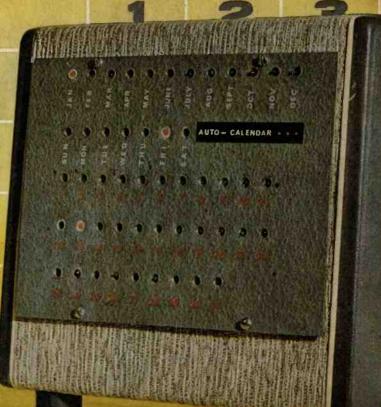
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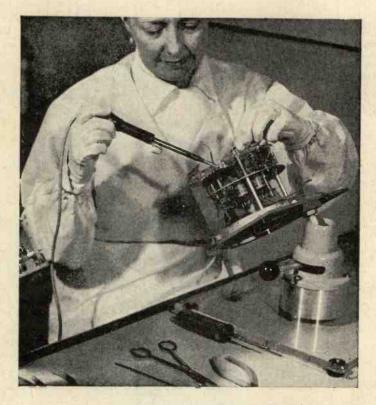
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Migh quality chrome fittings. Will
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- 21" Speaker.
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Buy yourself an easy to build 7 transistor radio and save at least £10.0.0. Now you can build this super 5 transistor superhet radio for under £4.10.0. No one else can offer such a fantastic radio with so many

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De luxe grey wooden cabinet size

12½ × 8½ × 3½. ★ Horizontal easy to read tuning scale printed grey with black letters, size 11½ × 2″. ★ High Q' territe rod aerial.

L.F. neutralisation on each separate stage.

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- * CALIBRATED DIAL
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 OF 'POP' STATIONS
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SMALLEST RADIO

Photograph shows actual size

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THE SINCLAIR MICROMATIC is a brand new design from an organisation world-famous for its production of micro-electronic equipment for constructors. It has behind it the Sinclair tradition of specialisation in microradio circuitry which, in the MICRO-MATIC, reaches fantastically high levels of performance. We have combined new circuitry with new elegance to make the SINCLAIR MICROMATIC professionally right in every detail whether you build it yourself or buy it complete in presentation case.

This makes the perfect personal radio, ready to serve wherever and whenever required. Its minutely proportioned case houses transistors, ferrite rod aerial and batteries and yet is considerably smaller than an ordinary matchbox. The MICROMATIC has an elegantly designed aluminium front panel with matching calibrated slow motion dial. New circuitry assures reception from a wide range of stations over the medium waveband, with excellent selectivity and quality. Here is a new set you will be proud to be seen using; you will also find it an ideal gift to give anyone. YET THIS BRILLIANT NEW DESIGN IS THE EASIEST OF ALL SINCLAIR RADIO BUILD - AND SETS TO BRITISH!

TECHNICAL DESCRIPTION

The Sinclair Micromatic is housed in a neat plastic case with attractive aluminium front panel

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Three special Sinclair transistors are employed in a six stage circuit of exceptional power and sensitivity. Two stages of powerful R.F. amplification are followed by a double diode detector from which the signal tuned in is passed to a high gain three stage audio amplifier. Automatic Gain Control counteracts fading from distant stations and maintains signal strength. The set is powered by two Mallory Mercury Cells Type ZM.312 which are readily obtainable from radio shops, Boots Chemists, Stores, etc., and cost 1/7 each. The cells will give approximately 70 hrs. continuous working life. Inserting the earpiece plug switches the set on, withdrawing it switches off.

Complete kit of parts to build Sinciair Micromatic including lightweight earpiece, case and instructions

59/6

Sinclair Micromatic ready built with lightweight earpiece, in presentation case,

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SINCLAIR STEREO 25 DE-LUXE PRE-AMP CONTROL UNIT

THE SINCLAIR STEREO 25 has been designed specially to ensure the highest possible standards of reproduction when used with two Z.12s or any other first class stereo power amplifier. Best possible components are used in the construction of this superb unit, whilst its appearance reflects the professional elegance characteristic of all Sinclair designs in hi-fi, radio and TV. The front panel of the Stereo 25 is in solid brushed and polished aluminium with beautifully styled solid aluminium control knobs. Mounting the unit is simple, and power is conveniently obtainable from the Sinclair PZ.3 which can also be used to supply two Z.12s to make a complete stereo assembly. Hi-fi enthusiasts seeking the ultimate in domestic listening will find all they want from this combination of Sinclair units. With a Micro FM for tuner, they will have an installation to compare favourably with anything costing from four to five times as much.

USE WITH ANY GOOD STEREO SYSTEM FOR

Performance figures obtained using Stereo 25, two Z.12s and o PZ.3.

- SEPRO 25, two Z./2s and o PZ.3.

 SENSITIVITY for 10 watts into 1.5 ohms load per channel. Mic.—2 mV into 50K ohms. Pick-up—3 mV into 50K ohms. Radic—20 mV into 4.7K ohms.

 FREQUENCY RESPONSE (Mic. and Radio)—25 c/s to 30 kc/s ± 1dB extending to 100 kc/s ± 3dB.

 EQUALISATION Correct to within ± 1dB on RIAA curve from 50 c/s to 20 kc/s.

TECHNICAL SPECIFICATIONS TONE CONTROLS

- Treble + 12dB to 10dB at 10 kc/s.
 Bass + 15dB to 12dB at 100 c/s.

 SIZE—6in.x2in.x2in. overall, plus knobs.
- ioned in brushed and polished solid aluminium with solid aluminium with solid aluminium knobs. Black figuring on front panel. FINISH - Front panel

BUILT, TESTED AND GUARANTEED

£9.19.6

"Although a complete novice to radio I was able to assemble it (Micro-FM) without undue difficulty thanks to your clear and lucid instructions. I receive all B.B.C. programmes and local.....very strongly."
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H.A., London, N.6

INCLAIR MICRO COMBINED FM TUNER AND POCKET FM RECEIVER This unique, superbly engineered FM superhet is the only set in the world which can be used both as an FM tuner and an independent FM pocket receiver just whenever you wish. Problems of alignment have been completely eliminated making the Micro-FM ready for use the moment you have built it. The pulse counting discriminator ensures best possible audio quality; sensitivity is such that the telescopic aerial included with the kit assures good reception in all but the very poorest reception areas. The Sinclair Micro-FM will give you all you want in FM reception and the satisfaction of building a unique design that will save you pounds.



7 TRANSISTORS NO ALIGNING PULSE COUNTING DISCRIMINATOR A.F.C.

TUNES 88-108 Mc/s

SIZE—less than 3"×13"×3"

FM superhet using 7 transistors and 2 diodes. The R.F. amplifier is followed by a self-oscillating mixer and three stages of I.F. amplification which dispense with I.F. transistormers and all problems of alignment. The final I.F. amplifier produces a square wave which is converted to produce the original modulation exactly. A pulse-counting discriminator ensures better audio quality. One output is for feeding to amplifier or recorder and the other enables the Micro-FM to be used as an independent self-contained pocket portable. A.F.C. "locks" the programme tuned in.

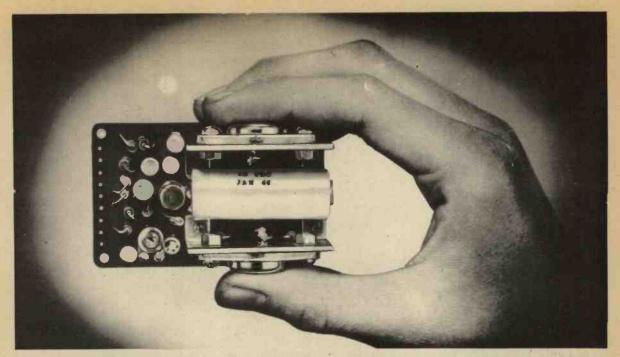
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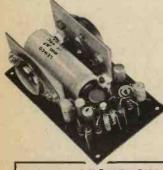
SINCLAIR Z.12

COMBINED 12 WATT HIGH-FIDELITY AMPLIFIER AND PRE-AMP

12 WATTS R.M.S. OUTPUT

8 TRANSISTOR CIRCUIT WITH CLASS B ULTRALINEAR OUTPUT

IDEAL FOR HI-FI (STEREO OR MONO) CAR RADIO, ELECTRIC GUITAR, P.A., INTERCOM, ETC.



