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Howard W. Sams

HANDBOOK OF ELECTRONIC TABLES & FORMULAS

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HANDBOOK OF ELECTRONIC TABLES AND FORMULAS

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PREFACE

In the Preface to the first edition of this book, published in November, 1959, we asked for recommendations of additional items to consider for inclusion in a future edition. Many suggestions were received and considered; most of them are incorporated in this volume. Hence, this book contains the information which users of the first edition—engineers, technicians, students, experimenters, and hobbyists—have told us they would like to have in a comprehensive one-stop edition.

The basic formulas and laws, so important in all branches of electronics, are given in Part One. Also included are nomographs to speed up the solution of problems involving Ohm's law, power, parallel resistance, and reactance.

Useful, but hard to remember constants, and standards which have been established by the government or industry, are included in Part Two. The comprehensive Table of Conversion Factors is especially helpful in electronic computations.

Part Three contains symbols and codes which have been adopted over the years. The latest semiconductor information is included, to keep you abreast of this rapidly expanding field.

Items of particular interest to electronics service technicians are included in Part Four. Data most often used in circuit design work are given in Part Five. The filter and attenuator configurations and formulas are particularly useful to service technicians and design engineers.

Mathematical tables, formulas, and other information are presented in Part Six. Binary numbers and an introduction to Boolean algebra—the tools of the computer field—are also included in this section. Many items of a miscellaneous nature are included in Part Seven.

No effort has been spared to make this revised handbook of maximum value to anyone, in any branch of electronics. Once again your comments, criticisms, and recommendations for additional data you would like to see included in a future edition, will be welcomed.

A handwritten signature in cursive script, reading "Newton W. Sams".

January, 1962

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Electronics Formulas and Laws

1. OHM'S LAW FOR DIRECT CURRENT

All substances offer some obstruction to the flow of current. Ohm's law states that the current which flows is directly proportional to the applied voltage and inversely proportional to the resistance. Thus:

$$I = \frac{E}{R}$$

$$E = IR$$

$$R = \frac{E}{I}$$

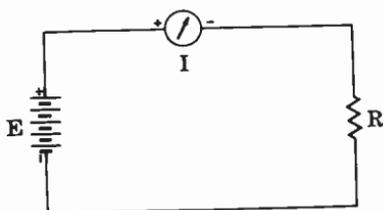


Fig. 1

where,

I is the current in amperes,

E is the voltage in volts,

R is the resistance in ohms.

2. DC POWER

The power P expended in load resistance R when current I flows under a voltage pressure E can be determined by the formulas:

$$P = EI$$

$$P = I^2R$$

$$P = \frac{E^2}{R}$$

where,

P is the power expressed in watts,

E is the voltage in volts,

I is the current in amperes,

R is the resistance in ohms.

Ohm's Law Nomograph

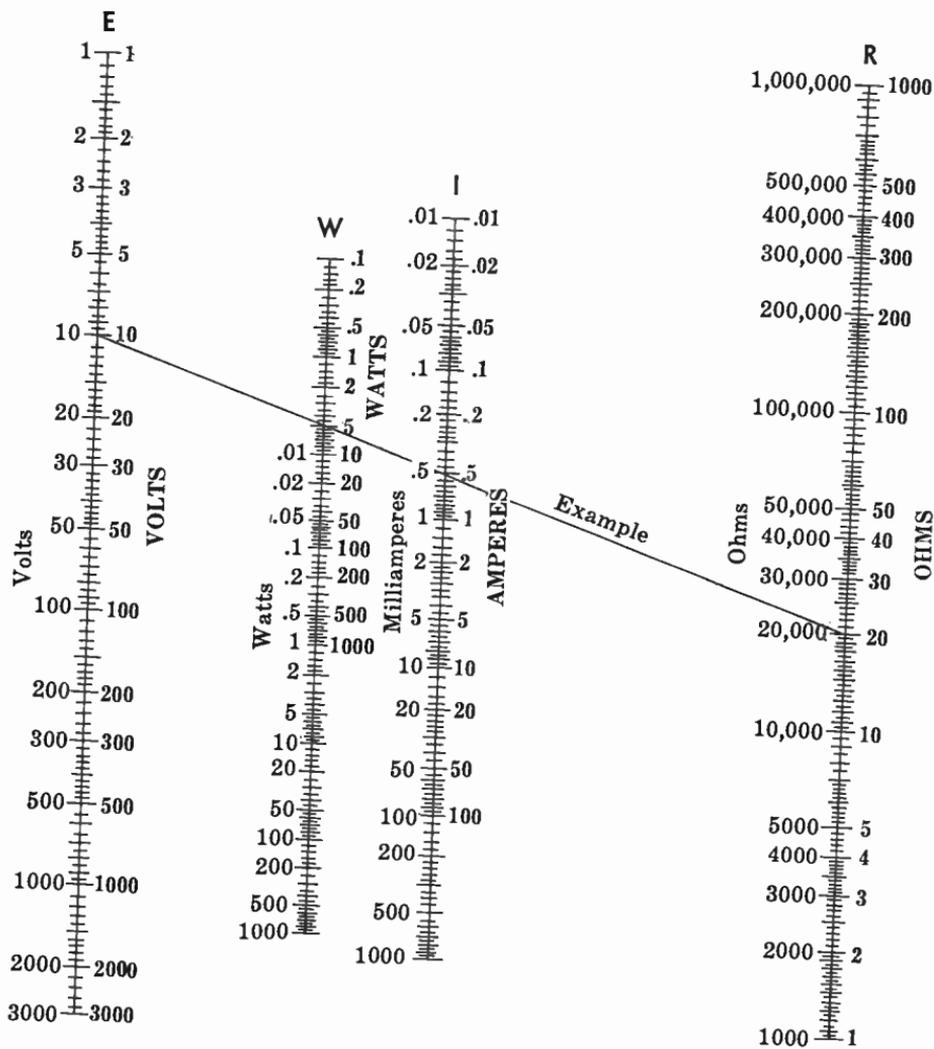


Fig. 2

3. OHM'S LAW NOMOGRAPH

The nomograph on the preceding page is a convenient way of solving most Ohm's law and DC power problems. If two values are known, the two unknown values can be determined by placing a straightedge across the two known values and reading the unknown values at the points where the straightedge crosses the appropriate scales. The figures in bold face (on the right side of all scales) cover one range of given values, and the figures in light face (on the left side) cover another range. For a given problem, all values must be read in either the bold- or light-face figures.

Example—What is the value of a resistor if a 10-volt drop is measured across it and a current of 500 milliamperes (.5 ampere) is flowing through it? What is the power dissipated by the resistor?

ANSWER: The value of the resistor is 20 ohms. The power dissipated in the resistor is 5 watts.

4. KIRCHHOFF'S LAWS

Kirchhoff's voltage law states: "The sum of the voltage drops around a DC series circuit equals the source or applied voltage. In other words, disregarding losses due to the wire resistance:

$$E_T = E_1 + E_2 + E_3$$

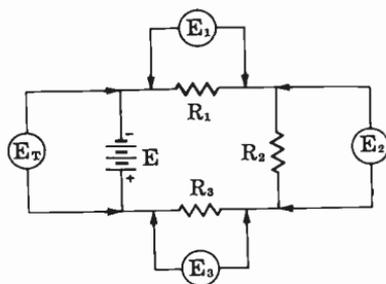


Fig. 3

where,

E_T is the source voltage,

E_1 , E_2 , and E_3 are the voltage drops across the individual resistors.

Kirchhoff's current law states: "The current flowing toward a point in a circuit must equal the current flowing

away from that point." Hence, if a circuit is broken up into several parallel paths, the sum of the currents through the individual paths must equal the current flowing to the point where the circuit branches, or:

$$I_T = I_1 + I_2 + I_3$$

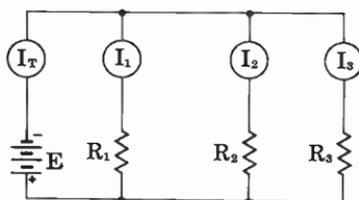


Fig. 4

where,

I_T is the total current flowing through the circuit,
 I_1 , I_2 , and I_3 are the currents flowing through the individual branches.

In a series-parallel circuit, the relationships are as follows:

$$\begin{aligned} E_T &= E_1 + E_2 + E_3 \\ I_T &= I_1 + I_2 \\ I_T &= I_3 \end{aligned}$$

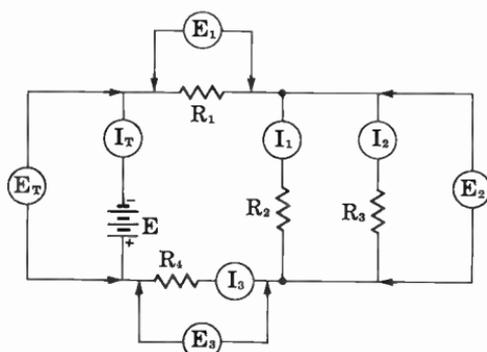


Fig. 5

5. RESISTANCE

The following formulas can be used for calculating the total resistance in a circuit.

Resistors in series (Fig. 6):

$$R_T = R_1 + R_2 + R_3 + \dots$$

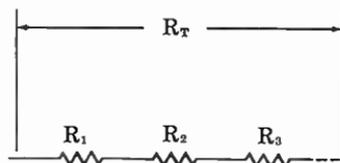


Fig. 6

Resistors in parallel (Fig. 7) :

$$R_T = \frac{1}{\frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} + \dots}$$

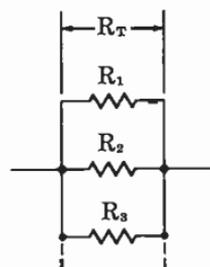


Fig. 7

Two resistors in parallel (Fig. 8) :

$$R_T = \frac{R_1 \times R_2}{R_1 + R_2}$$

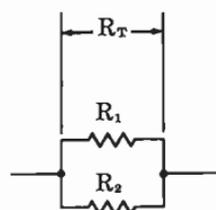


Fig. 8

where,

R_T is the total resistance of the circuit,
 R_1 , R_2 , and R_3 are the values of the individual resistors.

The equivalent value of resistors in parallel can be solved with the nomograph given in Fig. 9. Place a straightedge across the points on scale R_1 and R_2 where the known value resistors fall. The point at which the straightedge crosses the R_T scale will show the total resistance of the two resistors in parallel. If three resistors are in parallel, first find the equivalent resistance of two of the resistors, then consider this value as being in parallel with the remaining resistor.

If the total resistance needed is known, the straightedge can be placed at this value on the R_T scale and rotated to find the various combinations of values on the R_1 and R_2 scales which will produce the needed value.

Scales R_{1Y} and R_{TY} are used with the R_1 scale when the values of the known resistors differ greatly. The range of the nomograph can be increased by multiplying the values of all scales by 10, 100, 1,000, or more, as required.

Parallel Resistance Nomograph

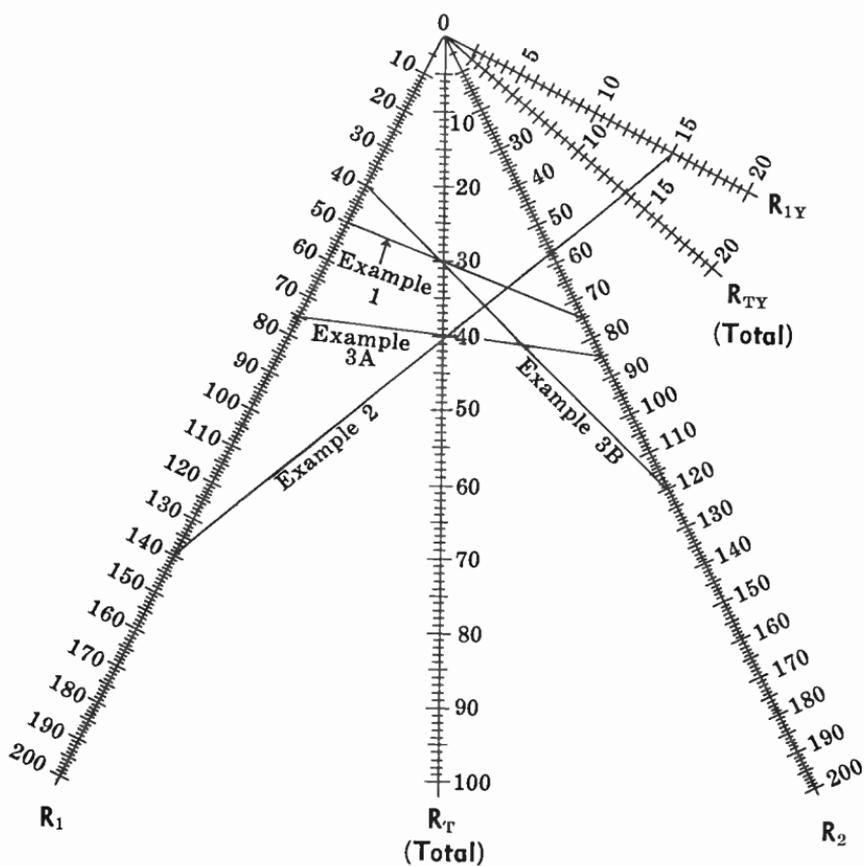


Fig. 9

Example 1—What is the total resistance of a 50-ohm and a 75-ohm resistor in parallel.

ANSWER: 30 ohms.

Example 2—What is the total resistance of a 1,500-ohm and a 14,000-ohm resistor in parallel?

ANSWER: 1,355 ohms. (Use R_1 and R_{1r} scales; read answer on R_{Tr} scale.)

Example 3—What is the total resistance of a 75-ohm, an 85-ohm, and a 120-ohm resistor in parallel?

ANSWER: 30 ohms. (First, consider the 75-ohm and 85-ohm resistors, which will give 40 ohms; then consider this 40 ohms and the 120-ohm resistor, which will give 30 ohms.)

6. CAPACITANCE

(A) Total Capacitance

The following formulas can be used for calculating the total capacitance in a circuit.

Capacitors in parallel (Fig. 10):

$$C_T = C_1 + C_2 + C_3 + \dots$$

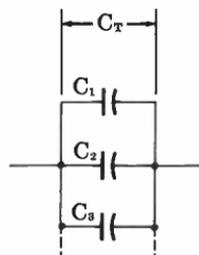


Fig. 10

Capacitors in series (Fig. 11):

$$C_T = \frac{1}{\frac{1}{C_1} + \frac{1}{C_2} + \frac{1}{C_3} + \dots}$$

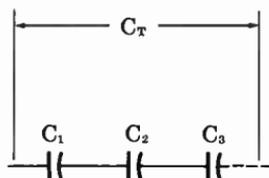


Fig. 11

Two capacitors in series (Fig. 12) :

$$C_T = \frac{C_1 \times C_2}{C_1 + C_2}$$

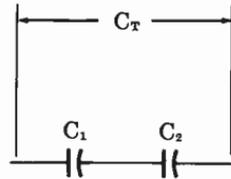


Fig. 12

where,

C_T is the total capacitance in a circuit,
 C_1 , C_2 , and C_3 are the values of the individual capacitors.

The parallel-resistance nomograph in § 5 can also be used to determine the total capacitance of capacitors in series.

The capacitance of a parallel-plate capacitor is determined by :

$$C = 0.2235 \frac{KA}{d} (N - 1)$$

where,

C is the capacitance in micromicrofarads,
 K is the dielectric constant,*
 A is the area of one plate in square inches,
 d is the thickness of the dielectric in inches,
 N is the number of plates.

(B) Charge Stored

The charge stored in a capacitor is determined by :

$$Q = CE$$

where,

Q is the charge, in coulombs,
 C is the capacitance in farads,
 E is the voltage impressed across the capacitor.

(C) Energy Stored

The energy stored in a capacitor can be determined by :

$$W = \frac{CE^2}{2}$$

where,

W is the energy in joules (watt-seconds),
 C is the capacitance in farads,
 E is the applied voltage in volts.

* For a list of dielectric constants of materials, see § 27.

(D) Voltage Across Series Capacitors

When an AC voltage is applied across a group of capacitors connected in series (Fig. 13), the voltage drop across the combination is, of course, equal to the applied voltage. The drop across each individual capacitor is inversely proportional to its capacitance. The drop across any capacitor in a group of series capacitors is calculated by the formula:

$$E_C = \frac{E_A \times C_T}{C}$$

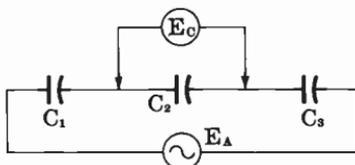


Fig. 13

where,

E_C is the voltage across the individual capacitor in the series (C_1 , C_2 , or C_3),

E_A is the applied voltage,

C_T is the total capacitance of the series combination,

C is the capacitance of the individual capacitor under consideration.

Note: C_T and C may be in any unit of measurement as long as the unit selected is the same for both.

7. INDUCTANCE

The following formulas can be used for calculating the total inductance in a circuit.

Inductors in series (with no mutual inductance) (Fig. 14):

$$L_T = L_1 + L_2 + L_3 + \dots$$

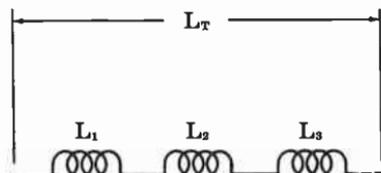


Fig. 14

Inductors in parallel (with no mutual inductance) (Fig. 15) :

$$L_T = \frac{1}{\frac{1}{L_1} + \frac{1}{L_2} + \frac{1}{L_3} + \dots}$$

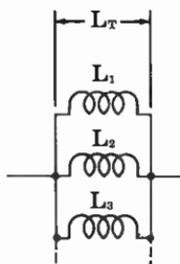


Fig. 15

Two inductors in parallel (with no mutual inductance) (Fig. 16) :

$$L_T = \frac{L_1 \times L_2}{L_1 + L_2}$$

where,

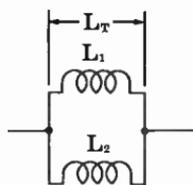


Fig. 16

L_T is the total inductance of the circuit,

L_1 , L_2 , and L_3 are the inductances of the individual inductors (coils).

The parallel-resistance nomograph in § 5 can also be used to determine the total inductance of inductors in parallel.

(A) Mutual Inductance

The mutual inductance of two coils with fields interacting can be determined by :

$$M = \frac{L_A - L_B}{4}$$

where,

M is the mutual inductance expressed in the same unit as L_A and L_B ,

L_A is the total inductance of coils L_1 and L_2 with fields aiding,

L_B is the total inductance of coils L_1 and L_2 with fields opposing.

(B) Coupled Inductance

The coupled inductance can be determined by the following formulas.

In parallel, with fields aiding :

$$L_T = \frac{1}{\frac{1}{L_1 + M} + \frac{1}{L_2 + M}}$$

In parallel, with fields opposing :

$$L_T = \frac{1}{\frac{1}{L_1 - M} + \frac{1}{L_2 - M}}$$

In series, with fields aiding :

$$L_T = L_1 + L_2 + 2M$$

In series, with fields opposing :

$$L_T = L_1 + L_2 - 2M$$

where,

L_T is the total inductance,

L_1 and L_2 are the inductances of the individual coils,

M is the mutual inductance.

(C) Coupling Coefficient

When two coils are inductively coupled to give transformer action, the coupling coefficient is determined by :

$$K = \frac{M}{\sqrt{L_1 L_2}}$$

where,

K is the coupling coefficient,

M is the mutual inductance,

L_1 and L_2 are the inductances of the two coils.

(D) Energy Stored

The energy stored in an inductor can be determined by :

$$W = \frac{LI^2}{2}$$

where,

W is the energy in joules (watt-seconds),

L is the inductance in henries,

I is the current in amperes.

8. Q FACTOR

The ratio of reactance to resistance is known as the Q factor. It can be determined by the following formulas.

For a coil wherein R and L are in series :

$$Q = \frac{\omega L}{R}$$

For a capacitor wherein R and C are in series :

$$Q = \frac{1}{\omega RC}$$

For a capacitor wherein R and C are in parallel :

$$Q = \omega RC$$

where,

Q is a ratio expressing the factor of merit,

ω equals $2\pi f$,

L is the inductance in henries,

R is the resistance in ohms,

C is the capacitance in farads.

9. RESONANCE

The resonant frequency, or the frequency at which the reactances of the circuit add up to zero ($X_L = X_C$), is determined by the formula :

$$f_R = \frac{1}{2\pi\sqrt{LC}}$$

where,

f_R is the resonant frequency in cycles per second,

L is the inductance in henries,

C is the capacitance in farads.

The resonant frequency of various combinations of inductance and capacitance can also be obtained from the reactance charts in § 14. Simply lay a straightedge across the values of inductance and capacitance, and read the resonant frequency from the frequency scale of the chart.

10. ADMITTANCE

The measure of the ease with which alternating current flows in a circuit is the admittance of the circuit.

Admittance of a series circuit is given by :

$$Y = \frac{1}{\sqrt{R^2 + X^2}}$$

Admittance is also expressed as the reciprocal of impedance; thus :

$$Y = \frac{1}{Z}$$

where,

Y is the admittance in mhos,

R is the resistance in ohms,

X is the reactance in ohms,

Z is the impedance in ohms.

11. SUSCEPTANCE

The susceptance of a series circuit is given by :

$$B = \frac{X}{R^2 + X^2}$$

When the resistance is zero, susceptance becomes the reciprocal of reactance; thus :

$$B = \frac{1}{X}$$

where,

B is the susceptance in mhos,

X is the reactance in ohms,

R is the resistance in ohms.

12. CONDUCTANCE

Conductance is the measure of the ability of a component to conduct electricity. Conductance for DC circuits is expressed as the reciprocal of resistance; therefore :

$$G = \frac{1}{R}$$

where,

G is the conductance in mhos,

R is the resistance in ohms.

Ohm's law formulas when conductance is considered are :

$$I = EG$$

$$G = \frac{I}{E}$$

$$E = \frac{I}{G}$$

where,

I is the current in amperes,

E is the voltage in volts,

G is the conductance in mhos,

R is the resistance in ohms.

13. ENERGY UNITS

Energy is the capacity or ability to do work. The joule is a unit of energy. One joule is the amount of energy required to maintain a current of one ampere for one second through a resistance of one ohm. It is equivalent to a watt-second. The watt-hour is the practical unit of energy; 3600 watt-seconds equals one watt-hour. The number of watt-hours is calculated :

$$\text{Watt-hours} = P \times T$$

where,

P is the power in watts,

T is the time in hours the power is dissipated.

See § 6 for the energy stored in a capacitor, and § 7 for the energy stored in an inductor.

14. REACTANCE

The opposition to the flow of alternating current by the inductance or capacitance of a component or circuit is called the reactance.

(A) Capacitive Reactance

The reactance of a capacitor may be calculated by the formula :

$$X_c = \frac{1}{2\pi fC}$$

where,

X_c is the reactance in ohms,

f is the frequency in cycles per second,

C is the capacitance in farads.

(B) Inductive Reactance

The reactance of an inductor may be calculated by the formula:

$$X_L = 2\pi fL$$

where,

X_L is the reactance in ohms,
 f is the frequency in cycles per second,
 L is the inductance in henries.

(C) Reactance Charts

Charts for determining unknown values of reactance, inductance, capacitance, and frequency are given on the following pages. The chart in Fig. 17A covers 1 to 1,000 cycles, Fig. 17B covers 1 to 1,000 kilocycles, and Fig. 17C covers 1 to 1,000 megacycles.

To find the amount of reactance of a capacitor at a given frequency, lay the straightedge across the capacitor value and the frequency. Then read the reactance from the reactance scale. By extending the line, the value of an inductance which will give the same reactance can be obtained.

Since $X_C = X_L$ at resonance, by laying the straightedge across the capacitance and inductance values, the resonant frequency of the combination can be determined.

Example—If the frequency is 10 cycles per second and the capacitance is 50 mfd, what is the reactance of the capacitor? What value of inductance will give this same reactance?

ANSWER: The reactance is 310 ohms. The inductance needed to produce this same reactance is 5 henries. Thus, it follows that a 50-mfd capacitor and a 5-henry choke are resonant at 10 cps. [Place the straightedge, on the proper chart (Fig. 17A), across 10 cps and 50 mfd. Read the values indicated on the reactance and inductance scales.]

15. IMPEDANCE

The basic formulas for calculating the total impedance are as follows.

For parallel circuits:

$$Z = \frac{1}{\sqrt{G^2 + B^2}}$$

Reactance Chart—1 cps to 1 kc

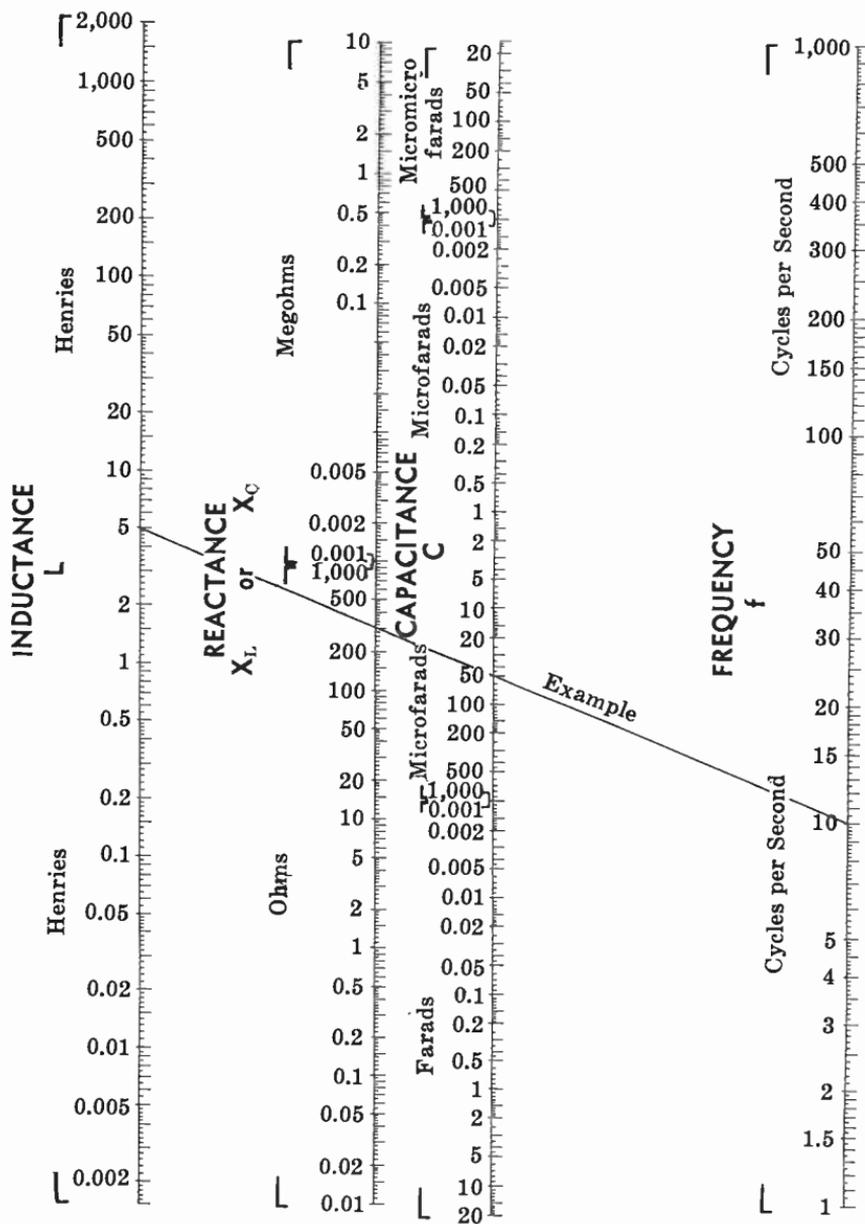


Fig. 17A

Reactance Chart — 1 kc to 1 mc

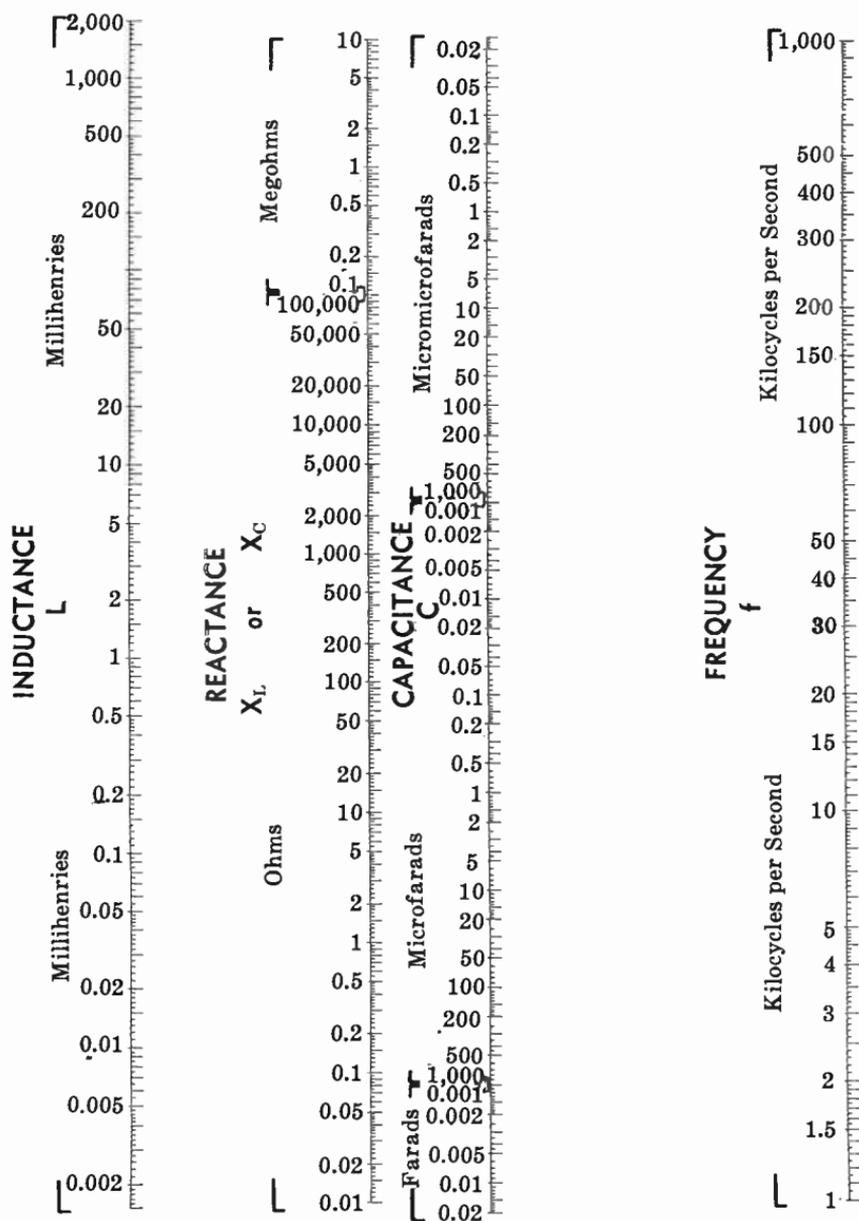


Fig. 17B

Reactance Chart — 1 mc to 1,000 mc

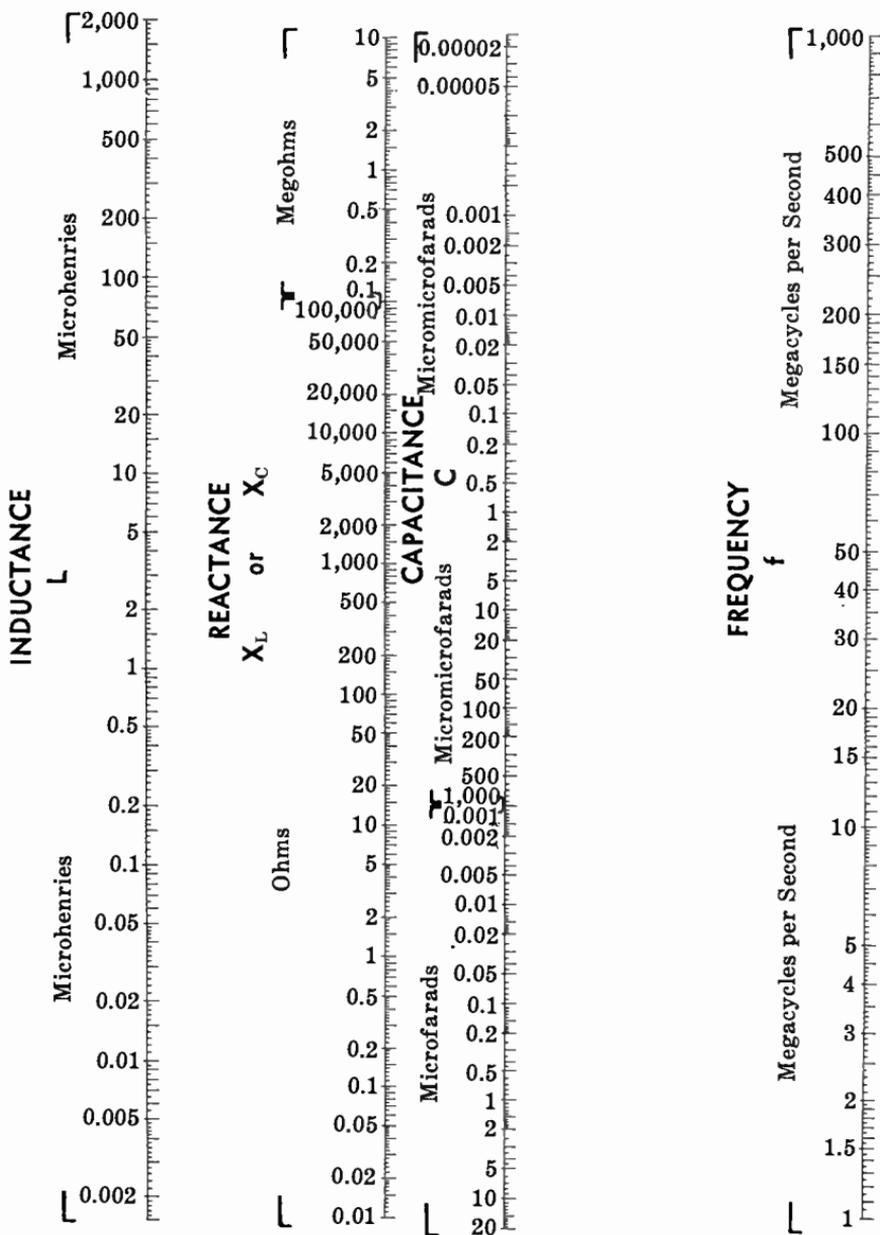


Fig. 17C

For series circuits:

$$Z = \sqrt{R^2 + X^2}$$

where,

Z is the total impedance,

G is the total conductance or the reciprocal of the total parallel resistance,

B is the total susceptance,

R is the total resistance,

X is the total reactance.

The following formulas can be used to find the impedance of the various combinations of inductance, capacitance, and resistance.

For a single resistance (Fig. 18):

$$Z = R$$

$$\theta = 0^\circ$$



Fig. 18

For resistances in series (Fig. 19):

$$Z = R_1 + R_2 + R_3 + \dots$$

$$\theta = 0^\circ$$



Fig. 19

For a single inductance (Fig. 20):

$$Z = X_L$$

$$\theta = 90^\circ$$



Fig. 20

For inductances in series (with no mutual inductance) (Fig. 21):

$$Z = X_{L_1} + X_{L_2} + X_{L_3} + \dots$$

$$\theta = 90^\circ$$



Fig. 21

For a single capacitance (Fig. 22):

$$Z = X_C$$

$$\theta = 90^\circ$$



Fig. 22

For capacitances in series (Fig. 23) :

$$Z = X_{C_1} + X_{C_2} + X_{C_3} + \dots$$

$$\theta = 90^\circ$$

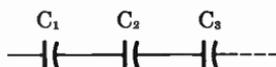


Fig. 23

For resistance and inductance in series (Fig. 24) :

$$Z = \sqrt{R^2 + X_L^2}$$

$$\theta = \arctan \frac{X_L}{R}$$



Fig. 24

For resistance and capacitance in series (Fig. 25) :

$$Z = \sqrt{R^2 + X_C^2}$$

$$\theta = \arctan \frac{X_C}{R}$$

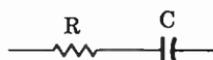


Fig. 25

For inductance and capacitance in series (Fig. 26) :

When X_L is larger than X_C

$$Z = X_L - X_C$$

When X_C is larger than X_L

$$Z = X_C - X_L$$

$$\theta = 0^\circ \text{ when } X_L = X_C$$

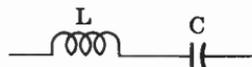


Fig. 26

For resistance, inductance, and capacitance in series (Fig. 27) :

$$Z = \sqrt{R^2 + (X_L - X_C)^2}$$

$$\theta = \arctan \frac{X_L - X_C}{R}$$

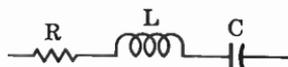


Fig. 27

For resistances in parallel (Fig. 28) :

$$Z = \frac{1}{\frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} + \dots}$$

$$\theta = 0^\circ$$

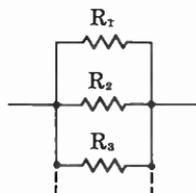


Fig. 28

For inductances in parallel (with no mutual inductance) (Fig. 29) :

$$Z = \frac{1}{\frac{1}{X_{L_1}} + \frac{1}{X_{L_2}} + \frac{1}{X_{L_3}} + \dots}$$

$$\theta = 90^\circ$$

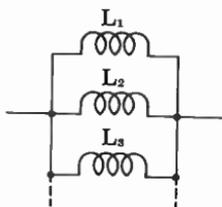


Fig. 29

For capacitances in parallel (Fig. 30) :

$$Z = \frac{1}{\frac{1}{X_{C_1}} + \frac{1}{X_{C_2}} + \frac{1}{X_{C_3}} + \dots}$$

$$\theta = 90^\circ$$

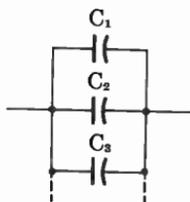


Fig. 30

For resistance and inductance in parallel (Fig. 31) :

$$Z = \frac{RX_L}{\sqrt{R^2 + X_L^2}}$$

$$\theta = \arctan \frac{R}{X_L}$$

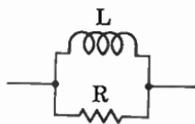


Fig. 31

For capacitance and resistance in parallel (Fig. 32) :

$$Z = \frac{RX_C}{\sqrt{R^2 + X_C^2}}$$

$$\theta = \arctan \frac{R}{X_C}$$

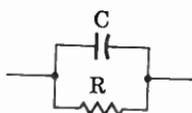


Fig. 32

For capacitance and inductance in parallel (Fig. 33) :

When X_L is larger than X_C :

$$Z = \frac{X_L X_C}{X_L - X_C}$$

When X_C is larger than X_L :

$$Z = \frac{X_C X_L}{X_C - X_L}$$

$$\theta = 0^\circ \text{ when } X_L = X_C$$

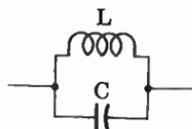


Fig. 33

For inductance, capacitance, and resistance in parallel (Fig. 34):

$$Z = \frac{RX_L X_C}{\sqrt{X_L^2 X_C^2 + R^2 (X_L - X_C)^2}}$$

$$\theta = \arctan \frac{R(X_L - X_C)}{X_L X_C}$$

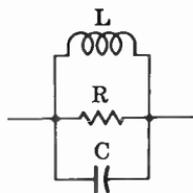


Fig. 34

For inductance and series resistance in parallel with resistance (Fig. 35):

$$Z = R_2 \sqrt{\frac{R_1^2 + X_L^2}{(R_1 + R_2)^2 + X_L^2}}$$

$$\theta = \arctan \frac{X_L R_2}{R_1^2 + X_L^2 + R_1 R_2}$$

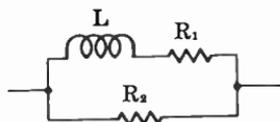


Fig. 35

For inductance and series resistance in parallel with capacitance (Fig. 36):

$$Z = X_C \sqrt{\frac{R^2 + X_L^2}{R^2 + (X_L - X_C)^2}}$$

$$\theta = \arctan \frac{X_L (X_C - X_L) - R^2}{R X_C}$$

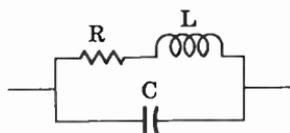


Fig. 36

For capacitance and series resistance in parallel with inductance and series resistance (Fig. 37):

$$Z = \sqrt{\frac{(R_1^2 + X_L^2)(R_2^2 + X_C^2)}{(R_1 + R_2)^2 + (X_L - X_C)^2}}$$

$$\theta = \arctan \frac{X_L (R_2^2 + X_C^2) - X_C (R_1^2 + X_L^2)}{R_1 (R_2^2 + X_C^2) + R_2 (R_1^2 + X_L^2)}$$

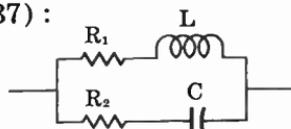


Fig. 37

where,

Z is the impedance in ohms,

R is the resistance in ohms,

L is the inductance in henries,

X_L is the inductive reactance in ohms,

X_C is the capacitive reactance in ohms,

θ is the phase angle in degrees by which the current leads the voltage in a capacitive circuit or lags the voltage in an inductive circuit. 0° indicates an in-phase condition.

16. OHM'S LAW FOR ALTERNATING CURRENT

The fundamental Ohm's law formulas for alternating current are given by:

$$E = IZ$$

$$I = \frac{E}{Z}$$

$$Z = \frac{E}{I}$$

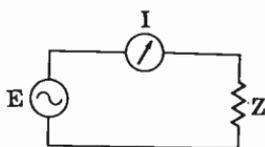


Fig. 38

where,

E is the voltage in volts,

I is the current in amperes,

Z is the impedance in ohms.

The power expended in an AC circuit is calculated by the formula:

$$P = EI \cos \theta$$

where,

P is the power in watts,

E is the voltage in volts,

I is the current in amperes,

θ is the phase angle in degrees.

The phase angle is the difference in degrees by which the current leads or lags the voltage in a reactive circuit. In a series circuit, the phase angle is determined by the formula:

$$\theta = \arctan \frac{X}{R}$$

where,

X is the inductive or capacitive reactance in ohms,
 R is the nonreactive resistance in ohms.

Therefore :

For a purely resistive circuit :

$$\begin{aligned}\theta &= 0^\circ \\ \cos \theta &= 1 \\ P &= EI\end{aligned}$$

For a resonant circuit :

$$\begin{aligned}\theta &= 0^\circ \\ \cos \theta &= 1 \\ P &= EI\end{aligned}$$

For a purely reactive circuit :

$$\begin{aligned}\theta &= 90^\circ \\ \cos \theta &= 0 \\ P &= 0\end{aligned}$$

17. AVERAGE, RMS, PEAK, AND PEAK-TO-PEAK VOLTAGE AND CURRENT

The following table can be used to convert sinusoidal voltage (or current) values from one method of measurement to another. To use the table, first find the given type of reading in the left-hand column, then find the desired type of reading across the top of the table. To convert the given value to the desired value, multiply the given value by the factor listed under the desired value.

Example—What factor must peak voltage be multiplied by to obtain rms voltage?

ANSWER: .707.

Table I. Average, Rms, Peak, and Peak-to-Peak Values

| Given Value | Multiplying Factor To Get | | | |
|--------------|---------------------------|--------|-------|--------------|
| | Average | Rms | Peak | Peak-to-Peak |
| Average | — | 1.11 | 1.57 | 3.14 |
| Rms | 0.9 | — | 1.414 | 2.828 |
| Peak | 0.637 | 0.707 | — | 2.0 |
| Peak-to-Peak | 0.32 | 0.3535 | 0.5 | — |

18. POWER FACTOR

Power factor is the ratio of true power to apparent power in an alternating circuit. Thus:

$$\begin{aligned} \text{pf} &= \frac{P_T}{P_A} = \frac{EI \cos \theta}{EI} \\ &= \cos \theta \end{aligned}$$

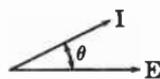


Fig. 39

where,

pf is the power factor,

P_T is the true power in watts,

P_A is the apparent power in volt-amperes,

$EI \cos \theta$ is the true power in watts,

EI is the apparent power in volt-amperes.

Therefore:

For a purely resistive circuit:

$$\theta = 0^\circ$$

$$\text{pf} = 1$$

For a resonant circuit:

$$\theta = 0^\circ$$

$$\text{pf} = 1$$

For a purely reactive circuit:

$$\theta = 90^\circ$$

$$\text{pf} = 0$$

19. TIME CONSTANTS

A certain amount of time is required, after a DC voltage has been applied to an R-C or R-L circuit, before the capacitor can charge or the current can build up to a portion of the full value. This time is called the time constant of the circuit. However, the time constant is not the time required for the voltage or current to reach the full value; instead, it is the time required to reach 63.2% of full value. During the next time constant, the capacitor is charged or the current builds

up to 63.2% of the remaining difference, or to 86.5% of the full value. Table II gives the per cent of full charge on a capacitor, or current buildup in an inductance after each time constant. Theoretically, the charge on the capacitor, or the current through the coil, can never reach 100%. However, it is usually considered to be 100% after five time constants.

Table II. Time Constants versus Per Cent of Voltage or Current

| No. of Time Constants | % Charge or Buildup | % Discharge or Decay |
|-----------------------|---------------------|----------------------|
| 1 | 63.2 | 36.8 |
| 2 | 86.5 | 13.5 |
| 3 | 95.0 | 5.0 |
| 4 | 98.2 | 1.8 |
| 5 | 99.3 | 0.7 |

Likewise, when the voltage source is removed, the capacitor will discharge or the current will decay 63.2%, or to 36.8% of full value during the first time constant. Table II also gives the per cent of full voltage after each time constant for discharge of a capacitor or decay of the current through a coil.

The time per time constant is calculated as follows.

For an R-C circuit (Fig. 40) :

$$T = RC$$

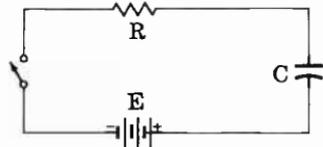


Fig. 40

For an R-L circuit (Fig. 41) :

$$T = \frac{L}{R}$$

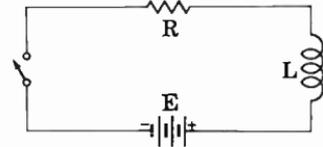


Fig. 41

where,

- T is the time in seconds,
- R is the resistance in ohms,
- C is the capacitance in farads,
- L is the inductance in henries.

In addition, the values can also be expressed by the following relationships :

| T | R | C or L |
|--------------|---------|------------------|
| seconds | megohms | microfarads |
| seconds | megohms | microhenries |
| microseconds | ohms | microfarads |
| microseconds | megohms | micromicrofarads |
| microseconds | ohms | microhenries |

20. TRANSFORMER FORMULAS

In a transformer, the relationships between the number of turns in the primary and secondary, the voltage across each winding, and the current through the windings are expressed by the equations :

$$\frac{E_p}{E_s} = \frac{N_p}{N_s} \quad \text{and} \quad \frac{E_p}{E_s} = \frac{I_s}{I_p}$$

By rearranging these equations, any unknown can be determined from the following formulas :

$$E_p = \frac{E_s N_p}{N_s} = \frac{E_s I_s}{I_p}$$

$$E_s = \frac{E_p N_s}{N_p} = \frac{E_p I_p}{I_s}$$

$$N_p = \frac{E_p N_s}{E_s} = \frac{N_s I_s}{I_p}$$

$$N_s = \frac{E_s N_p}{E_p} = \frac{N_p I_p}{I_s}$$

$$I_p = \frac{E_s I_s}{E_p} = \frac{N_s I_s}{N_p}$$

$$I_s = \frac{E_p I_p}{E_s} = \frac{N_p I_p}{N_s}$$

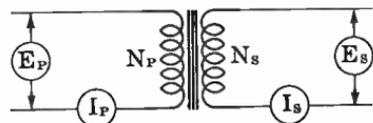


Fig. 42

The turns ratio of a transformer is determined by the following formulas :

For a step-up transformer :

$$T = \frac{N_s}{N_p}$$

For a step-down transformer:

$$T = \frac{N_p}{N_s}$$

The impedance ratio of a transformer is determined by:

$$Z = T^2$$

The impedance of an unknown winding is determined by the following:

For a step-up transformer:

$$Z_p = \frac{Z_s}{Z}$$

$$Z_s = Z \times Z_p$$

For a step-down transformer:

$$Z_p = Z \times Z_s$$

$$Z_s = \frac{Z_p}{Z}$$

where,

E_p is the voltage across the primary winding,
 E_s is the voltage across the secondary winding,
 N_p is the number of turns in the primary winding,
 N_s is the number of turns in the secondary winding,
 I_p is the current through the primary winding,
 I_s is the current through the secondary winding,
 T is the turns ratio,
 Z is the impedance ratio,
 Z_p is the impedance of the primary winding,
 Z_s is the impedance of the secondary winding.

21. VOLTAGE REGULATION

When a load is connected to a power supply, the output voltage drops because more current flows through the resistive elements of the power supply. Voltage regulation is a measure of how much the voltage drops and is usually expressed as a percentage. It is determined by the following formula:

$$\%R = \frac{E_1 - E_2}{E_2} \times 100$$

where,

$\%R$ is the voltage regulation in per cent,
 E_1 is the no-load voltage,
 E_2 is the voltage under load.

22. DC METER FORMULAS

The basic instrument for testing current and voltage is the moving-coil meter. The meter can be either a DC milliammeter or a DC microammeter. A series resistor converts the meter to a DC voltmeter, and a parallel resistor converts the meter to a DC ammeter. The resistance of the meter movement is determined first, as follows. Connect a suitable variable resistor R_a and a battery as shown in Fig. 43. Adjust resistor R_a until full-scale deflection is obtained. Then connect a variable resistor R_b in parallel with the meter, and adjust R_b until half-scale deflection is obtained. Disconnect

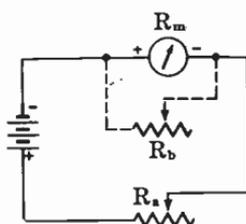


Fig. 43

R_b and measure its resistance. The measured value is the resistance of the meter movement.

(A) Voltage Multipliers

$$R = \frac{E_s}{I_s} - R_m$$

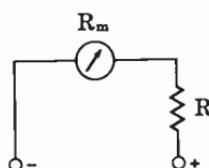


Fig. 44

where,

R is the multiplier resistance in ohms,

E_s is the full-scale reading in volts,

I_s is the full-scale reading in amperes,

R_m is the meter resistance in ohms.

