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CCTV CAMERA MODULES 46X70X29mm, 30 grams, 12v 100mA, auto electronic shutter, 3.6mm F2 lens, CCIR, 512x492 pixels, video outputis tv  $p_0$  f75.0m). Works directly into a scart or video input on a tv or video. IR sensitive, £79.95 ref EF137.

IR LAMP KIT Suitable for the above cameral enables the camera to be used in total darknessi £5.99 ref EF138.

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# PRACTICAL

### VOL. 25 No. 10 OCTOBER 1996

The No. 1 Independent Magazine for **Electronics, Technology and Computer Projects** 

# Projects and Circuits

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Our November '96 Issue will be published on Friday, 4 October 1996. See page 777 for details. Everyday Practical Electronics, October 1996

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\*\*CADCAM Recommended March 96

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understanding electronics leads to far greater control over the reproduced sound. The subjects covered include tape recording, tuners, power output stages, digital audio, test instruments and loudspeaker crossover systems. John's lifetime of experience and personal innova-tion in this field allow him to apply his gift of being so familiar with his subject that he can write clearly about it and make it both interesting and comprehensible to the reader

comprehensible to the reader. Containing 240 pages and over 250 line illustra-tions this new book represents great value for money at only £18.99 plus £2.50 postage. Send or telephone for your personal copy now.



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We stock a good range of books of interest to the electronics and audio enthusiast, including many reprinted classics from the valve era. Some were in last months advertisement, but see our list for the full range.

New this month is the GEC Valve designs book at £18.95, and the VTL Book, a modern look at valve designs, £17.95.







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# EVERYDAY PRACTICAL .ECTRONIC

### VOL. 25 No. 10 OCTOBER '96

### **CHEAP** ...

The theme of my piece this month is "cheap". Sounds awful doesn't it? What has triggered off this tacky thought? It all comes down to one thing - promotions. I don't mean the sort of promotion you get at work - or maybe you don't! - I mean the type of promotion we undertake to sell more copies of EPE.

We promote the magazine on a regular basis - it's a chain operation. Basically if we can stick something on the front cover that your friendly newsagent believes will help to sell more copies then he will take extra, we will hopefully get better availability and you, the interested shelf-browser, will buy more. If you like what you get you might even go on buying the magazine. If you don't like what you get please let us know.

The problem is that we have to pay for the free gift, and pay to bag it, and pay to stick it on the cover, and pay for the increased weight on postage and transport etc. And, unlike some magazines, we don't believe in putting up the cover price to give you a gift! So we have to come up with something that is cheap, but it must also be ''free' valuable to all our readers - we don't want to give you something that you think is cheap and of no use!

For our last promotion we gave all our UK readers a free set of headphones, since we only paid 25p per pair for them they were cheap, but they were good quality and we reckoned that anyone would find them useful - don't ask how we came to buy 25,000 sets of headphones at that price because I won't tell you, well I might if you make it worthwhile (but I'm not cheap you understand!).

### ... BUT UNIQUE

Anyway this month we have presented you with a free Understanding Active Components 48-page booklet, we believe it will interest most readers and be worth keeping on file. If it had been produced to sell in its own right it would probably carry a £1.95 price tag. However, we have produced 30,000 of these so the print and paper costs are very low and, because the material has been reprinted from our Electronics Service Manual the text, typesetting, drawings, etc. have already been paid for.

The author Mike Tooley won't thank me for saying the item is cheap, but I'm sure, like you, he will understand what I mean. Because the material has been taken from the Electronics Service Manual this little booklet is not available on its own - so your free gift is also unique.

By the way, the rest of the Manual (and our Modern Electronics Manual) can be bought cheaply at present - you will find them advertised on pages 756 and 797 of this issue - there is a £10 off discount available on these until 1 December. That's a cheap plug!

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Editorial Offices: EVERYDAY PRACTICAL ELECTRONICS EDITORIAL ALLEN HOUSE, EAST BOROUGH, WIMBORNE DORSET BH21 1PF Phone: Wimborne (01202) 881749 Fax: (01202) 841692. Due to the cost we cannot reply to orders or queries by Fax. E-mail: editorial@epemag.wimborne.co.uk Web Site: http://www.epemag.wimborne.co.uk See notes on Readers' Enquiries below - we regret lengthy technical enquiries cannot be answered over the telephone Advertisement Offices: EVERYDAY PRACTICAL ELECTRONICS ADVERTISEMENTS HOLLAND WOOD HOUSE, CHURCH LANE GREAT HOLLAND, ESSEX CO13 0JS

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Subscriptions: MARILYN GOLDBERG

Editorial: Wimborne (01202) 881749 Advertisement Manager:

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We are unable to offer any advice on the use, purchase, repair or modification of commercial equipment or the incorporation or modification of designs published in the magazine. We regret that we cannot provide data or answer queries on articles or projects that are more than five years old. Letters requiring a personal reply must be accom-panied by a stamped self-addressed envelope or a self-addressed envelope and international reply coupons. Due to the cost we cannot reply to queries by Fax.

All reasonable precautions are taken to ensure that the advice and data given to readers is reliable. We cannot, however, guarantee it and we cannot accept legal responsibility for it.

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We do not supply electronic components or kits for building the projects featured, these can be supplied by advertisers.

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# Constructional Project





Extend your creative options when shooting home video movies with this ''grey-to-white'' fader.

WiDEO FADER projects have appeared in Everyday Practical Electronics in the past, and these have all provided a conventional fade out to a black screen. This video fader is slightly different in that it provides a fade out to a white screen, or to a preset grey level if preferred. This gives the home video producer a few more creative possibilities from a circuit that is only marginally more complex than an equivalent fade-to-black circuit.

Prospective constructors should note that this fader is intended for use with a standard composite video signal. In normal use it is connected between the video output of a camcorder or VCR, and the video input of a VCR or television/monitor. It cannot be used with a u.h.f. television signal, or with any form of RGB signal.

### SYSTEM OPERATION

The block diagram of Fig. 1 helps to explain the way in which this video fader functions. The example waveforms of Fig. 2 show what the unit has to achieve, and also help to explain how it is achieved.

The top waveform (a) represents the composite input signal, but only for two and a bit lines. A short negative line synchronisation pulse is present at the beginning of each line, and this is followed by the colour burst signal. Next comes the main part of the signal, which is the picture modulation. The UK PAL system utilizes positive modulation, which means that the more positive the modulation voltage, the brighter the line at that point.

Simply fading out the entire video signal will not give the desired result. The picture modulation will be faded out, but the burst and synchronisation signals will gradually disappear as well.

As the signal was faded out, the synchronisation pulses would be attenuated, and proper synchronisation would be lost well before the signal was fully faded out. The picture modulation must be attenuated, but the rest of the signal must be left unaltered.

### SPLIT-UP

In order to do this it is necessary to separate the picture modulation and synchronisation signals, feed the picture signal through the variable attenuator, and then recombine the two parts of the signal again. The splitting of the signal is accomplished using two electronic analogue switches that are operated in anti-phase. Therefore, at any one time only one or other of the switches will connect its input signal through to the output.

One switch is fed directly with the input signal, and this switch is activated during



the initial part of each line scan, when the synchronisation and burst signals are present. The other switch is fed via the fader circuit, and this switch is active for the rest of the time. This is when the picture modulation is present.

The anti-phase control signals for the electronic switches are generated by a side chain, which starts with a synchronisation separator circuit. This clips the input signal in such a way that the picture and colour burst signals are stripped off, leaving somewhat amplified synchronisation pulses.

These pulses are fed to a monostable which is triggered on the leading edge of each synchronisation pulse. Its pulse duration is slightly longer than the time from the beginning of each synchronisation pulse to the end of the colour burst signal.

The output of the monostable is a positive pulse which activates the upper electronic switch (Fig. 1), which is fed with the unprocessed input signal. This switches the synchronisation pulses and burst signals straight through to the output in the required fashion. This signal is represented by the waveform of Fig. 2(b).

The other electronic switch is fed from the input via the fader circuit, and it is controlled by an inverted version of the signal from the monostable. It therefore passes the picture modulation through to the output, but blocks the synchronisation and burst signals.

This signal in its non-faded form is represented by Fig. 2(c), while Fig. 2(d) represents the picture signal when faded by 50 per cent. A buffer stage at the output ensures that the unit has a suitably low output impedance.

### POSITIVE FADE-OUT

As described so far the unit provides what is just an ordinary fade-out to a black screen. In order to obtain a fade-out to a white screen it is necessary to introduce a positive bias to the picture signal as it is faded out.

An output signal with 50 per cent fade is represented by waveform Fig. 2(e). The picture modulation has been reduced to half its normal amplitude, but the positive bias keeps the overall brightness of the screen quite high.

The signal output waveform, with a fully faded picture, is shown in Fig. 2(f). The picture modulation has been faded out to zero, but a strong positive d.c. level during

the picture modulation period gives a white level during each line scan.

The positive bias circuit is provided by a potentiometer which is ganged with the fader potentiometer, but is connected to operate out-of-phase with the fader control. Thus, as the signal is faded out, the bias level is steadily increased, ultimately giving a plain white screen.

The maximum bias level can be backedoff if required, so that the screen fades to a preset shade of grey rather than to white. To my eyes at any rate, a mid-grey background gives the best general purpose fadeout characteristic, but this is clearly a matter of personal choice. It is also a matter of using whichever background level is felt to be most appropriate to the subject matter.

### CIRCUIT DESCRIPTION

The main circuit diagram for the Video Fade-to-White unit is shown in Fig. 3. The circuit diagram for the 12V mains power supply unit is shown separately in Fig. 4.

The synchronisation separator is based on transistors TR1 and TR2 which are both used as common emitter amplifiers. The biasing of these two stages (or lack of it in the case of TR2) provides the required clipping of the signal with the picture and colour burst signals being effectively stripped away.

The monostable uses IC1 in a conventional 555 monostable configuration. IC1 is triggered by a high to low transition on pin 2, which gives the required triggering at the beginning of each negative synchronisation pulse. Resistor R8 and capacitor C6 are the timing components for IC1, and these set the theoretical pulse duration at 11 microseconds. A low power 555 is used for IC1 as this avoids problems with



Fig.2. Example waveforms which help to explain the way the Fader functions.

"crowbarring" of the power supply, and low power versions such as the TS555CN have the advantage of being somewhat faster than the standard 555.

One section of a CMOS 4001BE quad 2-input NOR gate is used for IC2. In this circuit the two inputs of IC2 are wired together so that it operates as a simple inverter, and it is used to generate the complement of the monostable's output signal. The other three gates of IC2 are not used, but their inputs are connected to the positive supply to prevent spurious operations of these gates.

### ANALOGUE SWITCHING

The electronic switches are provided by IC3, which is a CMOS 4016BE quad analogue switch. Only two of the switches



Fig.3. Main circuit diagram for the Video Fade-to-White project.



are needed in this application, and no connections are made to the other two.

The 4066BE is an improved version of the 4016BE, having faster operation and a lower "on" resistance. Both devices work well in this circuit, with no obvious difference in performance between the two components.

The unprocessed input signal is fed to IC3a, and it is controlled by the output signal from IC1 pin 3. The positive pulse from IC1 switches on IC3a during the initial part of each line scan, allowing the synchronisation and colour burst signals to pass through to the output.

Analogue switch IC3b is fed with the input signal via Fader potentiometer VR1a. This switch is controlled by the inverted signal from IC2, and it is therefore switched on while the picture modulation is present.

Varying positive bias is generated by a potential divider circuit which consists of resistor R11 and potentiometers VR2 and VR1b. As VR1a is adjusted to fade out the picture signal, VR1b provides an increasing resistance which provides a higher bias voltage. This takes the lower track terminal of VR1a steadily higher in voltage.

The maximum bias voltage can be controlled by VR2, and this enables the fadeout tone to be set for anything from a good white level to virtually black. The output buffer stage is a simple emitter follower amplifier based on TR3.

### POWER SUPPLY

The circuit requires a reasonably stable and well smoothed 12V supply, and the current consumption is around 15mA to 17mA. The unit can be powered from a 12V battery if desired, and eight HP7 size cells in a plastic holder are suitable. A mains power supply is likely to be a much more economic choice in the long term.

A suitable circuit diagram for the Mains Power Supply Unit (p.s.u.) is shown in Fig. 4. This is quite conventional with mains transformer T1 providing voltage step-down and isolation from the mains supply. Diodes D4 to D7 provide full-wave bridge rectification. IC4 is a monolithic voltage regulator that provides a very stable and well smoothed 12V output. Protection against overloads is provided by the built-in current limiting of IC4, and fuse FS1.

### AUDIO FADER

The unit has no built-in audio fader as this side of things is often handled by a separate audio mixer. However, if desired an Audio Fader can be incorporated in the Video Fader, and it is just a matter of adding input and output sockets plus a 10k logarithmic potentiometer. These are connected in the manner shown in the circuit of Fig. 5, which has VR3 connected in conventional volume control fashion.

Ideally VR3 would be ganged with VR1, but as VR1 is a dual-gang type already, having a combined video and audio fader control is probably not a practical proposition. A three-gang potentiometer would be required, with one gang having a different value and law to the other two.

### CONSTRUCTION

The Video Fade-to-White is built on a single-sided printed circuit board (p.c.b.), which is available from the EPE PCB Service, code 114. The topside component layout, full size underside copper track master and interwiring between off-board components are detailed in Fig. 6.



Fig.5. If required, an audio fader control can be added to the unit.

IC2 and IC3 are CMOS devices, and the standard anti-static handling precautions are therefore needed when dealing with them. The most important of these precautions is that they should be fitted in holders, and not soldered direct to the printed circuit board.

Low power versions of the 555 timer are often based on MOS technology, but are not usually vulnerable to static charges. It is still advisable to use a holder for ICL.

Do not fit IC2 or IC3 into their holders until the unit is finished in all other respects. Leave them in their anti-static packing until it is time to fit them into the holders, and touch their pins as little as possible when fitting them in place.

CO	MPONENTS
Resistors R1 R2, R3 R4 R5, R7 R6 R8, R15 R9 R10 R11 R12, R13 R14 All 0.25W 5	120Ω 47k (2 off) 18k 4k7 (2 off) 33k 10k (2 off) 1k 3k9 22k 100k (2 off) 470Ω % carbon film
Potention	neters
VR2	lin. 10k rotary carbon, lin.
Capacitor	s
C1, C9, C11	100µ radial elect 16V (3 off)
C2, C13, C14 C3 C4, C10 C5 C6 C7, C8 C12	100n disc ceramic (3 off) 220n polyester 10μ radial elect. 25V (2 off) 100n polyester 1n polyester 47μ radial elect. 16V(2 off) 1000μ radial elect. 25V
Semicon	ductors
D3 D4 to D7	1N4148 signal diode (3 off) 1N4002 100V 1A rectifier
TR1 TR2, TR3	(4 off) BC559 <i>pnp</i> silicon transistor BC549 <i>npn</i> silicon transistor
IC1	(2 off) TS555CN low power 555
IC2	4001BE CMOS quad 2-input NOR gate
IC3	4016BE or 4066BE CMOS quad analogue switch
IC4	μA78L12 12V 100mA positive regulator
Miscellar	eous
SK1 SK2	phono socket (2 off)
FS1	100mA 20mm quick-blow fuse
51 T1	rotary mains switch standard mains transformer; 230V a.c. primary, 12V 100mA secondary (see text)
Printed c EPE PCB strument c x 51mm; 20mm fuse pin d.i.l. ho plug; 6BA	rcuit board available from the Service, code 114; metal in- ase, about 203mm x 127mm control knob (3 off); pair of 9-clips; 8-pin d.i.l. holder; 14- older (2 off); mains lead and fixings or stand-offs; multi-

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strand connecting wire; solder, etc.



Everyday Practical Electronics, October 1996

It is not important to fit the other components in any particular order, but it is good practice to start with the resistors and capacitors and then fit the semiconductors. Fuse FS1 is fitted onto the board via a pair of printed circuit mounting fuse clips. Use plenty of solder when fitting these clips, so that they are securely anchored to the board.

### CASE

The unit is housed in a metal instrument case which needs to be about 200mm wide in order to comfortably accommodate the printed circuit board and mains transformer. The circuit board is mounted well towards the left hand side of the case so as to leave a generous amount of space for the mains transformer at the opposite end.

The p.c.b. must be mounted on plastic stand-offs that keep the underside of the board well clear of the metal case. Alternatively, 6BA or metric M3 screws can be used, but spacers at least six millimetres long should be used between the case and



Fig.6. Video Fade-to-White printed circuit board component layout, full size copper foil master and interwiring to off-board components.



Layout and wiring of components inside the metal case. Note the use of a dual potentiometer for the Fade control and the positioning of the p.c.b. and transformer at the far ends of the case.

the board. A solder tag is fitted on one of transformer T1's mounting bolts, and this acts as a chassis "earth" connection point.

On/off switch S1 should be mounted well towards the extreme right hand end of the front panel, close to the mains transformer. In other respects the front panel layout is not critical, but it is a good idea to choose one that avoids a lot of long wires crisscrossing the case.

Sockets SK1 and SK2 are fitted on the front panel of the prototype, but they can be mounted on the rear panel if you prefer to keep the connecting leads tucked away out of sight at the rear of the unit. Both sockets are phono types, which is the standard connector for amateur video equipment.

### FINAL ASSEMBLY

Details of the interwiring between off-board components and the p.c.b. are also provided in Fig. 6. This wiring is reasonably simple, but as the mains supply is involved it is essential to proceed with extra care, double-checking everything.

Projects which involve connections to the mains supply are potentially very dangerous, and are not really suitable for beginners unless carefully supervised.

Make quite sure that the mains Earth lead is reliably connected to the solder tag fitted on one of T1's mounting bolts.

Transformer T1 must provide a 12V winding having a current rating of 100mA or more. Modern mains transformers invariably seem to have centre-tapped windings or twin secondaries. A 6V-0V-6V type is suitable, and it is just a matter of ignoring the 0V centre-tap and connecting the other two tags to the printed circuit board. A transformer having twin 6V secondary windings is also suitable, and it is just a matter of connecting the secondaries in series as shown.

On the prototype VR1 and VR2 are ordinary rotary potentiometers, but some constructors might prefer to use slider types. Unfortunately, the range of slider potentiometers available these days is strictly limited. It is unlikely that a suitable slider potentiometer for VR1 could be obtained, or anything even vaguely similar. Rotary potentiometers are probably the only option in this case.

### IN USE

When initially testing the unit it is best to connect it between the video output of a VCR or Camcorder and the video input of a television set or monitor. This enables the effect of the unit to be seen immediately. Ordinary screened phono leads are used to provide the interconnections.

With the Grey control VR2 set in a fully

anti-clockwise direction, adjusting VR1 should enable you to obtain anything from a normal picture to a white screen with the signal fully faded.

Adjustment of VR2 should provide a wide range of grey levels with the picture faded. The faded picture should be very dark with VR2 fully backed-off, but it might not quite be possible to obtain a true black level. This is simply due to stray resistances and inductances in the circuit, and is not of any great significance.

It might be possible to obtain a "whiter white" by making resistor R11 a little lower in value, but overdoing things slightly could result in the system malfunctioning when fed with a fully faded signal. The monitor or VCR may well shut down if fed with even a slightly excessive white level.

The pulse duration from the monostable is slightly too long if there is a narrow strip down the left hand side of the screen which is not affected by VR1. This is unlikely to occur, but if necessary it can be corrected by reducing the value of R8 to 9-1 kilohms.



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# New Technology Update Small portable equipment is demanding continued improvement in the types of battery available, and is being rewarded – Ian Poole reports.

Not only is the demand for the number of batteries increasing, but people's expectations are also rising. Anyone who has used a portable computer will realise that battery life is relatively short between charges. Also portable phones need to be charged regularly.

To make batteries more convenient to use they need to be lighter, carry more charge and be smaller in size. To meet these requirements a number of new technologies are emerging. Much of the work is being directed towards the development of secondary or rechargeable batteries.

### **Green** Issues

Apart from the operational requirements, other issues are important. At the moment the most popular form of battery used for electronic equipment is the nickel cadmium or NiCad battery. Unfortunately this technology is not ideal from an environmental standpoint. The cadmium present in the chemistry of the cell can be hazardous if it is disposed of in an unsuitable manner. As a result some countries have banned their sale and other technologies must be used. In other countries where their sale and use is permitted they have to be disposed of in a suitable manner.

The first real contender to the NiCad is the nickel metal hydride or NiMH cell. This is very similar to the NiCad, having a positive plate made from nickel, and an electrolyte which consists mainly of potassium hydroxide. The difference is in the negative plate. This consists of a complex metal-hydrogen storage material. This acts in a very complicated way storing or giving up hydrogen during different parts of the cycle.

The performance of this type of cell is very similar to that of the NiCad, having almost exactly the same output voltage. It does hold a greater amount of charge. Typically a small NiCad cell may hold 800mA hours whereas an equivalent NiMH cell may hold around 1200mA hours. This increase gives it a distinct edge over the older NiCad. In addition to this the removal of the cadmium make the cell environmentally acceptable. As a result many companies are switching over to these newer cells.

Unfortunately there are a few disadvantages to the NiMH cell. Great care must be taken when charging them. They do not tolerate over charging or reverse charging. In view of this the cells are normally only sold as complete battery packs for computers or cell phones. Although having said this some single cells are now appearing on the market. Another problem follows on from the exact charging requirements. Today many systems use intelligent chargers. These note certain characteristics of the cell and can determine when to cease charging. For NiCad cells there is a small but pronounced increase in voltage as shown in Fig. 1. For NiMH cells this is very much smaller and can be difficult to detect. As a result it is necessary to detect both the terminal voltage and the cell temperature as this also rises when the cell is fully charged.

integrated circuits are available to control the charge and monitor the discharge of the batteries. To monitor the state of the battery, fuel gauge chips are used. These monitor the amount of current entering or leaving the cell and as a result they know how much charge is left. They also know the state of the battery in terms of its ageing, monitoring its capacity from one charge to the next. Often these chips are very complicated, sometimes containing a small microprocessor.

