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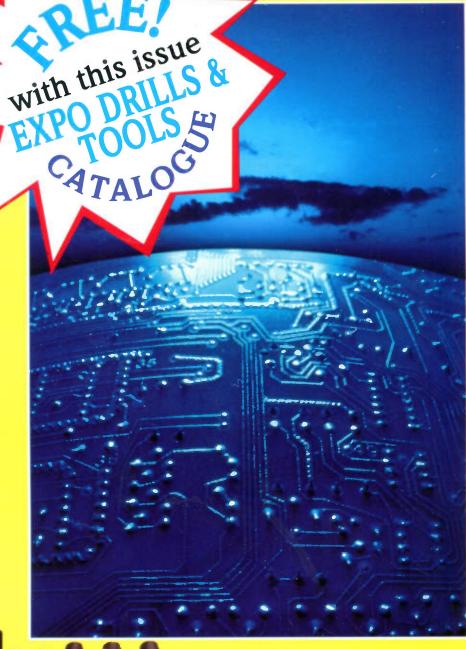
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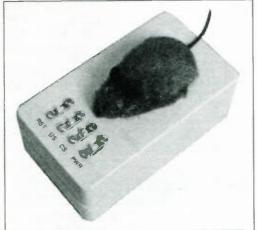
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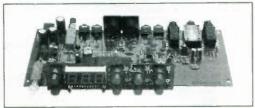
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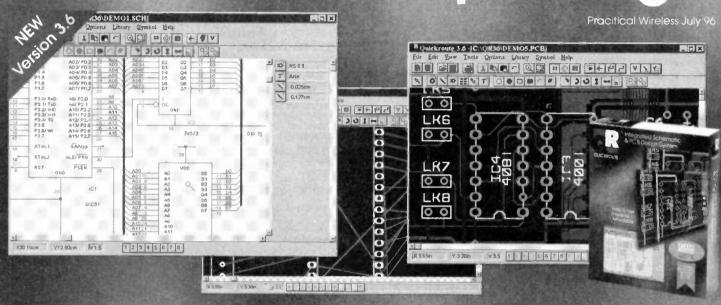




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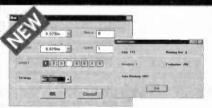
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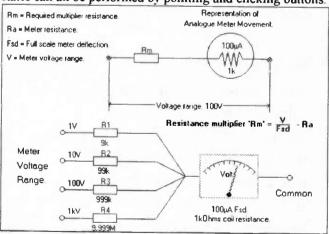
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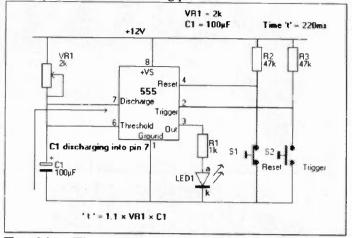


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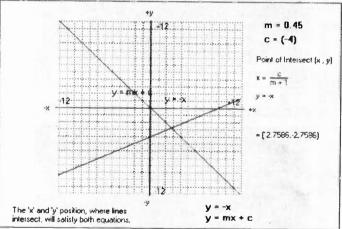
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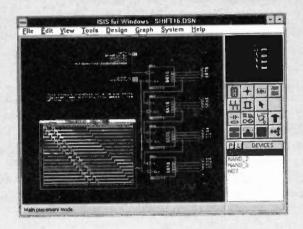
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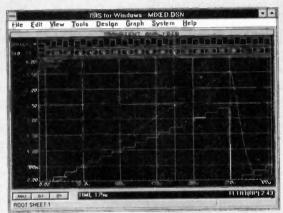
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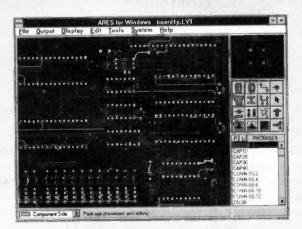
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Stepping Motors

MD38...Mini 48 step...£8.65 MD35...Std 48 step...£12.98 MD200...200 step...£16.80 MD24...Large 200 step...£22.95

8

SIMPLE PIC PROGRAMMER

PRICE!

PC BOARD & INSTRUCTIONS

INCLUDES 1-PIC16C84 CHIP SOFTWARE DISK, LEAD CONNECTOR, PROFESSIONAL

Kit 857 £12.99

Power Supply £3.99

EXTRA CHIPS: PIC 16C84 £7.36

Based on the design in February '96 *EPE* article, Magenta have made a proper PCB and kit for this project. PCB has 'reset' switch, Program switch, 5V regulator and test L.E.D.s. There are also extra connection points for access to all A and B port pins.

PIC16C84 LCD DISPLAY DRIVER

INCLUDES 1-PIC16C84
WITH DEMO PROGRAM
SOFTWARE DISK, PCB,
INSTRUCTIONS AND
16-CHARACTER 2-LINE
LCD DISPLAY

Kit 860 £17.99

Power Supply £3.99

FULL PROGRAM SOURCE CODE SUPPLIED – DEVELOP YOUR OWN APPLICATION!

Another super PIC project from Magenta. Supplied with PCB, industry standard 2-LINE x 16-character display, data, all components, and software to include in your own programs. Ideal development base for meters, terminals, calculators, counters, timers – Just waiting for your application!

★ Chip is pre-programmed with demo display ★

SUPER PIC PROGRAMMER

- READS, PROGRAMS, AND VERIFIES
- WINDOWS® SOFTWARE
- PIC16CXX AND 16C84
- USES ANY PC PARALLEL PORT
- USES STANDARD MICROCHIP ◆ HEX FILES
- OPTIONAL DISASSEMBLER SOFTWARE (EXTRA)
- PCB, LEAD, ALL COMPONENTS, TURNED PIN SOCKETS FOR 18, 28, AND 40 PIN ICs.

• SEND FOR DETAILED INFORMATION – A SUPERB PRODUCT AT AN UNBEATABLE LOW PRICE.

Kit 862 £29.99

Power Supply £3.99

PIC STEPPING MOTOR DRIVER

INCLUDES: PCB, PIC16C84 WITH DEMO PROGRAM, SOFTWARE DISK, INSTRUCTIONS AND MOTOR. Kit 863 £18.99

FULL SOURCE CODE SUPPLIED. ALSO USE FOR DRIVING OTHER POWER DEVICES e.g. SOLENOIDS.

Another NEW Magenta PIC project. Drives any 4-phase unipolar motor – up to 24V and 1A. Kit includes all components and <u>48 step motor</u>. Chip is pre-programmed with demo software, then write your own, and re-program the same chip! Circuit accepts inputs from switches etc and drives motor in response. Also runs standard demo sequence from memory.

PIC16C84 MAINS POWER 4-CHANNEL CONTROLLER & LIGHT CHASER

 WITH PROGRAMMED 16C84 AND DISK WITH SOURCE CODE IN MPASM Now features full

- ZERO VOLT SWITCHING –
 10 CHASE PATTERNS
- OPTO ISOLATED
- 4 X 3 KEYPAD CONTROL
- SPEED CONTROL POT.
- HARD FIRED TRIACS
- 4 CHANNELS @5 AMPS

4-channel chaser software on DISK and pre-programmed PIC16C84 chip. Easily re-programmed for your own applications. Software source code is fully 'commented' so that it can be followed easily.

Kit 855 £39.95 LOTS OF OTHER APPLICATIONS

PIC16C5X

IN CIRCUIT EMULATOR – WITH ON-LINE MONITOR.

The easiest way to get started. Allows single stepping through programs displaying the internal registers and driving the I/O pins. Software and hardware can be developed and tested together. Programs 16C54, 5, 6, & 7 chips. Full featured software runs under DOS at high speed

Kit 853 £99.00

Power Supply £8.99

SERIAL PC LEADS 9-WAY **£6.00** 25-WAY **£7.00**

WITH OPERATING

PROGRAMMING, AND CROSS ASSEMBLER

SOFTWARE.

RUNS WITH

ANY P.C

68000 DEVELOPMENT AND TRAINING KIT

- USED WORLDWIDE IN SCHOOLS COLLEGES & UNIVERSITIES
- DOUBLE EUROCARD, 2 SERIAL PORTS
- NOW WITH EXPANDED RAM & ROM
- FULL FEATURED MONITOR & LINE ASSEMBLER IN ROM
- CROSS-ASSEMBLER AND COMMS SOFTWARE DISK

FULL 8MHz 68000 16-BIT DATA BUS
 EXPANDABLE - PIT OPTION 68230

FULL MANUAL PLUS DATA
 SUPER LOW PRICE:

KIT 601.....**£69.95**

EXTRAS: 9-way P.C. lead **£6.99** 25-way P.C. lead **£6.99**

Case – black bottom, clear lid – £5.99

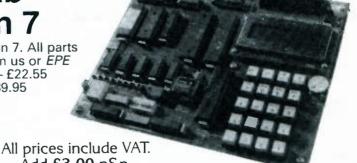
PSU +5V, +12V, -12V **£12.99**

Mini-Lab & Micro Lab Electronics Teach-In 7

As featured in *EPE* and now published as Teach-In 7. All parts are supplied by Magenta. *Teach-In* 7 is £3.95 from us or *EPE* Full Mini Lab Kit – £119.95 – Power supply extra – £22.55 Full Micro Lab Kit – £155.95 Built Micro Lab – £189.95



Tel: 01283 565435 Fax: 01283 546932







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MI	Sockets
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Air.	
Stamped Pin	
8 Pin DIL 0.3"	£0.06
14 Pin DIL 0.3"	£0.11
16 Pin DIL 0.3"	£0.11
19 Dis DIL 0.3"	£0.13
20 Pin DIL 0 3"	£0.12
24 Pin DH 0.6"	£0.13
28 Pin DIL 0.6"	£0.13
20 Pin DIL 0.3" 24 Pin DIL 0.6" 28 Pin DIL 0.6" 40 Pin DIL 0.6"	f0 19
Turned Pin	40.11
	£0.11
	£0.27
16 Pin DH, 0.3"	£0.31
18 Pin DIL 0.3"	€0.35
20 Pin DIL 0.3"	60.39
24 Pm DIL 0.6"	£0.39
28 Pin DIL 0.6"	£0.40
40 Pin DIL 0.6"	£0.46 £0.41 £0.78
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SIL Header Strip	
1 x 36 Way Straight	£0.38





PCB Box Headers



PCB Latch

10 Way Straight	£0.50	
16 Way Straight	£0.70	
20 Way Straight	£0.78	
26 Way Straight	£1.00	
34 Way Straight	£0.86	
34 Way Straight 40 Way Straight	£1.56	
50 Way Straight	£1.29	
10 Way 90°	£0.58	
16 Way 90°	£0.78	
50 Way Straight 10 Way 90° 16 Way 90° 20 Way 90°	£0.82	
26 Way 90°	£1.06	
34 Way 90°	£1.14	
40 Way 90°	£1.64	
50 Way 90°	£1.74	

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			Day of
4	Way	DIL	£0.5
6	Way	DIL.	£0.5
4	Way	DIL	£0.9

Z4 Way Dit.	20.70
40 Way DIL	£1.02
Transistion Head	ers
10 Way Transistion 14 Way Transistion	£0.49
14 Way Transistion	£0.47
16 Way Transistion	£0.47
16 Way Transistion 20 Way Transistion	£0.54
26 Way Transistion 34 Way Transistion	£0.62
34 Way Transistion	£0.67
40 Way Transistion 50 Way Transistion	£0,90
50 Way Transistion	£1.02

D Type Connectors



Solder Bucket	
9 Way Male Plug	£0.29
9 Way Female Socket	£0.30
15 Way Male Plug	£0.39
15 Way Female Socket	£0.39
15 Way H.D. Plug	£0.49
15 Way H.D. Socket	£0.78
23 Way Male Pho	£0.49
23 Way Female Socket 25 Way Male Plug	£0.49
25 Way Male Plug	£0.48
25 way remaie Plug	£0.50
IDC Rihbon Moun	ling
9 Way Male Plug	£1.20
9 Way Female Socket	£1.20
25 Way Male Plug	£1.26
25 Way Female Socket	£1.26
Right Angled PCB	

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9 Way Male Plug	£0.37
9 Way Female Socket	£0.35
15 Way H.D. Socket	£0.77
25 Way Male Plug	£0.53
25 Way Female Socket	£0.51
Plastic D Covers	
9 Way Cover - Grey	£0.30
9 Way Cover - Black	£0.30
15 Way Cover - Grey	£0.33
23 Way Cover - Grey	£0.36
23 Way Cover - Black	£0.36
25 Way Cover - Grey	£0.36
25 Way D Cover - Black	£0.36
9 to 9 Cover / Case	£0.96
25 to 25 Cover / Case	£0.86
Audio Connectors	

	with
2.5mm Jack Plug	€0.2
2.5mm Line Socket	£0.16
2.5mm Chassis Socket	£0.09
3.5mm Mono Plug	£0.2-
3.5mm Mono Line Skt	£0.30
3.5mm Mono Chassis Sk	
3.5mm Stereo Plug	£0.3.
3.5mm Stereo Line Skt	£0.3
3.5mm Stereo Chassis Sk	
4" Mono Plug	€0.30
Mono Line Socket	£0.35
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Stereo Line Socket	
4" Stereo Chassis Skt	£0.38
DIN Series	LU.44
2 Pin Line Plug	£0.18
2 Pin Chassis Socket	£0.15
2 11'- 4 - DI	40.1.

District Citie Ski	40.51
3.5mm Stereo Chassis Sk	£0.34
Mono Plug	£0.30
4" Mono Plug 4" Mono Line Socket	£0.35
14" Mono Chassis Socket	£0.40
Stereo Plug	£0.40
Mono Chassis Socket Stereo Plug Stereo Line Socket	£0.38
4" Stereo Chassis Skt	£0.44
DIN Series	20.44
	£0.18
2 Pin Chassis Sooker	£0.15
	£0.27
3 Pin Chassis Socket	
	£0.28
4 Pin Line Plug	£0.24
	£0.26
5 Pin Line Plug 180°	£0.26
5 Pin Chassis Skt 180°	£0.32
5 Pin Line Plug 240°	£0.24
5 Pin Chassis Skt 240	£0.32
5 Pin LinerPlug 360°	£0.24
5 Pin Chassis Škt 360°	£0.32
6 Pin Line Plug	£0.27
6 Pin Chassis Socket 7 Pin Line Plug	£0.32
7 Pin Line Plug	£0.34
7 Pin Chassis Socket	£0.34
8 Pin Line Plug	£0.35
8 Pin Chassis Socket	£0.36
Phono Series	
2795	

a)	
Red Line Plug	£0.20
Black Line Pfug	£0,20
Yellow Line Plug	£0.20
White Line Plug	£0.20
Red Line Socket	£0.20
Black Line Socket	£0.20
Yellow Line Socket	£0.20
White Line Socket	£0.20
Red Chassis Socket	£0.20
Black Chassis Socket	€0.20
Gold Plated Plug - Red	£0.64
Gold Plated Plug - Black	£0.64
XLR Series - metal	

XLR Series - metal	
Maria	
3 Pin Line Plug	£1.50
3 Pin Line Socket	£1.64
3 Pm Chassis Plug	£1.36
3 Pin Chassis Socket	£1.70

EN	OF	
5	BNC Plug 50Ω Solder	£0.
۲.	BNC Plug 50Ω Crimp	£O.
3	BNC Plug 75Ω Solder	£0.
≥.	BNC Plug 75Ω Crimp	£0.
D	BNC Chassis Socket	£0.
5	F Plug - Twist	£0.
_	F Pluy · Crimp	60

RF Connectors

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BNC Plug 50Ω Solder	£0.9
BNC Plug 50Ω Crimp	£0.5
BNC Plug 75Ω Solder	£0.9
BNC Plug 75Ω Crimp	£0.7
BNC Chassis Socket	£0.8
F Plug - Twist	£0.2
F Pluz - Crimn	£0.3
TNC Plug Solder	£1.2
TNC Plug Crimp	£0.7
UHF Plug 5mm Cable	£0.7
UHF Plug I Imm Cable	£0.6
UHF Chassis Skt- Sqr	£0.4
UHF Chassis Skt- Rnd	£0.5
Terminals	









503	
Sub-Miniature	
3A 125V 1A 250V	
5mm Ø Mounting Hole	
SPST 5 x 10mm	£0.58
SPDT 5 x 10mm	£0.60
SPDT C/Off 5 x 10mm	£0.86
DPDT 9.2 x 10mm	£0.66
Miniature	
6A 125V 3A 250V	
6.2mm Ø Mounting Hole	
CDCT 9 . 12	cn

6.2mm Ø Mounting Hole
SPST 8 x 13mm = #0.66
SPDT 8 x 13mm £0.60
SPDT C/Off 8 x 13mm £0.64
SPDT C/O Biased 2 way £1.04
SPDT C/O Biased 1 way £1.04
DPDT 12 x 13mm £0.72
DPDT C/Off 12 x 13mm £0.76
DPDT C/O Biased 2 way £1.28
DPDT C/O Biased 1 way£1.28
Standard
10A 250V Push on terminals
11mm Ø Mounting Hole SPST 18 x 30mm £1.14
SPST 18 x 30mm - £1.14
SPDT 18 x 30mm £1.28
SPDT C/Off 18 x 30mm £1.52
DPDT 21 x 30mm £1,60
DPDT C/Off 21 x 30mm £1.78
Slide Switches



Miniature 300mA 125V 7 x 15mm Mounting Hole DPDT 7 x 23mm £0.15 Standard 1A 125V 5.5 x 12mm Mounting Hole DPDT 12.5 x 35mm £0.24 DPDT C/O 12.5 x 35mm£0.27 Rotary Switches



150mA 250V	
Make before Break	22mm Ø
9.8mm @ Mounting	Hole
I Pole 12 Way	£0.84
2 Pole 6 Way	£0.84
3 Pole 4 Way	£0.84
4 Pole 3 Way	£0.84



Standard Square

IA 250V	مرا
39 x 15MM	
12mm O Mounting Hole	
Non Latching Push to M	ake
Black PTM	£0.60
Red PTM	£0.60
Blue PTM	€0.60
White PTM	£0.60
Latching	20,00
Black	£0.63
Red	£0.63
Blue	£0.63
White	£0.63
Rocker Switches	20.03
Miniature	
6A 250V Solder Tags	
SPST 21 x 14 x 16mm	
DPDT 21 x 24 x 22mm	£0.96
Standard	
15A 250V Push on Tags	

DPDT 21 x 24 x 22mm	£0.96	
Standard		
15A 250V Push on Tags		
SPST 30 x 11 x 22mm	£0.50	
DPD F 30 x 25 x 22mm		
Hluminated		
15A 250V Push on Tags		
SPST 30x14mm Red	£0.84	
DPDT 30x25mm Red	£1.40	
DPDT 30x25mm Amber		
DPDT 30x25mm Green	£1.40	
Relays		
PCB Mounting		
	£1.44	
LA 21VA DEDT LOV		

Relays	
PCB Mounting	
TA 24Vdc DPDT 5V	£1,44
LA 24Vdc DPDT 12V	£1.44
3A 110V SPDT 6V	£0.58
3A HOV SPDT 12V	£0.58
5A LIOV SPDT 6V	£0.72
5A LIOV SPDT 12V	€0.72
5A LIOV DPDT 6V	£0.93
5A 110V DPDT 12V	€0.93
5A 240V DPDT 6V	£1.76
5A 240V DPDT 12V	£1.76
10A 240V SPDT 6V	€1.25
10A 240V SPDT 12V	£1.44
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Computer Accessories Adaptors



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25f Gender Changer	£2.80
9 Male - 25 Female	£2.51
9 Female - 25 Male	£2.67
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9F - 6 Mini Din Female	£2.55
5M Din - 6F Mini Din	£3.02
5F Din - 6M Mini Din	£2.28
Testers / Patch Box	es
Mini Tester 7 LEDs	£6.68
Cheek Tester 18 LEDs	£7.11
Enhanced LED Switches	£15.53
25D Jumper Box M-F	£2.90
25D Patch Box M-F	£7.32
Anti-Static Wrist Strap	£5.30
RS232 Surge Protector	£5.43
Mains Surge Protector	£11.99
Leads & Cables	



1.5m Printer Lead	£3.40
5m Printer Lend	£9.38
10m Printer Lead	£12.38
Serial Printer 25M-9F	£4.20
Serial Printer 25M-25F	£4.45
Null Modem 9F-9F	£3.45
Null Modem 25F-25F	£4.63
Null Modem 9&25-9&25	£5.54
Modem Lead 25M-9F	£4.08
Modem Fead 25M-25F	£4.75
Interlink Lead 25F-9F	£6.50
Interlink Lead 25F-25F	£6.50
Interlink Lead 25M-25M	£6.50
Patch Lead 25M-25M	£4.66
Patch Lead 36M-36M	£5.90
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Power Cable 31 -2 x 312	£1.88
Power Cable 514-2 x 514	£2.24
Power Cable 514-2 x 31/2	€2.24
Power Cable 51 -31/2.51/4	£2.24
Networking	
BNC 1 Piece FMF	£2.40
BNC T Piece FFF	£2.40
BNC Coupler F	£1.02
BNC Coupler M	£1.65
BNC Ratcher Crimper	£17.44
RJ45 IDC Plug	£0.39
Thinner Cable per m	£0.48
riminer Cable per III	141.40

Please Phone for items not Listed



118 x 98 x 45mm	£1.83
150 x 100 x 60mm	£2.51
150 x 80 x 50mm	£2.51 £2.36
Diecast Aluminium	1
50 x 50 x 31mm	£2.24
100 x 50 x 25mm	£2.98
112 x 62 x 31mm	£3.55
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150 x 80 x 50mm	£5.36
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Two Piece Alumin	13.99
133 - 70 - 17	CA OR
133 x 70 x 37mm	£2.08
102 x 102 x 37mm 102 x 70 x 37mm	€1.94
102 x 70 x 37mm	£1.76
133 x 102 x 37mm 102 x 63 x 50mm	£2.19
102 x 63 x 30mm	£1.86
76 x 51 x 25mm	£1.34 £2.90
152 x 102 x 50mm	12.90
1/8 x 12/ x 65mm	£3.62
203 x 132 x /omm	14.68
162 x 63 x 25mm 152 x 102 x 50mm 178 x 127 x 63mm 102 x 102 x 63mm 102 x 102 x 63mm 133 x 102 x 63mm	£4.68 £2.15 £2.57 £3.23
152 x 102 x 65mm	12.57
122 X IVE A /OHIIII	13.23
Steev Aluminium	
Plastic coated steel	top,
Aluminium base	
152 x 114 x 44mm	£4.19
203 x 127 x 51mm 229 x 127 x 63mm	£4.68
229 x 127 x 63mm	£5.62 £3.04
114 x 63 x 57mm	£3.04
Wire & Cable	
Ribbon Cable Price per 300mm (1ft)	
Ribbon Cable Price per 300mm (1ft)	f0
Ribbon Cable Price per 300mm (1ft) 10 Way Grey Ribbon 16 Way Grey Ribbon	£0.11
Ribbon Cable Price per 300mm (1ft) 10 Way Grey Ribbon 16 Way Grey Ribbon 20 Way Grey Ribbon	£0.17
Ribbon Cable Price per 300mm (1ft) 10 Way Grey Ribbon 16 Way Grey Ribbon 20 Way Grey Ribbon 26 Way Grey Ribbon	£0.17 £0.22
Ribbon Cable Price per 300mm (1ft) 10 Way Grey Ribbon 16 Way Grey Ribbon 20 Way Grey Ribbon 26 Way Grey Ribbon	£0.17 £0.22 £0.28
Ribbon Cable Price per 300mm (1ft) 10 Way Grey Ribbon 16 Way Grey Ribbon 20 Way Grey Ribbon 34 Way Grey Ribbon 34 Way Grey Ribbon 40 Way Grey Ribbon	£0.17 £0.22 £0.28 £0.36
Ribbon Cable Price per 300mm (1ft) 10 Way Grey Ribbon 16 Way Grey Ribbon 20 Way Grey Ribbon 34 Way Grey Ribbon 34 Way Grey Ribbon 40 Way Grey Ribbon	£0.17 £0.22 £0.28 £0.36
Ribbon Cable Price per 300mm (1ft) 10 Way Grey Ribbon 16 Way Grey Ribbon 20 Way Grey Ribbon 34 Way Grey Ribbon 34 Way Grey Ribbon 40 Way Grey Ribbon	£0.17 £0.22 £0.28 £0.36 £0.48 £0.53
Ribbon Cable Price per 300mm (1ft) 10 Way Grey Ribbon 16 Way Grey Ribbon 20 Way Grey Ribbon 26 Way Grey Ribbon 34 Way Grey Ribbon 40 Way Grey Ribbon 60 Way Grey Ribbon 60 Way Grey Ribbon 60 Way Grey Ribbon	£0.17 £0.22 £0.28 £0.36 £0.48 £0.53 £0.64
Ribbon Cable Price per 300mm (H) 10 Way Grey Ribbon 16 Way Grey Ribbon 20 Way Grey Ribbon 20 Way Grey Ribbon 34 Way Grey Ribbon 34 Way Grey Ribbon 40 Way Grey Ribbon 60 Way Grey Ribbon Enamiciled Copper En 500 (202) Revi	£0.17 £0.22 £0.28 £0.36 £0.48 £0.53 £0.64
Ribbon Cable Price per 300mm (H) 10 Way Grey Ribbon 16 Way Grey Ribbon 20 Way Grey Ribbon 20 Way Grey Ribbon 34 Way Grey Ribbon 34 Way Grey Ribbon 40 Way Grey Ribbon 60 Way Grey Ribbon Enamiciled Copper En 500 (202) Revi	£0.17 £0.22 £0.28 £0.36 £0.48 £0.53 £0.64
Ribbon Cable Price per 300nm (1ft) 10 Way Grey Ribbon 10 Way Grey Ribbon 20 Way Grey Ribbon 26 Way Grey Ribbon 34 Way Grey Ribbon 40 Way Grey Ribbon 50 Way Grey Ribbon 60 Way Grey Ribb	£0.17 £0.22 £0.28 £0.36 £0.48 £0.53 £0.64 Wire
Ribbon Cable Price per 300nm (1ft) 10 Way Grey Ribbon 10 Way Grey Ribbon 20 Way Grey Ribbon 26 Way Grey Ribbon 34 Way Grey Ribbon 40 Way Grey Ribbon 50 Way Grey Ribbon 50 Way Grey Ribbon 60 Way Grey Ribbon 61 Way Grey Ribbon 62 Way Grey Ribbon 63 Way Grey Ribbon 64 Sway Granuelled 64 SwG Enamelled 65 SwG Enamelled	£0.17 £0.22 £0.28 £0.36 £0.48 £0.53 £0.64 Wire
Ribbon Cable Price per 300nm (Ift) 10 Way Grey Ribbon 16 Way Grey Ribbon 20 Way Grey Ribbon 24 Way Grey Ribbon 34 Way Grey Ribbon 40 Way Grey Ribbon 50 Way Grey Ribbon 60 Way Grey Ribbon Enametled Copper Per 50g (20z) Red 500g reels available 14 SWG Enamelled 16 SWG Enamelled 18 SWG Enamelled	£0.17 £0.22 £0.28 £0.36 £0.48 £0.53 £0.64 Wire
Ribbon Cable Price per 300nm (Ift) 10 Way Grey Ribbon 16 Way Grey Ribbon 20 Way Grey Ribbon 24 Way Grey Ribbon 34 Way Grey Ribbon 40 Way Grey Ribbon 50 Way Grey Ribbon 60 Way Grey Ribbon Enametled Copper Per 50g (20z) Red 500g reels available 14 SWG Enamelled 16 SWG Enamelled 18 SWG Enamelled	£0.17 £0.22 £0.28 £0.36 £0.48 £0.53 £0.64 Wire
Ribbon Cable Price per 300nm (Ift) 10 Way Grey Ribbon 16 Way Grey Ribbon 20 Way Grey Ribbon 24 Way Grey Ribbon 34 Way Grey Ribbon 40 Way Grey Ribbon 50 Way Grey Ribbon 60 Way Grey Ribbon Enametled Copper Per 50g (20z) Red 500g reels available 14 SWG Enamelled 16 SWG Enamelled 18 SWG Enamelled	£0.17 £0.22 £0.28 £0.36 £0.48 £0.53 £0.64 Wire £0.68 £0.72 £0.78 £0.78
Ribbon Cable Price per 300nm (Ift) 10 Way Grey Ribbon 16 Way Grey Ribbon 20 Way Grey Ribbon 24 Way Grey Ribbon 34 Way Grey Ribbon 40 Way Grey Ribbon 50 Way Grey Ribbon 60 Way Grey Ribbon Enametled Copper Per 50g (20z) Red 500g reels available 14 SWG Enamelled 16 SWG Enamelled 18 SWG Enamelled	£0.17 £0.22 £0.28 £0.36 £0.48 £0.53 £0.64 Wire £0.68 £0.72 £0.78 £0.83
Ribbon Cable Price per 300mm (1ft) 10 Way Grey Ribbon 16 Way Grey Ribbon 20 Way Grey Ribbon 20 Way Grey Ribbon 34 Way Grey Ribbon 40 Way Grey Ribbon 50 Way Grey Ribbon 50 Way Grey Ribbon 60 Way Grey Ribbon 60 Way Grey Ribbon 60 Way Grey Ribbon 61 Way Grey Ribbon 62 Way Grey Ribbon 63 Way Grey Ribbon 64 Way Grey Ribbon 65 Way Grey Ribbon 66 Way Grey Ribbon 67 Swog Enamelled 16 SWG Enamelled 24 SWG Enamelled 24 SWG Enamelled 24 SWG Enamelled 25 SWG Enamelled 26 SWG Enamelled	£0.17 £0.22 £0.28 £0.36 £0.48 £0.53 £0.64 Wire £0.68 £0.72 £0.78 £0.83 £0.87
Ribbon Cable Price per 300mm (1ft) 10 Way Grey Ribbon 16 Way Grey Ribbon 20 Way Grey Ribbon 20 Way Grey Ribbon 34 Way Grey Ribbon 40 Way Grey Ribbon 50 Way Grey Ribbon 50 Way Grey Ribbon 60 Way Grey Ribbon 60 Way Grey Ribbon 60 Way Grey Ribbon 61 Way Grey Ribbon 62 Way Grey Ribbon 63 Way Grey Ribbon 64 Way Grey Ribbon 65 Way Grey Ribbon 66 Way Grey Ribbon 67 Swog Enamelled 16 SWG Enamelled 24 SWG Enamelled 24 SWG Enamelled 24 SWG Enamelled 25 SWG Enamelled 26 SWG Enamelled	£0.17 £0.22 £0.28 £0.36 £0.48 £0.53 £0.64 Wire £0.68 £0.72 £0.78 £0.81 £0.83 £0.87 £0.97
Ribbon Cable Price per 300nm (ff) 10 Way Grey Ribbon 16 Way Grey Ribbon 20 Way Grey Ribbon 20 Way Grey Ribbon 34 Way Grey Ribbon 40 Way Grey Ribbon 50 Way Grey Ribbon 50 Way Grey Ribbon 60 Way Grey Ribbon 61 Way Grey Ribbon 62 Way Grawled 63 Way Gramelled 64 SWG Enamelled 18 SWG Enamelled 24 SWG Enamelled 24 SWG Enamelled 25 SWG Enamelled 26 SWG Enamelled	£0.17 £0.22 £0.28 £0.36 £0.48 £0.53 £0.64 Wire £0.68 £0.72 £0.78 £0.83 £0.87

3 x 70 x 37mm	£2.08
3 x 70 x 37mm 2 x 102 x 37mm 2 x 70 x 37mm 2 x 70 x 37mm 2 x 53 x 50mm x 51 x 25mm 8 x 127 x 63mm 2 x 102 x 50mm 8 x 127 x 63mm 2 x 102 x 63mm	£1.94 £1.76 £2.19
2 x /0 x 3/mm	£1./0
3 x 102 x 3/mm	61.04
2 x 03 x 3011111	£1.86
2 × 102 × 50mm	£1.34 £2.90 £3.62
8 x 127 x 63mm	63.62
3 x 152 x 76mm	£4.68
2 x 102 x 63mm	£2 15
3 x 102 x 63mm	£2.57
2 x 102 x 76mm	£4.68 £2.15 £2.57 £3.23
eel/Aluminium	
	l top,
luminium base	
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FIRST FIRST

It's not very often that we can claim a world first - sometimes we are not sure on this so we say nothing, but we have published a number of projects that we have not seen in other electronics magazines from around the world; it is, however, impossible to check every publication. What makes us so sure that the Theremin Midi/CV Interface is a world first is that this is a specialised area of music technology; all the Theremins available are well known, as are the various high technology music interfaces, etc. This is mainly because top level music making is a truly international business.