(B) Shunt-type Ohmmeter for Low Resistance

$$R_x = R_m \frac{I_2}{I_1 - I_2}$$

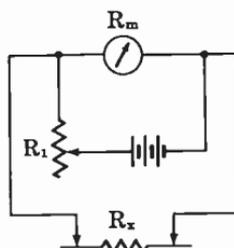


Fig. 45

where,

R_x is the unknown resistance,

R_m is the meter resistance in ohms,

I_1 is the current reading with probes open,

I_2 is the current reading with probes connected across unknown resistor,

R_1 is a variable resistance for current limiting to keep meter adjusted for full-scale reading with probes open.

(C) Series-type Ohmmeter for High Resistance

$$R_x = (R_1 + R_m) \frac{I_1 - I_2}{I_2}$$

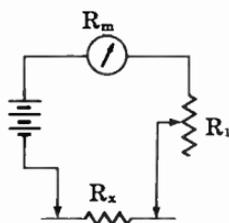


Fig. 46

where,

R_x is the unknown resistance,

R_1 is a variable resistance adjusted for full-scale reading with probes shorted together,

R_m is the meter resistance in ohms,

I_1 is the current reading with probes shorted,

I_2 is the current reading with unknown resistor connected.

(D) Ammeter Shunts

$$R = \frac{R_m}{N - 1} = \frac{I_m R_m}{I_s}$$

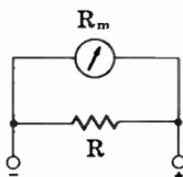


Fig. 47

where,

R is the resistance of the shunt,

R_m is the meter resistance in ohms,

N is the scale multiplication factor,

I_m is the meter current,

I_s is the shunt current.

(E) Ammeter With Multirange Shunt

$$R_2 = \frac{(R_1 + R_2) + R_m}{N}$$

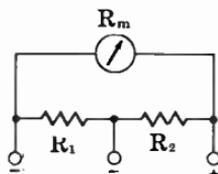


Fig. 48

where,

R_2 is the intermediate value in ohms,

$R_1 + R_2$ is the total shunt resistance for lowest full-scale reading,

R_m is the meter resistance in ohms,

N is the scale multiplication factor.

23. FREQUENCY AND WAVELENGTH

(A) Formulas

Since the frequency is the number of complete cycles per second and since radio waves travel at a fixed speed, it follows that a complete cycle occupies a given distance in space. The distance between two corresponding parts of two waves (the two positive or negative crests or the points where the two waves cross the zero axis in a given direction) constitutes the wavelength. If either the frequency or the wavelength is known, the other can be computed as follows:

$$f = \frac{300,000}{\lambda}$$

$$\lambda = \frac{300,000}{f}$$

where,

f is the frequency in kilocycles,

λ is the wavelength in meters.

If it is desired to calculate the wavelength in feet, the following formulas should be used:

$$f = \frac{984,000}{\lambda}$$

$$\lambda = \frac{984,000}{f}$$

where,

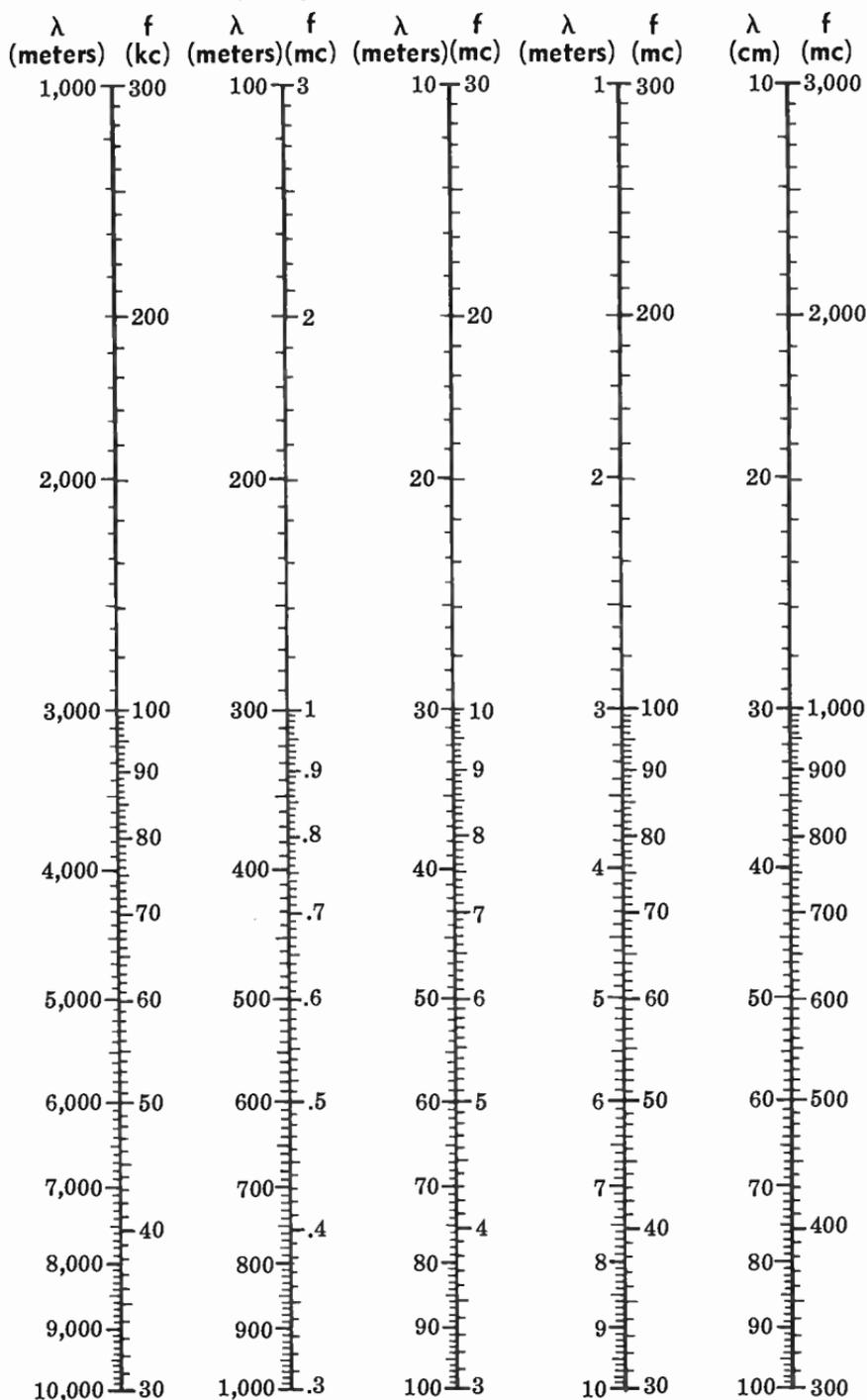
f is the frequency in kilocycles,

λ is the wavelength in feet.

(B) Conversion Chart

The wavelength of any frequency from 30 kc to 3000 mc can be read directly from the chart in Fig. 49. Likewise, if the wavelength is known, the corresponding frequency can be obtained from the chart for wavelengths from 10 centimeters to 1000 meters. To use the chart, merely find the

Frequency-Wavelength Conversion Chart



known value (either frequency or wavelength) on one of the scales, and then read the corresponding value from the opposite side of the scale.

Example—What is the wavelength of a 4-mc signal?

ANSWER: 75 meters. (Find 4 mc on the third scale from the left. Opposite 4 mc on the frequency scale we find 75 meters on the wavelength scale.)

24. TRANSMISSION-LINE FORMULAS

The characteristic impedance of a transmission line is defined as the input impedance of a line of the same configuration and dimensions but of infinite length. When a line of finite length is terminated with an impedance equal to its own characteristic impedance, the line is said to be matched.

(A) Coaxial Line

The characteristic impedance of a coaxial line is given by:

$$Z_0 = \frac{138}{\sqrt{k}} \log \frac{D}{d}$$

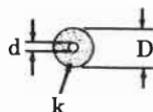


Fig. 50

where,

- Z_0 is the characteristic impedance,
- D is the inside diameter of the outer conductor,
- d is the outside diameter of the inner conductor expressed in the same units as D ,
- k is the dielectric constant of the insulating material* (k equals 1 for dry air).

The attenuation of coaxial line in decibels per foot can be determined by the formula:

$$a = \frac{4.6 \sqrt{f} (D + d)}{D \times d \left(\log \frac{D}{d} \right)} \times 10^{-6}$$

where,

- a is the attenuation in decibels per foot of line,
- f is the frequency in megacycles,
- D is the inside diameter of the outer conductor in inches,
- d is the outside diameter of the inner conductor in inches.

* For a list of dielectric constants of materials, see § 27.

(B) Parallel-Conductor Line

The characteristic impedance of parallel-conductor line (twin-lead) is determined by the formula:

$$Z_o = \frac{276}{\sqrt{k}} \log \frac{2D}{d}$$

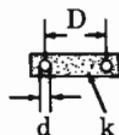


Fig. 51

where,

Z_o is the characteristic impedance,
 D is the center-to-center distance between conductors,
 d is the diameter of the conductors in the same units as D ,
 k is the dielectric constant of the insulating material between conductors* (k equals 1 for dry air).

25. MODULATION FORMULAS**(A) Amplitude Modulation**

The amount of modulation of an amplitude-modulated carrier is referred to as the percentage of modulation. It can be determined by the following formulas:

$$\%M = \frac{E_C - E_T}{2E_{AV}} \times 100$$

or,

$$\%M = \frac{E_C - E_T}{E_C + E_T} \times 100$$

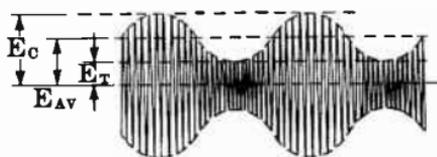


Fig. 52

where,

$\%M$ is the percentage of modulation,
 E_C is the amplitude of the crest of the modulated carrier,
 E_T is the amplitude of the trough of the modulated carrier,
 E_{AV} is the average amplitude of the modulated carrier.

Also, the percentage of modulation can be determined by applying the modulated carrier wave to the vertical plates and the modulating voltage wave to the horizontal plates of an oscilloscope. This produces a trapezoidal wave, as shown in Fig. 53. The dimensions A and B are proportional to the crest and trough amplitudes, respectively. The percentage

* For a list of dielectric constants of materials, see § 27.

of modulation can be determined by measuring the height of A and B, and using the formula:

$$\%M = \frac{A - B}{A + B} \times 100$$

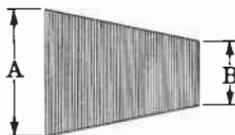


Fig. 53

where,

$\%M$ is the percentage of modulation,
A and B are the dimensions measured in Fig. 53.

The sideband power of an AM carrier is determined by:

$$P_{SB} = \frac{\%M^2}{2} \times P_C$$

The total radiated power is the sum of the carrier and the radiated powers:

$$P_T = P_{SB} + P_C$$

where,

P_{SB} is the sideband power (includes both sidebands),
 $\%M$ is the percentage of modulation,
 P_C is the carrier power,
 P_T is the total radiated power.

Note: The carrier power does not change with modulation.

(B) Frequency Modulation

In a frequency-modulated carrier, the amount the carrier frequency changes is determined by the amplitude of the modulating signal, and the number of times the changes occur per second is determined by the frequency of the modulating signal.

The percentage of modulation of an FM carrier can be computed from:

$$\%M = \frac{\Delta f}{\Delta f \text{ for } 100\%M} \times 100$$

where,

$\%M$ is the percentage of modulation,
 Δf is the change in frequency, or the deviation,
 Δf for 100% M is the change in frequency for a 100% modulated carrier. (For commercial FM, 75 kc; for television sound, 25 kc; and for two-way radio, 15 kc.)

The modulation index of an FM carrier is determined by:

$$M = \frac{f_d}{f_a}$$

where,

M is the modulation index,

f_d is the deviation in frequency,

f_a is the modulating audio frequency in the same units as f_d .

26. DECIBELS AND VOLUME UNITS

(A) Equations

The number of decibels corresponding to a given power ratio is 10 times the common logarithm of the ratio. Thus:

$$\text{db} = 10 \log \frac{P_2}{P_1}$$

The number of decibels corresponding to a given voltage or current ratio is 20 times the common logarithm of the ratio. Thus, when the impedances across which the signals are being measured are equal, the equations are:

$$\text{db} = 20 \log \frac{E_2}{E_1}$$

$$\text{db} = 20 \log \frac{I_2}{I_1}$$

If the impedances across which the signals are measured are not equal, the equations become:

$$\text{db} = 20 \log \frac{E_2 \sqrt{Z_1}}{E_1 \sqrt{Z_2}}$$

$$\text{db} = 20 \log \frac{I_2 \sqrt{Z_2}}{I_1 \sqrt{Z_1}}$$

(B) Reference Levels

The decibel is not an absolute value; it is a means of stating the ratio of a level to a certain reference level. Usually, when no reference level is given, it is 6 millivolts across a 500-ohm impedance. However, the reference level should be stated whenever a value in db's is given. Other units, which

do have specific reference levels, have been established. Some of the more common are:

- dbk —1 kilowatt
- dbm —1 milliwatt, 600 ohms
- dbv —1 volt
- dbw —1 watt
- dbvg —voltage gain
- dbrap—decibels above a reference acoustical power of 10^{-16} watts
- VU —1 milliwatt, 600 ohms (complex waveforms varying in both amplitude and frequency).

(C) Decibel Table

The decibel table on the following pages lists most of the current, voltage, and power ratios encountered, with their decibel values. If a db value is not listed and it is desired to find the corresponding ratio, first subtract one of the given values from the unlisted value (select a value so the remainder will also be listed). Then multiply the ratios given in the chart for each value. To convert a ratio which is not given in the table to a db value, first factor the ratio so that each factor will be a listed value; then find the db equivalents for each factor and add them.

Example 1—Find the db equivalent of a power ratio of .631.

ANSWER: 2-db loss.

Example 2—Find the current ratio corresponding to a gain of 43 db.

ANSWER: 141. [First find the current ratio for 40 db (100); then find the current ratio for 3 db (1.41). Multiplying, $100 \times 1.41 = 141$.]

Example 3—Find the db value corresponding to a voltage ratio of 150.

ANSWER: 43.5. [First factor 150 into 1.5×100 . The db value for a voltage ratio of 100 is 40; the db value for a voltage ratio of 1.5 is 3.5 (approximately). Therefore, the db value for a voltage ratio is $40 + 3.5$ or 43.5 db.]

Table III. Decibel Table (0 to 10.9 Db)

| Db | Current or Voltage Ratio | | Power Ratio | | Db | Current or Voltage Ratio | | Power Ratio | |
|-----|--------------------------|--------|-------------|--------|------|--------------------------|-------|-------------|--------|
| | Gain | Loss | Gain | Loss | | Gain | Loss | Gain | Loss |
| 0 | 1.000 | 1.0000 | 1.000 | 1.0000 | 5.5 | 1.884 | .5309 | 3.548 | .2818 |
| .1 | 1.012 | .9886 | 1.023 | .9772 | 5.6 | 1.905 | .5248 | 3.631 | .2754 |
| .2 | 1.023 | .9772 | 1.047 | .9550 | 5.7 | 1.928 | .5188 | 3.715 | .2692 |
| .3 | 1.035 | .9661 | 1.072 | .9333 | 5.8 | 1.950 | .5129 | 3.802 | .2630 |
| .4 | 1.047 | .9550 | 1.096 | .9120 | 5.9 | 1.972 | .5070 | 3.890 | .2570 |
| .5 | 1.059 | .9441 | 1.122 | .8913 | 6.0 | 1.995 | .5012 | 3.981 | .2512 |
| .6 | 1.072 | .9333 | 1.148 | .8710 | 6.1 | 2.018 | .4955 | 4.074 | .2455 |
| .7 | 1.084 | .9226 | 1.175 | .8511 | 6.2 | 2.042 | .4898 | 4.169 | .2399 |
| .8 | 1.096 | .9120 | 1.202 | .8318 | 6.3 | 2.065 | .4842 | 4.266 | .2344 |
| .9 | 1.109 | .9016 | 1.230 | .8128 | 6.4 | 2.089 | .4786 | 4.365 | .2291 |
| 1.0 | 1.122 | .8913 | 1.259 | .7943 | 6.5 | 2.113 | .4732 | 4.467 | .2239 |
| 1.1 | 1.135 | .8810 | 1.288 | .7762 | 6.6 | 2.138 | .4677 | 4.571 | .2188 |
| 1.2 | 1.148 | .8710 | 1.318 | .7586 | 6.7 | 2.163 | .4624 | 4.677 | .2138 |
| 1.3 | 1.161 | .8610 | 1.349 | .7413 | 6.8 | 2.188 | .4571 | 4.786 | .2089 |
| 1.4 | 1.175 | .8511 | 1.380 | .7244 | 6.9 | 2.213 | .4519 | 4.898 | .2042 |
| 1.5 | 1.189 | .8414 | 1.413 | .7079 | 7.0 | 2.239 | .4467 | 5.012 | .1995 |
| 1.6 | 1.202 | .8318 | 1.445 | .6918 | 7.1 | 2.265 | .4416 | 5.129 | .1950 |
| 1.7 | 1.216 | .8222 | 1.479 | .6761 | 7.2 | 2.291 | .4365 | 5.248 | .1905 |
| 1.8 | 1.230 | .8128 | 1.514 | .6607 | 7.3 | 2.317 | .4315 | 5.370 | .1862 |
| 1.9 | 1.245 | .8035 | 1.549 | .6457 | 7.4 | 2.344 | .4266 | 5.495 | .1820 |
| 2.0 | 1.259 | .7943 | 1.585 | .6310 | 7.5 | 2.371 | .4217 | 5.623 | .1778 |
| 2.1 | 1.274 | .7852 | 1.622 | .6166 | 7.6 | 2.399 | .4169 | 5.754 | .1738 |
| 2.2 | 1.288 | .7762 | 1.660 | .6026 | 7.7 | 2.427 | .4121 | 5.888 | .1698 |
| 2.3 | 1.303 | .7674 | 1.698 | .5888 | 7.8 | 2.455 | .4074 | 6.026 | .1660 |
| 2.4 | 1.318 | .7586 | 1.738 | .5754 | 7.9 | 2.483 | .4027 | 6.166 | .1622 |
| 2.5 | 1.334 | .7499 | 1.778 | .5623 | 8.0 | 2.512 | .3981 | 6.310 | .1585 |
| 2.6 | 1.349 | .7413 | 1.820 | .5495 | 8.1 | 2.541 | .3936 | 6.457 | .1549 |
| 2.7 | 1.365 | .7328 | 1.862 | .5370 | 8.2 | 2.570 | .3890 | 6.607 | .1514 |
| 2.8 | 1.380 | .7244 | 1.905 | .5248 | 8.3 | 2.600 | .3846 | 6.761 | .1479 |
| 2.9 | 1.396 | .7161 | 1.950 | .5129 | 8.4 | 2.630 | .3802 | 6.918 | .1445 |
| 3.0 | 1.413 | .7079 | 1.995 | .5012 | 8.5 | 2.661 | .3758 | 7.079 | .1413 |
| 3.1 | 1.429 | .6998 | 2.042 | .4898 | 8.6 | 2.692 | .3715 | 7.244 | .1380 |
| 3.2 | 1.445 | .6918 | 2.089 | .4786 | 8.7 | 2.723 | .3673 | 7.413 | .1349 |
| 3.3 | 1.462 | .6839 | 2.138 | .4677 | 8.8 | 2.754 | .3631 | 7.586 | .1318 |
| 3.4 | 1.479 | .6761 | 2.188 | .4571 | 8.9 | 2.786 | .3589 | 7.762 | .1288 |
| 3.5 | 1.496 | .6683 | 2.239 | .4467 | 9.0 | 2.818 | .3548 | 7.943 | .1259 |
| 3.6 | 1.514 | .6607 | 2.291 | .4365 | 9.1 | 2.851 | .3508 | 8.128 | .1230 |
| 3.7 | 1.531 | .6531 | 2.344 | .4266 | 9.2 | 2.884 | .3467 | 8.318 | .1202 |
| 3.8 | 1.549 | .6457 | 2.399 | .4169 | 9.3 | 2.917 | .3428 | 8.511 | .1175 |
| 3.9 | 1.567 | .6383 | 2.455 | .4074 | 9.4 | 2.951 | .3388 | 8.710 | .1148 |
| 4.0 | 1.585 | .6310 | 2.512 | .3981 | 9.5 | 2.985 | .3350 | 8.913 | .1122 |
| 4.1 | 1.603 | .6237 | 2.570 | .3890 | 9.6 | 3.020 | .3311 | 9.120 | .1096 |
| 4.2 | 1.622 | .6166 | 2.630 | .3802 | 9.7 | 3.055 | .3273 | 9.333 | .1072 |
| 4.3 | 1.641 | .6095 | 2.692 | .3715 | 9.8 | 3.090 | .3236 | 9.550 | .1047 |
| 4.4 | 1.660 | .6026 | 2.754 | .3631 | 9.9 | 3.126 | .3199 | 9.772 | .1023 |
| 4.5 | 1.679 | .5957 | 2.818 | .3548 | 10.0 | 3.162 | .3162 | 10.000 | .1000 |
| 4.6 | 1.698 | .5888 | 2.884 | .3467 | 10.1 | 3.199 | .3126 | 10.23 | .09772 |
| 4.7 | 1.718 | .5821 | 2.951 | .3388 | 10.2 | 3.236 | .3090 | 10.47 | .09550 |
| 4.8 | 1.738 | .5754 | 3.020 | .3311 | 10.3 | 3.273 | .3055 | 10.72 | .09333 |
| 4.9 | 1.758 | .5689 | 3.090 | .3236 | 10.4 | 3.311 | .3020 | 10.96 | .09120 |
| 5.0 | 1.778 | .5623 | 3.162 | .3162 | 10.5 | 3.350 | .2985 | 11.22 | .08913 |
| 5.1 | 1.799 | .5559 | 3.236 | .3090 | 10.6 | 3.388 | .2951 | 11.48 | .08710 |
| 5.2 | 1.820 | .5495 | 3.311 | .3020 | 10.7 | 3.428 | .2917 | 11.75 | .08511 |
| 5.3 | 1.841 | .5433 | 3.388 | .2951 | 10.8 | 3.467 | .2884 | 12.02 | .08318 |
| 5.4 | 1.862 | .5370 | 3.467 | .2884 | 10.9 | 3.508 | .2851 | 12.30 | .08128 |

Table III. Decibel Table—(Cont'd) (11.0 to 19.9 Db)

| Db | Current or Voltage Ratio | | Power Ratio | | Db | Current or Voltage Ratio | | Power Ratio | |
|------|--------------------------|-------|-------------|--------|------|--------------------------|-------|-------------|--------|
| | Gain | Loss | Gain | Loss | | Gain | Loss | Gain | Loss |
| 11.0 | 3.548 | .2818 | 12.59 | .07943 | 15.5 | 5.957 | .1679 | 35.48 | .02818 |
| 11.1 | 3.589 | .2786 | 12.88 | .07762 | 15.6 | 6.026 | .1660 | 36.31 | .02754 |
| 11.2 | 3.631 | .2754 | 13.18 | .07586 | 15.7 | 6.095 | .1641 | 37.15 | .02692 |
| 11.3 | 3.673 | .2723 | 13.49 | .07413 | 15.8 | 6.166 | .1622 | 38.02 | .02630 |
| 11.4 | 3.715 | .2692 | 13.80 | .07244 | 15.9 | 6.237 | .1603 | 38.90 | .02570 |
| 11.5 | 3.758 | .2661 | 14.13 | .07079 | 16.0 | 6.310 | .1585 | 39.81 | .02512 |
| 11.6 | 3.802 | .2630 | 14.45 | .06918 | 16.1 | 6.383 | .1567 | 40.74 | .02455 |
| 11.7 | 3.846 | .2600 | 14.79 | .06761 | 16.2 | 6.457 | .1549 | 41.69 | .02399 |
| 11.8 | 3.890 | .2570 | 15.14 | .06607 | 16.3 | 6.531 | .1531 | 42.66 | .02344 |
| 11.9 | 3.936 | .2541 | 15.49 | .06457 | 16.4 | 6.607 | .1514 | 43.65 | .02291 |
| 12.0 | 3.981 | .2512 | 15.85 | .06310 | 16.5 | 6.683 | .1496 | 44.67 | .02239 |
| 12.1 | 4.027 | .2483 | 16.22 | .06166 | 16.6 | 6.761 | .1479 | 45.71 | .02188 |
| 12.2 | 4.074 | .2455 | 16.60 | .06026 | 16.7 | 6.839 | .1462 | 46.77 | .02138 |
| 12.3 | 4.121 | .2427 | 16.98 | .05888 | 16.8 | 6.918 | .1445 | 47.86 | .02089 |
| 12.4 | 4.169 | .2399 | 17.38 | .05754 | 16.9 | 6.998 | .1429 | 48.98 | .02042 |
| 12.5 | 4.217 | .2371 | 17.78 | .05623 | 17.0 | 7.079 | .1413 | 50.12 | .01995 |
| 12.6 | 4.266 | .2344 | 18.20 | .05495 | 17.1 | 7.161 | .1396 | 51.29 | .01950 |
| 12.7 | 4.315 | .2317 | 18.62 | .05370 | 17.2 | 7.244 | .1380 | 52.48 | .01905 |
| 12.8 | 4.365 | .2291 | 19.05 | .05248 | 17.3 | 7.328 | .1365 | 53.70 | .01862 |
| 12.9 | 4.416 | .2265 | 19.50 | .05129 | 17.4 | 7.413 | .1349 | 54.95 | .01820 |
| 13.0 | 4.467 | .2239 | 19.95 | .05012 | 17.5 | 7.499 | .1334 | 56.23 | .01778 |
| 13.1 | 4.519 | .2213 | 20.42 | .04898 | 17.6 | 7.586 | .1318 | 57.54 | .01738 |
| 13.2 | 4.571 | .2188 | 20.89 | .04786 | 17.7 | 7.674 | .1303 | 58.88 | .01698 |
| 13.3 | 4.624 | .2163 | 21.38 | .04677 | 17.8 | 7.762 | .1288 | 60.26 | .01660 |
| 13.4 | 4.677 | .2138 | 21.88 | .04571 | 17.9 | 7.852 | .1274 | 61.66 | .01622 |
| 13.5 | 4.732 | .2113 | 22.39 | .04467 | 18.0 | 7.943 | .1259 | 63.10 | .01585 |
| 13.6 | 4.786 | .2089 | 22.91 | .04365 | 18.1 | 8.035 | .1245 | 64.57 | .01549 |
| 13.7 | 4.842 | .2065 | 23.44 | .04266 | 18.2 | 8.128 | .1230 | 66.07 | .01514 |
| 13.8 | 4.898 | .2042 | 23.99 | .04169 | 18.3 | 8.222 | .1216 | 67.61 | .01479 |
| 13.9 | 4.955 | .2018 | 24.55 | .04074 | 18.4 | 8.318 | .1202 | 69.18 | .01445 |
| 14.0 | 5.012 | .1995 | 25.12 | .03981 | 18.5 | 8.414 | .1189 | 70.79 | .01413 |
| 14.1 | 5.070 | .1972 | 25.70 | .03890 | 18.6 | 8.511 | .1175 | 72.44 | .01380 |
| 14.2 | 5.129 | .1950 | 26.30 | .03802 | 18.7 | 8.610 | .1161 | 74.13 | .01349 |
| 14.3 | 5.188 | .1928 | 26.92 | .03715 | 18.8 | 8.710 | .1148 | 75.86 | .01318 |
| 14.4 | 5.248 | .1905 | 27.54 | .03631 | 18.9 | 8.811 | .1135 | 77.62 | .01288 |
| 14.5 | 5.309 | .1884 | 28.18 | .03548 | 19.0 | 8.913 | .1122 | 79.43 | .01259 |
| 14.6 | 5.370 | .1862 | 28.84 | .03467 | 19.1 | 9.016 | .1109 | 81.28 | .01230 |
| 14.7 | 5.433 | .1841 | 29.51 | .03388 | 19.2 | 9.120 | .1096 | 83.18 | .01202 |
| 14.8 | 5.495 | .1820 | 30.20 | .03311 | 19.3 | 9.226 | .1084 | 85.11 | .01175 |
| 14.9 | 5.559 | .1799 | 30.90 | .03236 | 19.4 | 9.333 | .1072 | 87.10 | .01148 |
| 15.0 | 5.623 | .1778 | 31.62 | .03162 | 19.5 | 9.441 | .1059 | 89.13 | .01122 |
| 15.1 | 5.689 | .1758 | 32.36 | .03090 | 19.6 | 9.550 | .1047 | 91.20 | .01096 |
| 15.2 | 5.754 | .1738 | 33.11 | .03020 | 19.7 | 9.661 | .1035 | 93.33 | .01072 |
| 15.3 | 5.821 | .1718 | 33.88 | .02951 | 19.8 | 9.772 | .1023 | 95.50 | .01047 |
| 15.4 | 5.888 | .1698 | 34.67 | .02884 | 19.9 | 9.886 | .1012 | 97.72 | .01023 |

Note: For values from 20 to 180 db, see next page.

Table III. Decibel Table—(Cont'd) (20 to 180 Db)

| Db | Current or Voltage Ratio | | Power Ratio | |
|-------|--------------------------|------------------------|---------------------|-------------------------|
| | Gain | Loss | Gain | Loss |
| 20.0 | 10.00 | 0.1000 | 100.00 | 0.01000 |
| 25.0 | 17.78 | 0.0562 | 3.162×10^2 | 3.162×10^{-3} |
| 30.0 | 31.62 | 0.0316 | 10^3 | 10^{-3} |
| 35.0 | 56.23 | 0.0178 | 3.162×10^3 | 3.162×10^{-4} |
| 40.0 | 100.00 | 0.0100 | 10^4 | 10^{-4} |
| 45.0 | 177.8 | 0.0056 | 3.162×10^4 | 3.162×10^{-5} |
| 50.0 | 316.2 | 0.0032 | 10^5 | 10^{-5} |
| 55.0 | 562.3 | 0.0018 | 3.162×10^5 | 3.162×10^{-6} |
| 60.0 | 10^3 | 10^{-3} | 10^6 | 10^{-6} |
| 65.0 | 1.778×10^3 | 5.623×10^{-4} | 3.162×10^6 | 3.162×10^{-7} |
| 70.0 | 3.162×10^3 | 3.162×10^{-4} | 10^7 | 10^{-7} |
| 75.0 | 5.623×10^3 | 1.78×10^{-4} | 3.162×10^7 | 3.162×10^{-8} |
| 80.0 | 10^4 | 10^{-4} | 10^8 | 10^{-8} |
| 85.0 | 1.778×10^4 | 5.623×10^{-5} | 3.162×10^8 | 3.162×10^{-9} |
| 90.0 | 3.162×10^4 | 3.162×10^{-5} | 10^9 | 10^{-9} |
| 95.0 | 5.632×10^4 | 1.78×10^{-5} | 3.162×10^9 | 3.162×10^{-10} |
| 100.0 | 10^5 | 10^{-5} | 10^{10} | 10^{-10} |
| 110.0 | 3.162×10^5 | 3.162×10^{-6} | 10^{11} | 10^{-11} |
| 120.0 | 10^6 | 10^{-6} | 10^{12} | 10^{-12} |
| 130.0 | 3.162×10^6 | 3.162×10^{-7} | 10^{13} | 10^{-13} |
| 140.0 | 10^7 | 10^{-7} | 10^{14} | 10^{-14} |
| 150.0 | 3.162×10^7 | 3.162×10^{-8} | 10^{15} | 10^{-15} |
| 160.0 | 10^8 | 10^{-8} | 10^{16} | 10^{-16} |
| 170.0 | 3.162×10^8 | 3.162×10^{-9} | 10^{17} | 10^{-17} |
| 180.0 | 10^9 | 10^{-9} | 10^{18} | 10^{-18} |

Constants and Standards

27. DIELECTRIC CONSTANTS OF MATERIALS

The dielectric constants of most materials vary for different temperatures and frequencies. Likewise, small differences in the composition of materials will cause differences in the dielectric constants. A list of materials, and the approximate range (where available) of their dielectric constants, are given in Table IV. The values shown are accurate enough for most applications. The dielectric constants of some materials (such as quartz, *Styrofoam*, and *Teflon*) do not change appreciably with frequency.

Table IV. Dielectric Constants of Materials

| Material | Dielectric Constant (Approx.) | Material | Dielectric Constant (Approx.) |
|--------------------------|-------------------------------|------------------------------|-------------------------------|
| Air | 1.0 | Nylon | 3.4-22.4 |
| Amber | 2.6-2.7 | Paper (dry) | 1.5-3.0 |
| Bakelite (asbestos base) | 5.0-22 | Paper (paraffin coated) | 2.5-4.0 |
| Bakelite (mica filled) | 4.5-4.8 | Paraffin (solid) | 2.0-3.0 |
| Beeswax | 2.4-2.8 | Plexiglass | 2.6-3.5 |
| Cambric (varnished) | 4.0 | Polyethylene | 2.3 |
| Celluloid | 4.0 | Polystyrene | 2.4-3.0 |
| Cellulose Acetate | 3.1-4.5 | Porcelain (dry process) | 5.0-5.5 |
| Durite | 4.7-5.1 | Porcelain (wet process) | 5.8-6.5 |
| Ebonite | 2.7 | Quartz | 5.0 |
| Fiber | 5.0 | Quartz (fused) | 3.78 |
| Formica | 3.6-6.0 | Rubber (hard) | 2.0-4.0 |
| Glass (electrical) | 3.8-14.5 | Ruby Mica | 5.4 |
| Glass (photographic) | 7.5 | Shellac (natural) | 2.9-3.9 |
| Glass (Pyrex) | 4.6-5.0 | Silicone (glass) (molding) | 3.2-4.7 |
| Glass (window) | 7.6 | Silicone (glass) (laminated) | 3.7-4.3 |
| Gutta Percha | 2.4-2.6 | Slate | 7.0 |
| Isolantite | 6.1 | Steatite (ceramic) | 5.2-6.3 |
| Lucite | 2.5 | Steatite (low loss) | 4.4 |
| Mica (electrical) | 4.0-9.0 | Styrofoam | 1.03 |
| Mica (clear India) | 7.5 | Teflon | 2.1 |
| Mica (filled phenolic) | 4.2-5.2 | Vaseline | 2.16 |
| Micarta | 3.2-5.5 | Vinylite | 2.7-7.5 |
| Mycalex | 7.3-9.3 | Water (distilled) | 34-78 |
| Neoprene | 4.0-6.7 | Wood (dry) | 1.4-2.9 |

28. CONVERSION FACTORS

The following table lists the multiplying factors necessary to convert from one unit of measure to another, and vice versa. To use the table, locate the unit of measure you are converting from or the one you are converting to in the first column. Opposite this listing are the multiplying factors for converting either unit of measure to the other unit of measure.

Table V. Conversion Factors

| To Convert | Into | Multiply by | Conversely, Multiply by |
|-------------------------|----------------------|--|--|
| Acres | Square feet | 4.356×10^4 | 2.296×10^{-5} |
| Acres | Square meters | 4047 | 2.471×10^{-4} |
| Acres | Square miles | 1.5625×10^{-3} | 640 |
| Amperes | Microamperes | 10^6 | 10^{-6} |
| Amperes | Micromicroamperes | 10^{12} | 10^{-12} |
| Amperes | Milliamperes | 10^3 | 10^{-3} |
| Ampere-hours | Coulombs | 3600 | 2.778×10^{-4} |
| Ampere-turns | Gilberts | 1.257 | 0.7958 |
| Ampere-turns per cm. | Ampere-turns per in. | 2.54 | 0.3937 |
| Angstrom units | Inches | 3.937×10^{-9} | 2.54×10^4 |
| Angstrom units | Meters | 10^{-10} | 10^{10} |
| Bars | Atmospheres | 9.870×10^{-7} | 1.0133 |
| Bars | Dynes per sq. cm. | 10^6 | 10^{-6} |
| Bars | Pounds per sq. in. | 14.504 | 6.8947×10^{-2} |
| Btu | Ergs | 1.0548×10^{10} | 9.486×10^{-11} |
| Btu | Foot-pounds | 778.3 | 1.285×10^{-3} |
| Btu | Joules | 1054.8 | 9.480×10^{-4} |
| Btu | Kilogram-calories | 0.252 | 3.969 |
| Btu per hour | Horsepower-hours | 3.929×10^{-4} | 2545 |
| Bushels | Cubic feet | 1.2445 | 0.8036 |
| Calories, gram | Joules | 4.185 | 0.2389 |
| Centigrade | Celsius | 1 | 1 |
| Centigrade | Fahrenheit | $(^{\circ}\text{C} \times 9/5)$ $+ 32 = ^{\circ}\text{F}$ | $(^{\circ}\text{F} - 32)$ $\times 5/9 = ^{\circ}\text{C}$ |
| Centigrade | Kelvin | $^{\circ}\text{C} + 273.1 = ^{\circ}\text{K}$ | $^{\circ}\text{K} - 273.1$ $= ^{\circ}\text{C}$ |
| Chains (surveyor's) | Feet | 66 | 1.515×10^{-2} |
| Circular mils | Square centimeters | 5.067×10^{-6} | 1.973×10^2 |
| Circular mils | Square mils | 0.7854 | 1.273 |
| Cubic feet | Gallons (liq. U.S.) | 7.481 | 0.1337 |
| Cubic feet | Liters | 28.32 | 3.531×10^{-2} |
| Cubic inches | Cubic centimeters | 16.39 | 6.102×10^{-2} |
| Cubic inches | Cubic feet | 5.787×10^{-4} | 1728 |
| Cubic inches | Cubic meters | 1.639×10^{-5} | 6.102×10^4 |
| Cubic inches | Gallons (liq. U.S.) | 4.329×10^{-3} | 231 |
| Cubic meters | Cubic feet | 35.31 | 2.832×10^{-2} |
| Cubic meters | Cubic yards | 1.308 | 0.7646 |
| Cycles | Kilocycles | 10^{-3} | 10^3 |
| Cycles | Megacycles | 10^{-6} | 10^6 |

Table V. Conversion Factors—(Cont'd)

| To Convert | Into | Multiply by | Conversely, Multiply by |
|-------------------------|-------------------------|--|--|
| Degrees (angle) | Mils | 17.45 | 5.73×10^{-2} |
| Degrees (angle) | Radians | 1.745×10^{-2} | 57.3 |
| Dynes | Pounds | 2.248×10^{-6} | 4.448×10^5 |
| Ergs | Foot-pounds | 7.376×10^{-8} | 1.356×10^7 |
| Fahrenheit | Rankine | $^{\circ}\text{F} + 459.58 = ^{\circ}\text{R}$ | $^{\circ}\text{R} - 459.58 = ^{\circ}\text{F}$ |
| Faradays | Ampere-hours | 26.8 | 3.731×10^{-2} |
| Farads | Microfarads | 10^6 | 10^{-6} |
| Farads | Micromicrofarads | 10^{12} | 10^{-12} |
| Farads | Millifarads | 10^3 | 10^{-3} |
| Fathoms | Feet | 6 | 0.16667 |
| Feet | Centimeters | 30.48 | 3.281×10^{-2} |
| Feet | Meters | 0.3048 | 3.281 |
| Feet | Mils | 1.2×10^4 | 8.333×10^{-5} |
| Foot-pounds | Gram-centimeters | 1.383×10^4 | 1.235×10^{-6} |
| Foot-pounds | Horsepower-hours | 5.05×10^{-7} | 1.98×10^6 |
| Foot-pounds | Kilogram-meters | 0.1383 | 7.233 |
| Foot-pounds | Kilowatt-hours | 3.766×10^{-7} | 2.655×10^6 |
| Foot-pounds | Ounce-inches | 192 | 5.208×10^{-3} |
| Gallons (liq. U.S.) | Cubic meters | 3.785×10^{-3} | 264.2 |
| Gallons (liq. U.S.) | Gallons (liq. Br. Imp.) | 0.8327 | 1.201 |
| Gausses | Lines per sq. cm. | 1.0 | 1.0 |
| Gausses | Lines per sq. in. | 6.452 | 0.155 |
| Gausses | Webers per sq. in. | 6.452×10^{-4} | 1.55×10^7 |
| Grams | Dynes | 980.7 | 1.02×10^{-3} |
| Grams | Grains | 15.43 | 6.481×10^{-2} |
| Grams | Ounces (avdp.) | 3.527×10^{-2} | 28.35 |
| Grams | Poundals | 7.093×10^{-2} | 14.1 |
| Grams per cm. | Pounds per in. | 5.6×10^{-3} | 178.6 |
| Grams per cu. cm. | Pounds per cu. in. | 3.613×10^{-2} | 27.68 |
| Henries | Microhenries | 10^6 | 10^{-6} |
| Henries | Millihenries | 10^3 | 10^{-3} |
| Horsepower | Btu per minute | 42.418 | 2.357×10^{-2} |
| Horsepower | Foot-lbs. per minute | 3.3×10^4 | 3.03×10^{-5} |
| Horsepower | Foot-lbs. per second | 550 | 1.182×10^{-3} |
| Horsepower | Horsepower (metric) | 1.014 | 0.9863 |
| Horsepower | Kilowatts | 0.746 | 1.341 |
| Inches | Centimeters | 2.54 | 0.3937 |
| Inches | Feet | 8.333×10^{-2} | 12 |
| Inches | Meters | 2.54×10^{-2} | 39.37 |
| Inches | Miles | 1.578×10^{-5} | 6.336×10^4 |
| Inches | Mils | 10^3 | 10^{-3} |
| Inches | Yards | 2.778×10^{-2} | 36 |
| Joules | Foot-pounds | 0.7376 | 1.356 |
| Joules | Ergs | 10^7 | 10^{-7} |
| Joules | Watt-hours | 2.778×10^{-4} | 3600 |
| Kilograms | Tonnes | 10^3 | 10^{-3} |
| Kilograms | Tons (long) | 9.842×10^{-4} | 1016 |
| Kilograms | Tons (short) | 1.102×10^{-3} | 907.2 |
| Kilograms | Pounds (avdp.) | 2.205 | 0.4536 |
| Kilograms per sq. meter | Pounds per sq. feet | 0.2048 | 4.882 |

Table V. Conversion Factors—(Cont'd)

| To Convert | Into | Multiply by | Conversely, Multiply by |
|--------------------|--|--------------------------|----------------------------|
| Kilometers | Feet | 3281 | 3.408×10^{-4} |
| Kilometers | Inches | 3.937×10^4 | 2.54×10^{-5} |
| Kilometers | Light years | 1.0567×10^{-13} | 9.4637×10^{12} |
| Kilometers per hr. | Feet per minute | 54.68 | 1.829×10^{-2} |
| Kilometers per hr. | Knots | 0.5396 | 1.8532 |
| Kilowatt-hours | Btu | 3413 | 2.93×10^{-4} |
| Kilowatt-hours | Foot-pounds | 2.655×10^6 | 3.766×10^{-7} |
| Kilowatt-hours | Joules | 3.6×10^6 | 2.778×10^{-7} |
| Kilowatt-hours | Horsepower-hours | 1.341 | 0.7457 |
| Kilowatt-hours | Pounds water evaporated from and at 212°F. | 3.53 | 0.284 |
| Kilowatt-hours | Watt-hours | 10^3 | 10^{-3} |
| Knots | Feet per second | 1.688 | 0.5925 |
| Knots | Meters per minute | 30.87 | 0.0324 |
| Knots | Miles per hour | 1.1508 | 0.869 |
| Lamberts | Candles per sq. cm. | 0.3183 | 3.142 |
| Lamberts | Candles per sq. in. | 2.054 | 0.4869 |
| Leagues | Miles | 3 | 0.33 |
| Links | Chains | 0.01 | 100 |
| Links (surveyor's) | Inches | 7.92 | 0.1263 |
| Liters | Bushels (dry U.S.) | 2.838×10^{-2} | 35.24 |
| Liters | Cubic centimeters | 10^3 | 10^{-3} |
| Liters | Cubic meters | 10^{-3} | 10^3 |
| Liters | Cubic inches | 61.02 | 1.639×10^{-2} |
| Liters | Gallons (liq. U.S.) | 0.2642 | 3.785 |
| Liters | Pints (liq. U.S.) | 2.113 | 0.4732 |
| $\log_e N$ | $\log_{10} N$ | 0.4343 | 2.303 |
| Lumens per sq. ft. | Foot-candles | 1 | 1 |
| Lux | Foot-candles | 0.0929 | 10.764 |
| Maxwells | Kilolines | 10^{-3} | 10^3 |
| Maxwells | Megalines | 10^{-6} | 10^6 |
| Maxwells | Webers | 10^{-6} | 10^8 |
| Meters | Centimeters | 10^2 | 10^{-2} |
| Meters | Feet | 3.28 | 30.48×10^{-2} |
| Meters | Inches | 39.37 | 2.54×10^{-2} |
| Meters | Kilometers | 10^{-3} | 10^3 |
| Meters | Miles | 6.214×10^{-4} | 1609.35 |
| Meters | Yards | 1.094 | 0.9144 |
| Meters per minute | Feet per minute | 3.281 | 0.3048 |
| Meters per minute | Kilometers per hour | 0.06 | 16.67 |
| Mhos | Micromhos | 10^6 | 10^{-6} |
| Mhos | Millimhos | 10^3 | 10^{-3} |
| Microfarads | Micromicrofarads | 10^6 | 10^{-6} |
| Miles (nautical) | Feet | 6076.1 | 1.646×10^{-4} |
| Miles (nautical) | Meters | 1852 | 5.4×10^{-4} |
| Miles (statute) | Feet | 5280 | 1.894×10^{-4} |
| Miles (statute) | Kilometers | 1.609 | 0.6214 |
| Miles (statute) | Light years | 1.691×10^{-13} | 5.88×10^{12} |
| Miles (statute) | Miles (nautical) | 0.869 | 1.1508 |

Table V. Conversion Factors—(Cont'd)

| To Convert | Into | Multiply by | Conversely, Multiply by |
|-------------------------|----------------------|------------------------|----------------------------|
| Miles (statute) | Yards | 1760 | 5.6818×10^{-4} |
| Miles per hour | Feet per minute | 88 | 1.136×10^{-2} |
| Miles per hour | Feet per second | 1.467 | 0.6818 |
| Miles per hour | Kilometers per hour | 1.609 | 0.6214 |
| Miles per hour | Knots | 0.8684 | 1.152 |
| Milliamperes | Microamperes | 10^3 | 10^{-3} |
| Millihenries | Microhenries | 10^3 | 10^{-3} |
| Millimeters | Centimeters | 0.1 | 10 |
| Millimeters | Inches | 3.937×10^{-2} | 25.4 |
| Millimeters | Microns | 10^3 | 10^{-3} |
| Millivolts | Microvolts | 10^3 | 10^{-3} |
| Mils | Minutes | 3.438 | 0.2909 |
| Minutes (angle) | Degrees | 1.666×10^{-2} | 60 |
| Nepers | Decibels | 8.686 | 0.1151 |
| Newtons | Dynes | 10^5 | 10^{-5} |
| Newtons | Pounds (avdp.) | 0.2248 | 4.448 |
| Ohms | Milliohms | 10^3 | 10^{-3} |
| Ohms | Micro-ohms | 10^6 | 10^{-6} |
| Ohms | Micromicro-ohms | 10^{12} | 10^{-12} |
| Ohms | Megohms | 10^{-6} | 10^6 |
| Ohms | Ohms (International) | 0.99948 | 1.00052 |
| Ohms per foot | Ohms per meter | 0.3048 | 3.281 |
| Ounces (fluid) | Quarts | 3.125×10^{-2} | 32 |
| Ounces (avdp.) | Pounds | 6.25×10^{-2} | 16 |
| Picofarad | Micromicrofarad | 1 | 1 |
| Pints | Quarts (liq. U.S.) | 0.50 | 2 |
| Pounds (force) | Newtons | 4.4482 | 0.2288 |
| Pounds carbon oxidized | Btu | 14,544 | 6.88×10^{-5} |
| Pounds carbon oxidized | Horsepower-hours | 5.705 | 0.175 |
| Pounds carbon oxidized | Kilowatt-hours | 4.254 | 0.235 |
| Pounds of water (dist.) | Cubic feet | 1.603×10^{-2} | 62.38 |
| Pounds of water (dist.) | Gallons | 0.1198 | 8.347 |
| Pounds per sq. in. | Dynes per sq. cm. | 6.8946×10^4 | 1.450×10^{-5} |
| Poundals | Dynes | 1.383×10^4 | 7.233×10^{-5} |
| Poundals | Pounds (avdp.) | 3.108×10^{-2} | 32.17 |
| Quadrants | Degrees | 90 | 11.111×10^{-2} |
| Quadrants | Radians | 1.5708 | 0.637 |
| Radians | Mils | 10^3 | 10^{-3} |
| Radians | Minutes | 3.438×10^3 | 2.909×10^{-4} |
| Radians | Seconds | 2.06265×10^5 | 4.848×10^{-6} |
| Rods | Feet | 16.5 | 6.061×10^{-2} |
| Rods | Miles | 3.125×10^{-3} | 320 |
| Rods | Yards | 5.5 | 0.1818 |
| Rpm | Degrees per second | 6.0 | 0.1667 |
| Rpm | Radians per second | 0.1047 | 9.549 |

Table V. Conversion Factors—(Cont'd)

| To Convert | Into | Multiply by | Conversely, Multiply by |
|-------------------------|---------------------------------|------------------------|----------------------------|
| Rpm | Rps | 1.667×10^{-2} | 60 |
| Square feet | Acres | 2.296×10^{-5} | 43,560 |
| Square feet | Square centimeters | 929.034 | 1.076×10^{-3} |
| Square feet | Square inches | 144 | 6.944×10^{-3} |
| Square feet | Square meters | 9.29×10^{-2} | 10.764 |
| Square feet | Square miles | 3.587×10^{-8} | 27.88×10^8 |
| Square feet | Square yards | 11.11×10^{-2} | 9 |
| Square inches | Circular mils | 1.273×10^4 | 7.854×10^{-7} |
| Square inches | Square centimeters | 6.452 | 0.155 |
| Square inches | Square mils | 10^6 | 10^{-6} |
| Square inches | Square millimeters | 645.2 | 1.55×10^{-3} |
| Square kilometers | Square miles | 0.3861 | 2.59 |
| Square meters | Square yards | 1.196 | 0.8361 |
| Square miles | Acres | 640 | 1.562×10^{-3} |
| Square miles | Square yards | 3.098×10^6 | 3.228×10^{-7} |
| Square millimeters | Circular mils | 1973 | 5.067×10^{-4} |
| Square millimeters | Square centimeters | .01 | 100 |
| Square mils | Circular mils | 1.273 | 0.7854 |
| Tons (long) | Pounds (avdp.) | 2240 | 4.464×10^{-4} |
| Tons (short) | Pounds | 2,000 | 5×10^{-4} |
| Tonnes | Pounds | 2204.63 | 4.536×10^{-4} |
| Varas | Feet | 2.7777 | 0.36 |
| Volts | Kilovolts | 10^{-3} | 10^3 |
| Volts | Microvolts | 10^6 | 10^{-6} |
| Volts | Millivolts | 10^3 | 10^{-3} |
| Watts | Btu per hour | 3.413 | 0.293 |
| Watts | Btu per minute | 5.689×10^{-2} | 17.58 |
| Watts | Ergs per second | 10^7 | 10^{-7} |
| Watts | Foot-lbs per minute | 44.26 | 2.26×10^{-2} |
| Watts | Foot-lbs per second | 0.7378 | 1.356 |
| Watts | Horsepower | 1.341×10^{-3} | 746 |
| Watts | Kilogram-calories per minute | 1.433×10^{-2} | 69.77 |
| Watts | Kilowatts | 10^{-3} | 10^3 |
| Watts | Microwatts | 10^6 | 10^{-6} |
| Watts | Milliwatts | 10^3 | 10^{-3} |
| Watt-seconds | Joules | 1 | 1 |
| Webers | Maxwells | 10^8 | 10^{-8} |
| Webers per sq. meter | Gausses | 10^4 | 10^{-4} |
| Yards | Feet | 3 | .3333 |
| Yards | Varas | 1.08 | 0.9259 |

29. METRIC PREFIXES

(A) Unit Prefixes

The metric system, whereby a different prefix is assigned for each order of magnitude, is particularly suited for electronic values. In 1958 the International Committee on Weights and Measures assigned prefixes for the ninth and twelfth orders of magnitude (both positive and negative). (See Table VI.) This system eliminates the cumbersome double prefixes (micromicro-, "kilomega-, etc. In 1959 the National Bureau of Standards began using these terms; however, acceptance by industry in the United States has been slow, particularly in using the newer term "picofarad" instead of "micromicrofarad."