These chips are

becoming increas-

ingly important. Computers are a

very good example.

Both NiCad and

NiMH cells have a

rapid fall in voltage

once most of the

charge has been

used. This means it

is important to have

sufficient warning

to save any files

charge has gone

and the computer

ali

the

before



Fig. 1. Full charge characteristic of NiCad and NiMH cells.

### Li-ion Batteries

Another new technology is beginning to enter the market. Termed the lithium ion or Li-ion battery this has an even greater charge density than the NiMH cell, although it has not been developed as far. The cells are made from a carbon anode which is doped with lithium ions and an electrolyte of ethylene carbonate.

The characteristics of the lithium ion cell are very different to those of the NiCad and NIMH cells. The output voltage is in the region of three or four volts dependent upon the exact cell chemistry and the state of charge. It is also found that the battery voltage falls during discharge (see Fig. 2). Again this differs from the NiCad and NiMH ones where the output voltage remains almost constant until most of the charge is exhausted.

Charging these batteries is very critical. If they are overcharged then the lithium separates within the cell and this can be very dangerous in view of the flammable nature of lithium. Cells which have been overcharged have been known to burst into flame. Manufacture also has to be undertaken with care as one factory has already burned down! Nevertheless if the proper precautions are taken they should be quite safe.

### **Intelligent Batteries**

Battery technology does not stop with the chemistry in the cells. A variety of ceases operation. Many of the new portable computers have a small indication on the screen showing the amount of charge remaining, and this allows the user to tailor any operation to the amount of time left in the battery.

Charging is equally important. To ensure that the equipment operates for as long as possible between charges it is necessary to ensure that it is fully charged. However, it is also necessary not to let the battery become over charged otherwise the amount of charge which the battery can hold will be reduced and its life shortened.

This function is normally performed by a special charger chip which monitors the battery and looks for signs that full charge has been reached.



Fig. 2. Discharge curve of a Li-ion cell.



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# Constructional Project 10MHz FUNCTION GENERATOR ANDY FLIND

The new MAXO38 function generator chip can enhance the test gear facilities in your workshop.

OGETHER with the multimeter and the oscilloscope, a function generator is one of the most useful pieces of equipment an electronics enthusiast can possess. It generates signals over a wide range of frequencies, and gets its name from the fact that it can also provide various output waveforms. Usually these are triangular waves and square waves in addition to the basic sinewaves, and users soon discover the value of these for testing different types of circuit.

Square waves, for example, are useful when checking for overshoot and ringing, whilst a triangular waveform is handy when looking for amplifier cross-over distortion. Sinewaves are useful when checking for harmonic distortion. Often the output can have a variable d.c. offset voltage added to the a.c. signal, shifting its relative level higher or lower to suit different circumstances.

### **BASIC DESIGNS**

There are two basic approaches to function generator design. One is to construct from scratch using discrete components and i.c.s. The circuit usually works by supplying a capacitor with a constant current, using comparators to switch between charging and discharging at pre-determined voltages.

A square wave signal is then available from the comparators and a triangular wave from the capacitor, whilst the sinewave is created by processing the triangular wave with a "shaping" network.

Most commercial instruments are designed in this way and usually have maximum output frequencies of about 2MHz. Their circuits are generally very complex with many preset internal adjustments, the setting up of which requires sophisticated test equipment not normally possessed by home constructors. This explains why designs for such instruments rarely appear in the electronics hobby press. The other way to build one of these instruments is to use a special waveform generator i.c. with the current sources, threshold switching and sinewave shaping circuits all built-in. Until recently, the only readily available i.c. of this nature was the type 8038, made by various manufacturers and having different prefix letters, such as ICL8038, AMZ8038, XR8038, Z8038, for example.

The claimed maximum frequency can vary, depending on the manufacturer, from 300kHz right up to 1MHz, but in practice the 8038 is usually struggling at 200kHz. If reasonably "clean" square and triangular waveforms are desired, it is wise to regard 100kHz as the upper limit. Most home constructors, therefore, have been limited to building function generators working only to these maximum frequencies, which restricts their usefulness.

### MAX038 DEVICE

This situation has now changed. The new MAX038 i.c. from Maxim offers all three waveforms, is much easier to use than the 8038, and the claimed maximum frequency is in excess of 20MHz! A review of the MAX038 was published in *EPE* September '96.

At 10MHz the output waveforms are excellent, so at long last it is possible for the amateur enthusiast to build instruments capable of this frequency at reasonable cost. The i.c. is capable of much more than basic waveform generation. The output duty-cycle can be varied, it may be frequency-modulated, and it is even possible to phase-lock it to an external signal.

However, the intention with the present design is to provide a comparatively lowcost and simple instrument having just the three basic waveforms and a d.c. offset facility. A minimum of equipment is needed for setting up as there is only one internal preset adjustment to be made.



### A PRACTICAL DESIGN

The project consists of two parts, the function generator itself and a separate regulated power supply. The circuit diagram for the 10MHz Function Generator is shown in Fig. 1, where the heart of the design is the MAX038 chip IC1. This is supplied in a 20-pin d.i.l. (dual-in-line) package but many of the control inputs are not used in this design and, therefore, are simply grounded.

Output frequency is variable over each of six ranges by controlling the current flowing into pin 10. This is supplied from Frequency potentiometer VR1 through resistor R2, with the minimum value set by resistor R1 to give a sweep range ratio of slightly more than 10:1.

The six frequency ranges are set by the values of external capacitors (C1 to C10) which are selected by the Range switch S1 for connection to pin 5. The lowest range is 10Hz to 100Hz and requires a capacitor value of 4.7 microfarads. This is not readily available as a single component with a reasonable tolerance factor, so four 1 $\mu$ F polyester layer capacitors are connected in parallel together with one of 680nF to make up the value.

Theoretically, the error is less than 0.5 per cent so, as these are five per cent tolerance capacitors, this is acceptable. The remaining ranges are set with decade multiples of 4.7, with the exception of the highest range of 1MHz to 10MHz, where a small trimmer capacitor (VC1) is used in parallel with a 22pF fixed capacitor to allow compensation to be made for stray capacitance, probably of several picofarads.

Decade multiples of 4.7 are used in preference to the more common value of 2.2 as this helps to reduce the effects of stray capacitance. A higher control current is required as a result, but it remains well within the i.c. specifications.

### WAVEFORMS

Readers with experience of the type 8038 device will recall that all three waveforms (square, triangle and sine) were available simultaneously but at different amplitude levels. Furthermore, the square wave was supplied from an open-collector output requiring a pull-up resistor which led to the inevitable trade-off between speed and power dissipation.

A completely different approach is used in the MAX038. It has only one output, from pin 19, the waveform being selected internally by the logic levels applied to two control inputs, pins 3 and 4. In this circuit these are provided with pull-down resistors R3 and R4 and the Waveform selection switch S2 takes them high as appropriate.

When both pins 3 and 4 are low, the output is a square wave. If only pin 4 is high, the triangle wave is output. When pin 3 is high, the output is a sinewave, regardless of the state of pin 4.

Output signal amplitude is always 2V peak-to-peak and it is delivered from a very low impedance, which greatly simplifies the following circuitry.

A separate synchronisation (sync) output of normal logic level (nominally 0V to +5V, but actually slightly lower) is available from pin 14, and in this design it is



Fig. 1. Main circuit diagram for the 10MHz Function Generator.



Fig. 2. Circuit diagram for the power supply.

taken to socket SK1 through resistor R7. It can be used to drive external logic, a frequency meter, or for any other suitable purpose chosen by the user.

### POWER NEEDS

Power for the circuit around IC1 is  $\pm 5V$ , which is supplied to pins 17 and 20 respectively. There is a separate positive supply connection to pin 16 for the internal comparator that drives the sync output. This is supplied through resistor R5.

All the supply connections have local decoupling consisting of  $1\mu$ F tantalum bead capacitors in parallel with 1nF ceramics, in accordance with the manufacturer's data sheet. Maxim's suggested alternative is to use  $1\mu$ F ceramic capacitors, but these are too large and expensive for this design.

### OUTPUT STAGE

The maximum output voltage is boosted from 2V to 10V peak-to-peak by IC3. This is an EL2160 op.amp, a current feedback type having a unity gain bandwidth of 180MHz. The signal level is controlled by potentiometer VR3, which is a logarithmic type, chosen to give greater control over the lower part of the output amplitude range.

IC3 is used in the non-inverting configuration, and a d.c. offset is added to the output by adjusting the voltage of the point to which the resistors R11 and R12 are connected. This point must have a low impedance so it is supplied from the output of IC2, which is a unity gain follower for the Offset control potentiometer VR2, with comprehensive decoupling added by capacitors C22 to C25. Switch S3 is used to disable the offset feature when it is not required.

The circuit around IC2 and IC3 requires a power supply of  $\pm 15V$ .

### POWER SUPPLY UNIT

Full power supply details are shown in Fig. 2, where it will be seen that it is a straightforward design using standard regulator i.c.s. To simplify layout and construction of the main printed circuit board, the power supply is constructed on a separate board.

Power is taken from the 18V-0-18V

centre-tapped output of transformer T1 and rectified by diodes D1 to D4 to give both positive and negative supplies. These are then regulated to  $\pm 15V$  and  $\pm 15V$  by IC4 and IC5 respectively, and decoupled by capacitors C34 to C37. The  $\pm 15V$ voltages are further reduced to  $\pm 5V$  and  $\pm 5V$  by IC6 and IC7, with decoupling by capacitors C38 to C41.

The current drawn by the MAX038 is around 50mA from each 5V supply. Whilst this is within the capabilities of the 100mA type of regulator, it would be difficult to cope with the heat dissipation from their packages so 1A types are used instead. These have mounting lugs to which heatsinks can easily be fitted.



Fig. 3. Details of the component layout and full-size underside copper foil master track pattern for the power supply printed circuit board.

### CONSTRUCTION

Details of the two printed circuit boards (p.c.b.s) for this project are shown in Fig. 3 to Fig. 5. The boards are available from the *EPE PCB Service*, codes 118 and 119, Main Board and power supply (PSU) respectively.

Construction of this project should start with the power supply as this is needed for testing the main p.c.b. assembly. Regulators IC4 to IC7 are first secured with their heatsinks to the board with short M3.5 screws, with a dab of heatsink compound applied to each to aid heat dissipation, and the remaining components are then fitted in ascending size order.

For maximum ease of construction, this project has been designed to fit into a readily available plastic case with dimensions of 205mm  $\times$  140mm  $\times$  110mm which has two sets of internal slots for holding p.c.b.s or chassis plates.

The transformer and power supply board are mounted on an aluminium plate cut to fit into a pair of these slots, as shown in the final photograph. This plate is cut to the same size as the front and rear panels supplied with the case, but the internal slots need extending slightly at top and bottom to accommodate it. A few moments with a sharp knife will suffice.

The transformer and p.c.b. are fitted to the front-facing side, with short plastic spacers keeping the board clear of the plate. Note that the mounting tabs of the regulator i.c.s, and hence their heatsinks, are internally connected to their outputs so they should not touch any surrounding metalwork. The board is mounted in a vertical position with capacitors C30 and C31 at the bottom to assist with thermal dissipation.

A terminal block on the other side of the plate allows easy connection to the mains power lead and a hole fitted with a grommet allows wiring to pass through safely. The plate is earthed via a tag secured by one of the transformer mounting screws.

### TRANSFORMER NOTE

A note about transformers is appropriate here. Ideally, the input voltage to the 15V regulators IC4 and IC5 with a normal load should be about 20V to minimise heat dissipation. The voltage obtained from a rectified transformer output is usually closer to the peak value of the output than the stated value, which is given as an r.m.s. (root-mean-square) value, and on load it usually drops a bit.

Transformer outputs often deviate quite a bit from their stated values too. With this project a 20V-0-20V 6VA transformer gave around 29V on load which was a little high but tolerable. Based on this, a 15V-0-15V transformer should have been about right, but a 250mA type actually gave only 18V.

An 18V-0-18V 6VA transformer was then tried; this produced about 30V without load, but when loaded this fell to about 27V. This was an improvement on the 20V-0-20V unit so it was selected for the project. It has two separate output windings, connected together to make a centre tap as shown in Fig. 2. and Fig. 7.



Fig. 4. Details of the component layout for the main printed circuit board.

Testing of the power supply simply involves powering up the transformer and checking that the four output voltages are present and correct.

### MAIN P.C.B. PREPARATION

With the power supply complete, construction of the main p.c.b. can be commenced, positioning the components as shown in Fig. 4. For simplicity and also to minimise stray capacitance around highfrequency parts of the circuit, some of the controls are fitted directly to the p.c.b. with their shafts projecting through holes drilled in the front panel.

To ensure alignment of the holes and shafts, the p.c.b. can be used as a template for marking their positions. It should be placed behind the front panel, with the



Fig. 5. Full-size underside copper foil master track pattern for the main printed circuit board.

copper side facing away from it and the switch S1 and S2 positions on the left. The bottom edges of the p.c.b. and panel should be aligned and secured with adhesive tape whilst the centres for panel drilling are marked out through the p.c.b.

On the p.c.b. the small pads at the centres of the S1 and S2 positions mark their centres, whilst the slightly oversize pad between capacitors C7 and C9 marks the centre for socket SK1. Small holes in the ground plane also indicate the

positions of SK2, S3, S4 and D5. One of these holes can be enlarged later and fitted with a grommet to take the wiring to the front panel mounted components. The use of a small pilot drill is recommended to maintain accuracy when drilling the holes.

Following this operation, the p.c.b. can be assembled and tested. Assuming that you are using a p.c.b. assembly frame, the two link wires and the resistors and capacitors should be fitted first, in order of size. Care should be taken with the tantalum bead capacitors as the polarity markings on these are sometimes difficult to read.

To ensure good performance the author chose not to use sockets for the i.c.s, however, readers might wish to use them to protect the i.c.s from heat damage which might otherwise occur during soldering. If you use sockets make sure they are high quality ones since low cost ones may impair performance at high frequency.

Potentiometers and switches should be fitted next. The switches will probably have small "eyes" at the ends of their solder tags which should be cut off so that the tags can be pushed into the board from the component side and soldered.

Behind the nut and washer of each switch there should be a lugged washer for setting the number of positions available. On switch S1 this should be set to "6", on S2 to "3".

The potentiometers are fitted with their bodies on the copper (track) side, so it is best to solder three short lengths of bare wire to their connection points on the board first. When they are secured in place, they can be wrapped around the potentiometer tags and soldered. Some makes of potentiometer may not have shafts long enough to project through the front panel as intended, so where the recommended case is to be used this should be checked first!

### TESTING

The i.c.s should be fitted and tested in sequence, starting with IC1, for which only the 0V, +5V and -5V supplies need be connected. The output from pin 19 can be checked with an oscilloscope. The amplitude should be 2V peak-to-peak, and the three waveforms should be selectable with switch S2.

The frequency ranges should all operate correctly when selected by switch S1. If a frequency meter is available, set switch S1 to the "1kHz to 10kHz" range, and then adjust potentiometer VR1 to set the output frequency to 10kHz. Leaving VR1 at this setting, now check how well the corresponding points in the other ranges match up.

In the unlikely event of there being any serious discrepancies, these can then be investigated and rectified, perhaps by substituting other capacitors. This probably will not be necessary, though, as despite the use of five per cent components, the ranges matched up very well in the prototype.

Still with VR1 at the same setting, trimmer VC1 should be used to adjust the output in the top range to 10MHz. If a frequency meter is not available, VC1 should be set to the mid-point, which will probably be close enough.

It is likely that IC1 will be found to run slightly warm to the touch; this is quite normal.

IC2 should be fitted next, and will require the +15V and -15V supplies to be connected for testing. Offset control VR2 should cause the output at IC2 pin 6 to vary by about 1.4V to either side of zero. If this seems satisfactory, IC3 can be fitted and its output checked with the oscilloscope.

The Offset On-Off switch S3 is not connected at this stage so VR2 should provide a variable d.c. offset range of just

Cl	MPONE	NTS		Table 1. Out	put Attenuation	Details
		110	Ratio	R1	R2	% erro
Resistors	820	See	1:2	100 + 100 parallel	100	0
R2, R3, R4	10k (3 off)	000	1:3	100	150 + 150 parallel	0
R6, R12	2k7 (2 off)	TALK	1:5	100 + 100 series	68+820 parallel	0.37
R8 R9 R10	2k2	raye	1:10	330 + 120 series	56+6k8 parallel	0.02
R11, R17	270Ω (2 off)		1:20	390 + 560 series	56+820 parallel	0.38
R14 All 0.6W/ 1% motol fil	1k		1:30	1k5+47k parallel	56+680 parallel	0.2
Potentiometers			1:50	2k7 + 27k parallel	3+18 series	0.22
VR1, VR2 VR3	1k rotary carboi 1k rotary carboi	n lin. (2 off) n log.	1:100	6k8 + 18k parallel	47 + 3·3 series	0.11
C4 C5 C6 C7 to C10 C11, C19, C20, C2 C33, C36, C37, C C12, C13, C15, C1 C14, C16, C17, C2 C22, C23 C30, C31 C34, C35 C38, C39 VC1 Semiconductors D1 to D4 D5	1, C25, C32, 240, C41 8, C24, C27, C28 6, C29	<ul> <li>47n polyester layer</li> <li>47n polyester layer</li> <li>470n polyester layer</li> <li>680n polyester layer</li> <li>1µ polyester layer,</li> <li>100n ceramic disc (7</li> <li>1µ tantalum bead, 1</li> <li>100µ elect. radial,</li> <li>100µ elect. radial,</li> <li>100µ elect. radial, 1</li> <li>2p to 22p trimmer, s</li> <li>1N4003 1A rectifier</li> </ul>	, 5% er, 5% er, 5% 5% (4 off) (11 off) off) 35V (5 off) , 16V (2 off) , 35V (2 off) 35V (2 off) 10V (2 off) sub-min		Fig. 6. Output diagram. over $\pm$ 5V. Sharp noticed an appar values of R6 an calculations might cal $\pm$ 5V shift. Th	Pre 2 ut atter preyed n rent dis tagges is differ
D5 IC1 IC2 IC3 IC4 IC5 IC5 IC6 IC7 <b>Miscellaneous</b> S1, S2 S3 S4		red I.e.d. and moun MAX038CPP high-f generator TL071CN f.e.t. op.a EL2160CN current 7815 15V 1A regulat 7915 – 15V 1A regulat 7905 – 5V 1A regulat 7905 – 5V 1A regulat 2-pole 6-way rotary d.p.d.t. min. toggle	iting clip frequency wave amp feedback op-ar ator ulator tor lator switch (2 off)	eform mp	compensate for i IC3 through R11 the d.c. offset ran rected by adjustin resistors. Potentiometer ' a.c. signal level of tween 0V and 10V The optional att and Table 1 are dis	vR3 sh utput fro peak-to scussed

S1. 9	52
S3	
S4	
SK1	SK2
T1	0.12

50-ohm BNC chassis socket (2 off) 18V-0-18V 6VA transformer (see text)

Printed circuit board (2 off), available from the *EPE PCB Service*, codes 118 and 119; plastic case, 205mm x 140mm x 110mm; knob (5 off); heatsink, vaned, 19°C/W, for plastic packaged i.c.s (5 off) (see text); cable grommet (2 off); aluminium sheet (see text); 3-way terminal block, mains voltage rated; cable; connecting wire, solder, etc.

### pprox Cost uidance Only





% error

Full Scale

5V

3.3V

2V

1V

500mV

333mV

200mV

Fig. 6. Output attenuator circuit diagram.

over  $\pm 5V$ . Sharp-eyed readers may have noticed an apparent discrepancy in the values of R6 and R8 from those that calculations might suggest for a symmetrical  $\pm 5V$  shift. This difference is needed to compensate for input current drawn by IC3 through R11 and R12. Any errors in the d.c. offset range obtained can be corrected by adjusting the value of these two resistors.

Potentiometer VR3 should control the a.c. signal level output from IC3 pin 6 between OV and 10V peak-to-peak.

The optional attenuator shown in Fig. 6 and Table 1 are discussed later.

### OUTPUT LINEARITY

The output of the prototype was checked with a 40MHz oscilloscope. The sinewave maintained an excellent waveform to beyond 10MHz with hardly any perceptible drop in amplitude with rising frequency. The triangle wave gave similar performance, with slight rounding of the points observed as the maximum was approached.

Some ringing was noted with the square wave above IMHz, though a surprisingly good waveform was maintained to beyond 5MHz, which is going some for a square wave! Above this frequency, rise and fall slopes were a bit more visible, with small "dips" in the flat portions as maximum was reached.

It is likely that most of the imperfections seen were due mainly to the leads, probes and other limitations of the scope used, rather than to distortion actually present in the output.

### OUTPUT LOADING

IC3 dissipates heat when driving an output load. Consequently, to avoid damage, it should be fitted with a small heatsink. With the prototype, a piece cut from a heatsink similar to those used for the voltage regulators was glued to IC3 with a dab of resin adhesive, as seen in the photograph of this board.



Fig. 7. Interconnecting details for the printed circuit boards.

CALIBRATION

when using the instrument. The output of IC3 is internally limited to about 80mA, so the worst case would be a short-circuited output with a 5V offset applied. In this condition heat dissipation within the i.c. could be just under one watt. Obviously an 8-pin d.i.l. package will not stand this for long. Even though the output impedance is further limited to 50 ohms by the parallel resistors R15 and R16, the first rule is to avoid this condition!