This is not a project for the beginner and not a cheap one either, with the high cost of p.t.h. printed circuit boards and the special preprogrammed chip, but we are proud to be able to publish the design which would otherwise not have been available to the hobbyist. It is after all a world first!

SECOND FIRST

Of course, we like to be first if we can and this month I'm happy to report another first for EPE. The magazine is the first independent hobbyist magazine to be stocked in Maplin stores throughout the UK. See our Innovations page for more details. Our thanks to Maplin and to our distributors Seymour for making this possible.

THIRD FIRST

We also believe we were the first UK electronics hobbyist magazine to have a Web page and to make much of our project software available free on the Internet (on this last point we believe we are the only magazine in the world presently doing this). Our Web site now carries a back number ordering page and plenty of regularly updated information about the magazine. I'm pleased to say that it is generating interest, orders and congratulatory comments from around the world.

We are, of course, working on a number of new and exciting projects which may also represent firsts. So, stick with us, it should be another interesting year; which brings me to our regular thanks and Seasonal Greetings to all our readers we hope you have an enjoyable and peaceful 1997.



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EARTH RESISTIVITY METER



Your assistance to the local Archeological Society could be invaluable with this simple subterranean site detector at your command.

ESISTIVITY surveying is a method of detecting subterranean features and has been an investigative technique of archaeologists for many years. Archaeological features can often be detected when buried about one metre under the present ground level. Natural features such as gravel or peat beds buried under silt can be detected at much greater depths.

ROBERT BECK

The same survey will detect both natural and archaeological features. In general, the former tend to have ill-defined "soft" edges whilst the latter consist of geometric "man-made" shapes; if it "looks like" the outline of a building, it probably is!

HISTORICAL BACKGROUND

The technique of resistivity surveying was first used by Civil Engineers for investigating the proposed sites of dams, etc. Archaeologists first realised its potential in 1946. These early instruments were powered by hand cranked a.c. generators and used a resistance bridge configuration to perform measurements, similar to the early "Megger" insulation test sets, although the latter used d.c.

The readings were taken by simultaneously winding the generator handle and reading a meter calibrated in Ohms. As a series of readings across a site was required, the procedure was slow and tedious. With the arrival of the transistor, resistivity sets designed specifically for archaeology gradually became quicker to operate.

Early transistor sets progressed through an a.c. bridge configuration, which had to be balanced with a calibrated potentiometer for each reading, to the present commercial instruments which are designed to log the readings directly into a data logger, displaying results in the form of a map on a portable computer in the field.

It is interesting to note in passing that resistivity measurements have recently been used for crack measurement in metals and also in medical applications.

WHAT IS RESISTIVITY?

Resistivity is defined as the resistance of a metre cube of material across opposite faces. It is therefore a standardised way of comparing resistances of various materials:

 $\rho = RL/A$

Where:

 $\rho = resistivity$

R = resistance of material along its

length

= length

A = area of cross section

The principle upon which resistivity surveying works is as follows:

The resistivities of stone, concrete and similar materials are relatively high, whilst the resistivities of nearly all soils are relatively low. Often ditch and pit fillings, which can no longer be seen on the surface, have an even lower resistivity than the surrounding soil.

The combined resistivity of soil and any included material is termed the apparent resistivity. If we measure the resistivity across an area of ground that has a stone block buried somewhere in it, the apparent resistivity will increase at that particular point. Similarly, if we cross the site of a silted-up ditch, the reading will decrease, as illustrated in Fig. 1.

We therefore have a method of detecting building foundations, walls, silted-up ditches and pits, etc. However, various

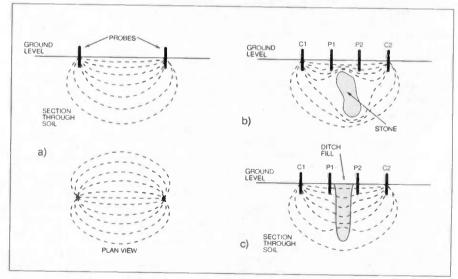
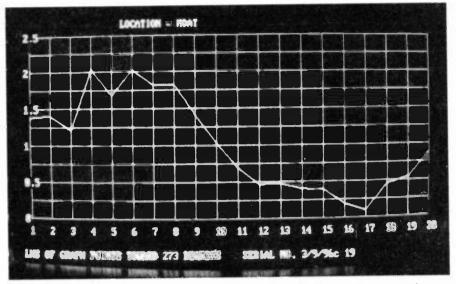


Fig. 1. Current paths set up by probe arrays: (a) current flow between two probes; (b) Wenner (see "Probe Configurations") array with stone below it; (c) Wenner array with ditch below it.



One way of analysing the sample results is to view them as a linear graph on a computer screen.

factors complicate the issue: the resistivity of soil depends upon its actual composition, the moisture present and the amount of compaction.

It therefore follows that taking just one or two readings over a site is meaningless and will convey no useful information to the operator. A series of readings must be methodically taken according to a prearranged plan.

The resistivity meter requires a system of probes pushed into the soil to a depth of about 250mm to make its measurements. Resistivity surveying can therefore be considered a non-destructive technique that will not harm an archaeological site – providing that you do not dig the site to check your results!

It is stressed that digging at sites of potential archeological interest should only be carried out under the supervision of suitably qualified archeologists. Advice on the ethics of amateur resistivity surveying, and about joining Archeological Societies, is given in Part 2, next month.

SOME PROBLEMS

Why can we not make earth resistivity measurements using the Ohmmeter that we already possess in our toolbox? It might be thought that a simple multimeter switched to a suitable Ohms range would be the most cost effective solution to resistivity measurement.

However, these meters use d.c. to perform resistance measurements. This presents some difficulties. The multimeter will respond to the following:

- 1. 50Hz mains derived currents circulating in the ground
- 2. "Battery effect", caused by chemical interaction between probes, and acids or alkalis naturally occurring in soils
- 3. Electrolytic effect of the measuring current passing through the soil.

The first two points are self explanatory but the third may need some clarification.

The electrolytic effect will cause a gradual increase in the contact resistance between the probes and the soil, making the reading on the multimeter gradually rise. This increase in contact resistance is caused by a film of gas coating the probes, due to water in the soil breaking

down into its constituent parts of oxygen and hydrogen under the influence of the measuring current. Try this experiment:

Connect a multimeter, set to the Kilohms range, to two probes pushed into the ground about 200mm deep and 500mm apart. The probes can be pieces of welding rod, metal pipe, etc. Then switch the multimeter on and record the resistance readings against time.

You can see in Table 1 that the readings tend to increase with time and never quite settle down. This demonstrates the electrolytic effect of the measuring current.

Table 1

Time	Kilohms	Kilohms (leads reversed)
0 sec.	6.36	9.66
10 sec.	6.66	10.00
20 sec.	6.76	10.15
30 sec.	6.81	10.28
40 sec.	6.87	10.34
50 sec.	6.91	10.40
1.0 min.	6.95	10.44
1.5 min.	7.06	10.53
2.0 min.	7.17	10.57
2.5 min.	7.23	10.59
3.0 min.	7.23	10.63
3.5 min.	7.30	10.66
4.0 min.	7.30	10.69
4.5 min.	7.28	10.70
5.0 min.	7.36	10.72

It can be seen from the results columns that reversing the leads gives a totally different set of increasing readings. This is the result of the "battery effect" combined with the electrolytic effect.

Change the multimeter to the Millivolts

D.C. setting and you will see a reading of, for example, 150mV, which demonstrates the "battery effect". Set the multimeter range to the Millivolts A.C. setting and a reading of, probably, 3mV to 4mV will be observed, thus indicating mains derived circulating currents.

Having now noted these complications we can consider ways of overcoming them.

SYSTEM REQUIREMENTS

An a.c. square wave oscillator needs to be used for supplying current to the soil. The frequency must not be too low or the electrolytic effect will become noticeable. Equally, the frequency must not be too high or ground inductive effects will become apparent. The frequency must not be a multiple of 50Hz otherwise we cannot use a synchronous rectifier at a later stage to remove unwanted 50Hz signals. The author's preference is to use 137Hz.

The oscillator is used to feed a constant current generator which enables a fixed current to be delivered to the soil, thus avoiding at least one variable. This current is fed into the soil via a pair of probes. known as the C_1 and C_2 probes.

The resultant voltage is picked out of the soil by a second pair of probes, known as the P₁ and P₂ probes and is a 'floating' voltage in that neither probe is at the instrument's 0V rail voltage.

This necessitates the use of a differential amplifier because neither input terminal of the input amplifier can be connected to earth. The input impedance of the differential amplifier should be as high as practical so as to swamp any contact resistance associated with the P₁ and P₂ probes.

The output of the amplifier then goes to a synchronous rectifier so that only those signals which are in phase with the oscillator are rectified. The rectified signal can now be fed to a digital multimeter which makes a convenient readout device. The block diagram in Fig. 2 illustrates the principle.

Any cube of soil that we wish to measure does not exist in isolation, it is part of the whole earth. Therefore the adjacent soil also helps to conduct the current. If a pair of probes is inserted into the soil, the current between them tends to fan out in all directions, gradually weakening as it spreads further from the centre line between the probes (see Fig. 1a).

The effect is analogous to that which can be seen when iron filings are used to trace the lines of force of a bar magnet. In the case of the soil cube, the electrons, being similarly charged, repel each other, to cause the fanning out of the current.

It is possible to connect an a.c. measuring device directly across the probes which

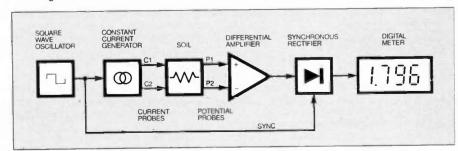


Fig. 2. Block diagram for a basic earth resistivity meter.

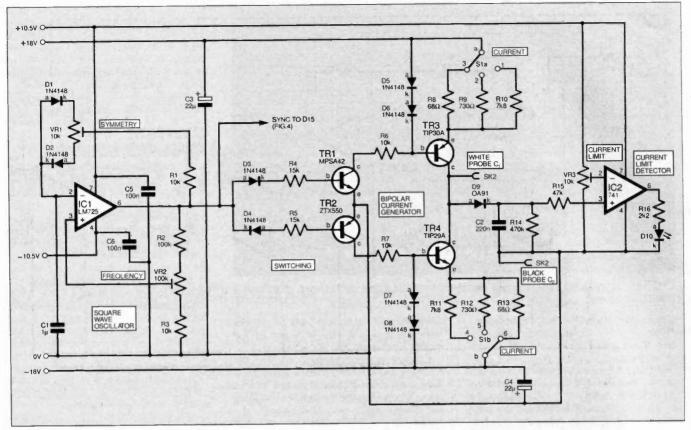


Fig. 3. Circuit diagram for the Current Generator.

are injecting the a.c. into the soil. We would have enough data to calculate the resistance between the probes using Ohm's Law, i.e. R = V/I.

This method does work but it has one major problem in that we are measuring voltage at either end of a hemisphere of current. If we introduce two separate electrodes and use them only for "picking off" a voltage, we have an electrode system that is more depth sensitive.

The reason for this is that, in the case of two probes only, we are measuring the effect of the current mainly running along the surface of the soil. Whereas, in the case of two pairs of probes, we are not measuring the effect of the current that is off the probes' horizontal axis to such a great extent, thereby forcing the probe configuration to be more depth sensitive compared to surface sensitive.

The potential difference being measured is on the flat surface of a hemisphere, not across the opposite faces of a cube. Therefore it follows that we are not calculating actual resistivity, which depends on the particular probe configuration in use. However, there is no need to calculate true resistivity figures, because only relative readings are required.

CIRCUIT DESCRIPTION

Having looked at a bit of theory, let's get right down to earth and describe the circuit for a simple Earth Resistivity Meter. The circuit diagram for the first part of it, the Current Generator, is shown in Fig. 3.

Op.amp IC1, together with its associated components, forms an oscillator giving a square wave output which is balanced about the 0V line, and at a frequency of

137Hz. The output appears at pin 6, with its amplitude being a little below the 10.5V supply rails.

The symmetry of the waveform is accurately set by preset potentiometer VR1 in conjunction with diodes D1 and D2, The precise frequency is set by preset VR2. Capacitor C1 forms part of the time constant for the oscillator.

A non-polarised polyester capacitor must be used for C1. It should not be an electrolytic capacitor as this would have a certain amount of leakage current, which may vary with temperature, and cause the oscillator to drift from the desired frequency.

The output at IC1 pin 6 is passed to the switching circuit, formed around transistors TR1 and TR2, which "enables" either the positive or negative half of the bipolar current generator, as appropriate. Positive constant current is generated by TR3 in conjunction with diodes D5 and D6, and selectable emitter load resistors R8 to R10. Negative constant current is similarly generated by the circuit around TR4, D7, D8 and switched resistors R11 to R13.

Selection of the emitter loads is carried out by the dual 3-way switch \$1a/b. The output current range is selectable at 0-1mA, 1mA or 10mA, in order of switch positions 1 to 3.

The selected current is available directly as an output at the collectors of TR3 and TR4, via socket SK1. The amount of current being delivered is detected by the circuit around IC2, which is, in fact, actually a voltage level detector. The voltage level is, of course, relative to the current being drawn via SK1.

Diode D9, resistor R14 and capacitor C2 form a rectifier and smoothing circuit. Op.amp IC2 is configured as a comparator,

with preset VR3 providing the reference voltage.

When the voltage across the current output goes to too high a value, indicating that the current generator is feeding into too high a load, l.e.d. D10 will light. This indicates that an erroneous reading is occurring, because there is insulficient voltage available to drive the demanded current.

In this case, the Current switch, S1a/S1b, should be set to a lower value which would accept a higher load resistance.

The voltage drop in the soil caused by the current driven through it is detected by the P₁ and P₂ probes, which feed their signals to a Differential Input Amplifier comprising IC3a, IC3b, IC4a and IC4b, as seen in Fig. 4.

Over-voltage protection for the dual amplifier IC3 is provided by Zener diodes D11 to D14. Being 9.1V diodes, any voltage between the probe and earth that is above 9.1V will cause one of the diodes to conduct, thus protecting the amplifier.

Amplifier gain is set by selecting one of three resistors, R23 to R25, by the Gain switch S2. The gain may be calculated from the following formula:

Gain = $1 + (2R_{FEEDBACK}/R_{SWITCH})$ thus:

 $Gain = 1 + (2 \times 10000/R_{SWITCH})$

The resistors chosen give switched gains of \times 10, \times 100 and \times 1000.

The amplified signal is passed to IC4b, which acts as a Synchronous Rectifier. A reference signal is obtained from pin 6 of IC1 (Fig. 3) and fed to diode D15. When the cathode (k) of D15 is positive, no voltage will be applied to the gate (g) of field effect transistor (f.c.t.) TR6. This will cause

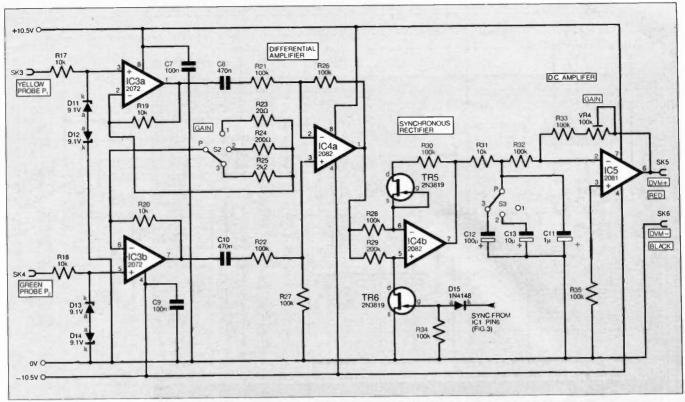


Fig. 4. Circuit diagram for the Differential Input Amplifier, Synchronous Rectifier and D.C. Amplifier.

the f.e.t. source-drain (s-d) path to conduct, thus grounding input pin 5 of IC4b.

The circuit then acts as an inverting amplifier with a gain of -1. Its input pin 5 is damped by resistor R29 which, because of its high resistance compared to the output impedance of the last stage, will cause no noticeable loading.

When the cathode of D15 is negative, the gate voltage of TR6 will be about -11V and the f.e.t. source-drain path will be high impedance, and so act as an open circuit. The circuit will then act as a non-inverting amplifier with a gain of +1.

Basically, the gain is determined by the relative values of resistors R28, R29 and R30. The inclusion of the f.e.t. TR5 in the feedback path helps to stabilise any tendency towards gain-change caused by temperature drift.

When the input signal to the Synchronous Rectifier (via D15) is positive, the output will be the same amplitude as the input, but will be reversed in polarity. When the input signal is negative, the output signal will also be negative, but still having the same amplitude as the input.

The rectified signal at IC4b pin 7 will always be negative, with any signals that are out of phase with the oscillator being superimposed as an a.c. waveform on the d.c. output signal.

The output from IC4b pin 7 is passed through a low-pass filter consisting of resistors R31, R32, and capacitors C11 to C13. This will remove most of the unwanted a.c. signals that are present. C12 and C13 can be switched in or out of the circuit by S3, so allowing the filter response times and effectiveness to be changed.

However, increasing the effectiveness of the filter by increasing the value of either of these capacitors will slow the response time of the circuit. The values chosen represent a suitable compromise for minimising the interference found in most rural locations.

The output from the D.C. Amplifier IC5 is then fed via sockets SK5 and SK6 to a digital voltmeter (DVM). A toolbox type digital multimeter, set to a relevant voltage range, is suitable, with connecting leads of about 500mm in length. If desired, a digital panel meter may be incorporated in the case containing the resistivity meter. It did not seem to be a cost effective exercise to build a digital indicator for this circuit.

Whatever type of indicator is used, it should have ranges from 0V to 10V d.c., down to 0V to 100mV f.s.d. (full scale deflection).

POWER SUPPLY

As shown in Fig. 5, power is supplied by two batteries, B1 and B2, which may be any type of battery that can supply 18V at only a few milliamps. Rechargeable NiCad cells stripped from old radio equipment

have been found to be ideal! An alternative suggestion is two PP9 batteries in series for B1, and a similar arrangement for B2.

The twin power supplies are regulated down to +10.5V and -10.5V by IC6 and IC7, in conjunction with Zener diodes D16 and D17.

CONSTRUCTION

These circuits are built on two printed circuit boards, whose details are shown in Fig. 6 and Fig. 7. The boards are available from the *EPE PCB Service*, code 131 (Current Gen.), 132 (Amp/Rect.).

It is recommended that d.i.l. (dual-inline) sockets should be used for all the integrated circuits (i.c.s). Mount the resistors, diodes and capacitors first, followed by the transistors and i.c.s. Correctly observe the polarity of all but the resistors.

Prepare a suitably sized diecast case by drilling holes for the sockets, p.c.b. fixing holes and switches. Mount these components and instal the p.c.b.s using 6BA

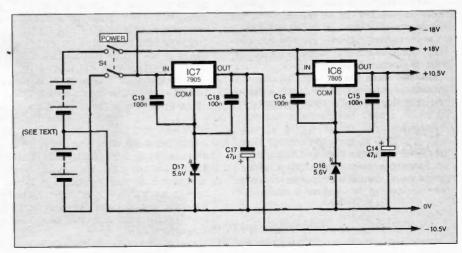


Fig. 5. Power supply circuit diagram.

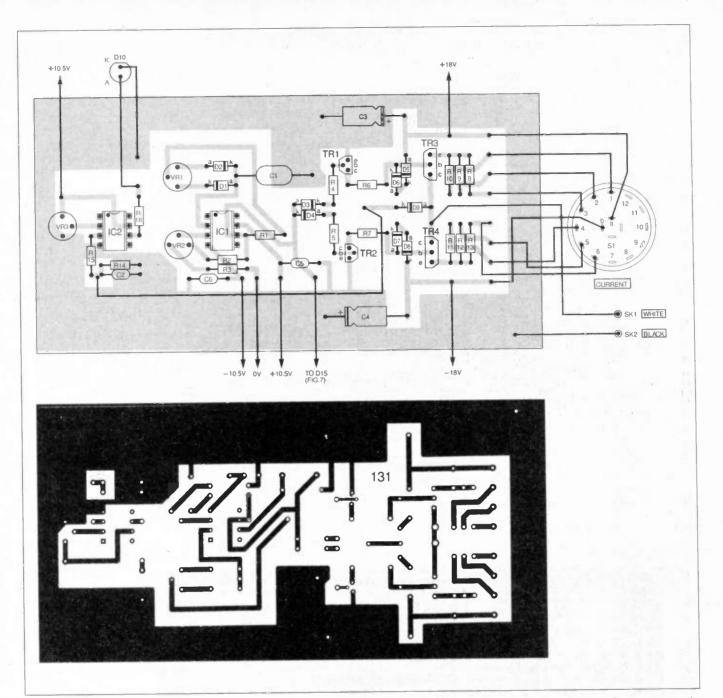


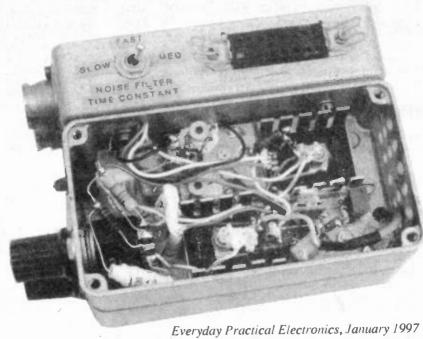
Fig. 6. Details of the component layout and full size underside copper foil track master pattern for the Current Generator p.c.b.

nuts and bolts, or sturdy p.c.b. mounting pillars.

The prototype of this circuit was actually constructed on stripboards which were mounted in three small diecast cases, each measuring 60mm × 110mm × 30mm, each one being bolted to the other with 6BA nuts and bolts.

However, with the p.c.b. design shown, only one box needs to be used; a suggested minimum size is about 140mm × 70mm × 60mm. Double-check the size of your assembly before buying a case, since individual component sizes may vary depending on the source. You might consider buying a diecast case with a rubber gasket round the lid to help minimise the risk of water ingress when out in the field!

The author's prototype, built on stripboard and mounted in three combined boxes.



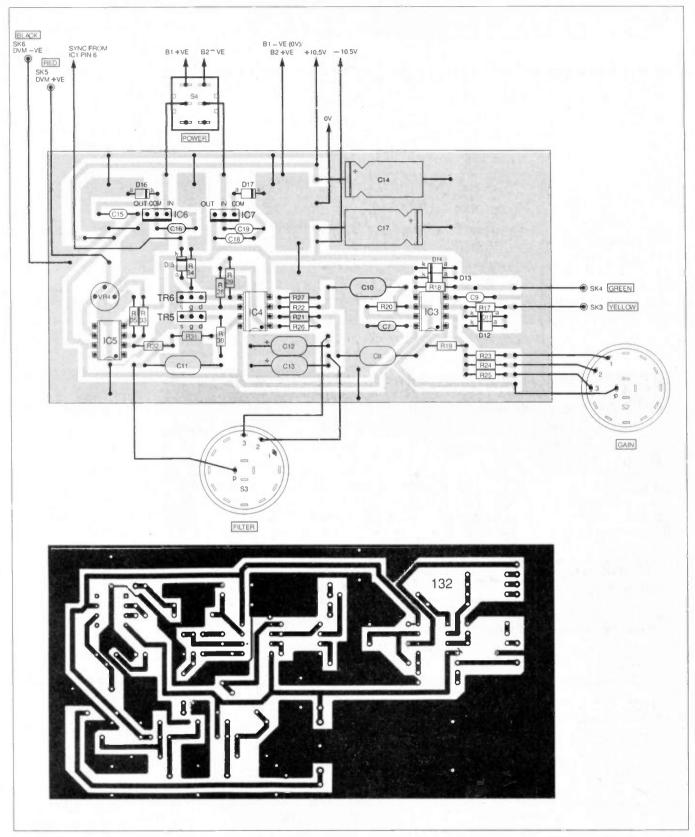


Fig. 7. Details of the component layout and full size underside copper foil track master for the Amplifiers and Rectifier p.c.b.

ADJUSTMENTS

- If you have an oscilloscope and frequency meter, proceed as follows:
- 1. Switch on. Measure the positive supply line at C15 + V_e and check that it is + 10·5V. Measure the negative supply line at C17 V_e and check that it is 10·5V.
- 2. Connect a frequency meter to IC1 pin 6 and set VR2 to give an output of 137Hz.

If no frequency meter is available, use a medium impedance earpiece connected between IC1 pin 6 and the 0V line and estimate a suitable tone, i.e. a little above 100Hz (rectified mains hum frequency).

3. Connect an oscilloscope to IC1 pin 6 and set VR1 so that both halves of the square wave are the same. Ascertain that the amplitude is about 11V, and that it is symmetrical about the 0V line. If no oscilloscope is available, set VR1 mid-way.

4. Temporarily connect a test resistor across the C_1 and C_2 terminals. Select the test resistor value and current generator output according to Table 2. Connect the

Table 2

Current Setting	Test Resistor	
0-1mA	10kΩ	
1mA	1kΩ	
10mA	100Ω	

COMPONENTS

R	e	si	S	t	0	r	S

R1, R3, R6, R7, R17 to R20. **R31** 10k (9 off) R2, R21, R22, R26 to R28, R30, R32 to R35 R4, R5 R8, R13 R9. R12

100k (11 off) 15k (2 off) 68Ω (2 off) 730Ω (2 off) R10, R11 7k8 (2 off) R14 470k **R15** 47k 2k2 (2 off) R16, R25 200 R23 R24 200Ω 200k

R29 All 0.6W 1% metal film

Potentiometers

10k horiz, preset (2 off) VR1, VR3 VR2, VR4 100k horiz, preset (2 off)

Capacitors

1μ metallised polyester, 100V 220n disc ceramic, 25V C3, C4 22µ axial elect. 63V (2 off)

C5 to C6, C7, C9, C15, C16, C18, C19 1

100n disc ceramic (8 off) C8, C10 470n polyester (2 off) C11 C12 C13 1μ tantalum bead, 35V 100μ axial elect. 35V 10μ axial elect. 35V C14, C17 47μ axial elect. 35V (2 off) Semiconductors

D9

TR1 TR2

TR3

TR4

IC1

IC2

IC3

IC4

IC5

IC₆

IC7

See

TALK

TR5, TR6

1N4148 silicon signal diode (9 off) D1 to D8, D15 OA91 germanium signal diode D10 red l.e.d. D11 to D14

BZY88C9V1 9.1V 500mW Zener diode (4 off) BZY88C5V6 5.6V 500mW Zener diode (2 off) D16, D17 MPSA42 npn transistor

ZTX550 pnp transistor

TIP30A *pnp* high power transistor TIP29A *npn* high power transistor 2N3819 *n*-channel f.e.t. (2 off) LM725 op.amp

741 op.amp 2072 dual op.amp 2082 dual op.amp

2081 op.amp 7805 +5V 1A voltage regulator 7905 -5V 1A voltage regulator

Miscellaneous

B1, B2 S1 to S3 18V battery - see text (2 off) 4-pole 3-way rotary switch (3 off) d.p.d.t. toggle switch S4 SK1 4mm socket, white 4mm socket, black (2 off) **SK2, SK6** 4mm socket, yellow 4mm socket, green SK3 SK4

SK5 4mm socket, red Printed circuit boards, available from the EPE PCB Service, codes 131 (Current Gen.) and 132 (Amp/Rect.); 8-pin d.i.l. socket (5 off); 4mm plugs, qty to suit; knob (3 off); case (see text); probe materials (see text); nuts, bolts and washers; connecting wire, solder, etc.