Table VI. Metric Prefixes

| Multiple | Prefix | Abbreviation | Multiple | Prefix | Abbreviation |
|-----------|--------|--------------|------------|--------|--------------|
| 10^{12} | tera- | T | 10^{-1} | deci- | d |
| 10^9 | giga- | G | 10^{-2} | centi- | c |
| 10^6 | mega- | M | 10^{-3} | milli- | m |
| 10^4 | myria- | My | 10^{-6} | micro- | μ |
| 10^3 | kilo- | K | 10^{-9} | nano- | n |
| 10^2 | hecto- | H | 10^{-12} | pico- | p |
| 10 | deka- | D | | | |

(B) Conversion Table

Table VII gives the number of places, and the direction, the decimal point must be moved to convert from one metric notation to another. The value labeled "units" is the basic unit of measurement—e.g., ohms, farads, etc. To use the chart, find the desired value in the left-hand column; then follow the horizontal line across to the column with the prefix in which the original value is stated. The number and arrow at this point indicate the number of places and the direction the decimal point must be moved to change the original value to the desired value.

Table VII. Metric Conversion Table

| Desired Value | Original Value | | | | | | | | | | | | | |
|---------------|----------------|-------|-------|--------|-------|--------|-------|-------|-------|--------|--------|--------|-------|-------|
| | Tera- | Giga- | Mega- | Myria- | Kilo- | Hecto- | Deka- | Units | Deci- | Centi- | Milli- | Micro- | Nano- | Pico- |
| Tera- | | ← 3 | ← 6 | ← 8 | ← 9 | ←10 | ←11 | ←12 | ←13 | ←14 | ←15 | ←18 | ←21 | ←24 |
| Giga- | 3→ | | ← 3 | ← 5 | ← 6 | ← 7 | ← 8 | ← 9 | ←10 | ←11 | ←12 | ←15 | ←18 | ←21 |
| Mega- | 6→ | 3→ | | ← 2 | ← 3 | ← 4 | ← 5 | ← 6 | ← 7 | ← 8 | ← 9 | ←12 | ←15 | ←18 |
| Myria- | 8→ | 5→ | 2→ | | ← 1 | ← 2 | ← 3 | ← 4 | ← 5 | ← 6 | ← 7 | ←10 | ←13 | ←16 |
| Kilo- | 9→ | 6→ | 3→ | 1→ | | ← 1 | ← 2 | ← 3 | ← 4 | ← 5 | ← 6 | ← 9 | ←12 | ←15 |
| Hecto- | 10→ | 7→ | 4→ | 2→ | 1→ | | ← 1 | ← 2 | ← 3 | ← 4 | ← 5 | ← 8 | ←11 | ←14 |
| Deka- | 11→ | 8→ | 5→ | 3→ | 2→ | 1→ | | ← 1 | ← 2 | ← 3 | ← 4 | ← 7 | ←10 | ←13 |
| Units | 12→ | 9→ | 6→ | 4→ | 3→ | 2→ | 1→ | | ← 1 | ← 2 | ← 3 | ← 6 | ← 9 | ←12 |
| Deci- | 13→ | 10→ | 7→ | 5→ | 4→ | 3→ | 2→ | 1→ | | ← 1 | ← 2 | ← 5 | ← 8 | ←11 |
| Centi- | 14→ | 11→ | 8→ | 6→ | 5→ | 4→ | 3→ | 2→ | 1→ | | ← 1 | ← 4 | ← 7 | ←10 |
| Milli- | 15→ | 12→ | 9→ | 7→ | 6→ | 5→ | 4→ | 3→ | 2→ | 1→ | | ← 3 | ← 6 | ← 9 |
| Micro- | 18→ | 15→ | 12→ | 10→ | 9→ | 8→ | 7→ | 6→ | 5→ | 4→ | 3→ | | ← 3 | ← 6 |
| Nano- | 21→ | 18→ | 15→ | 13→ | 12→ | 11→ | 10→ | 9→ | 8→ | 7→ | 6→ | 3→ | | ← 3 |
| Pico- | 24→ | 21→ | 18→ | 16→ | 15→ | 14→ | 13→ | 12→ | 11→ | 10→ | 9→ | 6→ | 3→ | |

30. STANDARD FREQUENCIES AND TIME SIGNALS

(A) WWV and WWVH

Time signals, audio frequencies, and a 36-digit binary timing code are broadcast continuously day and night from WWV, operated by the National Bureau of Standards near Washington, D.C. The WWV broadcast frequencies are 2.5, 5, 10, 15, 20, and 25 megacycles; and its modulation consists of 1-cps pulses and 440- and 600-cps tones. A similar station, WWVH, is located at Maui, Hawaii. It broadcasts on frequencies of 5, 10, and 15 megacycles.

Signals from WWV and WWVH are coordinated with Stations GBR and MSF at Rugby, England, and Station NBA in the Canal Zone. This coordination provides a more uniform system of time and frequency transmissions throughout the world. It also aids in the solution of many scientific and technical problems such as radiocommunications, geodesy, and tracking of artificial satellites.

WWV is silent for a four-minute period beginning approximately 45 minutes after each hour. The WWVH transmissions are silent for a four-minute period beginning approximately 15 minutes after the hour, and for 34 minutes beginning at 1900 Universal Time.

The frequencies transmitted from WWV and WWVH are accurate to within 1 part in 10 billion.

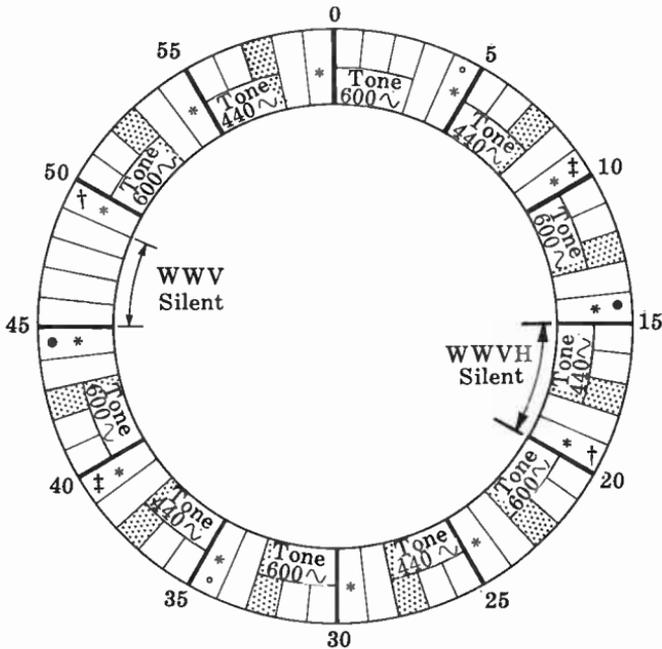
The drawing in Fig. 54 shows a breakdown of the transmissions during each hour. Each small division represents 1 minute; each large division, 5 minutes.

The audio-frequency signals are transmitted from WWV for precisely two minutes at the beginning of each five-minute period except at the beginning of each hour, when the transmission is for three minutes, and at 45 minutes after the hour when WWV is silent. The audio-frequency signal from WWVH is for precisely three minutes during the periods indicated in Fig. 54.

The timing code (a 36-bit, 100-pulses-per-second code carried on 1,000-cps modulation) is broadcast for one-minute intervals, 10 times per hour. This timing code is indicated by the shaded area in Fig. 54, and immediately follows the 440- and 600-cps modulation except at the beginning of each hour. The 440- and 600-cps modulations are alternated as shown in Fig. 54.

The code is binary-coded decimal (BCD), as shown in Fig. 55, and contains the time-of-year information (in Universal Time) in seconds, minutes, hours, and days. The code consists of nine binary groups each second, as shown in Fig. 55A. The groups appear in the following order: two groups for seconds, two for minutes, two for hours, and three for day of year. The expanded drawing at the bottom of Fig. 55A shows the make-up of the pulse code. A "0" pulse is 2 milliseconds long (or 2 cycles at 1,000 cps), and the "1" pulse is 6 milliseconds (6 cycles at 1,000 cps). The code is locked in phase with the frequency and time signals.

A complete time frame is 1 second. Fig. 55B shows the make-up of a typical time code. The time code is amplitude-



- * One Minute Announcement interval (See Fig. 56).
- † North Atlantic Propagation Notice—WWV.
- ‡ North Pacific Propagation Notice—WWVH.
- ° IWDS Warning—WWV.
- IWDS Warning—WWVH.

WWVH Silent Between 1900 and 1934 Universal Time

Fig. 54

modulated on 1,000 cps. The leading edge of the time-code pulses coincide with the zero axis of the positive-going 1,000-cps signal. The least significant binary group and least significant binary digit in each group occur first. The binary groups follow the 1-second reference marker. The start time occurs at the leading edge of all pulses.

The BCD contains a 100-per-second clocking rate, 10-per-second index markers, and 1-per-second reference markers. The 1,000-cps signal is locked to the code pulses so that millisecond resolution can be obtained easily.

The 10-per-second index markers consist of "1" pulses preceding each code group except at the beginning of the second, where there is a "0" pulse.

Each second begins at the leading edge of the "0" pulse, as shown in Fig. 55.

The 1-second reference marker is made up of five "1" pulses followed by a "0" pulse.

The code is spaced so that it follows each of the 10-per-second index markers. The last index marker is followed by an unused four-bit group of "0" pulses immediately preceding the 1-second reference marker.

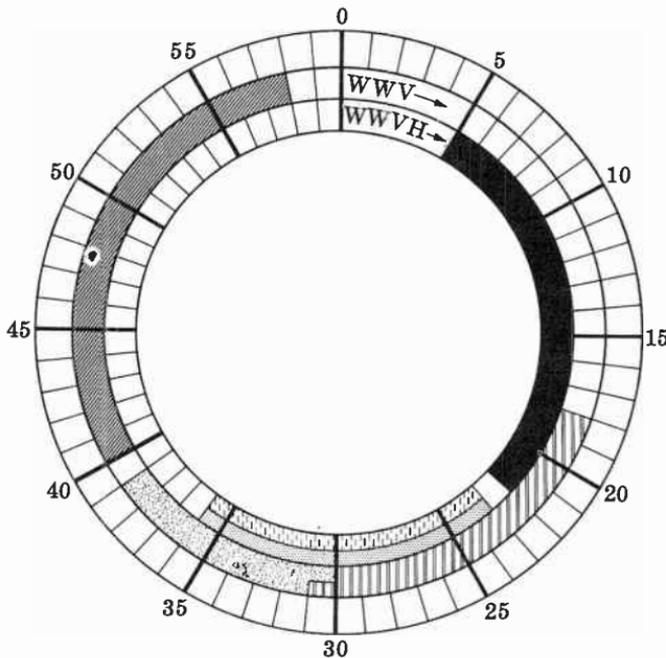
A five-millisecond pulse spaced at intervals of one second is also transmitted. The pulse transmitted by WWV consists of five cycles of a 1,000-cycle tone. The pulse transmitted by WWVH consists of six cycles of a 1,200-cycle tone. The 440- and 600-cps tone signal is interrupted for .04 second for each seconds pulse. The pulse starts .01 second after commencement of the interruption, and resumes .025 second after the pulse. For identification, the fifty-ninth second pulse is omitted, and the zero-second pulse is followed by another pulse 100 milliseconds later.

A voice announcement of Eastern Standard Time and call letters is given each five minutes from station WWV. This is followed by a telegraph-code announcement of Universal Time and another voice announcement of Eastern Standard Time. WWVH broadcasts call letters and Universal Time (UT) in telegraphic code only. The time given is the time at the resumption of the tone.

The drawing in Fig. 56 shows a breakdown of the transmissions during the one-minute announcement intervals marked with an asterisk (*) in Fig. 54. Each division on this drawing represents one second.

During announcement intervals at 19½ and 49½ minutes past every hour, propagation notices applying to transmission paths over the North Atlantic are transmitted from WWV. Similar forecasts for the North Pacific are transmitted from WWVH, during announcement intervals, at 9.4 and 39.4 minutes after the hour.

These notices, in telegraphic code, consist of a letter followed by a number. The letter signifies the propagation conditions at the time of the broadcast. The following designations are used:



-  Universal Time and Call Letters (Code).
-  IWDS Warning (Code) – WWV. (4.3 and 34.3 Minutes After Hour Only.)
-  North Pacific Propagation Forecast. (Approx. 9.4 and 39.4 Minutes After Hour Only.)
-  IWDS Warning (Code) – WWVH. (Approx. 14.4 and 44.4 Minutes After Hour Only.)
-  North Atlantic Propagation Forecast. (19.5 and 49.5 Minutes After Hour Only.)
-  Call Letters and EST (Voice) – UT (Code) – EST (Voice).

Fig. 56

N—Normal U—Unsettled W—Disturbance

The number following the letter applies to expected propagation conditions during the subsequent 6 or more hours. The following designations are used:

| | | |
|-------------|----------------|-------------|
| 1—Useless | 4—Poor to Fair | 7—Good |
| 2—Very Poor | 5—Fair | 8—Very good |
| 3—Poor | 6—Fair to Good | 9—Excellent |

At 4.3 and 34.3 minutes past the hour on WWV, and at approximately 14.4 and 44.4 minutes past the hour on WWVH, the IWDS (International World Day Service) warning is broadcast. This message reveals to experimenters in radio, geophysical, and solar sciences the content of the warning message issued at 1600 UT by the world warning agency on days when an outstanding geophysical event has occurred during the preceding 24 hours. This message is first broadcast at 1604.3 UT on WWV and at 1714.4 UT on WWVH.

If the IWDS warning declares an alert, the letters AGI AAAA are broadcast very slowly in code. This means that a significant magnetic storm has started or that an outstanding auroral display or increase in cosmic-ray flux has been reported or observed.

If a special world interval is in progress, the code letters AGI are followed by three extra-long dashes. This again indicates that an alert has been declared and that the geophysical activity is of sufficient interest to warrant special attention and intensified observations. Special world intervals usually last two or three days.

When there is no "state of alert" or "special world interval" in progress, the letters AGI EEEEE are broadcast.

(B) CHU

The Dominion Observatory at Ottawa, Canada, broadcasts time signals which can be heard throughout the North American continent and many other parts of the world. The frequencies are 3,330, 7,335, and 14,670 kc, and the transmission is continuous on all frequencies. The 3,330-kc transmitter has a power of 0.75 kw and the other two, 3 kw.

The frequencies are synthesized from a 100-kc crystal oscillator which is maintained accurate to within a few parts

in one billion. The "seconds" pips are also derived from this same oscillator and consist of 200 cycles of a 1,000-cps tone.

The "seconds" pips are broadcast continuously except for the 29th and the 51st through 59th pips, which are omitted each minute. In addition, the 1st to 29th pips are omitted during the first minute of the hour. The beginning of the pip marks the exact second. The zero pip has a duration of 0.5 second instead of the 0.2 second of the other pips.

During the first half-minute of each hour, CHU CANADA CHU is transmitted in code.

A voice announcement of the time is given each minute during the 10-second interval between the 50th and 60th second when the pips are omitted. The announcement is as follows: "CHU, Dominion Observatory Canada, Eastern Standard Time, _____ hours, _____ minutes." The time given refers to the beginning of the minute pip which follows, and is on the 24-hour system.

(C) Other Standards Stations

Throughout the world, there are many other stations which broadcast similar data. Table VIII lists some of them, and other data about stations operating on the standards frequencies. Table IX lists some other stations in the LF and VLF bands which broadcast similar data, but not on the frequencies assigned for standard-frequency operation.

31. FREQUENCY AND OPERATING POWER TOLERANCES

(A) AM Broadcast

The operating frequency tolerance of each station shall be maintained within ± 20 cycles of the assigned frequency.

The operating power of each AM broadcast station shall be maintained as near as practicable to the licensed power and shall not exceed the limits of 5 per cent above and 10 per cent below the licensed power except in emergencies.

(B) FM Broadcast

Operating frequency tolerance of each station shall be maintained within $\pm 2,000$ cycles of the assigned center frequency.

Table VIII. Other Standards Stations

| Call Sign | Location | Carrier Freq. (mc) | Modulation (cps) | Power (kw) |
|-----------|-------------------------------|------------------------|-------------------|------------|
| ATA | New Delhi, India | 10 | 1; 1000 | 1.0 |
| FFH | Paris, France | 2.5; 5; 10 | 1; 440; 1000 | 0.3 |
| HBN | Neuchatel, Switzerland | 2.5; 5 | 1; 500 | 0.5 |
| IAM | Rome, Italy | 5 | 1; 440; 600; 1000 | 1.0 |
| IBF | Turin, Italy | 5 | 1; 440; 1000 | 0.3 |
| JJY | Tokyo, Japan | 2.5; 5; 10; 15 | 1; 440; 1000 | 2.0 |
| LOL | Buenos Aires, Argentina | 2.5; 5; 10; 15; 20; 25 | 1; 440; 1000 | 2.0 |
| MSF | Rugby, England | 2.5; 5; 10 | 1; 1000 | 0.5 |
| OMA | Prague, Czechoslovakia | 2.5 | 1; 1000 | 1.0 |
| ZLFS | Lower Hutt, New Zealand | 2.5 | ----- | 0.03 |
| ZUO | Olifantsfontein, South Africa | 5 | 1 | 4.0 |
| WWVL | Fort Collins, Colorado | 20 kc | ----- | 1.0 |

Table IX. LF and VLF Stations

| Call Sign | Location | Carrier Freq. (kc) | Modulation (cps) | Power (kw) |
|-----------|-------------------------|--------------------|------------------|------------|
| WWVB | Fort Collins, Colorado | 60 | ----- | 5 |
| DCF77 | Federal German Republic | 77.5 | 1; 200; 440 | 12 |
| OMA | Czechoslovakia | 50 | ----- | 5 |
| GBR | Rugby, England | 16 | ----- | 300 |
| MSF | Rugby, England | 60 | 1; 1000 | 10 |
| NBA | Canal Zone (U. S. Navy) | 18 | 1 | 100 |

The operating power of each station shall be maintained as near as practicable to the authorized operating power and shall not exceed the limits of 5 per cent above and 10 per cent below the authorized power except in emergencies.

(C) TV Broadcast

The carrier frequency of the visual transmitter shall be maintained within $\pm 1,000$ cycles of the authorized carrier frequency.

The center frequency of the aural transmitter shall be maintained 4.5 megacycles $\pm 1,000$ cycles above the visual carrier frequency.

The peak power shall be monitored by a peak-reading device which reads proportionally to voltages, current, or power in the radio-frequency line. The operating power as so monitored shall be maintained as near as practicable to the authorized operating power and shall not exceed the limits of 10 per cent above and 20 per cent below the authorized power except in emergencies.

The operating power of the aural transmitter shall be maintained as near as practicable to the authorized operating power, and shall not exceed the limits of 10 per cent above and 20 per cent below the authorized power except in emergencies.

(D) Industrial Radio Service

The carrier frequency of stations operating below 220 megacycles in the Industrial Radio Service shall be maintained within $\pm 0.01\%$ of the authorized power for stations of 3 watts or less, and $\pm 0.005\%$ for stations with an authorized power of more than 3 watts. The frequency tolerance of Industrial Radio Service stations operating between 220 and 1,000 megacycles is specified in the station authorization.

(E) Citizens-Band Radio

The maximum plate power input to the anode (plate) circuit of the electron tube or tubes which supply energy to the radiating system of a station in this service shall not exceed the values given in Table X.

Table X. Power Limits of Citizens-Band Stations

| Class of Station | Maximum Plate Power Input (Watts) |
|------------------|-----------------------------------|
| A | 60 |
| B | 5 |
| C | 5* |
| D | 5 |

* A maximum plate power input of 30 watts is permitted on 27.255 mc only.

The carrier frequency of a station in this service shall be maintained within the percentages of authorized frequency given in Table XI.

Table XI. Frequency Tolerances of Citizens-Band Stations

| Class | Maximum Authorized Plate Power Input (Watts) | Frequency Tolerance % | |
|-------|--|-----------------------|--------|
| | | Fixed and Base | Mobile |
| A | 3 or less | .001 | .005 |
| A | Over 3 | .001 | .001 |
| B | 3 or less | --- | .5 |
| B | Over 3 | --- | .3 |
| C | 5 or less* | --- | .005 |
| C | Over 5 (27.255 mc only) | --- | .005 |
| D | 5 or less | --- | .005 |

* Class-C stations which have a plate power input of 3 watts or less and are used solely for remote control of objects or devices by radio (other than devices used solely as a means of attracting attention) are permitted a frequency tolerance of 0.01%.

32. COMMERCIAL OPERATOR LICENSES

The classes of commercial radio operator licenses issued by the Federal Communications Commission are classified basically as radiotelegraph and radiotelephone licenses.

(A) Examination Elements

Written examinations are composed of questions from various categories called elements. These elements, and the types of questions in each, are:

- Element 1.** *Basic Law.* Provisions of laws, treaties, and regulations with which every operator should be familiar.
- Element 2.** *Basic Operating Practice.* Radio operating procedures and practices generally followed or required in communicating by means of radiotelephone stations.
- Element 3.** *Basic Radiotelephone.* Technical, legal, and other matters applicable to the operation of radiotelephone stations other than broadcast.
- Element 4.** *Advanced Radiotelephone.* Advanced technical, legal, and other matters particularly applicable to the operation of the various classes of broadcast stations.
- Element 5.** *Radiotelegraph Operating Practice.* Radio operating procedure and practices generally followed or required in communicating by means of radiotelegraph stations primarily other than in the maritime mobile services of public correspondences.
- Element 6.** *Advanced Radiotelegraph.* Technical, legal, and other matters applicable to the operation of all classes of radiotelegraph stations, including operating procedures and practices in the maritime mobile services of public correspondences, and associated matters such as radionavigational aids, message traffic routing and accounting, etc.
- Element 7.** *Aircraft Radiotelegraph.* Basic theory and practice in the operation of radiocommunications and radionavigational systems aboard aircraft.
- Element 8.** *Ship Radar Techniques.* Specialized theory and practice applicable to the proper installation, servicing, and maintenance of ship radar equipment in general use for marine navigational purposes.

(B) Examination Requirements

Applicants for licenses must be able to transmit and receive spoken messages in English, and be able to pass the examination elements required for the license. The requirements for the various licenses are:

1. *Radiotelephone second-class operator licenses*. Written examination elements 1, 2, and 3.
2. *Radiotelephone first-class operator licenses*. Written examination elements 1, 2, 3, and 4.
3. *Radiotelegraph second-class operator license*. Transmitting and receiving code test of 16 code groups per minute. Written examination elements 1, 2, 5, and 6.
4. *Radiotelegraph first-class operator license*. Transmitting and receiving code test of 25 words per minute in conversational language and 20 groups per minute in code. Written examination elements 1, 2, 5, and 6.
5. *Radiotelephone third-class operator permit*. Written examination elements 1 and 2.
6. *Radiotelegraph third-class operator permit*. Transmitting and receiving code test of 16 code groups per minute. Written examination elements 1, 2, and 5.

33. AMATEUR OPERATOR PRIVILEGES

(A) Examination Elements

Examinations for amateur operator privileges are composed of questions from various categories, called elements. The various elements and their requirements are:

- Element 1(A):** *Beginner's Code Test*. Code test at 5 words per minute.
- Element 1(B):** *General Code Test*. Code test at 13 words per minute.
- Element 1(C):** *Expert's Code Test*. Code test at 20 words per minute.
- Element 2:** *Basic Amateur Practice*. Amateur radio operation and apparatus, including radiotelephone and radiotelegraph.
- Element 3(A):** *Basic Law*. Rules and regulations essential to beginners' operation, including sufficient elementary radio theory to understand these rules.
- Element 3(B):** *General Regulations*. Provisions of treaties, statutes, and rules and regulations affecting all amateur stations and operators.
- Element 4(B):** *Advanced Amateur Practice*. Advanced radio theory and operation applicable to mod-

ern amateur techniques, including—but not limited to—radiotelephony, radiotelegraphy, and transmission of energy for (1) measurements and observations applied to propagation, (2) radio control of remote objects, and (3) similar experimental purposes.

(B) Examination Requirements

Applicants for original licenses will be required to pass examinations as follows:

1. *Amateur Extra Class*. Elements 1(C), 2, 3(B), and 4(B).
2. *General Class*. Elements 1(B), 2, and 3(B).
3. *Conditional Class*. Elements 1(B), 2, and 3(B).
4. *Technician Class*. Elements 1(A), 2, and 3(B).
5. *Novice Class*. Elements 1(A) and 3(A).

Note: Examinations for licenses (1) and (2) above must be given by an FCC examiner. The examinations for licenses (3), (4), and (5) are taken by mail, under the supervision of a volunteer examiner.

34. AMATEUR ("HAM") BANDS

The various bands of frequencies used by amateur radio operators ("hams") are usually referred to in meters instead of the actual frequencies. The number of meters approximates the wavelength at the band of frequencies being designated. The meter bands and their frequency limits are given in Table XII. (Note: Frequencies between 220 and 225 mc are sometimes referred to as $1\frac{1}{4}$ meters, and between 420 and 450 meters as $\frac{3}{4}$ meter.)

Table XII. "Ham" Bands

| Band | Frequency (mc) |
|-----------|----------------|
| 80 Meters | 3.5—4.0 |
| 40 Meters | 7.0—7.3 |
| 20 Meters | 14.0—14.35 |
| 15 Meters | 21.0—21.45 |
| 10 Meters | 28.0—29.7 |
| 6 Meters | 50—54 |
| 2 Meters | 144—148 |

Table XIII. Types of Emission

| Type of Modulation | Type of Transmission | Supplementary Characteristics | Symbol | |
|-----------------------------------|--|--|--------|-----|
| 1. Amplitude | Absence of any modulation | ----- | A0 | |
| | Telegraphy without the use of modulating audio frequency (on-off keying) | ----- | A1 | |
| | Telegraphy by the keying of a modulating audio frequency or frequencies or by the keying of the modulated emission (special case: an unkeyed modulated emission) | ----- | A2 | |
| | Telephony | Double sideband, full carrier | | A3 |
| | | Single sideband, reduced carrier | | A3a |
| | | Two independent sidebands, reduced carrier | | A3b |
| | Facsimile | ----- | A4 | |
| | Television | ----- | A5 | |
| | Composite transmissions, and cases not covered by the above | ----- | A9 | |
| Composite transmissions | Reduced carrier | | A9c | |
| 2. Frequency (or phase) modulated | Absence of any modulation | ----- | F0 | |
| | Telegraphy without the use of modulating audio frequency (frequency shift keying) | ----- | F1 | |

| | | | | |
|---------------------|---|--|----|-----|
| | Telegraphy by the keying of a modulating audio frequency or audio frequencies or by the keying of the modulated emission (special case: an unkeyed emission modulated by audio frequency) | ----- | F2 | |
| | Telephony | ----- | F3 | |
| | Facsimile | ----- | F4 | |
| | Television | ----- | F5 | |
| | Composite transmissions and cases not covered by the above | ----- | F9 | |
| 3. Pulsed emissions | Absence of any modulation carrying information | ----- | P0 | |
| | Telegraphy without the use of modulating audio frequency | ----- | P1 | |
| | Telegraphy by the keying of a modulating audio frequency or of the modulated pulse (special case: an unkeyed modulated pulse) | Audio frequency or frequencies modulating the pulse in amplitude | | P2d |
| | | Audio frequency or frequencies modulating the width of the pulse | | P2c |
| | | Audio frequency or frequencies modulating the phase (or position) of the pulse | | P2f |
| | Telephony | Amplitude-modulated pulse | | P3d |
| | | Width-modulated pulse | | P3e |
| | | Phase-(or position-) modulated pulse | | P3f |
| | Composite transmissions and cases not covered by the above | ----- | P9 | |

35. TYPES OF EMISSIONS .

Emissions are classified according to their modulation, type of transmission, and supplementary characteristics. These classifications are given in Table XIII on pages 72 and 73. When a full designation of the emissions—including bandwidth—is necessary, the symbols in Table XIII are prefixed by a number indicating the bandwidth in kilocycles. Below 10 kc, this number is given to two significant figures.

36. TELEVISION CHANNEL FREQUENCIES

The chart in Fig. 57 (page 75) lists the frequency limits of all television channels and the frequency of the picture and sound carriers of each channel.

37. TELEVISION SIGNAL STANDARDS

The signal standards for television broadcasting are given in Figs. 58A and B (pages 76 and 77). Note: The standards given here are for color transmission. For monochrome transmission, the standards are the same except the color burst signal is omitted. Also, for color the vertical and horizontal scanning frequencies are 59.94 and 15,734.264 cps, respectively; for monochrome they are 60 and 15,750 cps.

38. AUDIO-FREQUENCY SPECTRUM

The audio-frequency spectrum is generally accepted as extending from 15 cps to 20,000 cps. Fig. 60 (page 79) gives the frequencies for each tone of the standard keyboard, based on the current musical pitch of A = 440 cps. Fig. 59 (page 78) shows the frequency range of various musical instruments and of other sounds. The frequency range shown for each sound is the range needed for faithful reproduction, and includes the fundamental frequency and the necessary harmonic frequencies. The frequency range of the human ear, and the various broadcasting and recording media, are also included in Fig. 59.

39. RADIO-FREQUENCY SPECTRUM

(A) Frequency Classification

The radio-frequency spectrum from 3 kc to 3,000,000 mc is divided into the various bands (shown in Table XIV on page 78) for easier identification.

Television Channel Frequencies

| Channel No. | Freq. Limits | | | | | |
|-------------|--------------|-----|----------|-----------|----------|-----------|
| | | | P 543.25 | 542 | P 717.25 | 716 |
| | | | S 547.75 | 26 | S 721.75 | 55 |
| | 54 | | P 549.25 | 548 | P 723.25 | 722 |
| | | | S 553.75 | 27 | S 727.75 | 56 |
| P 55.25 | 2 | 60 | P 555.25 | 554 | P 729.25 | 728 |
| S 59.75 | | | S 559.75 | 28 | S 733.75 | 57 |
| P 61.25 | 3 | 66 | P 561.25 | 560 | P 735.25 | 734 |
| S 65.75 | | | S 565.75 | 29 | S 739.75 | 58 |
| P 67.25 | 4 | 72 | P 567.25 | 566 | P 741.25 | 740 |
| S 71.75 | | | S 571.75 | 30 | S 745.75 | 59 |
| | | 76 | P 573.25 | 572 | P 747.25 | 746 |
| | | | S 577.75 | 31 | S 751.75 | 60 |
| P 77.25 | 5 | 82 | P 579.25 | 578 | P 753.25 | 752 |
| S 81.75 | | | S 583.75 | 32 | S 757.75 | 61 |
| P 83.25 | 6 | 88 | P 585.25 | 584 | P 759.25 | 758 |
| S 87.75 | | | S 589.75 | 33 | S 763.75 | 62 |
| | | 174 | P 591.25 | 590 | P 765.25 | 764 |
| | | | S 595.75 | 34 | S 769.75 | 63 |
| P 175.25 | 7 | 180 | P 597.25 | 596 | P 771.25 | 770 |
| S 179.75 | | | S 601.75 | 35 | S 775.75 | 64 |
| P 181.25 | 8 | 186 | P 603.25 | 602 | P 777.25 | 776 |
| S 185.75 | | | S 607.75 | 36 | S 781.75 | 65 |
| P 187.25 | 9 | 192 | P 609.25 | 608 | P 783.25 | 782 |
| S 191.75 | | | S 613.75 | 37 | S 787.75 | 66 |
| P 193.25 | 10 | 198 | P 615.25 | 614 | P 789.25 | 788 |
| S 197.75 | | | S 619.75 | 38 | S 793.75 | 67 |
| P 199.25 | 11 | 204 | P 621.25 | 620 | P 795.25 | 794 |
| S 203.75 | | | S 625.75 | 39 | S 799.75 | 68 |
| P 205.25 | 12 | 210 | P 627.25 | 626 | P 801.25 | 800 |
| S 209.75 | | | S 631.75 | 40 | S 805.75 | 69 |
| P 211.25 | 13 | 216 | P 633.25 | 632 | P 807.25 | 806 |
| S 215.75 | | | S 637.75 | 41 | S 811.75 | 70 |
| | | 470 | P 639.25 | 638 | P 813.25 | 812 |
| | | | S 643.75 | 42 | S 817.75 | 71 |
| P 471.25 | 14 | 476 | P 645.25 | 644 | P 819.25 | 818 |
| S 475.75 | | | S 649.75 | 43 | S 823.75 | 72 |
| P 477.25 | 15 | 482 | P 651.25 | 650 | P 825.25 | 824 |
| S 481.75 | | | S 655.75 | 44 | S 829.75 | 73 |
| P 483.25 | 16 | 488 | P 657.25 | 656 | P 831.25 | 830 |
| S 487.75 | | | S 661.75 | 45 | S 835.75 | 74 |
| P 489.25 | 17 | 494 | P 663.25 | 662 | P 837.25 | 836 |
| S 493.75 | | | S 667.75 | 46 | S 841.75 | 75 |
| P 495.25 | 18 | 500 | P 669.25 | 668 | P 843.25 | 842 |
| S 499.75 | | | S 673.75 | 47 | S 847.75 | 76 |
| P 501.25 | 19 | 506 | P 675.25 | 674 | P 849.25 | 848 |
| S 505.75 | | | S 679.75 | 48 | S 853.75 | 77 |
| P 507.25 | 20 | 512 | P 681.25 | 680 | P 855.25 | 854 |
| S 511.75 | | | S 685.75 | 49 | S 859.75 | 78 |
| P 513.25 | 21 | 518 | P 687.25 | 686 | P 861.25 | 860 |
| S 517.75 | | | S 691.75 | 50 | S 865.75 | 79 |
| P 519.25 | 22 | 524 | P 693.25 | 692 | P 867.25 | 866 |
| S 523.75 | | | S 697.75 | 51 | S 871.75 | 80 |
| P 525.25 | 23 | 530 | P 699.25 | 698 | P 873.25 | 872 |
| S 529.75 | | | S 703.75 | 52 | S 877.75 | 81 |
| P 531.25 | 24 | 536 | P 705.25 | 704 | P 879.25 | 878 |
| S 535.75 | | | S 709.75 | 53 | S 883.75 | 82 |
| P 537.25 | 25 | 542 | P 711.25 | 710 | P 885.25 | 884 |
| S 541.75 | | | S 715.75 | 54 | S 889.75 | 83 |
| | | | | 716 | | 890 |

P = Picture Carrier Freq.

S = Sound Carrier Freq.

All frequencies in mc.

Fig. 57

Television Signal Standards

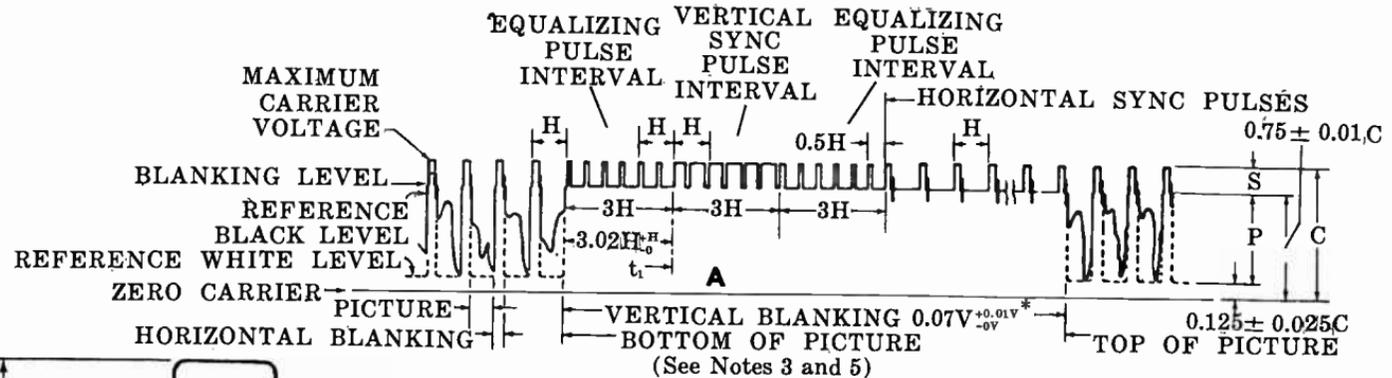
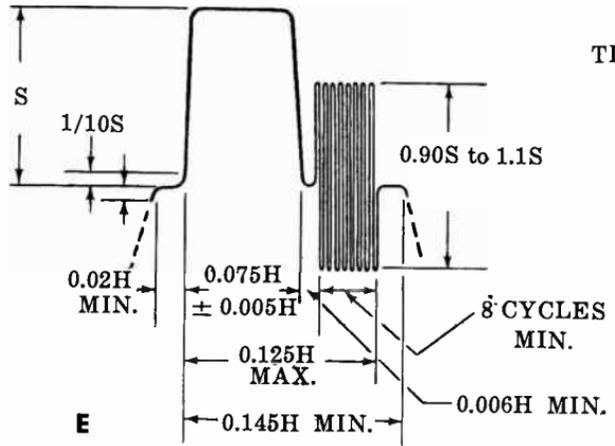
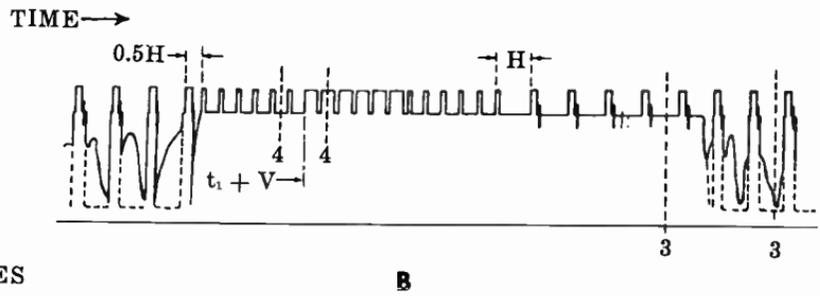


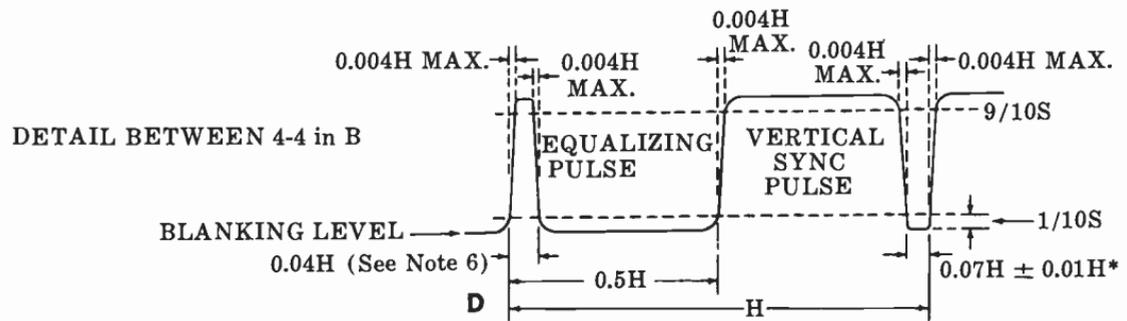
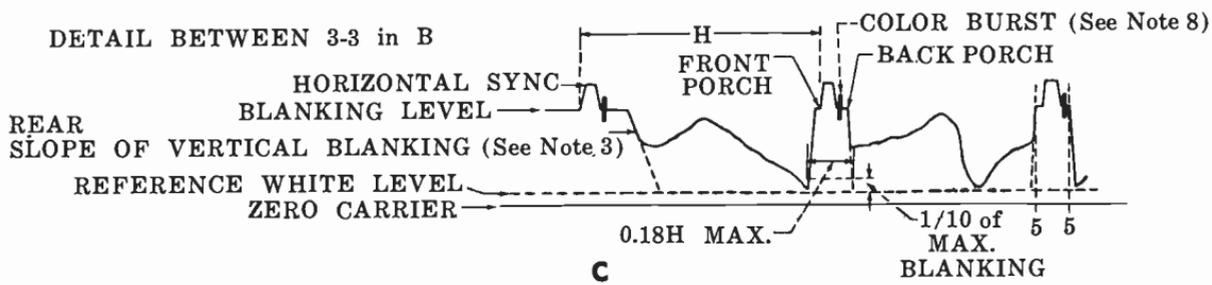
Fig. 58A



DETAIL BETWEEN 5-5 in C



Horizontal Dimensions Not to Scale in A, B, and C



NOTES

1. H = Time from start of one line to start of next line.
2. V = Time from start of one field to start of next field.
3. Leading and trailing edges of vertical blanking should be complete in less than 0.1H.
4. Leading and trailing slopes of horizontal blanking must be steep enough to preserve minimum and maximum values of (x + y) and (z) under all conditions of picture content.
5. Dimensions marked with asterisk indicate that tolerances given are permitted only for long time variations and not for successive cycles.
6. Equalizing pulse area shall be between 0.45 and 0.5 of area of a horizontal sync pulse.
7. Color burst follows each horizontal pulse, but is omitted following the equalizing pulses and during the broad vertical pulses.
8. Color burst to be omitted during monochrome transmissions.
9. The burst frequency shall be 3.579545 mc. The tolerance on the frequency shall be ±0.0003% with a maximum rate of change of frequency not to exceed 1/10 cycle per second per second.
10. The horizontal scanning frequency shall be 2/455 times the burst frequency.
11. The dimensions specified for the burst determine the times of starting and stopping the burst but not its phase. The color burst consists of amplitude modulation of a continuous sine wave.
12. Dimension "P" represents the peak excursion of the luminance signal at blanking level but does not include the chrominance signal. Dimension "S" is the sync amplitude above blanking level. Dimension "C" is the peak carrier amplitude.

Fig. 58B

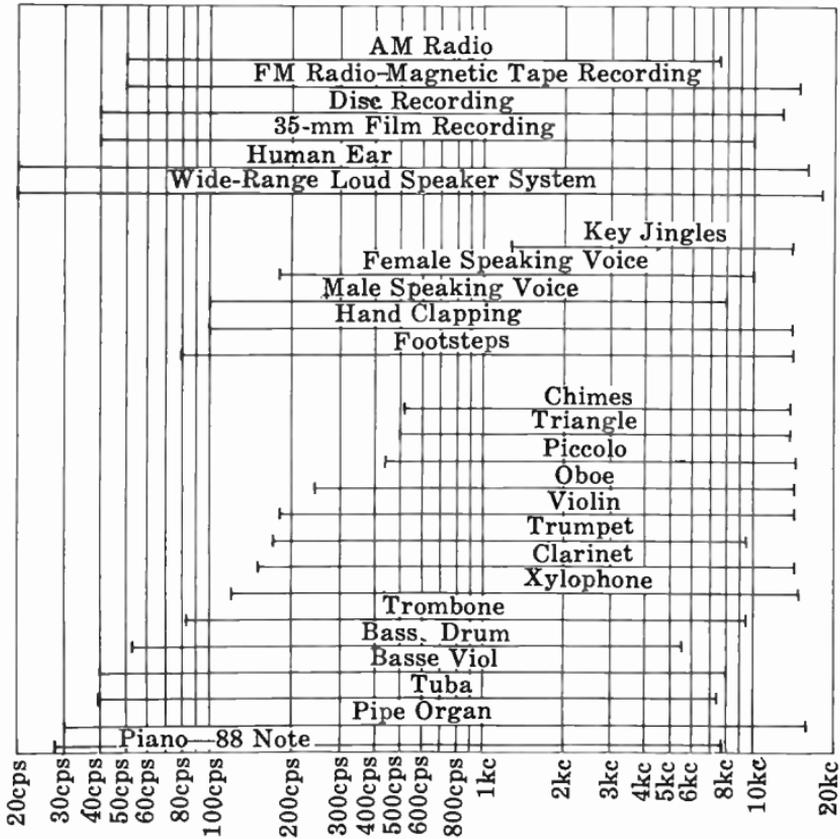


Fig. 59

Table XIV. Frequency Classification

| Frequency | Band No. | Classification | Abbreviation |
|----------------------|----------|----------------------------|--------------|
| 3–30 kc | 4 | Very low frequencies | VLF |
| 30–300 kc | 5 | Low frequencies | LF |
| 300–3000 kc | 6 | Medium frequencies | MF |
| 3–30 mc | 7 | High frequencies | HF |
| 30–300 mc | 8 | Very high frequencies | VHF |
| 300–3000 mc | 9 | Ultrahigh frequencies | UHF |
| 3000–30,000 mc | 10 | Super-high frequencies | SHF |
| 30,000–300,000 mc | 11 | Extremely high frequencies | EHF |
| 300,000–3,000,000 mc | 12 | — | — |

(B) FCC Allocations

The FCC allocations for the various services between 10 kc and 100,000 mc are given in Fig. 61A and B (located on the fold-out page between pages 180 and 181).

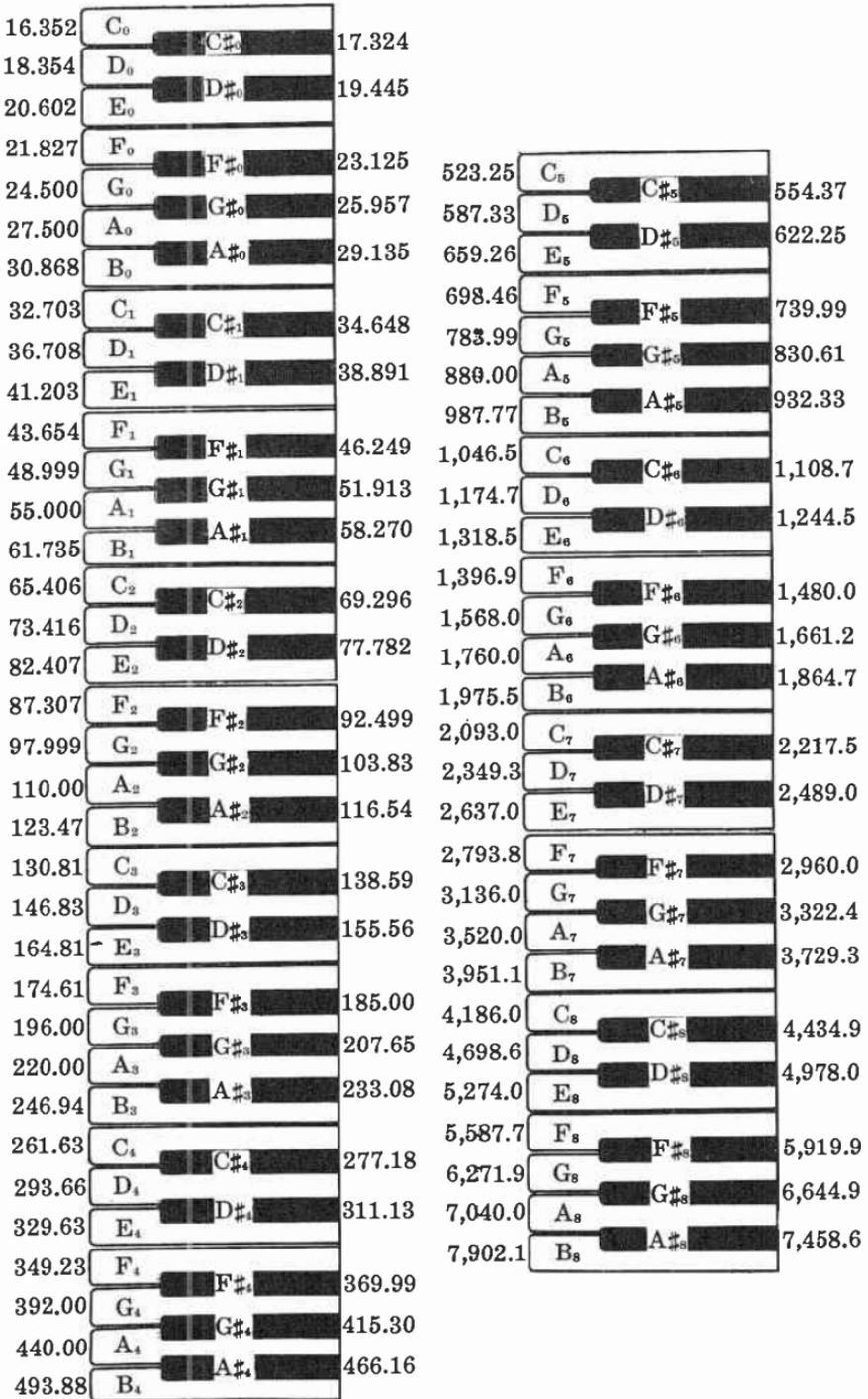


Fig. 60

Symbols and Codes

40. INTERNATIONAL Q SIGNALS

The international Q signals were first adopted to enable ships at sea to communicate with each other or to foreign shores without experiencing language difficulties. The signals consist of a series of three-letter groups starting with Q and having the same meaning in all languages. Today, Q signals serve as a convenient means of abbreviation in communications between amateurs. Each Q signal has both an affirmative and an interrogative meaning. The question is designated by the addition of the question mark after the Q signal. The most common Q signals are listed in Table XV.

