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MEMORIES

2114 300 NS 275p 4116 200 NS 300p 4116 150 NS 395p 4315 (4k×1) CMOS RAM 450 NS 995p 6514 (1k×4) CMOS RAM 450 NS 795p

EPROMS

7400

75p 80p 50p 195p 145p 104p 290p 105p 110p 290p 75p 73p 86p 88p 160p

7400	4041 4042	75p 73p		MOME	450	Z
7400 11p 7401 12p	4043	Bob	1702A 2708 45	0 NS	450p 425p	٧
7402 12p	4044	88p 160p	2708 45 2716 5\ 2532 32	450 NS K 450 NS	995p	
7403 13p 7404 17p	4045 4047 4048	99p 56p	2002.00		2995р	П
7409 18n I	4049	38p	0	UARTS		
7412 18 p	4050 4051	40p	AY-5-10 AY-3-10	13A	325p	١
7513 28p 7420 16p	4052 4053	75p	IM6402	IPL	398p 425p	L
7430 18p 7432 25p	4054	73p 111p	CH	ARACTE	R	
7440 16p	4055 405 6	121p 121p	RO-3-25	NERATO	450p	
7442 68p 7448 75p	4059 4060	560n		ARD ENG		1
7448 75p 7473 32p 7474 32p	4063	112p	AY-5-23	76	795p	1
7475 40n l	40 6 6 40 6 7	55p 422n	FLO	PPY DIS	iK	1.8
7476 40 p 7490 35 p	4068	19p	FD1771	TROLLE B-01	HS.	1
7492 50p	4069 4070	28n	S/D Inve	rted Bus B-01	2995р	L
7496 45p l	4071 4072	25p 25p	D/D Inve		4995p	l
74121 35p 74123 45p	4075	25p 20p 88p	S/D Inve	rted Bus	3495p	Ī
	4076 4077 4078		D/D Trui	B-01 Bus	5495p	s a c
74157 55p 74122 45p 74125 50p 74195 100p	4081	29p 23p	FD1794 S/D True	B-01 8us	3495p	d
74195 100p	4082 4085	25p 86p	FD1795	B D/D In	verted 5995p	F
74196 100p 74196 100p 74283 140p 74290 120p	4086 4089	68p	Bus, side FD1797	select B D/D Tr	ue Bus	:
74290 120p 74365 90p	4093 4094	68p		ct RTDIVIC	5995p	١.
74366 90 n	4095	225p 99p	6520		495p 795p	ŀ
74LS	4096 4098	325p	6532		8050	ŀ
74LS00 18p 74LS01 12p 74LS04 15p 74LS08 20p	4099 4501	180n	6551		1095p 375p	1:
74LS04 15p	4502	25p	6820 6821		425p	ľ
74LS08 20p 74LS10 19p	4503 4507	52n	0021		1095p 375p 425p 425p 425p	
74LS11 30p 74LS12 30p	4508 4510	288p 76p	6852 8212		395p	
74LS14 60p	4511	125p	8214		450p	
74LS15 38p 74LS20 19p	4512 4514	2500	8224		395p 395p	۲
74LS20 19p 74LS30 19p 74LS32 25p	4515 4516	290p	6852 8212 8214 8216 8224 8228 8251		495p 1125p	ŀ
74LS40 26p 74LS42 56p 74LS47 78p	4518 4520 4521 4526 4527 4528 4529 4531 4532 4538 4543	99p	0203		495n	Ľ
74LS47 78p 74LS48 85p	4521	230p	8257		1050p 1325p 797p	П
74LS49 99n	4526	1300	MC 144	12VL	797p	ı
74LS73 30p	4528 4529	99p	. ILZ80 CT(7	595p 595p	1
	4531	150-	. I Z80A P	10 FC	695p 695p	
74LS90 40p 74LS107 40p	4538	125p 150p	Z80 DN	IA MA	1995p 2495p	
74LS123 69p		70r	Z80 S10	0/0	2995p	Ì
74LS125 50p 74LS132 79p	4560 4569	225g	780 S1	10/0 0/1	3495p 2995p	
74LS138 69p 74LS151 75p	4572	46r 79r	280AS	10/1 0/2	3495p 2995p	
74LS153 75p 74LS155 65p	4584 4585	125 _F	Z80A S	10/2	3495p	1
74LS161 78p	LINE		IC's	LINEA	R	ı
74LS163 90p 74LS164 90p	∆Y-3-1 AY-3-8	350 910	795p 825p 30p 33p	MC1488 MC1489	90p	Ŀ
74LS168 190p 74LS174 99p	70 9 723		30p	DM8123	125p	
74LS175 99p 74LS195 87p		c	18p 595p	75150 75154	125p 125p	l
74LS221 110p	ICL710	7	695p		195p 250p	Г
74LS244 175p 74LS245 325p	ICL803 ICM72	16A	295p 1875p 1675p	75322 75324 75325 75361 75365	325p 325p	l
74LS251 120p 74LS257 110p	ICM72	16B	1675p	75361	350p	ì
74LS290 95p 74LS293 120p	1CL710 ICL710 ICL803 ICM72 ICM72 ICM75 LM301 LM318	AM	80p 30p		295p 50p	Γ
74LS293 120p 74LS366 57p 74LS373 170p	LM318	ı	50p 75p	75491/2	75p	Ł
74LS373 170p 74LS374 170p	LM324		45p 45p	75491/2 8T26 8T28	175p	l
741.518 39p 741.518 40p 741.51	LM318 LM324 LM339 LM380 LM149)	65p 65p	8T95 8T97	175p 175p	1
74LS393 135p 74LS490 140p	LIVI 187	1	550p 550p	1.50	_	1
74LS670 260p	LIM390	0	50n	TIL209	9р	ŀ
CMOS	LM391 LM391 LM136	5	225p 225p	TIL211	13p	
4002 19n	LM136 NE555	00	225p 125p 18p	TIL211 TIL212 TIL220 TIL222 TIL224	15p 12p 15p	9
4006 75 p	NE556		50p	TIL224	18p	т
4008 80n	RC413 SN764	77N	85p 175p			ľ
4009 35p 4010 45p	SN764 T8A81 TLO71	ODAS	85p	END500	YS 80p	1
4011 24p 4012 24p	1 TLO74		130p 75p	FND510 FND567	125p	Ŀ
4013 38p	TL082 TL084		110p 175p	DL704 DL707	85p 85p	ш
4014 70 p 4015 75 p	TL490)6	325n	MV5716	4 225p	1
4016 35p 4017 75p	XR220 XR220	7	375p	18014	OBC	I
4018 76p	4 pole	- CHE	99n	ISOLAT	120n	T
4020 88p	6 pole 8 pole		115p 140p	ILQ74 MCT6	325p 90p	-1
4021 100p 4022 88p	10 pole		175p	MCT6 TIL111	75p	1
4020 88p 4021 100p 4022 88p 4023 22p 4024 50p			SOCKETS	Y TEXAS	SALE	I
4025 20p	14 pin	90	20 pin	1 50 28 pir	25p	1
4027 45p	I o pin	100	2 Z pin	• + ₽ 9U pir		1
4025 20p	8 pin	7 p	1 B p in 20 p in	15p 24 pm	25p	

MIN

SPECIAL OFFER! 4K CMOS RAM (1K × 4) 450 NS

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The TC 5514P from Toshiba. CMOS equivalent of the 21141

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74685 145p 74097 125p 74098 125p 740107 100p 740161 145p 740163 145p 740193 175p 740193 175p 740193 175p 740193 45p

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31-DIGIT LIQUID CRYSTAL DISPLAY with 'low bat' indicator.

with 'low bat' indicator.

High Contrast Ratio
Wide Viewing Angle
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ULTRA low Power Consumption LCD 106

LED BAR GRAPH AND ANALOG METER DRIVER ew from National LM3914. Drives 10 LEO direct for making bar graphs, audio power meters nalog meters, LED Oscillators, etc. Units can be acked for more LEDs. A super versatile and trub markable IC

Only £2 25

X-TRA VALUE: All the components and high quality plated G-10 PC Boards are provided X-TRA CARE IN DESIGN: No wires between readout board and clock board. Large

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**CELLENCE IN IDEAS: 5 years of designed products for the amateur radio market.

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price! Unit operates on either 12VAC or 12VDC. Unit operates on either 12VAC or 12VDC. On board QUARTIZ XTAL TIMEBASE Automatic BATTERY BACKUP. Never worry about power failures again! Reads true 24 HOUR TIME and 31 DAY CALENDAR. Unique NOXIM CIRCUIT activates readouts with a handclap or they can be turned on Only the North Circuit activates readouts with a hander constantly. When used mobile readouts blank ignition is off. Special NOISE SUPPRESSION and battery reversal circuits. Bright \(\frac{1}{2}'' \) LEDs show hours, minutes and seconds.

Just clap your hands and the time appears for 5 seconds followed by the date for 4 seconds. A low cost 9V transistor battery provides stand-by power in the event of power failures up to 4 hours. With the addition of a low cost 12V 300MA transformer, the unit will work on AC.

TUNES SYNTHESIZER

795p 795p 795p 695p 995p 525p 1095p 795p 995p

55p 65p 575p 625p

8080A 8085A

Z8002 WD**9**000B

7805/7812 7905/7912 78H05SC 78HGKC

VOLTAGE REGULATORS

BIPOLAR PROMS

93511 2k < 8 50 NS

93448 512 · 8 40 NS 93453 1k × 4 40 NS p.o.a. 93451 1k 8 45 NS

The AY3-1360 is a MOS microcomputer synthesizer of preprogrammed tunes for applications in toys, music boxes and door chimes. The standard device has a set of 25 different popular and classical tunes. In addition there are 3 chimes making a total of 25 tunes.

there are 3 chimes making a total of 25 tunes.

FEATURES

Minimal external components.
Automatic switch-off signal at end of tune for power saving.
Envelope control to give organ or piano quality.
Sequential tune mode
4 door capability when used as door chime.
Operation with tunes in external PROM if required (12708).

quired (2 708):
Single supply (- 5V) operation
Tunes include: STAR WARS, BEETHOVEN'S
9TH AND STH, JINGLE BELLS, YANKEE
DOODLE, STAR SPANGLED, BANNER,
CLEMENTINE GOD SAVE THE QUEEN,
OSULE MIO, WESTMINSTER CHIMES, and
DESCENDING OCTAVE CHIME flux many
ore (1 with detailed specs and instructions)

SE 01 Sound Effects Kit NEW

The SE-01 is a complete kit that contains all the parts to build a programmable effects generator. Designed around the new Texas Instruments SN 76477 Sound Chip, the board provides banks of MINI DIP switches and post to program. When the program was supported to program with the program of the program was supported by the program of the programmatic pro specifications It runs on a 9V battery (not cluded). On board 100MV amp will drive a speaker directly, or the unit can be connected your stereo with incredible results? (Speaker r

COMPLETE KIT ONLY £14.99

UNIVERSAL SCR

C106D 400V/5A Sale

AY-3-8910

THE NEW GL COMPUTER SOUND CHIP

SOUND CHIP
The amazing AY-3-8910 is a fantastically powerful sound and music generator, cerfect for use with any 8-bit micro processor. Contains 3 tone channels noise generator, 3 channels of amplitude controls. 16-bit envelope period control, 2 parallel I/O, 30/A converters plus much more. All in 40 pin DIP. Super easy to interface to the S-100 or other Busses.
ONLY £8.50 VAT, including FREE reprint of BYTE 79 article! Also, add £2.25 for 60-page data manual.
"Perhaps the next famous composer will not direct a 150-piece orchestra but, rather, a trio of microcomputers controlling a bank of AY-3-8910s." BYTE July 79.

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TOTAL SECURITY! Completely invisible ultrasonic (23KHZ). Sound beam works like a photo-electric beam but is unaffected by light, heat or noise. Separate Transmitter and Receiver can be used from 6 inches to 25 feet! A solid object breaking the beam causes an output to glow that will sink up to 150MA to Drive a Relay. TRIAC etc. Complete electronics are provided. Works on 12VDC (unregulated) and draws less than 100MA. Use it for burglar alarms, object counters, automatic door openers, automatic door bells, electronic rat trap (?) and more. DNLY £19.93 P&P 67p + VAT.

WARBLE ALARM KIT

A fun EASY kit to assemble that emits an ear piercing 10 watt dual tone scream. Resembles European siren sound. Great for alarms or toys. Operates from 5-12VDC and up to 1 amp (using 12VDC 8 ohm speaker). Over five thousand have been sold. All parts including PC board, less speaker.

ONLY £4.99 P&P 67p + VAT.

LM1871 RC ENCODER/TRANSMITTER LM 1872 RC RECEIVER/DECODER

New from National. The LM 1871 is a complete six-channel digital proportional encoder and nix transmitter intended nor use as a low power, non-voice unlicenced communication device at Carriar fet quencies of 2 MM or of the communication device at Carriar fet quencies of 2 MM or of a discontrolled hobby toy and industrial applications, the encoder section can provide a serial input of six words for hard wired, infra-red or fibre optic communications links. Channel add logic is provided to control the number of encoded channels from three to six, allowing increased design flexibility. When used with the LM 1872 RC receive/decoder, allow cost RF inked encoder and decoder system provides two analog and two DN/DFF decoded channels. Super versatile chip. Just out Just look at the festures – low current 9V battery operation – on-chip RF oscillator/transmitter – one timing capacitor for six proportional control of the provider of the pr from National. The LM 1871 is a complete six-channel digital ortional encoder and HF transmitter intended for use as a low

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12 page data
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SAVE THE QUEEN, WESTMINSTER CHIME and DESCENDING
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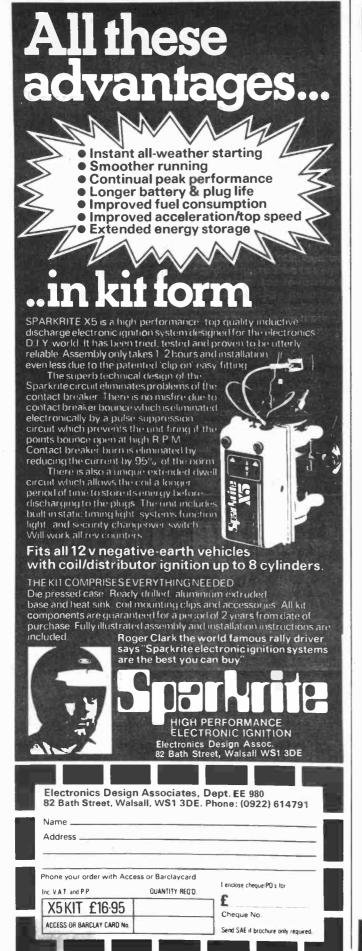
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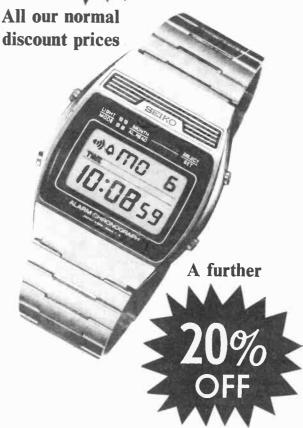
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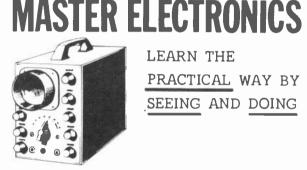
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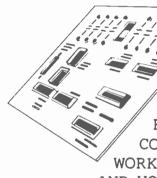
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HEF4030	58	HEF4094	219	UA7812CU	78	UA741CT	47	8C108C	18	TIP31	48
HEF4031	250	HEF4104	208	UA7815CU	78	Zener	- 0	BC109	14	TIP32	54
HEF4035	138	HEF4502	114	UA7912CU	97	Diodes	10	BC1098	19	TIP41C	76
HEF4040	107	HEF4505	714	UA7915CU	97		. 2 2	BC109C	20	TIP42C	76
HEF4041	94	HEF4508	230	UA78L05CS	38	400mW C41		BC148	10	TIP2955	75
HEF4042	83	HEF4510	135	UA78L12CS	38	BZY88/BZ)		9C158	10	TIP3055	60
HEF4043	100	HEF4511	157	UA78L15CS	38	+ Voltage	9 !	BC177	17	TIS43	36

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Order Code

Dipped Ty 63 40 63 Moulded 9 9 #F 9 0015 9 0022 8 10 0047 8 11 0047 8 13 0068	
9 0015 9 0022 8 9 10 0033 10 0047 11 0068	
8 10 .0033 9 11 .0047	
8 11 17 .015	
9 13 .022 .033 0 31 .047	
26 36 30 40 23 32 47 D.I.I So	ock
10 39 54 80 59 8 Pin Lor	w I
3	0 39 54 8 Pin Lo

	Polyest	Orde	r Code					
Dipped Type, C280/352 Style Moulded Type, 10.2mm Pitch						Cap 35: Cap 36: + Value		
	u F	352	360	μF	362	380		
	2001		7 .	1.1	7	9		
	.0015		7	.15	8	10		
	.0022	6	7	.22	9	11		
	.0033	6	7	:33	- 11			
	.0047	6	7	.47	14			
	.0068	6	7	.68	17			
	.01	6	8	1.0	21			
	.015	6	8	1.5	30			
	.022	6	8	2.2	35			
	.033	6	8					
	.047	6	8					
	.068	7	8			,		

μF	V	10	16	25	35	40	50	6:
.4	7							1
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3.3								
4.7						7		1
6.8				7			В	1
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15			7	8			9	1
22		7	8			9	11	
33			8	9		11		
47		8	9		112			
68			9	11				
100		9						
150		11						

Profile Socket Tin 12 DIL SKT 8 Profile Socket Tin 14 DIL SKT 14 Profile Socket Tin 16 DIL SKT 16 Delo Pen, Blue Inh, Slow Drying Order Code Skeleton Presets, Miniature RESISTORS Carbon Film, Fixed 0.25W, E24 Values IR

Carbon Film, Fixed		
0.25W, E24 Values IRO-10M, 5% Tol.	2 each	Res RD%
100/100 (Mult 10	/Value)	
0.5W, £12 Values IRO-4M7, 10% Tol.	3 each	Res RO%
	-	Value
Metal Film, Fixed		
0.5W, E24 Values, SRI-IM, 2% Tol.	8 each	Rei MR30
2 5W 512 Velum 100 27F 5% Tol	SC nach	D- ODES

		٠	Value
ol. Tol.	each each		Res MR30 Res PR52 Value

2.399, E12 1	randes, FUN-27F	K, 5% 101.	10 44
Metal Glaz	e, Fixed		
0 EW 534 1	Ash 184 2284	Ch You	16

MAINS TRANSFORMERS

Ш	0.1W, E3 Values, 100R-IM, Lin, Vertical Mounting 0.1W, E3 Values, 100R-IM, Lin, Horizontal Mount	8	Min. Preset Min. Preset
	Skeleton Presets, Standard		+ Value
4	0.3W, E3 Values, 100R-4M7, Lin. Vertical Mounting		Std. Preset
- 1	0.3W, E3 Values, 100R-4M7, Lin. Horizontal Mount	+1	Std. Preset
. 1	Potentiometer, Rotery		· Valua
30	0.5W, E3 Velues, 1K-2M2 Lin.	39	Ro Pot Lin
	0.25W, E3 Values, 4K7-2M2 Log.	39	Ro Pot Log
- 1	Potentiameter, Slider		+ Value
- 1	0,5W, E3 Values, 2K2-47C . Lin.	45	SI Pot Lin
17	0.25W, E3 Values, 1K0 - 1M0 Log	45	SI Por Log
			Value

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MAINS THATSI OTHER	0
Secondaries may be connected in series or parallel to give wide voltage range Primaries 0-220, 240V	
6vA - Clamp Type Construction	235 each
Approx 18% Regulation, F.C. 54, H36, W.	35
0-4.5V, 0-4.5V Secondaries 0-3V, 0-6V 0-12V, 0-12V 0-15V, 0-15V 0-20V, 0-20V	Trans 6
20VA - Clamp Type Construction	360 each
Approx. 16% Regulation F.C. 70, H48, W4	46
0.4.5V, 0.4.5V Secondaries	Trens 2

Approx. 16% Regulation F.C. 70, H48, W49	6		
0-4.5V, 0-4.5V Secondaries		Trens	20 V A
0-6V, 0-6V			
0-12V, 0-12V			
0-15V, 0-15V			
0-17.5V, 0-17.5V			
0-20V 0-20V			

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5.82" x 2.9" .1" prich V-Q DIP Board	135	200-21084E
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DS Pins .040 [100)	44/Peck	200-21087G
SS Pins .040 (100)	44/Pack	200-210178
Verowire Kit [1-pen, 2-wire, 25-comb]	454/Krt	200-21341D
Verowine Combs (25)	109/Pack	200-21339F
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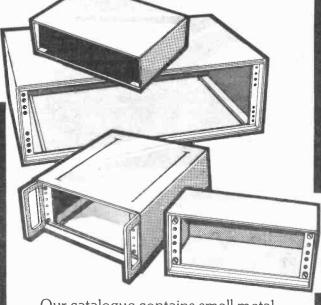
		Order Code
L112 W62 D31	99	Case BIM2003 OR
L150 W80 D50	131	Cate BIM2005 OR
L190 W110 D60	223	Cesa BIM2006 OR
Plastic Boxes with M	etal Lids	
Recessed Top Box		
ABS Base, C/W Brass Bu	rihes, In Drange	
1mm Aluminium Top P	anal Finished Gre-	
		Order Code
L85 W56 D29	112	Case BIM4003 OR
L111 W71 D42	150	Cara BIM4004 GR
L161 W96 D53	208	Cata BIM4005 OR
Quecast Boxes		

Aluminium Box and Lid in Natural Fi L113 W83 031 124 L152 W82 D50 215 L192 W113 D61 334			Order Code Cess BIM5003 NA Cess BIM5005 NA Cess BIM5006 NA		
SWIT	CHES			Order Code	
Miniet	re Toggle - Honeywe	11		Order Code	
SPOT		6	7	SW 8 A 1011	
SPOT	C/O#	6	3	SW 8A 1021	
SPDT	T Double Bias To Centre		0	SW 8A 1041	
DPDT	POT		9	SW 8A2011	
DPDT	C/Off	11	3	SW 8A2021	
Minist	re Push - C & K				
SP	Push To Make, Momen	ary 62	,	SW 8531	
co	Birt To Brest Manager			CW RETT	

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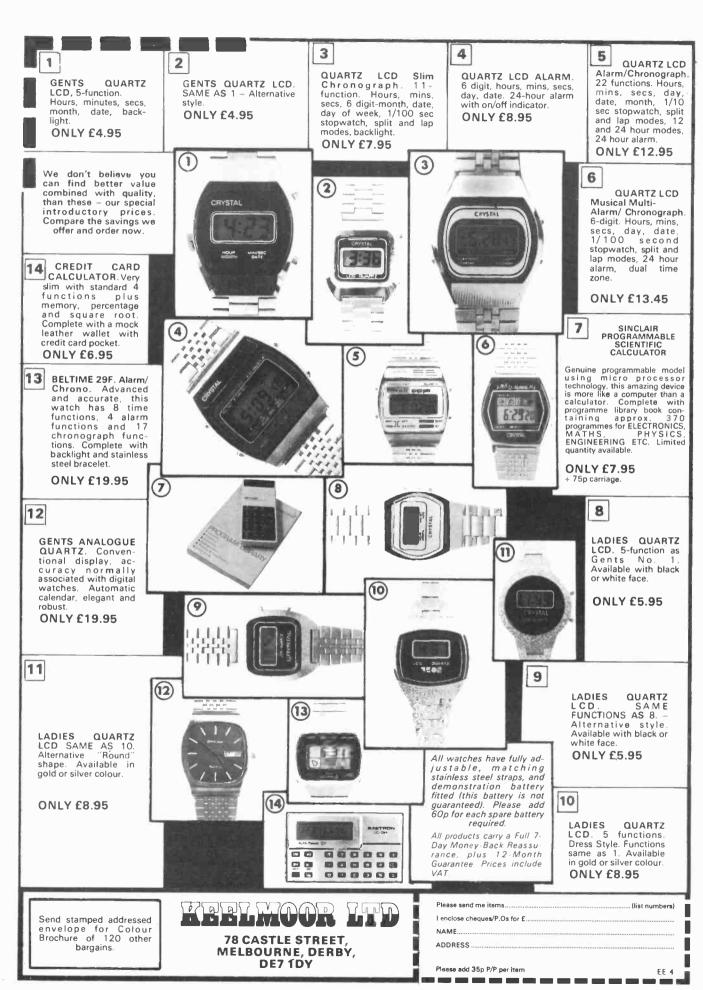
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THIS MONTH'S SNIP

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SOUND AND LIGHT UNITS

SOUND AND LIGHT UNITS

3 CHANNEL SOUND TO LIGHT KIT Complete kit of parts for a three channel sound to light unit controlling over 2000 watts of lighting. Use this at home if you wish but it is plenty rugged enough for Disco work.