The amazing adaptability and rugged construction of this very powerful and exceptionally compact amplifier make it possible to use just one type of unit with outstanding success in an unusually wide variety of applications. Eight special H.F. transistors are used in a highly original circuit to achieve the characteristics demanded of any quality amplifier irrespective of price, yet this Sinclair unit costs well under £5, including its own integrated pre-amplifier. The Z.12 accepts radio, microphone and pick-up inputs. Detailed instructions for connecting

these in mono and stereo are given in the manual supplied with every unit. A number of different control networks are also shown. The Z.12 will operate efficiently from any supply between 6 and 20 V. d.c, making it very convenient to run the amplifier from a car battery. Where it is required to run the Z.12 from mains supply, the PZ.3 is recommended. Those wishing to have a ready made pre-amp control unit can feed inputs via the Stereo 25, which, with two Z.12s will provide the finest stereophonic hi-fipossible—and the saving in cost is fantastic.

PZ.3 MAINS POWER SUPPLY UNIT

This special power supply unit uses advanced transistorlsed circuitry to achieve exceptionally good smoothing. Ripple is a barely measurable 0.05 v. The PZ.3 will power two Z.12s and a Stereo 25 with case.



TECHNICAL SPECIFICATIONS Size 3 in. × 1½ in. × 1½ in.

- Class "B" ultralinear output ■ RESPONSE 15-50,000 c/s ± 1 dB.
- Suitable for 3, 7·5 or 15Ω speakers. Two 3Ω speakers may be used in parallel
- INPUT-2mV into 2kΩ
- OUTPUT—12 watts R.M.S. continuous sine way a (24 w. peak); 15 watts music power (30 w. peak)
- Signal to noise ratio better than 60dB.
- Quiescent current consumption—15mA.

Built, tested and guaranteed. Ready far immediate use. With Z.12 manual.



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EL91 4/6
EL91 4/6
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PL500 13/6
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TECHNICAL DETAILS:

The unit is a compact and self contained loudspeaker system which only needs to be fitted into a simple cabinet of the recommended design to produce a high fidelity loudspeaker of the highest quality.

The unit consists of a 5in. bass unit 4in. tweeter and crossover network mounted on a duralumin plate which forms the front panel of the commonted on a duralumin plate which forms the front panel of the com-

mounted on a duratumin plate which forms the front panel of the complete enclosure.

The method of assembly of the module is unique in that the cone and synthetic rubber surround of the Sin. bass unit are mounted directly onto the duratumin front panel and the ceramic magnet is supported on substantial pillars attached to the panel. The conventional chassis with all its disadvantages is thus eliminated.

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Free constructional details of the recommended cabinet are readily available from us.

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High class receiver covering 550 ke/s.-31 mc/s. on 4 bands. Incorporate 7 valves plus rectifier, RF stage, illuminated '8' meter, 1.5µ' sensitivity, electrical bandspread on the 80/40/20/15 and 10 metre bands, silder rule dial, aerial trimmer, B.F.O., noise limiter. Output for phones or speaker. Operates on 115/220/240 v. A.C. Supplied brand new and guaranteed with manual. 24 gns. Carr. 10/r.



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800 v. P.I.V. 500mA. 5/8 800 v. P.I.V. 5 amp. 7/8 400 v. P.I.V. 500mA. 3/8 70 v. P.I.V. 1 amp. 3/8
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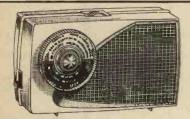
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● 7 stages—5 transistors and 2 diodes Fully tunable over Medium and Long Waves

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TRANSONA SIX

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POWER AMP. **MA-12**



STEREO AMP. S-99



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05-2



VVM, IM-13U

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RF-1U

IG-82U

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VOL. 3 No. 2 FEBRUARY 1967

PRACTICAL ELECTRONICS

CAREERS IN ENGINEERING

T may at first seem out of place for a hobby magazine to concern itself with the subject of careers. A hobby after all is supposed to be an activity pursued for pleasure and quite apart from one's normal occupation. It is also usually, but not necessarily, distinct in character from the daily job of work.

Since a considerable number of our readers are still at school, and since an even larger number are undoubtedly parents, we feel there are certain good reasons for focusing attention here on the opportunities that exist for a career in electronics.

Every day advertisements for electronic engineers in the National Press make abundantly clear the fact that demand exceeds supply. But if the shortage of qualified engineers is serious today how much more acute will this become in the vital years ahead as the horizons of technology—especially electronics broaden out still further?

Now, at last, a determined effort has been made to contact those youngsters who will soon be making decisions concerning their future. The staging of the Engineers' Day Exhibition at the Science Museum in London during the last Christmas holiday period was an excellent idea. If attendance is any criterion, its success would seem assured.

This exhibition sponsored by the Ministry of Technology contained exhibits by some 20 national industries and Government departments. The school boy (and school girl) visitors for whom it was primarily intended had the opportunity of learning something about the day to day activities of the engineer—often from first hand as well as from the visual displays.

The electronics-minded found an amazing variety of doors open to them. They will be able to practice their skill or art in environments as diverse as medical research or coal mining; in rail transport or in the armed forces; or perhaps in the field of atomic and nuclear research or radio communications. When the vast variety of opportunities in the non-nationalised sector of our economy is also taken into account, the choice awaiting qualified engineers is truly staggering.

And finally, to those who may hesitate to mix business and pleasure, a word or two of reassurance: no need to fear that once one becomes a professional, the pleasures of amateur electronics will disappear. Electronics is a BIG subject, you know.

THIS MONTH

CONSTRUCTIONAL PROJECTS VERSATILE BLOCKING 97 **OSCILLATOR** 107 AUTO CALENDAR DOORBELL REPEATER 118 RECORDING LEVEL 130 INDICATOR 137 CAR BURGLAR ALARM SPECIAL SERIES THE ELECTRONIC ORGAN-3 99 CLASSIC COMMUNICATION RECEIVERS—R1155 128 **GENERAL FEATURES** STICK-ON WIRING 96 102 LASERS FREQUENCY DIVISION 122 SILICON PLANAR **TRANSISTORS** 141 NEWS AND COMMENT EDITORIAL 95 THE 73 PAGE 112 MARKET PLACE 115 AUDIO TRENDS 121 **BOOK REVIEWS** 125 **ELECTRONORAMA** 126 **MEETINGS** 134 NEWS BRIEFS 146 DETACHED PARTICLES

Our March issue will be published on Friday, February 17

READOUT

All correspondence intended for the Editor should be addressed to: The Editor, PRACTICAL ELECTRONICS, George Newnes Ltd., Tower House, Southampton Street, London, W.C.2. Editorial and Advertisement Offices: PRACTICAL ELECTRONICS, George Newnes Ltd., Tower House, Southampton Street, London, W.C.2. Phone: Temple Bar 4363. Telegrams: Newnes Rand London. Subscription Rates Including postage for one year, to any part of the world, 36s. © George Newnes Ltd., 1967. Copyright in all drawings, photographs and articles published in PRACTICAL ELECTRONICS is specially reserved throughout the countries signatory to the Berne Convention and the U.S.A. Reproductions or imitations of any of these are therefore expressly forbidden.

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STICK-ON WIRING

RELATIVELY new proprietary brand of circuit wiring technique, which is versatile in experimental work, is now available to readers from Peak Sound (Harrow) Limited.

It has been given the name "Cir-kit" because it is quite a simple way of making a component layout match closely to its associated circuit diagram, therefore making checking, circuit reading, and fault location so much easier.

Cir-kit is generally obtained in sheet form and strip. The sheet can be cut to almost any required shape with a pair of scissors or metal shears. Curved, angular, and straight strips can be cut from the sheet. Both sheet and strip forms have an adhesive backing and protective paper. Hence the copper can be stuck to laminated plastics, cardboard, wood or similar insulating material.

It is possible to arrange crossed over-lapping strips, frequently seen on circuit diagrams, without short-circuit risks; not easily achieved with conventional printed circuit board without connecting link wires.

HOW TO USE

A series of photographs is shown here to illustrate how Cir-kit is actually applied to the s.r.b.p. board.

Cut one of the required lengths of copper strip (or cuttings from the sheet); stick down before proceeding to the next piece. Do not remove the paper backing until after cutting (1); maximum protection is still given to the adhesive until it is required to be stuck in position. No moistening of the adhesive is required.

It is not necessary to drill any holes until the whole layout is complete. This way the adhesive will have a better chance to settle. If a mistake is made the strip can still be lifted and adjusted without spoiling it or the board.