Table XV. Q Signals

| Signal | Question | Answer or Advice |
|--------|--|---|
| QRG | Will you tell me my exact frequency? | Your exact frequency is . . . kc (or mc). |
| QRH | Does my frequency vary? | Your frequency varies. |
| QRK | What is the readability of my signals? | The readability of your signals is |
| QRM | Are you being interfered with? | I am being interfered with. |
| QRN | Are you troubled by static? | I am troubled by static. |
| QRO | Shall I increase power? | Increase power. |
| QRP | Shall I decrease power? | Decrease power. |
| QRQ | Shall I send faster? | Send faster. |
| QRS | Shall I send more slowly? | Send more slowly (. . . . words per minute). |
| QRT | Shall I stop sending? | Stop sending. |
| QRU | Have you anything for me? | I have nothing for you. |
| QRV | Are you ready? | I am ready. |
| QRX | When will you call again? | I will call you again at hours [on kc (or mc)]. |
| QSA | What is the strength of my signals? | The strength of your signals is |
| QSB | Are my signals fading? | Your signals are fading. |
| QSL | Can you acknowledge receipt? | I am acknowledging receipt. |
| QSM | Shall I repeat the last message I sent you? | Repeat the last message you have sent me. |
| QSO | Can you communicate with direct or by relay? | I can communicate with direct (or by relay through). |
| QSV | Shall I send a series of V's? | Send a series of V's. |
| QSY | Shall I change to transmission on another frequency? | Change to transmission on another frequency [or on kc (or mc)]. |
| QSZ | Shall I send each word or group twice? | Send each word or group twice. |
| QTH | What is your location? | My location is |

41. "10" SIGNALS

The abbreviations based on the number 10 plus a suffix was originally used for communication between police units. Now they are often used in other forms of two-way communications. The most common signals are given in Table XVI.

Table XVI. "10" Signals

| Signal | Meaning | Signal | Meaning |
|--------|--------------------------------|--------|--------------------------------------|
| 10-1 | Unable to copy | 10-27 | Operator on duty |
| 10-2 | Signal good | 10-30 | Does not conform to rules |
| 10-3 | Affirmative—granted—will do | 10-33 | Emergency traffic this station |
| 10-5 | Relay | 10-36 | Confidential information |
| 10-6 | Busy | 10-41 | Beginning tour of duty |
| 10-7 | Off the air | 10-42 | Ending tour of duty |
| 10-8 | On the air | 10-44 | Message received by all concerned |
| 10-9 | Repeat | 10-60 | What is next number? |
| 10-10 | On detail, but subject to call | 10-61 | CW traffic |
| 10-11 | Remain in service | 10-62 | Teletype traffic |
| 10-12 | Visitors or officials present | 10-63 | Any answer our number . . . |
| 10-13 | Weather and road conditions | 10-64 | Message for local delivery |
| 10-14 | Correct time | 10-65 | Net message assignment |
| 10-16 | Pick up (. . .) | 10-66 | Cancellation |
| 10-17 | Urgent—rush present detail | 10-67 | Clear for net message |
| 10-18 | Anything for us? | 10-68 | Dispatch information |
| 10-19 | Nothing for you | 10-88 | Advise present phone number of . . . |
| 10-20 | Location | 10-91 | Too weak; talk closer to mike |
| 10-21 | Call . . . by telephone | 10-92 | Too loud; talk farther from mike |
| 10-22 | Reporting in person to . . . | 10-93 | Frequency check |
| 10-23 | Arrived at scene | 10-94 | Give a test |
| 10-24 | Finished with last assignment | | |
| 10-25 | Disregard last information | | |

42. THE INTERNATIONAL CODE

| | | |
|-------------------------|--------------------------|-------------|
| A . . | M . . | Y |
| B | N . . | Z |
| C | O | 1 |
| D . . . | P | 2 |
| E . . | Q | 3 |
| F | R . . . | 4 |
| G . . . | S . . . | 5 |
| H | T . . | 6 |
| I . . | U . . . | 7 |
| J | V | 8 |
| K . . . | W . . . | 9 |
| L | X | 0 |
| Question Mark | Period | |
| Error | Comma | |
| Wait | End of Message | |

43. GREEK ALPHABET

The Greek alphabet is given in Table XVII. The items for which each letter is a symbol are also listed. The small Greek letter is the symbol for all the items listed unless a capital letter is indicated (cap).

Table XVII. Greek Alphabet

| Letter | | Name | Designates |
|------------|------------|---------|--|
| Small | Capital | | |
| α | A | Alpha | Angles, coefficients, attenuation constant, absorption factor, area. |
| β | B | Beta | Angles, coefficients, phase constant. |
| γ | Γ | Gamma | Specific quantity, angles, electrical conductivity, propagation constant, complex propagation constant (cap). |
| δ | Δ | Delta | Density, angles, increment or decrement (cap or small), determinant (cap), permittivity (cap). |
| ϵ | E | Epsilon | Dielectric constant, permittivity, base of natural (Napierian) logarithms, electric intensity. |
| ζ | Z | Zeta | Co-ordinate, coefficients. |
| η | H | Eta | Intrinsic impedance, efficiency, surface charge density, hysteresis, co-ordinates. |
| θ | Θ | Theta | Angular phase displacement, time constant, reluctance, angles. |
| ι | I | Iota | Unit vector. |
| κ | K | Kappa | Susceptibility, coupling coefficient. |
| λ | Λ | Lambda | Wavelength, attenuation constant, permeance (cap). |
| μ | M | Mu | Prefix <i>micro-</i> , permeability, amplification factor. |
| ν | N | Nu | Reluctivity, frequency. |
| ξ | Ξ | Xi | Co-ordinates. |
| \omicron | O | Omicron | — |
| π | Π | Pi | 3.1416 (circumference divided by diameter). |
| ρ | P | Rho | Resistivity, volume charge density, co-ordinates. |
| σ | Σ | Sigma | Surface charge density, complex propagation constant, electrical conductivity, leakage coefficient, sign of summation (cap). |
| τ | T | Tau | Time constant, volume resistivity, time-phase displacement, transmission factor, density. |
| υ | Υ | Upsilon | — |

Table XVII. Greek Alphabet—(Cont'd)

| Letter | | Name | Designates |
|----------|----------|-------|--|
| Small | Capital | | |
| ϕ | Φ | Phi | Magnetic flux, angles, scalar potential (cap). |
| χ | χ | Chi | Electric susceptibility, angles. |
| ψ | Ψ | Psi | Dielectric flux, phase difference, coordinates, angles. |
| ω | Ω | Omega | Angular velocity ($2\pi f$), resistance in ohms (cap), solid angles (cap). |

44. ELECTRONIC SYMBOLS AND ABBREVIATIONS*

A—Ammeter; ampere; area

a—Ampere

AC, a.c., a-c, ac—Alternating current

AF, a.f., a-f, af—Audio frequency

AFC, afc—Automatic frequency control

AGC, agc—Automatic gain control

AM, am—Amplitude modulation

Amp, amp., Amps, amps.—Ampere; amperes

Ant, ant.—Antenna

AVC, a.v.c., avc—Automatic volume control

B—Susceptance

b—Magnetic flux density

BC, bc—Broadcast

BFO, bfo—Beat-frequency oscillator

C—Capacitance; capacitor

°C—Degrees Celsius or centigrade

cm—Centimeter

cps—Cycles per second

CW, cw—Continuous wave

db—Decibels

DC, d.c., d-c, dc—Direct current

d.c.c., dcc—Double cotton-covered

DPDT, d.p.d.t., dpdt—Double-pole, double-throw

DPST, d.p.s.t., dpst—Double-pole, single-throw

d.s.c., dsc—Double silk-covered

E, e—Voltage

e.c., ec—Enamel-covered

EMF, emf—Electromotive force

ERP—Effective radiated power

F, f—Farad

f—Frequency

°F—Degrees Fahrenheit

FM, f.m., fm—Frequency modulation

G—Conductance

G_m, gm, g_m—Mutual conductance

GCT—Greenwich Civil Time

gnd—Ground

H, h—Henry

HF, h.f., h-f, hf—High frequency

hp—Horsepower

hy.—Henry

I—Current

IF, i.f., i-f, if—Intermediate frequency

ips—Inches per second

j—Joule; an imaginary number; an operator to rotate a vector quantity 90° counterclockwise

K— $\times 1000$; dielectric constant; a numerical value that does not change during a given period

k—Dielectric constant

KC, kc—Kilocycle

kv—Kilovolt

kva—Kilovolt ampere

KW, kw—Kilowatt

KWH, kwh—Kilowatt hour

L—Inductance; inductor

l—Length

LF, l.f., l-f, lf—Low frequency

M—Mutual inductance; $\times 1000$

m—Meter

ma—Milliamperes

* For Greek letters used as symbols (such as Ω , ω , and ψ), see the Greek alphabet in § 43.

| | |
|--|---|
| MC, Mc, mc —Megacycle | sec —Second; secondary |
| mcw —Modulated continuous wave | s.s.c., ssc —Single silk-covered |
| meg —Megohm | SHF; s.h.f., shf —Super-high frequencies |
| MF, m.f., m-f, mf —Medium frequency | SW, sw —Short wave |
| mf, mfd —Microfarad | t —Time |
| mh —Millihenry | T —Temperature |
| mm —Millimeter | trf —Tuned radio frequency |
| mmf, mmfd —Micromicrofarad | UHF, uhf —Ultrahigh frequencies |
| mv —Millivolt (sometimes microvolt) | V, v —Volt; voltmeter |
| mw —Milliwatt (sometimes microwatt) | VHF, vhf —Very high frequencies |
| NC —No connection | VOM, vom —Volt-ohm-milliammeter |
| OD —Outside diameter | VTVM, vtvm —Vacuum-tube voltmeter |
| P —Power | VU —Volume unit |
| pf —Power factor | W —Watt; work |
| p-p —Peak-to-peak | w —Watt |
| Q —Merit of a coil or capacitor; quantity of electricity | wh, whr —Watt-hour |
| R —Resistance; resistor | X —Reactance |
| RC, R-C —Product of resistance time capacitance; resistor-capacitor | X_c —Capacitive reactance |
| RF, r.f., r-f, rf —Radio frequency | X_L —Inductive reactance |
| RFC —Radio-frequency choke coil | Y —Admittance |
| rms —Root mean square | Z —Impedance |
| rpm —Revolutions per minute | μa —Microampere |
| s.c.c., scc —Single cotton-covered | μf —Microfarad |
| s.c.e., sce —Single cotton enamel | μh —Microhenry |
| | μμf —Micromicrofarad |
| | ∨ —Cycles per second |

45. SEMICONDUCTOR ABBREVIATIONS

The following symbols and abbreviations have been adopted as standard by the Electronic Industries Association (EIA) and the National Electrical Manufacturers Association (NEMA).

| | |
|--|---|
| B, b —Base electrode for units employing a single base | BV_{REO} —Breakdown voltage, emitter to base, collector open |
| b₁, b₂, etc. —Base electrodes for more than one base | BV_R —Breakdown voltage, reverse |
| BV_{CBO} —Breakdown voltage, collector to base, emitter open | C, c —Collector electrode |
| BV_{CEO} —Breakdown voltage, collector to emitter, base open | C_{ib} —Input capacitance (common base) |
| BV_{CEB} —Breakdown voltage, collector to emitter, with specified resistance between base and emitter | C_{ic} —Input capacitance (common collector) |
| BV_{CES} —Breakdown voltage, collector to emitter, with base short-circuited to emitter | C_{ie} —Input capacitance (common emitter) |
| | C_{ob} —Output capacitance (common base) |
| | C_{oc} —Output capacitance (common collector) |
| | C_{oe} —Output capacitance (common emitter) |
| | E, e —Emitter electrode |

- f_{hfb} —Small-signal, short-circuit, forward-current, transfer-ratio cutoff frequency (common base)
 f_{hfc} —Small-signal, short-circuit, forward-current, transfer-ratio cutoff frequency (common collector)
 f_{hfe} —Small-signal, short-circuit, forward-current, transfer-ratio cutoff frequency (common emitter)
 f_{max} —Maximum frequency of oscillation
 G_{pB} —Large-signal average power gain (common base)
 G_{pC} —Small-signal average power gain (common base)
 G_{pC} —Large-signal average power gain (common collector)
 G_{pC} —Small-signal average power gain (common collector)
 G_{pE} —Large-signal average power gain (common emitter)
 G_{pE} —Small-signal average power gain (common emitter)
 h_{FB} —Static value of the forward-current transfer ratio (common base)
 h_{fb} —Small-signal, short-circuit, forward-current transfer ratio (common base)
 h_{FC} —Static value of the forward-current transfer ratio (common collector)
 h_{fc} —Small-signal, short-circuit, forward-current transfer ratio (common collector)
 h_{FE} —Static value of the forward-current transfer ratio (common emitter)
 h_{fe} —Small-signal, short-circuit, forward-current transfer ratio (common emitter)
 h_{iB} —Static value of the input resistance (common base)
 h_{ib} —Small-signal value of short-circuit input impedance (common base)
 h_{iC} —Static value of the input resistance (common collector)
 h_{ic} —Small-signal value of short-circuit input impedance (common emitter)
 h_{iE} —Static value of the input resistance (common emitter)
 h_{ie} —Small-signal value of short-circuit input impedance (common emitter)
 $h_{i\epsilon}$ (real)—Real part of small-signal value of short-circuit input impedance (common emitter)
 h_{OB} —Static value of open-circuit output conductance (common base)
 h_{ob} —Small-signal value of open-circuit output admittance (common base)
 h_{OC} —Static value of open-circuit output conductance (common collector)
 h_{oc} —Small-signal value of open-circuit output admittance (common collector)
 h_{OE} —Static value of open-circuit output conductance (common emitter)
 h_{oe} —Small-signal value of open-circuit output admittance (common emitter)
 h_{rB} —Small-signal value of open-circuit, reverse-voltage transfer ratio (common base)
 h_{rc} —Small-signal value of open-circuit, reverse-voltage transfer ratio (common collector)
 h_{re} —Small-signal value of open-circuit, reverse-voltage transfer ratio (common emitter)
 I , i —Intrinsic region of a device (where neither holes nor electrons predominate)
 I_B —Base current (DC)
 I_b —Base current (rms)
 i_b —Base current (instantaneous)
 I_C —Collector current (DC)
 I_c —Collector current (rms)
 i_c —Collector current (instantaneous)
 I_{CBO} —Collector cutoff current (DC), emitter open
 I_{CEO} —Collector cutoff current (DC), base open
 I_{CER} —Collector cutoff current (DC), with specified resistance between base and emitter
 I_{CEX} —Collector current (DC), with specified circuit between base and emitter
 I_{CES} —Collector cutoff current (DC), with base short-circuited to emitter
 I_E —Emitter current (DC)
 I_e —Emitter current (rms)
 i_e —Emitter current (instantaneous)
 I_{EBO} —Emitter cutoff current (DC), collector open
 I_F —Forward current (DC)
 i_F —Forward current (instantaneous)
 I_O —Average output (rectified) current
 I_R —Reverse current (DC)

- i_R —Reverse current (instantaneous)
 K_θ —Thermal derating factor
 L_c —Conversion loss
 N, n —Region of a device where electrons are the majority carriers
 NF —Noise figure
 P, p —Region of a device where holes are the majority carriers
 P_{IB} —Total power input (DC or average) to the base electrode with respect to the emitter electrode
 P_{IE} —Total power input (instantaneous) to the base electrode with respect to the emitter electrode
 P_{CB} —Total power input (DC or average) to the collector electrode with respect to the base electrode
 P_{CE} —Total power input (instantaneous) to the collector electrode with respect to the base electrode
 P_{CE} —Total power input (DC or average) to the collector electrode with respect to the emitter electrode
 P_{CE} —Total power input (instantaneous) to the collector electrode with respect to the emitter electrode
 P_{EB} —Total power input (DC or average) to the emitter electrode with respect to the base electrode
 P_{EE} —Total power input (instantaneous) to the emitter electrode with respect to the base electrode
 P_{IB} —Large-signal input power (common base)
 P_{ib} —Small-signal input power (common base)
 P_{IC} —Large-signal input power (common collector)
 P_{ic} —Small-signal input power (common collector)
 P_{IE} —Large-signal input power (common emitter)
 P_{ie} —Small-signal input power (common emitter)
 P_{OB} —Large-signal output power (common base)
 P_{ob} —Small-signal output power (common base)
 P_{OC} —Large-signal output power (common collector)
- P_{oc} —Small-signal output power (common collector)
 P_{OE} —Large-signal output power (common emitter)
 P_{oe} —Small-signal output power (common emitter)
 P_T —Total power input (DC or average) to all electrodes
 p_T —Total power input (instantaneous) to all electrodes
 R_B —External base resistance
 R_C —External collector resistance
 $r_{CE}(\text{sat})$ —Collector-to-emitter saturation resistance
 R_E —External emitter resistance
 R_L —Load resistance
 T —Temperature
 T_A —Ambient temperature
 T_C —Case temperature
 t_d —Delay time
 t_f —Fall time
 t_{fr} —Forward recovery time
 T_J —Junction temperature
 T_{opr} —Operating temperature
 t_p —Pulse time
 t_r —Rise time
 t_{rr} —Reverse recovery time
 t_s —Storage time
 T_{stg} —Storage temperature
 t_w —Pulse average time
 θ —Thermal resistance
 θ_{J-A} —Thermal resistance, junction-to-ambient
 θ_{J-C} —Thermal resistance, junction-to-case
 V_{BB} —Base supply voltage (DC)
 V_{BC} —Base-to-collector voltage (DC)
 V_{bc} —Base-to-collector voltage (rms)
 v_{bc} —Base-to-collector voltage (instantaneous)
 V_{BE} —Base-to-emitter voltage (DC)
 V_{be} —Base-to-emitter voltage (rms)
 v_{be} —Base-to-emitter voltage (instantaneous)
 V_{CB} —Collector-to-base voltage (DC)
 V_{cb} —Collector-to-base voltage (rms)
 v_{cb} —Collector-to-base voltage (instantaneous)
 V_{CC} —Collector supply voltage (DC)
 V_{CE} —Collector-to-emitter voltage (DC)
 V_{ce} —Collector-to-emitter voltage (rms)

- V_{ce} —Collector-to-emitter voltage (instantaneous)
- $V_{CE(sat)}$ —Collector-to-emitter saturation voltage
- V_{EB} —Emitter-to-base voltage (DC)
- V_{eb} —Emitter-to-base voltage (rms)
- v_{eb} —Emitter-to-base voltage (instantaneous)
- V_{EC} —Emitter-to-collector voltage (DC)
- v_{ec} —Emitter-to-collector voltage (rms)
- v_{ec} —Emitter-to-collector voltage (instantaneous)
- V_{EE} —Emitter supply voltage (DC)
- V_F —Forward voltage (DC)
- v_F —Forward voltage (instantaneous)
- V_{CBP} —DC open-circuit voltage (floating potential) between collector and base, with emitter biased in reverse direction with respect to base
- V_{ECF} —DC open-circuit voltage (floating potential) between emitter and collector, with base biased in reverse direction with respect to collector
- V_{RT} —Reach-through voltage
- V_R —Reverse voltage (DC)
- v_R —Reverse voltage (instantaneous)

46. EIA TRANSFORMER COLOR CODE

The following diagrams illustrate the color code for transformers recommended by the EIA.

(A) Power Transformers

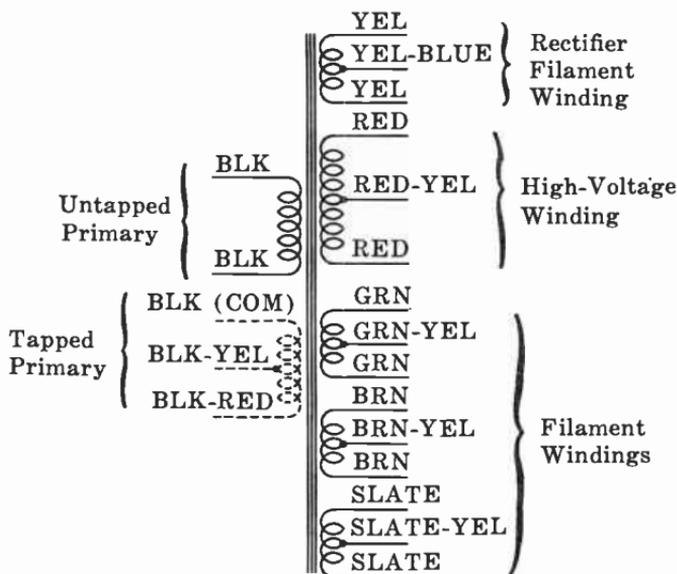


Fig. 62

(B) IF Transformers

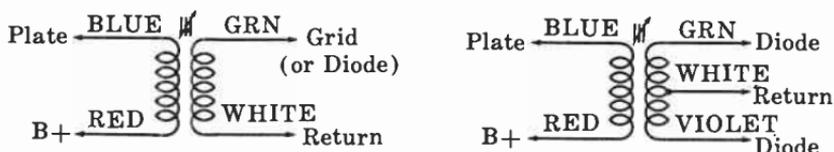


Fig. 63

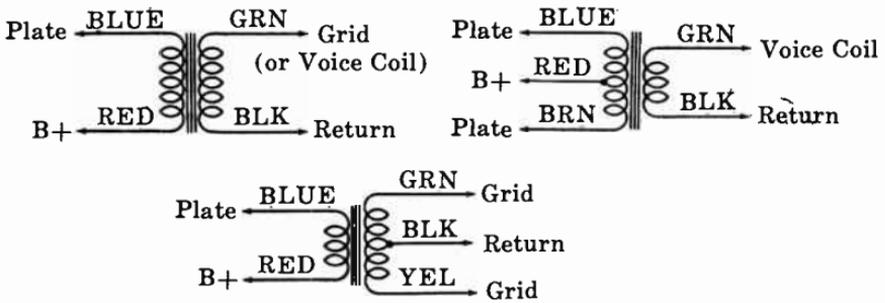
(C) Audio Output and Interstage Transformers

Fig. 64

47. RESISTOR AND CAPACITOR COLOR CODES

The present method and some of the older methods of color-coding resistors and capacitors are given in Figs. 65A and B (pages 89 and 90).

48. ELECTRONIC SCHEMATIC SYMBOLS

The most common schematic symbols are illustrated in Figs. 66A, B, C, and D (pages 91, 92, 93, and 94).

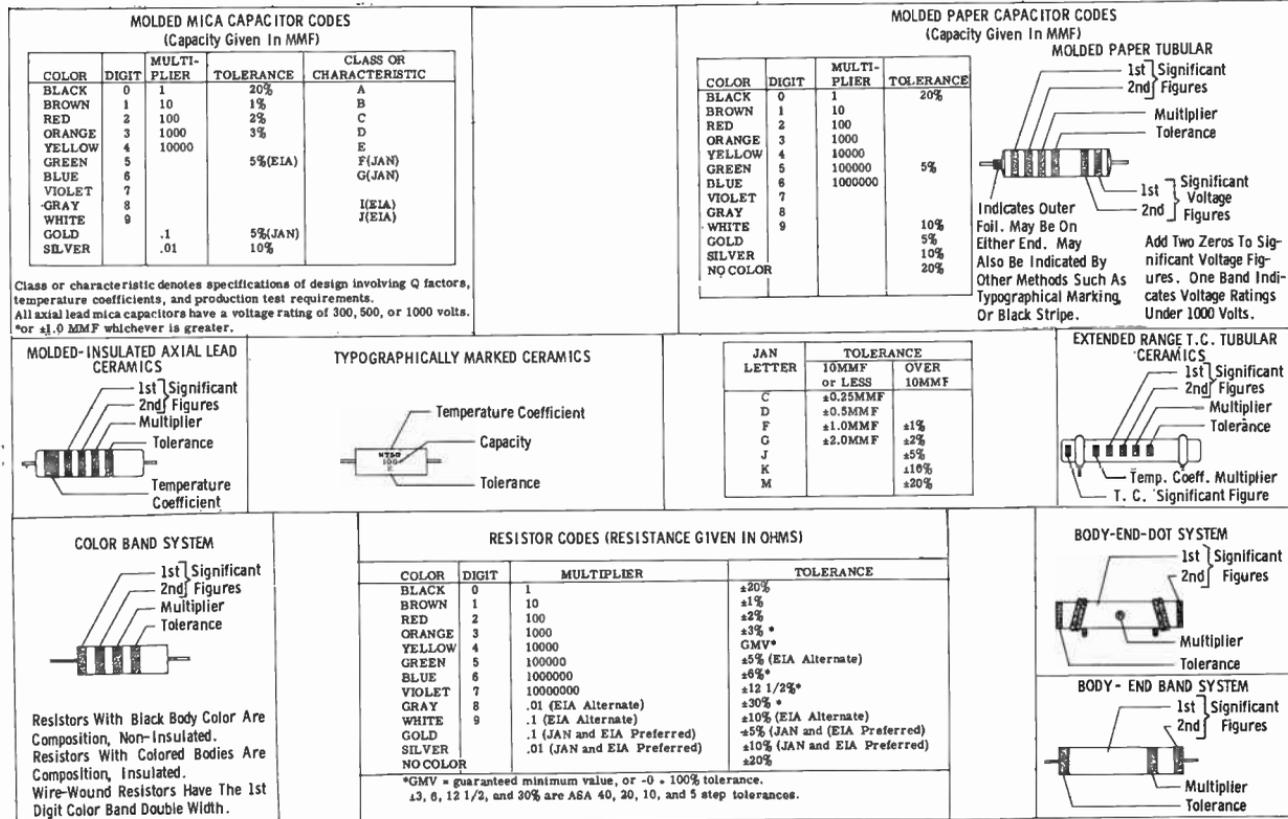


Fig. 65A

Resistor and Capacitor Color Codes—(Cont'd)

| DISC CERAMICS (5-DOT SYSTEM) | | CERAMIC CAPACITOR CODES (CAPACITY GIVEN IN MMF) | | | | | | HIGH CAPACITY TUBULAR CERAMICS INSULATED OR NON-INSULATED | | |
|--|--|---|-------|---|-------------------------------|--|--|--|--------|--|
| | | COLOR | DIGIT | MULTI- PLIER | TOLERANCE 10MMF or LESS | TOLERANCE OVER 10MMF | TEMPERATURE COEFFICIENT PPM/°C | | | EXTENDED RANGE TEMP. COEFF. SIGNI- FICANT FIGURE |
| | | BLACK | 0 | 1 | ±2.0MMF | ±20% | 0(NPO) | 0.0 | -1 | |
| DISC CERAMICS (3-DOT SYSTEM) | | BROWN | 1 | 10 | ±0.1MMF | ±1% | -33(N033) | 1.0 | -10 | |
| | | RED | 2 | 100 | | ±2% | -75(N075) | 1.5 | -100 | |
| | | ORANGE | 3 | 1000 | | ±2.5% | -150(N150) | 2.2 | -1000 | |
| | | YELLOW | 4 | 10000 | | | -220(N220) | 3.3 | +1 | |
| | | GREEN | 5 | | ±0.5MMF | ±5% | -330(N330) | 4.7 | +10 | |
| | | BLUE | 6 | | | | -470(N470) | 7.5 | +100 | |
| | | VIOLET | 7 | | | | -750(N750) | | +1000 | |
| | | GRAY | 8 | .01 | ±0.25MMF | | +30(P030) | | +10000 | |
| | | WHITE | 9 | .1 | ±1.0MMF | ±10% | General Purpose Bypass & Coupling +100(P100) (Jan) | | | |
| | | SILVER | | | | | | | | |
| | | GOLD | | | | | | | | |
| | | | | Ceramic capacitor voltage ratings are standard 500 volts, for some manufacturers, 1000 volts for other manufacturers, unless otherwise specified. | | | | | | |
| CURRENT STANDARD JAN AND EIA CODE | | BUTTON SILVER MICA | | MOLDED FLAT PAPER CAPACITORS (COMMERCIAL CODE) | | MOLDED FLAT PAPER CAPACITORS (JAN CODE) | | | | |
| MOLDED CERAMICS Using Standard Resistor Color-Code | | BUTTON CERAMICS | | STAND-OFF CERAMICS | | FEED-THRU CERAMICS | | | | |

Fig. 65B

Electronic Schematic Symbols

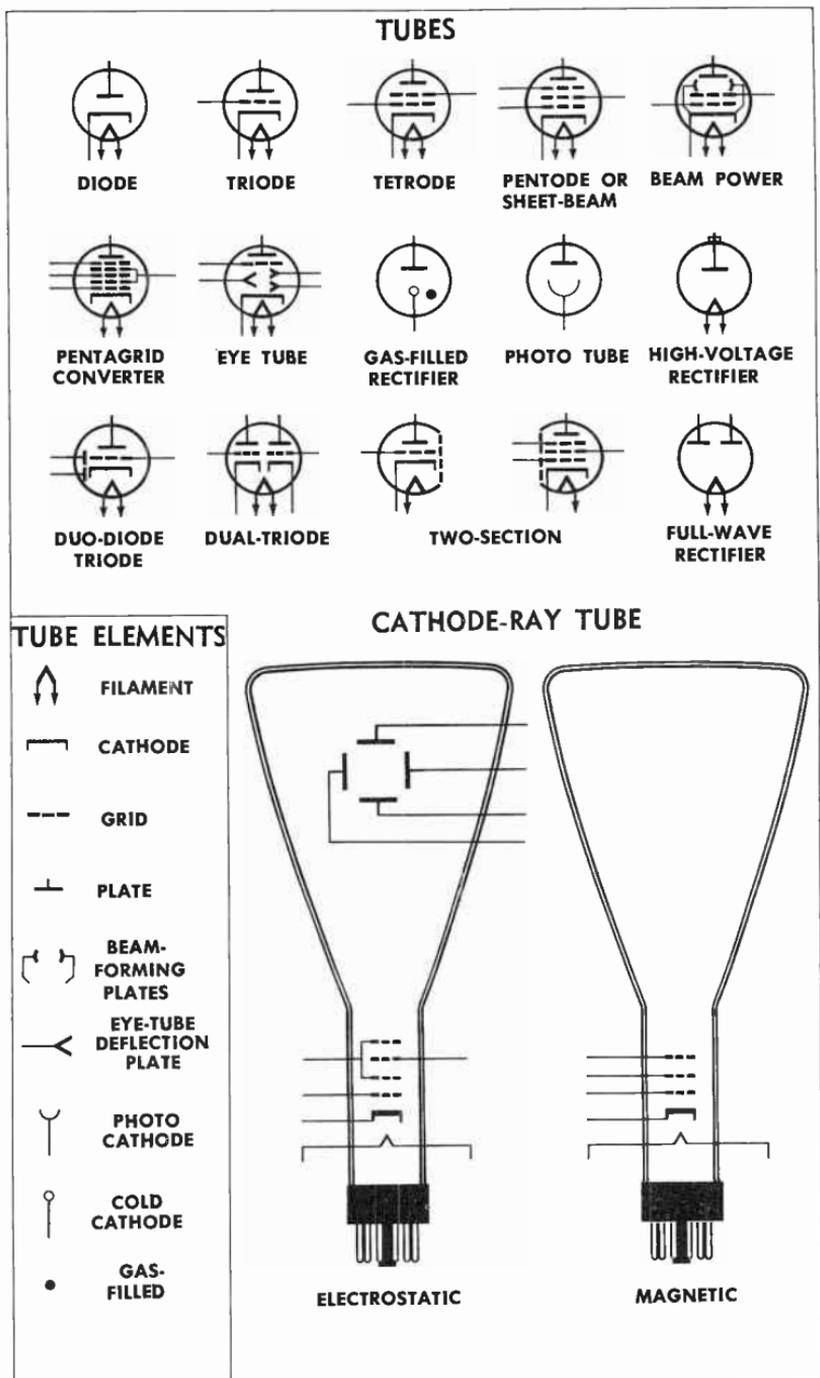


Fig. 66A

Electronic Schematic Symbols—(Cont'd)

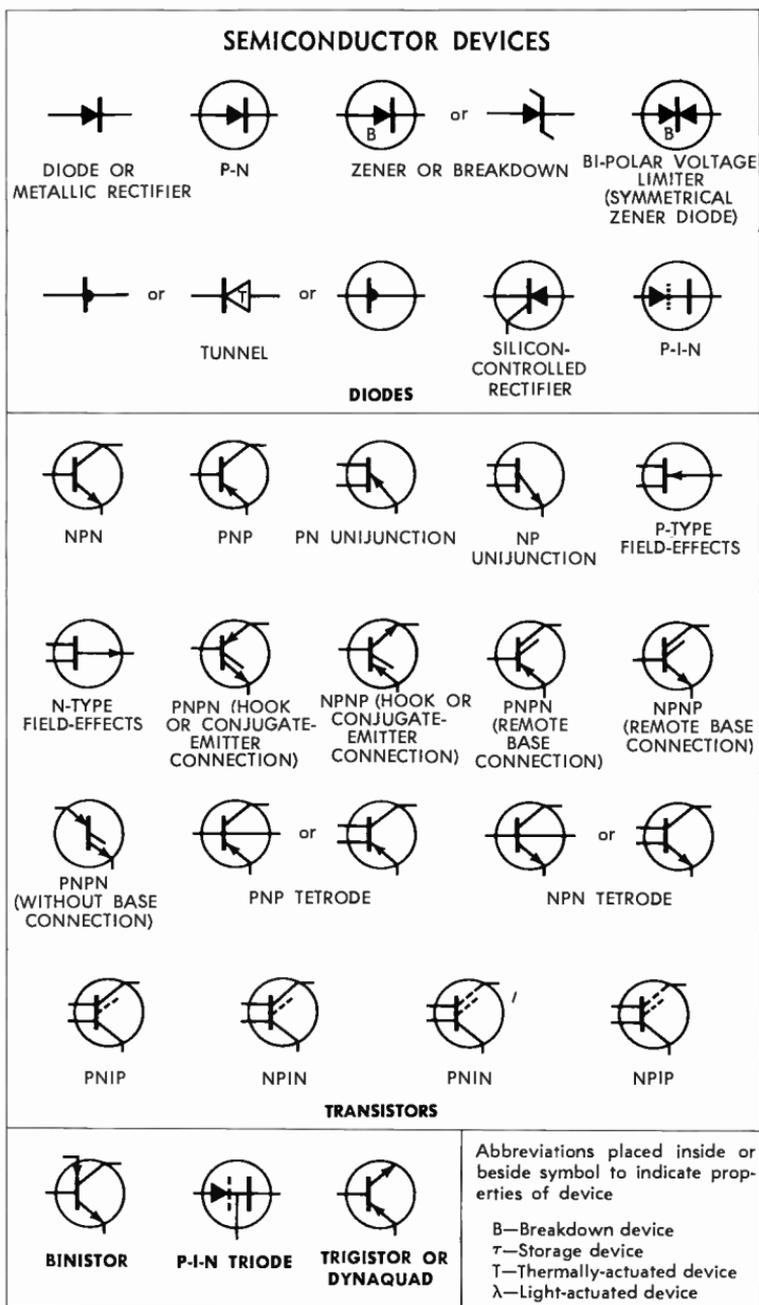


Fig. 66B

Electronic Schematic Symbols—(Cont'd)

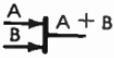
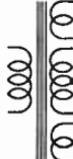
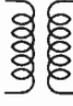
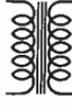
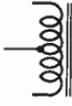
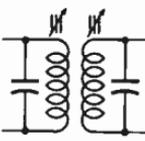
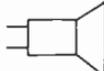
| | | |
|---|---|--|
| <p>COMPUTER SYMBOLS</p>  <p>AND GATE</p>  <p>OR GATE</p>  <p>NOT GATE</p> | | <p>BATTERIES</p>  <p>ONE-CELL</p>  <p>MULTICELL</p> |
| <p>PIEZOELECTRIC CRYSTALS</p>  <p>FREQUENCY DETERMINING</p>  <p>Monaural PHONO CARTRIDGES</p>  <p>Stereo PHONO CARTRIDGES</p> | <p>WIRING</p>  <p>WIRES CONNECTED</p>  <p>WIRES CROSSING</p> | <p>GROUNDS</p>   |
| <p>RESISTORS</p>  <p>FIXED</p>  <p>VARIABLE</p>  <p>TAPPED</p>  <p>TEMPERATURE COMPENSATING</p> | | |
| <p>CAPACITORS</p>  <p>FIXED</p>  <p>VARIABLE</p>  <p>Polarized ELECTROLYTICS</p>  <p>Non-polarized ELECTROLYTICS</p>  <p>SPARK PLATE</p> | | <p>LAMPS</p>  <p>FILAMENT</p>  <p>NEON</p> |
| <p>INDUCTORS</p>  <p>AIR CORE</p>  <p>POWDERED-IRON CORE</p>  <p>IRON CORE</p>  <p>VARIABLE CORE</p> | | <p>FUSES</p>   |
| <p>METERS</p>  <p>A—AMMETER</p>  <p>V—VOLTMETER</p>  <p>G—GALVANOMETER</p>  <p>MA—MILLIAMMETER</p>  <p>μA—MICROAMMETER</p> | | |
| <p>TRANSFORMERS</p>  <p>POWER</p>  <p>AIR CORE</p>  <p>IRON CORE</p>  <p>VARIABLE CORE</p>  <p>AUTO-TRANSFORMER</p>  <p>IF</p> | | |
| <p>SPEAKERS</p>  <p>GENERAL</p>  <p>PM</p>  <p>DYNAMIC</p>  <p>EM</p>  <p>ELECTRO-STATIC</p> | | <p>ELECTRO-STATIC TRANSDUCER</p>  |

Fig. 66C

Electronic Schematic Symbols—(Cont'd)

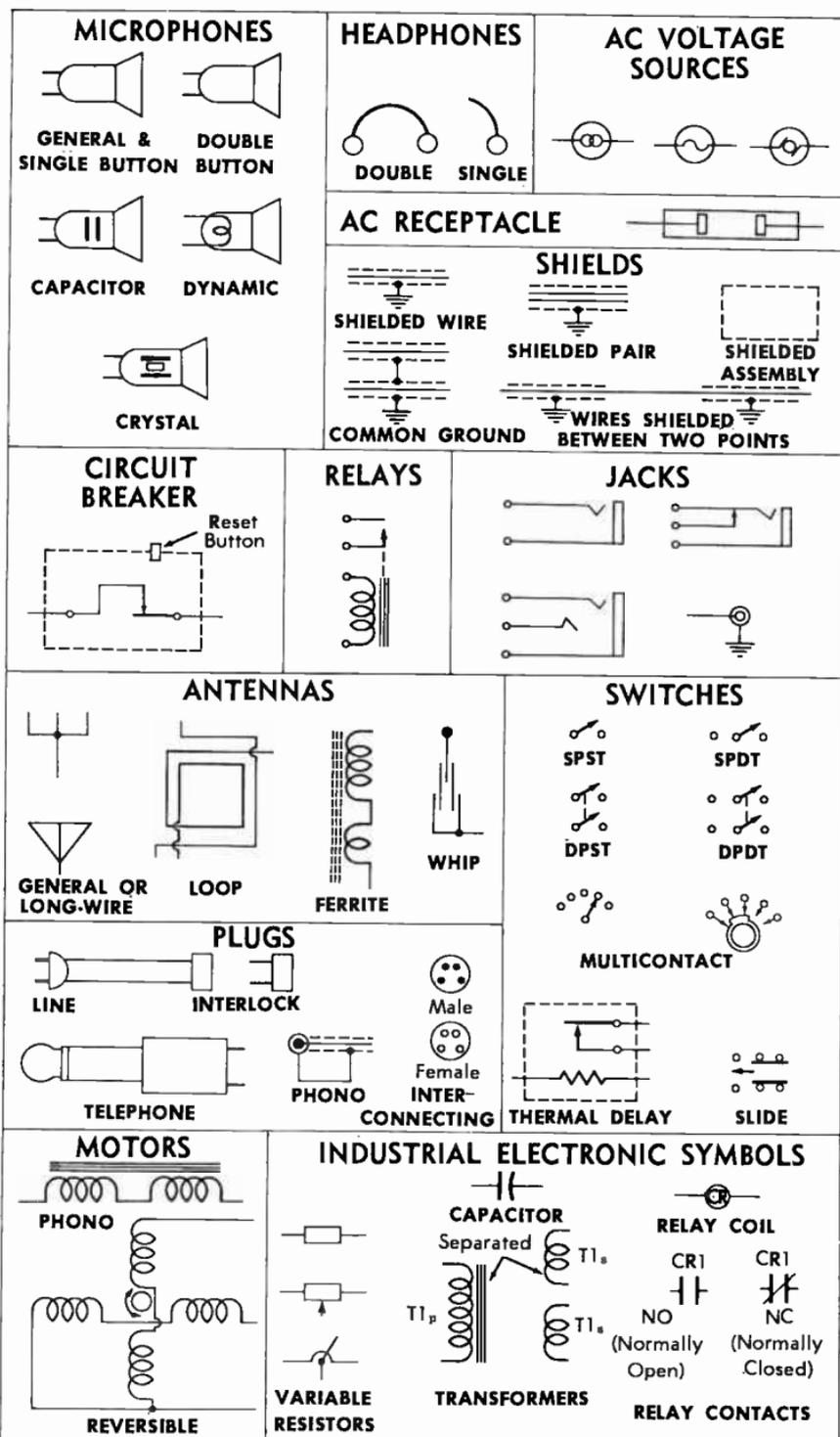


Fig. 66D

Service and Installation Data

49. COAXIAL CABLE CHARACTERISTICS

Table XVIII lists the most frequently-used coaxial cables. The electrical specifications include the impedance in ohms, capacitance in micromicrofarads per foot, attenuation in db per 100 feet, and the outside diameter. (See page 43 for formulas.)

Table XVIII. Coaxial Cable Characteristics

| Type RG... /U | Imp. (ohms) | Cap. (mmf per ft.) | Diam. (inches) | Attenuation—db per 100 ft. | | | | | REMARKS |
|---------------------|----------------|--------------------------|-------------------|----------------------------|----------|-----------|-----------|------------|-------------------------------|
| | | | | 1 mc | 10 mc | 100 mc | 400 mc | 1000 mc | |
| 5 | 52.5 | 28.5 | .332 | .21 | .77 | 2.9 | 6.5 | 11.5 | Small, double braid |
| 5A | 50 | 29 | .328 | .16 | .66 | 2.4 | 5.25 | 8.8 | Small, low loss |
| 6 | 76 | 20 | .332 | .21 | .78 | 2.9 | 6.5 | 11.2 | IF & video |
| 8 | 52 | 29.5 | .405 | .16 | .55 | 2.0 | 4.5 | 8.5 | General purpose |
| 9 | 51 | 30 | .420 | .12 | .47 | 1.9 | 4.4 | 8.5 | General purpose |
| 9A | 51 | 30 | .420 | .16 | .59 | 2.3 | 5.2 | 8.6 | Stable attenuation |
| 11 | 75 | 20.5 | .405 | .18 | .62 | 2.2 | 4.7 | 8.2 | Community TV |
| 13 | 74 | 20.5 | .420 | .18 | .62 | 2.2 | 4.7 | 8.2 | IF |
| 14 | 52 | 29.5 | .545 | .10 | .38 | 1.5 | 3.5 | 6.0 | RF power |
| 16 | 52 | 29.5 | .630 | — | — | — | — | — | RF power |
| 17 | 52 | 29.5 | .870 | .06 | .24 | .95 | 2.4 | 4.4 | RF power |
| 19 | 52 | 29.5 | 1.120 | .04 | .17 | .68 | 1.28 | 3.5 | Low-loss RF |
| 21 | 53 | 29 | .332 | 1.4 | 4.4 | 14.0 | 29.0 | 46.0 | Attenuating cable |
| 22 | 95 | 16 | .405 | .41 | 1.3 | 4.3 | 8.8 | — | Twin conductors |
| 23 | 125 | 12 | .65 X .945 | — | .4 | 1.7 | — | — | Twin conductors (balanced) |
| 25 | 48 | 50 | .565 | — | — | — | — | — | Pulse |
| 26 | 48 | 50 | .525 | — | — | — | — | — | Pulse |
| 27 | 48 | 50 | .675 | — | — | — | — | — | Pulse |
| 28 | 48 | 50 | .805 | — | — | — | — | — | Pulse |
| 33 | 51 | 30 | .470 | — | — | — | — | — | Pulse |
| 34 | 71 | 21.5 | .625 | .065 | .29 | 1.3 | 3.3 | 6.0 | Flexible, medium |
| 35 | 71 | 21.5 | .945 | .064 | .22 | .85 | 2.3 | 4.2 | Low-loss video |
| 36 | 69 | 22 | 1.180 | — | — | — | — | — | — |
| 41 | 67.5 | 27 | .425 | — | — | — | — | — | Special twist |
| 54A | 58 | 26.5 | .250 | .18 | .74 | 3.1 | 6.7 | 11.5 | Flexible, small |

Table XVIII. Coaxial Cable Characteristics—(Cont'd)

| Type RG... /U | Imp. (ohms) | Cap. (mmf per ft.) | Diam. (inches) | Attenuation—db per 100 ft. | | | | | REMARKS |
|---------------------|----------------|--------------------------|-------------------|----------------------------|----------|-----------|-----------|------------|------------------------------|
| | | | | 1 mc | 10 mc | 100 mc | 400 mc | 1000 mc | |
| 55 | 53.5 | 28.5 | .206 | .36 | 1.3 | 4.8 | 10.4 | 17.0 | Flexible, small Pulse |
| 56 | — | — | .535 | — | — | — | — | — | |
| 57 | 95 | 17 | .625 | .18 | .71 | 3.0 | 7.3 | 13.0 | Twin conductors |
| 58 | 53.5 | 30 | .195 | .38 | 1.4 | 5.2 | 11.2 | 20.0 | General purpose |
| 58A | 50 | 30 | .195 | .42 | 1.6 | 6.2 | 14.0 | 24.0 | Test leads |
| 59 | 73 | 21 | .242 | .30 | 1.1 | 3.8 | 8.5 | 14.0 | TV lead-in |
| 60 | 50 | — | .425 | — | — | — | — | — | Pulse cable |
| 61 | 500 | — | — | — | — | — | — | — | Special 500-ohm twin-lead |
| 62 | 93 | 13.5 | .242 | .25 | .83 | 2.7 | 5.6 | 9.0 | Low capacity, small |
| 63 | 125 | 10 | .405 | .19 | .61 | 2.0 | 4.0 | 6.3 | Low capacity |
| 64 | 48 | 50 | .495 | — | — | — | — | — | Pulse |
| 65 | 950 | 44 | .405 | — | — | — | — | — | Coaxial delay line |
| 71 | 93 | 13.5 | .250 | .25 | .83 | 2.7 | 5.6 | 9.0 | Low capacity, small |
| 77 | 48 | 50 | .415 | — | — | — | — | — | Pulse |
| 78 | 48 | 50 | .385 | — | — | — | — | — | Pulse |
| 87A | 50 | 29.5 | .425 | .13 | .52 | 2.0 | 4.4 | 7.6 | Teflon dielectric |
| 88 | 48 | 50 | .490 | — | — | — | — | — | Pulse |
| 101 | 75 | — | .588 | — | — | — | — | — | — |
| 102 | 140 | — | 1.088 | — | — | — | — | — | — |
| 108 | 76 | 25 | .245 | — | — | — | — | — | Twin conductors |
| 114 | 185 | 6.5 | .405 | — | — | — | — | — | Extra flexible |
| 117 | 50 | 29 | .730 | .05 | .20 | .85 | 2.0 | 3.6 | Teflon & Fiberglas |
| 119 | 50 | 29 | .470 | — | — | — | — | — | Teflon & Fiberglas |
| 122 | 50 | 29.3 | .160 | .40 | 1.70 | 7.0 | 16.5 | 29.0 | — |
| 126 | 50 | 29 | .290 | 3.20 | 9.0 | 25.0 | 47.0 | 72.0 | Teflon & Fiberglas |
| 140 | 73 | 21 | .242 | .33 | 1.03 | 3.3 | 6.9 | 11.7 | Teflon & Fiberglas |
| 141 | 50 | 29 | .195 | .35 | 1.12 | 3.8 | 8.0 | 13.8 | Teflon & Fiberglas |
| 142 | 50 | 29 | .206 | .35 | 1.12 | 3.8 | 8.0 | 13.8 | Teflon & Fiberglas |
| 143 | 50 | 29 | .325 | .24 | .77 | 2.5 | 5.3 | 9.0 | Teflon & Fiberglas |
| 144 | 72 | 21 | .395 | .16 | .53 | 1.8 | 3.9 | 7.0 | Teflon & Fiberglas |
| 174 | 50 | 30 | .10 | — | — | — | 19.0 | — | Miniature coaxial |

50. TEST-PATTERN INTERPRETATION

The Indian Head test pattern in Fig. 67 is transmitted by many TV stations and is also used in the flying-spot scanner type of video pattern generators. In addition, many of the features of this pattern are incorporated in the individual test patterns of TV stations. The test pattern is a quick and accurate way of checking receiver adjustments and operating conditions.

In the following explanation, the significance of each point indicated by an arrow and letter on the test pattern is

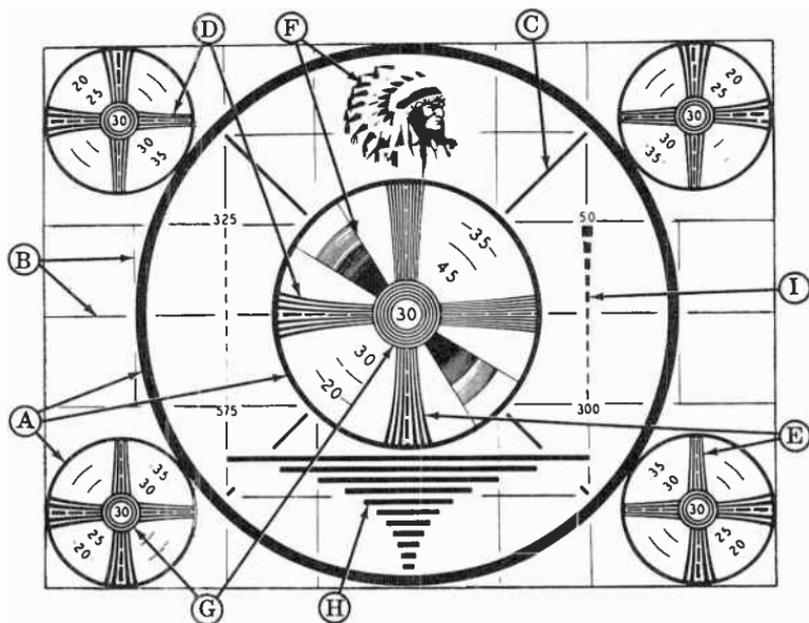


Fig. 67

explained. For example, the letter **A** indicates the circles at each corner and the two circles in the center of the pattern.