Approx Cost Guidance Only

excl. case and probes

Table 3

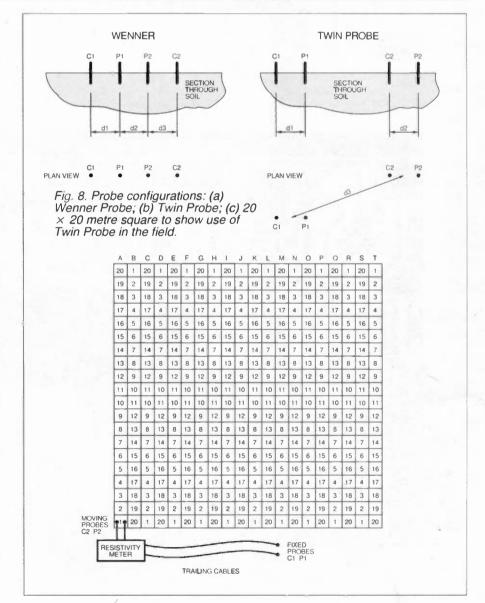
Gain	Load	Output
× 10	10Ω	0·1V
× 10	100Ω	1V
× 10	1000Ω	10V
× 100	1Ω	0·1V
× 100	10Ω	1V
× 100	100Ω	10V
× 1000	0·1Ω	0·1V
× 1000	1Ω	1 V
× 1000	10Ω	10V

oscilloscope across the resistor (scope probe tip to C1). The oscilloscope should show a 137Hz trace at approximately ± IV, symmetrical about the OV line, at all three settings of current selector switch SI

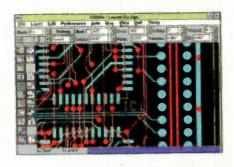
If any discrepancy is noted, the appropriate resistor (R8 to R13) on switch S1 should be checked. These resistors may be made up with a series and/or parallel connection of more than one resistor if a high degree of accuracy is desired.

- 5. Set the test resistor to 10Ω . Set the amplifier gain switch (S2) to × 100. Adjust preset VR4 for a d.c. output of exactly 1V across SK5 and SK6.
- 6. Connect P_1 to C_1 , and P_2 to C_2 . Connect a resistance box or a series of fixed resistors between P₁ and P₂. Set the amplifier gain (S2) and the resistance box to the figures in Table 3 and check that the output is correct.
- 7. Set the test resistor to $10k\Omega$ and switch S1 for a current output of 1mA. Adjust preset VR3 until the l.e.d. D10 just

This completes the tests and adjustments. Let's now probe deeper:



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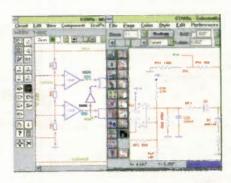
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PROBE CONFIGURATIONS

Now let's look at some probing factors before considering the probes themselves.

There are several probe configurations that may be used, but the two that are now widely employed are the Wenner and the Twin Probe:

Wenner configuration

In the Wenner configuration, as illustrated in Fig. 8a, all probes are equally spaced in a straight line. A spacing of about one metre being suitable for general use. The two outer probes being C_1 and C_2 with the two inner probes being P_1 and P_2 .

The Wenner is suitable for linear traverses to check a site for anomalies (readings caused by buried features) before a more detailed survey is carried out.

To convert instrument readings for this configuration to resistivity, use the following formula:

 $\rho A = 2\pi dV/I$

where:

ρA = apparent resistivity

d = probe spacing

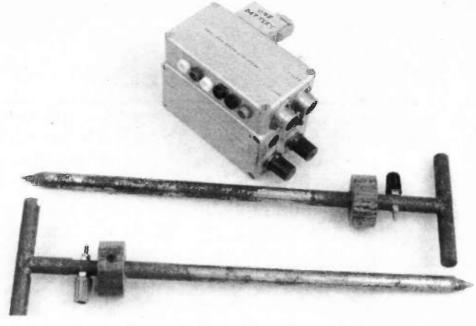
V = indicated voltage divided by the amplifier gain.

I = current

Twin Probe configuration

In the Twin Probe configuration, as illustrated in Fig. 8b, probes C_1 and P_1 are inserted just off the area to be surveyed and are known as the fixed pair. Probes C_2 and P_2 are moved across the area to be surveyed as a pair at the same distance apart.

This moving pair is placed in the squares of a grid previously laid out with strings or measuring tapes, as represented in Fig. 8c.



Two of the short probes alongside the author's prototype model.

The spacing of the C_1 and P_1 probes should equal that of the C_2 and P_2 probes and be about 500mm. The spacing between the fixed pair and the moving pair can be anywhere between 15 metres and 50 metres.

Probes C_2 and P_2 may be fixed to a frame (as shown next month, for example), complete with the electronic unit to make a very easy to use setup.

To convert instrument readings for this configuration to resistivity, and referring to Fig. 8b, use the following formula:

$$\rho A = (2\pi V / I) \times (I / ((2 / dI) - (2 / d3)))$$

Construction of the probes themselves is very simple; none of the materials or their

dimensions are critical and may be dictated by what is to hand.

In Fig. 9a is shown a substantial probethat is made out of stainless steel tubing with a brazed on T-handle and tip which assists in soil penetration. This probe is designed to be used with the operator in a standing position.

A set of four probes made up as in Fig. 9a make ideal Wenner probes because, as this configuration needs to be continually moved, tall probes avoid bending the back.

A smaller version of Fig. 9a is shown in Fig. 9b; this has a 4mm screw terminal added, an alternative method of wire connection. Probes may be constructed of materials other than stainless steel, which is expensive and a little difficult to procure.

An extremely simple probe is shown in Fig. 9c and which may be constructed from 6mm diameter metal rod, i.e. brazing or uncoated welding rod, mild steel, silver steel, etc. A depth guide consisting of a band of paint or insulating tape is added and connections are made to the top of the rod with a crocodile clip.

The depth stop illustrated in Fig. 9d is adjustable by means of an Allen key. The material need not be insulating, and could be of metal if desired.

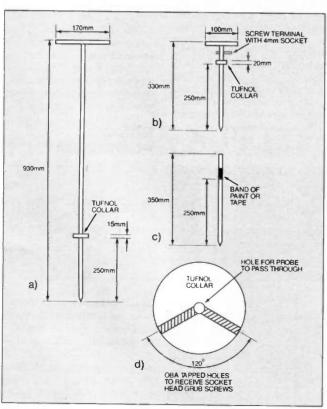
PART TWO

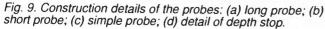
In the concluding article next month, the techniques and ethics of earth resistivity surveying will be discussed.

QBASIC PROGRAM

A copy of the author's program – for displaying graphics of the earth resistivity results – written in QBasic (for a PC-Compatible computer), is available from the Editorial Office for the sum of £2-50 UK, £3-10 overseas surface mail or £4-10 airmail. This is to cover admin costs and postage, the disk itself is *free*. You are welcome to copy this program and give it to your friends. See *PCB Service* for ordering details.

The program can also be down-loaded *free* from our FTP site: ftp://ftp.epemag.wimborne.co.uk, in the sub-directory: pub/PICS/Earth.Meter.







Innovations

A roundup of the latest Everyday News from the world of electronics

SWATCH, MERCEDES AND THE SMART CAR

Has the pollution-free urban-mobility problem been cracked at last?

- by Hazel Cavendish

T is hard to think of anything more beneficial to life in our polluted cities today than the development of a viable micro-car based on innovative electronics and having zero emissions.

With an increasing number of major cities all over the world planning to ban conventional petrol-engined cars from their centres, it has been obvious that a lucrative opportunity existed for a manufacturer of a really small unit of transport for the city worker.

SWATCHMOBILE

The good news is that the innovative Swiss Swatch company has joined forces with Mercedes-Benz to build just such a car in France, using the genius of Swatch's Nicolas Hayek and the expertise of Mercedes-Benz in a combination of microelectronics and precision mechanics which offer safety and high performance in its urban mobility concept. Mercedes will engineer the car and Swatch will sell it.

The MK Micro Compact Car known as the SMART car (nicknamed the Swatchmobile by the Motor trade) is promised to the world in 18 months in its initial petrol version, followed by a turbodiesel in 1999, and finally an all-electric zero-emissions model in the year 2000, with a project cost of DM 2 billion.

"Individual mobility" is the name of the game, the car being a two-seater, two feet shorter than a Mini, which will take two adults or one adult and two children and, although small outside, is remarkably spacious in its interior.

"Our task is to turn our vision of a systematically futuristic vehicle into a marketable product that will stand up to competition," says Hans Jurg Schar, Executive Vice-President of Sales.

SINCLAIR APPROVAL

Britain's micro-car guru, Sir Clive Sinclair, has always backed the electric car, saying that Britain is out-of-date in regarding it as a lethargic vehicle which is short of range. For some time he has been urging that we need to consider "second cars" for local use to combat urban pollution.

"Keep the Volvo for longer trips, and rent it out for occasions, but use the electric town car for shopping and taking the children to school", he says, pointing out that the town car needs a range of only 40 miles and a top speed of 40mph, with the added advantage of good reliability and probably 100,000 miles before service is needed.

The remarkable feature of the SMART project is its multi-national character. The head office of MC AG is at Swatch HQ in Biel, Switzerland, where marketing, sales, finance and controlling divisions are located. Development of the car takes place in Renningen, Germany, but production is in the hands of MCC France at Hambach in Lorraine, chosen because it is sited logistically in central Europe and is served by a network of international traffic connections.

Here a large-scale international industrial park, "Europole", is currently under construction, where planning permission was granted at very short notice—hardly surprising in view of the number of jobs the project is bringing to the area.

VEIL OF SECRECY

Unfortunately for journalists, a veil of secrecy is drawn over the details of the electronics used in the car. Many telephone calls and faxes to both Swatch and Mercedes have produced polite evasions and a snowstorm of publicity material which reveals little technical data. With both America and Japan working feverishly towards the same goal, this is perhaps understandable. SMART is undoubtedly a hot number.

We are told there is an electronically controlled drive power management system, and an expendable "Mobibox" module which provides the vehicle with "communications infrastructure for enhanced mobility" and which is an important part of the safety system.

The highlight of the design is said to be the automated manual six-speed transmission which saves fuel and makes driving particularly enjoyable. "Precise electronic control replaces raw muscle power, so that a light tap on the gearshift suffices to change to the next gear", says the Company leaflet. An electronic immobilizer is also included, as no doubt the SMART will be irresistible to car thieves in

In March 1998 the 900cc three-cylinder eco-turbo petrol machine with intercooler and dual ignition will be introduced to the market. Four litres of petrol will take you 100kms, while the Diesel model will only require three litres to cover that distance. Acceleration is remarkably nippy, being 0 to 60kph in six to seven seconds with the top speed at a surprising 100kph.

NiCad POWERED?

What of the battery – the stumbling block with all electric cars? Mum's the word, unfortunately, but perhaps a hint that something entirely new may have been developed is given by the statistic that car batteries account for 500 jobs in the local industrial infrastructure, by far the highest number, apart from those connected with the production of tyres.

Sir Clive Sinclair hazarded a guess that the car will probably develop the nickelcadmium battery as being the most suitable choice.

A right-hand drive version of the car will be produced, though it may be five years before it is available in Britain.



Demo model of the nippy Swatch-Merc SMART car - the production models will have doors!

MAPLIN STOCKS EPE

THERE'S great news for Maplin customers and EPE readers! EPE. vour favourite electronics magazine, is now on sale in all of Maplin's 35 stores nationwide.

Moreover, we are the first independent electronics magazine to become available from Maplin. And this is a coup for both Maplin and EPE! Just think, next time you nip into your local Maplin store for the odd resistor or hifi system, or browse through their new "ginormous" MPS catalogue, you can pick up EPE as well. So, on both counts, you're bound to get good reading.

Both we and Maplin are delighted with this beneficial initiative. It will certainly help to expand the electronics market in which you, we and they

have such an intense interest.

Indeed, on a very serious level, the health of the hobbyist electronics market is actually under threat by the actions of some of the major retail newsagents. Some are hinting that they will only continue to stock specialist magazines if the publisher provides them with an "incentive". We place on record our strong objections to this marketing ploy.

By such restrictive actions, specialist publications catering for a diverse range of activities, not just electronics, could be forced off the shelves of many newsagents. It is not in the public interest, your interest, or that of the publishers, or of the retailers who advertise in the associated publica-

tions, that this should happen.

But the warning signs are there, and we must take appropriate action, adopting not just Plan B, but C to Z as well; so should other electronics retailers, adopting Maplin's enlightened outlook by stocking EPE, the independent Number One Magazine for Electronics Technology and Computer Projects. (We also applaud the foresight of Cirkit, Greenweld and Omni who already do so!) Other retailers, you are invited to ask us for details on how you too can sell EPE from your stores.

Readers, what can you do? For a start, complain to the manager of any store which appears reluctant to stock EPE and other specialist magazines. Secondly, encourage your local electronics retailer to keep EPE on his counter. Thirdly, and to really safeguard your continued receipt of EPE, take out a yearly or two-yearly subscription! This will also save you money - obviously a good deal is on offer! See page 70 for

details.

A further plan which both we at EPE and Maplin are developing strongly is our presence on the Internet. We have a wealth of material available from our Web site at http://www.epemag.wimborne.co.uk, and there is free access to the software required for some of our constructional projects.

Maplin, via their site, provide on-line data for many of the special chips and components they stock. On their site they also have, for example, the demo software for the PCS32 Digital Storage Oscilloscope Interface which Robert Penfold reviews so favourably in this issue. Have a good browse of Maplin's informative site, at http://www.maplin.co.uk.

For more information about Maplin and their stores (they even have overseas branches), call them on 01702 554000.

EASY LOGGING

DATA logging is a subject referred to in this month's Earth Resistivity Meter article. That design uses the author's own logging software, but for many other situations you could well find that Lascar's new EasyLog EL-2 unit will provide suitable facilities.

EL-2 is a hand-held multi-function module which, in conjunction with a suitable sensor, will measure, display, record and control temperature, voltage, current, humidity, pH, frequency and rate count. The module is configured using Windows-based control software, EL-WIN, and

the stored data can be saved and graphically presented or exported to popular spreadsheets.

The in-built display consists of a 31/2 digit I.c.d., and the non-volatile memory can record up to

8000 readings. Power is supplied from a 3.6V long-life Lithium batter.

For more information, contact Lascar Electronics Ltd., Module House, Whiteparish, Salisbury, Wilts, SP5 2S. Tel: 01794 884567.



LOW COST

IF YOU are in need of low cost electronics design software, why not consider the new ED-Win NC package from Visionics? It is the noncommercial licence version of their successful EDWin EDA software, and which is available at a fraction of the cost. It includes all the

features of its bigger brother.

Prices of EDWin NC start at just £49, including VAT, for the basic version, which comprises schematics, p.c.b. layout, 500-device library, basic autorouter, full post processing facilities, although it has a limit of 100 components per circuit. Several extended versions

are available, at up to only £114.

The system is delivered on CD-ROM (which, of course, many computers now have as standard) and includes comprehensive manuals. The software runs under Windows 3.1x, 95 or

For more information, contact Swift Designs Ltd., Business & Technology Centre, Bessemer Drive, Stevenage, Herts, SG1 2DX. Tel: 01438

PRESS-N-PEEL APPEAL

OVER the years, many innovative printed circuit board prototyping materials hit the headlines, though not all of them have withstood the test of user acceptance. The Press-N-Peel (PNP) technique, however, seems as though it could well represent welcome breakthrough for the prototyping market.

With PNP, no expensive materials or equipment are necessary, not even an ultraviolet exposure unit. All you need, basically, is access to a photocopier and a hot domestic smoothing iron. This product is so versatile that you can photocopy a p.c.b. layout from a magazine page and have a board ready for drilling in little more than the time it takes to etch it. If you use computerised p.c.b. drafting software, you can even output a print of your board direct onto PNP, via a suitable printer of course!

Once the image has been printed onto PNP, you are ready to transfer the circuit to "raw" copper-clad p.c.b. material - no more resist coated copper, no more light source, just plain copper clad fibre-glass or equivalent.

Using your household iron set to about 150°C (Hot), you simply lay the PNP image down onto the copper-clad board and smooth it down with the iron. You can tell by the darkness of the image when the transfer has stuck.

the board When cooled, the film is peeled leaving the area of trackwork stuck to its surface. Etching is then done in the usual way, after which the PNP resist is wiped off using the PNP stripper solvent supplied.

It all seems like child's play - so we've asked our Tech-Ed to try it on his next prototype!

For further information, contact Press-N-Peel Etching Supplies Ltd, 18 Stapleton Road, Peterborough 6TD. Tel: 01733 233043.



New Technology

lan Poole highlights the battle against the ever incre problems of environment pollution and waste facing today's i.c. manufacturers... lan Poole highlights the battle against the ever increasing today's i.c. manufacturers..

GREEN issues are playing an increasing role in today's technology. For example many cars are now being designed to be recyclable, as are many other products. In the realm of electronics, battery technology is one area where the subject has been covered in recent months in this column.

However, this is not the only area where "conservation" is of great importance. The manufacture of integrated circuits (i.c.s) uses vast amounts of energy. There are also many dangerous substances which are used in the process, and a number of unfriendly by-products are produced.

Vast Quantities

The integrated circuit industry manufactures a vast number of circuits each day. The average household is likely to buy at least two or three products each year which contain i.c.s. Multiply these figures by the numbers of households, and it is possible to see that even to supply a country like the UK, vast numbers of i.c.s

These i.c.s only cover those required for domestic use. Commercial users also consume enormous quantities of chips as well.

To be able to meet this demand, it is estimated that a typical i.c. manufacturing plant makes around two million i.c.s a month. There are many fabrication plants dotted around the world and the number is growing all the time as the recession recedes and demand rises. This increase is expected to last for some time, making the current problem of pollution from these plants worse than it is today.

Typically, it takes about ten gallons of water to make each i.c.. This means that a plant manufacturing two million i.c.s a month will use 20 million gallons of water. This is in addition to the large amounts of heat required in processes such as diffusion and epitaxy. Turning the raw silicon into complete i.c.s requires hundreds of steps to be completed.

Additional problems are caused by the use and creation of toxic substances. Although it is possible to dispose of certain amounts of toxic chemicals, the amounts now being produced are reaching levels where the increase cannot continue indefinitely. This is particularly true for plants manufacturing gallium arsenide chips!

Groundwork

Until recently comparatively small amounts of work had been undertaken to look into ways of creating more environmentally friendly processes. Even now the work is in its early stages and will take many years to incorporate into the large number of plants around the world.

The first stages involved assessing the amount of water which was used. During the manufacture of an i.c. there are many different stages including etching, doping, epitaxial growth and the like. After many of these stages it is necessary to wash or rinse the chips with very pure water to remove the impurities from the surface.

Computer simulations have now been devised to simulate some of the processes. In a typical rinse operation a cassette containing about 50 wafers is lowered into a water container. This undergoes several cycles of rapid filling and draining after which the water is allowed to flow through the container to remove the last impurities.

The computer simulations showed that slowing the rate at which the water is allowed to flow removes the impurities more effectively.

CAD Developments

The key to all of these improvements has been the development of programmes to enable these predictions to be made. Manufacturing i.c.s is a large but relatively niche market and as such CAD software for some of the more specialist applications has to be specifically written if required.

This is a costly business and unless companies and organisations see real benefits they are unlikely to undertake the work. Now that green issues are becoming more important, and the impact on the environment is more likely as a result of the vast numbers of chips being manufactured the impetus is there to develop the required simulation tools.

Before these first simulation tools were developed the extent of the savings were not obvious. Now that they can be shown, the tools are likely to be developed further and used much more extensively. Already, Hewlett Packard has implemented some changes as a result of them and they have confirmed that making the suggested process changes reduce cold water consumption by up to 80 per cent and reduce the times in some areas by considerable

The time reductions alone can represent an attractive proposition for manufacturers because they allow more efficient usage of the plant. This results in a larger throughput and greater return on investment. In view of the phenomenal costs of i.c. fabrication plants this is particularly important.

Major Savings

Having proved that there are major savings in terms of environmental pollution, and greater financial gains for

manufacturers, work is progressing to investigate other areas of the operation of i.c. manufacture. Much of the focus will be placed upon extending the capabilities of existing tools and developing new ones which will be able to model other areas of production.

It is pointed out that in this way process changes can be simulated on computers relatively easily before large amounts of investment are placed into changing the existing plant, or overloaded production lines are stopped to update them.

A number of other areas for research have also been outlined. The first is to further develop the ideas behind the rinsing and cleaning operations, to make them more efficient and save more water.

One approach that will be used is to investigate methods of recycling more water. Another will involve looking at how to reduce the level of chemicals which need to be used, and washed from the wafers and from the system as a whole.

Another area for concern is in the use of chemicals called perfluorocarbons. These currently replace chlorofluorocarbons which were previously used and are now known to damage the ozone layer.

The chemicals used now are far less damaging to the ozone layer, but any reduction in the levels escaping into the atmosphere will help reduce the depletion of ozone.

One of the other areas to come under investigation is the lapping or polishing process. This is used to bring the wafers to a very high degree of smoothness. With half micron semiconductor technology in use today, very high degrees of smoothness are required, often to atomic levels.

To achieve this different levels of lapping or polishing are used and then this is followed by chemical etching. This leaves residues which can contain chemicals which are hazardous if not properly treated. To be able to reduce the environmental effects new processes are being proposed which will convert the residue to a solid form which can be handled and disposed of safely.

Future

With the ever increasing number of integrated circuits being produced, and their increase in size and complexity, the environmental impact of this industry will grow if it continues unchecked.

The improvements demonstrated so far show that reducing the environmental effects can progress hand in hand with improvements in efficiency. If this proves to be the case, then perhaps more industries may follow suit.

Is your PCB design package not quite as "professional" as you thought? Substantial trade-in discounts still available.

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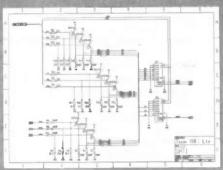
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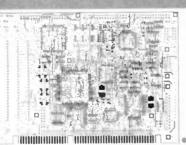
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Back annotation from BoardMaker2









Board Maker

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Constructional Project

PSYCHO RAT

NICK SHELDON

Using the power of logic, Psycho Rat demonstrates the psychology of "conditioning".

ogy which can be demonstrated with dedicated electronic hardware. One of these is a learning theory known as classical conditioning, and it is that which will be described in this article. To demonstrate this "conditioning", a practical model in the form of "Psycho Rat" has been produced.

To a pure scientist, psychology can sometimes seem nebulous, lacking a real core of experimentally proven, mathematically expressed theories. Some psychologists are proud of this state of affairs, describing their vague, quasi-mystical ramblings as "idiographic." The opposite, scientific approach is termed "nomothetic."

SCIENCE OF BEHAVIOUR

Early psychology was defined as "the science of consciousness", and relied heavily on speculative introspection. As a reaction against this, in 1913 J.B. Watson founded a movement known as behaviourism, which instead defined psychology as "the science of behaviour." The objective was to make psychology as rigorously scientific as other sciences, such as physics and chemistry.

Watson popularised the work of the Russian physiologist I.P.Pavlov, who had researched the digestive process. In the course of Pavlov's experiments, it was noticed that the dogs, which formed the experimental subjects, sometimes salivated before food was given to them.

Rather than dismissing this inconvenient finding, Pavlov researched it, and discovered what came to be known as "classical conditioning".

Two kinds of stimuli were defined by Pavlov: conditional and unconditional. An unconditional stimulus could be the sight of food, which the innate, automatic, unconditional response would be to salivate.

If a bell was sounded when the food was produced, this bell became capable of producing the same response. In Pavlov's terms, the bell would be a conditional, learnt stimulus. Watson believed that all learning could be described in terms of

the learnt associations between stimuli and responses. This became known as "S-R psychology".

CLASSICAL LOGIC

Perhaps surprisingly, classical conditioning can be represented in terms of Boolean functions. There are two inputs: the unconditional (US) and conditional (CS) stimuli, and one output: the response (R).

Before conditioning takes place, the situation can be described with the Truth Table shown in Fig. 1. This shows that the response (R) simply equals the unconditional stimulus (US) input, the reason being that the (ultimately) conditional stimulus is neutral prior to conditioning. Consequently, this input has no effect at this stage, the output only being true if the unconditional input is true.

US	CS	R
0	0	0
0	1	0
1	0	1
1	1	1

US	CS	H
0	0	0
0	1	1
1	0	1
1	1	1

HC CC D

R=US

 $\mathbf{R} = \mathbf{US} + \mathbf{CS}$

Fig. 1. Initial Truth Table Fig. 2. "OR" Truth Table

After conditioning, the Truth Table changes to that shown in Fig. 2., which indicates that the new function is the OR of the unconditional and conditional stimuli. This is because the output (R) is now required to be true if either the conditional stimulus input OR the unconditional stimulus input is true, or both are true (inclusive OR).

The situation which changes the state of the system is the occurence of the unconditional stimulus at the same time as the conditional one, i.e. the AND of the two stimuli. Psychologists rather grandly call this a temporal contiguity.

The basic circuit thus consists of five elements: 1, the logic to provide the first truth table; 2, the logic to provide the second truth table; 3, a means to detect

the temporal contiguity; 4. a means to store the learnt state; 5. A data selector to choose between the outputs of 1 and 2. A block diagram is shown in Fig. 3.

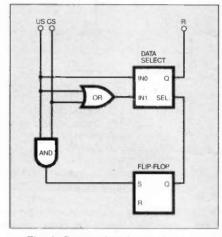


Fig. 3. Data select block diagram.

The more complex elements of the circuit, sections 4 and 5, can themselves be analysed with Truth Tables and constructed out of individual gates. The reason for this approach is three-fold: first, a typical hobbyist's spares box is more likely to contain gates than complex logic i.e.s; second, it is very instructive to see how these more complex functions are built up; and third, this approach does not increase the i.e. count.

Taking the S-R (Set-Reset, not stimulus-response!) of the flip-flop which forms part 4 of the circuit, the gate level implementation is shown in Fig. 4. This can be analysed by considering it as having two

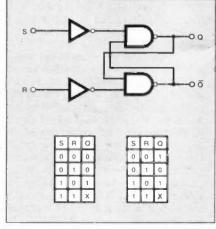


Fig. 4. Gate level implementation.

truth tables - one for each state. The condition when S and R are both high is undefined, and is shown in both truth tables as an "X"

The first of the two Truth Tables in Fig. 4 is for the flip-flop initially in the reset state. Consequently, the reset (R) input has no effect, change only taking place when the set input is true, changing the flip-flop to the Set state.

The second Truth Table in Fig. 4 shows the situation when the flip-flop is set. Here, the set (S) input has no further effect, change only taking place when the Reset input is true.

Part 5 of the circuit, the data selector, can be analysed as shown in Fig. 5. The resulting gate level implementation also being shown in the same figure. The data selector can be considered as having three inputs: the two data inputs and the select input.

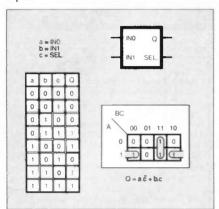


Fig. 5. Data analysis.

Taking the select input as selecting input I when it is high (1), the Truth Table is determined as follows: when input 0 (a) and input 1 (b) are both false (=0), the output Q is false irrespective of what value c, the select input, takes. When input 0 is false but input 1 is true (=1), the output O is true only when the select input is high (selecting input 1). When input 0 is true but input 1 is false, the reverse situation takes place, namely, the output Q is true only when the select input (c) is false (selecting data input 0). Finally, when both input 0 and input 1 are true, the output Q is high irrespective of the select input's status.

KARNAUGH MAP

This three input Boolean function can be represented with an 8-element Karnaugh map, also shown in Fig. 5. The map can be thought of as representing the surface of a toroid - a ring doughnut-like structure

Consequently, the edges of the map are really in contact with each other, top with bottom and left with right. This is important, because the logical minimisation (simplification of gate implementation) which the Karnaugh map allows depends on groups of "ones" being spotted, and, as can be seen from Fig. 5, one of these two groups is at either edge of the map.

The vertical block of ones in the third column of the Karnaugh map has two variables in common: B and C. this means that this portion of the map can be represented with the logical formula B AND C. Note that the variable A is not required.

The second group also has two variables in common: A and NOT C. This means that this part of the map can be represented by the Boolean function A AND NOT C. These two functions are then combined by ORing them to produce the complete data selector logic.

FINAL LOGIC

The complete theoretical circuit of Fig. 6 can be constructed entirely out of NAND gates with no increase in complexity. De Morgan's law states that A OR B = NOT (NOT A and NOT B), i.e. two inputs ORed together is the same as two inputs both inverted, ANDed and then inverted once more. This is shown stage by stage in the Truth Table Fig. 6.

Consequently, the OR gate can be simulated with an AND gate having both inputs and the output inverted (see Fig. 7) - in other words, a NAND gate with both

а	b	ā	Б	а∙Б	ā.b	a+b
0	0	1	1	1	0	0
0	1	1	0	0	1	1
1	0	0	1	0	1	1
1	1	0	0	0	1	1

Fig. 6. Demonstration Truth Table.

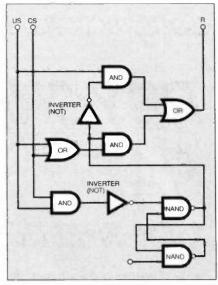
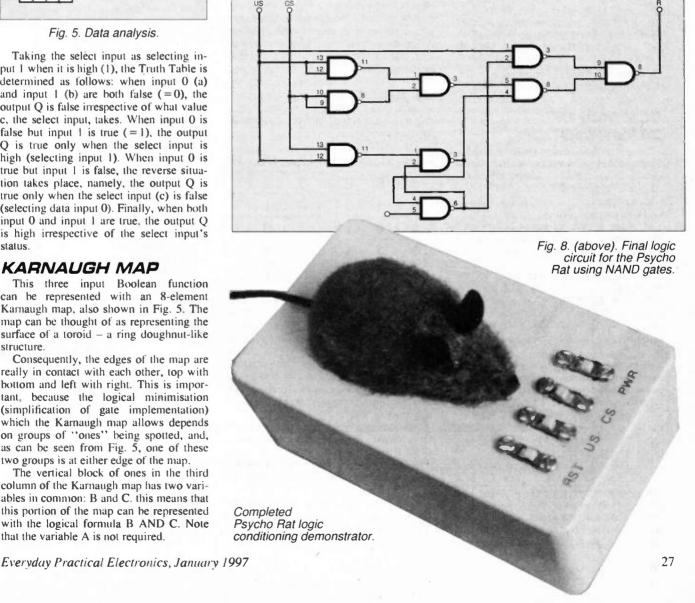


Fig. 7. Theoretical circuit using NAND gates.

inputs inverted with other NANDS. The inverter in the data selector can be obviated by utilising the inverted output of the S-R flip-flop, and replacing the AND gates of the data selector with NAND gates permits the OR function to be provided by another NAND gate, again courtesy of De Morgan. The final logic for our Psycho Rat using NAND gates is shown in Fig. 8.