When satisfied that each piece is correctly laid, smooth down all the strips firmly, then mark the hole positions with a corribor on the corpor (2)

with a scriber on the copper (2).

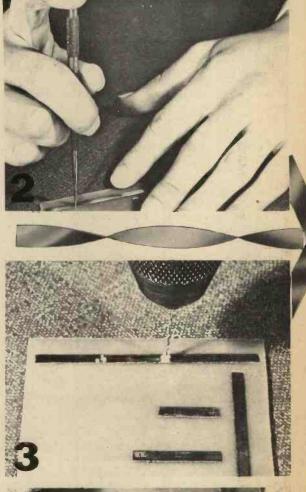
Use a small sharp drill (No. 60) to take the component wires (3). It is possible that a burr will form on the adhesive side of the copper during drilling and lift it slightly from the board. If this does happen, press down firmly again. Do not worry too much about this as the soldered wires will ultimately hold the copper quite firmly. The adhesive may become temporarily softened by heat and the copper again may lift slightly. Wait for it to cool and press down again firmly into position.

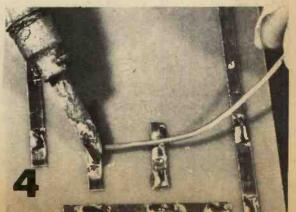
It is best to use the soldering iron in the same manner as with transistor leads, i.e. a hot iron applied quickly to avoid excessive overheating (4).

Crossovers can be effected by building up the circuit on both sides of the board or by placing one strip over another. The makers claim that the adhesive acts as an insulator, but to be quite sure it is better to leave the paper backing on where the top piece overlaps the underneath strip.

Where high component density is necessary the sheet material can be stuck on the laminate. Instead of etching the waste areas, cut them and peel them off, leaving a "printed circuit" appearance.







Versatile Blocking Oscillator

by G.M. HARVEY

FROM one simple basic circuit configuration three versions of a blocking oscillator can be built using Cir-kit stick-on wiring to provide a useful test signal injector, a morse practice oscillator, and an electronic siren.

BASIC CIRCUIT

The basic configuration is shown in Fig. 1. To this may be added a few components as described later to

give the required function.

The heart of these three projects is an astable blocking oscillator; the transformer Tl provides regenerative feedback, by phase inversion, from the collector to the base of TR1. The pulse repetition frequency of this oscillator is a function of the product of the base resistor chain (R1, VR1, R2) and the capacitor Cl and, as such, a considerable degree of pitch variation is obtained through varying the potentiometer VR1.

The waveshape characteristics, in the process of blocking and relaxing, are ramp or sawtooth at the base and pulse at the collector with a negative pip on the

trailing edge. See Fig. 2.

SIREN

In Fig. 3 is shown the siren circuit. Here, C2 is an electrolytic capacitor connected between the junction of R1 and VR1, and battery positive. The open primary terminal of T1 is connected via a small 3 ohm loudspeaker to battery negative. Switch S2 is used to disconnect the battery from the timing circuit. R1 and C2 in this configuration provide a time constant so that an increasing voltage to the base progressively raises the pitch of the note until charging is completed.

With the release of S1, capacitor C2 now replaces the battery and discharges through VR1, T1, R2, and the base/emitter diode of TR1 the whole action providing a

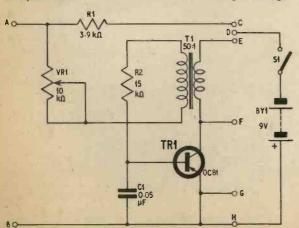
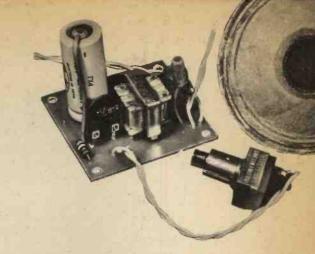


Fig. 1. Basic circuit to which must be added certain components as shown in Figs. 3, 4 and 5



slow pitch decay. The setting of VR1 will be a compromise between final pitch and decay rate and is therefore arbitrary. A possible application of this novelty would be to inject some realism into those toy electric motor car circuits that are proving so popular.

MORSE OSCILLATOR

In the morse practice oscillator (Fig. 4) C2 is omitted and C1 is changed to 100pF. This circuit runs at a frequency of about 1,000c/s with a range of pitch adjustment provided by VR1. S2 can be made a morse key to switch on the oscillatory action of the circuit.

SIGNAL INJECTOR

Finally, we come to the test signal injector which provides again an audio signal of about 1,000c/s. The

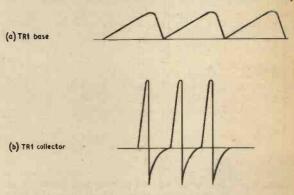


Fig. 2. Waveforms at base and collector of TRI

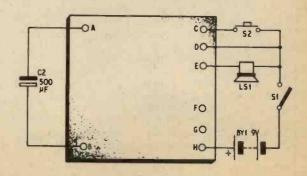
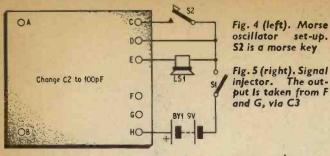
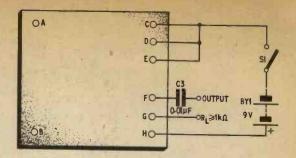


Fig. 3. Basic board plus components for making up the stren





loudspeaker is shorted out, the output being taken via capacitor C3 from the collector. See Fig. 5.

The signal content is harmonically broad as the output pulse is sharp edged and of brief duration, a characteristic of the blocking oscillator, and as such could be used for fault finding in a.f. and r.f. stages.

When unloaded, the output voltage was 4 volts peakto-peak with no substantial reduction at loads down to 1 kilohm. Below this value the output falls rapidly.

This demonstrates the excellent practicability of this injector as a valve and transistor circuit tester. To use it to test a radio or audio amplifier, a probe from C3 should be applied to the valve grid pin or transistor base. C3 should be rated at a high voltage (about 350V) to avoid accidental damage to TR1 from valve circuits. The test piece common line is connected to TR1 emitter.

The volume control of the unit under test should be turned to a maximum and signal injection should be applied to the output stage, then progressively to each preceding stage until the faulty or inoperative stage has been discovered; this of course becomes evident by the disappearance of the signal.

To check that this injector circuit is functioning, there should be an audible whistle coming from the transformer. If this is not working, the connections to one of the transformer windings should be reversed to correct the feedback phase.

CONSTRUCTION

Make up the basic circuit first as shown in Fig. 6 using the Cir-kit technique described on page 96. Then add the extra components required referring to the appropriate circuit diagram in Fig. 3, 4, or 5.

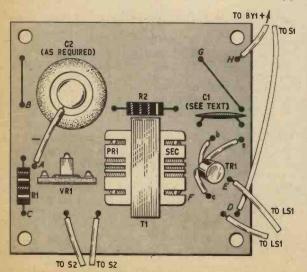


Fig. 6. Component layout of the basic board. Connections for C2, LS1, S1, S2 and BY1 as required are shown. C3 would be connected to F

COMPONENTS

Resistors

RI $3.9k\Omega$ R2 $15k\Omega$ Both 10% 1 watt carbon

Potentiometer

VRI 10kΩ linear carbon preset skeleton

Capacitors

0.05 µF disc ceramic 20V

or 100pF disc ceramic 20V (see text)

500µF elect. 15V

C3 0.01 µF ceramic 750V (Radiospares Hi-K)

Transformer

TI 50:1 "Miniature" output transformer (Radiospares)

Transistor

TRI OC81 (Mullard)

Switches

SI Single-pole on/off toggle

S2 Single-pole push button switch or Morse key (see text)

Miscellaneous

BY1 Battery 9V type PP9
LS1 3\Omega 3in diameter loudspeaker (see text)
Cir-kit copper "wiring" kit (see page 96)

P.V.C. wire, tinned copper wire

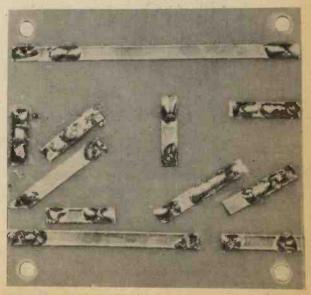


Fig. 7. Copper Cir-kit stuck on the underside and soldered



THE ELECTRONIC ORGAN

By ALAN DOUGLAS, Sen. Mem. I.E.E.E.