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Projects... Theory ... and Popular Features ...

This month TTL logic provides a link between three different projects. These projects moreover illustrate how self-supporting, and even selfsufficient, our hobby can be. So let's consider each in turn.

First there is the *Duo-Deci Timer*. A useful item of equipment and a typical "end-product" of a building session. This instrument will find many applications around the home, perhaps in the kitchen or maybe in the photographer's darkroom, but there are numerous other uses of course.

Whilst building this timer it would be helpful or, at least instructive, to check out the operation of the logic circuitry. But the constructor does not have to go and buy an expensive instrument, he simply sets to and makes one. For the second project in our TTL linked trio happens to be a TTL Logic Probe.

This handy little instrument will prove indispensable to all who build and experiment with TTL logic circuits. It enables one to ascertain the state of the logic ("high" or "low") at any point, under working conditions. Worthy also of a mention is the homely touch introduced by the adaptation of a Multicore solder dispenser as the probe case. (How's that for conservation as well as self-sufficiency!)

Now the Duo-Deci Timer, like many other projects, is designed to operate

from a battery. But if one prefers, a mains power supply unit can be used instead. That is just one possible use for the remaining item of our trio, the TTL Power Supply Unit.

Designed to provide the maximum voltage needed for TTL devices, this compact unit will be an asset on the workbench, especially when running dynamic tests on TTL circuit hook-ups, or on completed projects. Or it may be employed as a permanent source of power in place of a battery.

Test equipment and power supplies are essential ancillaries in the hobbyist's workshop. They play their part during the creation of other—perhaps more imposing and more splendid projects, destined in all probability for use away from the workshop and by "non-electronics" persons.

The fact that they are home-made gives added cause for pride of possession, and substantiates the claim that electronics is to a considerable degree self-supporting.

Sorry to finish on this note, but the price of EE will regrettably be increased to 60p as from the next issue (October). This is necessary because of increasing costs affecting the publishing business in general.

Fed Bennett.

Our October issue will be published on Friday, September 19. See page 569 for details.



Readers' Enquiries

We cannot undertake to answer readers' letters requesting modifications, designs or information on commercial equipment or subjects not published by us. All letters requiring a personal reply should be accompanied by a stamped self-addressed envelope.

We cannot undertake to engage in discussions on the telephone.

Component Supplies

Readers should note that we do not supply electronic components for building the projects featured in EVERYDAY ELECTRONICS, but these requirements can be met by our advertisers.

All reasonable precautions are taken to ensure that the advice and data given to readers are reliable. We cannot however guarantee it, and we cannot accept legal responsibility for it. Prices quoted are those current as we go to press.

ELECTRONICS

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Back Issues

Certain back issues* of EVERYDAY ELECTRONICS are available worldwide price 70p inclusive of postage and packing per copy. Enquiries with remittance should be sent to Post Sales Department, IPC Magazines Ltd., Lavington House, 25 Lavington Street, London SE1 0PF. In the event of non-availability remittances will be returned.

* Not available: October 1978 to May 1979.

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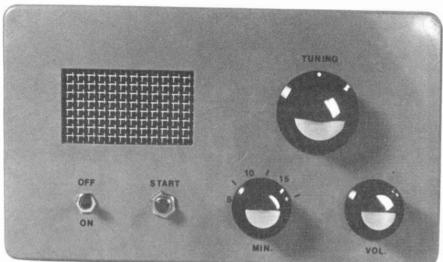
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By R. A. PENFOLD





BEDSIDE RADIO

THIS two i.c. medium wave radio is primarily intended for use as a bedside set, although it can provide sufficient volume for normal domestic use.

There is an optional one i.c./one transistor timer circuit which can be used to automatically switch off the receiver after a switch-selected delay of 5, 7¹2, 10, 12¹2, 15, or 17¹2 minutes. This gives a simple "snooze" facility of the type fitted to many clock radios and other receivers these days.

THE CIRCUIT

Fig. 1 shows the complete circuit diagram of the receiver including the timer circuitry. The range circuitry is shown in the inset of Fig. 1.

The r.f. and detector stages use a ZN414 i.c. (IC1) in a standard configuration. A tuned circuit is formed by L1 and C3. One end of this is coupled to earth by C2 and the other end couples into the input of IC1.

The low impedance coupling winding on the ferrite aerial is not needed because the ZN414 device has a buffer stage at the input which produces a high input impedance, and gives good results with direct connection to the ferrite aerial. The buffer stage is followed by three stages of amplification which provide a considerable amount of gain.

These are in turn followed by a transistor detector stage which has R2 as its load resistor and C4 to provide the necessary r.f. filtering. R1 is a

bias resistor. The ZN414 has a simple a.g.c. (automatic gain control) action which reduces the gain on strong signals so as to reduce the possibility of overloading and to provide a more consistent audio output level.

A nominal supply potential of 1.3V is required for the r.f. and detector circuitry. This is derived from the main 9 volt supply using a simple shunt stabiliser incorporating R3, D1, and D2, the two silicon diodes being forward biased to produce a voltage drop of 0.65V across each. The supply is decoupled by C1 and C6.

AUDIO STAGE

A TBA820 i.c. (IC2) is used in the audio amplifier section of the receiver, and this is a type which can have its input direct coupled to the volume control. In this case the input is coupled to volume control VR1 via R4, this resistor forming an r.f. filter in conjunction with C7.

There was found to be a small amount of r.f. breakthrough and consequent instability without this additional r.f. filtering. Capacitors C9, C10, C12, plus R6 are also needed in order to ensure good stability. The audio output from IC1 to the volume control is coupled by C5 and this also provides d.c. blocking.

The output signal is coupled to the loudspeaker by way of d.c. blocking capacitor C11 and the break contact of phone socket SK1. This break con-

tact automatically switches out the loudspeaker when an earphone is in use. Both crystal and magnetic earphones are suitable.

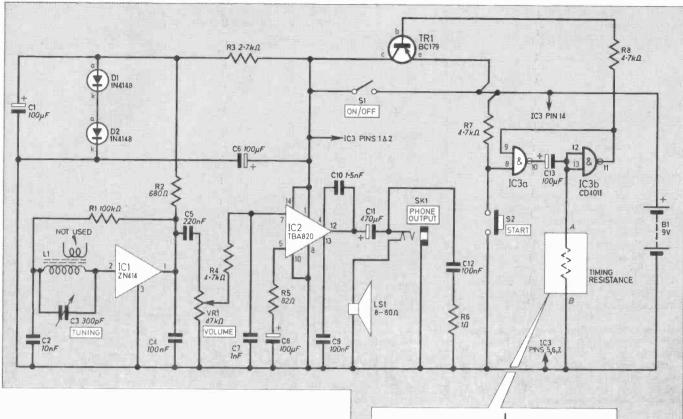
The voltage gain of the amplifier is controlled by R5, and the specified value actually gives a gain of approximately 73 times. This is sufficient to fully drive the amplifier from the signal level of about 30mV r.m.s. produced at the output of IC1.

The maximum output power is about 200mW r.m.s. or so, although it is somewhat less than this when using speakers of more than about 35 ohms impedance. The circuit will work well with any normal speaker having an impedance in the range 8 to 80 ohms.

TIMER

It is important for the timer circuit to have a very low quiescent current consumption since it is permanently connected to the battery supply, and unlike the rest of the receiver is unaffected by on/off switch S1.

A cmos i.c. has therefore been used as the basis of the timer as it has a stand-by current consumption of only a fraction of a microamp, and will not significantly affect battery life. Two of the four gates in a 4011 two-input NAND gate package are used in a conventional cmos monostable circuit. The inputs of the unused gates are connected to one of the supply lines prevent them from being spuriously operated by stray pick-up, but these gates are otherwise ignored.



OPERATING PRINCIPLE

The two inputs of gate 2 are connected in parallel so that it works as an inverter, and its output is high since the input is taken low by the timing resistance. Transistor TR1 is fed from the output of the monostable, and is cut off when the output is in the high state.

The output of gate 1 is low because one input is taken high by R7, and the other is taken high by the output of the monostable. If either or both its inputs are taken low, however, gate 1 output will go high.

Momentarily operating S2 will indeed take one input of gate 1 low, causing its output to go high. This signal is coupled to the input of gate 2 by C13, causing its output to go low and switch on TR1 with the base current it supplies via R8. TR1 then effectively connects the positive battery terminal to the radio circuitry, and the set becomes operational.

The voltage at the negative terminal of C13 now gradually falls as this component charges up through the timing resistance. Eventually the voltage here will fall below the transition voltage of gate 2, resulting in the output reverting to the high state and the radio being switched off.

Both inputs of gate 1 are then back at the high state once again, and its output therefore returns to the low state. The circuit is now back in its original state and is ready to be started on another timing run by briefly operating S2 once again.

Fig. 1. Complete circuit diagram of the Bedside Radio. The resistive network which controls the time period for the automatic switch off is contained in the inset and is connected into the main circuit at the points A and B. It can also be seen that the small coupling winding on the tuning coil is not used in this design. The unused pins of IC3 are tied to the power lines to prevent spur-

TIMING RESISTANCE

ious triggering.

It is possible to control the time for which the set is switched on by means of the timing resistance, with the switch on time being roughly proportional to the value of this resistance.

Switch S3 provides six different resistance values, and presets are used so that these resistances can be trimmed to give the six nominal times specified at the beginning of this article.

Of course, on/off switch S1 must be in the "off" position when using the timer or S1 will keep the set switched on regardless of the timer circuit.



VR7

VR5 4-7ΜΩ

S3

VR4 4-7ΜΩ

> VR3 4·7ΜΩ

Front view of the Bedside Radio.



COMPONENT PANEL

Most of the components are assembled on a 0.1 inch matrix stripboard having dimensions of 37 holes by 24 strips $(3_4 \times 2_2)$ inches). This is a standard size in which the board is sold. The component layout is shown in Fig. 2.

Drill the 3.3mm diameter mounting holes for the panel and the ferrite aerial, and make the 22 breaks in the copper strips before inserting and connecting the components. Be careful not to omit any of the 10 link wires.

The cmos chip IC3 is the last component that is connected, and it should be left in its protective packaging until it is time to fit it onto the board. It should either be soldered into place using an iron having an earthed bit or it should be fitted into an i.c. socket. Handle the device as little as possible.

The Ambit ferrite aerial used in the prototype has plastic mounting clips which enable it to be easily mounted on the component panel using a couple of short M3 or 6BA bolts and fixing nuts.

A Denco MW5FR aerial also works well in this circuit, and can be mounted on the panel using a couple of 9.5mm "P" type cable clips.

CASE

A plastics box measuring about 190 \times 110 \times 60mm is used as the case for the prototype. The case cannot be much smaller than this if it is to comfortably accommodate all the components, and a metal type is not suitable as it would screen the ferrite aerial and virtually eliminate any signal pick-up.

The component panel is mounted on the removable rear section of the case using a couple of M3 or 6BA fixings, but it is not finally bolted into place until it has been wired up to the rest of the receiver.

The layout of the front panel can be seen from the photographs. The rectangular cutout for the speaker can be cut using a fretsaw or a miniature file. Alternatively a grill of small holes can be drilled. A piece of speaker cloth or fret is glued over the rear of the cutout and the speaker is carefully glued onto this taking

COMPONENTS

Resistors

R1 $100k\Omega$ 680Ω R7 4.7kΩ R3 2·7kΩ R4 4·7kΩ R8 4 · 7kΩ 4.7MΩ

R5 82Ω

All 1W carbon ± 5%

Potentiometers

 $47k\Omega$ carbon log. VR2-VR7 4·7MΩ vertical preset (6 off)

Capacitors

100μF 10V elect. C1 C2

10nF polyester type C280 300pF solid dialectric variable (Jackson Dielecon or similar) C3

100nF polyester type C280

220nF polyester type C280 100µF 10V elect.

1nF ceramic plate

100µF 10V elect. 100nF polyester type C280 1.5nF ceramic plate C9

470μF 6·3V elect. C11

C12 100nF polyester type C280 C13 100µF 10V elect.

Semiconductors

ZN414 tuned radio frequency i.c. IC1

IC2 TBA820 a.f. amplifier i.c.

IC3 CD4011 CMOS quad 2-input NAND gate

BC179 npn silicon

1N4148 small-signal silicon diode (2 off) D1. 2

Switches

S1 S2 s.p.s.t. miniature toggle

push-to-make, release-to-break

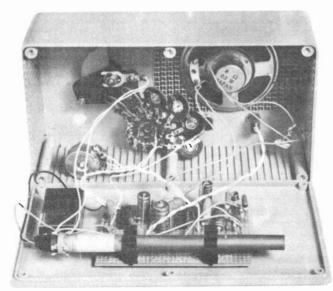
S3 2-pole, 6-way rotary type

Miscellaneous

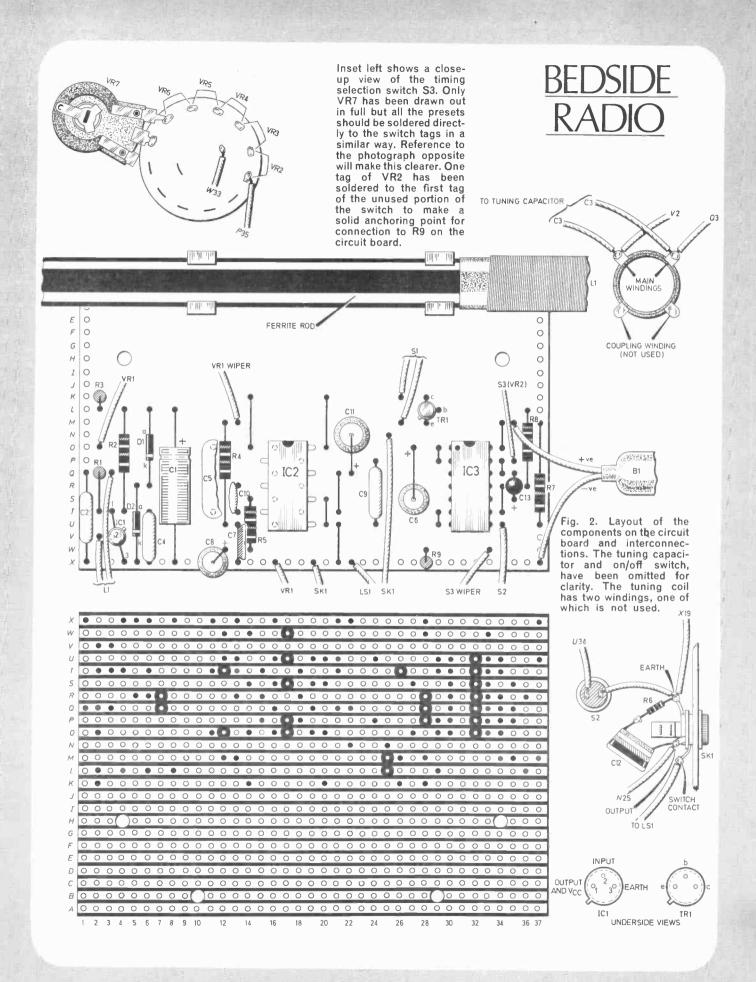
9V type PP3 B1

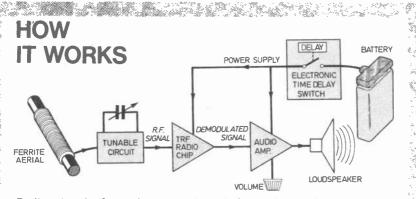
miniature moving coil loudspeaker, 8 to 80Ω impedance

SK1 3.5mm jack socket with single break contact
L1 Aerial coil, Ambit type MCW2 or Denco type MW5FR, or any other m.w. ferrite aerial coil wound on 9.5mm diameter ferrite rod with fixing clips Case, dimensions 190 × 110 × 60mm plastic or wood; 0.1 inch matrix stripboard 37 holes × 24 strips; battery connectors; speaker fret; connecting wire.



View inside the completed unit. Timing selection switch S3 can be clearly seen with its complement of variable resistors, VR2 to VR7.





Radio signals from the transmitter induce electrical signals in the ferrite aerial. A certain portion of these are selected by the tuned circuit and passed onto the t.r.f. radio chip where they are processed into a low frequency or audio signal. This is then passed into the audio amplifier i.c. the output of which is used to drive a loudspeaker.

Power to the unit passes through an electronic time delay switch. This consists of a monostable circuit which keeps the radio switched on for a preset period after the main switch has been turned off, thus allowing the listener to dose off to sleep without needing to turn off the set manually.

care not to smear any adhesive onto the diaphragm. Use a good quality adhesive such as an epoxy type.

When the other components have been fitted onto the front panel and the earphone socket has been mounted on the left hand side panel of the case, the remaining wiring can be completed. This is illustrated in Fig. 2.

ADJUSTMENT

Thoroughly check all the wiring for mistakes, and when confident that there are no errors, connect a battery and switch on. In most locations it should be possible to receive a number of stations at good volume even during daylight hours, and it should be possible to pick up more after dark.

The frequency coverage of the set depends to some extent on the position of the aerial coil on the ferrite rod. If the set cannot tune down to stations at the low frequency end of the band (the vanes of VC1 fully meshed), this can be corrected by moving the coil further onto the ferrite rod.

A lack of coverage at the other end of the band can be currected by moving the coil towards the end of the rod.

When a suitable position for the coil has been found it should be glued or taped in place to prevent it from slipping out of adjustment.

PRE-SET RESISTORS

The six preset resistors are adjusted by empirical means to give the correct time delays with a reasonable degree of accuracy, starting with VR2 which sets the 5 minute switch off delay. Resistors VR3 to VR7 are then adjusted in sequence to set the 7^{1}_{2} , 10, 12^{1}_{2} , 15, and 17^{1}_{2} minute delay times respectively.

The presets must be adjusted in this order. This is a rather time consuming task and unfortunately there is no short cut, but at least in this application a high degree of accuracy is not necessary, and it is only necessary to get the actual times within a few seconds of the specified ones.

which is like a miniaturised but greatly improved version of Kew.

Apparently Len or Bill have what are

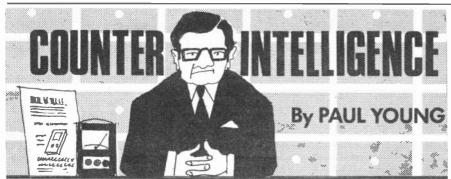
Apparently Len or Bill have what are called "Green Fingers". On the way home this will be contrasted by the little woman with her own garden which looks like an inferior version of the Matto Grosso.

However, there is another side to the coin. When a fuse blows, the toaster, or vacuum breaks down, then we electronic types come into our own, someone ought to say that we have "Blue Fingers".

Only a short while ago my wife switched on our electric cooker, there was an almighty flash and a bang and the company fuse had blown. This would have had the Lens and the Bills yelling for help and dialling 999, but did old "Blue Fingers" turn a hair? Not a bit of itl in a trice he had the back off the cooker and quickly sized up the situation.

The main supply is connected to terminals with insulators big enough to carry the National Grid. The positive terminals had been arcing across to the earthed metalwork until the heat had split the insulation into about three pieces. The negative insulator was perfectly good, so I swapped them over. I reasoned that the potential difference between the negative line and earth was minimal although this is not always the case.

An interesting sidelight on this, is the fact that the cooker is fed through a 30 amp fuse and a 60 amp before the company fuse which is rated at 120 amps. Only the 120 amp fuse had blown. This looks like a practical example of Froud's Law "A transistor protected by a fast acting fuse will protect the fuse by blowing first"!



Mail Order and Books

This is a time with shortening days when the old hands will be deciding on their next project, and equally important, many new recruits will be joining their ranks. In one or two issues about this time, I usually devote some space to giving guidance on component buying and this year will be no exception.

I will commence as I usually do with pointing out that considerable use has to be made of firms who offer Mail Order facilities, and the first step is the acquisition of at least four good catalogues. It is best to accept the fact, straight away, that the number of electronic components is now so vast, that you are unlikely to be able to get all your requirements from one supplier.

Also, I think a few extra reference books would not come amiss. First of all I would suggest Basic Electronics prepared by Malcolm Plant for the Schools Council. It is in five parts which can be purchased

separately and is modestly priced. 'Eventually I would suggest that Foundations of Wireless and Electronics by Mr. G. Scroggie is a "must".

Another book I would strongly recommend is the *Dictionary of Electronics* published by Penguin. Lastly I would suggest the *Towers International Transistor Selector*.

Blue Fingers

I am certain that many of our readers are married men and will confirm what I am about to say.

You find that within a few months of being spliced, you are being compared, always unfavourably, to Betty or Daisy's husband, Len or Bill. Compared to them you are a lazy good for nothing!

you are a lazy good for nothingl
It turns out that Len or Bill, regularly
clean all the windows, paint the house
inside and out, and needless to say do
all the gardening.

When you visit them, you are certain to have a conducted tour of the garden



Dave Barrington

Vowel Power

Most of our readers will no doubt have heard of the Texas Speak and Spell education aid which lets children have fun while learning to spell. Now comes news that it has been given a bigger

The standard machine has a 240-word vocabulary and now by the addition of a plug-in word module a further 140 words has been added. The new plug-in word memory, called "Vowel Power", works in exactly the same way as the built-in processor but concentrates on words with difficult vowel sounds.

The new words relate to vowel sounds in four categories: short vowel sounds such as neck and much; long vowel sounds like wheel and toast; two letter or blended vowel sounds like cloud and clown; and words where the letter "r" changes the vowel sound sound-such as germ and church.

An improved voice synthesis is another feature of the Speak and Spell which retails for about £50. The plug-in word memory, which is the first of a series, retails for about £15.

Remote ICs

A couple of exciting new integrated circuits for the experimenter take the spotlight this month.

Currently not on general supply, but available from Celdis Ltd, is a two-chip remote control system comprising the Plessey SL490 pulse-transmitting remote controller and ML920 receiver.

The SL940 is a bipolar, pulse transmitting circuit. Single-pole switches are used to select the required command which is transmitted as one of 32 5-bit code words. These words can be modulated as PPM onto a single carrier frequency or transmitted as baseband pulses.

The ML920 receiver is a 24-pin PMOS/ LSI integrated circuit which, after de-modulation of the incoming signal, first verifies and compares two consecutive code words. The signal is then decoded to give 20 channels, three analogue controls plus six other control functions.

Features of the receiver i.c. include all timing from an on-chip oscillator and automatic error detection. Only 6µA of current is taken from the 9V supply by the transmitter on standby.

Typical applications would be the remote control of toys and models and domestic remote controls such as garage door operation, TV and hi-fi control. The transmitter and receiver can be combined to give a flexible system using as the control link a cable, sound, ultrasonics, visible light, infrared or radio frequency.

Further details, price and stockists can be obtained from Celdis Ltd., Active Components Division, Dept EE, 37 Loverock Road, Reading, Berks, RG3 1ED.

Remote Control

Talking of radio frequency, the Toko i.c.s. KB4446 and KB4445, available from Ambit International, provide the designer with the opportunity to build a 4-channel f.m. radio control receiver and transmitter on the 27MHz band.

All necessary data is contained in a comprehensive data sheet which comes with the i.c.s. Also contained in the data sheet are two circuits, one for the transmitter and one for the receiver. The system is based on the standard 27MHz band, i.e. 9.6V operation for the transmitter and 4.8V for the receiver, 1-2ms pulse width.

The transmitter i.c. (KB4445) only requires the channel and r.f. timing components together with an r.f. power transistor around it to give a practical working circuit. In the case of the receiver (KB4446) there are two input tuned coils together with a mixing coil, an i.f. ceramic filter and a detector coil, which with a sprink-ling of R's and C's is all that is required. With the addition of a transistor in the r.f. input stage the sensitivity can be increased from 40μ V to 2μ V.

To sum up, these i.c.s. are a good buy for the home constructor wishing to develop his own radio control system.

Available from Ambit International, Dept EE, 200 North Service Road, Brentwood, Essex, CM14 4SG, the current price of the KB4445 is £2.30 and the KB4446 £2.65 including VAT. If purchased as a pair the combined cost will be £4.75. A charge of 35p post and packaging is levied.

The versatility of the miniature EZ test hooks have often proved invaluable in the workshop when checking out experi-mental "lash-ups". The only criticism has been that the interconnecting wires tended to get in the way and often been more an hindrance than help.

To allow greater flexibility of movement. when making test connections, EZ Hooks have recently been introduced joined by a p.v.c. coil cord which expand from a closed position of 180mm to 915mm. The leads are available in ten colour-coded colours.

Further information on the complete range of EZ Hooks is available from the British Central Electrical Co. Ltd., Dept EE, Unit 10 Carvers Industrial Estate, Southampton Road, Ringwood, Hants, BH241JS.