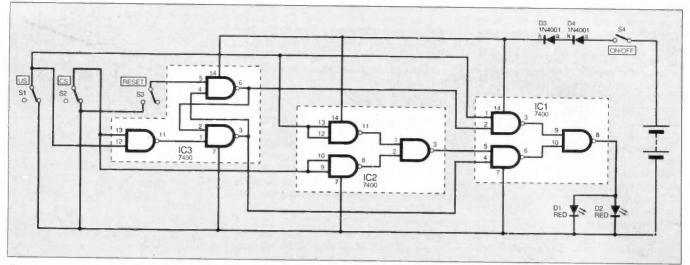


Fig. 9. Complete circuit diagram for the Psycho Rat using three quad 2-input NAND gate i.c.s

PSYCHO RAT

The complete circuit diagram for the Psycho Rat is shown in Fig. 9. Two diodes D3, D4), in the positive supply line, drop the battery voltage to about 4.8V for the TTL circuitry.

The "stimuli" for the Rat are provided by two switches, one for the Unconditional Stimulus (S1) and one for the Conditional Stimulus (S2). Miniature s.p.d.t. slide switches were used, allowing the inputs to float high when operated (being standard 7400 TTL this is permissable).

Response in the rat is shown by its eyes lighting up! This is achieved by using two 3mm l.e.d.s (D1, D2) wired in parallel. Note that current limiting resistors are not needed.

A third switch, S3, is provided to reset the flip-flop, which on switching on may be initially set, and a fourth switch (S4) controls the power supply.

CONSTRUCTION

The circuit was finally built on a P.C. Bimboard, having been transferred from

a plug-in type Bimboard where it had been ' "prototyped". This can also be easily transferred to stripboard. The Bimboard component layout is shown in Fig 10.

The completed board and associated components were cased in a white plastic box, with the top half of a clockwork plastic mouse fixed to its top. The wiring for the "eyes" (l.e.d.s) is taken through a hole in the box's lid and through the underside of the rat.

Letraset rub-down transfers were used for labelling-up the switches. A small section of the P.C. Bimboard was removed with a hacksaw so that the circuit would fit into the largest white plastic box available, white having been chosen for ease in labelling.

IN ACTION

"Psycho" is operated as follows. First, it is switched on, and the Reset switch \$3 momentarily operated, in case the flip-flop is set. The effect of the unconditional stimulus is then demonstrated - the US

COMPONENT

Semiconductors

D1, D2 3mm light

emitting diode, TALK red (2 off) 1N4001 1A 50V Page

See

D3. D4 rec. diode (2 off)

IC1 to

IC3 7400 quad 2-input NAND gate (3 off)

Miscellaneous

S1 to

R₁

miniature s.p.d.t. slide

switch (4 off)

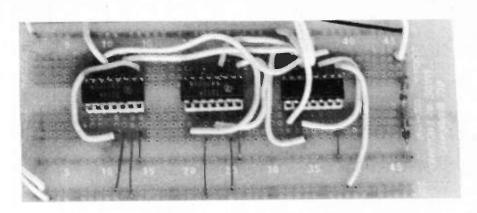
AA size 1.5V battery (4 off), with holder

Plastic ABS white case, size 143mm x 58mm x 81mm; P.C. Bimboard; 14-pin d.i.l. socket (3 off); battery clip; 2-way terminal block; rubber feet (4 off); rubdown lettering (Letraset); clear varnish to protect lettering; multistrand connecting wire; self-tapping screws (12 off):

solder etc.

Approx Cost Guidance Only excluding Rat, Batts and

Letraset FLAT-D2 ON OFF RESET B1 +V US Fig. 10. Component layout for the P.C. Bimboard version of Psycho Rat.





this stage. However, if the unconditional stimulus is presented at the same time as the conditional stimulus, thereafter the conditional stimulus will also light the rat's eyes - it has been conditioned.

Psycho Rat has been successfully used with students on courses from GCSE to undergraduate level. It is a very simple system. The cross-impact of electronics and behaviourist psychology is known as 'stenobehaviourism'

switch S1 is operated, and the rat's eyes light up. The (ultimately) conditional stimulus is

initially neutral prior to conditioning, and can be demonstrated to have no effect at

with David Barrington

Mains Failure Warning

As we are dealing with mains supplies here, the first comment we must make regarding the Mains Failure Warning project is: exercise extreme care when building this unit and make sure the METAL case is safely "earthed"

The effectiveness of the warning depends largely on the choice of buzzer and it should be a good quality type. It must be capable of producing a high sound output from a supply of only 7V and have a small current requirement of around 5mA to 10mA.

The p.c.b. mounting buzzer used in the model came from Maplin (2 01702 554000), code KU56L, and is rated for 3V to 15V d.c. operation, with an internal drive circuit. A suitable remote mounting sounder would be their "High Power", 3V to 24V version, code

The p.c.b. mounting mains transformer was purchased from Electromail (2 01536 204555), code 209-140. The 3V/11mAh p.c.b. mounting batteries are RS types and were also ordered through the same source, code 593-552.

The printed circuit board is available from the EPE PCB Service, code 126.

Theremin MIDI/CV Interface

Like last month's EPE Theremin, some of the parts called-up for the Theremin MIDI/CV Interface are special items and will not be generally available.

The author/designer, Adam Fullerton, is able to supply the pre-programmed PC87C51FB microcontroller for the sum of £45 each, inclusive pap. Orders should be sent to Adam at The Dene, Hindon, Salisbury, Wilts., SP3 6EE. Make cheques payable to Adam Fullerton.

So that readers can select their own requirements, Jake Rothman (author of the EPE Theremin) has put together a range of kits for the MIDI/CV. He is also able to supply a ready-programmed micro for the same price. See his advertisement on page 51 for details. - Note the new address and phone number.

The printed circuit board set is available from the EPE PCB Service, code 130.

Earth Resistivity Meter

Apart from the ingenuity of constructing the probes, the only items which may cause concern to constructors of the Earth Resistivity Meter are some of the specified semiconductor devices.

The 2072/81/82 op.amps are Texas devices that do not appear to be stocked by any of our advertisers. However, they appear to be up-grade versions of the readily available TL072, TL081 and TL082 series and these can be used in this circuit, in fact, almost any op.amp will probably work, and this will result in a significant saving.

The TIP29A and TIP30A power transistors seem to be "old hat" now and not that easy to find, but the 5A 40W TIP31A and TIP32A versions can be substituted instead.

A copy of the author's program written in QBasic (for PC-Compatible computers), is available from the Editorial Office for the sum of £2.50 UK, £3.10 overseas surface mail or £4.10 airmail. This is to cover admin costs and postage, the software itself is free. You are welcome to copy this program and give it to your friends. See PCB Service (page 67) for ordering details.

The program can also be downloaded *free* from our FTP site: ftp://ftp.epemag.wimborne.co.uk, in the sub-directory:

pub/PICS/Earth.Meter.

Psycho Rat

The only component problem likely to cause any local sourcing difficulties for the *Psycho Rat* is the P.C. Bimboard. This is a "hardwiring" version of the component plug-in prototyping block and is currently listed by Maplin as a Plugblock PCB, code YR87U. You can, of course, transfer the layout to stripboard if you wish.

The choice of "rodent" is left to individual choice, but at this time

Service, codes 131 (Current Gen.) and 132 (Amp/Rect.).

The printed circuit boards are available as a set from the EPE PCB

of year most toy shops should be able to come up with a suitable

subject.

TAKE NOTE

November '96 Central Heating Controller We have received an E-Mail communication from Mr. David Lilley, who has successfully completed and installed the Central Heating Controller from our Nov '96 issue, highlighting a solution to a problem which other readers may encounter. He writes:

The programmer worked fine during testing with no load connected to the relay outputs. However, when installed, it ceased to function when one of the relays had operated – highlighted by a blank display. The only way to restore function was to remove and reconnect all power.

My CH system makes use of motorised valves to control water flow and I guessed that these were creating mains interference when operating, which was being fed back to the controller housing by the relay connections, and corrupting the microcontroller memory.

A 220nF X-Class capacitor connected across the pole of each relay and the mains Neutral connection solved the problem, and the programmer now functions flawlessly.

Many thanks for an excellent and practical article. David Lilley.

RING BINDERS FOR EPE

This ring binder uses a special system to allow the issues to be easily removed and reinserted without any damage. A nylon strip slips over each issue and this passes over the four rings in the binder, thus holding the magazine in place.

The binders are finished in hard wearing royal blue p.v.c. with the magazine logo in gold on the spine. They will keep your issues neat and tidy but allow you to

remove them for use easily.

The price is £5.95 plus £3.50 post and packing. If you order more than one binder add £1 postage for each binder after the *initial* £3.50 postage charge, (for overseas readers the postage is £6.00 each to everywhere except Australia and Papua New Guinea which costs £10.50 each).

Send your payment in £'s sterling cheque or PO (Overseas readers send £ sterling bank draft, or cheque drawn on a UK bank or pay by credit card), to Every-day Practical Electronics, Allen House, East Borough, Wimborne, Dorset BH21 1PF. Tel: 01202 881749. Fax: 01202 841692 (We cannot reply to queries or confirm orders by Fax due to the cost).

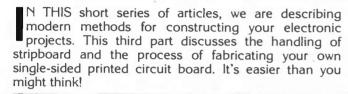
We also accept credit card payments. Mastercard (Access) or Visa (minimum credit card order £5). Send your card number and card expiry date plus cardholders

address (if different to the delivery address).

BUILD YOUR OWN PROJECTS

Alan Winstanley

Part 3



Future parts will look at case and enclosure preparation, workshop tips and tricks – in fact, everything you need to know to get satisfying results when building your latest *EPE* project!

Alan is, of course, Surgeon-in-Chief at Circuit Surgery, and enjoys all aspects of electronics.

Part Two of Build Your Own Projects, various methods for constructing electronic circuits were outlined, for building a quick prototype or assembling it in a more permanent form. The all-important topic of soldering was described, too.

This month, we look in more detail at the methods of fabricating circuits and also means of producing printed circuit boards (p.c.b.s) at home or in the workshop. So let's get down to the "nitty gritty" of assembling circuit boards!

Some years ago, stripboard was the standard "bread-and-butter" medium with which most hobbyist circuits were assembled, and it was unusual to see a printed circuit board on our projects pages. The reverse is now true, because affordable personal computer software packages (see our advertising pages) have made the design of p.c.b.s simpler than ever before.

Never-the-less, stripboard *does* still have a role to play, but it tends to be used more during the prototyping stages or for building fairly small projects where the time and trouble of fabricating a p.c.b. couldn't really be justified. Stripboard is also useful for gaining general soldering practice, perhaps using surplus components.

ising surplus components.

GET STRIPPING

Stripboard can be snapped to shape by scoring it, holding it over a sharp edge and breaking it along a row of holes, then filing the edges till smooth; I prefer to use a junior hacksaw though, for more accurate results. It's worth examining the cut edges closely to ensure that no copper swarf is present which may short adjacent strips together. Clean up any potential trouble spots using a fine file.

If necessary, clean up the copper strips with an abrasive rubber block specially made for removing tarnish. If you are working from a published design, check with the component layout master to see whether any mounting holes are needed to carry the board. These will usually be M3 (3mm) or so, diameter, but they should not be drilled too close to a corner or the board will probably break.

Special "spotface cutter" being used on stripboard copper strips to break tracks. A sharp twist-drill will also do the trick.

The mounting hardware may need to be insulated from the underside copper strips of the board, especially if steel nuts, bolts and spacers etc. are used. This is easily done using a special "spot face cutter" or even an ordinary handheld twist drill.

Drill away the copper strip (there's no need to go through the entire board!) at the appropriate places, to ensure the mounting hardware isn't in contact with the rest of the circuit. Continue by making the remaining breaks, in the copper strips as required, perhaps as you go along.

SOLDERING ON

Now it's possible to progress by soldering all the components into place on the surface-side (topside) of the stripboard, using the advice given in last month's article. It's best by far to start with the smallest, "fiddly" components while you still have an uncluttered board to work on, so start with link wires, then small resistors and other discrete components.

Link wires may be formed from tinned copper wire (e.g. approximately 20s.w.g.) which is bent to length using long-nose or round-nose pliers. If any link wires require insulating, this can easily be effected

with p.v.c. sleeving, which is slipped over the wire before soldering into place. Usually, though, plain uninsulated tinned copper wire is used and you

simply need to ensure that it's pulled reasonably tight at one end with pliers before soldering, to produce a neat straight wire which doesn't touch anything nearby.

Soldering continues by fitting in the remaining components, ensuring that all polarised parts (e.g. electrolytic capacitors and bridge rectifiers) are correctly orientated. Delicate semiconductors should not be overheated or they risk being damaged – but in any event it should take only a couple of seconds to make the perfect joint, as described last month. Some parts (e.g. large axial-lead capacitors) may benefit from being secured with a dab of hot melt glue, to help protect them against vibration.

BE ON GUARD

Never forget, CMOS devices are sensitive to static discharge and special measures are needed to handle them. The idea is to prevent any lurking electrostatic voltages from "zapping" the CMOS part, by diverting the static to ground (electrical earth) instead.

Preferably insert CMOS components into place last of all, after all other

soldering etc. has been completed. Also, ensure your soldering iron is well earthed so that no charge is carried over by the iron to the CMOS device. Before handling a CMOS component itself, discharge any static on your body by touching a well-earthed part (e.g. a water pipe or an earth terminal).

More ambitious users may want to wear an anti-static wrist strap which is plugged into an earthing point (e.g. a mains outlet Earth) via a special adaptor (which usually includes a one megohm (1M) resistor to ground). Anti-static bench mats are also available which prevent any static charge accumulating, since the mat is electrically earthed and partly conductive.

Integrated circuits – whether CMOS or bipolar – are often best used in conjunction with d.i.l. (dual-in-line) sockets to prevent thermal damage arising, and to enable faulty i.c.s to be swapped out if necessary. Unless you are using a p.c.b. assembly frame, possibly hold the sockets flush against the board with a little insulating tape while you solder their pins underneath.

Parts which may become warm (e.g. some higher-power resistors) should be "stood off" the board slightly, to allow air to circulate. Remember to finish with the largest parts last of all.

Take care not to heat the copper strips excessively or the adhesive will be damaged and the copper will lift away. You should *always* check the board very closely for errors afterwards.

Common oversights include components soldered into the wrong location, missing wire links and breaks, or incomplete breaks. Soldering defects include excess solder being applied (often with tiny "whiskers" of solder shorting adjacent strips), or the occasional "dry joint" (see last month).

FLYING LEADS

With the components now in place, the board will invariably require connection wires to be soldered to it. You can solder these "flying leads" directly to the board, or use a solder terminal-pin and solder the wire to that instead.

Flying leads are always potential weak spots because vibration may cause the wire joint to "work harden" in due course and



"Hot-melt" glue is useful for protecting larger parts from breaking loose due to vibration.



Anti-static wrist-strap is preferable when handling CMOS devices.

it will then fracture, even if you use multistranded flexible connecting wire.

Final options for the completed stripboard include using a flux-remover to clean up the solder-side of the board, and then to spray on a coating of aerosol lacquer to help prevent the copper from oxidising.

PRINTED CIRCUIT BOARD

In preference to stripboard, the most popular form of construction now used at the centre of most of our projects is the printed circuit board. (Commonly referred to as the "p.c.b.")

The constructor has two options: either purchase a ready-made p.c.b. from our *PCB Service*, or alternatively, fabricate the board from scratch. The first option is easy – see our p.c.b. listing elsewhere in this issue!

Hopefully, though, you will wish to try to make your own boards, and we encourage everyone to "try their hand" if they can afford it. Do-it-yourself production has the added benefit of allowing you to make modest batch runs of boards if needed, and you can also modify the design within reason and produce an updated board at a later date.

Printed circuit boards are usually made using glass reinforced fibre board which is immensely strong. It's fairly easy to produce boards to close tolerances but it does require the use of at least one noxious chemical (usually Ferric Chloride) which should be treated with respect.

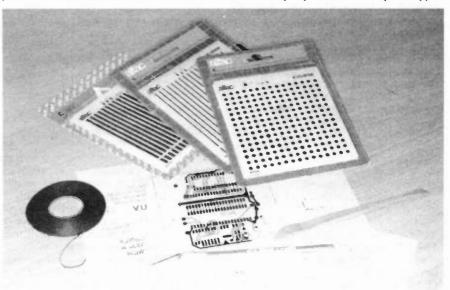
Also, the preferred way of fabricating boards requires some additional equipment, in the form of an ultra-violet exposure unit, which may be priced beyond more modest budgets. A low-voltage "mini drill", capable of accurately drilling holes of roughly Imm diameter, is another essential requirement. (See the Expo Drills & Tools Catalogue which is free with this issue.)

All the major catalogues have a section on "PCB Fabrication" or similar, and you should refer to these to obtain some idea of the product availability and their prices.

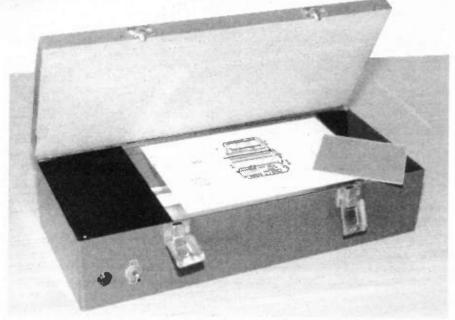
GETTING STARTED

How do you make printed circuit boards? Well, the normal method involves using a "blank" copper-clad board which is coated with an ultra-violet light-sensitive chemical, often called "UV resist". You may purchase the boards ready-coated (something I normally do, mostly to save time) which you cut to size – an electric jigsaw is useful – or you can try to coat your own blank boards using an aerosol spray UV resist.

This latter option requires practice and I don't always obtain consistent results: it's worth a try if you have some spare copper-



Materials required to create a p.c.b. artwork master.



Placing the artwork on a UV exposure unit. (Protect eyesight from UV.)

clad board available which you would like to use with the ultra-violet process to be described next.

One way or another, the p.c.b. master pattern has to be translated onto a stable clear film (normally a polyester sheet) as "positive" artwork. The black areas of the film represent the copper in the layout.

Almost every *EPE* project using a p.c.b. includes a 1:1 copper track pattern from which a photographer can produce a photo-positive for you, or you can trace the design onto film for yourself, using special p.c.b. drafting symbols and tapes. (Photocopies of the artwork can also be transparentised using special sprays available from office stationers. Ed.).

With more complex boards, the tracing option is a lengthy job which takes some practice and dexterity, but which can be a satisfying and creative task. A range of p.c.b. drafting materials is available in a variety of shapes (round pads, dual-in-line pads, straight lines, curves, etc.) from the larger mail-order houses, and the constructor has to physically place self-adhesive die-cut symbols, or rub transfers down onto the film, using the magazine artwork as a guide.

Copper tracks are formed by physically cutting line transfers to suitable length using a scalpel, and then rubbing these

down to trace the routes of the tracks. Larger black areas can be outlined with transfer lines and the central areas filled in with matt black enamel paint, for example.

It is important that the centres of component leadouts are accurately copied onto the artwork, especially those of d.i.l. integrated circuits and p.c.b. mounting capacitors etc., or the parts will mis-align and won't fit the board. Any mistakes in the artwork can be corrected by removing the the transfers with Sellotape or lifting off the die-cut materials with a scalpel. Eventually, the constructor will produce an accurate copy of the p.c.b. artwork onto film which can now be transferred onto the copper clad board.

One tip: clearly label which side of the artwork is which, or you risk producing a mirror image of the board by accident! So label the appropriate side "This Side Copper Track View" or similar. The artwork can then be stored for repeated use or modification in the future: keep it away from any sources of heat because this may distort the film.

LIGHT WORK

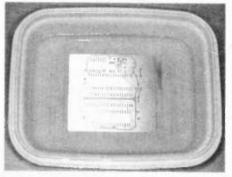
The next stage of processing involves using the artwork as a 'mask', by exposing a sensitised (UV resist-coated)

Materials needed for developing and etching printed circuit boards: Ferric Chloride crystals, developer, photoresist, caustic soda, plastic tongs, plastic tray, disposable gloves and photoresist copper board.

copper clad board to ultra-violet light, with the artwork placed over the board. The UV light source MUST be shielded from vision when in use as it is potentially harmful to stare directly at the source. A UV light box is best for consistent results, though some constructors build their own versions using UV lamps.

The artwork will prevent the UV light from passing through any black areas, but the clear regions of the artwork permit UV light to pass onto the resist-coating. It may take between 2 to 20 minutes for the resist to be fully exposed, depending on several factors, but do be prepared to experiment when you prepare boards this way for the first time.

When exposure is complete (and note that it's not necessary to use a darkroom when processing UV board), the board is placed into a liquid developer. This will quickly remove all the UV-exposed areas of the resist, leaving you with a perfect copy of your artwork made in the resist layer of the board, with raw copper everywhere else.



Exposed p.c.b. immersed in developer to remove unwanted resist.

The board is then dipped into a suitable etching liquid, which is usually Ferric Chloride solution held in a photographer's developing tray. This will completely etch away all of the raw copper in a process which takes say 15 to 30 minutes or so, depending on the age of the etchant and its temperature (warning it before use is recommended. Ed.).

After etching is complete and all the unwanted copper has been removed, the board is carefully washed down with water and the now-redundant UV etch-resist is then stripped away with a solvent or an abrasive block, to reveal the copper track pattern itself. Finally, the board is drilled to accept the components, after which the printed circuit board is ready for soldering.

The UV method is extremely accurate, and it will reproduce every imperfection in the artwork. It's often a good idea to examine and "touch up" the etch resist pattern prior to dipping into the Ferric Chloride: small quantities of acetone (e.g. nail varnish remover) can be used on a cotton bud to remove any unwanted resist, and conversely, an etch-resist pen can be used to add small areas of resist by hand, if necessary.

OTHER METHODS

Readers may hear of other "unofficial" methods of p.c.b. processing, and these are worth experimenting with. In the simplest applications, it's possible to use the transfers as etch-resist, by applying them directly onto plain copper board, which can then be etched straight away.

The so-called "toner transfer" system involves taking a good-quality photocopy of the (magazine) artwork onto clear acetate film, and then literally ironing this onto plain copper clad board! The gentle heat from the clothes iron will re-melt the toner which will now adhere to the copper, to form an etch resist. (See the news item about Press-N-Peel on our Innovations page. Ed.)

Computer users sometimes experiment by outputting p.c.b. artwork from screen onto clear film using an inkjet printer, but results are not always consistent. The creation of the artwork is often the greatest hurdle, and it is definitely worth experimenting with other techniques of artwork "origination". The most advanced techniques use CAD packages which output computer files directly to computer-aided manufacturing systems, and will not be discussed here.

RIGHT CHEMISTRY

Most mail order sources will provide the chemicals required to process printed circuit boards. Ferric Chloride is usually shipped in granular form, to which water must be added in accordance with manufacturer's recommendations.

The solution can be re-used many times, but must only be stored in plastic or glass containers, firmly sealed with the correct plastic cap (not metal). Being toxic and corrosive the fluid must be stored away from children or pets.

You must not allow etchant to come into contact with metal fittings (e.g. kitchen taps) since the product will indelibly stain many materials. Great care must be taken to ensure that it is not splashed onto skin or in the eyes. Disposable gloves and splash-proof goggles are sensible precautions when in use.

These days, there is more emphasis on the "environmental friendliness" of

chemical products, and the disposal of corrosive Ferric Chloride may understandably prick the conscience of some readers. First, the etchant will not be accepted at domestic refuse sites in the UK, and it is irresponsible to pour it on soil.

Since only very small quantities are involved, however, opinions generally seem to favour fully diluting it down and then letting it run to waste by pouring it down an outside drain, accompanied by plenty of running water. I view this as currently the most realistic and safest method of disposal, though constructors in Holland and Germany may have further restrictions due to their Special Chemical Waste regulations.

IN THE BAG

If disposal is indeed a problem then one excellent alternative which is worth considering seriously is the Seno/GS 'Etch in a Bag' system. I strongly recommend it for home or hobby use, because the Ferric Chloride is always kept in a heavy gauge sealed polythene tube and, if used correctly, it's virtually impossible to come into contact with the harmful liquid itself.

Special sliding seals are used to "sectionalise" the poly tubing, releasing the etchant over the board in a closed environment. It will accommodate up to a standard "Eurocard" 160mm × 100mm, and etching can be accelerated by warming the poly bag with a hair drier. A special neutraliser powder is included which permits safe disposal of exhausted etchant, with a completely clear conscience!

This ingenious product is available from ESR Electronic Components (Tel. 0191 251 4363 Fax 0191 252 2296) and ElectroValue Ltd. (Tel. 01784 442253, Fax 01784 460320). In my view, the Seno/GS is a must for the hobbyist working at home.

Other chemicals which will be needed include the developer solution, and etch-

resist remover. For developer, I generally use Sodium Hydroxide solution which I make up as needed by adding about 10 grammes of domestic Caustic Soda granules (available from chemists) to a litre of warm water, though this sometimes requires some trial and error. Common-sense precautions are necessary when handling caustic soda solution: avoid splashing the eyes or skin.

You can also buy a ready-made developer solution which is more convenient and will give consistent results. Etch-resist removal is easily effected with acetone used on a cotton-bud or a swab; it's readily available as nail varnish remover from the same chemist, whom by now will be giving you funny looks!

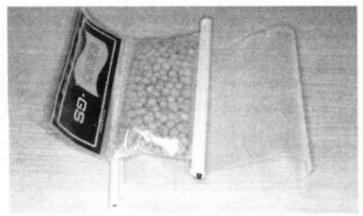
PERSEVERE WITH UV

My advice is to persevere with the UV system because it does sometimes need practice before acceptable results are evident. Success depends on ensuring that the exposure time is just right. This depends on how thick and sensitive (or "fast") the resist itself is, how far away the UV source is, and the strength of the light.

• Not enough UV (under exposure), and the etch-resist will not be exposed all the way through its depth: it will then be impossible to develop the board fully.

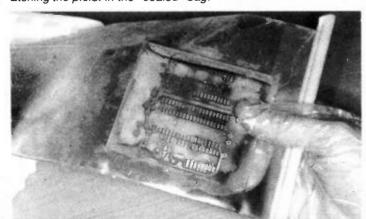
● Too much UV (over exposure) and the finest copper tracks may be undermined by the UV light, and they will disappear during developing. In precision layouts, this would obviously be unacceptable. However, it is usually not a bad idea to over-expose slightly since you would have to be quite unlucky to cause any damage this way.

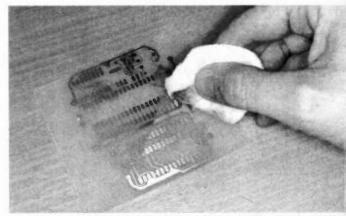
Under-exposure is a real nuisance which only becomes apparent during developing. It is virtually impossible to return the board to the UV source and expose the board for a further period, whilst trying to maintain the accuracy and alignment of the track pattern at the same time.



Steno/GS "Etch in a bag" granules prior to adding water.

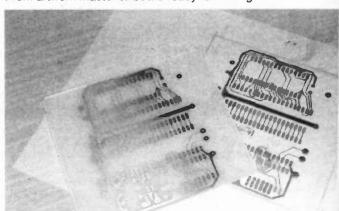
Etching the p.c.b. in the "sealed" bag.





Removing etch resist with acetone, after developing, to reveal copper track.

From artwork master to board ready for drilling.



The only real answer to this may be to remove the resist, and to spray on an aerosol resist coating, and try again. Personally, I often experience very inconsistent results with spray-on resist, due to the variations in the thickness of the final coating, but it's still worth a try.

Generally speaking though, using offthe-shelf products and a ready-made UV exposure unit, there is no real reason why you can't obtain perfect results, and p.c.b. production is a technique which adds another dimension to the hobby. Using the materials shown in the photos, I processed the p.c.b. first time as shown, and the final results were very rewarding.

FOLLOW THE DRILL

Having removed the etch resist, the final phase of p.c.b. fabrication is to carry out the necessary drilling. It's at this point that you suddenly appreciate why there is a small hole in the middle of every solder pad on the artwork

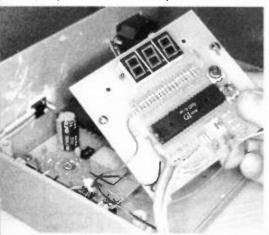
The centre of the pad is etched away, leaving a tiny drilling centre which acts as a starting point for the whirring drill. Without it, the drill will "wander", with possible disastrous results, and it becomes very much harder to drill the hole precisely.

There's no real substitute for buying a low-voltage d.c. drill with power supply. These are the best and most accurate way of drilling holes through the board, as ordinary electric drills really are too massive for this precise task. A drill may cost £15 to £30 or more and the power supply may double this cost. (Consider using your bench power supply if it is suitably rated.)

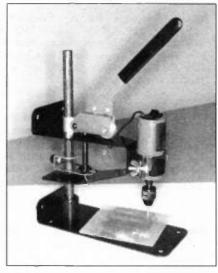
Which type of drill to buy, depends on your budget and interest, but ideally select a reasonable d.c. drill fitted with proper bearings inside, to ensure smooth running. The cheapest drills are nothing more than simple d.c. motors fitted with a chuck, and they can be quite crude to use, but at least they will help you make a start.

An extremely useful accessory for your p.c.b. drill is a vertical drill stand. This will be specially made to fit your machine and it allows you to set the height and cutting depth of the drill. They are worth investing in if you are at all serious and you need more precise control over your work; I managed for years without one.

However, cheaper drill stands (say, £30 or so) may not be as consistent or as easy to use as their more expensive counterparts which have twin pillars and are more



Completed p.c.b. with all parts soldered into place.



Low voltage drill in a stand, for more accurate control.

accurate and smooth-operating. Check the supplier's catalogues carefully.

BIT OF A TWIST

Turning to the "business end" of the p.c.b. drill itself, you will need to buy a small selection of drills which are specially made for fine work. P.C.B. drilling machines use miniature "collets" or chucks to accept them.

Usually, most holes are drilled at 1-0mm diameter, though 0-8mm may be used for dual-in-line chips and other finer wires. For larger devices, such as the larger tags of p.c.b. mounting potentiometers, or transformers, relays, etc. 1-3/1-4mm diameter is the common choice. Handy sets of drills can be bought which offer a selection of common sizes: top these up with individual items when they wear out.