THE CONSOLE:

MANUALS and
PEDALBOARD

The organ is the only keyboard instrument in which the feet are used to play notes as well as the hands. Therefore the feet cannot be used to help to balance the body. All organists know that some consoles are extremely comfortable to play, others never seem right. This is because the proportions of the different parts are not properly related.

GOOD CONSOLE DESIGN

Fig. 3.1 shows a section of a good three manual console design and you will notice several things. Both upper manuals are slightly inclined to the horizontal, the top one having a little more rake. The bottom one is parallel with the ground. All proper organ keys are the same size so far as the visible parts are concerned.

But you can see that each manual overhangs the next to a definite extent and is also spaced away from its neighbour by a known amount. If an organ were to have four or five keyboards, some of these dimensions would change slightly, showing how critical it is to assure comfort.

One often sees statements claiming that a console is made to Royal College of Organist's (RCO) standards, but in fact there are no RCO standards except that an agreed design was reached for a pedalboard many years ago and we can certainly call this an RCO pedalboard. However there are many slight variants on this in existing pipe organs. The Incorporated Society of Organ Builders is now working on dimensions for a standard console.

It is obvious that, feet being larger than fingers, more space must be allowed between pedal keys than between manual keys. To prevent the reach for the furthest away keys becoming too great for comfort, these are inclined towards a point behind the centre of the bench. However, this would still make it uncomfortable if the keys were flat, as the knee would be bent up too much in the centre of the pedalboard. Therefore a position is found where middle D is comfortable, then each key to the left or right is progressively raised slightly so that, at the extreme ends, only a limited leg extension is required.

To relate these things, we go back to Fig. 3.1 and drop a plumb line from Mid D to the pedal key below. This should be D₁₅. The whole pedalboard is then moved fore or aft until the distances shown are reached. All

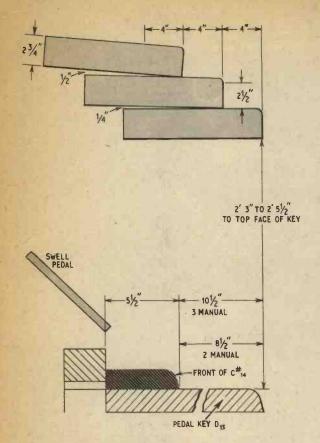


Fig. 3.1. This sectional drawing shows the critical dimensions in a three manual console

these measurements added together give an excellent playing balance, but of course there are shorter and taller people and they can generally accommodate themselves by means of an adjustable bench.

A great many small organs have short stub pedals of 13 notes compass and these include all the undesirable features of the flat pedalboard. No proper use can be made of published organ music with these elementary devices and this is indeed an example of spoiling the ship for a hap'orth of tar. But for the rhythmic fan they appear to be adequate.

CHURCH ORGAN DESIGNATIONS

Now, having assembled the parts which will control the organ, we begin to see the difference between the church and theatre approach. In our Fig. 3.1, we could call the manuals, from the top downwards: upper, middle, lower; or, swell, great, choir; or solo, main, accompaniment.

All these designations appear in the literature; why so? Well, the first example is certainly non-commital and quite logical; but it is little used. The second example can only refer to the church organ because these names have been so used for several hundred years. This is a good opportunity to explain these names. The swell manual is an expressive one, so called because the sound "swells out" when shutters regulating the volume of enclosed pipes associated with this manual only are operated. The middle keyboard, the great, was not always so called; but at all times it has been the main source of sound and to this end, no pipes on it are ever enclosed so none can be altered in volume. The lower keyboard is a later addition to the pipe organ and is called the choir because it contains a selection of quietly voiced stops to accompany singing (of a choir, not a full congregation). This manual is often enclosed, that is, has moveable shutters enclosing pipework to regulate the sound; but equally, it is often

You can see from the above that each keyboard is a complete organ, with its own independent pipes, though some of these can be interconnected by mechanical means.

THE MIGHTY WURLITZER

When we examine the last category, we find an entirely different conception of organ playing. When the late Robert Hope-Jones, with his usual prophetic imagination, saw that the silent film needed a new form of sound accompaniment, he met with a very chilly reception from the British organ builders—in spite of the fact that he was an accomplished organ builder and had many fine instruments to his credit some of which are still in regular use. So he wasted no time but went to the Rudolph Wurlitzer company in New York, who welcomed him with open arms. This was the start of the "mighty Wurlitzer", the most successful and beautifully engineered of all theatre organs.

Now Hope-Jones started life as a telephone engineer, so he knew a great deal about relays and the idea of miles of wire did not daunt him at all. And this is the crux of the whole thing; the theatre pipe organ is an



The horseshoe type console of a modern Compton theatre organ

electro-mechanical switching system capable of instantly connecting or cross-connecting almost any conceivable tonal arrangement by pressing buttons. Included in these tonal schemes were cymbals, drums, gongs, even full-sized pianos. Non-tonal adjuncts were train and boat whistles, sirens, motor horns, wind and wave noises, bird calls, rain, thunder and various other effects useful in the cinema. All had to work with precision, reliability and the correct loudness. Hope-Jones called this his "unit orchestra".

Therefore, whereas in a church organ each keyboard has its own pipes, Hope-Jones put his sets on unit chests, which merely means that anything which made contact with this chest could operate all the pipes thereon. So it was quite easy to make the chests "float", in other words, all the chests would appear on all manuals and pedal and be playable from all. So there was now no difference between the sounds possible on the various manuals, and they were called solo and accompaniment; the other manual (if used) being sometimes called "main", sometimes nothing at all.

So, with fully floating action there was no need for

So, with fully floating action there was no need for couplers except perhaps from manual to pedal, since this department alone had larger and more massive low pitched pipes which could not be played in chords.

COLOUR CODING FOR STOPS

Hope-Jones also at this time (55 years ago) introduced his colour-coding system for stops, which is still in use, and he also designed the large and comfortable stop key found on theatre consoles. This system uses white for flutes, tibias, and diapasons; red for reeds of all kinds; yellow or amber for string tones; black for non-tonal stops, e.g. tremulants, etc. Incidentally, why the name stop? Again, we go back nearly 400 years to find the "wooden shaft which, when pressed in, stopped the wind from entering that set of pipes".

The foregoing should help the reader to understand why the different parts of the organ are so named, and naturally with pipes we would expect a very different kind of sound from the two types; but with electronics, this is not so likely to be so, since only in the most elaborate and costly organs would we find separate generators for each rank, i.e. an exact correspondence with pipes. More than likely, we would find a worse state of affairs, where one set of generators has to be shared out amongst all the tonal requirements of the organ. So let us have a quick look at generating methods.

ELECTRONIC GENERATING METHODS

It is taken for granted that we are not interested in precision-made electro-mechanical systems and must concentrate on static electronic circuits. So, there are only two forms open to us; those having an independently tuned oscillator for every note; and those in which only the notes of the top octave are independently tuned, all other notes being obtained by frequency division. There is something to be said for both, and indeed organs by the most eminent makers use both systems.

All readers are aware that some organ voices are smooth and luscious; some are thin and keen; yet others are sonorous and reedy. Does this not suggest it is going to be rather hard to form all of these from one single kind of waveform, no matter what its shape? It is done, of course, but as a rule the circuitry is formidable and some restrictions are necessary. Or, alternatively, all the voices become degraded and lose fidelity. Then again, we have to be able to mix stops;



Modern Wurlitzer organ, fully transistorised

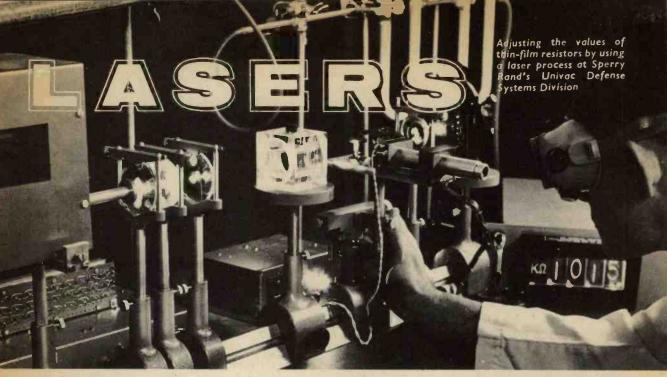
if all come from a common waveform there can be considerable losses.

But these factors are not so important as the basic and inescapable fact that in a pipe organ—church or theatre—one does not hear all the sounds at the same instant and that, although perhaps in theory the harmonic content is equally regulated for each pipe in each stop, it is not so in fact and in any event the pipes do not stand in tune for more than a few hours. Thus we find innumerable small beats and phase differences which impart a great richness to the sound.

