 | 3510 | |
| 2145 | 2300 | 2430 | 3202 | 3520 | |
| 2155 | 2305 | 2435 | 3215 | 3550 | |
| 2220 | 2320 | 2442 | 3237 | 3570 | |
| 2220 | 2020 | | | 3580 | |
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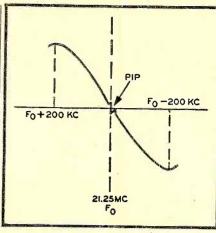


Fig. 7. The S-curve obtained at the output of an FM detector.

One further point before we discuss the two methods. When the sweep generator is connected to the input of the receiver for alignment of the input and r.f. circuits, check with the manufacturer's data to determine whether a resistive matching network should be inserted between the generator and the set. In some sets, it makes no visible difference in the response curves whether or not the generator output is matched to the receiver input; in others it does. When information concerning the manufacturers' preferences are not available, it is best to match the signal generator output to the receiver input.

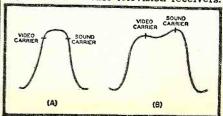
Matching the generator to the receiver input terminals can be accomplished by means of the resistor network shown in Fig. 9. The values for resistors A, B, and C are determined as follows:

- Resistor A is made equal to the stated output impedance of the generator.
- 2. A+B+C should equal the stated receiver input as closely as possible.
- 3. B and C should be equal to each other.

To illustrate the use of these rules, let us suppose that the stated output for a sweep generator is 30-ohms. Resistor A, then, would be 30-ohms, The receiver input is 300-ohms, requiring that resistors B and C each be 135 ohms. (300 minus 30 equals 270 and 270 decided by 2 equals 135 ohms.) Values as close as possible to these computed should be used.

(Continued on page 158)

Fig. 8. The r.f. response curves for channels 7 through 13 for (A) Farnsworth and (B) General Electric television receivers.



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| 12K7 GT | 3V4 | 50L6 GT | 6X5 GT | 7017 GT | 35B5 | 3Q4 | 6J5 | 6AT6 | 32L7 |
| 25Z6 GT | 6C5 | 6K7 GT | 6SA7 GT | 117L7 GT | 50B5 | 3\$4 | 6SJ7 | 6X4 | 12A8 |
| 6A7 | 12SA7 GT | 6A8 GT | 6SD7 GT | 117Z3 | IT4 | 1B4 | 12SJ7 | 6BJ6 | |
| 47 | LOCK T C.T | 5Y3 GT | 6SK7 GT | 12AT6 | IL4 | 12K8 | 6AJ5 | 6AK5 | |



COAXIAL 12" PM SPEAKER \$27.50 VALUE NET **\$12**95

Designed by one of America's fingst speaker, speaker, for FM high fideling in the \$500.00 bracket. Has 12" Ainico V PM with 4" built-in 'tweeter'. The bi-passifiter is built-in. Just hook on to any 8 ohn output transformer. Will take approximately 18 watts. This speaker, when we are offering a co-axis speaker at only \$12.95. Stock No. 4-12X. Weight 8 lbs. Only a few hundred available.

15" ALNICO SPEAKER \$19.95

JUKO BOX TYPE, JUMBO 15" PM speaker, with 1½", 8 olun voice coil. Ilas 21.5 oz. of Alnico V magnet. (Equal to 110 oz. of ordinary magnet material). This speaker is so finely tooled, it should sell for \$100.00. Designed for full base response, such as required of juke boxes, etc. Will take 20 watts average 30 watts peak audio power. Made by a nationally known speaker builder. Latest 1948 production. Individually cartoned, Weight . 1bs. Stock No. M2. Net \$19.95, 2 for \$38.00.

Heavy duty 12" PM speaker, with 12.1 oz. of Alnico V magnet. (Edual to 60 oz. of ordinary magnet material). Has 8 ohm voice coil. Will take 15 watts average or 22 watts peak audio power. Made by a nationally known speaker manufacturer. This is a fine speaker for all type of public address and radio set use. Good base and treble response. Latest 1948 production, individually cartoned, Weight ... lbs. Retail price \$25.00, Net \$9.95 each. Stock #2K1.

15" 1000 OHM FIELD \$13.95

Nationally known make—15" 1000 ohm speaker, 1½" 16 ohm voice coil. Will take 25 watts. Factory cartoned, fully guaranteed. Stock No. 15UZ

NET \$13.95, Two for......\$26.50

Popular P.M. Speakers

AT LESS THAN HALF PRICE EVERY SPEAKER GUARANTEED

| Alnico V, mag\$0.99 | |
|--------------------------------------|------|
| Amico v. mag | |
| 5 in. P.M. 1 oz. | |
| Alnico V. mag | |
| 5 in. P.M. 1.47 oz. Alnico V. mag \$ | 1.19 |
| 5 in P M 2 15 oz. Alnico V. mag | 1.49 |
| 6 in PM 1.47 oz. Alnico V. mag | 1.49 |
| 6 in. P.M. 2.15 oz. Alnico V. mag | 1.98 |
| 6 in. P.M. 3.16 oz. Alnico V. mag. | 2.95 |
| 8 in. P.M. 2.15 oz. Alnico V. mag | 2.95 |
| S in. P.M. 3.16 oz. Alnico V. Mag | 3.45 |
| 10 in. P.M. 20 oz. Alnico 3. mag | 4.45 |
| | 4 95 |
| 12 in P.M. 7 oz. Alnico V. mag | 0.05 |
| 12 in. P.M. 46 oz. Alnico 3. mag | 3.33 |

| | | SAVE | ON | FIL | ELD | 21 | rE. | ΑI | (1 | :K | 3 | | | |
|----|-----|-----------|--------------|--------|--------|-------|-----|-----|----|------|-----|-----|-----|-----|
| 4 | in | Dynamic. | 450 | ohm | field | | | | | | | | .\$ | 1.8 |
| 5 | in | Dynamic. | 450 | ohm | fie d | | | | | | | | | 1.8 |
| 5 | in. | Dynamic. | 1000 | ohm | field | | | | | | ٠. | | | 1.8 |
| 8 | in. | 2 ohm fie | ld fo | r hea | vy du | ity : | ant | 0 1 | a | tio | 1 | 18€ | ١. | 2.9 |
| 8 | in. | Dynamic. | 1000 | ohm | field | | | | | | | | | 2.9 |
| 12 | in. | Dynamic. | 1000 | olun | field | | | | | ٠. | ٠. | ~:· | | 4.9 |
| 12 | in. | RCA 450 | \mathbf{R} | eg. 10 |).00 r | iet : | 1/4 | " | Vo | 1 Ce | 9 (| 0 | 11 | |
| Se | COD | Price | | | | | | | | | | | | 4.5 |

SPEAKERS WITH OUTPUT ATTACHED

5 in. P.M. 1.47 oz. Alnico V. mag. with 50L6 output. Special \$1.49 in. P.M. 1.47 oz. Alnico V. mag. with Push-Pull output trans. Scop \$1.69 5½ in. G.E. P.M. Square with 50L6 output trans. mounts in place of regular 6 in. speaker. \$1.85 6 in. P.M. 1.47 Alnico V. magnet with 7000 ohm primary output trans. Special \$2.25 Heavy Duty 8" 450 Ohm Speaker with 6V6 output.\$2.95

POPULAR OVAL SPEAKERS

| | | | | | • |
|--------|--------|----------|-----------|-------|--------|
| 4x6 ir | . P.M. | 1.47 oz. | Alnico V | . mag | \$1.49 |
| 5x7 in | . P.M. | 2.15 oz. | Alnico V. | mag | 1.95 |
| 4×8 D | vnamie | 450 ohr | n field | | 1 95 |

VIBRATOR SCOOP \$1.99



June, 1948

Heavy Duty Vibrator—Made for 6-110 volt amplifiers, Freq. 60 CPS. Scoop price. \$1.99 135 ma 6-110 volt conventional power transformer, with all windings; will run phono motor. \$5.95 (Use with above vibrator)

WALNUT SPEAKER BAFFLE \$16.95

Walnut floor type speaker baffle. Size 12x22x26 inches. Will accommodate either 12 or 15 inch speakers. Air relief cut-outs in corner of grill. Weight 30 lbs. A \$25.00 value for only \$16.95. weight 30 lbs, A \$25.00 value for only \$16.95. Stock #L-25. Net \$16.95. Why not order one of less with any of the speakers listed in adiacent copy?

BIG SALE OF GENERAL ELECTRIC AUTO AERIALS

Genuine General Electric Auto Aerials, Individually factory cartoned All are made by Ward. This is a real scoop on autoaerials. Order a good supply now, and save from 50 to 75 cents, on these top quality aerials. G.E. Model UZA-006, same as Ward SC-6. Side covi 3 section 66", 36" shielded lead List \$4.95.

section 66" 36" shielded lead List \$4.95. \$2.49 Sale Price
G.E. Model UZA-007, same as Ward SC-8. Side cowl 4 section 100" 36" shielded lead List \$6.95
Sale Price
G.E. Model UZA-011, same as Ward TCF-3. Universal top-cowl mounting, 3 section 56". With 36" shielded lead. List \$5.35.
Sale Price
G.E. Model UZA-012, same as Ward DCF-3. 3 Section 56" fits all fenders, regardless of contour. Shielded lead. List \$6.25.
Sale Price
Sale Price __\$3.10 Sale Price

PORTABLE P.A.

18 watt complete portable public address system. Has inputs for a crystal or dynamic mike and phono pickup. Has push-pull 7C5 tube in output. Attractive leathers the covered split type cashes yetem wired ready to play. Stock No. RC-18. Net \$39.95. Priced complete with two system wired ready to play. Stock No. RC-18. Net \$39.95. Priced complete with crystal mike and desk stand.

\$59.50 VALUE MUSICAL AMPLIFIER WHILE THEY LAST \$19.95





8 watt musical amplifier, 4 tube AC type, linbuts for crystal or dynamic mike and phono or instrument picking. 2 gain controls and tone control. Has heavy duty built-in 8" speaker, Attractive leatheretic covered case. Made by a large manufacture to sell at \$59.95. Brand new, fully guaranteed, For 110 voit AC operation. Our scoop price, \$19.95. Stock No. C-LX. Contact instrument pick-up, \$6.95 extra. Deluve instrument pick-up; with volume control, \$8.95 extra. Crystal mike and desk stand \$4.95. Shipping weight, 20 lbs.



14-WATT AMP. \$29.95 THIS AMP. SHOULD **SELL FOR \$50.00**

SELL FOR \$50.00

Here is a high fidelity amplifer scoop we may never be able to offer again. Literature tory cartoned, 14 watt average output; 25 watt peak output. Matches 4-8-16 or 500 ohm line. Complete with tubes 68L7, 68N7, 2-128L7, 2-6V6gt and 5V3. Designed for 110 voit AC, 60 cycle operation. Frequency response 50 to 12,000 CPS. Hum level down 69 DB. Gain for two mikes and one phono pick-up. Eastern amplifer. Model E14A. except it has 2-6L6 output tubes, giving 30 watts output... Net \$44.95

TUBULAR ELECTROLYTICS

In paper tubes with pig tail leads

8 Mfd. 450 Volt Tubular... 59c each; 10 for \$ 4.50 8x8 Mfd. 450 Volt Tubular... 59c each; 10 for \$ 5.25 8x8 Mfd. 450 Volt Tubular... 49c each; 10 for \$ 4.50 50x30 Mfd. 150 Volt Tubular... 49c each; 10 for \$ 4.50 50x30 Mfd. 150 Volt Tubular... 49c each; 10 for \$ 4.25

75% OF ALL THE TUBES YOU USE 49c EACH

Guaranteed Standard Brands

| | Carton | ed and U | icartonec | |
|------------------|-----------|-----------|--------------|-----------------|
| 12AH7 | 6 K Z | 6S L.7 | 12S G 7 | 12SQ7 |
| 27 | 9001 | 6SN7 | 12SH7 | 12SR7 |
| 26 | 9002 | 68G7 | 12817 | 50L6 |
| 78 7 6 | 9003 | 6S R7 | 12SA7 | 128K7 |
| 76 | 1625 | 6V6 GT | 12SL7 | 25L6 GT |
| 384 | 6SA7 | 6X5 GT | 12SC7 | 35L6 GT |
| 5U4G | 6SC7 | 6A B7 | IT4 | 35 Z5 GT |
| 5Y3G | 6SF7 | 12AT6 | IR5 | 35W4 |
| 6AC7 | 6SQ7 | 12BA6 | 185 | 50B5 |
| 6C5 | 6SH7 | 12BE6 | 6R7 | |
| 6H6 | 6SJ7 | 12H6 | 6L7 | |
| 615 | 6SK7 | 12J5 GT | 7 Z 4 | |
| 59c each | 11/2 Volt | Octal-IN5 | GT. IH5 | GT, IA7 GT, |
| | | | | |

172 Voic Octai—183 61, 173 61, 173 61, 174 61, 175 61, 174 61, 175 61, 174 61, 175 61, 174 61, 175 61,

SCOOPLON NEW C.R. TURES

| Brand New Fully Guara | nteed |
|--------------------------------------|----------------|
| 3 API\$1.95 5 FP7 . | \$1.95 |
| 3 BPI 1.95 7 FP7 \$2. | 05 |
| 5 RP4—Has white screen; ideal for to | levision\$2.95 |

DETROLA CHANGER \$12.95 2 for \$25.00

Detrola Changer, Base size 11½x12 inches, \$12.95. Two for \$25.00. Aero Changer, Base size 12x13 inches, \$12.95. VM-800 Changer, Base size 13x14 inches, \$14.95



General Instrument changer, base size 10½x12", \$16.95. Seeburg, triple post, World's best, base size 14x14 inches, \$37.95. Made to fit leatherette bases for above changers, \$1.95. Specify type of changer for base.

REPLACEMENT MOTOR FOR CHANGER.....\$1.49

SMALL PHONO MOTOR. This 110 volt AC, 60 cycle phono motor is used on 80% of all automatic changers. Order one just to have around for replacement.

Scoop price, \$1.49; Two for.....\$2.79

WIRELESS RECORD PLAYER In Two Tone Plastic \$10.95

Nationally known wireless type record player, with RCA silent sapphire pick-up. Beautiful two tone plastic case. Self starting phono motor, with two tube tunable broadcast band phono oscillator, which easily fits under plasic base. Automatic switch turns on moror when pick-up arm is raised. Stock #3-RC.

1948 MODEL-MIKE-BROADCASTER

1948 MODEL—MIKE-BROADCASTER
ONLY \$7.95
Broadcasts 800 to 1500
KC from either a phonograph pick-up or a ctvsreal control of the property of t

3-TUBE PHONO. OSC. ONLY \$3.95



Model DE-4—Phonograph oscillator. Broadcasts from 800 to 1500 KC. Gain for 800 to 1500 KC. Gain for 800 crystal pick up. A new powerful circuit is used to assure plenty of power. Has variable gain control for proper modulation. Priced with tubes ready to operate, two 50B5 and 34W4. Model DE-4 Net.

SUPERHET BROADCAST TUNER for connection to phono amp. or P.A. system. Compact chassis 5x3½x3 inches. May be mounted inside the record player cabinet, Requires only three connections to ambifier.



cannet, Requires only three connections to amplifier. Uses 68A7 or 128A7; 68K7 or 128TA7 and crystal diode. Complete with tubes, loop antenna, dial and instructions for connecting to any amplifier. Net 87.95. Specify if tuner is to be used with AC or AC-DC type amplifier.

SEND 25% DEPOSIT,—BALANCE C. O. D. 1225 McGEE ST., KANSAS CITY, MISSOURI

RADIO COMPANY McGEE

WRITE FOR CATALOG Prices F.O.B. K.C.



BRAND NEW BC-645

9.95 TWO \$19.00

A small complete Transmitter and superhet receiver, for the 450 megacycle band. Diagrams for building AC Dower supply and conversion furnished, Ideal for MCW. CW or phone. The tubes (4-TF7, 4-TH7, 2-TE6, 2-6F6, 2-955 and WE-316A) are worth more than our sale price. BC-645 I.F.F. unit \$9.95 each, Two for \$19.00 Extra WE-316A tube 99c. 12 yolt DC dynamotor (furnished all power) \$2.95, BC-645 shipping weight 25 lbs.





Super value. Folded Di-pole antenna, for FM and Television. Complete with 60 feet of twin 300 ohm line and 4 low-loss stand-off insulators. This folded di-pole covers frequencies 42 through 108 megacycles. Trombone action makes exact tuning to any one weak station. Furnished with adjustable mounting bracket. Has 5 foot mast, Made for Stromberg-Carlson. Stock No. Mt-300—Net \$4.95. Weight 4 lbs. Individually packed.

OUR LEADER **FULL SIZE 3-WAY** PORTABLE RADIO



Full size 3 way portable radio. Operates on self contained 300 hour bat, or 110 volt AC - DC. Has 4 tubes plus disc, rectifier. A full superhet circuit. Attractive tan leatherete case. Made o sell for \$39.95 our price only \$22.95 weight 10 lb. Made by Nationally known mfg. 71/7-9, 90 pack bat. \$2.95.

"HOTTEST PICK ME UP RADIO IN AMERICA" NO TALLER THAN A PEN

NET EACH \$19.95 IN LOTS OF 3 \$58.50

Model 747—3 way personal radio, Receives broadcast 550 to 1650 KC. Small size only 4x5x8 inches. However, uses full size parts with 2-gang condenser and loop, Priced complete with 4 miniature tubes and disc rectifier. These sets are only slightly larger than the smallest personal radio, Volume tone like a big set. Kit of batteries \$2.05 extra.

Volume and



G.E. VARIABLE RELUC-TANCE PICK-UP.\$4.65

Scoop—Pre-amplifier for General Electric Variable Reluctance pick-up. Easily connected to any act or AC-DC amplifier. Wired and Tested with 68C7 or (128C7) tube. Diagram for connections is furnished. Specify whether you want pre-amplifier for AC or AC-DC use. Net price, Pre-amp, with Tube and G.E. Pick-up—\$6.95.

G.E. Variable reluctance pick-up cartridge with permanent needle. Net \$4.69.



kit Model J-41. Our leader record player kit. Fine tone, low needle scratch; includes two-tone leatherette covered portable case, rim-drive photo motor, high output crystal pick-up and 5" Alnico 5 PM speaker. 70L7 ready wired and tested amplifier. No wiring to do, just mount the parts in the case. Has the tone and volume

controls. Kit Model J-41

POWERFUL SINGLE RECORD PLAYER KIT Z-26.
Housed in an attractive leatherette covered cabinet.
Latest 78 RPM rim drive motor and light weight pickup. Ready wired and tested 701.7 type rube amplifier.
Tone and volume control. 5"
PMI speaker (Alnico V). This kit easily slips together. Priced complete with tubes and hook-up instructions. Kit Z-26. Net \$9.95



PARTS SALVAGE SCOOPS PACKARD BELL PRE-AMP \$1.99



Housed in a handy aluminum case 5x4x5, priced complete with tubes 6SL7, 7, has many usable parts. Relay and control PL68 plug and patch cord.



RELAY SCOOP \$2.95

Auto pilot amplifier salvage scoop. Has 6 high resistance relays that operate in tube plate circuits on less than 8 mills. Also 4 controls. Choke cond., etc. Less tubes. Used but in good condition. Weight 12 Stock No. C-IT. Net \$2.95; two for \$5.50.

AZMITH CONTROL 99c

A remote control for azimith indicators. Has toggle switch, miniature pilot lite and socket. Brand new, Type MN 52H, weight 2 lbs. Net 99 cents.

8-WATT AMPLI-FIER WITH P.P. 50 L6 \$7.95



BINGO AMPLIFIER \$13.95
Bingo Amplifier. We offer you the above push pull 5016 amplifier in a small leatherette case with 8-in buit-in speaker for only \$13.95. Ideal for paging and announcing. Stock No. BG-4. Weight 14 lbs. Crystal mike and stand, \$4.95.

SCOOP! 110 M.C. REC. \$7.95



BC-733 D Localizer Receiver
Freq. 108-110 Mc; Tube
complement; 10 tubes—1
128Q7, 2—128R7, 1—12A6,
1—AHIGT. 2—128G7, 3—
717A. Now only.... 57.95
NEW CONDITION
A RED HOT VALUE.

CARBON HAND MIKE, 99c



Army carbon hand mike with push-to-talk switch, cord and plug. Brand new and factory cartoned. While they last, 99c each; two for \$1.89; ten for \$6.90.

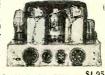
R-89 \$6.95
R-89/ARN-5 Glide Path
Receiver II tube superhet.
Formerly used for blind
I an d in g. Adaptable for
many uses. Receives 326 to
925 MC Contains the me.

18.0 d lng. Adaptable for many uses. Receives 326 to 335 MC. Contains six relays. 11 tubes 7-6435. 11 tubes 7-6435. A beautiful piece of equipment. Has three crystals. Priced complete with xtals and tubes. R-89/ARN-5 Used condition. Net. \$6.95

MODULATOR SALVAGE \$2.95

Another red hot value in salvage. All kinds of good usable parts in this unit. Con. Res. Relays, Modulation trans, and tubes VR 150. 1275 and 1625. Originally designed to modulate the BC-457 W. E. Transmitter. You can find many uses for this BC-456 Modulator scoop.

28V Dynamotor





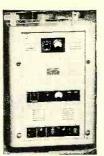
ANT CURRENT **METERS \$1.95**

Antenna Current Meter as used with the popular command transmitters. Has 0 to 10 2 inch. Thurmo coupled meter. Built in vacuum condenser. A scoop

Used \$1.95; two for..... New \$2.95; two for.....

PRICES KANSAS CITY

RCA M 2545



Ship board master amplifier. 23 tubes including 2 6L6 and other 6 volt type tubes. D B Meter. Built-in tube checker. Designed for 110 volts AC 60 cycle use. Has spare parts kit of trans and chokes. Only those who have worked with this amplifier will know its terrific value. Brand new with tubes, only \$139.50. Cost the gov. up in the thou-

POWER PACK SCOOP

Small power pack for 110 volt 60 cycle use. Produces 1.5 volt DC A voltage at 200 to 350 mil's. plus 100 volt DC B voltage at 25 mills. Convert 1.5 volt battery radios to 110 volts AC. Stock No. CV-1. Weight 4 lbs. Net \$3.95; two for \$7.50.

PORTA-POWER

POKIA-FOWEK
Electro Poeta Power. Converts any 4, 5, or 6 tube
1½ volt, 90 volt portable or
farm radio to 110 volt AC
operation. Multiple socket
arrangement makes easy,
quick connection possible.
Every shop should have one of these, Regular \$9.95
value. Scoop price



VEEDER ROOT METER



Counts number of feet of trailing wire antennae; number turns when winding on coil; applicable for many uses; beautiful bakelite case, jewelled dialite, pilot light enclosed, 3 position switch, counts up to 1000.

3" SELSYN INDICATOR Works on 16 to 25v. 60 cycle

Two for

EACH

\$4.45



ARC-4 \$14.95

IDEAL FOR 2 METERS Priced Complete With 20 Tubes—and 12-28 Volt Dynamotor

FOUR CHANNELS CRYSTAL CONTROLLED. ARC-4 for VHF frequencies 140 to 144 megacycles. There are 7 tubes in the transmitter: 832, two 1614, two 6V6 and two 6L6. The receiver section has 13 tubes: two 6AC7, four 6N7, three 12SJ7, two 12SQ7 and two 12A6. The unit is acqually two receivers and one transmitter in one piece. One receiver is for stand-by use. Has built on dynamotor for 12 or 24 volt DC operation. Priced complete with tubes and four crystals and dynamotor. Hams convert this for two meter operation. It's a scoop at this price. Used.



Crystal Calibrator \$2.95

Crystal Calibrator, gives 50 KC beat note through an Xtal synced, multivibrator, Furnished complete, less 200 KC Crystal, With tubes 128A7 and 2—128L7 A handy item to have. Scoop price...\$2.95



SCR-518 \$2950 ALTIMETER **Brand New**

Famous SCR 518 A Altimeter. Brand new factory cartoned. Worth over \$900.00. Made by RCA. Complete as pictured. Has 29 tubes, tured. Has 29 tubes tured. Has 29 tubes and 300.00 factor. Reads altitude up to 30.000 ft. Operates on 28 volts. D.C. Complete with tubes. 6SK7. 28012. 2 6SM7. 6C8. 6SN7, 6F8, 23D4. 6V6, 10 6AC7. 3 2X2, 954, 955, 956. 615 and 3 in. CR tube 1808P. A RED hot scoop at only \$29.95 complete.

15 SCOOP

BRAND NEW

BRAND NEW

AM 61A Indicator Amplifier.
Brand new factory cartoned. Has
28 volt DC Blower motor and
dan. 2 2mfd 1000 volt cond. 2
2X .5 mfd, 1000 volt cond. 2
2X .5 mfd, 1000 volt cond. and
many other parts. Complete with
15 tubes, 7 6SN7, 3 VR 105,
5Y3. 3 6SL7, 8016. As a salvage
item this is a RED Hot Buy. The
tubes are worth more than our
price. Weight 30 lbs. Net \$9,95



McGEE RADIO COMPANY

SEND 25% DEPOSIT-BALANCE C.O.D. 1225 McGEE ST., KANSAS CITY, MISSOURI RADIO NEWS

8-TUBE RADIO KIT WITH COAXIAL SPEAKER, \$37.95



A COMBINED BROADCAST SUPERHET RADIO CHASSIS AND 15 WATT P. A. SYSTEM HEAVY DUTY 12" P.M. SPEAKER CROW 8" SLIDE RULE DIAL, 2 GANG COND. REC. BROAD, 550 TO 1700 KC AND 19 TO 49 METERS PUSH PULL 6V6-TONE CONTROLS

INPUTS FOR CRYSTAL OR DYN. MIKES AND PHONO-PICKUP. WE FURNISH EVERYTHING TO BUILD THIS DELUXE CHASSIS

DETROLA CHASSIS \$16.95 Detrola Factory wired and tested

TO BUILD THIS DELUXE CHASSIS

WHY NOT ORDER THE ARMCHAIR CABINET
WITH THIS KIT

HAS INPUT GAIN FOR THE G.E. VARIABLE
RELUCTANCE PICKUP
C-CHASSIS SIZE 9/xxi1x8" HIGH
OCCUPATION OF THE G.E. VARIABLE
RESULTANCE PICKUP
Here is something new in radio. A real 15 wait power amplifier with bass and treble controls. Has extra gain stage
for crystal or dynamic mikes. And on the same chassis, a standard superhet radio receiver. We furnish all parts,
knobs, escutcheon plate and tubes: GSA7, GSN7, GSN7, GSN7, GSV7, GSV7, two GV6 and 5 V3. No cabinet, Extra care in
designing the power supply section assures low hum level, making this unit ideal for recording as well as schematic diagram and photos of the completed chassis. Weight 35 lbs.

PRK-24 Radio-Amp. Kit
with 12" P.M. speaker
With tubesNet

**PRE-24 Radio-Amp. Kit
with 12" P.M. speaker
With tubesNet

**PRE-25 Cinaudagraph wide range speaker. (Has builtin high frequency tweeter). This is our finest
kit

**WIDE DECORDED \$49.95

With tubesNet ARMCHAIR

CABINET \$29.95

Will House PRK-24 or CPR-15

4 TUBE RADIO

KIT \$6.95

3-WAY **PORTABLE KIT** \$16.95 • 4 Tubes Plus Disc Rectifier • 300 Hour Battery Pack Included

Beautifully
Built Portable

Case

or CPR-15

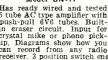
Beautifully made walnut armchair cabinet. Outside dimensions 24" high, 10½" deep, and 27" wide, Ample room for radio receiver 14" long, 9" high and 10" deep. Will hold a changer up to 14" square. Will accommodate speaker up to 12". Has record album storage compartment. Hinged lid covers changer compartment. Cabinet Ar-15 Net \$29.95. Detrola automatic changer \$12.95 extra.

BLOND ARMCHAIR CABINET \$34.95

wired and tested chassis. Size 71½ deep, 4½" tall and 13" long Receives 550 to 1000 K.C. RF stage and 3 gang tuning condenser. Loop ant. Fitched kiass slide rule dial. With tubes 2 6SK7, 6847, 6807, 686, 583, 8 in. Heavy duty speaker. This chassis is ideal for the above arm chair cabinet. Input for phono pick up. Tone control and phono switch. Brand new. Should sell for \$40.00 Stock No. DTR-6 Net \$16.95. Weight 20 Lbs.

4 tube AC-DC, TRF radio leit. Ideal for students and beginners. Every part furnished to build this kit, including tubes, diagram and photos. Has Alnico V PM speaker and tubes 128K7, 12817, 2085 and 35W4. Plastic cabinet with slide rule dial. Receives broadcast 550 to 1600 KC. This is the easiest type of radio to build. Kit Model TF-4 Net \$6.95. Weight 6 lbs.

Build this powerful, 4-tube, 3-way portable kit. Operates on 110 volts AC or DC or self contained batteries, Receives broadcast 550 to 1650 K.C. Incorporates a standard superhet circuit with AVC and loop Ant. Has Alnico 5 PM Speaker, 2 gans condenser. All parts and batteries are furnished including tubes. Disc Rectifier, 1R5, 1T4, 185 and 384. Has attractive leatherette portable cabinet size 7x9x9. Weight 14 lbs, Kit Model 3-ZA.





DELUXE WIRE RECORDER \$79.95





DELUXE WIRE RECORDER \$79.95

This wire recorder incorporates all necessary circuits for recording and playbacks. Has built-in graser circuit. The amplifier is of the AC bransformer type, with push-pull 6V6 output tubes. Has tone control and fader control. Input stage for wire recording from either crystal mike, radio receiver or phono pick-up. Amplifier is wired, tested and ready to operate. This init is classified as a kit, only because you have to mount the Webster wire recording mechanism, amplifier and speaker. Everything is furnished, including a 15 minute spool of recording wire. Kit includes wired and tested 12 watt amplifier, expressly made for wire recording and public address use. Leatherette split type case and 10" PM speaker, furnished with regular \$52, 92 Webster wire recording mechanism. Kit model GN-12. Net \$79.95. Crystal mike and desk stand \$4.95 extra.

PORTABLE RADIO DISC-RECORDER

890.00 value for only \$54.95.
We furnish every part to build a powerful radio and dual speed recorder. The attractive leatherette case houses the sensitive superhet broadcast radio and General Industries R90L 33½ and 78 RPM dual speed recorder; play back mechanism, The 6 tube receiver and amplifier is all on one chassis; 128A7, 128L7, mike gair; two 33L6 push-pull output; plus disc rectifier. Has plenty of gain for crystal or dynamic mike. Has 6" heavy duty PM speaker and tone control. Kit G-31, everything complete, with tubes and diagram. \$54.95. Crystal mike and destand \$4.95 extra. This is without a doubt one of the best values in kits we have ever offered. Wt. 40 lbs.

Build this new super Midget Broadcast Radio. Has beau-tifully made walnut cabinet. Size 7½x1½x5½. Attractive slide rule dial. Incorporates silderule dial. Incorporates a standard superhet circuit with 456 KC IFS & AVC. Has 2 gang condenser and loop ant. Every part including Alnico V. PM speaker and tubes. 12BE6, 12AT6, 50B5 & 35W4. Furnished as well as photo and easy-to-follow diagram. Weight 5 lbs. Model KP-T.

WIRE RECORDER \$69.95

Portable Wire Recorder Model GN-II







KIT, \$54.95



SUPER MIDGET KIT, \$10.95 OUR SUPER VALUE



BUILD A RADIO Like you would buy 5-TUBE KIT **ONLY \$9.95**

Made from Detrola Components



Components
Attractive 13" blond cabinet AC-DC radio kit, with illuminated slide rule dial. Incorporates a standard 2 gang superhet circuit. Loop antenna, ready-punched chassis. This is another one of our line production radio kits. Every part is furnished. Includes tubes: 128A7, 128K7, 14A7, 35Z5 and 50L6. Diagram. photos and instructions are included. Has full 5" Alnico 5 PM speaker. Receives broadcast, 555 to 1650 KC. Shipping weight 9 lbs. Model TF-6. Net \$9.95.

Model TF-6 wired and tested.....\$14.95

· Zalabla wal

1949 MODEL AC-DC KIT \$12.95

This is our latest and finest AC-DC radio kit. Receives Broadcast, 540 to 1650 KC. Has full length illuminated sliderule dial, illuminated sli

AMERICAN AND FOREIGN KIT \$14.95

550 to 1600 KC and 6 to 18 MC



and 6 to 18 MC

This radio kit is housed in an attractive grey opalescent finished metal cabinet, Incorporates a standard 2 gang superhet circuit. Receives Broadcast (556 to 1600 KC) and foreign short wave (6 to 18 Megacycles). This kit is complete, nothing else to buy; just as all our kits. Ready-punched chassis. It will go together just as it would down a production line. Has full 5" PM speaker. Complete with tubes: 128A7, 128K7, 128Q7, 35Z6, 50J6, Diagram, photos and instructions are furnished, Shipping weight 10 lbs. Kit model DT-5. Net \$14.95

12 WATT AMPLIFIER KIT, \$10.95



Push Pull 6V6's Gain for Mike

for Mike

KIT MODEL AC-12. 12

wat amplifier kit. Ideal for
high quality record player
as well as public address or
recording amplifier. Matched
crol fades from phono to microphone. Gain enough for
crystal or dynamic microphone. 100 mil power transformer, for 110 volt AC 66 cycle operation. Priced complete with tubes: 2-6V6, 6SNT. 6SHT and rectifier.
12" Alnico 5 PM speaker \$6.95 extra; crystal microphone and desk stand \$4.95 extra.
The above AC-12 amplifier wired and tested ready to
operate net \$14.95 Specify stock No. AC-1125, 12 inch
Alnico V PM speaker \$5.95 extra. Crystal mike and desk
stand \$4.95.

20-WATT UTILITY AMP. KIT, \$17.95

20-WATT UTILITY AMP. KIT, \$17.95
Build this 20 watt utility
110 volt AC, 20 Watt power
amplifler. Ready punched
chassis, size 12 x 6 x 2½
inches. Has two input circuits. one mike and one
phono. Mike stage has 135
DB gain, for crystal or dynamic mike. Has bass and
treble controls. Designed for use with PM speakers; has
\$-16 ohm output transformer, All parts and easy-tofollow diagram furnished, including tubes: 2—68N7,
635, 2—616GA, 523. Kir Model 20-T.X.... Net \$17.95



INTER COM



INTER COM KITS \$7.95

Inter-com kit. All Darts furnished to build a small two - way call system (Master and one sub-station speaker) Has 3" speaker and tubes 70L7 and 12SL7. Has separate 3" speaker for sub-station. Ready punched chassis. Everything complete. less cabinet. Diagrams and photo furnished. Kit TB-3. Net Price \$7.95.

Personal

PORTABLE RADIO KIT MAKES A \$32.50 RADIO

Weighs Only 31/2 Lbs.

Complete with Batteries

\$14.95

Size: 61/2"x31/4"x41/8" Two-Tone Ivory, Red Plastic Cab. • Loop Aerial, Built-in Lid

■ 4-Tube Superhef ■ AVC. ■ Looks like and is a Commercial Radio Kit
■ Two-Gang Cond., Lucite Dial ■ Simple Assembly and Wiring Instructions

This kit is ready for immediate delivery. The same nationally known factory that manufactures tens of thousands of this radio, is line-producing this radio kit for us. Every part, from the cabinet down to the last resistor, is matched. The chassis is ready punched; all you do, is mount the parts and wire. This radio kit will assemble into a heautiful personal radio for you, just the same as it does for the factory. We furnish you a diagram, photograph of the competed chassis and full assembly instructions so that those with a minimum nowledge of radio may wire this kit. The beautiful case is made of metal with plastic hinged lid and snap on back. The lucite face of the receiver has an inlaid gold design. The circuit is the conventional two gang superhet type, with A.V.C. Receives the broadcast band, 40 to 1650 KC. Uses miniature tubes: IR5 converter, IS5 detector A.V.C. If amplifier and 384 power amplifier. Almico V PM speaker. The loop antenna is built in the lid. Radio comes on automatically when lid opens, Operates on self-contained batteries. Priced complete with tubes and 67½ volt "B" battery and flash cell (Not AC-DC). Nothing else to buy. Model X.45, Price \$14.95. Include Postage for 6 lbs.

SCOOP MODEL X.45 PERSONAL ROBATABLE MIT WARDS CARD TO THE AMPLIFIER TO THE PRICE AND THE PRICE AND

SCOOP MODEL X-45 PERSONAL PORTABLE KIT WIRED AND TESTED WITH BATTERIES. NET \$17.95

SCOOP MODEL X-45 PERSONAL PORTABLE KIT WIRED AND TESTED WITH BATTERIES. NET \$17.95

SEND 25% DEPOSIT—BALANCE C.O.D.

VALUE AS CITY MISSO McGEE RADIO COMPANY WRITE FOR CATALOG SEND 25% DEPOSIT—BALANCE C.O.D. PRICES F.O.B. K. C. 1225 McGEE ST., KANSAS CITY, MISSOURI



What's New in Radio

NEW CARDIOID MIKE

The Turner Company of Cedar Rapids, Iowa has developed a new cardioid microphone for use in commercial broadcast, recording studios, and high quality p.a. systems.

Known as the Model 77, this new unit has been designed to effectively control feedback and features a wide-range



pickup at the front and a sharply attenuated output at the rear.

Discrimination between front and rear is approximately 15 db. at all frequencies. Response is within plus or minus 5 db. from 70 to 10,000 c.p.s. Level is 62 db. below 1 volt/dyne/sq. cm. at high impedance. The unit is equipped with a 4-position output switch giving 50, 200, 500 ohms or high impedance output and features a tilting head and quick disconnect cable.

Additional details on the Model 77 may be secured by writing *The Turner Company*, Cedar Rapids, Iowa.

HEAVY DUTY TEST LEADS

A new set of high voltage, heavy duty test leads, the Model 910, is being manufactured by *Reiner Electronics Company* of New York to meet the requirements of television measurements.

These leads are tested at 20,000 volts and are rated at 15,000 volts. The tips are of case hardened steel, so that the points cannot become blunt or dulled despite hard use. A special construction permanently anchors the insulated conductor to prod handles which are made of a high quality material having zero moisture absorption, extremely low power factor and surface leakage, and extremely high resistance.

A combination thumb rest and shield, designed to prevent leakage and creep-

age is provided for maximum protection and ease of handling. The set consists of one black and one red lead, each 54 inches long.

Reiner Electronics Company, 152 West 25th Street, New York 1, New York will supply additional details and prices on request.

CONDUIT FITTINGS

Cannon Electric Development Company of Los Angeles has added three new conduit fittings to its line of AN connectors and accessory fittings.

The AN3060 Conduit Coupling is used for connecting either flexible or rigid aluminum, brass or other conduit; the AN3064 Box Connector is used with the AN3066 Conduit Coupling locknut to form a termination inside conduit boxes or panel, and the AN3068 Conduit Coupling Adapter is used to make a coupling between any two male-threaded conduit fittings.

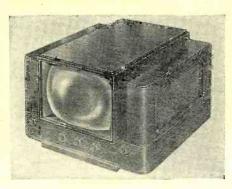
Standard finish on all these items is tin plate or natural. Melted petrolatum, conforming to specification AN-VV-0-236, is used as an over-all coating. Material is diecast aluminum or bar stock.

Copies of bulletin sheets covering the above fittings may be secured by writing the Catalogue Department, Cannon Electric Development Company, 3209 Humboldt Street, Los Angeles 31, California.

TELEVISION KIT

Transvision, Inc. has announced the availability of a television kit which features a new-type cabinet with built-in lens.

In addition to magnifying and clarifying the picture, the new lens is said to



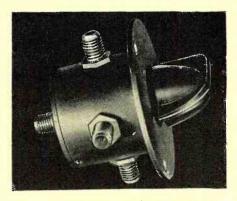
create the effect of apparent rotation of the picture so that when the observer moves, the picture still seems to be in focus and clearly visible from any angle.

The kit, which is being marketed as the Model 10BL, comes complete with a 10" tube and cabinet with built-in lens. The unit uses the electromagnetic directview picture tube, has complete FM radio, receives all channels in any area, and comes completely supplied with antenna and lead-in wire. The cabinet is available in mahogany, walnut, or blonde finishes.

Transvision, Inc., 385 North Avenue, New Rochelle, New York will supply additional data and prices on request.

COAXIAL SWITCH

The Workshop Associates Incorporated has developed a new coaxial switch designed to be used with RG-59/U coaxial cable. The new unit is used to switch



from one television channel to another utilizing the company's new television receiving system.

The unit provides for switching any one of four antennas to a receiver. The switch may also be used to meet the television sales demonstration problem. By using additional switches, any number of television sets can be demonstrated from one location. The switch maintains a low standing wave ratio.

A complete line of solderless, silverplated coaxial connectors for RG-59/U is available as extra accessories.

The Workshop Associates Incorporated, 66 Needham Street, Newton Highlands 61, Massachusetts has additional details available on request.

POWER CONVERSION UNIT

Radio amateurs will be especially interested in the new power conversion unit being offered by Radio Products Sales Company of Los Angeles.

By means of the new unit, d.c.-operated war surplus dynamotors, receivers, transmitters, relays, and motors may be operated from a.c. power mains without rewiring the equipment.

Units are available for any voltage or amperage rating. Standard units are available covering these popular model dynamotors: DMDX, 12 volts, 2 amps.;

Wishing Radio Shop, 6114 Mackingbird

TILLMAN F. BABB, Wilshire Radio Shop, 6114 Mockingbird Lane, Dallas, Texas. Tillman knows his tubes, and like thousands of outstanding servicemen, he prefers Ken-Rad tubes. They're quality, through and through.

"KEN-RAD TUBES PAY OFF!"

"Ken-Rad tubes? I'll say I use them!

"Ken-Rad tubes have been doing a job for me for 13 years. And I'll say this there's not a better tube made. They perform well and stand up.

"You can depend on them to make customers happy. Happy customers build business.

"And I'm not letting customers down. I'm selling quality. It pays off!

"That's why I'm for Ken-Rad tubes!"

"Ken-Rad tubes are MADE TO PAY OFF"

"We make Ken-Rad tubes to stand up—satisfy users—and build business for servicemen.

"Before a Ken-Rad tube is sent to you it must pass a series of tests for noise, microphonics, static, life, short, appearance, gas, air and hum.

"That's why Ken-Rad tubes meet your most exacting demands—for quality, stamina, endurance.

"That's why they'll bring customers back satisfied."



ROBERT HAGAN, Shop Foreman, Quality Laboratory, is in charge of the strict Life Test, above. It's typical of the numerous tests that Ken-Rad tubes must pass before leaving the plant.

The Serviceman's Tube

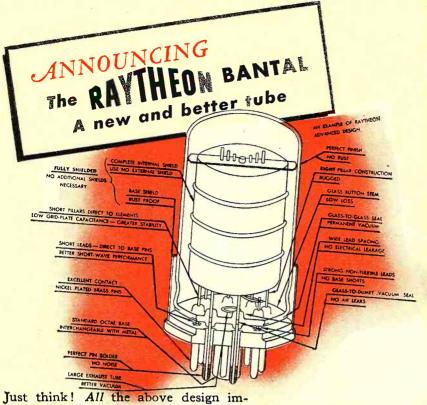
178-GA7-8850

KEN-RAD Radio Tubes

PRODUCT OF GENERAL ELECTRIC COMPANY

Schenectady 5, New York





Just think! All the above design improvements and construction advantages in one tube—the RAYTHEON BANTAL tube.

- Rugged Eight Pillar Construction
- Completely Shielded Internally No external shielding hardware or installation labor! Increases your service profit!
- Made In Eight Popular Types 6SA7GT-6SJ7GT-6SK7GT-6SQ7GT-12SA7GT-12SJ7GT-12SK7GT-12SQ7GT
- Superior Performance Assures Customer Satisfaction And Repeat Business
- All At No Extra Cost!

Your Raytheon Distributor — sponsor of the famous Bonded Dealer-Service Program — is now delivering Bantal Tubes.

Look for this distinctive marking on the Raytheon Bantal Tube. The 12SK7GT Tube illustrated replaces ordinary "GT" and Metal 12SK7 Tubes. Only the Bantal Tube is needed in stock!



RAYTHEON MANUFACTURING COMPANY

RADIO RECEIVING TUBE DIVISION

NEWTON, MASSACHUSETTS - CHICAGO, ILLINOIS - LOS ANGELES, CALIFORNIA

RADIO RECEIVING TUBES . SPECIAL PURPOSE TUBES TRANSMITTING TUBES . HEARING AID TUBES

PE-77, 12 volts, 39 amps.; DM-310A, 24 volts, 1.1 amps.; 5DY83AB1, 28 volts, 5 amps.; PE-103, 12 volts, 10 amps.; DM-28, 24 volts, .7 amp.; PE-73C, 24 volts, 19 amps.; and the 12 volts, 4.5 amps. unit is also considered standard.

All complete installation diagram and price data are free upon request. Address all correspondence to Seymour Friedman, Department C-35, Radio Products Sales Company, 1501 South Hill Street, Los Angeles 15, California.

VIBRATOR DEAL

Radio servicemen are now being offered a new sturdy and practical metal stock cabinet in combination with a group of fast-moving vibrators and buffer capacitors by *P. R. Mallory & Co., Inc.* of Indianapolis, Indiana.