CONSTRUCTIONAL PROJECTS

Weather Centre

This months concluding article for the Weather Centre project deals with the hardware. It is difficult to generalise on any supply problems as this will obviously vary from area to area and any good DIY or Hardware shop should be able to supply most items.

The TV aerial claw clamp for securing the boom to mounting pole was purchased

through a Tandy store.

The only electronic items of note in this part of the Weather Centre are the infra red emitter (TIL32) and the infra red detector (TIL78). These are available from several suppliers and should not be difficult to find.

Lights Failure Monitor

No purchasing problems should be experienced with components for the Lights Failure Monitor.

In view of the large number of semiconductor devices required some advertisers may even be willing to quote a special price for a "semiconductor pack" for this project.

Bedside Radio

Most components for the Bedside Radio are generally available and should not cause concern.

However, should any readers have difficulty in obtaining the Dielecon 300pF tuning capacitor this is available from Home Radio. Also, suitable aerials are the MCW2 from Ambit International and the MW5FR from Denco Ltd., Dept EE, 355 Old Road, Clacton-on-Sea, Essex, CO15

Precision Parking Pad Choosing and locating a magnet for the reed switch operation could prove quite a problem for the Precision Parking Pad. Probably one of the Eclipse range from James Neill (Sheffield) Ltd., would prove most suitable. The Minor 801 magnet or the 811 Power Magnet would seem to be ideal. These should be stocked by any good hardware shop.

No troubles should be encountered with the rest of the components for this project as they are generally available from most advertisers.

Duo-Deci Timer

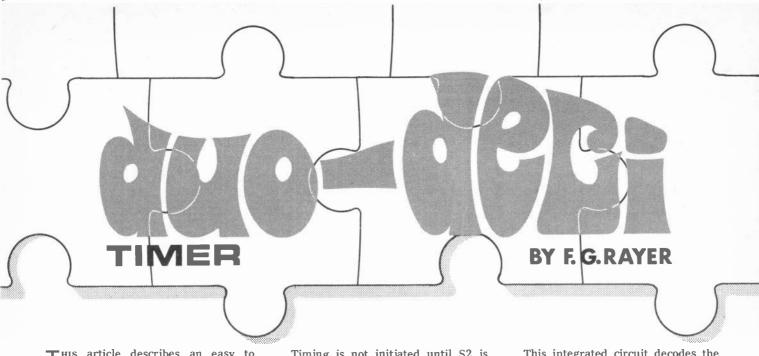
Checking through the list of components for the Duo-Deci Timer we cannot foresee any supply snags. People like Maplin, Watford, and Marshalls seem to stock most items.

TTL Logic Probe

No buying problems should be experienced with parts for the TTL Logic Probe. Most of our advertisers who specialise in semiconductors should be able to meet any orders.

TTL Power Supply

Standard parts are used throughout the TTL Power Supply and there should be no problems in obtaining components. The transformer should have an output of at least 6V and a rating of not less than 2A. The Universal Chassis member is available from Home Radio, catalogue number CU56A and the voltage regulator, type LM309K, can be found in most suppliers' catalogues.



This article describes an easy to build two-digit timer with optional decimal point.

To time an egg, develop a film or do some other process taking up to a maximum of 9.9 minutes, the "fast" range is used.

For fixing and washing film or prints, barbecuing sausages or parking time watching, the "slow" range is selected.

Operation is from a 4.5 volt battery or from a mains operated battery eliminator if the timer is used extensively.

CIRCUIT OPERATION

Fig. 1 shows the complete circuit and its operation is straight forward and easily followed. Power is applied to the circuit via S3 and no more than 5 volts should be used because of the TTL devices in the unit.

The "fast" or "slow" range is selected by means of S1. With S1 in the "0·1" position, capacitor C1 charges through VR1 and R1. When the emitter of the unijunction transistor TR1 reaches sufficient potential due to C1 charging, TR1 conducts and discharges C1.

The process is repeated over and over again, and VR1 is adjusted so that this takes place at 0·1 minute or 6 second intervals. When S1 is in the "1" position, C1 charges through VR2 and R2 so that pulses are produced at the rate of one per minute instead of one every tenth of a minute.

The decimal point on X1 is illuminated when S1b is in the 0·1 position. It will be seen that the device will read down to 0·1 minutes on the "fast" range and 1 minute on the "slow" range and it is felt that this is easily close enough for the sort of activities the author has in mind. The two-range, two-figure indication also allows considerable simplification.

Timing is not initiated until S2 is closed. When this happens S2a applies voltage to TR1 and associated components whilst S2b previously held open to keep the display at 00 closes to allow the pulses to be counted.

COUNTER

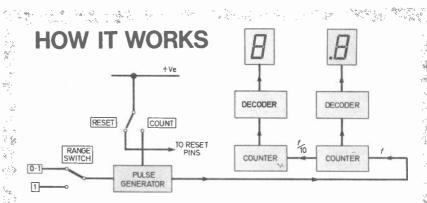
The counter i.c. IC4 is driven by the pulses from TR1 via TR2. These pulses are delivered at either 0·1 or 1 minute intervals, according to the setting cf S1. The 7490 chip, IC4, is a binary coded decimal decade counter. It receives pulses at pin 14 and translates these into a binary output at pins 11, 8, 9 and 12. These binary outputs pass to pins 6, 2, 1 and 7 of the 7447 decoder-driver i.c. IC3.

This integrated circuit decodes the binary inputs into a form that will drive the displays X1 and X2 and this appears at pins 9 to 15. Decoding is so arranged that the correct sectors of the seven-segment display are illuminated to display the numbers.

The components IC1, IC2 and X2 thus count from 0 to 9 as pulses arrive at pin 14 of IC4.

TENS AND UNITS

At the next pulse, IC4 provides an input to IC3 which is decoded to return the numeral to 0 and a pulse passes from pin 11 of IC4 to pin 14 of IC2. This then provides a binary output for the number one which is decoded by IC1 and thus the "tens" numeral is advanced.



An oscillator provides pulses at the rate of one every second or tenth of a second according to the setting of the range switch.

These pulses are passed on to the first counter which causes a sevensegment display to count up by one every time a pulse is received.

Every tenth pulse causes the display to return to zero and pass a single pulse on to the next stage where it is counted in the same way.

When 99 pulses have been received, the displays both return to zero and the process starts all over again.

To reset, the power is removed from the oscillator and fed to the reset inputs of the counters.

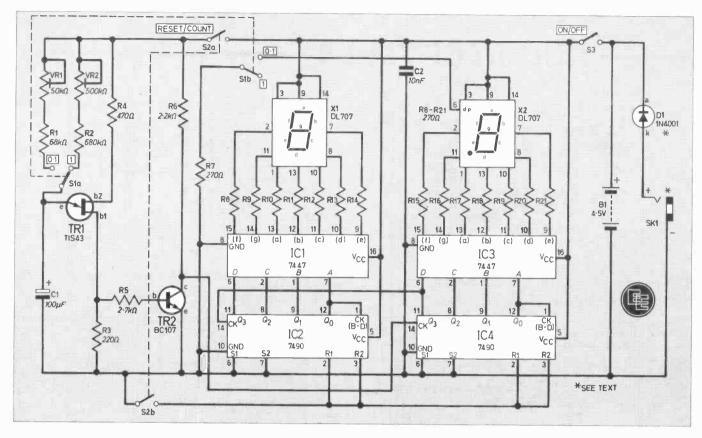


Fig. 1. Full circuit diagram of the Duo-Deci Timer.

This continues until 99 is reached. For the "fast" range, the decimal point is switched on and lies to the right of the units digit, that is between the two numbers. In fact this forms part of X2 and is illuminated when pin 6 is earthed.

If a battery eliminator is used, it should be plugged into SKI. It must be at a voltage of less than 6 volts.

Diode DI is used to provide protection against the battery eliminator being connected the wrong way round and also drops the voltage down by about 0.6 volt thus allowing the more common kind of eliminator or even a large 6 volt battery to be used.

Outside view of completed unit.





THE CASE

The timer is designed to fit into a case measuring $100 \times 70 \times 40$ mm, and is therefore very compact in construction

Cut the 0·1 inch s.r.b.p. matrix board down to 76×52mm and place it against the top of the case. This will enable you to position the holes for the three 8BA mounting bolts which can be drilled through the board and the case. Once the holes have been drilled, the three 8BA bolts can be fastened in position and spacers added so that the board stands about 8mm clear of the front of the case.

Apertures are made to match the positions of the displays X1 and X2. This can be done accurately by drilling a few small holes so that a small flat file can be introduced. The holes are then filed to shape, checking as necessary that they will agree with the actual positions of the displays on the circuit board.

Afterwards, with the board removed, make three slots for the switches. Again a few small holes are drilled and the holes filed to shape. Of course you will also need to drill holes for the securing screws as well as these slots. The switches should be left off for the time being.

The battery used in this project is a three-cell flat battery type 1289 and it lies horizontally on top of the circuit board. Card or similar material is placed between the board and the battery.

THE I.C.S

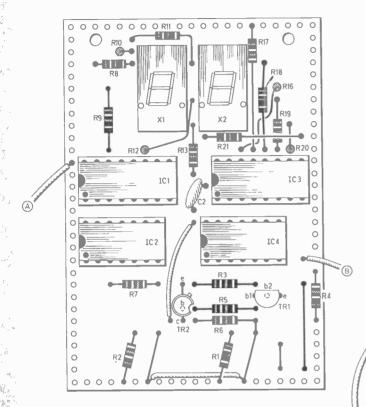
The i.c.s fit into 14- and 16-pin d.i.l. holders. Although not absolutely essential, they save a great deal of time and trouble when securing the i.c.s and there's no worry about thermal damage. This also applies to the displays X1 and X2.

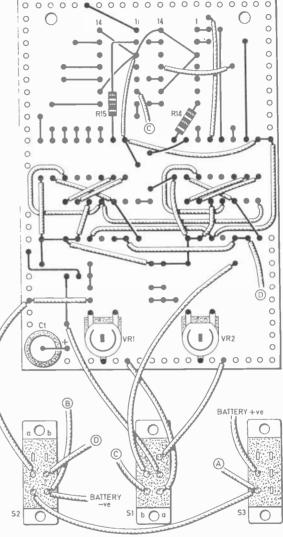
Make sure you insert the i.c.s correctly when all the construction is completed. Pin one is always identified by a spot or indentation on the body.

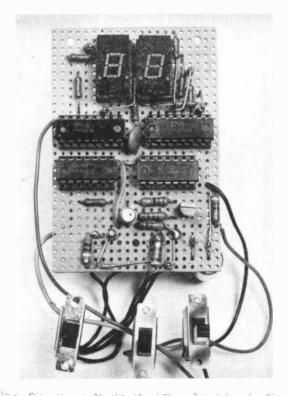
CIRCUIT BOARD

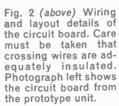
Assembly again is fairly compact and a few points should be noted. Fig. 2 shows the top or display side and also the underside. Pre-sets VR1 and VR2 are mounted on the underside so that they can be adjusted.

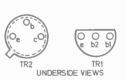
DUO-DECI TIMER











FILLUMANTS
approximate
SUST. £10

When fitting the components make sure that all components are mounted lower than the top of the display chips. The transistors will therefore be very close to the board. Care must be taken to heatsink the transistors when soldering.

The resistors R7 to R21 which are in series with various segments of the displays should be as small as possible in size and 18 watt types will be adequate.

The first job when assembling the board is to wire the power lines to the i.c.s; positive to pins 3, 9, and 14 on X1 and X2, pins 16 on IC2/4 and pins 5 on IC1/3; negative to pins 6, 7 and 10 on IC2/4, and pins 8 on IC1/3. Other connections can then be put in as shown in Fig. 2.

Positive and negative circuits are wired with thin flex or 22 s.w.g. wire, although 30 s.w.g. is strong enough elsewhere and is much more easily handled. Sleeving is added as and when required.

With R16, R20 and R21, the leads should be shaped so that no short circuits can arise, these components being near R17, R18 and R19.

It is helpful to use colour coding for some of this wiring, especially things such as red for positive, black for negative and orange for re-set

COMPONENTS ****

Resistors

R1 $68k\Omega$ R2 680kO 2200 RR R4 470Ω R5 $2 \cdot 7k\Omega$ $2 \cdot 2k\Omega$

R7-R21 270Ω & W miniature (15 off)

All 1W carbon + 5% unless otherwise specified



Potentiometers

50kΩ miniature horizontal preset VR2 $500k\Omega$ miniature horizontal preset

Capacitors

100μF 6V elect. 10nF disc ceramic

Semiconductors

TIS43 n-channel unijunction

TR2 BC107 npn silicon

7447 b.c.d. to seven segment decoder/driver (2 off)

IC2, IC4 7490 b.c.d. decade counter (2 off) 1N4001 1A 50V silicon diode D1

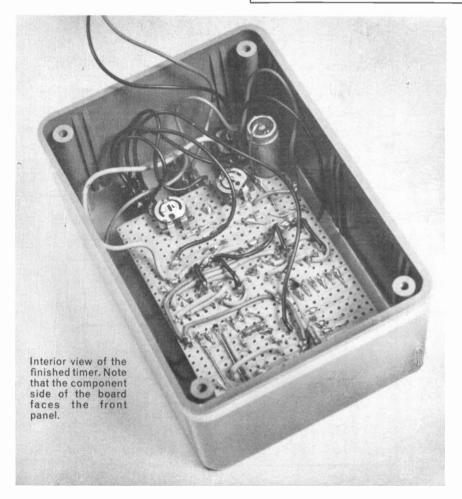
X1. 2 DL707 8mm common anode seven segment display (2 off)

Miscellaneous

S1, 2, 3 SK1 d.p.d.t. slider switch (3 off)

3.5mm jack or other socket to suit battery eliminator

B1 4.5V flat pack battery type 1289 Plastics box, size $100 \times 70 \times 40$ mm; 0.1 inch perforated s.r.b.p. board, size 52×76 mm; 14 pin d.i.l. i.c. sockets (4 off); 16 pin d.i.l. i.c. sockets (2 off); 16 pin d.i. nuts, bolts and spacers; inter-connecting wire; stiff wire for battery connectors.



OFF-BOARD CONNECTIONS

The switches and battery are wired to the board using thin stranded wire. Situate the switches approximately on the front panel according to Fig. 2 and wire them to the various points on the board, leaving an inch or so of extra wire. Note that S2 and S3 are joined. Battery negative also runs from S2.

Flat clips for the battery can be made from thin metal or paper clips and soldered to the leads, so that they can be fastened to the battery. Make sure that you connect up with the correct polarity.

TESTING

This is most readily done before fitting the board or switches in the case. Initially set VR1 and VR2 at about middle position. Closing S3 should illuminate the displays and setting S1 at the 0.1 position should light up the decimal point.

With S2 closed, a count should begin to appear and run to 9.9. Meanwhile, VR1 can be adjusted so that the units change at exactly six-second intervals, or ten per minute.

Afterwards adjust VR2 for oneminute intervals. Opening S2 returns

the displays to zero.

The switches can then be bolted to the case and the board located on its three bolts and fixed with nuts. The back of the case can then be screwed in position. I

Experiments for

TEACH-IN 80

Part11

EXPERIMENT 11.1:

WEIN BRIDGE OSCILLATOR

Components needed: $100 \text{k}\Omega_4^*W$ resistor, $10 \text{k}\Omega_4^*W$ resistors (2 off), $330\Omega_4^*W$ resistor, $0.1 \mu\text{F}$ capacitors (2 off), CA3140 op-amp, BC108 transistor, BC478 transistor.

A sine wave oscillator circuit which drives a loudspeaker is shown in Fig. 11.11a with the layout of the components on the Tutor Deck in Flg. 11.11b.

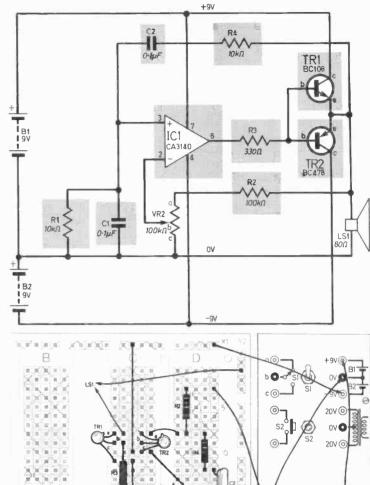
Because the op-amp itself cannot supply enough current to drive a loud-speaker directly, a buffer has been added in the form of the complementary pair transistors TR1 and TR2, with the resistor R3 used to limit the output current of the op-amp.

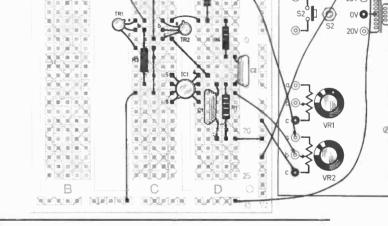
Feedback has been taken from the point where the buffer joins the speaker and a conventional Wien Bridge circult has been used.

The gain has been made variable by using a potentiometer VR2 to vary the voltage fed back to the inverting input.

When the circuit has been connected up note how altering the setting of the potentiometer VR2 alters the output. For part of the track there is no output: the icop gain is less than one. As the pot is turned up the oscillation begins but as it is increased the sound becomes much harsher because the output is being distorted as the voltage hits the power rail. At a smaller range of settings the sound is quite clean because a pure (or nearly pure) sine wave is being produced.

Fig. 11.11(a) (top right) The circuit of Experiment 11.1.
Fig. 11.11(b) The layout of Experiment 11.1 on the Tutor Deck.



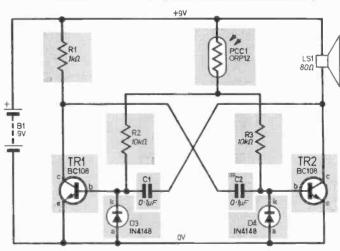


EXPERIMENT 11.2:

TRANSISTOR MULTIVIBRATOR

Components needed: $1k\Omega$ $\frac{1}{4}W$ resistor, $10k\Omega$ $\frac{1}{4}W$ resistors (2 off), ORP12 light dependent resistor, $0\cdot 1\mu F$ capacitors (2 off), BC108 transistors (2 off), IN4148 diodes (2 off).

The circuit of Fig. 11.12a shows a simple multivibrator whose frequency is set by the amount of light falling on a light dependent transistor.



EXPERIMENT 11.3:

OP-AMP MULTIVIBRATOR

Components needed: $10 \mathrm{k}\Omega$ $\frac{1}{4}\mathrm{W}$ resistors (2 off), 330Ω $\frac{1}{4}\mathrm{W}$ resistor, ORP12 light dependent resistor, $0.1 \mu\mathrm{F}$ capacitor, CA3140 op-amp, BC108 transistor, BC478 transistor.

An op-amp version of the multivibrator is shown in Fig. 11.13a with the layout on the Tutor Deck in Fig. 11.13b. Again the output buffer circuit has been used to enable the op-amp to drive a speaker.

When the output (at the speaker) is at its most positive the capacitor charges at a rate determined by the resistance of the l.d.r. The voltage at pin 3 of the op-amp

will be approximately +7V.

When the voltage on C1 reaches this voltage the inverting input will be higher than the non-inverting so that the output will now swing to near the negative supply rail. The voltage at pin 3 is now —7V and C1 discharges through the l.d.r. until it reaches this voltage. The output then swings positive and the cycle starts again.

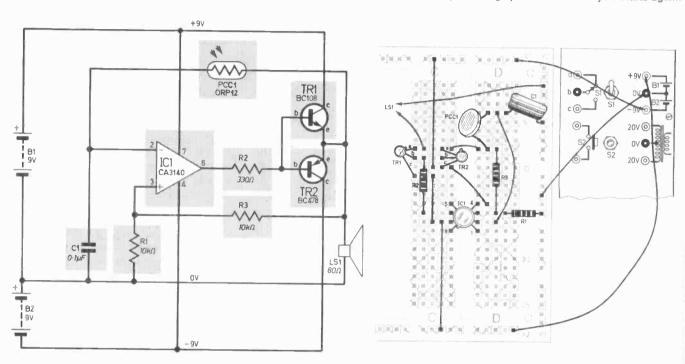
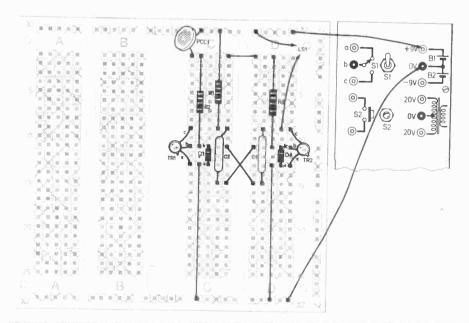


Fig. 11.13(a) The circuit of Experiment 11.3.

Fig. 11.13(b) The layout of Experiment 11.3 on the Tutor Deck.



The on and off times are the same for both TR1 and TR2 since the circuit is symmetrical. The load of one of the transistors is the speaker itself which saves using a separate amplifier stage.

Moving the hand across the l.d.r. will change the note from a high pitch to a very low pitch.

Note the diodes which are placed across the base to emitter junctions of both transistors. These are required to prevent the voltage on the base being pulled to —8·3V when the collector voltage on the opposite transistor goes from 9V to 0V. If the base is pulled more than 5V negative with respect to the emitter, there is the possibility that the transistor will be damaged.

Fig. 11.12(a) (far left) The circuit of Experiment 11.2.
Fig. 11.12(b) The layout of Experiment 11.2 on the Tutor Deck.



N EXT to the common bipolar transistor the most important semi-conductor device must be the field effect transistor or f.e.t.

Discrete f.e.t.s are similar to ordinary transistors in that they have three terminals, one of which controls the current flow from one of the other terminals to the third. However the principles upon which f.e.t.s are based are quite different from the bipolar transistor and hence it has unique properties which enable it to be used in applications where bipolar transistors need a great deal of external components to do the same job.

The other reason why f.e.t.s. are so important is that they are by far the most widely used type of transistor in logic integrated circuits (i.c.s).

F.e.t.s can be made very small and therefore an extremely large number of logic elements can be packed together on a single chip of silicon. This has enabled the development of microprocessors with tens of thousands of components on a single chip at a price that is well within the grasp of amateur constructors.

THE FIELD EFFECT

The field effect principle was developed in the early fifties, just when mass manufacture of bipolar transistors was starting.

The basic idea behind field effect is superficially much easier to understand than the principles behind the bipolar transistor.

A diagram of the geometry of a junction field effect transistor is shown in Fig. 12.1. Essentially the f.e.t. consists of a chip of silicon,

SOURCE DRAIN

P-TYPE

GATE

part of which is doped so as to be *n*-type and part of which is *p*-type. The n-type region forms a **channel** through the *p*-type region and terminals are placed at either end of this region, these being given the names **source** and **drain**.

A third terminal makes contact with the *p*-type area of the chip under which the channel passes. This terminal is the control input and is termed the gate.

The diagram shows the channel made of *n*-type material but a complementary type of f.e.t. can be made with the channel made from *p*-type material and the rest of the chip *n*-type.

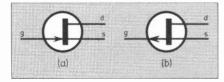
The description of the action of the field effect transistor which follows assumes *n*-type **channel**, but the operation of a *p*-**channel device** is similar except that all the voltage polarities are reversed.

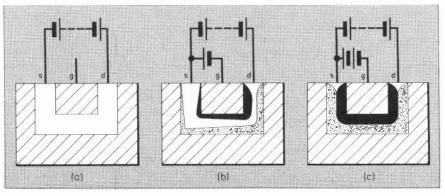
Fig. 12.2 shows the symbols for both *p*-type and *n*-type channel devices. As with the bipolar transistor, an arrow in the symbol distinguishes between the two types.

The channel through the f.e.t. normally has quite low resistance so that if a voltage is applied across the source and drain then a Fig. 12.1 (left) Diagram of the construction of an *n*-channel type junction f.e.t. The source and drain make contact with a channel which is completely surrounded by the gate region.

Fig. 12.2 (below) (a) the symbol for an n-channel junction f.e.t. and (b) the symbol of a p-channel junction f.e.t.

Fig. 12.3 (below) The reduction of the effective conductivity of the channel is shown as the gate is made progressively more negative with respect to the source. At (a) the gate is unconnected so there is no field. At (b) the gate is slightly negative thus reducing the effective cross-section of the channel and at (c) the gate is so negative that no current can flow through the channel.





current will flow. If now the gate is taken negative with respect to the source then the *p-n* junction will be reverse biased and a field will be set up within the channel.

The effect of this field is to reduce the number of current carriers in part of the channel. This effectively reduces the cross-sectional area of the channel thereby increasing its resistance. This effect is increased as the gate voltage is made more negative until a point is reached where the effective cross section of the channel has been reduced to zero making current flow from source to drain very difficult. Fig. 12.3 shows this process in diagrammatic form.