Usually, drills (or more correctly, twist drills or drill bits) are made of high-speed steel ("HSS") which is adequate for p.c.b. work. However, it is a sad fact that glassfibre boards wear down their cutting edges very quickly, so treat HSS drills as consumable items and always keep some spares.

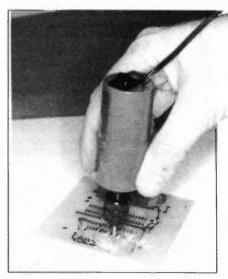
Be wary of tungsten carbide drill bits, which are up to ten times more costly: although they are much harder, they need to be run at high speeds and are extremely brittle. They will readily snap under hand pressure unless you use them in conjunction with a drill stand, but they do slice through glass-fibre with great ease.

Don't forget that you can buy other accessories for your drill, including cutters, grinding stones and polishing wheels, which you might find useful for model-making or other hobbies.

There's nothing more annoying than discovering an undrilled copper pad just as soldering commences, so check the board for omissions, and finish by drilling the larger diameter holes for the mounting hardware if used. Readers should be aware that the dust particles resulting from drilling glass-fibre boards can be intensely irritating to sensitive skins, so try to avoid skin contact and certainly do not inhale the product – also wear gloves if necessary.

SOLDERING P.C.B.s

The techniques for soldering a p.c.b. are very similar to those described earlier for stripboard. Extra care is needed



Drilling a p.c.b. by hand using a low voltage drill.

with finer tracks or smaller-diameter copper pads, though, since these will lift off if heated excessively. (Super Glue could be used as a repair.) It will take longer to solder joints positioned in large copper areas, due to the heatsinking action of the copper: a higher-capacity iron is sometimes useful at these times.

As before, start with the smallest parts first and finish with the bulkiest items. Large parts (e.g. transformers) must be completely flush against the board, otherwise vibration or knocks in use may cause the components to loosen the underside copper tracks and damage the copper foil permanently; hot melt glue will again act as a bonding agent to help protect flying leads and large parts (that don't become hot!) from vibration damage. An optional coat of spray-on lacquer will help protect the copper foil from corrosion and moisture.

As with stripboard, flying leads can be soldered directly to the board or to solder-in terminal pins. In the case of mains-voltage connections, by far the safest and most reliable method of connecting these to a p.c.b. is to use screw-terminal blocks soldered to the board. Because the mains wire itself remains unsoldered, it will not become brittle through flexing or vibration (or, more dangerously, break off from the board completely) and will remain reliable in service. More of this next month.

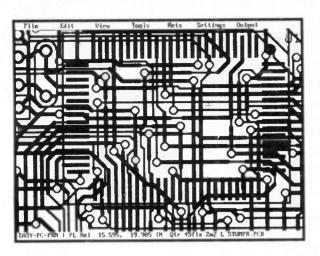
All in all, with modern materials which are readily available today, there's no reason why you can't produce results which you can be really proud of.

NEXT MONTH

In Part Four, next month, we examine workshop techniques related to plastic and metal enclosures used to house your project. We'll also check out basic metalworking methods plus case preparation, along with other tricks and tips to help you enjoy assembling your electronic prototypes.

• Internet users may like to know that a "Soldering FAQ" (Frequently Asked Questions) is currently under construction, condensed from this series. It will offer an on-line resource to help beginners with the "Art of Soldering". Check our web site for the latest news.

THE Autorouter for EASY-PC Pro' XM!

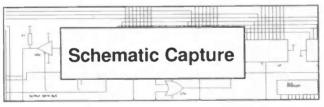


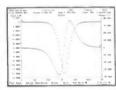
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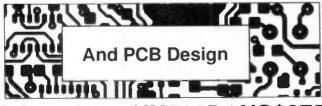




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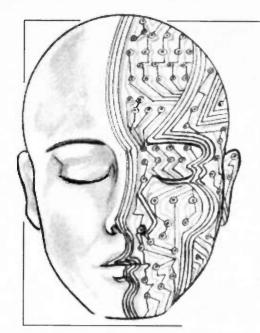
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Bicycle Mileometer - Pedal Power

THE simple circuit design shown in Fig. 1 can be used along with a ready-made l.c.d. counter module, to form a Bicycle Mileometer with an accuracy of approximately five per cent.

A reed switch, S1, is affixed to one of the forks of the cycle and a magnet is fixed to the wheel rim. The magnet causes the reed to close with each revolution, and with a wheel size of between 24 inches to 26 inches, a distance of 100th of a mile is travelled after eight revolutions of the wheel.

The circuit counts the eight pulses and then advances an l.c.d. counter each time the cycle travels 0.01 miles. Resistor R1, R2 and capacitor C1 debounce the pulse from switch S1, and each pulse then clocks IC1, a 4017 decade counter.

On the eighth pulse, pin 6 of IC1 goes high which drives transistor TR1 and causes the opto-isolator to "clock" the counter – increasing the count by 1/100th of a mile. On the next count, pin 9 goes high which resets the counter at pin 15, and the "count to eight" process re-starts.

The counter is a small battery operated unit available from Maplin, Tandy, etc. I added a Letraset "decimal point" to the left of the two least-significant digits on the display to give a direct readout in miles, which is permanently displayed. The circuit itself can be driven by a 9V PP3 battery. (The 1LD74

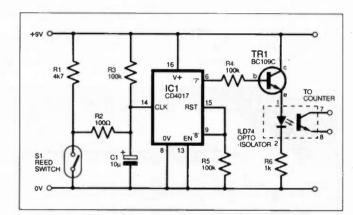


Fig. 1. Circuit diagram for the Bicycle Mileometer.

opto-isolator is a dual type, available from Farnell (Tel. 0133 263 6311) as Stock Code 325-909, but a single channel type e.g. TIL191 may be a suitable alternative. A.W.)

Nick Dossis, Middlewich, Cheshire.

Simple Stereo Amplifier - Undercover Sounds

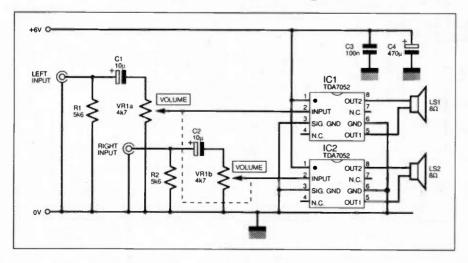


Fig. 2. Circuit diagram for a Simple Stereo Amplifier.

was once asked to build a Stereo Amplifier to permit a personal stereo to provide music in a trailer tent, and my simple solution is shown in circuit diagram Fig. 2. The circuit uses two TDA7052 bridge amplifiers, one per channel.

A stereo dual-ganged potentiometer VR1 acts as a Volume control, whilst capacitors C1 and C2 decouple the signal input. Resistors R1 and R2 are needed by some personal radios or stereos. Capacitors C3 and C4 decouple the 6V power supply.

I used four D-cells to power the unit. The two loudspeakers must have a minimum impedance of 8 ohms, as shown. (I selected two low cost Maplin 1.5W speakers).

Alan Bradley, Belfast. This novelty circuit utilises the Holtek HT82231 PCM speech synthesis chip (Maplin Order Code AE12N – A.R.W.) which is preprogrammed with eight animal sounds, the best six of which are used in this application. To add further to the novelty, the sounds are initiated using touch-sensitive switching, each being based around a pair of NAND gates.

In Fig. 3, IC7 is the sound generator i.e.; VR1 and R9 control the internal os-

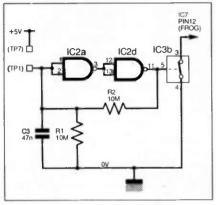


Fig. 4. Touch switch circuit.

cillator speed whilst the output (pin 19) drives a single transistor buffer TR1. This in turn drives the loudspeaker LS1, and the l.e.d. D1 provides a visible indication of operation.

Touch Tones

The animal tones are selected by grounding pins 7 to 15. By using two NAND gates as a pulse generator (see diagram of a single touch switch in Fig. 4), it is possible to select any of the control pins via a transmission gate. When the touch pads are shorted by skin resistance, the resulting voltage on the gate input is inverted and then inverted back by the following NAND to drive a transmission gate. This causes the respective control pin of the sound chip to be grounded.

The touch switch is latched on by resistor R2 and the capacitor C3 charges in about 47ms, then discharges through R1 in around 470ms, thus resetting the input at the first NAND gate and toggling the switch.

Three 4011 chips (IC2, IC4, IC5) and two 4066 chips (IC3, IC6) provide the six touch switches in total. Note that

one touch pad (TP7) is common to all switches, being at the positive rail.

Power was derived from a 9V battery using a 5V regulator (IC1). In the final assembly the touch pads were made from six 10mm squares of 1mm copper sheet with a 160mm long strip for TP7. Copper clad board could perhaps be used.

D. Stringwell, Scunthorpe, North Lincolnshire.

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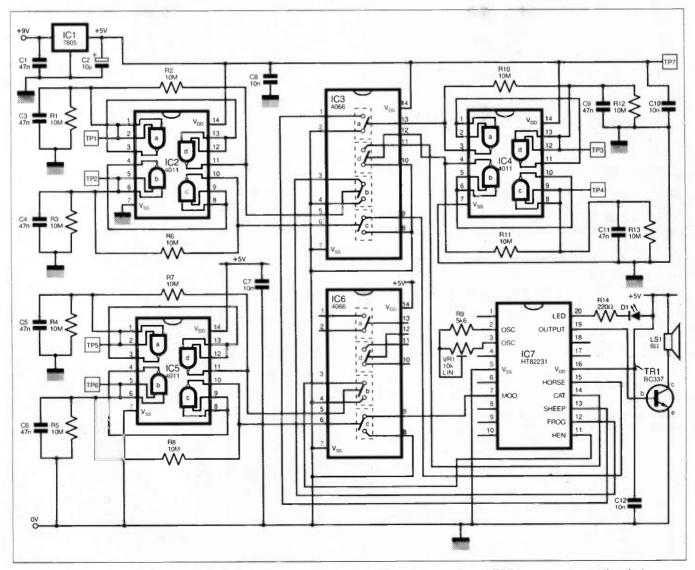


Fig. 3. Main circuit diagram for the Animal Sound Generator. Note that touch pad TP7 is common to all switches.



A three-in-one module for your PC that really measures-up to the ''real'' thing!

WHILE the idea of virtual instruments is not new, it is only recently that sophisticated systems have become available at affordable prices. The basic idea of a virtual instrument is to utilize a computer plus suitable software and an interface of some kind to replace a complex piece of measuring equipment.

The modern trend is to have on-screen "virtual" controls operated via the mouse, rather than having "real" controls on the Interface Unit. It is from this that the virtual instrument name is derived.

Systems of this type are used for all sorts of weird and wonderful things, including electronic test equipment. The "virtual instrument" reviewed here is the Velleman PCS32 Storage Oscilloscope for PCs.

Scope For A PC

Provided you already own a suitable PC, this unit offers a 2-Channel Storage Scope having a 32MHz sampling rate and an 8-bit vertical resolution for just £324-99. Furthermore, it can be switched to operate as a Spectrum Analyser or a transient recorder. (Better still, if you are a 'dab hand' at soldering, you can select a Single Channel Kit for £173-39, add a Second Channel Kit for £66-29 and a Upgrade Software for £25-49. In addition, a Demo Disk is available for £3-05 – the Demo is also available free on the Internet).

It does not require a particularly advanced PC. The minimum requirement is a 80386 processor, VGA display, mouse, and 460k of free conventional memory. The spectrum analyser program and the oscilloscope's r.m.s. readout additionally require a maths co-processor (which is built into 80486DX and Pentium microprocessors).

What You Get

The version of the PC Scope supplied for review is readymade, and is supplied complete with a soft carrying case, manual, two probes with cables and plugs, parallel cable for connection to the computer, and a mains power supply adaptor. The accompanying A5 size manual has 98 pages, but includes instructions in four languages. It tells the experienced user everything he or she needs to know in order to get the system "up and running", but those who are new to oscilloscopes will need to obtain a book or two on the subject.

The probes are standard oscilloscope type which connect to the BNC connectors on the front panel of the interface. Both include an "×10" facility which extends the system measuring range.

The power supply unit is of the oversize mains plug variety, and the one supplied with the review system had a continental

two-pin plug. However, units sold in the UK will be supplied with proper three-pin supply units for direct connection to UK mains outlets. The Interface can be powered from rechargeable batteries (not supplied as standard) if portable operation is required.

The Interface connects to printer port one (LPTI), and there is no option to use port two. As most PCs will probably have a printer already connected to port one, either a printer sharer will be needed, or the printer must be relegated to port two.

Operating software is supplied on a 3.5 inch high density disk, and is easy to install. A set-up program copies everything onto the hard disk for you. The program runs under MS/DOS, and does not require Windows. It should run from within Windows if required, provided there is sufficient free memory available. The mouse driver must be loaded before running the program via the batch file copied to the hard disk.

Facts and Figures

A maximum sampling rate of 32MHz is very respectable, but it does not mean that the unit has a bandwidth of 32MHz. As with any sampling system, the sampling rate must be at least two or three times higher than the maximum input frequency. The effective bandwidth is therefore about 10MHz or so.

While this is rather less than that of most conventional oscilloscopes, it is still adequate for most purposes, including the display of PAL video signals. The two channels operate independently, and the maximum sampling rate therefore remains at 32MHz when both channels are used.

Input impedance is the usual one megohm, and this is shunted by about 30p (picofarads) of capacitance. The maximum input voltage is 100 volts a.c./d.c. The timebase range is switchable from 100ms per division to 100ns, with the usual 1-2-5-10sequence. Triggering can be on the positive or negative edge of



The complete PCS32 outfit, minus carrying case.

the waveform, and can be from channel one or channel two. There is no provision for external triggering.

Input sensitivity is switchable from 10 millivolts to 5 volts per division, again with the usual 1-2-5-10 sequence. The $\times 10$ setting on each probe provides additional ranges of 20V and 50V per division. It also boosts the input impedance to 10 megohms. and reduces the input capacitance.

Software and Interface

The software is really three different programs, one for each function the system provides, but on-screen switches enable you to move quickly and easily from one to another. The oscilloscope program provides an on-screen representation of an oscilloscope front panel and c.r.t., complete with controls that are operated via the mouse.

For example, to operate one of the pushbutton switches you simply place the pointer over it and "click" on it with the mouse. With the rotary controls you simply "click" on the appropriate number around the on-screen control knob. The other two sections of the software operate in essentially the same fashion, but with suitably modified control layouts.

Although most of the action takes place on the screen, there are actually a few controls on the interface itself. For each channel there is a "Y" position control, and a three-position miniature toggle switch which offers a.c. and d.c. coupling, or the option of "earthing" the input. The only other control on the interface is the on/off switch on the rear panel.

I found little difficulty in adjusting to the use of a combination of virtual and actual controls. This is certainly made easier by the fairly convincing on-screen representation of a scope front panel together with the use of mouse control.

The PC532 Interface is housed in a tough plastic case having silver anodised front and rear panels. It has standard BNC connectors for the Y1 and Y2 inputs. It seems to be well made, and should stand up to many years of use.

"I have no hesitation in recommending the system. and might even be tempted to buy one myself."

Scope

Probably the vast majority of users will buy this system primarily as an oscilloscope, and will regard the Transient Recorder and Spectrum Analyser as useful "extras." The eight-bit resolution of the oscilloscope gives a vertical resolution of 256 pixels, which is high enough to show complex waveforms in a fair amount of detail. In this respect it seems to be a fair match for the modestly dimensioned c.r.t.s fitted to most conventional 'scopes.

At very fast sweep speeds the horizontal resolution suffers due to the relatively small number of samples taken per sweep. This can give a rather ragged looking waveform using the normal (linear) interpolation, but there is the option of using "smoothed" interpolation to give a better looking waveform. This option only operates on the three highest sweep speeds.

Triggering can be positive or negative, and there is the option of continuous triggering or single-shot operation. The trigger level is set using two virtual pushbuttons, and an on-screen marker, left hand side of the display, shows the selected trigger level. Triggering can be switched off if a free-running timebase is required.

On-Screen

In addition to the Y position controls on the interface, there are on-screen X position controls. The system takes more samples than the screen can display at one time, and the X position controls enables the "missing" right hand section of the waveform to be scrolled onto the screen.

There is a "SAVE" control which writes the screen display to the hard disk in TIFF format. The file can then be loaded into a TIFF compatible program, which includes many illustration programs, word processors, and desktop publishing programs. I had no difficulty in loading saved files into programs such as Corel Draw! and Micrografx Designer. See Fig. 1.

The top section of the "c.r.t." screen shows the selected input

sensitivities and sweep rate. The bottom section shows the calculated r.m.s. voltage of the signal on channel one. There are also three other figures which operate in conjunction with two pairs of moveable on-screen markers. The basic idea is to move the markers so that they tightly enclose one complete cycle. The figures in the bottom part of the "c.r.t." area then show the period of one cycle, input frequency, and peak-to-peak input voltage.

Oscilloscope Specifications

Minimum system requirements

IBM compatible PC with 80386 processor and maths

co-processor

VGA display

Free Printer port LPT1

Mouse

460Kb free conventional memory

Technical Data

Vertical Deflection

Sensitivity: 10mV to 5V/Div Frequency Range: D.C. to 16MHz Input Impedance: 1MΩ//30pF

D.C. - A.C. - Gnd Input coupling:

Input voltage: 100V max (D.C. + peak A.C.)

Horizontal Deflection

100ns to 100ms/Div Timebase

Triggering

single, automatic or free running Trigger mode:

positive or negative Slope:

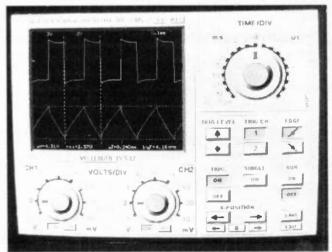
adjustable in steps of 1/2 division Level: Channel 1 or Channel 2 Trigger Channel:

Digital Storage

Resolution: 8-bit

Sampling rate: 32MHz (max) Memory size: 4Kb/channel

Interpolation: linear or smoothed



PC screen picture showing the "virtual" controls for the Storage Oscilloscope. The scope "screen" displays stored signals from a simple triangular/squarewave oscillator. Imperfections on both signals are clearly displayed.

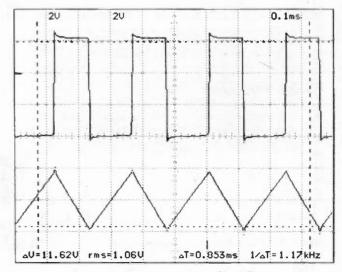


Fig. 1. Screen printout via Corel Draw.



PCS32 PC Scope Interface front panel layout.

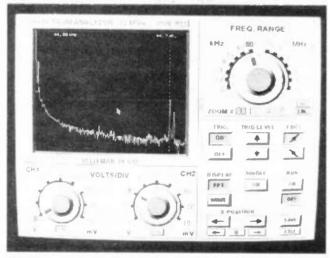
The frequency display is useful, and saves wear on your pocket calculator. It would be better still if the program worked out the input frequency and peak-to-peak voltages for you.

Spectrum Analyser

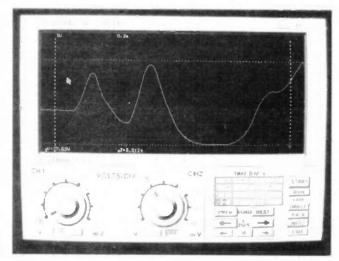
The Spectrum Analyser function shows the frequency components present in a signal, and their relative strengths. A repetitive signal such as a squarewave or a triangular signal consists of a fundamental frequency plus various harmonics (multiples of the fundamental frequency).

Using the Spectrum Analyser it is possible to determine which particular harmonics are present, and their strength relative to the fundamental signal. It will also show any signals at non-harmonically related frequencies caused by imperfections or noise on the signal.

When switched to the Spectrum Analyser mode the screen display is similar to the one used for the Oscilloscope mode. However, only one channel or the other can be active at any one time,



Spectrum analysis of a 1kHz sinewave showing high frequency noise.



Recording a low frequency signal using the Transient Recorder.

and the timebase operates in terms of the maximum display frequency. There are seven ranges from 800Hz to 16MHz.

The X-axis represents frequency, and can have either logarithmic or linear scaling. The Y-axis represents amplitude, and the amplitude scaling is always logarithmic (10dB per division). The display can be switched to a conventional waveform display if required.

A conventional spectrum analyser is based on a swept bandpass filter, but this is not the method used in this case. Instead, some advanced mathematics are used to analyse the digitised signal and calculate its frequency content. It is for this reason that this facility requires a PC which has a maths co-processor.

Results from the Spectrum Analyser seem to be very plausible, giving suitable displays for a range of test waveforms. Even using a relatively slow PC (a 33MHz

30386DX) it only took about two seconds for the signal to be analyzed and the results to be displayed.

"The use of 'virtual' controls is not simply a gimmick, it really does help to make the systems quicker and easier to use."

The display shows the amplitude difference between two vertical axis screen markers. More usefully, it also shows the frequency represented by a horizontal screen marker. To determine the frequency of a peak in the display you simply move the marker over the peak, and read-off the frequency.

Transient Recorder

A somewhat different screen layout to the other two is shown by the Transient Recorder Program, but it still uses what is broadly the same method of control. The "c.r.t." area occupies the full width of the screen.

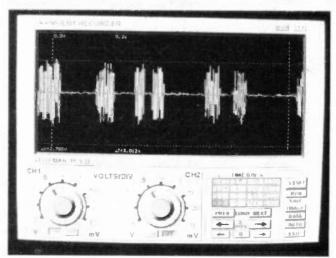
A Transient Recorder is really just a form of low frequency oscilloscope. The one in this system operates with a timebase range of 50ms to 2000s per division. The required speed is selected via sixteen on-screen pushbutton controls.

The storage scope function operates by first taking in a full set of readings, and then producing the display. The Transient Recorder operates in ''real-time'', with transients being displayed as they occur.

This is obviously a more specialised function than the standard storage scope function, but it does have its uses. For example, it can be useful when testing envelope shapers in electronic music equipment, and it can also be used for such things as recording data from temperature sensors over a long period of time. In fact the type of thing where a conventional oscilloscope is mediocre or completely useless.

Conclusion

I did not have a chance to use the PCS32 system over a long period of time, but during a test period of two or three weeks it always functioned well. It did not work properly with a 75MHz Pentium PC, but this seemed to be due to a lack of free memory. A boot-up disk which omits any unnecessary drivers should cure problems of this type.



The Transient Recorder used to monitor intermittent bursts of signal.

AVAILABLE OPTIONS

 Full PCS32 System
 51950
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 51268
 £173-39

 Second Channel Kit
 51270
 £66-29

 Upgrade Software
 51949
 £25-49

 Constant
 £25-49
 £25-49

Demo Disk 51269 £3-05 (Inc. P&P)

(The Demonstration software is also available free on the internet – http://www.maplin.co.uk/velleman/velleman.htm)
These prices include VAT, – carriage is Free on orders over £30.

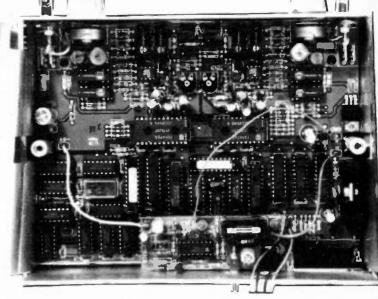
Judging by this internal shot of the PC Scope Interface, the task ahead looks fairly daunting if you undertake the DIY approach – but the rewards will be most satisfying.

Provided you are familiar with oscilloscopes, the system is very straightforward to use. In fact, it is so straightforward to use that the information on the back of the box tells you practically everything you need to know in order to use the equipment effectively. The use of virtual controls is not simply a gimmick, and it really does help to make the systems quicker and easier to use.

Although PC prices are falling, the cost of a "ready-built" PCS32 system and a suitable PC is still considerable, and likely to total £1000 or more. At this sort of price the system still represents quite good value for money, but virtual instruments are most attractive to those who already own a suitable computer system.

A Dual-Beam Storage Scope, Spectrum Analyser, and Transient Recorder, with the ability to print out results from any of them, are all here for just £324-99. This represents a remarkable bargain. I have no hesitation in recommending the system, and might even be tempted to buy one myself!

For around the same price or less it is possible to obtain a few ready-made oscilloscopes, but they have relatively limited specifications. For some types of servicing a conventional oscilloscope might still be a better option. If you just require a basic oscilloscope, a conventional instrument provides a simpler and less cumbersome alternative to this system. If you require anything more



than basic scope functions and have a suitable PC, there seems to be no conventional instrument that offers a similar specification at a comparable price.

Prices

The system reviewed here is the complete and ready-built version of the PCS32. For those who have the necessary experience there is a single channel kit version which has only the storage scope software. A second channel upgrade kit is available, as is a software upgrade to provide the spectrum analyser and transient recorder functions. Finally a demonstration disk is available, and this should help to give prospective purchasers the "feel" of the system. All items are available from Maplin Electronics, PO Box 3, Rayleigh, Essex, SS6 2BR (Tel. 01702 554000). The order codes and prices are listed in the Options Panel.

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INTERFACE

Robert Penfold



TWO or three recent *Interface* articles have been devoted to computerised test equipment of the measuring variety. Computers are also used to control signal generation, which is the subject of this month's article.

There are two basic approaches to the problem, one of which is to use purely digital techniques to generate the basic signal, with linear circuits only being used if some waveform conversion is required (a squarewave being converted to a sinewave for example). This method has the advantage of producing what are normally very accurate output frequencies, but practical circuits are usually quite complex. It is an interesting subject, and one that will be covered at a

Going Digalogue

The second and more simple method uses a combination of digital and analogue techniques ("digalogue" circuitry?). The basic technique is to use a digital-to-analogue converter to generate the control voltage for a v.c.o. (voltage controlled oscillator).

A high degree of linearity is available from modern digital-to-analogue converters, but the linearity of v.c.o.s tends to be not so good. Also, v.c.o.s often have large offset voltages that can complicate matters

However, a simple setup of this type can provide reasonable accuracy. In fact, the accuracy should be at least as good as that obtained from a conventional signal generator having a calibrated control knob.

One slight drawback of this method is that suitable frequency measuring equipment is needed in order to get the finished unit working accurately.

Stepping Up

Of course, any form of digital control produces an output signal that is incremented in steps, rather than having the fully variable output frequency of a conventional signal generator. Provided there are a sufficient number of steps this should not be of any practical significance, and the resolution of the system will be adequate for any normal testing. Eight-bit resolution gives 256 output frequencies per range, which is adequate for all but the most critical of testing.

The circuit diagram for a simple 8-bit Digital-to-Analogue Converter, based on a ZN426E (IC1), is shown in Fig. 1. Converters based on the ZN426E DAC have been covered in previous *Interface*, articles, and so we will not dwell on this part of the unit. Any 8-bit latching output port should drive the circuit properly, including a PC printer port.

The maximum output voltage from IC1 is 2.55V, but this is boosted to around 9V by the simple non-inverting amplifier based on IC2. Note that

the CA3140E used for IC2 is a type that can operate as a single supply d.c. amplifier.

Most other operational amplifiers (741C)LF351N, TLO71CP, etc.) will not work The this circuit. CA3140E has PMOS input stage, and the standard anti-static handling precautions should therefore be observed when dealwith this component.

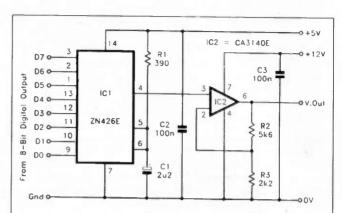


Fig. 1. Circuit diagram for the D/A Converter. The full scale output is about 9V.

Signal Processing

Circuit details for the v.c.o. and signal processing stages appears in Fig. 2. IC3 is a CMOS 4046BE "micropower" phase-locked loop, but in this circuit only the v.c.o. section is utilized.

No connections are made to the other sections of the device, apart from the input to the phase comparator (pin 3) which is connected to the 0V rail. This is done simply to avoid spurious operation of the unused stages.

The analogue-to-digital converter circuit (Fig. 1) provides the control voltage to pin 9 of IC3. C4 is the timing capacitor, and the timing resistance is provided by resistor R5 and preset VR2. The latter is adjusted so that an output frequency of 255kHz is obtained with the output voltage from the converter at maximum.

With perfect linearity and no offset voltage, this would give an output frequency range of 0Hz to 255kHz with a resolution of 1kHz. In practice the linearity of IC3 is far from perfect, and there is a small offset voltage. In other words, a small input voltage is needed before IC3 will start to oscillate.

A resistance from pin 12 to "ground" (0V) can be used to trim out the offset and to some extent improve the circuit's linearity. This is the purpose of resistor R4 and preset VR1.

Two basic approaches are possible when adjusting preset VR1. You can either opt for a slightly restricted output frequency range but with very good linearity, or a wide frequency range with reduced frequency accuracy.

Setting-Up

In either case it is a matter of first setting preset VR2 for the correct full scale output frequency. In other words, write a value of 255 to the converter (IC1) and then adjust VR2 for an output frequency of 255kHz.

Next the converter's output is set at a low voltage, and VR2 is adjusted for the appropriate output frequency. For example, a value of 25 could be written to the converter, and VR2 would then be set for an output frequency of 25kHz. This procedure is repeated a few times until good accuracy is obtained at both ends of the frequency range.

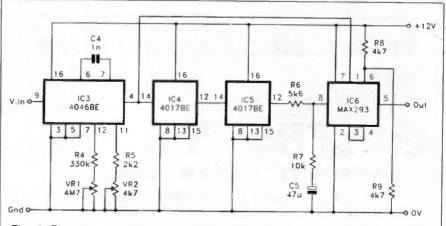


Fig. 2. The v.c.o. (voltage controlled oscillator) and signal processing stages. IC6 provides a sinewave output signal.

Using calibration frequencies of 25kHz and 250kHz gives a useful 10:1 frequency span, and good accuracy from 25kHz to 250kHz. Unfortunately, the accuracy on frequencies below 25kHz is not likely to be very good, especially at the lowest output frequencies.

Better accuracy at low frequencies can be obtained by using a calibration frequency of (say) 2kHz instead of 25kHz. The problem with doing this is that the mid-range accuracy is likely to suffer.

Since relatively few frequencies are available below 25kHz, there is little to be gained in using these frequencies, but a lot to be lost in terms of overall frequency accuracy. Consequently, it is probably best to opt for an accurate 10:1 frequency span having good accuracy, and leave frequencies below about 20kHz unused.