Known as the "2448 Vibrator Deal", this offering includes six vibrators which



are said to cover 75% of normal replacement requirements. The metal cabinet is designed for simplified stocking of these parts and also to facilitate inventory checking. The new unit is a companion piece to the volume control cabinet which the company made available last year.

Further information may be obtained from *Mallory* distributors or from *P. R. Mallory & Co., Inc.,* Indianapolis, Indiana.

SHURE NEEDLES

Shure Brothers, Inc. has announced that its new "Muted Stylus" needles are available in osmium or sapphire.

These replacement needles are the only units that can be used in the company's "Muted Stylus" crystal cartridges. These new units feature silent tracking and simple fingertip replacement.

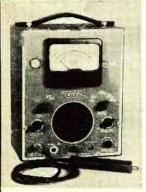
The Model A62A (osmium) and the Model A61A (sapphire) are packaged in a unique point-of-sale card.

Further information on these replacement needles may be secured by writing Shure Brothers, Inc., 225 W. Huron Street, Chicago 10, Illinois.

NEW HAM RECEIVER

National Company, Inc. is in production on the new NC-33 receiver which is be(Continued on page 160)

IRVING JOSEPH WHERE PRICE IS AN OBJECT AND EVERY ITEM QUALITY IS UNDERSTOOD - EVERY INICON WE SHIP IS RACKED IID BY AN IINICON QUALITY IS UNDERSTOOD - EVERY ITEM WE SHIP IS BACKED UP BY AN UNCON-DITIONAL GUARANTEE.



EICO MODEL 113-A SIGNAL TRACER WITH **VACUUM TUBE PROBE**

Permits rapid tracing or following a signal audibly through the receiver from antenna to speaker, locating the faulty section quickly. Isolates the precise cause of trouble with the VTVM section by making point to point checks giving both audible and visual indications. fect for checking distortion or fading. Signal may be traced through entire receiver without interfering with normal op-

MULTI-ANALYST

- Wide frequency response from 30 cycles to 300 mc.
- High input impedance of 26 megohms on DC.
- All electronic AC and DC voltmeter and ohmmeter.
- DC and AC ranges 0-5, 10, 100, 500, 1000 volts.
- Ohmmeter reads from .1 ohm to 100 megohms in six ranges.
- Built-in speaker for monitoring either IF, RF or AF channel.
- VTVM cannot be damaged by overloading.
- Tests-phono pick-ups microphones, etc. for distortion or voltage output.
- Will substitute for any defective stages in radio receiver or

Yours Net \$89.50

Write for further information on Eico Signal Generator and Eico VTVM.

FIDELOTUNER FOR YOUR F-M LISTENING PLEASURE SOME OUTSTANDING FEATURES:



Clip the

Size II" long, 6" wide, 6%" Each \$31.50 Lots of 3 \$28.50

0Z4 (CK-1005)



Full wave gas rectifier-octal base. Makes a perfect replacement for 0Z4

44c ea. 10 for \$410 100 for \$700

NEW 3-WAY PERSONAL GLOBE PORTABLE **RADIO**

that tops them all for VALUE!

- 4 Tube super circuit, plus life-time selenium rectifier.
- Battery operation for outdoors -II0 volt AC or DC indoors.
- Alnico 5" PM Speaker.
- Weighs only 41/2 lbs. with bat-
- Beautiful plastic case measures 81/2x41/2x4 inches.
- Four beautiful gleaming colors: Maroon—Ivory—Tan—Black.
- Performance equal to regular \$39.95 models.
- 4 ATTRACTIVE COLORS
- MAROON DIVORY TAN

Each \$29.95

Lots of 3 \$27.50 Lots of 6 or more \$24.50

This is the set they rave about. Small, compact and beautifully de-

signed in colorful plastic. Use it outdoors on battery operation -

indoors on any 110 voit AC or DC

current. You'll marvel at its fine

operation-its wonderful tone-its



A FULL POWERED SUPERHETERODYNE RADIO

great sensitivity.

Styled for tomorrow. Powered for sharp, clear reception. A wonderously toned superhet circuit. In practically unbreakable plastic cabinet. An amazing value.

Tele-Tone Model 165 \$9.95



MODEL 159 5 TUBE AC-DC TABLE MODEL

MODEL 166 5 TUBE SUPER-HETERODYNE with handle



.....\$19.95 | Ivory only\$16.95 Walnut

MODEL 183-3 Tube Record Player



Push-Pull Output. Cabinet Dimensions -13 1-16" Width — 7 High—12%" Deep.

\$34.95

MODEL 182-2 TUBE RECORD **PLAYER**

High Power Output. Cabinet Dimensions



12½" Wide — High—10¾"Deep.

\$19.95



JFD TWIN LEAD 300 ohm WIRE

Extruded parallel ribbon-type lead-in wire. Insulated with polyethylene—300 ohm impedance. Excellent for FM and TV receivers. Made to withstand weather and use. No. TW200—100' Reel \$2.91

Also available in 500' and 1000' spools.

TERMS

Minimum order \$2.00. All orders shipped f.o.b. Chicago, 25% deposit on all c.o.d. shipments.

IRVING JOSEPH 220 S. Halsted St., Chicago 6, III.

HEATHKIT SERVICE INSTRUMENTS BUILD . . . LEARN . . . SAVE

Laboratories—Service Shops, Hobbyists.

HEATHKIT

GENERATOR KIT SIGNAL

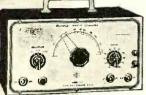


NOTHING ELSE TO BUY

Every shop needs a good signal generator. The Heathkit fulfils every servicing need, fundamentals from 150 Kc. to 30 megacycles with strong harmonics over 100 megacycles cavering the new television and FM bands. 110 V 60 cycle transformer operated power supply.
400 cycle audio available for 30%

modulation or audio testing. Uses 65N7 as RF oscillator and audio amplifier. Complete kit has every part necessary detailed blueprints and instructions enable the builder to assemble it in a few hours. Large easy to read calibration. Convenient size 9" x 6" x 434". Weight 41/2 pounds.

HEATHKIT SINE AND SQUARE WAVE



\$34.50

NOTHING ELSE TO BUY

AUDIO GENERATOR KIT

The ideal instrument for checking audio amplifiers, television response, distortion, etc. Supplies excellent sine wave 20 cycles to 20,000 cycles and in addition supplies square wave over same range. Extremely low distortion, less than 1%, large calibrated dial, beautiful 2 color panel, 1% precision calibrating resistors, 110 V 60 cycle power transformer, 5 tubes, detailed blueprints and instructions, R.C. type circuit with excellent stability. Shipping weight 15 pounds.

HEATHKIT SIGNAL TRACER KIT



\$19.50

NOTHING ELSE TO BUY



NOTHING ELSE TO BUY

Reduces service time and greatly increases profits of any service shop.
Uses crystal diode to follow signal from antenna to speaker. Locates faults immediately. Internal amplifier available for speaker testing and internal speaker available for amplifier testing. Connection for VTVM on panel allows visual tracing and gain measurements. Also tests phonograph pickups, microphones, PA systems, etc. Frequency range to 200 Mc. Complete ready to assemble. 110 V 69 cycle transformer operated. Supplied with 3 tubes, diode probe, 2 color panel, all other parts. Easy to assemble, detailed blueprints and instructions.

Small portable 9" x 6" x 43/4". Wt. 6 pounds. Ideal for taking on service calls. Complete your service shop with this instrument.

HEATHKIT HIGH FIDELITY AMPLIFIER KIT

Build this high fidelity amplifier and save two-thirds of the cost. Push pull output using 1619 tubes (military type 616's), two amplifier stages using a dual triode (65N7), and a phase inverter give this amplifier a linear reproduction equal to amplifiers/selling for ten times this price. Every part supplied; punched and formed chassis, transformers (including quality output to 3-8-15 ohm voice coil), tubes, controls, and complete instructions. Add postage for 20 lbs. 12" PM speakers for above..........\$6.95

NEW 1948 HEATHKIT 5 INCH OSCILLOSCOPE KIT

A necessity for the newer servicing technique in FM and television at a price you can afford. The Heathkit is complete, beautiful two color panel, all metal parts punched, formed, and plated and every part supplied. A pleasant evening's work and you have the most interesting piece of laboratory equipment available.

Check the features - large 5" 5BP1 tube, compensated vertical and horizontal amplifiers using 6SJ7's, 15 volts to 30 M cycle sweep generator using 884 gas triode, 110 V 60 cycle power transformer gives 1100 volts negative and 350 volts positive.

Convenient size 81/2" x 13" high 17" deep, weight only 26 pounds.

All controls on front panel with test voltage and ext. syn post. Complete with all tubes and detailed instructions. Shipping weight 35 lbs.

Order today while surplus tubes make the price possible.

The NEW HEATHKIT VACUUM TUBE VOLTMETER KIT

The most essential tool a radio man can have, now within the reach of his pocketbook. The Heathkit VIVM is equal in quality to instruments selling far \$75.00 ar mare. Features 500 microamp meter, transformer power supply, 1% glass enclosed divider resistors, ceramic selector switches, 11 megahms input resistance, linear AC and DC scale, electronic AC reading RMS. Circuit uses 6SN7 in balanced bridge circuit, a 6H6 as AC rectifier and 6X5 as transformer power supply rectifier. Included is means of calibrating without standards. Average assembly time less than four pleasant hours, and you have the most useful test instrument you will ever own. Ranges 0-3, 30, 100, 300, 1000 volts AC ar DC. Ohmmeter has ranges of scale times 1, 100, 1000, 10M and 1 megahm, giving range .1 ohm to 1000 megahms. Complete with detailed instructions. Add postage for 8 lbs:



\$39.50

NOTHING ELSE

TO BUY

NOTHING ELSE TO BUY

HEATHKIT

CONDENSER CHECKER KIT

A condenser checker anyone can afford to own. Measures capacity and leakage from .00001 to 100 MFD on calibrated scales with test voltage up to 500 volts. No need for tables or multipliers. Reads resistance 500 ohms to 2 megohms. 110V 60 cycle transformer operated complete with rectifier and magic eye indicator tubes.

Easy quick assembly with clear detailed blueprints and instructions. Small convenient size 9" x 6" x 43/4". Weight 4 pounds. This is one of the handiest instruments in any service shop.



NOTHING ELSE

A WORD ABOUT HEATHKIT INSTRUMENTS

All Heathkit service instruments are supplied complete in every way — grey crackle cabinets, 2 color calibrated panels, all tubes, test leads (where required) etc. All are 110 V transformer operated. Calibrations are complete and exact, 1% precision resistors are supplied where needed.

Heath engineers are ready to assist and advise. Heathkits are sold direct to customer, order from this ad. All are





COMPA

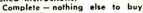
HARBOR, MICHIGAN BENTON

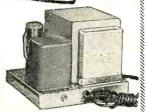
ACCESSORIES

COMMAND SETT BEST of SURPLUS

TRANSMITTER POWER SUPPLY KIT

For BC645, 223, 522, 274N's, etc. Ideal for powering military transmitters. Supplies 500 to 600 volts at 150 to 200 MA plate, 6.3 at 3.6A, also 9V and 12V A.C. Kit supplied complete with husky cased Acme 110V 60 cycle power transformer, 5U4 rectifier. Sprague oil filled condenser, cased choke, punched chassis, and all other parts, including detailed instructions.







110V RECEIVER POWER SUPPLY KIT

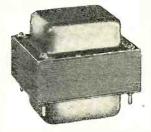
With 24 volt filament, no wiring changes inside set, punched chassis and volume control \$5.95

5" PM SPEAKER

| | With output transformer, matching headphone output | \$2.80 |
|----|--|--------|
| 1 | Dual receiver rack FT277A with connecting plugs | \$1.00 |
| 00 | Cinala tamamittan yash | \$1.00 |
| | MILITARY CONVERSION POWER | |
| 11 | TRANSFORMERS | |

Convert your military receivers without rewiring the filament. "A" type supplies 500 VCT at 50 MA, 5V at 2A and 24V at 1/2A. "B" type supplies 500 VCT at 50 MA, 5V at 2A and 12V at 1 amp. State whether A or B type desired...

POWER TRANSFORMER Specials



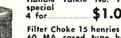
A wonderful buy in a new production heavy duty power transformer, Primary 117V 60 cycle. Secondaries supply 746 V.CT at 220 MA, 6.3V. at 4.5 A., and 5V at 4 A. An ideal transformer for high quality amplifier modulator, small transmitter or quality radio. Will handle 13 tube radio receivers. Supply is limited, order early.

\$3.95 ... 3 \$995



INPUT AND OUTPUT TRANSFORMER

TRANSFORMER
Two units in one case carbon microphone input and output from 155 to 150 ohm load used in Handie Talkie No. 744 special \$1.00



Filter Choke 15 henries at 60 MA cased type her-metically sealed No. 643, each....\$1.00



OUTPUT TRANSFORMER Push pull 6V6's to 6-8 ohm voice coil excellent characteristics
No. 800. 3 for... \$1.95



OUTPUT TRANSFORMER Couples, 6C4, 6J5, etc. to 500 or 5,000 ohm line No. 716. 2 for \$1.00



MIDGET AMATEUR TRANSMITTER KIT

Complete kit to assemble a 1 Watt battery operated amateur 80 meter transmitter, including tube and crystal. Range up to 500 miles. Only accessories needed are sending key and batteries. Complete instructions supplied. Add postage for 2 lbs.

ACCESSORIES

Key (add postage for 2 lbs.) \$1.00 Kit of batteries (add postage for 4 lbs.) 3.25



AN/APNI RADIO ALTIMETERS

Brand new, complete with tubes, dynamotor, antennae, indicator, switch, plugs and instruction manual. Consists of 420 MC transmitter and receiver. Converts into excellent boat radar indicating in feet, or amateur 420 MC rig. In original crate.

HEARING AID HEADPHONES The Army's best — eliminate flat ears and outside noise. Complete with transformer for conversion from low to high impedance. With cord and



\$3495

T32 TABLE MICROPHONE







6 pounds. \$1.50

Dynamotor A — Input output 1000 volts at 350 MA. Shipping Weight 72 pounds. \$5.05

Dynamotor 8 – Input 6 or 12 volts, output 500 volts, 160 MA. Shipping Weight 30 pounds. \$5.95



Single hole mounting octal, brown, low loss, bakelite, less brown, low los locking rings, 25 FOR \$1.00 2 hole flange mounting octal bakelite 1-5/16" mounting

SOCKET SPECIALS

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Another Method of POWER SUPPLY CONTROL

By JACK D. GALLAGHER, W5HZB

Plate power on last—filament power off last—in spite of switching order—a foolproof system.

ANY articles have been written about power supply construction and protective devices therein to prevent turning on plate voltages first, but a great majority of the methods employed were based on the operation of a relay. Also various switching arrangements were devised so that no line voltage would be present if the switch controlling the high voltage plate transformer was turned on first. Then, if the operator saw that no filament voltage was applied when he flipped one switch, he turned that switch off and turned on a second switch, which turned on the filaments. However, if the operator forgot to turn off the first switch he threw, both filament and plate voltages would be applied simultaneously when he flipped the remaining switch.

In order to eliminate the possibility of turning on plate voltage first in high voltage power supplies, the following features are found desirable and should be incorporated in the power supply switching system:

1. Irrespective of the switch thrown first, all filament voltages should be applied first.

2. In spite of the switch thrown last, all filament voltages should be turned off last.

3. No one switch, or combination of switches, when turned on in succession should turn on both filament and plate voltages simultaneously.

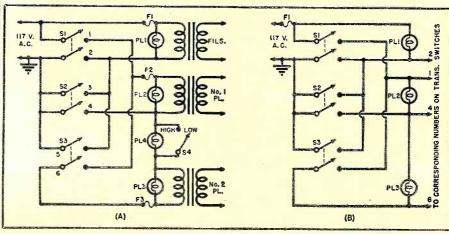
Although not an essential ingredient in cooking up a foolproof switching

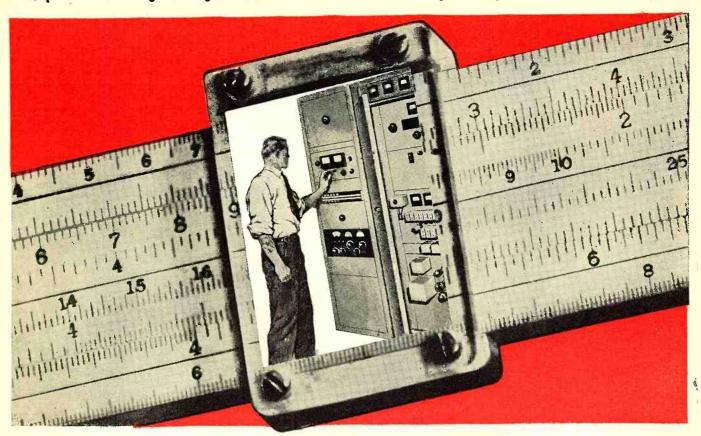
arrangement for a power supply, a method of controlling the transmitter from the operating table should be considered. Also, the same three features should be incorporated in the control box as are incorporated in the transmitter itself.

The three d.p.s.t. toggle switches are the main switches which control each of the transformers shown. The filament transformer represents all of the filament transformers in the transmitter. Plate transformer No. 1 represents the oscillator and buffer plate transformers, and plate transformer No. 2 represents the high voltage transformer. Any bias supply may be connected in parallel with the primary of the filament transformer or plate transformer No. 1. S4 is a s.p.s.t. toggle switch which shorts out the lamp in series with one side of the high voltage plate transformer primary. This is a simple method of obtaining low voltage for tuning-up purposes. The lamp (PL_4) may be a 150 or 200 watt bulb, while PL_1 , PL_2 and PL_3 are standard 115 volt pilot lamps.

It can be seen from Fig. 1A that any d.p.s.t. switch will turn on the filament voltage and PL_1 . However, the discussion to follow will assume that S_3 has been turned on first. In this case, the filament voltage is applied first. Turning on S_1 will not turn on either plate supply. If the remaining switch (S_2) is then turned on, both plate supplies will be turned on simultaneously. This, of course, does not present any problem since the filaments are already on.

Fig. 1.





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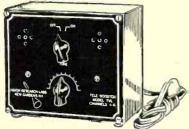
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S, is left off (the low position), until all tuning has been accomplished, then it is turned on for full plate voltage to the transmitter final.

Turning off the transmitter may be accomplished by turning off S3 first, which will turn off the high voltage first. Either S₁ or S₂ will then turn off the remaining plate voltage, and the last switch thrown will turn off the filament voltage. If S_1 (or S_2) is turned off first, both plate supplies will be turned off together, and S, will turn off the filaments last. Of course there are many different combinations. involved when turning the transmitter on and off by all the methods possible with the switches shown, but none of these arrangements will turn on any plate voltage first, or turn on both filament and plate voltages at the same time.

Fig. 1B shows the connections to three d.p.d.t. switches inside a 3" x 4" x 5" metal box which may be mounted on the operating table. Once the transmitter has been tuned up and S_{\star} (Fig. 1A) left closed, the transmitter may be turned off and operated from the operating table by means of the connections in Fig. 1B. The same switching facilities are incorporated in the control box as are found in the transmitter, with the exception of S_{\star} .

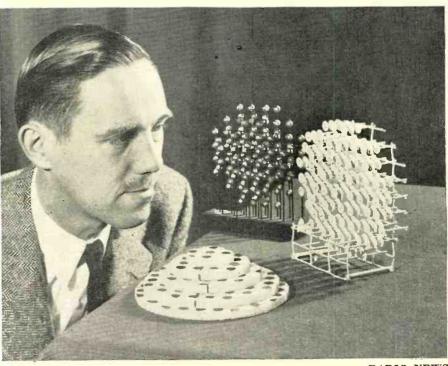
Only four wires are needed, as shown in Fig. 1B, to connect the

switching arrangement in the control box with that in the transmitter. Of course the line voltage obtained for the control box must be correctly polarized with the line voltage entering the transmitter, otherwise the switching arrangement at the operating position would not work properly. If the line voltage to the control box (as shown in Fig. 1B) is not used, it will be necessary to run six wires from the control box to the transmitter.

The size of the control box will depend on the switches and panel lights selected for the purpose. In any case however, the box should be fastened securely to the operating table. The size of the fuses shown in Figs. 1A and 1B will depend on the current drawn by each supply. Their location does not have to conform to Fig. 1A, but they should be used wherever possible. If it is desired to control the primary of the high voltage plate transformer (No. 2) by a relay, the wires connected to 5 and 6 of S3 should be disconnected and the primary of the relay connected to these points, then the remaining wires should be connected to the appropriate contacts of the relay.

The three features set forth at the beginning of this article have been fulfilled. However, the connections to the switches were not as easily conceived as the simplicity of the diagrams might indicate.

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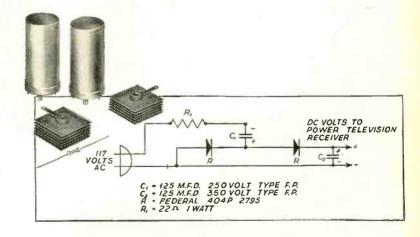
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| with relay fuse box and filters\$5.35 |
| DM-21 Dynamotor; Part of BC-312 and BC- |
| 314 14v in 235v, 100 ma out\$2.4/ |
| DM-34 Dyn: 12v in. 220v. 80 ma out\$2.29 |
| DM-35 Dyn: 12v in. 625v, 225 ma out \$3.25 |
| PE-101-C Dyn Hnit: 12 or 24v in, outputs |
| 800v. 20 ma. 400v. 135 ma. 9v. 1.1A\$2.75 |
| PE-55Den Unit · 12v or 24v in, either 16 or |
| 25 amp, 500v out, either 200 or 400 ma\$3.75 |
| PE. 906 Inverter Unit: rotary converter, 28v |
| in 80v at 500 VA 800 ev. out 3.95 |
| PE-103 Dynamotor, used\$6.95 |
| DM32A—each95c 3 for\$2.00 |
| |

OUTPUT TRANSFORMER

Hi-Fi; used is Scott-made Navy receiver. Fully potted, Pri. 5000 ohms, output secondary 600 ohms CT, inverse-feedback secondary \$1.49

TUBES

| BRAND NEW! | | BRAND NEW! | |
|---------------|------|---------------|----|
| 2J32\$1 | 9.95 | 832A\$2.9 | 5 |
| 869B 1 | 9.95 | 837 1.9 | 5 |
| 872A | .95 | 838 2.9 | 5 |
| 6G6 | .79 | 839 2.9 | 5 |
| 304TL | 1.95 | 5BP4 1.9 | 5 |
| 2C26A | .69 | 5BP1 1.3 | 9 |
| 841 | .59 | 5CP1 1.3 | 9 |
| 6AK5 | .69 | 5FP7 1.3 | 9 |
| INSGT | .69 | 12BE6 | 9 |
| 6AT6 | .69 | 12SF7 | 9 |
| 6H6 | .49 | 864 | 9 |
| 6J5 | .49 | 954 | 9 |
| 6J6 | 49 | RK34 | 9 |
| 6SJ7 | .59 | 35W4 | 19 |
| 6SF7 | .39 | 1625 | 9 |
| 5R4 | .59 | 1629 | 9 |
| 36 | .39 | 2051 | 39 |
| 10Y | .49 | 90014 | 19 |
| 12A6 | .39 | 9002 | 19 |
| 12C8 | .49 | 7000 | 19 |
| 12H6 | .39 | 9004 | 19 |
| 12J5 | .39 | 9005 | 19 |
| 12K8 | .69 | | 19 |
| 12SJ7 | .59 | 7193 | 39 |
| 12SR7 | .59 | 110 VAC Neon | |
| 12AT6 | .49 | Light | 39 |
| Amperite | 10T1 | | |

Write for lot prices!

C-I AUTO PILOT AMPLIFIER

The complete amplifier includes one rect. 7X4. 3—7F7's for amplification and control. 3—7N7's for signal discrimination. 1 power transformer, 6 relays. 4 control pots, chokes, condensers, etc. Convert for use on radio controlled models, doors, etc. Operates from 24 V. DC. Size: 9½x8½x7-5/7". Complete. Used—good condition

SELSYN METER TO INDICATE POSITION C-71A/APQ-13

Contains 2" meter, FS-100uA, Weston 506, 0-300 V, 0-30 MA, with 6 precision resistors, as external multipliers and shunts; toggle switches, push switches, rotary switch, pots, knobs, etc. \$4.95 GOOD CONDITION

TORQUE AMPLIFIER AM 19/APA-14

Provides amplification of information from Flux Gate Compass to drive torque unit and differential gear of azimuth differential unit CN-4/APA-14. Input 26 VDC and 115 V; 400 cy. Part of stabilization assembly AN/APA-14. With plugs, 3-6SN7-GT; 2-6H6, transformer, oil-filled condensers. EXCELLENT CONDITION \$2.95

MEGAPHONE—Brand New

Only 40 of these to sell. Amplifier straps on shoulder, then just hold megaphone and speak in mike mounted on rear of projector. Amplifier is conventional type, shipped with tubes. Amplifier-dry battery operated less battery

NLY

\$29.95

SELSYN INDICATORS

| For use wit rection of b AC supply. eter, only | th beam rotators for indicati- beam. Operate from 15-24V. Small model, 3 inch diam- | on of di- 60 cycle \$2.45 |
|--|---|---------------------------------|
| Large model | 1, 5 inch diameter, only | 2.95 |
| | GE METER | |

PHANTOM ANTENNA Brand New

Used with any 80 meter transmitter as a dummy load for adjusting transmitter for maximum output before going on air. Freq, range: 2MC to 4.5MC, with in struc. man u al, enclosed in metal case with cover.....\$1.95 ea.



Cover......\$1.95 ea.

SCR-518-A

Radar altimeter 515 mc. Fast screen CR tube, hivoltage power supply, connectors, cables, 29 tubes;
1—SK7, 2—8012, 2—6817, 1—678G, 1—68N7GT,
1—678G, 1—23D4, 1—676G, 1—670GT, 10—6AC7,
3—2X2, 1—954, 1—955, 1—956, 1—615, 1—1808P1
cathode ray tube.

Prand new

\$24.95

R-5/ARN-7 COMPASS RECEIVER

Very late model ADF receiver. Includes broadcast band. Frequency 100 to 1750 kc, in 4 bands. 5-gang tuning capacitor. With 15 tubes: 4-6K7, 1-6L7, 1-6L5, 2-6B8, 2-6F6, 1-6K7, 1-6SC7, 2-2051, 1-5Z4. SCHEMATIC FURNISHED. SPECIAL\$19.95

BC-433-G COMPASS RECEIVER

SCR-269-G ADF receiver, similar to the R-5/ARN-7 described above and uses same tubes. Frequency 200-1750 kc in 3 bands. SCHEMARIC FURNISHED.

Like new, SPECIAL. \$14.95

TRANSFORMER AND CHOKE SPECIALS

this up at ONLY

POWER SUPPLY FOR BC-223

PE-125 VIBRATOR TYPE

12 or 24 voit input DC; output 475 voits-200 ma

8 voits DC at 4.5 amps. BRAND NEW

\$8.95

SPRAGUE PULSE FORMING NETWORKS Used in small radar modulators, available sizes, 67 ohms impedance. 7.5 Kilowatt in H-603, one micro second, 200 pulses per second H-601. 3 micro seconds, 200 pulses 2.95 3,95 per second 4.95 ALL THREE ABOVE FOR ONLY...

OIL-FILLED CONDENSERS

| .25 MFD at 1500 VDC | |
|----------------------------|---|
| .25 MFD at 15,000 VDC\$4.9 | |
| 2 MFD 220 VAC | 3 |
| | |
| .25 MFD at 6000V DC\$1.4 | ļ |
| 2 MFD at 600V DC | 2 |
| 4 MFD at 220V AC | 2 |
| .5 MFD at 750V AC | 2 |
| 2 X .25 at 2000V DC | |
| 3000 MFD at 3V DC | i |

SALES, INC. ARROW

MAIN OFFICE

59 WEST HUBBARD ST., CHICAGO 10, ILL. Telephone SUPerior 5575

NORTH SIDE BRANCH 1802 NORTH HUMBOLDT BLVD.

SOUTH SIDE BRANCH

8310 SOUTH HALSTED ST.

DOLLARS COUNT

* * * * * * *

Now, when your dollar is getting smaller, "Servicing with a STAR" is more than good radio sense . . . it's good dollar sense! This is no time to buy your test equipment blind. It's time to weigh your money against value — if you do, you'll choose STAR.

TUBE CHECKER

Model TE-1 * This compact

checker gives you precision testing at a low price.

Features: checks

*

*

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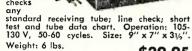
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Weight: 6 lbs. Price, ONLY...

\$29.95

STAR TESTER



SET TESTER



Combination * tube checker and multitester in a handsome

Model MT-12

REDUCED PRICE...

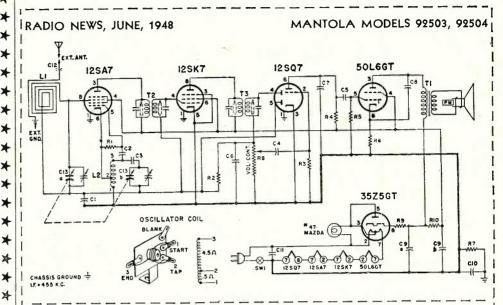
\$53.50

Instruments come completely equipped with batteries, test leads, instructions, etc. They are available at all leading jobbers. Inspect them and convince yourself. If your jobber is out of stock — order direct from

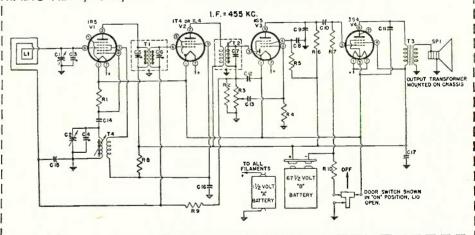
STAR MEASUREMENTS CO.

Dept. R-4, 442 East 166 Street New York 56, N.Y. Catalogs mailed on request.

(FOR PARTS LIST SEE PAGE 104)

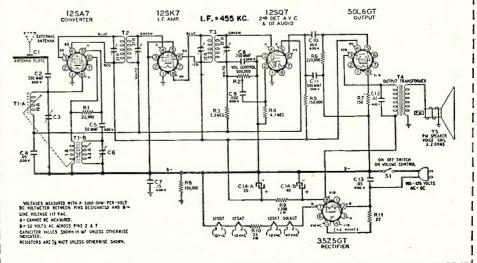


EMERSON MODEL 508 SERIES 8-7434351 AND UP IRADIO NEWS, JUNE, 1948

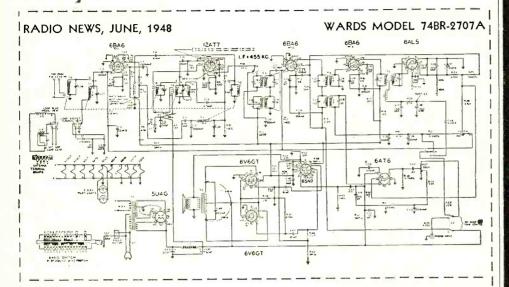


RADIO NEWS, JUNE, 1948

BELMONT MODEL A-5D118

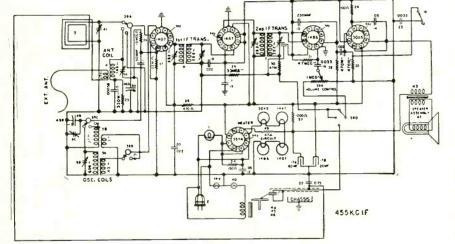


Here, and on following pages, are circuit diagrams and parts lists of many new postwar radio receivers. Radio News will bring to you other circuits as quickly as possible after we receive them from manufacturers.



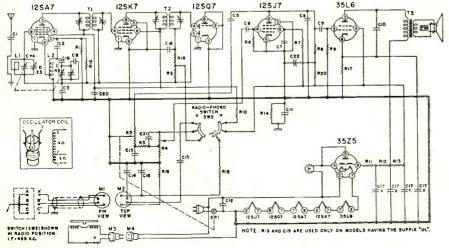
RADIO NEWS, JUNE, 1948

CROSLEY MODEL 56TP-LI



RADIO NEWS, JUNE, 1948

ADMIRAL MODEL 7C60 CHASSIS 6B1



June, 1948

War Surplus Bargains



R5/ARN-7 RECEIVER

ONLY

1995

control heads available \$4.50

Three bands 200 to 1750 KC. Complete with 17 tubes required. This set is ideal for conversion to home broadcast Receiver addition to ham shack, etc. Reported sold for many times the price when brand new. A Receiver that would be hard to pick up at this price. No cables or plugs

TRANSMITTER & REC



Operates on any of its 4 predetermined crystal controlled frequencies in the range of 140 MC. Complete with tubes, remote control, junction box, shock mounting base and connecting plugs. This unit is ideal for amateur UHF or mobile telephone. Operates from self-contained 24 V DC dynamotor. 12 V available upon request.

BC-221 FREQUENCY METER

Covers 125—20,000 KC Battery operated. A beautiful instrument \$49.95

T-12-B CARBON MICRO-PHONES Handmike\$1.00

HS-33 HEADPHONES 600 ohm (Used)75c

HEADPHONE EXTENSION

ILLARD LEAD ACID CELLS

6 V. (dry-chgd.) \$3.00 6 V. (in metal carrying case—dry-chgd.) \$4.00 (Add electrolyte, specific gravity 1.265 drugstore)

ART/13 CONTROL HEAD WITH CONNECTING PLUG

DYNAMOTOR MODULATOR

NTENNA RELAY UNIT .\$1.25

NTERPHONE AMPLIFIER \$1.95

All Prices F.O.B. Indianapolis

TERMS: CASH WITH ORDER

537 N. CAPITOL AVE. INDIANAPOLIS, IND.

SUPER PEAK SPECIALS

unmimmmmmmmmy 4 METER BARGAINS FOR THIS MONTH

\$2.95 EACH

10 FOR \$24.75

- 10 FOR \$24.75

 2" GE 0-1 Amp RF
 (thernal Thermo)
 2" Weston 150-0 150 Microamps
 (Sperry Scale)
 2" GE 0-30 Amps DC
 (Internal shunt)
 2" Sun 0 | MA
 Basic (Volt Scale)



SPERTI RE VACUUM SWITCH
9200 volts peak 8 amps. Used
as antenna switch in Collins
RT 13. Brand \$1.75 \$1.75

FEDERAL SELENIUM FECTIFIER

wave. 36 volts input, 28 volts output at 6.1



DAVEN AUDIO FREQUENCY METER-Model 837E

SCOPE TRANSFORMERS

Hermetically Sealed. 1800 v. 4 ma, 6.3 v. @ .\$ amps 2.5 v. @ 1.75 amps\$5.95 ea.

AMERTRAN TRANSTAT

and Variable Stepdown Transformer 110/220 volts 60 cycle input. Output variable plus or minus 10% of 115 volts at 3.5 amps. Also can be connected to give different voltage combinations. Brand new ______only \$12.95



CHOKE SPECIALS

Western Electric Filter Choke 4.3 henry 620 mills 42 ohms DC resistance. 47%x53%- x53% Ceramic Insulators . \$4.95 ea. NYT Choke—8 Hy 160 ma. 140 ohms DC . \$1.29 Western Electric Filter Choke 4.3 henry 620 mills 42 ohms DC resistance, 476×55%- x5% Ceramic Insulators ... \$4.95 ea. NYT Choke—8 Hy 160 ma. 140 ohms DC ... \$1.29

METER SPECIALS (Brand New)

| 1/2" | 01 ma Basic | \$3.95 |
|------|---------------------------|--------|
| 2" | 0.5 ma (amp scale) | 1.95 |
| 2" | 0-1.2 ma (0-100 scale) | 2.49 |
| 2" | 0-120 ma RF | 4.95 |
| 3" | 0-50 amps AC | 4.95 |
| | 0-75 amps AC | |
| 3" | 0-20 ma DC | 2.95 |
| 3" | 200-0-200 volts DC | 2.95 |
| | 0-10 ma | |
| | 0-2 ma DC | |
| | 0-20 ma DC | |
| | 0 15 ma DC (square) | |
| 3// | 0-150V AC | 3.95 |
| | 0-150 volts AC | |
| - | Rectifier type (Linear) | 5.95 |
| 3" | 0-50 microamps | 9.95 |
| 3" | Running Time Meter | 7.95 |
| 4" | I-O-I ma DC (Blank scale) | 3.95 |

OIL CONDENSERS Nationally Known

| 2 mfd 600 vdc \$.39 | 3 mfd 3000 vdc\$3.95 |
|-----------------------|-------------------------|
| 4 mfd 600 vdc59 | 1 mfd 5000 vdc., 4.50 |
| 3/3 mfd 600 vde79 | .1 mfd 7500 vdc 1.95 |
| 14 mfd 600 vdc. 1.35 | .1/.1 mfd 7500 vdc 2.45 |
| 2 mfd 1000 vdc79 | .01/.01 12 KV de. 5.75 |
| 4 mfd 1000 vdc95 | 65 mfd 12500 vdc 12.95 |
| 2 mfd 1500 vdc. 1.25 | .75/.35 mfd (dual) |
| I mfd 2000 vdc . 1.15 | 8/16 KV de14.95 |
| | |

MISCELLANEOUS SPECIALS

| MISCELLMIEGOS SPECIALS | |
|--|-------|
| 2-11 mmf. Butterfly with ball bearings\$ | .59 |
| G.E. S.P.D.T. Relay 10000 ohm coil | .59 |
| Heineman Circuit Breaker 5 amp. 110V. A.C. | .89 |
| G.E. Solenoid W/Microwitches 24 V.D.C | .69 |
| Ohmite 25 ohm 25 watt Rheostat | .39 |
| Microswitch 10 amp. (interlock) | .59 |
| C. H. Bat Handle Switch-D.P.S.T. 1/2 H.P. | .95 |
| Veeder Root Counter | .95 |
| Single Plate to P.P. input 3:1 ratio trans | .49 |
| 500 foot Drums R G/8 U Coax | 24.50 |
| 4 Quadrant Phasing Condenser | 1.95 |
| Trim Commercial Phones (High Imp.) | 4.50 |

If not rated, 25% with order, balance C.O.D.— Minimum order \$3.00.

PEAK ELECTRONICS CO. 188 WASHINGTON ST., DEPT. MR NEW YORK 7, N. Y.

"SURPLUS RADIO CONVERSION MANUAL" by R. C. Evenson and O. R. Beach, Published by Techno-Graphic Publications, Los Angeles. 115 pages. Price \$2.50.

This handy little manual should cure a lot of conversion headaches. The authors of this book have covered conversion details and diagrams for the BC-221 frequency meter, the BC-342, BC-312, and the BC-348 receivers, the BC-412 radar oscilloscope, the BC-645 transmitter-receiver, the BC-946B receiver, the SCR-274N receivers, the SCR-274N transmitters, the SCR-522 transmitter and receiver, the TBY transceiver, the PE-103A dynamotor, and the BC-1068A/1161A receiver. In addition, the book includes an "Electronic Surplus Index", a cross index of A/N tubes and their commercial equivalents, an amateur allocation chart, and a commercial television and FM channel listing.

Complete data is given for each conversion along with the necessary circuit diagram and component changes. A copy of this manual should find a place in every ham shack whose operator is using surplus wartime equipment.

"TELEVISION ENCYCLOPEDIA" by Stanley Kempner. Published by Fairchild Publishing Company, New York. 415 pages. Price \$6.50.

* * *

The need for a definitive work on the subject of television has been known in the industry for some time but it remained for Mr. Kempner to compile this non-technical reference book covering all of the major aspects of video.

The author has gathered together in one small handbook innumerable facts on the television industry including a historical survey of television in the form of a chronological record of its evolution from the earliest research in electronics to the present day; biographical sketches of pioneers and contemporaries in the fields of science, entertainment, information, and commerce who have helped to bring television to its present state; a glossary of technical and trade terms including semi-technical, easily-understod descriptions of the operation, construction, and programming techniques of television; a section on "The Urban Market for Television"; and an extensive television bibliography designed to facilitate research of a more specialized nature.

The encyclopedia is illustrated with historic as well as contemporary photographs.

RADIO NEWS' readers who have enjoyed his articles on television will find the same clarity of presentation in Mr. Kempner's full length treatise on video.

-30-

CUT HOLES 1/2 to 31/2



RADIO CHASSIS PUNCH

• Save hours of work . . . no reaming or tedious filing. Punch cuts through chassis quickly . . . makes accurate, clean holes for sockets, plugs, and other receptacles. Just turn with an ordinary wrench. There's a GREENLEE Punch in each of these sizes: 1/2"; 5/8"; 3/4"; 7/8"; 1"; 11/6"; 11/8"; 15/2"; 13/6"; 11/4"; 13/8"; 11/2"; 21/4". Write for complete facts. Also get information on Knockout Punches and Cutters for conduit and meter holes up to 31/3", Greenlee Tool Co., 1886 Columbia Avenue, Rockford, Illinois.



LAKE SPECIALS

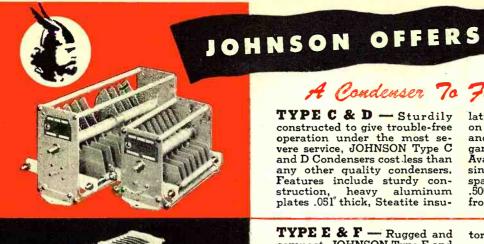
| LARE SPECIALS | |
|---|--------|
| Each | Per 10 |
| Natl, Brand Phono Pickup\$ 1.95 | |
| Natl. Brand Phono Motors 3.65 | 35.00 |
| Gen. Ins. Record Changers | 33.00 |
| 12"x11" | 130.00 |
| 12"X11" | 130.00 |
| Allig. Port Cab. for any changer | |
| 171/2x171/2x10" Cutout for | |
| 6" Spkr 7.95 | 75.00 |
| SPEAKERS | |
| 3" 450 Ohm | 14.00 |
| 4" 450 Ohm | |
| 5" 2750 Ohm or 450 Ohm 1.69 | |
| | |
| 5" PM with 50L6 Transformer 1.39 | 13.00 |
| 6" PM 1.59 | |
| 8" PM-1000 or 1800 Ohm field 3.50 | |
| 5" Permatic Speaker-Special49 12" PM Heavy Duty Alnico-5 5.95 | |
| 12" PM Heavy Duty Alnico-5 5.95 | |
| 12" Dynamic 450 or 1000 Ohm 5.65 | 53.00 |
| PARTS | |
| | |
| 500M Ohm Chgo, Tel. Vol. cont. | |
| & switch | 3.50 |
| & switch | |
| Cond | 3.90 |
| 40x40 Mfd, 150 V Natl, Brand | |
| Cond | 3.90 |
| 40x40 Mfd. 150 V 20 Mfd. 25 V-F.P | |
| 25 V-F.P | 3.75 |
| Universal AC DC Line Cords50 | |
| All other Sizes from 135-350 Ohms .45 | |
| 100' 7x26 Bare Aerial Wire 22 | |
| 70 Mil, Power Transf. 6 Volt 1.95 | 17.50 |
| 40 Mil. 21/2 V. Power Transf85 | |
| | |
| AUTO AERIALS AND SUPP | |
| 68" 3 Section Natl. Brand Aerial. 1.75 | |
| 96" 3 Section Natl. Brand Aerial. 2.50 | |
| 3 Section Univ. Mount 2.25 | |
| Spark Plug Suppressors 10 | .95 |
| Distributor Suppressors .10 Generator Condensers ½ Mfd20 7" Auto 6 Volt Speaker .3.65 | .95 |
| Generator Condensers 1/2 Mfd | 1.95 |
| 7" Auto 6 Volt Speaker 3.65 | 35.00 |
| 7" Auto PM Dvn. Spkr. Heavy | |
| Duty 3 65 | 33.00 |
| Duty 3.65 4 Prong Std. Oak Vibrator 1.39 | 13.50 |
| Sale on Tubes—For Limited Time O | |
| 50-10% Discount on List Prices | of |
| National Brand Tubes! | 01 |
| Mational Brand Lubes! | |

Lake Radio Sales Co

Write for our new 1948 illustrated catalog!

615 W. Randolph Street DEPT. A

Chicago 6, III.

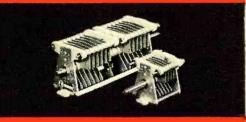


A Condenser 70 Fit Every Need!

TYPE C & D - Sturdily constructed to give trouble-free operation under the most severe service, JOHNSON Type C and D Condensers cost less than any other quality condensers. Features include sturdy con-struction, heavy aluminum struction, heavy aluminum plates .051" thick, Steatite insu-

lation and center rotor contacts on all dual models. Both front and rear shaft extensions permit

Available in 52 different models, single or dual sections, with spacing varying from .175" to .500" and maximum capacities from 50 to 1,000 mmfd.



TYPE E & F - Rugged and compact, JOHNSON Type E and F Condensers for medium and low power transmitters have more capacity per cubic inch and occupy less panel space for their rating than any other condenser on the market. Features include Steatite insulation, sta-

tor mounted above to reduce capacity to ground, front and rear shaft extensions that permit ganging.

Available in 45 different models, single or dual sections, spacing .045" to .125", and maximum capacities from 35 to 500 mmfd.