The essential point to note is that the f.e.t. is operated with its p-n junction reverse biased so that only a tiny leakage current flows through the gate terminal. They can therefore be described as voltage operated devices rather than current operated devices as bipolar transistors are.

It is the fact that the gate terminal of f.e.t.s has extremely high impedance that gives them their unique properties. The main application area is in the amplification of signals from high impedance sources, that is sources which cannot stand low impedances placed across them. A crystal for instance as used in high stability oscillators cannot supply current and so the high impedance of the f.e.t. is very useful.

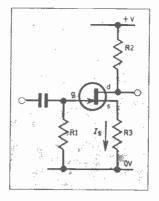
F.E.T. CHARACTERISTICS

Table 12.1 shows the characteristics for a 2N3819 n-channel f.e.t. Because the device operation is different from the bipolar transistor, the parameters quoted are different.

Like the transistor we need to know the maximum current which can be passed through the f.e.t. without damaging it. This is given the name $I_{\rm dss\,(max)}$. The maximum power dissipation is quoted as $P_{\rm tot\,(max)}$.

The maximum drain to source voltage is $V_{\rm ds\,(max)}$, and the maximum drain to gate and gate to source voltage are $V_{\rm dg\,(max)}$ and $V_{\rm gs\,(max)}$ respectively.

The leakage current through the gate terminal is an important parameter in f.e.t.s since the lower this is, the higher the input impedance can be. This parameter is given the name $I_{\text{gas}(\text{max})}$.



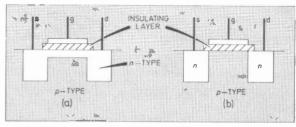


Fig. 12.4 (left) This circuit shows a simple way of biasing a junction f.e.t. so that the gate is negative with respect to the source. The voltage drop across R3 determines the negative bias since R1 holds the gate at 0V.

Fig. 12.5 (a) shows the construction of an *n*-channel depletion type m.o.s.f.e.t. and (b) an enhancement type m.o.s.f.e.t. The gate is separated from the silicon by an oxide insulating layer.

TABLE 12.1: 2N3819 characteristics

Type	P _{tot} (max)	/ _{dss} (max)	/ _{gss} (max)	V _{ds} (max)	V _{gs} (max)	V _{dg} (max)	Yfs
2N3819	200mW	20mA	2n A	25V	25 V	25V	4000μmho

The "gain" of an f.e.t. cannot be expressed in the same way as in a transistor since what is important is the change in current from source to drain with the change in voltage on the gate with respect to the source.

Now current divided by voltage is the inverse of resistance and is given the name **conductance**. The change in current produced by a change in voltage is therefore given the name **transconductance** and given the symbol $Y_{\rm fs}$. Its units are **mhos** or **micromhos**, one mho being a change of one amp for a change of one volt.

F.E.T. BIASING

The circuitry around f.e.t.s is different from that around bipolar transistors because of the fact that virtually no current flows in the gate terminal.

In order to use an *n*-channel f.e.t. as a linear amplifier the gate must be biased negative with respect to the source. If there is only a single supply rail then a simple way of achieving this is as shown in Fig. 12.4.

Current flowing through the source resistor R3 will produce a voltage drop across this resistor which can be calculated using Ohm's Law. A resistor R1 connects the gate to the 0V line and since virtually no current flows through this resistor, the gate will be at 0V. Because of the voltage drop across R3, the gate will therefore be negative with respect to the source which is what we are trying to achieve.

The resistor connected to the gate can be made large so that the input impedance of the circuit is kept high. Values of a few megohms and upwards are common. The signal which is to be amplified can be applied using a.c. coupling to the gate and the output can be taken from the drain.

As well as the f.e.t.s which we have looked at so far which go under the name of **junction f.e.t.s** there has grown up a number of other types of f.e.t. and we will now take a look at some of the more important types.

M.O.S.F.E.T.S.

Undoubtedly the most important type of f.e.t. to the semiconductor integrated circuit manufacturer is the metal oxide silicon (or semiconductor) f.e.t., usually abbreviated to m.o.s.f.e.t.

The underlying principle of the m.o.s.f.e.t. is the same as the junction f.e.t. in that an electric field is used to control the conductivity of a channel, but the construction and detailed operation are different.

Instead of the gate terminal being a connection to a part of the silicon, an insulating layer is formed over the channel, the gate being an area of metal on top of this insulating layer which completely covers the channel.

Two types of m.o.s.f.e.t. can be produced: in one the field produced by the gate to source voltage can decrease the conductivity of the channel, as in the junction f.e.t., or increase it, this being known as a

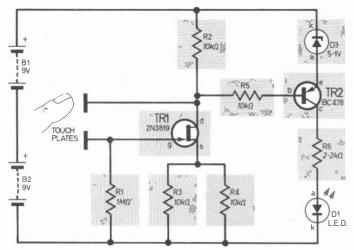
EXPERIMENT 12.1 TOUCH SWITCH

Components needed: $10k\Omega$ ¼W resistor (4 off), $2 \cdot 2k\Omega$ ¼W resistor, $1M\Omega$ ¼W resistor, 2N3819 f.e.t., BC478 transistor, 5 · 1V 400mW Zener diode.

The circuit of Fig. 12.10a shows a simple touch switch that can be built using an *n*-channel junction f.e.t. type 2N3819. The f.e.t. is biased into conduction using the self-biasing arrangement as described in the text. In this state there should be only about 2V across R2 the drain resistor.

A finger has a skin resistance of around a few hundred kilohms so when it is placed across the two contacts the biasing of the f.e.t. is substantially changed causing a much greater drain current to flow and hence a greater voltage to be developed across R2.

The voltage change across R2 is detected by TR2. A $5\cdot1V$ Zener diode is



placed in series with the emitters othe base must be at least 5.8V (Zener voltage $+V_{be}$) below the positive rail before

it will conduct. The load for TR2 is formed by the l.e.d. and its current limiting resistor R6.

Fig. 12.10(a) (top right) The circuit of Experiment 12.1. Fig. 12.10(b) (below) The layout of Experiment 12.1 on the Tutor Deck.

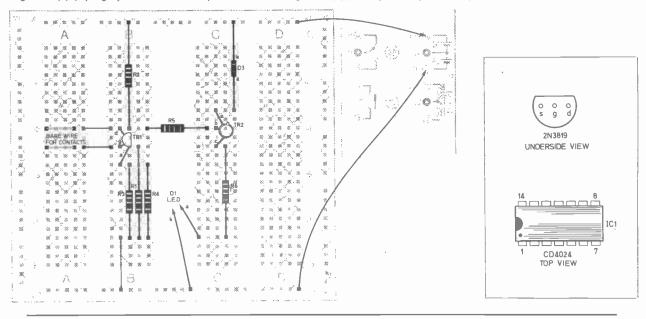
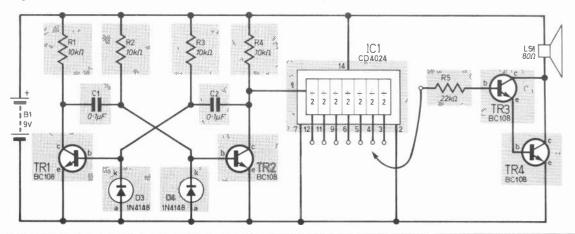


Fig. 12.12(a) The circuit of Experiment 12.3. Fig. 12.12(b) (right) The layout of Experiment 12.3 on the Tutor Deck.



EXPERIMENT 12.2: TIME DELAY USING A F.E.T.

Components needed: $1M\Omega$ $\frac{1}{4}W$ resistor (2 off), $10k\Omega$ $\frac{1}{4}W$ resistor (2 off), $2\cdot 2k\Omega$ $\frac{1}{4}W$ resistor, 10μ F 16V tantalum capacitor, 2N3819 f.e.t., BC478 transistor, $5\cdot 1V$ Zener diode.

The circuit of Fig. 12.11a shows a timer circuit using the same f.e.t. as Experiment 12.1. There is no source resistor in this circuit as we want to keep the voltage across the two $1 M \Omega$ resistors R1 and R2 as low as possible.

When the pushbutton is pressed C1 charges up to about 16V. The gate of TR1 is at a voltage of about 1.5V so about 1.5V divided by $2M\Omega$ (0.75 μ A) flows through R1 and R2.

When the pushbutton is released, C1 will start to discharge. Because of the very high impedance of TR1 gate, all the discharge current flows through R1 and R2. The drain voltage will thus fall steadily until the voltage across R3 is large enough to cause TR2 to conduct when the l.e.d. will light.

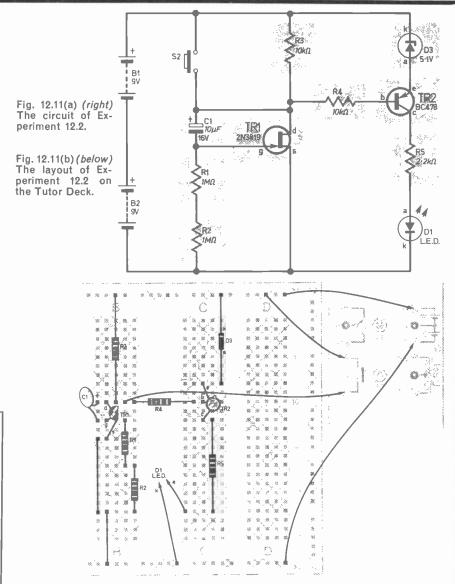
The changeover from l.e.d. off to l.e.d. on is not particularly rapid and a Schmitt trigger in place of TR2 would be advantageous.

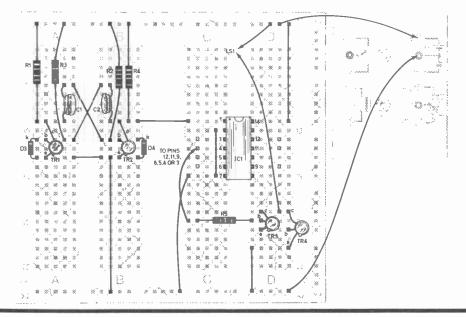
To start the timing cycle again, press the pushbutton.

EXPERIMENT 12-3: VARIABLE PITCH OSCILLATOR

Components needed: $10k\Omega$ $\frac{1}{4}W$ resistors (4 off), $22k\Omega$ $\frac{1}{4}W$ resistor, $0\cdot1\mu\mathrm{F}$ capacitors (2 off), CD4024 7-stage CMOS divider, BC108 (4 off), 1N4148 diodes (2 off).

This circuit (Fig. 12.12a) makes use of a CMOS integrated circuit type CD4024. This circuit contains seven dividers connected in series each of which will divide their input frequency by two.





TR1 and TR2 are connected to form a multivibrator as has been described in detail in a previous issue. The voltage at the collector of TR2 is a square wave of frequency about 700Hz. This is applied at the start of the divider chain.

TR3 and TR4 are connected in the Darlington pair configuration. This is so that the relatively small output current which the CMOS circuit can supply can be used to drive the loudspeaker.

The loudspeaker driver can be connected to any of the output pins of the divider. Working along the pins in sequence as shown in the circuit, the output tone will have a gradually lower pitch. In fact each step lower will be an octave below the previous note.

This circuit illustrates how integrated circuits can be used to perform complex functions which would take many discrete transistors to build. It also shows how easy it is to drive CMOS circuits since we do not have to use a precise power supply nor one of high current capability. Nearly all the current drawn from the batteries goes into the speaker.

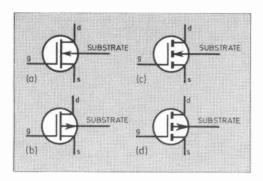
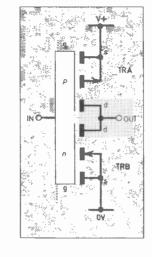


Fig. 12.6. The symbols for the various types of m.o.s.f.e.t. (a) and (b) are depletion types whilst (c) and (d) are enhancement types. (a) and (c) are n-channel and (b) and (d)

Fig. 12.7 (right) A CMOS inverter formed from a complementary pair of enhancement type m.o.s.f.e.t.s.



depletion type m.o.s.f.e.t.; in the other there is no channel between the drain and source until a gate voltage of a given magnitude is applied, this being known as an enhancement type m.o.s.f.e.t.

Fig. 12.5 shows the geometry of the two types, which, like the junction f.e.t. can either be made with a p-channel or an n-channel.

The symbols distinguish between the depletion and enhancement types by using a dotted line between the drain and source to indicate that the enhancement type needs a gate voltage to complete the path (Fig. 12.6).

12.1. How many p-n junctions

12.2. Large scale integrated cir-

cuits are usually made with

12.3. CMOS logic uses what

which type of transistor:

b) junction f.e.t.

c) m.o.s.f.e.t.

are there in a junction f.e.t.:

a) 1

b) 2

c) 3

d) 4

a) bipolar

PART 12 QUESTIONS

The n-channel m.o.s.f.e.t. is an important member of the family since it can be used with a single positive power supply. The gate does not need to be biased negative with respect to the source since a positive voltage on the gate is needed to produce current flow in the drain-source circuit.

LOGIC INTEGRATED CIRCUITS AND F.E.T.S.

High density logic integrated circuits use field effect transistors almost exclusively although the technologies used vary widely.

change of 0.5V in the gate voltage. What is its transconductance:

- a) 3000 µmho b) 300 umho
- c) 3mho
- d) 0.3mho

12.5. A 2N3819 f.e.t. with a transconductance of 4000µmho is blased so as to act as a linear amplifier. What change in drain current would be produced for a 1V change in gate voltage:

- a) 4 µ A b) 4mA
- 40µA c)
- d) 2.5mA

type of m.o.s.f.e.t.: a) n-channel depletion

- b) n- and p-channel depletion
- c) p-channel enhancement d) n- and p-channel enhancement

12.4. A m.o.s.f.e.t. when suitably biased produces a change of 1-5mA drain current for

PART 11 ANSWERS

11.1 b). 11.2 c). 11.3 a). 11.4 b). 11.5 a).

The attraction of f.e.t.s in integration is that the actual f.e.t.s can be made very small in comparison with the area needed by bipolar types. They are also relatively simple to fabricate and consume only minimal power.

Logic circuits have been produced with an all p-channel m.o.s.f.e.t.s, all n-channel m.o.s.f.e.t.s and with both types on the same chip. This latter type of circuit goes under the name of complementary m.o.s. logic which is usually abbreviated to cmos. It is outstanding for its extremely low power consumption and warrants a more detailed look.

CMOS LOGIC

Complementary m.o.s. logic circuits use both n-channel and p-channel enhancement type m.o.s.f.e.t.s on a single piece of silicon. A single cmos switch is shown in Fig. 12.7.

Transistor A requires its gate to be negative with respect to its source in order for it to conduct. Transistor B requires its gate to be positive with respect to the source for it to conduct.

Since the two drains are connected and the two gates are connected it will be seen that when one transistor is on the other is off and vice versa.

In the off state the transistors have very high impedance so while one transistor is off and the other is on (it does not matter which) hardly any current will flow from one power supply rail to the other. It is possible for both transistors to conduct but this only happens when the gate voltage is exactly halfway between the power supply rails. If the switching voltage is rapid then this current will only flow for a very short time.

When either of the transistors is in the on state, its impedance is very low so the voltage at the common drain terminal will swing almost from one power supply rail to the other as the gate voltage is swung from low to high.

Another important feature of смоs circuits is that they will work over a very large range of power supply voltages. Typical commercial cmos circuits will operate with power supplies of anything from 3 to 15V. This contrasts dramatically with TTL logic circuits which will only operate with a voltage of $5V \pm 0.5V$.

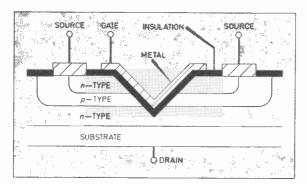


Fig. 12.8. The construction of a VMOS transistor. This differs from ordinary m.o.s.f.e.t.s in that it has a v-channel cut into the silicon.

The wide operating power supply range means that the power rail does not necessarily have to be pure d.c. but a large a.c. component can also be tolerated. Thus the power supply for a CMOS circuit does not have to be well-smoothed as it does for TTL and so can be relatively uncomplicated and thus cheap.

One problem with cmos circuits is that they can be damaged by the static voltage which is often present on the body. This is because the tiny capacitance on the gate has a very low leakage and so any charge tends to produce very large voltages which exceed the breakdown voltage of the junctions.

Try to avoid touching the leads of the i.c.s until they are in the circuit, leaving them in the conductive foam in which they are supplied.

F.E.T.S. IN LINEAR I.C.S.

In the last few years integrated circuit manufacturers have managed to combine f.e.t. and bipolar

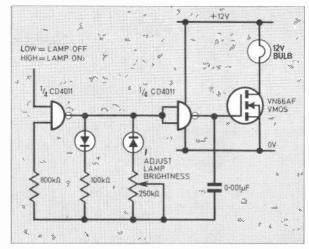


Fig. 12.9. This circuit illustrates how easy it is to interface low power logic in the form of CMOS to a high current output in the form of a lamp.

transistors on a single chip thus producing operational amplifiers with extremely high input impedances but good drive capability and speed. Usually just the input stage is f.e.t. but some op-amps are made entirely from m.o.s.f.e.t.s.

The CA3140 op-amp which has been used in past articles is a combination of m.o.s. and bipolar technologies and the figures quoted earlier testify to its extremely high input impedance.

POWER F.E.T.S.

Until the last couple of years f.e.t.s have not been produced which are capable of operating at high currents or powers. This gap has now been filled by a new breed of discrete f.e.t. known as v-channel m.o.s.f.e.t.s or vmos for short.

Conventional geometry of m.o.s.f.e.t.s meant that high currents could not be achieved with-

out huge chip area so a radically different geometry was needed. Fig. 12.8 shows a typical vmos transistor and it will be seen that instead of simply building up layers on the surface of the silicon, a *v*-shaped groove has been cut which is used for the gate.

VMOS transistors can handle currents of 10A but even higher current types are now appearing. They tend to be of the *n*-channel enhancement type since this allows a single power supply to be used. The real attraction of these vmos transistors is that currents of 10A can be switched by low power logic like cmos making interfacing between logic and things like lamps or relays very simple indeed. Fig. 12.9 shows a typical circuit.

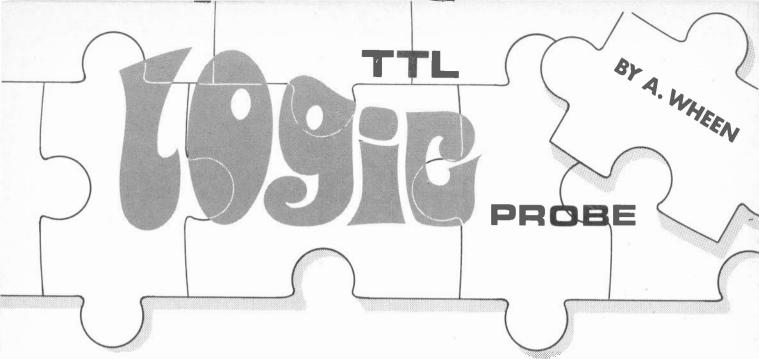
At the moment the price for these devices is very high but no doubt as the demand increases the price will fall and we will be seeing them used in EE projects.

JACK PLUG & FAMILY.

BY DOUG BAKER







ONE of the most useful pieces of test equipment for troubleshooting digital circuits is a logic probe. The probe to be described, which is for use on TTL devices, uses three l.e.d.s to indicate the state of the logic under test; these l.e.d.s are labelled HIGH, LOW and PULSE.

The HIGH and Low l.e.d.s indicate logic 1 and logic 0 respectively, and when the point under test is oscillating between logic 1 and logic 0 the relative brightness of these two l.e.d.s gives some idea of the mark-space ratio of the waveform.

The l.e.d. labelled PULSE flashes on for one second every time the logic level at the probe input changes state. This can be used for detecting very short duration positive or negative-going spikes, which are much too fast to be visible on the HIGH and LOW l.e.d.s.

CIRCUIT DESCRIPTION

IC1 is a quad Schmitt NAND circuit, with gates IC1a and IC1b being used as inverters and buffers. When the probe input is high (logic 1), D1 will light; similarly, when the probe input is low (logic 0), D2 will light. Since TTL regards an opencircuited input as being at logic 1, the output of gate IC1a will go low whenever the input is an open circuit.

To prevent the probe from indicating logic 1 for an open circuit input, TR1 was included in the circuit. Although a BC183 was used in the original design, any small npn transistor should operate satisfactorily in this circuit.

Integrated circuit IC2 is a quad 2-input exclusive-on device, and is wired so as to produce a short negative-going pulse whenever the probe input changes state. Since gates IC2a, b and c are all acting as inverters, the two inputs to gate IC2d are at opposite logic levels, and so the output of gate IC2d is high. However,

when the output of ICla changes state, this change will not be reflected in the output of gate IC2 until about 45 nanoseconds later because of the propagation delays in gates IC2a, b and c. Thus, for about 45 nanoseconds, the inputs to gate IC2d are at the same level, causing a 45 nanosecond negative-going pulse to be produced.

This pulse sets the flip-flop formed by IC1c and d, and D3 lights to indicate that a change of state at the probe input has been detected. The flip-flop resets itself about one second later when the voltage across C1 has dropped to 0.9 volt; C1 is then charged up again via R4.



CIRCUIT BOARD

The circuit is built on a piece of 0·lin matrix stripboard, size 9 strips by 29 holes. The i.c.s can be soldered directly to the board or mounted in Soldercon pins. If you wish to use i.c. sockets, note that some types mount the i.c. so high off the board that they will not fit in the case. Similarly, if you wish to use resistors rated at more than ¹4 watt, check that they can be fitted into the spaces allocated.

The case used in the prototype was an exhausted container for Multi-core solder with three holes drilled in the side and spaced so that the three l.e.d.s on the circuit board can be seen through them.

The layout of the components on the topside of the board and the breaks to be made on the underside are shown in Fig. 2. Note that there are some link wires to be connected beneath the i.c.s, and also on the underside of the board.

Begin by cutting the board to size and then filing it so that it is a little smaller than the internal diameter of the case.

Next make the cut-outs and solder in position all the link wires (above and below the board) followed by the components. Note the orientation of the l.e.d.s. These should be inserted so that the height to their tips above the board is a little more than the radius of the case. In this way, when the board is fixed in position the l.e.d.s will protrude a little allowing them to be seen more easily.

Drill three suitably sized holes in the case to align with the l.e.d.s on the board when the latter is in its final position.

Connect flying leads to the board, about 80mm to reach the probe point and about 1m for the supply lines. Red and black leads to represent "+" and "-" respectively are advised.

PROBE POINT

For the tip of the probe a small nail was used. The nail was driven through the centre of a cork shaped to fit the conical end of the tube and the section of the nail protruding from the cork was covered with rubber sleeving. It was necessary to enlarge the hole at the end of the tube so that the nail with its sleeving cover would fit tightly in it.

Solder the probe lead from the board to the head of the nail and cover the joint with some insulating tape.

Push the cork into the tube so that the nail protrudes through the hole in the tube. The cork can be glued in place, but in the prototype this was found to be unnecessary.

LOGIC PROBE

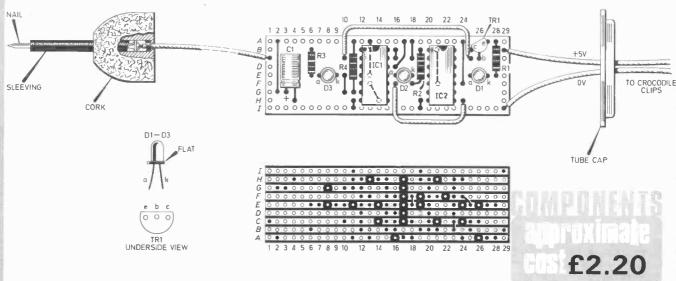


Fig. 2. Circuit board layout and construction. Note that there are three wire links on the underside of the board.

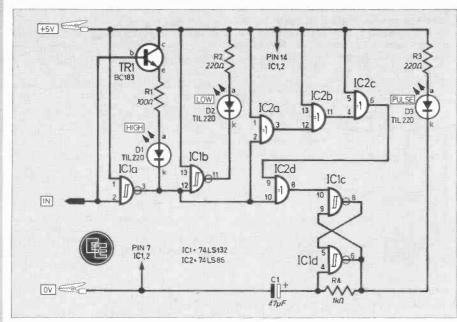
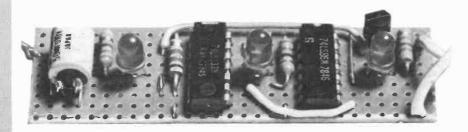


Fig. 1. Full circuit diagram of the Logic Probe.

The photograph below shows a close up view of the circuit board. The logic probe can be seen in its case in the right hand photograph.