Output loading should be kept in mind

However, an instrument such as this will not normally be used for driving heavy loads with large voltages, so it should not be a problem. A more typical case might be driving a 50 ohm load with a 3V peak-to-peak signal, where the dissipation is only about 160mW. With the heatsink it can sustain this indefinitely.

### COMPLETION

Final assembly consists of fitting sockets SK1 and SK2, switches S3 and S4, and the l.e.d. D5 plus its resistor R17 to the panel and connecting them as shown in Fig. 7. This resistor should have its leads insulated with some heat-shrink film or insulating tape. Screened leads should be used for the sockets, keeping them as short as possible.

The front panel and p.c.b. have to be slotted into position together, so it is preferable to first make the connections between them, fit leads for the remaining connections, and then place them in the case.

Calibration of the Frequency control VR1 is best carried out with the help of a frequency meter, the author's Analogue Frequency Meler project in EPE February '96 being well suited to this task.

One of the middle ranges, perhaps the 1kHz to 10kHz range, can be used, the

control positions being marked "1" to "10". All the ranges on the prototype actually reached the "11" point, so this was also marked. The Offset control can be calibrated with a d.c. voltmeter. The output Level control can be calibrated with an oscilloscope, or a DVM (digital voltmeter) set to an a.c. range can be used



if a low frequency sinewave is selected; about 70Hz would be suitable.

Note that a DVM will show the level in volts r.m.s. whereas a function generator output is usually calibrated in volts peakto-peak, so the reading on the meter should be 0.354 times the value to be marked on the control.

For instance, to calibrate the point for "2", the level should be adjusted for a DVM reading of 0.708V. The logarithmic potentiometer used for VR3 in the prototype gives 1.5V at just over centre scale, 2V at about 2.0 o'clock and 5V at about 3.0 o'clock, giving some idea of the low-end range expansion to be expected.

There will undoubtedly be occasions when a lower range of output levels will be needed. This is not provided in the instrument itself as it might cause degradation of the signal at high frequencies. In many cases a simple external resistive attenuator as shown in Fig. 6 can be used.

Table 1 shows component values and arrangements for various levels of attenuation, using resistors from the ordinary E12 range. These have been selected for use on the assumption that this design has an output impedance of 50 ohms, and that they will be driving an input impedance of 50 ohms. This means that stages can be connected in series, e.g. two 1:10 stages will give 1:100 for a 100mV range, three will give 10mV and so on.

Be aware that the 1:2 and 1:5 stages may cause excessive dissipation in IC3, especially if used with a large output d.c. offset so, as this will also be attenuated anyway, it is better to keep it switched out when using attenuation.





### **10MHz Function Generator**

The Maxim MAX038CCP waveform generator chip which forms the heart of the 10MHz Function Generator project can be obtained from Electromail (#01536 204555) code 810-396, or Maplin (#01702 554161) code DT25. We understand, Maxim will also supply direct against credit card orders (#Tel: 01734 303388).

To date, the only source we have found for the current feedback op.amp type EL2160CN (Elantek) has been Electromail, see above. Quote code 177-5424 (the four digit bit is correct!).

The 6VA twin 18V secondary mains transformer used in the final model also came from the above company, code 804-919. The 20V version mentioned in the article is a Maplin WB16S. This can be used, but costs about twice as much and will warm-up the p.s.u. chips a bit more! The case was purchased from Maplin, Verobox 203, code LL07H. Don't forget, if you elect to use i.c. sockets they must be high quality low-profile types.

### Vehicle Alert

Two most important points to remember when building the Vehicle Alert are: the unit has been designed for continuous operation from the mains supply - so take extreme care; and the use of a "fully isolated" jack socket for connecting the remote sensor to the main unit. Obviously, the main unit must therefore be situated in a dry indoor location close to a mains supply socket. Use double-insulated cable for all external interconnections.

A 3.5mm plastic-bodied chassis mounting jack socket should be widely available, but if difficulties do arise order the CX93B socket and HF80B plug from Maplin. They also supplied the mains transformer, code WB01B.

''air'' The special pressure switch can be purchased from Electromail (#01536 204555), code 407-209. Finally, use nylon nuts and bolts for securing the pressure switch, circuit board and buzzer in position

### Direct Conversion Topband and 80m Receiver

Several items called-up for the Direct Conversion Topband and 80m Receiver are "special" components and may not be available from your favourite component advertiser. The 10-turn "tuning" potentiometer, used in the model, is of Spectrol (534 series) manufacture and, for the value specified by the author, appears to be only listed by Farnell (#0113 263 6311), code 351-829. They are also the only supplier of the larger size

'counting" drive mechanism, all-be-it a 15-turn type, code 146-835. The 10-turn pot. will govern the drive "count".

The varicap diodes and Toko inductors were all purchased from Cirkit (01992 448899). For the inductors type KANK3333R quote stock code 35-33330 and 35-33340 for KANK3334R(L3). For the KV1235 "triple" varicap diode quote 12-12355.

### Video Fade-to-White

All components required to put together the Video Fade-to-White project should be readily available from most of our component adver-tisers. A low power version of the 555 timer, such as the TS555CN, is recommended for the Fader to avoid any possible power supply problems and also has a faster response.

For details of all this month's p.c.b.s, see page 803.

### Component Analyser

Page 590, Fig. 1 and "Comp. List". Resistor R2 should ideally be 100k not 47k. Fig. 2, Blue probe lead should connect to IC7c pin 9 August 1996 instead of 3. The p.c.b. is correct.

**TAKE NOTE** 

Simple Exposure Timer

Sepember 1996 To ensure safety, there should be NO touchable metal parts on the outside of the case. Also you must use double-insulated calbe for all external leads.



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Analogue ICs	Positive 2Amp T0220	74LS290 0.47	4000 Series	BC237B 0.1	14	Thyristors	FLASH TUBES	Surface Mounte	d Transistors
CGY40 24.42 CGY50 4.21	78S06 +5v 0.78 78S09 +9v 0.97	74LS293 0.31 74LS295 0.55	4000 0.15	BC300 0.3	.14	2N5052 0.27	By Heimann	BC807/25 0.13	BCX71K 0.18
HKZ101 10.04	78s10 + 10v 0.97	74LS298 0.21	4002 0.15	BC301 0.3	30	BR103 0.38	AGA0017 2.82	BC818/40 0.15	BFP180 0.92
TL071CP 0.26	78S12 +12V 0.78 78S24 +24V 0.97	74LS366 0.18 74LS367 0.18	4006 0.31	BC328 0.1	14	BR303 1.23 C106D1 0.55	AU0023 12.75 BU90641 4.08	BC8468 0.15	BFP181 0.87
TL074CN 0.36	Positive Variable	74LS368 0.18	4008 0.31	BC337 0.1	14	TIC106D 0.47	BUB0861 4.55	BC8668 0.15	BFP183 0.87 BFP193 C.87
TBA120S 0.84	723C14 14DIL 0.35 LM317T 0.45	74LS373 0.32 74LS374 0.32	4009 0.21	BC516 01	14	TIC106M 0.65 TIC126D 0.65	DU7670 6.74	BC857B 0.15	BFP280 1.14
TBA1201 0.99	LM317K 1.58	74LS375 0.28	4011 0.15	BC517 0.1	14	Z0102NA 0.55	TRIGGER	BCV46 0.24 BCV47 0.24	BFR35AP 0.81
UAA170 1.77	LM338K 5.50	74LS390 0.24 74LS393 0.21	4012 0.15	BC546B 0.1 BC547B 0.1	.11	Triacs	TRANSFORMERS	BCW80D 0.17	BFR92P 0.72
TBB200 4.36	Negative 100maT092	74LS541 0.35	4014 0.31	BC548B 0.1	.11	BTA166008 1.28	DCB mounting:	BCW61D 0.17 BCW86G 0.17	BFR181 0.69 BFR183 0.60
TBB206G,SMD 5.19	79L05-5v 0.26	74LS670 0.68	4015 0.34	BC549C 0.1 BC550C 0.1	.11	TIC206D 0.57	ZS1052 1.36	BCW68G 0.17	BFR193 0.68
L293E 2.40 L297 3.75	79L15 -15v 0.26	74HC00 0.21	4018 0.20	BC556B 0.1	.11	TIC225D 0.78	Flying leads: 751050/01 1.48	BCX41 0.26 BCX42 0.26	BFR280 0.76 BFT92 0.84
LM301AN 0.27	79L24 -24v 0.50	74HC02 0.21	4018 0.31	BC557B 0.1 BC558C 0.1	.11	TIC246D 1.10	231002/11 1.40	BCX70K 0.16	BFT93 0.76
TCA305A 2.81 DG308 2.25	7905 -5v 0.26	74HC03 0.21 74HC04 0.21	4019 0.25	BC559C 0.	.11	OPTO D	EVICES	Other SMD prode	ucts available:
LM306N 0.65	7906 -8v 0.32	74HC08 0.21	4022 0.31	BC560C 0.1	.11	SMD LEDs	and min @ 10mA 0.25		
LM311N 0.30	7908-6V 0.32 7912-12v 0.26	74HC10 0.21 74HC11 0.21	4023 0.15	BC640 0.2	23	LYS260 YELLOW 0.4	Imcd min @ 10mA 0.25	Ceramic & tantak RF cho	um capacitors kas
LM336Z 1.00	7915 -15v 0.32	74HC14 0.24	4025 0.15	BC877 0.2	.27	LGS260 GREEN 0.4	Imcd min  10mA 0.26	Ferrit	
LM339N 0.31	7918 -16V 0.32 7820 -20V 0.32	74HC20 0.22 72HC21 0.22	4026 0.42	BC880 0.2	.23	ELOS SIMINI OND. RL3 RED	0.09	Hall-effect Integrated	devices circuits
TCA355B 2.73	7924 -24v 0.32	74HC27 0.22	4028 0.31	BCY59 0.:	.30	YL3 YELLOW	0.10	LEDs & Opto	-couplers
TCA355G,SMD 2.52	Negative Variable	74HC30 0.22 74HC32 0.22	4029 0.31	BCY71 0.1	.18	GL3 GREEN	0.10	resiste	ors and
LM380N 1.26	Digital ICs 74LS	74HC42 0.36	4035 0.47	BD131 0.4	.45	RL5 RED	0.09	variate	016
LM380N8 1.31	74LS00 0.13	74HC51 0.24 74HC73 0.28	4040 0.31	BD135 0.3	.45	GL5 GREEN	0.10	temperature	sensors
LM382N 2.52	74LS02 0.13	74HC74 0.25	4042 0.26	BD136 0.3	.25	LEDs 10mm dia.	0.10	NICAD Rec	hargeables
ZN414Z 1.20	74LS04 0.22	74HC75 0.32	4043 0.31	BD140 0.	.37	L813ID red 12	-40mcd 0.17	RX6U AA	0.5Ah 0.96
ZN416E 1.50 ZN423 1.16	74LS08 0.13 74LS08 0.13	74HC85 0.36	4046 0.33	BD201 0.	.40	L813SRD red 20 L813SRC red 20	0-350mcd 0.34 00-3000mcd 1.10	RX14U C	1.2Ah 2.06
ZN425E 4.75	74LS10 0.13	74HC93 0.39	4047 0.26	BD232 0.4 BD233 0.5	.40	BLUE LEDs	00.00001100	RX22 PP3	1.2An 2.15 0.11Ah 4.68
ZN427E 10.50 ZN428E 8.30	74LS11 0.13 74LS13 0.13	74HC107 0.24 74HC109 0.26	4050 0.24	BD237 0.	.35	L538T	1.45	QUICK CHARG	E
TCA440 1.95	74LS14 0.15	74HC112 0.25	4052 0.37	BD238 0.2 BD239C 0.2	.35	5V AND 12V LEDS	0.14	RX6P AA	0.65Ah 1.12
TL497 1.35	74LS20 0.13	74HC113 0.27 74HC123 0.36	4053 0.37	BD681 0.	.37	L53-GD5V 5v GREEN	0.14	RX20P D	1.6Ah 2.36
555 0.26	74LS22 0.13	74HC125 0.25	4066 0.18	BD682 0.	.35	L53-ID12V 12v RED		INDUSTRIAL	
NE566 0.45	74LS27 0.13	74HC126 0.36 74HC131 0.38	4070 0.15	BF187 0.	.50	L53-GD12V 12v GREE	EN 0.14	RX14S C RX14SP C	2,0Ah 2.98 2,2Ah 3,43
SLB0587 2.00	74LS32 0.13	74HC133 0.20	4072 0.21	BF173 0.	.50	LDRs		RX20SP D	5,1Ah 4.35
SAB0800 4.91	74LS37 0.13	74HC137 0.32 74HC138 0.24	4075 0.17	BF178 0.	,36	ORP12 12	mm dia. 0.79	CHARGERS FO	
741C8 8DIL 0.21	74LS40 0.13	74HC139 0.25	4077 0.18	BF420 0.	1.14	SIEN	IENS	CHARGER	6.43
747C14 14DIL 0.45	74LS42 0.21	74HC147 0.32	4081 0.21	BF421 0. BF457 0.	.18	Mo bavo	the largest	CX550PX4 4 CEL	
TCA785 3.74	74LS51 0.13	74HC151 0.30	4093 018	BFX29 0.	.42	vvenave	line largest	CX1200P UNIVER	ISAL QUICK
TBA800 0.84	74LS54 0.23	74HC153 0.32	4502 0.42	BFX84 0. BFX85 0.	.42	Range o	fSiemens	CHARGER	14.45
TBA810S 0.45 TBA820 0.84	74LS73 0.30 74LS74 0.15	74HC154 097 74HC157 0.31	4511 0.32	BFX87 0.	.37	Stock Ite	ms of any	PCB MOUNTIN	IG 0.14h 2.05
TBA820M 0.50	74LS75 017	74HC181 0.36	4514 0.78	BFX88 0 BFY50 0	36		atributor	MP3.6 3.6v	0.1Ah 3.26
TCA965B 3.67 TCA991 1.40	74LS76 0.30 74LS83 0.26	74HC164 0.36 74HC166 0.36	4518 0.31	BFY51 0	42	U.K DI	sinduloi	TELEPHONE	4.05
ZN1034E 2.45	74LS85 0.35	74HC174 0.32	4519 0.31	BFY52 0.	0.42	ELECTO	VITC	GP700AA 3 x AA GP280K3 3 x FLA	4.25 T 5.10
TAE1453G,SMD1.49	74LS86 0.17 74LS90 0.25	74HC175 0.33 74HC192 0.41	4520 0.31	BSS87 0.	.94	CAPACI	IORS	LITHIUM	
1488 0.25	74LS92 0.26	74HC193 0.41	4526 0.42	BSS89 0	.47	RADIAL		CR2016	1.27
1489 0.25	74LS93 0.31	74HC194 0.41	4528 0.36	BSS98 0.	0.40	RE4.7100 4.71	F 100v 0.07	CR2032	1.27
TDA2002 0.60	74LS107 0.21	74HC240 0.36	4541 0.31	BSS125 0.	0.97	RE10100 100	F 100v 0.08	Camcorder B	atteries
ULN2003 0.40	74LS109 0.18	74HC241 0.36	4543 0.47	BSS135 0. BSS192 1.	1.03	RE2235 22u	F 35v 0.07 By Ur	niross. Compatible with m	ost makes of Camera.
ULN2004 0.40 TDA2030 0.95	74LS112 0.23 74LS113 0.18	74HC245 0.36	4572 0.42	BTS412B 2	2.83	RE2263 220 RE4725 47u	F 25v 0.07		
TAE2453A 1.47	74LS122 0 26	74HC259 0.36	4586 0.36	BU208A 1. BU326A 1.	1.30	RE4763 47u	F 63v 0.10 VP22	0v 1.4Ah 14.37 VP	522 9.6v 1.6Ah 43.77
TAE2453G,SMU2.03 SDA2506/5 3.70	74LS123 0.26 74LS125 0.24	74HC273 0.38	2N697 0.38	BU407 1	1.00	RE10016 100	uF 25v 0.08 VP66	6 0v 1.7Ah 16.65 VP	520 12v 1.5Ah 43.77
SDA2516/5 1.53	74LS126 0.38	74HC279 0.36	2N930 0.42	BU426A 1. BU508A 1	1.28	RE10063 100	uF 63v 0.15 VP77	9 8 1.7 Ah 17.80 VP	30 12v 2.3Ah 29.00
CA3046 0.89 CA3080E 0.78	74LS132 0.18 74LS136 0.14	74HC280 0.36 74HC283 0.37	2N3053 0.26 2N3055 0.60	BUSOBAFI 1	1.45	RE22025 220 RE22063 220	UF 63V 0.14 VP 22	9.8v 1.2Ah 28.70	300 Cristiger 10.44
CA3130E 0.94	74LS138 0.26	74HC367 0.29	2N3702 0.14	BU508DFI 1	1.30	RE47010 470	uF 10v 0.13 VP96	32 9.8v 1.3Ah 24.15	
CA3140E 0.47 MC3340 2.20	74LS139 0.28 74LS145 0.47	74HC373 0.44	2N3703 0.14 2N3704 0.14	BU526 0	0.96	RE47025 470	WF 50v 0.29	VALVES	D TYPE
SG3524 1.00	74LS148 0.83	74HC390 0.42	2N3705 0.14	BU306 0 BUT11AF 1	J.96 1,30	RE47063 470	uF 63v 0.32	ECC81/12AT7 5.50	CONNECTORS
LM3900N 0.45 LM3909N 1.42	74LS151 0.28 74LS153 0.28	74HC540 0.48	2N3706 0.14 2N3710 0.18	BUW84 0	0.96	RE100010 100 RE100025 100	OuF 10V 0.22 IOuF 25V 0.22	ECC83/12AX7 5.50	DP98.9 pin 0.19
LM3914N 1.90	74LS154 0.63	74HC541 0.48	2N3711 0.14	BUZ11 1	1.10	RE100063 100	OuF 63v 0.53	ECF82 6.00	DP158 15 pin 0.26
LM3915N 1.25 SAB4209 4.04	74L5156 0.27 74LS157 0.28	74HC4002 0.22	2N3771 1.94 2N3772 1.94	BUZ11A 1	1.12	RE220016 220 RE220025 220	OuF 10V 0.37 IOuF 25V 0.38	EL:84/68Q5 4.50	Sockets
TLE4214 2.62	74LS158 0.28	74HC4015 0.56	2N3773 1.94	BUZ71A 1	1.23	RE470010 470	OuF 10v 0.32	ECL82 5.85	DS98 9 pin 0.20
RC4558P 0.40 TDA4601 1.73	74LS161 0.28 74LS163 0.28	74HC4017 0.45	2N3819 0.42 2N3820 0.73	BUZ73 1	1.58	HE4/0016 470	GE AXIAL	KT66 10.00	DS258 25 pin 0.26
TDA4601D 1.90	74LS164 0.28	74HC4020 0.52	2N3904 0.14	BUZ74 1 BUZ80 2	1 56	411385 14	385v 0.30	KT68 13.00	Hoods
TDA4805 1.86 TDA4700A 9.58	74LS165 0.46	74HC4022 0.42	2N3906 0.14 2N4036 0.73	BUZBOA 3	3.23	832.2350 2.2	uF 350v 0.36	EZ80 5.25 EZ81 3.75	DH9 9 wey 0.34 DH15 15 wev 0.43
TDA4718A 4.73	74LS169 0.36	74HC4040 0.54	214284 0.26	IRF520 0	0.77	5010350 100	IF 350v 0.74	GZ34 6.50	DH25 25 way 0.44
7106 2.35	74LS173 0.21	74HC4046A 1.35 74HC4049 0.32	2N4289 0.27	IRF540 1	1,66	5022350 22	F 350v 0.92	VALVE BASES	SCART
ICM7565 0.51	74LS175 0.28	74HC4050 0.32	BC106B 0.16	IRF630 1	1.15	41100350 470	2F350V 1.50 24F350V 1.86	B9A PCB 1.50	PS2480 plug 0.63
ICL7611 1.25	74LS191 0.31	74HC4051 0.54	BC108C 0.16	IRF820 0	0.79	AERIAL	SOLDERING	B9A CHASSIS 1.50	MRS871J line sockat
Begulatore	74LS194 0.31	74HC4053 0.54	BC109C 0.16	IRF822 0	0.70	AMPLIFIERS	IRONS	CHASSIS 1.95	0.98 T113F 1.5m Scart -
Positive 100ma TO92	74LS196 0.31	74HC4080 0.54	BC126 0.27	IRF840	1.83	12HG TWIN 10.24	ANCEP 15W 11.00	SOLDER	Scart lead 2.10
78L05 +5V 0.27	74LS221 0.31	74HC4075 0.2	BC161 0.33	MJE2955T 0	0.52	4WA 4 WAY 17.00	ANXSBP 25W 11.67	SR3A (ORYX) 9 50	POWER LEADS
76L08 +8v 0.27	74LS240 0.36	74HC4078 0.23	BC168B 0.12	MPS6534 0	0.44	1WPTVA	ANST4 STAND 3.50	LILO (ORBITEC)5.40	13A plug to IEC 6A
78L10+10v 0.27	74LS241 0.38	74HC4316 0.3	BC179B 0.22	MPSA12	0.14		OW TO OPP	FD	accket, 2 muite
78L12 + 12v 0.27 78L15 + 15v 0.27	74LS243 0.28	74HC4351 0.77	BC162 014	TIP31A	0.31	H H	OW TO OKL	<b>EK</b>	0//141_ 1.50
78L24 +24v 0.27	74LS245 0.28	74HC4353 0.7	BC183 0.14	TIP41A	0.36	Totalize your of	der / Add £1.00 p+;	Then V.A.T	SWITCHES
7805 +6v 0.26	74LS247 0.28	3 75HC4510 0 7	BC183L 0.14	TIP42A	0,36	Mail and telepho	one orders to Staines	please	TOGGLE
7806 +8v 0.27	74LS253 0.31	74HC4514 1.4	7 BC184L 0.14	TIP42C	0.63	Visitors always	welcome at the Me	nchester Shop or	3101 SPDT 0.39
7810 +10v 0.27	74LS256 0.30	74HC4515 1.4	7 BC212 0.14	TIP110	0.60	By prior arrange	ement st Staines w	arehouse.	3201 DPDT 0.50
7812 +12v 0.26	74LS257 0.3 74LS259 0.2	74HC4518 0.7 5 74HC4518 0.5	BC212L 0.14	TIP122	0.49				29AS SPST 1.17
7815 +15V 0.27 7818 +18v 0.27	74LS266 0.10	3 74HC4520 0.5	0 BC213L 0.14	TIP127	0.49	All Prices are a	xclusive of V.A.T ar	nd	2985 DPDT 1.38
7820 +20v 0.27	74LS273 0.3	74HC4538 0.5 74HC4543 0.5	BC214 0.14 D BC214L 0.14	TIP3055	0.72	may change with	hout prior notice. E&	OE CALL	centre-off 1.40
7624 +24v 0.27									

## A roundup of the latest Everyday News from the world of electronics **YOUTH SCORES AGAIN IN DURACELL AWARDS**

From Laser Plumb Bob to Vibration Data Logger, Sailcraft Speedo and Super-safety Domestic Irons, they're winners! – Hazel Cavendish

F WE had any need to be reminded that Britain's young are leading from the front in innovative technology, this year's prizewinners in the fourth annual Duracell Science and Technology Schools Competition – run in conjunction with the Association for Science Education – proves it beyond any doubt.