TYPE G - The JOHNSON Type G Condenser is widely used as a neutralizing condenser for medium and low power stages. It's equally famous for its outstanding performance in grid and plate tuning at high and ultra high frequencies. Features include front and rear

shaft extensions and universal mounting bracket and locking

Available only in single sections with single end plate. Seven models from which to choose. Capacities from 3.5 to 52 mmfd. Plate spacing from .045" to .225".



TYPE H — Combining minimum weight with small size, JOHNSON Type H Condensers are designed especially to withstand heavy vibration. Steatite end plates prevent any possi-bility of "short circuit loops" and permit panel mounting

with both rotor and stator insulated from ground. Aluminum plates are .020" thick. End plates are 1½" square.

Available in 17 different models,

single or dual sections, spacing .030" or .080", and maximum capacities from 25 to 100 mmfd.



TYPE J - A midget condenser with big condenser characteristics, Type J has wider spacing than most small types, yet occupies little more space. It is ideal for oscillator and low power stages. Universal type mounting brackets make possible a variety of mountings in-

cluding chassis, panel or inside tube socket type inductors. Steatite end plate.

Available only in single sections with single end plate. Six different models with maximum capacities from 7 to 102 mmfd. Plate spacing is .025".



MIDGET AIR VARI-

ABLES - Here are three of the smallest air variables ever

produced.
SINGLE TYPE — Available in four models: 1.55 to 5.14 mmf, 1.73 to 8.69 mmf, 2.15 to 14.58 mmf, and 2.6 to 19.7 mmf.

DIFFERENTIAL TYPE - Available in four models: 1.84 to 5.58 mmf, 1.98 to 9.30 mmf, 2.32 to 14.82 mmf and 2.67 to 19.30 mmf. BUTTERFLY TYPE — Available in four models: 1.72 to 3.30 mmf, 2.10 to 5.27 mmf, 2.72 to 8.50 mmf, and 3.20 to 11.02 mmf.



Write For New Complete **JOHNSON** Condenser Catalog

TYPE N - When space is limited, yet you need extremely high voltage rating, fine adjustment with uniform voltage breakdown rating throughout the full capacity range, the JOHNSON Type N Neutralizing Condenser is the perfect answer.

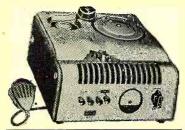
Available in three different models. Capacity range in each type is approx. 1.5 mmfd. to 10.5 mmfd., peak RF breakdown ratings at 2 MC ranges from 8,500 with the N125 to 14,500 for the N375.



JOHNSON...a famous name in Radio E. F. JOHNSON CO., WASECA, MINNESOTA

All Mail Orders Shipped Promptly!

SAVE ON THESE MONEY-SAVING VALUES!



2 TUBE WIRELESS PHONO OSCILLATOR



This fine piece of equipment is being sold at almost the price of the tubes alone. A real bargain while quantity lasts.

Each \$3.25

6 TUBE DETROLA PHONO COM-BINATION AC CHASSIS

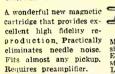
Complete with tubes, speaker, and Completely wired. \$14.95



6 TUBE DETROLA AC-DC CHASSIS Complete with tubes, speaker, antenna, Completely wired. \$9.95

G.E. VARIABLE RELUCTANCE

CARTRIDGE





Made for Models as shown 1-General shown 1-General Electric 2-Clark-stan 3-Pickering 4-Lear. Order by number

Requires preamplifier. \$7.95 List Each

4.67

PREAMPLIFIER FOR G. E. VARIABLE RELUCTANCE CARTRIDGE

RELUCIANCE CA 35x35x416". Increases output, and equalizes cart-ridge for flat response. At-taches easily. Complete with tube and diagram.

4.82 Net, each



List, each \$9.00

WEBSTER CHICAGO MODEL 78 WIRE RECORDER NEW SIMPLIFIED ADAPTER MAKES IT EASY TO CONVERT ANY RADIO INTO A WIRE RECORDER COMBINATION

The Model 78 Wire Recorder is especially adaptable for home use in connection with a radio receiver or with a high fidelity public address type amplifier and speaker. Compact in design with simple push button controls. Model 78 comes complete with necessary cords, plugs, nicrophone, 15-min. spool of wire, and full instructions for easy connection. Head phones may also be used for quiet, private play back of a recording.

List price \$153.00

Net \$158.00 \$99.96

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WEBSTER CHICAGO HIGH QUALITY

| 15 min. spool | \$2,25 ea. | Lots of | 10\$1.30 ea. |
|---------------|------------|---------|--------------|
| 30 min. spool | 3.00 ea. | Lots of | 10 1.95 ea. |
| 1 hour spool | 5.00 ea. | Lots of | 10 3.25 ea. |

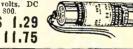
ALL NEW FULLY GUARANTEED STANDARD BRAND TUBES

| | 35Z550c | 826 450 |
|-----|----------|----------|
| | 12A6 | 50L659c |
| - | 50B559c | 1LC697c |
| - 1 | 25L659c | 1LN5 |
| 1 | 6K760c | 1H559c |
| - 1 | 117Z6 | 1A759c |
| - | 117L798c | 50A5 |
| - 1 | 1N5 | 12SQ759c |
| - | 12K759c | 35L659c |
| - 1 | 70L798c | 35W4450 |
| 1 | VT5249e | 0Z4 |
| - | 7N750c | 6N7850 |
| ì | 12BE6 | 59c |
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Vacuum Tube Voltmeter

(Continued from page 60)

These ranges were selected so that the original meter scale, which was calibrated 150 microamperes full-scale with markings at 60 and 90, could be used. This obviated drawing a new scale. The builder has the choice of drawing a new scale or using other voltage dividers to give readings which will correspond to the markings on the scale of the meter being used. It is suggested, however, that a 20-division scale be used, in which case a voltage divider providing readings of 1, 10, 100, and 1000 volts full-scale would be employed. No trouble should be encountered in securing a "low volts" reading of 1 volt full-scale. Refer to Fig. 1 for a diagram of this voltage divider.

The input resistance (Fig. 2) totals 15 megohms which is a practical value for all d.c. voltage measurements. Resistors R_1 through R_4 were mounted directly on the 4-position wafer switch which is used as the voltage range selector. The value for R₁ was made up of a 10 megohm and a 3 megohm resistor which read a little on the high side. R_2 comprised a 1 megohm unit and a 350,000 ohm resistor. R_3 is made up of a 100,000 ohm and a 35,000 ohm resistor, while R₄ is a standard 15,000 ohm unit.

The complete circuit diagram is given in Fig. 2. It will be readily recognized as a balanced bridge type cathode follower. The cathodes of V₁ and V_2 are connected directly to the grids of V_3 and V_4 respectively. Note that the input tube is neither in the bridge nor the meter circuit. V_1 and V_2 are supplied by a very low voltage taken from the bleeder circuit, Ro and R_{10} . Heavy degeneration is developed through their 5 megohm cathode resistors. Their total plate current is of the order of 4 μ a. while the plate current of V_3 and V_4 is approximately 1 ma. The bleeder current is approximately 0.375 ma: with 45 volts of "B" battery.

The circuit is self-explanatory. The only thing to remember is that pins 1 and 7 on the tube sockets must be connected together as these become the positive connections to the batteries. Pins 5 on the tube sockets are connected to negative and these connections are used for the cathode leads.

A small bracket which holds the tube sockets, the calibrating potentiometer, and the resistor strip is bolt-ed to the panel. The resistors are mounted either on the tube sockets or to this resistor strip. The "on-off" d.c. positive and d.c. negative switch is located to the left of the panel and the "zero-adjust" potentiometer is to the right. Below this and in the center is located the voltage range switch. The bottom of the panel carries the jacks for the test leads, the center jack being ground. The jacks shown in the photograph are Amphenol units.

The panel and bracket are constructed out of 1/16" aluminum. A wrin-

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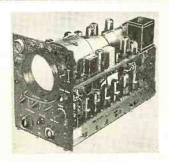
Diag. and Conversions: BC-348, SCR-522, BC-375, SCR-274, SCR-274-10 meter mobile.

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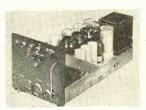
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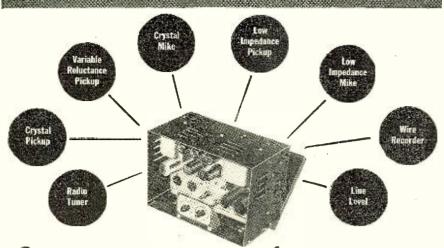
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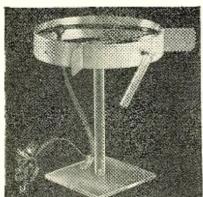
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kle varnish was applied to the panel to give the instrument a professional appearance. Small dials were drawn on a piece of bristol board and then attached to the instrument. The bracket which holds the tubes was laid out in such a manner that the tubes would clear the meter when they were inserted in their sockets.

After all wiring is completed and checked against the circuit diagram the batteries should be soldered or connected in the circuit. Before the tubes are put in the sockets a voltage check should be made with a voltmeter. If everything checks OK, the potentiometer, R_{14} , is set for maximum resistance and the tubes are inserted in the sockets. By adjusting potentiometer R_{13} , located on the front panel, it should now be possible to zero the meter. No deflection of the meter should be noticed when the test leads are shorted. If a noticeable deflection occurs, a different tube should be tried in V_1 . Several tubes of questionable quality were tried in V_1 and showed up defective in this position.

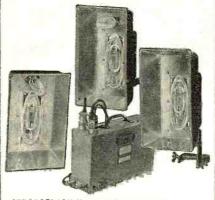
A cabinet was constructed of ¼" plywood to house the instrument and its associated batteries. The cabinet measures 4¼" x 7" x 3¾". Brackets were made to hold the batteries in place. These are mounted on the subpanel in back of the instrument. This sub-panel is mounted to the main panel by means of four ¼" metal spacers, 2%" long.

This v.t.v.m. needs no calibration other than the standard scale divisions. It is advisable to have a scale with at least fifteen divisions so that voltages as small as .1 volt may be read with ease. A new scale may be drawn if the meter being used does not have a suitable one. For extreme accuracy, if a new scale is used, the meter should be calibrated against another meter of known accuracy.

An a.c. probe was constructed for measuring a.c. voltages such as r.f., a.f., and power line. The probe used consisted of a crystal diode, such as the 1N34, and a .02 μfd . mica condenser. (Details for constructing this probe were given in the article, "Sensitive Probe Uses Crystal Diode" by Rufus P. Turner in the May, 1947 issue of RADIO NEWS.) The probe used with this instrument was constructed of bakelite tubing %" i.d. and 3" long. A bakelite disc was inserted at the prod end and the tip of a standard test prod was inserted in the disc. A metal disc was inserted at the other end and to this was attached the spring end of an Amphenol connector. This was soldered to the disc with a piece of single conductor, shielded microphone wire and attached to the Amphenol connector. Measurement of voltages over 50 volts a.c. are not recommended with this probe as the heavier voltages may damage the 1N34.

Just a word about the operation of the instrument. It was found that the "A" batteries weakened first so the instrument should be turned on only when it is in use and turned off as soon as the job is finished.

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| 6F6/[6]369 | 8012 3.93 | 957 |
| 665 /6H5 08 | 8020 4 95 | 958A49 |
| 6G6 1.08 | 900149 | 1614 150 |
| 6H6G48 | 900259 | 1616 2.75 |
| 6H6M68 | 900349 | 161939 |
| 614 1.98 | 900449 | 1622 1.49 |
| 615 | 900649 | 1624 |
| 617 88 | 2 A PI 1 95 | 162539 |
| 6K5G 1.10 | 2APIA 4.95 | 1620 45 |
| 6K6GT74 | 3API 3.25 | 1635 1.90 |
| 6K7 | 3BP1 1.98 | 1641/RK6084 |
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| 6L6 1.24 | 3FP7 2.98 | 205188 |
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| 83V 1.25 | 91P12 3.95 | 49**Box 60 |
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| @12¢ |
| 5AB-800ma, 4, 10 Amp @096 |
| 7AG-200ma, @ 10¢ |
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| @306 |
| TELEPHONE Grasshopper fuse WE 3A |
| @09¢ |
| FUSE HOLDERS LF #1075 for 3AG |
| @ 25¢ |
| FUSE HOLDERS LF #442001 for 4AG |
| @ 30¢4 for [.00 |
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| Dual Mtg @ 20¢ |
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| Rite T'day HEINEMAN CIRCUIT BREAKER 3, 5. 10 & 15, 20, 30, 40, |
| BREAKER 3, 5, 10 & 15, 20, 30, 40, |
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| Heineman Dual 10 Amp \$2.95; |
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| SQ'D KLIXON & CH 5, 10, 20, 25, 33, 35, |
| 60. 70 Amps each 98¢ |
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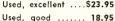
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FAMOUS BC-6 5 9 PORT-A B L E FM TRANSCEIV-ER, 27 to 38.9 Mc, xtal con-trolled; ideal Mc, xtar trolled; idea "hams, for "hams," police, seismograph crews, park service, etc. Battery oper-ated power supply 6, 12 or 24 volt, As mograph or 24 voit. A shown, with all tubes. speaker and meter, less handset & ytals.

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Infinitesimal

(Continued from page 42)

In practical operation the microscope normally is used at magnifications between 5000 and 10,000 diameters. Obtained at such values is the best combination of image brightness, size of the photographic field, and time of photographic exposure. Any desired additional magnification is obtained by photographic enlargement, making possible a much greater total useful magnification of the specimen.

In general, absorption of electrons (from the beam) does not occur in the very small and extremely thin specimens that are usually placed under observation. Occasionally, however, certain types of specimens absorb electrons from the beam and the released energy appears as heat. The temperature of the specimen, itself, may often be raised (in this manner) to such a high degree that decomposition and structural changes take place. As an additional limitation, the electron beam generates sufficient heat to kill all life cells, and then dehydrate the remaining inert mass.

During periods of observation, molecular or chemical changes in the specimen often take place, due to the artificial conditions existing in the vacuum chamber of the microscope.

Such limitations, however, are but

obstacles eventually to be overcome by the scientist and engineer.

It is important to note that it is not always advantageous to use the Electron Microscope, when similar information supplied by the optical or light microscope is sufficiently accurate and adequate. Contrary to sweeping statements circulated by over-zealous press agents, the Electron Microscope has not replaced the light microscope!

A fair consideration of both types of magnifying instruments reveals that they actually supplement each other. For low-order magnification, the light microscope is more versatile, and entirely adequate for many forms of scientific research. When powerful magnification is required, the Electron Microscope can be depended upon to supply finely focused images of high resolution. The amount of magnification plus resolution required are the determining factors as to which of the two types of microscopes to use. Thus, there is a place in science for both instruments.

The precise ability to probe the submicroscopic—at high magnifications with high resolution-identifies the scientific importance of the Electron Microscope. It makes visible many objects which have never before been seen, bringing a new depth of vision to science and industry alike, helping to improve the way of life for all man--30-

NEW YORK TV OWNERSHIP

THE research division of WPIX, New York has just released some interesting figures regarding television receiver ownership in the New York area.

The study reveals that nearly three out of four sets are in the homes of families with modest incomes. Distribution of 31,755 home receivers in the New York viewing area was studied and 53 per-cent of the sets were found to be in New York City with 47 per-cent installed in the suburbs.

When the New York City list was analyzed as to the neighborhoods in which the set owners lived, WPIX discovered that only 26.5 per-cent of the sets were in the higher income localities. The remainder were in homes that made up the middle, lower middle, and poor income neighborhoods.

Brooklyn leads the list with 41.6 per-

cent of the City total yet that borough has not a single high income district, according to the survey. Sets in the middle and lower income groups in this borough outnumbered those in the middle income group by six to one.

By income levels, the survey found that 12.5 per-cent of the sets were in high income districts and 14 per-cent in the upper middle income neighborhoods throughout the city. The great bulk of the sets, 60 per-cent, were found in the middle income level and the two lowest income groups accounted for more home sets than did the highest, according to the survey.

Thus, 26.5 per-cent of the television receivers were installed in upper middle and high income homes while over 73 per-cent were to be found in middle, and poor income districts. -30

GOPHER HAMFEST

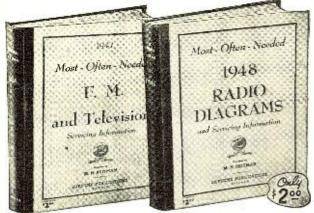
⊓HE St. Paul and Minneapolis Radio Clubs are sponsoring their first postwar Gopher Hamfest on June 18 and 19 at the Nicollet Hotel in Minneapolis.

A special program has been planned featuring the best in technical talks and prizes. An amateur contest, put on by the Dakota Division Radio Clubs, has been scheduled for the entertainment at the turkey dinner to be held Saturday night.

Advanced registration fee (By June 14th) is \$5.00 with late registrants paying \$5.50 for their admission. Ladies will be admitted for \$3.50. Free rooms at hams' homes for advance registrants will be provided if requested.

For tickets and further information write to Gopher Hamfest, Box 685, Minneapolis, Minnesota.

-30-



F.M. and Television

Use this new giant manual of factory instructions for trouble-shooting, repairing, and alignment of any 1947-1948 F.M. and Television set. Every popular make, including new F.M. tuners, AM-FM combinations, and all types of television receivers. Detail circuit diagrams, theory of operation, test hints, alignment data, including both meter and oscilloscope methods. This is the material you need to fix any modern F.M. or Television set. Don't turn this profitable work away for lack of knowledge and information. Use this newest Supreme manual to save time and money on your very next F.M. job. Data presented on 192 large pages, 8½x11 in. Sturdy, manual-style 500 lished. Special price.

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New 1948 and F.M. Manuals

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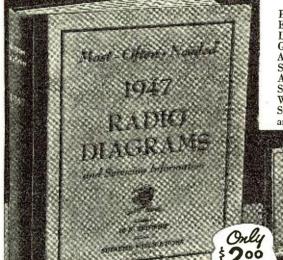
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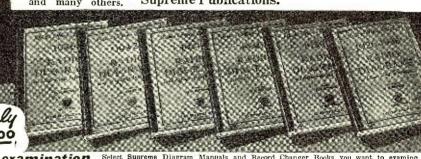
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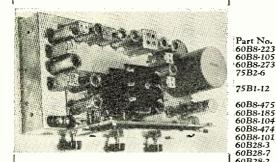
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60B8-333 60B8-473 64B1-12

65B6-4 64B1-30 A1341 64B1-14 64B1-25

64B1-22

65B6-18 64B1-23 64A2-2 64B1-15 67A14-1

65B6-6 Part of L1

69B13 69A14 72B3 72B4 98A33-10

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60B8-475 60B8-224

60B8-474 60B8-151 60B8-154

67A10 64A2-2 64B1-22 64B1-12

68A18 69C44 69A43 98A4 72B50 72B51

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Parts List

FOR CIRCUIT DIAGRAMS APPEARING ON PAGES 94 and 95

| | | | . , . |
|--------------|--|------------------------------|--|
| ADA | IIRAL MODEL 7C60 | 100-71 | C_{10} —.004 µfd., 600 v. cond. C_{11} —500 µµfd. mica cond. C_{12} —.02 µfd., 400 v. cond. C_{13} —.05 µfd., 400 v. cond. C_{14} —40/20 µfd., 150/150 v. |
| TLD. | | 129-2 | C11-500 µµfd. mica cond. |
| , | Code and Description | 100-26 | C_{12} —.02 $\mu fd.$, 400 $v.$ cond. |
| ' | R ₁ -22,000 ohm, ½ w. res. R ₂ -1 megohm, ½ w. res. | 100-13 | C ₁₃ —.05 µfd., 400 v. cond. |
| 3 | R ₂ —1 megohm, ½ w. res. R ₃ —27,000 ohm, ½ w. res. R ₄ —1 megohm vol. control & | 119-92 | C_{14} —40/20 $\mu fd.$, 150/150 $v.$ |
| | R4-1 megohm vol. control & | 126.10 | etec. cona. |
| | sw. (tappea at 300,000 onns) | 136-18 | T ₁ —Complete permeability tun- |
| | R ₅ , SW ₁ -2 megohm tone con- | 108-157-H | ing unit To—Input i.f. coil with trimmere |
| _ | trol & sw. | 108-157-0 | T ₂ —Input i.f. coil with trimmers T ₃ —Output i.f. coil with trim- |
| | R ₆ —4.7 megohm, ½ w. res. | 200-131-0 | mers |
| ? | R7—1.8 megonm, ½ w. res. | 105-139 or | |
| | R ₀ -100,000 ohm, 72 to res | C-12C-11763-3 | T ₄ —Output trans. T ₅ —4 in. PM speaker |
| ; | R ₁₀ —100 ohm. ½ w. res. | 114-268 | T ₅ -4 in. PM speaker |
| • | R ₅ —4.7 megohm, ½ w. res. R ₇ —1.8 megohm, ½ w. res. R ₈ —100,000 ohm, ½ w. res. R ₉ —470,000 ohm, ½ w. res. R ₁₀ —100 ohm, ½ w. res. R ₁₁ —33 ohm, 1 w. res. R ₁₂ —220 ohm, 1 w. res. R ₁₃ —1000 ohm, ½ w. res. | | |
| | R ₁₂ -220 ohm, 1 w. res. | WARDS | MODEL 74BR-2707A |
| | R ₁₃ —1000 ohm, 1 w. res. | Part No. | Code and Description |
| f | R ₁₄ —150,000 ohm, ½ w. res. R ₁₅ —22,000 ohm, ½ w. res. R ₁₆ —10 megohm, ½ w. res. | C-9B1-21 | R ₁ -22.000 ohm. ½ w. res. |
| 3 | R_{15} —22,000 ohm, $\frac{1}{2}$ w. res. | C-9B1-21 C-9B1-31 | R ₁ -22,000 ohm, ½ w. res. R ₂ , R ₁₀ -1 megohm, ½ w. res. |
| 2 | R ₁₆ —10 megohm, ½ w. res. | C-9B1-52 | R3-150 ohm, 1/2 w. res. |
| 1 | | C-9B2-79 | R ₄ -27,000 ohm, 1 w. res. |
| , | P. 32 000 ohm 1/2 w res | C-9B1-17 | R ₅ -4700 ohm, ½ w. res. |
| , | R ₁₈ —100,000 ohm, ½ w. res. R ₁₉ —33,000 ohm, ½ w. res. (UL models only) | C-9B1-11 | R ₈ -470 ohm, ½ w. res. |
| 3 | R ₂₀ —47,000 ohm, ½ w. res. C ₁ —.005 µfd., 600 v. cond. | C-9B4-76 | R ₇ —15,000 ohm, 2 w. res. |
| | C_1 —.005 $\mu fd.$, 600 $v.$ cond. | C-9B1-19 C-9B1-62 | R ₈ —10,000 onm, ½ w. res. |
| | (early models only) | C-9B1-02 C-9B2-15 | Ry Ry 2200 ohm 1 su res |
| | C ₂ —50 μμfd. ceramic cond. | C-9B1-31 | R ₁ , R ₁₀ —I megohm, ½ w. res. R ₁ —150 ohm, ½ w. res. R ₁ —27,000 ohm, ½ w. res. R ₂ —4700 ohm, ½ w. res. R ₃ —4700 ohm, ½ w. res. R ₄ —15,000 ohm, ½ w. res. R ₅ —10,000 ohm, ½ w. res. R ₅ —10,000 ohm, ½ w. res. R ₄ —1000 ohm, ½ w. res. R ₅ —1000 ohm, ½ w. res. R ₁₁ , R ₁₅ —2200 ohm, I w. res. R ₁₂ , R ₃₅ , R ₄₃ —I megohm, ½ w. res. |
| | C ₂ —50 µµfd. ceramic cond. C ₃ , C ₁₆ , C ₂ —.1 µfd., 200 v. cond. C ₄ a, C ₄ b—Two-section gang | | res. |
| | C ₁ a, C ₄ b—I wo-section gang | C-9B1-48 | R ₁₃ , R ₁₆ —68 ohm, ½ w. res. R ₁₄ , R ₁₇ —39,000 ohm, 1 w. res. |
| | C_5 —.002 $\mu f d$., 600 v . cond. C_6 , C_9 , C_{15} —.01 $\mu f d$., 400 v . | C-9B2-81 | R14, R17-39,000 ohm, 1 w. res. |
| | C_6 , C_9 , C_{15} —.01 μfa ., 400 V . | C-9B1-13 | Ru-1000 ohm 1/2 tu res. |
| | C ₇ , C ₁₂ , C ₁₄ , C ₂₀ —.05 µfd., 400 | C-9B1-23 | R ₁₉ —47,000 ohm, ½ w. res. R ₁₉ —27,000 ohm, ½ w. res. R ₂₁ —3.3 megohm, ½ w. res. R ₂₁ —22,000 ohm, ½ w. res. |
| | v. cond. | C-9B1-79 | R_{10} —27,000 ohm, $\frac{1}{2}$ w. res. |
| | Co-15 unfd, ceramic cond. | C-9B1-34 | R ₂₁ —3.3 megonm, ½ w. res. |
| | C_{10} —.03 $\mu fd.$, 400 $v.$ cond. | C-9B1-78 C-9B1-80 | Res Res 33 000 ohm 1/2 w ret |
| | C_{11} —.18 $\mu fd.$, 200 $v.$ cond. | C-9B1-30 C-9B1-29 | R_{23} , R_{28} —33,000 ohm, $\frac{1}{2}$ w. res. R_{24} , R_{26} , R_{37} —470,000 ohm, $\frac{1}{2}$ |
| | C_{13} —.001 $\mu fd.$, 600 $v.$ cond. | C-9B1-29 | w. res. |
| | C ₁₀ 03 µfd., 400 v. cond. C ₁₁ 18 µfd., 200 v. cond. C ₁₃ 001 µfd., 600 v. cond. C ₁₇ -, 30/30/20/20 µfd., 150/150 | C-9B1-302 | R25-15 megohm. 1/2 w. res. |
| | /150/25 v. elec. cona. | A-10A-13001 | R ₂₅ —15 megohm, ½ w. res. R ₂₇ —400,000 ohm vol. control |
| | C18-250 µµfd. ceramic cond. | | (8 su). |
| | C ₁ 9—.02μfd., 400 v. cond. (UL models only) | C-9B1-94 | R ₂₉ , R ₄₄ —470,000 ohm, ½ w. res. R ₃₀ —4.7 megohm, ½ w. res. R ₃₁ —500,000 ohm tone control |
| | C21-50 µµfd. ceramic cond. | C-9B1-35 | R ₃₀ 4.7 megohm, ½ w. res. |
| 1 | C23-3-30 µµfd. trimmer (late | A-11A-12988 | R ₃₁ —500,000 ohm tone control |
| • | models only) | C-9B1-86 | & radio-phono sw. |
| | L ₁ —Loop antenna | C-9B1-68 | R ₃₂ —100,000 ohm, ½ w. res. R ₂₃ , R ₃₄ —3300 ohm, ½ w. res. R ₃₆ , R ₄₂ —51,000 ohm, ½ w. res. |
| | L ₂ —Osc. coil | C-9B1-200 | R36, R42-51,000 ohm. 1/2 w. res. |
| | T ₁ —First i.f. trans. | C-9B4-55 | R ₃₈ -270 ohm, 2 w. res. |
| Δ. | T ₂ —Second i.f. trans. | C-9B1-83 | Rss. Rs.—56.000 ohm. ½ w. res. |
| · · | T ₃ -Output trans. | C-9B1-66 | R40-2200 ohm, 1/2 w. res. |
| | | C-9B1-50 | R45-100 ohm, 1/2 w. res. |
| IANTO | LA MODELS 92503 92504 | C-9B1-42 | R ₄₀ —2200 ohm, ½ w. res. R ₄₅ —100 ohm, ½ w. res. R ₄₅ —22 ohm, ½ w. res. R ₄₇ —5600 ohm, ½ w. res. |
| | Code and Description | C-9B1-81 | K17—5000 ohm, ½ w. res. |
| 3 | R_1 —22,000 ohm, $\frac{1}{2}$ w. res. | C-8G-11732 C-8G-13695 | C ₁ , C ₁₁ —470 μμ ₁ α. conα. |
| 3 5 5 | R2-1 megohm, 1/2 w. res. | C-8G-11484 | C ₂ -1000 µµfd. cond. C ₃ -50 µµfd. cond. |
| ? | R ₃ -4.7 megohm, ½ w. res. R ₄ -220,000 ohm, ½ w. res. R ₅ -470,000 ohm, ½ w. res. | C-8G-13018 | Ci-62 uufd. cond. |
| \$ 4 | R470 000 ohm 1/2 w. res | C-8D-11304 | C ₁ -62 \(\mu\)fd. cond. C ₅ 02 \(\mu\)fd., 200 \(\nu\). cond. C ₆ , C ₇ , C ₉ , C ₁₄ , C ₅₁ , C ₅₅ -1000 |
| 1 | Rs—150 ohm. 1/2 w. res. | C-8G-13201 | C ₆ , C ₇ , C ₉ , C ₁₄ , C ₅₁ , C ₅₃ —1000 |
| 4 | R ₅ —150 ohm, ½ w. res. R ₇ —150,000 ohm, ½ w. res. | | uutd. cond. |
| • | R8-1 megohm vol. control & sw. | C-8G-11789 | C ₈ —10 μμfd. cond. C ₁₀ —15 μμfd. cond. |
| | R ₉ 33 ohm, 1 w. res. | C-8G-13017 | C 1500 d d |
| | R ₁₀ -1000 ohm, 1 w. res. | C-8G-11731 | C ₁₂ —1500 µµfd. cond. |
| | C ₁ —1000 thin, 1 w. res. C ₁ —1 μfd., 200 v. cond. C ₂ —50 μμfd. mica cond. C ₂ —02 μfd. 400 v. cond. | A-8G-12495-6 A-8G-12495-4 | C ₁₃ —4.7 µµfd. cond. C ₁₅ —2.2 µµfd. cond. C ₁₆ —51 µµfd. ceramic cond. |
| | C ₂ —50 μμfd. mica cond. | C-8G-13026 | C ₁₆ —51 uufd. ceramic cond. |
| | | C-8G-12159 | C17, C25, C26-20 µµfd. ceramic |
| | C ₈ —250 uufd, mica cond. | | cond. |
| | C ₄ , C ₅ —.01 μfd., 400 v. cond. C ₆ —250 μμfd. mica cond. C ₇ —500 μμfd. mica cond. | C-8G-12160 | C18, C19-91 µµfd. ceramic cond. |
| | C ₈ 02 µfd., 400 v. cond. | C-8D-11734 | C20, C23, C24, C30, C31, C43, C44— |
| | C ₂ 02 µfd., 400 v. cond. C ₂ 50/30 µfd., 150/150 v. elec. | C-8G 11724 | .006 µfd., 600 v. cond. |
| | cond. | C-8G-11734 C-8D-10761 | C ₂₁ —100 µµfd. ceramic cond. C ₂₂ , C ₂₉ —.01 µfd., 400 v. cond. |
| | C ₁₀ —18 µfd., 200 v. cond. C ₁₁ —.05 µfd., 400 v. cond. C ₁₂ —.005 µfd., 600 v. cond. | C-8G-13025 | C27, C28—150 µµfd. ceramic |
| | C ₁₂ — 005 ufd 600 v. cond | J 0 | cond. |
| | (early models only) | C-8G-11789 | C32-10 µµfd. ceramic cond. |
| | C13-Two-gang cond. | C-8G-11891 | C ₃₃ —51 µµfd. ceramic cond. |
| | C ₁₃ —Two-gang cond. L ₁ —Loop antenna | C-8G-13060 | C ₃₄ —51 μμfd. ceramic cond. C ₃₅ , C ₃₆ —50 μμfd. dual mica |
| | L2—Osc. coil | A-8F-13047 | cond μμja. auai mica |
| | L_2 —Osc. coil T_1 —Output trans. T_2 —First i.f. trans. T_3 —Second i.f. trans. | C-8F-229 | cond. C ₃₇ —150 μμfd. mica cond. |
| | T2-First i.f. trans. | C-8G-13059 | C ₃₈ —1500 µµfd. ceramic cond. |
| | 13—Secona 1.j. trans. | C-8G-13201 | C39, C40-1000 µµfd. ceramic |
| ***** | (O) 7 (O) 7 (O) 7 (O) 10 (O) 1 | | cond |
| BELM | ONT MODEL A-5D118 | A-8C-13132 | C ₄₁ —10 µfd., 50 v. elec. cond. C ₄₂ —.02 µfd., 200 v. cond. C ₄₅ , C ₄₈ —.05 µfd., 400 v. cond. |
| • | Code and Description | C-8D-11304 | C ₄₂ —.02 μfd., 200 v. cond. |
| 8 | R ₁ —22,000 ohm, ½ w. res. | C-8D-10813 | C ₄₅ , C ₄₆ —.υ ₅ μ _j α., 4υυ v. conα. |
| | R ₂ , S ₁ —500,000 ohm vol. control | C-8D-10760 C-8D-10770 | C ₄₈ , C ₄₆ , C ₃₀ µ _{fd} , 400 v. cond. C ₄₈ , C ₅₄ , C ₁₀ , 200 v. cond. C ₄₈ , 002 µ _{fd} , 200 v. cond. C ₄₉ , 002 µ _{fd} , 600 v. cond. C ₅₀ , 330 µ _{fd} , ceramic cond. |
| 4 | 8 sw. | C-8D-10770 C-8D-10789 | C49002 ufd 600 v. cond. |
| 4 5 | R ₃ —3.3 megohm, ½ w. res. R ₄ —4.7 megohm, ½ w. res. | C-8G-11741 | C50-330 µµfd. ceramic cond. |
| 6 | R ₅ , R ₈ —150,000 ohm, ½ w. res. | C-8D-13439 | C ₅₂ 25 µfd. 400 v. cond. |
| | R ₆ -220,000 ohm, ½ w. res. | A-8C-12154 | C5225 µfd. 400 v. cond. C55-10 µfd., 450 v. elec. cond. C56, C57, C59, C60, C61-Plate |
| 27 2 3 | R ₇ —150 ohm, ½ w. res. | A-2M-12518 | C56, C57, C59, C60, C61-Plate |
| 3 | R ₉ —1200 ohm, 1 w. res. | 4 OF 1255 | trimmer cond. |
| | R_{10} —33 ohm, 1 w. res. | A-8E-13575 | C ₅₈ —Trimmer cond. |
| 3 | R_{11} —27 ohm, $\frac{1}{2}$ w. res. | C-8J-11321 B-8C-11629 | C_{62} —.02 μfd ., 600 ν . cond. C_{63} —30/30 μfd ., 450/450 ν . |
| | C ₁ —Antenna plate C ₂ —300 unitd, mica cond. | B-8C-11629 | elec. cond. |
| | C ₂ —300 µµfd. mica cond. C ₃ , C ₆ —Dual trimmer | | T ₁ -Power trans. |
| | C_4 —.05 μ fd., 200 v . cond. | B-12C-13042 | T2-Output trans. for speaker |
| | C ₅ —50 uufd. mica cond. | C-13A-13009-1 | T ₃ —Input i.f. trans. |
| | C_7 —.15 $\mu fd.$, 400 $v.$ cond. | C-13B-13014-1 | T.—Outbut i.f. trans. |
| | Cs-250 µµfd. mica cond. | C-203-11745-1 | T ₅ —Ratio det. coil assembly |
| | 0. 250 //// | | |
| | C ₉ 002 µfd., 600 v.cond. | B-13E-13028 | T ₆ —FM antenna coil assembly |
| | C ₉ —.002 µfd., 600 v.cond. | | T ₆ —FM antenna coil assembly RADIO NEWS |

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| L6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | ea. | 39 | c |
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39 12B6GT
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231.6GT/G
251.5GGT/G
252.5GGT/G
252.5GGT/G
252.5GGT/G
35.5GGT/G
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35.44
352.3
352.3GT/G
352.3GT/G
35.39/44
41
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50A5
50L6GT
56
57
50L6GT
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57
77
88
77
89
99
11726GT/G
182B
1231
16644 6A K5 6B7 6C4 6C5GT 6C5MG 6C6 6C8G 6D6 6F5 6F6GT /G 6J5GT/G 617GT 29 45 53 45 39 45 20 76 89 29 29 6K6GT/G 6K7G 6K7GT/G 6K8G 6L6G 6Q7GT 6R7 6R7GT 49 39 37 45 39 32 37 39 47 47 39 39 6SA7 6SA7GT/G

B-13E-13031 B-13D-13027 B-13D-13030 B-13C-13029 B-13C-13032 AM antenna coil assembly T:—AM antenna coil assembly
T:—FM osc. coil assembly
T:—FM r.f. coil assembly
T:—FM r.f. coil assembly
T:—AM osc. soil assembly
T:—AM osc. shunt coil ass'bly
L:—Choke coil assembly
L:—Broadcast loop antenna B-13D-12974 A-16A-13033 A-16A-13243 B-14MA-11066-5 EMERSON MODEL 508

Code and Description

R1—100,000 ohm, 1/4 w. res.

R2, R6—1 megohm, 1/4 w. res.

R3—3 megohm vol. control

R4—10 megohm, 1/4 w. res.

R5—4.7 megohm, 1/4 w. res.

R5—4.7 megohm, 1/4 w. res.

R5—4.7 megohm, 1/4 w. res.

R6—10,000 ohm, 1/4 w. res.

R1—820 ohm, 1/4 w. res.

R1—1000 ohm, 1/4 w. res.

R1—10000 ohm, 1/4 w. res.

R1—10000 ohm, 1/4 Part No. 320970 321210 390040 321450 321370 321330 310730 340470 900140 or 900120 920120 cond.
C₃, C₁₂—.0001 μfd.ceramiccond.
C₁₀—.001 μfd., 100 v. cond.
C₁₁, C₁₃—.003 μfd., 150 v. cond.
C₁₄—.0002 μfd. cond.
C₁₄—.0002 μfd. cond.
C₁₇—8 μfd., 100 v. elec. cond.
L₁—Loop antenna
SP₁—PM speaker
T₁—First i.f. trans.
T₂—Second i.f. trans.
T₃—Output trans. (for speaker 180002)
T₁—Output trans. (for speaker 180002) 928010 920130 920140 910110 or 928020 925070 700030 180002 or 180020 720240 720260 734090 T_3 T₃—Output trans. (for speaker 180020)
T₄—Osc. coil 734204 716040

CROSLEY MODEL 56TP-L

Code and Description

1—Type 47, 6.3 v. dial light

2—Cable and plug assembly

3—Antenna loop assembly

4—Antenna coil assembly

5A,5B—Two-sect.coil assembly

6—Firet if, trans. Part No. W-48858 C-132300-1 AC-134605 AW-134993 AW-134965 AW-q34158 B-134995 6—First i.f. trans.
7—Second i.f. trans.
8A, 8B, 8C—Two-section var.
cond. with trimmer

9B-Two-sect. AB-134982 trimmer GC-210685-143 B-226638-55 39001-65

39001-67 39001-73 39001-10 W-134988 39001-63

cond. with trimmer
9A, 9B—Two-sect. trimmer
cond.
10—580 μμfd., 300 v. mica cond.
11—50 μμfd., 50 v. mica cond.
12, 14—05 μfd., 200 v. cond.
13—11 μfd., 200 v. cond.
15—250 μμfd., 500 v. mica cond.
16, 23—3300 μμfd., 600 v. cond.
17A, 17B—60/20 μfd., 150/100 v. elec. cond.
18, 19, 20—022 μfd., 200 v. cond.
22—075 μfd., 200 v. cond.
22—075 μfd., 200 v. cond.
24—100 ohm, ½ w. res.
25—330,000 ohm, ½ w. res.
26—15 megohm, ½ w. res.
27—22,000 ohm, ½ w. res.
31—47,000 ohm, ½ w. res.
31—47 megohm, ½ w. res.
32, 33—470,000 ohm, ½ w. res.
34—150 ohm, ½ w. res.
34—150 ohm, ½ w. res.
36—470 ohm, ½ w. res.
37—1200 ohm, ½ w. res.
38A, 38B, 38C, 38D—Fo ur-section band change sw.
39A, 39B—1 megohm vol. control & sw.
41—Antenna trimmer
42—Tone control sw.
43—Output trans. 39001-65 39281-7 39281-28 39281-38 39281-21 39281-34 39281-23 39281-35 39281-29 39281-8 39281-11

39015-26 B-134720 C-46846-6

41—Antenna trimmer 42—Tone control sw. 43—Output trans. Part of 3 W-134939 B-134940

43—Output trans.
44—Phono motor & spindle assembly
46—Tone arm & cartridge a'by
47—Speaker
49—47 ohm, I w. res. C-134724

B-135023 W-137367

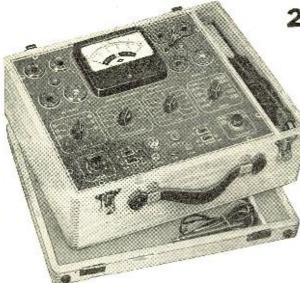
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- Tests all tubes including 4, 5, 6, 7, 7L, Octals, Loctals, Television, Magic Eye, Thyratrons, Single Ended, Floating Fila-ment, Mercury Vapor Rectifiers, New Miniatures, etc. Also Pilot Lights.
- · Tests by the well-established emission method for tube quality, directly read on the scale of the meter.
- Tests leakages and shorts of any one element against all elements in all tubes.
- · Tests both plates in rectifiers.
- Tests individual sections such as diodes, triodes, pentodes, etc., in multi-purpose
- New type line voltage adjuster.

Model 777 operates on 90-120 Volts 60 cycles AC. Housed in beautiful hand-rubbed cabinet. Complete with fest leads, tubes, charts and detailed operating instructions. Size 13" x 121/2" x 6".

V.O.M. SPECIFICATIONS:

- DC Volts: (at 20,000 Ohms per Volt) 0 to 7.5/15/75/150/750/1,500 Volts
- · AC VOLTS: (At 10,000 Ohms per Volt) 0 to 15/30/150/300/1,500/3,000 Volts
- DC CURRENT: 0 to 1.5/15/150 Ma. 0 to 1.5 Amperes
- RESISTANCE: 0 to 5,000/50,000/500,000 Ohms. 0 to 50 Megohms
- DECIBELS: (Based on zero decibels equals .006 Watts into a 500-Ohm line.) -10 to + 18 db., + 10 to + 38 db.,+30 to + 58 db.

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The New Model 650 SIGNAL GENERATOR



RANGE 100 Kilocycles to 105 Megacycles

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- ★ Audio Modulating Frequency-400 cycles pure sine wave-less than 2% distortion.
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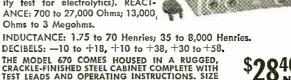
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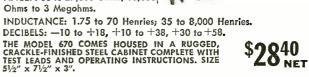
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The New Model 670 SUPER METER

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D.C. VOLTS: 0 to 7.5/15/75/150/ 750/1500/7500. A.C. VOLTS: 0 to 15/30/150/300/1500/3000 Volts. OUTPUT VOLTS: 0 to 15/30/150/ 300/1500/3000. D.C. CURRENT: 0 to 1.5/15/150 Ma.; 0 to 1.5 Amps. RESISTANCE: 0 to 500/100,000 ohms, 0 to 10 Megohms. CAPACITY: .001 to .2 Mfd., .1 to 4 Mfd. (Quality test for electrolytics). REACT-ANCE: 700 to 27,000 Ohms: 13,000, Ohms to 3 Megohms.







The New Model 247 TUBE TESTER

Features: Incorporates a newly designed element selector switch which reduces the possibility of obsolescence to an absolute minimum. Any pin may be used as a filament pin and the voltage applied between that pin and any other pin, or even the "top-cap."

New free-point system permits the Model 247 to overcome the difficulties encountered with other emission type tube testers when checking Diode, Triode and Pentode sections of multi-purpose tubes, because sections can be tested individually when using the new Model 247. The special isolating circuit allows each section to be tested as if it were in a separate envelope.

The Model 247 provides a super sensitive method of checking for shorts and leakages up to 5 Megohms between any and all of the terminals. Continuity between various sections is individually indicated.

One of the most important improvements, we believe, is the fact that the

One of the most important improvements, we believe, is the fact that the 4 position fast-action snap switches are all numbered in exact accordance with the standard R. M. A. numbering system. Thus, if the element terminating in pin No. 7 of a tube is under test, button No. 7 is used for that test. Model 247 comes complete with new speed-read chart. Comes housed in handsome, hand-rubbed oak cabinet sloped for bench use. A slip-on portable hinged cover is included for outside use. Size 10 % " x 8 % " x 5 % ".

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108

Industrial Electronics

(Continued from page 59)

controlled in an electrical circuit. For example, simple on-off switches and small potentiometers in the grid circuits of tubes can control extremely large amounts of power. The speed and direction of large electronically controlled motors supplying many horsepower may be regulated by a compact control station containing simple push-button switches and small potentiometers, situated at any distance from the motor and the main control circuit. Other types of remote controls, such as servo systems and pulsing drive systems, have been of considerable value in the control of such industrial equipment as conveyors, cranes, drilling and tapping machines, engine lathes, laundry machines, knitting and winding machines, printing presses, and wherever else accurate remote control is needed.