COMPONENTS

Resistors	See
R1 100Ω	366
R2 220Ω	Shon
R3 220Ω	Oliop
R4 $1k\Omega$	Talk
All &W carbo	n ± 5%
	page 553

Capacitor C1 $47\mu\text{F}$ 10 V elect.

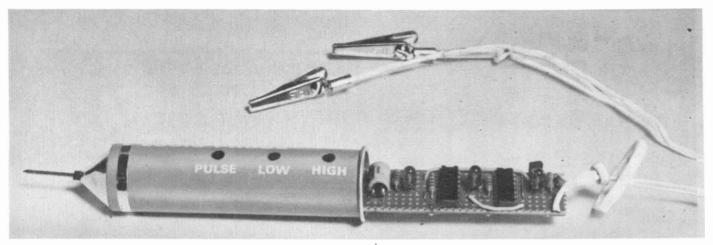
C1 47μ F 10V elec Semiconductors

IC1 74LS132 TTL quad 2-input Schmitt NAND gates IC2 74LS86 TTL quad 2-input exclusive-OR gates TR1 BC183 silicon npn

Miscellaneous

o-1 inch matrix stripboard, size 9 strips × 29 holes; Multicore solder dispenser (case); crocodile clips (2 off); stranded p.v.c. covered wire about 1 meter each red and black; cork and nail (probe tip assembly).





Exploded view of the unit showing the board ready for insertion in its case.

Next, drill a small hole in the white plastic cap which fits on the ends of the tube. Feed the supply wires through this hole and knot it inside the cap, allowing about 25mm of slack between the circuit board and the knot. The circuit board can now be fitted into the tube.

Ensure that l.e.d.s are lined up with their holes and then push the board upwards so that the l.e.d.s protrude through the holes. Secure in this position with a piece of polystyrene or foam sponge, Fit the cap

on the tube and crocodile clips on the two supply wires emerging from the cap.

TESTING

Carefully connect the supply leads to the power rails on a TTL circuit, or a p.s.u. set to +5 volt. Touch the probe on to the positive supply rail and the probe should indicate HIGH, D1 lit. Similarly, the probe should indicate Low (D2 lit) when touching the negative supply rail, and should

not indicate anything when the probe is not touching anything.

Check that the PULSE l.e.d., D3, flashes when the probe is touched on to the negative supply rail, and once again when it is removed from the supply rail.

Note that this l.e.d. will not flash when the probe touches the positive supply.

If all is well the case may be painted and the three l.e.d.s labelled with their function as shown in the photographs.



Readers' Bright Ideas; any idea that is published will be awarded payment according to its merit. The ideas have not been proved by us.

BIT REMOVAL

When one wishes to renew the copper bit of a soldering iron, one almost always finds that it is almost impossible to remove the old bit, since the surface between the bit and the bit holder has become badly corroded.

It may be possible to remove the old bit by drilling it out, but one normally adopts the easier task of replacing both the bit and the bit holder.

This problem can be avoided if a copious layer of silicone grease is placed on each new bit before it is placed in the bit holder. The grease should be kept well away from the tip of the bit which will be used for soldering, but the regions which will come into contact with the bit holder should be well covered.

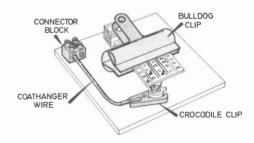
When the soldering iron is used, the silicone grease is converted into a white coating which seems to prevent appreciable

oxidation of the copper surface. The bit can be removed quite easily after the split pin has been taken out, since the white coating crumbles away.

J. B. Dance, Alcester, Warks.

MINI-BENCH

I have devised a simple, inexpensive circuit board holder for when you are soldering, as seen below.



To hold the circuit board I used a bulldog clip. The metal clasps could also act as heatsinks, but where delicate boards were used I stuck draught excluder tape along them. To hold the component in place coathanger wire is used with a crocodile clip attached to the end. This is held in place by a screw terminal block fitted to the base.

R. Harrison, Witham, Essex.

MEXT MONTH

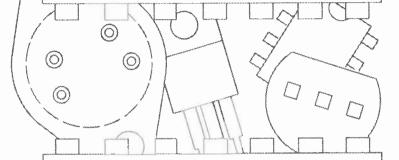
INTRODUCING MICROCIRCUITS

This special feature puts the layman in the picture concerning the silicon chip or integrated circuit. It provides a good lead-in to our NEW SERIES, commencing in the same issue.

I.C.s EXPLAINED

This series will discuss specific types of i.c.s. and illustrate typical circuit applications. The first four parts deal with LINEAR I.C.'s.

EE OPENS A NEW SEASON WITH A CLOSE LOOK AT MICROCIRCUITS



AND AS A VALUABLE BACK-UP TO THESE ARTICLES THERE'S A



UGALLCHART

GUIDE TO POPULAR LINEAR I.C.s with every copy of the October issue

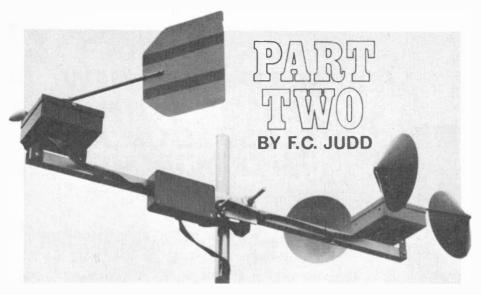
CONSTRUCTIONAL PROJECTS INCLUDE

AUDIO EFFECTS UNIT
PHONE CALL CHARGE JOGGER

DARKROOM CONTROLLER BICYCLE ALARM

Everyday ELECTRONICS

OCTOBER 1980
ISSUE ON SALE
FRIDAY, SEPTEMBER 19



This second part of the Weather Centre deals with the construction of the sensors and final adjustment and setting up.

The main outdoor items are the anemometer and wind direction units both of which are mounted on a boom that can be attached to a short mast on a chimney stack or similar position clear of the roof top of the home.

ANEMOMETER

The anemometer or wind speed unit is housed in an aluminium box as in the illustrations. Some mechanical work is involved in making the wind cups, chopper disc, etc, and it would be a good idea to study all the drawings and photographs before making a start.

The wind cups are first carefully cut out of aluminium sheet and folded into the required cone shape. The joins can be riveted or secured with small screws and nuts after which each cup is mounted on its arm with a 4BA screw and nut (see Figs. 13 and 14).

The three arms and cups should next be attached to the circular mounting plate (see Fig. 17). This consists of a 40mm diameter brass disc onto which a collar has been soldered. The disc is drilled through the centre with a 6mm clearance hole.

CHOPPER

The next stage is to make the circular Perspex infra-red chopper disc as in Fig. 17. Cut the material as near round as possible and slightly oversize then drill a 6mm hole through the centre.

Fit the nearly formed disc to an arbor and mount it in an electric drill which has been clamped to the bench. Using a file (for example a "Surform" type), to cut the disc edges, continue to turn the disc until it is perfectly circular and of the correct diameter.

The same method is used to turn the brass discs and also the rain protection discs, one of which is shown on Fig. 17.

The chopper disc is finished off by drilling 18 equally spaced 6mm diameter holes according to the diagram. The bushes used for the shaft are standard $^3{}_8$ inch brass types and the collars for the brass discs can be cut from standard $^1{}_4$ inch brass spindle couplers.

The disc should be given a couple of coats of paint to make it completely opaque before it is installed in the final unit.

The next step is to build the circuit board according to Fig. 11. The infrared l.e.d. D14 and the photo-transistor TR3, should be arranged so that they stand off the board and are bent at right angles facing each

other making sure that they are directly in line.

The completed board should then be mounted in position inside the aluminium box. The shaft which will take the chopper disc should be placed carefully in the bush through the bottom of the box and the chopper disc inserted between D14 and TR3. The shaft can then be pushed through the disc from beneath and tightened in position.

The top is then placed on the enclosure and the rotating assembly screwed in position. Note that there is a 6mm perspex disc between the cup assembly and the bush in the top of the case.

CABLES

The cables from the circuit board need only be about 600mm long and consist of one single screened wire and a single insulated wire. These are eventually connected to a junction box on the boom.

When assembly is complete the wind cups should rotate freely with a slight breeze on them. The cups should rotate quite easily and smoothly in a wind down to 2 m.p.h.

WIND DIRECTION UNIT

A 16-point compass wind direction indication is obtained from eight l.e.d.s on the readout display, these being activated by a series of reed relays operated by a magnet attached to a disc which is in turn fastened to the shaft of the wind vane (see Fig. 14).

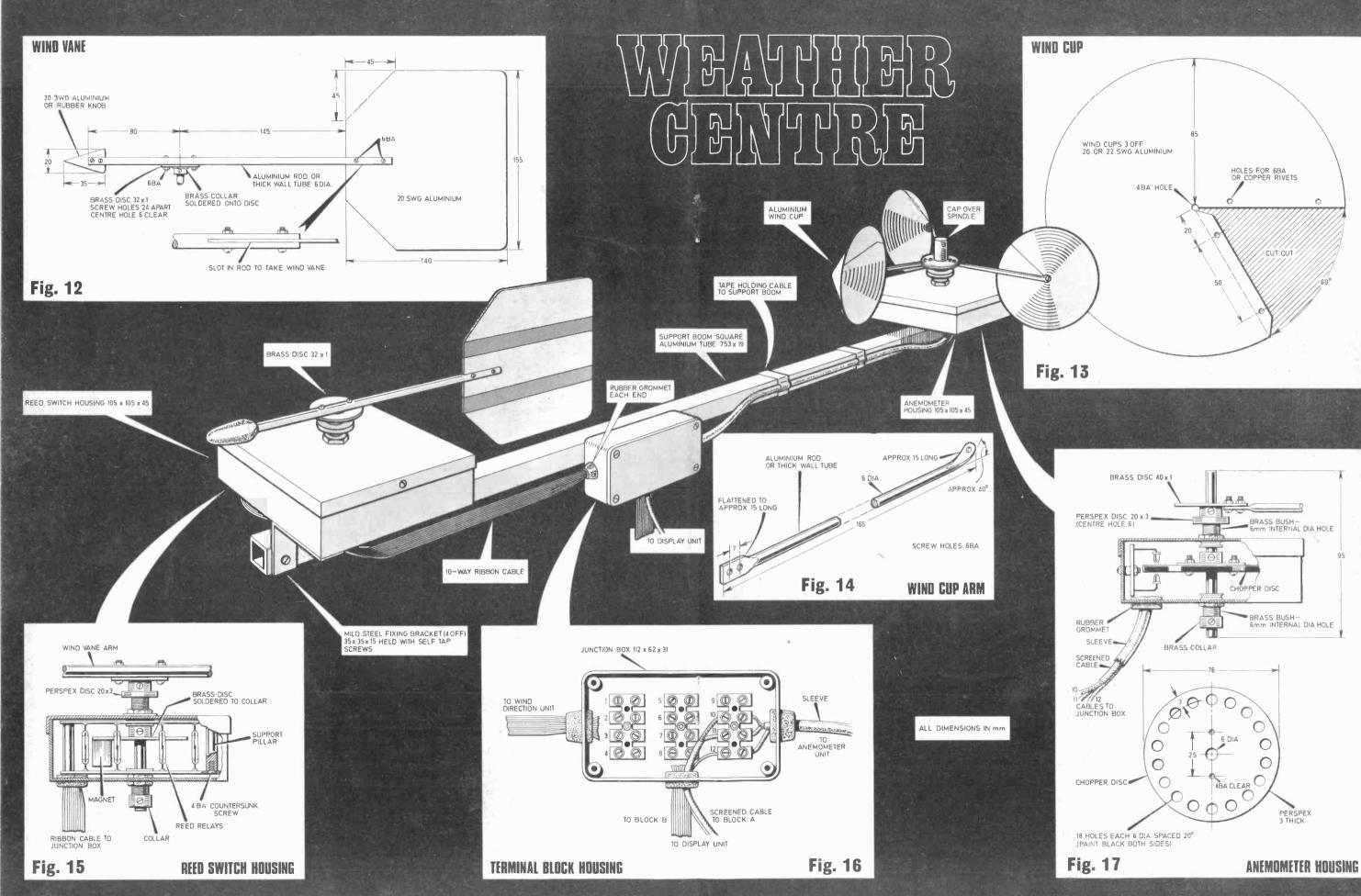
As can be seen from Fig. 15, the reed relays are assembled in a circle on circuit boards and enclosed in a protective aluminium box. These circuit boards can either be printed circuit boards or plain s.r.b.p. board with Veropins at the appropriate locations.

However, whichever method is used, the reed relays are all connected together on the top board as a common return and have separate connections on the bottom board. The lead outs here are by means of 10-way ribbon cable.

The diagram in Fig. 15 shows how the unit is put together. The metal work is almost identical to that of the wind speed unit, the only difference being that the rotating chopper disc is replaced by a brass disc to which a magnet has been glued with epoxy resin.

MAGNET AND ROTOR

In assembly of the direction unit, the one point that should be noted is that the rotor assembly and bottom board must be placed in position before the top board is soldered in. If this is not adhered to, it becomes



appropriate switch closed, as the vane is naived slowly round by hand from N through to N.

an oscilloscope is available, a preliminary check could also be made on the anemometer unit. Connect up a 12V battery with positive going to connection 12 on the terminal block, negative to connection 10. The output from connection 11 can then be fed to the oscilloscope.

Spinning the cups should produce a nearly uniform square wave as shown in Fig. 3 from Part One, last month

TEMPERATURE DIODES

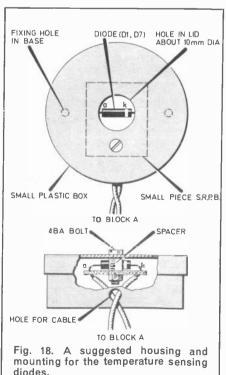
The final items in this project are the temperature sensing diodes D1 and D7 which are mounted in small plastic boxes, such as those used for typewriter ribbons, for protection.

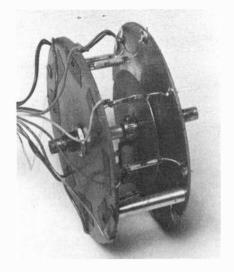
Before this is done, however, the equipment needs calibrating for each diode.

The specified meter has a scale of 0 to 100 in major units of 20, subdivided into divisions of 10 and 2 and therefore a total of 50 divisions. Each of these represent two degrees of temperature or 2 m.p.h. of wind speed.

TEMPERATURE CALIBRATION

No two diodes, even of the same type, have exactly the same current/ resistance characteristics, so the equipment must be calibrated separately for each sensing diode. For this purpose two wires are temporarily soldered to the ends of the diodes.





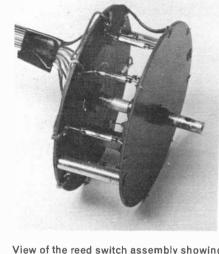
View of the reed switch assembly showing lower circuit board and common connection of the switches.

OUTSIDE TEMPERATURE

Take one diode and connect it up to the outside temperature terminals on the back of the main display unit. Make sure that the cathode of the diode is connected to the common or earthed input terminal.

Set the wind speed select switch S3 to "wind speed cal" and the temperature select switch S1 to "0 degrees cal". The l.e.d. D8 should be flashing slowly. Adjust VR3 until the meter reads 0 degrees which is 40 on the normal meter scale.

For the next stage a small dish or glass of freezing mixture is needed. This should ideally consist of ice and water at zero degrees Celsius and the easiest way to obtain this is to put

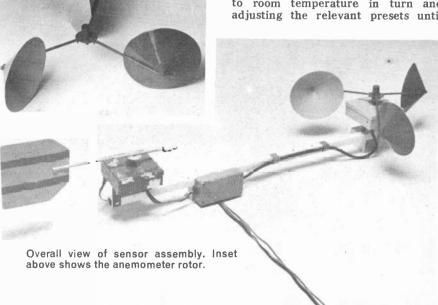


View of the reed switch assembly showing the upper circuit board and individual switch connections leading to the ribbon

the water into the dish or glass and place it in a freezer until ice is just beginning to form. Set the temperature select switch S1 to "outside temperature" and the wind speed select switch S3 to "temperature" and place the diode in contact with the mixture. Set VR5 about half way and adjust VR4 until the meter reads approximately 0 degrees.

Remove the diode from the ice/ water mixture and wait for a few minutes for the meter to increase its reading and then remain stationary. This will be at room temperature. Next adjust VR5 until the meter is reading the correct temperature. This can be verified with a normal mercury in glass thermometer.

Now return the diode to the ice/ water mixture and readjust VR4 so that the meter reads 0 degrees and keep on moving the diode from ice to room temperature in turn and adjusting the relevant presets until



impossible to place the rotor disc with the magnet in position.

The unit is then finished off according to the illustrations and photographs.

MAIN CABLE

The main cable from the direction indicator is a 10-way flat ribbon type available in 10 or 25 metre lengths. Connections to the wind speed unit are made via a single screened cable plus one of the wires of the 10-way cable. The nine other colour coded wires to the direction indicator unit are connected as in Fig. 16.

Connections of all cables from the wind speed and direction units are terminated at a 12-way terminal block housed in a small plastic box. This is mounted on the metal boom to which the wind speed and direction units are fixed (see Fig. 16). The boom itself can be fixed to a stub mast quite easily with a standard TV aerial claw clamp.

The whole assembly must, however, be mounted reasonably clear of the house roof top and any obstruction likely to impede the flow of air or cause fluctuation in wind direction, for example, a chimney stack in the path of the wind from any direction around the units.

HARDWARE

20 or 22s.w.g. aluminium sheet for wind cups; ‡ inch (6mm) aluminium rod or thick wall tube; ‡ inch square-section aluminium tube for boom; Perspex and brass for chopper and discs as per diagrams; $\frac{2}{8}$ inch ($\frac{1}{4}$ inch bore) brass bushes (4 off); standard $\frac{1}{4}$ inch bore brass spindle couplers for making collars (4 off); aluminium boxes $4\times4\times1\frac{1}{2}$ inch, Bi-Pak type BA2 or similar (2 off); mild steel or aluminium angle for unit supports as per diagrams; small circular or square plastic boxes for temperature sensors; zinc plated self tapping screws; TV aerial claw clamp for securing boom to mounting pole.

Connections down to the readout display are made via the junction box. and use the 10-way ribbon cable plus one run of single core screened cable.

PRELIMINARY CHECKS

When the wind speed and direction units are fully assembled on the boom the short cables from these to the junction box can be connected.

Take the whole assembly outside. preferably when there is a light wind blowing. When held horizontal at head height, the anemometer cups should rotate freely and the direction vane move to a position 180 degrees to the wind direction, that is the small arrow should point into the

Further notes on setting up will be given later, but a check could be made at this stage to confirm that all the reed relays are operating by connecting an ohm-meter between the common lead and each reed relay connection.

The meter should show continuity at each main compass point, with the

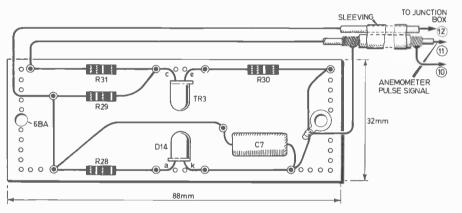
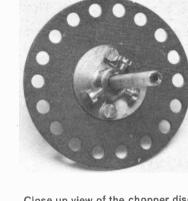
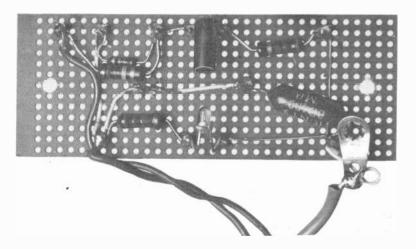
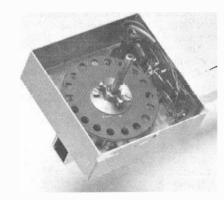


Fig. 11. Circuit board layout for the wind speed sensor unit. The photograph below shows the top view of the prototype board.

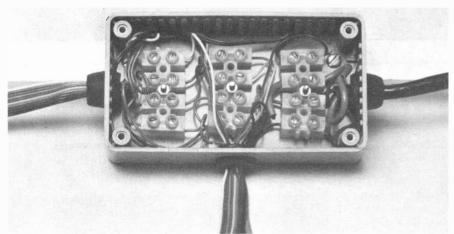


Close up view of the chopper disc.





Interior view of completed wind speed detector unit.



Interior view of the terminal block on the sensor assembly. This can be compared with Fig. 16.

correct reading appears every time.

The circuitry for the outside temperature of the unit is now calibrated for this particular diode. This diode must be kept only for outside temperature measurement.

INSIDE TEMPERATURE

The procedure for setting up the inside temperature circuit is exactly the same but using the diode sensor chosen for this connected up to the appropriate input terminals. In this case the presets VR1 (zero degrees) and VR2 (room temperature) are used. This diode must be kept only for inside temperature measurement.

DIODE MOUNTING

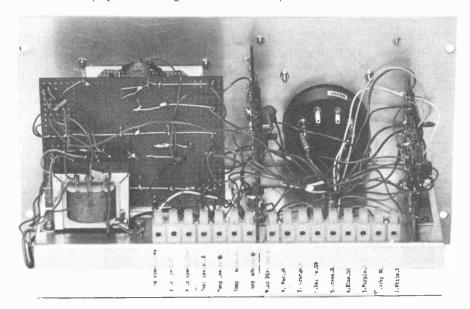
Each diode can now be mounted in a small plastic box and provided with a pair of connecting leads long enough to reach the final positions from the readout display unit.

Likewise, the wind speed and direction unit can now be permanently mounted in position, although it would be a good idea to connect it up to the display unit and quickly check the wind speed and direction functions before finally installing the wind speed/direction sensor unit in its permanent location.

WIND SPEED

Calibration is completed by setting up the display unit for correct wind speed. Set the wind speed select switch S3 to "wind speed cal". The l.e.d. D8 should be flashing slowly. Adjust VR6 until the meter reads 19, that is about half a division below 20. Calibration for wind speed is now complete for 0 to 100 m.p.h. but can always be checked again by repeating the above procedure.

Rear view of display unit showing sensor connection points and terminal blocks.



At this point the meter can be labelled. First, remove the meter cover and very carefully release the scale itself by undoing the securing screws. Then slide the scale outward underneath the pointer. Calibration figures for temperature and wind speed can be put on with Letraset or drawing ink as shown in the photographs. Equally carefully, replace the scale and meter cover.

The Weather Centre is now ready for use.

SENSOR LOCATION

The sensor for outside temperature should be mounted about 1.5m above ground on a North-facing wall or location shaded from direct sunlight. Make sure that water cannot enter the enclosure by sealing the lid all the way round with tape or epoxy resin. The sensor for inside temperature can of course be used anywhere in the house, the most likely place being the main living room. Alternatively, it can be used in a greenhouse.

The wind speed/direction sensors should be mounted well clear of any obstructions such as chimney stacks that might cause a disturbance in the air flow. The boom should also be lined up so that the reed relay S4 corresponding to the N l.e.d. D15 is in fact pointing North. Wind speed is measured in miles per hour or knots, either of which can be converted to the Beaufort scale. A printed scale is provided (see Fig. 10) for the constructor to fasten onto the front of the display unit for reference.

However, it must be remembered that even when the wind is blowing steadily, there are still fluctuations in wind speed known as gusts and lulls. For example, when the general wind speed is averaging 20 m.p.h. the speed over a period of a few minutes may fluctuate between 10 and 30 m.p.h.

Wind direction never remains absolutely steady either and even with normal wind the vane may move rapidly between two or three main compass points. For example, with a generally West wind the l.e.d. indicators may show SW and NW frequently together with W. If the dominant indication is West, then this will be the main direction.

FURTHER INFORMATION

Bona fide applicants, such as school teachers, students engaged in weather studies, colleges, etc can usually obtain all kinds of information on weather and weather forecasting, quite free from the Independent TV companies' weather departments and you might also like to try your local Meteorological Office weather station, whose address is usually in the telephone directory.

Everyday News

CHALLENGE OF THE CHIP

The chips are down at the Science Museum and they're there for all to see! Over 200 microprocessors are on show, some working, in an exhibition on the first floor of the Science Museum, London

Aimed at showing the present and future possibilities of the chip in everyday life, this is an exhibition that tells the story from the beginning through to displays of applications of the very near future. It deals with the invention, development, and applications of the transistor, integrated circuit and the methods by which they are made on a minute scale.

Electronic games and toys take up a large section of the exhibition. This is because most people come into contact with microchip technology through these and therefore they come to terms with them more easily than just looking at a piece of technical equipment.

A large number of manufacturers and suppliers have contributed objects and equipment for display. The aim is to attract as many people as possible to this free exhibition. To this end special evening openings are being held to enable staff of industrial and commercial organisations to attend at their leisure.

Super Market

One exhibit, that of a supermarket checkout point, is manned and the continuous demonstration shows just one application of the chip together with laser technology.