Now in a system having independently tuned oscillators we get just this, if these oscillators use inductances. Small differences in the iron/air ratio, stacking factor, grain orientation, etc. provide differences in harmonic amplitudes which can be used to great effect. Naturally these oscillators cannot be sinusoidal, but it is possible to retain a sinusoidal tank circuit, which is good for stability, and obtain some 40 harmonics elsewhere in the circuit. Of course, one could be very clever and use grain-oriented laminations or powdered iron cores; and at once these advantages disappear. There is an economic limit to the number of these so-called free-phase oscillators one can use, but we can profitably form the main core of the organ with this circuitry.

FREQUENCY DIVIDER SYSTEM

The divider arrangement is very economical in cost and space, but is phase-locked and limited to (usually) a square wave output. This would be available at many pitches, and since one must key the signal directly with constantly-running dividers, the problem of click suppression becomes very serious at high frequencies. A square wave of this kind is devoid of even harmonics, but we must have these for some voices so when we come to discuss this divider system for actual use, we will show how even harmonics can be introduced when required.



PART 2

RUBY LASERS

The ruby laser was the first type of laser to be developed; it first appeared about 1960. It provides an intermittent output in the form of light flashes of high intensity, whereas the output of the gas laser is continuous.

The ruby crystal itself used in this type of laser consists of aluminium oxide containing about 0.05 per cent of chromium oxide. The crystal is in the form of a cylindrical rod, perhaps 10cm in length by 1cm in diameter.

The two ends of the crystal are carefully polished and made parallel to each other before a reflective coating is deposited on them. The ruby crystal is placed at one of the foci of an elliptical mirror (see Fig. 5), a flash tube being placed at the other focus. The mirror is polished on its inner surface. Almost the whole of the light emitted by the flash tube is focused by the mirror onto the ruby crystal. Some ruby lasers employ simpler systems without an elliptical mirror.

The flash tube used is similar to the type of flash tube used in photography, but may be much more powerful. The energy emitted by the flash tube raises the energy level of many of the atoms in the ruby crystal, but almost immediately the excited atoms lose some of their energy to the crystal lattice, which is thus raised in temperature.

The atoms are left in an excited metastable state. Photons emitted by some of these atoms travel through the crystal and are amplified as they move by normal laser action. The amount of light builds up very quickly and escapes through one of the end mirrors.

The output flash from both the flash tube and from the ruby crystal has a duration of about one millisecond. The laser action stops when the number of atoms in the excited state is too small for photon amplification to continue. By J. B. Dance M.Sc.

The power output of a ruby laser can be very large. Power levels of over one megawatt can be obtained for a period of about one millisecond. If a suitable lens is used to focus this light, the energy is adequate to punch small holes through a steel plate of considerable thickness as shown in Fig. 6.

Such lasers can obviously cause severe burning of the skin and suitable precautions must be taken when they are being used. They are finding medical applications, especially in the treatment of detached retinas, but are also being used against certain types of cancer. It has been suggested that they might be used for drilling minute holes in teeth. They are not likely to be used for communications work, since their light output is intermittent.

The cost of a ruby laser varies with the power output which it is designed to provide. The ruby crystal used in a fairly small laser will cost about £100, but the price increases rapidly with increasing crystal size. The flash tube and its power supply are quite expensive items, whilst the elliptical mirror is not by any means cheap. Thus it seems unlikely that ruby lasers will be used by many amateurs.

The ruby laser is one example of a class of lasers known as doped crystal lasers. The crystal used in these types of laser contains impurity atoms dispersed in a crystal of another material. It is one of the inner orbits of the impurity atoms which give rise to the laser action. The electrons in these inner orbits are essentially isolated from the effects of the neighbouring atoms. Another example of a doped crystal laser is the neodymium doped glass type, but this can operate only in the infra-red region.

Q-SWITCHING

The ruby laser can provide a much higher power output than a gas laser, but a technique known as "Q-switching" can be used to increase the output power

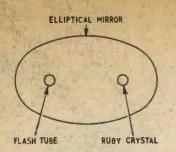


Fig. 7. A ruby laser with a Kerr Cell for Q-switching. The output beam is taken through one of the end mirrors which is only partially silvered. The elliptical mirror has been omitted for clarity

CELL

RUBY

FLASH TUBE

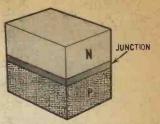
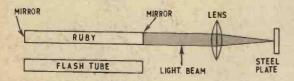


Fig. 8. A semiconductor laser

Fig. 5. Section through a ruby laser



MIRROR

Fig. 6 (left). The use of a ruby laser to punch a hole through a steel plate. The elliptical mirror around the ruby crystal and the flash tube has been omitted for clarity

considerably. It is not possible to feed an unlimited amount of power from a flash tube into a ruby crystal, since the crystal would be damaged.

An upper frequency limit (typically two flashes per minute) is imposed on ruby lasers, since the crystal would overheat at higher rates unless the energy per flash is reduced. In the Q-switching technique the total output energy of the flash is not much increased, but the energy is delivered in a very much shorter time, perhaps in one hundredth of a microsecond.

In a Q-switched laser an absorber is introduced so that laser action cannot take place whilst the number of excited atoms is increasing. When the number of excited atoms has reached a maximum, the absorber is removed and the whole of the stored energy is released in a minute fraction of a second.

In practice an electronic absorber (such as a Kerr Cell) is used, since it can be made transparent to the radiation in a minute fraction of a second by the application of an electrical pulse (See Fig. 7). A laser has a Q factor very similar to the Q of a tuned circuit. The introduction of an absorber lowers this Q factor. Thus the operation of the laser occurs when the Q is switched from a low value to a high value.

SEMICONDUCTOR LASERS

A completely different form of laser has been made using gallium arsenide pn junctions. It has been known for some time that a gallium arsenide junction diode will emit infra-red light when suitably biased. However, if two opposite edges of a gallium arsenide crystal are polished (Fig. 8) so that they form parallel faces, and the current per unit area passing through the junction is great enough, a kind of laser action occurs which results in the emission of coherent light from the junction region.

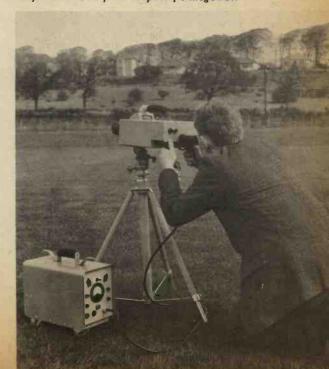
Although gallium arsenide is the most commonly used material in semiconductor lasers, various other semiconductor materials can be employed. Gallium arsenide emits infra-red light, but other wavelengths in the infra-red region can be obtained by the use of other semiconductor materials.

In a semiconductor laser the electrons injected into the junction region lose some of their energy when photons are formed. These photons can cause other electrons to lose energy and form photons by stimulated emission. The laser action can take place only at high current densities where the number of electrons in the conduction band exceeds that in the valency band of the semiconductor material.

The semiconductor laser is a small and rugged device which has an appearance somewhat similar to that of a transistor to which a suitable window has been fitted. At room temperature a semiconductor laser should be operated only by pulses, since if a continuous current high enough to produce laser action is used, the heat developed will damage the semiconductor junction.

These lasers are much more commonly used at liquid air temperatures where a very high efficiency can be obtained. An applied potential of the order of 1 volt at some tens of milliamps will produce a light output power of the order of ten milliwatts.

Barr and Stroud laser rangefinder for objects up to 10 kilometres distant. The transmitter uses a Q-switching ruby laser with a peak output of I megawatt





The G. & E. Bradley ruby laser. The ruby crystal and flash tube are contained in the elliptical box to the right of the mouth of the operator

The main limitation of the gallium arsenide laser is its low output power. Nevertheless the brightness (light emitted per square centimetre) of the junction region is very great, although the junction is very small. Owing to this small junction area, the light beam will have a divergence of a few degrees due to diffraction effects.

Semiconductor laser light is easily modulated by altering the current flowing through the junction region. However, the frequency is not very stable and therefore the use of semiconductor lasers in communication systems would tend to provide a noisy output.

OTHER TYPES

Various other types of laser have been developed, but at the moment they are seldom found outside laser research laboratories.