A. The six circles serve as a check for the adjustment of the Height, Width, Vertical Linearity, Horizontal Linearity, and Horizontal Drive controls and the ion-trap magnets, as well as the over-all operation of the vertical, horizontal, and power-supply circuits. All circles should be round and should not overlap the sides of the picture tube by more than three-fourths of an inch.

B. The eight squares along the horizontal axis and the six squares along the vertical axis indicate the standard aspect ratio of 4:3. These squares serve as a check for rectangular distortion caused by misadjusted or missing anti-pincushion magnets or by defects in the deflection yoke.

C. The four diagonal lines are used to check interlace. Poor interlace due to improper operation of the vertical-oscillator circuit will make the lines appear jagged.

D. The horizontal wedges located at each corner and in the center of the pattern serve as a check of the vertical resolution and interlace. Note the point where the horizontal lines are no longer clear and straight. The breaks in the

center line indicate 50-line intervals. That is, starting from the left (on the center and left-hand wedges), the first break indicates vertical resolution of 150 lines; the others, 200, 250, 300, and 350. The first break to the right of the center circles indicates 500 lines, then 450, 400, 350, and 300. The wedges at the top and bottom of the right side of the pattern give the same information except that the wedge is reversed. The numbers (20, 30, 35, and 45) between the vertical and horizontal wedges in each circle indicate these vertical resolution check points, with the last zero omitted.

E. The vertical wedges at each corner and at the center of the pattern indicate the horizontal resolution. Hence, they serve as a check on all video-amplifying circuits and alignment. Note the point where the vertical lines are no longer clear. Each break in the center line of the vertical wedge indicates 50 lines, as explained for D. The horizontal resolution can be converted to bandwidth by dividing the number of lines by 80. For example, if the lines are no longer clear at the 300-line point, the bandwidth equals 300 divided by 80, or 3.75 mc.

F. The two diagonal wedges and the Indian head indicate the contrast ratio. Therefore, they can be used to check the adjustment of the Contrast, Brightness, and AGC controls, as well as the video-amplifying and picture-tube circuits. When video-amplifier and picture-tube circuits are operating properly and the controls are properly adjusted, four degrees of shading should be observed, ranging from black at the center to light gray at the outermost point on the wedge.

G. The bull's-eyes at each corner and at the center of the pattern indicate receiver focus. Hence, they serve to check the adjustment of the focusing device or, if electromagnetic focusing is employed, of the low-voltage power supply.

H. The eleven horizontal bars represent half cycles of square-wave signals, and are used to check the low-frequency response or phase shift of the receiver. The bars, from top to bottom, represent the following video signals: 19 kc, 28 kc, 38 kc, 56 kc, 75 kc, 113 kc, 150 kc, 225 kc, 300 kc, 450 kc, and 600 kc. If the low-frequency response is satisfactory, the bars will be sharply defined. However, if the receiver has poor low-frequency response due to a defect in the video-amplifier circuit or misadjustment of the Fine

Tuning, Contrast, or AGC controls, the bars will have trailing black or white edges.

1. The single resolution lines at each side of the center circle represent the width of a single line ranging from 50 to 575 lines, in steps of 25. These lines are used to check for ringing in the video amplifier at frequencies from approximately 600 kc to 7 mc. When ringing occurs at any frequency, the resolution line corresponding to that frequency will be repeated several times at evenly spaced intervals. To convert the resolution lines to the frequency, divide the number of lines by 80, as explained in the foregoing for E.

51. CLASSES OF VACUUM-TUBE OPERATION

Class-A amplifiers are biased so that the AC input signal is on the linear portion of their characteristic curve, as shown in Fig. 68.

The output signal is a faithful reproduction of the input signal. Plate current flows at all times in a Class-A amplifier. Class-A amplifiers are used in audio or other applications where distortion cannot be tolerated. Their efficiency is around 20 to 25%.

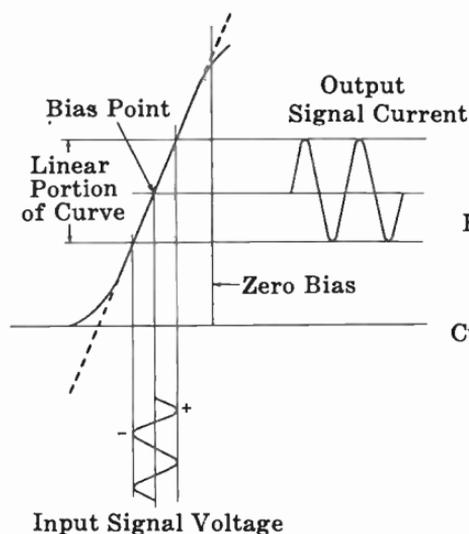


Fig. 68

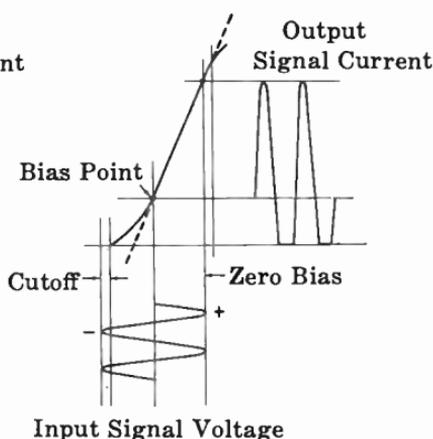


Fig. 69

Class-AB amplifiers are biased as shown in Fig. 69. Here, plate current will flow more than one half but less than a full cycle. Higher plate voltages and currents can be employed than for Class-A amplifiers because the increased negative grid bias will hold the plate current within the plate-dissipation rating. For this reason, more power output can be obtained from Class-AB operation. Class-AB amplifiers may be operated either single-ended or in push-pull.

Class-AB amplifiers are subdivided into two classes, AB_1 and AB_2 . In a Class- AB_1 amplifier, no grid current will flow.

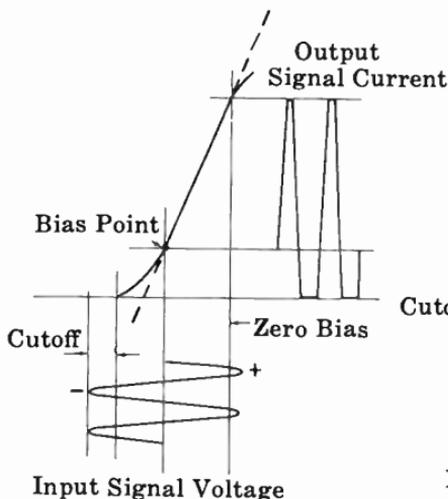


Fig. 70

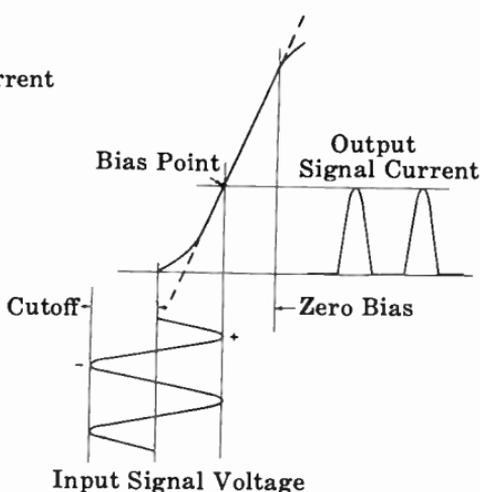


Fig. 71

That is, the peak signal voltage applied to each grid is never greater than the negative grid bias; therefore, the grid is never driven positive. In a Class- AB_2 amplifier, grid current will flow because the peak signal is greater than the negative grid bias and the grid is driven positive during a portion of the cycle, as shown in Fig. 70. The efficiency of Class-AB amplifiers varies from 40 to 75%, depending on the bias voltage.

Class-B amplifiers are biased at or near cutoff, as shown in Fig. 71. When an exciting grid voltage is applied, plate current is near zero; therefore, it will flow only during approximately half of a cycle. Because plate current flows for only one half the cycle, Class-B amplifiers must be operated in push-pull. More power can be obtained from Class-B amplifiers than from Class-A or Class-AB amplifiers without

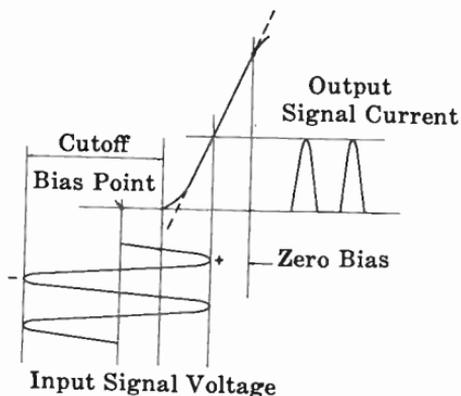


Fig. 72

excessive plate dissipation. The efficiency of Class-B amplifiers is around 40 to 60%.

Class-C amplifiers are biased below cutoff, as shown in Fig. 72. Therefore, plate current flows for less than half of a cycle. More power can be obtained from Class-C than Class-B amplifiers. Usually, Class-C amplifiers are used in a selective-tuned circuit, such as those employed in RF amplifiers. The high distortion, characteristic of Class-C amplifiers, is overcome by the flywheel effect of the tuned circuits. The efficiency of Class-C amplifiers is around 50 to 80%.

52. MINIATURE LAMP DATA

Table XIX (page 102) lists the most common miniature lamps and their characteristics. The outline drawings for each lamp are given in Fig. 73 below.

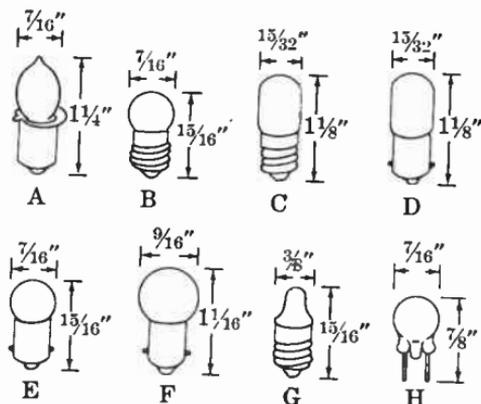


Fig. 73

Table XIX. Miniature Lamp Data

| Lamp No. | Volts | Amps | Bead Color | Base | Bulb Type | Fig. No. |
|----------|-------|-------|------------|---------|-----------|----------|
| PR2 | 2.4 | 0.50 | Blue | Flange | B-3½ | A |
| PR3 | 3.6 | 0.50 | Green | Flange | B-3½ | A |
| PR4 | 2.3 | 0.27 | Yellow | Flange | B-3½ | A |
| PR6 | 2.5 | 0.30 | Brown | Flange | B-3½ | A |
| PR12 | 5.95 | 0.50 | White | Flange | B-3½ | A |
| 12 | 6.3 | 0.15 | — — — | 2-Pin | G-3½ | H |
| 13 | 3.8 | 0.30 | Green | Screw | G-3½ | B |
| 14 | 2.5 | 0.30 | Blue | Screw | G-3½ | B |
| 40 | 6.3 | 0.15 | Brown | Screw | T-3¼ | C |
| 41 | 2.5 | 0.50 | White | Screw | T-3¼ | C |
| 42 | 3.2 | 0.35* | Green | Screw | T-3¼ | C |
| 43 | 2.5 | 0.50 | White | Bayonet | T-3¼ | D |
| 44 | 6.3 | 0.25 | Blue | Bayonet | T-3¼ | D |
| 45 | 3.2 | 0.35† | Green† | Bayonet | T-3¼ | D |
| 46 | 6.3 | 0.25 | Blue | Screw | T-3¼‡ | C |
| 47 | 6.3 | 0.15 | Brown | Bayonet | T-3¼ | D |
| 48 | 2.0 | 0.06 | Pink | Screw | T-3¼ | C |
| 49 | 2.0 | 0.06 | Pink | Bayonet | T-3¼ | D |
| 50 | 6.3 | 0.20 | White | Screw | G-3½ | B |
| 51 | 6.3 | 0.20 | White | Bayonet | G-3½ | E |
| 55 | 6.3 | 0.40 | White | Bayonet | G-4½ | F |
| 57 | 14.0 | 0.24 | White | Bayonet | G-4½ | F |
| 112 | 1.1 | 0.22 | Pink | Screw | TL-3 | G |
| 222 | 2.2 | 0.25 | White | Screw | TL-3 | G |
| 233 | 2.3 | 0.27 | Purple | Screw | G-3½ | B |
| 291 | 2.9 | 0.17 | White | Screw | T-3¼ | C |
| 292 | 2.9 | 0.17 | White | Screw | T-3¼ | C |
| 1490 | 3.2 | 0.16 | White | Bayonet | T-3¼ | D |
| 1891 | 14.0 | 0.23 | Pink | Bayonet | T-3¼ | D |
| 1892 | 14.0 | 0.12 | White | Screw | T-3¼ | C |

* Some brands are .50 amp.

† Some brands are .50 amp and white bead.

‡ Frosted.

53. GAS-FILLED LAMP DATA

The characteristics of the more common gas-filled lamps are given in Table XX. The value of external resistance needed for operation with circuit voltages from 110 to 600 volts is given in Table XXI.

Table XX. Gas-Filled Lamps

| Number | Hours of Average Useful Life* | Type Gas | Max. Length In inches | Base | Amps | Volts | Watts† |
|--------|-------------------------------|----------|-----------------------|-------------------------|--------|---------|--------|
| AR-1 | 3,000 | Argon | 3 1/2 | Medium Screw | 0.018 | 110-125 | 2 |
| AR-3 | 1,000 | Argon | 1 5/8 | Cand. Screw | 0.0035 | 110-125 | 1/4 |
| AR-4 | 1,000 | Argon | 1 1/2 | Double-Contact Bayonet | 0.0035 | 110-125 | 1/4 |
| NE-2 | Over 25,000 | Neon | 1 1/16‡ | Unbased | 0.003 | 110-125 | 1/25 |
| NE-2A | Over 25,000 | Neon | 27/32‡ | Unbased | 0.003 | 110-125 | 1/25 |
| NE-17 | 5,000 | Neon | 1 1/2 | Double-Contact Bayonet§ | 0.002 | 110-125 | 1/4 |
| NE-30 | 10,000 | Neon | 2 1/4 | Medium Screw§ | 0.012 | 110-125 | 1 |
| NE-32 | 10,000 | Neon | 2 1/16 | Double-Contact Bayonet§ | 0.012 | 110-125 | 1 |
| NE-34 | 8,000 | Neon | 3 1/2 | Medium Screw | 0.018 | 110-125 | 2 |
| NE-40 | 8,000 | Neon | 3 1/2 | Medium Screw§ | 0.030 | 110-125 | 3 |
| NE-45 | Over 7,500 | Neon | 1 5/8 | Cand. Screw | 0.002 | 110-125 | 1/4 |
| NE-48 | Over 7,500 | Neon | 1 1/2 | Double-Contact Bayonet | 0.002 | 110-125 | 1/4 |
| NE-51 | Over 15,000 | Neon | 1 3/16 | Miniature Bayonet | 0.0003 | 110-125 | 1/25 |
| NE-56 | 10,000 | Neon | 2 1/4 | Medium Screw§ | 0.005 | 220-250 | 1 |
| NE-57 | 5,000 | Neon | 1 5/8 | Cand. Screw§ | 0.002 | 110-125 | 1/4 |
| NE-58 | Over 7,500 | Neon | 1 5/8 | Cand. Screw | 0.002 | 220-250 | 1/2 |

* Life on DC is approximately 60% of AC values.

† For 110-125V operation.

‡ The dimension is for glass only.

§ On DC circuits the base should be negative.

Table XXI. External Resistances Needed For Gas-Filled Lamps

| Type | 110-125V | 220-300V | 300-375V | 375-450V | 450-600V |
|-------|------------------|----------|-----------|-----------|-----------|
| AR-1 | Included in Base | 10,000 | 18,000 | 24,000 | 30,000 |
| AR-3 | Included in Base | 68,000 | 91,000 | 150,000 | 160,000 |
| AR-4 | 15,000 | 82,000 | 100,000 | 160,000 | 180,000 |
| NE-2 | 200,000 | 750,000 | 1,000,000 | 1,200,000 | 1,600,000 |
| NE-2A | 200,000 | 750,000 | 1,000,000 | 1,200,000 | 1,600,000 |
| NE-17 | 30,000 | 110,000 | 150,000 | 180,000 | 240,000 |
| NE-30 | Included in Base | 10,000 | 20,000 | 24,000 | 36,000 |
| NE-32 | 7,500 | 18,000 | 27,000 | 33,000 | 43,000 |
| NE-34 | Included in Base | 9,100 | 13,000 | 16,000 | 22,000 |
| NE-40 | Included in Base | 6,200 | 8,200 | 11,000 | 16,000 |
| NE-45 | Included in Base | 82,000 | 120,000 | 150,000 | 200,000 |
| NE-48 | 30,000 | 110,000 | 150,000 | 180,000 | 240,000 |
| NE-51 | 200,000 | 750,000 | 1,000,000 | 1,200,000 | 1,600,000 |
| NE-56 | Included in Base | — | — | — | — |
| NE-57 | Included in Base | 82,000 | 120,000 | 150,000 | 200,000 |
| NE-58 | Included in Base | — | — | — | — |

54. LIGHT PROPERTIES OF COLOR TV

When we speak of light, we usually think of light coming from the sun or the light emitted from some artificial lighting source, such as electrical lighting. This light is referred to as direct light. Another type of light is indirect or reflected light, which is given off by an object when direct light strikes it. The difference between these two types of light is that the indirect light depends upon the direct light. When light is not shining upon an object, no light will be given off unless the object contains self-luminating properties.

White light is made up of different colors. This composition can be shown by passing light through a prism. The light spectrum is broken up into its constituent wavelengths, each representing a different color. The ability to disperse the light by a prism stems from the fact that light of shorter wavelengths travels slower through glass than does light of longer wavelengths. The spectrum ranges from violet on the lower end to red on the upper end. In between fall blue, green, yellow, and orange. A total of six distinct colors are visible when white light passes through a prism. Since the colors of the spectrum pass gradually from one to the other, the theoretical number of colors becomes infinite.

There are three color attributes used to describe any one color or to differentiate between several colors. These are (1) hue, (2) saturation, and (3) brightness. Hue is the quality used to identify any color under consideration, such as red, blue, or yellow. Saturation is a measure of the absence of dilution by white light, and can be expressed with such terms as rich, deep, vivid, or pure. Brightness defines the amount of light energy contained within a given color.

Color may be produced by either of two processes. When working with paint pigments, the subtractive process is employed. The other process of mixing colors is called the additive process. This process is used in color television. The colors in the additive process do not depend upon an incident light source. Self-luminous properties are characteristic of the additive colors. Phosphorescent signs which glow in the dark are good examples of this process. Cathode-ray tubes contain self-luminance properties; so it is only logical that the additive process would be employed in color television.

The three primaries for the additive process of color mixing are red, green, and blue. Two requirements for the primary colors are that each primary must be different and that the combination of any two primaries must not be capable of producing the third. Red, green, and blue were chosen for the additive primaries because they fulfilled these requirements and because it was determined that the greatest number of colors could be produced by the combination of these three colors.

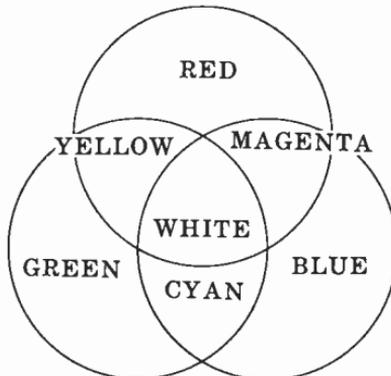


Fig. 74

The three additive primaries used in color television are shown in Fig. 74. From the illustration we can see that by mixing colors in certain proportions, we can obtain the following:

Red + Green = Yellow

Red + Blue = Magenta

Blue + Green = Cyan

Yellow + Blue = White

Cyan + Red = White

Magenta + Green = White

Red + Blue + Green = White

Cyan + Magenta + Yellow = White

It is not necessary to overlap the primary colors in the additive process to produce a different color. They may be placed close to each other, and at a certain viewing distance the two colors will blend and produce the new color.

To be compatible, the composite color signal must contain a complete black-and-white signal to which an additional signal is added to convey the color information. The black-and-white signal (also called the luminance signal) carries all the information pertaining to the brightness of the scene being televised, by means of amplitude modulation of the carrier envelope. The other color attributes—hue and saturation—are carried by the color signal.

To keep the color signal from interfering with black-and-white reception of the composite color signal, the color information is included within the 4.25-mc video band by an interleaving process. This process is possible because the energy of the luminance signal concentrates at specific intervals in the frequency spectrum. The spaces between these intervals are relatively void of energy, and the energy of the chrominance signal can be caused to concentrate in these spaces.

The color or chrominance signal is conveyed by means of a subcarrier at 3.579 megacycles. This frequency was chosen so that the interleaving process could be accomplished. This chrominance signal is modulated in both phase and amplitude. A change in the phase of this signal represents a change in the hue of the scene, and a change in amplitude

represents a change of color saturation. A color sync signal which keeps the receiver circuits synchronized to the color information is included in the composite signal. This signal is placed on the "back porch" of the horizontal blanking pedestal and is transmitted at a fixed or reference phase. This signal is known as the "color burst" signal.

55. RELAY REWINDING DATA

The following nomograph can be used if it is desired to rewind a relay for operation on a different voltage. To calculate the wire size needed for operation on the desired voltage, first lay a straightedge across the points where the present voltage and the desired voltage appear on the first

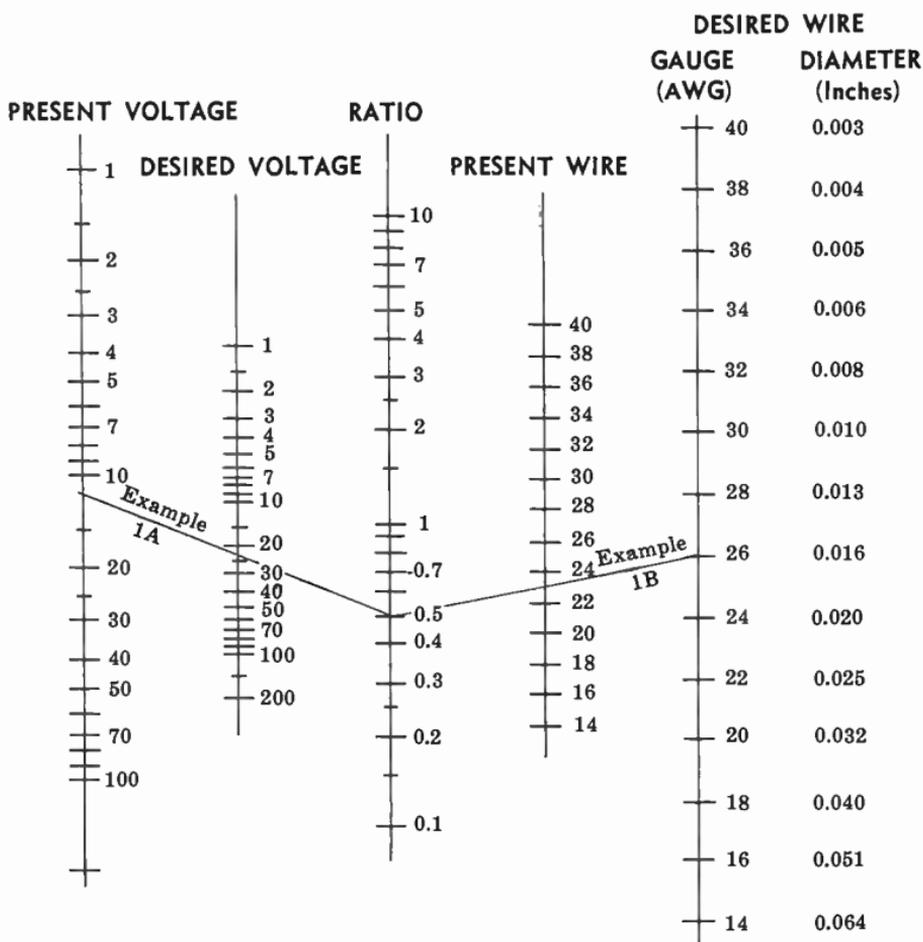


Fig. 75

two columns, and note the point where the straightedge intersects the ratio column. Then lay the straightedge across this point on the ratio column and the present wire gauge column. Read the wire gauge needed for the desired voltage from the fifth column. Directly opposite this point, the wire diameter (in inches) is also given.

Example—What size wire is needed to rewind a relay wound with No. 23 wire and designed for 12-volt operation, for operation on 24 volts?

ANSWER: No. 26 (0.0159 inch diameter). [First lay the straightedge across 12 in the first column and 24 in the second column. Note the point where the straightedge crosses the third column (.5), and lay the straightedge across this point and across 23 on the fourth column. Read the desired size from the fifth and sixth columns.]

56. SPEAKER CONNECTIONS

The following diagrams show the proper connection methods for single- or multiple-speaker operation.

(A) Single Speaker

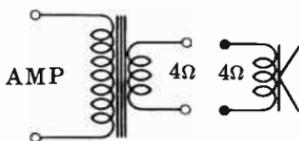


Fig. 76

(B) Two Speakers in Series

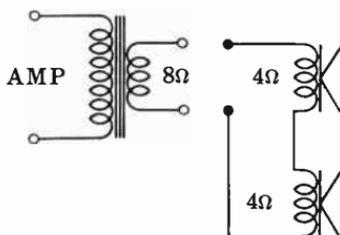


Fig. 77

(C) Speakers in Parallel

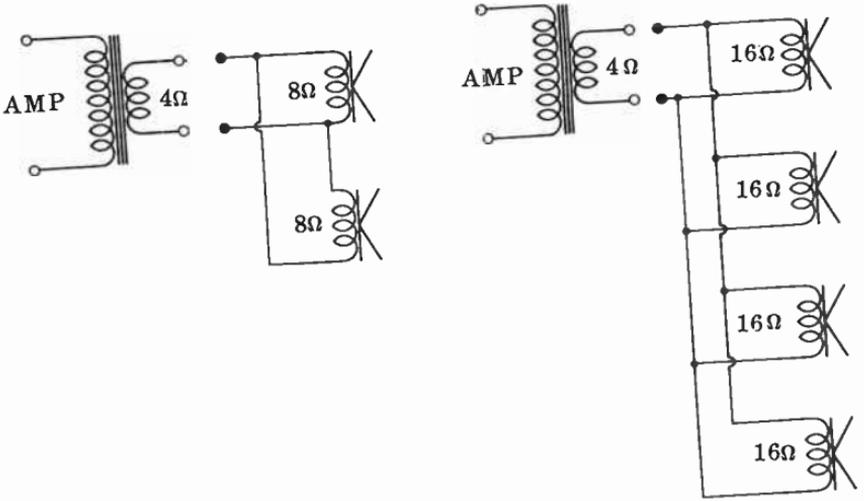


Fig. 78

(D) 70.7-Volt Hook-up Using Matching Transformers

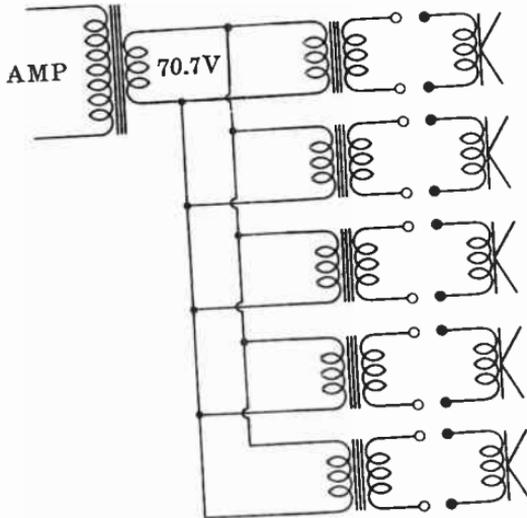


Fig. 79

57. MACHINE SCREW AND DRILL SIZES

The most common screw sizes and threads, together with the tap and clearance drill sizes, are given in Table XXII. The number listed under the "Type" column is actually a combination of the screw size and the number of threads per inch. For example, a No. 6-32 screw denotes a size No. 6 screw with 32 threads per inch.

Table XXII. Machine Screw and Drill Sizes

| Type | Tap Drill | Clearance Drill | Type | Tap Drill | Clearance Drill |
|------|-----------|-----------------|---------|-----------|-----------------|
| 1-64 | 53 | 47 | 10-24 | 25 | 13/64 |
| 1-72 | 53 | 47 | 10-32 | 21 | 13/64 |
| 2-56 | 50 | 42 | 12-24 | 16 | 7/32 |
| 2-64 | 50 | 42 | 12-28 | 14 | 7/32 |
| 3-48 | 47 | 36 | 1/4-20 | 7 | 17/64 |
| 3-56 | 45 | 36 | 1/4-28 | 3 | 17/64 |
| 4-40 | 43 | 31 | 5/16-18 | F | 21/64 |
| 4-48 | 42 | 31 | 5/16-24 | I | 21/64 |
| 5-40 | 38 | 29 | 3/8-16 | 5/16 | 25/64 |
| 5-44 | 37 | 29 | 3/8-24 | Q | 25/64 |
| 6-32 | 36 | 25 | 7/16-14 | U | 29/64 |
| 6-40 | 33 | 25 | 7/16-20 | 25/64 | 29/64 |
| 8-32 | 29 | 16 | 1/2-13 | 27/64 | 33/64 |
| 8-36 | 29 | 16 | 1/2-20 | 29/64 | 33/64 |



FLAT



ROUND



OVAL



FILLISTER



BINDING



STOVE



HEX



WASHER



PHILLIPS



ALLEN RECESS



BRISTO



CLUTCH

Fig. 80

58. TYPES OF SCREW HEADS

The most common types of screw heads are listed and illustrated in Fig. 80 on the preceding page.

59. RESISTANCE OF METALS AND ALLOYS

The resistance for a given length of wire is determined by:

$$R = \frac{KL}{d^2}$$

where,

R is the resistance, in ohms, of the length of wire.

K is the resistance, in ohms per circular mil foot, of the material,

L is the length of the wire in feet,

d is the diameter of the wire in mils.

The resistance, in ohms per circular mil foot, of many of the materials used for conductors or heating elements is given in Table XXIII. The resistance shown is for 20°C (68°F).

Table XXIII. Resistance of Metals and Alloys

| Material | Symbol | Resistance (ohms per cir. mil foot) |
|-------------------|----------|--|
| Nichrome | Ni-Fe-Cr | 675 |
| Nichrome V | Ni-Cr | 650 |
| Manganese Nickel | Ni-Mu | 85 |
| Pure Nickel | Ni | 60 |
| High Brass | Cu-Zn | 50 |
| Commercial Bronze | Cu-Zn | 25 |
| Platinum | Pt | 63.8 |
| Iron | Fe | 60.14 |
| Zinc | Zn | 35.58 |
| Molybdenum | Mo | 34.27 |
| Tungsten | W | 33.22 |
| Aluminum | Al | 16.06 |
| Gold | Au | 14.55 |
| Copper | Cu | 10.37 |
| Silver | Ag | 9.796 |

60. COPPER WIRE TABLE

Copper wire sizes ranging from American wire gauge (B & S) 0000 to 40 are listed in Table XXIV (pages 112 and 113). The turns per linear inch, diameter, area in circular mils, current-carrying capacity, feet per pound, and resistance per 1000 feet are included in the table.

Table XXIV. Copper Wire Table

| AWG B & S Gauge | Turns Per Linear Inch | | | Nylon | Diameter (Inches) | Circular Mils | Current Carrying Capacity @700 CM Per Amp | Feet Per Lb. (Bare) | Ohms Per 1,000 Ft. @ 20° C |
|-----------------------|-----------------------|--------|--------|-------|----------------------|------------------|---|---------------------------|----------------------------------|
| | Enamel | D.C.C. | S.C.C. | | | | | | |
| 0000 | — | — | — | — | .4600 | 211,600 | 302.3 | 1.561 | 0.04901 |
| 000 | — | — | — | — | .4096 | 167,800 | 239.7 | 1.968 | 0.06180 |
| 00 | — | — | — | — | .3648 | 133,100 | 190.1 | 2.482 | 0.07793 |
| 0 | — | — | — | — | .3249 | 105,500 | 150.7 | 3.130 | 0.09827 |
| 1 | — | 3.3 | 3.3 | — | .2893 | 83,690 | 119.6 | 3.947 | 0.1239 |
| 2 | — | 3.6 | 3.8 | — | .2576 | 66,370 | 94.8 | 4.977 | 0.1563 |
| 3 | — | 4.0 | 4.2 | — | .2294 | 52,640 | 75.2 | 6.276 | 0.1970 |
| 4 | — | 4.5 | 4.7 | — | .2043 | 41,740 | 59.6 | 7.914 | 0.2485 |
| 5 | — | 5.0 | 5.2 | — | .1819 | 33,100 | 47.3 | 9.980 | 0.3133 |
| 6 | — | 5.6 | 5.9 | — | .1620 | 26,250 | 37.5 | 12.58 | 0.3951 |
| 7 | — | 6.2 | 6.5 | — | .1443 | 20,820 | 29.7 | 15.87 | 0.4982 |
| 8 | 7.6 | 7.1 | 7.4 | — | .1285 | 16,510 | 23.6 | 20.01 | 0.6282 |
| 9 | 8.6 | 7.8 | 8.2 | — | .1144 | 13,090 | 18.7 | 25.23 | 0.7921 |
| 10 | 9.6 | 8.9 | 9.3 | — | .1019 | 10,380 | 14.8 | 31.82 | 0.9989 |
| 11 | 10.7 | 9.8 | 10.3 | — | .09074 | 8,234 | 11.8 | 40.12 | 1.260 |
| 12 | 12.0 | 10.9 | 11.5 | — | .08081 | 6,530 | 9.33 | 50.59 | 1.588 |
| 13 | 13.5 | 12.0 | 12.8 | — | .07196 | 5,178 | 7.40 | 63.80 | 2.003 |
| 14 | 15.0 | 13.8 | 14.2 | 14.9 | .06408 | 4,107 | 5.87 | 80.44 | 2.525 |
| 15 | 16.8 | 14.7 | 15.8 | — | .05707 | 3,257 | 4.65 | 101.4 | 3.184 |

| | | | | | | | | | |
|----|-------|------|-------|-------|---------|-------|------|--------|---------|
| 16 | 18.9 | 16.4 | 17.9 | 18.6 | .05082 | 2,583 | 3.69 | 127.9 | 4.016 |
| 17 | 21.2 | 18.1 | 19.9 | — | .04526 | 2,048 | 2.93 | 161.3 | 5.064 |
| 18 | 23.6 | 19.8 | 22.0 | 23.2 | .04030 | 1,624 | 2.32 | 203.4 | 6.385 |
| 19 | 26.4 | 21.8 | 24.4 | — | .03589 | 1,288 | 1.84 | 256.5 | 8.051 |
| 20 | 29.4 | 23.8 | 27.0 | 28.9 | .03196 | 1,022 | 1.46 | 323.4 | 10.15 |
| 21 | 33.1 | 26.0 | 29.8 | — | .02846 | 810.1 | 1.16 | 407.8 | 12.80 |
| 22 | 37.0 | 30.0 | 34.1 | 36.0 | .02535 | 642.4 | .918 | 514.2 | 16.14 |
| 23 | 41.3 | 31.6 | 37.6 | — | .02257 | 509.5 | .728 | 648.4 | 20.36 |
| 24 | 46.3 | 35.6 | 41.5 | 44.7 | .02010 | 404.0 | .577 | 817.7 | 25.67 |
| 25 | 51.7 | 38.6 | 45.6 | — | .01790 | 320.4 | .458 | 1,031 | 32.37 |
| 26 | 58.0 | 41.8 | 50.2 | 55.7 | .01594 | 254.1 | .363 | 1,300 | 40.81 |
| 27 | 64.9 | 45.0 | 55.0 | — | .01420 | 201.5 | .288 | 1,639 | 51.47 |
| 28 | 72.7 | 48.5 | 60.2 | 69.4 | .01264 | 159.8 | .228 | 2,067 | 64.90 |
| 29 | 81.6 | 51.8 | 65.4 | — | .01126 | 126.7 | .181 | 2,607 | 81.83 |
| 30 | 90.5 | 55.5 | 71.5 | 86.2 | .01003 | 100.5 | .144 | 3,287 | 103.2 |
| 31 | 101.0 | 59.2 | 77.5 | — | .008928 | 79.70 | .114 | 4,145 | 130.1 |
| 32 | 113.0 | 62.6 | 83.6 | 106.0 | .007950 | 63.21 | .090 | 5,227 | 164.1 |
| 33 | 127.0 | 66.3 | 90.3 | — | .007080 | 50.13 | .072 | 6,591 | 206.9 |
| 34 | 143.0 | 70.0 | 97.0 | 133.0 | .006305 | 39.75 | .057 | 8,310 | 260.9 |
| 35 | 158.0 | 73.5 | 104.0 | — | .005615 | 31.52 | .045 | 10,480 | 329.0 |
| 36 | 175.0 | 77.0 | 111.0 | 167.0 | .005000 | 25.00 | .036 | 13,210 | 414.8 |
| 37 | 198.0 | 80.3 | 118.0 | — | .004453 | 19.83 | .028 | 16,660 | 523.1 |
| 38 | 224.0 | 83.6 | 126.0 | 206.0 | .003965 | 15.72 | .022 | 21,010 | 659.6 |
| 39 | 248.0 | 86.6 | 133.0 | — | .003531 | 12.47 | .018 | 26,500 | 831.8 |
| 40 | 282.0 | 89.7 | 140.0 | 263.0 | .003145 | 9.89 | .014 | 33,410 | 1,049.0 |

Design Data

61. VACUUM-TUBE FORMULAS

The following formulas can be used to calculate the vacuum-tube properties listed.

Amplification factor :

$$\mu = \frac{\Delta E_p}{\Delta E_g} \text{ (with } I_p \text{ constant)}$$

AC (dynamic) plate resistance :

$$r_p = \frac{\Delta E_p}{\Delta I_p} \text{ (with } E_g \text{ constant)}$$

Mutual conductance (transconductance) :

$$g_m = \frac{\Delta I_p}{\Delta E_g} \text{ (with } E_p \text{ constant)}$$

Gain of an amplifier stage :

$$\text{Gain} = \mu \frac{R_L}{R_L + r_p}$$

where,

μ is the amplification factor,
 Δ is the variation or change in value,
 E_p is the plate voltage in volts,
 E_g is the grid voltage in volts,
 I_p is the plate current in amperes,
 R_L is the plate-load resistance in ohms,
 r_p is the AC plate resistance in ohms,
 g_m is the mutual conductance in mhos.

62. TRANSISTOR FORMULAS

The following formulas can be used to calculate the transistor properties listed.

Input Resistance:

$$R_i = \frac{\Delta V_i}{\Delta I_i}$$

Current Gain:

$$A_i = \frac{\Delta I_c}{\Delta I_b} \text{ (with } V_c \text{ constant)}$$

Voltage Gain:

$$A_v = \frac{\Delta V_c}{\Delta V_b} \text{ (with } I_c \text{ constant)}$$

Output Resistance:

$$R_o = \frac{\Delta V_o}{\Delta I_o}$$

Power Gain:

$$A_p = \frac{\Delta P_o}{\Delta P_i}$$

The current gain of the common-base configuration is *alpha*:

$$\alpha = \frac{\Delta I_c}{\Delta I_e} \text{ (with } V_c \text{ constant)}$$

The current gain of the common emitter is *beta*:

$$\beta = \frac{\Delta I_c}{\Delta I_b} \text{ (with } V_c \text{ constant)}$$

A direct relationship exists between the *alpha* and *beta* of a transistor:

$$\alpha = \frac{\beta}{1 + \beta} \qquad \beta = \frac{\alpha}{1 - \alpha}$$

where,

α is the current gain of a common-base configuration,
 A_v is the voltage gain,
 A_i is the current gain,
 A_p is the power gain,
 β is the current gain in a common-emitter configuration,
 I_b is the base current,
 I_c is the collector current,

I_c is the emitter current,
 I_i is the input current,
 I_o is the output current,
 P_i is the input power,
 P_o is the output power,
 R_i is the input resistance,
 R_o is the output resistance,
 V_b is the base voltage,
 V_c is the collector voltage,
 V_i is the input voltage,
 V_o is the output voltage.

63. THREE-PHASE POWER FORMULAS

In a three-phase system, there are three voltages, each separated by a phase difference of 120° : The power-supply input transformers may be connected in either a delta or a Y (star). Fig. 81 shows how the terminals are placed in relationship to the coils. In the delta connection, there is one coil between each pair of terminals; and in the Y connection, there are two. The voltage between two terminals of the Y-connected coil is equal to $\sqrt{3}$ times the voltage across one winding.

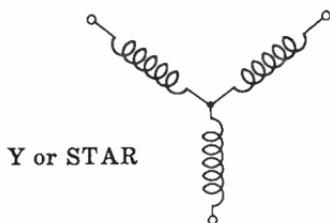
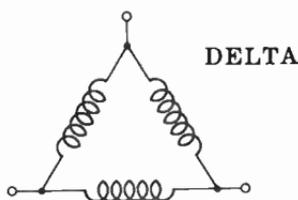


Fig. 81

The formulas for determining the voltage across the secondary winding for each of the four possible connections are as follows:

Δ to Y:

$$E_s = E_p \times N \times \sqrt{3}$$

Y to Δ :

$$E_s = \frac{E_p \times N}{\sqrt{3}}$$

Δ to Δ:

$$E_s = E_p \times N$$

Y to Y:

$$E_s = E_p \times N$$

where,

E_s is the secondary voltage,
 E_p is the primary voltage,
 N is the turns ratio.

64. COIL WINDINGS

(A) Single-Layer Coils

The inductance of single-layer coils can be calculated to an accuracy of approximately 1% with the formula:

$$L = \frac{(N \times A)^2}{9A + 10B}$$

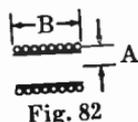


Fig. 82

To find the number of turns required for a single-layer coil with a given inductance, the foregoing formula is rearranged as follows:

$$N = \frac{\sqrt{L(9A + 10B)}}{A}$$

where,

L is the inductance in microhenries,
 N is the number of turns,
 A is the mean radius in inches,
 B is the length of the coil in inches.

(B) Multilayer Coils

The inductance of a multilayer coil of rectangular cross section can be computed from the formula:

$$L = \frac{0.8(N \times A)^2}{6A + 9B + 10C}$$

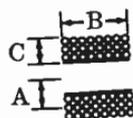


Fig. 83

where,

- L is the inductance in microhenries,
- N is the number of turns,
- A is the mean radius in inches,
- B is the length of the coil in inches,
- C is the depth of the coil in inches.

(C) Single-Layer Coil Chart

The chart on the following page provides an easy method for determining either the inductance or the number of turns for single-layer coils. When the length of the winding, the diameter, and the number of turns of the coil are known, the inductance can be found by placing a straightedge from the "Turns" scale to the "Ratio" (diameter \div length) scale and noting the point where the straightedge intersects the "Axis" scale. Then lay the straightedge from the point of intersection of the "Axis" scale to the "Diameter" scale. The point at which this line intersects the "Inductance" scale indicates the inductance (in microhenries) of the coil. The number of turns can be determined by reversing the procedure.

After finding the number of turns, consult the wire table in § 60 to determine the size of wire to be used.

Example—What is the inductance of a single-layer coil having 80 turns wound to 4 inches in length on a coil form 2 inches in diameter?

ANSWER: 130 microhenries. (First lay the straightedge as indicated by the line labeled "Example 1A." Then lay the straightedge as indicated by the line labeled "Example 1B.")

65. FILTER FORMULAS

(A) Constant-k Filters

A constant-k filter presents an impedance match to the line at only one frequency, and a mismatch at all others. The three basic configurations are the T, L (half-section), and pi.

A constant-k low-pass filter will pass frequencies below and attenuate those above a set frequency. Fig. 85 gives the circuit configurations, attenuation characteristics, and impedance characteristics of the three types of constant-k low-pass filters.

The attenuation of the L section is equal to half that of the T or pi sections. The impedance of the filter is equal to

Single-Layer Coil Chart

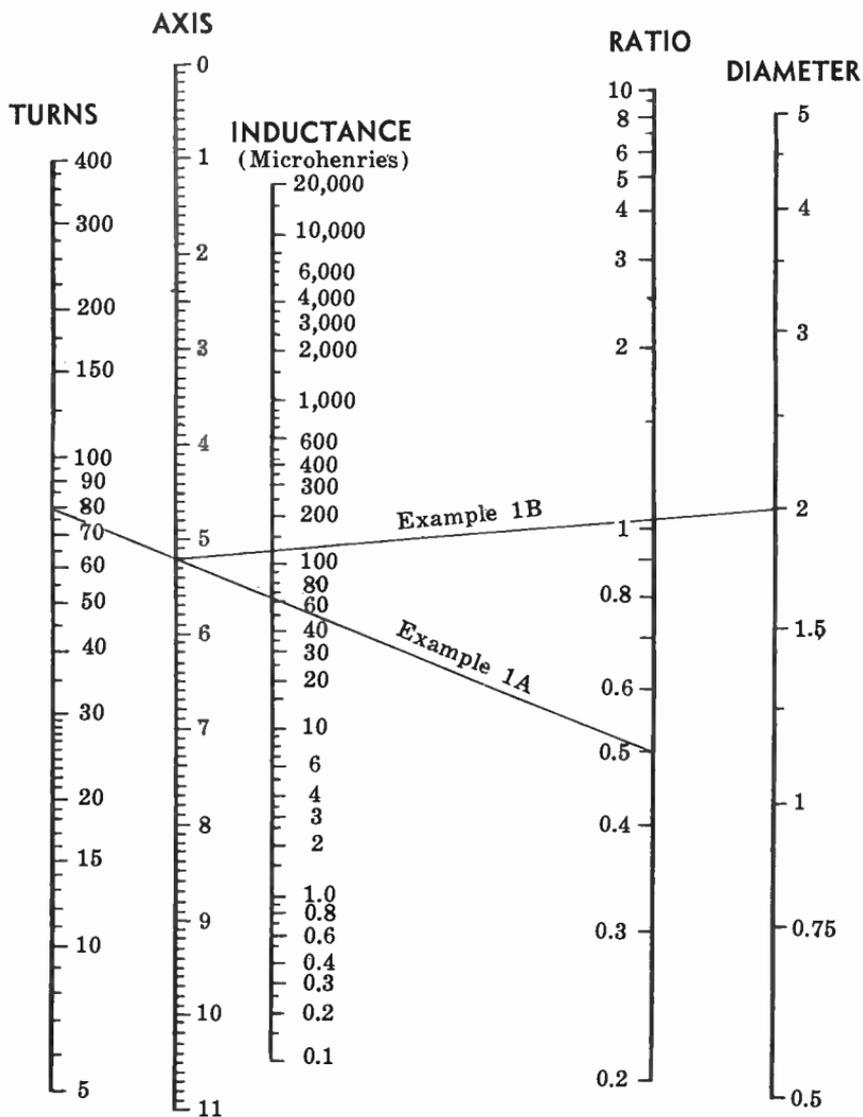


Fig. 84

the characteristic impedance of the line (Z_0) at zero frequency only. For all other frequencies, the input and output impedance of the filter are equal to Z_I or Z_I' , as shown in Fig. 85.

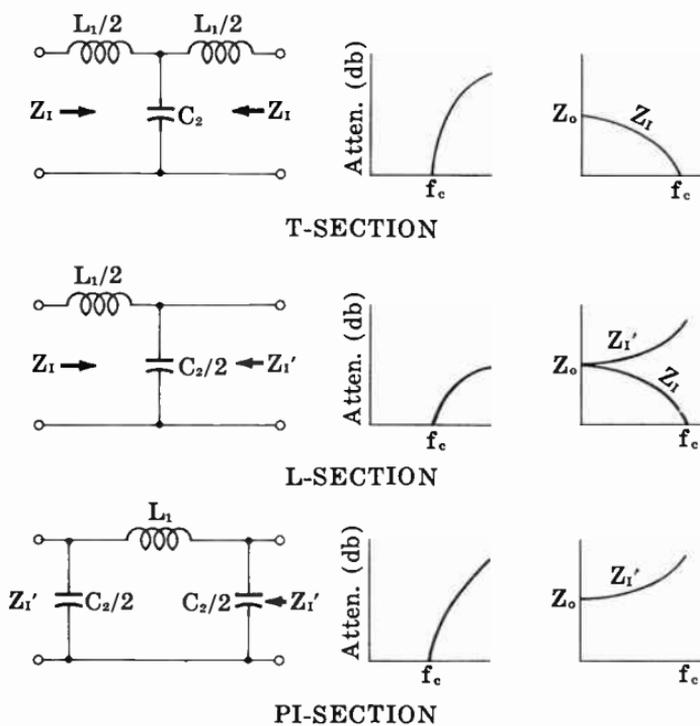


Fig. 85

The values for L_1 , C_2 , Z_0 , and f_c can be computed from the following formulas:

$$L_1 = \frac{Z_0}{\pi f_c}$$

$$C_2 = \frac{1}{\pi f_c Z_0}$$

$$Z_0 = \sqrt{\frac{L_1}{C_2}}$$

$$f_c = \frac{1}{\pi \sqrt{L_1 C_2}}$$

The values computed for L_1 and C_2 must be divided in half, where specified in Fig. 85. That is, the coils in the T

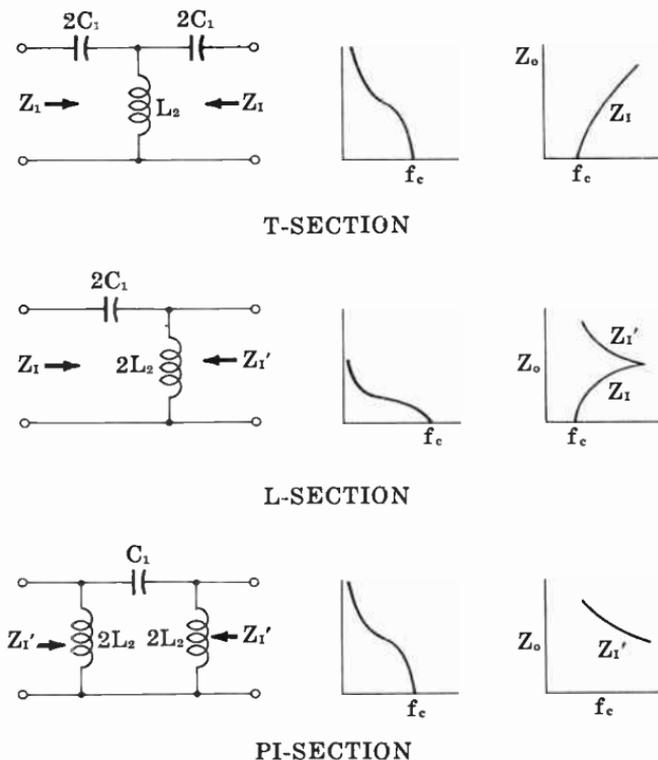


Fig. 86

and L sections, and the capacitors in the L and pi sections, are equal to one-half the computed value.