Each item "purchased" is passed over a window instead of the assistant lifting the item up to read the price. A laser beam scans the window until it reads a barcode (thick and thin black lines printed onto the packing of the item purchased), the information is fed to a microcomputer in the cash register automatically.

The printed bill gives details of the item: the price, an abbreviated "title" for each purchase i.e. B.FAST CEREA for Corn Flakes (a breakfast cereal). The bill is totalled after the assistant touches the total button or touchplate. They then enter the amount of money tendered, the printout gives the amount of change due, the till drawer opens, when it closes the date and time of purchase prints out and a receipt number and message appear "THANK YOU, CALL AGAIN".



Another very interesting exhibit, contributed by Marconi Avionics, is a large model of an advanced fighter plane of the future, demonstrating the role of the microprocessor in "tomorrow's" military and civilian aircraft.

whole family will find something of interest and fun in its presentation. Due to run until "at least the end of the year" it will be interesting to see how many items stand the pace of continuous use.

This is an exhibition that

is a must for everyone. The

TX9 Exported

The new and highly successful Thorn TX9 TV chassis has attracted world-wide attention. An agreement recently signed allows the TX9 design to be assembled from kits of parts in Hong Kong and China. Similar agreements have also been made with electronics companies in Italy and Scandinavia.



Anxiety about health hazards from visual display units has been largely dispelled in a report from the VDU Eye Test Advisory Group.

The report claims that there is no significant radiation hazard and that complaints of strain arise from method of use of the equipment and not the equipment itself. The report, however, urges the need for regular checks of the eyesight of continuous users.

Audio Agreement

A step forward to industry standardisation in digital audio discs has been made by a new agreement between Sony and Philips who are already in agreement on compatible video discs.

The audio discs will use 16-bit encoding on a 12cm disc and will be single-sided with a playing time of one hour. The discs play through an optical laser system with no wear on the disc.

Computer manufacturer LogAbax has estimated that computers are being installed in the UK at a rate of 400 a week, mostly to small or medium business users.

NEWSPAPER by Satellite _

The New York Times is sending facsimile pages by high speed satellite data link to Chicago for local printing. Two pages are transmitted every 212 minutes through unattended earth terminals at each end using 10 metre diameter dishes.

... from the World of Electronics



-ANALYSIS-

TWO WORLDS

The electronic hobbyist soon acquires a good knowledge of what's happening and what's new in consumer electronics. He or she gets full exposure to component and kit availability through electronics constructor magazines such as EVERYDAY ELECTRONICS. The lastest in ready-mades can be seen in every shopping centre. Whether we buy or build our equipment it ends up in our homes and, in the jargon of the economjst, we are all members of the consumer electronics market.

Less well known to the hobbyist is the other world, that of electronic capital equipment also sometimes called "professional" electronics. This world is largely hidden from the

public although we benefit daily from it.

The world of electronic capital equipment embraces the radio and TV transmitters and studio equipment, the radars and other navigational equipment that speed us on our holiday flights, the computers that remind us of our bank overdraft, the police radio network which helps preserve law and order, the industrial automation keeping industry going, and defence electronics which helps maintain peace.

Electronic capital equipment design and manufacture is a success story that is overlooked by the media who much prefer to report the failures of steel or shipbuilding, or industrial unrest. This industry is producing £1,500 million worth of equipment and systems a year and selling it profitably. About one third of the total is exported and after deducting imports in the same categories there is a surplus of £140 million in overseas trade balance.

The workforce of some 100,000 people is increasing yearly despite the fact that i.c.s have reduced labour content in the finished product. Another big plus factor is the level of enthusiasm in the industry and consequent lack of disputes. After all, everybody knows they are backing a winner and don't want to see it nobbled when order books are at their

best ever levels.

There is only one snag. The sky would be the limit but for the fact of a chronic shortage of engineers and technicians. This is where the hobbyist can help while, at the same time, promoting his or her own interests. Anyone who understands the fundamentals of electronics can carve a career in an industry in which there is virtually no limit to growth. The jobs are there waiting to be filled and providing you are keen (which most hobbyists are) and know your basics the firm will help train you.

It's worth thinking about.

Brian G. Peck

USA Buys British

Multi-million pound orders have been received by Redifon Simulator Ltd for flight simulators for the new generation Boeing 757 and 767 jet aircraft for the United States.

Britain's aerospace industry, which has a large electronics content, is having a record year with exports targeted at £1,500 million. Over 50,000 trade visitors from 100 countries will attend the Farnborough Air Show in September.

Teletext in Print

The Department of Industry has just published a leaflet on "Teletext" as part of a campaign to make the public more aware of the TV information service in which the UK leads the world—who said the printed word was on the way out?

Copies of the Teletext leaflet are available free from MAP Information Centre, Freepost, Dept of Industry, Room 114, Dean Bradley House, 52 Horseferry Road, London SW1 2BR.

WORRIED UNION

The Post Office Engineering Union is reported as "being worried" over the implementation by the BPO of the new System X digital telephone network, the first exchanges of which will enter service this year. Reason for Union concern is System X reliability of a measured call failure rate of one in 10,000, needing a staffing of only one technician per 10,000 lines, far fewer than at present.

In Union eyes System X is far too good. Subscribers, however, will welcome the improved reliability.

SOLAR TELEPHONES

British company Lucas Energy Systems has won a £1·2 million contract for solar panels to power a rural telecommunications network in Colombia. Sun power will be converted to 100kW of electrical energy through

Japan's JVO and Britain's Thorn EMI are joining forces in the video disc business. The new tie-up will challenge RCA and Philips for dominance in the market place.

All three manufacturers have different proposed systems with none so far recognised as an industry standard.

Electronic Translation

The EEC Commission is reported to be investigating schemes for electronic translation between the six official languages used daily by the 7,000 civil servants in Brussels.

Automatic translation from one language to another would ease the task of, if not dispense with, the present force of highly paid translators. 2,550 solar panels distributed throughout the network.

This is believed to be the largest single order ever taken in this area of solar panels and was won against fierce competition from the USA, Japan and France,

GOLD STANDARD

One of the measures of health in the electronics industry is gold consumption, used in high quality components and assemblies. The UK industry doubled its gold intake during the past year to a value of £60 million, fourth highest of the electronics producing nations with only the USA, Japan, and Germany ahead in the gold usage league table.

The prospect of a flat "hang-on-the-wall" TV receiver is still a dream of the future according to speakers at a recent IEE colloquium on the topic. Except, that is, for tiny screens. For the foreseeable future the conventional c.r.t. will remain on top.

Underwater Colour

An underwater colour TV camera for deep sea (up to 2,000ft) inspection of structures has been developed by Marconi Avionics. Special signal processing brings out colours which otherwise are obscured by sea water and can reveal information vital to safe maintenance.

The camera is housed in an anodised aluminium housing similar in specification to that used on naval torpedoes. It can be hand-held by a diver or operated by remote control.

RADIO WORLD

By Pat Hawker, G3VA

Electronics and reliability

Over many years, industry has been striving to overcome the feeling of many of the public that complex electronics equipment, although capable of doing many wonderful things, can still prove to be rather unreliable, particularly when it is used in hostile environments.

Semiconductors rather than glass valves have done much to improve matters, although, it could be argued, better packaging and materials research have done even more. It was said, for example, that over 90 per cent of the early radar cathode-ray tubes arrived overseas during wartime in a damaged or broken condition due to bad packaging.

The need to put equipment into packages capable of being launched into space and working unattended for from five to seven years has led to intensive work on discovering and overcoming failure mechanisms, and this has had a valuable spinoff throughout the industry. In the past decade, the number of service calls to the domestic colour TV set has dropped, on average, from over four per year to less than one.

But the 1980 Observer single-handed Atlantic yacht race cannot have done this image any good. Much was expected of the French Argos automatic position-reporting-via-satellite equipment that had performed well during some earlier events. But this time, using new deck-mounted equipment, more than 30 of the units failed within a matter of days.

According to preliminary reports this seems to have been due more to the redesigned plastics casing than due to the electronics. Instead of flexing, the plastics apparently stiffened and cracked in the presence of salt water, letting the highly conductive sea water reach batteries and electronic circuitry; so it now seems a case of "back to the drawing board".

This again emphasises a very old rule: mechanical engineering remains a vital part of good electronic engineering.

The UK domestic environment is much kinder to electronic equipment than is the case in many parts of the world—and very much kinder than any form of mobile service. One still hears complaints that "tropicalisation" is less effective than it might be when up against the combined onslaught of heat, humidity, dust and insects; semiconductors, on the other hand, have a particular dislike for low temperatures.

Printed circuit boards still give trouble, including those elusive hairline cracks and the peeling off of the copper; carbon 'pots' dislike moisture; rubber, springs, push-button switches etc can deteriorate rapidly in the tropics. The thin wires found in many receivers are vulnerable to hard use, while connectors, plugs and sockets and the like are all too easily damaged when used under field conditions.

Another problem is that while, for example, modern large-scale integrated circuits can form effective multi-channel synthesisers for hand-held equipment, the power they consume is considerable, particularly where dry batteries are stored at unsuitable temperatures.

CB at the crossroads

As someone entirely sympathetic towards the concept of an "Open Channel", it is possible to understand why the frustrated CBers feel that only by keeping up constant pressure on Parliament, the Home Office and the media are they likely to live long enough to receive more than promises. But it has to be said that much of their "propaganda" is undoubtedly over-pitched and by no means easy to justify.

This could rebound on the movement in future as a similar (successful) campaign did in Australia a few years ago. Neville Williams, editor of *Electronics Australia* makes this clear in a trenchant editorial "CB radio is at the crossroads" in a recent issue of that magazine. It seems well worth quoting, if only as a warning:

"In 1977, with much fuss and fanfare, citizens band radio in Australia was legalised. On the one hand, the move was seen as a victory for human rights and free speech; on the other an opportunity for numerous companies to make a fast buck. For a while, CB was very much the "in" thing.

"But within 12 months, the scene had changed. For many, the fast buck dream had turned into a nightmare. And the platitudes about human rights and free speech had been buried under an avalanche of everything from jargon to obscenity. From being a "cause", CB became the target for widespread ridicule.

"Massive desertions from the ranks of licensed CBers followed, including at least two groups which the CB movement could ill afford to lose. One such involved many of the original human rights, free speech campaigners who had seen in CB a potential means of exchanging informed opinion on many subjects; they hadn't counted on the high level of adolescent ambient!

"The other group included people with an evolving interest in the technology of communication. Many such have moved into the ranks of amateur radio and have adopted the accepted manner and mores of the amateur fraternity.

"A large proportion of those who remain are not really CBers at all; they have no licence, no inhibitions about equipment, power, channels, or the way they use those channels. Ultimately, the Government will have to crack down on them and a recent prosecution in Sydney may provide an advance sample: a \$A1,000 fine, plus costs, plus confiscation of all equipment."

Letters of Authority

So while the long-drawn-out controversy over CB rumbles on, with ever wilder estimates of the number of "illegals" or pirates using 27MHz CB equipment in the UK (between 150,000 and 200,000 according to some sources though about 15,000 to 25,000 seems a much more likely figure for regular users), less is heard about the "legal" use of 27MHz in the UK for radiopaging and model control.

I gather there are some 5,000 licences or "Letters of Authority" for radio-paging systems, plus as many again for inductive-loop systems. Since each system represents an average of about 20 pocket receivers or "bleepers", total users of both types of system must now amount to over 200,000. There are some 23,000 subscribers to the Post Office radio paging systems which opened in 1973 in the Thames Valley area and in 1976 in the London area, with plans to extend this nationwide.

Many of these systems operate on v.h.f. or u.h.f. and on 27MHz the systems are for "bleeping" only, on other bands systems may include talkback, "talk through" (ability to speak to another pocket set user via the control unit) etc, although the regulations are currently being changed so that systems providing speech facilities will be known in future as "local communications networks" as an intermediary category between "paging" and "private mobile radio".

Government-funded organisations are not ''licensed'' but operate under a ''Letter of Authority'' issued by the Home Office.

Licences for 27MHz radio control of models have long been available in the UK although for some reason or other the authorities have not been prepared to issue licences covering the garage-door opening systems long popular in the United States.

Radio Control

A consumer boom in radio control of models is expected in the United States following the introduction of new special-purpose integrated-circuit devices by National Semiconductor Corporation. These, it is claimed, will make it possible to build complete, multi-channel, proportional-control systems with an operating range of about 100 metres for a small fraction of the cost of current designs.

Tail-pieces

An American study suggests that watching television now occupies more waking hours than any other activity except work (43 hours per week for the typical household) based on a survey of 309 urban and suburban homes.

The recent revival by a Russian newspaper of the charge that the BBC external services are used to broadcast messages to secret agents makes one hope that, if this is so, which seems extremely doubtful, then it is conducted more effectively than the famous "personal messages" to the wartime French Resistance, when the vital "D-Day is coming" messages were known in advance to the Germans and could have led to a disaster had not the Germans mishandled the information they obtained from the messages!

Complete Audio/Tuner Kits



Mk III FM Tuner series

The Mark III series FM tuner has been updated, and now includes a centre zero tuning meter as standard. The instruction manual has been meticulously revised, enabling easy assembly by constructors of various levels of experience - a preview copy may be purchased for £1.00.

Mark III A series 'Reference series' tuner modules£171.35 £171.35 inc.

'Hyperfi' modules, with switched Mark III B series IF BW, pilot cancel decoder

£198 95 inc

A matching synthesiser unit will be made available later this year, and can be retrofitted to either version. All versions include digital frequency readout/clock, VU deviation meters, 6 preset stations, 10 turn pot manual tuning, toroidal PSU, output level adjustment, 110/240v AC input. Full alignment service available.

Power Amplifier Style and performance - with a real 'belt and braces' PSU design.

After a couple of preview comments, it seems that many of you are waiting to hear about the matching HMOSFET power amplifier for the Mk III tuner. Well, it's out at last - complete with twin toroidal PSUs for comfortable 80W RMS per channel, over 100W peak, but limited by thermal shutdown of the HMOS, 10W-100W log LED output peak indicator, DC offset protection and switch-on pause relay. AC or DC input coupling, direct or relay protected output terminals. The works. Only one version of this item: Complete kit£178.25 inc. Carr. £5

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More features and facilities, thanks to DC switching and control design two tape in/outs. 2 low pass, 2 high pass active filters, genuine volume related loudness, 1dB channel matching, with DC volume, balance, bass and treble controls. Suitable for bus/remote control, tape dubbing, switched monitor etc. 80d8 S/N+, THD -75dB or better, Pluggable PU equalization boards, tone control override. Price for complete unit about £149 ex VAT.

Semiconductors

Radio/Communications ICs

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3

POWER MOSFETS 100W PA's made simple

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Things like ICM7216B, ICL8038, 8080A, 6800P, 2708, NE555, NE556, etc Contain yourselves, RF fans I Not yet ready for

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NE of the more insidious equipment breakdowns that plague the motorist is that of bulb failure. Often he will not notice until he either makes a special check (which should after all be carried out weekly) or he is stopped by the police, and we need hardly quote the old adage that ignorance of the law is no defence.

The device described here gives continuous monitoring of all external lighting equipment apart from the direction indicators and will give an instant warning should one of the bulbs go open circuit in use.

When failure of a monitored light bulb occurs, a corresponding l.e.d. illuminates at the same instant on a display unit installed inside the car.

CIRCUIT

Although the circuit may look a little daunting at first, closer inspection reveals that it consists of ten individual identical sections plus a test facility.

Fig. 2 shows the complete circuit and it should be noted that each of the boxes A to J contain the same circuit network which is shown in Fig. 1.

At this point we should point out that the components are numbered in a slightly novel way in that all components associated with each box have the letter of that box after their reference number.

For example the transistor in box C is referred to as TR1C or the l.e.d. in box H is referred to as D2H, and so on.

Let us take circuit A for the moment. This is monitoring the offside front side-light. The monitoring circuit is so arranged that there is a diode D5A in circuit between the bulb and its switch.

Consider Fig. 1. Suppose the light bulb is operational. When the switch is closed, a current will flow through the silicon diode D5A and the light bulb.

A voltage of 0.7 volts is dropped across the diode. This voltage is large enough to provide the germanium transistor TR1 with sufficient base bias to switch it on.

In this mode TR1 acts as a short circuit across the l.e.d. D2 thus preventing it from lighting up.

OPEN CIRCUIT

Let us take another case, this time with the bulb open circuit. When the switch is closed, current will not be able to flow through the diode. Hence the voltage across the diode will fall

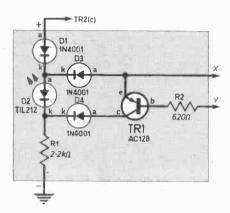


Fig. 1. Circuit dagram of one of the sensor modules of the Lights Failure Monitor.

£9·00

to zero and the transistor will switch off.

Of course there will no longer be a short circuit across the l.e.d. so it will light up indicating that the bulb has failed.

A further point should be made that when the light switches are off, then no current will flow into the sensing network at all so the unit is in effect switched off.

TEST FACILITY

No monitoring unit is completely free from failure in itself so a test facility is provided to make sure that all the l.e.d.s are functional.

Essentially we have a line that feeds every l.e.d. via diode D1. When we wish to test the system, the base of TR2 is grounded via R3. This switches on TR2 which allows current to flow through every l.e.d. in the system and light them all up.

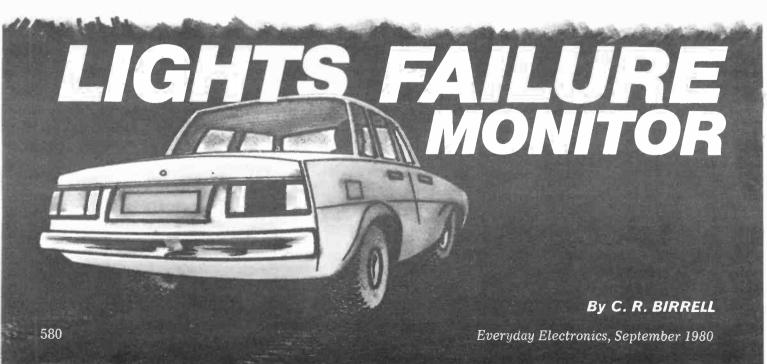
It is then very easy to spot a faulty indicator. Diodes D1 are necessary to prevent current flowing back down the test line when it is not being used.

NEGATIVE EARTH

As can be seen from the circuit diagrams in Fig. 1 and Fig. 2, this unit has been designed for a negative earth system.

Fortunately nearly all new cars are built this way. However modifying this circuit for the older positive earth system poses several problems mainly because of the fact that the current flowing through the bulbs is going in the opposite direction.

In fact modification would involve changing the design of each boxed module, not to mention redesigning Fig. 2 so the author has decided to restrict himself to a negative only version.



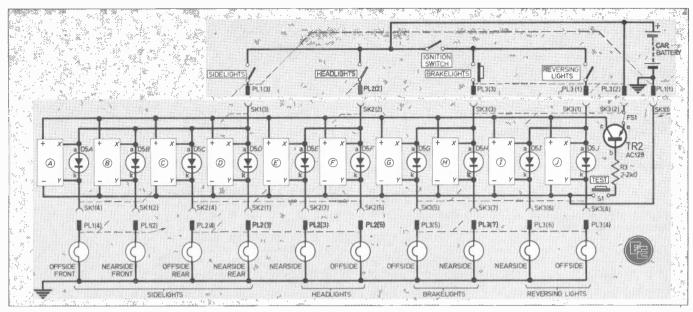


Fig. 2. Complete circuit diagram of the Lights Failure Monitor. Note that each lettered box contains the circuit elements from Fig. 1.



CIRCUIT BOARD

The main part of the Monitor is built on a piece of $0\cdot 1$ inch stripboard, 37 strips by 14 holes and the component layout is shown in Fig. 3.

Straight away it can be seen that the spacing between components is very close so some care will be needed in construction.

The board should first be prepared by making all the breaks in the copper strips. This can be done using a spot face cutter or small twist drill.

When this is completed solder the resistors and diodes in place. It is necessary to do this first because the wire links must fit around these components and in fact these can be put in next.

FINISHING OFF

The board is finished off by soldering in the transistors, fuse clips and lead-off wires.

Readers will notice that the l.e.d.s are wired straight onto the board. Make sure that you leave long enough leads so that they will fit into their holders in the case.

In the prototype this meant bending the leads through ninety degrees so that they would slot into their holders in the side of the case.

CASE

The circuit board is mounted in a plastics box 112 x 62 x 30mm. This should first be drilled and cut to accept the three sockets, test switch and the ten l.e.d.s.

This involves marking up the side of the box with the correct drilling dimensions and making the holes, preferably with a hand drill. Larger holes can be made by making a small hole and opening it out with a file.

The sockets and switch are then fastened in position and the clips for the l.e.d.s pushed through their respective holes.

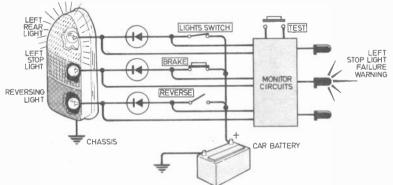
INSTALLATION

Before attempting to install the Monitor, study the diagram in Fig. 4 very carefully.

The main task is to insert the diodes D5A to D5J in series with the power cables from the light switch to the bulbs. This involves finding the correct wire that feeds each bulb to be monitored and reference to your car manual may be necessary in order to work out the colour code of the individual wires within the vehicle's wiring harness.

The most convenient way to install the diodes is to insert them between

HOW IT WORKS



A diode is connected in series with each light bulb to be monitored and the voltage drop across each diode is also monitored.

If the light bulb is working, a current will flow through the diode which will keep the l.e.d. in the display unit turned off.

If the light bulb is open circuit then no current will flow and the l.e.d. will turn on indicating where the fault lies.

LIGHTS FAILURE MONITOR

Fig. 3. Circuit board layout for the display unit. The cathodes on the l.e.d.s may be identified by a flat on the casing next to the cathode lead.

It can also be seen that only one channel has been fully labelled. Each channel is identical and their layouts are exactly the same.

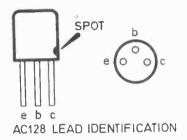
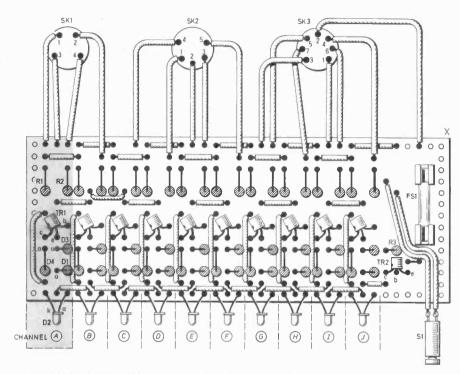
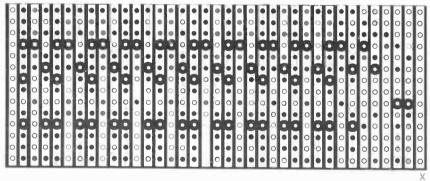
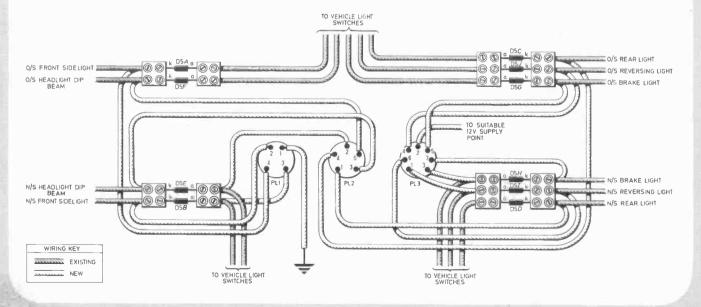


Fig. 4. Wiring diagram for installing the unit in the vehicle. The new and existing wiring can be seen clearly. Note that the contact numbering on the three plugs corresponds with the pin numbering on the sockets in Fig. 3. Care must also be taken to ensure that the correct diodes are used for D5E and D5F.







COMPONENTS TO THE

Resistors

R1A-J $2 \cdot 2k\Omega$ (10 off) R2A-J 620 Ω (10 off) 2·2kΩ R3 All ‡W carbon ± 5%

Semiconductors

AC128 pnp germanium (10 off) TR1A-J

TR2 AC128 pnp germanium

D1A-J 1N4001 small signal silicon diode (10 off) TIL212 yellow I.e.d. including clips (10 off) D2A-J D3A-J 1N4001 small signal silicon diode (10 off)

1N4001 small signal silicon diode (10 off) D4A-J 1N5400 3A silicon diode (4 off) BYZ13 6A silicon diode (2 off) D54-D

D5E-F 1N5400 3A silicon diode (4 off) D5G-J

push-to-make momentary action switch

PL₁ 4-pin DIN plug

PL2 5-pin 240 degree DIN plug

7-pin DIN plug 4-way DIN socket PL3

SK1

5-way 240 degree DIN socket SK2

SK3 7-way DIN socket

500m A 20mm cartridge fuse FS₁

Plastics case, 112 × 62 × 30mm; 0·1 inch stripboard 37 strips × 14 holes; twoway screw terminal block (2 off); three-way screw terminal block (2 off); connecting wire.

two terminal blocks and use the terminals at the opposite end of the blocks to connect up the severed ends of the wire. Fig. 4 will make this clear.