Much research is being carried out on new methods of introducing the pumping energy in an attempt to raise the efficiency of the system. In one type of laser the pumping energy is provided by a chemical reaction in the material surrounding the active laser material, whilst the use of nuclear fuel inside a laser to provide the required energy has been suggested.

THE SAFE USE OF LASERS

There being as yet no statutory regulations governing the safe operation of lasers, there is published, by the Ministry of Aviation, a document "Laser Systems-Code of Practice". The notes given here were compiled from this document and extracted from "A General Guide to the Safe Use of Lasers" published by the Electronic Engineering Association.

Attention is concentrated on the hazard to vision, but it should not be forgotten that laser devices often use high voltages and that normal precautions must be taken against electric shock and the explosive failure of ancillary equipment.

Danger to the Eyes in Direct Viewing

The focusing action of the lens in the eye may concentrate the light on to a small spot on the retina for a considerable range of visible and infra-red wavelengths. If the energy in the beam is sufficient, tissue will be heated and killed, resulting in blindness at that spot. Higher energies will cause damage to the cornea, iris, lens and eyeball itself. Complete blindness may result. while the subject may be unaware that damage is taking place. This is particularly so with lasers working outside the visible region.

Other Effects on the Eye

Infra-red radiation is known to cause corneal cataract (so-called "glass blowers cataract") with excessive exposure. Many laser wavelengths are now in use experimentally which might cause this effect. The common helium-neon laser, for example, often works at 1.15μ and at 3.39μ wavelengths as well as in the visible region.

Effect on the Skin

At sufficiently high levels energy will produce burning of skin; other damage, such as rupture of the cell walls, is also to be expected. Investigation of these effects is at an early stage.

Note that some gas lasers, for instance those using argon, produce considerable amounts of ultra-violet radiation from the sides of the tube which can cause

burns also.

A laser should not be used in the open without great caution. The effective "range for safe viewing" and polar diagram for the laser should be known accurately, taking account of possible reflections and off-axis lobes.

Safety Spectacles

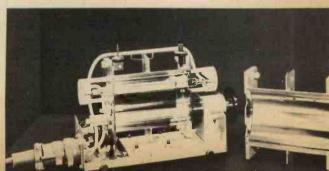
There are a number of commercial spectacles available which give some protection to the eyes from laser radiation. They may be either of wideband absorption or narrowband reflection type. Neither type should be relied on to give a major part of the protection between a laser beam and the eye. Before use they should be tested to ensure that they do not shatter or become transparent during exposure. They should be chosen carefully for the wavelength required and marked distinctively to prevent accidental use of the wrong type.

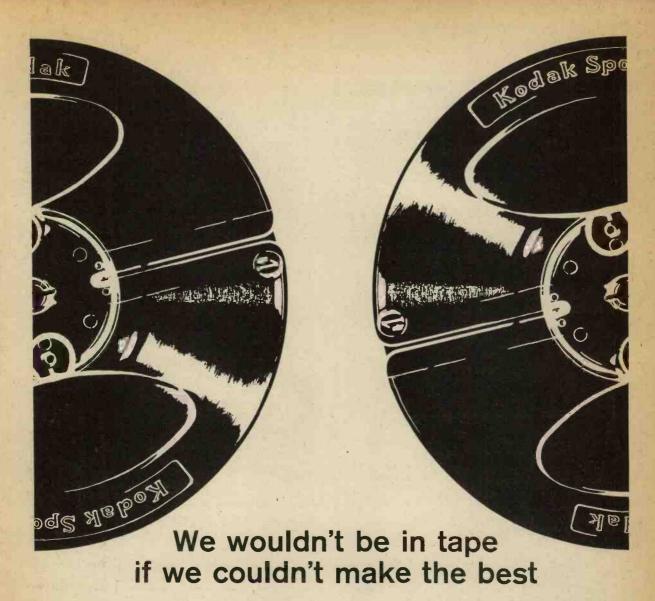
When using protective glasses the pupil is likely to be enlarged because of the reduced ambient light reaching

the eye, and this should be taken into account.

In the present state of medical knowledge, it is clearly desirable to exclude from further risk those who already possess obvious retinal defects. It is, therefore, recommended that those about to undertake work with lasers should have a retinal examination, and that a photographic record should be taken.

The head of the M.E.L. laser is in the form of an elliptical reflecting cavity in which the flashtube is mounted along one foci and the laser rod along the other. In this photograph the two halves of the cavity have been separated to show the construction





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by D.F. Moody B.Sc.

HE DESIGN of this auto-calendar is interesting as it attempts to combine factors which, as usual, often conflict with one another, and so compromise is an essential ingredient. For example, long life must be attained as a prime requisite; low power consumption is desirable as the apparatus is left on continually; moderate cost: insensitivity to mains fluctuations, small overall physical size and so on.

It is hoped that the design presented is a reasonable compromise and that, even if the reader is not prepared to put his hand a bit deeper into his pocket and construct this equipment, he will obtain some useful information from the article and appreciate the tremendous variety of uses of the host of modern components.

RING COUNTERS

The circuit is essentially a counting circuit using cold cathode tubes as elements, chosen as they are relatively cheap and are self-indicating with a pleasing orange glow.

The day name and day number rings are stepped in parallel, and the month ring is driven in series from the day number ring. Feedback is applied to the day number ring to control the number of elements in this ring in accordance with the number of days in each

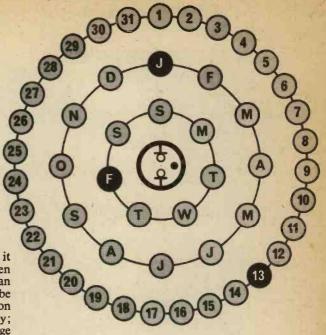
month. See Fig. 1.

The calendar is told when to change date in the most appropriate way, i.e. by the coming of dawn, detected by an externally mounted cadmium sulphide cell. When not illuminated this cell has a very high resistance, and so the voltage at the junction of VR1 and R2 is high. R3 is chosen such that there is sufficient base current in TR1 to ensure saturation. Hence the collector voltage on TR1 is very small, with all the voltage dropped across R4.

With light now falling on the cell, its resistance decreases and so the voltage across C2 falls. This large capacitance ensures that no transient fluctuations (such as lightning at night) will affect the calendar.

As the voltage falls so does the base current into TR1. Hence when the base current has fallen sufficiently TR1 will leave saturation and the collector voltage will rise. When it reaches the striking voltage of VI, VI will ignite. Due to C3, V1 thinks that it is striking from a low impedance source and so gives a good pulse into the base of TR2.

By choosing the ratio of R4 and R5 correctly, VI cannot oscillate but will settle down to a stable condition. As the base current into TR1 is further



reduced, it is effectively cut off. The collector voltage of TR1 is held at a safe level by the voltage drop across R4 due to the current flow through V1.

The current pulse into the base of TR2 is amplified by TR2 and is then fed into the gates of SCR1 and SCR2. Hence these thyristors will fire and as explained later will step the day name and number counters by one.

The feedback system from the month ring to the day number ring is a bit too complex to describe in the space available, but it can be seen that when day number 1 tube strikes it feeds a current pulse into the base of TR3 which amplifies it and feeds it into the gate of SCR3

which then steps the month ring.

The push to make switches S1, S3 and S4 are provided to enable the correct date to be set up initially. S2 is the leap year/ordinary year switch to correct for the 29th day in February. In the position shown it is an ordinary year. It should be changed (if necessary) at the beginning of a new year so that it is not forgotten. Switching it at any time other than the 28 or 29 February will obviously not affect any other date.