Increased Range

The output from pin 4 of IC3 is a reasonably good squarewave signal having a peak-to-peak amplitude of about 12V. IC4 and IC5 act as divide-byten circuits which provide two additional frequency ranges.

Maximum output frequency from pin 12 of IC4 is 25kHz, and the resolution is 100Hz. A maximum output frequency of 2-5kHz is available from pin 12 of IC5, and has a resolution of 10Hz. Both signals are 12V peak-to-peak squarewayes.

nals are 12V peak-to-peak squarewaves. The output from IC5 is processed by IC6 to produce a form of sinewave output. A repetitive signal such as a squarewave type consists of a fundamental frequency plus harmonics (multiples) of that frequency. By using heavy lowpass filtering it is possible to attenuate the harmonics to an insignificant level, so that a reasonably pure sinewave is left. In this case the lowpass filtering is provided by IC6, which is a switched capacitor filter.

A normal R/C lowpass filter consists of a resistor and a capacitor connected in the manner shown in Fig. 3a. Resistor R_a limits the rate at which capacitor C_a can

charge and discharge.

If the input frequency is low enough, this current limiting has no significant effect since only a very low current is needed in order to keep the charge on C_a equal to the input voltage. Above a certain frequency the limiting effect of R_a becomes very significant, and causes increasing losses through the circuit.

In fact, it ultimately results in each doubling of the input frequency causing the loss through the circuit to

be doubled. The cutoff frequency is governed by the values of R_a and C_a , and it is inversely proportional to their values.

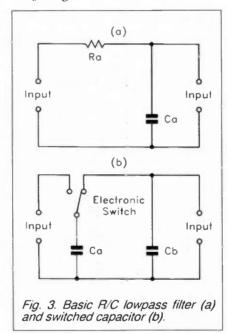
A Switch In Time

A higher attenuation rate can be obtained by using several filter stages in series. A variable cutoff frequency can be produced by using variable resistors or capacitors. However, a *C/R* filter having a large number of stages plus a variable cutoff frequency is rather impractical, especially where electronic control of the cutoff frequency is required.

A basic "switched" capacitor filter uses the arrangement shown in Fig. 3b. This is similar to the C/R lowpass filter, but the resistor has been replaced by a small capacitor (C_a) and an electronic

switch.

The latter is controlled by a clock oscillator, and continuously alternates between its two settings. Capacitor C_b is the filter capacitor, and is the equivalent of C_a in Fig. 3a.



Like R_a in the R/C filter, the switch and capacitor C_a provide a signal transfer from the input to the output of the circuit. If the input voltage rises, C_a is repeatedly charged from the input signal and discharged into C_b . If the input voltage falls, C_a is repeatedly charged from C_b and discharged into the signal source.

The main factors governing the cutoff frequency are the relative values of C_a and C_b , and the clock frequency. It is this second point that is of great practical importance, and in most practical circuits the cutoff frequency is one fiftieth or one hundredth of the clock frequency. The cutoff frequency can be varied by altering the clock frequency, and there is no difficulty driving a multi-stage filter from a common clock signal.

Sharp Filtering

Filtering a squarewave signal to produce a passable sinewave requires some pretty sharp filtering. The MAX293 used for IC6 is an 8th order elliptic filter which does the job very well. Its cutoff frequency is one hundredth of the clock frequency.

The clock signal is taken direct from the v.c.o., and the signal input of IC6 is driven with the divided-by-100 signal from IC5 via an attenuator. IC6 therefore allows the fundamental signal from IC5 to pass unhindered, but the harmonics (which are at upwards of 200 times the clock frequency) are severely attenuated. The output level from IC6 is approximately 10V peak-to-peak.

One drawback of this method of sinewave generation is that the output waveform is a stepped type, although the stepping can be removed using conventional lowpass filtering. This method does not produce highly pure output waveforms anyway, and the distortion level is comparable to a simple Function Generator at about one per cent.

Switched Range

The simplest way of providing additional sinewave frequency ranges is to replace capacitor C4 with two or three switched capacitors. A value of 10nF will provide a maximum output frequency of 255Hz with a resolution of 1Hz.

Due to the self-capacitance of the 4046BE, a value of 33pF rather than 100pF provides a maximum output frequency of 25·5kHz. The resolution is then 100Hz.

The 4046BE cannot be guaranteed to operate right up to the frequency of 2.55MHz needed to produce a 25.5kHz sinewave, but the three devices tested all just about managed it. In order to obtain good accuracy on all three ranges R4, R5, VR1, and VR2 should be duplicated for each range, and selected via the range switch.

Each range of the circuit can then be individually calibrated.

CIFIC WAVE SOUNDS
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Post Code

THEREMIN MIDI/CV INTERFACE

ADAM FULLERTON

Part 1

Retro-fit your Theremin into a MIDI chain for 21st Century music control!

NCE the birth of the Theremin some 78 years ago, there have been few variations on the basic theme, and the design philosophy on which they are based has remained relatively unchanged. As such, it is fair to say that the Theremin has for some years been thought of, if at all, as a product of a bygone era, a veritable dinosaur in the world of the silicon chip.

However, things are changing. Since the advent of the microprocessor, technology has exploded at an exponential rate. Many old ideas and concepts have received the "retro-refit" treatment thereby bringing them into line with today's technology. It is an all-encompassing process from which nothing can escape indefinitely, not even Theremins.

This project gives the Theremin its long awaited "refit". It is hoped that it may be a step towards attracting the new interest which will be necessary for the continued development of this unique musical instrument into the 21st century.

DESIGN OBJECTIVE

The objective was to produce a generic MIDI/CV interface that could be used with any existing Theremin without the necessity for modification or a special interface connector. It is an ideal complement to the EPE Elysian Theremin of Nov/Dec '96. (MIDI, by the way, stands for Musical Instrument Digital Interface, and CV stands for Control Voltage.)

It seemed like the best way to do this was to analyse the Theremin's audio signal. The resulting design is a combined hybrid of analogue and digital electronics.

This MIDI/CV Interface is not only useful for Theremins, but it can be used to interface any monophonic (one note at a time) musical instrument to MIDI. The human voice is no exception to this, so into the domain of pitch to MIDI!

PROJECT OUTLINE

It is stressed that this design is too complex to be tackled by newcomers to electronics. Although the project appears straightforward to construct, if any trouble-shooting does turn out to be required, beginners could find themselves in difficulties.

The Theremin MIDI/CV Interface (MCV for short) is a pitch/amplitude to MIDI and CV interface. There are 128 user patches which can be loaded from the front panel, or footswitch or remotely via the MIDI program change message. Each patch contains detailed setup parameters, including Octave Range, Pitch Bend Range, Amplitude Sensitivity, Velocity Sensitivity. Volume Sensitivity, Tone Offset, Program Change, and more!

A Hold footswitch is available to allow a note to be held. Two Control Voltage outputs are provided for Pitch and Amplitude. The Gate and Trigger signals are amplitude threshold switched, with control of the switch threshold. The source signal of the CV interface may also be switched to incoming MIDI, to allow use as a standard MIDI to CV converter.

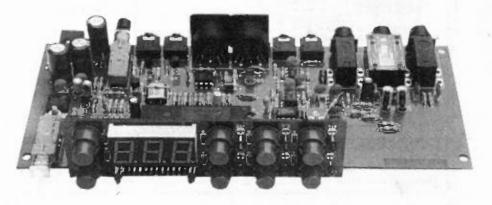
The MCV is capable of simultaneous Theremin to MIDI and MIDI/CV conversion. The Pitch Bend controller (1 to 48 semitones definable) is used in conjunction with the RPN 54H (Registered Parameter Number 54 hex) Portamento control to follow the pitch of the Theremin. Pitch is resolved down to ± 2.5 cents over eight octaves, with 10 cents hysteresis (to reduce the amount of useless MIDI data transmitted from "wobbly hand syndrome").

The Channel Volume message is used to control the amplitude, and can be assigned to Channel Pressure (aftertouch),

SPECIFICATIONS

- ★ Interfaces to any Theremin
- ★ Pitch and amplitude sensitivity
- ★ 128 user-programmable patches
- ★ Real-time pitch readout
- ★ 8-octave pitch tracking
- ★ ±2.5 cents pitch resolution
- ★ 14-bit pitch bend data
- ★ Octave range control to 1 semitone
- ★ Glissando and Portamento options
- ★ Auto-octave switching
- ★ Velocity sensitivity
- ★ Volume sensitivity
- ★ Octave and tone transpose control
- ★ Tone offset
- ★ MIDI merge Theremin sequence control
- ★ 4-function footswitch control
- ★ CV voltage and scaling control
- ★ Two 1V/octave voltage outputs
- ★ Gate and Trigger 5V/15V and switch definable
- ★ Aftertouch and Poly-pressure assignment
- ★ Echo-back facility
- ★ 3-digit 7-segment l.e.d. display
- ★ 19-inch rack case, 1/2 width 1U

poly-pressure and virtually any other MIDI controller. An Echo-back facility is provided since there is no MIDI THRU terminal. This merges the Theremin MIDI data with incoming MIDI data, allowing the user to control sequencers with a Theremin.



HOW IT WORKS

The project is shown divided down into its basic blocks in Fig.1, allowing each part to be discussed in bite sized chunks.

Each of the blocks could be divided down further to provide a more complex and accurate block diagram, but given the simplicity of the circuit concept, the basic block diagram is sufficient to explain the operation.

As indicated by this diagram, the CPU (Central Processing Unit) block is the core of the design; the analogue and digital hardware are carefully bound together by the software executed by the CPU.

Pre-programmed CPUs (microcontrollers) are obtainable as detailed later.

Throughout this article, reference is made to various software listings of the control codes used by the CPU. These are partial extracts from the main software and may be of interest to programmers.

Space prevents their inclusion here, but they are available on 3.5inch. PC-compatible disk from the Editorial office (see the EPE PCB Service page – you get all sorts of other software on this disk as well!). The listings are also available FREE from our web site: ftp://ftp.epemag.wimborne.co.uk in sub-directory pub/PICS/MIDICV.

For copyright reasons, the *full* software code listing for the MCV is not available for examination.

THEREMIN INPUT

The Theremin input block must extract the pitch and the amplitude of the incoming signal, and present it in a form that can be readily understood by the CPU. Pitch or frequency may be equally represented by time since t = 1/f (t = time and f = frequency);

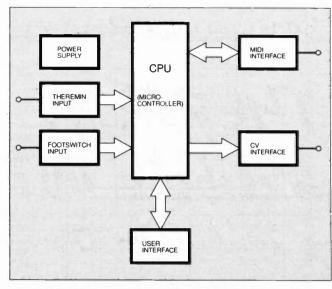


Fig. 1. Block diagram for the Theremin MIDI/CV Interface.

the conversion is simple, and time is easily measured by a CPU.

If the Theremin produces a complex waveform, it may require heavy low-pass filtering or a DSP (Digital Signal Processor) running a Fast Fourier Transform (FFT) algorithm to extract the fundamental harmonic. However, the Theremin output

is close to that of a sine wave so the fundamental harmonic is readily available.

The Theremin signal is fed into two separate circuits, one to extract the amplitude of the signal, and one to extract the pitch. The changing amplitude of the Theremin signal is referred to as the envelope.

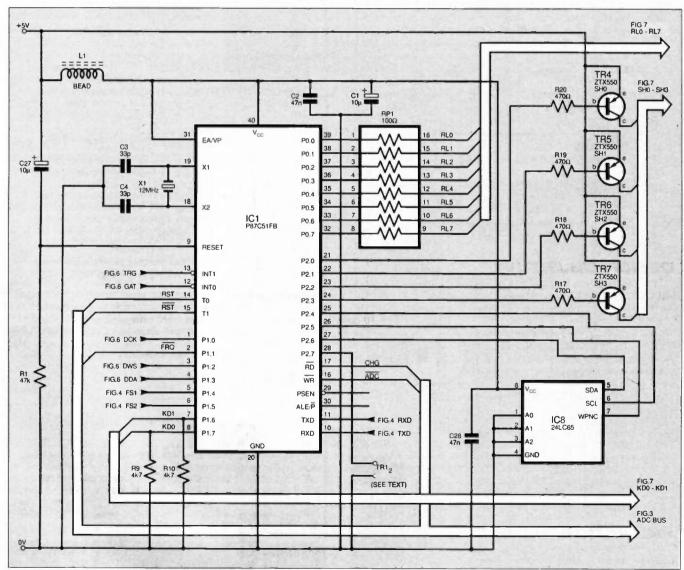


Fig. 2. Circuit diagram for the heart of Theremin MIDI/CV Interface, the microcontroller. Also seen are the ADC, and the l.e.d. bus drivers.

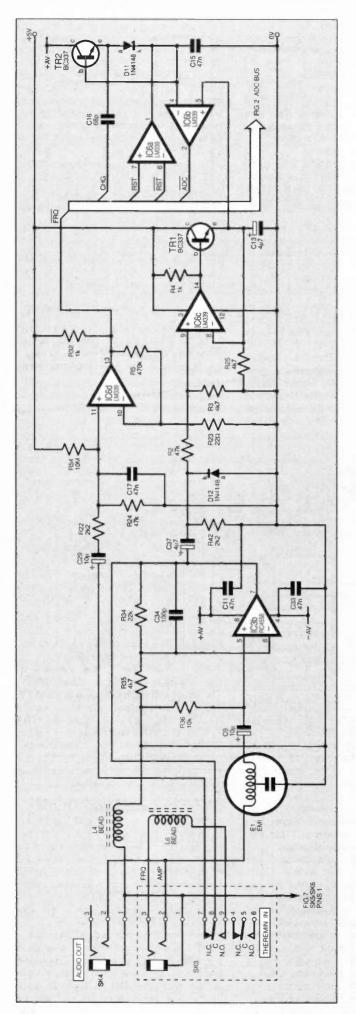


Fig. 3. Circuit diagram for the Theremin input stage.

COMPONENTS

Resistors R1, R2, R24	47k (3 off)
R3, R9, R10, R14, R25, R35, R37, R38, R41, R44, R51, R52 R4, R8, R12, R15, R32,	4k7 (12 off) See
R43, R45, R46, R53 R5	1k (9 off) 470k SHOP
R6, R7, R11, R48 R13, R36, R39, R40	220Ω (4 off) 10k (4 off) TALK Page
R16, R26, R27, R47 R17 to R20, R28, R29	33Ω (4 off) 470Ω (6 off)
R22, R30, R31, R42, R49, R50	2k2 (5 off)
R23 R34	22() 22k
R54 RP1	10M 100Ω 8-resistor module
All resistors 0.25W 5% carbon	tilm or better

Potentiometer

VR1 10k horizontal preset

Capacitors C1, C26 C2, C6 to C8, C10 to C12, 10 µ tantalum, 6.3 V (2 off) C15, C17 to C25, C28, 47n ceramic, 63V (21 off) 33p ceramic, 63V (2 off) C32, C33, C35, C36 10μ radial elect. 16V (5 off) 4μ7 radial elect. 16V (2 off) C5, C9, C27, C29, C38 C13, C37 470μ radial elect. 35V (3 off) C14, C30, C31 C16 68p ceramic, 63V C34 100p ceramic, 63V C39 47μ radial elect. 16V

Semiconductors

D1, D2, D14 to D16. D18 to D20 red l.e.d. (8 off) D3 to D12, D17, D24, D25 1N4148 signal diode (13 off) 1N4001 rectifier diode (3 off) BZX79C16 16V 500mW Zener D21 to D23 D26 diode D27 BZX79C5V1 5V1 500mW Zener diode TR1, TR2, TR8 to TR10 BC337 npn transistor (5 off) ZTX550 npn transistor (5 off) TR3 to TR7 IC1 P87C51FB microcontroller, pre-programmed (see text) LM7805 5V 1A voltage IC2 regulator IC3 to IC5 RC4558 dual op.amp (3 off) IC6 LM339 quad comparator IC7 6N138 opto-isolator IC8 24LC65 8K serial EEPROM

Miscellaneous

IC9

E1 L1 to L6 ferrite beads, mini, general purpose r.f. (6 off) SK1 RCA power input socket, p.c.b. mounting SK2, SK4. SK9 1/4in. stereo jack socket, p.c.b. mounting (3 off) multi-pole 1/4in. jack socket, p.c.b. mounting SK3 SK5 to SK8 3.5mm stereo jack socket (4 off) 5-way 180° DIN socket, p.c.b. mounting (2 off) SK10, SK11 S1, S2 s.p.d.t. latching pushswitch, p.c.b. mounting (2 off) S3 to S10 s.p. push-to-make switch, p.c.b. mounting, large button (8 off) 12MHz crystal X2 3-digit 7-segment I.e.d. display, p.c.b. mounting, common anode

TDA1543 dual serial ADC

Printed circuit boards (3 off) available as a set from the *EPE PCB Service*, code 130; d.i.l. sockets (see text); 19-inch rack mounting case, 1/2 1U; 12V a.c. 500mA mains adaptor; red filter for display; switch caps for S1 and S2 (2 off); nuts; bolts; washers; solder, etc.

Approx Cost Guidance Only

£135 excl. case

MICROCONTROLLER

One of the Intel MCS-51 single chip microcontroller family is used as the "brains" (CPU) of the circuit, designated as IC1 in Fig. 2. Timing is set by the 12MHz crystal, X1; capacitors C3 and C4 are the additional components required to complete the oscillator circuit.

Between them, components C27 and R1 provide a reset signal when power is applied. Everything else in the way of control is provided by the microcontroller, giving a "plug in and go" solution.

Device IC8 is a serial electrically erasable programmable read-only memory (EEPROM). This provides the microcontroller with a non-volatile memory facility, and having just a simple three-wire interface.

The Microchip 24C65 EEPROM used as IC8 is an 8K byte device having a high endurance block of memory that may be written to and erased more than 10,000,000 times. This makes it particularly suitable for this application.

The software code for accessing the EEPROM is on the EPE disk as Listing 1.

INPUT CIRCUIT

Referring to the circuit diagram in Fig. 3, socket SK3 is the Theremin input point. When a stereo jack plug is inserted here, the tip of the plug is connected to the input buffer circuitry (for amplitude extraction), and the collar is connected directly to the pitch extraction circuit, to allow a continuous pitch signal to be injected.

Component El is a passive EMI (electromagnetic interference) filter that helps reduce any r.f. (radio frequency) entering the buffer circuit. Inductor L4, a ferrite bead, assists similarly.

Components C9 and R36 a.c. couple the input signal to IC3b, which is wired as a voltage follower with a gain of 5.6, as set by R34 and R35. Capacitor C34 helps with high frequency stability.

When a mono jack plug is inserted into socket SK4 and there is no plug in SK3, the pitch extraction circuit is fed directly from the output of the input buffer. The gain of the input buffer is quite high because of the simplicity of the pitch extraction circuit. Small amplitude signals are more difficult for it to deal with.

Inductor L6, also a ferrite bead, assists with r.f. immunity at SK3.

ENVELOPE EXTRACTION

From the output of 1C3b, capacitor C37 a.c. couples the signal to the envelope extractor around IC6c, configured as a voltage comparator. Diode D12 prevents this signal from dropping below -0.6V while resistors R2 and R3 attenuate its positive aspect.

Resistors R4 and R25, transistor TR1 and capacitor C13 form the basis of a peak hold circuit. If the input voltage is greater than the voltage on C13, the open collector output of IC6c is in a high impedance state. Resistor R4 pulls the base of TR1 high causing C13 to be charged, capturing the peak input voltage on this capacitor.

When the voltage on C13 is a few microvolts greater than the input voltage, the open collector output of IC6c becomes low impedance, pulling the base voltage of TR1 down to 0V. This stops C13's charge current and holds the peak voltage, leaving R25 to set a time constant over which C13's voltage will fall to 0V.

The voltage on C13 is a crude half-wave rectified representation of the amplitude of the Theremin signal. The fact that it is crude does not really matter since the software can provide more complex digital filtering to smooth over the cracks.

The next part of the circuit allows the microprocessor to convert the voltage on C13 into a number. Rather than use an analogue-to-digital converter (ADC) chip, a "home baked" circuit was used for component cost reasons.

Capacitor C16, transistor TR2 and diode D11 form an "edge-to-voltage converter" in conjunction with integrator capacitor C15. The microprocessor applies a pulse to C16 from pin 17, which causes D11 and TR2 to dump a small lump of charge onto C15. Each pulse applied to C16 by the microcontroller is counted until comparator IC6b reports (via its output pin 2) that the voltage on C15 is greater than the voltage on C13.

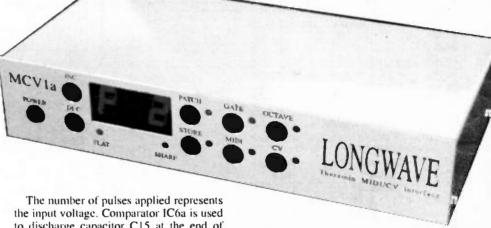
software implementation is preferred; this also allows easier printed circuit board (p.c.b.) routing, because it gives freedom of choice of the port pins used.

The use of a digital filter to process the samples adds a good "feel" to the performance of the circuit. The digital filter used was a simple implementation of an R/C low-pass filter written in C. The mathematics boils down to a multiplication, an addition and a subtraction. The following C code illustrates the implementation of this filter.

sampleo = (K * accumulator);accumulator = accumulator - sampleo + samplei;

K = cutoff frequency to sample rate coefficient sampleo = output sample samplei = input sample accumulator = analogy of a capacitor

This shows how easy it is to implement a digital filter, simply two lines of C! However, the function shown in Listing 3 on the disk is the final implementation.



to discharge capacitor C15 at the end of each conversion.

If you place an oscilloscope probe on pin 1 of IC6 you will see many waveforms, each ramp waveform represents an amplitude sample. If you look carefully, you will also see little bright spots on the ramp line. This is because an interrupt service routine (ISR) briefly stops the microcontroller from executing the amplitude extraction function.

Since there is only a high impedance path to ground, the charge on C15 remains for quite some time, so this small interlude from the conversion function does not affect the result.

This unusual "edge-to-voltage" circuit evolved to allow frequency independent operation, making it possible for ISRs to occur within the conversion function.

The function that performs the analogue to digital conversion was written in assembler for speed and is on the disk as Listing 2. Notice in the Listing how the bit-addressable architecture of the microcontroller makes it easy to code.

It is also possible to implement this same "ADC" type circuit with a timer. Most microcontrollers have timer output pins that can generate clocks etc. Used in conjunction with the timer capture, the software overhead can be greatly reduced.

Since in this application processing time is not an element of great concern, a

A type definition and structure evolved, and one low-pass filtering function. The C code has been taken from both the header and library files to illustrate this.

The gate should open (play a note) at an input signal level of approximately 80mV. The signal will reach saturation at about 6V. This gives the amplitude extraction circuit a dynamic range of 37dB, since the MIDI Volume Controller contains only seven bits of data. This allows a maximum dynamic range of 48dB. Thus this type of circuit is a fairly good way to provide adequate dynamics with a low component cost.

PITCH EXTRACTION

Still referring to Fig. 3, the pitch extraction circuit behaves as a zero crossing detector, turning the input waveform into a square wave from which the period of the waveform can be accurately timed. Capacitor C29 and resistor R24 a.c. couple the signal. Then R22 and C17 form a first order low-pass filter that feeds to the noninverting input of IC6d.

Between them, R5 and R23 provide a small amount of hysteresis to give clean transitions to the signal edges. This square wave is connected to a timer capture input on the microcontroller (IC1 pin 2). Each high to low transition on this pin causes a 16-bit timer read, allowing the software to calculate the time of each cycle.

Calculating the MIDI note number and pitch bend values from the cycle time is the interesting bit. The algorithm in disk Listing 4 was the one ultimately used. The entire calculation is performed by a scaling function and a look-up table. This is often referred to as the "Blue Peter" approach to maths (and here is one I did earlier!).

The software look-up table is in 2.5 cents (musical intervals of time), rather than frequency as might have been expected. The scaling function manipulates the cycle time to fit the table, producing an "octave" offset value. A binary chop or successive approximation function then looks up the note number and cent offset. Job done!

Rather than use a calculator to derive the table, the easy option of a Perl script was taken. If you are unfamiliar with Perl, disk Listing 4 may look a bit cryptic, but close examination should reveal how the table calculation is performed. The table generated by the Perl script is shown in disk Listing 5.

The scaling function that fits the cycle time to the table was written in C and is detailed in disk Listing 6.

MIDI INTERFACE

Referring back to Fig. 1, the MIDI Interface block provides the standard MIDI connections. The MIDI THRU facility was omitted, though, since a software implementation that could merge incoming MIDI data with data generated by the Theremin was preferred, leaving only MIDI IN and MIDI OUT terminals.

The MIDI circuits as implemented in Fig. 4 are fairly standard. IC7 provides the MIDI IN optical isolation. Transistor TR3 is the MIDI OUT driver, rather than the more commonly used gate driver circuit. The footswitch part of the circuit is referred to shortly (User Interface). Since the microcontroller has a fully featured asynchronous serial port no other hardware is needed.

The software MIDI handlers are fairly simple with only small buffers allocated to the THRU and OUT data, since the incoming MIDI data is processed on "the fly". The MIDI IN translation function breaks down into a "jump into a jump table" function written in assembler for speed. The code in disk Listing 7 illustrates how the incoming MIDI data is translated.

In Listing 7, the macro named %STATE is a routine that puts the address of the data processing function in the MIDI_H and MIDI_L registers, so that when the data is received the microcontroller can execute the required data processing function.

Real-time MIDI messages have further meaning which is translated in the same way. The assembler in disk Listing 8 details further translation, in which MIDI_Idle is the address of a RETurn. Entering the address of MIDI_Idle into MIDI_H and MIDI_L will throw away any further incoming MIDI data bytes.

Although little of the incoming MIDI data is received, functions for all of the messages itemised in a rather out-of-date copy of the MIDI specification were implemented to allow the software to validate each MIDI message as it is received. This is because the software has a THRU emulation mode and it is the easiest way of preventing corrupted or bad MIDI data from being re-transmitted.

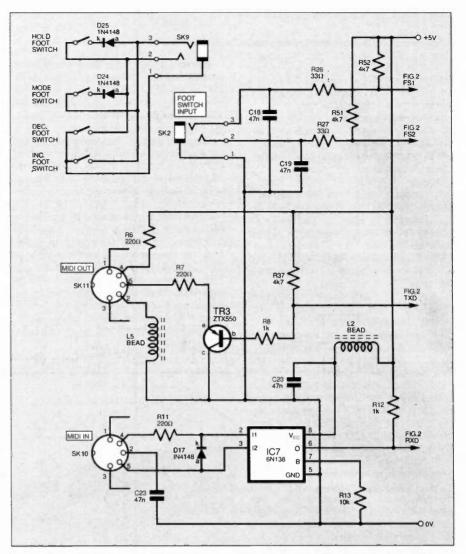


Fig. 4. MIDI ports and footswitch interface circuits. IC7 is an opto-coupler.

The MIDI transmit function is more simple but with terwoven the microcontroller's serial interface hardware. The serial port is set 10 interrupt the program execution on both transmission and reception MIDI data. The code in disk Listing shows the transmit data buffering and the interrupt vector MIDI processing.

CV INTERFACE

The CV Interface block can be broken down into several smaller building blocks, as shown in Fig. 5. Most of the commercial MIDI to

CV designs over the past few years have utilised circuits capable of producing 0-5 volts from an 8-bit DAC (digital-to-analogue converter). Since the range of the *EPE Elysian Theremin* is greater than five octaves, and many synthesizers accept voltage ranges greater than 0-5V, it seemed

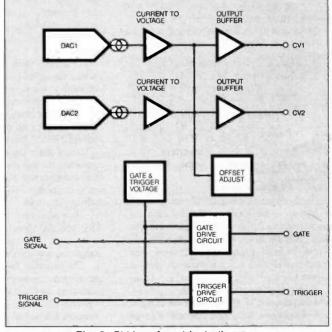


Fig. 5. CV Interface block diagram.

necessary to design a CV interface with a little more "guts"

little more "guts".

For the CV output, a dual 16-bit DAC was chosen. Measurements made, though, would suggest that its performance in this application gives only 12 bits of resolution. This is still better than most.

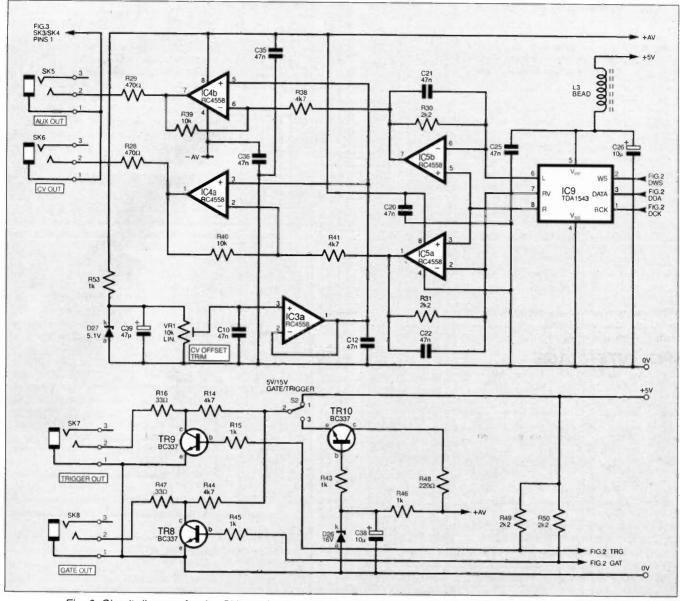


Fig. 6. Circuit diagram for the CV Interface, comprising the ADC plus the Trigger and Gate pulse circuits.

The DAC's circuit diagram is in Fig. 6. In it, the dual 16-bit DAC, IC9, is serially interfaced with the microcontroller by only three connections, from pins 1, 2 and 3.

Currents output from IC9 pins 6 and 8 are converted into voltages by op.amps IC5a and IC5b. Resistors R30 and R31 control the gain of these converters, while C21 and C22 provide some low-pass filtering.

Resistors R38 to R41 set the gain of the output buffers IC4a and IC4b, to give an output voltage range of 10V (ten octaves at 1V/octave). IC3a is used in conjunction with preset potentiometer VR1 to provide offset adjustment, allowing the output voltages to be trimmed, to give maximum flexibility. Output current limiting is provided by R28 and R29.

The Gate output signal must be capable of generating both voltage and switch-type signals. This is done by a single transistor, TR8, and a pull-up resistor, R44. Transistor TR8 is a robust BC337 type, and R47 is a current limiting resistor to prevent accidental damage.