(7) One of the new and increasingly important fields of application of industrial electronics is in the non-destructive testing of materials. The requirements of competition in sales and production, emphasizing the need for reliability and dependability of the product, have demonstrated the importance of rapid and reliable methods of testing important and critical parts, and have been an outstanding incentive to the development of such types of tests. In the past, large quantities of material in many processes could be tested for certain properties only by testing suitably chosen samples of the entire lot, because of the destructive nature of the test itself. The application of electrical and magnetic principles has made it possible in many cases to perform non-destructive total inspection of the entire quantity as a simple routine procedure. Some of these methods have played an important part in the success of certain types of engineering activities. For instance, the reliability of aviation engines and parts is due to a great extent to magnetic test methods which have prevented defective parts from being placed in service, while x-ray radiography may be said to have been the turning point in sound and reliable welding. Electronic methods are also widely employed in the measurement of dimensions, displacement, velocity, acceleration, fluid flow, pressure, temperature, illumination, and other factors. Many manufacturers who originally started using such inspection methods because of government requirements, have learned its value and will continue using it for the information it provides, enabling them to improve quality, reduce costs, and budget labor more ade-

(8) Another important phase of elec-June, 1948

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tronic technique which is of tremendous importance to almost every branch of industry is the use of electronics to improve industrial safety equipment. Electronic circuits are used in safety control devices to indicate when plant equipment is operating under unsafe conditions and to stop or slow down the equipment until safe operating conditions are restored. For example, equipment can be protected against operating speeds which are too great, and furnaces against temperatures which are too high. In the use of safety equipment for protecting workers from being hurt by industrial machinery, one of the most important considerations is whether the machine operator will cooperate in its use. Since photoelectric equipment is simple and rugged, and interrupting a light beam requires little physical effort or even conscious thought, it will remain operative where thoughtless operators might be tempted to bypass devices requiring more strenuous effort. This application of electronics in promoting greater safety for industrial personnel and equipment pays high dividends in preventing costly damage to expensive plant equipment and in the protection of employes from accidents.

It is well known to every radio technician that in addition to their desirable properties, electron tubes have certain undesirable characteristics. These characteristics can be decided drawbacks when tube circuits are used for industrial applications, unless they are carefully taken into account. Experience has shown that as far as their practical effect upon a desired result is concerned, most of these faults may be largely eliminated by careful choice of the circuits in which the tubes are used. The cir-

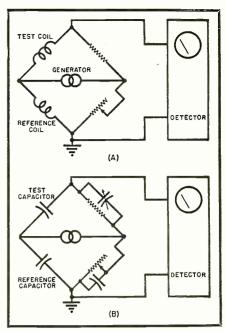
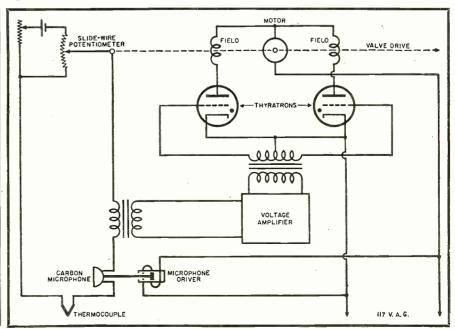


Fig. 7. (A) Basic type of circuit to measure core loss and inductance for the inspection of metal objects inserted in a test coil. (B) Circuit to measure resistivity and power factor for the inspec-tion of dielectric objects inserted in test condenser. (See text for explanation).

cuits must be engineered so that the results are not affected by normal variations in the operating characteristics and possible slow changes in some of the parameters in regular operation. There are a few basic principles which have been found useful in helping to choose circuits in such a manner as to reduce considerably most of the noticeable effects of aging and other normal circuit variations. The fewest possible number of tubes should be used as the controlling elements. A "feedback" circuit in which the result is compared to the

Fig. 8. Temperature control circuit using motor-balanced thermocouple-potentiometer.



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NEW...Sensational TRANSVISION Development now offers LARGE-IMAGE DIRECT-VIEW TELEVISION at low cost!

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Roto-picture effect: Picture "rotates," giving the appearance of being in focus and clearly visible from every angle! Uses 10" Electromagnetic Direct-view Picture Tube.

Features new-type cabinet with built-in lens which magnifies, clorifies and heightens contrast of the picture. The lens also creates the effect of apparent rotation of the picture, so that when the observer moves, the picture still seems to be in focus and clearly visible from any angle.

ECONOMICAL KIT, EASY TO ASSEMBLE. In point of value, this Television Kit provides the opportunity of acquiring a LARGE-IMAGE direct-view television set at a VERY LOW PRICE; also very economical from a tube replacement angle. This model is available in KIT FORM, for easy assembly; no technical knowledge required. Simple step-by-step instructions are included. Saves as much as 50% over the cost of receivers with similar picture magnitude.

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- Uses 7" Electrostatic Picture Tube
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FEATURES: Though it has a 7" tube, the effect is equivalent to a 10" set because the built-in lens magnifies the picture. Also picture performance is superior because the lens clarifies and heightens contrast of the image. Picture "rotates" apparently, as the observer moves, giving the effect of always facing the observer. This is effective to a very wide angle. Pre-tuned for

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cause should be used whenever the tube circuit is to regulate power flow to some device. Wherever possible, steps should be taken to insure that grid circuit voltages change at a high rate over wide ranges at the instant that control of the tube is required. Thus, saturating transformers providing peaked voltages, or capacity-coupled circuits or some other expedient, according to the need, should be provided Since tubes may respond almost instantaneously, the most careful construction and layout of parts to obtain minimum intercircuit coupling, together with careful shielding and filtering is essential in order to avoid difficulty due to stray transient voltages.

The most important principle which applies to the use of electronic controls is that each application must be studied individually and an individual control system designed for each installation. In the setting up and installation of systems, as well as for spares and renewals, the individual components of the system should be checked carefully for each of the following points:

- 1. Reliability of the manufacturer of the control device, and of the service agreement offered.
 - 2. Simplicity of the device.
- 3. Whether or not the device employs up-to-date tubes.
- 4. Operation limits, such as temperature and vibration, of the device. These should be compared with the actual conditions of installation.
- 5. Cost of renewal tubes and sources from which they are available.
- 6. Whether or not the device serves a function which only electron tubes can perform. Often a simpler, mechanical or non-electronic device is available which requires less maintenance time and ex-
- 7. Power handling capacity of the relay, if it is a relay device, should be compared with the actual load to be imposed on it.
- 8. Efficiency of the device. Tubes and lamps age gradually before final failures. Lenses and mirrors may not always be as efficient as when new and clean. Atmosphere may be full of fine dust.
- 9. Grade of insulation on low-power circuits. Moisture must be considered. For example, a phototube passes only a few microamperes, hence any leakage because of reduced resistance may be serious.
- 10. Adequacy and sturdiness of construction.
- 11. Ease of removal of parts for maintenance.
- 12. Space required for mounting.
- 13. Cost and maintenance.

Every industrial control application must be considered as custom-built, even when standard packaged units are used in the final setup. Otherwise, the

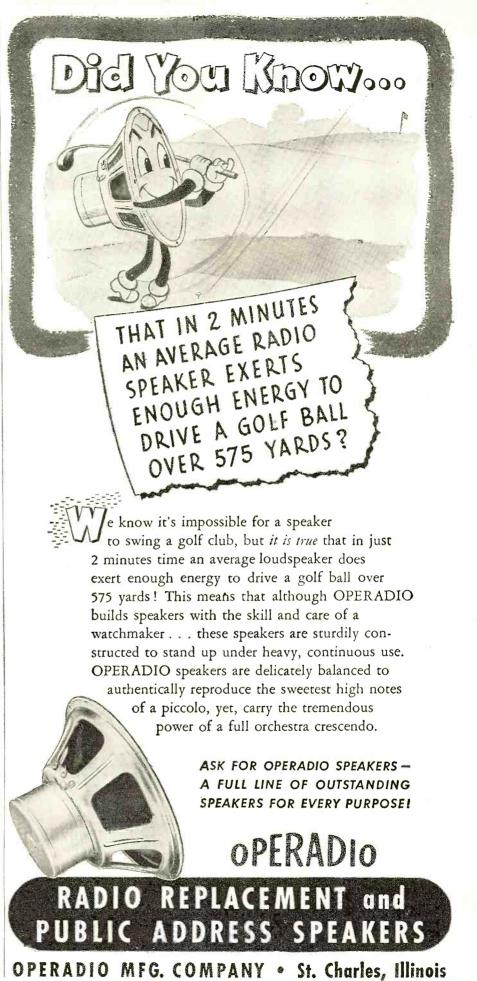
application of electronics to industrial control will tend to become a gadget business through failure to utilize electronics properly. The possibilities which electronic principles and methods offer, when correctly applied and properly coordinated to electrical and mechanical design, are too great for this to be permitted to occur.

As in the case of all other radio and electronic equipment, one of the most important requirements for intelligent servicing is a thorough understanding of the principles and operation of the equipment. This factor is especially important in industrial equipment because of the large amount of money and responsibility which are involved in keeping a large production process operating continuously.

The basic principles involved in the design of industrial electronic circuits are already known to the radio serviceman. The difference is only in the manner in which these principles are applied. A few of the most basic types of electronic control circuits will be described here to familiarize the serviceman with the type of circuit design and to provide an indication of the basic approach to industrial electronic circuits. These fundamental circuits form the basis of a large proportion of the electronic control equipment which is in use in industry at the present time.

Photoelectric controls. The most fundamental photoelectric control device, and the one which has found the widest application up to the present time, is the photoeletric relay. The basic alternating current photoelectric relay consists of a phototube connected to control a thyratron, as shown in Fig. 2A. The phototube may be connected in such a manner that the thyratron will conduct and energize the relay when the illumination is increased, or when it is decreased, depending upon the particular application. In the circuit shown, when no light is applied to the phototube, the thyratron grid is biased to a negative potential with respect to the cathode, and the tube passes no current. The grid and plate voltage relations are shown in Fig. 2B. The grid voltage eg consists of the direct voltage eb on which is superimposed the alternating voltage eps in such phase that the tube will always break down at the beginning of the positive half-cycle of the anode voltage Ea. The reason for applying a.c. as well as d.c. voltage to the grid is in order to keep the current through the thyratron and the relay essentially constant regardless of the amount of illumination on the phototube. The operation of the circuit is as follows: When the phototube is illuminated, a current flows through it and the grid resistor R, resulting in the voltage drop ep across R. The total grid voltage et is shown

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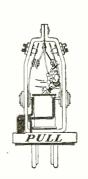
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exactly at the point to cause breakdown, since the voltage et is shown equal to the critical grid voltage ec. When the thyratron fires, the relay is energized and the operation is completed. Interruption of the beam of light reduces ep and causes the relay to

The alternating-current photoelectric relay requires the light impulse to last an appreciable length of time for proper operation. However, many processes require a control which will respond to a light impulse lasting only a few microseconds. Units for performing this function make use of the lock-in characteristic of the thyratron. A typical circuit is shown in Fig 4. It should be noted that in such circuits provision must always be made to open the plate circuit of the thyratron to de-energize the tube, for instance, by means of an auxiliary control relay as shown in the circuit of Fig. 4. When great sensitivity and speed of response are required, the output of the phototube may be applied to the grid of a high-vacuum amplifier which, in turn, is coupled to the grids of one or more thyratrons.

Timing controls. Automatic timing and timing control by means of electronic circuits are generally accomplished by making use of the principle that a certain finite time is required for a condenser to accumulate a given amount of charge when a potential is applied to it through a resistance. The time required for a given amount of charge to accumulate can be varied by changing the resistance or the capacity. The circuit and mathematical relations of this process are quite well known, and are repeated briefly in Fig. 3 for convenient reference. The time required for the voltage across the condenser to reach a definite value may be used either to delay an operation for a given period after the receipt of an impulse, or to perform an operation for a given period after the receipt of an impulse, or in multiple combinations to control more complex timing sequences. Also, by allowing a condenser to charge in series with a known resistance and voltage for a period of time, and then measuring the voltage across the condenser, a measure of the charging time can be obtained

A few basic types of electronic timing relays are shown in Fig. 6. The operation of the time delay relay shown in (A) may be explained briefly as follows: When S is closed, plate voltage is applied to the tube and current starts flowing. As the current increases the voltage drop across potentiometer R1 causes a charging current to flow through resistor R_2 to condenser C_2 producing a negative bias at the grid of the tube. Thus the plate current through the tube cannot build up rapidly. After a pre-

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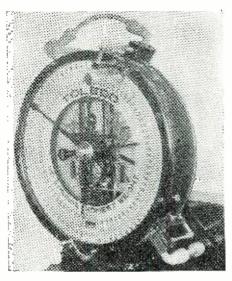
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determined time, dependent upon the adjustment of R_1 , the plate current will be sufficient to operate the relay. The maximum delay obtainable is proportional to the product of R_2 and C, therefore to obtain sufficient sensitivity of adjustment, resistor R_2 should be changed for different time delay ranges. This circuit is capable of providing delay times between 0.05 second and 3 minutes, and once an adjustment of the potentiometer has been made, the delay remains constant within 5 per-cent.

Another type of time delay relay, which is a.c. operated, is shown in Fig. 6B. When the starting switch S is open, condenser C charges, through grid rectification, to a voltage determined by the setting of the potentiometer R_s and the magnitude of R_s and R_s . The tube cannot conduct while S is open. When S is closed, plate current does not begin to flow until the charge on C is dissipated through R_s , thus giving the required delay.

A circuit in which the closing of a switch causes a relay to close for a definite time, and then release, is shown in Fig. 6C. Rs is large enough so that normally the grid bias of the tube keeps the current below the operating level of the relay. When S is thrown to position 2, the instantaneous potential of the grid becomes that of the cathode, and the plate current of the tube rises sufficiently to close the relay. As condenser C charges, the tube current gradually approaches its normal value. When the current has decreased sufficiently, the relay again opens. The length of time the relay stays closed is varied by changing the value of variable resistor Ri. The back contacts of the switch are connected to discharge C when S is opened, so that there will be no initial charge on C at the beginning of the next operation.

Motor Controls. The most widely used method of electronic control for large size motors, such as are used in industrial applications, is by converting the alternating-current supply to direct current to permit the use of shunt-wound d.c. motors. Electronic controls may be used either to supply full d.c. power and control to the motor, or to regulate the speed of a d.c. motor which is driven by a motor-generator set. In applications where speed regulation is desired, but where full electronic control is not necessary, the speed regulator system shown in Fig. 1 may often be used. This arrangement consists of a d.c. motor driven by a motor-generator set whose field is energized by the electronic regulator. The speed of the motor determines the voltage developed by the speed indicating generator, whose output is then applied through an amplifier and regulating circuit to the grids of the thyratrons which supply the generator field.



Photoelectric equipment shown mounted on a scale for automatic weighing control.

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Temperature control. There are many methods of controlling and measuring temperatures by electronic methods. The electronic circuit in a temperature control system performs the function of converting the output of the temperature-indicating device (such as thermocouples, resistance thermometers, radiation pyrometers, etc.) into a form in which it regulates the action of the control circuit. A basic type of temperaturecontrol system, making use of a thermocouple indicating element in a motorbalanced potentiometer arrangement for controlling the temperature of the system by means of valves or dampers coupled to the motor, is shown in Fig. 8. Any d.c. unbalance voltage between the thermocouple and the potentiometer is converted to a.c. by means of a carbon microphone driven directly from the 60 cycle line. The converted voltage is then amplified and applied to the grids of the

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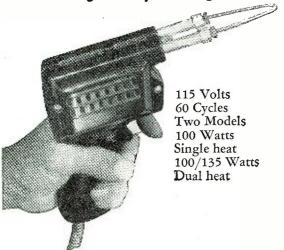
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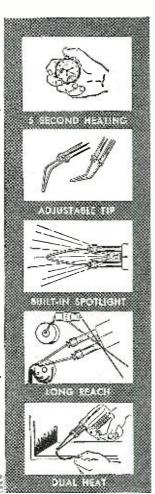
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thyratrons and, depending upon the polarity of the d.c. unbalance voltage, one or the other of the tubes will fire and drive the motor in the proper direction to rebalance the circuit. The anode of each thyratron is connected directly in series with one of the field windings of a d.c. series-wound commutator motor, which is coupled to the potentiometer slider and may be directly coupled to a valve or damper that controls the operation of the heating or cooling system. This type of control system may be used for other types of applications by eliminating the balancing motor. Then, instead of the motor windings, two magnetic relays would be connected in the plate circuit of the thyratrons, one to control a heating system and the other a cooling system, or to turn a heater on and off.

For high temperatures, the radiation pyrometer is the most suitable measuring device. The relation between the temperature of an object and its radiation has been thoroughly investigated, and is determined according to definite mathematical formulas. The amount of radiant energy may be determined quantitatively by either a thermocouple or a photocell, which has previously been calibrated in terms of temperature by means of an incandescent filament whose temperature characteristic is known. For most control purposes the photoelectric pyrometer is usually preferable to the thermocouple type, since it is much more rugged, has a very rapid response, and its output may be applied directly to the vacuum tube control circuit. A typical curve of relative phototube response is given in Fig. 5. There is no upper limit to the temperatures which can be measured by pyrometers, while the lower limit may go as low as about 110 degrees C depending upon the particular design of instrument. The photoelectric pyrometer, when used for control purposes, consists essentially of a simple photoelectric relay controlled by the amount of incident illumination-the output of the phototube being amplified by a stable vacuum-tube amplifier whose output drives the control circuit. Photoelectric pyrometers of this type have been used with excellent results in conjunction with a wide variety of control equipment for many types of applications, particularly in controlling the temperatures of furnaces and incandescent ma-

Electronic testing of materials. Various types of electronic circuits can be used for testing different characteristics of materials. Two basic circuit arrangements for determining characteristics of materials under test by electronic methods are shown in Fig. 7. The circuit in A makes use of magnetic induction principles applied to the testing of metal

objects. It consists of a simple a.c. bridge with a voltage detector to indicate the amount of unbalance. Two identical coils form two arms of the bridge; and two resistances, one of which may be variable, form the other two arms. One of the two coils serves as the reference coil, and the other as the test coil into which the metal parts are inserted for testing. Variation in the metallurgical properties of the specimen inserted in the test coil will cause the core loss and inductance to vary, thus unbalancing the bridge. To use this circuit for testing, two standard parts must first be positioned in the coils and the bridge balanced. Then the reference specimen is left in the reference coil, the part to be tested inserted in the test coil, and the amount of unbalance measured by the voltage detector. If the indication is within previously determined acceptance limits the piece is accepted; if the indication is outside these limits it is rejected. This simple magnetic induction principle is the basis also of a number of more complicated commercially developed materials testers.

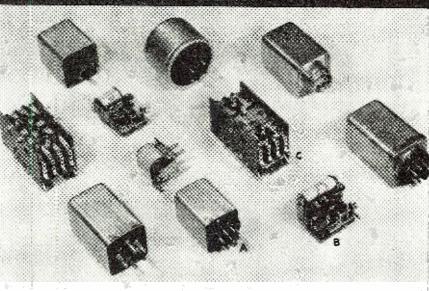
Measurements of resistivity and power factor have been found of great value in determining properties of dielectric materials and objects. These measurements can conveniently be performed by means of the simple bridge circuit shown in (B) of Fig. 7, and the procedure is similar to that used in magnetic induction testing. In this case the test specimens are made the dielectric material in two identical test condensers, and any difference in resistivity and power factor is measured by the bridge circuit. Resistivity and power factor measurements furnish a convenient practical method for determining the moisture content of a large variety of both solid and liquid non-conducting materials, and a number of electronic moisture indicators have recently been developed which depend essentially upon measurement of the power factor of the material.

Servicing

Because of the great cost of production stoppages due to equipment failures, preventive maintenance of industrial electronic equipment is of much greater importance and much more desirable than repair after a breakdown which may interrupt production. Electronic control circuits for industrial applications are therefore ruggedly constructed, conservatively rated, and have a minimum of moving parts to break or get out of adjustment. However, they are nevertheless subject to damage in operation due to such factors as vibration which may loosen connections or break wires, tube failures, relay contacts requiring cleaning or getting out of adjustment, and dust and dirt which reduce the effectiveness of the optical systems of photoelectric devices.

June, 1948

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The basic procedures for maintaining electronic equipment in good working order are essentially the same as the procedures used to keep any piece of mechanical or electrical equipment working. Careful periodic inspections should be made for surface defects, and any which are found should be corrected immediately. Necessary repairs or adjustments should be made, and the equipment cleaned thoroughly and tested under actual operating conditions as a final check. The procedures which should be followed in the maintenance of electronic control circuits are closely analogous to the methods used in the maintenance of commercial broadcast equipment, where loss of air time due to equipment failures may result in considerable expense to the broadcast sta-

Although industrial electronic equipment varies in electrical and mechanical design for different applications, a few simple rules are helpful in keeping all types of equipment in proper operation:

- 1. Carefully read and follow instructions issued by the manufacturer.
- 2. Tubes should be carefully checked before being put into regular service. (Receiver type tubes may be checked in any standard commercial tube tester. Phototubes may be checked in a specially constructed test instrument containing a variable light source, a polarizing voltage and a vacuum-tube voltmeterand should be tested under the most unfavorable light conditions which will be encountered in service. Thyratrons may be checked in an instrument which measures total emission and plate voltage necessary to fire the tube with a given value of grid bias. Other tubes such as cathode-ray tubes, ignitron rectifiers and high-power oscillator tubes must be checked in the circuits in which they are used.) All tubes should be given a final operational check in the equipment in which they are used.
- 3. Inspection and test plate current of tubes at regular intervals, preferably every month or oftener if they have 24hour duty service.
- 4. Keep a record of the plate current. Be sure the filament or heater voltage is the same each time the tube is tested.
- 5. When the plate current begins to fall off, or there is any other indication that tube performance is falling off, replace the tube before it goes bad.
- 6. Inspect connections and mechanical parts for looseness, and tighten them. Vibration tends to loosen electrical connections as well as mounting bolts which hold such heavy parts as transformers, reactors, and filter condensers in place. If frequent tightening is found necessary, the panel should be shock mounted to reduce the vibration.

7. Keep the installation free from dirt and moisture.

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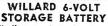
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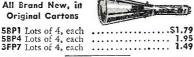
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- 8. If trouble from burned-out tubes is common, keep a record of filament voltage and of variations in line supply voltage over a 24-hour period. Use a recording voltmeter if one is available.
- 9. Inspect water-cooling and vacuumpumping systems periodically.
- 10. Maintain free circulation of air about the device and particularly about the tubes.
- 11. As most bulbs become very hot during operation, do not let them come in contact with any metallic object or be subjected to drops or spray of liquid. Cooling air streams should be distributed over the entire tube, not concentrated on one spot.
- 12. Clean lenses and mirrors of photoelectric equipment regularly, using lens tissue.
- 13. Avoid extraneous light to phototubes, directly or by reflection.
- 14. Inspect relays and contactors more frequently than similar devices used with motors. The former operate at higher speed and more often than the latter.
- 15. Indicating meters should be inspected at periodic intervals and any abnormal readings investigated immediately. Encourage machine operators to report any irregularities in the performance of their machines and associated controls.

Preventive maintenance consists primarily of constant attention to small details which indicate when equipment may break down. If the above steps are taken, the equipment will remain in the best operating condition that can be attained by preventive maintenance, and expensive work stoppages will be kept to a minimum.

However, in spite of all the precautions which can be taken, equipment will inevitably break down. When this happens, swift and accurate trouble shooting together with the necessary adjustment, repair, or replacement must follow as soon as possible. The procedures which must be employed in servicing industrial electronic circuits are essentially the same as those which are followed in servicing any other type of electronic circuit. Power supplies should be checked first to insure that blown fuses or some other defect in the power supply are not preventing power from being applied to the control circuit. If the power supply is functioning properly, the trouble should then be looked for in the control circuit from the symptoms of the equipment failure, or by inspection of the equipment and measurement of the operating voltages and currents. The value of keeping records which show all important voltage, current, resistance, and capacitance values is demonstrated on such occasions.

With the applications of electronic controls constantly increasing in a wide

variety of industrial operations in factories and plants of all sizes and types, the radio repairman can find an important place in the installation and maintenance of industrial electronic equipment. There are a great variety of circuits available for performing many different control functions, and an installation in a single plant or factory may contain equipment made by a number of different electronic manufacturers. If the complete plant installation does contain electronic control equipment supplied by different companies, no one manufacturer will supply complete maintenance service. Furthermore, not all of the companies supplying electronic controls are in a position to service their equipment throughout the country, particularly on short notice in emergencies, and the size of the installation may be too small to warrant the fulltime employment of an electronic maintenance department plus all the necessary equipment. Time is a major factor in keeping down the expenses involved in any breakdown of production, and since local radio repairmen are immediately available on the spot at any hour, they are in the most logical position to supply such service. Because of the many benefits both to the users of electronic controls and to the radio repairman, industrial electronics can be expected to become a major field of operations for the radio serviceman. -30-

HAMS HELP RESEARCH

PROFESSOR Serge Korff, New York University College of Engineering, reported recently that in planning and carrying out his recent cosmic ray expedition to Puerto Rico he was aided by the radio link established between the University's ham station and another amateur installation on the island.

Through the amateur contacts, intricate details were handled in a few days which normally would have taken weeks via the mails. Professor Korff also advised that other ham stations will cooperate with New York University on cosmic ray research projects to be carried out this summer in the vicinity of Denver.

Amateur radio station W2DSC was established at New York University College of Engineering in September 1946 by the Signal Corps Unit of the Reserve Officers Training Corps. Under the leadership of Major Leonard Drazen and Professor Philip Greenstein, the NYU amateur radio club which operates the station has a membership of seventy-five.

Professor Korff noted that the surprising thing is that this ham station which was initiated for purely instructional purposes has paid off dividends in research fields as an important communication facility. -30

June. 1948



ALL THESE FEATURES AT LOW COST

- Metalseal crystal
- High level: 54db below I volt/dyne/sq. c.m.
- Smooth response: ± 5db from 50-7000 c.p.s.
- Corrosive resistant aluminum diaphragm
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Microphones BY TURNER

It's the new Turner Model S20X Hand Microphone for home recording, public address and amateur work. Beautifully finished in rich baked brown enamel. Light in weight and convenient to use. Fits the hand perfectly, hangs on a hook when not in use.

Its performance is the kind you expect in a microphone costing three times as much. Response to voice and music pickups is smooth and flat over the most desired frequency range. Level is exceptionally high. The entire circuit is shock mounted to withstand rough treatment and is equipped with barometric compensator.

SEND NOW FOR BULLETIN



TURN TO TURNER FOR SOUND PERFORMANCE

CRYSTALS LICENSED UNDER PATENTS OF THE BRUSH DEVELOPMENT CO



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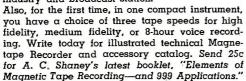
8 HOURS OF CONTINUOUS PLAY ON THE MAGNETAPE RECORDER

Now — on this one amazing instrument, you can record and play back with unmatched fidelity, any sound that can be heard. Enjoy complete operas and



30 Second Rewind

complete operas and symphonies without record-changing pause, or annoying needle talk and needle chatter. Edit and rearrange your recorded material with ease. The ideal recorder-reproducer for home, office, industry and broadcast station.





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Speeds Accurate Analysis of Audio Circuits! Simplifies Selection of Components! Saves Valuable Time!

Here's an instrument that will do most of the jobs usually assigned to a square wave generator costing about 10 times as much! The B&W Sine Wave Clipper provides a test signal particularly useful in examining the transient and frequency response of audio circuits. Designed to be driven by an audio oscillator, the clipper provides a clipped sine wave—hence the name "Sine Wave Clipper!" Used in engineering work, repair work, or with equipment under development, it will quickly pay for itself many times over.

See it at your favorite parts distributor's, or write for complete information.

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| .1 | $2500 \dot{\mathbf{v}}$ | .75 | .00005 | 5000 V | .85 |
| ī | 7500 V | 1.65 | .000067 | 2500 V | .20 |
| 2x.1 | 7000 V | 4.10 | .00007 | 2500 V | .20 |
| .12 | 15000 V | 7.95 | .00025 | 2500 V | .25 |
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| .25 | 4000 V | 2.15 | .0005 | 2500 V | .25 |
| .25 | 6000 V | 3.75 | .00072 | 5000 V | .85 |
| 10x.25 | 600 V | 1.05 | .0008 | 5000 V | .85 |
| .5 | 600 V | .28 | .0001 | 2500 V | .25 |
| .5 .5 .5_ | 1000 V | .40 | .0011 | 5000 V | .85 |
| .5 | 2000 V | .75 | .002 | 1200 V | .20 |
| .75 | 2000 V | .60 | .002 | 3000 V | .65 |
| .77 | 330 VA | | .0025 | 1200 V | .15 |
| 1.0 | 1000 V | .45 | .00275 | 2000 V | .25 |
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| 2.0 | 1000 V | .60 | .004 | 2500 V | .35 |
| 4.0 | 600 V | .60 | .005 | 1000 T. | |
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TECHNICAL RADIO PARTS CO.

265 Greenwich St. Dept. RN-1 N. Y. 7, N. Y.

GROUND SIDE INDICATOR

By ALFRED H. FORTIER

AM AT present building a small radio receiver in which I am using the compact selenium rectifier power supply described in the April, 1947 RADIO NEWS ("Versatile Power Supply," page 67).

Since the metal chassis is grounded through the power line, I wanted a simple indicator to enable me to tell when the plug was inserted in the correct position.

The schematic diagram (Fig. 1) illustrates the simple circuit devised for this

purpose.

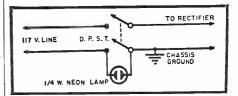
The switch used in this circuit must be of the type with a metal handle (such as a toggle) so that when the hand contacts the handle the former is electrically connected to the chassis through the switch mounting. Under this condition the neon lamp will glow (before the switch is turned "on") if the plug is inserted "backwards," but will not glow if the plug is in the correct position to ground the chassis through the grounded side of the power line.

The current which passes through

The current which passes through the body to light the lamp is so very small that it cannot be felt and is entirely safe. The switch must be a double-pole type so that no current will bleed back through the filter circuit to light the lamp falsely.

—30—

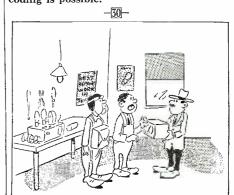
Fig. 1.



CABLING MADE EASY

PLASTIC telephone cord covers, sold everywhere in ten cent and hardware stores to prevent kinking of telephone cords, are ideal to use for holding the separate wires of homemade interconnecting cables neatly, firmly but flexibly together without the tedious work of lacing with cord.

These cord covers are about four feet long, and more than one can be used if a greater length is desired. They are available in various colors so that color coding is possible.



"Johnson fixes all the pilot light assemblies!"



Specials!



PP-51/AFQ-9 RECTIFIER-POWER UNIT

400 cycle 115 V. Contains 4—5R4GY tubes, 2—4Mfd, 1000 V. DC condensers, 2—1 Mfd, 1500 V. DC condensers, 400-2600 cycle transformers, power resisters, ct. Weight 38 lbs. Size 21"L x 5%"W x 7%"H...... \$4.95



PP-2/APQ-5 POWER UNIT



T-26/APT-2 RADAR TRANSMITTER

T-26/APT-2 RADAR TRANSMITIER
Contains tunable VHF circuit using 2—JAN CTL
703A's or 368AS tubes, Other tubes are: 2—5R4GY's,
1—2X2, 1—807, 1—6AG7, 2—6AG7's, and 1—931A.
Other parts such as 24 V. DC motor and blower, HV condensers and transformers, terminal strips and Amphenol connectors, knobs, fuse houlders, etc. make this unit invaluable for parts alone. Weight approx. 45 lbs.
Size 21"L x 10½"W x 7¾"H,

19.715 in metal case. \$9.75

DETROLA AIRCRAFT RECEIVER



T-39/APQ-9 RADAR TRANSMITTER

Loaded with VHF parts and tubes such as 2—RCA 8012's, 1—931A, 2—807's, 1—6AG7, 2—6AC7's. The RCA 8012's, are rated at 50 W. input to 500 Mic. Contains variable parallel-plate oscillator silver plated, ventilating blower and motor, ceramic tap switch, pots, terminal strips, gears. counters, ctc. Weight 36 lbs.

Size 22"L x 10½"W x 7¾"H. \$9.75



SPERRY A-5 AUTO PILOT AMPLIFIER RACK
Contains 115 V. AC volumeter and 350-450 cycle Frequency
meter. A total of 4 amplifier chassis comp. etc with following tubes included in rack: 2—1631's, 6—1632's, 3—1633's,
3—1634's, and 2—1644 tubes. Numerous transformers, resistors and condensers make this unit invaluable for parts.
Weight 38 lbs. Size 12"L x 14"W x 101/4"H.....

DYNAMIC HANDMIKE

DYNAMIC HANDMIKE

High impedance type—with press-to-talk switch that shorts microphone when released and operates a relay or other circuit when depressed. Designed for close talking PA and mobile communications service. Speech is brisk and clear, Made to stand rough handling, Black wrinkie finished. Has 6 ft. 3 conductor shielded rubber covered cable and standard amphenol plug. Made by Electro-Votee for the Signal Corps. Comparable mikes list at \$28.00.

\$7.95

MATEUR VHF MOBILE XMTR—RCVR

Western Electric No. 233A 12 Volt VHF Xmtr-Revr with tubes, Has Ballentine dynamotor—6 or 12 V. input, 500 V. 16 amps, output—buint-in, Four channel crystal controlled. For operation in range of 140-144 Mc. Transmitter has seven tubes; \$82, two 1614, two 6V6, and two 616, Receiver section has 18 tubes; two 6AC7, four 6N7, three 12817, four crystals and dynamotor. Hams can convert this for 2 meler operation. It is a scoop at this price. Used \$29.50 but guaranteed in good condition.

Screw base type with receptacle, 3 V. very tiny size. Used for aircraft instrument illumination, Ideal for model makers, hobbycraft designers, etc. Shipping weight 2 lbs. per hox of 25. Brand new.

Each 10.00

Gross

BC-314 RECEIVER

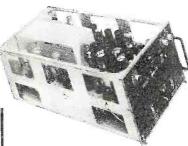
Frequency coverage 150-1500 Ke. in 4 ranges. Two RF stages, 1st detector, two IF stages, second detector, RF oscillator. CW oscillator and audio. Total, 9 tubes. 14 V. DC at 5.3 amps, imput to dynamotor. Easily converted for 110 V. AC. Use headphones or speaker or both.

New, with manual S89.50

Used 69.50

ANTENNA KNIFE SWITCH

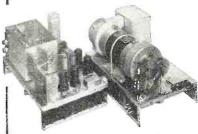
Has 2½" porcelain insulator bakelite base, heavy blades
4" long.
Single Pole Double Throw. \$0.75
Double Pole Double Throw. 1.00
Triple Pole Double Throw. 1.25



SN8/APQ-5B

Contains 31 usable tubes consisting of 2—616's, 3—6AC7's, 2—2050's, 1—68ATGT, 2—78105's, 1—68ATGT, 2—78105's, 1—68ATGT, 2—78105's, 1—7875's, 1—787

20,000 and 1000,000 ohms value. Relay DPDT, variable condensers. Amphenol and Cannon connectors, tap swifehes, networks and transformers make this another invaluable partsitem at the advertised low price, Weight 28 lbs. Contained in aluminum case \$14.95



TYPE CRZ-43AA AIRCRAFT RADIO RECEIVER

Another item for the VHF experimenter. Contains ten tubes: 6-SH7's, 2-6H6's and 2-7193's, Relays, condensers, resistors, Amptiend connectors, dynamotor, carbon pile voltage regulator and numerous other parts, Weight арргох. 32 lbs. Size, 12"W x 11"H x 8"D...... \$6.95

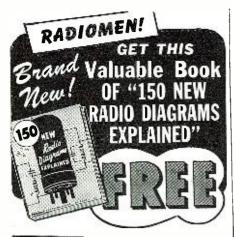


BC-800A RADAR TRANSMITTER & RECEIVER

RECEIVER
Londed with tubes and components for the VHF experimenter. Contains 19 tubes including 1-955, 3-156's, 1-6226, 1-51MG, 1-6V6CT, and 1-6H6CT/G. Several 11F tuned drenits, 7 amphenol classis fittings, sockets, 24 V. blower and motor (will operate on 110 V. AC), 2-4Mfd, 600 V. condenses, and many other resistors and parts. Weight approx. 40 lbs. In metal case 12½"W x 11½"H x 8"D. \$14.95



Unless Otherwise Stated, All of This Equipment Is Sold As Used CASH REQUIRED WITH ALL ORDERS Orders Shipped F.O.B. Collect



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Mac's Service Shop

(Continued from page 64)

"Another precaution," Mac continued, "is always to pull the receiver plug before you go probing around with the ohmmeter; and it is also a good idea to check first with the voltmeter before using the ohmmeter if the set has just been turned off. Quite often an open speaker field winding or bleeder resistor will allow the filter condensers to remain fully charged even though the line plug has been pulled for several seconds. To put the ohmmeter across a fully charged filter condenser will damage the instrument as quickly as placing it across the same points with the set turned on."

"Why do you always plug sets you are working on into one of those three outlets marked 'Receiver Test?'" Barney inquired.

"Because those three sockets are fed from the line through an isolation transformer with a tapped secondary. The tap-switch just below that 150 volt a.c. meter allows me to put any voltage from 90 to 130 volts on those outlets. That is a great help in cracking some kinds of intermittents.'

"Why do you call that an isolation transformer?"

"Because that is its main job. It isolates the receiver fed by its secondary from the line-voltage circuit that has one side grounded. Lots of a.c.-d.c. sets have one side of the line attached directly to the chassis, and quite often you will find a transformer set in which the bypass condenser from one side of the line to the chassis has been shorted out by lightning. If you had one of these sets plugged directly into

the light circuit, and if the hot side happened to be the one going to the chassis, and if you touched the chassis with one hand and any grounded object with the other-

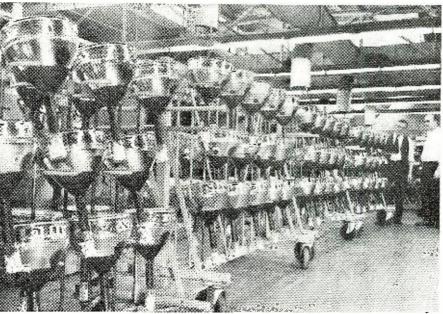
Barney rolled his eyes toward the ceiling and pretended to be plucking an imaginary harp to show he understood. For once, though, Mac did not smile at his clowning.

"Barney," he said seriously, "I do not expect you to remember everything I tell you, but here is one thing I want you never to forget: Never underestimate the danger that lurks in any electrical circuit. Working with radios every day, as you soon will be, it is all too easy to fall into a 'Who's afraid?' attitude toward the shocks you can get from a receiver. Just try to remember that there are hundreds of people lying out in the cemetery looking at the wrong side of the grass who were put there by the 110-volt a.c. house current. It only takes from seventy to ninety milliamperes of current to cause death. Under the right conditions, sixty volts or less can drive that much current through your body. Many of the sets you will be working on will have upward of seven hundred volts across the power transformer secondary, and any of them can furnish more than a hundred milliamperes of current,"

"Yet," Mac continued, "you will hear some chowder-heads in the service game boasting about how often they are 'bitten' with electricity every day. They seem to think it is to their credit. If they had any sense, they would know that the good mechanic is always the careful mechanic."

Barney, too, looked sober as he promised, "I'll remember that, Mac." -30-

Racks of television picture tubes which have just been "aluminized" in the Buffalo, New York tube works of General Electric Company. The aluminum is vaporized on the back of the fluorescent screen inside the tube and acts as a reflector to improve light output image detail, and contrast. Thomas O. Moffit, foreman, and James S. Klock inspect the tubes



126

NEW GUARANTEED SURPLUS!!

SYNCHROS







Pioneer Autosyns—AY-1, AY-14, AY-20, AY-30, AY-54, AY101D, 851, etc.

Kollsman 775-01. G.E. 2J5HA1, 2J5FB1, 2J6F3, 2JD5HB1, 2J1F1, 2J1G1, 2J1H1, etc.

DC MOTORS

John Oster. Series wound. 27V 7000 rpm. 1/100 H.P. Stock #SD-30. Price \$2.75 ea. Westinghouse—1171391, 27V 6.5 amps. series. Fan cooled, 3" diam. 4½" lg., ½ H.P. Cont. duty. Stock #SD-156. Price \$6.75 ea. Delco 5069370, 27.5V Alnico field. 10,000 rpm. Similar to S-65 but has straight shaft extension. Stock #SD-16. Price \$4.75 ea. net.

DC Timing Motor—Haydon ½ rpm. 29 volts, 100 mils. Stock #SD-157. Price \$3.75 ea. Constant Speed DC Motor—G.E. 5BA25MJ24. 24V DC 7100 rpm. RC noise filter. Stock #SD-100. Price \$8.50 ea.

G.E. Reversible—5BC26AC134. 1/20 H.P. 24V @ 3.4 Amps. Shunt wound. Cont. duty 4½" diam. x 6½" lg. 1¾" shaft extension, %" diam. 2½" sq. 1" conduit box mounted on motor. Explosion proof.

Stock #SD-143. Price \$12.50 ea.

250 RPM. Delco 5067127. 27V P.M. field. 11/4" diam. x 31/4" lg. 42 tooth 5/8" pitch diam. pinion on 0.250 shaft.
Stock #SD-108. Price \$2.95 ea.

110 RPM. G.E. Aircraft Motor. 5BA10AJ18D. 27V @ 0.7 amps. 1 oz./ft. 1\%" diam. x 3\\2" lg. \\4" shaft extension 0.250 diam. with removable coupling.
Stock #SD-98. Price \$2.95 ea.

Radio Compass Loop LP-21-LM. Stock #SD-99. Price \$9.50 ea. net.

Phase Shift Capacitor—4 stator single rotor.

0-360° phase shift. Stock #SD-114. Price \$4.75 ea.

Magnesyn—Pioneer CL-3, 6 power. Transmitter or receiver. Stock #SD-6. Price \$3.75 ea.

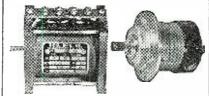
NULL TYPE SYNCHRO INDICATOR



Precision position indicator. Uses Bendix size 5 Selsyn, rectifier tube, transformer, magic eye tube and illuminated 360° dial. Ideal for Hams, labs and experimenters. May be used with SD-43 Synchro transmitter. transmitter.

Stock #SD-119. Price \$6.95 each.

SERVO MOTORS



Pioneer CK-2, 10047-2-A for 400 cycles: Diehl FP-25-3, FPE-25-11 (CDA-211052) and ZP-105-8 (CDA-211377) for 60 cycles.

400 CYCLE MOTORS

E.A.D. J-33. 115V 3 phase. Synchronous. 8000 rpm. 2" x 3". Stock #SD-59. Price \$6.75 ea. E.A.D. J-72B. 115V 2 phase induction motor. 4700 rpm. Stock #SD-140. Price \$9.75 ea. Westinghouse Blower. Type FL. 6700 rpm. Capacitor type motor. 17 C.F.M. blower. Outlet 34" x 114". Includes capacitor. Stock #SD-144. Price \$6.75 ea. Quantity prices on request.

DC Motor-Delco 5069466

Alnico field. 27.5V 10,000 rpm. 1" x 1" x 2". Use as motor or as tachometer generator. Stock #SD-65.



Price \$1.95 each Add 15c for P.P. & handling

Microwave Antenna-

AS-217A/APG 15B. 12 Cm dipole and 13 inch parabola housed in weatherbroof Radome 16" diam. 24V DC 16" diam. 24V DC spinner motor for conic scan. Stock #SD-95. Shipping wt. 70 lbs.

Price \$9.50 ea.



Remote Position Indicating System-



6-12V 60 cycles. 5 inch indicator with 0 to 360° dial. Heavy duty transmitter. Stock #SD-115. Price \$9.95 per system.



Size 5 Synchro Generator

Similar to Navy Ordnance type 5G with shaft detail per Army Ordnance Dwg. C-78414. sions 18" x 8" x 10". 115V 60 cy. Stock #SD-43. Price \$9.50 ea. Stock #SD-164. Price \$79.50 ea.

INVERTERS





Pioneer 12116, 12117, 12121, 12123, etc.

Holtzer Cabot MG-149F, MG-149H, MG-153F,

General Electric 5D21NJ3A. etc.

Leland 10563, PE-218, etc.

Wincharger PU-7/AP, etc.

60 CYCLE AC MOTORS

G. E. Reversible, 1/150 H.P. Shunt wound, 40 volts 5000 rpm. Split field. Stock #SD-18. Price \$4.75 ea. Stock #SD-19. Similar to above but not split field. Price \$2.75 ea.

Barber-Colman. 0.001 H.P. wound shaded pole type. Reversible by relay or s.p.d.t. switch. Stock #SD-27. Price \$3.75 ea.

Timing Motor—Haydon 1 rpm. 115V AC. Stock #SD-133. Price \$2.85 ea.

G. E. Amplidyne-5AM45DB15. MG-16-A. Input 115V 60 cy. Output 250V DC at 0.6 amps. Cont. Duty. Stock #SD-147. Price \$59.50 ea.

DC Selsyn System-24V DC transmitter and indicator. Indicator calibrated for flap position, 360° dial easily added. Stock #SD-129. Price \$9.50 per system.

Pioneer Magnetic Amplifier Assembly. Saturable core type output transformer. 400 cycle. Operates from plates of 6SN7 to supply 1 phase of servo motor. Stock #SD-44. Price \$8.75 ea.

Aircraft Amplidyne-G.E. 5AM31NJ18A. Input 27V DC @ 44 amps. Output 60V DC @ 8.8 amps. 530 watts. 10 min. duty. Air cooled. 11¾" x 5½". Stock #SD-111. Price \$14.50 ea.