The construction of the device has been divided

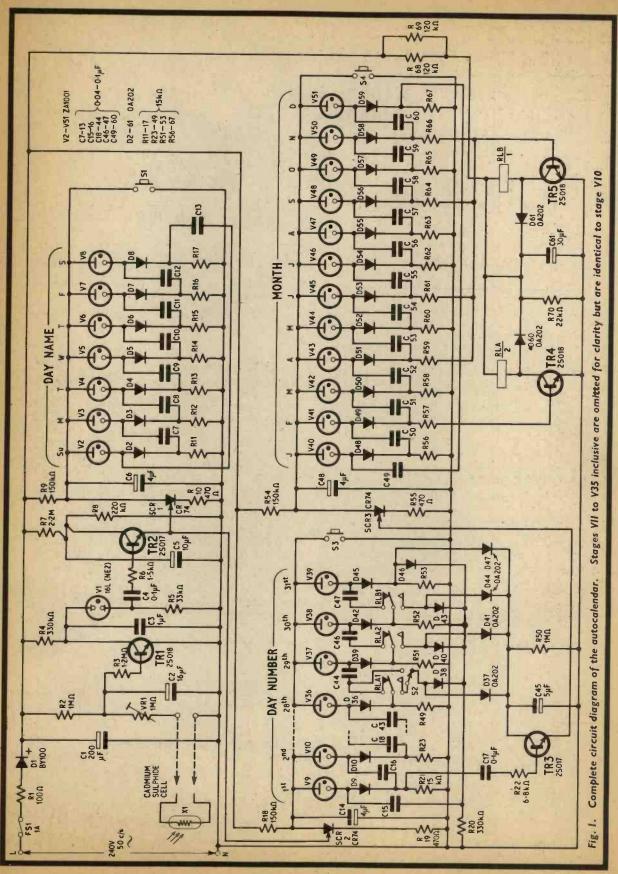
conveniently into three parts:

- (a) Board one. This holds the three ring counters.
- (b) Board two. This holds the remainder of the circuit with the exception of the relays, the large smoothing capacitor C1, the manual controls and the cadmium sulphide cell.
- (c) Unit construction and installation.

BOARD ONE—FUNCTION

The operation of the ring counter can be seen by considering one of the cold cathode tubes conducting. The common rail voltage will then be the sum of the maintaining voltage of the tube and the voltage developed across the cathode resistor. This is arranged to be less than the striking voltage of any other tube and so the condition is stable.

If the common rail voltage is reduced, i.e. by closing the shunt switch S1, S3 or S4, or by firing the shunt



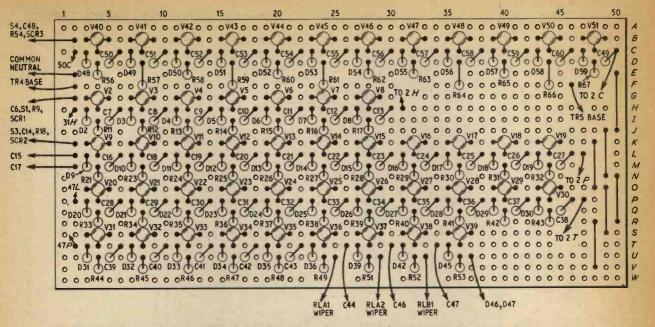


Fig. 2a. Component layout of Board I. All components are viewed end on. Pins are inserted as in text

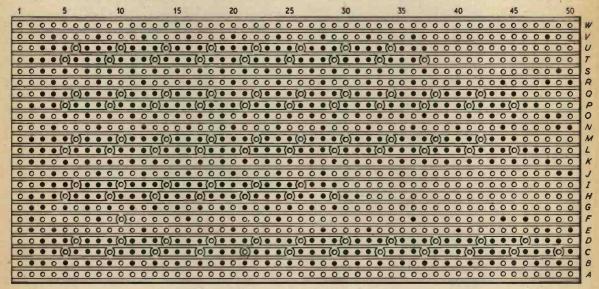


Fig. 2b. Underside view of Board I showing copper strip breaks and connections

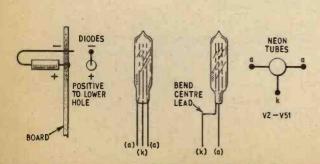


Fig. 3. Mounting details of diodes and cold cathode tubes on Board I. Resistors and capacitors are mounted similarly to the diodes

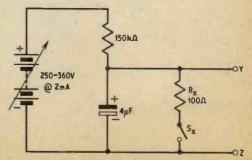
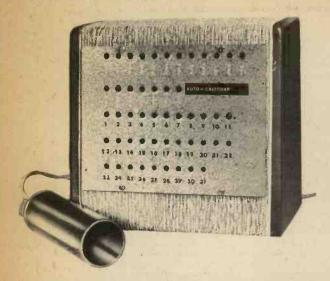


Fig. 4. Test circuit for Board I. The battery can be a variable d.c. supply unit

AUTO GAUENDAR



thyristor, then the tube which was conducting extinguishes. The capacitor joining the cathode resistor of the extinguished tube to the cathode of the next tube is charged to a voltage equal to the voltage across the cathode resistor. Due to the diode this capacitor cannot lose its charge, and so the cathode of

the next tube is made negative.

If the switch is opened (or the thyristor extinguished) the common rail voltage starts to rise with a time constant determined by the shunt capacitor and the common feed resistor. This time it is made sufficiently long to ensure that the tube which was conducting is completely de-ionised. Hence the next tube with its cathode negative has a greater voltage across it than any other and will strike first.

In this way the glow is transferred round the ring. In the case of the day name and month rings the loops contain a fixed number of elements (seven and twelve respectively). In the case of the day number ring the number of elements is controlled by feedback system from the month loop so that the number of elements is varied from 28 to 31 to cater for the different number of days in different months. The 29th day of February in a leap year is taken care of by a manually operated slider switch, S2.

Board one holds the day name, day number and month ring counters, and will measure about 8in × 4in and about lin in depth. These figures will depend on

the pitch of the Veroboard used.

The layout is such that the cold cathode tubes (being self-indicating) are viewed end on as indicated in Fig. 2.

Board 1 will be attached to a face plate which is drilled such that the holes correspond to the positions of the cold cathode tubes. Hence at any one time there will be three cold cathode tubes glowing, one indicating the month, one the day name and the other the day number.

COMPONENT LAYOUT

With the high density grouping of components required to keep the overall dimensions of the unit within reasonable limits, construction on Veroboard is essential. Design of layout is considerably eased by the repetitive nature of the ring counters, which also helps to reduce assembly errors.

The pitch of the Veroboard has been given although this will depend on the size of the components used, especially the capacitors; it would be best therefore to buy the Veroboard after the components, choosing the smallest pitch that enables you to site the components without too much difficulty.

ASSEMBLY

Assembly of board one, although time consuming, is relatively simple if approached in a methodical manner.

First cut the board to the right size, giving 23 copper strips each with 50 holes. Then place the board in front of you, plain side up and insert a piece of wire through hole C5; turn the board over and remove the copper from around this hole; proceed like this until all the holes similarly shown in Fig. 2b have been done.

The resistors should be mounted first and they will take heat better than other components. Bend one lead of the resistor alongside the body of the resistor and then cut the leads as shown similarly for the diodes

in Fig. 3. Do this to all resistors.

A useful technique when assembling components vertically is to cover one of the holes on the copper side with solder. Then, holding the board in the left hand, keeping the component in the desired holes with pressure from your left-hand index finger, touch the solder blob lightly with the iron when the lead will slip through the hole and be held in place by the solder. The board can then be laid flat and the leads soldered

When all the resistors have been fitted, the capacitors and diodes should be assembled. Observe the correct polarity connections. The utmost care should be taken when the cold cathode tubes are being fitted as the glass around the lead-outs will break if the wires are strained too much. Bend the centre lead as shown (Fig. 3.), so that the three leads fit neatly into the three holes. Again, cut the leads before soldering the tube in.

Mount the tubes vertically to the board so that when the face plate has been drilled the glass pips at the top

of the tubes coincide with the holes.

It will be noticed that there is some variation in tube length. As it is desirable to keep the distance from the top of each tube to the board the same, it will be necessary to mount the shorter tubes a little further out from the board, but keep leads as short as possible as this will give the tubes greater rigidity.

When this has been done solder the wire links, and then check carefully all the soldered joints. The board

is now ready for testing.

Connecting pins are inserted in holes B2, E2, F2, F46, G2, K2, L2, M2, T26, T30, T34, U25, U29, U33, and U37 for easy accessibility during testing and interunit connection.

TESTING BOARD ONE

For adequate testing of Board 1, a variable stabilised power supply, giving 250 to 360 volts 2mA d.c. will be required with two resistors: 150 kilohms, 1 per cent, 1 watt; 100 ohms, 20 per cent, ½ watt. See Fig. 4.

One press-to-make switch and a capacitor 4µF 250V are also required. The purpose of testing Board 1 by itself is first to check that the connections are correct and that faulty components are located while it is still relatively easy to change them. If testing is omitted before the complete unit is built then, due to the closeness of components, fault finding will be made very much more difficult.