Pull-up resistor R44 provides the voltage which is switched by S2 from either a +5V or a +15V reference. A 16V reference is provided via R46 and Zener

diode D26. Then TR10, R43 and C38 form a capacitance multiplier to provide a smoothed +15V reference. R48 is a current limiting resistor to protect TR10.

Similarly to Gate output control, Trigger output control is provided by the circuit around TR9.

The Gate and Trigger signals are provided by the microcontroller. Because the port pins of the microcontroller cannot source current (they only have weak pull-up resistors of about 40k), R49 and R50 provide the current to turn transistors TR9 and TR10 on/off as required.

On testing the prototype, it was found that there was a minor problem inherent in the p.c.b. design layout. The offset adjustment circuit caused small voltage variations from the +5V rail to be added to the CV outputs. This was cured by adding components R53, C39 and Zener diode D27, as shown in Fig. 6. These components do not have allocated positions on the p.c.b. and need to be added separately. How this is achieved is detailed when p.c.b. assembly is discussed (next month).

The software that drives the CV interface was written to accept MIDI note numbers and pitch bend data to simplify the software development. Because the whole interface

only requires connection to five port pins, the software implementation was easy.

The most complex part was writing the port pin driver routines for the DAC. Because DAC conversion occurs frequently, it was necessary for the function to be as fast as possible. The assembler code used is given in disk Listing 10.

As 16 bits are transmitted, the function is called twice, taking 120µs to send both bytes. It could have been made fractionally faster by making a trade with code space, but this often results in difficult to maintain "spaghetti" code.

USER INTERFACE

The User Interface circuit diagram is shown in Fig. 7. It is designed around eight pushbutton switches (\$3 to \$10), a 3-digit 7-segment l.e.d. display (\$2) and eight individual l.e.d.s. (D1, D2, D14 to D16 and D18 to D20).

Transistors TR4 to TR7 (see Fig. 2) drive the four column signals (SH0 to SH3) of the matrix. Both the l.e.d.s and the switches share the same column driver signals but the rows (RL0 to RL7) are different.

The l.e.d. matrix is driven one column at a time by the microcontroller, with the corresponding l.e.d. data being placed on the

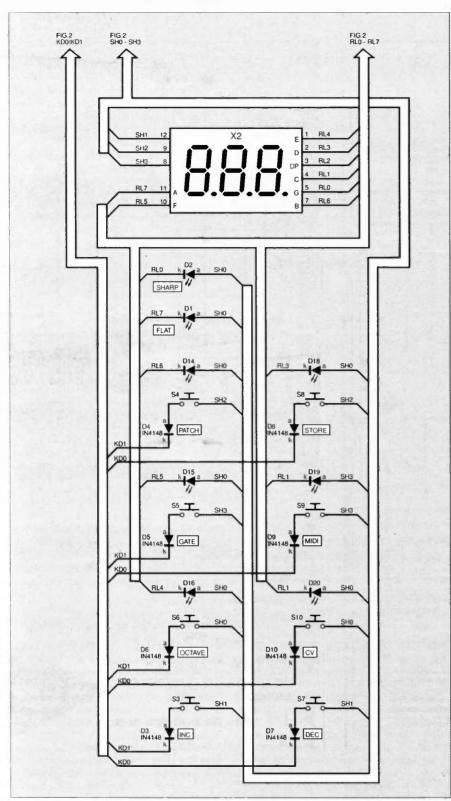


Fig. 7. The User Interface circuit diagram.

port pins connected to the resistor module RP1 (in Fig. 2), which limits the maximum intensity of the l.e.d.s.

When a scan line is high, the microcontroller can establish if a switch is pressed by examining its respective return line (KD0 and KD1). Diodes D3 to D10 prevent reflections when more than one switch is pressed simultaneously, allowing "shift function" operations to be performed by the software.

The footswitch (see Fig. 4) works in a similar multiplexed way, providing four switched modes (Hold, Mode, Decrement,

Increment) via only three wires, through jack socket SK9. Diodes D24 and D25 are steering diodes that allow the Hold and Mode footswitches to be read by the microcontroller.

The software maps the keys into two registers, one remembers the last reading of the keyboard, and the other holds the current reading. An Exclusive-OR of the two registers reveals the changes, while an AND with the last reading masks "key offs", providing a quick and easy way to identify "key on" events.

POWER SUPPLY

Looking now at Fig. 8, the circuit diagram for the power supply, a 12V a.c. power source is fed in via socket SK1. Diodes D22 and D23 half-wave rectify the a.c. to provide +Ve and -Ve power supply rails of approximately ± 17V.

Capacitors C14, C30 and C31 provide power line smoothing. IC2 regulates the +17V down to +5V. Diode D21 minimises the risk of voltage drop on the +AV (+17V) power rail when the digital part of the circuit consumes bursts of current on the +5V line.

Physically, C7 is placed very close to SK1 since this capacitor helps remove noise spikes that may prevent correct operation of the digital circuitry. Further decoupling capacitors are placed close to the power pins of the i.c.s to reduce power rail noise.

The i.c.s that consume current in a noisy way have ferrite beads in series with their power pins, to help reduce the amount of high frequency noise (h.f.) on the power rails (L1/IC1, L2/IC7, L3/IC9). It has already been seen that such beads are used at SK3 (L6) and SK4 (L4), another is used at SK11 (L5).

Extensive use of ground planes on the p.c.b. further helps to reduce the transmission of h.f. noise, particularly to the analogue circuitry. It also provides good earthing and helps remove "hum loops".

It is intended that mains-derived 12V a.c. power for the unit is supplied by a commercial a.c. power adaptor. It should have a rating of at least 500mA, and preferably higher if you want very brightly glowing l.e.d.s.

RESOURCE

Pre-programmed microcontrollers for this project are available, see *Shoptalk*.

PART TWO

It is recommended that you do not begin p.c.b. assembly until you have read the concluding part of this project next month.

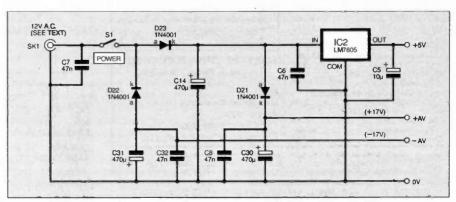


Fig. 8. Power supply circuit diagram.

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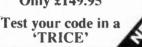
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REPOR by Barry Fox



Out-of-line ISDN

Early modems ran at 300 bits per second and cost £200. The first 2400 bps designs cost nearly £1000. Now 28.8 kilobits per second is the de facto standard, with fax capability thrown in, for around £100. The latest work at 33.6 kbps, which is near the theoretical limit for an analogue speech line.

Now we are seeing ISDN modems, which are not really modems at all. They act as an interface between digital equipment (e.g. a PC) and a digital phone line that carries data at 64 kbps, and higher multiples. The interface responds to the same Hayes "AT" commands as an analogue modem, so most users think of an ISDN interface as a modem. An ISDN terminal adaptor works like a modem in reverse. It converts digital line pulses into analogue signals, so that an ordinary phone, fax or modem can work with an ISDN line

First interfaces and adaptors cost around £1000. The price is now down to around £400. It will drop like a stone as soon as the price of using an ISDN line falls and more people can afford the connection. But high hopes of a price cut were recently dashed.

Imaginative Marketing

Until recently the cheapest way to sign up for ISDN was to pay BT £400 (plus VAT) for an ISDN-2 connection and then pay £336 a year for line rental. In June, Oftel, the telecommunications watchdog, told BT to be more "imaginative" in its marketing. BT responded with what it quaintly called a "flexible approach". The rental on existing lines went up by £16 a year and new users faced a bewildering range of options, which bundle a "free call allowance with rental and installation costs.

June Campbell, BT's Marketing Manager of ISDN services, said it was "good news for small businesses". Jo Baxter, BT's Pricing Manager, told me that the new tarriffs made ISDN "more affordable"

Oftel disagreed and gave BT "a few days" in which to come up with a better deal. Director General Don Cruickshank threatened legal action if BT did not

Fielding Objections

BT claimed that it costs over £1000 to install a line. It is hard to see how this can be because the connection is made using existing copper pair wires and a new connector box. Perhaps BT is trading the low cost of most intallations against bizarre exceptions. Recently BT tried to back out of an installation which cost £25,000 because it involved digging a trench to bury a new cable for four miles, crossing three

roads and a river, and then completing the last 200 metres of the run with an overhead cable wrapped in a steel coating to protect it from shot gun pellets on a farmer's land.

BT has now juggled its "flexible" figures and Don Cruickshank is happy. He says that BT's revised tariffs include "worthwhile price cuts". The Telecommunications Users Association is not happy. In fact it is "very disappointed" at Oftel's capitulation. As an ISDN user, so

"All BT has done is move the figures around and introduce complex tariffs" says TUA Chairman Bill Mieran. "ISDN is still too expensive. We thought Oftel wanted to do something about it, but it hasn't'

Out of three new options, the cheapest connection charge is £199 (plus VAT), with free calls worth £105 a year, but users must pay £535 a year rental for a minimum of two years. If people do not use all their free calls they get no refund. Another option leaves connection at £400 and increases the rental to £352.

Home Office Barrier

Pharmaceuticals giant Zeneca typifies the way both small and large businesses could benefit from ISDN, if only prices were lower. Zeneca has divisions scattered around the country and linked by an office network. The company encourages some researchers to spend one or two days a week working from home and using a laptop PC and phone line. They get more work done because they are undisturbed. Using an ISDN line, instead of an analogue line and fast modem, doubles the speed at which a researcher can download a large reference file.

"ISDN removes the barrier between home and office working" says Phil Barton, Zeneca's Telecoms Strategy Manager. "But at BT's rates the typical cost to Zeneca is £1000 a year. So some staff have to use analogue lines.

Germany Calling

BT will not say how many people are connected to its ISDN-2 service, but Racal-Datacom, which makes ISDN

connection equipment, estimates 0.2 million by the end of the year. In Germany, Deutsche Telekom has connected nearly 2 million people. It is not hard to see why.

Deutsche Telekom will switch on a new subscriber for 200DM (around £85), with the cost halved if the subscriber fits the wires to the connection box instead of calling out an engineer. Line rental is then 138 DM (£60) a quarter. Special offers bundle over a hundred pounds' worth of free calls with the purchase of ISDN hardware.

Phil Barton warns that it is unfair, and counter-productive, to use the giveaway prices in France and Germany as a stick with which to beat BT.

"Those countries still have monopoly providers which can afford to subsidise ISDN and charge ridiculously low prices. It is fairer to look at prices in Scandinavia and North America, where there has been de-regulation. We expect to pay a reasonable premium, say twice the business rental rate for an analogue line, because of the higher cost of the network technology. But BT already charges four times the rate and is now raising the hurdle to around six

Cable Improves the Rate

The latest news is that cable TV companies are offering subscribers the chance to use a cable modem. This uses a spare analogue TV channel for digital data. Nynex has just signed a deal with Motorola to supply equipment for a trial in Manchester. The data rate is 10 megabits per second downstream into the home or office, with a 768 kbps return path back to the cable head end. The return path can be used to send compressed video of telecon-ference quality, while the downstream data pipe can carry VHS quality video or hifi stereo at faster than real time for local storage and replay. If the cable service starts to offer a high speed interconnect for business users, you can be sure that BT will suddenly find a way to cut ISDN pricing.

BT SHOUTS BACK

BT and VIAG Intercom have launched legal proceedings in Germany to prevent the telecoms company Global One from trading in breach of European competition rules.

Global One is a joint venture between Deutsche Telekom (DT), France Telecom (FT) and Sprint Corporation. DT is the monopoly operator in Gennany and the largest telecoms company in Europe; FT is the monopoly operator in France and the second largest operator in Europe.

A BT spokesperson said, "As a result of being owned by two monopolists, Global One has an unfair advantage in comparison with its competitors'

The creation of Global One was cleared by the European Commission subject to the company's competitors being able to obtain supplies from two operators in addition to DT and FT. This was intended to create a level playing field for third-part operators.

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PACIFIC WAVES

In these days of high stress, why not relax to the soothing sounds of the

"high seas" in the comfort of your own home!

little doubt that one of the most relaxing

There can be sounds of nature

is that of ocean waves breaking along a wide shore. It calms the soul, and in these stress-filled times a stroll along such a beach isn't simply a pleasure, it's a therapy.

The "Pacific Waves" project described next month is designed to create surf sounds as realistically as possible for playing through any ordinary domestic stereo system.

HOW TO USE INTELLIGENT L.C.D.s

The ability of intelligent liquid crystal display modules to show not just numbers, but also letters, words and all manner of symbols, makes them a good deal more versatile than the familiar 7-segment light emitting diode displays.

However, getting them to work properly can often pose problems for those who are unfamiliar with the techniques required. Once you do know how they should be programmed, though, they are remarkably simple to use and can enhance the capabilities of all manner of constructional

In this two-part series of articles, we present an utterly practical guide to interfacing and programming the character-based I.c.d. modules which use the Hitachi HD44780 (or compatible) controller chip, as do most modules which are available to the hobbyist.

PsiCom EXPERIMENTAL CONTROLLER

This project should allow owners of the Psion Series 3a "palmtop" computer to use it for controlling external equipment with simple software programs, either by switching, or with an analogue control voltage.

The technique employed might also be usable with other devices employing an l.c.d. screen. It requires no electrical connection to the controlling equipment.

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FEBRUARY '97 ISSUE ON SALE FRIDAY, JANUARY 3

Constructional Project

MAINS-FAILURE WARNING

TERRY de VAUX-BALBIRNIE

An audible alarm for fridges and freezers.

HIS simple Mains-Failure Warning project will be of interest to anyone wishing to guard against mains appliances being switched off accidentally.

Fridges and freezers are obvious targets but some readers will wish to protect such items as aquarium and reptile heaters, greenhouse equipment and emergency water pumps. It may also have applications with medical and scientific apparatus.

ENJOY YOUR TRIP

Common causes of mains failure are blown fuses, tripped RCD units, children playing with switches and people pulling on wires. However, it often happens that an appliance is accidentally switched off when it is plugged into one of a row of sockets and the wrong one is disconnected.

Another frequent cause is when the appliance is unplugged to allow the socket to be used for some other purpose – such as for the vacuum cleaner – and it is not plugged back in afterwards.

The Mains-Failure Warning provides an alarm by sounding a pulsing tone if the supply is disconnected for any reason. In the prototype, the sounder was mounted on the circuit board inside the case. However, it would be possible to connect it remotely so that, for example, a signal could be provided in the house if the supply in the garage failed.

CONNECT AND FORGET

The unit is built in a small aluminium case with a neon indicator mounted on the side which confirms that the supply is connected. An on-off switch is provided on the circuit board inside the box and is only accessible when the lid is removed.

This prevents inadvertent operation which would prevent the circuit from working and defeat its purpose. It will probably be used only when the device is removed from service for some reason (since otherwise it would sound continuously because the supply would be disconnected).

In use, the appliance to be protected is connected to the mains through the Mains Failure Warning unit. While a supply exists, a set of small nickel-cadmium cells is maintained in a charged state.

When the supply fails, the circuit obtains power from these cells which then operate the audible warning device. Using a rechargeable supply in this way has the advantage of there being no conventional

Important Warning: Constructing this project requires mains connections to be made. Any reader who is uncertain of being able to make a safe job must seek the help of a competent electrician.

batteries to check and replace – the unit can be connected up and forgotten.

There is a switch (also accessible by removing the case lid) which provides "boost" charging if the alarm has been required to sound over a long period and this allows the batteries to be re-charged in a short time. In the prototype, the specified buzzer operated for 12 hours approximately on a full charge although the sound becomes weaker towards the end.

CIRCUIT DESCRIPTION

The complete circuit diagram for the Mains Failure Warning project is shown in Fig. 1. A sub-miniature mains transformer, T1, provides a nominal 12V d.c. output using the conventional arrangement of bridge rectifier D1-D4 and smoothing capacitor C1.

While the mains supply is on, transistor TR1 receives base (b) current via resistor R1 and will be turned on. Thus, the collector goes low so keeping the reset input, pin 4, of timer IC1 low also. This disables the i.c. which has no further effect.

Assume that On-Off switch S2 is on. The 7.2V nickel-cadmium battery pack (consisting of two separate 3.6V units, B1 and B2, connected in series) is charged by current entering via diode D5 and resistor R5 alone or R6 connected in parallel with R5 when the Boost switch S1 is on.

Connecting the resistors in parallel in this way will lower the effective value and

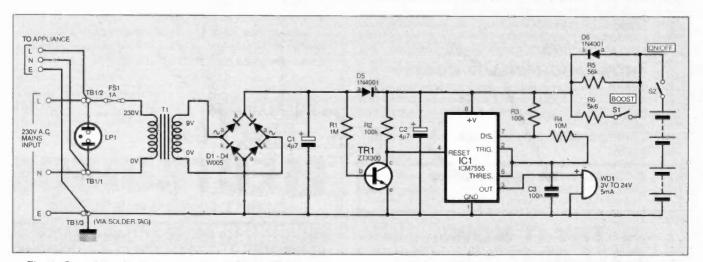


Fig. 1. Complete circuit diagram for the Mains-Failure Warning. S1 and S2 are d.i.l. switches mounted on the circuit board.

increase the current. Diode D6 is reversebiased with respect to current entering the battery and so has no effect.

Resistor R5 limits the current to 100µA approximately which is low enough to prevent overcharging when current flows continuously. With S1 set to Boost, the charging current rises to about 1mA.

MAINS FAILURE

When the mains supply fails, transistor TR1 no longer receives base current so it switches off. Its collector (c) therefore goes high and with it, IC1 Reset pin 4.

Diode D5 prevents base current entering TR1 from the battery pack. However, IC1 does receive a supply from this with current flowing through diode D6 which is now forward biased as far as current flowing out of the batteries is concerned.

SOUND ADVICE

With IC1 pin 4 high, the timer is enabled. Since it is configured as an astable its output, pin 3, will constantly switch on and off at a rate dependent on the values of resistors R3, R4 and capacitor C3.

With the values specified this will be about once per second and, because it is not thought to be particularly critical, no adjustment is provided. If a faster rate is preferred, resistor R4 may be reduced in value and *vice-versa*. The output of IC1

operates the audible-warning device (solid state buzzer) WD1 direct.

The effectiveness of the warning depends largely on the choice of sounder and how it is situated. It must be as loud as possible combined with a small current requirement (5mA to 10mA). Moreover, it must be capable of producing a high sound output using a supply of only 7V.

Readers are warned against using small cheap devices which may not be loud enough to attract attention. Good coverage is obtained by mounting the sounder flat on the printed circuit panel as shown in the photograph. For louder results, it could be mounted on short stalks so that its top lies level with the surface of the box.

It is also possible to use a buzzer attached to the box externally. This should be of the panel-mounting type and chosen to have a sound output at least equal to that specified in the parts list. The same type of audible warning device could be used if it is to be situated remotely and more will be said about this later.

CONSTRUCTION

The Mains-Failure Warning is built on a small, single-sided, printed circuit board (p.c.b.) and the component layout, interwiring and underside copper foil master pattern are shown in Fig. 2. This board is available from the *EPE PCB Service*, code

126. All components except terminal block TB1 and neon indicator LP1 are mounted on-board which makes construction particularly straightforward.

Prepare the p.c.b. by drilling the four holes to mount it in the case later. Add the soldered components in the following order. First, transformer T1, fuseholder FS1, the i.c. socket (but do not insert the i.c. itself yet), d.i.l. switches S1 and S2 (both set to off) and all resistors and capacitors.

Note that resistors R3 and R4 are mounted vertically against the board. Take care over the polarity of electrolytic capacitors C1 and C2.

Follow with the bridge rectifier, diodes, transistor, nickel-cadmium batteries and audible warning device taking care over the orientation of all these components. Attach the plastic cover to the fuseholder.

Complete construction of the circuit board by soldering 10cm pieces of mainstype wire of 3A rating minimum direct to the lower transformer primary winding tag and the adjacent fuseholder tag (see Fig. 2) on the copper track side of the board. For safety reasons, make certain that these wires are secure and cannot dislodge in service.

Finally, solder a piece of stranded wire 5cm long to the "earth point (E)", about half-way along one side of the p.c.b. in line with the warning buzzer. This lead

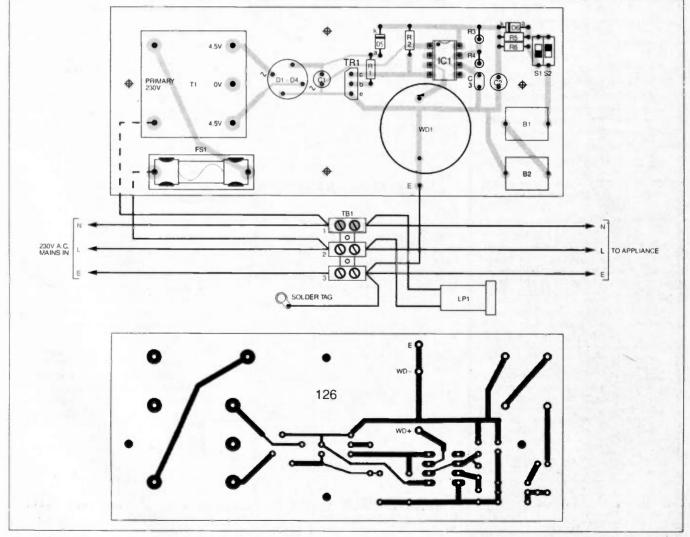
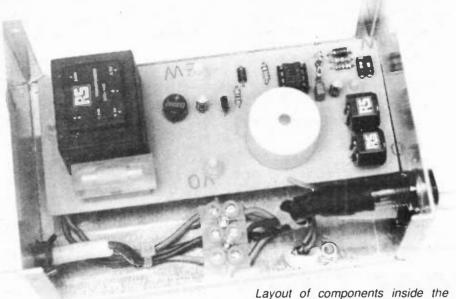


Fig. 2. Mains-Failure Warning printed circuit board component layout, interwiring and full size copper foil master. Note that the leads from TB1 to the transformer primary and the fuse FS1 should be rated at 3A and be soldered directly to the underside copper pads as indicated.



metal case. Make sure the p.c.b. is mounted on nylon spacers and secured with nylon screws and nuts. You must use strain relief grommets for the mains leads, protective sleeving over the neon leads at TB1 and cover the top of TB1 with some insulating tape.

COMPONENTS

Resistor	S	See
R1	1M	QUAD D
R2, R3	100k (2 off)	
R4	10M	TALK
R5	56k	Page
R6	5k6	. ago

All resistors 0.25W 5% carbon film

Capacitors

C1, C2 4 μ 7 p.c.b. mounting radial elect. 16V (2 off)
C3 100n sub-min. metallised polyester

Semiconductors

D1 to D4 W005 50V 1·5A bridge rectifier
D5, D6 1N4001 50V 1A rect. diode

(2 off)
TR1 ZTX300 npn silicon transistor
IC1 ICM7555 CMOS timer

Miscellaneous

B1 3-6V 11mAh
nickel-cadmium, p.c.b.
mounting, batteries (2 off)
T1 sub-miniature p.c.b. mains
transformer. 230V a.c.
primary and 4-5V-0V-4-5V
secondary rated at 1-2VA
(100mA)
LP1 mains neon indicator

WD1 piezo buzzer, p.c.b.
mounting, 10mA 3V to 24V
d.c. operation, 90dB
output minimum – see text

S1/S2 dual s.p.s.t. d.i.l. switch
1A 20mm ceramic mainstype fuse, with 20mm
p.c.b. fuseholder and
plastic cover

Printed circuit board available from EPE PCB Service, code 126; aluminium box, size 125mm x 85mm x 60mm approx.; 8-pin d.i.l. socket; strain relief grommet (2 off); screw terminal block — 3 sections required; stand-off insulators (4 off); mains wire and plug for input lead; 3-5mm mono jack plug and socket or other small connector for remote sounder if required.

Approx Cost Guidance Only £30

will eventually go to the terminal block at point TB1/3.

SOUNDER

As mentioned previously, the audible warning device will normally be mounted on-board. However, if it is to be situated remotely, solder 8cm pieces of light-duty stranded connecting wire *direct* to the solder pads marked "WD+"; and "WD-", via the topside of the board.

The external connections can then be made through a small plug and socket—for example, a 3-5mm mono jack-type socket mounted on the side of the box. If the sounder itself is to be mounted on the side of the box, the flying leads already attached to it may need to be extended, a hole drilled and a rubber grommet used to prevent the sharp edges cutting the wires.

CASE PREPERATION

Prepare the aluminium case to receive the p.c.b. by drilling four holes in the base to correspond with those already made in the board. Drill a large hole in the case lid for the sound to pass through — this must be carefully measured so that it lies directly above sounder WD1 when the circuit board is in position.

Drill holes in the end panels for the strain-relief bushes to be used on the input and output mains wires. These are an essential safety requirement since they prevent the wires possibly pulling free in service which could be very dangerous.

Choose a three-section piece of screw terminal block appropriate to the load (for example, 3A for up to 720W rating on 240V) and drill the holes to secure this. Drill holes for the neon indicator LP1 and solder tag. Note that the solder tag is used to Earth the case and, for safety reasons, it is essential to include it. Secure all these components.

ASSEMBLY

Mount the p.e.b. on the base of the box using 10mm long plastic stand-off insulators on the bolt shanks. It is essential for the soldered connections to be maintained at least 5mm clear of the metalwork.

This is particularly important for the mains connections at T1 primary. If necessary, place a piece of plastic between these and the base of the box as an additional precaution.

Refer to Fig. 2 and connect the three wires leading from the board to terminals TB1/1, TB1/2 and TB1/3 on the screw terminal block as shown. If the buzzer is to be situated remotely, drill a small hole in the side of the box and mount the socket.

If one terminal of the socket makes electrical contact with the metalwork (the usual arrangement with some jack sockets) it is *essential* for this to be made the *negative* one. That is, the one connected to the copper pad marked WD— on the p.c.b. Attach self-adhesive plastic feet to the base of the box.

Insert IC1 into its socket observing the orientation. As a precaution, observe simple anti-static measures before handling it. The simplest method is to touch something which is earthed, such as a water tap, before touching the pins.

REDUCING THE STRAIN

Make up the mains input wire using a suitable length of 3-core wire (even if the appliance itself needs no earth connection) and of a rating appropriate to the load being used. Cut off the end 5cm and remove the piece of earth wire (yellow/green) – discard the other two.

Secure one end of the mains input wire through the strain relief grommet, trim the three wires to size and, referring to Fig. 2, connect them up to the terminal block TB1 along with the existing ones leaving a little slack. Use the short piece of the earth wire removed previously to connect the mains Earth at the terminal block to the solder tag.

Fit the other end of the mains lead with a plug. If this is of the standard UK type, choose the correct value of fuse for the appliance being used.

Connect the neon indicator LP1 to the mains Live and Neutral on the output side of the terminal block as shown. Use heat-shrinkable sleeving at LP1 tags to provide insulation and make them impossible to touch.

If the buzzer is to be situated remotely, connect it temporarily to a short piece of twin wire with the appropriate plug on the other end. Take care to observe the polarity or it will not work. Switch \$2 on. If there is any charge in the cells, the buzzer should start bleeping.

Before proceeding, check that all mains connections, including those at the fuseholder and neon indicator, are shielded so that it is impossible for the fingers to touch them whilst the lid of the case is removed. The unit may now be tested since it does not need an appliance connected for it to work.

TESTING

Plug the unit in to the mains – the neon indicator should light and if the buzzer has been sounding it should now stop. If the buzzer did not sound before due to the batteries being discharged, set d.i.l. switch \$1 to boost and leave the circuit on for about 30 minutes. This will allow sufficient charge to accumulate for testing to take place.

Now switch off the mains supply. The buzzer should start bleeping after a delay of about 20 seconds (that is, when capacitor C1 has discharged sufficiently to fail to maintain TR1 in the on state). When the supply is re-connected, the warning should stop immediately.

Unplug from the mains and switch S2 off to silence the sounder. If S1 was set to boost, switch it back to the normal charge

rate.

Connect the appliance cable via the unused strain relief grommet to the terminal block TB1 along with the LP1 neon indicator connections and circuit board Earth wire, see Fig. 2. Switch S2 on, replace the lid and re-test. If all is well, the unit may be put into permanent service.

If the buzzer is to be connected remotely (such as from a garage or greenhouse), due to one lead being connected to the mains Earth, a double-insulated cable must be used for this purpose as, under exceptional fault circumstances, it could become 'live' up to 230V a.c. Ordinary 2-cored mains cable is suitable (each core separately insulated with both jointly wrapped by an external insulating sheath). The buzzer should also be housed in a small plastic box with a hole drilled in the front for the sound to pass through.

ALARM CHECK

It would be a good idea to check the alarm by switching off the mains supply every few weeks. If the buzzer has ever sounded for a long period so that the batteries are flat, the Boost switch S1 may be used to restore them as quickly as possible. This takes 14 hours and the switch should *NOT* be left in the *on* position any longer.

With the Boost switch off, complete charging will take about six days although a useful amount of charge is accumulated in a few hours. It is suggested that \$1 switch is not used unless the batteries are totally discharged due to the possibility of overcharging and consequent damage to them.

Remember that NiCad cells do not last indefinitely. Check each year for any sign of deterioration. Replacement may be necessary after about 5 years of service.

Ohm Sweet Ohm

Max Fidling

Barking Mad

Rooting around in the shack the other day, near my pile of old washing machine motors and rusty biscuit tins containing various assorted electronic goodies, I came across the defunct remnants of an earlier project, when yours truly had declared war against some light-fingered members of the criminal fratemity!

I had decided that it was time to fit a burglar alarm to Chez Fidling, not that I've anything worth pinching, but not being one to spend money if I can ''do it myself'', I'd spent quite some time rummaging through various magazines in search of suitable circuits. As usual, I hoped to cobble something together on the cheap! However, I didn't relish the prospect of drilling holes through every wall in sight, feeding miles of wires everywhere and putting contact switches on just about everything including the toilet seat, so I'd decided on a more cunning plan instead...

One thing had caught my eye as I flicked through an advertiser's "surplus" pages in my favourite magazine, while munching my breakfast one morning. It appeared to be a small box containing the electronic circuitry to imitate the growl of a dog.

It was battery operated and when triggered was supposed to give the impression that your home was populated by a pack of fierce hounds, guaranteed to strike terror into the heart of any cotton-picking opportunists! Quite how it worked I wasn't sure, but guessing that it contained a sample chip which would be fun to play with, I duly wrote out an order and cycled off to the post box.