Entries came from schools all over England, Scotland, Wales and Northern Ireland. It is interesting that neither a London school nor any of the major public schools produced a finalist, with the state sector and small private schools in the provinces emerging strongly in science education.

Quite apart from the 16-year old overall winner's original and marketable invention (for which a patent has already been lodged) the competition is notable for introducing one of the youngest inventors in the country, an 11-year old Polish boy who is a finalist for the second year running.

Although only one girl is amongst the finalists this year, a North country science teacher remarks that her sex are featuring outstandingly in science classes, particularly when the subject is introduced in the nine to ten years age group in middle school.

Mike Amos, Duracell's Vice President of Human Resources for Europe, says "This year's entries continue to demonstrate the wealth of enthusiasm and creativity being fostered in our schools". Competition Judge Maggie Hannon, who is Senior Inspector, Science, for the Liverpool Education Authority, has commented on the improvement in quality this year of both the students' written work and the finish of the devices.

The Duracell competition is designed for 15 to 17 year olds, but is open to younger students, although they are judged by the same criteria as the older ones. Five first prize winners are selected – six this year because one invention was developed by a two-boy team – and as well as winning prizes for themselves and their schools, student's devices are in contention for the overall prize of an all expenses paid trip to the USA, awarded for outstanding creativity and innovation.

### **Bob Plumbs It!**

This year Robert Jordan, aged 16, a pupil at Woodlands High School in Gillingham, Kent, was the overall winner,



Robert Jordan (16) and his award winning Laser Plumb Bob.

receiving his prize from the Royal Society in London and winning £1,000 for his school technology department and £250 for himself with his battery-powered "Laser Plumb Bob". His trip to Massachusetts will include a visit to the famous Institute of Technology there – a thrill for anyone with a bent for technology.

Robert was working with his stepfather at a building site where workmen were erecting partition walls when he got the idea which inspired his award-winning device. He watched the workmen using a plumb bob and line to ensure that ceiling fixings were fitted directly above and perpendicular to predetermined markings on the floor of the building. He noticed that they were finding this a precarious, tedious and labour-intensive task, and went away to think of a way technology could be used to help.

A year later he had designed and made his Laser Plumb Bob at the school's Young Engineers' Club, with advice from his science teacher. His plumb bob sits on a tripod, using gravity to ensure it is precisely vertical. A gimbal, made from a large ball bearing with a pendulum holding the battery, is set on smaller roller bearings which compensate for any unevenness on the floor or surface. A laser diode with a low divergence beam points upwards from inside the ball bearing. When switched on, it shoots the laser at the ceiling, leaving a mark indicating the required position of the wall.

The Laser Plumb Bob will also have other uses, such as detecting the movement of a bridge. It will cost about  $\pounds 100$  to manufacture.

### **Vibration Logger**

Eleven-year-old Martin Rosinski, the son of a Polish scientist now working at Newcastle University, emerges as a finalist for the second time, having beaten children more than three years older than himself. He has produced the prototype of a "Shipment Vibration Data Logger" which can establish exactly when valuable equipment is damaged during transit.

His device monitors acceleration levels by using a microcontroller linked to an analogue-to-digital converter, which systematically records the output of a miniature accelerometer. The data on the shock or vibration levels that a package of fragile instruments receives during shipment is stored in the form of a histogram. An intelligent liquid crystal display provides a simple way of displaying the required information. "Martin is a highly gifted

"Martin is a highly gifted boy, and ideal scientist material," said David Elliott, his science teacher at Coates Endowed Middle School at Ponteland near Newcastle. "He is away ahead of his contemporaries, and very probing with his questions, with a mind always looking ahead. He is well beyond GCSE standard with this latest project. In fact, after winning this prize he is already working on ways to reduce the size of his device with an output to a computer."



With his Vibration Logger, Martin Rosinkski (11) beat children more than three years older than himself.

### **Sailboard Speedo**

A two-boy team from Monmouth School has won equal first prize for an interesting "Sailcraft Speedometer" which measures and displays the speed of a dinghy or – appropriately for our times – a sailboard. This should prove useful for competition use as sailboards have become a hot number among the young. Now skippers and sailboar-

Now skippers and sailboarders can improve their technique by getting the optimum performance from their craft. Air speed has proved not to be an accurate or entirely useful measurement when sailing, and using land speed for a water-based object is complicated and relatively expensive.

Matt Chandler and Will Johnson have based their device on measuring the water speed as it flows past the craft. An impeller is used to rotate a slotted disk through a photoelectric gate. This generates pulses which are counted and numerically output to a display.

### Modern Iron Age

The two other finalists have based their inventions on the domestic iron, showing the intelligent interest young scientists can bring to solving everyday household problems.

766

Simon Lee Todd of Bolton School was so upset when his mother burnt a hole while ironing his favourite pair of trousers that he set out to perfect an "Iron Safety Device". Countless housewives will have cause to thank him if it reaches the market.

Simple as so many of the best inventions are, his electric iron has a circuit which triggers an alarm when the iron is horizontal and *does not* move for more than five seconds.

When the iron is placed in a horizontal position a mercury tilt switch is closed, which activates a timing device.

The time is constantly reset by a vibration detector which pulses open and shut when the iron is in motion. If the iron stops moving and the mercury switch is still closed, the fivesecond countdown will end and the alarm will be triggered. The iron is easily reset by merely placing it in the vertical position. Lucy Ann Eyles of Matravers School, Westbury, demonstrated a pragmatic concern for the problem of inadvertently putting away a dangerously hot iron at the conclusion of ironing, or touching it when it is still hot and sustaining a painful burn.

Her solution is an iron stand made from heat-proof material which not only covers the whole of the metal plate and stops the ironer from

(F3) communications satellite

by three crew members of the Space Shuttle Endeavour on

mission STS-49. The astronauts

from left to right are: Richard J.

Hieb. Thomas D. Akers and

*Intelsat VI* was launched on 14 March 1990 by a Titan

rocket but due to a malfunc-

tion it was not raised to a geosynchronous orbit. The main

goal of the mission was to

capture the satellite and bring

Pierre J. Thuot.

burning his or her hands, but also utilises a sensor in the form of a bimetallic strip which switches on a light emitting diode when the temperature hits 40°C, and thus warns the operator not to touch the iron until the light goes out.

It is so simple and yet basic that one wonders why no manufacturer has thought of it before – perhaps because manufacturing design has been dominated by men up to now?

### HIGHER-TECH X-RAY SYSTEM The first London hospital implements revolutionary archiving X-ray techniques – by Hazel Cavendish

LOCKHEED Martin, the US giant most commonly associated with Defence developments of awe-inspiring complexity, would appear to be beating their swords into ploughshares – in a manner of speaking. One of the most exciting developments in hospital efficiency this century has been introduced at a cost of £8 million to the Hammersmith Hospital in West London, where the entire conventional X-ray set-up has been replaced by the American firm's electronic X-ray archiving and communication system.

The new picture archive with its high quality monitors cuts out the need for hundreds of thousands of X-ray films which the hospital produced, filed and handled each year, replacing them with 160 workstations in every department of the hospital, from wards and operating theatres to outpatient and casualty units.

Hammersmith is only the second hospital in Europe to adopt this electronic system; the other is the Danube Hospital in Vienna.

The Lockheed Martin Western Development Laboratories, which have long specialised in integrating complex information systems, have given the world the Vantage Picture Archiving and Communication system (PACS) as a digital and image management system for diagnostic examinations and powerful, high-speed communication network.

The core of Vantage PACS is the Information Storage Unit, an integrated central host computer and image storage system. In its smallest configuration it processes 150 requests for image transfers per minute, and at its most powerful, 600 per minute.

Described as a "breath-taking development" by Dr Nicola Strickland, consultant radiologist responsible for implementing the system, it will not only make doctors' work immeasurably quicker and simpler, but will increase efficiency throughout any hospital adopting it, and greatly benefit the patient – particularly those in intensive care.

### Connect National Consumer Electronics Show A VISION OF TOMORROW AT CONNECT

THERE are 20 pairs of tickets to be given away *Free* to Cinem *EPE* readers for *Connect* 96 at the National Consumer home

EPE readers for Connect 96 at the National Consumer Electronics Show taking place at Birmingham's NEC from 18-27 October 1996. Connect is proudly proclaimed by its organisers to

be "an entertainment experience transporting you into tomorrow's electronic world". It will feature a custombuilt TV studio, giving a unique insight into the world of television and a sneak preview into Central's new £15 million HQ in Birmingham.

The Connect Sound Stage will be a state of the art "UFO" structure and will be the focal point for the impressive entertainment line-up planned for the show, which includes top chart bands, DJs, light shows and special effects displays.

There will be interactive displays, a Hi-Fi and Home

Cinema Theatre. New Media Village, and the latest in home entertainment products which can be purchased at the exhibition in the Retail Village.

Connect, the Home PC Show, Autumn Ideal Home Show and the International Motor Show are all taking place simultaneously. Connect tickets cost £7 for adults and £5 for children and senior citizens, and include entry into the Autumn Ideal Home Show and Home PC Show. *BUT*, the first 20 callers to phone 0121 767 4114 will each get a pair of tickets *free* – as long as they also quote "Everyday Practical Electronics, reference CO9". (Don't phone us direct at EPE for these tickets – we haven't got them!)

This offer has been made available through the Home Interest Division, dmg Exhibition Group Ltd.

**OUR COVER PHOTO** THE dramatic photograph on our front cover shows the capture of the *Intelsal VI* is installed.

installed. For the first time in the Shuttle's history, three members participated in an Extravehicular Activity (EVA). Mission STS-49 (7-16 May 1992) was Endeavour's first flight.

Whilst Intelsat is not a television satellite, the photograph does set the scene for our Introduction to Satellite Television feature this month. Photo has been used by courtesy of NASA/Science Photo Library.

### MICROCHIP have introduced the PIC16C84A EEPROM-Simultaneously introduce the PIC16C83, which is a

MICROCHIP have introduced the PIC16C84A EEPROMbased microcontroller, an upgrade on the popular PIC16C84 used recently in several *EPE* projects. The new device features a greater endurance performance than the standard version – 10 million erase/write cycles compared to one million. The other parameters remain unchanged.





For more information, contact: Arizona Microchip Technology Ltd., Dept. EPE, Unit 6, The Courtyard, Meadowbank, Furlong Road, Bourne End, Bucks SL8 5AJ. Tel: 01628 851077.

### **New SMPSU Chips**

NATIONAL Semiconductor have expanded their Simple Switcherpower converter family with the introduction of two new 3A flyback power converters. Called the LM2585 and LM2586, the i.c.s are DC/DC converters which deliver high power in a small form factor and are designed for ease of use.

The new devices feature an increased operating frequency of 100kHz, allowing designers to specify smaller external magnetic components and capacitors, shrinking the overall p.c.b. area. Other advantages include: synchronisation of multiple devices; external turnoff; flyback, forward and step-up modes; availability in 3-3V, 5V and 12V versions.

They are also supported by "Switchers Made Simple" design software which provides complete design solutions, including schematics, component lists and vendor information.

For more information contact: National Semiconductor European Customer Support Centre on (0) 49 180 5327 832. National's World Wide Web site can be found at: http://www.national.com



### DIGITAL CAPACITANCE METER INTERFACE

A PC-based Transistor Tester was described in last month's *Interface* article, and this month we continue in a similar vein with a PC-based Digital Capacitance Meter.

Robert Penfold

The unit has four measuring ranges of zero to 2550pF, 25 $\cdot$ 5nF, 255nF, and 2 $\cdot$ 55 $\mu$ F. It is based on six inexpensive integrated circuits, and it interfaces to the host PC via one of its printer ports.

### **Counting On It**

The block diagram of Fig.1 helps to explain the basic way in which the Digital Capacitance Meter Interface functions. It operates using a simple gate and counter system. A clock oscillator feeds into a nine-bit binary counter via a gate. The latter is controlled by a monostable.

The duration of the output pulse from the monostable is governed by the value of a resistor and a capacitor. The capacitor is the component "under test", and the pulse duration is proportional to the value of the test component.

Suppose that the clock frequency is one kilohertz (1kHz), and that the monostable produces an output pulse of one millisecond per nanofarad (ms/nF) of test capacitance. At the end of the pulse, the value stored in the counter would be equal to the value of the test component in nanofarads. For example, a 150n component would produce a pulse duration of 150ms (0.15 seconds), and with 1000 clock pulses per second this would result in 150 pulses being fed to the counter.

In practice, the monostable actually provides a pulse duration of under 100 nanoseconds per nanofarad. However, the clock frequency is made proportionately higher so that the correct relationship between capacitance and final counter value is still obtained.

The clock frequency is made adjustable so that it can be trimmed to compensate for any variations from one monostable to another, and the unit can be accurately calibrated against a close tolerance capacitor. The monostable has four switched timing resistors, and these give the unit its four measuring ranges.

### On Display

INTER FACE

The computer provides the display and most of the control logic. Each control cycle starts with a handshake output of the computer pulsing high to reset the counter to zero.

### **Interface Circuit**

The main circuit diagram for the Digital Capacitance Meter Interface is shown in Fig. 2. The circuit for the eight-bit input port and connections to the printer port are provided in Fig.3.

Taking Fig.2 first, the clock oscillator is a standard 555 astable (IC1). Its output frequency can be trimmed using pre-



Next, another handshake output pulses high in order to trigger the monostable. The computer then waits long enough for the pulse to end, and reads the contents of the counter via an eight-bit input port.

There is a slight snag in that the printer port does not actually have eight inputs. Four handshake inputs and a handshake output, plus some simple logic circuitry, are used to read the counter a nibble (four bits) at a time.

The counter is a nine-bit type, but the system only has eight-bit resolution. The ninth bit of the counter is used to provide an overflow warning if the test capacitance is too high for the range in use. If the maximum count of 255 is exceeded, bit nine goes high, and this is detected by a software routine via a handshake input of the printer port. set potentiometer VR1, and it is typically about 16kHz to 17kHz. IC2a and IC2b act as the signal gate, and they enable the clock signal to pass through to the counter (IC3, IC4) when the input signal to IC2a is "high".

The other two NOR gates in IC2 are used in a simple CMOS monostable. S1 is the range switch, and resistors R6 to R9 are the Range resistors. In order to obtain good accuracy on all ranges R6 to R9 should have a tolerance of one per cent.

The full scale value is 2.55n with R6 in circuit, running through to  $2.55\mu$  with R9 switched into circuit. The test component can be an electrolytic or other polarised type, but it *must* be connected with the *polarity* indicated in Fig.2.

It was possible to obtain a fifth range on the prototype interface using a timing resistance of about 1.2 kilohms (1k2). This



gives a full scale value of  $25.5\mu$ , but it cannot be guaranteed to work well on all units built to this design. The extra timing resistor *must be a preset* type so that it can be adjusted to give accurate results.

The counter circuit is comprised of two 4024BE seven-bit counters wired in series (IC3 and IC4). Only the first nine outputs are used, and the final five outputs of IC4 are left unconnected.

The eight least significant outputs drive the eight-bit input port, and the ninth bit drives a handshake input via an inverter based on transistor TR1. The inversion provided by TR1 is not actually of any significance, and its real purpose is to ensure that the CMOS output of IC4 can drive the TTL compatible input of the printer port.

### **Input Port**

The 8-bit Input Port (Fig.3) is basically the same as the one described in the *Interface* feature published in Feb '95 issue of *EPE*. The main difference is that IC5 has been changed from a 74LS244 to a 74HC244 octal buffer. This gives sufficient drive to operate the TTL compatible inputs of the printer port, but also gives CMOS compatible inputs that will interface to the counter circuit correctly.

The only other change is that a CMOS inverter (IC6) has been used in place of the 74LS TTL type of the original design. For a detailed explanation of how this port functions refer to the Feb '95 issue (see Back Issues page).

Five handshake inputs are available on the printer port, and bits three to six of the handshake address are used to provide the eight-bit input port. This leaves bit seven free to read the overflow output of the counter. One handshake output is used to control the eight-bit input port, leaving three unused, plus the eight data outputs of the port.

The suggested method of connection uses data output D0 to trigger the monostable, and D1 to reset the counter. Using two data outputs rather than handshake outputs avoids the possibility of inadvertently upsetting the operation of the input port when controlling the interface (or vice versa).



### Software

The program, Listing 1, is set to the appropriate range using keys "1" to "4" on the keyboard. To stop the program either press the "S" key or use the normal CONTROL-BREAK combination.

The program prints to the screen the range in use, and the capacitance value in the appropriate units (e.g. "1.57u" rather than simply "157"). Where appropriate, it also prints an "OVER-LOAD" warning on the screen.

The first few lines of the program simply set up the initial operating conditions, and start the program on Range 3. Variable "R" is the value by which read values are multiplied in order to give a reading in the appropriate units. String variable "B\$" is the letter displayed after the value, and is either "p", "n", or "u". Lines 130 to 160 detect if keys "1" to

Lines 130 to 160 detect it keys "1" to "4" have been pressed and, when appropriate, branch the program to one



# of four sub-routines. These make the necessary changes to the two variables, and change the range number displayed on the screen. Line 170 detects whether or not the "S" key has been pressed, and ends the program if it has.

The Reset and Trigger pulses are generated at lines 70 to 110. Line 180 and 210 simply provide a short delay which prevents the port being read before the count has been completed. With fast PCs it might be necessary to use a higher value at line 180 in order to obtain a long enough delay.

Lines 190 and 200 read bit nine of the counter, and branch the program to a subroutine if it is set high. The subroutine simply prints a overload warning on the screen.

A simple routine at lines 220 to 280 reads the port. The returned value is then multiplied by variable "R" and printed to the screen followed by B\$. Line 340 loops the program indefinitely so that a continuous stream of readings are taken and displayed.

Note that the addresses found in this listing are correct for printer port 1. If you use printer port 2, addresses &H378, &H379, and &H37A should be changed to &H278, &H279, and &H27A respectively.

To calibrate the system, switch it to Range 2 and connect a close tolerance 22n capacitor across sockets SK1 and SK2. Then simply adjust preset VR1 to produce the correct reading of "22.0n" on the screen.

### Improvements

There are six unused data outputs on the printer port, and this should permit the unit to be fully controlled from the computer. Four of the unused outputs could be used to control four small relays which could be use in place of Range switch S1.

The software would then be modified to select the correct range resistor when one of the range keys was operated. It should be possible to implement a system of auto-ranging, and there is certainly plenty of scope for experimentation here.

# Special Feature INTRODUCTION TO SATELLITE TELEVISION Mike Rutherford

The basic operation of current and proposed systems.

ELCOME to the world of satellite television. It has definitely come to stay! In a few years it has become firmly established across the world as a simple and reliable means of receiving television and radio broadcasts. It's simplicity, to the layman, is brought about by the incredibly sophisticated transmission and reception techniques to which have been applied mass-production techniques. The result is a well-priced product, but to reason that it is cheap because it is simple would be extreme folly.

It has all been made possible by the invention of the microchip which allows a lot of electronics to be cranimed into a small space and is repeatable in vast quantities.

Satellite broadcasting has very few disadvantages but it does not herald the end of terrestrial transmissions. The latter have the advantage that, because of the need for several transmission sites to enable coverage of the entire country, regional programmes can be put out easily. Also, in the event of a war, the enemy cannot disable a network of terrestrial stations as easily as he can knock out one satellite by jamming it or by actually destroying it.

But, for the aspiring broadcaster with his sights on a National or Pan-European service, the satellite is the answer!



Fig.1. The Clarke Orbit.

### GEOSTATIONARY

The suggestion that a satellite could be stationed in an orbit around the Earth above the equator that would be synchronous with the Earth's rotation (geostationary) was first made by Arthur C. Clarke in the article *Extraterrestrial Relays* in *Wireless World*, October 1945.