Linear Actuator-Foote Bros. 10801. 1/6th H.P. reversible DC motor. 24V at 11.5 amps. Linear travel 5 inches, Limit switches for end of travel. Stock #SD-161. Price \$12.50 ea.

Inverter-Wincharger PU-7/AP. Input 28V DC at 160 amps. Output 115V 400 cycles at 21.6 amps. Voltage and frequency regulated. Continuous duty. Net weight 75 lbs. Dimen-

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Servo-Tek Products Co.

Surplus Division

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Open account shipments to rated concerns, others may order C.O.D.

CLIFTON, N. J.

June, 1948

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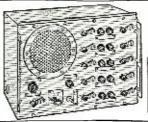
SENSATIONAL CLOSEOUT! 10 STATION INTER-COM 16 Watts PP Output

*Standard 3 wire control system.
*Operates on 110 volt, 60 cycle AC.
Price includes all tubes and 3
metal - housed sub - stations as
shown. Complete instruction sheet
included. Shog. Wt. 60 lbs. BRAND NEW

PP 616 OUTPUT

TRANSFORMER

Fully shielded, upright mtg., output trans-







4-8-15

Ship, weight 4 lbs.

POWER TRANSFORMER SPECIAL

Primary 115 volt, 60 cycle. Secondary 720 volt CT at 150 MA., 6.3 volt CT at 4 Amps., 5 volt at 3 4.45 Amps. Dimensions 3%" L. x 31/8" W. Mtg. Dimensions 21/2" x 31/8". Shipping weight 6 lbs.

each 3 for \$12.50



SHURE CARBON MIKE

T-17-B. Single button carbon with press to talk switch. 5 foot rubber cord and Pl68 plug. Orig. 2 each. Brand new. 3 for \$2.25

I" DIAL LIGHT ASSEMBLY

WITH DIMMER

An attractive, sturdy metal dial light in Red. Clear, and Amber glass jeweis. Screw type socket. Extends %" beyond panel, 2½" in the rear. Remarkable Value!



616's. Mtg. centers 33%". 3' H. x 2½" W. x 3" D. Primary 6600 ohm to each ohm voice coil. 3 for \$7.00

BRAND NEW AMERTRAN TRANSTATS

VOLTAGE REGULATORS

130/230 volts, 50/60 cycles. Max. output
65 KVA. Single phase, 0-260V Commutator Range. 2½ Amps. Max. Shipping \$24.95

115 volts, 60 cycle. Max output .25 KVA.
Single phase, 103-106 V Commutator \$12.95

Range. Max. Amps. 2.17. Ship. wgt. 15 lbs.
115 volts, 400 cycles. Load KVA output
7.2. Output 75-120 volts. 6 Amps. Max.
Shipping weight 14 lbs.

FILTER CHOKE

Hermetically sealed 15 henry, 70 Mil Choke, 420 ohm DC resistance. Mfd. to Navy spees. by Stancor. Dimensions $2\frac{1}{2}$ " W. $\times 2\frac{5}{8}$ " D. $\times 4\frac{3}{4}$ " H. Mfg. centers $1\frac{7}{8}$ " x $2\frac{1}{3}$ ". Shpg. Wt. 5 lbs. 3 for \$2.25

RAYTHEON **MAGNETRONS**

723 A/B \$4.79

TERMS: 20% cash with order. Balance C.O.D. All prices F.O.B. our warehouse in New York City. No orders under \$2.50.

ACORN ELECTRONICS CORP. 80 Vesey St. New York 7, N. Y.

HARD TO GET

SURPLUS CIRCUIT

DIAGRAMS

A COMPLETE SERIES OF SCR-274-N COMPONENTS

AS LISTED BELOW BC-453 REC. BC-456 MOD.
BC-454 REC. BC-457 TRAN.
BC-455 REC. BC-458 TRAN.
BC-946 REC. BC-459 TRAN.
BC-422 ANT. BC-696 TRAN.
RELAY UNIT & BC-450 RADIO CON. BOX

ALSO DIAGRAMS COVERING .

ASB-4 ARB (Navy) BC-211 Collins MBF APN-4 APN-9 BC-412 BC-645 APS-13 ASB-5 ASR-8 BC-733 APT-5 SCR-522

\$1. Each Any 3 \$2. All 14 \$3.50 IF YOU WANT CIRCUITS NOT LISTED WRITE US . . . IF YOU HAVE CIRCUITS NOT LISTED LET US KNOW - WE CAN USE THEM.

COMING SOON-

HOW TO BUILD A TELEVISION REC. FOR ONLY \$75.00!

Complete constructional data, including: Chassis layout, wiring diagrams, parts placement drawings, parts list and ALL the dope you need to build a Complete Television set including picture tube. This is not a surplus, but built from standard activities. \$3.50

Orders will be filled in the order received.

TEC PUBLICATIONS

2221 GRAND AVE., LONG BEACH, CALIF.

"America's Best Buy" TUBULAR ELECTROLYTICS Fresh Stock. Fully Guaranteed

| Capacity | w.v. | Each | per 10 | 100 |
|-----------|------|--------|--------|---------|
| 25 mfd | 25V | \$0.17 | \$1.59 | \$14.95 |
| 50 mfd | 50V | .21 | 1.79 | 16.95 |
| 100 mfd | 50V | .24 | 2.29 | 19.98 |
| 20 mfd | 150V | .21 | 1.89 | 17.95 |
| 30 mfd | 150V | .22 | 1.95 | 18.95 |
| 40 mfd | 150V | .23 | 2.04 | 19.74 |
| 50 mfd | 150V | .24 | 2.14 | 20.45 |
| 20-20 mfd | 150V | .29 | 2.49 | 22.98 |
| 30-20 mfd | 150V | .32 | 2.95 | 25.98 |
| 40-20 mfd | 150V | .36 | 3.25 | 29.95 |
| 50-30 mfd | 150V | .39 | 3.49 | 32.98 |
| 8 mfd | 450V | .21 | 1.99 | 19.50 |
| 8-8 mfd | 450V | .42 | 3.98 | 35.76 |
| 16 mfd | 450V | .39 | 3.74 | 33.78 |
| | | | | |

BY-PASS CONDENSERS

| .01 | \$0,06 | \$0.55 | \$ 4.60 |
|-----------|--------|---------------|---------|
| 02 600V | .06 | .55 | 4.75 |
| .05 600V | ,06 | .55 | 4.95 |
| .1 600V | .07 | .65 | 4.49 |
| .25 600V | .11 | .98 | 8.95 |
| .005 | .14 | 1.25 | 9.95 |
| 007 1700V | .14 | 1.25 | 9.95 |
| 01 | .15 | 1.30 | 10.20 |
| 02 1700V | .16 | 1.40 | 10.95 |
| | | | |

An assortment of 50 of the above By-pass condensers. Fine value for the small shop or experimenter, only \$2.98

RESISTOR ASSORTMENT 100 assorted 1/4-1/2-1 watt carbon resistors. All RMA color coded. Special \$1.29.



CRYSTALS 98c each

Your frequency plus or minus 10 KC

Meter, 3500-4000KC 40 Meter, 7000-7300KC for multiplying into Meter, 7300-7425KC 10 Meter, 7300-7425KC 6 Meter, 6250-6750KC 2½ Meter 8000-8222KC 10

Postage extra 20% deposit on COD. Write for latest bargain list featuring "America's Best Buys.

POTTER RADIO CO. 1314 McGee St., Kansas City 6, Mo.

Within the Industry

(Continued from page 30)

tronics Section. Mr. Horton will be concerned principally with the formulation and utilization of new and improved plastics and other non-metallic materials that may be of use in the work of the section. He was previously associated with the Plax Corporation as chief chemist in the organic chemical section.

GEORGE F. PLATTS, was recently appointed executive vice-president of Clippard In-

strument Laboratory, Inc. of Cincinnati, Ohio. Mr. Platts' new duties will consist of expanding the sales, sales promotion, and advertising activities of the concern, marketing a line of r.f.



and television coils, laboratory and service type electronic and electrical test equipment.

Prior to joining the Clippard organization, Mr. Platts was general manager, electric products division, of McQuay-Norris Mfg. Co. Mr. Platts holds the rank of Commander in the United States Naval Reserve, and during World War II served in connection with the No. 2 Secret Weapon Project, the VT (Proximity Fuse). Later he became a resident inspector of naval material at the Crosley Division and Sylvania Electric Products Inc. He is a senior member of the IRE.

RAYTHEON MANUFACTURING CO. has announced the appointment of Norman B. Krim as manager of the Receiving Tube Division.

*

Mr. Krim succeeds Carl J. Hollatz, vice-president of Raytheon's subsidiary, Belmont Radio Corp. of Chicago, who now becomes general manager of Belmont and will devote his full time to that branch of the company.

* * * J. A. MILLING has been appointed to the newly-created position of Commercial

Vice President of the RCA Service Company. In his new position Mr. Milling will supervise merchandising, sales, advertising, and promotional activities of the service company, which



is the servicing organization of the RCA Victor Division.

Mr. Milling received his degree in electrical engineering from Clemson College. In 1928 he joined RCA and served in the engineering, advertising, and sales divisions of the Tube Depart-

ment until 1935 when he was transferred to the home office at Camden, New Jersey to direct replacement parts and test equipment sales. In 1939, after serving for a year as co-ordinator of the RCA Victor Division's television activities, he was made supervisor of the company's commercial activities in small radio sets. He was transferred to the Manufacturing Department in 1942 and the following year he was appointed manager of the Indiana plant and General Manager of all the company's manufacturing activities in April, 1944. Prior to his new appointment Mr. Milling was General Manager of the newly-formed Parts Division.

PAUL H. WENDEL has joined the "Photofact" staff of Howard W. Sams & Co., luc. of Indianapolis.

After his discharge from the AAF in 1945, Mr. Wendel joined the staff of RADIO NEWS as an associate editor and later served as business manager of Radio Maintenance Magazine.

-30-

TV NET EXTENSIONS

To MEET the growing needs of telephone and Telegraph Company has announced extensive plans to provide additional intercity network facilities this year extending from the east coast as far west as the Mississippi River.

Included in the plans are 2000 miles of television network channels in the midwest from Buffalo to St. Louis which will be available in time for the football season this fall. The existing eastern network, which stretches along the coast from Boston to Washington, will also be increased and extended in time for the national political conventions which start in June in Philadelphia. In addition it is expected that the new midwestern network will be connected with the east coast network by the end of the year, linking these two sections of the country by television

Two television channels, so that one program can be sent in each direction, will be provided in early October to connect Cleveland, Toledo, Chicago, and St. Louis and one channel to carry programs from this network to Buffalo.

Two additional television channels from New York to Washington to serve these cities and Philadelphia and Baltimore will be added to the present eastern network by June, thus doubling the television channels between these cities. During the political conventions, three of these television channels can be set up to carry separate programs from Philadelphia to cities on the network, both north and south. This network will also be extended south by the addition of one channel which will enable programs to be received in Richmond, Virginia.

In December the new midwestern and the eastern networks will be linked by connecting Philadelphia and Cleveland with coaxial cable. It will then be possible for the first time for the same television program to be broadcast simultaneously by stations in cities linked to the network from Boston to St. Louis.

—30—

TELEVISION NDUSTRIES Co.

PICTURE IF & SOUND IF STRIP and FRONT END. This sensational picture If & Sound If Strip developed by our engineering staff enables you to build a 10"-12"-15"-20" direct view or projection type

receiver with FM sound. Supplied with a 13 channel RF front end unit. The front end covers channels from 44 to 88 mc/s and 174 to 216 mc/s (13 channels). Matched antenna input for 300 ohm line. Tubes:

1-6J6 RF amplifier 1-6J6 converter 1-6J6 oscillator.

\$119.50

PICTURE IF 5 picture IF stages of amplification and second detector. SOUND IF STAGES 2 IF stages -with limiter and discriminator. VIDEO amplifiers 2 stages video with a frequency response of 4.5 mc/s ONE DC RESTORER. IF FREQUENCY audio 21.25 — picture 25.75.



Preture IF band width 4.5 mc/s. All the above circuits and tubes are contained on one chassis. Front end unit on separate chassis. Both picture IF and sound IF delivered completely wired, tested, tubed, and matched ready for use.

DUMONT INPUTUNER

The Dumont Imputuner tunes continuously from 44 to 216 megacycles without a break—covers all 13 television channels as well as FM, amateur, and aviation channels. For ease and convenience of operation no band switching of any kind is required when tuning



\$97.90

from channel to channel with the imputuner system. Just one simple operation to reach any desired station.



Deflection Yoke similar to RCA part # 20 IDI

\$13.75

LIS

BAUSCH & LOMB TELEVISION PROJECTION LENS





Television Industries Co. is proud to announce that they have been appointed national wholesale distributors for the Bausch & Lomb f: 1.9 Television Projection Lens. Sample orders filled immediately. § 1 7 5 0 0

3125. DEALERS



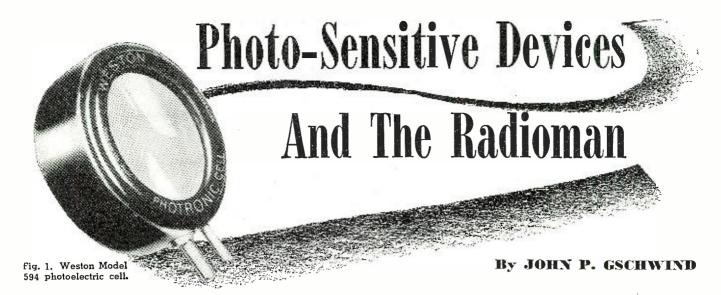
R. F. POWER SUPPLY
27-30 K.V. \$125.00
Projection Television

Contact Us for your Local Distributor



540 BUSHWICK AVE. BROOKLYN 6, N. Y.

June, 1948



Servicing or building photoelectric operated devices is not difficult. Here are a few pointers to remember.

OME years ago I had occasion to construct my first "light-controlled" unit-a simple dooropener for a chicken house. A friend of mine wanted a device that would turn his flock out into the chicken yard at full daylight every morning. As the daylight hour varies throughout the year, a time-clock switch would not do the job and a photocell actuated device was indicated. Since then I have made a nice profit constructing and servicing hundreds of varied types of light sensitive installations. But the time spent delving into highly technical treatises on photocells and phototubes in an attempt to solve my problem of the moment has always been excessive. There are many fine books and papers on the subject, but all that I have seen are highly technical, theoretical discussions by the engineer and for the engineer. In this article I will try to avoid unnecessary theory and confine my remarks to the practical aspects of photocells and phototubes, their types and uses and the principal circuits.

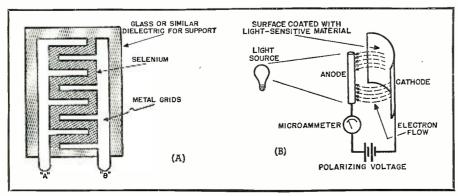
It might be well to insert a word here concerning the distinction between "photocell" and "phototube." The two terms have entirely separate meanings, and cannot be used interchangeably. A photocell is a cell whose electrical properties are affected by illumination, such as photovoltaic or photoconductive cells. A phototube refers specifically to a vacuum or gasfilled tube in which electron emission is produced directly by light falling on an electrode (the cathode). This distinction will be clarified in the following discussion.

As you undoubtedly know, a lightsensitive device is a device (not necessarily a "tube," viz., the Weston cell) that undergoes an electrical change when exposed to light. The various light-sensitive devices can be divided into three basic groups because of the three basic electrical changes resulting from this action of light. First, (and without arranging them in any order of importance) we have the "photovoltaic" cell, which from its name indicates that it actually creates a difference in potential when subjected to light. An early form of the photovoltaic cell was made by immersing a lead anode and a copper oxide

cathode into an electrolyte of lead nitrate solution. Light striking the electrolyte produced an ionization which caused a difference in potential between the copper oxide and the lead. This was literally a voltaic cell battery whose amount of activity was in proportion to the amount of light impinging upon the electrolyte. While it probably was the inspiration for the term "photovoltaic cell," this early unit was so unwieldy as to have few useful applications. The best-known type of photovoltaic cell consists of a metal disc coated with a light-sensitive material such as selenium, which is covered with a transparent conducting surface (such as a diaphanous mirror). Light passes through the transparent conducting surface and strikes the selenium, forcing off some passing electrons to the metal disc thus resulting in a difference of potential between the metal disc and the transparent conducting surface. Naturally, in production models, insulators are interposed between the transparent conducting surface and the selenium covered metal, and collector rings or some such devices are utilized as terminals. The Weston cell shown in Fig. 1 is typical. The current produced may be measured by a microammeter, and such a combination unit constitutes the standard "photoelectric light meter" as used by lighting engineers. The popular "photoelectric exposure meter" for photographic use is the same basic unit combined with a dial that enables the user to interpret the indicated current changes as usable units of photographic exposure. This type of cell has proven to be invaluable for use with portable lightintensity indicating devices because it produces its own current and no external power source is necessary. Further, although its frequency discrimination when subjected to the visual and near-visual bands is slight, by the

Fig. 2. (A). Internal construction of a commercially-built photo-conductive cell. Light falling on the selenium decreases the resistance between connectors "A" and "B".

(B) Construction details and circuit hookup for a photo-emissive type of phototube.





AN/PRS-1 MINE DETECTOR

Used by the armed forces in campaigns all over the world, for locating intricately hidden mines, the AN /PIRS-1 detector can perform an amazingly great number of duties for you. It can locate buried water pockets, water pipes, tree stumps . everything; whether metallic or not, as long as it has bulk. Every home owner, camper, and prospector needs one. The detector uses headphones and meter for both aural and visual indication. All units include detector unit and amplifier, all tubes, cables, etc.

| New, | complete | \$12.74 |
|------|-----------|-------------|
| With | Batteries | \$21.76 |



INDICATOR BC 704 A

Indicator Part of Radar Set SCR 521, Makes an excellent foundation unit for a high gain scope. Has following tubes: 4-6AC7, 3-6H6, and 1-5HPI CR tube. Comes enclosed in metal shield. New, with all tubes, less power supply supply. With wooden carrying case... \$17.50

Microwave Tubes (Magnetrons)

| Tube | Freq. Range | Pk. Pwr. Out. | Price |
|------------------|--------------------------------|-------------------|---------|
| 2J31 | 2820-2860 mc | 285 Kw | \$15.00 |
| 2J21-A (725-A) | 9345-9405 mc | 50 Kw | \$25.00 |
| 2J22 | 3267-3333 me | 265 Kw | \$15.00 |
| 5156 | 2992-3019 mc | 275 Kw | \$15.00 |
| 2J27 | 2965-2992 mc | 275 Kw | \$15.00 |
| 2J31 | 2820-2860 me | 285 Kw | \$15.00 |
| 2J32 | 2780-2820 mc | 285 Kw | \$15.00 |
| 2J38 | PKG, 3249-3263 me | 5 Kw | \$25.00 |
| 2 J 55 | PKG. 93 ₄ 5-9105 mc | 50 Kw | \$25.00 |
| 3.J31 | 24.090 mc | 35 Kw | \$17.50 |
| W.E. 700-A | 680-710 mc | 100 Kw | \$30.00 |
| W.E. 720-BY | 2800 | 1000 Kw | \$25.00 |
| MAGNETS for 2J: | 21-A (725-A), 2J22, | 2J26, 2J27. | |
| | 31, each | | \$8.00 |
| Field Strength D | | le Face ameter | Price |
| 4850 | 5/8″ | 3/4" | \$8.00 |
| 1500 | 114" | ι%" | \$8.00 |
| 1000 | Adjustable | | |
| (Electromagnet) | 2%" to 3" | 21/2" | \$12.00 |

ANTENNA EQUIPMENT

ANTENNA AN/122-A. Used in Adrock array of 4 elements, these dipoles make efficient, lightweight beams for the 6 or 2 meter band. Each dipole element is 12' long, overall, made of 3,8" dural tubing. One side of dipole is adjustable in length by means of a bevel gear arrangement to facilitate fine tuning. Get four of them for only \$20.00 or \$5.65 canh.

ANTENNA AN/104-A. The famous Ax-bandle antenna, used with the St'R 522. Ideal for that mobile quarter wave on 2 meters. Streamline construction. Two units can be used as an efficient dipole for 2 meters or FM & TV. reception. Each unit consists of a copper sheath 21" long, molded about a sturdy wooden support with an 83-1R connector. \$.75 ca. or 2 for \$1.35.

AN-128 A. 2 meter directive array consisting of 2 vertical diholes working against a square reflector, approx. 4'x3'. Surge impedance is 50 ohms. New, complete with support seasonably.

Schematic diagram ARC-5 xmtr. and revr. ca. 506

BC 306. Antenna variometer unit for BC 375 transmitter.

BC 306. Antenna variometer unit for BC 375 transmitter.
New \$4.95

CATHODE RAY TUBES

5BPI'S...\$1.20 3BP1...\$1.25 3FP7 \$1.20 5FP7...\$1.75



PE 73 CM (G.E.) Power supply for BC 375 Innut: 28 VDC Output: 1000 VDC @ 350 Ma. New \$4.95 BD 77KM Power Supply for BC 191 with spare fuse links, etc. Input 14 v.d.c. Output 1000 v. @ 350 ma. New \$9.95 Used excellent condition \$1.95 Used excellent condition \$2.95 Used \$2.95 Ma. \$9.95 Used \$2.95 Ma. \$9.95 Used \$2.95 Ma. \$9.95 Used \$2.95 Used \$2. PE 73 CM (G.E.) Power supply for BC 375 In-put: 28 VDC Output: 1000 VDC @ 350 Ma. New \$4.95

DM-25: In 12VDC 2.3A Out 250DVC 50 ma. \$2.49 DM-42: In 14VDC. Out 515/1030 VDC 215/260
10a. and 2/SVDC \$3.95
BD-AR 93. Input: 28vdc @ 3.25 amp. Output:
375 vdc @ 150 ma. Pioneer, New ...\$4.95

INVERTERS

PE 206-A. Input: 28 v.d.c. (2) 38 Amp. Output: 80 voits (2) 500 volt-amp, 800 cv. Leiand Electric. New, complete with instruction book, relays, filters, etc. \$12.50 PE 218-Input: 25-28 v.d.c. (2) 92 amp. Output: 115 volts, 1500 volt-amps, 389/500 cv. Leiand Electric. New \$35.00: Used, good condition. \$20.00

CERAMICON CAPACITORS

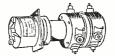
| 1 | (Erie, Centralab) | \$7.50 per 100 |
|---|-------------------|----------------|
| ı | 3 mmf±5% | |
| ı | 5 minf±5% | 100 mmf±5% |
| ł | | 115 mmf±2% |
| 1 | 8.5 mmf ±.5 mmf | 120 mmf |
| Į | | 240 mmf±3% |
| | 15 mmf±2.5 mmf | 250 mmf |
| | 48 mmf±2% | 500 mmf+15-30% |
| ı | 50 mmf±20% | 1000 mmf±5% |
| | 60 mmf±3% | |

SILVER-MICA BUTTON CAPACITORS

| ł | | (Erie, Centralab) \$9.50 per 100 .±2.5mmf .±2.5mmf .±2.5mmf .±10% |
|---|---------|---|
| ı | 185 mmf | ±2.5mmf |
| ı | 175 mmf | ±2.5mmf |
| ı | 500 mmf | ±10% |

Sonar Sound Detection Unit

MOTOR DRIVEN SWITCH



Switch operates at 1800 rpm, using internal 24 VDC motor. Switch is DPDT, and was originally designed for automatic switching of YAGI radar antennae\$2.00

ARC-5 ACCESSORIES CONVERSION COILS FOR ARC-5

TRANSMITTERS P.A. Coils

| 1 | 1117114011 | ** " • = 15.0 | |
|--|-----------------------------------|---------------------------------------|-----------------------------------|
| M.O. Coils | P.A. Coils | Antenna Loading Coils | Freq. Range |
| \$1.00 each #6029 #6030 #6032 | \$1.00 each #7247 #9293 | \$.85 each #6033 #6034 #6035 | 3-4 Mc. 4-5.3 Mc. 7-9.1 Mc. |
| CONVERSION I 1-ANTENNA CO | OlL, in any o | | equency range |
| ARC No. 6558 tion, 3 sections, 33:1 | variable recei .03" spacing, | ving eapacitor, 8 rotors. Wor | 62 mmf/secm drive ratio |
| ARC No. 4990, v spacing, 11 rotor ARC 5632 Var. X 16 rotors, worm | rs. Each mtg. capacitor | , 29.2—117 mmf. | \$1.00 .06" spacing. |
| Single revr. mtg. Single shock mou DUAL CONTRO | racks, \$1.00; nts for rack \$ | dual | \$1.50 \$1.00 |

POWER CHOKES

| 6 Hy @ 150 ma | \$1.50 |
|--|----------|
| 6 Hy @ 150 ma. Dual Choke: 2-2 Hy @ 100 Ma. | \$. 9(|
| Dual Choke: 7 Hy @ 75 Ma. 11 Hy @ 60 Ma | . \$1.50 |
| 8.5 h @ 125 ma | \$1.50 |
| 25 h @ 65 ma. 1 h @ 12A 46 ohms | . \$1.10 |
| 1 h @ 12A 46 ohus | . \$9.93 |

BC375 TUNING UNITS



From BC 191 & BC 375 TU 9B-7700 to 10.000 ke, TU 26B 209-500 kc, TU 22 B 350 to 650 kc, Will supply elosest unit to specied Frequency at time of shipment. Each \$2.25

BC 1267 XMTR-RCVR.

RELAYS
7220-24. Contactor, SPST, 24-28 vdc, contacts 400 amps. vdc, \$1.20
1077BF, Antenna changeover, DPDT, 28
vdc. TELEPHONE RELAYS
GR 206, DPST, 500 ohms, 24 vdc (Normally onen) open) St.05
SC 5853 A. SPST w/spdt section, 24 vdc,
1000 chms St.10
Send for complete listing of W.E. telephone
relays in stock.

HEADSETS

Dynamic mike and headset combination. A high quality, efficient unit, used in B-19 tank Xmrs.

Mike and polmes complete, new\$2.75

R-15 headsets: 8000 ohms impedance, rubber cushions. Comes with 8" cord and plug PL 55 New\$1.95 HS 30 headset. Insert type headset cuts out background noise, and low impedance (500 ohms) assures efficiency and fidelity. A MUST for every ham at this price\$.85 Xfmr to match 8000 ohms output\$.35

CROSS POINTER **INDICATOR**

Two 0-200 microampere movements, 3" case, many applications\$2.50



TWEETER SPEAKER

Made by W.E. this unit was originally used in battle announcing system aboard ships. Response up to 17,000 cps. 1½" radiating surface, perm magnet, dynamic type. Wt. 4½ lbs. New, with spare cone. \$9.95

BUTTERFLY CAPACITOR

All merchandise guaranteed. Mail orders promptly filled. All prices, F.O.B. New York City. Send Money Order or Check. Shipping charges sent C.O.D.

COMMUNICATIONS EQUIPMENT CO.

131 "N" Liberty St., New York City 7, N. Y.

Digby 9-4124



NEW G-C TUBE **PULLER**

Makes it easy to remove or insert miniature tubes . . . simple to operate. Inserts or extracts tubes where fingers will not reach — into hard-to-reach places. Sayes time and money. Ends

tube breakage. Prevents burnt fingers. Nc. 5093-Miniature PullerList \$ 1.65 Nc. 5093-D-Display of 12 List 19.80

NEW G-C FIELD CHASS EZ



Holds almost any radio PAT. PEND.
chassis in position! Has special reversible hooks for flanged type chassis or, to tilt chassis back if necessary. Made with slide acquistment—takes only 5 seconds to install. No parts to lose—will never wear out. A real convenience for the radio serviceman! No. 5207-Chass

Ez ... List \$3.65



Have you seen the new G-C "Speedex" Wire Strippers ... write for illustrated literature.

.....List \$1.00

RADIO DIVISION, DEPT. H

G-C Products are available at leading distributors. Write for your copy of our new illustrated catalog.

GENERAL CEMENT Mfg. Co., Rockford, III., U. S. A.

Manufacturers of over 3,000 products + Sales offices in principal cities

SHOOTS TROUBLE FASTER! MAKES MORE MONEY FOR YOU ON JOB OR AT



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at distributor at distributor or postpaid, direct. Sorry, no COD's. Ohloan's add 3% State Sales Tax

MULTI-FREQUENCY GENERATOR

In radio service work, time means money. Locate trouble faster, handle a much greater volume of work with the SIGNALETTE. As a trouble shooting tool, SIGNALETTE has no equal. Merely plug in any AC or DC line, start at speaker end of circuit and trace back, stage by stage, listening in set's speaker. Generates RF, IF and AUD10 Frequencies, 2500 cycles to 20 Megacycles. Also used for checks on Sensitivity, Gain, Peaking, Shielding, Tube testing. Wt. 13 oz. Fits pocket or tool kit. See at your dist, or order direct.



Instrument Laboratory, Inc.

PT. N. 1125 BANK STREET CINCINNATI 14, OHIO QUALIFIED JOBBERS WRITE, WIRE FOR DETAILS.

AMSCO'S JUNE SPECIALS

BUILD YOUR OWN 6-TUBE SUPERHETERODYNE RECEIVER



6 tube super-het. 2 band receiver . . . slug tuning. We furnish all parts less tubes.

\$8.95



110V 60 cy. Drawer type. Has milliammeter on front panel. Com-plete with tubes - 6V6, 6J7, 45, 80 and VR105. \$9.95

MASTER CONTROL FOR RADIO COMPASS Complete with meter... __\$1.39

SERVICE KIT Includes assortment of: 100 Resistors, 1/2 and 1.

watt.
50 Condensers, paper,
mica electrolytic &

can. 10 Switches, Toggle, Gang & Rotary. 100 ft. Spaghetti, various

sizes. 12 Knobs, round and bar.

lbs. Hookup Wire. Fuses. Volume Controls. 2Õ

10 Type Sockets. 11 lb. Hardware (screws, nuts, lugs, etc.)

Wire Wound Resistors-10 & 25 Watt. 25 Connectors, Plugs,

Ties. 10 Jacks (Phone) & Tip. 12 Padder Condensers.

Terminal Boards. 25 Ceramic Insulators

2 Panel Lights (1 neon).

1 Screw Driver. 1 Tube Puller. 2 Allen Wrenches. 2 Panel Fuse Holders.

4 Binding Post Strips, and many other valuable items.

Your Cost \$9.95 Complete WRITE FOR OUR 1948 CATALOG AMERICAN SALES CO.

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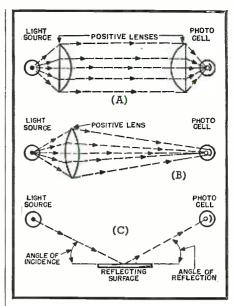
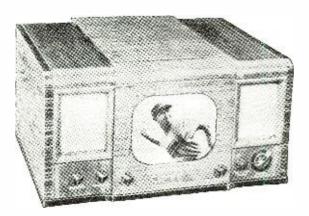


Fig. 3. (A) A small light source can be concentrated and made to operate a photocell at relatively great distances. (B) A single lens is used to concentrate beam of light on photocell. (C) Light beam is reflected before being concentrated on cell.

addition of sharp cut-off filters (layers of glass or other transparent material dyed to permit the passage of just certain desired colors or frequencies of light) between the cell and the light source, it is possible to employ these units to match or sort colors. There are two major disadvantages to the photovoltaic type of cell in general use. First, the amount of current generated by the cell is so small that it. will only operate delicate meters or extremely sensitive relays. Where these photovoltaic cells are employed to actuate counting or separating mechanisms it is necessary to have the first sensitive relay actuate a second heavier relay that can handle the additional current necessary. The other major disadvantage lies in the fact that they are somewhat sluggish in their response to rapid changes of light intensity. In my own experience I have found that they are much better for positive use, that is where the action desired is to be as a result of light falling on the unit, rather than for negative use, where the desired action is to be the result of the cessation of light. This is probably because all those I have used seem to have a "fatigue factor" where the amount of current produced decreases when the cell is subjected to a high intensity of light for long periods of time.

The second group-type of light-sensitive device is termed the "photoconductive cell." This group is comprised of photocells that vary their electrical conductivity in proportion to the amount of light.

Most of these depend upon selenium, or a combination of selenium and other elements, as the variable resistance portion of the cell. Some of the commercial models of this type cell utilize two comb-like grids with the teeth placed as shown in Fig. 2A.



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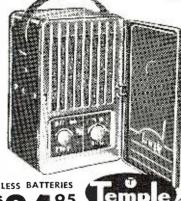
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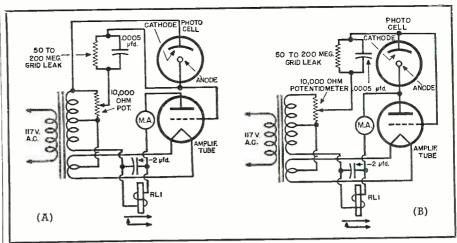


Fig. 4. Basic amplifier circuits that may be used with photo-emissive type photocells. (A) Plate current increases with increase in light. (B) plate current decreases with increase in light.

These grids are made of a conductive metal and are mounted on glass or other dielectric. Selenium or a similar material is then placed in a layer either under or over and in contact with the grids. When light strikes the selenium its electrical resistance decreases. According to some technical references, this increase of conductivity of the selenium is caused by the fact that the light impact "loosens" electrons from the selenium atoms and thereby permits freer movement. As this article is designed to be practical rather than technical and although physicists may disagree as to the causes, I do know that some cells I have used have "dark to light" resistance variations as much as ten or twenty times. For example, a cell with a normal "dark" resistance of five megohms may have its resistance lowered to less than one-half megohm when subjected to a powerful light. These "photoconductive cells" may be used in a simple series circuit (with battery or other external power source) to control the operation of a light relay or, because of the high resistance of the cell, may also be used in a vacuum tube circuit, in series with the grid, to cause a resultant variation of the grid bias. The primary disadvantage of this type has been its extreme sluggishness, the ordinary cell requiring a lapse of several seconds from the time of full illumination until reaching point of lowest resistance, and a similar lapse for recovery of resistance after the light has been removed. However I have used some commercial cells of this type that are fast enough to be entirely suitable for "audio-modulated" light, so their timelag must be as little as one ten-thousandth of a second!

The third group type may be called the "photoemissive type" of phototube. As may be surmised from the name, the operation of these tubes depends upon the principle that certain metals (such as sodium, potassium, and lithium) have the property of emitting electrons when subjected to light. (In actual practice the oxides or hydrides of these metals are com-

monly used as they are more sensitive than the pure metals.) This property of "electron emission" permits the construction of a vacuum tube in which the cathode does not have to be heated. The cathode is a metal plate surfaced with one of the previously mentioned sensitive materials and the anode is a rod or bar of conductive material as shown in Fig. 2B. When light strikes the light sensitive material electrons are thus released and consequently a current flow from this light-sensitive cathode to the anode or plate is permitted. Some manufacturers insert small amounts of certain rare gases (such as argon, krypton, neon) into their vacuum tubes, just as is done with the "gaseous" type of radio tubes because ionization of these gases, as a result of bombardment by the electrons emitted by the light sensitive material, will produce a greater total number of electrons flowing between the cathode and plate and so increase the flow of current. The current flow through this type of tube is very low so some form of amplification is generally necessary. However, this offers no great handicap because if we take a simple vacuum tube amplifier and connect the cathode of the phototube (the light-sensitive surface) to the grid of the vacuum tube and add a grid resistor, and connect the anode of the phototube to the plate of the amplifier tube we then have a phototube amplifier. Additional stages of amplification may be added if necessary, and either direct, resistance, or transformer coupling may be used. Fig. 4 illustrates two basic amplifier circuits utilized with this type of tube. In circuit "A" the plate current is increased with an increase of light while in circuit "B" the plate current is decreased with an increase of light. Thus, by choice of the proper circuit to fit the job, the necessary plate current can be kept low except at the times that the unit causes the desired action. Most of the modern commercial phototubes in this group are very stable, suffering from practically no "light-fatigue" effect. They are, in general, comparatively free

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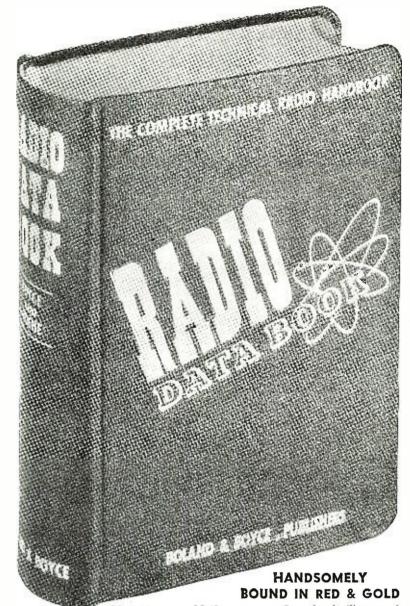
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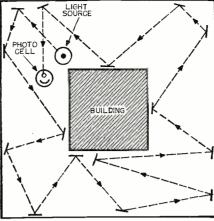


Fig. 5. A typical long-throw estate protection layout. Note that the light to the photocell actually crosses the light from the "source" and that the reflectors are not necessarily parallel to building or fence.

from sluggishness and are able to handle the complete range of audio and even ultra-audio frequencies.

A basic knowledge of light is all that is necessary in order to set up the optical requirements of a workable photoelectric device. As shown in Fig. 3A, a small light source can be kept concentrated and thus be made to operate a light-sensitive device at relatively great distances. During the last war the Germans had several fine units whereby this principle was used to transmit voice. This was "wireless" but not radio, and there was no danger of pickup by undesired persons. The light source was audio modulated and the light directed by narrow beam direct to the light-sensitive device of the authorized receiver. Now let's get back to the optical knowledge necessary to construct and install most light-sensitive devices. A positive lens (any lens that is thicker at the center than it is at the edges) will take light traveling as parallel rays and bring these rays together to form a point of light behind the lens. For our purposes, the distance from the lens to this point of convergence is the "focal length." Conversely, if we place a point source of light behind a positive lens and at a distance equal to the focal length, the light rays will become parallel after passing through the lens. These parallel rays of light can then be "re-converged" by means of another positive lens placed its focal length in front of the light-sensitive device as shown in Fig. 3A. It is also possible to utilize just one lens to direct a concentrated light beam on the cell or tube as shown in Fig. 3B. In this case, the lens is separated from the light source by a distance greater than its focal length (the exact distance should be determined by experimentation, although it is possible to arrive at it by the use of an optical formula). Now, besides the fact that for practical purposes light travels in a straight line, we only need to remember the additional rule that its "angle of reflection is always equal to its angle of incidence." (Fig. 3C)

Let's take a look at some typical installations and see the practical use of these principles. In Fig. 4 we have standard "door-opening" circuits. The same fundamental setup could be used for actuating a counting device on a moving production line simply by having the light and phototube or cell on opposite sides of the moving units to be counted. This system would therefore be ideal for use in counting vehicles passing a given spot on a highway, or pedestrians passing a store. In the latter case both the lightsensitive device and light source could be in the store window, with a mirror or other reflector mounted on a post or other support at the curb edge of the sidewalk. Naturally, as the beam would be broken twice for each passerby the total recorded would have to be divided by two.

A similar installation, but one using many reflectors or mirrors could be made to actuate an alarm if an intruder were to enter any part of an estate or plant (see Fig. 5). For this protector or burglar alarm work it is preferable to use the non-visible light frequencies (infrared or ultraviolet) as visible light would serve to warn the intruder and might disturb residents living in or near the actual installation.

Other uses include fire-alarm installations where the presence of smoke reduces the amount of light allowed to fall on the cell or tube (also utilized to detect improper combustion when placed in smokestacks of commercial buildings). We have explained how, by the use of selective color filters, it is possible to make the cells and tubes responsive only to certain specific light frequencies. It is also possible to make a photocell or phototube apparently responsive to a light frequency to which it is not normally responsive. This is accomplished by passing the "unresponsive-frequency" light through a filter that has been dyed with the proper fluorescent material (or reflecting it from a surface coated with the same fluorescent substance). The "unresponsive-frequency" light "beats" against the fluorescent material (with a sort of heterodyne effect) and produces a light frequency to which the device is responsive.

That does it! We've shown you that photoelectric devices are of three groups, i.e., the "battery" type, the "variable resistor" type, and the "unheated diode" type. All of these components are regularly used by you in radio. We've shown you that the amplification necessary is fundamentally the same as that used by you in radio. And we have also shown you that the light wave can be made to perform like a radio wave, and even "heterodyne". With all these points of similarity you should have no hesitancy in building or servicing these devices. And remember that your imagination is the only limiting factor, because any switch that you want closed (or opened) can be actuated by a photocell or phototube! -30

Single Sideband

(Continued from page 55)

any receiver thus providing the superselectivity of Fig. 4.

Fig. 1 illustrates the commercially manufactured "805" selectivity-gainer. A drawn aluminum pan 4-15/16 inches long by 3% inches wide carries a switch to cut the "805" into or out of the circuit. On top of this pan are four special 100 kc. i.f. transformers and three new miniature tubes. Beneath the pan are mounted the resistors and condensers along with the six projecting wires for connection to the receiver.

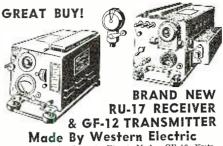
The i.f. transformers may look rather large when compared with the size of the tubes. These units were selected deliberately as the usual small i.f. cans tend to cut down the "Q" of the i.f. coils they house and shield. When seeking the degree of selectivity shown in Fig. 4, it is necessary to use larger units. Aluminum i.f. cans measuring 1% inches square were used in order to keep their side walls far enough away from the i.f. coils so as not to impair coil "Q." However, another step was necessary in order to achieve the selectivity shown in Fig. 4.

Referring to Fig. 2, at the left appears a 6BE6 converter tube. By tapping its signal grid onto the second detector diode plate of our receiver (and retuning the last i.f. transformer secondary for loudest signal to compensate for the added capacity of the 6BE6) the 455 kc. signal is taken from the output of the receiver i.f. amplifier. The 6BE6 oscillator circuit L_i , C_i plus R_i , C_i oscillates at the receiver i.f. minus 100 kc. For a 455 kc. i.f. receiver, the powdered ironcore slug of L_1 would be adjusted to tune L_i , C_i to 355 kc.

Thus we have a new i.f. in the 6BE6plate circuit. This new, second i.f. is 100 kc. It will pass through special transformers T_1 , T_2 , T_3 , and T_4 to get the selectivity of Fig. 4. Since these are critically-coupled transformers we will lose signal voltage as the signal progresses through them, but gain tremendously in selectivity. The gain loss of the four i.f. transformers is made up, with something to spare, by the 6BA6 i.f. amplifier tube.

One of the cogent reasons for poor selectivity in almost all existing receivers is due to the low resistance loading of the diode second detector on the last i.f. transformer. This loading is usually such that the selectivity contribution of the last i.f. transformer is lost in almost all receivers. In order to avoid this loss of selectivity, the diode second detector is used across the receiver's last i.f. transformer secondary. Here it performs its original function of providing a.v.c. for the receiver and continues to allow b.f.o. injection just as usual for c.w. reception.

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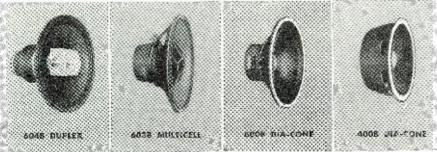
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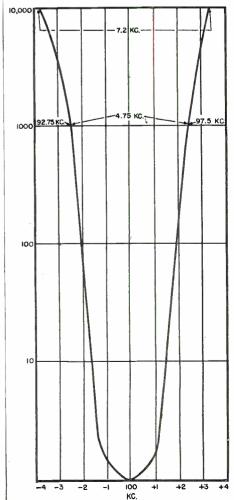
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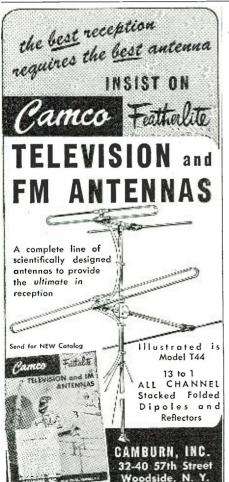
To avoid reduction in the hard-sought selectivity we turn to the non-loading "infinite impedance" second detector, the 6C4 of Fig. 2. Transformers T_1 and T2 couple the 6BE6 converter to the 6BA6 i.f. amplifier and are, in turn, coupled to each other through the 10 mmfd. condenser, C_4 . T_3 and T_4 are similarly coupled by C_7 . This is simpler than using amplifier tubes between T_1 T_2 , and T_3 T_4 . Such tubes would be undesirable from a gain standpoint since almost any receiver today has ample sensitivity-it is the selectivity that is lacking. To feed output of the 6C4 detector back into the receiver a.f. amplifier we disconnect the lead of the blocking condenser between the second detector load resistor and the a.f. volume control and connect it to the junction of the two 6C4 cathode resistors, R_5 and R_6 .

Due to the close physical proximity of elements making up commercially practical i.f. transformers, some capacity coupling exists between primary and secondary circuits. The effect of such capacity coupling is to vitiate hard-bought selectivity. The remedy for this situation is to provide special decoupling shields between each pair of i.f. coils. These are diagrammed in Fig. 2 as a dotted line

Fig. 4. The straight-sided selectivity curve of the "805" i.f. and converter.