A high-pass filter will pass all frequencies above and attenuate all those below a set frequency.

The circuit configurations, attenuation characteristics, and impedance characteristics of constant-k high-pass filters are given in Fig. 86. The formulas for computing L_2 , C_1 , Z_0 , and f_c are as follows:

$$L_2 = \frac{Z_0}{4\pi f_c}$$

$$C_1 = \frac{1}{4\pi f_c Z_0}$$

$$Z_0 = \sqrt{\frac{L_2}{C_1}}$$

$$f_c = \frac{1}{4\pi \sqrt{L_2 C_1}}$$

Notice that the values computed for C in the foregoing formulas must be doubled in the T and L sections. Likewise, the value computed for L must be doubled in the L and pi sections.

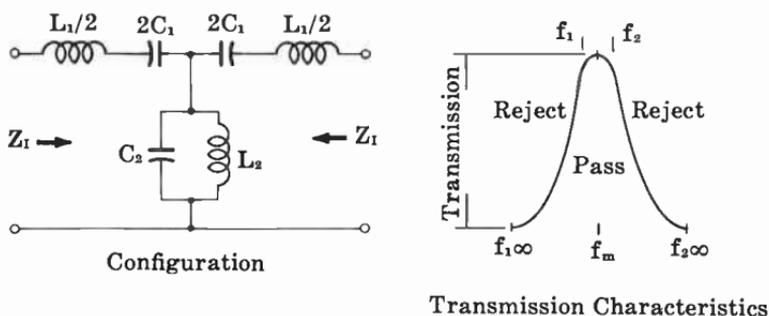


Fig. 87

Bandpass filters will pass frequencies of a certain band and reject all others. The configuration and the transmission characteristics for a constant-k bandpass filter are given in Fig. 87. The formulas for computing the various values are:

$$L_1 = \frac{Z_0}{\pi(f_2 - f_1)}$$

$$L_2 = \frac{(f_2 - f_1)Z_0}{4\pi f_1 f_2}$$

$$C_1 = \frac{(f_2 - f_1)}{4\pi f_1 f_2 Z_0}$$

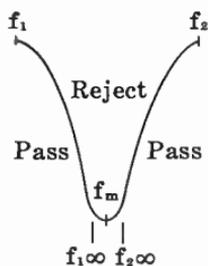
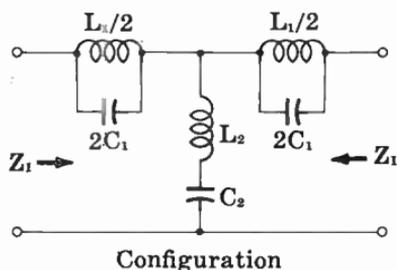
$$C_2 = \frac{1}{\pi(f_2 - f_1)Z_0}$$

$$f_m = \sqrt{f_1 f_2} = \frac{1}{2\pi\sqrt{L_1 C_1}} = \frac{1}{2\pi\sqrt{L_2 C_2}}$$

$$Z_0 = \sqrt{\frac{L_1}{C_2}} = \sqrt{\frac{L_2}{C_1}}$$

As before, some values must be doubled or halved, as shown in Fig. 87.

A band-rejection filter will reject a certain band of frequencies and pass all others. The configuration and the transmission characteristics of a constant-k band-rejection filter



Transmission Characteristics

Fig. 88

are given in Fig. 88. The formulas for computing the component values, frequencies, and line impedance are:

$$L_1 = \frac{(f_2 - f_1) Z_0}{\pi f_1 f_2}$$

$$L_2 = \frac{Z_0}{4\pi (f_2 - f_1)}$$

$$C_1 = \frac{1}{4\pi (f_2 - f_1) Z_0}$$

$$C_2 = \frac{(f_2 - f_1)}{\pi f_1 f_2 Z_0}$$

$$f_m = \sqrt{f_1 f_2} = \frac{1}{2\pi \sqrt{L_1 C_1}} = \frac{1}{2\pi \sqrt{L_2 C_2}}$$

$$Z_0 = \sqrt{\frac{L_1}{C_2}} = \sqrt{\frac{L_2}{C_1}}$$

where,

L_1 and L_2 are the inductances of the coils in henries,
 C_1 and C_2 are the capacitances of the capacitors in farads,
 f_1 and f_2 are the frequencies at the edge of the passband,
 in cycles per second,

f_m is the frequency at the center of the passband, in cycles
 per second,

$f_{1\infty}$ and $f_{2\infty}$ are the frequencies of infinite attenuation, in
 cycles per second,

Z_0 is the line impedance in ohms.

(B) M-Derived Filters

In an m -derived filter, the designer can control either the impedance or the attenuation characteristics. The values are first computed as for a constant- k filter and then modified by an algebraic expression containing the constant m . The

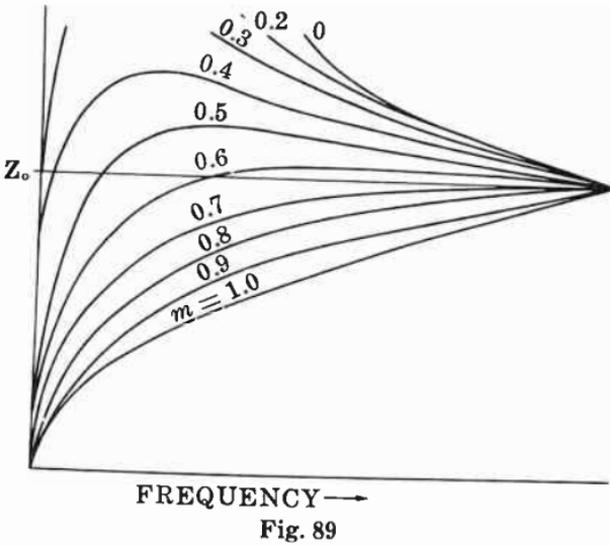


Fig. 89

term m will be a positive number between zero and one, and its value governs the characteristics of the filter.

Two frequencies—the cutoff and the frequency of infinite attenuation—are involved in the design of m -derived filters. By selecting the proper value for m , it is possible to control the spacing between the two frequencies. Fig. 89 shows the effect which different values of m have on the impedance

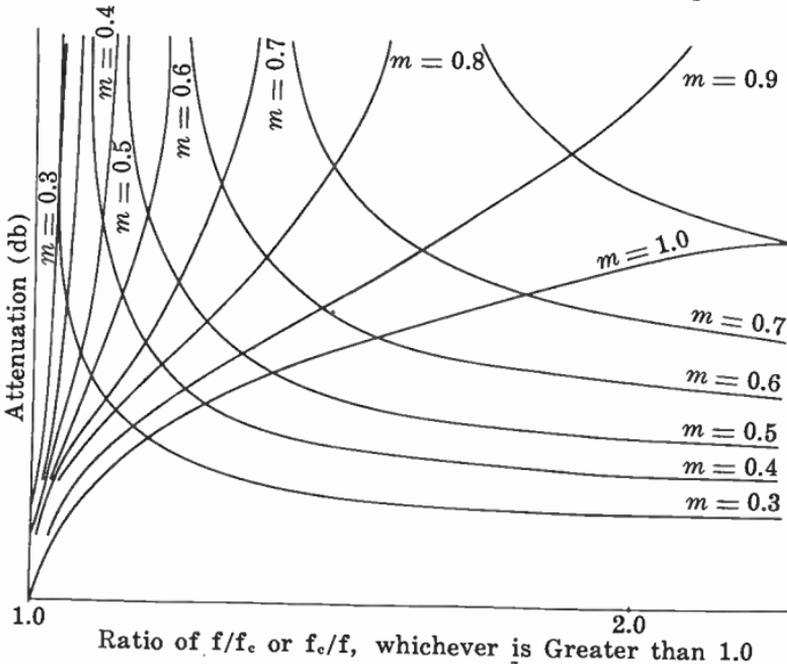


Fig. 90

characteristics. Note that the best impedance match is obtained when m is equal to 0.6; hence this value is usually employed.

The attenuation characteristics for the various values of m are given in Fig. 90. The attenuation rises to maximum and then drops on all curves. This graph applies to both low- and high-pass filters.

The value of m is determined from the formulas:

$$m = \sqrt{1 - \left(\frac{f_c}{f_\infty}\right)^2}$$

or,

$$m = \sqrt{1 - \left(\frac{f_{\infty}}{f_c}\right)^2}$$

Select the formula which will give a positive number.

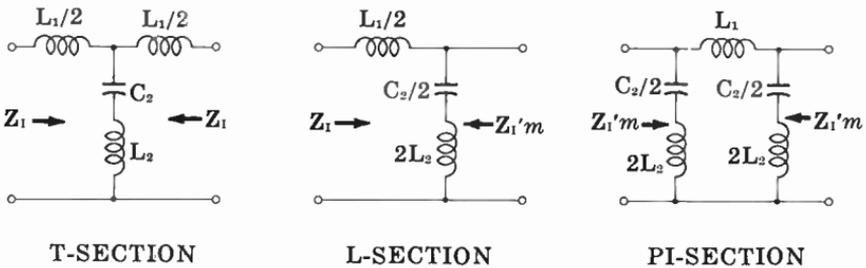


Fig. 91

The configurations for m -derived filters are classified as either series or shunt. Those for the series m -derived low-pass filters are given in Fig. 91. The formulas are as follows:

$$L_1 = m \left(\frac{Z_0}{2\pi f_c} \right)$$

$$L_2 = \left(\frac{1-m^2}{4m} \right) \left(\frac{Z_0}{2\pi f_c} \right)$$

$$C_2 = m \left(\frac{1}{\pi f_c Z_0} \right)$$

For a series m -derived high-pass filter (Fig. 92), the formulas are:

$$L_2 = \frac{\left(\frac{Z_0}{4\pi f_c} \right)}{m}$$

$$C_1 = \frac{\left(\frac{1}{4\pi f_c Z_0} \right)}{m}$$

$$C_2 = \left(\frac{4m}{1 - m^2} \right) \left(\frac{1}{4\pi f_c Z_0} \right)$$

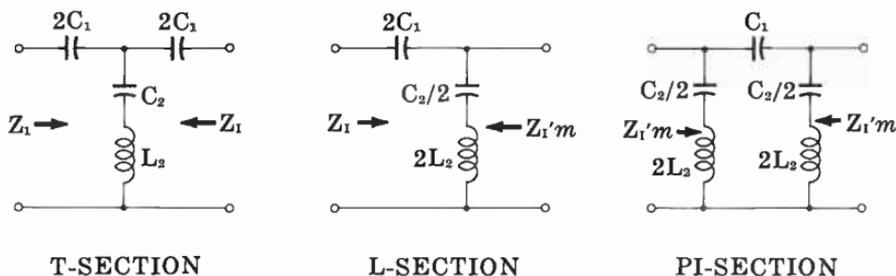


Fig. 92

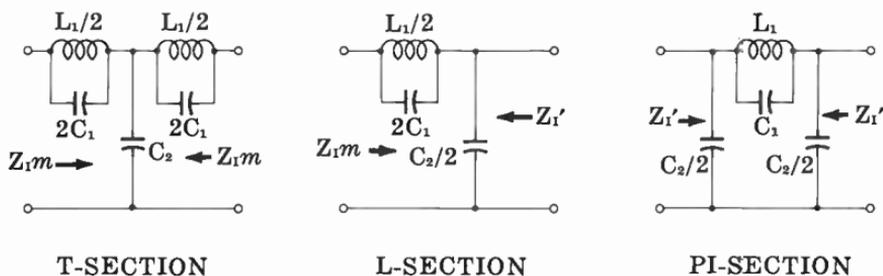


Fig. 93

The configurations for shunt m -derived low-pass filters are given in Fig. 93. The formulas for computing the component values are:

$$L_1 = m \left(\frac{Z_0}{\pi f_c} \right)$$

$$C_1 = \left(\frac{1 - m^2}{4m} \right) \left(\frac{1}{\pi f_c Z_0} \right)$$

$$C_2 = m \left(\frac{1}{\pi f_c Z_0} \right)$$

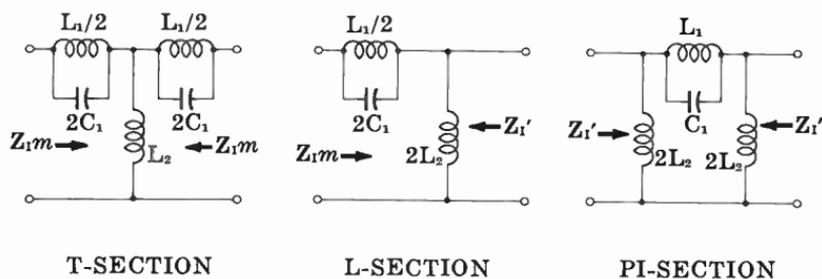


Fig. 94

For shunt m -derived high-pass filters (Fig. 94), the formulas are:

$$L_1 = \left(\frac{4m}{1 - m^2} \right) \left(\frac{Z_o}{4\pi f_c} \right)$$

$$L_2 = \frac{\left(\frac{Z_o}{4\pi f_c} \right)}{m}$$

$$C_1 = \frac{\left(\frac{1}{4\pi f_c Z_o} \right)}{m}$$

where,

L_1 and L_2 are the inductances of the coils in henries,
 C_1 and C_2 are the capacitances of the capacitors in farads,
 m is a constant between 0 and 1,
 Z_o is the line impedance in ohms,
 f_c is the cutoff frequency in cycles per second.

66. ATTENUATOR FORMULAS

(A) General

An attenuator is an arrangement of noninductive resistors used in an electrical circuit to reduce the audio- or radio-signal strength without introducing distortion. The resistors may be fixed or variable. Attenuators can be designed to

work between equal or unequal impedances; hence, they are often used as impedance-matching networks.

Any attenuator working between unequal impedances must introduce a certain minimum loss. These values are given in the graph of Fig. 95. The impedance ratio is the input impedance divided by the output impedance, or vice versa—whichever gives a value of more than one.

A factor is used in the calculation of resistor values in attenuator networks. Called *K*, it is the ratio of current, voltage, or power corresponding to a given value of attenuation in decibels. Table XXV gives the value of “*K*” for the more common loss values.

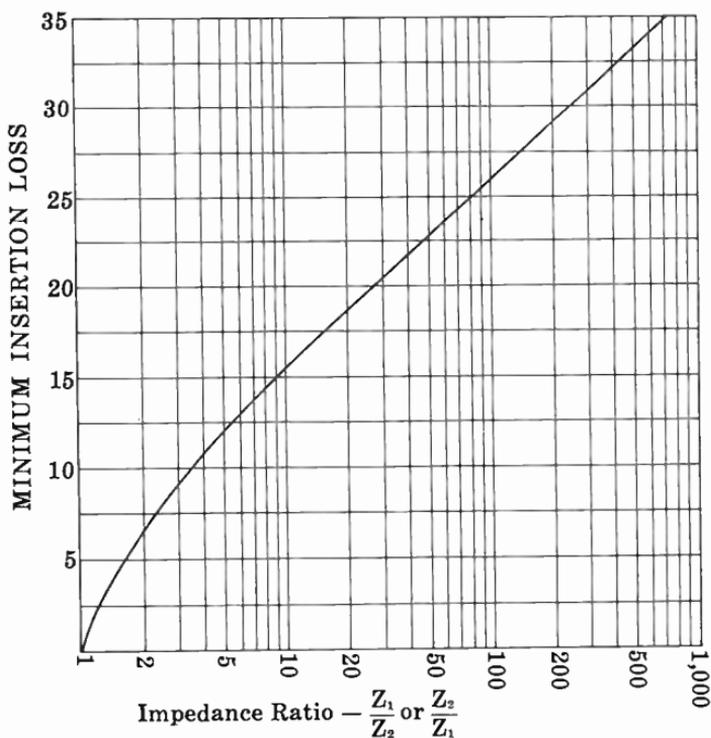


Fig. 95

The four steps in the design of a pad are: (1) Determine the type of network required. (2) If impedances are unequal, calculate the ratio of input to output impedance (or output to input impedance) and refer to Fig. 95 for the minimum loss value. (3) From Table XXV find the value of *K* for the desired loss. (4) Calculate the resistor values, using the following formulas.

Table XXV. K Factors for Calculating Attenuator Loss

| db | K | db | K | db | K | db | K |
|-----|--------|------|---------|------|---------|-------|-----------------|
| .05 | 1.0058 | 9.5 | 2.9854 | 29.0 | 28.184 | 49.0 | 281.84 |
| .1 | 1.0116 | 10.0 | 3.1623 | 30.0 | 31.623 | 50.0 | 316.23 |
| .5 | 1.0593 | 11.0 | 3.5481 | 31.0 | 35.481 | 51.0 | 354.81 |
| 1.0 | 1.1220 | 12.0 | 3.9811 | 32.0 | 39.811 | 52.0 | 398.11 |
| 1.5 | 1.1885 | 13.0 | 4.4668 | 33.0 | 44.668 | 54.0 | 501.19 |
| 2.0 | 1.2589 | 14.0 | 5.0119 | 34.0 | 50.119 | 55.0 | 562.34 |
| 2.5 | 1.3335 | 15.0 | 5.6234 | 35.0 | 56.234 | 56.0 | 630.96 |
| 3.0 | 1.4125 | 16.0 | 6.3096 | 36.0 | 63.096 | 57.0 | 707.95 |
| 3.5 | 1.4962 | 17.0 | 7.0795 | 37.0 | 70.795 | 58.0 | 794.33 |
| 4.0 | 1.5849 | 18.0 | 7.9433 | 38.0 | 79.433 | 60.0 | 1000.0 |
| 4.5 | 1.6788 | 19.0 | 8.9125 | 39.0 | 89.125 | 65.0 | 1778.3 |
| 5.0 | 1.7783 | 20.0 | 10.0000 | 40.0 | 100.000 | 70.0 | 3162.3 |
| 5.5 | 1.8837 | 21.0 | 11.2202 | 41.0 | 112.202 | 75.0 | 5623.4 |
| 6.0 | 1.9953 | 22.0 | 12.589 | 42.0 | 125.89 | 80.0 | 10,000 |
| 6.5 | 2.1135 | 23.0 | 14.125 | 43.0 | 141.25 | 85.0 | 17,783 |
| 7.0 | 2.2387 | 24.0 | 15.849 | 44.0 | 158.49 | 90.0 | 31,623 |
| 7.5 | 2.3714 | 25.0 | 17.783 | 45.0 | 177.83 | 95.0 | 56,234 |
| 8.0 | 2.5119 | 26.0 | 19.953 | 46.0 | 199.53 | 100.0 | 10 ⁶ |
| 8.5 | 2.6607 | 27.0 | 22.387 | 47.0 | 223.87 | | |
| 9.0 | 2.8184 | 28.0 | 25.119 | 48.0 | 251.19 | | |

(B) Combining or Dividing Network

$$R_B = \left(\frac{N - 1}{N + 1} \right) Z$$

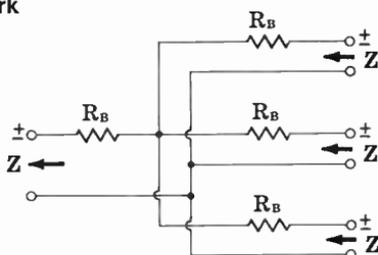


Fig. 96

where,

R_B is the resistance of the building-out resistors in ohms,
 N is the number of circuits fed by the source impedance,
 Z is the source impedance in ohms.

(C) T-Type Attenuator (Between Equal Impedances)

$$R_1 \text{ and } R_2 = \left(\frac{K - 1}{K + 1} \right) Z$$

$$R_3 = \left(\frac{K}{K^2 - 1} \right) 2Z$$

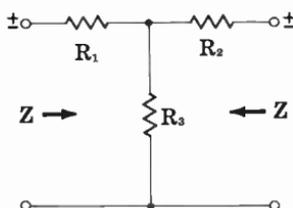


Fig. 97

(D) H-Type Attenuator (Balanced-T Attenuator)

Calculate the values for R_1 , R_2 , and R_3 as for an unbalanced T-attenuator (Fig. 97). Then halve the values of R_1 and R_2 , as shown in Fig. 98. The tap on R_3 is exactly in the center.

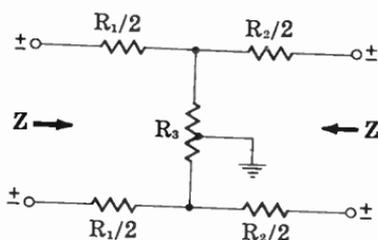


Fig. 98

(E) Taper Pad (T-Type Attenuator Between Unequal Impedances)

$$R_1 = Z_1 \left(\frac{K^2 + 1}{K^2 - 1} \right) - 2\sqrt{Z_1 Z_2} \left(\frac{K}{K^2 - 1} \right)$$

$$R_2 = Z_2 \left(\frac{K^2 + 1}{K^2 - 1} \right) - 2\sqrt{Z_1 Z_2} \left(\frac{K}{K^2 - 1} \right)$$

$$R_3 = 2\sqrt{Z_1 Z_2} \left(\frac{K}{K^2 - 1} \right)$$

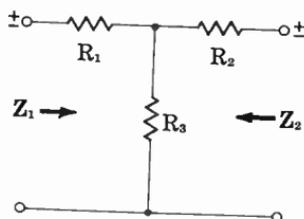


Fig. 99

where,

Z_1 is the larger impedance.

(F) Bridged-T Attenuator (Unbalanced)

$$R_1 = Z$$

$$R_5 = (K - 1)Z$$

$$R_6 = \left(\frac{1}{K - 1} \right)Z$$

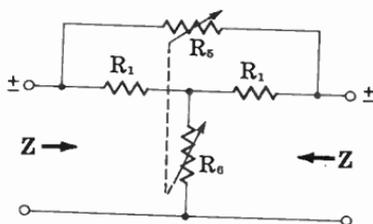


Fig. 100

R_5 and R_6 are connected to a common shaft, and each varies inversely in value with respect to the other.

(G) Balanced Bridged-T Attenuator

Calculate the values for R_1 , R_5 , and R_6 as for an unbalanced bridged-T attenuator (Fig. 100). Then halve the values as shown in Fig. 101.

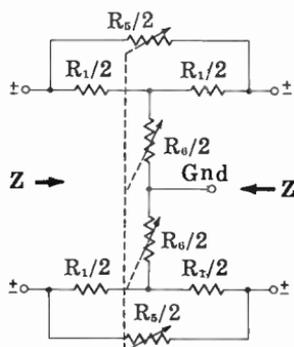


Fig. 101

(H) L-Type Attenuators

An L-type attenuator can supply an impedance match in only one direction. If the impedances it works out of and into are unequal, it can be made to match either—but not both—impedances. The arrows in the following illustrations indicate the direction of impedance match.

Between equal impedances and with the impedance match in the direction of the series arm:

$$R_1 = Z \left(\frac{K - 1}{K} \right)$$

$$R_2 = Z \left(\frac{1}{K - 1} \right)$$

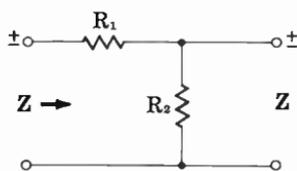


Fig. 102

Between equal impedances and with the impedance match in the direction of the shunt arm:

$$R_1 = Z (K - 1)$$

$$R_2 = Z \left(\frac{K}{K - 1} \right)$$

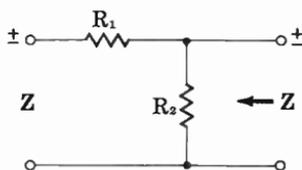


Fig. 103

Between unequal impedances and with the impedance match toward the larger value:

$$R_1 = \left(\frac{Z_1}{S} \right) \left(\frac{KS - 1}{K} \right)$$

$$R_2 = \left(\frac{Z_1}{S} \right) \left(\frac{1}{K - S} \right)$$

where,

$$S = \sqrt{\frac{Z_1}{Z_2}}$$

Between unequal impedances and with the impedance match toward the smaller value:

$$R_1 = \left(\frac{Z_1}{S} \right) (K - S)$$

$$R_2 = \left(\frac{Z_1}{S} \right) \left(\frac{K}{KS - 1} \right)$$

where,

$$S \text{ equals } \sqrt{\frac{Z_1}{Z_2}}$$

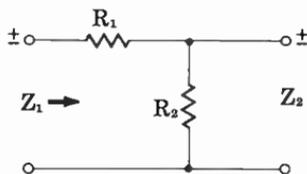


Fig. 104

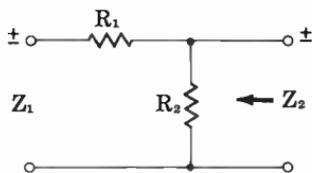


Fig. 105

(I) Pi-Type Attenuator (Between Equal Impedances)

$$R_1 = Z \left(\frac{K + 1}{K - 1} \right)$$

$$R_2 = \left(\frac{Z}{2} \right) \left(\frac{K^2 - 1}{K} \right)$$

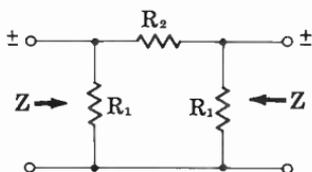


Fig. 106

(J) Pi-Type Attenuator (Between Unequal Impedances)

$$R_1 = Z_1 \left(\frac{K^2 - 1}{K^2 - 2KS + 1} \right)$$

$$R_2 = \left(\frac{\sqrt{Z_1 Z_2}}{2} \right) \left(\frac{K^2 - 1}{K} \right)$$

$$R_3 = Z_2 \left(\frac{K^2 - 1}{K^2 - 2\frac{K}{S} + 1} \right)$$

where,

$$S \text{ equals } \sqrt{\frac{Z_1}{Z_2}}$$

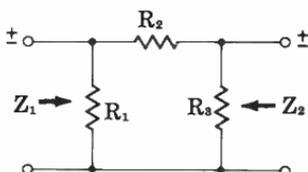


Fig. 107

(K) O-Type Attenuators

Calculate the values for a pi-type attenuator (Figs. 106 and 107), then halve the values for the series resistors as shown in Figs. 108 (balanced) and 109 (unbalanced).

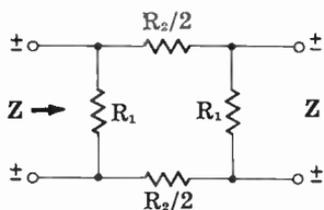


Fig. 108

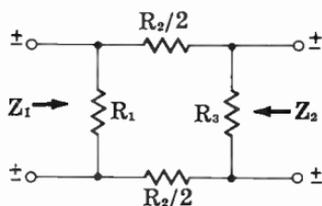


Fig. 109

(L) U-Type Attenuator

For impedance match in the direction of the series arms:

$$R_1 = \left(\frac{Z_1}{2S} \right) \left(\frac{KS - 1}{K} \right)$$

$$R_2 = \left(\frac{Z_1}{S} \right) \left(\frac{1}{K - S} \right)$$

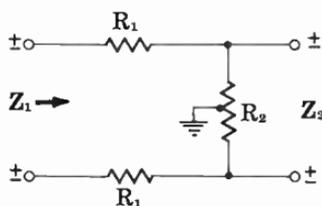


Fig. 110

For impedance match in the direction of the shunt arm:

$$R_1 = \left(\frac{Z_1}{2S} \right) (K - S)$$

$$R_2 = \left(\frac{Z_1}{S} \right) \left(\frac{K}{KS - 1} \right)$$

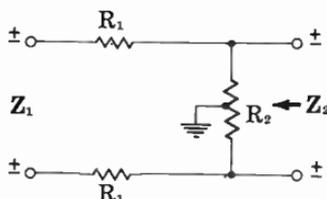


Fig. 111

where,

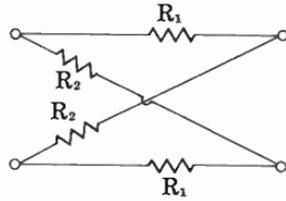
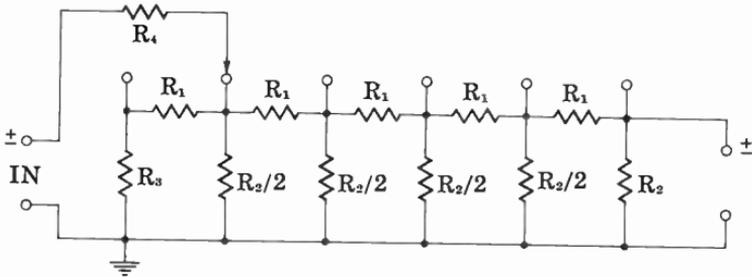
The arrows indicate the direction of the impedance match,

$$S \text{ equals } \sqrt{\frac{Z_1}{Z_2}}$$

(M) Lattice-Type Attenuator

$$R_1 = \left(\frac{K - 1}{K + 1} \right) Z$$

$$R_2 = \left(\frac{K + 1}{K - 1} \right) Z$$

**Fig. 112****(N) Ladder-Type Attenuator****Fig. 113**

$$R_1 = \left(\frac{K^2 - 1}{2K} \right) Z$$

$$R_2 = \left(\frac{K + 1}{K - 1} \right) Z$$

$$R_3 = \frac{R_2 \times Z}{R_2 + Z}$$

$$R_4 = \frac{Z}{2}$$

$$Z_{in} = Z_{out}$$

where,

K depends on the loss per step—not on the total loss.

Mathematical Tables and Formulas

67. MATHEMATICAL CONSTANTS

| | |
|--|---------------------------------|
| $\pi = 3.1416$ | $(2\pi)^2 = 39.4786$ |
| $\pi^2 = 9.8696$ | $4\pi = 12.5664$ |
| $\pi^3 = 31.0063$ | $\frac{\pi}{2} = 1.5708$ |
| $\frac{1}{\pi} = 0.3183$ | $\frac{\sqrt{\pi}}{2} = 1.2533$ |
| $\frac{1}{\pi^2} = 0.1013$ | $\sqrt{2} = 1.4142$ |
| $\frac{1}{\pi^3} = 0.0323$ | $\sqrt{3} = 1.7321$ |
| $\sqrt{\pi} = 1.7725$ | $\frac{1}{\sqrt{2}} = 0.7071$ |
| $\frac{1}{\sqrt{\pi}} = 0.5642$ | $\frac{1}{\sqrt{3}} = 0.5773$ |
| $\frac{1}{2\pi} = 0.1592$ | $\log \pi = 0.4971$ |
| $\left(\frac{1}{2\pi}\right)^2 = 0.0253$ | $\log \pi^2 = 0.9943$ |
| $2\pi = 6.2832$ | $\log \sqrt{\pi} = 0.2486$ |
| | $\log \frac{\pi}{2} = 0.1961$ |

68. MATHEMATICAL SYMBOLS

| | |
|------------------------------------|------------------------------------|
| \times or \cdot Multiplied by. | $+$ Positive, add, and plus. |
| \div Divided by. | $-$ Negative, subtract, and minus. |
| $=$ Equals. | |
| \neq Does not equal. | $>$ Is greater than. |

| | | | |
|--------------|-----------------------|----------------|----------------------------|
| < | Is less than. | \cong | Equal to or greater than. |
| \pm | Plus or minus. | \leq | Equal to or less than. |
| \equiv | Identical with. | \perp | Perpendicular to. |
| \therefore | Therefore. | $ n $ | Absolute value of n . |
| \parallel | Parallel to. | \approx | Is approximately equal to. |
| \angle | Angle. | $\sqrt{\quad}$ | Square root. |
| \ll | Is much less than. | | |
| \gg | Is much greater than. | | |

69. DECIMAL EQUIVALENTS OF FRACTIONS

The decimal equivalents to four places of fractions by 64ths are given in Table XXVI.

Table XXVI. Decimal Equivalents of Fractions

| Fraction | | | | Decimal | Fraction | | | | Decimal |
|----------|-------|------|-----|---------|----------|-------|--|-------|---------|
| 1/64 | | | | 0.0156 | 33/64 | | | | 0.5156 |
| | 1/32 | | | 0.0313 | | 17/32 | | | 0.5313 |
| 3/64 | | | | 0.0469 | 35/64 | | | | 0.5469 |
| | | 1/16 | | 0.0625 | | 9/16 | | | 0.5625 |
| 5/64 | | | | 0.0781 | 37/64 | | | | 0.5781 |
| | 3/32 | | | 0.0938 | | 19/32 | | | 0.5938 |
| 7/64 | | | | 0.1094 | 39/64 | | | | 0.6094 |
| | | | 1/8 | 0.1250 | | | | 5/8 | 0.6250 |
| 9/64 | | | | 0.1406 | 41/64 | | | | 0.6406 |
| | 5/32 | | | 0.1563 | | 21/32 | | | 0.6563 |
| 11/64 | | | | 0.1719 | 43/64 | | | | 0.6719 |
| | | 3/16 | | 0.1875 | | | | 11/16 | 0.6875 |
| 13/64 | | | | 0.2031 | 45/64 | | | | 0.7031 |
| | 7/32 | | | 0.2188 | | 23/32 | | | 0.7188 |
| 15/64 | | | | 0.2344 | 47/64 | | | | 0.7344 |
| | | | 1/4 | 0.2500 | | | | 3/4 | 0.7500 |
| 17/64 | | | | 0.2656 | 49/64 | | | | 0.7656 |
| | 9/32 | | | 0.2813 | | 25/32 | | | 0.7813 |
| 19/64 | | | | 0.2969 | 51/64 | | | | 0.7969 |
| | | 5/16 | | 0.3125 | | | | 13/16 | 0.8125 |
| 21/64 | | | | 0.3281 | 53/64 | | | | 0.8281 |
| | 11/32 | | | 0.3438 | | 27/32 | | | 0.8438 |
| 23/64 | | | | 0.3594 | 55/64 | | | | 0.8594 |
| | | | 3/8 | 0.3750 | | | | 7/8 | 0.8750 |
| 25/64 | | | | 0.3906 | 57/64 | | | | 0.8906 |
| | 13/32 | | | 0.4063 | | 29/32 | | | 0.9063 |
| 27/64 | | | | 0.4219 | 59/64 | | | | 0.9219 |
| | | 7/16 | | 0.4375 | | | | 15/16 | 0.9375 |
| 29/64 | | | | 0.4531 | 61/64 | | | | 0.9531 |
| | 15/32 | | | 0.4688 | | 31/32 | | | 0.9688 |
| 31/64 | | | | 0.4844 | 63/64 | | | | 0.9844 |
| | | | 1/2 | 0.5000 | | | | 1 | 1.0000 |

70. POWERS OF TEN

(A) Exponent Determination

Large numbers can be simplified by using powers of ten. For example, some of the multiples of ten from 1 to 1,000,000, with their equivalents in powers of ten are:

$$\begin{aligned} 1 &= 10^0* \\ 10 &= 10^1 \\ 100 &= 10^2 \\ 1000 &= 10^3 \\ 10,000 &= 10^4 \\ 100,000 &= 10^5 \\ 1,000,000 &= 10^6 \end{aligned}$$

Likewise, powers of ten can be used to simplify decimal expressions. Some of the submultiples of ten from 0.1 to 0.000001, with their equivalents in powers of ten are:

$$\begin{aligned} 0.1 &= 10^{-1} \\ 0.01 &= 10^{-2} \\ 0.001 &= 10^{-3} \\ 0.0001 &= 10^{-4} \\ 0.00001 &= 10^{-5} \\ 0.000001 &= 10^{-6} \end{aligned}$$

Any whole number can be expressed as a smaller whole number, and any decimal can be expressed as a whole number, by moving the decimal point to the left or right and expressing the number as a power of ten. If the decimal point is moved to the left, the power is positive and is equal to the number of places the decimal point was moved. If the decimal point is moved to the right, the power is negative and is equal to the number of places the decimal point was moved.

For example:

$$\begin{aligned} 123 &= 1.23 \times 10^2 \\ 456.7 &= 4.567 \times 10^2 \\ 78,900 &= 78.9 \times 10^3 \\ 0.00012 &= 1.2 \times 10^{-4} \\ 0.0345 &= 34.5 \times 10^{-3} \\ .678 &= 67.8 \times 10^{-2} \end{aligned}$$

* Any number to the zero power is 1.

(B) Addition and Subtraction

To add or subtract using powers of ten, first convert all numbers to the same power of ten. The numbers can then be added or subtracted, and the answer will be in the same power of ten. For example:

$$\begin{aligned}
 9.32 \times 10^2 + 17.63 \times 10^3 + 297 &= ? \\
 9.32 \times 10^2 &= 0.932 \times 10^3 \\
 17.63 \times 10^3 &= 17.630 \times 10^3 \\
 297 &= \underline{0.297 \times 10^3} \\
 18.859 \times 10^3 &= 18,859
 \end{aligned}$$

$$\begin{aligned}
 18.47 \times 10^2 - 1.59 \times 10^3 &= ? \\
 18.47 \times 10^2 &= 1.847 \times 10^3 \\
 1.59 \times 10^3 &= \underline{1.590 \times 10^3} \\
 .257 \times 10^3 &= 257
 \end{aligned}$$

(C) Multiplication

To multiply using powers of ten, add the exponents. Thus:

$$\begin{aligned}
 1000 \times 3721 &= 10^3 \times 37.21 \times 10^2 \\
 &= 37.21 \times 10^{3+2} \\
 &= 37.21 \times 10^5 \\
 &= 3,721,000
 \end{aligned}$$

$$\begin{aligned}
 225 \times .00723 &= 2.25 \times 10^2 \times 7.23 \times 10^{-3} \\
 &= 2.25 \times 7.23 \times 10^{2+(-3)} \\
 &= 2.25 \times 7.23 \times 10^{-1} \\
 &= 16.2675 \times 10^{-1} \\
 &= 1.62675
 \end{aligned}$$

(D) Division

To divide using powers of ten, subtract the exponent of the denominator from the exponent of the numerator. Thus:

$$\begin{aligned}
 \frac{10^5}{10^3} &= 10^{5-3} \\
 &= 10^2 \\
 &= 100
 \end{aligned}$$

$$\begin{aligned} \frac{72,600}{.002} &= \frac{72.6 \times 10^3}{2 \times 10^{-3}} \\ &= \frac{72.6 \times 10^{3+3}}{2} \\ &= 36.3 \times 10^6 \\ &= 36,300,000. \end{aligned}$$

(E) Combination Multiplication and Division

Problems involving a combination of multiplication and division can be solved using powers of ten by multiplying and dividing, as called for, until the problem is completed. For example:

$$\begin{aligned} \frac{3900 \times .007 \times 420}{142,000 \times .00005} &= \frac{3.9 \times 10^3 \times 7 \times 10^{-3} \times 4.2 \times 10^2}{1.42 \times 10^5 \times 5 \times 10^{-5}} \\ &= \frac{3.9 \times 7 \times 4.2 \times 10^2}{1.42 \times 5} \\ &= \frac{114.66 \times 10^2}{7.1} \\ &= 16.1493 \times 10^2 \\ &= 1614.93 \end{aligned}$$

(F) Reciprocal

To take the reciprocal of a number using powers of ten, first (if necessary) state the number so the decimal point precedes the first significant figure of the number. Then divide this number into 1. The power of 10 in the answer will be the same value as in the original number, but will have the opposite sign. For example:

$$\begin{aligned} \text{Reciprocal of } 400 &= \frac{1}{400} \\ \frac{1}{400} &= \frac{1}{.4 \times 10^3} \\ &= 2.5 \times 10^{-3} \\ &= .0025 \end{aligned}$$

$$\begin{aligned} \text{Reciprocal of } .0025 &= \frac{1}{.0025} \\ \frac{1}{.0025} &= \frac{1}{.25 \times 10^{-2}} \\ &= 4 \times 10^2 \\ &= 400 \end{aligned}$$

(G) Square and Square Root

To square a number using powers of ten, multiply the number by itself, and double the exponent. Thus:

$$\begin{aligned}(7 \times 10^3)^2 &= 49 \times 10^6 \\ &= 49,000,000 \\ (9.2 \times 10^{-4})^2 &= 84.64 \times 10^{-8} \\ &= .000008464\end{aligned}$$

To extract the square root of a number using powers of ten, do the opposite. (If the number is an odd power of 10, first convert it to an even power of ten.) Extract the square root of the number, and divide the power of ten by 2. Thus:

$$\begin{aligned}\sqrt{36 \times 10^{10}} &= 6 \times 10^5 \\ &= 600,000 \\ \sqrt{5.72 \times 10^3} &= \sqrt{57.2 \times 10^2} \\ &= 7.56 \times 10 \\ &= 75.6\end{aligned}$$

71. OPERATION OF THE SLIDE RULE

The slide rule (Fig. 114) is an instrument designed to perform mathematical calculations with a high degree of accuracy. For example, the common 10-inch slide rule has an accuracy of one-tenth of one per cent. Operations such as multiplication, division, extraction of square and cube roots, and finding trigonometric functions such as sine, cosine, and tangent can all be performed on the slide rule.

There are six scales on the front of the slide rule. The letter *A*, in the upper left-hand corner of the body, denotes the *A* scale. On the left side of the slide, the letters *B*, *CI*, and *C* denote their respective scales. The letters *D* and *K*, at the lower left corner of the body, indicate these scales.

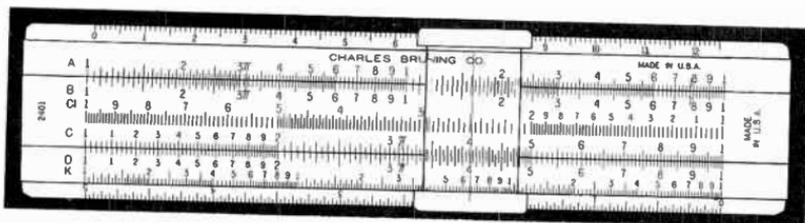


Fig. 114

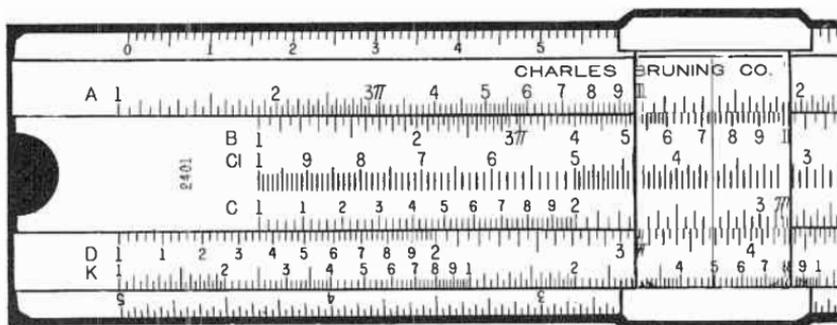


Fig. 115

The number 1 on the left end of the slide is called the left index, and the number 1 on the right end is the right index.

The C and D scales, which are identical, are used for multiplication and division. As a sample problem in multiplication, let us multiply 136 by 27. First place the left index of the slide on 136 on the D scale. Then slide the runner to 27 on the C scale, and read your answer (3672) on the D scale, as shown in Fig. 115.

Notice that the slide rule is accurate to three places, as illustrated by the sample problem. The fourth number can be estimated close enough for practical purposes.

As a sample problem in division, let us divide 390 by 0.7. Place the runner on 390 on the D scale; then push the slide to the left until 7 on the C scale is over the 390, as shown in Fig. 116. Finally, place the runner at the right index, and read the answer (557) on the D scale.

The CI, or reciprocal, scale is the same as the C scale except its numbers increase from right to left. Hence, any number on the CI scale is the reciprocal of the number directly below it on the C scale. The CI scale can be used with

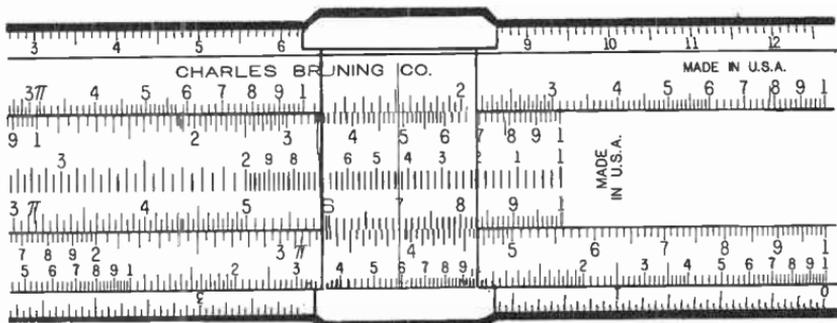


Fig. 116

the *C* and *D* scales for multiplication and division, including problems involving several multiplication and division operations in sequence.

As a sample problem in multiplication, take $26 \times 32 \times 6$. Place the left index of the slide on 26 of the *D* scale. Then slide the runner to 32 on the *C* scale, as shown in Fig. 117. Multiplying by 6 is the same as dividing by the reciprocal of 6. To do this, place the 6 on the *CI* scale under the hair-line of the runner (Fig. 118), and read the answer (4992) under the left index.

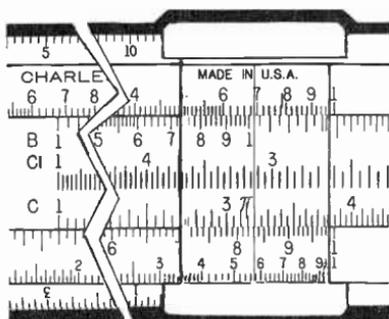


Fig. 117

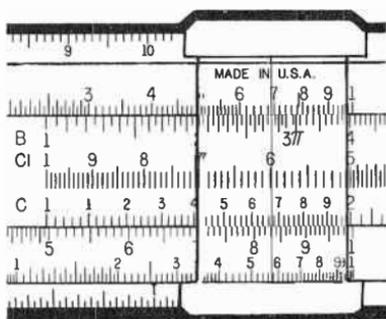


Fig. 118

The *A* and *B* scales, which are identical, are located on the upper portion of the body and slide. The *A* and/or *B* scales are used with the *C* and/or *D* scales for finding the square or square root of a number.

Example problem: Find the square root of 625. First place the runner at 625 on the *A* scale. Then read the answer (25) on the *D* scale (Fig. 119).

The slide rule can be used for finding the square root of the sum of two squares, as you might wish to do if you were

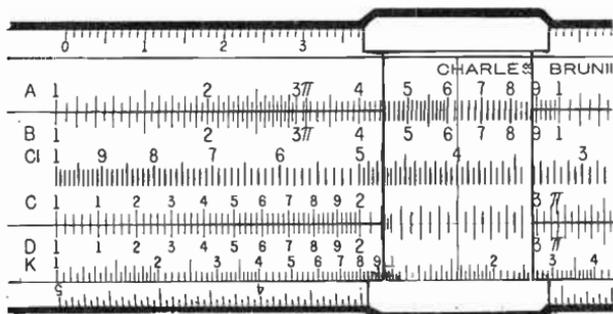


Fig. 119

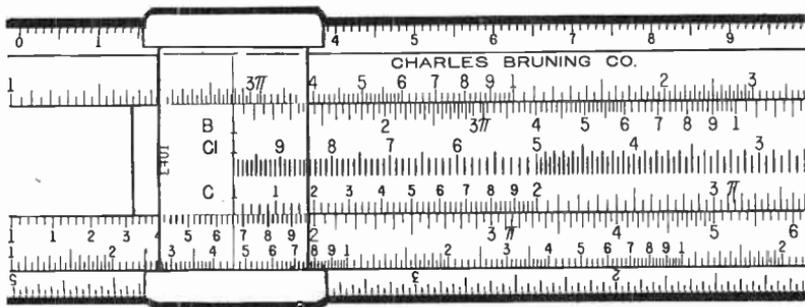


Fig. 120

solving a right triangle. For example, if the two sides of a right triangle are 3 and 5, find the hypotenuse in the following manner:

Divide the 5 by the 3, by placing 3 on the C scale opposite 5 on the D scale. Square the quotient by reading 2.78 on the A scale opposite the left index of the B scale (Fig. 120). Mentally add 1 to get 3.78, and set the left index of the B scale to 3.78 on the A scale. Extract the square root by going to the D scale and reading 1.945 opposite the C index mark. Without changing the slide, multiply by 3 (the number by which you originally divided) to obtain the answer (5.83) on the D scale (Fig. 121).

The K scale is used with the D scale for finding the cube and cube root. Each number on the K scale is equal to the cube of the number above it on the D scale. Conversely, to extract the cube root of a number, set the runner to this number on the K scale, and read the cube root on the D scale.

The back of the slide is shown in Fig. 122. On it are the sine, log, and tangent scales. The sine scale is at the top and is designated by the letter S on the right side of the

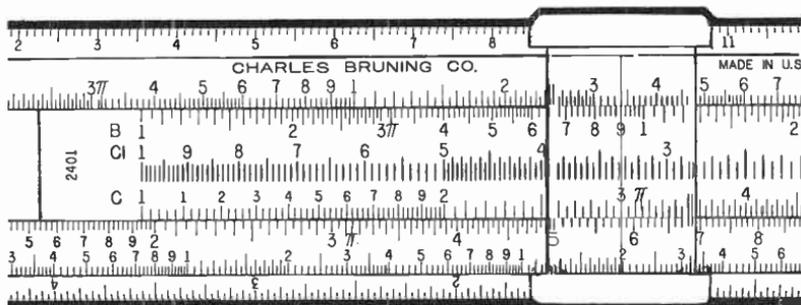


Fig. 121

slide. The log scale, designated by the letter *L*, is in the middle; and the tangent scale, designated by the letter *T*, is at the bottom.

The "inch" and "centimeter" scales on the rule are only a convenience—they are not used in any slide-rule operations.