Once a satellite has flown clear of the drag imposed by the Earth's atmosphere, it attains a linear speed of about 6900 m.p.h.. If the satellite remains close to the earth it will complete one orbit in less time than it takes the Earth to make one rotation. The surface speed of the Earth is about 1,000 m.p.h., the circumference at the equator is 24,000 miles and it takes 24 hours to rotate once. The Earth's *angular* velocity is 15 degrees per hour.

The satellite must achieve an angular velocity also of 15 degrees per hour to appear stationary from Earth. As the approximate speed of the satellite is 6,900 m.p.h., the circumference of it's orbit must be  $6,900 \times 24 = 165,600$  miles. Expressed as a radius this becomes 26,356. Subtract the radius of the Earth (4,000 miles) and you get 22,356 which is about 56 miles out, but the figures are all very approximate. In fact the Clarke Orbit is 22,300 miles above the Earth's surface and lays directly over the equator, see Fig. 1. The

mathematics are fairly simple to understand, anyway!

We do not live on the equator! If we did we would perspire and our satellite dishes in some instances would face almost directly upwards. In our temperate climate at 53 degrees north we would get a view of the Clarke Orbit similar to the one shown in Fig. 2. Facing true south we would get an elevation of nearly 40 degrees, and this would curve downwards off to the east and west. The total orbit sweep it is practical to use from 53 degrees North is about 120 degrees of arc (Fig. 2). At the extremities reception is curtailed by trees and buildings – not on the horizon but those close-by. Satellite reception demands a clear view of the satellite by the dish.



Fig.2. View of Clarke Orbit from Earth – approximate UK position.

### UPLINK

Satellite TV programmes are sent up to the satellite from an earth station on a band of frequencies slightly above those used for the downward transmission into our homes. The uplink frequencies are in the 14GHz band. A powerful transmitter is used on the ground to ensure a clean signal is received by the satellite, 22,300 miles away (Fig. 3). One dish can send about eight channels or more to the satellite. though in theory a great many more could be accommodated. In practice, the number is kept down for other technical reasons associated with the combining of the outputs of several transmitters into one feedhorn on the dish.

The uplink signals are converted to the downlink frequencies by the equipment on board the satellite and each piece of equipment is known as a transponder. A transponder receives the incoming signal, converts its frequency to that used for the downlink and transmits it via the dish or horn antennas pointed back at Earth. The power output stage of the transponder is a travelling wave tube (TWT), a valve in fact, designed for producing power at microwave frequencies. TWTs have been


Fig.3. Arrangement of the uplink.

around since the Second World War. Because they are thermionic devices they have a limited life.

The dish or horn antennae used for transmitting the signals on the downlink back to Earth are shaped to give coverage of predetermined areas of the Earth's surface so that the strongest signals can be sent to where the "customers" are situated.



Everyday Practical Electronics, October 1996

### THE SATELLITE

Satellites are usually cylindrical (Fig. 4), though rectangular or spherical ones have been used and are in no way inferior. Power is derived from solar-cell panels which extend from the craft on stalks, and the outer shell of the satellite itself is sometimes completely covered by solar cells also. The cells generate current from the sun's radiation to provide operating supplies for the equipment on board, and to maintain the batteries in a fully-charged state.

Along with the batteries are containers of compressed gas. The gas can be directed to jets on the satellite's exterior to control the attitude of the craft in orbit, i.e. to keep the antennas pointing earthwards. This is necessary because the satellite's position drifts slightly, and has to be maintained in one spot accurately. (Otherwise we would have to keep moving our dishes down here on Earth!)

Obviously the quantity of gas available for attitude correction is finite, and is designed to last the life of the satellite – said to be about ten years. The maintenance of all of the satellite's systems on board is monitored by a telemetry channel accessed though a separate antenna on the craft. The travelling wave tube bays contain the power output stages of the transponders, sixteen in all on the Astra satellites.

At certain times of the day the satellite will move briefly into the shadow of the Earth, and the solar power will "drop out". This will occur during the night in the UK, possibly at peak viewing times, but the batteries take over the supply and re-charge again when the satellite leaves the Earth's shadow. given Ku-band. This is also called the Water-Absorption Band because the signals in the frequency range 10.7GHz to 12GHz are attenuated by moisture. This means that satellite reception suffers when it rains or snows, and even thick cloud cover can reduce the signal strength to produce "sparklies" on your pictures.

In many countries the first choice of the available spectrum space for communication is given to defence, then to governmental and diplomatic agencies, and then to commercial users, and lastly to entertainment. Possibly this is how we got Ku-band!

However, Ku-band is not all that bad now that higher transponder powers are available and, on the receiving side, improved-performance LNBs (Low Noise Blocks) are available. The dish acts as a "magnifying-glass". A concave mirror magnifies as well as reflects, you can use a concave mirror as a burning-glass as it will concentrate the sun's rays by focussing them into one spot. The action of the microwave dish is similar, but works on radio frequencies instead of light-waves, focussing the radio waves from the satellite into the throat of the feed-horn on the LNB, see Fig. 5.

The LNB, is the small box fastened to the end of the pole that protrudes from the dish and has a funnel-shaped device which faces the dish. The LNB contains several separate items for the reception of satellite signals. It is sited at the focus of the dish to collect the magnified satellite signals from space. Microwave signals can be polarised vertically or horizontally.

### POLARISATION

TV aerials are fitted vertically or horizontally, depending on the signal polarisation, a similar arrangement exists with satellite signals and it means that two transmitters can share the same frequency if they have different polarity. The selection of vertically or horizontally polarised transmissions is done by the LNB right at the input.



Fig.5 (above). Receiving dish and offset LNB. Fig.4 (left). Arrangement of a typical television satellite.

# Satellite direct-to-

home broadcasting is

banned in Iran and

some Middle-Eastern

states. It is tolerated

but is

elsewhere



Fig.7. Satellite downlink channel arrangement (frequencies in GHz).

The very weak signals from the satellite are then passed through amplifiers which are designed to contribute very little noise themselves, which would spoil reception with snowy pictures. Finally, the clean signals are then converted down en-bloc to a lower band of frequencies for piping to the receiver unit via co-axial cable. Very high quality co-axial cable should be used for this link to ensure the maximum possible signal transfer from the dish to the receiver unit.

The receiver enables the viewer to select the desired satellite TV channel, descramble it if necessary, and pass it to the VCR and TV, either in a standard form similar to terrestrial u.h.f. TV signals or as separate video and audio signals directly into the display section of the TV or the video and audio recording circuits of the VCR.

### HOME SET-UP

The commonest arrangement used in the average home which also sports a video cassette recorder will be the one shown in Fig. 6. The satellite receiver has a socket for the viewer's u.h.f. terrestrial TV aerial as well as the socket for the cable coming from the satellite dish. Within the satellite receiver are the tuner and descrambling circuits and a modulator, which is a small and rudimentary TV transmitter.

The u.h.f. terrestrial TV signals are passed though the satellite receiver and the selected satellite TV channel is added to them before they pass out of the "r.f." socket for onward feeding to the VCR or TV set. The modulator is tuneable to allow the satellite TV channel to be placed where it does not cause interference to terrestrial TV. A similar system is used on VCRs.

U.H.F. TV plus satellite TV signals are passed into the VCR and here another modulator, usually on Channel 36, though some now use Ch. 60, adds the output of the VCR to the five incoming u.h.f. signals (four u.h.f. TV plus satellite). The six available channels are then fed to the TV receiver and can be tuned in the normal way.

Although this is the most common connection method, improved performance can be obtained on modern equipment by using the 21-pin SCART connection which takes video plus audio directly from the satellite receiver to the VCR and the TV. The use of the SCART system avoids distortion introduced by the simple modulators used in satellite receivers and VCRs, and gives cleaner, clearer pictures and sound. This direct connection method is to be preferred and eventually will become the first choice of connection methods with r.f. linking as the "alternative".

SCART-connected signals are normally accessed via the "AUX" or "EXT" selection button. Some VCRs and TVs call it "L1" etc, and some "S1" etc. On some TVs the "0" button selects it.

### CHANNELS

Each transponder aboard the satellite is allocated a frequency and polarity. The standard frequency spacing employed is 29-5MHz between channels of similar polarity (Fig. 7). The standard spacing between adjacent channels of different polarity is a half channel-width, or 14-75MHz. The half-channel spacing virtually removes the possibility of crosstalk from adjacent channels of opposite polarities. There are four active satellites in the *Astra* group which can deliver 64 channels, 16 per satellite, within the frequency span of 10-71425GHz to 11-68550GHz.

The arrangement of channels for one of the satellites is shown in Fig. 7. The bandwidth of each channel is 27MHz and within that space is provision for one vision carrier and four stereo pairs (or



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eight mono programmes) on subcarriers. In practice only three stereo pairs are used. The subcarriers are spaced at 7.02, 7.20, 7.38, 7.56, 7.74MHz and 7.92MHz from the vision carrier centre frequency. Sound and vision are frequency modulated. On some channels there still exists a single monophonic subcarrier at 6.5MHz, but this is being phased out rapidly to make way for digital radio. The frequencies quoted are for the unmodulated carriers.

### RECEIVER

A block diagram of a typical satellite receiver is shown in Fig. 8. This consists of a tuner for selection of the desired programme, a descrambling circuit, normally for Videocrypt-encoded video, a section which puts up the on-screen messages like "Your card has expired" or the set-up menus, sound, and the output modulator circuit.

Sound is handled by a comprehensive set of circuits which will probably include the Wegener Panda Stereo expander circuits as well as the subcarrier selection circuits which enable the viewer to have speech in another language, for instance. There is a modulator provided also for viewers without SCART connections on their TVs or VCRs.

All functions within the receiver are under the control of the main microprocessor. This chip masterminds tuning, descrambling, on-screen messages, sound and the modulator output channel, amongst many other things. It also handles the infra-red remote control system, translating its commands into actions.

The receiver is powered from an electronic high-efficiency power supply, also under the control of the microprocessor, and enabling the receiver to be set to its standby mode when not required for viewing. In the standby mode some of the internal circuits of the receiver and the LNB on the dish are kept powered-up. This avoids tuning drift problems which may occur if the entire installation is powered-up from cold. It also allows the timer clock to function and enliven the receiver for a timed recording of a satellite TV programme.

### MODULATION

Satellite TV uses frequency modula-tion (f.m.) at present. Terrestrial TV uses amplitude modulation (a.m.) at present, see Fig. 9. In amplitude modulation the strength of the carrier wave is varied by the video signal whilst the frequency of the signal is maintained constant. In frequency modulation the frequency of the carrier wave is varied by the video and audio subcarrier signals whilst the strength is held constant. This allows the transmitter to always operate at full power, improving the reception of such signals. It also ignores, to a large extent, any impulsive interference and is remarkably resilient under adverse reception conditions.

On the other hand, f.m. requires considerably more bandwidth, i.e. an f.m. signal would occupy about three times the spectrum space required by an equivalent a.m. service. In satellite TV there is, fortunately, plenty of space in the spectrum, at least, at present.



Fig.9. Frequency and amplitude modulation.

### CHANNEL SPECTRUM

The channel bandwidth is 27MHz and includes the audio subcarriers. The video bandwidth is standard for a 625-line signal, allowing a 5-5MHz bandwidth. For PAL colour signals the colour subcarrier is placed at the standard 4-4MHz. When demodulated and processed, the video signal is fully compatible with all 625-line TV receivers. Fig. 10 shows the channel spectrum.

Along with the picture signal (video), there are accompanying audio channels. Four stereo pairs are also available for use as follows:

- A: 7.02MHz and 7.20MHz
- B: 7-38MHz and 7-56MHz
- C: 7.74MHz and 7.92MHz

D:

8-10MHz and 8-28MHz (not in

use at present)

Some receivers allow selection of individual carriers of a stereo pair to permit multi-lingual monophonic operation. This means that up to eight separate mono audio channels can be accessed.

### RADIO

On most of the TV channels there are spare audio subcarriers, and as most radio is in stereo at the present time, some television and radio stations broadcasting on the satellite as well as on terrestrial transmitters considered it useful to put their radio programmes on them. Currently there are 29 stations using *Astra* with more on *Eutelsat*.

Some of the stations are only in mono on terrestrial transmissions because they are using long or medium waves. BBC Radio 5 is an example, as is Virgin.

Not all of the transmissions are available all of the time, and many come and go. A notable bonus of satellite radio is the ability to receive BBC World Service, pushed off 464 metres some years ago and relatively inaudible on its other frequencies since then.

Obviously it is not necessary to use a television receiver to hear satellite radio if a small audio amplifier and a pair of loudspeakers is available close to the satellite receiver. Since the advent of radio on





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Fig.11. Videocrypt scrambling.

Astra many viewers/listeners have incorporated better audio facilities in their "TV corner", and all satellite receivers include audio output sockets.

### SCRAMBLING

A television picture is made up of lines, in our case 625 of them, though only about 575 are used. The total duration of each line is 64 microseconds, though the active portion of the line is only 52 microseconds.

Videocrypt scrambling is achieved by taking the active portion of each television line and slicing it into two within the cutting limits in an apparently random manner (Fig. 11). The two portions are stored in memory, and the latter portion is read out of memory first, the former portion being joined onto it to give a line which makes no sense.

The apparently random manner (called pseudo-random) is actually a sequence of 65,000 numbers corresponding to the cutting-point of a line. It is generated by a computer and the pseudo-random byte sequence can be identified by a code called its "seed". Half of the seed is held in the viewing card, the other half is transmitted.

This is called the "cut and rotate" method and is the basis of most European scrambling systems. Others are Luxcrypt and Syster, and use a pseudo-random number sequence to delay the start of each line by a small amount. Videocrypt can now be "pirated", but its design is such that it can easily be changed without affecting the basic system, defeating the pirates at no extra cost to the legitimate viewer.

### DESCRAMBLING

Obviously the reverse of scrambling is principally the method used for

descrambling, but the decoder has to know what the random number sequence is. The seed is the key to the coding, with half of the seed carried in the "smart card", and the other half on the transmission. The two halves are united in the descrambler circuitry and verified over the air. If verification is a success the seed is then used to identify the pseudorandom number sequence and the decoder synchronises with the encoder, resulting in viewable video once more.

The cut-point is determined by the decoder and the incoming scrambled lines are cut again at the correct place, stored in memory and read-out is again from memory 1, containing the "A" portion of the line, then memory 2 containing the "B" portion. The decoding is not performed on an analogue video signal, the incoming video is digitised at 14MHz before being descrambled. This results in a seamless join.

### DIGITAL TV

Current TV transmissions are in analogue form, that is to say that the signal transmitted bears a direct resemblance to the picture being scanned and the sound picked up by the microphones. Analogue transmissions allow fairly rudimentary circuitry to be employed for reception, and the analogue method has been used since the start of television experimentation by Baird and others in the 1920s.

Terrestrial analogue transmission suffers from a number of defects which impair the enjoyment of television for anyone less than the electronics enthusiast. Signals pick up reflections causing ghosting, aircraft can cause fluttering of the picture in some areas and electrical interference from many sources impairs the quality of reception. A satellite transmission does not suffer from these impairments, but each service occupies a channel over three times the bandwidth of a terrestrial one. The benefits of a digital service are, therefore, slightly different for satellite and terrestrial transmissions.

In a digital service the picture to be transmitted is scanned in the normal way, but the signal voltage from the camera is not used directly. Instead it is "sampled" by a much faster train of pulses, the voltage of the video waveform being taken on every pulse and turned into a binary number corresponding to it. We are left with a stream of data which can be processed and transmitted. Because some form of memory is used in the receiver, the digital data can be sectioned into "packets" for vision, sound, teletext, etc., and one single carrier wave replaces the four or more which are currently in use.

Furthermore, standard error correction techniques can be applied to the signal which will enable the receiver to ignore anything that is not true data, such as reflected signals and interference. In fact, a digital service can be tailored to occupy a smaller bandwidth than current analogue ones, and provide more services to the end-user at the same time.

Cable TV will benefit also from digital services, allowing it greater programme capacity within existing arrangements, and full "interactive" services can be offered – if we can be persuaded that we really need them.

### PROCESSING

The real attraction of digitally encoded TV is the amount of processing one can employ to remove redundant information. Watch a television picture and you will realise that, from frame to frame – and there are 25 frames every second – there is much that does not alter.

In digital TV one can, by storing in memory a previous frame, get a comparison between one frame and the next. Only the changes in the picture need be transmitted. At the receiver the memory is refreshed only where changes have taken place.

Complete scene changes are accommodated by circuitry which re-writes a complete picture in four or five frames, the picture on the screen changing only when the complete picture has been built-up. Techniques such as these reduce the bit rate to a maximum of 15Mbit/s, and is often as low as 2Mbit/s.

Four stereo or eight mono sound channels and a serial data channel are included in the data stream. One could watch the progress of a computer game on TV and download the program for it into your PC at the same time!

A final note – the first digital TV transmissions for public consumption in the UK will be from *Astra* (probably in 1998 when receiver prices should have fallen).

Several manufacturers have developed receivers with a 500-channel capability. The initial cost of these receivers is high and the domestic electronics trade will have to learn a whole new TV engineering philosophy if they are to provide installation and repairs. Whatever happens, the future should be very interesting!

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Next month we start with details of a full specification professional design Theremin which will be described together with full constructional details over two months, we then follow up with a MIDI Theremin Interface in the January and February issues. The full specification

Theremin provides wide free space control movement, employs standard components with a minimum inductor count and uses varicap tuning of both pitch and volume aerials. It provides a continuous output for pitch monitoring and has both loudspeaker and headphone outputs.

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# Constructional Project



Protect yourself and your family – be soundly warned when vehicles enter the driveway.

This circuit is useful for signalling the movement of cars along a driveway and for similar purposes. It works by sensing the increased air pressure inside a flexible tube over which the vehicle passes. Tubing up to a length of about three metres (10 feet approx.) has been tested successfully with the prototype unit and this will be sufficient to monitor practically any driveway.

Remember, it only takes about a metre (three feet) of tubing to "cover" a driveway for a car of average width since the wheels on one side will trigger the unit.

There are two parts to the system – a pressure sensor plus tubing placed at ground level close to the position being monitored, and a mains-operated power supply. These sections may be situated any reasonable distance apart.

The circuit has been designed for continuous operation and has negligible power consumption. Note that although the sensor and tubing will probably be placed outdoors, the main unit *must* be situated in a *dry indoor* location close to a mains supply socket.

### GOOD IMMUNITY

Most readers will use the Vehicle Alert circuit for detecting four-wheel vehicles, or motorbikes or bicycles – that is, two pulses being provided by the pressure sensor. It would be a simple matter to arrange for any other number of pulses, up to nine, to trigger the unit. This may be useful for certain applications – for example, three pulses to respond to a car towing a trailer or caravan.

The system is reasonably immune from people triggering it since they are likely to give only one pulse within a five-second period. However, it will respond to cars and bicycles which provide two pulses within this time (that is, due to the front and rear wheels passing over the tubing).

When car tyres pass over the tubing, it will be squashed, causing an increase in

r the signal will be given it moves. m – d at being ower TRIGGI

pressure inside it. There could also be an increase in pressure due to any rise in temperature of the air inside, although such a change is likely to be small and no problems were experienced with the prototype unit.

The audible signal is given by a buzzer situated inside the main unit. Alternatively, the buzzer may be placed remotely. The operating time is adjustable between about 0.5 and 20 seconds. Note that the circuit cannot distinguish between an approaching vehicle and one which is retreating, so a signal will be given in whichever direction it moves.



Referring to the circuit diagram Fig. 2, switch S1 is the Pressure Sensor connected to the circuit through the plug and socket pair PL1/SK1. The pressure sensor has a diaphragm which moves when air pressure is applied to one side of it through an inlet port. This causes the contacts to "make".

Note that some devices do not give a true on-off switching action but provide a varying voltage output proportional to the pressure applied. Some of these are described as piezo devices and are *unsuitable* in this application.

IC1 is a dual timer integrated circuit (that is, it contains two identical units) and IC3 contains a single timer of the same type. All three timers are configured as monostables which operate when a lowgoing pulse is applied to the appropriate trigger input. Once triggered, the corresponding output will go high (close to the positive supply voltage) for a certain time then revert to low.



Fig. 1. Block diagram for the Vehicle Alert system.

### CIRCUIT DESCRIPTION

The system is illustrated by the block diagram in Fig. 1, while the Vehicle Alert circuit diagram, excluding the power supply, is shown in Fig. 2.

Referring to Fig. 1 first, an increase of air pressure inside the tube operates the contacts of a pressure sensor switch which simultaneously triggers two monostables having timed periods of 50 milliseconds and five seconds, respectively.

Pulses from the 50ms monostable are registered by the decade counter. If the required number of pulses do not arrive within the longer monostable period, the counter will be reset and the circuit revert to its original state. If the correct number of pulses (or more) do arrive, the third Consider IC1 first. A trigger pulse derived from pressure sensor switch S1 (or pushbutton Test switch S2 connected in parallel with it) provides a low-going pulse which is transferred via capacitor C1 to the trigger inputs of both timers (IC1 pins 6 and 8). The outputs of both timers will therefore go high simultaneously.

After the timers have been triggered by this pulse, capacitor C1 rapidly discharges through resistors R1 and R2 ready for another pulse to be received. A further purpose of resistor R2 is to maintain the trigger inputs in a normally high condition, which prevents false operation.

### CLEAN SWITCHING

The timed periods of the monostables are set by the values of two pairs of external components. These are resistor R3 and capacitor C2 connected to IC1 pins 1 and 2 for the first (5s) timer, and resistor R4 and capacitor C3 connected to pins 12 and 13 for the second (50ms) timer.