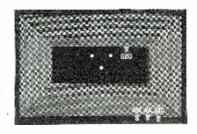


RADIO NEWS





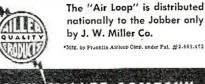
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Philip Rand started a new trend to real, badly-needed receiver-selectivity with his Q-5er. Byron Goodman carried it forward with his "Lazy-Man's Q-5er". We applaud both steps, but felt that even more could be attained by special

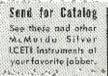
design to really give every ham super-het, new or old, the "New Look"

selectivity OST advocates.

Our answer is Model 805, 100kc. I.F. Amplifier. Connect it between your last i.f. secondary and your audio volume control and you get a small boost in gain. But what you really get is single-side-band selectivity — a selectivity curve 2.4kc. wide across the flat top, skirts falling so steeply as to be only 4.7kc. broad 1000 times (60 db.) down, only 7.2kc. wide 10,000 times down! As Byron Goodman says of this new look selectivity, it will "cut thru the QRM and pull out the desired signal like nothing you ever saw or heard". Take Model 805, only 3 7/8" wide, 4 15/16" long, 5 5/8" high, make 6 simple connections to your 455/465 kc. i.f. receiver, (which can usually supply 6.3 V. ac. at 75 Amps. and 110 to 250 volts d.c. at 25 ma. to the 805) and you have that post-war receiver with the "new look"

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between each pair of i.f. coils. These shields work wonders in steepening the selectivity curve skirts. Permeability tuning is a "must" for all i.f. transformers since it permits the use of high-"Q" fixed i.f. tuning condensers which "stay put." Iron-core i.f. coils are also necessary in order to get maximum circuit "Q" and hence effective selectivity.

With the aid of Fig. 2, and the accompanying parts list, the home constructor should have no difficulty in building an "805." If he follows the layout of Fig. 3 he will automatically get short grid and plate leads and if parts placement and wiring correspond to Fig. 3 no trouble will develop due to instability or oscillation. Good quality parts should be employed in conjunction with the specified i.f. transformers.

Alignment of transformers T_1 , T_2 , T_3 and T_4 can be effected with a 100 kc. signal from any good signal generator. Tuning of L₁ is accomplished after i.f. transformer alignment and after the "805" has been connected to a receiver. Then a signal is tuned in "on the nose" with switch S1 set to "Out," after which S_1 is set to "In" and the signal tuned in by adjustment of the L_1 core only. After that the "805" requires no operating attention or adjustment-just cut it out with S_1 for local high-fidelity reception, cut it in by means of S, for super-selective broadcast band and short-wave reception.

Almost any receiver can supply the 3/4 ampere at 6.3 volts a.c. or d.c. required for the "805" tube heaters and any good receiver can supply the 25 milliamperes plate current at 100 to 250 volts d.c. required by the three tubes in the "805." If not, a small power supply for the "805" can be assembled out of standard parts or a small filament transformer, filter choke, a couple of electrolytics, and a 100 milliampere selenium rectifier can be mounted on the end of the "805" pan to make it completely selfpowered.

Little has been said so far of the noise reduction possible with the "805." Since the most effective way to reduce noise in radio reception is to cut down the passband of the receiver, the sharper it is, the less noise. This has been proved with the "805" amplifier for with its selectivity a minimum of four times better than the average communications receiver it "slices" the noise mighty thin. This will reduce noise by a minimum of four times and, in practice, usually considerably more.

To the ham reader it has already become evident that selectivity, such as shown in Fig. 4, will provide "singlesignal" c.w. reception. If the receiver b.f.o. is set to yield a 1000 cycle audio beat note, then the audio image will be 2000 cycles away. Since the "805" selectivity curve drops from "2 times

down" to "2000 times down" in no more that 1 kc. it follows that 60 db. (1000 times) audio image suppression is secured

Substituting a balanced modulator for the 6BE6, another for the 6C4, applying a 100 kc. oscillator and output of a speech amplifier to the first tube, we can take out of the third tube a "single sideband suppressed carrier" signal for combination therein with a transmitter oscillator. -30-

Open Letter

(Continued from page 43)

We have found from a survey, that "B" and "C" supply defects make up 85% of radio receiver troubles. In testing supply voltages the radio technician must make the tests at the tube socket and in the majority of cases finds himself handicapped.

The radio serviceman has no special beefs about the design of the circuit, and the resultant reproduction. These are the selling points of any radio receiver. He appreciates the fact that a receiver performs no better than its alignment. In transportation and use almost anything can happen. Alignment screws can work out of adjustment. Humidity and temperature changes can add to the other maladjustments to spoil reception. For this reason the technician has purchased an r.f. test oscillator. Now he finds the chassis must be removed from the cabinet in order to permit alignment of the circuits. (a bad feature)

So, a few more suggestions to manufacturers are in order:

All adjustment screws should be accessible from the top or back of the receiver.

Convenient input points should be provided for test signal inputs on the top side. This would obviate the need for the chassis to be turned upside down when the set is aligned. Receiver i.f. and r.f. circuits should not be exposed to test wires carrying r.f. and i.f. frequencies. In many sets the calibrated dial is part of the cabinet. It should be part of the chassis.

In some service notes on alignment procedure it is stated "connect output meter to voice coil." But the notes do not tell you how without removing the output transformer.

In many sets with phonograph or record changer equipment, the record playing apparatus must be removed, with consequent loss of time, in order to get at any part of the chassis or even to remove the chassis from the cabinet. This is particularly disturbing when all that is desired is to test the tubes which cannot be removed without this extra effort.

A great many receivers have no indi-June, 1948

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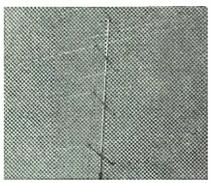
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cation on the chassis itself of the model number or manufacturer. This information is frequently on a paper sticker in the cabinet or on the chassis which soon falls off from the heat and is lost. The model number and manufacturer's name should be stamped or etched right on the chassis proper.

Another source of annoyance to the radio serviceman is the use of low melting point plastic covered wire. Apart from the frequently sickening odor that is experienced when a hot soldering iron gets near the wire the insulation melts off or chars, forming a resistive path to the chassis that may be detrimental.

Some of the "spun-in" i.f. components would not be so bad if the manufacturer were to supply a can opener to get at the coils or other parts when they are defective.

With regard to the marking of com-

ponents there are some serious problems.

The i.f. frequency should be marked on each i.f. can.

The tube sockets should each be properly labelled, such as: "6H6—Discriminator." This should be stamped into the metal chassis right near the socket.

Radio servicemen are sometimes damned as worshipping the "Goddess of Destruction." Were the manufacturers of receivers to plan their sets with an eye towards the possibility of maintenance in the future they could perform the greatest service to the radio repair industry.

The radio repairman is an extremely important cog in the radio industry's machinery. He is, in fact, the direct contact between the consumer and the manufacturer of radio receivers.

-30-

EXPERIMENTAL MULTI-CHANNEL V.H.F.

STROMBERG-CARLSON Company is collaborating with the General Telephone System in establishing an experimental multi-channel v.h.f. radio-telephone toll link between Johnstown and Northville, New York.

The new installation is said to be one of the first multi-channel links of its kind in the independent telephone field. Two conversations may be carried on at the same time in the experimental equipment.

The radio link covers a 26-mile stretch over rugged Adirondack mountain country. At the Johnstown end of the circuit, both the transmitting and receiving antennas are mounted atop 40 foot cedar poles on a 970 foot hill. The Northville antennas, deeper in the mountains, are located on a 1345 foot eminence. The transmitting antenna is erected on a 90 foot steel tower, the receiving antenna on a 65 foot cedar pole. The elevation of both ends of the radio link provides a direct line uninterrupted by hills or other obstacles lying between.

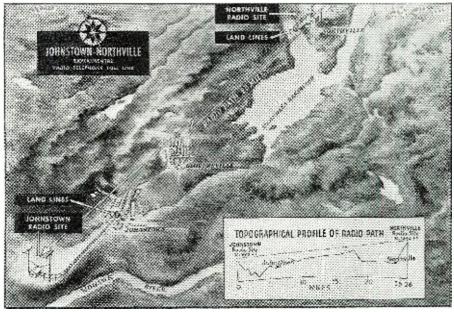
Low-powered wide-band FM transmitters designed by Link Radio Corporation have been installed at each end.

After completion of various transmission tests, advanced engineering models of the telephone terminal equipment are to be constructed, adopting improvements found desirable from experiments in the toll link, and incorporating circuits which will permit operation with either manual ringdown or dial trunks with full two-way supervision.

Stromberg-Carlson engineers point out that the experiment may lead to significant changes in multi-channel toll circuits for the telephone industry. Single channel radio circuits are now proving valuable in serving isolated ranches and farm houses cut off from telephone service because of the prohibitive costs of constructing land lines, or small areas separated from the central exchange by unusually rough terrain, as well as for toll service.

-30-

Topographical map of proposed multi-channel v.h.f. radio-telephone toll link.



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| 2"\$1 | .10 3". | \$1.10 | 4" | | \$1.19 |
|-------------|------------|----------|----------|--------|------------------|
| 5"\$1 | .39 6". | \$1.6 | 9 8" | Heavy | Magnet \$3.59 |
| 10" Heavy | Magnet | \$4.59 | 12" | 16 oz. | Slug\$5.25 |
| 12" PM Ex | tra Heavy, | for High | Fidelity | Maximu | ım Power, 46 oz. |
| Alnico Mag | gnet | | | | en 05 |
| (Nationally | Known). | | | | \$9.95 |

FLUORESCENT LAMPS for DESK or BENCH

COMPLETE WITH 15 WATT LAMPS.

STANDARD GUARANTEED 4 Prong VIBRATORS \$1.19 ea. 10 for \$9.80

| 40 x 40 150 volt condensers, | 10 for | \$4.50 |
|------------------------------|-------------------|--------|
| F.P. 20-10 450 volts 25-25V | condensers 10 for | \$4.50 |

BUFFER CONDENSERS

| .01 | 2000 | volt | for | \$1.90 |
|------|------|------|-----|--------|
| .005 | 2000 | volt | for | \$1.90 |

CROWE HEADS for AUTOMOBILE RADIOS

A dial to fit any radio and car 1940 thru 1948— Custom Dash Mounting Dials

| Under 1940—Universal Underdash Mounting Dial. Dealers Price\$ | 3.82 |
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| Tuning Units 706-T1 up thru 720-T1. Dealers Price\$ | 1.71 |
| Tuning Units with switch 706-T2 up thru 720-T2. Dealers Price\$ | 2,40 |
| Volume control units 700-VI. Dealers Price\$ | 0.73 |
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| When ordering, specify Make and Model of car and make | and |

Complete dial kit consists of "Head, Tuning Unit and Volume Control Unit".

We carry a complete line of all auto radio equipment and

AUTO AERIALS

66" and 96" Chrome Finished Rust Proof, with Shielded Lead, Side Cowl

| 66" 3 Section | \$1.29 |
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| 96" 4 Section | \$1.59 |
| 61/2" PM Auto | Speakers Alnico 5 Magnet \$1.69 |

Radio Parts Company, 614 RANDOLPH ST., CHICAGO 6, ILL.

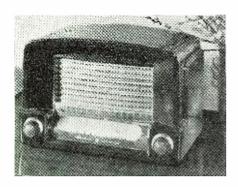
NEW RECEIVERS

---- on the Market

LOW-PRICED TABLE MODEL

General Electric Company has announced production on several low-priced table model receivers.

One of the units in the new line is the Model 115. This set is available in



either an ivory or rosewood plastic cabinet. The receiver is an a.c.-d.c. superheterodyne equipped with a "Dynapower" speaker using a *GE* Alnico 5 permanent magnet.

The receiver has four tubes plus rectifier and carries the Underwriters' Laboratories approval.

For further details on the Model 115 and other receivers in this new low-priced line, address inquiries to the Receiver Division, General Electric Company, Electronics Park, Syracuse, New York.

TABLE COMBINATION

The Model 1401 is *Philco Corporation's* 1948 version of its popular table model radio-phonograph which plays single records automatically.

Housed in an ultra-modern cabinet of glowing ebony and mahogany, this new

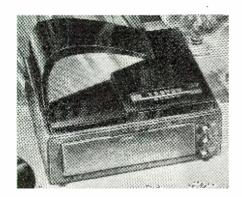


table model radio-phonograph is designed to fit in with any style of furniture. It is colorfully accented by a gold-colored metal grille and a brilliantly lighted dial.

The record playing unit automatically adjusts to ten and twelve inch records. A sensitive radio circuit provides quality performance for standard broadcasts.

Five tubes, including rectifier, provide more than ample power output for both records and radio. A built-in aerial system and automatic volume control have been included.

Philco International Corporation at 50 Broadway, New York 4, New York has additional details available on the Model 1401 to those requesting them.

EMERSON TV UNIT

Emerson Radio and Phonograph Corp. has announced production on a compact television unit which measures 16½ inches wide, 16 inches high, and 20 inches deep.

Known as the Model 571, this set contains 21 tubes plus 7 tube rectifiers and covers all channels. The new receiver boasts a 10 inch screen and sells in the moderate price class.

Further details on the Model 571 may



be secured from *Emerson Radio and Phonograph Corp.*, 111 Eighth Avenue, New York, New York.

AM TUNER

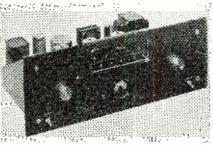
An advanced design standard broadcast tuning unit, with a frequency coverage of from 550 to 1700 kc. for professional use, has been developed by *The Kappler Company* of Los Angeles.

A unique bridge-type balanced modulator employed in the superheterodyne circuit eliminates noise ahead of the i.f. amplifier and cancels second order modulation products.

According to the company, extremely uniform sensitivity and bandpass characteristics are achieved and controlled entirely in the i.f. amplifier. The infinite impedance second detector provides a

high ratio of d.c. to a.c. load impedance which results in low distortion.

For complete details on this new AM



tuner write *The Kappler Company*, 7302 Melrose Avenue, Los Angeles 46, California.

FM-AM TABLE MODEL

The Home Radio Division of Westingbouse Electric Corporation has developed an unusually compact FM-AM table model radio which has been designated the M-182.

Employing war-developed miniature tubes, the unit is housed in a cabinet measuring only 9 inches high, 13½ inches wide, and 7 inches deep. The circuit uses five miniature tubes and a miniature rectifier. The frequency range of the AM band is from 540 kc. to 1600 kc. and is calibrated in eight major divisions. The FM band covers the frequency range of from 88 to 108 mc., calibrated in nine major divisions.

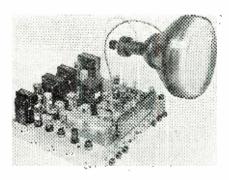
The set is equipped with a 5 inch permanent magnet dynamic speaker with Alnico V magnet. The model gives one watt of undistorted output and has two built-in antennas with connections for two outside antennas.

Further information may be obtained from the *Home Radio Division*, Westinghouse Electric Corporation, Sunbury, Pa.

TV AND FM RECEIVER

Duval Radio & Television Corp. has announced a new 15" television and FM receiver, the Model 15C.

Available as a completely wired and tested unit, less the cabinet, this receiver tunes continuously from 44 to 216 mc. A switch is provided to turn off



sweep and high voltage circuits when FM reception alone is desired.

A line of cabinets to house this re-

ceiver is now being contemplated.

The company will welcome inquiries about this unit. Write direct to the manufacturer, *Duval Radio & Television Corp.* at 423 Grove Street, Jersey City 2, New Jersey.

AIR KING PORTABLE

With the advent of the "portable season," Air King Products Co., Inc. has recently introduced the new "Pockette" portable which is tiny enough to fit in the palm of the hand.

The new 4-tube radio measures only 3 inches by 5¾ inches by 5¾ inches and weighs one pound, eleven ounces. The portable is available in three color combinations, ebony with nickel trim, maroon with gold trim, and ivory with gold trim.

The "Pockette" turns on when the lid is opened and shuts off automatically when the lid is closed. The set utilizes two standard batteries, one an ordinary flashlight unit and the other a standard 45 yolt "B" battery. The loop an-



tenna is built into the cover of the "Pockette" and the case is of polystyrene with vinylite carrying strap. The metal grille is especially treated to withstand outdoor elements.

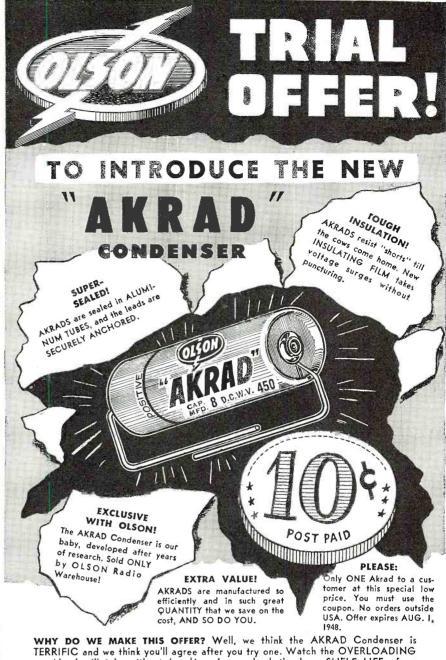
Further information will be furnished by *Air King Products Co., Inc.,* 170 53rd Street, Brooklyn 32, New York.

LIGHTWEIGHT PORTABLE

Radio Corporation of America is currently merchandising the 1948 version of the company's popular lightweight aluminum "Globe Trotter" portable.

The unit has been restyled and features functional improvements and a lower retail price. The streamlined portable, designated the Model 8BX6, is designed for three-way operation and uses five tubes and one rectifier. The automatic lid switch turns the radio on when the lid is opened and off when it is closed.

The portable comes in aluminum and June, 1948



TERRIFIC and we think you'll agree after you try one. Watch the OYERLOADING an Akrad will take without breaking down; check the long SHELF LIFE of an Akrad. We back up every AKRAD Condenser with a 100% GUARANTEE—so get one NOW from OLSON, the Radio Parts King of America. A REAL INVESTMENT for only a DIME!

VALUABLE COUPON!

SEND THIS COUPON WITH ONLY 10c TO

OLSON RADIO WAREHOUSE INC.

73 E. MILL ST., DEPT. 122

AKRON, OHIO

—and you will receive one 3 MFD 450 V. "AKRAD" CONDENSER, Hurry! Offer expires AUG. 1, 1948.

NAME

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PROJECTION TELEVISION!

Convert your RCA 630 or Crosley 307 to this

OUTSTANDING TELEVISION CONVERSION

The gigantic picture this set is capable of projecting must be seen to be believed! One set con-

OF 1948!

verted by a Los Angeles



It was viewed by 4800 people at one sitting! A 12x16-foot rear projection plastic screen

our type was used.

F 1.9 TELEVISION PROJECTION LENS

Dimension— Length 7', Diameter 4'4'. F 1.9 EF. 5 in. (127.0 mm). This lens incorporates in barrel a corporates in lens for corrective lens for use with a 5TP4 pro-jection tube. It is easily removable for



easily removable for use with flat type tubes. Lens can be utilized to project picture sizes from several inches to 7x9 feet. Made by Bausch & Lomb Optical Co. \$125.00

Mounting ring available for above lens. Price \$2.50

30 KV RF POWER SUPPLY

Dimensions— Length 14', Width 11', Height 11',' This unit has a low voltage supply separate from high volt-age pack Low volt-age pack Low volt-age DC supply has



age DC supply has control which enables you to vary voltage irom approximately 12 KV to 40 KV. Unit has focus control built in for use with 5TP4 projections. tion tube. Dealers' Price, complete....

STAND FOR PROJECTION TELEVISION SETS

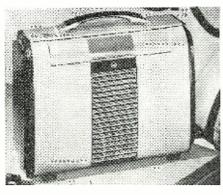
Dimensions—23" High, 25" Wide, 18½" Depth. For use with RCA 630 chassis or Crosley table model sets. Unit mounted on ball bearing soft tired wheels. Depth is designed to accommodate RF Power Supply. Open grill allows free circulation of air. This stand a natural for mounting scopes and other lab. equipment for easy mobility. Specify whether for Television use or shop. Stand as shown in top hotto. photo.
Dealers' Price.....

REAR PROJECTION TELEVISION SCREENS

Dealers' Price of screen, per sq. foot......

Include 25% Deposit With Order, Balance C.O.D

Pianeers in Projection Television SPELLMAN TELEVISION CO., INC. 130 WEST 24th STREET * NEW YORK 11, N. Y.



maroon and measures 10 inches high, 13 inches wide, and 51/2 inches deep. A deluxe traveling jacket to protect the portable is available as an accessory.

The Home Instrument Department, Radio Corporation of America, Camden, New Jersey, will supply additional details to those requesting them.

"TELEPROJECTOR"

Lynn Television Company of Upper Darby, Pennsylvania, has announced production on a projection television unit which will provide images 9 by 12 feet in size.

Designed especially for theaters, churches, schools, auditoriums, taverns and clubs, this new unit is capable of presenting images of any size up to 9 by 12 feet using either front or rear projection.

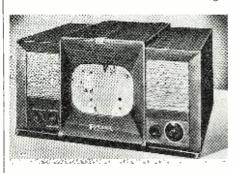
Complete details, including prices and shipping dates, will be supplied by Lynn Television Company, 241 Fairfield Avenue, Upper Darby, Pennsylvania, to those requesting this information.

FADA TV SET

Fada Radio and Electric Company, Inc. is currently introducing a new table model television receiver, the Model 799.

The new unit is housed in a walnut veneer cabinet which is hand rubbed to a piano finish. Picture size is 6 % inches by 81/2 inches, providing approximately 54 square inches of material.

Special features of the Model 799 include full thirteen channel coverage



with fine tuning, FM sound system, a.f.c. horizontal hold, stabilized vertical hold, two stages of video amplification, noise saturation circuits, balanced 300ohm antenna input circuit, and undistorted audio power output of 2.5 watts with a maximum of 4 watts.

The receiver, which operates on 117 volts a.c., uses a 5" electromagnet dynamic speaker. The cabinet measures 24% inches long, 13% inches high, and 191/8 inches deep.

Further information on the Model 799 and other receivers in the company's line will be furnished by Fada Radio and Electric Company, Inc., 525 Main Street, Belleville, New Jersey.

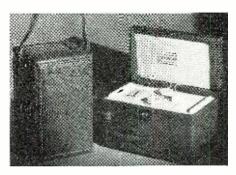
"TRIXIE"

Jewel Radio Corporation of New York has added a three-way personal portable to its line of home receivers.

The Model 801 "Trixie" uses four tubes plus a selenium rectifier and has a PM Alnico speaker. Tuning range is from 540 to 1650 kc.

The "Trixie" is housed in a case of simulated python, alligator, or natural leather covering trimmed with saddle stitching. The interior is completely dressed with ivory plastic loop cover and dial panel.

The portable will operate with the cover open or closed and when carried is



in direct line and hearing range acoustically with the ear.

The cabinet is 7% inches long, 4% inches wide and 4% inches deep. The set weighs $4\frac{1}{2}$ pounds with batteries.

Available in red, green, or brown python, alligator, or tan, further details on this radio will be furnished on request by Jewel Radio Corporation, 583 Avenue of the Americas, New York 11, New York.

"MARS" TV RECEIVER

"Mars" Television, Inc. is currently making deliveries in the New York area on the new "Mars" 12 inch home television receiver.

The receiver features the company's "Dual-Tuner"—two dials performing all the tuning functions. One is the station selector for all 13 channels and the other is the sound and picture control.

Ease of servicing is another feature claimed for the new receiver. The set utilizes two separate chassis, one for the complete sound receiver and picture and the other for the complete sweep circuit. Both are connected by safety plugs and when servicing is needed, the entire chassis may be replaced in the matter of seconds. The picture tube is inde-

Fixing Radios the Old

The Feiler Stethoscope does everything but make the actual repair. And the Stethoscope does it faster, better and much easier. Thousands of radio men, many with little ex-

Hard Way?

perience, are already fixing radios and other electronic equipment this new way.

You will find that just this one low priced unit and a few basic hand tools are all you need to fix practically any radio.

Here is the new Model TS-5 "Pocket Stethoscope" built to take out on the job. It's light, compact and rugged yet performs like the bench models. Stethoscopes are available in 4 types ranging from \$9.85 to \$34.95.



The "Inside Story" of the STETHOSCOPE—
how it works—how it instantly locates trouble in any circuit—is yours for the asking.
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1000 pieces of LATEST MODEL, Standard Brand Test Equipment to be sold this month. Tube Checkers, Signal GENERATORS, OSCILLOSCOPES, VTVM'S, MULTI-TESTERS, etc.

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Get a TRIPLE BONUS on EACH piece of equipment valued at \$40.00 or more. Just fill out the coupon below. Act now!



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□ Experimenter

June, 1948



Bardwell & McAlister's new line of Commercial Amplifiers answers the great demand of sound engineers for commercial amplifiers embodying the principles used in "custom-built" units which have been successful in the sound equipment of the motion picture industry. These principles result in high fidelity reproduction at any setting of volume controls up to full rated output with less than 4% distortion, versatility of application, ease of operation and the longer life found only in Bardwell & McAlister Studio Quality Amplification Systems. Manufactured by Union Craftsmen and fully licensed.

PRODUCT

Write for our sound equipment catalog and technical bulletins. Dealer inquiries invited.

BARDWELL & McALISTER, INC.

BOX 1310, HOLLYWOOD 28, CALIFORNIA

TUBES!

NATIONALLY ADVERTISED BRANDS TUBES!

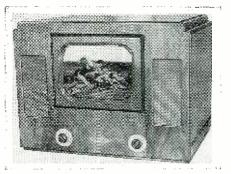
Sylvania — Tung-Sol — National Union — Raytheon — Philco — Hytron All new tubes. 100% guaranteed. Individually boxed. TYPE PRICE TYPE PRICE PRICE PRICE TYPE OZ4 IA5GT IA7GT ID8GT IF4 IG4GT 6L6 - . 6L6GA 6ST7\$.80 6L6GA 6N7 6R7G 6SA7GT 6SC7 6SF5 6SF7 80 54 54 65 65 65 50 .50 .80 .80 .50 .50 H5GT \$\$F7 \$\$H76T \$\$176T \$\$176T \$\$K76T \$\$176T \$\$N76T \$\$Q7 \$\$Q7 \$\$8Q7 \$\$R7 7A7 7B5 7B6 7E6 7 H7 7Y4 A3 A6 A7 A8 GAC7/1852 6B4G 6B86 35A5 ... 35L6GT ELECTRIC PORTABLE PHONOGRAPH 35**Y**4 ... 35**Z**5**G**T PORTABLE PHONOGRAPH Leatherette Covered. 2 Watt Amp-lifier. Plays 12 inch records with cover closed. 5 inch Alnico 5 Speaker. Rim drive constant speed, Self starting motor, High fidelity pickup. Size 17"x13"x 7½". List Price \$29.95. 35W4 39/44 H6GT 53 70L7GT NET PRICE\$15.95 LOTS OF THREE\$14.95 9 117Z6GT TERMS: 25% with Order— Balance C.O.D.—F.O.B. Chicago

ORDER TODAY FROM

1313 West Randolph St.

FRANKLIN ELLIS CO. 1313 Wes

pendently mounted and never has to be removed in case of servicing. By using three transformers for the sweep circuit, receiver, and high voltage, heat is re-



duced to a minimum as these power supplies are only extended to 75 percent of their capacity.

Further data on the new 12" receiver is available from "Mars" Television, Inc., 1441 Broadway, New York 18, New York.

A.T. & T. FILES TV NET RATES

MERICAN Telephone and Telegraph Company has filed rates with the Federal Communications Commission covering charges for television network facilities which became effective May 1st.

Under the proposed rates a television channel between two cities will cost the broadcaster \$35 a month per airline mile for eight consecutive hours each day, and \$2 a month per mile for each additional consecutive hour. For occasional or part-time service the rate will be \$1 per airline mile for the first hour of use and one-quarter of that amount for each additional consecutive 15 minutes.

For the use of terminal equipment and its maintenance, there is a charge of \$500 per month for connecting stations to the television network for eight consecutive hours daily. For stations which require only occasional service, the charge is \$200 per month plus \$10 per hour of use.

Rates now in effect for sound broadcasting will apply for the separate sound channel needed for the complete television program.

In addition to the present Eastern television network, the Bell System is now constructing 2000 miles of network channels in coaxial cables and radio relay systems in the midwest. By the end of the year the Midwestern network will be joined to the Eastern network, which will be increased and extended. At first some sharing of the available channels will be necessary on certain routes. Under these circumstances, a special schedule of rates will apply.

About 40 million people, it is estimated, live within the areas which Bell System television facilities will reach by the end of 1948.

RADIO NEWS

Chicago 7, III.

Phono System

(Continued from page 63)

lower frequencies where the diaphragm travel might be excessive.

A simple coaxial speaker may be devised merely by mounting a small three or four inch PM type speaker inside of a twelve inch speaker. However, as individual preferences differ widely, it may be found more desirable to mount the low and high frequency speakers on different sides of the room. If a number of people are listening, they may then exercise a form of personal tone control by turning their heads in the proper direction, or changing their position in

For good low frequency response the low frequency speaker must be adequately baffled, the reason being that a loudspeaker produces two wave trains, one from the front, and one from the rear and if not separated or altered in some manner the low frequency wave trains will tend to cancel each other. A ten cubic foot enclosure of the bass reflex type may be constructed from plywood and two-by-fours and will give excellent results for frequencies as low as forty or fifty cycles, although speakers may be mounted in walls or ceilings and give excellent results. If a cabinet type enclosure is used, it is suggested that the record player be placed elsewhere to eliminate to possibility of acoustic coupling between the low frequency speaker and the pickup, which may cause distortion or oscillation at higher volume levels.

Although there are a number of excellent pickups available on today's market, surprising quality may be obtained from a conventional crystal such as the L-26A. As crystal pickups are capacitive devices having an internal capacitance of approximately 1500 mmfd. the high frequency response is considerably attenuated by the shunt capacitance. By using an unusually low value of load resistor of the order of ten thousand ohms, this shunt capacitance can be minimized, and several pickups treated in this manner showed nearly flat response from fifty to six thousand cycles. This provides a greatly improved clarity of tone, but also means lowered output and for this reason three stages are used in each of the amplifiers. Jewel point needles are usually best for tonal reproduction, but may introduce excessive record wear. Cactus needles, it might be noted, performed surprisingly well with increased high boost and introduced much lower wear.

The over-all electrical characteristics of the author's amplifier extend from below twenty c.p.s. to well above twenty thousand, using conventional output transformers and without inverse feed-June, 1948

Modern Hams Junk Old-Style "Cans"!





First basic improvement in headset design in 50 years

TELEX MONOSET

- Gives clear, crisp "near as here" reception
- Blocks outside noise
- Eliminates that "top-heavy" feeling
- Ends headachy ear pressure

Man, what relief to get rid of those pressure headaches from old-style earphones!

The TELEX MONOSET swings lightly under the chin like a stethoscope—never gets in your hair! The TELEX MONOSET delivers the signal into the ears, excludes all room noise automatically. The TELEX MONOSET gives undistorted output at maximum volume ..: plenty of "sock" easily adjusted with the built-in volume control.

Modernize your rig with a MONOSET

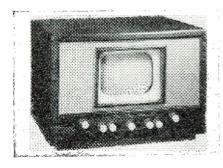
successor to the earphone! Write Department BT for information.

> Canadian Distributors Sono Film, Ltd., Winnipeg





A Beautiful Cabinet To Double The Value Of Your Chassis!



Specially Designed For Your "Transvision" Kit (12" and 15" Standard Models)

A hand-crafted cabinet made of the best 3/4 inch walnut and mahogany, finished by expert piano polishers, for the custom-builder who seeks to give his set the advantage of commercial styling combined with exclusive construction. Dimensions; 291/2 inches wide, 21 inches high, 20 inches deep.

INCLUDES THESE BETTER FEATURES:

- 8 inch Rola P. M. speaker for natural tone
 Specially built milk-white Lucite mask, curved to fit 12" picture tube—protected with safety
- glass. Conveniently glass.
 Conveniently located slide switch operates
 concealed illumination for Lucite printed dial
 and jewel-covered light in base.
 English design recessed base—felt cushioned.
 Thoroughly ventilated for heat dissipation.

IT'S THE "NEW LOOK" FOR THE **COMMERCIAL BUILDER!**

This highly polished cabinet comes to you completely assembled, drilled for shafts, wired and ready for your chassis. Nothing else to buy. Furnished complete with step-by-step instructions and following kit of parts to complete installation of chassis; pin jacks, plugs, onyx catalin knobs (6 plain, 1 with pointer), special low-loss antenna block, assembly to raise CR tube, masonite backboard drilled for ventilation, heavy stack output transformer, fuse holder, strap for CR tube, caution labels, nuts, washers, bolts, screws.

12" MODEL

WALNUT OR MAHOGANY (BLOND MAH. \$10 ADD.) Available for both 5 and 7 shaft chassis

15" MODEL

F.O.B. B'klyn. N. Y. Terms: 10% with order, balance C.O.D. Order direct or thru distributor

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108 HAVEMEYER STREET BROOKLYN 11, N. Y.

Be an Expert Learn to be a Telegraph or Radio Operator. Thousands of men needed. Intensely interesting work good pay. Learn at home or where-wer you are, quickly, easily, with the famous Candler Code Speed System. Quality for Amateur or Commercial License. Book of particulars Free.

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MOTOR GENERATORS

Brand New War Surplus Machines built by Allis Chalmers Co. to U. S. Navy Specifications.

Input: 115 V. D.C. at 14 amps., 3600 rpm. Output: 120 V. A.C., 60 CY. 1 ph. at 10.4 amps., 1000 Watts continuous duty. Ball bearings. Splashproof. Fully enclosed. Centrifugal starter. Frequency adjustable to load. Price \$97.50.

\$97.50.
machine but for 230 V. D.C. input. Price \$125.00.
parts kit with extra brushes brush-holders, field
bearings, etc., for either machine, \$29.50.
All prices FOB Tuckahoe, New York
ELECTRONICRAFT, INC.
5 Waverly Place, Tuckahoe 7, New York

back. However, due to the limited power handling capabilities of loudspeakers at very low frequencies, it may be found desirable to deliberately attenuate the very low frequencies below fifty or a hundred c.p.s. to improve the clarity of the bass reproduction and to reduce speaker resonance.

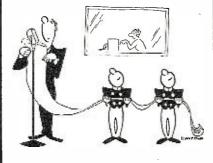
Assuming that the reproducing system is in excellent shape, room acoustics may alter the character of the reproduced sound to a considerable degree. Wall reflections may do much to destroy the clarity of reproduction, especially at high volume levels. A soft rug on the floor and acoustic paneling or wall drapes may help to cut down reflections.

An excellent way to check the overall response of a phonograph system is to obtain a standard tone record which contains the range of frequencies between fifty and ten thousand cycles and, with the amplifier controls in the proper position, the entire range should be clearly reproduced. If desired the acoustic response curve of the entire system may be plotted by placing a microphone of known characteristics in front of the loudspeakers, and connecting it to a small amplifier of flat response driving an output meter. When a standard tone record is played the meter will indicate the acoustic output curve of the system. If desired the microphone may be placed in various portions of the room to determine the most favorable acoustics.

The addition of an inexpensive radio tuner will transform this system into an excellent radio phonograph, or your present console may be easily converted by the addition of another audio amplifier.

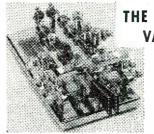
The parts cost for the entire system should run considerably less than one hundred dollars, including an automatic record changer.

Fig. 1 shows a somewhat smaller and less expensive amplifier which is especially adaptable to apartments and record booths where greater volume is not required. In either application it is desirable that a pickup with low needle talk be used, as needle chatter is quite objectionable when the amplifier is run at low levels.



"... and now a word from our sponsor!"

now ready for Immediate Delivery...



THE MELEHAN VALIANT

> DELIVERED PRICE \$**27**50

25% required on all C. O. D. merchandise. Calif. purchasers please add 21/2% sales tax.

"Truly, the World's Finest Telegraph Key" EXCLUSIVE FEATURES OF THE MELEHAN VALIANT

- · Automatic dots plus automatic dashes.
- · Adjustable from fifteen to eighty words per
- Massive base 4x1/2x7 inches and cradle unit provide solid foundation.
- Purely mechanical in operation, self-contained and self-sufficient, no superfluous electrical forces being utilized.

Deliveries of this superior instrument have been interrupted because the manufacturer would not substitute inferior materials or in any way change the perfected design.

MELEHAN RADIO PRODUCTS CO.

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3 Conductor Rubber Covered Cable per Ft. . . 36

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| 150 Watt 5 chm W W Phoestat 4" Diemoter | CI 05 |

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| Shaft | |
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| Steel Cans | |
| 4 x 4 x 268e | 8 x 10 x 10\$2.06 |
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| Sloping Front Meter Case, | Cut for 3 inch Meter. |
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100,000 ohm, precision made G.R. type, 25 watt, 6" diameter. Brand new. \$1.95 Heineman Circuit Breakers, 5 amp., 95c





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| MICAMOLD PAPER MOLDED CONDENS. |
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RADIO PARTS DISTRIBUTORS 925 E. 55th St., Chicago 15, III.

International Short-Wave

(Continued from page 70)

"There were but four of us present on the premises at 2130 hours when the place was stormed by a detachment armed from head to foot. They took us —two men and two women—as prisoners, without telling us what our fate might be. In the morning, they asked us to keep on working 'with' them. We refused indignantly and were rather surprised that they permitted us to return to our homes. To be quite true, I must tell you that they fetched me shortly afterwards, took me to the Kempeitain, and took vengeance for all our past contests—I was very nearly beaten to death before they had finished with me.

"Meanwhile, their dream of transforming Radio Saigon into a branch of the Japanese propaganda service had come true. From March 10 to the beginning of September 1945, the station was operated by the Japs-entirely and exclusively. When the British troops came in September 1945, the Japs had turned over the station to the Viet Minh, who abandoned it immediately.

"We began broadcasting again on September 26, and that was indeed a great day for those among us who had devoted a large part of our activities to Radio Saigon for several years before the Japanese 'period.' Matters were not quite so easy as we might have wished, however, for part of our equipment had been sabotaged by either the Japs or the Viet Minh.

"But we made the best of it, and that lasted until April 8, 1946, another fateful date in the history of Radio Saigon. It was on that day that the arsenal which was just opposite our premises was blown up, the explosions lasting for some 56 hours. Radio Saigon was practically burned down, with all the technical equipment being utterly destroyed. The first explosion occured at 1020, and we are proud to say that we resumed broadcasting at 1800. We borrowed whatever material we could find (from the Post Office Department), and from the Army, installed it in a private house, and simply went on!

"To the present day, we are still in that house-working under difficult conditions, but making our 'Voice' heard the world over in eight languages, 15 hours a day. Our former building is being rebuilt.

"With the gradual improvement in our equipment, the number of overseas listeners to our English broadcasts is increasing. We will be delighted to verify all correct reports and hope that many of you will continue to keep us posted on the reception of Radio Saigon in your various countries."

Radio Saigon is operated by Direction RADIO NEWS Federale de l'Information et du Tourisme —that is, it is under official control. Studios are located in Saigon at 198, Rue Chasseloup Laubat. The audiofrequency equipment of the emergency studios is composed of a 7-tube mixerline amplifier, 2 dynamic microphones, 2 turntables and magnetic pick-ups, and one monitoring amplifier. The more elaborate designs in the studios are the microphone relays and announcer's warning system - working on 12-volt batteries. The line amplifier injects modulation in a 500-ohm matched telephone line which relays the station to Phu-Tho, an Annamese village about four miles from Saigon, where the transmitters are located.

Frequencies used by Radio Saigon are 11.78, 6.165, and 1050 kc. The 6.165 antenna is a non-directional deltamatched, and the 11.78 one is a nondirectional half-wave matched. Output power is 12 kw., input power is 50 kw. Modulation is listed Class A. The 1050 kc. transmitter has an output power of 1500 watts, input power of 5 kw.

At last report, Radio Saigon was scheduled daily on 11.78, 6.165, and 1050 kc. at 1800* (or 1830) to 2000; 2130-0030, and 0300-1030; English periods at 1945-2000, 0500-0545, 0830-0930; news 1945, 0500, 0900. The Listeners Letterbox (in English) is radiated on Mondays around 0540. The medium-wave channel, 1050 kc., is used also at 0030-0300.

Recently, Radio Saigon has been using a Post Office Department outlet, FZS, 18.388, daily at 1030-1100 for a beam to France in French ("L'Indo-Chine Parle a la France," consisting of messages by people in Indo-China to friends and relatives in France). This special beam may or may not be in operation by this time.

Several other outlets are reported operating from Indo-China. One is Radio France, 6.048, Hanoi, reported mornings to around 0900, news 0700; is officially listed at 0645-0800 with 1 kw. power; in summer may use 9.465V (which was the case last year)

Such is the Saigon Story!

Radio in Japan

We are pleased this month to present this late information on radio activities in Japan (as supplied by Art Cushen, New Zealand, and Ellis Ogilvie, Washington state). Verifications are now being issued by the Broadcasting Corporation of Japan, Tokyo, by letter from R. H. Niino, vice-chief of the Liaison Section. Latest schedules are listed below (those received by Cushen and Ogilvie were not the same, so I have used those which appeared most logical):

(*Note: Unless otherwise indicated, time herein is American EST; add 5 hours for GCT; "news" means in the English language unless otherwise stated.)



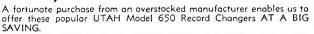
HERE ARE A FEW TYPICAL OF WHAT IS TO BE FOUND IN THE BIG NEW B-A CATALOG #481

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Has heavy, die cast base plate 10¾"x 12½". Mounting size approx. 12¼"x 13¾", extends 5¾" abbve and 2" below mounting. Operates from 110 volts, 60 cycle.

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Radio

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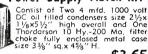
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- IDEAL FOR Radia Serviceman's parts and tool kit
- Tube carrying case
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1000 V. - 200 Ma. Power Supply FILTER KIT



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2 MFD. 2500 VOLT OIL FILLED CONDENSER

Well known brand. Ceromic pillar terminals, in hermetically sealed metal case, size overall 13/x33/x51/y² high. Comes with handy removable mtg. bracket and solder lug terminals.



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121/2 FOOT ANTENNA TELESCOPES DOWN TO 1 FOOT 4"

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Stranded trinned conductors (3 copper, 4 steel) flexible, yet unusually strong to stand long runs. Conductor is rubber covered with overall weatherproof saturated braid; OD 5/32".

Perfect for lead-ins, telephone, intercoms, etc. BRAND NEW in original factory wound coils. \$4.95

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| Tolerance | 1% or better | 35c eacl |
|-----------|--------------|-----------------|
| OHMS | 10.000 | 53.32 |
| | 14.460 | 53.96 |
| I-WW | 15.000 | 280 |
| 4.300 | 17.000 | 988 |
| 8,000 | 17.300 | 1.123 |
| 95.000 | 20.000 | 1.200 |
| | 20.520 | 4.000 |
| WW-3 | 26.500 | 11.000 |
| 4.4 | 40.000 | 20.000 |
| 4.35 | 41.800 | 80.000 |
| 13.52 | 46.000 | 82.000 |
| 20 | 54.500 | 400.000 |
| 30 | 66.000 | 600.000 |
| 70 | 92.000 | 1411 F |
| 105.8 | 109,000 | WW-5 |
| 125 | 120.000 | 1.500 |
| 130 | WW-4 | 4.000 |
| 147.5 | | 100.000 |
| 220.4 | 1.563 | 125,000 |
| 366.6 | 4.3 | 268,000 |
| 414.3 | 5.1 | 700,000 |
| 750 | 12 | 750.000 |
| 1,000 | 13.333 | 800.000 |
| 2.200 | 14 | 1 megohm |
| 2,230 | 20 | WW-13 |
| 4.000 | 22 | |
| 5.000 | 23.29 | 100 |
| 7.500 | 33.22 | 40.000 |
| | | |

| Tolerance 3% | % or better | 25c each |
|--------------|-------------|----------|
| WW-3 | 12.000 | 4.000 |
| 30 | 33.000 | 84.000 |
| 110 | | 250,000 |
| 235 | WW-4 | 290.000 |
| 2.500 | 3.94 6 | WW-5 |
| 4.000 | 10 | 84.000 |
| 4.300 | 10.2 | 220.000 |
| | | |

| Tolerance 59 | % or better | 19c each |
|--------------|-------------|----------|
| WW-3 | 100 | WW-13 |
| 30 | 110 | 15.000 |
| 35 | 2.500 | 22.000 |
| 40 | W W -4 | 100.000 |
| 50 | 250,000 | 110.000 |

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2000-3000 Volt DC Supply, similar to above but with lower output voltage. Ready to operate from 115 Volt power line.

Price Complete \$7.95

TRANSTAT **VOLTAGE REGULATORS**

Model #29144

Fixed Winding 115 Volts--- 60 cycles Commutators range 103-126 Volts
Maximum output .25 KVA
Housed in shielded case 5" x 6" x 6" Price \$6.95

Type RH

Fixed Winding 115 Volts—400 cycles Commutator range 75-120 Volts Load — .72 KVA Price \$1.95 Housed in shielded case 5½" x 6" x 6½"

Write for free descriptive catalog R-6 listing a large

EDLIE ELECTRONICS, INC.

131 Liberty Street, New York 6, N. Y. Telephone: WOrth 4-1169

kw.), JKG, 7.257, 1455-0900 (may be from 1525).