As each different vehicle has a different wiring harness, it is impossible to give precise details as to



page 553

where you should cut the lighting cables and insert the diodes. However you should try to do this as close to the proposed site of the display unit as possible, and far away from any possible sources of damp.

resistors with 10 per cent tolerance-they are allowed to be up to 10 per cent higher or lower than their nominal value. These are cheap components and good enough for most purposes. A 100 ohm re-* sistor could, for example, have an actual value of anything between 90 and 110 ohms.

I showed, with the aid of a diagram, that when the tolerance is taken into account, the preferred values just about cover all values. Naturally, the family of 5 per cent resistors will have its own set of preferred values.

There would be little point, I told them, in making a 200 ohm resistor if this value was covered (just about) by the upper limit of a 180 ohm (198 ohm) or the lower limit of a 220 ohm (198 ohm) resistor.

I went on to tell the class that when the actual value of a new carbon resistor is measured it is often surprisingly close to the nominal value-perhaps within 2 per cent-but it will not always stay that way. In service, its value "drifts" and if it is subject to mis-use it may easily go outside its 10 per cent limit. Hot running was one particular cause to be avoided.

Once all the diodes have been installed the wires that lead to the display unit can be attached as in Fig. 4. These should be terminated with the appropriate DIN plugs. An earth and positive supply should also installed

SYSTEM TESTING

At this stage the system can be tested. Plug the three DIN plugs into their appropriate sockets on the back of the display unit. When the test button is pressed all the l.e.d.s should light up.

Each individual circuit should be checked next. To do this, loosen or remove each monitored bulb in turn. When the relevant switch is activated in the car, the corresponding l.e.d. should light up indicating that the circuit is faulty (in fact we have simulated an open circuit bulb).

As soon as you are satisfied that everything is working properly, the terminal blocks should be insulated, for example by binding with p.v.c. tape, and then fixed securely in the

car.

The display unit can be finished off by labelling the indicator l.e.d.s using Letraset or other self adhesive transfers and then the display unit can be firmly attached to the dashboard or other suitable location inside the vehicle. H

R. de Vaux-Balbirnie

NDREW was gazing into the large compartmented drawers which we had adapted to carry our stock of resistors. The thing which struck him was the apparent 'silly values' to be found—390, 470, 560 ohms and so on. He asked why the values did not run—350, 400, 450, 500 and simplify the whole business. He argued that calculations would be much easier that way and I agreed.

I told him that these were called "preferred values" and that I would talk to the whole class about them.

I told them that we were talking about ordinary carbon

Carrent Commence

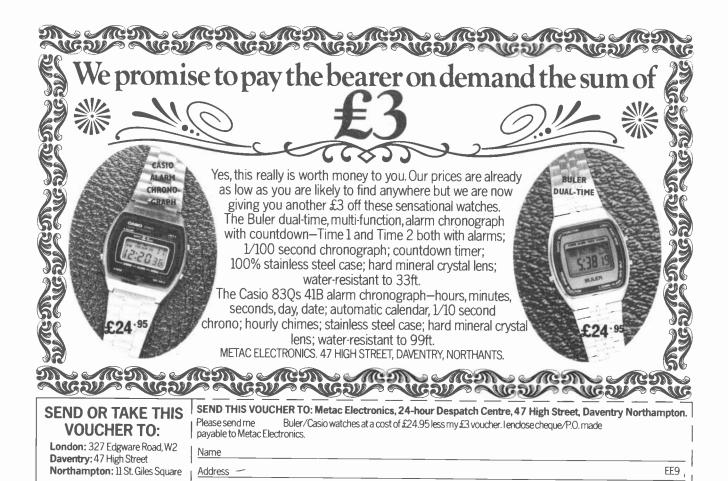
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WORKSHOP MATTERS

By Harry T. Kitchen

R.F. Sources

A few months ago (May) we looked at audio frequency signal sources, and this month I want to extend the frequency range to cover radio frequencies.

Such sources are invaluable whilst trouble-shooting or designing equipment, and again we have a very wide specification/price spectrum. The latter figure can range from a few tens of pounds for the very basic sorts of oscillator, to $\times \pm 100$ and even more for the precision signal generator. Your ambition must therefore be tempered by your pocket

Oscillators

The term "oscillator" is used to describe a signal source where neither frequency or output voltage is closely controlled, (though advertising literature would often have you think otherwise). Such instruments comprise, essentially, (in the older type) two-separate valve oscillators, one for the radio frequency, the other for an audio frequency with which the former is modulated.

In the modern version oscillator, we usually have two transistors which fulfill precisely the same functions.

Modulation, incidentally, is the process of causing the *amplitude* of the radio frequency to vary at the same frequency as the audio frequency. Demodulation, at the receiver, consists of removing the radio frequency, leaving us with the audio frequency.

The process of modulation in such a simple oscillator consists of varying the voltage supplied to the r.f. oscillator at the required a,f. frequency. Thus, when the voltage is at its maximum, the r.f. oscillator oscillates more vigorously then when the supply is at its lowest level.

when the supply is at its lowest level.

There is very little control over the "depth" of modulation, and the output voltage is extracted from the oscillator stage, possibly via a secondary winding on the oscillator coil.

The output control is a glorified volume control used for potting down the output voltage. As it is closely coupled to the oscillator varying loads will affect the frequency as well as the actual output voltage. Such an oscillator cannot be seriously considered for precision work, but within its limitations it is a useful tool.

Signal Generators

We come now to the precision brigade, instruments that are entitled to the description signal generators, and our pockets must not only be very deep but also very well filled.

Signal generators should be capable of providing an accurate and stable frequency; accurate and stable output voltage; a means of setting the output voltage to a pre-determined point on an output

meter so that the precise output voltage from the attenuators can be determined, should be capable of being set, and reset to any pre-determined frequency and voltage; should have variable modulation depth; zero leakage; zero f.m. on an a.m. signal. A formidable list, justifying the high cost. Let us look at some of these items in greater detail.

The stability of frequency and output voltage will be clear, as will the requirements of setting, and resetting, accuracy. What of variable modulation depth, zero leakage, and zero f.m. on a.m.?

Modulation Depth

Earlier we saw that the r.f. signal is modulated by the a.f. signal and thus varied in amplitude at the frequency of the a.f. signal. Theoretically it is possible to achieve 100 per cent. modulation where the r.f. signal varies from zero, when the a.f. signal is zero, to a maximum when the a.f. signal is at its peak.

In practice this is difficult to achieve since the modulating device, valve or transistor, cannot be completely saturated to achieve zero output, nor completely cut-off to achieve maximum output.

The normal, everyday, modulation depth is 30 per cent, and the modulating frequency is typically 400Hz or 1kHz, with provision for an external modulation frequency of variable depth. A variable modulation depth is essential for checking for detector distortion in receivers, and for this reason purity of the modulation signal is important.

Zero Leakage

Zero leakage is impossible to achieve, but certainly the leakage of the oscillator frequency should be extremely low. If we are, as is sometimes necessary, measuring receiver sensitivity at the microvolt level, then even a very low leakage via the mains lead, which after all can act as a transmitting aerial, can invalidate our measurements.

The signal generator must be a box within a box; the oscillator contained in a leak-proof box, within the main cabinet. Mains input must be meticulously filtered to prevent the egress of the oscillator frequency.

For precise attenuation the various stages must be isolated from one another so that there is no possibility of the oscillator frequency getting out other than by the designed method.

Zero F.M. on A.M.

So far it has been accepted, albeit tacitly, that we are discussing a.m. oscillators and generators only. The presence of an f.m. signal on what should be a purely a.m. signal can be embarassing when measuring receiver selectivity.

Let us suppose that we are working at 1MHz, and that the generator has a (unwanted) deviation of 25kHz, so that our nominal 1MHz signal is actually sweeping from 975kHz to 1·025MHz. This means that our receiver can be up to 5 per cent inaccurate without us knowing about it, possibly an error of some magnitude, equally possible an error of considerable magnitude.

Fundamental Tuning

Some of the cheaper sorts of oscillator are equipped with an additional scale enabling tuning to be effected on harmonics, whereas proper tuning is effected on fundamental frequencies only.

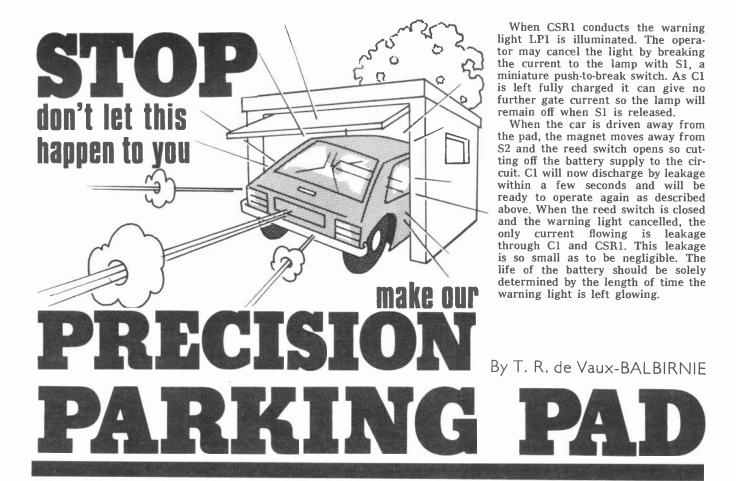
Fundamental tuning, if used as intended, restricts the user to the highest frequency provided. That means if the maximum frequency is 100MHz, then that is as high as you can go—officially. Unofficially you can go higher; using the second harmonic you can go up to 200MHz, the third harmonic enables you to go up to 300MHz, and so on.

This, in my opinion, is an undesirable practice, as it is all too easy to pick up the wrong harmonic, particularly if the frequency calibration is at all inaccurate. The only safe and accurate way is to use a fundamental frequency, though in an emergency it is possible to use the second harmonic and tune to twice the required frequency, that is 88MHz if 176MHz is required.

On harmonics the output signal is reduced, and this can also affect accuracy particularly if an insensitive receiver is involved.

Contributory factors to accurate measurement are the use of cables of the correct impedance to terminate the output from sig-gen's (as signal generators are invariably termed by those "who know") and the use of a dummy aerial. The reasons involve e.m.f. and p.d., and we will look at these in some detail in the next article.





THE PAP referred to in the title is a block of plastic foam which activates a warning light when compressed by pressure from a car bumper. With this pad suitably placed on the garage end wall and a separate unit housing the warning light, the device will ensure that the car will be parked close to the end wall without the possibility of damage and without assistance. Parking like this is sometimes necessary when the garage is only just big enough for the car or when two vehicles have to be squeezed in.

One feature of the circuit is that it requires no setting for day-to-day use. Nothing need be remembered on approaching the pad—the lamp will always be ready to signal attention. When the time for battery replacement approaches it will be seen that the warning light becomes dim long before the circuit fails to operate altogether.

The most difficult part of the project is not the electronics, which are very simple, but the construction of the pad unit itself. Experimental pads which reduced their electrical resistance when they were squashed were tried but they proved unreliable. A far better solution was found using a reed switch operated by a magnet. As the foam is compressed the magnet approaches the reed switch to the point where it switches on.

CIRCUIT DESCRIPTION

The circuit diagram of the Precision Parking Pad is shown in Fig. 1. When the magnet approaches the reed switch, S2 closes (switches on) and connects the battery to C1. This voltage step is transmitted to the gate of CSR1 triggering it into conduction and C1 continues to charge up through the gate circuit. Once the thyristor has been fired in this way it will continue to conduct even when C1 is fully charged and the gate voltage and current drops to zero.

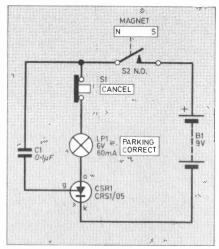


Fig. 1. The complete circuit diagram for the Precision Parking Pad.

Starts here

PAD AND SWITCH

The foam pad itself was a 100mm cube offcut. Perhaps an old cushion could provide a suitable piece of foam or even a cheap car sponge. The magnet was bought from a local hardware shop. Although several types were offered, the kind shown in the illustration proved most effective. Good results will only be obtained with a powerful magnet made from modern materials.

The reed switch is of the normal cpen type—i.e. it switches on when the magnet is moved near. Two types of reed switch were tried.

The first was about 25mm long and the other about 38mm. Both worked very well but the longer switch proved slightly more sensitive and was finally chosen for the prototype. For testing purposes, a simple battery and bulb test-circuit should be made up with the reed switch placed in

PRECISION PARKING PAD



The completed prototype warning light unit fitted to the garage wall. For convenience, a position close to the drivers side window is suggested. The battery is to be situated between this unit and the pad for easy replacement.

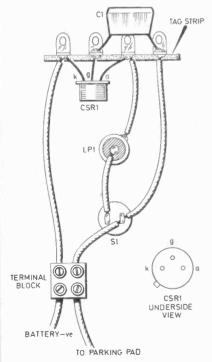


Fig. 4. Circuit construction details. The tag-strip, LP1 and S1 are mounted on the rear face of the blank socket box cover. Care should be exercised when drilling this cover as it is very brittle and likely to chip and crack.

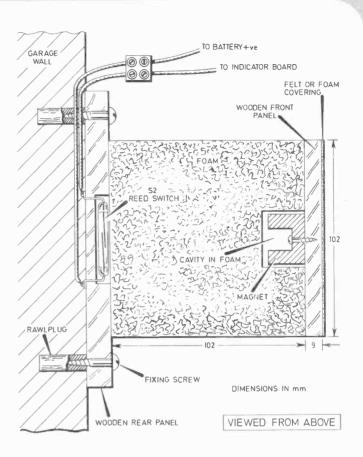
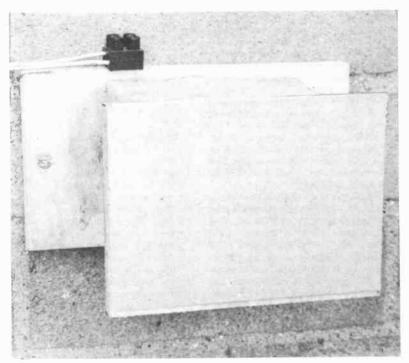


Fig. 3. Cut-away view of the pad assembly showing magnet and reed switch fixing. Note that the horizontal dimension of the foam cube will vary according to the magnet and reed switch used, and will depend on the findings with the test circuit (Fig. 2.).



The completed pad assembly securely screwed to the garage end wall at bumper height.

series as shown in Fig. 2. The bulb should light when the magnet is moved to within about 70mm from the reed switch. Careful note of the best relative positions for these two components should be made so that they may be adhered to in the final construction.

The rear panel of the pad assembly was made from 12mm-thick plywood and has a cavity chiselled into it to accommodate the reed switch, see Fig. 3. This protection is necessary as reed switches are very fragile components and could easily be damaged if the pad was carelessly used.

Checks should be made to ensure that even with the foam fully compressed, the magnet cannot touch the reed switch.

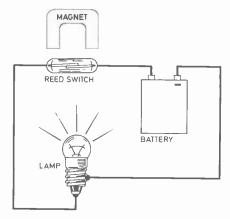


Fig. 2. A test circuit for determining the operating distance of the magnet from the reed switch.

In the prototype, the reed switch was secured by gently bending the end connectors at right angles and passing them through two holes drilled for the purpose. They protruded a short distance through the panel and were then bent over. Soldered connections were then made to them.

The wires leading from the reed switch must be run in grooves cut into the rear of the panel so that they will be protected from abrasion when the unit is finally attached to the wall. The wires lead to a piece of miniature terminal block mounted in a convenient position.

The front panel of the pad assembly was made of 10mm-thick plywood and has the magnet attached to it. The magnet chosen had a handy hole drilled in it so a wood screw was used to attach it. A cavity must be cut in the foam to accommodate the magnet. In the prototype, this was cut using a razor blade. It does not need to be particularly neat as it will be covered up.

The foam is sandwiched between the top and bottom panels using a suitable adhesive. This adhesive must be chosen with care as some have a devastating effect on foam. It is essential to try it out on a scrap piece first.

COMPONENTS

C1 0·1μF plastic or ceramic CSR1 CRS1/05 or similar 1 A 50 V thyristor

S1 miniature push-to-break, release-to-make button switch

S2 reed switch with normally open contact

LP1 6V 60m A m.e.s. bulb 9V type PP9 or other, see text

Tagstrip, 4-way; magnet (811); 13A plastic surface mounting mains socket box with plain plastic cover; battery clips to suit; materials for pad assembly; bellwire; 2-way terminal block (2 off).

Approx. cost Guidance only (see page 553) £2.50 excluding battery

When the pad assembly is complete it may be checked by squashing the foam by hand and listening carefully. It is likely that a click will be heard somewhere along the travel as the reed switch operates. When relaxed it should click open again. If the clicks cannot be heard then an electrical test should be made using the battery and bulb test-circuit again (Fig. 2).

COMPONENT ASSEMBLY

When the pad assembly has been checked, the circuit proper may be built. This was constructed on a piece of 4-way tag strip as shown in Fig. 4.

To house the prototype warning light assembly, a standard 13 amp surface mounting plastic box was obtained of the type used for mains sockets. At the same time a plain plastic cover was bought. These items are readily available from electrical

dealers. The circuit was mounted on the cover using two small nuts and bolts to hold the tagstrip in place. Holes were drilled for the indicator light and the push-to-break switch. Great care must be taken.

For the indicator light, the prototype used a 6 volt bulb with the connections soldered direct to it. This is the cheapest way and gives maximum brightness. If a neater appearance is required then a proper panel indicator light may be used. Fix the panel-mounted components in place and wire up as shown in Fig. 4.

BATTERY AND SETTING UP

In the prototype, a PP3 battery was mounted inside the box. These little batteries, however, tend to have a rather short life so it is advised that a larger battery be placed outside the case. It should be noted that it is quite in order to use a 9 volt battery to operate a 6 volt bulb in circuits such as this. There is a voltage drop of about 1 volt across the thyristor and there is an additional voltage drop across the internal resistance of the battery.

When the whole project has been constructed a suitable place for the pad assembly must be chosen. Tests should be made to find the best position so that the foam will be squeezed fairly and squarely by the car bumper. When the best position has been found, the unit should be mounted on the wall with two wood screws plugged in the usual way.

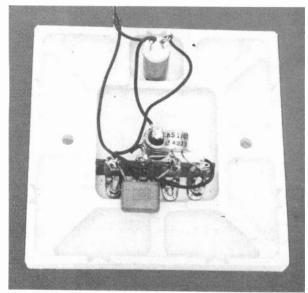
The indicator unit is wired to the pad assembly and battery by means of light-duty twin wire such as bell wire via the terminal blocks. It is best to mount this unit on the wall in such a way that the light can readily be seen from the driving position. If it is placed at window level then the unit may be cancelled before getting out of the car so conserving battery power.

When using the parking pad, the car is driven up very slowly to the pad and stopped as soon as the indicator lamp lights. The cancel button is then pressed.

One final refinement is a felt covering for the wooden front panel. This prevents any chance of scratching the bumper.

In terms of broken light clusters and bent bumpers, this unit should recover its cost in no time! $\mbox{\em \mu}$

Completed circuitry on the rear face of the socket cover.



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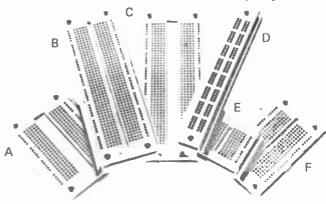
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STOCKING UP— SEMICONDUCTORS

Two previous articles have been devoted to resistors and capacitors. This month we discuss certain semiconductor devices that should be acquired by the beginner to start a stock of useful components.

DIODES

Diodes are one-way devices—they will pass current only if connected in circuit right way round, that means anode connected to the positive side of the circuit and cathode to the negative side.

Diodes are broadly divisible into four classes: (1) small-signal diodes, as used for detection in radio receivers, and also in logic circuits; (2) power diodes, used for rectifying alternating current; (3) Zener voltage reference diodes; (4) photodiodes and light-emitting diodes (l.e.d.s).

A small quantity of class (1) should be held in stock since they are frequently needed. They are small components and inexpensive. Suggested types and quantities to be held as stock are given in Tables 1—3.

The larger "power" type diodes (or rectifiers) are more expensive and in comparison bulky in size. They are available also as bridge rectifiers—four rectifiers integrated within a package. Power diodes are made in a variety of voltage and current ratings, and are best purchased as required, for some specific purpose.

If a diode is connected in reverse, that is anode to negative side of circuit, the diode will not conduct. Should, however, the applied voltage be sufficiently high, the diode will "breakdown" and conduct. If the voltage subsequently falls below the breakdown value, the device will become a barrier to current flow once again.

This property is exploited in devices known as Zener voltage reference diodes. These are used for maintaining the voltage level or to provide a reference voltage at some point in a circuit.

FOR BEGINNERS

Zener diodes are made with various "breakdown" voltages; from 2.7 volts upwards. A few Zeners should be held in stock. Those suggested in Table 4 should cover many normal needs.

Light emitting diodes are becoming increasingly commonplace, replacing filament lamps for signal and indicating purposes in many electronic projects, and it is worthwhile holding a small stock of selected types—see Table 5. The most practical colour is red, but these devices are available in green and yellow also.

Photodiodes are but rarely used and can be disregarded for the present.

TRANSISTORS

Despite the large number of different transistor types, the constructor can cover many of his needs from a very small selection of smallsignal, audio frequency transistors.

BC108 is an essential general purpose transistor for the constructor. Closely related types are the BC107 and the BC109, the latter being a lownoise version of the BC108. These three types are available in TO-18 cans.

Another popular general purpose transistor is the ZTX300. This is made in a plastic package, the leads being arranged in what is known as "E line" configuration.

These transistors and a few others are listed in Table 6, which includes in the final ("Qty") column recommended quantities that the new constructor should obtain and hold as initial working stock.

Other types of transistors, including special types such as field effect transistors (f.e.t.s) and unijunction

TABLE 1 GERMANIUM SIGNAL DIODES

Туре	Max p.i.v.	Current	Qty
O A91	100 V	20m A	4

TABLE 2 MINIATURE 1A PLASTIC ENCAPSULATED DIODES

Туре	Max p.i.v.	Qty
1 N4001	50 V	4
1N4004	400 V	4

TABLE 4 ZENER VOLTAGE REFERENCE DIODES

Туре	Voltage	Qty
BZY88	5·1 V	2
BZY88	5·6 V	2
BZY88	10 V	2

TABLE 5 LIGHT EMITTING DIODES

Туре	Colour	Dia.	Qty
T1L220	Red	5mm	4

TABLE 7 INTEGRATED CIRCUITS

Туре	Function	Qty
741	Operational Amplifier Timer	3
555	Timer	3

transistors, will be required from time to time, but these are best purchased as the need arises.

INTEGRATED CIRCUITS

Integrated circuits (i.c.s) are now so commonly used that it makes sense for the beginner to purchase a few of the more popular types. We suggest just two types to commence with: the 741 operational amplifier and the 555 timer. See Table 7.

Both of these i.c.s are available in 8-pin dual-in-line packages.

TABLE 3: HIGH SPEED SILICON SWITCHING DIODES

Туре	Max Voltage	Max Current	Qty
1N4148	75 V	75 m A	4

TABLE 6: TRANSISTORS

Туре	Material	Outline	Application	Qty
BC107 BC108 BC109 BFY51 ZTX300 2N3704 2N3702	npn S npn S npn S npn S npn S npn S pnp S	TO-18 TO-18 TO-18 TO-39/TO-5 E-line TO-92 TO-92	Audio driver stages General purpose Low noise audio General purpose General purpose Audio amplifier Audio amplifier	5 5 2 2 2 2 2

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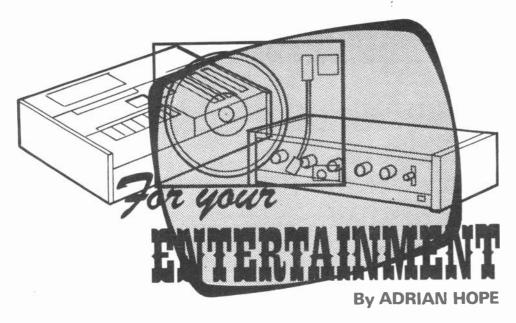
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A Cautionary Tale

Beware the creeping calculator disease. Can you still do any mental arithmetic

Here's a true cautionary tale.

Recently a sixth former left school with an impressive string of 'A' levels and an assured place at university to study engineering. To fill in the few months between school and college he took a temporary job as a milkman. Or more accurately, he tried to take a job as a milkman.