The purpose of the second monostable is to eliminate the effect of contact bounce in switch S1 or S2. This would cause multiple triggering and false operation. Only the first "make" of the switch contacts will trigger the monostables and "clean" output pulses will be provided by R7. The wire link as shown configures the circuit to operate with two pulses.

The collector of TR2 provides a low pulse to the third monostable (IC3) at its trigger input pin 2 via capacitor C4. Resistor R9 maintains the trigger input in a normally high condition which prevents false operation.

The timed period of IC3 is related to the values of capacitor C5, fixed resistor R10 and preset potentiometer VR1. With the

values specified, this can be varied between about half a second (with VR1 at minimum resistance) and 20 seconds (VR1 at maximum). It could be increased by raising the value of resistor R10 or capacitor C5.

With IC3 output pin 3 high, transistor TR3 is turned on by the base current entering through resistor R11. This operates the sounder, WD1, connected in its collector circuit.



Fig. 2. Complete circuit diagram, excluding power supply, for the Vehicle Alert.

the shorter one suitable for counting by decade counter IC2.

Further trigger pulses arriving within the 50ms period will have no effect. After this time, all contact bouncing will have ceased and the shorter monostable will be ready to respond again.

### ABLE TO COUNT

The output of the shorter-period monostable IC1, pin 9, is applied to IC2's clock input pin 14. Providing the reset input, pin 15, is low (assume for the moment that this is so) any pulses provided by switches S1 or S2 will be registered and successive IC2 outputs will go "high" in turn.

The standby state – that is, with no pulses having been received – is output Q0 (pin 3) high. On receipt of the first pulse, output Q1 (pin 2) will go high followed by outputs Q2 to Q9 in turn (pins 4, 7, 10, 1, 5, 6, 9 and 11, respectively). Note that only connections to outputs Q2 and Q3 (pins 4 and 7) are shown in Fig. 2.

While high, the output from the fivesecond monostable, pin 5, turns on transistor TR1 due to base (b) current entering via resistor R5. The transistor provides a low state at its collector (c) which is applied to IC2 pin 15 (reset input). This "enables" the chip.

After the five seconds time-out of the monostable, transistor TR1 turns off and its collector goes high. This resets the counter and maintains it in this state.

The five-second timing is regarded as the maximum that it would take for both axles of a slow moving vehicle to pass over the tubing. It could be altered if necessary by raising or lowering the value of resistor R3 in proportion, a larger value providing a longer timing period.

With either IC2 output pin 4 (which turns on after two pulses) or output pin 7 (after three), transistor TR2 is turned on due to base current entering via resistor



### POWER SUPPLY

As shown in Fig. 3, power is supplied by the conventional arrangement of mains transformer T1, bridge rectifier REC1 and smoothing capacitor C6. Fuses FS1 and FS2 protect the secondary and primary windings, respectively, and S3 is the mains On-Off switch.

The specified mains transformer limits the sounder current to 100mA maximum but, in practice, this is sufficient for all small sounders of the specified type.

### IMPORTANT SAFETY NOTE

Since constructing this circuit involves making mains connections, the reader must be satisfied with his or her ability to make a safe job. If there is any doubt whatsoever, the services of a qualified electrician must be sought.

All safety measures referred to in the text must be followed. In particular, the circuit must be constructed using an Earthed metal box and be correctly switched and fused. An insulating cover must be provided for all internal mains connections.

### CONSTRUCTION

Most of the components for the Vehicle Alert are mounted on a single-sided printed circuit board (p.c.b.). The component layout and full-size foil master track pattern are shown in Fig. 4. This board is available from the *EPE PCB Service*, code 117.

Begin construction by drilling the three mounting holes and soldering the i.c. sockets into position. Do not unpack the i.c.s themselves yet, however. Follow with the resistors, including preset VR1, noting that some are mounted flat against the board while others are fitted vertically.

Add the capacitors, taking care over the polarity of electrolytic capacitors C5 and C6. Solder the three transistors into position observing their correct orientation (the "flats" all face the right-hand edge of the circuit panel). Add the bridge rectifier, again taking care over the orientation, as marked on the body.

The p.c.b. as shown will provide for triggering on either two or three pulses from the pressure switch S1. The mode is selected by linking resistor R7 to pin 4 or pin 7 of IC2. If two-pulse triggering is required, link points Z and X on the p.c.b. If three-pulse triggering is needed, link points Z and Y.

If any other number of pulses up to nine is required, then point Z should be wired directly to the appropriate pin on the socket for IC2. This should be done using a piece of light-duty insulated wire on the copper track side of the board. For four to nine pulses, the pin numbers to use are 10, 1, 5, 6, 9 and 11 respectively.

### CASE PREPARATION

Prepare the suggested case for internal components by marking out and drilling three mounting holes in the base to correspond with those already made in the p.c.b. Also drill holes for the transformer and chassis fuseholder, FS1. Drill holes in the rear panel for the strain relief bush to be used on the mains lead, panel fuseholder





Fig. 3. Circuit diagram for the mains derived power supply for the Vehicle Alert.

FS2, pushbutton Test switch S2 and jack socket SK1 to which the sensor connections will be made.

Finally, drill the front panel for the mains on-off switch S3 and sounder WD1 – if mounted internally. (The finished appearance of the unit will be enhanced if the sounder is mounted internally rather than on the outside.)

### CONNECTIONS

Mount the p.c.b. on plastic supports so

later and is requirement.

above the 5mm base of the box. all com-Mount ponents for which holes have been drilled. When attaching the transformer, include a solder tag on one of its fixings. This will be used to "Earth" the case essential safety

that the soldered

joints stand at least

requirement. Refer to Fig. 5 and complete the internal wiring apart from that for the mains input. Note that the wire connecting fuse FS2 to switch S3 must be made with mains-type wire of 3A rating minimum.

an

Observe the correct polarity for the leads of the sounder WD1 or it will not work.

When wiring up the jack socket SK1, note that many types have one terminal (the sleeve) connected to the metalwork.



Fig. 4. Printed circuit board component layout and full size underside copper foil master for the Vehicle Alert. The completed p.c.b. (below) is mounted well clear of the case base on nylon bolts with "locking" nuts.



Everyday Practical Electronics, October 1996



Fig. 5. Interwiring between off-board components and p.c.b. Note wiring between fuse FS2 and switch S3 must be made with 3A minimum mains-type wire. Also, socket SK1 must be an insulated (plastic bodied) type.

However, a fully insulated (plastic bodied) type socket *MUST* be used here – i.e. neither terminal makes metalic contact with the case. Make the ''tip'' connection to the upper ''S2'' pad as shown in Fig. 5.

### MAINS LEAD

Make up the mains supply input lead by cutting off a piece of mains-rated cable having a capacity of 3A minimum. Remove 8cm of the outer sheath from one end, pass the wire through the hole made for the purpose and secure it using a strain relief bush. It is essential to use a proper strain relief here – do *not* tie a knot in the wire or secure it using a piece of string!

Refer to Fig. 5 again and connect the cable as shown. The specified mains switch contains a neon indicator which is convenient because it requires both a Live and a Neutral connection. It thus acts as an anchorage point for the Neutral feed wire. If a switch without a built-in neon indicator is used, the Neutral wire should be connected directly to the transformer primary lead using a single piece of 2A screw terminal block.

Solder the Earth wire securely to the solder tag leaving some slack inside the case. Attach a mains plug to the other end of the lead and insert a 2A or 3A fuse. Fit a 250mA glass fuse in the chassis fuseholder (FS1) and a 1A ceramic mainstype in the panel fuseholder (FS2).

Make an insulating cover for the entire left-hand side of the box. This will provide protection to all the mains connections (this cover has been removed in the photograph to show the internal details).

Finally, attach self-adhesive plastic feet to the base of the box.

### TESTING

All the i.c.s are CMOS components and there is a possibility of them being damaged by static charge which might exist on the body. To avoid this, touch something which is earthed (such as a water tap) before unpacking them and touching the pins. Insert them into their sockets observing the correct orientation.

Note that all testing and operation must be carried out with the lid of the case in position. When making adjustments, the mains plug must be removed from the socket.

Adjust preset VR1 fully clockwise (as viewed from the edge of the circuit panel) for minimum sounder time.

The circuit should be checked for correct operation *before* the pressure sensor is connected. Plug the unit in to the mains and switch on – the sounder may give a bleep and this is of no consequence. If the circuit has been set for two pulses, press switch S2 twice. The buzzer should bleep.

Wait for ten seconds (so that the circuit is definitely reset) and repeat the test a few times. Next, press S2 once, wait for ten seconds and press it again. The buzzer should remain silent. If the unit has been set for three pulses, work accordingly.

Remember, when making tests you will need to wait for up to ten seconds each time to allow the counter to reset. The bleep time may be adjusted by anti-clockwise rotation of preset VR1.



Layout of components inside the metal case. The sounder is also mounted using nylon nuts and bolts.

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### UNDER PRESSURE

To mount the pressure switch S1 inside the specified small plastic box it will be necessary to gently bend the tags so that it will fit. The plastic (unused) port labelled "low" should also be cut off short.

On the same side as this port a recess will be seen to accommodate a small Allen (hexagonal) key. This may be used to

adjust the switch for the required sensitivity. (This may not be necessary, so do not be too hasty in buying an Allen key to fit.)

Drill holes in the rear of the box for the two small fixings which will secure the switch. Drill a further hole to allow the Allen key to be inserted, if necessary.

Attach the switch temporarily. The position of the port labelled "high" should now be carefully measured and a hole drilled in the lid of the box to correspond with this.

It should be large enough to allow narrow bore (3mm diameter) tubing to be attached (see photographs). Remove and re-attach the switch with spacers on the nylon bolt shanks so that the inlet port protrudes slightly through the hole in the lid.

Measure the length of double-insulated cable to be used between the pressure switch and main unit, the cable should be soldered to the pressure switch S1 at one end (polarity unimportant), and to plug PL1 at the other end.

### **ADAPTING WELL**

Decide on the length of tubing to be used and the route it is to follow. Begin with a piece of 3mm diameter and attach it to the sensor port. Using a plastic adaptor, connect the main section consisting of a piece of wider diameter tubing (see photograph).

Good results were obtained using plastic tubing having an inside diameter of 5mm or 6mm. Tubing sold for winemaking was found to be suitable. It must be of a type which springs back into shape quickly. Adaptors may sometimes be made from old pen parts. Alternatively. a local school may help with the ordering of tubing and adaptors since they are standard chemistry materials.

Fit the tubing into position taking care not to cause kinks. Seal the end furthest from the sensor position using a small plastic plug – such as the end of a plastic pen. Readers will need to make their own arrangements to prevent people tripping over the tubing by, for example, fitting it in a groove in a piece of wood. Do not run the tubing over a rough or stony surface which will puncture it after a short time.

A rise in air temperature outside will cause an increase in pressure inside the tubing but this was not sufficient to cause problems in the prototype unit. Even so, it would be best to avoid direct sunlight shining on it. Making a very small vent hole in the end cap should minimise any problem. It will allow expanded air to escape yet will not be large enough to have an effect on rapid changes, such as when car wheels pass over the tubing.

It may be found that the sensitivity of the pressure switch is satisfactory as supplied. However, it may be adjusted using an Allen key (size 1.27mm) through the hole drilled for the purpose. To make the adjustment, clip the probes of a multimeter, set to a resistance or buzz-test range, to the terminals of the switch.

Turn the Allen key very slowly anti-clockwise until the switch operates continuously (near-zero resistance). Now rotate it slightly clockwise until the contacts open (infinite resistance). Further adjustment may be needed over a trial period. Do not adjust the switch too critically or operation will be unreliable.



The smaller diameter "pressure" tubing connected to the pressure switch and, via a plastic adaptor, to the larger diameter "driveway" tubing.



The completed remote pressure switch unit, with pressure tube, linked to the main Vehicle Alert circuit box.

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The pressure

risk.

switch is mounted

inside the small plastic

box with nylon nuts and bolts.

to align with the "high" port.

A hole must be drilled in the lid

EXTERNAL SAFETY

When finally installing the pressure

switch unit outside, it is imperative to bear

in mind the safety aspects of the cabling.

The remote location of the sensing box

would extend the mains earth (via 0V rail

of 12V supply) outside the building if the prefered "insulated" jack socket were not

used. Under exceptional mains fault condi-

tions, it could be "live" up to 240V a.e.

relative to any nearby surfaces at ground

potential (e.g. metal railings, metal green-

house frames) and may present a shock

Readers should ensure that the cable to

the remote sensing box is double insulated

and that there is no possibility of exter-

nal contact being made with the electri-

cal connections within the box. Ordinary

twin-cored mains cable is suitable (each

core separately insulated with both jointly

wrapped by an external insulating sheath).

Also observe the precaution of using a

fully insulated jack socket as specified.

Twin flex, e.g. bell wire or similar, is

not suitably insulated. If in any doubt,

consult a qualified electrician.



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SUPPORT We will give continuing support to our users and products. Future expansion planned – 17CXX Programmer – smart card reader/writer and more.







Our monthly Help Desk looks at retriggerable monostable timers, making those plastic project boxes sparkle like new, and a new way our overseas readers (and UK ones!) can snaffle those codes for our PIC-based microcontroller projects.

### **PICs away Chaps**

DIPPING into this month's post-bag (and sifting through our "electronic" mailbox, too), by E-mail came the following topical comments from *Dr. Pieter le Roux* in South Africa:

Referring to your comments on PIC programming (Take Your Pic, Circuit Surgery, July 96), I have a lot of sympathy with gifted programmers who wish to keep their code copyrighted – I certainly would!

However, out here in South Africa it is extremely difficult to obtain even the released codes using the methods you provide (floppy disk by post) because of the poor exchange rates which makes foreign purchases prohibitively expensive. The delays using (affordable) surface mail make one lose interest in favour of the subsequent two months projects which you publish!

Parts can be very difficult to source, making PICs about the only project that readers out here can safely attempt, since they seldom need a lot of specialised peripheral devices. So my questions are:

When will the WWW site to which you allude, be available? Is there some other means of obtaining the source codes when new PIC projects are released?

We recognise all of these problems, hopefully the Maplin outlet in Somerset West will help to reduce the component supply problems in South Africa. You will be pleased to hear that all available project PIC files are now available by free "anonymous FTP" from our server. Overseas readers with an Internet connection will find this tremendously useful, we hope.

. The files for the PIC-Tock Pendulum Clock project (Sept. '96 issue), for example, were immediately availdate of publicaable from the of that issue. The URL tion is ftp://ftp.epemag.wimborne.co.uk/pub /PICS/pictock. Note that certain PIC project source codes are not available as they remain the property of their respective designers.

Our World Wide Web site is also open,

growing slowly and surely – we hope you have spotted the URL and E-mail address on our cover and *Editorial* page! Also, check our *Net Work* column for current information.

### Shining Example

My thanks to *Mark McGuinness* of Clondalkin, Dublin, whom I know is a regular *Surgery* reader and *Ingenuity Unlimited* contributor. Mark suggests:

I've found that some plastic boxes which arrive by mail order come complete with unwanted scratches visible on one or more sides of the box. These can spoil a project's appearance.

I have found that using an aerosol spray paint, the scratches can be hidden and you can give the box a more attractive colour, too! It is a good idea to drill the holes etc., first, before spray painting the box, to preserve the paint finish.

These days, plastic boxes can form a major part of the cost of project building, and I shop around the same as everybody else, so I object if it arrives bashed in the post. It is not widely known that one of the best ways of polishing scratches (minor ones, anyway) out of plastic is to use traditional *metal polish*.

Something like "Brasso" or chrome polish paste (try a cycle shop) is excellent – all you need is some elbow grease! Paste-type metal polishes are based on a micro-abrasive (e.g. very fine grade aluminium oxide powder in an oily base) and at surface level these smooth off the plastic and eventually leave a mirror finish.

Spray-painting a plastic box can be trickier than you'd think. The older cellulose-based paints have a characteristically pungent smell and they can actually melt many plastics, doing irreparable damage to the surface which you will never clean up. More than once, I have damaged my carefully-applied rub-down lettering with a cellulose-type clear lacquer, which dissolved the lettering and the plastic with it!

Nowadays, it is usual to use acrylicbased formulations instead and these can leave a superb mirror finish on plastic surfaces. (Car touch-up paint is based on these same modern acrylics.) It is still wise to test the plastic first (e.g. spray a small area inside the lid, and you are right, Mark, always do the drilling and fabricating beforehand! Professionals actually use a RAL colour-matched aerosol paint to touch up those boring but bashed, grey boxes.

You might be interested in my new feature series *Build Your Own Projects* which commences very soon here in *EPE*, once I have got more film loaded in my camera! You'll find lots of interesting information to help you get the best results for your money!

### Flashing L.E.D.s

A topic which to old hands is "done to death", but still important to many people, especially our younger readers, is how to use light-emitting diodes (l.e.d.s) correctly! It crops up very frequently on Internet newsgroups.

They have a very low operating or "forward voltage" (typically, 1.8V to 2.2V) which needs to be taken into account when using them at a higher voltage than this. You need a *series-limiting resistor* which is used as shown in Fig. 1. The resistor



*Fig.1(a) Series resistor calculation, (b) using an l.e.d. on an a.c. supply.* 

(*R*) causes two things to happen: first, it creates a voltage drop; and second, it limits the current.

To calculate the resistor value, you need to know *three* things: the supply voltage you are using; the forward voltage of the l.e.d. and, how much current you would like to flow through the device.

The more current flowing, the brighter it will be, but there is usually nothing to be gained by exceeding more than 10mA to 20mA or so. In normal operation, the forward voltage appears "automagically" across the l.e.d. so you have to "lose" the excess voltage somewhere – across the resistor.

It is pretty easy once you get the hang of it. In the example of Fig. 1a, the supply voltage is  $\pm 10V$ , and the supplier's catalogue says that the l.e.d. *forward* voltage is 2V.

So, first we have got to lose 8V across the *series* resistor. Second, let's decide that we want 10mA to flow. The series resistor is then easily calculated with Ohms Law:

 $\mathbf{R} = \mathbf{V}/\mathbf{I}$ 

so R = 8V/10mA (0.01A) = 800 ohms. The nearest preferred value is 820 ohms, which would be fine.

What would happen if you had only a 560 ohm resistor available, for example? Well, the l.e.d. will still try to maintain 2V, so the current will be 8V/560 ohms = 15mA. This is still well within a typical l.e.d.'s specification. If you want to use them on an a.c. supply, a reverse-parallel diode is needed as shown in Fig. 1b.

If you want to save some work but spend more money, you can buy l.e.d.s with resistors already built in. Ready-made flashing light-emitting diodes (f.l.e.d.s) are a neat way of adding one of these blinking beacons to your project (see February and April '96 issues).

The main factor to watch for is really just the supply voltage, since this varies depending on the type of f.l.e.d. you've bought. Check the specs, carefully at the time of purchase. Some types are safe to use from, say, 3:5V to 13V absolute maximum, other varieties have a 5V maximum.

There is a potential trap using the f.l.e.d. types! If you want to use them with a higher voltage, then when the flasher l.e.d. is ON, forward current flows as usual, so you'd think you could use a series resistor as before. But when the f.l.e.d. turns OFF, there is hardly any current flowing, so there is no voltage drop across the resistor, and all the supply voltage appears across the f.l.e.d. instead!

Therefore, if the supply rail is higher than the f.l.e.d,'s maximum voltage rating,



Fig.2. Using flashing l.e.d.s at higher voltages.

it is wise to take extra precautions by using, for example, a Zener diode across the f.l.e.d. to protect it against over-voltages. This means that the series resistor should allow for a nominal Zener current (say, 5mA) too. The supply rail is  $\pm 24V$ and the f.l.e.d. in Fig.2 is rated at 8.5mA and runs safely at 10V in this example, thanks to the Zener.

### **Retriggerable Timers**

A question arose on a particular type of timer called a "retriggerable" monostable. *Mr. J. M. Bloodworth* of Maidenhead asks for guidance:

"Could you explain a little about retriggerable monostables. I have spent years waiting to see some examples of how this can be done."



Fig.3. Classic 555 monostable.

The familiar 555 monostable is shown in Fig. 3. This has a period of roughly 10 seconds (1.1 *RC*). My experience has highlighted one or two hidden snags which you might need to take into account when using this as the basis for an appliance timer circuit or whatever.

Closing switch S1 starts the time period, and switch S2 resets it. Providing you open S1 again before the chip times out, you're OK.

Furthermore, sending more trigger signals makes *no difference* once the 555 has started timing. But if the trigger signal is present just *as the ten seconds are up*, then the 555 output *remains high*, and it will only go low when the trigger signal is finally removed! Then, the timing period is the same length as the

trigger signal.

The monostable's operation is well known - the capacitor Cis discharged by an internal transistor within the 555 at pin 7 when the timing period has elapsed. The retriggerable monostable you're interested in will re-start the timing period if a fresh trigger signal is sent.

You cannot do this directly with the 555 and it is therefore necessary to discharge the capacitor by some other means. This is accomplished by adding an external *pnp* transistor in parallel with the 555's internal discharge (pin 7) transistor and also hooking the base (b) lead to the trigger pin (2), as shown in Fig. 4.

When a (negative-going) trigger signal is received, pin 2 of IC1 and TR1 base (b) are grounded. Therefore the 555 triggers internally so its output toggles high, but the transistor also turns hard on which keeps the timing capacitor (C) discharged.

The output remains latched high, but the monostable period cannot *actually* start until the triggering signal is then *removed*; then TR1 turns off, capacitor *C* charges up as normal and the monostable will time out. It is not technically a true retriggerable monostable because the output latches when a "trigger" is received, but the actual timing period does not commence until the trigger is removed.