JOAK1 - Relay station, Nazaki (5 kw.), JKF, 9.655, 1455-0245 (may be from 1725): JKF2, 4.910, 0255-0900, 1525-1715.

JOAK1 - Relay station, Kawaguchi (0.3 kw.), JO9K, 9.550, 1900-2100, 2300-0020

JOAK2 — Relay station, Nazaki (5 kw.), JKA, 7.285, 1555-1800, 1920-2000, 2120-2200, 0255-0830.

JOAK2 - Relay station, Kawachi (5 kw.), JKG, 9.690, 1555-1800, 1920-2000, 2120-2200; JKG2, 4.930, 0255-0830.

WVTR - Relay station, Nazaki (5 kw.), JKD, 6.015, 1615-0900; AFRS programs.

WVTR — Relay station, Yamata (5 kw.), JKE, 9.605, 1615-0345; JKE2, 4.860, 0355-0900; AFRS programs.

JOAK1 - Relay station, Kawachi (7.5 kw.), JVW, 15.225, 1750-0230; JVW2, 9.505, 0255-0900.

It is explained that "short-wave broadcasts for Overseas have not yet been operated in Japan since the end of the war-except for the Japanese Repatriation Camps abroad. The shortwave broadcasts in Japan have been presented by the Broadcasting Corporation of Japan for (1) sending the programs of the Armed Forces Radio Service from WVTR, key station in Tokyo, to AFRS network stations in Japan; (2) sending BCJ programs from JOAK, key station in Tokyo, to BCJ network stations in Japan, and (3) to send BCJ programs from JOAK, key station in Tokyo, to the Japanese Repatriation Camps in the areas of Taihoku, Shanghai, Chungchun, Peiping, and Tietsin."

World Radio Handbook

The Summer Edition of World Radio Handbook (in English), compiled by O. Lund-Johansen, Copenhagen, Denmark, is now available for distribution. This is a valuable guide for the SWL. For further details, write me at 948 Stewartstown Road, Morgantown, West Virginia, USA.

Club Notes

Austria-Following is a list of 1948 officials of the Australian DX Radio Club (South Australia), one of the most active clubs in the world:

President, J. N. Paris; vice-presidents, E. H. Suffolk, A. W. Wright; secretarytreasurer, John Pickering, 59, Richmond Road, Westbourne Park, South Australia; competition judges (BCB and SW), J. N. Paris, J. Pickering, R. G. Gillett, (Amateur), G. Goldsmith, T. Fluck; singletons officer, A. M. Peterson; delegate to ADXBC headquarters, E. H. Tinning; DX editor, R. G. Gillett; club editor, J. N. Paris; circulation manager

JOAK1 — Relay station, Yamata (5 J. D. Riley; publishers, J. D. Riley, M. A. Mead: auditor, Gordon L. Duffield; Victorian representative, E. H. Tinning; patrons, E. W. Paton, C. C. Wicks, K. McDonald, L. Bennett, T. P. Hoey, J. S. Larkin, Arne Skoog, Ken Boord, J. N. Paris, J. D. Riley, E. H. Suffolk, R. G. Gillett, J. Pickering, G. Goldsmith, D. G. Garratt, M. A. Mead. Regular monthly meetings of this group are held on the third Wednesday at new headquarters, Rechabite Chamber, Victoria Square, in Adelaide. Monthly house organ is DXSA

Verification Data

Polskie Radio, Noakowskiego 20, Warsaw, Poland, is now verifying by attractive card depicting colored map of Poland on one side with various transmitter locations and verie data on reverse. KZCA (not KOFA), Salzburg, Austria, verified by nice card, giving power of 300 watts on 7.220, and 1 kw. on 1104 kc. Duration about two months. QRA is Blue Danube Network, Radio Station KZCA, c/o T/3 Robert Graff, A.P.O. No. 541, c/o P.M., New York, N. Y., USA. TGTA, the new Guatemalan outlet on 6.335, verified by Spanish letter, stating schedule to be 1900-0000; relays medium-wave TGT on 1390 kc.; address, Radio Bolivar, Avenida Bolivar 13-201, Guatemala City, Guatemala; report was sent in Spanish. Radio Suisse S.A., Geneva, verified commercial reception of the Prangins transmitters, HBL, 9.345, and HBQ, 6.672, heard during the St. Moritz Olympics. The person who answered the report, strangely enough, was the technician who was in charge of the transmissions from St. Moritz, and commented that he found the report an amusing "throwback" of his conversations with New York. Data on the stations is identical since the same transmitter was used-Marconi type S.W.B. 7A, 20 kw. on modulated telegraphy (A2), 12 kw. on telephony and facsimile (A3 and A4), aerial is rhombic directed to North America. A verie was received from SAT-9, 19.425, Horby, Sweden, but no details were given other than that transmitter is single side-band, working with suppressed carrier. (Kary,

I have received an attractive verifacation card (folds to form an envelope) from CQM-4, Bissau, Portuguese Guinea; card bore the notation "No. 9." Information given was power of 1000 watts; Telefunken equipment; directional antenna with reflector; frequency of 7.048 (37.76 m.), schedule 1630-1800 EST (2130-2300 GMT).

* * * Last Minute Tips

By this time, PCJ, "The Happy Station," Hilversum, Holland, should be operating in the 21-megacycle band as well as on its previous channels.

A station is being heard on 6.170 before HER3, Berne, Switzerland, obliterates it at 0030; language is Greek; Athens? (Beck, N.Y.)

An Indonesian has been heard in California on 6,170 signing off at 1000; seems to be in dual with a station on about 7.115 which also leaves the air at 1000; the last 15 minutes seems to be in parallel; musical signature is a chorus, sounds like "Santa Lucia," but may be different. Both stations use this sign-off, which signature has also been heard on the 11.765 frequency at its 1030 closedown. The Batavia outlet on 10.365 is much better than last year, signs off 1030. (Dilg)

Swedish radio journals say Scubari, Albania, is heard on about 8.216 at 1300-1400. Can anyone confirm?

Leslie H. Taylor, England, sends us some data which he noted was "not contained" in the worldwide SW list (February, March RA,DIO NEWS)-4.138 is the USSR Artic distress wave; 4.185 is the common wave for all British Royal Navy ships; 4.220 is the normal USSR distress wave; call of Salisbury, Rhodesia, 3.665, is ZEA, while Bulawayo, 3,800, has the call-sign ZEB; on 6.006, Rabat, Morocco, uses 50 kw.; call of Tananarive on 6.064 is FIQA; Paris transmitters on 6.160 and 6.175 are at Allouis; XPRA, 6.404, has 1.5 kw.; Dakar on 6.917 also uses call of FCA; call of Cuecna, 7.100, is EAJ7; the French transmitter on 7.280 is at Allouis, while the 7.240 outlet is at Realtort in the south of France; he says the station listed XMAC on 7.340 should be XMNG (incidentally, Sanderson, Australia, recently mentioned hearing XMNG on this frequency at 0645 with news in Chinese); location of XMNG was not given by Taylor or Sanderson; Moscow's 7.360 outlet is RWG, call of Pointe-a-Pitre is FG8AH; call of Sofia on 7.671 is LZB, call on 9.358 is LZC; he says OTC3 call in addition to OTM2; also he reports "there seems to be some confusion with regard to GKU. This trans-(Continued on page 156) mitter is at Portishead, near



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8.920, and GDB2, 6.795; and at 2145 GMT (1645 EST) from GCX, 8.920, and GIJ, 6.985." DeMyers, Michigan, reports hearing a weak signal on approximately 5.880 that may be Praia, Cape Verde Islands, supposed to run to 1700 sign-off daily. He recently received a verification from Noumea, New Caledonia, was posted December 17, 1947, and reached him March 1, 1948; gave schedule as 1100-1200, 1830-2100 local time (presumably 16 hours ahead of EST), and frequency as 6.210.

Stockholm expects its two new 100kw. transmitters to be delivered by British Marconi by the middle of next year. (Anderson, Calif.)

Bristol and is 'keyed' from the station at Highbridge near Burnham-on-Sea.

The line is extended at certain times to London and Abinger for 'time' at

1000 GMT (0500 EST) during January-March, GIC on 8.640 it at Seafield (may be 'Leafield'), Oxfordshire, and is 'keyed' from London, working ships

between 0048-0158 GMT (1948-2058

EST). Official British Post Office news

bulletins in 'morse' (c.w.) are radiated

from MIJ, 7.447, GDI, 7.780, and GAH, 8.065; there is also a ships' news service at 0145 GMT (2045 EST) from GCX,

Recently, Jerusalem has been broadcasting direct to American networks instead of by landline via Cairo, on either ZNT-18, 19.210, or ZNT-19, 19.140. Heard around 0800 weekdays, around 0900 Sundays. Operated by Palestine Broadcasting Service (PBS), Postmaster's Department. (Kary, Pa.)

Best signal from Radio Espana Independiente lately has been on 13.035 at 1840-1852; both man and woman read the news, alternately (in Spanish); has usual "Viva Republica" and march fanfare at sign-off. (Kary, Pa.)

PPT, Amsterdam, Holland, has been heard on 21.5 at 1330. (Osterman,

A station believed to be Radio Belgrade on about 9.505, is heard in Illinois at 0300 when a bell tolls for about 45 seconds, as a sign the station is closing down; there is a short announcement in a foreign language, then station leaves the air. (Foerster)

VPO-22, Bridgetown, Barbados, has been heard on 20.590 around 0825 in contact with London. (Kary, Pa.)

HC1VT, 7.000, Ambato, Ecuador, has been heard at 2155?2300 sign-off. (Foerster, Illinois)

Radio Budapest, Hungary, has stated that its short-wave station has been off the air since the end of the war but that it is now planned to resume transmissions (within a year), according to a Swedish DX broadcast. Some Europeans have recently reported Radio Budapest heard on about 9.369 but I believe the station actually was Radio

Sofia, Bulgaria, which is reported to me as operating that high these days although is listed 9.350.

XEBT, 9.625, Mexico City, appears to have a daily newscast (in English) now at 2230-2245. (Worris, Florida)

Radio Teheran, Iran, was heard some time ago around 0800 in a special broadcast directed to New York on 18.560. (Precourt, N.Y.)

A station heard on 12.395 shortly after 2100 with a good signal (in Russian language) is assumed to be Baku, Azerbaijan S.S.R. (Foerster, Illinois)

Here are late tips from our Brazilian observer, Villela: PTA, Rio de Janeiro, Central Radio of the Brazilian Army, 6.750, 10.590, 15.615, broadcasts a special army news program (Portuguese) at 1100; power is 1 kw.; later contacts chief stations of the several military districts, using any of these frequencies **--**6.750, 6.825, 7.605, 7.665, 8.025, 10.120, 10.590, 10.970, 13.090, 13.330, 15.490, 15.615. PFN2, Departamento Estadual de Informacoes (DEI), Sao Paulo, 4.300, 7.635, broadcasts news to newspapers (phone). PYZ2, 9.220, Rio de Janeiro, is scheduled 1800-1840.

A new station heard with powerful signals, in clear, on 15.345 (measured 15.349) is a Greek outlet announcing as both "Radio Athens" and "The Voice of Greece." Appears to be on the air daily at 1730-1830 (may not be complete schedule); news (in English) is read by a man at 1730-1745; remainder of program is devoted to various types of Greek music; woman announces in Greek; opens and closes with Greek National Anthem. (Kary, Pa.) Heard in Illinois with good signal, in clear; asked for reports and gave QRA of 4 Rigillis Street, Athens, Greece. (Foerster) Quite a good signal here in West Virginia, no QRM noted.

The Greek Underground station which had been operating on 7.700 has lately been heard on 7.863 at 0100-0130; has slight CWQRM but is usually audible to fair; begins with Greek National Anthem, then a man talks in Greek: sometimes a woman alternates with speech. Signs off with the same Anthem. (Simonian, Mass.)

Radio Eirrean, Ireland, has informed Kary, Pa., that "at present a new 100 kw. short-wave station is in course of completion and is expected to be radiating shortly in the 16- and 48-meter bands."

Vienna, 9.666 (measured), has been logged by Kary, Pa., signing on at 2345 with march selection; announces as Radio Wien; news in German 0000; fair signals but has some QRM from BBC to 0000; afterwards two "unlisted" Russians in parallel are noted on 9.660 and 9.672; these Soviets literally "squeeze" Vienna; they carry the Soviet Home Service.

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Aldridge, Washington state, reports Moscow has been heard to North America around 1900 on a high frequency of 30.500, strong signal. Harm-

According to a DX broadcast from Stockholm, Swedish DX-ers have heard a new Jewish transmitter in Palestine using the call: "This is Palestine Calling, Haganah station;" operating on 13.890 at 0400-0420, 1700-1720, 1800-1820, and at other times. Various languages heard, including Swedish.

Recently, Bucharest, Roumania, has been heard in Sweden on approximately 11.880 in parallel with 9.252 and 6.210 from before 1500 to after 1600; asking for reports in French, English, German, and Romanian. (Holmberg, Sweden).

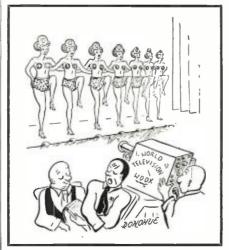
Miers, Germany, reports Baden-Baden, 6.237, has news in French, relayed from Paris, at 0230; latest schedule of Stuttgart, 6.180, is weekdays 0500-1800 Sundays 1200-1800. Summer Time went into effect in Central Europe on April 18.

ISWC, London, reports Armed Forces Radio Station WVGT, 18.100, as located on Guam, and heard in New Zealand around 0100.

XMPA, 12.200, Nanking, now signs off 1000. (Dilg, Calif.)

Major, Western Australia, airmailed these tips: XQIO, 9.950, China, heard with fair signal 0815; XGOY, 15.17 and 9.660, Chungking, heard with news 0700; KZBU, 6.100, Cebu City, Philippines, news 1100; ZBW3, 9.525, Hong Kong, now relays BBC news 0800; Batavia, Java, now announces as Radio Indonesia;" JKOA, 9.410, Seoul, Korea, The Korean Broadcasting System, heard with good signal at 0530-0830. Also from Australia, Sanderson airmails that BFES, Singapore, 11.735, is heard with news 0445; a station heard at 0100 on about 9.35 has announced as Radio Polskie and is presumed to be Warsaw, interval signal of piano notes, had news in Polish.

-30-



"Sometimes I get so bored I wish I were back in radio servicing again!"

Television Receivers

(Continued from page 78)

Method A. Connect a sweep generator to the input terminals of the set. (All antenna lead-in lines should be disconnected.) Connect the "hot" vertical input terminal of the oscilloscope, through a 10.000-ohm resistor, to screen-grid of the mixer. (If the mixer is a triode, connect to the plate-end of the plate bypass condenser.) Couple the output of an AM signal generator loosely to the receiver input terminals. Set the receiver to whatever channel it is desired to align and adjust the sweep generator to swing across the entire channel. The AM signal generator will act as a marker indicator producing a pip on the response curve whenever its frequency matches that of the sweep generator. By changing the frequency of the AM generator and noting the position of the pip on the response curve, we can accurately determine the extent of this curve.

With the apparatus operating, the circuit response pattern will appear on the oscilloscope screen. Adjust the input and r.f. coil adjustments for maximum amplitude, symmetry, and flat-topped appearance. The manufacturer's service bulletin will indicate which components to adjust. Determine, by changing the frequency of the AM generator, where the sound and video carriers would appear on the curve. These two points should be within 90 per-cent of the maximum amplitude of the curve. The same procedure is followed on all channels, in each instance changing the receiver selector switch and the sweep and AM generator frequencies.

Method B. In this method, the sweep and AM signal generator are connected as in Method A. The oscilloscope, however, is shifted to the output of the video second detector. (Retain the 10,-000-ohm resistor.) Now, the oscilloscope screen will contain the response pattern of the video i.f. stages because whatever signal is present at the output of the r.f. section must first pass through the video i.f. amplifiers before it reaches the oscilloscope. The r.f. adjustments are then made until the video i.f. response pattern on the screen has the proper form and maximum amplitude. Just what the correct i.f. response should be will be noted in a later article.

The foregoing represent the procedures recommended by essentially all television receiver manufacturers. Some receivers however, have the front-end section pre-tuned, simplifying the alignment. Philco, for example, requires only a slight adjustment on Channel 10 for the input and r.f. circuits. Once these trimmers are adjusted, all other channels will possess the correct response

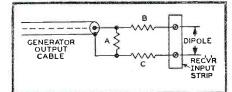


Fig. 9. Resistive matching section designed to match signal generator output impedance to the receiver input impedance.

and only the oscillator coils will require adjustment for each channel. Du Mont goes one step farther and eliminates all r.f. or oscillator adjustments. If the "Inductuner" goes out of alignment, they recommend that it be taken out and sent back to the factory for re-alignment. This latter instance, however, is unusual. Practically all other manufacturers indicate how their units can be set aright by the serviceman.

One final word about emergency alignments of the r.f. stages. It sometimes happens that after a set has been installed in a home, one of the r.f. tubes (r.f. amplifier, mixer, or oscillator) goes bad, necessitating replacement. Due to the high-frequency operation of these circuits, replacement of a tube can throw the circuits out of alignment. This is especially true of the oscillator. If the misalignment is slight and the job of hauling the receiver back to the shop too great, good results may often be obtained by watching the effect of any adjustments on a received test pattern. First bring in the sound by adjusting the oscillator tuning. Then adjust the input and r.f. tuning to bring in the pattern with best resolution and maximum brilliance. It is generally best not to attempt these adjustments with pictures other than test patterns. And under no circumstances should the other sections of the receiver be aligned without the proper tools and equipment. Every serviceman will learn sooner or later that although the customer may want the set in a hurry, he wants it in good operating condition. Telling him later that the temporary adjustments were made at his request will seldom excuse you for not giving him a perfect job in the first place. All a customer remembers is how badly the set operates and not why it operates so.

(To be continued)



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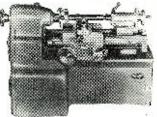
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FORMERLY SOLD FOR \$60.75 NEW LOW PRICE NOW \$41.50

A small lathe for radio shops, jewel-ers, laborato-ries, dentists, hobbycrafters

shops, jewelj ers, laboratories, dentists,
hobbycrafters,
machine shops, schools, etc. Automatic Feed. Work
capacity 3" between centers. Swing over bed 2". Constructed of steel and cast iron, Accurately machined
and finished. Fan-Cooled Motor mounted inside the base.
Complete with 1¼" face plate, 2 la'he centers, tool post
and rocker, one lathe dog, one tool-bit and test rod.

THE MANSON LATHE KIT Former Price \$36.25.

New Low Price Only \$24.50

The ManSon Lathe Kit contains the following accessories, packed in a compartment box 6" long, 4" wide, with hinged cover:

1—4-jaw Chuck and Wrench 1—Drill Chuck 1—Center Countersink

Drill
-Tool Bits—Ground
and sharpened Lathe Dogs—Sizes 3/16" & %"

1-1%" Face Plate with 8 Drilled and Tapped

8 Drilled and Tappe holes 4—Collets—Sizes 1/32, 1/16", 3/32", 1/8" 1—Collet Chuck 1—Allen Wrench

Send 20% Deposit, Balance C.O.D.

OFFENBACH & REIMUS CO. 372 Ellis St., San Francisco 2, Calif.

What's New in Radio

(Continued from page 84)

ing marketed in the low-priced field.

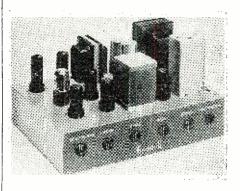
The communications receiver covers all frequencies from 500 kc. to 35 mc. The unit operates from 110-120 volt a.c. or d.c. which makes it suitable for shipboard and other uses where only d.c. is available. The receiver features electrical bandspread on all bands. An automatic noise limiter assures optimum reception under all operating conditions while a c.w. oscillator with pitch control provides exceptionally good c.w. recep-

A catalogue sheet covering the NC-33 is available on request from National Company, Inc., Malden, Massachusetts.

D.N.S. AMPLIFIER

The Minnesota Electronics Corporation has added three new amplifiers to its line of Goodell Dynamic Noise Suppressor Amplifiers.

The new Model NSA-2 has a power output of 10 watts, with a high frequency response under dynamic operat-



ing conditions to beyond 12,000 c.p.s. Effective reduction of objectionable noise amounts to more than 25 db. as a result of two complete high frequency reactance tube filter sections and one low frequency reactance tube.

Continuously variable treble and bass controls are provided. Both controls boost clockwise and attenuate counterclockwise, with the center position giving flat response. Separate inputs are provided for radio and phono with a front panel switch. Power and input facilities for a magnetic pickup preamplifier are provided by means of a tube socket connection. Tube line-up is as follows; one 5U4G, three 6SJ7's, one 6H6, one 6SN7, and two 6L6's.

Further details on this amplifier and the other new units in the Goodell line may be secured by writing The Minnesota Electronics Corporation, 204 Oppenheim Building, St. Paul, Minnesota.

CRYSTAL REPLACEMENT

A new "Silent Sapphire Crystal Pickup" which may be used as a replacement for any of 70 different crystals

employed in the pickup arms of a wide variety of different makes and models of phonographs, is now being marketed by the Renewal Sales Section of the RCA Tube Department.

A companion unit to the company's



"Magic Tone Cell" which replaces crystals in RCA Virtor radio-phonographs and record players, the new pickup has similar electrical characteristics but is of smaller size to fit a wide range of record players made by other manufacturers.

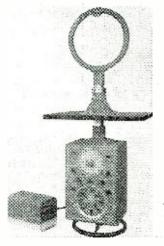
The unit features a permanent jewelpoint stylus which eliminates needle changing and provides excellent tonal qualities.

Further details are available from the Renewal Sales Section, RCA Tube Department, Radio Corporation of America, Camden, New Jersey.

DIRECTION FINDER

A new addition to their line of marine electronic equipment has been announced by Applied Electronics Company of San Francisco.

The DFR-8 Direction Finder is of the overhead mounting type and features a mechanical excellence which may be at-



tributed to the liberal use of machined bronze and aluminum castings.

The manufacturer claims exceptional

The Hottest Combination in Years! Sensational New ...

PORTABLE RADIO AND CAMERA COMBINATION

It's here . . . the Cameradio, indispensable for trips, hikes, ball games, every outdoor and vacation activity. Combines a fine Reflex Camera and a powerful Radio into one easy-to-carry unit. Order now . . . you'll double the enjoyment of every weekend!

TOM THUMB CAMERA-RADIO Combination

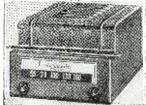
- Precision Built
- Excellent Tone Quality
- Full Vision Slide-Rule Dial
- The Ideal Vacation Companion
- Portable Radio, Battery Operated
- Reflex Camera, Standard # 127 Films

ONLY Less Batteries

ANOTHER PROGRESSIVE SPECIAL! AUTOMATIC

Tops in car radios, now at a new low price! Six-tube superhetrodyne, with steady, full-toned reception. Mounting brackets included for easy installation in your car. Don't miss this big bargain!

- Six Tube Superhetrodyne Three Gang Condenser
- Powerful Long Distance Reception Fits All Cars, Easy Installation ONLY ...
- Mounting Brackets Included





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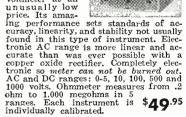
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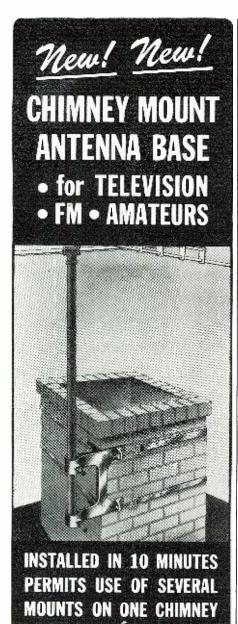
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NATION WIDE RADIO

(The Serviceman's Supply House)
572 W. Randolph St., Chicago 6, Illinois

June, 1948



"Chimney Mount" is a brilliantly engineered new antenna base that can be installed in 10 minutes without the use of special tools or drilling of holes. Several can be strapped to one chimney - also mounts on pole, 2 x 4, side of house or to any rectangular roof extension. Fastens aerial to highest point with galvanized steel bands having a combined tensile strength of more than 3,000 pounds. Made of corrosion-resistant aircraft-type aluminum alloy. Weight: 3 lbs.



sensitivity, selectivity, and stability for toggle serves to place the noise limiter the unit through the use of powderediron, slug-tuned r.f. circuits and high gain miniature series tubes.

The frequency range of the DFR-8 is 130 kc. to 5600 kc. The equipment may be operated from any conventional ship supply voltages.

Additional information on the DFR-8 Direction Finder may be secured from Applied Electronics Company, 807 Ellis Street, San Francisco 9, California.

VIBRATOR LINE

American Television & Radio Co. of St. Paul, Minnesota, is now in production on a complete line of auto radio vibrators designed for use in standard vibratoroperated auto and household radio re-

The new ATR vibrator line features ceramic stack spacers. Details of the line are included in the new 34-page ATRVibrator Guide which has just been released.

A copy of the guide describing the line may be secured from American Television & Radio Co., 300 East Fourth Street, St. Paul 1, Minnesota.

--30-

SCR-274N

(Continued from page 51)

two windings add or the method will not work. A voltmeter will be of assistance in this test.

A 6X5 rectifier is used to eliminate the need for the normal rectifier winding. The use of a dual-section filter condenser provides adequate hum free d.c. from the power supply.

In the event it is desired to change over to six volt tubes, all the tubes used in these receivers have equivalents in the six volt series, with the exception of the 12A6. A 6V6 may be used in its stead with no circuit changes.

Photos of two different conversions are shown. The one in Fig. 5 includes an a.c. power supply and an "outboard" ten-meter converter. The unit shown in Fig. 1 includes a built-in speaker, tenmeter converter, a.v.c., noise limiter, and audio gain control, and is designed for use in a car, taking its power from the "B" supply in the regular auto radio. Six volt tubes are used in this version, and the b.f.o. has been changed to an added audio stage. An a.v.c. circuit has been wired in, and several resistor values changed to give improved performance. The complete circuit for this version is shown in Fig. 3. If the main operation is to be on phone it is recommended that this type of conversion be

In this conversion, the left hand toggle switch controls the "B" supply of the auto radio, the knob in the center is the audio gain control, and the right hand

in or out of the circuit. The output transformer has been replaced by one of the midget universal types, to match the output tube to the two inch speaker mounted in the space formerly occupied by the dynamotor.

So far this article has dealt only with the conversion necessary to use these receivers on their original frequencies. The BC-453 and BC-946 do not have much appeal for high frequency work due to the low i.f. frequency, although they both have excellent selectivity.

The i.f. frequency of the BC-454 is 1415 kc. while the BC-455 uses an i.f. of 2830 kc. With i.f. frequencies of this order, excellent image rejection is achieved. This is especially important if the receivers are to be converted to the tenmeter band. There are two possible methods of changing the receiver frequencies. The simplest method is the rewinding of the coils to cover the tenmeter band. This method has the disadvantage of making the receiver useless on its original frequency as well as creating problems of cut and try to obtain the proper tracking over the band. While this is not too difficult if the proper equipment is on hand, few amateurs have the necessary instruments and experience to obtain optimum results.

A far more satisfactory method of using the receivers on ten meters is the use of a broad-band converter. By this means, the original calibration and tracking of the receiver is not disturbed, greater over-all stability is obtained, and considerable gain results. No added controls are necessary, and the converter may be constructed in a very limited space.

The bottom view of the receiver, Fig. 2, shows such a converter built into the space between the plug-in coils and the front panel. The construction of the converter in such a crowded space is rather difficult however, and if space permits it is recommended that the method followed in the receiver shown in Fig. 5 he used

In this version, the entire converter is built into a cut down i.f. can and mounted at the side of the receiver. The socket for the 6J6 converter tube is mounted on the top of the can while the two screws on the side of the can are the slugs used to tune the coils in the input and oscillator circuit.

The entire converter is mounted on a bracket of aluminum which is fastened to the receiver chassis by means of short machine screws. The condenser used to tune the antenna circuit and permit matching is on the rear of the can and is not visible in the photos.

The diagram of the converter portion is shown in Fig. 6. It is essential that the antenna coil L_1 be of the slug-tuned

type to permit adjustment of the inductance. This portion of the circuit will be recognized as that of the popular R9'er and has the advantage of matching the antenna or feeder impedance accurately.

A 6J6 was selected as a combined mixer and oscillator. A triode mixer has a very favorable signal-to-noise ratio, and the stability of the 6J6 as an oscillator is excellent. As the 6J6 has only one cathode, the oscillator grid leak R2 is returned directly to the cathode, while bias for the mixer portion is developed across the resistor R3 in series with the cathode tap on the oscillator coil.

The oscillator coil may be either of the slug-tuned type or wound on a piece of rod or tube. A slug-tuned coil is preferable as the bugaboo of adjusting to the proper value by spacing turns or squeezing, is eliminated. In the event an air core coil is used in this position, it will be necessary to use a variable trimmer condenser across the coil to permit setting the frequency.

The plate of the mixer portion of the 6J6 is connected directly to the stator of the trimmer condenser mounted at the left of the receiver. A 2.5 millihenry r.f. choke acts as a plate load for the mixer.

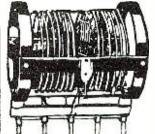
Input to the converter is through a connector of the type sold for auto radio use. This permits the use of a coaxial type feeder and allows rapid disconnection if the receiver is to be used on its original frequency.

The shielding of these receivers is excellent, and this is of the utmost importance if a converter is to be used. In one version, pickup of signals on the original range of the receiver was eliminated by removal of the antenna post. In the other version, the post was shielded by means of a small can made from a defunct electrolytic condenser. This can may be removed simply by removing one screw and the antenna connected to the post. The receiver may then be used on its original frequency.

An explanation of the operation of this type of converter is probably in order. The input circuit, consisting of L_1 , C_1 , C_2 , and R_1 , is broadly resonant in the band of 27 to 30 mc. The oscillator circuit is tuned to a frequency depending on the original range of the receiver. In the case of the BC-454, the oscillator is tuned to a frequency of 24 mc., while for the BC-455, the oscillator operates on 21 mc. Incoming signals in the range of 27 to 30 mc. beat with the oscillator frequency, and the regular tuning dial of the receiver is used. As the receiver in itself is selective, only a narrow band of frequencies is passed by the receiver, in the same manner in which the receiver operates by itself. The selectivity of the entire unit is exactly the same as the receiver itself. In effect the receiver

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BC-733 D Localizer Receiver
Freq. 108-110 Mc; Tube complement: 10 tubes—
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12SG7, 3—717A. NEAR NEW CONDITION.
Companion to the glide path receiver. Also



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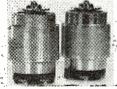
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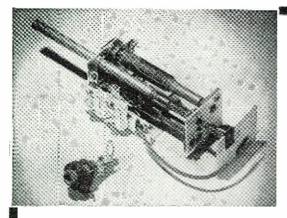
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June, 1948



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acts as a tunable i.f. chanel. This is essentially the same method used in the new Collins receiver. As the effective i.f. frequency is high, there is no difficulty with image response.

Determination of the received frequency is simple if it is remembered that the receiver dial will indicate this value simply by adding the frequency of the oscillator to that appearing on the dial. For example if a BC-454 is used, and the receiver dial indicates 5 mc. on a received signal, the frequency of that signal is 5 plus the converter oscillator frequency of 24 mc. or 29 mc. As the converter oscillator is fixed-tuned, it is possible to make it very stable with the result that there is no drift and the calibration does not change.

The two receivers converted were both purchased equipped with tuning cranks. Most receivers however, are sold minus these cranks, and in this event it will either be necessary to purchase these cranks in surplus, or use some other method of tuning. There are several possibilities. One is the removal of the threaded sleeve, and the use of a standard ¼ inch shaft coupling. A piece of ¼ inch i.d. brass or copper tubing, if squeezed slightly, will be a 'snug fit on the dial shaft. A piece of ¼ inch shaft may then be placed in the free end of the tubing and soldered in place. Any type of knob may then be used.

If a.v.c. is added to the receiver, it will be necessary to provide an audio gain control, in place of the r.f. gain normally used. The wiring leading to this control should be shielded, as well as the wiring to the noise limiter switch if a noise limiter is used. The noise limiter does not introduce noticeable distortion, and the inclusion of such a switch is not absolutely necessary.

A 1N34 crystal was used as the noise limiter, but it would be preferable to use a diode such as a 6AL5 or 6H6. The disadvantage of the crystals lies in their relatively low reverse resistance, which acts as a load on the detector circuit, reducing the effectiveness of the limiter. Some crystals will be found to give considerably better performance in this circuit than others, and if several are available, the best one should be selected. If a tube is used, the cathode of the tube goes to the audio coupling condenser, C10. The point at which the limiter operates may be changed by changing the value of R₁₄. Increasing the value of this resistor will result in greater limiting action, but the distortion will also increase.

If it is desired to use one of the fixedtuned converters to extend the range of the receiver to the ten meter band, the input and oscillator coils should be mounted at right angles, or shielded from each other. There is sufficient coupling between the two sections of the tube to give satisfactory injection, and no

provision need be made for any adjustment of injection. Triode converters are noticeably free from a critical value of injection voltage.

If a converter is used, the adjustment is simplicity itself. When construction has been completed, the frequency of the converter oscillator should be set, by adjustment of the tuning slug if a slug-tuned coil is used, or adjustment of the padding condenser if an air core coil is used. If the receiver used is a BC-454, the oscillator should be set to 24 mc. If a BC-455, the oscillator should be placed on 21 mc. A calibrated receiver or frequency meter will be of considerable assistance in this operation.

An antenna should then be connected to the converter and the receiver tuned until a signal is heard. The station transmitter used with a dummy load, or a modulated signal generator may be used to furnish the signal in the event no stations can be heard. When the signal has been tuned in, the coil slug and antenna condenser C_1 should be adjusted simultaneously for maximum signal strength.

When the adjustment has been completed, the signal may be peaked by means of the antenna trimmer on the receiver. This trimmer will require little or no adjustment in tuning over the band.

All tuning is done with the regular dial, and the converter will require no further attention or tuning unless an antenna system with a different feeder impedance is used.

Of the two receivers converted, the BC-454 gave somewhat better performance. Selectivity of this receiver is also somewhat better, being in the vicinity of 7.5 kc. at two times down.



Recording of Sound

(Continued from page 67)

The cathode circuit effects noted are due to fluctuations in the voltage drop across the cathode resistor, occasioned by variations in the d.c. component of plate current. The current indicated by the plate-circuit milliammeter is the average value of the fluctuating "signal" plate current, is identical with the d.c. component, and is the current that produces the cathode resistor drop. These facts may be better comprehended when it is remembered that the fluctuating signal plate current (Fig. 9) is an alternating current, corresponding to the signal, superimposed upon a direct current. It will be evident from the fundamental relations of this combination that the average value of plate current, as indicated by the plate-circuit milliammeter, will be constant in the company of the alternating component under distortionless operating conditions.

June, 1948

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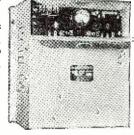
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Fig. 9 is a graphical representation of signal plate current. Imax. is the maximum value reached by the fluctuating plate current; I0, the zero-signal value; Imin., the minimum value. From these values, it may be shown that the percent second-harmonic content (often the most troublesome distortion factor) is equal to:

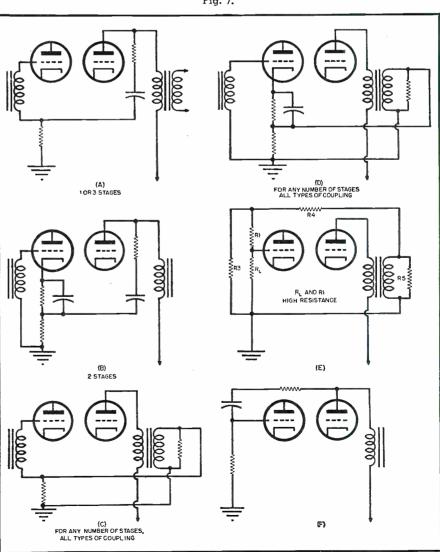
 $100[\frac{1}{2}(Imax+Imin)-Io]/(Imax-Imin)$ Quantitative methods of checking distortion are harmonic analyses, and are concerned with measurement of the actual amount of energy present in each separate harmonic of the signal frequency (or in the total harmonic content) and establishment of percentages with respect to the fundamental frequency. The most representative methods employed in wave analysis and the apparatus necessary thereto will be described presently.

The cathode-ray oscilloscope is notably useful in the observation of wave shapes. When the horizontal plates of the ray tube are energized by a sawtooth wave sweep-oscillator-amplifier circuit to furnish the linear time base, and a signal voltage which it is desired to observe is applied to the vertical plates through a substantially flat-response amplifier, the cathode-ray trace will be an exact reproduction of the waveform of the applied signal voltage.

An audio-frequency amplifier may be checked for distortion with the oscilloscope in the manner illustrated in Fig. 10. At the left is an audio oscillator possessing an output voltage waveform of known purity, next is the amplifier under test, and at the right is an oscilloscope having horizontal and vertical amplifiers with substantially flat frequency responses.

It is the purpose of the oscillator to supply a signal of as pure waveform as practicable to the amplifier, and that of the oscilloscope to reproduce the wave shape of the signal after it has passed through the amplifier. In order that as little distortion as possible be introduced by the instruments themselves, the oscillator used for such a test must be of exceptionally high quality and the amplifiers in the oscilloscope must possess an excellent frequency characteristic.

Fig. 7.



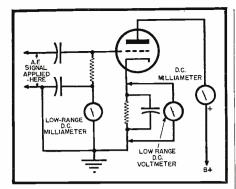


Fig. 8.

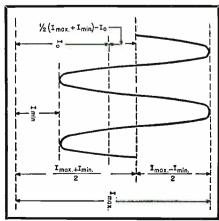
Likewise, the oscilloscope sweep circuit must be uncompromisingly linear in its characteristic.

If the amplifier had no distortion at all, the signal it delivered to the oscilloscope would be an exact reproduction of the input signal waveform. This is never encountered in practice, however, the most efficient amplifier arrangement being beset with the distortion characteristics of its tubes and other components.

For observations, a perfect sine wave (or, better still, a tracing of a single cycle from the test oscillator) might be inscribed on the transparent viewing screen of the oscilloscope, and signals from the amplifier matched to this pattern to discover variations from the original shape due to amplifier distortion. In making such a test, it would of course be necessary to adjust both oscilloscope amplifier gain controls in such a manner that the maximum amplitude and width of the signal trace coincided with those dimensions of the inscribed pattern.

With the low percentages encountered with most well-designed amplifying equipment, it will be difficult to estimate the percentage of harmonic content from the reproduced wave shape, in the oscilloscopic method, unless the operator makes use of the transparent screens furnished by some oscilloscope manufacturers for the purpose. These screens carry printed patterns of single cycles

Fig. 9.



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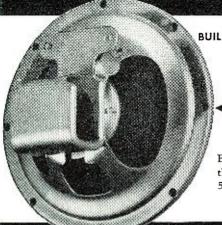
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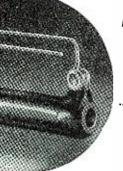
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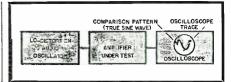


Fig. 10.

corresponding to the shapes obtained (variations from true sinusoidal) with various low percentages of distortion. Severe cases would result in images similar to Fig 11 which is an exaggerated representation of pronounced third-harmonic content.

Frequency Bridges

Certain bridge circuits, notably the Wien bridge (see Fig. 12) can be used for the identification of frequencies in the audio-frequency spectrum. If an alternating voltage is delivered to the bridge circuit, the latter may be adjusted for a null at that particular signal frequency. The null point would not hold for the same voltage of another frequency. Thus the adjustable element of the bridge might be calibrated to read directly in cycles-per-second.

The Wien bridge in its most useful form for this purpose would have its constants so chosen that the ratio arm R_2 is twice the ohmic value of R_1 , the condensers C1 and C2 are equal in capacitance, and the two simultaneously adjustable resistance legs R_3 and R_4 , are at all positions equal. Under these conditions, the frequency of the impressed voltage at null would be equal to:

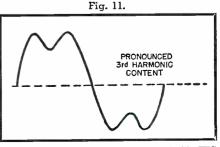
 $f = 1/2 \pi RC$

Where:

f is the frequency in cycles-persecond.

R is the resistance of R_2 or R_4 in ohms, C is the capacitance of C_1 or C_2 in farads.

Since the bridge may be balanced for only one frequency at a time, it would appear that any residual voltage indicated by the vacuum-tube voltmeter M, at null would be due to some other frequency or frequencies (such as harmonics of the fundamental.) This harmonic voltage would be due to the total of harmonic voltages present. As such, the bridge might be connected, as shown in Fig. 12, to the output circuit of an audio-frequency ampifier which is passing a signal from a high-quality audio oscillator.



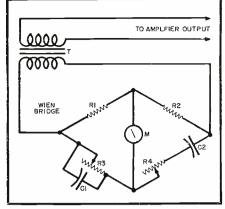


Fig. 12.

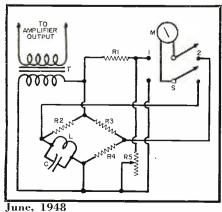
While the device might be used as shown as such a harmonic totalizer, the percentage total harmonic content with respect to the readings of the meter before and after null would not be reliable, nor would its error be uniform for all frequencies. These facts are due to the peculiar inability of the bridge to attenuate various harmonics equally.

Another popular type of bridge harmonic totalizer (developed by UTC) is shown in Fig. 13. Here, three legs of the bridge, R2, R3, and R1, contain pure resistance, while the fourth leg contains the shielded parallel resonant circuit, LC, which is resonant at the test frequency. The transformer T, like the one shown in the bridge previously described, must have an excellent frequency characteristic.

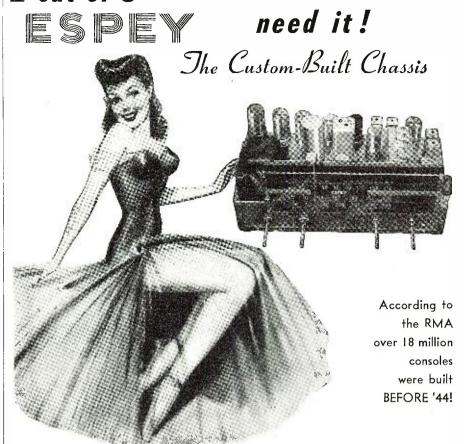
At resonant frequency of LC, the inductive reactance of the tuned circuit equals the capacitive reactance, the former is cancelled by the latter, and the bridge balances as if all four legs were pure resistance. Any voltage applied by the circuit to the vacuum-tube voltmeter is then due to harmonics of the test frequency (and it is assumed that these harmonics have been delivered to the bridge by the amplifier under measurement).

In operation, the double-pole, doublethrow switch, S, is thrown to position 2 and the bridge balanced with the assistance of the vacuum-tube voltmeter,

Fig. 13.



2 out of 3



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 $\%H = 100R_5/(R_4 + R_5)$

A dial indicator attached to the potentiometer R_s may be calibrated directly in these percentages.

(To be continued)

REFERENCE

*"The Aerovox Research Worker", Vol. 9, Nos. 6 and 7; Vol. 12, No. 7. Aerovox Corporation.

Receiver Design

(Continued from page 47)

type oscillator the cathodes of the two sections are tied together or are capacitively coupled for oscillator coupling. The 7F8 and the 6J6 are the most frequently used tubes in this type of circuit. The dual-triode converter has a high input resistance and a low noise level which contributes to its popularity.

The tuning condenser is mechanically sturdy and can be tuned easily. It does rely on wiping contacts for grounding the rotor and these contacts must be kept clean and lubricated for quiet operation.

Variable Inductance Tuner

Another type of tuner is the Meissner variable inductance tuner. It is used in their Model 2961. The r.f., oscillator, and mixer stages are constructed on a separate chassis which is completely shielded. A side view of this tuner is shown in Fig. 1 with the side shield removed.

The antenna terminals are on top of the chassis directly over the antenna coil. The primary is a two-turn coil with the center tap connected to the chassis. This primary is closely coupled to the antenna coil. The input is matched to a balanced 300-ohm line.

The tuning is accomplished by inserting the "blades" between the turns of the coils. The coils consist of three turns of wire. There are two "blades" on each tuning section which slice between the turns. The "blades" are cam shaped and mounted off-center on the tuning shaft. In this type of tuning there is no connection required between the rotor and the coils. Each of the tuning sections is insulated from the other by an insulated section in the tuning shaft. This is to prevent feedback through the tuning shaft from the mixer to the input coil. A shield is placed between the mixer and r.f. stage to further lessen feedback.

The theory of operation of this tuner is that the insertion of the "blades" in the coils not only reduces the coupling

between the coils but the "blade" itself acts as a shorted turn and further reduces the inductance. With the "blade" in the coil, inductance is at a minimum and the unit is tuned to the high frequency end of the band. This is opposite of the condenser-tuned coil for the completely meshed condenser tunes to the low frequency end. There is a slight increase in capacity when the "blades" are meshed. The change in capacity is very slight as compared to the change in inductance. This slight change in capacity is due in part to the wide spacing of the "blades" from the coils and also because the tuning shaft is not connected to the chassis.