The dairy in question has a policy of giving every new milkman a half hour

arithmetic test.

"I'm afraid I haven't brought my cal-culator" explained the would-be engineer. "No matter" said the dairy foreman "We wouldn't let you use it in the test anyway'

The student never did work as a milkman. Stripped of his calculator, he was arithmetically helpless and failed the test miserably.

Innumerate Society

Are we becoming an "innumerate" society? I raised the subject with the head of the maths department of a large London comprehensive school along with some

of the school governors.

"We are educating children for a technological age" was the reply. It seems that as far as schools are concerned, calculators became acceptable as an everyday tool and an exam aid, when their cost fell below £10. The maths master argued that skills like long division and long multiplication are no longer of much importance.

What does matter, he believes, is the ability to "estimate" an answer to check that a calculator answer isn't totally haywire, for instance through mis-keying a decimal point. But isn't this based on the wholly false premise that everyone now carries a calculator around with them at all times? What about holiday trips to the beach or to restaurants where you may need to split a bill accurately several ways. And what happens if your calculator batteries run down when you want to check the price of 13 litres of petrol at an odd number of francs per litre?

The teacher's argument is that where accuracy matters, for instance in business, there will now always be a calculator to hand. There will also be an electronic cash register in most shops so all you need is a rough estimation to check the decimal point.

Exactly the same arguments against "progress" were raised, argued the teacher, when schoolchildren were no longer required to work out square roots the hard way. But, as that student who tried-but-failed-to become a milkman found out to his cost, long multiplication and division are far closer to real life than square roots. It's part of the everyday routine of a milkman to work out the cost of several dozen bottles of milk at an awkward cost per pint.

The parent governors had a ready but unconvincing answer to the cautionary milkman tale. "Educate the dairy into allowing the use of calculators". Furthermore I never thought I'd hear a mathematics teacher say "call it £100" when explaining how he would divide a restaurant bill of £98.55 between a large party of diners caught without their calculators. But he did.

Wristwatch Calculators

In the future calculators will become even more accessible than they are now. There is one coming soon from Japan that you wear on the wrist like a wrist watch; and of course it doubles as a watch, alarm and stop watch as well. But should we always take the easy way out?

Language translators with synthesised speech are already available and will become cheaper and cheaper. Should we bother to learn languages in the future? There is already a prototype portable electronic "typewriter" that stores long messages in a solid state memory. Is it worth learning to write?

Have you noticed how on television, especially in programmes imported from the USA, every important written message or caption is read out aloud? Need we now bother to learn to read? It's easy to lose sight of the sociological questions which are being posed by electronic answers.

Before Their Time

I'll bet that few people working today in electronics will even recognise the name John Sargrove. I certainly didn't until the Institution of Electronic and Radio Engineers organised an evening meeting to remind a few interested people of Sargrove's work.

In a nutshell he was another of those unfortunate inventors, like Alec Reeves, Charles Babbage and Alan Blumlein, who were way ahead of their time. It was Reeves who invented PCM in the 1930's, long before transistors were available to make the system work.

Working a few years earlier than Reeves, Blumlein invented stereo and film recording long before the industry was ready for it. And it was in the early 19th Century that Babbage first laid plans for a computer which was the mechanical equivalent of today's electronic calculator.

Although it is not widely recognised, John Sargrove, who died in 1974, worked soon after World War II on a system of total automation for radio and TV receiver production. Although the scheme, christened ECME (Electronic Circuit Making Equipment) won Sargrove the first ever Clerk Maxwell premium in 1946, the idea was too far ahead of its time to become a commercial success.

Automated Radio

His dream was to build a factory which would build radios almost untouched by human hand. Those who remember him recall that "he wanted every Indian to have a radio".

Of course, in the 40's all radios had to rely on valves and all automation equipment for building them had to rely on mechanical relays. Transistors and solid state switching were still a pie in the sky.

Nothing to be daunted, Sargrove designed a radio that was based on large integrated circuits with sockets for valves. But the circuits weren't i.c.s as we know them. Each was a large board with 15 solder joints, 15 capacitors, two variable condensers (capacitors) and several valve sockets. But everything was laid out by robot hands. The resistors were deposited as layers and only the glass valves were plugged in by hand. The Sargrove production line was actually used by Cossor in 1947 to produce radios. Unfortunately the scheme was short

He originally saw ECME as "the answer to the vexed problem of post war labour problems". But very soon fears of job shortages replaced concern over labour shortage. The Daily Mirror ran a centre spread on the risks to employment presented by automation. Sargrove himself argued that automation didn't create unemployment. What it created was the need to redeploy a labour force from tedious repetitive jobs into more rewarding and constructive work.

Energetically he went out round the country and lectured on his ideas. His faith in the viability of automated factory production of electronic equipment sprang from experience of the valve and light bulb industry. If these precision products can be made in millions by total automation why not circuit boards and whole radios?

It's unclear why exactly ECME failed. But in part it was due to the problems of automating such a complicated multistage process with mechanical relays. There was always some moving part somewhere ready to go wrong. What's more political pressure to kill off the idea mounted.

The idea surfaced again in the 50's when an attempt was made to produce an automated TV production plant. But that too failed for the same reasons.

Sargrove then concentrated his energies on automation processes that, although ingenious, were slightly less ambitious and considerably less touchy. For instance he built machinery to match the colour of rosary beads, sort good from bad coffee beans and check the weight of balls of bakers' dough prior to baking into bread.

These are all more difficult than they may sound but didn't bother the politicians. He also produced the tiniest condenser mic of the time, no larger than a farthing.

Wisdom of Automation

The real irony of the Sargrove saga is that foreign factories, especially those in Japan and Italy, have long since seen the wisdom of automation. Although it is an expensive investment to automate, once the lines are running the mass-produced output is cheap and reliability is high. Workers displaced from routine jobs can often be redeployed in to more stimulating posts.

Printing works and car factories in Italy and almost every industrial factory in Japan now borrow from Sargrove's pioneering ideas of over 30 years ago. Many are heavily automated and very successful.

In the UK we are still debating the wisdom, cost and morality of automation, rather like the captain of a sinking ship worrying about the menu for that night's dinner.

University Industrial Units

During the last decade over 30 British Universities have opened "industrial units" offering companies the benefit of their scientific experience on a consultancy basis. These are intended to be self-supporting departments, set up by the parent University and staffed by university scientists, but operating on a commercial basis.

For example UMIST in Manchester has a Corrosion Unit which worried companies will-approach when their pipe lines or swimming pools spring a leak or their foundations show unaccountable signs of rusting or rotting. At the Department of Cybernetics of Reading University, a Research Unit in Instrument Physics was established in 1969 and has been self-supporting since 1972.

Just some of this excellent pioneering development work undertaken by Universities was highlighted by a recent visit to Reading University.

Ambisonics

One project which will probably already be familiar to some readers is the Ambisonics surround sound system. This is best described as "second generation quadraphonics" and already the BBC, IBA and many European radio stations

are appraising the system. A cross-licensing deal has been struck with the Japanese company Nippon-Columbia and the project is being financed by the NRDC.

Essentially Ambisonics differs from the old, and now obsolete, quadraphonic systems because there is no attempt at conveying four separate channels of sound for feeding to four loudspeakers. The original sound information is mixed or coded into two, three or four channels in dependence on the number of recording or transmission channels available e.g. two on a stereo record, four on a four track tape and so on.

This information is decoded in accordance with the type of reproduction system available. Surround sound in the azimuth or horizontal plane is conveyed by two or three channels, or even by two-and-a-half channels (a "half channel" has limited frequency bandwidth and limited amplitude level). Surround sound with height, or "periphony", is conveyed by four channels.

A demonstration of periphony at the Audio Engineering Society Convention in London, earlier this year used a four channel system and eight loudspeakers, above, around and below the listener. It certainly gave an appetite-whetting foretaste of the future of domestic audio.

Unfortunately no major record company has yet adopted the Ambisonic system. They are doubtless all too scared by the memory of the quadraphonic flasco of non-standardisation.

Driverless vehicles

One of the first Reading commissions was to produce a driverless tractor, intended for the Third World countries. It proved a pointless exercise because in the Third World there is no shortage of labour, but a considerable shortage of cash to spend on high technology!

This situation wasn't realised until Reading scientists had built a driverless tractor which ploughed a field, without human aid, by sensing signals transmitted from wire aerials laid down each side of the field. The Road Research Laboratory heard of this system and in 1973 commissioned work on a driverless bus using a similar system based on wires buried underneath the road.

Experimental cars, vans and even a coach were duly produced. But at the last minute plans to run test projects in British cities were abandoned as a result of local spending cuts.

Nothing daunted, Reading suddenly realised that they had unwittingly produced an automatic control system for a vehicle which could readily be converted into a manual control operable from a single joystick, like a model aircraft control. Such a system would obviously be a boon for handicapped drivers and they soon succeeded in putting a 50 seater coach under the control of a single joystick that could be moved by one finger.

Now the Thalidomide Trust is financing the development of add-on joystick control units for use in cars for the disabled. Around 20 vehicles are currently being modified at the cost of around £2,000 each and should be on the road by 1981.

Speech Therapy

Doctors and speech therapists are faced with an especially difficult problem

when trying to teach speech to patients born without a roof to their mouth. This is because human speech relies on an exceedingly complex pattern of contact between the tongue and roof of the mouth.

Reading has now built an imitation roof palate which contains a matrix of tiny electrical contacts. These are connected by super-fine wires to a microprocessor which is coupled to a cathode ray tube screen. This screen displays the pattern of tongue movement over the imitation palate and so helps the patient to follow the example of a tutor.

Speech therapists in British hospitals should soon be using some of these electronic aids.

Moisture Meter

In quite a different technology it is remarkably difficult to measure the amount of water in a solid, such as a house wall. But it can be very necessary to do so. The Reading answer, developed for the Building Research Establishment, is a circuit which registers the capacitive effect of the water rather than the conductive effect as normally sensed by a probe.

A hole is cut in the wall and then plugged with a central metal rod and silver sleeve. This plug creates a capacitor of which the dielectric constant depends on the amount of water in the wall.

A very high frequency current, of around 60MHz, is fed into the plug and its capacitance value read out alongside a scale of moisture content. In practice water has such a high dielectric constant that there is an 80-fold difference between a dry and wet wall.

Unfortunately there is a snag. Because any impurity such as salt in the water makes it conductive, the measurement readout will normally be a very confusing mixture of conductance and capacitance.

The answer is simple once you've thought of it. Conductance and capacitance are 90 degrees out of phase, so the readout is made phase sensitive to offer one value for conductance and another, displaced by 90 degrees, for capacitance. The conductance readout gives a measure of the salt content of the wall and the capacitance readout gives a measure of the amount of water present.

A similar electronic system is used to measure the "lushness" of pasture. Normally pasture has to be collected, burned and analysed to establish its water content or lushness.

Reading use a capacitance meter and a grid of condenser plates interleaved with the pasture. An accurate moisture content readout of the pasture between the plates can thus be obtained.

The system is so sensitive that it is sent haywire by the presence of a human body within 10 metres range. So the readouts have to be transmitted as a 3MHz signal.

The signal is mixed in a receiver with a signal from a tunable local oscillator. The result is a variable beat tone from the receiver, like that which issues from a metal detector.

The beat tone is zeroed by adjustment of the local oscillator by the operator. This gives a direct readout of the signal frequency coming from the condenser plates in the pasture. This in turn gives a direct tell-tale of the amount of water in the pasture which is serving as a dielectric between the plates.

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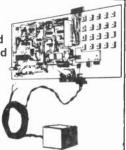


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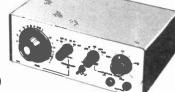
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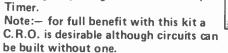
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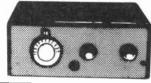


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A READER has asked; "In articles about the reception of frequency-modulated radio transmissions I frequently come across the term, quadrature detector. Please explain what this means."

An f.m. signal, when it leaves the transmitter, has a constant amplitude. That is, the peak and trough sizes of the waves do not change. Only the

frequency changes.

At the receiver, noise picked up along with the signal or generated by the components in the receiver itself can cause the amplitude to vary. But any variations are eliminated by a limiter which in effect slices the tops and bottoms off the incoming waves so that they end up all cut down to the same size. By limiting the signal in this way the effects of noise are greatly reduced. This accounts for the much lower "background hiss" of an f.m. receiver compared with an a.m. receiver.

Limiting

Let's consider an f.m. transmitter which is not at the moment carrying any programme material. It sends out a steady frequency at a steady amplitude; nothing changes. At the receiver, after limiting, this signal is transformed into a steady square wave, Fig. 1a.

When the programme is transmitted this square wave will change in frequency, higher or lower, according to the variations in the voltage generated by the microphone in the studio. But for the time being there is no programme. It follows that the square wave of Fig. 1a must produce

no output.
When its frequency varies, however, it means that a programme is being transmitted and it must then produce an audio output which for low distortion must be exactly proportional to its frequency.

Sampling

In a quadrature detector the noprogramme wave is sampled at regular intervals. But the sampling periods are so timed that the samples consist of equal parts of positive and negative bits of the wave. These average out to zero because the positive bits just cancel the negative bits. You can think of the sampling process as switching. The wave is applied to a high speed switch which when on lets it pass but when off stops it.

If the "ons" and "offs" are timed as shown in Figs. 1a and b, then the positive samples are equal in size to the negative samples. If you think of the positive samples as charging a capacitor then it is clear that the negative samples will discharge it by the same amount. The result is that there is no net charge.

Modulation

If the transmitter is now modulated by a programme the frequency varies. For negative going points in the audio modulation the frequency may go low. For positive points it may go high. The sampling periods must be adjusted so that the output goes positive or negative in sympathy.

Suppose the wave form of Fig. 1c is the limiter output for a strong negative interval of the audio wave. If we sample at the times shown then the whole of each negative half cycle is passed by the sampling switch and none of the positive half cycles. So the output is now as negative as it can be (Fig. 1d). For positive-going modulation the frequency goes high and for maximum positive output samples must accept the whole of each positive half cycle, Figs. 1e and f.

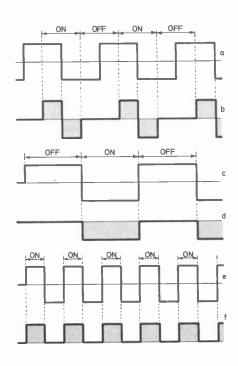


Fig. 1. Waveforms illustrating the operation of the quadrature detector.

When the audio is less intense the samples must include some positive bits and some negative bits but not equally positive and negative. In this way the cancellation will be incomplete and a certain amount of output will be produced. This can be positive or negative depending on whether the positive or negative bits are larger. By adjusting the timing of the samples any amount of net output can be obtained, from "full positive" to "full negative".

This is the principle of the quadrature f.m. detector (also called a quadrature demodulator and a quadrature discriminator). All that remains is to say how it can be made to work.

How It Works

This requires some automatic method of adjusting the sampling times so that the correct outputs are obtained. This is a lot easier than it sounds. The standard method is to use the limited signal itself to time the sampling. The limited signal is applied to two parts of the detector at the same time. One is just to the sampling switch, which lets it pass or not. The other is to the timing mechanism which turns the switch on or off.

It so happens that all the clever work of adjusting the timing to suit the frequency can be done by one quite ordinary *LC* circuit tuned to approximately the frequency of the wave shown in Fig. 1a. This produces just enough phase shift to make the switch turn on and off as at (a).

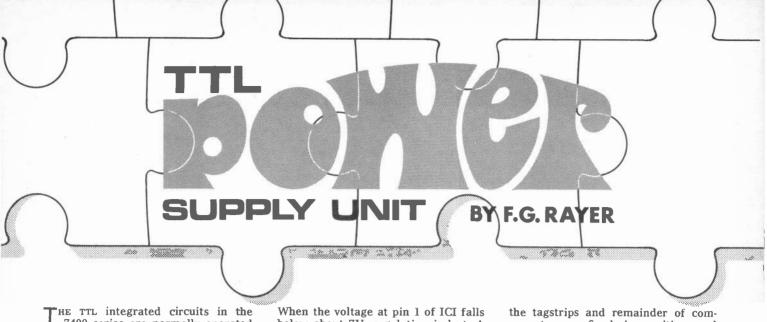
If the frequency now goes low the phase shift changes and moves the timing towards Fig. 1c. If the frequency increases the sampling times are moved towards (e). The amount by which the times are moved is in proportion to the frequency and so the net output is also in proportion to the frequency which is what is required. As the frequency swings up and down in sympathy with the audio at the studio so the output swings positive or negative in the right way to reproduce the original audio wave.

Quadrature

It is a curious feature of quadrature demodulators that they can be converted from f.m. detectors to a.m. detectors just by changing the phasing of the sampling timer. To be precise, when the detector is used for a.m. it is no longer a quadrature detector.

Quadrature just means that the sampling times are a quarter of a cycle out of phase with the input signal, as they are in (a). For a.m. detection the signal is not limited and the detector samples the positive peaks.

In this case the samples must be in phase with the signal.



THE TTL integrated circuits in the 7400 series are normally operated at between 4.75V and 5.25V and the TTL Power Supply Unit described here is intended particularly for these. The output is approximately 5V and this is regulated so that there is negligible change in voltage from no load conditions up to a maximum available load current of 1A. Short circuit protection built in.

CIRCUIT DESCRIPTION

The full circuit diagram of the unit is shown in Fig. 1. Transformer T1 steps down the a.c. mains from 240V to 6.3V and isolates the low voltage circuit. Single-pole switch S1 is the on-off switch and the neon indicator LP1 shows when the power is on.

The si.icon bridge rectifier D1-D4 has four leads. Two are for the a.c. input from the transformer secondary, the two others are the positive and negative d.c. outputs. Direct current from these leads charges the smoothing or reservoir capacitor C1. About 9V will be present across C1. Instead of a bridge rectifier, four individual 1A silicon diodes could be used.

The LM309K integrated circuit is packaged in a TO-3 can and incorporates the voltage regulation and short circuit protection devices.

With the components shown, maximum current is about 1A and short-circuit current a little over 1.5A.

when the voltage at pin I of ICI falls below about 7V, regulation is lost. A short circuit in the output circuit would naturally be corrected as soon as noticed but with Tl and the bridge rectifier rated at 2A, these items are not damaged.

CASE

The metal case is made from a single piece of flanged aluminium 100mm x 200mm (e.g. a single Universal Chassis member.) A 90 degree section is cut from each flange 63mm from each end and after all the holes have been drilled, the piece is bent to form an open box as shown in Fig. 3.

After assembly a piece of perforated metal is bent to form a cover, and is fixed with short self-tapping screws run into the flanges.

ASSEMBLY

The component layout is shown in Fig. 2. Before components are mounted all burrs and irregularities should be removed from the case. The front panel components are then fixed in position.

Pins 1 and 2 of IC1 should not touch the metal case and the integrated circuit should rest flat on the side of the case. A tag screwed to the integrated circuit can provide connections to the metal chassis and pin 3. After the transformer is in position it can be wired up. Finally

the tagstrips and remainder of components are fixed in position and interwired. Note that the neon indicator should be the type with a series resistor incorporated.

The mains cable enters the case through a grommet and is connected up as shown. Current is drawn from a 3-pin plug fitted with a 2 or 3 amp fuse. Internal wiring can be of insulated flex, or 20 s.w.g. covered.

APPLICATIONS

The supply is very suitable for any TTL project incorporating 74 series i.c.s requiring 5V. Take care to connect the supply with the correct polarity. The output voltage has been found to change by only about $0.05 \, \text{V}$ for loads from zero to $500 \, \text{mA}$. This power supply unit will run quite large and complex projects as well as simpler devices which may have been operated from a $4.5 \, \text{V}$ battery supply.

COMPONENTS

Capacitors

C1 4700μF 12V elect. C2 470μF 12V elect.

C3 10nF ceramic or plastic

Semiconductors

D1-D4 50V 2A bridge rectifier IC1 LM309K voltage regulator i.c.

Miscellaneous

T1 mains primary/6·3V 2A secondary transformer S1 s.p.s.t. mains toggle

SK1, 2 3mm sockets (one red, one black)

Tagstrips: 4-way with one earthed mounting tag (1 off), 2-way with one earthed mounting tag (1 off); solder tags (2 off); three-core mains cable; rubber grommet; p.v.c. covered wire; 100mm × 200mm piece of flanged aluminium (e.g. Universal Chassis member No. CU56A from Home Radio); 226mm × 74mm piece of perforated metal for cover; nuts, bolts, washers for securing transformer, i.c. and tagstrips.

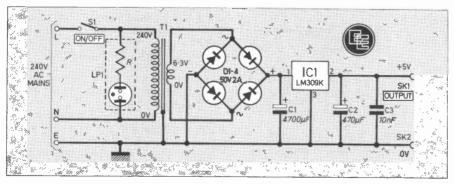
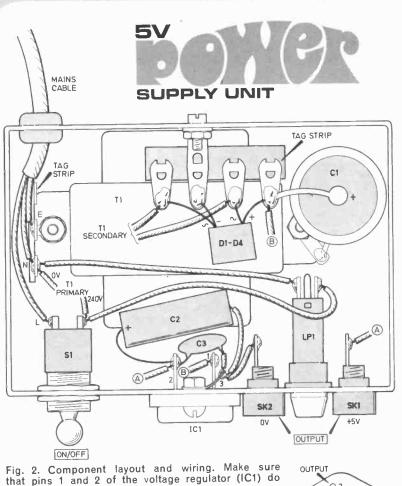
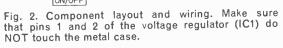
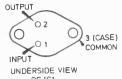
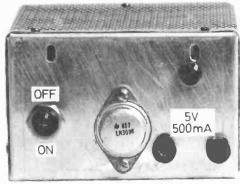


Fig. 1. Circuit diagram of the 5V Power Supply Unit.

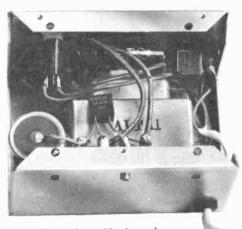




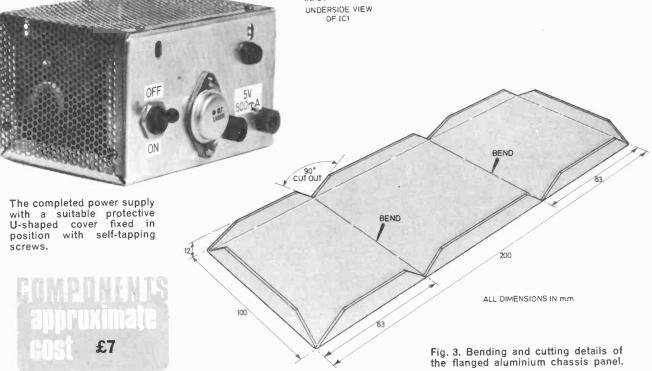




Components mounted on the front panel.



Internal positioning of components. Due to the close density care must be taken to ensure that components do not short on the transformer, particularly S1, IC1 and LP1.



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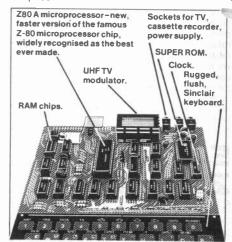
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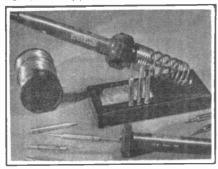
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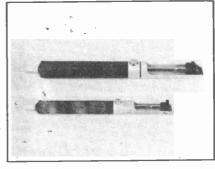
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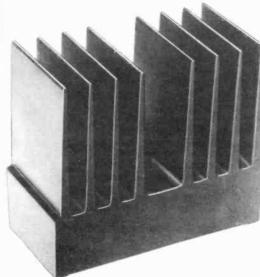
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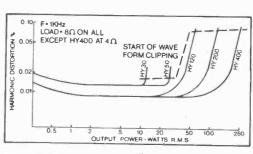
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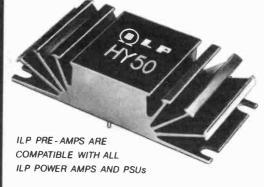
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Load impedance - all models $4\,\Omega$ - ∞ Input sensitivity - all models 500 mV Input impedance - all models 100K Ω

Frequency response - all models 10Hz - 45KHz - 3dB



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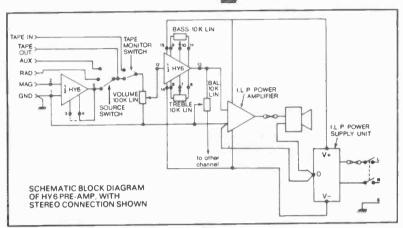


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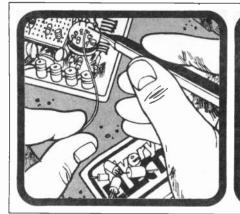
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