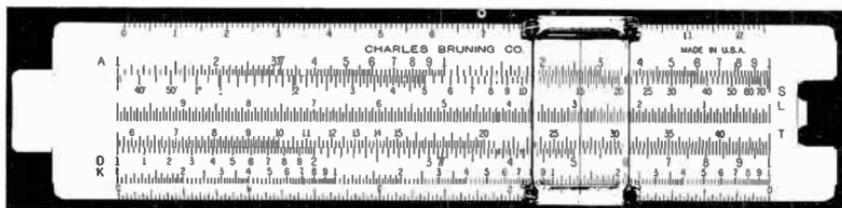


Fig. 122

72. ALGEBRAIC OPERATIONS

(A) Transposition of Terms

The following rules apply to the transposition of terms in algebraic equations:

$$\text{If } A = \frac{B}{C}, \text{ then:}$$

$$B = AC$$

$$C = \frac{B}{A}$$

$$\text{If } \frac{A}{B} = \frac{C}{D}, \text{ then:}$$

$$A = \frac{BC}{D}$$

$$B = \frac{AD}{C}$$

$$C = \frac{AD}{B}$$

$$D = \frac{BC}{A}$$

If $A = \frac{1}{D\sqrt{BC}}$, then:

$$A^2 = \frac{1}{D^2 BC}$$

$$B = \frac{1}{D^2 A^2 C}$$

$$C = \frac{1}{D^2 A^2 B}$$

$$D = \frac{1}{A\sqrt{BC}}$$

If $A = \sqrt{B^2 + C^2}$, then:

$$A^2 = B^2 + C^2$$

$$B = \sqrt{A^2 - C^2}$$

$$C = \sqrt{A^2 - B^2}$$

(B) Laws of Exponents

A power of a fraction is equal to that power of the numerator divided by the same power of the denominator.

$$\left(\frac{a}{b}\right)^x = \frac{a^x}{b^x}$$

The product of two powers of the same base is also a power of that base; the exponent of the product is equal to the sum of the exponents of the two factors.

$$a^x \cdot a^y = a^{x+y}$$

The quotient of two powers of the same base is also a power of that base; the exponent of the quotient is equal to the numerator exponent minus the denominator exponent.

$$\frac{a^x}{a^z} = a^{x-z}$$

The power of a power of a base is also a power of that base; the exponent of the product is equal to the product of the exponents.

$$(a^x)^y = a^{xy}$$

A negative exponent of a base is equal to the reciprocal of that base, with a positive exponent numerically equal to the original exponent.

$$a^{-x} = \frac{1}{a^x}$$

A fractional exponent indicates that the base should be raised to the power indicated by the numerator of the fraction; the root indicated by the denominator should then be extracted.

$$a^{\frac{x}{y}} = \sqrt[y]{a^x}$$

A root of a fraction is equal to the identical root of the numerator divided by the identical root of the denominator.

$$\sqrt[x]{\frac{a}{b}} = \frac{\sqrt[x]{a}}{\sqrt[x]{b}}$$

A root of a product is equal to the product of the roots of the individual factors.

$$\sqrt[x]{ab} = \sqrt[x]{a} \times \sqrt[x]{b}$$

(C) Quadratic Equation

The general quadratic equation:

$$ax^2 + bx + c = 0$$

may be solved by:

$$x = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$

73. GEOMETRIC FORMULAS

(A) Triangle

$$\text{area (A)} = \frac{bh}{2}$$

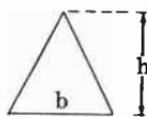


Fig. 123

(B) Square

$$\text{area (A)} = b^2$$

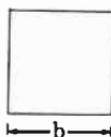


Fig. 124

(C) Rectangle

$$\text{area (A)} = ab$$

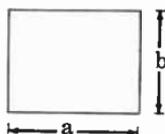


Fig. 125

(D) Parallelogram

$$\text{area (A)} = ah$$

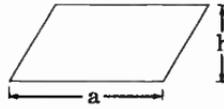


Fig. 126

(E) Trapezoid

$$\text{area (A)} = \frac{h}{2}(a + b)$$

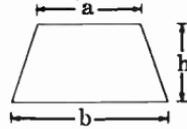


Fig. 127

(F) Trapezium

$$\text{area (A)} = \frac{1}{2} [b(H+h) + ah + cH]$$

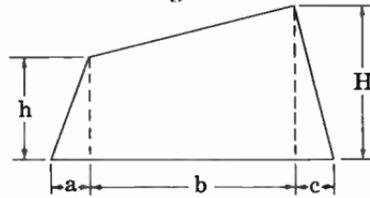


Fig. 128

(G) Regular Pentagon

$$\text{area (A)} = 1.720 a^2$$

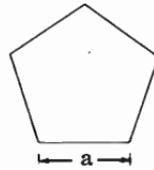


Fig. 129

(H) Regular Hexagon

$$\text{area (A)} = 2.598 a^2$$



Fig. 130

(I) Regular Octagon

$$\text{area (A)} = 4.828 a^2$$

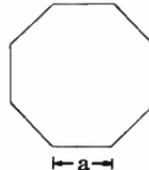


Fig. 131

(J) Circle

$$\text{circumference (C)} = 2\pi R$$

$$= \pi D$$

$$\text{area (A)} = \pi R^2$$

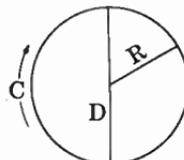


Fig. 132

(K) Segment

$$\text{chord } (c) = \sqrt{4(2hR-h^2)}$$

$$\text{area } (A) = \pi R^2 \left(\frac{\theta}{360} \right) - \left(\frac{c(R-h)}{2} \right)$$

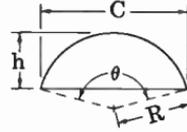


Fig. 133

(L) Sector

$$\text{area } (A) = \frac{bR}{2}$$

$$= \pi R^2 \left(\frac{\theta}{360} \right)$$

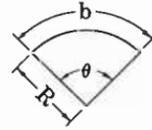


Fig. 134

(M) Circular Ring

$$\text{area } (A) = \pi(R^2 - r^2)$$

$$= 7854 (D^2 - d^2)$$



Fig. 135

(N) Ellipse

$$\text{circumference } (C) = \pi(a+b) \left[\frac{64-3 \left(\frac{b-a}{b+a} \right)^4}{64-16 \left(\frac{b-a}{b+a} \right)^2} \right]$$

$$\text{area } (A) = \pi ab$$

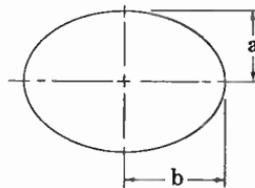


Fig. 136

(O) Sphere

$$\begin{aligned} \text{area (A)} &= 4\pi R^2 \\ &= \pi D^2 \end{aligned}$$

$$\begin{aligned} \text{volume (V)} &= \frac{4}{3} \pi R^3 \\ &= 1/6 \pi D^3 \end{aligned}$$



Fig. 137

(P) Cube

$$\begin{aligned} \text{area (A)} &= 6b^2 \\ \text{volume (V)} &= b^3 \end{aligned}$$

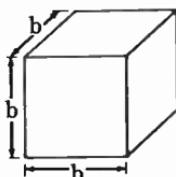


Fig. 138

(Q) Rectangular Solid

$$\begin{aligned} \text{area (A)} &= 2 (ab + bc + ac) \\ \text{volume (V)} &= abc \end{aligned}$$

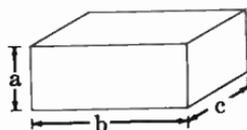


Fig. 139

(R) Cone

$$\begin{aligned} \text{area (A)} &= \pi RS \\ &= \pi R \sqrt{R^2 + h^2} \\ \text{volume (V)} &= \frac{\pi R^2 h}{3} \\ &= 1.047 R^2 h \\ &= 0.2618 D^2 h \end{aligned}$$

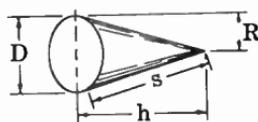


Fig. 140

(S) Cylinder

$$\begin{aligned} \text{cylindrical surface} &= \pi Dh \\ \text{total surface} &= 2\pi R(R+h) \\ \text{volume (V)} &= \pi R^2 h \\ &= \frac{c^2 h}{4\pi} \end{aligned}$$

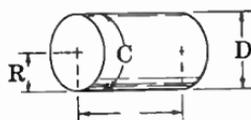


Fig. 141

(T) Ring of Rectangular Cross Section

$$\begin{aligned} \text{volume (V)} &= \frac{\pi c}{4} (D^2 - d^2) \\ &= \left(\frac{D+d}{2} \right) \pi bc \end{aligned}$$

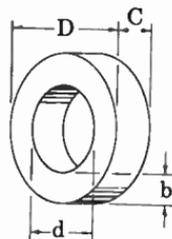


Fig. 142

(U) Torus (Ring of Circular Cross Section)

$$\begin{aligned} \text{total surface} &= 4\pi^2 Rr \\ &= \pi^2 Dd \\ \text{volume (V)} &= 2\pi^2 R \times r^2 \\ &= 2.463 D \times d^2 \end{aligned}$$

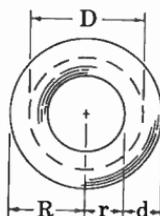


Fig. 143

74. TRIGONOMETRIC FUNCTIONS

(A) Plane Trigonometry

In any right triangle, the values in Table XXVII are valid if we let:

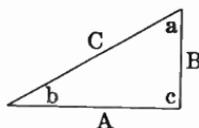


Fig. 144

a equal the acute angle formed by the hypotenuse and the altitude leg,

b equal the acute angle formed by the hypotenuse and the base leg,

A equal the side adjacent to $\angle b$ and opposite $\angle a$,

B equal the side opposite $\angle b$ and adjacent to $\angle a$,

C equal the hypotenuse.

Table XXVII. Trigonometric Formulas

| Known Values | Formulas for Unknown Values of | | | | |
|----------------|--------------------------------|---------------------------|---------------------------|-----------------------|-----------------------|
| | A | B | C | $\angle b$ | $\angle a$ |
| A & B | — | — | $\sqrt{A^2 + B^2}$ | $\arctan \frac{B}{A}$ | $\arctan \frac{A}{B}$ |
| A & C | — | $\sqrt{C^2 - A^2}$ | — | $\arccos \frac{A}{C}$ | $\arcsin \frac{A}{C}$ |
| A & $\angle b$ | — | $A \tan \angle b$ | $\frac{A}{\cos \angle b}$ | — | $90^\circ - \angle b$ |
| A & $\angle a$ | — | $\frac{A}{\tan \angle a}$ | $\frac{A}{\sin \angle a}$ | $90^\circ - \angle a$ | — |
| B & C | $\sqrt{C^2 - B^2}$ | — | — | $\arcsin \frac{B}{C}$ | $\arccos \frac{B}{C}$ |
| B & $\angle b$ | $\frac{B}{B \tan \angle b}$ | — | $\frac{B}{\sin \angle b}$ | — | $90^\circ - \angle b$ |
| B & $\angle a$ | $B \tan \angle a$ | — | $\frac{B}{\cos \angle a}$ | $90^\circ - \angle a$ | — |
| C & $\angle b$ | $C \cos \angle b$ | $C \sin \angle b$ | — | — | $90^\circ - \angle b$ |
| C & $\angle a$ | $C \sin \angle a$ | $C \cos \angle a$ | — | $90^\circ - \angle a$ | — |

The expression "arc sin" or "sin'" indicates an angle whose sine is. . . . Similarly, "arc tan" or "tan'" indicates the angle whose tangent is . . . , etc.

(B) Table of Trigonometric Functions

Table XXVIII gives the natural sines, cosines, tangents, and cotangents of angles. To find these values for angles from 0° to 45°, use the headings at the top of the table and the degree listings in the left-hand column. For angles from 45° to 90°, use the headings at the bottom of the table and the degree listings in the right-hand column. Note: Read the degree listings in the right-hand column from bottom to top; thus, the 10' listing directly above 89° signifies 89° 10'.

Table XXVIII. Natural Trigonometric Functions

| Degrees | Sin | Cos | Tan | Cot | |
|---------|--------|--------|--------|--------|---------|
| 0° 00' | 0.0000 | 1.0000 | 0.0000 | ∞ | 90° 00' |
| 10 | .0029 | 1.0000 | .0029 | 343.77 | 50 |
| 20 | .0058 | 1.0000 | .0058 | 171.89 | 40 |
| 30 | .0087 | 1.0000 | .0087 | 114.59 | 30 |
| 40 | .0116 | .9999 | .0116 | 85.940 | 20 |
| 50 | .0145 | .9999 | .0145 | 68.750 | 10 |
| 1° 00' | 0.0175 | 0.9998 | 0.0175 | 57.290 | 89° 00' |
| 10 | .0204 | .9998 | .0204 | 49.104 | 50 |
| 20 | .0233 | .9997 | .0233 | 42.964 | 40 |
| 30 | .0262 | .9997 | .0262 | 38.188 | 30 |
| 40 | .0291 | .9996 | .0291 | 34.368 | 20 |
| 50 | .0320 | .9995 | .0320 | 31.242 | 10 |
| 2° 00' | 0.0349 | 0.9994 | 0.0349 | 28.636 | 88° 00' |
| 10 | .0378 | .9993 | .0378 | 26.432 | 50 |
| 20 | .0407 | .9992 | .0407 | 24.542 | 40 |
| 30 | .0436 | .9990 | .0437 | 22.904 | 30 |
| 40 | .0465 | .9989 | .0466 | 21.470 | 20 |
| 50 | .0494 | .9988 | .0495 | 20.206 | 10 |
| 3° 00' | 0.0523 | 0.9986 | 0.0524 | 19.081 | 87° 00' |
| 10 | .0552 | .9985 | .0553 | 18.075 | 50 |
| 20 | .0581 | .9983 | .0582 | 17.169 | 40 |
| 30 | .0610 | .9981 | .0612 | 16.350 | 30 |
| 40 | .0640 | .9980 | .0641 | 15.605 | 20 |
| 50 | .0669 | .9978 | .0670 | 14.924 | 10 |
| 4° 00' | 0.0698 | 0.9976 | 0.0699 | 14.301 | 86° 00' |
| 10 | .0727 | .9974 | .0729 | 13.727 | 50 |
| 20 | .0756 | .9971 | .0758 | 13.197 | 40 |
| 30 | .0785 | .9969 | .0787 | 12.706 | 30 |
| 40 | .0814 | .9967 | .0816 | 12.251 | 20 |
| 50 | .0843 | .9964 | .0846 | 11.826 | 10 |
| 5° 00' | 0.0872 | 0.9962 | 0.0875 | 11.430 | 85° 00' |
| 10 | .0901 | .9959 | .0904 | 11.059 | 50 |
| 20 | .0929 | .9957 | .0934 | 10.712 | 40 |
| 30 | .0958 | .9954 | .0963 | 10.385 | 30 |
| 40 | .0987 | .9951 | .0992 | 10.078 | 20 |
| 50 | .1016 | .9948 | .1022 | 9.7882 | 10 |
| 6° 00' | 0.1045 | 0.9945 | 0.1051 | 9.5144 | 84° 00' |
| 10 | .1074 | .9942 | .1080 | 9.2553 | 50 |
| 20 | .1103 | .9939 | .1110 | 9.0098 | 40 |
| 30 | .1132 | .9936 | .1139 | 8.7769 | 30 |
| 40 | .1161 | .9932 | .1169 | 8.5555 | 20 |
| 50 | .1190 | .9929 | .1198 | 8.3450 | 10 |
| 7° 00' | 0.1219 | 0.9925 | 0.1228 | 8.1443 | 83° 00' |
| 10 | .1248 | .9922 | .1257 | 7.9530 | 50 |
| 20 | .1276 | .9918 | .1287 | 7.7704 | 40 |
| 30 | .1305 | .9914 | .1317 | 7.5958 | 30 |
| 40 | .1334 | .9911 | .1346 | 7.4287 | 20 |
| 50 | .1363 | .9907 | .1376 | 7.2687 | 10 |
| | Cos | Sin | Cot | Tan | Degrees |

Table XXVIII. Natural Trigonometric Functions—(Cont'd)

| Degrees | Sin | Cos | Tan | Cot | |
|---------|------------|------------|------------|------------|----------------|
| 8° 00' | 0.1392 | 0.9903 | 0.1405 | 7.1154 | 82° 00' |
| 10 | .1421 | .9899 | .1435 | 6.9682 | 50 |
| 20 | .1449 | .9894 | .1465 | 6.8269 | 40 |
| 30 | .1478 | .9890 | .1495 | 6.6912 | 30 |
| 40 | .1507 | .9886 | .1524 | 6.5606 | 20 |
| 50 | .1536 | .9881 | .1554 | 6.4348 | 10 |
| 9° 00' | 0.1564 | 0.9877 | 0.1584 | 6.3138 | 81° 00' |
| 10 | .1593 | .9872 | .1614 | 6.1970 | 50 |
| 20 | .1622 | .9868 | .1644 | 6.0844 | 40 |
| 30 | .1650 | .9863 | .1673 | 5.9758 | 30 |
| 40 | .1679 | .9858 | .1703 | 5.8708 | 20 |
| 50 | .1708 | .9853 | .1733 | 5.7694 | 10 |
| 10° 00' | 0.1736 | 0.9848 | 0.1763 | 5.6713 | 80° 00' |
| 10 | .1765 | .9843 | .1793 | 5.5764 | 50 |
| 20 | .1794 | .9838 | .1823 | 5.4845 | 40 |
| 30 | .1822 | .9833 | .1853 | 5.3955 | 30 |
| 40 | .1851 | .9827 | .1883 | 5.3093 | 20 |
| 50 | .1880 | .9822 | .1914 | 5.2257 | 10 |
| 11° 00' | 0.1908 | 0.9816 | 0.1944 | 5.1446 | 79° 00' |
| 10 | .1937 | .9811 | .1974 | 5.0658 | 50 |
| 20 | .1965 | .9805 | .2004 | 4.9894 | 40 |
| 30 | .1994 | .9799 | .2035 | 4.9152 | 30 |
| 40 | .2022 | .9793 | .2065 | 4.8430 | 20 |
| 50 | .2051 | .9787 | .2095 | 4.7729 | 10 |
| 12° 00' | 0.2079 | 0.9781 | 0.2126 | 4.7046 | 78° 00' |
| 10 | .2108 | .9775 | .2156 | 4.6382 | 50 |
| 20 | .2136 | .9769 | .2186 | 4.5736 | 40 |
| 30 | .2164 | .9763 | .2217 | 4.5107 | 30 |
| 40 | .2193 | .9757 | .2247 | 4.4494 | 20 |
| 50 | .2221 | .9750 | .2278 | 4.3897 | 10 |
| 13° 00' | 0.2250 | 0.9744 | 0.2309 | 4.3315 | 77° 00' |
| 10 | .2278 | .9737 | .2339 | 4.2747 | 50 |
| 20 | .2306 | .9730 | .2370 | 4.2193 | 40 |
| 30 | .2334 | .9724 | .2401 | 4.1653 | 30 |
| 40 | .2363 | .9717 | .2432 | 4.1126 | 20 |
| 50 | .2391 | .9710 | .2462 | 4.0611 | 10 |
| 14° 00' | 0.2419 | 0.9703 | 0.2493 | 4.0108 | 76° 00' |
| 10 | .2447 | .9696 | .2524 | 3.9617 | 50 |
| 20 | .2476 | .9689 | .2555 | 3.9136 | 40 |
| 30 | .2504 | .9681 | .2586 | 3.8667 | 30 |
| 40 | .2532 | .9674 | .2617 | 3.8208 | 20 |
| 50 | .2560 | .9667 | .2648 | 3.7760 | 10 |
| 15° 00' | 0.2588 | 0.9659 | 0.2679 | 3.7321 | 75° 00' |
| 10 | .2616 | .9652 | .2711 | 3.6891 | 50 |
| 20 | .2644 | .9644 | .2742 | 3.6470 | 40 |
| 30 | .2672 | .9636 | .2773 | 3.6059 | 30 |
| 40 | .2700 | .9628 | .2805 | 3.5656 | 20 |
| 50 | .2728 | .9621 | .2836 | 3.5261 | 10 |
| | Cos | Sin | Cot | Tan | Degrees |

Table XXVIII. Natural Trigonometric Functions—(Cont'd)

| Degrees | Sin | Cos | Tan | Cot | |
|---------|--------|--------|--------|--------|---------|
| 16° 00' | 0.2756 | 0.9613 | 0.2867 | 3.4874 | 74° 00' |
| 10 | .2784 | .9605 | .2899 | 3.4495 | 50 |
| 20 | .2812 | .9596 | .2931 | 3.4124 | 40 |
| 30 | .2840 | .9588 | .2962 | 3.3759 | 30 |
| 40 | .2868 | .9580 | .2994 | 3.3402 | 20 |
| 50 | .2896 | .9572 | .3026 | 3.3052 | 10 |
| 17° 00' | 0.2924 | 0.9563 | 0.3057 | 3.2707 | 73° 00' |
| 10 | .2952 | .9555 | .3089 | 3.2371 | 50 |
| 20 | .2979 | .9546 | .3121 | 3.2041 | 40 |
| 30 | .3007 | .9537 | .3153 | 3.1716 | 30 |
| 40 | .3035 | .9528 | .3185 | 3.1397 | 20 |
| 50 | .3062 | .9520 | .3217 | 3.1084 | 10 |
| 18° 00' | 0.3090 | 0.9511 | 0.3249 | 3.0777 | 72° 00' |
| 10 | .3118 | .9502 | .3281 | 3.0475 | 50 |
| 20 | .3145 | .9492 | .3314 | 3.0178 | 40 |
| 30 | .3173 | .9483 | .3346 | 2.9887 | 30 |
| 40 | .3201 | .9474 | .3378 | 2.9600 | 20 |
| 50 | .3228 | .9465 | .3411 | 2.9319 | 10 |
| 19° 00' | 0.3256 | 0.9455 | 0.3443 | 2.9042 | 71° 00' |
| 10 | .3283 | .9446 | .3476 | 2.8770 | 50 |
| 20 | .3311 | .9436 | .3508 | 2.8502 | 40 |
| 30 | .3338 | .9426 | .3541 | 2.8239 | 30 |
| 40 | .3365 | .9417 | .3574 | 2.7980 | 20 |
| 50 | .3393 | .9407 | .3607 | 2.7725 | 10 |
| 20° 00' | 0.3420 | 0.9397 | 0.3640 | 2.7475 | 70° 00' |
| 10 | .3448 | .9387 | .3673 | 2.7228 | 50 |
| 20 | .3475 | .9377 | .3706 | 2.6985 | 40 |
| 30 | .3502 | .9367 | .3739 | 2.6746 | 30 |
| 40 | .3529 | .9356 | .3772 | 2.6511 | 20 |
| 50 | .3557 | .9346 | .3805 | 2.6279 | 10 |
| 21° 00' | 0.3584 | 0.9336 | 0.3839 | 2.6051 | 69° 00' |
| 10 | .3611 | .9325 | .3872 | 2.5826 | 50 |
| 20 | .3638 | .9315 | .3906 | 2.5605 | 40 |
| 30 | .3665 | .9304 | .3939 | 2.5386 | 30 |
| 40 | .3692 | .9293 | .3973 | 2.5172 | 20 |
| 50 | .3719 | .9283 | .4006 | 2.4960 | 10 |
| 22° 00' | 0.3746 | 0.9272 | 0.4040 | 2.4751 | 68° 00' |
| 10 | .3773 | .9261 | .4074 | 2.4545 | 50 |
| 20 | .3800 | .9250 | .4108 | 2.4342 | 40 |
| 30 | .3827 | .9239 | .4142 | 2.4142 | 30 |
| 40 | .3854 | .9228 | .4176 | 2.3945 | 20 |
| 50 | .3881 | .9216 | .4210 | 2.3750 | 10 |
| 23° 00' | 0.3907 | 0.9205 | 0.4245 | 2.3559 | 67° 00' |
| 10 | .3934 | .9194 | .4279 | 2.3369 | 50 |
| 20 | .3961 | .9182 | .4314 | 2.3183 | 40 |
| 30 | .3987 | .9171 | .4348 | 2.2998 | 30 |
| 40 | .4014 | .9159 | .4383 | 2.2817 | 20 |
| 50 | .4041 | .9147 | .4417 | 2.2637 | 10 |
| | Cos | Sin | Cot | Tan | Degrees |

Table XXVIII. Natural Trigonometric Functions—(Cont'd)

| Degrees | Sin | Cos | Tan | Cot | |
|---------|--------|--------|--------|--------|---------|
| 24° 00' | 0.4067 | 0.9135 | 0.4452 | 2.2460 | 66° 00' |
| 10 | .4094 | .9124 | .4487 | 2.2286 | 50 |
| 20 | .4120 | .9112 | .4522 | 2.2113 | 40 |
| 30 | .4147 | .9100 | .4557 | 2.1943 | 30 |
| 40 | .4173 | .9088 | .4592 | 2.1775 | 20 |
| 50 | .4200 | .9075 | .4628 | 2.1609 | 10 |
| 25° 00' | 0.4226 | 0.9063 | 0.4663 | 2.1445 | 65° 00' |
| 10 | .4253 | .9051 | .4699 | 2.1283 | 50 |
| 20 | .4279 | .9038 | .4734 | 2.1123 | 40 |
| 30 | .4305 | .9026 | .4770 | 2.0965 | 30 |
| 40 | .4331 | .9013 | .4806 | 2.0809 | 20 |
| 50 | .4358 | .9001 | .4841 | 2.0655 | 10 |
| 26° 00' | 0.4384 | 0.8988 | 0.4877 | 2.0503 | 64° 00' |
| 10 | .4410 | .8975 | .4913 | 2.0353 | 50 |
| 20 | .4436 | .8962 | .4950 | 2.0204 | 40 |
| 30 | .4462 | .8949 | .4986 | 2.0057 | 30 |
| 40 | .4488 | .8936 | .5022 | 1.9912 | 20 |
| 50 | .4514 | .8923 | .5059 | 1.9768 | 10 |
| 27° 00' | 0.4540 | 0.8910 | 0.5095 | 1.9626 | 63° 00' |
| 10 | .4566 | .8897 | .5132 | 1.9486 | 50 |
| 20 | .4592 | .8884 | .5169 | 1.9347 | 40 |
| 30 | .4617 | .8870 | .5206 | 1.9210 | 30 |
| 40 | .4643 | .8857 | .5243 | 1.9074 | 20 |
| 50 | .4669 | .8843 | .5280 | 1.8940 | 10 |
| 28° 00' | 0.4695 | 0.8829 | 0.5317 | 1.8807 | 62° 00' |
| 10 | .4720 | .8816 | .5354 | 1.8676 | 50 |
| 20 | .4746 | .8802 | .5392 | 1.8546 | 40 |
| 30 | .4772 | .8788 | .5430 | 1.8418 | 30 |
| 40 | .4797 | .8774 | .5467 | 1.8291 | 20 |
| 50 | .4823 | .8760 | .5505 | 1.8165 | 10 |
| 29° 00' | 0.4848 | 0.8746 | 0.5543 | 1.8040 | 61° 00' |
| 10 | .4874 | .8732 | .5581 | 1.7917 | 50 |
| 20 | .4899 | .8718 | .5619 | 1.7796 | 40 |
| 30 | .4924 | .8704 | .5658 | 1.7675 | 30 |
| 40 | .4950 | .8689 | .5696 | 1.7556 | 20 |
| 50 | .4975 | .8675 | .5735 | 1.7437 | 10 |
| 30° 00' | 0.5000 | 0.8660 | 0.5774 | 1.7321 | 60° 00' |
| 10 | .5025 | .8646 | .5812 | 1.7205 | 50 |
| 20 | .5050 | .8631 | .5851 | 1.7090 | 40 |
| 30 | .5075 | .8616 | .5890 | 1.6977 | 30 |
| 40 | .5100 | .8601 | .5930 | 1.6864 | 20 |
| 50 | .5125 | .8587 | .5969 | 1.6753 | 10 |
| 31° 00' | 0.5150 | 0.8572 | 0.6009 | 1.6643 | 59° 00' |
| 10 | .5175 | .8557 | .6048 | 1.6534 | 50 |
| 20 | .5200 | .8542 | .6088 | 1.6426 | 40 |
| 30 | .5225 | .8526 | .6128 | 1.6319 | 30 |
| 40 | .5250 | .8511 | .6168 | 1.6212 | 20 |
| 50 | .5275 | .8496 | .6208 | 1.6107 | 10 |
| | Cos | Sin | Cot | Tan | Degrees |

Table XXVIII. Natural Trigonometric Functions—(Cont'd)

| Degrees | Sin | Cos | Tan | Cot | |
|---------|--------|--------|--------|--------|---------|
| 32° 00' | 0.5299 | 0.8480 | 0.6249 | 1.6003 | 58° 00' |
| 10 | .5324 | .8465 | .6289 | 1.5900 | 50 |
| 20 | .5348 | .8450 | .6330 | 1.5798 | 40 |
| 30 | .5373 | .8434 | .6371 | 1.5697 | 30 |
| 40 | .5398 | .8418 | .6412 | 1.5597 | 20 |
| 50 | .5422 | .8403 | .6453 | 1.5497 | 10 |
| 33° 00' | 0.5446 | 0.8387 | 0.6494 | 1.5399 | 57° 00' |
| 10 | .5471 | .8371 | .6536 | 1.5301 | 50 |
| 20 | .5495 | .8355 | .6577 | 1.5204 | 40 |
| 30 | .5519 | .8339 | .6619 | 1.5108 | 30 |
| 40 | .5544 | .8323 | .6661 | 1.5013 | 20 |
| 50 | .5568 | .8307 | .6703 | 1.4919 | 10 |
| 34° 00' | 0.5592 | 0.8290 | 0.6745 | 1.4826 | 56° 00' |
| 10 | .5616 | .8274 | .6787 | 1.4733 | 50 |
| 20 | .5640 | .8258 | .6830 | 1.4641 | 40 |
| 30 | .5664 | .8241 | .6873 | 1.4550 | 30 |
| 40 | .5688 | .8225 | .6916 | 1.4460 | 20 |
| 50 | .5712 | .8208 | .6959 | 1.4370 | 10 |
| 35° 00' | 0.5736 | 0.8192 | 0.7002 | 1.4281 | 55° 00' |
| 10 | .5760 | .8175 | .7046 | 1.4193 | 50 |
| 20 | .5783 | .8158 | .7089 | 1.4106 | 40 |
| 30 | .5807 | .8141 | .7133 | 1.4019 | 30 |
| 40 | .5831 | .8124 | .7177 | 1.3934 | 20 |
| 50 | .5854 | .8107 | .7221 | 1.3848 | 10 |
| 36° 00' | 0.5878 | 0.8090 | 0.7265 | 1.3764 | 54° 00' |
| 10 | .5901 | .8073 | .7310 | 1.3680 | 50 |
| 20 | .5925 | .8056 | .7355 | 1.3597 | 40 |
| 30 | .5948 | .8039 | .7400 | 1.3514 | 30 |
| 40 | .5972 | .8021 | .7445 | 1.3432 | 20 |
| 50 | .5995 | .8004 | .7490 | 1.3351 | 10 |
| 37° 00' | .6018 | .7986 | .7536 | 1.3270 | 53° 00' |
| 10 | .6041 | .7969 | .7581 | 1.3190 | 50 |
| 20 | .6065 | .7951 | .7627 | 1.3111 | 40 |
| 30 | .6088 | .7934 | .7673 | 1.3032 | 30 |
| 40 | .6111 | .7916 | .7720 | 1.2954 | 20 |
| 50 | .6134 | .7898 | .7766 | 1.2876 | 10 |
| 38° 00' | 0.6157 | 0.7880 | 0.7813 | 1.2799 | 52° 00' |
| 10 | .6180 | .7862 | .7860 | 1.2723 | 50 |
| 20 | .6202 | .7844 | .7907 | 1.2647 | 40 |
| 30 | .6225 | .7826 | .7954 | 1.2572 | 30 |
| 40 | .6248 | .7808 | .8002 | 1.2497 | 20 |
| 50 | .6271 | .7790 | .8050 | 1.2423 | 10 |
| 39° 00' | 0.6293 | 0.7771 | 0.8098 | 1.2349 | 51° 00' |
| 10 | .6316 | .7753 | .8146 | 1.2276 | 50 |
| 20 | .6338 | .7735 | .8195 | 1.2203 | 40 |
| 30 | .6361 | .7716 | .8243 | 1.2131 | 30 |
| 40 | .6383 | .7698 | .8292 | 1.2059 | 20 |
| 50 | .6406 | .7679 | .8342 | 1.1988 | 10 |
| | Cos | Sin | Cot | Tan | Degrees |

Table XXVIII. Natural Trigonometric Functions—(Cont'd)

| Degrees | Sin | Cos | Tan | Cot | |
|---------|--------|--------|--------|--------|---------|
| 40° 00' | 0.6428 | 0.7660 | 0.8391 | 1.1918 | 50° 00' |
| 10 | .6450 | .7642 | .8441 | 1.1847 | 50 |
| 20 | .6472 | .7623 | .8491 | 1.1778 | 40 |
| 30 | .6494 | .7604 | .8541 | 1.1708 | 30 |
| 40 | .6517 | .7585 | .8591 | 1.1640 | 20 |
| 50 | .6539 | .7566 | .8642 | 1.1571 | 10 |
| 41° 00' | 0.6561 | 0.7547 | 0.8693 | 1.1504 | 49° 00' |
| 10 | .6583 | .7528 | .8744 | 1.1436 | 50 |
| 20 | .6604 | .7509 | .8796 | 1.1369 | 40 |
| 30 | .6626 | .7490 | .8847 | 1.1303 | 30 |
| 40 | .6648 | .7470 | .8899 | 1.1237 | 20 |
| 50 | .6670 | .7451 | .8952 | 1.1171 | 10 |
| 42° 00' | 0.6691 | 0.7431 | 0.9004 | 1.1106 | 48° 00' |
| 10 | .6713 | .7412 | .9057 | 1.1041 | 50 |
| 20 | .6734 | .7392 | .9110 | 1.0977 | 40 |
| 30 | .6756 | .7373 | .9163 | 1.0913 | 30 |
| 40 | .6777 | .7353 | .9217 | 1.0850 | 20 |
| 50 | .6799 | .7333 | .9271 | 1.0786 | 10 |
| 43° 00' | 0.6820 | 0.7314 | 0.9325 | 1.0724 | 47° 00' |
| 10 | .6841 | .7294 | .9380 | 1.0661 | 50 |
| 20 | .6862 | .7274 | .9435 | 1.0599 | 40 |
| 30 | .6884 | .7254 | .9490 | 1.0538 | 30 |
| 40 | .6905 | .7234 | .9545 | 1.0477 | 20 |
| 50 | .6926 | .7214 | .9601 | 1.0416 | 10 |
| 44° 00' | 0.6947 | 0.7193 | 0.9657 | 1.0355 | 46° 00' |
| 10 | .6967 | .7173 | .9713 | 1.0295 | 50 |
| 20 | .6988 | .7163 | .9770 | 1.0235 | 40 |
| 30 | .7009 | .7133 | .9827 | 1.0176 | 30 |
| 40 | .7030 | .7112 | .9884 | 1.0117 | 20 |
| 50 | .7050 | .7092 | .9942 | 1.0058 | 10 |
| 45° 00' | 0.7071 | 0.7071 | 1.0000 | 1.0000 | 45° 00' |
| | Cos | Sin | Cot | Tan | Degrees |

75. BINARY NUMBERS

(A) Binary Digits

In the binary system of numbers, there are only two digits—0 and 1. All numbers are written as successive powers of 2. Actually, in the decimal system, all numbers are written as successive powers of 10, although we don't normally think of them in this way. For example, decimal 3487 is actually:

$$\begin{array}{r}
 3 \times 10^3 = 3000 \\
 4 \times 10^2 = 400 \\
 8 \times 10^1 = 80 \\
 7 \times 10^0 = \underline{7} \\
 \hline
 3487
 \end{array}$$

With binary numbers, a like system is used except the base (radix) is 2 instead of 10. For example, the binary numbers corresponding to decimal numbers 0 through 10 are 0, 1, 10, 11, 100, 101, 110, 111, 1000, 1001, 1010. Each number is written as a succession of powers of 2. For example, binary 1010 actually means:

$$\begin{array}{r} 1 \times 2^3 = 8 \\ + 1 \times 2^1 = 2 \\ \hline 10 \end{array}$$

The powers of 2, from 0 to 20, are given in Table XXIX. Thus, to write a number above decimal 1,048,056 using binary numbers requires a minimum of 21 digits!

Table XXIX. Powers of 2

| Power | Decimal | Power | Decimal | Power | Decimal |
|-------|---------|----------|---------|----------|-----------|
| 2^0 | 1 | 2^7 | 128 | 2^{14} | 16,384 |
| 2^1 | 2 | 2^8 | 256 | 2^{15} | 32,768 |
| 2^2 | 4 | 2^9 | 512 | 2^{16} | 65,536 |
| 2^3 | 8 | 2^{10} | 1,024 | 2^{17} | 131,072 |
| 2^4 | 16 | 2^{11} | 2,048 | 2^{18} | 262,144 |
| 2^5 | 32 | 2^{12} | 4,096 | 2^{19} | 524,288 |
| 2^6 | 64 | 2^{13} | 8,192 | 2^{20} | 1,048,576 |

(B) Conversion

To convert from binary to decimal or from decimal to binary, you could use Table XXIX and compute the equivalent in the other numbering system as was done in the previous section. However, there are simpler methods. To convert from decimal to binary, successively divide the decimal number by 2. Write down a 1 if there is a remainder and a 0 if not, until the division gives a 0. For example, to convert decimal 22 to binary:

$$\begin{array}{r} 2)22 \\ \hline 2)11 \quad R = 0 \\ 2)5 \quad R = 1 \\ 2)2 \quad R = 1 \\ 2)1 \quad R = 0 \\ \hline 0 \quad R = 1 \end{array}$$

The least significant figure is at the top; thus, the binary number corresponding to decimal 22 is 10110.

To convert from binary to decimal, take the first binary digit, double it, and add your answer to the second digit. Write this sum under the second digit. Then double this number, add it to the third digit, and write the sum under the third digit. Continue this process up to and including the last digit, as follows:

| | | | | | |
|---|---|---|----|----|----|
| 1 | 0 | 1 | 1 | 0 | 1 |
| | 2 | 5 | 11 | 22 | 45 |

The number under the last digit (45) is the decimal equivalent of binary 101101.

(C) Addition

Binary addition has only four rules:

| | | | |
|---|---|---|----|
| 0 | 0 | 1 | 1 |
| 0 | 1 | 0 | 1 |
| 0 | 1 | 1 | 10 |

Following these rules, any binary number can be added. Thus:

$$\begin{array}{r} 1011 \\ 110 \\ \hline 10001 \end{array}$$

To simplify the carry when $1 + 1 = 10$, place the carry under the next digit. Then add the partial total and the carries, as follows:

$$\begin{array}{r} 111101 \\ 10110 \\ \hline 101011 \\ 11 \\ \hline 1010011 \end{array}$$

(D) Subtraction

Binary numbers can be subtracted directly, as follows:

$$\begin{array}{r} 1111 \\ - 111 \\ \hline 1000 \end{array}$$

However, a simpler method is to complement the subtracted number and add. In the binary system, a number is

complemented by merely changing all 0's to 1's and all 1's to 0's and adding 1 to the final digit. Thus:

$$\begin{array}{r} 1111 \\ -0111 \\ \hline \end{array} \quad \text{complemented} \quad \begin{array}{r} 1111 \\ +1001 \\ \hline 11000 \end{array}$$

The first digit in the answer is disregarded. Hence, the answer is 1000 (decimal 8), the same as before.

(E) Multiplication

Binary multiplication is similar to decimal multiplication. All products are the same as in decimal multiplication. That is:

$$\begin{aligned} 0 \times 0 &= 0 \\ 1 \times 0 &= 0 \\ 1 \times 1 &= 1 \end{aligned}$$

To multiply 1011 by 101:

$$\begin{array}{r} 1011 \\ 0101 \\ \hline 1011 \\ 0000 \\ 1011 \\ \hline 110111 \end{array}$$

(F) Division

Binary division is similar to decimal division. Thus, to divide 1101001 by 101:

$$\begin{array}{r} 10101 \\ 101 \overline{)1101001} \\ \underline{101} \\ 110 \\ \underline{101} \\ 101 \\ \underline{101} \\ 0000 \end{array}$$

76. FUNDAMENTALS OF BOOLEAN ALGEBRA

Boolean algebra is based on symbolic logic, which states that an idea must be either true or false—it can be nothing else. The symbols A, B, and C are used to designate the various conditions (or computer inputs). Two connectives—AND and OR—express the relationship between two statements.

OR is the logical equivalent of a parallel switch circuit. That is, a statement is true if any switch is closed, or if they are all closed. OR is symbolized by a + sign. Thus, "A OR B" is written "A + B."

AND is the logical equivalent of a series switch circuit—all switches must be closed to satisfy the condition. AND is symbolized by a multiplication sign ($A \cdot B$) or no sign at all. For example, $A \cdot B$ and AB both mean A AND B. The various symbols are given in Table XXX. Table XXXI summarizes the various logical statements, explains their meanings, and shows the equivalent switch circuit for the statement.

Table XXX. Basic Rules of Symbolic Logic

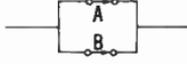
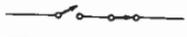
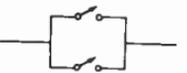
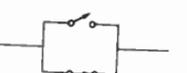
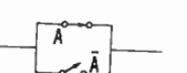
| Symbol | Logic | Switch | Meaning | Circuit |
|-------------------|----------|---------|---|---|
| 1 | True | Closed | The statement is true, the circuit is closed. |  |
| 0 | False | Open | The statement is false, the circuit is open. |  |
| · | Series | A and B | A is in series with B. |  |
| + | Parallel | A or B | A is in parallel with B. |  |
| \bar{A} or A' | Not A | | Opposite of A (If $A = 0$, $\bar{A} = 1$; if $A = 1$, $\bar{A} = 0$). | |

Table XXXI. Summary of Logical Statements

| Logic | Meaning | Circuit |
|-----------------------|---|---|
| $0 \cdot 0 = 0$ | An open in series with an open is open. |  |
| $0 \cdot 1 = 0$ | An open in series with a closed is open. |  |
| $1 \cdot 1 = 1$ | A closed in series with a closed is closed. |  |
| $A \cdot \bar{A} = 0$ | A switch in series with its negation is open. |  |
| $0 + 0 = 0$ | An open in parallel with an open is open. |  |
| $0 + 1 = 1$ | An open in parallel with a closed is closed. |  |
| $1 + 1 = 1$ | A closed in parallel with a closed is closed. |  |
| $A + \bar{A} = 1$ | A switch in parallel with its negation is closed. |  |

77. COMMON LOGARITHMS

The logarithm of a quantity is the power to which a given number (base) must be raised in order to equal that quantity. Thus, any number may be used as the base. The most common system is the base 10. Logarithms with the base 10 are known as common, or Briggs, logarithms; they are written \log_{10} , or simply \log . When the base is omitted, the base 10 is understood.

A common logarithm of a given number is the number which, when applied to the number 10 as an exponent, will produce the given number. Thus, 2 is the common logarithm of 100, since 10^2 equals 100; 3 is the logarithm of 1000, since 10^3 equals 1000, etc. From this we can see that the logarithm of any number except a whole number power of 10 consists of a whole number and a decimal fraction.

(A) Characteristic of a Logarithm

The whole-number portion of a logarithm is called the *characteristic*. The characteristic of a whole number, or of

a whole number and a fraction, has a positive value equal to one less than the number of digits preceding the decimal point. The characteristic of a decimal fraction has a negative value equal to one more than the number of zeros immediately following the decimal point. The characteristics of numbers between .0001 and 99,999 are:

| Numbers | Characteristic |
|------------------|----------------|
| .0001 to .0009 | -4 |
| .001 to .009 | -3 |
| .01 to .09 | -2 |
| .1 to .9 | -1 |
| 1 to 9 | 0 |
| 10 to 99 | 1 |
| 100 to 999 | 2 |
| 1,000 to 9,999 | 3 |
| 10,000 to 99,999 | 4 |

(B) Use of Logarithm Table

The *mantissa*, or decimal-fraction portion, of a logarithm is obtained from Table XXXII. To find the mantissa for the logarithm of any number, locate the first two figures of the number in the left-hand column (N); then, in the column under the third figure of the number, the mantissa for that number will be found.

For example, to find the logarithm of 6673, first locate 66 in the left-hand column (N); then follow across to the column numbered 7. The mantissa for 667 (.8241) is located at this point. The characteristic for the logarithm of 6673 is 3. Therefore, the logarithm of 6670 is 3.8241. For most computations, greater accuracy will not be required.

If accuracy to four places is desired, the columns labeled *Proportional Parts* may be used. These columns list the numbers to be added to the logarithm to obtain four-place accuracy. In the foregoing, we obtained the logarithm for 6670 (3.8241), but we wanted the logarithm for 6673; therefore, we use the *proportional parts* column to find the proportional part for 3. This is 2. Therefore, the logarithm for 6673 is 3.8241 plus .0002, or 3.8243.

The *mantissa* of a logarithm is usually *positive*, whereas a *characteristic* may be either *positive* or *negative*. The total logarithm is the sum of the mantissa and the characteristic.

Thus, the mantissa of .0234 is .3692, and the characteristic is -2 . The total logarithm is $-2 + .3692$, or -1.6308 . A negative logarithm is difficult to use; therefore, it is more convenient to convert the logarithm to a positive number. This is possible by adding 10, or a multiple thereof, to the characteristic when it is negative, and compensating for this by indicating the subtraction of 10 from the entire logarithm. Thus, the logarithm of .0234 would be written $8.3692 - 10$, since $-2 + .3692$ equals $8 + .3692 - 10$. This logarithm may now be used like any other positive logarithm, except that the -10 must be considered in determining the characteristic of the answer.

(C) Antilogarithms

An antilogarithm (abbreviated *antilog* or \log^{-1}) is a number corresponding to a given logarithm. To find an antilog, locate in the logarithm table the mantissa closest to that of the given logarithm. Record the number in the *N* column directly opposite the mantissa located, and annex to this the number on the top line immediately above the mantissa. Next determine where the decimal point is located, by counting off the number of places indicated by the characteristic. Starting between the first and second digits, count to the right if the characteristic is positive, and to the left if it is negative. If greater accuracy is desired, the *proportional parts* columns of the logarithm table can be used, in the same manner described in the foregoing for finding the mantissa.

To find the antilog of 3.4548, locate 4548 in the table. Then read the first two figures of the antilog from the *N* column (28) and the third figure directly above the mantissa (5). Thus, the three figures of the antilog are 285. Locate the decimal point by counting off three places to the right, from the point between the 2 and the 8, to obtain 2850.0—the antilog of 3.4548.

In the foregoing example, if the logarithm had been $-2 + .4548$, the procedure would have been the same except for the location of the decimal point. The decimal point in this example would be located by starting at the point between the 2 and the 8, and counting two places to the left to obtain 0.0285—the antilog of $-2 + .4548$.