Padded Cell

Several days later, a padded bag arrived and I ambled over to the shack bearing my latest loot. It was rather a chilly morning and Piddles the cat was tucking into his grub in the shack, next to the old electric fan heater whose whirr punctuated the air and made the floorboards rattle like the inside of a throbbing Douglas Dakota.

The cat munched on blithely as I started to tinker on the bench with the "Phantom Dog Woofer (batteries not included)". Ripping open the electronic canine's carton, the plastic plunder tumbled out onto the bench. It was quite an impressive box which had a grille on the front panel, presumably for the speaker or the horn.

Not being one to bother with batteries, I hooked up the bench power supply, which has been set to the usual 9V (give or take a few), and waited excitedly to see what would happen. Nothing! A quick wiggle of the wiring, a twiddle of the bench power supply – still nothing! Not a growl, not even a snivelling wet-nosed whimper! Hmmm...

If in doubt, always read the instructions, I guess, so I peered at the accompanying tiny bit of paper headed "Instruction Manual" for inspiration. Barely decipherable in a smudgy black ink, the voluminous Instruction Bit of Paper bore a mystical message:

"Placing Phantom Dog Woofer on door lever and battery switch red color is on for working properly", it said in a strange Taiwanese tongue, cross-referring to a thumbnail sketch, but I got the gist. "Leave room immediately for Phantom Dog Woofer now protecting door handle if touched thereafter!" it burbled. Aha! The plot "thinned".

Evil Eye

The cunning canine gizmo sat defiantly on the bench; I half expected a tail to pop out and start wagging, but instead the black box remained there, waiting to be taken the electronic equivalent of walkies. Examining the plastic moulding revealed that on the underside of the plastic hook, which I guessed hung onto a door knob, there was a large shiny metal contact, probably part of some kind of antenna which would trigger the circuit.

Anyway, I poked it with a screwdriver blade to see what would happen. Bark! Bark! WOOOF!! WOOOF!! The box unleashed a chorus reminiscent of the Last Hound of the Baskervilles! At this point, a petrified Piddles, in mid-munch, sat bolt upright and then with a squeal hurtled off towards the door!

WOOOF!! WOOOF!! The Taiwanese Terrier continued its "rappaw" with an absent Piddles. A small screwdriver slot was found on the casing which invited a twiddle with the screwdriver, and the canine clamour resolved itself more to a Chihuahuan "Yap!" as the meter on the bench power supply pulsed in sympathy.

By this time the cat had wised up to the fact that he'd been 'had', and duly relieved (in more ways than one) he ambled back to his grub and started clattering the bowl noisily next to the fan heater, giving me an evil stare as usual. Meantime, having got the hang of the *Phantom Dog Woofer*, the next thing was to try it on the toilet door handle and see if I could catch the Boss at the operative moment! What a bargain!



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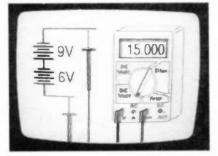


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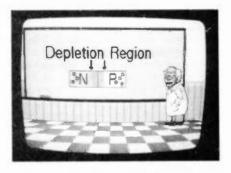
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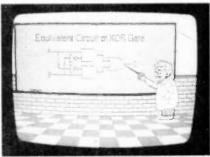


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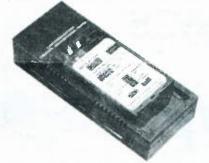
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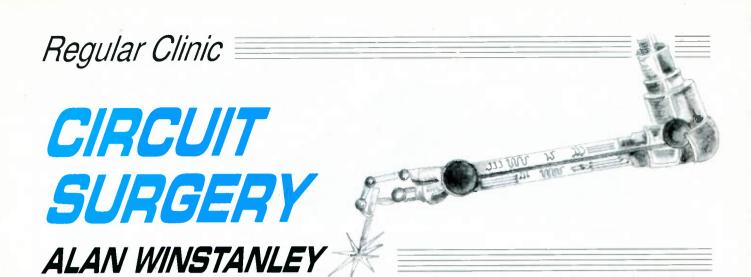
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Our monthly column for readers' queries and tips looks at a novel but effective reverse-voltage protection circuit, also "Zapping" of Nickel-Cadmium cells, linking l.e.d.s together, and how to Monitor a PSU output.

Simple Protection

ERE'S a further selection of readers' comments and queries, starting with a follow-up from September's column. Geoff Kermode of Whitley Bay, Tyne & Wear, shares these simple tips with us. Geoff writes:

Your reverse polarity protection system in September's Circuit Surgery reminds me of a simple GCSE CDT circuit 1 developed some time ago. This was a lighting system for a model railway using four 12V 20W dichroic bulbs.

I used a 13.8V CB power supply which had 4mm terminals (binding posts). There was the possibility of reversing the polarity, which would have damaged the lighting system.

As in many battery applications, it's necessary to minimise the voltage drop through the system to ensure maximum brightness at full power. Rectifiers couldn't be used because of this, so I designed the simple circuit of Fig. 1. The voltage drop arises through relay contact resistance. Thick-gauge wires, and plenty of solder minimises losses too.

At these high currents even the resistance of a fuse can be significant. An l.e.d. or buzzer can be added as shown in Fig. 2 to warn of incorrect polarity.

Thank you very much for two excellent columns!

Thanks for writing, and for the tips. With apologies to those who are less interested in batteries, but it's an immensely popular subject. Here are some tips from regular reader *David Dewey* of Bovingdon, Herts, who comments:

I use a NiCad Charger and some tricks of mine may interest your readers. Most gadgets need two or more cells in series and often one discharges before the remainder.

In order to prevent "memory build-up" I discharge the others individually through a diode in series with a resistor (about 22 ohms for AA batteries). Thus, they are all fully discharged without dropping below about 0.6V.

Sometimes, in general use, one cell falls to OV and stays that way, even after trying to recharge it. This hints at an internal short. It is worth trying to "zap" the cell with a heavy current (many amps) for a second or two.

I use two or three charged cells in series, hooked in parallel to the "dud" cell with thick wire. A volumeter across the dud NiCad will hopefully jump from 0V after a few seconds, to about 1-2V. Then disconnect immediately!

Finally, I mark NiCads of the same batch when purchased, and use cells from the same batch wherever possible to make a stack. This ensures good rotation of cells.

"Zapping" of cells is sometimes practised prior to reading the Last Rites to a NiCad, it's a bit unofficial and you really must only "nuke" it for one to two seconds. The dendrites in the cell may form whiskers which can be fused away but it's a sure sign that the cell's on its way out!

Also, younger readers should know that a **cell** is one individual 1-2V NiCad, these may be joined together in series to form a **battery** but they should **not** ordinarily be

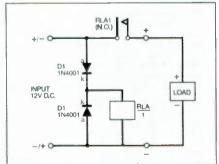


Fig. 1. Using a relay to minimise voltage drop losses while offering reverse voltage protection.

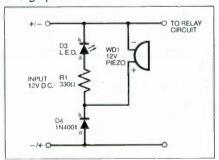


Fig. 2. Adding a buzzer to warn of reverse battery polarity.

connected in parallel, because their voltages will not be equal and one cell is likely to shunt the others.

Keeping Tabs on Batteries

In last September's column 1 commented on methods of soldering wires or tabs to batteries. From *Mr Ken Maynard*, by E-mail:

With reference to soldering batteries, (Hot Batteries – September issue) I only do this if they have tags already fitted. Soldering to any type of battery requires that the terminal top be cleaned with a file to remove the plating, then it's possible to solder the battery without overheating it.

Also Ben Musson comments by E-mail: Many times I've soldered lengths of cable onto NiCads without any problem, using standard tinllead solder. As long as the terminal surface is sufficiently roughened using sandpaper, the solder takes well and the cell does not get too warm.

And from Christer Renberg of S-461 67 Trollhättan, Sweden, comes further advice if you're having a ticklish time soldering those stubborn substances.

My suggestion is to use a solder called "KR-19" that wets on stainless steel and other difficult materials. It's made by Almit of Japan with a very effective fluxing agent that wets on almost any metal without the need for excessive heat.

I learned this trick when I was involved in trying to grade and recycle surplus electronic equipment. I set my temperature-controlled iron to 370°C and wet both surfaces together with KR-19 super-solder. Good luck with your soldering!

Solder KR-19 isn't a product I've come across. Does anyone have any alternatives or further information? I'm also very pleased to see that p.c.b, holders are at last becoming available for coin cells, e.g. Maplin Order Code GU00A et al, or Farnell Stock Code 676-482. Maplin also stock a further range of snap-in battery clips for p.c.b. use.

(Open the new Maplin "MPS" catalogue and you could be forgiven for thinking you've picked up an RS Components catalogue by mistake: however, the MPS catalogue is, in my opinion, now easily the best one available

in this market and I strongly recommend that you buy a copy.) Incidentally, coin cell dimensions are a topic I'm hoping to tackle in a future column.

General soldering tips were offered in the series *Build Your Own Projects* (Dec '96) which continues in this issue. I have, incidentally, been absolutely astonished by the interest shown in this series, and I thank everyone who's kindly contacted us to say how much they've enjoyed reading it.

We're hoping to put an "on-line" guide to soldering with extra photos onto the Internet at our World Wide Web site (http://www.epemag.wimborne.co.uk), following several requests from Internet users everywhere. If you have any queries or comments arising from the Build Your Own Projects series, why not share them and drop Circuit Surgery a line?

Parallel Bars

Mr. Soar of Doncaster raised a query concerning the use of light-emitting diodes (l.e.d.s) in parallel. He writes:

I recently saw a suggested circuit showing two l.e.d.s. being driven in parallel with each other, should they not be connected in series to prevent a "current hogging" effect?

Preferably, yes. Otherwise the one with the lowest forward voltage will "shunt" the others, and it will draw an unfair share of the available current.

The "hog" will often be the brightest l.e.d. whilst the others may not be as bright as they could be. The remedy is to ensure that each has its own series dropper resistor, or you could place the devices in series instead.

Interestingly, some super-large sevensegment displays (say 70 to 100mm high) use an internal combination of parallel and series l.e.d.s: e.g. Maplin's 100mm display (Order Code JX86T) uses no less than eight l.e.d. chips per segment: two l.e.d.s in parallel, then each parallel pair in series four times; if you see what I mean.

Bench Metering

Constructing a Bench Power Supply? Mr Alan McCusker is! A small problem with monitoring the output voltage and current is easily solved. Mr McCusker writes:

I enclose a circuit diagram of a 723-based power supply I'm making, to which I would like to add two meters (analogue, moving iron) to monitor the voltage and current. I would appreciate any help or advice to enable me to connect them.

No problem, ammeters are placed in series with the current being measured, whilst a voltmeter measures the potential difference between two points. Fig. 3 shows how. Also a double-pole single-throw switch is useful for isolating the power from the load instantly.

Usually, switching off the mains supply does not instantaneously power-down the load, because a voltage remains across the p.s.u.'s smoothing capacitors for a short period. Hence the d.p.s.t. switch following the p.s.u.

A cute trick is to add a "constant current" l.e.d. directly across the supply rails; this needs no resistor and will light whenever the d.c. supply is switched on, provided it exceeds a few volts. If the l.e.d. extinguishes, then you may have a direct short across your power supply. The trouble

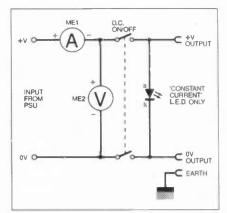


Fig. 3. Metering a power supply.

is, these l.e.d.s. suddenly seem incredibly hard to obtain. Can anyone help?

One quite important point though, concerns your choice of meter. Usually, moving *coil* types are used, or if you can afford it, a digital voltmeter instead. Not many constructors may be aware that if you bolt a moving *iron* meter to a steel panel, you may seriously affect the accuracy of the meter readings. Aluminium panels seem OK though.

At your service

Circuit Surgery is your page. If you have any questions to ask or comments to make, please write to Alan Winstanley, Circuit Surgery, Wimborne Publishing Ltd., Allen House, East Borough, Wimborne, Dorset BH21 1PF. E-mail alan@epemag. demon.co.uk



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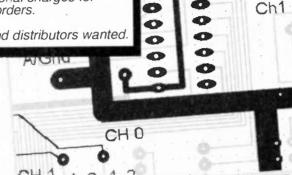


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Multi-Project PCB	932	£3.00
Light-Activated Switch Switch On/Off Timer		
Continuity Tester Auto Battery Charger	934	£5.36
National Lottery Predictor	935	£5.34
R.F. Signal Generator - R.F./Mod. MAY'95	936	€6.48
Coil & Power Supply (pair)	937a/b 938	£6.10 £7.78
Club Vote Totaliser	939	£6.05
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Phase splitter PIC-DATS 4 -channel Light Chaser	941 942	£6.71 £7.90
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Ultra-Fast Frequency Generator and Counter – Oscillator/L.C.D. Driver Timed NiCad Charger Single-Station Radio 4 Tuner Twin-Beam Infra-Red Alarm – Transmitter/Receiver Games Compendium	994/995 (pr) 100 101 102/103 (pr) 104	£12.72 £6.99 £7.02 £10.50 £6.09
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Earth Resistivity Meter Current Gen. – Amp/Rect. Theremin MIDI/CV Interface (Double sided p.t.h.) Mains Failure Warning	131/132 (pr) 130 (set) 126	£12.70 £40.00 £6.77

Software programs for the *EPE* projects marked above with an asterisk (*) are available altogether on a *single* 3.5 inch PC-compatible disk, or as needed via our Internet site. The same disk also contains the following additional software: Simple PIC16C84 Programmer (Feb '96), PIC Disassembler (unpublished). The disk (order as "PIC-disk") is available from the *EPE PCB Service* at £2.50 (UK) to cover our admin costs (the software itself is *free*). Overseas £3.10 surface mail, £4.10 airmail. Alternatively, the files can be downloaded *free* from our Internet FTP site: ftp://ftp.epemag.wimborne.co.uk.

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SURFING THE INTERNET

NET WORK

ALAN WINSTANLEY

WELCOME to our page for Internet users! First, an update of developments on our web site: the URL as always is http://www.epemag.wimborne.co.uk Now there is a Back Issues Order Form which enables you to place orders by E-mail, on line. This method is currently "insecure" until the Secure Server is running, but it provides a convenient and reasonably safe way of purchasing by credit card. You can browse the form to find out which back issues are available. Also, all you need to know about our Fax on Demand service (UK only), is now on /epeonfax.htm. Files for the Earth Resistivity Meter and Theremin MIDIICV Interface are on our FTP site in the sub directory PICS.

Here is the News

Internet users often hear about "news", but in our context, "news" has nothing to do with reporting current affairs at all! More correctly called *Usenet* (Unix User Network), this system allows like-minded users to circulate topical comments, questions, and a whole lot more, to anyone "subscribing" to their particular "newsgroup".

There are some 20,000 different newsgroups now available covering virtually every topic imaginable. Newgroups do business under such prosaic names as sci.electronics.basic or comp.infosystems.www.authoring, rec.autiques.radio + phono, rec.autos.makers.vw.aircooled, and a whole lot more besides!

Usenet consists of global E-mail messages circulating around the planet, which will be delivered to the computers of everyone subscribing to those particular newsgroups, whenever they dial up to access the Internet. An individual newsgroup relates to one particular area of interest.

If you're into alt.music.makers.theremin, for example, you can raise a question ("start a new thread") and "post" it to that newsgroup. Your question will then be read by every other Usenet reader who subscribes to that same newsgroup. It's a bit like sending an E-mail to every other member of the same club.

Others may respond by posting a "follow up" to your query. You will be able to read this on your own screen when you download the latest news via your Service Provider. Other users too will join in by adding further follow-ups themselves. Thus, the thread develops and branches out, and it's not uncommon for a simple query to explode into a thread containing several hundred follow-ups, all of which you may choose to read on your own screen.

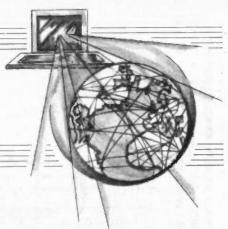
A Soft Line

Software makes life easy. It's very desirable to use an "off-line newsreader" (examples include *Turnpike* and *Forte Free Agent*) which will enable you to quickly dial up the Internet, send and receive news messages, and then hang-up. The act of physically browsing the news on-screen, can be performed while you are disconnected, in order to save the phone bill. You can compose your own follow-ups, off-line, too.

Most groups are unmoderated, so things are a bit of a free for all. Groups have a ''charter'' which is a mutually-agreed and formal policy of what may and may not be posted there – the idea being to discourage users from clogging up a newsgroup with unwanted or ''off-topic'' traffic. Very occasionally, things may become unpleasant when tempers fray.

Netiquette

Many newsgroups are discussion groups in which participants have a healthy respect for other readers of the group. The principles of so-called "netiquette" apply, which embrace the generally common-sense rules of courtesy and consideration. Failure to observe such netiquette may attract "flames" — hostile messages from disgruntled Usenet users, both publicly (in the newsgroup) and by personal E-mail! Thus, the system polices itself.



After a complete re-organisation, the structure of Usenet includes the following "top levels":

comp Anything to do with computer software or hardware e.g. comp.lang.c + +

news Usenet administration matters, e.g. news.admin.misc rec Recreation, past-times, e.g. rec.aquaria.marine.misc sci Science-related areas, e.g. sci.agriculture.beekeeping alt "Alternative" newsgroups, e.g. alt.alien.visitors or

alt.animals.horses.icelandic!

There are many more groups which were created outside of the formal Usenet structure but which circulate in much the same way. For example, demon.service is a place where customers of London-based Demon Internet Services Ltd. can voice their complaints. Demon.local is the equivalent of chatting at a bar somewhere in England, and so on. Thus, Usenet ofters a fountain of worthwhile information which can help solve many thorny problems.

Usenet has another side which I will briefly mention, if only so that you can steer clear of it if you wish. Given that anything goes on Usenet, "each to their own" is definitely the golden rule. To be honest, whether some people approve of some newsgroups or not, is irrelevant as far as Usenet is concerned – don't subscribe to them if you don't like them.

Some notorious groups include the alt.binary and alt.sex ones. The "binary" tells you that material including very large binary or executable files (e.g. *.zip or *.exe files) may be posted there, and a number of groups exist for posting material in the form of graphical images (.gif or .jpg pictures) and movies, complete with soundtrack. You have been warned!

Usenet can be highly addictive, and before you know it, you are itching to log on again to see if anyone has followed up your own articles. Or you see an article with which you disagree strongly, so you spend an hour composing a reply. Usenet can steal your time and is best used with a strong sense of discipline, or it will take over your life! I strongly recommend "taking" a newsgroup for about two weeks to see what the general level is like, before you dip in with your own articles or follow-ups.

It takes all sorts on Usenet, and you will meet many of them! Both *Netscape Navigator* and *MS Internet Explorer* include a newsreader, and you could dabble by configuring either of them to read news. Have a great time.

Links

Here are this month's selection of links, which are readymade for you on my Net Work page on our web site: EPE Elysian Theremin builders should visit Rosedene Audio's site at http://www.fullerton.demon.co.uk. Into the MAX038 function generator chip? Try Maxim's site http://www.maxim-ic.com/for Maxim application notes (in Adobe Acrobat format). A new and very promising technical data base of more than 70,000 component references complete with data sheets is at web site http://www.tds-net.com.

Valve (vacuum tube) fans should drop in on Tube Dude's Webpage of Vacuum Tube Lore on http://www.cdc.net/~gesic. Manufacturers 4 Q D are heavily into battery motor controllers, electric vehicles etc. and offer a handy resource of circuits and FAQs at http://www.argonet.co.uk/users/4qd.

A site of interest for the electronic engineer is to be found at http://www.worldaccess.nl/~bema. And finally, readers, a "welcome aboard" to our friends at *Maplin*, and we wish them well with their new web site on http://www.maplin.co.uk. See you soon for more *Net Work!*

My E-mail address is alan@epemag.demon.co.uk





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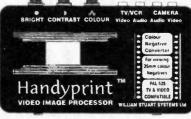
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SP24		Cmos 4001	SP145		x ZTX300 transistors
SP25		555 timers	SP146		x 2N3704 transistors
SP26	4 x	741 Op.amps	SP147	5	x Stripboard 9 strips/
SP27	4 x	Cmos 4002			25 holes
SP28		Cmos 4011	SP148		x 2mm lighthouse Leds-Red
SP29		Cmos 4013	SP151		x 8mm Red Leds
SP30		Cmos 4025	SP152		x 8mm Green Leds
SP32		Cmos 4077	SP153		x 8mm Yellow Leds
SP33		Cmos 4081	SP156	3	x Stripboard, 14 strips/
SP36 SP37		10/25V radial elect. caps.	CD460	40	27 holes
5P37	15 X	100/35V radial elect.	SP160 SP161		x 2N3904 transistors x 2N3906 transistors
SP41	20 v	caps. Mixed transistors	SP164		x C106D thyristors
SP42		Mixed 0.25W C.F. resistors			x LF351 Op.amps
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SP103		14-pln DIL sockets	SP175		x 1/63V radial elect. caps.
SP104		16-pin DIL sockets	SP192		x Cmos 4066
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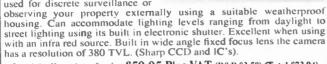
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Bridged Mono ALL POWERS INTO 4 OHMS

Features:

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VISA

OMP MOS-FET POWER AMPLIFIER MODULES SUPPLIED READY BUILT AND TESTED.

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THOUSANDS OF MODULES PURCHASED BY PROFESSIONAL USERS



OMP/MF 100 Mos-Fet Output power 110 watts R.M.S. into 4 ohms, frequency response 1Hz - 100KHz -3dB, Damping Factor > 300, Slew Rate 45V/uS, T.H.D. typical 0.002%, Input Sensitivity 500mV, S.N.R. -110 dB. Size 300 x 123 x 60mm PRICE £40.85 + £3.50 P&P

OMP/MF 200 Mos-Fet Output power 200 watts R.M.S. into 4 ohms, frequency response 1Hz - 100KHz -3dB, Damping Factor > 300, Slew Rate 50V/uS, T.H.D. typical 0.001%, Input Sensitivity 500mV, S.N.R. -110 dB. Size 300 x 155 x 100mm. PRICE \$64,35 + \$4.00 P&P

OMP/MF 300 Mos-Fet Output power 300 watts R.M.S. into 4 ohms, frequency response 1Hz - 100KHz -3dB, Damping Factor > 300, Slew Rate 60V/uS, T.H.D. typical 0.001%, Input Sensitivity 500mV, S.N.R. -110 dB. Size 330 x 175 x 100mm. PRICE \$81.75 + \$5.00 P&P

OMP/MF 450 Mos-Fet Output power 450 watts R.M.S. into 4 ohms, frequency response 1Hz - 100KHz -3dB, Damping Factor > 300, Slew Rate 75V/uS, T.H.D. typical 0.001%, Input Sensitivity 500mV, S.N.R. -110 dB, Fan Cooled, D.C. Loudspeaker Protection, 2 Second Anti-Thump Delay. Size 385 x 210 x 105mm. PRICE C132.85 + C5.00 P&P

OMP/MF 1000 Mos-Fet Output power 1000 watts R.M.S. into 2 ohms, 725 watts R.M.S. into 4 ohms, frequency response 1Hz - 100KHz -3dB, Damping Factor > 300, Slew Rate 75V/uS, T.H.D. typical 0.002%, Input Sensitivity 500mV, S.N.R. -110 dB, Fan Cooled, D.C. Loudspeaker Protection, 2 Second Antl-Thump Delay. Size 422 x 300 x 125mm. PRICE \$259.00 + \$12.00 P&P

OTE: MOS-FET MODULES ARE AVAILABLE IN TWO VERSIONS: TANDARD - INPUT SENS 500-MY, BAND WIDTH 100KHZ. EC (PROFESSIONAL EQUIPMENT COMPATIBLE) - INPUT SENS 75MY, BAND WIDTH 50KHZ. ORDER STANDARD OR PEC.

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EMINENCE:- INSTRUMENTS, P.A., DISCO, ETC

ALL EMINENCE UNITS 8 OHMS IMPEDANCE

B* 100 WATT R.M.S. MEB-100 GEN. PURPOSE, LEAD GUITAR, EXCELLENT MID, DISCO.
RES.FREQ. 72Hz, FREQ. RESP. 70 4KHz, SENS 97dB.

PRICE C32.71 + C2.00 P&P

10* 100 WATT R.M.S. ME10-100 GUITAR, VOCAL, KEYBOARD, DISCO, EXCELLENT MID.
PRES. FREQ. 71Hz, FREQ. RESP. TO 7KHz, SENS 97dB.

PRICE C33.74 + C2.50 P&P

10* 200 WATT R.M.S. ME10-200 GUITAR, KEYB'D, DISCO, VOCAL, EXCELLENT HIGH POWER MID.
PRES. FREQ. 65Hz, FREQ. RESP. TO 3.5KHz, SENS 99dB.

12* 100 WATT R.M.S. ME110-100LE GEN. PURPOSE, LEAD GUITAR, DISCO, STAGE MONITOR,
PRES. FREQ. 49Hz, FREQ. RESP. TO 6KHz, SENS 100dB.

12* 100 WATT R.M.S. ME12-100LT (TWIN CONE) WIDE RESPONSE, P.A., VOCAL, STAGE
MONITOR. RES. FREQ. 42Hz, FREQ. RESP. TO 10KHz, SENS 98dB.

PRICE C35.64 + C3.50 P&P

12* 200 WATT R.M.S. ME12-200 GEN. PURPOSE, GUITAR, DISCO, VOCAL, EXCELLENT MID.
PRES. FREQ. 58Hz, FREQ. RESP. TO 6KHz, SENS 98dB.

PRICE C46.71 + C3.50 P&P

12* 300 WATT R.M.S. ME12-300GP HIGH POWER BASS, LEAD GUITAR, KEYBOARD, DISCO ETC.
RES. FREQ. 47Hz, FREQ. RESP. TO 5KHz, SENS 103dB.

PRICE C70.19 + C3.50 P&P

15* 200 WATT R.M.S. ME15-300 HIGH POWER BASS, INCLUDING BASS GUITAR.
PRICE C70.72 + C4.00 P&P

15* 300 WATT R.M.S. ME15-300 HIGH POWER BASS, INCLUDING BASS GUITAR.
PRICE C70.73 + C4.00 P&P

15* 300 WATT R.M.S. ME15-300 HIGH POWER BASS, INCLUDING BASS GUITAR.
PRICE C70.72 + C4.00 P&P

15* 300 WATT R.M.S. ME15-300 HIGH POWER BASS, INCLUDING BASS GUITAR.
PRICE C70.73 + C4.00 P&P

15* 300 WATT R.M.S. ME15-300 HIGH POWER BASS, INCLUDING BASS GUITAR.
PRICE C70.73 + C4.00 P&P

15* 300 WATT R.M.S. ME15-300 HIGH POWER BASS, INCLUDING BASS GUITAR.
PRICE C70.73 + C4.00 P&P

15* 300 WATT R.M.S. ME15-300 HIGH POWER BASS, INCLUDING BASS GUITAR.
PRICE C70.73 + C4.00 P&P

15* 700 WATT R.M.S. ME15-300 HIGH POWER BASS, INCLUDING BASS GUITAR.
PRICE C70.73 + C4.00 P&P

15* 700 WATT R.M.S. ME15-300 HIGH POWER BASS, INCLUDING BASS GUITAR.
PRICE C70.73 + C4.00 P&P ALL EMINENCE UNITS B OHMS IMPEDANCE

EARBENDERS:- HI-FI, STUDIO, IN-CAR, ETC ALL EARBENDER UNITS 8 OHMS (Except E898-50 & E010-50 which are dual impedance tapped @ 4 & 8 ohm)

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10° 50 WATT E810-50 DUAL IMPEDENCE, TAPPED 4/8 OHM BASS, HI-FI, IN-CAR.

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10° 50 WATT E810-100 BASS, HI-FI, STUDIO.

PRICE C13.65 + \$2.50 P&P

10° 100 WATT E810-100 BASS, HI-FI, STUDIO. PRICE £13.65 + £2.50 P&P RES. FREO. 35Hz. FREO. RESP. TO 3KHz. SENS 96dB. PRICE \$30.39 + \$3.50 P&P RES. FREQ. 35Hz, FREQ. RESP. TO 3KHz, SENS 96dB. PRICE \$30.39 + \$3.50 P&P
12" 100 WANT EB12-100 BASS, STUDIO, H-FI, EXCELLENT DISCO.

RES. FREQ. 26Hz, FREQ. RESP. TO 3 KHz, SENS 93dB. PRICE \$42.12 + \$3.50 P&P
FULL RANGE TWIN CONE, HIGH COMPLIANCE, ROLLED SURROUND
5"4" 60WATT EB5-6OTC (TWIN CONE) HIFF, MULTI-ARRAY DISCO ETC.

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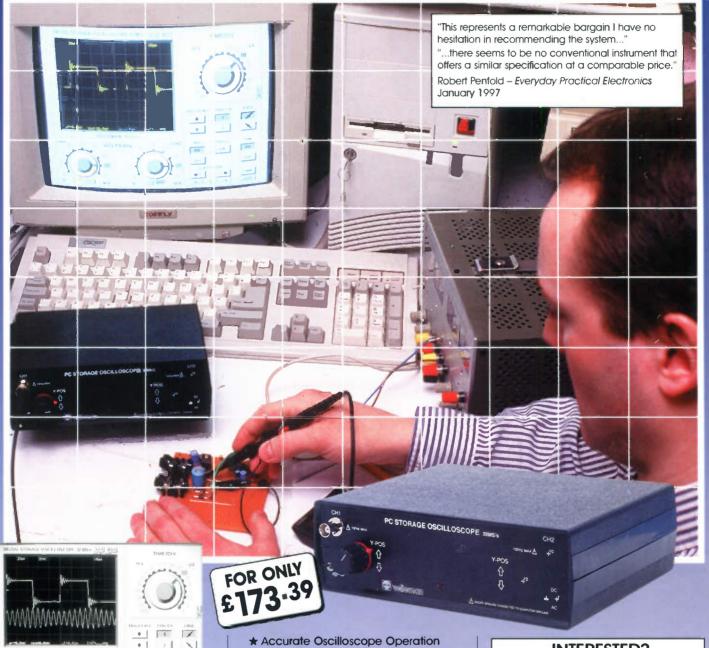
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