Nonetheless, the period will recommence again if the trigger is briefly applied once more, when the capacitor will recharge from near zero, having been discharged by TR1. Maybe you can adapt it for your needs.

The capacitor may have a small residual voltage across it (400mV as measured), depending on how hard the transistor saturates, which may affect accuracy but it may be good enough for many purposes. Another option would be to use a small MOSFET transistor which might shunt the capacitor down to a lower voltage. There is room for experimentation.

There are indeed other true retriggerable chips available, notably TTL timers including the 74122 (single) or 74123 (dual) monostable retriggerable timers, but they are really only good for fractions of a second in high speed logic circuits. The 74121 is also a non-retriggerable chip but is more complex to use. Whilst not being inherently retriggerable, the 555 is better for general use.

### At your service

Circuit Surgery is your page. If you have any questions to ask or comments to make, please write to Alan Winstanley, Circuit Surgery, Wimborne Publishing Ltd., Allen House, East Borough, Wimborne, Dorset, BH21 1PF, E-mail **alan@epemag.wimborne.co.uk** 

We cannot guarantee an individual reply nor undertake to answer questions on commercial equipment but we do try to help wherever possible.



Fig.4. Retriggerable 555 monostable.



### Your Number's Up

If there was a best time for telecommuniations watchdog Oftel to announce that the UK was again running out of telephone numbers, it was when they did. August, with many people away on holiday, including MPs. But there was still outrage.

There was also a lot of nonsense talked and written. For example, people still see BT and Oftel as one and the same organisation, or partners in conspiracy, when in fact lawyers for Oftel and BT get rich on the running battles between the two quite separate organisations. It does not help that other telecoms operators, such as Mercury, seldom bother to contribute to the open debate.

There are two reasons why Britain is short of telephone numbers.

Gone are the days when you phoned a company's switchboard and asked them to try and connect you to Mr Jones. You now dial Mr Jones on his *direct* dial extension, or send a fax to his personal machine. The explosion in cellphones, answering and paging services adds to the fax explosion and direct dialling.

Also, the UK uses telephone numbers inefficiently, because we try to tie subscribers' numbers to their locations. When you phone long distance to Wigan you know it's Wigan because of the code, and cannot be fooled into thinking it is a local call.

Oftel clings to this tradition, while allowing a proliferation of premium phone lines and answering services which leave users paying long distance rates for local calls and being charged literally pounds per minute for special services.

### **Passing the Buck**

Put all this together, add some good old British muddle, and you get the current mess. Add another ingredient, "passing the buck", and no-one feels the need even to say sorry for the mess.

The one over-riding impression I got from the press conference called by Oftel to announce the number shortage was the overwhelming confidence of Director General Don Cruickshank that none of it was anything to do with him. Not once did I see even a flicker of sympathy for the small businesses who will now have to pay yet again to reprint their stationery, change their signs, reprogram memory diallers and security devices and warn clients round the world of the new numbers.

After reassuring that the next number change will cost less than the last change, *Phoneday* in April 1995, Cruickshank dismissed all questions on the actual cost. "I don't know how much *Phoneday* cost. How should I know? Why should I? It cost nothing because of the net benefit"

The bare facts are that London's telephone subscribers face their *third* number change in ten years. Four more cities face their *second*. The only other option is for businesses to start using a completely new range of numbers from domestic subscribers.

The details are to be found in a Consultative document, *The National Numbering Service, Options for the Future –* 2 which is available *free* of charge from Oftel. You have until 18 October to comment. Oftel then decides in December what to do before five cities including London run out of numbers by the year 2000.

"This leaves plenty of time for planning" says Cruickshank. He works on the principle that people are happy to reprint stationery and re-write signs every couple of years.

### Sorry – Wrong Number!

Until 1990 BT was responsible for telephone numbering. In April that year, with BT's monopoly slipping away, Oftel started to take over responsibility, initially relying on TNAB, a Telephone Number Advisory Board, for guidance. In June 1994, Oftel took over complete responsibilty.

In May 1990 Oftel implemented BT's plan to split London's numbering from 01 to 071 and 081. Oftel then planned a national code change for Easter 1994, with every number in the UK growing an extra "1" at the front, to make London's numbers 0171 and 0181. The codes for Leeds, Sheffield, Nottingham, Leicester and Bristol changed completely at the same time.

Industry was so slow to react that Oftel had to delay the national *Phoneday* upheaval until April 1995. Don Cruickshank appeared on the *Newsnight* TV programme to pledge that "Once we have put the '1' in front of all the present numbers, no-one who has such a number will have to change again during their lifetime".

But even before *Phoneday* dawned, rapid business expansion in Reading, Belfast, Southampton and Portsmouth had made it inadequate. Last year Oftel gave Reading a completely new code, which came into operation in April 1996.

In last year's Consultation document, Oftel proposed an idea, called "Overlay", from the US to save other cities. In New York City new subscribers get 917 codes while existing subscribers keep their 212 and 718 numbers. So as a British zone runs out of 01 numbers, new subscribers would get 02 numbers. Oftel says it abandoned the overlay scheme because consumer groups objected that people living next door to each other would have different codes and so need to dial long strings of numbers to talk to a next door neighbour. When reminded of his now-broken pledge, Cruickshank simply says that all bets were off when he had to abandon the 02 overlay idea.

### **Equal Misery**

Having ploughed through Oftel's obscure documents I would say it is a safe bet that most people never realised Oftel was offering them a straight choice – either accept that new subscribers in crowded cities like London will get quite different numbers, or be prepared for everyone in those cities to have to change all their numbers.

Oftel's new fix is to change all the numbers in the five most starved cities (London, Cardiff, Belfast, Southampton and Portmsouth). Old and new subscribers alike will all get 02 numbers. So, London's 0171 and 0181 codes

So, London's 0171 and 0181 codes will become 020 or 022. Because the area code is now one digit shorter, the local number can be extended by one digit (to increase the number pool tenfold) without making the total number string too long for existing equipment, in the UK and abroad, to handle.

Remember, that foreign countries have to dial extra digits to get into the UK. The current international limit is 12 digits, and although it will soon rise to 15 this will not help old switchboards in Russia etc.

Don Cruickshank rejects the suggestion that his new policy inflicts "equal misery" on everyone, to ensure that no-one can complain of unequal treatment. He prefers to describe it as policy of "equal opportunity". Remember that when you are paying for new notepaper and signs.

### **Personal Number**

There is one alternative option. This is to leave domestic numbers untouched and persuade businesses to migrate onto a new set of numbers which all begin 05.

Another new idea is to use the 07 code for "Find me anywhere" or "portable" numbers. Subscribers keep the same number for life, regardless of which phone service they are using, and who they are paying to provide it, e.g. BT, Mercury, Cellnet, Vodafone, Orange, or One-2-One. But this will be slow to catch on. The service operators want to stop subscribers "churning" onto a rival service, and what better way to achieve this than make them reprint all stationery as a punishment!



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passengers. Order Net, 25. 1 x 0-1mA Panel Meter, Full vision face 70mm square. Scaled 0-100. Order Ref: 756. 2 x Lithium Batterles, 2:5V penlight size. Order Ref:

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5 x 13A Rocker Switch. Three tags so on/off, or changeover with centre off. Order Ref: 42. changeover with centre off. Order Ref: 42. Mini Cassette Motor, 9V. Order Ref: 944.

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 Cor Mid Colloce 100 Colloce 100 Content of the content of

50 x Mixed Silicon Diodes. Order Ref: 293. 1 x 6 Digit Mains Operated Counter. Sta

Standard size but counts in even numbers. Order Ref: 28.

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FIGURE-8-FLEX. Figure-8 flat white pvc lead, flexible with 4 sq.mm cores. Ideal for speaker extensions and bell circuits. Also adequately insulated for mains lighting. 50m coil, £2, Order Ref: 2P345. 12m coil, £1, Order Ref: 1014.

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# Constructional Project



Tuning into the world amateur bands couldn't be easier with this receiver!

S AN introduction to short wave listening on the amateur bands, probably the easiest type of receiver to construct is of the direct conversion variety. This type of receiver is at its best when resolving single sideband (SSB) and Morse code (CW) signals. This is perfect for the H.F. amateur bands since most stations use these modes of transmission nowadays.

The demise of the Sunday morning "A.M. nets" on topband sadly occurred in the 1970s in the Midlands area. SSB is, of course, a more effective communications medium for weak signal work and also theoretically uses only half the bandwidth of an equivalent a.m. transmission.

The consequence of using SSB on topband does mean that the casual listener tuning around the "high end" of medium wave will never resolve any amateur transmissions on a domestic set. This is a great shame because many people (me included) got bitten by the bug listening to such signals.

### TOPBAND

Until recently, topband or 160 Metres was the lowest frequency range available to radio amateurs and novices. It extends from 1.8MHz to 2.0MHz, this is just above the upper limit of the medium waveband.

A new allocation at 73kHz means that topband is no longer the lowest frequency range available. However, 73kHz does have a lot of restrictions imposed on it at present and is only available to those who have applied for a special notice of variation to the basic amateur licence.

Topband behaves in a similar manner to medium wave with local ground wave stations coming in loud and clear during the day. After dusk the band opens up to Europe and beyond with skywave being the predominant mode of propagation.

The reason for this is one of the layers of the ionosphere called the *D*-layer.

Everyday Practical Electronics, October 1996

During the day, solar radiation causes the D-layer to become heavily ionised. This layer absorbs radio energy at low frequencies and so prevents long distance reception.

At night in the absence of solar radiation, the D-layer disappears to some degree and allows radio waves to pass through to the upper layers of the ionosphere. These reflect the radio signals back down to earth, usually at some considerable distance.

Expect to hear stations up to about 50km during the daytime on top band. In the evening (particularly during the winter) it is possible to hear stations as far away as America or even further.

The 80 Metre band behaves slightly differently. Its frequency range extends from 3-5MHz to 3-8MHz. Also, because of its higher frequency range, groundwave range is reduced and the D-layer has slightly less influence.

Weakish signals up to around 200km can be received during the day although these tend to be unstable and very prone to fading. Reception from just about anywhere on the globe is possible at night.

The communications range

of both the amateur

bands is affected by many factors such as the time of day, month of the year, the sunspot cycle, solar flares etc etc. With so many different variables it becomes difficult to predict whether a path to a certain country will be viable or not - All this adds to the fascination of tuning the amateur bands.

### CALLING CARD

Each radio amateur has a unique callsign allocated to him (or her) by the Radiocommunications Agency. There are around 60,000 licensed amateur radio stations in Great Britain and many hundreds of thousand worldwide. Stations in Great Britain are prefixed by the letter "G" (or 2E0 for a novice station) for example. (All G callsigns have now been issued and so the latest series of newcomers have the prefix "M".)

If you obtain a copy of the amateur radio callbook (available from good book shops) then it is possible to find out where the station you are listening to is located. Amateurs are always keen to receive reception reports from shortwave listeners and will often send out a QSL card to confirm the report.

Radio amateurs are not just restricted to voice and Morse code communications on these bands either. Radio teletype, Slowscan television, Facsimile and Data trans-

PRESELECT

AF GAIN

BAND

missions (Packet radio) are also used. These modes can all be resolved



Front panel layout and lettering.

with this receiver connected to a suitable decoder.

### DIRECT CONVERSION

The direct conversion principle relies on a local oscillator operating on the same frequency as the suppressed carrier of the transmitter and a product detector. The wanted output from the product detector lies in the audio frequency spectrum and is indeed the resolved audio from the SSB transmitter.

For CW the local oscillator is tuned a few hundred hertz away so that the result is an audible beat note. Since there is no intermediate frequency, the majority of the systems gain lies within the audio spectrum.

With this type of receiver the chances of r.f. instability occurring due to layout are much reduced. The design featured here

has good sensitivity since an r.f. amplifier is included ahead of the mixer, good selectivity due to the active filtering used and a wide dynamic range as a result of the digital balanced mixer.

### CIRCUIT DESCRIPTION

The full circuit diagram, except for power supply, for the Direct Conversion Topband and 80 Metre Receiver is shown in Fig. 1. Suggested Power Supply/Charger circuit details being given in Fig. 2.

Incoming r.f. from the antenna is fed to the primary side of coil L1. This transformer/coil is bought to resonance at the required frequency by a pair of back-toback varicap diodes VD1 and VD2.

From here, r.f. at the "hot" end of the secondary of L1 is then fed to the gate (g)

of the field effect transistor (f.e.t.) TR1, an r.f. amplifier in common source configuration. The drain (d) of TR1 is d.c. coupled to the base (b) of transistor TR2, an emitter follower. The output of TR2 feeds the primary coil of L2, the secondary being resonated at signal frequency by varicaps VD3 and VD4. The inclusion of capacitor C4 was found to be unnecessaryy in the final model.

### LOCAL OSCILLATOR

The variable frequency oscillator (v.f.o.) comprises a tuned circuit consisting of transformer L3 which is bought to resonance by the variable trimmer capacitor VC1 and varicap diode VD5. Variable bias to VD5 is provided by Tuning control VR2 and is fed via resistor R29 and C23. C24 is a d.c. blocking capacitor.

Transistor TR4 maintains oscillations at the desired frequency and TR5 is an emitter follower. Its base (b) being connected to the hot end of coil L3 via capacitor C28.

Transistor TR5 acts as a buffer and prevents subsequent circuitry loading the oscillator stage. The output of TR5 is sufficient to drive the CMOS divider chain formed by IC4.

The v.f.o. (variable frequency oscillator) covers the frequency range 6-9MHz to 8-1MHz, this being divided by IC4 to give 3450kHz, to 4050kHz for 80 metres and 1725kHz to 2025kHz for 160 metres. The tuning rate of VR2 is 60kHz/rev on 80 metres and 30kHz/rev on 160 metres which is more than adequate for SSB/CW resolution.

Since the v.f.o. runs at a different frequency to the received frequency,



Everyday Practical Electronics, October 1996

**790** 



Circuit diagram for the combined PSU/Charger.

### CONSTRUCTION

All components for the Direct Conversion Topband and 80 Metre Receiver, with the exception of the aerial socket, tuning controls, switches, loudspeaker and power supply, are mounted on a single printed circuit board. This board is available from the EPE PCB Service, code 116. The power supply components are wired directly around the mains transformer and the NiCad pack positioned in the base of the metal case next to the p.c.b.

If you are not familiar with the use of a soldering iron then it is suggested that a little practice is done on a piece of stripboard before attempting construction of

3.301

and

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amplifier

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Technical Studies

Topband and 80m Receiver.

C21

C22

791

this receiver. A 15W soldering iron with a fine tip is recommended.

Two of the i.c.s (IC1 and IC4) are static sensitive and should be mounted in sockets. In fact, it is a good idea to use d.i.l. sockets for all the i.c.s. Do not mount any i.c.s in their sockets at this stage but wait until board construction has been completed.

### CIRCUIT BOARD

Printed circuit board (p.c.b.) component layout and underside full size copper track master are shown in Fig. 4.

Start construction by positioning and soldering the 12 solder pins around the periphery of the board. Following this, the resistors can be positioned and soldered, cropping off any excess lead length with a pair of wire snips. Note that resistors R37 and R38 are not mounted on the board but are soldered directly on the tags of potentiometer VR2 (see Fig.5).

Next, the capacitors can be soldered in position taking care to observe the polarity of the electrolytics, failure to do so can result in some quite spectacular (and potentially dangerous) results! This should be followed by the inductors, be careful not to damage the leads, there are very fine wires attached to the pins on these and it is all too easy to damage them.



The completed p.c.b. is sited above a piece of aluminium foil to give additional circuit screening.

The transistors and varicap diodes are next in line to be soldered into position. Start with the five transistors taking care to insert them into the board the correct way round.

The five varicaps are also polarity conscious so do take care. Also, these devices are supplied as three varicaps all encapsulated in *one* package (you need two of these). It is necessary to separate them into individual devices. Use a junior hacksaw. One or two light strokes with the saw in the grooves should enable them to be snapped apart.



Fig.4. Printed circuit board component layout and full size copper track master.

COMPONENTS	Table 1: Typical Voltages Here is a list of voltage readings, with respect to ground (0V), taken on the prototype receiver around the semiconduc-
PSU/CHARGER	20V d.c. range with an input impedance of 10 megohms.
Resistors           R39, R40 15Ω         0.6W 1% metal film (2 off)           R41         82Ω 1W           R42         200Ω 1W	IC1 Pins 1, 2, 15, 16 12V IC5 Input 15V IC1 Pins 3 to 5 5-2V IC5 Common 0V IC1 Pins 6 to 8, 10 0V IC5 Output 12V IC1 Pins 9 12 to 14 6V
Capacitors     TALK       C30, C31 22n ceramic disc (2 off)     C32       C32     470μ radial elect. 35V	IC1 Pin 11 either 0V or 12V depending on S1 TR1 Gate TR1 Source 0·7V
Semiconductors D1, D2 1N4002 1A 100V rect. diode (2 off)	IC2 Pins 1 to 3, 5 to         6V         TR2 Collector         10.7V           10, 12 to 14         6V         TR2 Collector         10.7V           IC2 Pin 4         12V         TR2 Base         7.8V
Miscellaneous T1 230V mains transformer, with 6VA 20V-0V-20V secondaries	IC2 Pin 11         0V         TR2 Emitter         7.1V           IC3 Pin 1, 8         7.6V         TR3 Collector         10.1V
FS1 100mA 20mm fuse, with panel mounting fuseholder S2 d.p.d.t. switch S3 d.p.d.t. mains toggle switch	IC3 Pin 2 to 7,         TR3 Base         2·8V           10 to 12         0V         TR3 Emitter         2·2V           IC3 Pin 9, 13         0·2V         0·2V         0·2V
NiCad (12 off), with holder; 3-core mains cable, fitted with IEC female plug; mounting bolts; solder etc.	IC3 Pin 14         16V         TR4 Collector         11·7V           TR4 Base         2·1V           IC4 Pin 1         8·3V         TR4 Emitter         2·4V
Approx Cost Guidance Only	IC4 Pin 2, 16         12V           IC4 Pin 3 to 6         6V         TR5 Collector         12V           IC4 Pin 7 to 15         0V         TR5 Base         5V           TR5 Emitter         7.7V

Finally, the integrated circuits (i.c.s) can be plugged into place. Again, be particularly careful to get them the right way round.

### PRELIMINARY CHECKS

Check the printed circuit board thoroughly for dry joints and shorts. Also check once more that all components are inserted in the right place and if polarity conscious the right way round. A few minutes checking these things now could well save hours of fault finding at a later stage.

Next, measure the resistance between the *output* side of the voltage regulator IC5 and ground (0V). This should be around 1000 ohms. If it is dramatically higher or lower than this value then you have a problem, so re-check everything on the board.

If all is well apply 15V d.c. (observe polarity) to the circuit. Place an ammeter in line, around 60mA should be being drawn, gross deviations from this indicate a fault condition, you cannot proceed until this figure is correct.

Temporarily connect up loudspeaker LS1 and a.f. gain potentiometer VR1. Re-apply power to the board and if all is well a fair amount of "hiss" should be evident from the loudspeaker with VR1 set to maximum resistance.

If a frequency counter or oscilloscope is available then examine pin 4 of 1C4 with a "times ten" (X10) probe. A frequency of around 2MHz (squarewave approx. 12V pk/pk) should be available and should be adjustable by turning the core of coil L3.

Try applying 0V and 12V to the junction of R29 and C23 and the frequency should jump by around 600kHz. If all is well so far and there are no significant differences between the voltages given in Table 1 then all is probably correct.

### FINAL ASSEMBLY

Before anything is attempted, holes for the three potentiometers, two (three) switches, the BNC socket, the power inlet socket, the four mounting holes for the main p.c.b. and the loudspeaker grille must be drilled.

If the case you are using is a plastic one then it is a good idea to glue a piece of aluminium foil just slightly larger than the size of the board directly below where the p.c.b. is to be mounted. This prevents hand capacitance from causing the v.f.o. to change frequency and also helps prevent unwanted r.f. getting at the audio stages. The foil must be "earthed" and this can be accomplished through the mounting posts for the board.

If you want to label the control panel with Letraset, or similar, then now is the time. Once the controls and sockets are installed the task becomes infinitely more difficult. Don't forget to lacquer the front and rear of the box to prevent the Letraset from getting rubbed off.