(D) Multiplication

Numbers are multiplied by adding their logarithms and finding the antilog of the sum. For example, to multiply 682×497 , proceed as follows:

$$\begin{aligned} \log N &= \log 682 + \log 497 \\ \log 682 &= 2.8338 \\ + \log 497 &= \underline{2.6964} \\ \log N &= 5.5302 \\ \text{antilog } 5.5302 &= 339,000. \end{aligned}$$

To multiply $.02 \times .03 \times .5$, proceed as follows:

$$\begin{aligned} \log N &= \log .02 + \log .03 + \log .5 \\ \log .02 &= -2 + .3010 = 8.3010 - 10 \\ + \log .03 &= -2 + .4771 = 8.4771 - 10 \\ + \log .5 &= -1 + .6990 = \underline{9.6990 - 10} \\ \log N &= 26.4771 - 30 \\ &= -4 + .4771 \\ \text{antilog } -4 + .4771 &= .0003 \end{aligned}$$

(E) Division

Numbers are divided by subtracting the logarithm of the divisor from the logarithm of the dividend, and finding the antilog of the difference. For example, to divide 39,200 by 27.2, proceed as follows:

$$\begin{aligned} \log N &= \log 39,200 - \log 27.2 \\ \log 39,200 &= 4.5933 \\ - \log 27.2 &= \underline{1.4346} \\ \log N &= 3.1587 \\ \text{antilog } 3.1587 &= 1441 \end{aligned}$$

To divide .3 by .007, proceed as follows:

$$\begin{aligned} \log N &= \log .3 - \log .007 \\ \log .3 &= -1 + .4771 = 9.4771 - 10 \\ -\log .007 &= -3 + .8451 = \underline{7.8451 - 10} \\ \log N &= 1.6320 - 0 \\ \text{antilog } 1.6320 &= 42.86 \end{aligned}$$

(F) Raising to Powers

A given number can be raised to any power by multiplying the logarithm of the given number by the power to which the number is to be raised, and finding the antilog of the product. For example, to raise 39.7 to the third power, proceed as follows:

$$\begin{aligned} \log N &= \log 39.7 \times 3 \\ \log 39.7 &= 1.5988 \\ \log N &= 1.5988 \times 3 \\ &= 4.7964 \\ \text{antilog } 4.7964 &= 62,570 \end{aligned}$$

(G) Extracting Roots

Any root can be extracted from a given number by dividing the logarithm of the given number by the index of the root, and finding the antilog of the quotient. For example, to extract the cube root of 149, proceed as follows:

$$\begin{aligned} \log N &= \log 149 \div 3 \\ \log 149 &= 2.1732 \\ \log N &= 2.1732 \div 3 \\ &= 0.7244 \\ \text{antilog } 0.7244 &= 5.301 \end{aligned}$$

Table XXXII. Common Logarithms

| N | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Proportional Parts | | | | | | | | |
|----|------|------|------|------|------|------|------|------|------|------|--------------------|---|----|----|----|----|----|----|----|
| | | | | | | | | | | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 10 | 0000 | 0043 | 0086 | 0128 | 0170 | 0212 | 0253 | 0294 | 0334 | 0374 | 4 | 8 | 12 | 17 | 21 | 25 | 29 | 33 | 37 |
| 11 | 0414 | 0453 | 0492 | 0531 | 0569 | 0607 | 0645 | 0682 | 0719 | 0755 | 4 | 8 | 11 | 15 | 19 | 23 | 26 | 30 | 34 |
| 12 | 0792 | 0828 | 0864 | 0899 | 0934 | 0969 | 1004 | 1038 | 1072 | 1106 | 3 | 7 | 10 | 14 | 17 | 21 | 24 | 28 | 31 |
| 13 | 1139 | 1173 | 1206 | 1239 | 1271 | 1303 | 1335 | 1367 | 1399 | 1430 | 3 | 6 | 10 | 13 | 16 | 19 | 23 | 26 | 29 |
| 14 | 1461 | 1492 | 1523 | 1553 | 1584 | 1614 | 1644 | 1673 | 1703 | 1732 | 3 | 6 | 9 | 12 | 15 | 18 | 21 | 24 | 27 |
| 15 | 1761 | 1790 | 1818 | 1847 | 1875 | 1903 | 1931 | 1959 | 1987 | 2014 | 3 | 6 | 8 | 11 | 14 | 17 | 20 | 22 | 25 |
| 16 | 2041 | 2068 | 2095 | 2122 | 2148 | 2175 | 2201 | 2227 | 2253 | 2279 | 3 | 5 | 8 | 11 | 13 | 16 | 18 | 21 | 24 |
| 17 | 2304 | 2330 | 2355 | 2380 | 2405 | 2430 | 2455 | 2480 | 2504 | 2529 | 2 | 5 | 7 | 10 | 12 | 15 | 17 | 20 | 22 |
| 18 | 2553 | 2577 | 2601 | 2625 | 2648 | 2672 | 2695 | 2718 | 2742 | 2765 | 2 | 5 | 7 | 9 | 12 | 14 | 16 | 19 | 21 |
| 19 | 2788 | 2810 | 2833 | 2856 | 2878 | 2900 | 2923 | 2945 | 2967 | 2989 | 2 | 4 | 7 | 9 | 11 | 13 | 16 | 18 | 20 |
| 20 | 3010 | 3032 | 3054 | 3075 | 3096 | 3118 | 3139 | 3160 | 3181 | 3201 | 2 | 4 | 6 | 8 | 11 | 13 | 15 | 17 | 19 |
| 21 | 3222 | 3243 | 3263 | 3284 | 3304 | 3324 | 3345 | 3365 | 3385 | 3404 | 2 | 4 | 6 | 8 | 10 | 12 | 14 | 16 | 18 |
| 22 | 3424 | 3444 | 3464 | 3483 | 3502 | 3522 | 3541 | 3560 | 3579 | 3598 | 2 | 4 | 6 | 8 | 10 | 12 | 14 | 15 | 17 |
| 23 | 3617 | 3636 | 3655 | 3674 | 3692 | 3711 | 3729 | 3747 | 3766 | 3784 | 2 | 4 | 6 | 7 | 9 | 11 | 13 | 15 | 17 |
| 24 | 3802 | 3820 | 3838 | 3856 | 3874 | 3892 | 3909 | 3927 | 3945 | 3962 | 2 | 4 | 5 | 7 | 9 | 11 | 12 | 14 | 16 |
| 25 | 3979 | 3997 | 4014 | 4031 | 4048 | 4065 | 4082 | 4099 | 4116 | 4133 | 2 | 3 | 5 | 7 | 9 | 10 | 12 | 14 | 15 |
| 26 | 4150 | 4166 | 4183 | 4200 | 4216 | 4232 | 4249 | 4265 | 4281 | 4298 | 2 | 3 | 5 | 7 | 8 | 10 | 11 | 13 | 15 |
| 27 | 4314 | 4330 | 4346 | 4362 | 4378 | 4393 | 4409 | 4425 | 4440 | 4456 | 2 | 3 | 5 | 6 | 8 | 9 | 11 | 13 | 14 |
| 28 | 4472 | 4487 | 4502 | 4518 | 4533 | 4548 | 4564 | 4579 | 4594 | 4609 | 2 | 3 | 5 | 6 | 8 | 9 | 11 | 12 | 14 |
| 29 | 4624 | 4639 | 4654 | 4669 | 4683 | 4698 | 4713 | 4728 | 4742 | 4757 | 1 | 3 | 4 | 6 | 7 | 9 | 10 | 12 | 13 |
| 30 | 4771 | 4786 | 4800 | 4814 | 4829 | 4843 | 4857 | 4871 | 4886 | 4900 | 1 | 3 | 4 | 6 | 7 | 9 | 10 | 11 | 13 |
| 31 | 4914 | 4928 | 4942 | 4955 | 4969 | 4983 | 4997 | 5011 | 5024 | 5038 | 1 | 3 | 4 | 6 | 7 | 8 | 10 | 11 | 12 |
| 32 | 5051 | 5065 | 5079 | 5092 | 5105 | 5119 | 5132 | 5145 | 5159 | 5172 | 1 | 3 | 4 | 5 | 7 | 8 | 9 | 11 | 12 |
| 33 | 5185 | 5198 | 5211 | 5224 | 5237 | 5250 | 5263 | 5276 | 5289 | 5302 | 1 | 3 | 4 | 5 | 6 | 8 | 9 | 10 | 12 |
| 34 | 5315 | 5328 | 5340 | 5353 | 5366 | 5378 | 5391 | 5403 | 5416 | 5428 | 1 | 3 | 4 | 5 | 6 | 8 | 9 | 10 | 11 |
| N | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Proportional Parts | | | | | | | | |
| | | | | | | | | | | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |

Table XXXII. Common Logarithms—(Cont'd)

| N | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Proportional Parts | | | | | | | | |
|----|------|------|------|------|------|------|------|------|------|------|--------------------|---|---|---|---|---|---|----|----|
| | | | | | | | | | | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 35 | 5441 | 5453 | 5465 | 5478 | 5490 | 5502 | 5514 | 5527 | 5539 | 5551 | 1 | 2 | 4 | 5 | 6 | 7 | 9 | 10 | 11 |
| 36 | 5563 | 5575 | 5587 | 5599 | 5611 | 5623 | 5635 | 5647 | 5658 | 5670 | 1 | 2 | 4 | 5 | 6 | 7 | 8 | 10 | 11 |
| 37 | 5682 | 5694 | 5705 | 5717 | 5729 | 5740 | 5752 | 5763 | 5775 | 5786 | 1 | 2 | 3 | 5 | 6 | 7 | 8 | 9 | 10 |
| 38 | 5798 | 5809 | 5821 | 5832 | 5843 | 5855 | 5866 | 5877 | 5888 | 5899 | 1 | 2 | 3 | 5 | 6 | 7 | 8 | 9 | 10 |
| 39 | 5911 | 5922 | 5933 | 5944 | 5955 | 5966 | 5977 | 5988 | 5999 | 6010 | 1 | 2 | 3 | 4 | 5 | 7 | 8 | 9 | 10 |
| 40 | 6021 | 6031 | 6042 | 6053 | 6064 | 6075 | 6085 | 6096 | 6107 | 6117 | 1 | 2 | 3 | 4 | 5 | 6 | 8 | 9 | 10 |
| 41 | 6128 | 6138 | 6149 | 6160 | 6170 | 6180 | 6191 | 6201 | 6212 | 6222 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 42 | 6232 | 6243 | 6253 | 6263 | 6274 | 6284 | 6294 | 6304 | 6314 | 6325 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 43 | 6335 | 6345 | 6355 | 6365 | 6375 | 6385 | 6395 | 6405 | 6415 | 6425 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 44 | 6435 | 6444 | 6454 | 6464 | 6474 | 6484 | 6493 | 6503 | 6513 | 6522 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 45 | 6532 | 6542 | 6551 | 6561 | 6571 | 6580 | 6590 | 6599 | 6609 | 6618 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 46 | 6628 | 6637 | 6646 | 6656 | 6665 | 6675 | 6684 | 6693 | 6702 | 6712 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 7 | 8 |
| 47 | 6721 | 6730 | 6739 | 6749 | 6758 | 6767 | 6776 | 6785 | 6794 | 6803 | 1 | 2 | 3 | 4 | 5 | 5 | 6 | 7 | 8 |
| 48 | 6812 | 6821 | 6830 | 6839 | 6848 | 6857 | 6866 | 6875 | 6884 | 6893 | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 7 | 8 |
| 49 | 6902 | 6911 | 6920 | 6928 | 6937 | 6946 | 6955 | 6964 | 6972 | 6981 | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 7 | 8 |
| 50 | 6990 | 6998 | 7007 | 7016 | 7024 | 7033 | 7042 | 7050 | 7059 | 7067 | 1 | 2 | 3 | 3 | 4 | 5 | 6 | 7 | 8 |
| 51 | 7076 | 7084 | 7093 | 7101 | 7110 | 7118 | 7126 | 7135 | 7143 | 7152 | 1 | 2 | 3 | 3 | 4 | 5 | 6 | 7 | 8 |
| 52 | 7160 | 7168 | 7177 | 7185 | 7193 | 7202 | 7210 | 7218 | 7226 | 7235 | 1 | 2 | 2 | 3 | 4 | 5 | 6 | 7 | 7 |
| 53 | 7243 | 7251 | 7259 | 7267 | 7275 | 7284 | 7292 | 7300 | 7308 | 7316 | 1 | 2 | 2 | 3 | 4 | 5 | 6 | 6 | 7 |
| 54 | 7324 | 7332 | 7340 | 7348 | 7356 | 7364 | 7372 | 7380 | 7388 | 7396 | 1 | 2 | 2 | 3 | 4 | 5 | 6 | 6 | 7 |
| 55 | 7404 | 7412 | 7419 | 7427 | 7435 | 7443 | 7451 | 7459 | 7466 | 7474 | 1 | 2 | 2 | 3 | 4 | 5 | 5 | 6 | 7 |
| 56 | 7482 | 7490 | 7497 | 7505 | 7513 | 7520 | 7528 | 7536 | 7543 | 7551 | 1 | 2 | 2 | 3 | 4 | 5 | 5 | 6 | 7 |
| 57 | 7559 | 7566 | 7574 | 7582 | 7589 | 7597 | 7604 | 7612 | 7619 | 7627 | 1 | 2 | 2 | 3 | 4 | 5 | 5 | 6 | 7 |
| 58 | 7634 | 7642 | 7649 | 7657 | 7664 | 7672 | 7679 | 7686 | 7694 | 7701 | 1 | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 7 |
| 59 | 7709 | 7716 | 7723 | 7731 | 7738 | 7745 | 7752 | 7760 | 7767 | 7774 | 1 | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 7 |
| N | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Proportional Parts | | | | | | | | |
| | | | | | | | | | | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |

Table XXXII. Common Logarithms—(Cont'd)

| N | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Proportional Parts | | | | | | | | |
|----|------|------|------|------|------|------|------|------|------|------|--------------------|---|---|---|---|---|---|---|---|
| | | | | | | | | | | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 60 | 7782 | 7789 | 7796 | 7803 | 7810 | 7818 | 7825 | 7832 | 7839 | 7846 | 1 | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 6 |
| 61 | 7853 | 7860 | 7868 | 7875 | 7882 | 7889 | 7896 | 7903 | 7910 | 7917 | 1 | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 6 |
| 62 | 7924 | 7931 | 7938 | 7945 | 7952 | 7959 | 7966 | 7973 | 7980 | 7987 | 1 | 1 | 2 | 3 | 3 | 4 | 5 | 6 | 6 |
| 63 | 7993 | 8000 | 8007 | 8014 | 8021 | 8028 | 8035 | 8041 | 8048 | 8055 | 1 | 1 | 2 | 3 | 3 | 4 | 5 | 5 | 6 |
| 64 | 8062 | 8069 | 8075 | 8082 | 8089 | 8096 | 8102 | 8109 | 8116 | 8122 | 1 | 1 | 2 | 3 | 3 | 4 | 5 | 5 | 6 |
| 65 | 8129 | 8136 | 8142 | 8149 | 8156 | 8162 | 8169 | 8176 | 8182 | 8189 | 1 | 1 | 2 | 3 | 3 | 4 | 5 | 5 | 6 |
| 66 | 8195 | 8202 | 8209 | 8215 | 8222 | 8228 | 8235 | 8241 | 8248 | 8254 | 1 | 1 | 2 | 3 | 3 | 4 | 5 | 5 | 6 |
| 67 | 8261 | 8267 | 8274 | 8280 | 8287 | 8293 | 8299 | 8306 | 8312 | 8319 | 1 | 1 | 2 | 3 | 3 | 4 | 4 | 5 | 6 |
| 68 | 8325 | 8331 | 8338 | 8344 | 8351 | 8357 | 8363 | 8370 | 8376 | 8382 | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 6 |
| 69 | 8388 | 8395 | 8401 | 8407 | 8414 | 8420 | 8426 | 8432 | 8439 | 8445 | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 6 |
| 70 | 8451 | 8457 | 8463 | 8470 | 8476 | 8482 | 8488 | 8494 | 8500 | 8506 | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 5 |
| 71 | 8513 | 8519 | 8525 | 8531 | 8537 | 8543 | 8549 | 8555 | 8561 | 8567 | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 5 |
| 72 | 8573 | 8579 | 8585 | 8591 | 8597 | 8603 | 8609 | 8615 | 8621 | 8627 | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 5 |
| 73 | 8633 | 8639 | 8645 | 8651 | 8657 | 8663 | 8669 | 8675 | 8681 | 8686 | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 5 |
| 74 | 8692 | 8698 | 8704 | 8710 | 8716 | 8722 | 8727 | 8733 | 8739 | 8745 | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 5 |
| 75 | 8751 | 8756 | 8762 | 8768 | 8774 | 8779 | 8785 | 8791 | 8797 | 8802 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 5 | 5 |
| 76 | 8808 | 8814 | 8820 | 8825 | 8831 | 8837 | 8842 | 8848 | 8854 | 8859 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 77 | 8865 | 8871 | 8876 | 8882 | 8887 | 8893 | 8899 | 8904 | 8910 | 8915 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 78 | 8921 | 8927 | 8932 | 8938 | 8943 | 8949 | 8954 | 8960 | 8965 | 8971 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 79 | 8976 | 8982 | 8987 | 8993 | 8998 | 9004 | 9009 | 9015 | 9020 | 9025 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 80 | 9031 | 9036 | 9042 | 9047 | 9053 | 9058 | 9063 | 9069 | 9074 | 9079 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 81 | 9085 | 9090 | 9096 | 9101 | 9106 | 9112 | 9117 | 9122 | 9128 | 9133 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 82 | 9138 | 9143 | 9149 | 9154 | 9159 | 9165 | 9170 | 9175 | 9180 | 9186 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 83 | 9191 | 9196 | 9201 | 9206 | 9212 | 9217 | 9222 | 9227 | 9232 | 9238 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 84 | 9243 | 9248 | 9253 | 9258 | 9263 | 9269 | 9274 | 9279 | 9284 | 9289 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| N | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Proportional Parts | | | | | | | | |
| | | | | | | | | | | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |

Table XXXII. Common Logarithms—(Cont'd)

| N | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Proportional Parts | | | | | | | | |
|----|------|------|------|------|------|------|------|------|------|------|--------------------|---|---|---|---|---|---|---|---|
| | | | | | | | | | | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 85 | 9294 | 9299 | 9304 | 9309 | 9315 | 9320 | 9325 | 9330 | 9335 | 9340 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 86 | 9345 | 9350 | 9355 | 9360 | 9365 | 9370 | 9375 | 9380 | 9385 | 9390 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 87 | 9395 | 9400 | 9405 | 9410 | 9415 | 9420 | 9425 | 9430 | 9435 | 9440 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 88 | 9445 | 9450 | 9455 | 9460 | 9465 | 9469 | 9474 | 9479 | 9484 | 9489 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 89 | 9494 | 9499 | 9504 | 9509 | 9513 | 9518 | 9523 | 9528 | 9533 | 9538 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 90 | 9542 | 9547 | 9552 | 9557 | 9562 | 9566 | 9571 | 9576 | 9581 | 9586 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 91 | 9590 | 9595 | 9600 | 9605 | 9609 | 9614 | 9619 | 9624 | 9628 | 9633 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 92 | 9638 | 9643 | 9647 | 9652 | 9657 | 9661 | 9666 | 9671 | 9675 | 9680 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 93 | 9685 | 9689 | 9694 | 9699 | 9703 | 9708 | 9713 | 9717 | 9722 | 9727 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 94 | 9731 | 9736 | 9741 | 9745 | 9750 | 9754 | 9759 | 9763 | 9768 | 9773 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 95 | 9777 | 9782 | 9786 | 9791 | 9795 | 9800 | 9805 | 9809 | 9814 | 9818 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 96 | 9823 | 9827 | 9832 | 9836 | 9841 | 9845 | 9850 | 9854 | 9859 | 9863 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 97 | 9868 | 9872 | 9877 | 9881 | 9886 | 9890 | 9894 | 9899 | 9903 | 9908 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 98 | 9912 | 9917 | 9921 | 9926 | 9930 | 9934 | 9939 | 9943 | 9948 | 9952 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 99 | 9956 | 9961 | 9965 | 9969 | 9974 | 9978 | 9983 | 9987 | 9991 | 9996 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 3 | 4 |
| N | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Proportional Parts | | | | | | | | |
| | | | | | | | | | | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |

Miscellaneous

78. POWER CONSUMPTION OF HOME ELECTRICAL EQUIPMENT

The power consumption for many items of home electrical equipment by an average family is given in Table XXXIII. The approximate usage of each item is also listed where applicable.

Table XXXIII. Power Consumption of Home Electrical Equipment

| Item | Approx. Kwh per Month | Remarks |
|--|-----------------------|------------------------------|
| Blanket (automatic) | 15 | 8 hr. per day (used 7 mo.) |
| Clock | 1½ | |
| Coffee Maker | 15 | 25 hr. per mo. |
| Dishwasher | 25 | 1½ washings per day |
| Dryer (clothes) | 50 | 10 hr. per mo. (family of 4) |
| Fan (10-inch) | 1 | 25 hr. per mo. |
| Food Freezer | 40 | 8 cu. ft. |
| Garbage Disposal Unit | ¾ | 4 min. per day |
| Iron | 6 | 12 hr. per mo. |
| Ironer | 10 | 10 hr. per mo. (family of 4) |
| Lighting | 65 | |
| Mixer | ¾ | 5 hr. per mo. |
| Oil Furnace (not including circulator fan) | 30 | (200-500 KW-hours per year) |
| Radio | 10 | 130 hr. per mo. |
| Range | 90 | (Family of 4) |
| Refrigerator | 22 | 8 cu. ft. |
| Roaster | 12 | 16 hr. per mo. |
| Sandwich Grill | 4 | 5 hr. per mo. |
| Sewing Machine | 1 | |
| Television | 18 | 90 hr. per mo. |
| Toaster | 3 | 3 hr. per mo. |
| Vacuum Cleaner (upright) | 2¼ | 6 hr. per mo. |
| Vacuum Cleaner (tank) | 3¼ | 6 hr. per mo. |
| Washer (wringer-type) | 2 | 12 hr. per mo. (family of 4) |
| Washer (automatic) | 3 | 12 hr. per mo. (family of 4) |
| Water Heater | 350 | (Family of 4) |

79. TEMPERATURE CONVERSION

The nomograph in Fig. 145 can be used to convert from degrees Fahrenheit to degrees Celsius (or vice versa) for any temperature between absolute zero and 540°F. (281°C). The term Celsius was officially adopted, in place of centigrade, by international agreement in 1948; however, acceptance of the new term has been slow in Europe, and still slower in the United States. Actually, Celsius and centigrade scales differ slightly—the Celsius scale is based on 0° at the triple point of water (.01°C), and centigrade has 0° at the freezing point of water. For all practical purposes, though, the two terms are interchangeable.

Two absolute temperature scales are also in use. The Fahrenheit absolute scale is called the Rankine—0° Rankine equals -459.67° Fahrenheit. The Celsius absolute scale is the Kelvin—0° Kelvin equals -273.16° Celsius (or centigrade).

The following formulas can be used to convert from any temperature to the other:

$$^{\circ}\text{F.} = (^{\circ}\text{C.} \times 9/5) + 32$$

$$^{\circ}\text{F.} = ^{\circ}\text{R.} - 459.67$$

$$^{\circ}\text{F.} = 9/5 (^{\circ}\text{K.} - 273.16) + 32$$

$$^{\circ}\text{C.} = 5/9 (^{\circ}\text{F.} - 32)$$

$$^{\circ}\text{C.} = ^{\circ}\text{K.} - 273.16$$

$$^{\circ}\text{C.} = 5/9 (^{\circ}\text{R.} - 491.67)$$

$$^{\circ}\text{R.} = ^{\circ}\text{F.} + 459.67$$

$$^{\circ}\text{R.} = (^{\circ}\text{C.} \times 9/5) + 491.67$$

$$^{\circ}\text{R.} = 9/5 (^{\circ}\text{K.} - 273.16) + 491.67$$

$$^{\circ}\text{K.} = ^{\circ}\text{C.} + 273.16$$

$$^{\circ}\text{K.} = 5/9 (^{\circ}\text{F.} - 32) + 273.16$$

$$^{\circ}\text{K.} = 5/9 (^{\circ}\text{R.} - 491.67) + 273.16$$

Temperature Nomograph

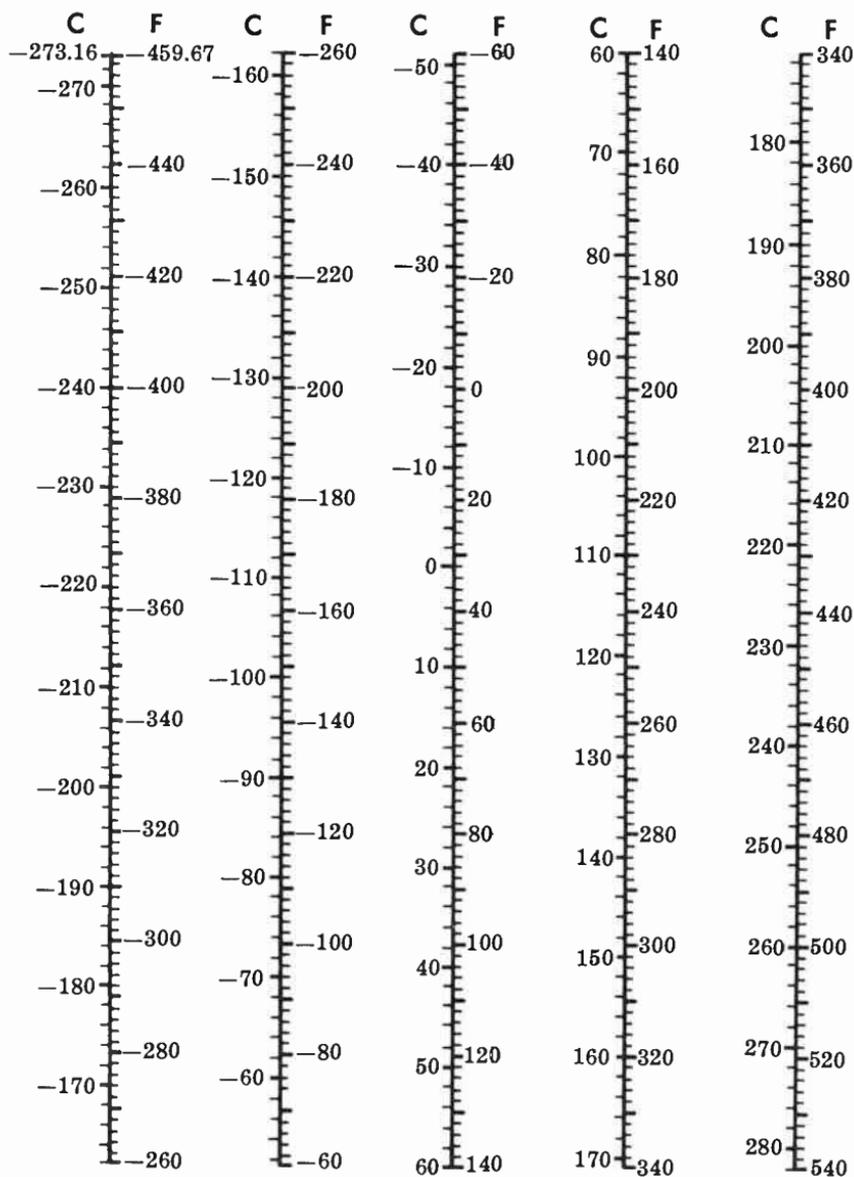


Fig. 145

80. CHARACTERISTICS OF THE ELEMENTS

A list of all the known elements (103) is given in Table XXXIV. The symbol, atomic number, and atomic weight are included for each element. Where known, the melting and boiling point of each element is also given. A value shown in parentheses indicates the value is approximated; the asterisk (*) indicates the mass number of the longest-lived of the known available forms of the element, usually synthetic; < indicates the value may be lower; > indicates the value may be higher.

Table XXXIV. Characteristics of the Elements

| Element | Symbol | Atomic Number | Atomic Weight | Melting Point °C | Boiling Point °C |
|-------------|--------|---------------|---------------|------------------|------------------|
| Actinium | Ac | 89 | *227 | — | — |
| Aluminum | Al | 13 | 26.97 | 660.1 | 1800 |
| Americium | Am | 95 | *243 | — | — |
| Antimony | Sb | 51 | 121.76 | 630.5 | 1380 |
| Argon | A | 18 | 39.944 | -189.2 | -185.7 |
| Arsenic | As | 33 | 74.91 | (820) | 615 |
| Astatine | At | 85 | *210 | — | — |
| Barium | Ba | 56 | 137.36 | 850 | 1140 |
| Berkelium | Bk | 97 | *249 | — | — |
| Beryllium | Be | 4 | 9.013 | 1350 | (1500) |
| Bismuth | Bi | 83 | 209.00 | 271.3 | 1450 |
| Boron | B | 5 | 10.82 | 2300 | 2550 |
| Bromine | Br | 35 | 79.916 | -7.2 | 58.8 |
| Cadmium | Cd | 48 | 112.41 | 320.9 | 766 |
| Calcium | Ca | 20 | 40.08 | 810 | 1170 |
| Californium | Cf | 98 | *249 | — | — |
| Carbon | C | 6 | 12.01 | >3500 | (4200) |
| Cerium | Ce | 58 | 140.13 | 640 | 1400 |
| Cesium | Cs | 55 | 132.91 | 28 | 670 |
| Chlorine | Cl | 17 | 35.457 | -101.6 | -34.7 |
| Chromium | Cr | 24 | 52.01 | 1615 | 2200 |
| Cobalt | Co | 27 | 58.94 | 1492 | 3000 |
| Copper | Cu | 29 | 63.54 | 1083 | 2300 |
| Curium | Cm | 96 | 247 | — | — |
| Dysprosium | Dy | 66 | 162.46 | — | — |
| Einsteinium | E | 99 | *254 | — | — |
| Erbium | Er | 68 | 167.2 | — | — |
| Europium | Eu | 63 | 152.0 | — | — |
| Fermium | Fm | 100 | *255 | — | — |
| Fluorine | F | 9 | 19.00 | -223 | -187 |
| Francium | Fr | 87 | *223 | — | — |
| Gadolinium | Gd | 64 | 156.9 | — | — |
| Gallium | Ga | 31 | 69.72 | 29.7 | >1600 |
| Germanium | Ge | 32 | 72.60 | 958.5 | (2700) |
| Gold | Au | 79 | 197.0 | 1063 | 2600 |

Table XXXIV. Characteristics of the Elements—(Cont'd)

| Element | Symbol | Atomic Number | Atomic Weight | Melting Point °C | Boiling Point °C |
|--------------|--------|---------------|---------------|------------------|------------------|
| Hafnium | Hf | 72 | 178.6 | 1500 | (>3200) |
| Helium | He | 2 | 4.003 | < -271.4 | -268.94 |
| Holmium | Ho | 67 | 164.94 | — | — |
| Hydrogen | H | 1 | 1.0080 | -259.14 | -252.8 |
| Indium | In | 49 | 114.76 | 155 | >1450 |
| Iodine | I | 53 | 126.91 | 113.5 | 184.35 |
| Iridium | Ir | 77 | 192.2 | 2443 | (>4800) |
| Iron | Fe | 26 | 55.85 | 1533 | 3000 |
| Krypton | Kr | 36 | 83.8 | -169 | -151.8 |
| Lanthanum | La | 57 | 138.92 | 826 | 1800 |
| Lawrencium | Lw | 103 | — | — | — |
| Lead | Pb | 82 | 207.21 | 327.4 | 1620 |
| Lithium | Li | 3 | 6.940 | 186 | >1200 |
| Lutetium | Lu | 71 | 174.99 | — | — |
| Magnesium | Mg | 12 | 24.32 | 651 | 1100 |
| Manganese | Mn | 25 | 54.94 | 1260 | 1800 |
| Mendelevium | Mv | 101 | *256 | — | — |
| Mercury | Hg | 80 | 200.61 | -38.87 | 356.9 |
| Molybdenum | Mo | 42 | 95.95 | 2620 | 3700 |
| Neodymium | Nd | 60 | 144.27 | 840 | — |
| Neon | Ne | 10 | 20.183 | -248.67 | -245.9 |
| Neptunium | Np | 93 | *237 | 639 | — |
| Nickel | Ni | 28 | 58.69 | 1453 | 2900 |
| Niobium | Nb | 41 | 92.91 | 2500 | 3200 |
| Nitrogen | N | 7 | 14.008 | -209.86 | -195.81 |
| Nobelium | No | 102 | 251 | — | — |
| Osmium | Os | 76 | 190.2 | 2700 | (>5300) |
| Oxygen | O | 8 | 16.000 | -218.4 | -183 |
| Palladium | Pd | 46 | 106.7 | 1552 | 2200 |
| Phosphorus | P | 15 | 30.975 | 44.1 | 280 |
| Platinum | Pt | 78 | 195.23 | 1769 | 4300 |
| Plutonium | Pu | 94 | 242 | — | — |
| Polonium | Po | 84 | 210 | — | — |
| Potassium | K | 19 | 39.100 | 62.3 | 760 |
| Praseodymium | Pr | 59 | 140.92 | 940 | — |
| Promethium | Pm | 61 | *145 | — | — |
| Protactinium | Pa | 91 | *231 | — | — |
| Radium | Ra | 88 | 226.05 | 960 | 1140 |
| Radon | Rn | 86 | 222 | -110 | — |
| Rhenium | Re | 75 | 186.31 | (3000) | — |
| Rhodium | Rh | 45 | 102.91 | 1960 | >2500 |
| Rubidium | Rb | 37 | 85.48 | 38.5 | 700 |
| Ruthenium | Ru | 44 | 101.1 | 2500 | >2700 |
| Samarium | Sm | 62 | 150.43 | >1300 | — |
| Scandium | Sc | 21 | 44.96 | 1200 | (2400) |
| Selenium | Se | 34 | 78.96 | 220 | 688 |
| Silicon | Si | 14 | 28.09 | 1420 | 2600 |
| Silver | Ag | 47 | 107.880 | 960.8 | 1950 |
| Sodium | Na | 11 | 22.997 | 97.5 | 880 |
| Strontium | Sr | 38 | 87.63 | 800 | 1150 |

Table XXXIV. Characteristics of the Elements—(Cont'd)

| Element | Symbol | Atomic Number | Atomic Weight | Melting Point °C | Boiling Point °C |
|------------|--------|---------------|---------------|------------------|------------------|
| Sulfur | S | 16 | 32.066 | 113-119 | 444.6 |
| Tantalum | Ta | 73 | 180.95 | 3005 | (> 4100) |
| Technetium | Tc | 43 | *99 | — | — |
| Tellurium | Te | 52 | 127.61 | 452 | 1390 |
| Terbium | Tb | 65 | 158.93 | 327 | — |
| Thallium | Tl | 81 | 204.39 | 303.5 | 1650 |
| Thorium | Th | 90 | 232.12 | 1845 | > 3000 |
| Thulium | Tm | 69 | 168.94 | — | 3500 |
| Tin | Sn | 50 | 118.70 | 231.9 | 2260 |
| Titanium | Ti | 22 | 47.90 | 1820 | (> 3000) |
| Tungsten | W | 74 | 183.92 | 3380 | 5900 |
| Uranium | U | 92 | 238.07 | 1133 | — |
| Vanadium | V | 23 | 50.95 | 1735 | (3000) |
| Xenon | Xe | 54 | 131.3 | -140 | -109.1 |
| Ytterbium | Yb | 70 | 173.04 | — | — |
| Yttrium | Y | 39 | 88.92 | 1490 | (2500) |
| Zinc | Zn | 30 | 65.38 | 419.47 | 907 |
| Zirconium | Zr | 40 | 91.22 | 1750 | > 2900 |

81. MEASURES AND WEIGHTS

(A) Linear Measure

| | | | |
|----------|-------------|-----------------|------------------------|
| 1 inch | = 1000 mils | 1 furlong | = 40 rods |
| 1 hand | = 4 inches | 1 statute mile | = 8 furlongs |
| 1 foot | = 12 inches | 1 statute mile | = 5,280 feet |
| 1 yard | = 3 feet | 1 nautical mile | = 6076.1 feet |
| 1 fathom | = 6 feet | 1 nautical mile | = 1.1508 statute miles |
| 1 rod | = 5½ yards | 1 league | = 3 miles |

(B) Square Measure

| | | | |
|---------------------|------------------|------------|-------------------|
| 1 sq. foot | = 144 sq. inches | 1 township | = 36 sq. miles |
| 1 sq. yard | = 9 sq. feet | 1 acre | = 160 sq. rods |
| 1 sq. rod | = 30¼ sq. yards | 1 acre | = 43,560 sq. feet |
| 1 section (of land) | = 1 sq. mile | 1 sq. mile | = 640 acres |

(C) Volume Measure

| | | | |
|---------------|--------------------|------------------|---------------|
| 1 cu. foot | = 1,728 cu. inches | 1 cu. yard | = 27 cu. feet |
| 1 U.S. gallon | | = 231 cu. inches | |

(D) Liquid Measure

| | | | |
|----------------------|--------------|------------|--------------------------|
| 1 pint | = 4 gills | 1 barrel | = 31½ gallons |
| 1 quart | = 2 pints | 1 hogshead | = 2 barrels (63 gallons) |
| 1 gallon | = 4 quarts | 1 tun | = 252 gallons |
| 1 barrel (petroleum) | = 42 gallons | | |

(E) Dry Measure

| | |
|-------------------------------------|---|
| 1 quart = 2 pints = 67.2006 cu. in. | 1 bushel = 4 pecks = 2150.419 cu. in. |
| 1 peck = 8 quarts = 537.605 cu. in. | 1 barrel = 2.381 bushels = 7056 cu. in. |

(F) Avoirdupois Weight

(For other than drugs, gold, silver, etc.)

| | |
|---|-------------------------------------|
| 1 dram (dr.) = 27.3437 grains* | 1 hundredweight (cwt.) = 4 quarters |
| 1 ounce (oz.) = 16 drams | 1 ton (tn.) = 20 cwts. |
| 1 pound (lb.) = 16 ounces | 1 short ton = 2000 pounds |
| 1 quarter = 25 pounds | 1 long ton = 2240 pounds |
| 1 pound avdp. = 7000 grains = 453.59 grams = 1.2153 pounds troy | |

(G) Troy Weight

(For gold, silver, etc.)

| | |
|--|--|
| 1 pennyweight (dwt.) = 24 grains* | 1 ounce troy (oz.t.) = 20 pennyweights |
| 1 pound troy (lb.t.) = 12 ounces troy = 240 pennyweights = 5760 grains | |

(H) Apothecaries' Weight

(For drugs)

| | |
|---|--------------------------------------|
| 1 scruple (s. ap.) = 20 grains* | 1 dram apoth. (dr. ap.) = 3 scruples |
| 1 ounce apoth. (oz. ap.) = 8 drams apoth. | |
| 1 pound apoth. (lb. ap.) = 12 ounces apoth. | |
| = 96 drams apoth. | |
| = 288 scruples | |
| = 5760 drams | |

82. METRIC EQUIVALENTS**(A) Length**

| | |
|----------------------------|--|
| 1 centimeter = 0.3937 inch | 1 inch = 2.5400 centimeters (cm.) |
| 1 meter = 3.2808 feet | 1 foot = 0.3048 meter |
| 1 meter = 1.0936 yards | 1 yard = 0.9144 meter |
| 1 kilometer = 0.6214 miles | 1 mile (statute) = 1.6093 kilometers (km.) |

(B) Area

| | |
|--------------------------------|-------------------------------|
| 1 sq. cm. = 0.1550 sq. inch | 1 sq. inch = 6.4516 sq. cm. |
| 1 sq. meter = 10.7639 sq. feet | 1 sq. foot = 0.0929 sq. meter |
| 1 sq. meter = 1.1960 sq. yards | 1 sq. yard = 0.8361 sq. meter |
| 1 hectare = 2.4710 acres | 1 acre = 0.4047 hectare |
| 1 sq. km. = 0.3861 sq. mile | 1 sq. mile = 2.5900 sq. km. |

* The grain is the same in avoirdupois, troy, and apothecaries' weights.

(C) Volume

1 cu. cm. = 0.0610 cu. inch
 1 cu. meter = 35.3145 cu. feet
 1 cu. meter = 1.3079 cu. yards

1 cu. inch = 16.3872 cu. cm.
 1 cu. foot = 0.0283 cu. meter
 1 cu. yard = 0.7646 cu. meter

(D) Capacity

1 liter = 61.0250 cu. inches
 1 liter = 0.0353 cu. feet
 1 liter = 0.2642 gallon (U.S.)
 1 liter = 0.0284 bushel (U.S.)
 1 liter = 1000.027 cu. cm.
 1 liter = 1.056 quarts (liquid)

1 liter = 0.9081 quart (dry)
 1 liter = 2.2046 pounds of water @ 4°C
 1 cu. inch = 0.0164 liter
 1 cu. foot = 28.3162 liters
 1 gallon = 3.7853 liters
 1 bushel = 35.2383 liters

(E) Weight

1 gram = 15.4324 grains
 1 gram = 0.0353 ounce avdp.
 1 kg. = 2.2046 pounds avdp.
 1 kg. = 0.0011 ton (short)
 1 ton (metric) = 1.1023 tons (short)
 1 ton (metric) = 0.9842 ton (long)

1 grain = 0.0648 gram
 1 ounce (avdp.) = 28.3495 grams
 1 pound (avdp.) = 0.4536 kg.
 1 ton (short) = 907.1848 kg.
 1 ton (short) = 0.9072 ton (metric)
 1 ton (long) = 1.0160 ton (metric)

(F) Pressure

1 kg. per sq. cm. = 14.223 lbs. per sq. inch
 1 lb. per sq. inch = 0.0703 kg. per sq. cm.
 1 kg. per sq. meter = 0.2048 lb. per sq. foot
 1 lb. per sq. foot = 4.8824 kg. per sq. meter
 1 kg. per sq. cm. = 0.9678 normal atmosphere
 1 normal atmosphere = 1.0332 kg. per sq. cm.
 1 normal atmosphere = 1.01325 bars
 1 normal atmosphere = 14.696 lbs. per sq. inch

83. WINDS**Table XXXV. Wind Designations**

| Designation | Miles per hour | Designation | Miles per hour |
|-----------------|----------------|---------------|----------------|
| Calm | Less than 1 | Moderate gale | 32 to 38 |
| Light air | 1 to 3 | Fresh gale | 39 to 46 |
| Light breeze | 4 to 7 | Strong gale | 47 to 54 |
| Gentle breeze | 8 to 12 | Whole gale | 55 to 63 |
| Moderate breeze | 13 to 18 | Storm | 64 to 72 |
| Fresh breeze | 19 to 24 | Hurricane | Above 72 |
| Strong breeze | 25 to 31 | | |

84. WEIGHT OF WATER

| | | | |
|------------------|------------------------|-----------------------|-----------------|
| 1 cubic inch | = .0360 pound | 1 imperial gallon | = 10.0 pounds |
| 12 cubic inches | = .433 pound | 11.2 imperial gallons | = 112.0 pounds |
| 1 cubic foot | = 62.4 pounds | 224 imperial gallons | = 2240.0 pounds |
| 1 cubic foot | = 7.48052 U.S. gallons | 1 U.S. gallon | = 8.33 pounds |
| 1.8 cubic feet | = 112.0 pounds | 13.45 U.S. gallons | = 112.0 pounds |
| 35.96 cubic feet | = 2240.0 pounds | 269.0 U.S. gallons | = 2240.0 pounds |

85. HYDRAULIC EQUATIONS

Lbs. per sq. in. = $0.434 \times$ head of water in feet

Head in feet = $2.31 \times$ lbs. per sq. inch

Approximate loss of head due to friction in clean iron pipes is:

$$\frac{0.02 \times L \times V^2}{64.4D} \text{ ft.}$$

where,

L is the length of pipe in feet,

V is the velocity of flow in foot-pounds per second,

D is the diameter in feet.

In calculating the total head to be pumped against, it is common to consider this value as being equal to the sum of the friction head and the actual head.

$$\text{Horsepower of waterfall} = \frac{62 \times A \times V \times H}{33,000}$$

where,

A is the cross section of water in square feet,

V is the velocity of flow in foot-pounds per minute,

H is the head of fall in feet.

86. MISCELLANEOUS

(A) Falling Object

The speed acquired by a falling object is determined by the formula:

$$V = 32t$$

where,

V is the velocity in feet per second,

t is the time in seconds.

The distance traveled by a falling object is determined by the formula:

$$d = 16t^2$$

where,

d is the distance traveled in feet,
 t is the time in seconds.

(B) Speed of Sound

The speed of sound through air at 0°C. is usually considered to be 1087.42 feet per second, and at normal temperature, 1130 feet per second. The speed of sound through any given temperature of air is determined by the formula:

$$V = \frac{1087 \sqrt{(273 + t)}}{16.52}$$

where,

V is the speed in feet per second,
 t is the temperature in degrees Celsius.

(C) Cost of Operation

The cost per hour of operation of an electrical device is determined by the formula:

$$C = \frac{Wtc}{1000}$$

where,

C is the cost per hour of operation,
 W is the wattage of the device,
 t is the time in hours,
 c is the cost per kilowatt hour of electricity.

(D) Conversion of Matter Into Energy

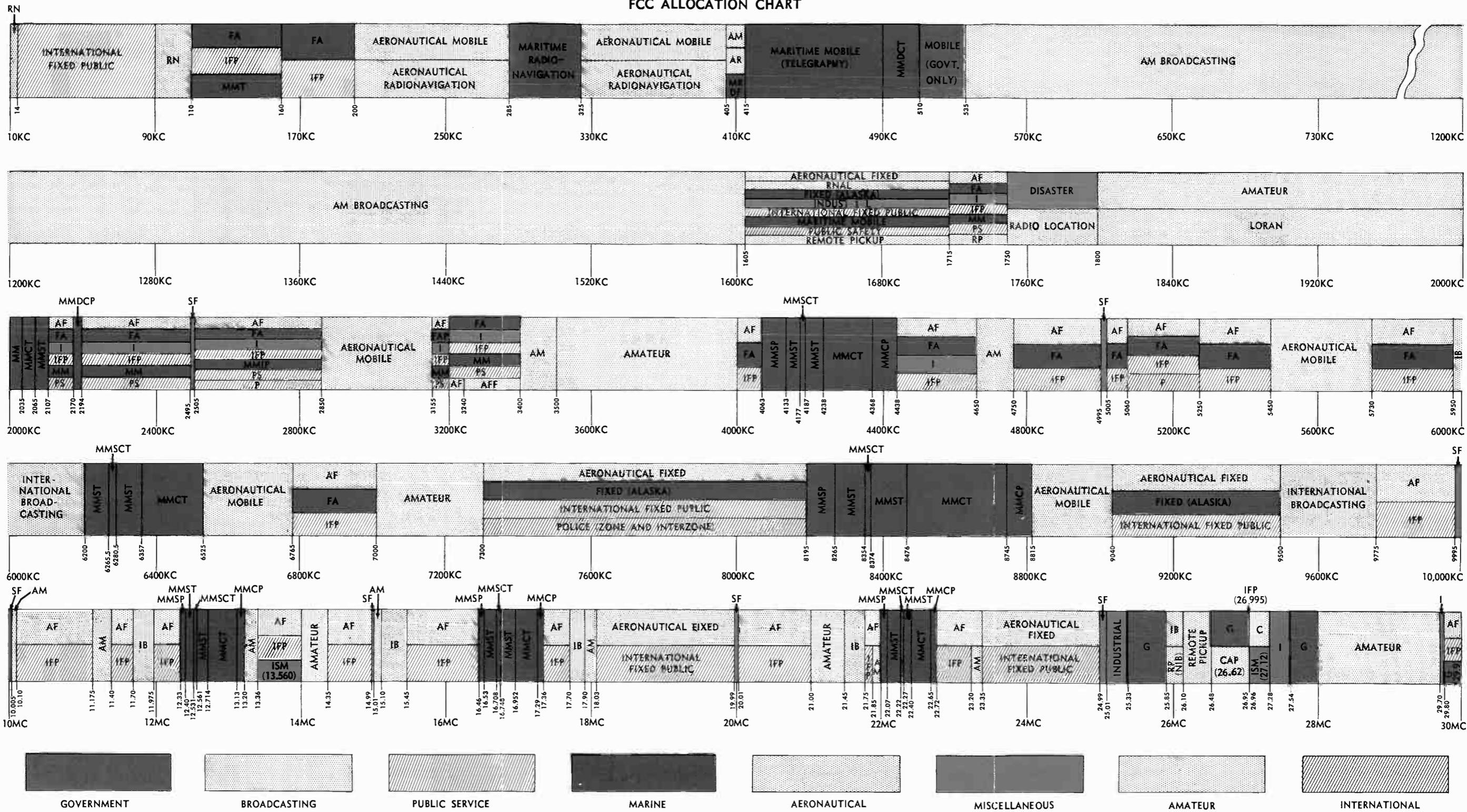
The conversion of matter into energy (Einstein's theorem) is expressed by:

$$E = mc^2$$

where,

E is the energy in ergs,
 m is the mass of the matter in grams,
 c is the speed of light in centimeters per second ($c^2 = 9.10^{20}$).

FCC ALLOCATION CHART



For key to abbreviations, see page 181

Fig. 61A

World Radio

FCC ALLOCATION CHART—(Cont'd)

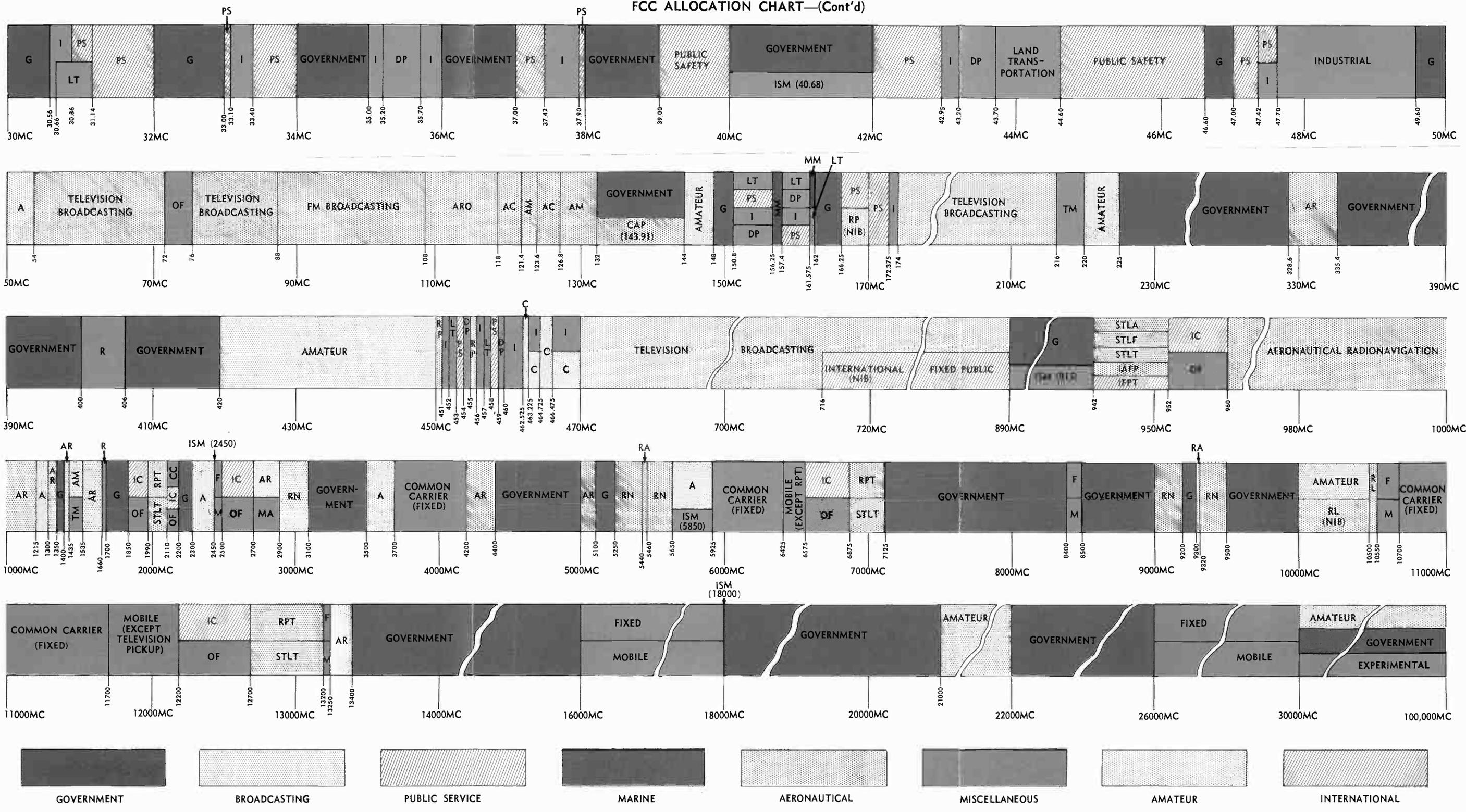


Fig. 61B Hory RADIONAVIGATION

Key to Abbreviations for FCC Allocation Chart

| | |
|--|---|
| A —Amateur | MMDCP —Maritime Mobile Distress and Calling (Telephony) |
| AC —Airdrome Control | MMDCT —Maritime Mobile Distress and Calling (Telegraphy) |
| AF —Aeronautical Fixed | MMIP —Maritime Mobile (Intership Telephony) |
| AFF —Aviation (Flight Test and Aeronautical Fixed Only) | MMSCP —Maritime Mobile Ship Calling (Telephony) |
| AM —Aeronautical Mobile | MMSCT —Maritime Mobile Ship Calling (Telegraphy) |
| AR —Aeronautical Radionavigation | MMSP —Maritime Mobile Ship (Telephony) |
| ARO —Aeronautical Radionavigation (Omnidirectional Radio Range) | MMST —Maritime Mobile Ship (Telegraphy) |
| C —Citizens Radio | MMT —Maritime Mobile (Telegraphy) |
| CC —Common Carrier | MRDF —Maritime Radionavigation (Radio Direction Finding) |
| CAP —Civil Air Patrol (Land and Mobile) | (NIB) —Noninterference Basis |
| DP —Domestic Public | OF —Operational Fixed |
| F —Fixed | P —Police |
| FA —Fixed (Alaska) | PS —Public Safety |
| FAP —Fixed (Alaska and Puerto Rico) | R —Radiosonde |
| G —Government | RA —Racon |
| I —Industrial | RL —Radiolocation |
| IAF —International Aeronautical Fixed | RN —Radionavigation |
| IAFP —International Aeronautical Fixed (Alaska, Hawaii, and U.S. Possessions) | RNAL —Radionavigation (Aeronautical and Land) |
| IB —International Broadcasting | RP —Remote Pickup |
| IC —International Control | RPT —Remote Pickup (Television) |
| IFP —International Fixed Public | SF —Standard Frequency |
| IFPT —International Fixed Public (Puerto Rico and Virgin Islands) | STLA —Studio Transmitter Link (AM Broadcast) |
| ISM —Industrial, Scientific, and Medical Equipment | STLF —Studio Transmitter Link (FM Broadcast) |
| LT —Land Transportation | STLT —Studio Transmitter Link (Television) |
| M —Mobile | TM —Telemetry |
| MA —Meteorological Aids | |
| MM —Maritime Mobile | |
| MMCP —Maritime Mobile Coastal Telephony | |
| MMCT —Maritime Mobile Coastal Telegraphy | |

Allocations Shown Are Current Through November, 1961.

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