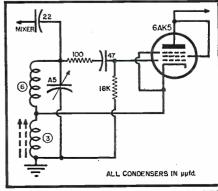
The tuning "blades" are specially designed and cut to give proper tracking. Final adjustments of tracking may be accomplished as follows: The coils are trimmed at the high frequency end with capacity trimmers. At the center of the band the center turn of the coil may be moved off its axis for tracking adjustment. At the low frequency end of the band the two outer turns are compressed or spread out, whichever is required, for proper tracking. Careful adjustment of these coils provides excellent tuner sensitivity.

The tuner uses a 6AG5 as an r.f. amplifier and another 6AG5 as a mixer. A 6C4 is used as a separate oscillator. The 6AG5 is one of the more efficient r.f. amplifier tubes at the higher frequencies. The input resistance of this tube is fairly high at FM frequencies and good gain is realized from the tube.

The oscillator is a hot cathode type. The oscillator voltage is coupled from the cathode of the oscillator, through a 10 mmfd. condenser to the cathode of the mixer which is 4700 ohms above ground. There is no shield between the oscillator coil and the r.f. coil which allows some inductive coupling between these coils.

Mechanically this type of tuner is simple and should be trouble-free. There are no wiping ground contacts and only two bearings. The tuning action is a rotary motion which enables coupling

Fig. 7. Method for spreading the short-wave bands of the "guillotine" tuner.



to the tuning shaft with a minimum of dial cord and pulleys.

The "Guillotine" Tuner

This tuner has been employed in the General Electric FM receivers that we have examined to date. It is used to tune both FM bands and to spread the short-wave bands. Although it is actually a variable inductance tuner, it receives its name "guillotine" from its peculiar physical shape.

The "coils" consist of two frames connected at their open ends. Tuning is accomplished by inserting a vane between the two frames. This reduces the mutual inductance between the two turns. The vane acts as a shorted turn and further reduces the inductance. The vane and frames are made of silverplated brass and are tool made. This makes possible positive control of tracking and calibration as the vane can be slotted to give the required change in inductance for a given change in vane motion. Both terminals extend through the chassis where direct connections can be made to the "coil." Each "coil" is mounted next to its respective tube, thus shortening the leads. This can be seen in Fig. 5. The antenna "coil" at the left of the picture is mounted at a right angle to the oscillator and r.f. "coils" to prevent feedback.

The vanes and AM tuning slugs are connected to the platform which is moved up and down with the tuning control. A metallic cable, seen in the center, is strung in windlass fashion to pull the platform down. A spring with the correct tension is used for raising the platform. Another version of this tuner is shown in Fig. 6. The "coils" and vanes in this unit are slightly smaller than those in the unit of Fig. 5. The insulated bar to which the vanes are connected is hinged and is raised by a cam on the tuning shaft which can be seen directly behind the tuning drum. The bar is pulled down by a spring. These units tune the high FM band only.

A schematic of the input circuit is shown in Fig. 2. All switching has been eliminated except that required for FM operation. The tuned circuit is composed of the antenna choke coil (1), condenser (A1) and the tuning coil (2). The signal is introduced across the antenna choke coil which is shunted by a 100 mmfd. condenser. The antenna trimmer (A1) has a capacity of 3-30 mmfd. When the receiver is switched to the low band FM, a 150 mmfd. condenser is shunted across the antenna choke coil and (A1) is shunted by (A2). (A2) has a range of 80-130 mmfd. Thus the tuner can be switched from one band to the other with a minimum of circuit changes. A 6AK5 is used as an r.f. amplifier.

Switching the oscillator from one band to the other is done with a mini-June, 1948

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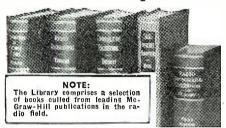
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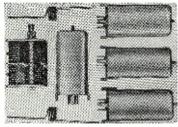


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BROOKS RADIO DIST. CORP. 80 Vesey St., Dept. B., New York 7, N. Y. mum of switching as illustrated in Fig. 4. The tuned circuit is composed of the FM oscillator coil (3), condenser (A3) and the cathode choke (4). (A3) has a 3-30 mmfd. capacity range. When switched to the low FM band, the circuit composed of (A4), the oscillator cathode choke coil (5), the 47 mmfd. and the 56 mmfd. condensers, is shunted across the FM oscillator coil. The oscillator voltage is coupled from the oscillator cathode to the mixer grid with a 10 mmfd. condenser.

Efficient spreading of the short-wave bands is obtained as shown in Fig. 7. A short-wave oscillator loading coil (8) is connected in series with the FM tuning coil (3). (A5), having a capacity range of 475-565 mmfd., is the shortwave trimmer. The FM tuning coil is a small part of the total inductance in the circuit and can produce only a small change in the total inductance. There are no wiping contacts in this tuner and noisy tuning or microphonic howl seems unlikely.

In spite of the mass of the tuning mechanism these units seem to be smooth in tuning and the backlash on the samples we have examined is negligible.

(To be continued)

Gang Tuning

(Continued from page 48)

the coil plus wiring and socket capacity. This must be estimated but will average 10 to 15 micromicrofarads.

To determine the values of L and C for the oscillator, the same formulas are used, except that K_1 and K_2 are calculated for the end frequencies of the desired oscillator range, depending upon the choice of an intermediate frequency.

As a guide in winding coils on Millen forms see Table 1.

It can be seen from this table that the slug will vary the inductance over a range of about 1.6 to 1.0 between full-in and full-out positions. If a value of L between two of the coils listed in the chart is needed, it is a simple matter to interpolate closely enough to get the desired value to fall within the range of adjustment. Inductance can also be computed from any of the standard inductance formulas, bearing in mind that the slug will increase the value in accordance with the ratio just given.

Slightly higher Q is obtained if the slug enters the form from the bottom of the form, as the brass adjusting screw tends to lower the Q slightly. The adjusting screw can be cut off and reslotted if it projects too far for the chassis depth. The threads are a nonstandard 6-40, so care should be used to avoid damaging them.

The advantages of this method of gang tuning are immediately apparent

| | IRNS & RE SIZE | SPACING | L (max.) | L (min.) |
|-----|-------------------|--------------|----------|----------|
| 114 | t. #32 en. | closewound | 106 | 67.5 |
| 40 | t. #32 en. | closewound | 31 | 20 |
| 36 | t. #28 en. | closewound | 18.3 | 11.6 |
| 18 | t. #22 en. | closewound | 5.07 | 3 |
| 12 | t. #18 en. | closewound | 1.98 | 1.40 |
| 5 | t. #22 en. | doublespaced | .81 | .53 |

Table I

when one aligns a receiver using it. Bandspread may be varied over rather wide limits, since both inductance and the fixed to variable capacity ratio may be readily changed. Bandspread is increased by decreasing the padder value, and increasing L to bring the frequency range back to that desired. Alignment is not a straightforward procedure, but it should not present any serious problems, either

Since the local oscillator frequency is the governing factor, it should be aligned first. Set up an accurate signal generator on the desired band. With the r.f. coil removed and a resistor of 20,000 to 50,-000 ohms substituted for it between grid and ground of the mixer stage, tune the receiver to the high end of the band (minimum capacity). Tune the signal generator back and forth slowly until the point of response is found. If this response occurs at a higher frequency than that desired, increase the padder capacity until the response is at the desired high frequency end of the band. Check the low frequency end of the band by tuning the receiver to the low end of the band and tuning the signal generator back and forth until the response is found.

Position of the low frequency response should be shifted by tuning the coil slug. Both these adjustments should be rechecked at least five times, as there is a noticeable interaction! Once the oscillator is adjusted to cover the desired range, the r.f. coil can be replaced, and the r.f. circuit peaked by varying the padder at the high end, and the coil slug at the low end of the band, rechecking several times as before. Just a tip, if a plate tickler oscillator is used, take the injection from the plate, not the grid

To prove his theories, the author built the receiver described by C. V. Haves in the February, 1947, issue of RADIO NEWS, with the exception that the converter and oscillator were built according to the schematic diagram, Fig. 1. Tracking error was checked using a "resonator", a four inch piece of polystyrene tubing with a brass slug in one end and a powdered iron slug in the other. The test is conducted by inserting first one end, then the other, in the r.f. coil. If the brass gives an increase in output, the inductance is too large, while if the iron

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gives an increase, the inductance is too small. If both ends cause a decrease in output, tracking is perfect at that frequency. This test was conducted at six different frequencies in the 80 meter band, and the tracking error was negligible.

In building a receiver following these ideas, it is recommended that a tuning condenser of about 50 micromicrofarads per section be used, as this will give a fairly high C/L ratio and tends to minimize drift. For the same reason, the padder condensers should be of the small zero or negative drift ceramic type. There is room enough inside the coil form shield to mount them, provided about one half inch of the coil form is cut off. A hole can be drilled in the top of the shield for access to the screw.

Another advantage not previously mentioned, is that the dial calibration can be readily reset to the desired end points, even though the i.f. frequency of the receiver may be changed somewhat. This is a decided help in dodging i.f. interference when an i.f. in the vicinity of 1600 kc. is used.

In closing, the author wishes to point out that the formulas given may be used in figuring tank circuit constants for any application where it is desired to cover a given definite range of frequencies, that is, a v.f.o. tank.

D.C. Supply

(Continued from page 69)

As a matter of fact, the improvement in all of the various characteristics discussed is brought about by one simple circuit addition. It improves stabilization, regulation, internal impedance, and

First, let us look at a fault that is common to many regulated power supplies, excessive starting voltage. If the rectifier and series rheostat tubes heat up quicker than the control tube, the bias on the rheostat tube will be zero momentarily and the power supply will deliver its maximum possible voltage. This may be high enough to cause damage, either to components in the

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By JOHN E. LOVETT

N THE belief that many servicemen In the benefithat many sample and inexpensive condenser tester, I am passing along details on such a unit. The complete schematic is shown in Fig. 1. The purpose of the unit is primarily that of testing for leaks, opens, and shorts in condensers, but it may be used for the same purpose on resistors, chokes, etc. Also, by insertion of test leads in the proper jacks it is possible to obtain a fairly wide range of variable capacity, resistance, or voltage.

Condensers may be inserted directly in the circuit by placing their negative leads in the neon light jack and their positive terminals in the d.c. jack. If the condenser is good, the neon light will flash (the length of the flash depending on the capacity of the condenser), and then go out. If the con-denser is open there will be no flash. If shorted, a continuous glow will indicate this condition. With a leaky condenser, the light will flicker continuously. In the case of condensers of high value, a quicker charge may be obtained by first inserting the condenser from d.c. to ground. The d.c. to ground is variable from 35 to 165 volts by means of R_2 .

An a.c. jack is provided for testing those condensers whose capacity is too low to show a charging flash on the neon light. By placing the positive terminal to the a.c. jack and the negative terminal to the neon light jack a continuous glow will result if the unit is not open, even on low value micas. Low value condensers will show shorts on the d.c. jack. The a.c. to ground is variable from 25 to 110 volts by means of R1.

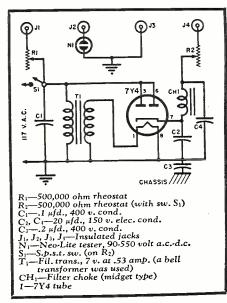
A bell transformer was used for the filament of the rectifier. Its secondary was rated at 10 volts but when it was connected into the circuit its voltage was just about the required value. If the secondary proves to be too high, it may be regulated by means of resistors.

Parts used in this tester are not critical. Volume controls were used to control the voltage but any variable resistance might have been used in their place.

If it is not convenient to place the condenser in the jacks, test leads may be used with clips replacing the regular cord tips. These leads may also be used to place a condenser of any desired value across one in a circuit.

With the line switch in the "off" position and using the test leads, the a.c. and ground jacks furnish a variable resistance from 100 to 500,000 ohms. This is accomplished by variation of control

Fig, l.



unit to which the supply is connected, or to meters connected into the circuit. A simple means will be shown which provides a time delay during this starting period and eliminates the undesirable starting surge. It is necessary to add that this time delay circuit adversely influences the characteristics discussed previously to a slight degree. This will be reviewed.

Circuit Change for Improved Operation

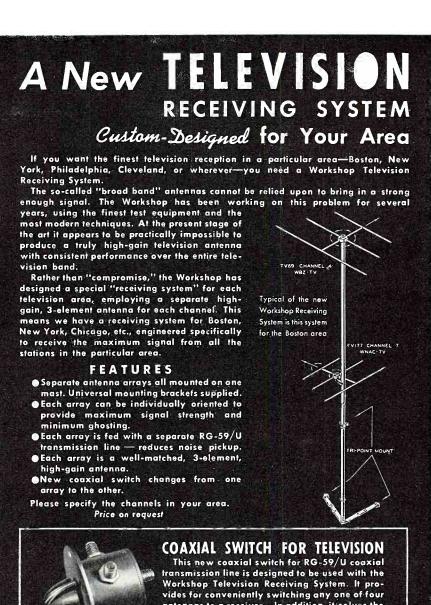
Before showing the circuit change involved, let us take a hasty glance at the conventional regulator, Fig. 2A, representing one version. Here we recognize the rheostat tube, RT, in series with the supply and providing the variable voltage drop. It is in effect an electronic rheostat and does the regulating. It does so by virtue of the fact that its bias is supplied by the plate current of the control tube, CT. The grid of the control tube is connected into the output circuit and its bias is affected by any changes in output voltage. Thus we have the usual feed-back d.c. amplifier-type voltage regulator whose action is amply covered by the references in the bibliography. Its characteristics regarding stabilization, etc. are in the order of values reviewed above.

A method which has been devised to improve the regulation so that the variations of regulated output voltage may be reduced to zero or even reversed is presented herewith. This is accomplished very simply as shown in Fig. 2B, which adds a potentiometer or resistor in the screen supply circuit. This reinforces the regulating action as described below and reduces the output voltage variations. They can be made negative if the screen voltage adjustment is run up high enough.

Suppose the load current is reduced. The output voltage tends to rise, causing the control tube grid to go in a positive direction. The regulating action carries through to keep the output voltage from rising excessively.

As this occurs, the unregulated input voltage, E, does rise, due to the normal regulation of the rectifier and filter. With RS in the circuit, the control tube screen voltage goes more positive. Since this is the same direction as the change in control grid voltage, the regulating action is reinforced or made more effective than before. It has been found that the variation in output voltage reduces as the setting of RS is advanced, until it runs through zero and finally becomes negative. By this simple means then, the ultimate in regulating action is achieved. In a commercial design it would be adequate to pick two resistors of proper value to accomplish this condition and use them since adjustment of this compensating action would not ordinarily be required.

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Since the internal impedance of the supply is determined by dividing the voltage variation by the value of current variation which produces it, it follows then that by the addition of the compensating action described above with its attendant reduction in output voltage variations, the output impedance of the supply is correspondingly reduced. With the proper degree of compensation, the impedance is reduced to zero and may be made negative if desired.

Since the output impedance is a characteristic that may appear to have more significance in some applications than that of voltage variations, it may be well to emphasize the fact that it may thus be reduced to zero.

This arrangement also reinforces the regulating action with respect to changes of supply voltage. An increase in supply voltage tends to increase the regulated output voltage and causes the grid of the control tube to go in a positive direction. Since at the same time this increase in supply voltage causes the screen voltage to move in a positive direction, it reinforces the regulating action and the variations in output voltage may be reduced to zero by proper setting of RS.

Since hum voltages in the source may be regarded as equivalent to the existence of variations in supply voltage, the analysis of the previous paragraph may be used to show that hum in the output may be reduced to zero. It is apparent that the setting of RS that provides constant output voltage when supply voltage varies will also cancel out all hum voltages, since they are equivalent.

It should be pointed out that zero variation of output voltage with respect to load curent changes will be obtained with one setting of RS whereas zero variation with respect to supply voltage changes may require another. The setting therefore would be made to satisfy the requirement. If both are desirable, the regulation of the source, E, will have to be made of proper value to bring these two settings together.

For example, assume as one extreme case that the source has very good regulation. If so, changes in load current would change E very little, and RS would have to be set high to get zero regulation in the output. Under that condition, however, the system would be highly overcompensated for supply voltage variations, since they would then affect the screen voltage a great deal. If, on the other hand, the regulation of E is very poor, changes of load current would produce large changes in E and RS would have to be set very low. The system would then be undercompensated for changes in supply voltage. A proper value of regulation in E then would enable the choice of one setting of RS or the use of fixed resistors to

accomplish perfect regulation for changes either of load current or supply voltage.

This reinforcing action may be secured by using other grids in the same general manner and will not be enlarged upon. Also, if desired, an arrangement may be used to keep the d.c. screen voltage constant on the control-tube as RS is varied. This would not ordinarily be needed and is not shown, since the usual variation will not be great enough to appreciably alter the operation of the system. The screen could readily be kept at constant d.c. potential however by connecting it in a variable divider which could be coupled to RS mechanically, such as a dual potentiometer, to drop the voltage as RS raises it. Any similar compensating arrangement will equally effective.

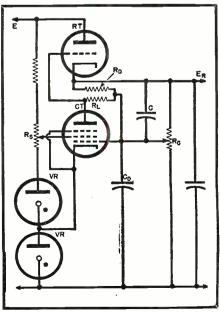
Typical Performance

A model power supply was constructed for use in a piece of special test equipment, shown in Fig. 1. The power supply is the lowest of the three panels. A voltmeter is shown at one side and the output voltage adjusting potentiometer appears immediately below it. The load milliammeter appears at the other side and its "Push to Read" unshorting switch appears below it. Other views of the power supply appear in Figs. 4 and 6, and the layout of parts and simplicity of arrangement are clearly shown. The added compensating potentiometer may be seen. Fig. 3 shows the schmatic.

This power supply is rated 100 ma. at 200 to 350 volts d.c. The following performance is obtained:

1. Stabilization: The output was adjusted to 270 volts and was then connected through an 0-2-1/2 volt d.c. voltmeter to 270 volts of "B" batteries. By

Fig. 5. Time delay circuit RdCd has been added to the regulator shown in Fig. 3.



this means, a 2-½ volt change in output voltage would give full scale reading on the meter. The primary voltage was set at 120 volts, then the output voltage change was checked when the primary voltage was dropped to 110 volts. This was done first with no compensation (screen potentiometer set at zero), then repeated with different settings. See Tabe 1, "Stabilization".

The first figures given (Output Voltage Change) are the result of slow changes in primary voltage. The second row are transient changes that occur in the output when the primary voltage is dropped suddenly. Within a few seconds the voltage reaches the value given in the upper row and therefore is the same as for slow changes.

The cause of this transient condition is the time delay circuit, shown in Fig. 5. This circuit is explained in a later section. A study of the circuit will reveal that the changes in primary voltage change the plate current in the control tube. The bias on the rheostat tube, RT, then tends to drift while the voltage on the delay condenser, CD, reaches its new operating level. Thus it is imposible to set the compensating potentiometer to reduce both the steady state and transient changes in output voltage to zero.

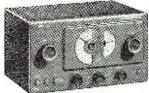
By disconnecting *CD*, the transient condition disappears. The quick changes in primary voltage then produce precisely the same changes in output voltage as slow changes do and, at midrange on the compensating potentiometer, the stabilization is made perfect as measured in the manner described. Thus, where perfect stabilization is the prime requirement, the time-delay cirsuit is not used.

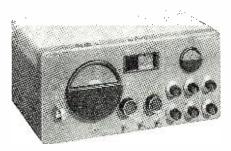
2. Regulation: The same setup was used as before. For this test the load was increased from 50 to 75 millamperes with different degrees of adjustment on the compensating potentiometer. The performance data is given in Table 1, "Regulation".

These measurements indicate that perfect regulation is obtained with a compensating potentiometer setting of about ¾ of maximum. With the delay circuit in use, we note that the same effect takes place as in the case of stabilization transients as explained above. Where time-delay is not needed, the time delay circuit may therefore be omitted and no transient will appear.

Whereas perfect stabilization occurs with ½ maximum setting of the potentiometer, we observe that ¾ maximum setting is required in this particular power supply for perfect regulation. As pointed out previously, these two points may be brought together by choice of proper regulation in the rectifier-filter circuit. Since more compensation seems to be needed for regulation (¾) than

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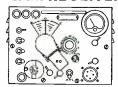
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for stabilization (½), we know that increasing the voltage variation out of the filter as load is changed, which is the regulation of the rectifier-filter, will permit compensation with a lesser setting of the potentiometer. Therefore, a little poorer regulation in the rectifier-filter will bring the two settings together and permit perfect stabilization and regulation at the same setting. If necessary, a resistor may be added in the circuit to do this, and it would be placed in the rectifier-filter circuit at any convenient point.

3. Internal Impedance: Since the internal impedance may be calculated from the data taken on regulation, this has been done and appears in Table 1, "Internal Impedance."

A question is likely to be raised concerning the effects of using a power supply with a negative internal impedance, the fear being that motorboating or oscillation may be set up due to it. In general, it may be stated therefore that instability due to negative power supply impedance will occur only when such negative impedance is higher than the positive impedance of any load connected to it.

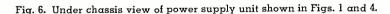
4. litter: Most power lines, and particularly those in industrial areas where much of our laboratory work is done, suffer from transient conditions, where the voltage jumps sharply for a few cycles from time to time. This is ironed out in the output of the regulated power supply, as in any other primary voltage variation. It is possible to make a very sensitive measurement of jitter however with a vacuum tube voltmeter since it is a transient or a.c. variation. Very sensitive vacuum tube voltmeters are in common use and these may be used. A typical measurement on the supply under consideration is as follows: Average

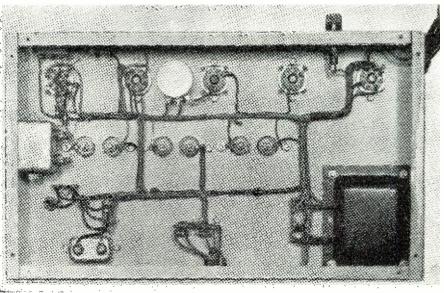
jitter with no compensation—20 millivolts; Average jitter with best compensation—less than 1 millivolt.

5. Hum: Since hum in the output is equivalent to voltage variations in the output due to input voltage (to the regulator) variations, it is reduced in like manner, as follows: Hum with no compensation—4 millivolts; Hum with best compensation—less than 0.2 millivolts.

When a regulated power supply is first turned on, the rectifier and rheostat tubes may heat up faster than the control-tube. The rheostat tube will then have zero bias, since the control-tube is not yet drawing plate current, and the regulated output will rise to its maximum attainable value. In general, this is undesirable and it may be dangerous, since regulated supplies involve rather large voltages to take care of the usual voltage drop across the rheostat tube. If the output voltage desired is rather low, the high initial d.c. may be dangerous to the equipment connected to it.

This starting surge, which will last from the time the rheostat tube begins to conduct until the control-tube has heated up, can readily be eliminated by adding the RD-CD delay combination shown in Fig. 5. Inspection of this circuit will show that the condenser, CD, holds the grid of RT near ground potential when the rheostat tube first begins to conduct. This puts a high bias on it and limits its initial plate current to a minute value. Of course this small current will permit ER to build up slowly and it will be found that the rheostat tube "lifts itself by its bootstraps," since CD charges up slowly and limits the speed of the rise by holding high bias on the tube. It is necessary to use an RC product of only one or two to get a long delay for this reason. One megohm and one microfarad will permit the output





voltage to rise to half its normal maximum after a time interval of several seconds.

These values are probably sufficient for any case where the rheostat tube is indirectly heated and will not be conducting more than just a few seconds before the control-tube takes over control. If, however, the rheostat tube is a quick or direct filament type, the constants may be readily increased to provide somewhat longer time delay.

- 1. The regulation, stabilization, jitter, and hum reduction of a conventional regulated d.c. power supply may be made virtually perfect and the internal impedance reduced to zero by the simple change of adding a small amount of unregulated voltage to a grid of the control-tube. This requires only a potentio-
- 2. By combination of the above with a proper degree of variation of unregulated supply voltage with respect to load, the variation of regulated output may be made virtually zero both for changes of load current and supply voltage with the same setting of the potentiometer, or a resistor may be used.
- 3. By the addition of a condenser-resistor combination to the conventional supply, a starting time-delay is furnished to limit the speed of build up of the output voltage, thereby avoiding the high output voltage that can result with a quick heating rheostat tube and without some such protective device.

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-30-

Modulation Percentage

(Continued from page 52)

obtain modulation patterns. The .5 mfd. condenser must be mounted as close as possible to the plate terminal of the last i.f. tube socket and connected by means of a short length of shielded hookup wire to a coaxial cable connector at the rear of the receiver chassis. A length of flexible coaxial cable is plugged into this connector and is hooked at its other end to the "high" horizontal input terminal of the oscilloscope. The outer shield of the cable is connected to the "low" (ground) horizontal input terminal. A 50,000 ohm, 1 watt carbon resistor is connected by the shortest path between the "high" horizontal and vertical input terminals. The oscilloscope amplifiers must not be used, since in general they will not pass the high radio frequencies. Employ the "DIRECT" input, and switch off the linear sweep oscillator.

The stray capacitances introduced by these connections will disturb the receiver circuit somewhat, so that it may be necessary to realign the last i. f. trimmers after the connections have been completed. By employing coaxial cable, as shown in Fig. 2, the external capacitances are kept constant. If an individual operator does not care to install the coaxial connector, he may run the coaxial cable, through a hole in the rear of the receiver chassis, directly to the coupling condenser. However, this arrangement will not permit easy disconection when desired.

To insure that alignment is preserved in the last i.f. stage when the cable and oscilloscope are disconnected from the receiver, a plug may be prepared as a substitute for the cable and oscilloscope capacitance and resistance. This plug is inserted into the coaxial chassis connector whenever the cable is removed. Such a plug is shown in Fig. 2. The capacitance of condenser C must equal the total capacitance of the cable and oscilloscope input circut, and the resistance R must be equal to the internal resistance between the horizontal de-

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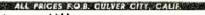
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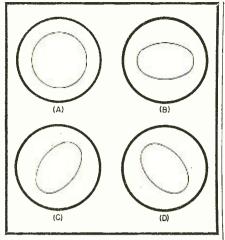


Fig. 3. Patterns obtained with various resistance-capacitance combinations.

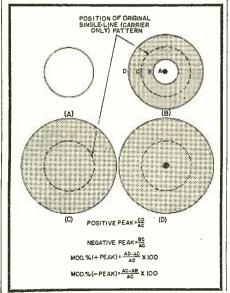
flecting plate and ground (usually a half-megohm). These values must be chosen for an individual case. The capacitance will be determined largely by the length of the coaxial cable. Also, internal oscilloscope resistance will vary with different models. Obtain the correct resistance value by referring to the oscilloscope circuit diagram.

Operation of the System

It is a comparatively simple matter to tune-in signals and to check modulation by the oscilloscopic method. This system is useful also for checking extraneous modulation, such as hum, noise, and parasitics on c. w. signals (switch-off the beat frequency oscillator in the receiver when making the latter tests).

Naturally, most accurate results will be obtained when the received signal is

Fig. 4. Modulation patterns obtained from received signals. (A) Carrier only. (B) Under 100 per-cent modulation. (C) 100 per-cent modulation. (D) Over 100 percent modulation. Equations at bottom are used for calculating modulation percentage measurements on (B).



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in the clear, free from static, and not fading, and when the receiver is operating correctly. The receiver must have low hum level and all of its circuits must be correctly adjusted. It is advisable for the operator to check several signals of known modulation percentage on several carrier frequencies, in order to verify receiver performance. Any inaccuracies introduced by the receiver itself will be very small in a receiver of modern design.

Substitution Tester

(Continued from page 53)

most commonly used as grid-bias, coupling, and for other purposes. The values of the six resistors are 400, 50,000, 100,-000, 500,000 ohms and 2 and 5 megohms. By the same token, seven condensers most commonly used for bypass, coupling, filter, and other purposes were selected. The seven values are; .001, .01, .05, .10, .25, 30 and 50 mfd.

The use of continuity testing is now an accepted procedure in the service profession. With this instrument, these tests do not require the use of any additional unit. A continuity tester is used in conjunction with the substitution decade. This portion of the instrument affords continuity tests of both resistors and condensers. The line plug, located at the rear of this instrument, can be inserted into any 110 volt a.c. 60-cycle line. Continuity is indicated by means of neon indicator on the front panel. If the neon indicator lights, continuity is indicated.

Leakage of condensers can also be tested by means of this neon indicator. An open condenser is indicated by the failure of the neon to light, however, if the condenser is shorted a continuous glow will result. Many present day condensers have a definite percentage of leakage, however the amount is insufficient to affect operation of a receiver. This leakage may often affect the neon by causing it to glow slightly. A leaky condenser is indicated by a series of rapid flashes, the amount of leakage being determined by the rapidity of the flashes. Resistors can be tested for continuity in the same fashion. When checking resistances, the neon indicator will glow continuously, the brilliancy of the neon varying with the amount of resistance.

This substitution tester also incorporates an output meter, a unit not often available to servicemen. An indicator of the neon type, the output meter can aid the serviceman in the efficient and rapid alignment of radio receivers. The receiver under test is aligned in the conventional manner, the brilliancy of the neon being continuously observed. Maximum brilliancy of the neon indicates correct and full alignment. Connection of



tridge that opens broad new vistas of listening pleasure.

The Astatic Magneto-Induction Pickup represents the first clean break with traditional principles employed in the manufacture of magnetic type reproducers. Discarded now is the need for delicately spaced "air gaps," which collect lint and dust, become a prime source of trouble in other type magnetic pickups. Their elimination in the Magneto-Induction cartridge is a newly opened door to peak fidelity of reproduction that is stable and troublefree, even under the most consistent service or adverse climatic conditions.

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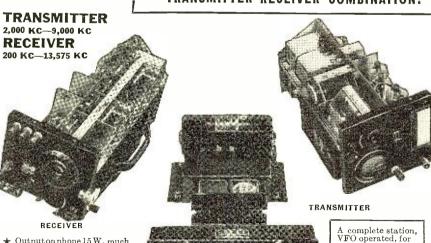
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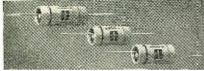


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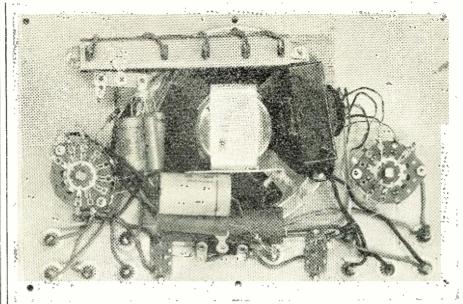
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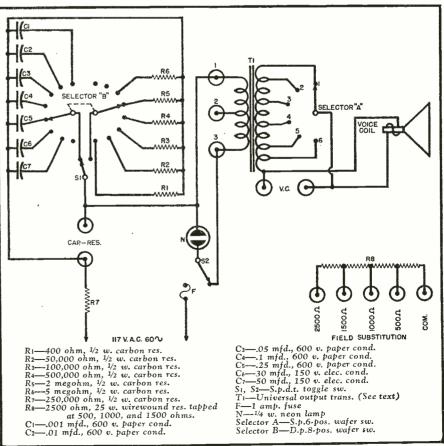
All component parts for this substitution tester are mounted on the front panel. Wafer switch at right is control "A". Tapped resistance at top of speaker is the field substitution resistor.

the output meter is made by means of input jacks 1, 2, and 3.

A complete circuit diagram of the instrument is shown in Fig. 2. The condensers are rated at 600 volts with the exception of the two electrolytics which are rated at 150 volts. The resistors are ½ watt units. The voice coil resistance of the speaker is 2.5 ohms. Field im-

pedances are made available by means of a heavy-duty, tapped wirewound resistor. The resistor is tapped at 500, 1000, 1500 ohms. All component parts are mounted on the front panel which is easily accessible by removal of the six panel mounting screws. The instrument is housed in a grey crackle metal cabinet measuring 10 by 7 by 5 inches.—30—

Fig. 2. Complete circuit for the commercially-built substitution tester.



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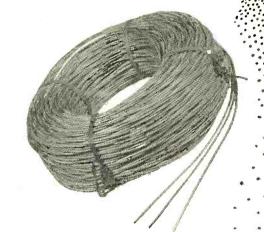
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This unit sold complete with power trans-former. 3 tubes and 3 controls . . . all wired and tested. Diagrams supplied.

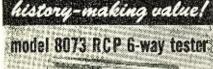
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Spot Radio News

(Continued from page 20)

will be a day! "For tens of thousands of radio stations around the world," as Mr. Coy points out, "it will be F-Day-when they shift to new frequencies. It will be a day of sweeping changes for stations employing long distance 'high' frequencies." He adds, with emphasis: "But I don't want to start a panic among American broadcasters or American radio listeners-let me make it as plain as a pikestaff that these changes do not affect this nation's broadcasting frequencies."

SPEAKING OF FCC, it's repetition to say that they are in hot water and will be for some time if not permanently. To state the problem again: How can enough room be made in the spectrum for all the services clamoring to use it? This, in Mr. Coy's view, is the toughest problem facing FCC and the industry-"a national problem in need of sound planning for the future domestically." He believes that "the most significant factor is the problem of getting the fullest use of the spectrum above about 30 megacycles. Except for a certain band of frequencies that require international standardization because of their use by ships and aircraft," he points out, "this upper spectrum is free to be divided." How is another, and knotty question that Mr. Cov frankly recognizes, but thinks should be shared, not only with the industry, but with electronic engineers. If they don't do their job (as they have so far done magnificently) there is going to be trouble all along the line, especially as the air become more and more crowded. "Certainly we cannot expect to utilize this part of the spectrum," he says, "without serious restrictions on the geographic location of stations unless we wage a relentless war on spurious emissions and unwanted harmonic radiations. The suppression requirements are particularly severe for services in which the offending transmitters are adjacent to or move among the affected receivers, such as in the amateur and urban mobile services, or are of very high power, as in FM and television. I should like to impress on engineers the seriousness of this problem and ask them to consider as incomplete any transmitter design which fails to include adequate provision for such suppression. As to receiver design, it is evident that many present broadcast receivers are deficient in regard to suppression of oscillator radiations and in selectivity." As for dividing up the spectrum fairly, Mr. Coy faces the future with resolution but with full realization of the seriousness of the problem, both tomorow and in the foreseeable future.

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"It becomes increasingly evident," he says, "that the most careful planning will have to be done on a continuous basis if the objectives of the Communications Act and the desires of the American people are to be met. Planning has been done and is being done. But the point I should like to stress is that we must, from time to time, readjust our sights and make as certain as it is possible for us to do that the next generation will be able to derive the maximum benefits from the public domain we call ether."

THIS IS NOT to imply that everything at FCC is on a one-big-happy-family basis by a long shot. The Commission was recently accused by Senator Charles W. Tobey, of the Senate Interstate Commerce Committee, of playing along with RCA, which the Senator claims did everything it could to block FM progress. He even went so far as to claim that FCC altered the records in FM allocations, a claim also made by Prof. Edwin H. Armstrong, FM inventor. While the Tobey fireworks were exploding on the Hill, FCC faced another problem in the FM field, raised by the FM Association. FMA has asked revocation proceedings against holders of FM construction permits who are negligent in putting their stations on the air. In one of the strongest statements of the young Association's existence, FMA charged that "many broadcasters have obtained FM construction permits to keep competition out, but have not adhered to FCC regulations which require that stations be on the air eight months after construction permits are issued." A resolution, adopted unanimously by the FMA Board of Directors in behalf of the Association's 250 members, asks that FCC conduct "show cause" revocation proceedings in cases where the Commission "feels that the construction permit holders have been negligent" in putting stations on the air. FMA spokesman J. N. (Bill) Bailey, executive director of the Association, managed to get in a plug for his favorite brand of radio while fulminating against FCC. Because of the "acute shortage of FM channels in certain areas," he stated, building delays "are depriving the public of the finest aural broadcast service attainable in the present state of radio art." Statistically, FMA stated its case to FCC as follows: "There are today 442 commercial FM stations on the air. In January, 1947, Charles R. Denny, former FCC chairman, stated that 700 FM stations should be in operation by the end of that year. Mr. Denny based his prediction on the number of construction permits and conditional grants issued by FCC. But today, fourteen months after that prediction, little more than half that number are in operation. We believe the



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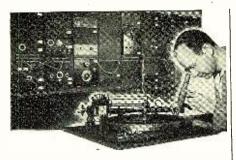
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time is here for drastic action on FCC's part."

EDWIN H. (FM) ARMSTRONG, incidentally is apparently not going out of the inventing business now that his favorite brainchild has become so popular. Recently he applied to FCC for an experimental television station in the upstairs band. Mr. Armstrong wants authority to use 480-500 mc. with 50-kw. transmitter full time, plus "as much antenna gain as appears proper for the television system." Last word is that he plans to experiment in color as well as black-andwhite. He plans to do his work at his laboratories at Alpine, N. J. The frequencies he wants are at the lower end of the band now set aside for television experimentation, and the band extends up to 900 mc. Desire of television stations for commercial outlets within the present low-band (ranging between 44 and 216 mc.) has already stirred concern for development of the higher area. Prof. Armstrong hasn't deserted FM by his new interest. Indeed, FM is what got him busy on television.

The AFCA

(Continued from page 45)

tion of private industrial capacity encouraged them to maintain liaison with ten selected associations as sources of general information relating to industrywide manufacturing capacity. Armed Forces Communications Association was one of those ten associations. Its growth during the two years since it was founded has been more than was anticipated. Americans interested in being on record as wanting to assist our country in securing and maintaining superiority in communications for our Air Force, Army and Navy are joining in increasing numbers, especially since the worsening world situation has become known to them. Membership is not restricted to former, present or future sailors, soldiers or airmen, but solely to Americans.

And in conclusion I should like to quote from a statement made recently by the Commandant of the Air University. His views seem to me most timely. He said, "The United States faces a state of insecurity in the future unparalleled in our history. Times have changed, and very much the worse for us. Time was when we could count with certainty upon a warning period measured in many months at the very least before any real damage could possibly be brought against us. Isolated, safe and secure behind our great ocean barriers, we could have watched the slow, laborious build-up of the great amphibious force and its enormous logistic train which alone could have constituted a real threat. We should have been able to mobilize and train, to de-

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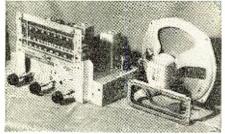
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fend against one of the most difficult and perilous of military operations—an ocean crossing with a landing and build-up on a hostile shore in the face of determined opposition. With such security no wonder we have developed into one of the least military minded nations in the world. But what a change is here!!" EDITORS NOTE: The immediate need for close cooperation between the military and industry is so great at this time that RADIO NEWS has made its vast coverage available to the AFCA. Chapter notes and other association news will appear regularly in this magazine).

More detailed information about the association may be had on request to National Headquarters, 1624 Eye Street, N.W., Washington 6, D. C.

-30-

RADIO JOBS ABROAD

THE Civilian Recruitment Office, Signal Corps Photographic Center, 35-11 35th Avenue, Long Island City 1, New York has just released a list of positions being offered with the Signal Corps in the areas indicated.

Positions are "expected" appointments on a two year basis, unless otherwise indicated. Men from 21 to 50 are acceptable for these positions. Positions in Japan include a radio engineer, a telephone repeater repairman, teletype mechanic, and ultra-high-frequency equipment repairman. Jobs on Guam, Saipan, Tinian, and Iwo-Jima (for one year appointment) include radio engineer, radio engineering aide, radio traffic control operator, electrical draftsman, radio repairman, radar repairman, radio station engineer, and instrument repairman. A signal engineer is needed in Manila while Hawaii can use an electrical engineer and a radio engineer. There is a position open in Germany for a radio engineer.

These positions are just a few of those offered and persons interested in further details regarding these jobs should contact the Civilian Recruitment Office at the above address.

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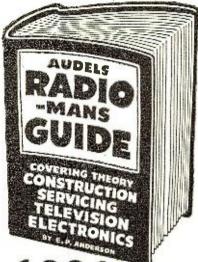
WE ARE SORRY ---

Despite the fact that RADIO NEWS takes every reasonable precaution to insure the accuracy of material printed in the magazine, the release appearing in the April issue regarding the American Airlines training school is in error.

American Airlines has advised us that the company is in no way connected with the school mentioned in the release and that they are not seeking applicants for radio positions, such as were involved in the item, at this time.

We sincerely regret any inconvenience we may have caused our readers or American Airlines. The item originally came to us from a source we considered completely reliable.

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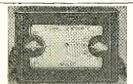
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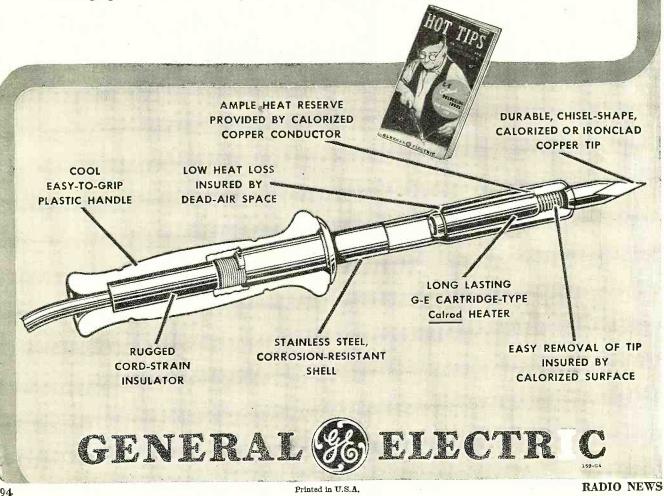
G-E Calrod—The Soldering Iron with Long Life

- The shell material, Type 18-8 stainless steel, will withstand hard usage without collapsing.
- The heater will withstand repeated jarring or rough handling, because it is embedded in highly compacted magnesium oxide.
- The life of the tip is considerably lengthened by the calorized surface. This retards corrosion during long hours of idling.
- The heater is dependably protected against grounding by the highly compacted, magnesium-oxide insulation.

FREE—With each G-E Soldering Iron

Packed with each Calrod Soldering Iron is a booklet that contains a wealth of information about soldering, tips to make the job easier and a flux chart that will be invaluable.

For additional information on G-E Calrod Soldering Irons write: General Electric Company, Electronics Park, Syracuse, New York.





EQUALLY MATCHED

Split the reed assembly of a Mallory vibrator down the middle and the two halves will match each other so accurately that no scale made will register a significant difference.

This precise distribution of weight is a major factor in assuring accurate output, reliable operation and long life.

Mallory Vibrators Make



The Mallory Replacement Vibrator Guide is free. The Vibrator Data Book is \$1.00—from your distributor or by mail.

the Best Replacements

Such careful manufacturing makes Mallory vibrators free of bounce and chatter and dependable in starting. More of them are used in original equipment than all other makes combined. That's convincing proof

they are the best replacement vibrators for you to stock.

In addition to assured quality, Mallory offers the most complete line in the business. Mallory standardization permits 12 basic vibrators to meet 90% of your replacement requirements. But a complete line of 52 vibrators is available to meet virtually every vibrator need.

Mallory "2448" Vibrator Deal

This deal gives you a handsome storage and display cabinet for your stock of vibrators, together with a selection of vibrators and buffer capacitors that will answer 75% of your requirements.



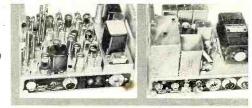
You pay only the service man's net price of \$2.4.48 for the six vibrators and twelve buffer capacitors. There is no charge for the attractive, convenient cabinet. Your Mallory distributor has them in stock for immediate delivery.

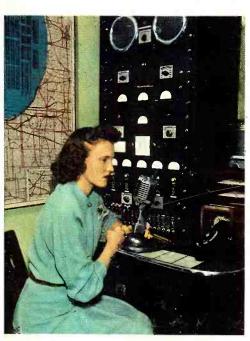
MORE MALLORY VIBRATORS ARE IN USE THAN ALL OTHER MAKES COMBINED

CAPACITORS . . . CONTROLS . . . VIBRATORS . . . SWITCHES . . . RESISTORS . . . RECTIFIERS . . . VIBRAPACK* POWER SUPPLIES . . . FILTERS *Reg. U. S. Pat. Off.

P. R. MALLORY & CO., Inc., INDIANAPOLIS 6, INDIANA

Greyhound Bus improves service, saves mileage, reduces delays with *Motorola* 2-way radio





Dispatchers communicate directly with drivers to adjust schedules to changing load conditions.

and Sylvania Lock-In Tubes...

BY MAINTAINING 2-WAY RADIO COMMUNICATION between dispatchers and buses on the road in the Chicago area, Greyhound has effected substantial operating economies — and at the same time has improved quality of its service to riders! Schedules are quickly readjusted, extra sections added, runs combined — as the dispatcher works with the up-to-the-minute reports coming in from drivers.

The 2-way communication is maintained by FM equipment built by Motorola, Inc., Chicago—using Sylvania Lock-In Tubes in the mobile units. These famous tubes stay put in their sockets, no matter how rough the road. They have no soldered joints, few welded ones. Short, direct connections reduce losses. Getter is located on top; separation of getter material from leads cuts down leakage.

This electrical and mechanical superiority makes the Lock-In the ideal choice for equipment on the road, in the air, on the rails . . . for marine radar, FM, television. See Sylvania Distributors, or write Radio Tube Division, Emporium, Pa.

SYLVANIA FELECTRIC

MAKERS OF RADIO TUBES; CATHODE RAY TUBES; ELECTRONIC DEVICES; FLUORESCENT LAMPS, FIXTURES, WIRING DEVICES; ELECTRIC LIGHT BULBS