COMP	ONENTS Approx	x Cost nce Only £	50 excluding case			
RECEIVER						
Resistors R1, R6, R29 R2, R16 R3, R9, R10, R33 R4 R5 R7, R27 R8, R11 to R14, R17, R14, R17,	150k (3 off)         2k2 (2 off)         33001(4 off)         22001         1k         33k (2 off)         TALK	C14, C16 C15, C17 C19 C21 C23 C24, C28 C25 C29 VC1	10n polyester (2 off) 3n3 polyester (2 off) 1000μ radial elect, 25V 470μ radial elect., 16V 1μ radial elect., 16V 22n polyester (2 off) 330p ceramic plate 22μ radial elect., 16V 22p miniature film trimmer			
H18, H20 to R26, R31 R15 R19 R28 R30, R34, R35, R37 R32 R36 R38 All 0.6W 1% me Potentiomete VR1, VR3	10k (15 off) 1k2 560k 4Ω7 47k (5 off) 100Ω 560Ω 82k tal film <b>rs</b> 100k rotary carbon, lin. (2 off) 100k 10-turn rotary, lin.	Semiconduct VD1 to VD5 TR1 TR2 to TR5 IC1 IC2 IC3 IC4 IC5	KVT235 triple a.m. tuning varicap diode (2 off – see text) 2N3819 <i>n</i> -channel f.e.t. BC548 <i>npn</i> transistor (4 off) 4053BE triple 2-channel analogue multiplexer TL074 quad low-noise f.e.t. op.amp LM380 power op.amp 4520BE dual binary counter 7812 12V 1A regulator			
Capacitors C1, C2, C5, C22 C3, C11, C20 C4 C6 to C9, C18 C26, C27 C10 C12 C13	100n polyester (5 off) 10μF radial elect. 16V (3 off) Not fitted (see text) 22n ceramic disc (7 off) 100n ceramic disc 100p ceramic plate 47n ceramic disc	L1, L2, L3 S1 Printed circu the EPE PC loudspeaker, 8 suit; BNC ch (SK1); knob (3 VR2; multistran pins; solder etc	Toko KANK3333R inductor (2 off) Toko KANK3334R s.p.d.t. toggle switch uit board available from <i>B Service</i> , code 116: Ω 76mm dia.; case to assis mounting socket 0 off); counting drive for o connecting wire; solder			

Everyday Practical Electronics, October 1996

Once this has been completed, the loudspeaker LS1 can be glued into position behind the speaker grille and the p.c.b. bolted into position and interwiring commenced, following Fig. 5. Connect up controls VR1, VR2 and VR3, loudspeaker LS1, the switches and the BNC socket SK1 (the latter should ideally be connected with 50 ohm coaxial cable but audio screened lead will suffice). It is also desirable but not absolutely essential that the two varicap tuning feeds are via screened cable also, thin audio type cable is ideal.

### ALIGNMENT

Don't worry, there are only four items to adjust and no test equipment is required. If a counter is available then that's fine but not essential. Similarly an r.f. signal generator and oscilloscope would be useful. If you have these then connect as follows: Oscilloscope across the loudspeaker; Counter to pin 4 1C4, via a X10 probe, and R.F. Generator to the aerial input socket SK1.

The v.f.o. needs to be aligned first. Set preset capacitor VC1 midway. Tuning pot. VR2 to its "earthy (0V)" end and adjust the core of coil L2 until the counter reads 1725kHz.

If a counter is not available then attach a small length of wire to pin 5 of IC4 and tune a Medium Wave radio (preferably one with a digital readout) to 864kHz (343 metres). Adjust the core of L2 until a carrier is received.

Now adjust VR2 to its "hot" end (fully clockwise) and adjust VC1 until the counter reads 2025kHz. Alternatively,

using the Medium Wave receiver tune to 1008kHz (298 metres) and adjust VC1 until a carrier is heard.

These two previous adjustments will interact and so should be repeated until the two band edges are correctly defined. The actual coverage will be 1725kHz to 2025kHz on the lower range and 3450kHz to 4050kHz on the upper range.

Of course, it is possible to change the frequency coverage to suit personal needs. Lowering the values of resistors R37 and R38 will increase the tuning range at the expense of resolution. The two frequency ranges covered will always be harmonically related and the upper frequency limit will be around 6MHz.

Now the front end can be aligned. Set the v.f.o. to 3450kHz, i.e. high range and VR2 at its earthy end. Set Preselect control



Fig.5. Interwiring details for the power supply and between off-board components and printed circuit board.



Layout of components inside the completed prototype receiver.

VR3 so that there is 5V on its wiper (w) and either connect an antenna or apply a signal from an r.f. generator, 100 microvolts, unmodulated and 3451kHz.

A 1kHz tone or noise should be heard from the loudspeaker depending on the signal source. Adjust the ferrite cores in coils L1 and L2 for maximum as observed on the oscilloscope (or ears), reducing the signal strength as appropriate to prevent overloading.

The sensitivity can be measured if the generator is calibrated and should be better than one microvolt for 12dB SINAD. This has not been checked and is of little consequence on 1.f. bands due to the high natural noise level.

SINAD (signal-to-interference, noise and distortion ratio) is a measure of readability, the term is similar to signal-to-noise ratio as used to evaluate hifi equipment. A SINAD of 12dB basically means that the signal is 12dB or about 16 times more powerful than all interference, noise and distortion put together.

### POWER SUPPLIES

Choice of power supply is very much up to the individual. The supply can be from dry cells, NiCads or from the mains via a suitable step-down unit.

The regulation of the latter must be good in order to ensure that the LM380 doesn't get too much voltage when the volume is turned down low. Either use a regulated supply or at least use a good quality transformer with say 10 per cent regulation or better. Make sure that the unloaded voltage is *less* than 18V.

The prototype is run from 12 AA type NiCads which have a 600mAH capacity and so will run the set for about eight hours continuous. Also included is a charging circuit which can be active whilst the receiver is in use, see Fig. 2.

The charge rates are about 10mA when switched on (70mA diverted to power the set) and 50mA to 60mA when switched off and in charge mode (recommended charge rate for AA cells). A completely discharged set of NiCads will take about 15 hours to fully recover.

### ANTENNAS

The Receiver requires a good antenna/aerial in order to function properly. This should ideally be resonant although a half-wave dipole for topband would be 75 metres long, supported at each end via an insulator and centre fed with coaxial cable.

This is obviously not going to be possible in a lot of cases! A good compromise is a random length long wire antenna running the length of the garden.

Do note that indoor antennas are not recommended. These tend to pick up far too much interference from domestic appliances. A foot (30.5cm.) of wire outdoors is better than 10ft (305cm.) in the loft!

A good "earth" will also help enormously. A metal rod driven into the ground two or three feet is fine. Remember that water or gas piping may not be a good ground due to the modern practice of using plastic pipes. When using an aerial and earth setup such as this an aerial tuning unit

(ATU) will

improve reception enormously. The ATU matches the impedance of the antenna to the impedance of the receiver's input terminals (50 ohm unbalanced).

One possibility for people with limited space is an active antenna. These consist of a small loop or "whip" and an amplifier.

Results can be very good, mainly because the unit can be positioned away from sources of interference. The disadvantage is the need to remotely power the device and also the need to waterproof the amplifier unit.

### IN USE

The Receiver is very easy to use, expect a little warm up drift of the order of a couple of kilohertz. Simply adjust the Preselector (VR3) for maximum loudness and tune in stations with VR2, the Tune control.

If you have never tuned in an SSB station before then a little patience and practice soon leads to reliable results. In order to obtain natural sounding speech you have to hit on the right frequency to within about 50 Hertz or so or you will end up with people sounding like "Donald Duck".

When there are a group of amateurs on a "Net" then they will seldom all be on exactly the same frequency so don't worry, the name of the game is communication certainly do not expect "hifi".

Do not use VR3 as a volume control, use VR1 the A.F. Gain control, failure to observe this protocol will result in reduced performance. One thing that has been noticed is that local stations are LOUD, this is due to the lack of any a.g.c. (automatic gain control).

In conclusion, I hope you have many hours of fun both building and operating the Direct Conversion Receiver. I have a number of receivers in the shack that cover 160/80 metres but for its simplicity, this little box of tricks rivals the best of them in terms of selectivity, sensitivity and audio quality.

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### Drink Aid for the Blind

AN ELDERLY member of my congregation having gone blind, had great difficulty in making a cup of tea. She couldn't tell whether she had poured enough milk or enough hot water.

The simple solution to this problem is shown in Fig. 1. It is an audio oscillator based around IC1, a 555 astable which drives a piezo dise directly.

Transistor TR1 acts as a switch which will enable the audio oscillator when the two probes detect liquid. By using two sets of probes formed at different lengths (see inset diagram), the audio alarm will activate when enough milk and then water, has been added.

The circuit is powered by a small 12V battery (e.g. MN21 type) which should give many years continuous service as the quiescent current is virtually nil.

The device was housed in a small circular plastic box, approximately 4cm in diameter. The probes were formed from sheathed, thick solid-core copper wires protruding from either side, so that the container could clip onto the side of the cup.

Rev. Thomas Scarborough, Fresnaye, South Africa.



Fig. 1. Circuit diagram and possible probe arrangement for the Drinks Aid for the Blind. Note, the longest probe is for the milk level.

### **Chart Recorder Input Attenuator**

- 1 m



Fig.2. Chart Recorder Range Extender circuit.

THE CIRCUIT diagram shown in Fig. 2 was designed to adapt a laboratory chart recorder with 100mV input for full-scale deflection, to accept input voltages of 1V, 2V, 5V or 10V at the flick of a switch.

The op.amp IC1 is configured as an inverting amplifier, whose feedback resistance is much less than the input resistance (R1), therefore the output voltage will be a fraction of the input signal. Range switch S1 selects four different feedback resistors which consist of fixed metal film resistors and a 20-turn cermet trimmer, which is adjusted to give 100mV output at the selected input voltage range.

For example, on the 2V range, if  $R_{IN}$  is R1 (1M) and  $R_{F}$  is the feedback resistor value, then  $V_{OUT} = -R_{F}/R_{IN} \times V_{IN}$ . By setting the input value at 2V and the output at 100mV,

$$V_{OUT} = \frac{(R3 + VR2)}{R1} \times V_{IN}$$
  
so  $(R3 + VR2) = \frac{(10^{-2} \times 1^{6})}{2}$   
and  $(R3 + VR2) = 50,000$ 

If R3 is set at 47 kilohms (47k) then VR2 is trimmed to 3k. In practice VR2 should be adjusted to give 100mV output at 2V input. The other ranges are set up in the same manner.

Frank Sweeney, Glasgow

### Heads or Tails Indicator

- fifte cff [t cff e U DESIGNED to simulate by electronic means the tossing of a coin, the simple circuit of Fig. 3 is based upon a 4049 HEX inverter i.e., of which two inverters are used. IC1a and IC1b are wired as an astable oscillator which causes two l.e.d.s (light-emitting diodes) D1 and D2 to alternate rapidly, at a frequency too high to be distinguished by the naked eye. Both l.e.d.s. therefore appear to be constantly illuminated.

When the "Spin" switch S2 is closed, this has the effect of freezing the display, and the l.e.d. which was illuminated at the instant the switch was closed will now be continuously alight. Opening the switch enables the oscillator onec more.



Fig.3. Circuit diagram for the Heads or Tails Indicator.

I found that there was an equal chance of either l.e.d. lighting, and the circuit can be used in board games, for example, to choose which player will move first.

Mark McGuinness, Clondalkin, Dublin, Ireland.

### **Please Take Note**

Mini Roulette – August 1996

*Page 643, Fig.2.* IC1 pins 2 and 6 should be connected to capacitor C1 negative.

# **Ohm Sweet Ohm** Max Fidling

## Fore!

Golf, to me, is a pretty futile kind of sport. I can't see the point of hitting a golf ball with one of those golf sticks and taking all day to do it. Why not just carry it over and drop it in by hand? Much simpler!

Which brings me to the subject of *trolleys*, as in electrically powered golf ones. It appears that you have not arrived in the golfing fraternity until you've bought an electric trolley to hold your golf "bats" and paraphernalia. I always thought that the idea of this sport was to get some exercise, so having a motorised caddy thing was defeating the object, if you ask me.

So anyway, Terry, an acquaintance of mine, was an avid golf player and he would be found on the greens most Saturdays. After a few rounds he and his opponents would venture to the bar for "a few more rounds of the other sort" (his standard joke), and it was at the Club watering hole that the subject of electric trolleys cropped up.

One of his fellow players owned such a beast which had an annoying intermittent fault. What was needed, they concluded, was someone who could check it out (preferably for no charge) and fix it accordingly. Guess who? *Correct!* Fidling's name was volunteered!

My friend's car drew up outside the house and the electric trolley was thus delivered. Trundling it up the garden path to the shack, I manoeuvred this thing into the shed, complete with its recharger, and I set about it with the ''talking voltmeter'' and multi-coloured screwdriver set.

The cat was busily scoffing his lunch, the shack taking on a heady fragrance of *rabbit and salmon* cat food. This mingled well with the smell of freshly-mown grass, because I'd put the lawnmower in there as well.

So with hardly any room to spare in the shack, one foot rested on the mower

and I contorted myself around this gadget awkwardly, occasionally getting a whiff of cat food. Piddles munched on blithely.

### **Bunkered**

The trolley had a likely-looking electrical cover which came away with a few twiddles of the screwdriver. Clicking a few switches and generally fiddling around pulling at things (because I hadn't the faintest idea how it worked), had no effect, but the talking multimeter confirmed that there was life in the old thing yet. "Six Point Three Volts!" it declared triumphantly, as I poked it across a small lead-acid battery.

The moggy mooched over, having decided to leave the rest of his grub (typical), and sniffed one of the tyres of the trolley. By now I was hanging precariously over the mower, more like a circus contortionist than a member of the electronics elite, and I shooed the cat out of the way with my spare foot as I fidgeted and tugged the electrical innards of the trolley a little more, balancing agilely on the lawnmower and bending over to rummage.

Piddles, sensing an opportunity to bug me, ambled in the way again, his tail tickling my nose as I tried-to finish screwing the trolley's electrical box together once again! As usual, I had a few too many screws remaining over, but they'll never know, I told the cat, as I tipped them into a jam-jar I kept for the purpose. Funny how screws never seem to go back the same way.

### **On A Charge**

Stuffing the trolley up against the mower to make more room, I turned my attention to the recharger thingy which was moulded into a large mains plug. This plugged into the trolley and I took it apart in a jiffy.

Reaching out to the shelf near the bench, I grabbed my favourite tin of



*ElectroLube* and started to squirt this inside the recharger liberally, followed by a good blast of air duster to round things off impressively, as I disappeared temporarily in a cloud of aerosol spray. (Useful thing, air duster: it's good for splatting flies on the window of the shed and rendering them senseless.) Everything looked ship-shape and I screwed the recharger unit back together.

I teetered over the trolley once more, standing with one foot on the mower, having given up hope of finding a fault. Before calling it a day I gave the onoff switch one last tug by grabbing the handle and squeezing the switch. The trolley immediately burst into life like a mad Hoover possessed!

With a motorised *whirr* it careered aimlessly out of control, hitting the cat's halfempty food bowl, and scattering the morsels of *Rabbit and Salmon* everywhere! Letting go of the switch, the demonic golf trolley stopped and stood to attention, as though controlled by an unforeseen hand.

*Yikes!* What a mess! Piddles, fearless as ever, started lapping up the surplus grub. Meantime, I'd had enough - and I'm not sure to this day if the owner fathomed out why his trolley was returned smelling distinctly of rabbit and salmon!

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Software programs for the following *EPE* projects (PIC-microcontrolled except for Met Office) are available altogether on a *single* 3·5 inch PC-compatible disk, or as needed, via our Internet site: Met Office (Dec '95 – GWBasicO; Simple PIC16C84 Programmer (Feb '96); PIC-Electric Meter (Feb '96); PulStar (June '96); Games Compendium (July '96); PIC-Tock Pendulum Clock (Sept '96); PIC Disassembler (unpublished). The disk (order as "PIC-Disk") is available from the *EPE PCB Servie* at £2.50 (UK) to cover our admin costs (the software itself is *free*). Overseas £3.10 surface mail, £4.10 airmail. Alternatively, the software files can be downloaded *free* from our internet FTP site: ftp://ftp.epemag.wimborne.co.uk

### EPE PRINTED CIRCUIT **BOARD SERVICE Order Code** Project Quantity Price

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Everyday Practical Electronics, October 1996

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**O**UR World Wide Web site (http://www.epemag.wimborne. Co.uk) is up and running and we hope you'll drop in at regular intervals. It is constantly being updated, and you can also link to the *Dept. of Electrical Engineering, University* of Hull to see the latest developments on their "Mouse Organ" student assignment. Also, our FTP site is located at ftp://ftp.epemag.wimborne.co.uk where we are uploading various PIC and support files.

### Snaffle more Stuff with FTP

File Transfer Protocol (FTP) is the means by which you can copy files residing on the Internet, onto your own computer. You might want to download anything from simple text files to software applications, bug fixes or perhaps the latest drivers for your hardware. You'll frequently hear references to "anonymous FTP". *Anonymous* implies that *anybody* can connect to a remote "FTP Server" to copy (download) files onto their own "local" computer. You can FTP using basic terminal-type software from a DOS prompt equivalent, but your life will be made much happier with graphical programs running in, say, Windows. A slight handicap for DOS users is that most FTP servers run the Unix operating system as standard.

We've uploaded all available computer-based files (e.g. for our PIC projects) to our own FTP server in the /pub/PIC'S directory and these are freely available to you as "anonymous FTP users". Proceed as follows if you've not done this before. I have to assume for now that you're using Windows-based software.

Open an FTP session and you'll be prompted for the location or address of the FTP server. Enter just **ftp.epemag.wimborne.co.uk** – when it asks you for a password, you would normally type in your full E-mail address, since most transfers are logged. This will be sufficient to enter and then navigate your way around.

You can't damage FTP servers – they won't let you delete or rename any files. Remembering that you'll be on a Unix machine; these have a directory and file structure pretty similar to those in DOS or Windows, but there are some differences.

Unix uses the forward slash (/) in file pathnames. You may be confronted with /pub/docs/epe\_info.txt as a file pathname. Unix files and directories can also have longer names, for example pub/PICS/games.compendium

With graphical-based software, all you need do is double click on "folder" symbols to open out that directory on-screen: it's exactly like using Windows File Manager or Explorer. It's easy! Navigate your way through the directories on the remote computer until you find what you're looking for. You're compelled to start with our "public" (/pub) directory. Expect some greetings messages to pop up on screen.

Next question: is the file a binary type or an ASCII (text file)? Somewhere on your software, you'll now need to set the file type. Plain text files mostly finish with a \*.txt extension (ours do, anyway.) Software files, graphics, "ZIP" files etc. are binary and you must select this or you will download "garbage". In my experience, ASCII text files generally seem to download OK whichever you select. Now, you're ready to snaffle the stuff!

### Drag Net

Windows-based software (e.g. Turnpike, or Procomm for Windows) should support "Drag and Drop" file transfer. You can navigate around your own local machine using File Manager-type windows. Beforehand, perhaps create a special directory called *incoming* on your machine for receiving FTP downloads. Click on the filename you desire and "drag" it onto your chosen directory.

Release the mouse and after confirmation, the transfer will commence. It could take seconds to many minutes depending on file size and conditions; there may be a progress indicator. You should then use your software's "Disconnect" command (or quit) after the transfer is complete, or instead open another address. With Turnpike, I find I have to both *Disconnect* and *Stop*, to close some sessions.

You can practice on the file epe\_info.txt which I've placed in the /pub/docs directory on our server. Try entering the FTP address in your Web browser, too, and see what happens!

Those using command-line systems (e.g. KA9Q) start with an ftp> prompt where you can type in the following commands; italics represent typical commands displayed. Type the bold text as follows, remembering you're entering *Unix* commands now. open ftp.epemag.wimborne.co.uk

[enter username] anonymous

[enter password] type your full E-mail address here cwd pub/docs [Change Working Directory – cd may work too] ascii [sets ASCII transfer mode] hash [optional: displays a # to indicate transfer progress] get epe\_info.txt [fetches the file epe\_info.txt] quit [disconnects]

### Survival Chart

Also try the massive FTP Server maintained by Demon Internet Services, on ftp://ftp.demon.co.uk where you'll find tons of Amiga. Mac and PC files all available by anonymous FTP. *Niche Software*, for example, have a (binary!) *PCB Designer* demo file called pcbdemo.zip available from ftp.demon.co.uk in the /pub/ibmpc/win3/apps/pcbdemo directory. You'll often fetch zipped (compressed) files and you *must* become familiar with file compression tools such as PKZIP/UNZIP. They are simple but essential.

One text book for novices is *The Complete Idiot's Guide to the Internet* by Peter Kent (2nd edition, Alpha Books, ISBN 1-56761-535-X £18.95). Although Americanised, I recommend it because I like the style very much; it's fun, not patronising and will answer many FTP related questions, and it shows all those essential Unix commands I can't list here, on a fluorescent *Internet Survival Cheat Sheet!* It's good for getting to grips with Internet jargon, too.

### Surf Boarding

It's time to apply the sunblock and strut your surfboard! The on-line version of *Net Work* will be found on our web site, where we've "made" the URL links shown here, to save you having to type them in manually. A worthwhile directory of passive and active components, CPUs, EMC, PCBs and more, is maintained in Belgium by Vincent Himpe on http://www.ping.be/~ping0751

Thanks to Steve Walton for the pointer to http://www.parallaxinc.com for PIC development tools, BASIC Stamps with more links leading off. Steve also mentions http://www.albany.net/allinone/ as a useful (Top 5% Site) source of Internet search engines. It looks good – I'll be looking at search engines in a future column.

Follow the alt.comp.hardware.homebuilt newsgroup? The FAQ and lots more will be found on Dave Baldwin's FTP site ftp://ftp.netcom.com/pub/di/dibald, says Tom Boyd. I saw Amstrad PCW and Notepad files there too. A fundamental Teach-In style package of self-study material on digital electronics is posted in Hong Kong from http://www.hkstar.com/~hkiedsci which is intended for high-school students.

You can see the latest version of the Digital Storage Scope FAQ maintained by John Seney on http://www.mv.com/ipusers/wd1v (that's wd-one-v). There are many links for robotics fans, radio hams and Macintosh users too. Theremin enthusiasts will be intrigued by http://www.Nashville.Net/~theremin/EPEArticle.html.

See you next month. My E-mail address is: alan@epemag.demon.co.uk.

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VIDEO PROCESSOR UNITS?/6v 10AH BATTS/12V 8A TX Not too sure what the function of these units is but they certainly make good strippers! Measures 390X320X120mm, on the front are controls for scan speed, scan delay, scan mode, loads of connections on the rear. Inside 2x 6v 10AH sealed lead acid batts, pcb's and a 8A? 12v torroidial transformer (mains in). Condition not known, may have one or two broken knobs due to poor storage. £17.50 ref VP2

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