COMPONENTS . . .

```
C47 0.04µF or 0.1µF paper ISOV (T.C.C. type
Resistors
                                                                          CP113G/4G)
        100Ω 6W
  R1
                                                                    C48 4µF elect. 300V (T.C.C. Elkomold)
  R2
        IM\Omega
                                                                    C49-C60 0.04µF or 0.1µF paper 150V (T.C.C. type
        1.2M\Omega
  R3
                                                                    CP113G/4G) (12 off)
C61 30μF elect. 150V (Hunts)
        330kΩ ½W
  R4
  R5
        33k\Omega
  R6
        1.5kΩ
                                                                 Cold Cathode Tubes
  R7
        2.2M\Omega
                                                                    VI 16L (NE2) (Hivac)
V2-V51 ZA1001 (Philips) (50 off) (Henry's Radio)
  R8
        220kΩ
  R9
        150kΩ IW, 1%, high stab.
  RIO 470\Omega \frac{1}{4}W, 5%, high stab. (7 off)
RII-RI7 15k\Omega \frac{1}{4}W, 5%, high stab.
                                                                 Transistors
                                                                    TRI 25018
TR2 25017 or 25018
  RI9 470Ω ½W
                                                                                             (Texas)
                                                                    TR3 2S017 or 2S018
  R20 330kΩ
                                                                    TR4 25018
  R21 15k\Omega \frac{1}{4}W, 5%, high stab.
R22 6.8k\Omega
                                                                    TR5 25018
        6-8kΩ
  R23-R49 15k\Omega \frac{1}{4}W, 5%, high stab. (27 off)
                                                                  Thyristors
  R50 IM\Omega
                                                                    SCR1, 2, 3 CR74 or CRS140 (S.T.C.) (3 off)
  R51-R53 15kΩ ¼W, 5%, high stab. (3 off)
  R54 150kΩ IW, 1%, high stab.
                                                                  Diodes
  R55 470Ω ±W
                                                                    DI BY100
  R56-R67 15k\Omega \pm W, 5%, high stab. (12 off)
                                                                    D2-59 OA202 or OA200 (Mullard) (58 off)
  R68 120kΩ IW, 5%
R69 120kΩ IW, 5%
                                                                    D60, D61 OA202 (Mullard) (2 off)
  R70 22kΩ IW, 5%
                                                                  Cadmium Sulphide Cell
  All 10%, 4 watt except where otherwise stated
                                                                    XI I watt, type 2 (Proops Bros.) or ORP15 (Mullard)
Potentiometer
                                                                  Relays
  VRI IMΩ linear carbon preset miniature
                                                                    RLA, RLB 14kΩ, 2 sets of changeover contacts
                                                                                 (2 off) (Magnetic Devices Ltd. series 2400)
Capacitors
  C1
C2
        200µF elect. 350V
                                                                  Switches
         16µF elect. 350V
                                                                    SI Single pole, on/off, push to make
S2 Single pole, changeover, slide swi
  C3
C4
        1μF paper 150V
0·1μF paper 150V
                                                                         Single pole, changeover, slide switch
                                                                    S3 Single pole, on/off, push to make
  C5
        10μF elect. 50V
                                                                         Single pole, on/off, push to make
        4μF elect. 300V (T.C.C. Elkomold)
                                                                         Double pole, on/off, slide or toggle switch for
  C7-C13 0.04 pF or 0.1 pF paper 150V (T.C.C. type
                                                                         the mains (optional)
  CP113G/4G) (7 off)
C14 4μF elect. 300V (T.C.C. Elkomold)
                                                                  Fuse
   C15 0.04 pF or 0.1 pF paper 150V (T.C.C. type
                                                                    FSI IA anti-surge cartridge fuse with holder
         CP113G/4G)
   C16 0.04 pF or 0.1 pF paper 150V (T.C.C. type
                                                                  Miscellaneous
         CP113G/4G)
                                                                     Veroboard 0.15in hole matrix, 3.75in x 17in,
  C17 0.1 μF paper 150V
C18-C44 0.04 μF or 0.1 μF paper 150V (T.C.C. type
                                                                     Perforated board same size to match above
  CP113G/4G) (27 off)

C45 5μF elect. 50V

C46 0.04μF or 0.1μF paper 150V (T.C.C. type
                                                                     Aluminium sheet 18 s.w.g. 5in × 17½in
                                                                     Wood for case required later
                                                                     Tube for mounting XI required later
         CP113G/4G)
                                                                    Tinned copper wire 20 s.w.g.
```

Month Ring

Connect pin B2 to point Y on the test circuit.

Connect pins E2, F2, F46 to point Z on the test circuit. Switch the power supply on. It is likely that more than one tube may ignite as there is no preferential priming of any one tube. Adjust the d.c. supply to about 280V and then press the switches and release. Continue doing this until one tube is glowing and then leave the circuit alone for about two minutes. This is to allow time for any priming of any other tube to disappear.

Adjust the supply to 300V and by pressing the switch step the glow around the ring. If the glow steps around correctly then the components and joints appear

satisfactory

This test should then be carried out with supply voltages in the range 270V to 360V. The circuits should still perform properly. If the glow jumps about, then check carefully for dry joints. If one tube refuses

to ignite the likely cause will be that the diode in its cathode circuit is faulty. Check this with an ohmmeter after switching off the h.t. If this appears to be all right then it is possible that the cold cathode tube is faulty, in which case it should be replaced.

Day Name Ring

Connect pin G2 to point Y on the test circuit. Connect pin E2 to point Z on the test circuit. Carry out tests as above.

Day number ring

Connect pin K2 to point Y on the test circuit. Connect pin E2 to point Z on the test circuit. Connect capacitors (the ones which you have used on the board) between pins U25-T26, U29-T30, U33-T34, U37-L2.

Carry out tests as above.

Next month: Board 2 construction and assembly

the 7707 page by Jack Hum G5UM

"No Royal Road", part two

"There is no royal road to obtaining an amateur radio transmitting licence". Thus had said Mr Smith of Herne Bay to the young hopeful of whom we wrote here last time... hopeful of becoming a transmitting amateur, less hopeful when he discovered the definition of "royal road" to be "a means of attaining without trouble".

Mr Smith by the use of this phrase had made it clear that, like most of the worthwhile things in life, the transmitting permit was not to be had for the asking: it would need to be

worked for.

All this was in the mid-Nineteen Twenties. Yet what was said then is true today; and although, still, no royal road exists, aspirants to the transmitting licence in the mid-Nineteen Sixties enjoy the considerable advantage of knowing much more accurately than was formerly the case exactly what they must do to get it.

They can obtain from the Post Office a useful pamphlet (and it is free) called How to become a radio

amateur.

They can buy a variety of books to help them to pass the Radio Amateurs' Examination.

They can sit this examination very conveniently at the local "tech".

And as for morse code, today's "young hopeful" (and the old hopefuls too) can work up his speed to the obligatory "twelve per" by following one of the slow morse broadcasts which are organised by the R.S.G.B. in many urban areas. For a final polish up of his code speed he can seek the co-operation of one of his local transmitting men—and there are 13,000 of them the length and breadth of the land.

Self Taught

Forty years ago there were a bare 2,000 of them—and none of the facilities described above. Morse

was very largely self taught. And even though there was no Radio Amateurs' Examination to measure the strength of a person's claim to be granted a transmitting licence, it was still necessary to show oneself to be versed in "wireless lore" if one harboured any hope at all of persuading authority to part up with the coveted permit.

This was done by means of a rather curious device called "the line of experiment". In the "Twenties the British amateur transmitting fraternity were licensed to operate their stations "for experimental purposes", not for general communication as is the case today. Forbidden to transmit the CQ general call to all stations, they became the only group of amateur transmitters in the world to use the word TEST as a synonym for the "general call". They were "testing" in the interest of their "lines of experiment". At least this characteristic was a distinguishing feature of the U.K. radio man!

Said the Post Office to the mid-Twenties applicant for a transmitting permit (the term "licence" is a postwar one): "Convince us that you are engaged on a particular line of experiment that justifies the need to transmit and we will consider your

case".

Many and varied were the "experiments" dreamed up by young hopefuls like our correspondent-with-Mr Smith, but what can be said with some truth is that if you had a good "line" the Post Office would swallow it!

One one side of them were "the military", keen to hold on at all costs to the wavelengths ("frequency" was not yet in use) which they had occupied during World War One and the years following. On the other side sound broadcasting's claim for

space could be heard with increasing amplitude. Somewhere in the middle were the poor amateurs—the "licensed experimental stations". (For a time even the nation's quarter-million receiving stations were considered to be "experimental"!)

Climate of Caution

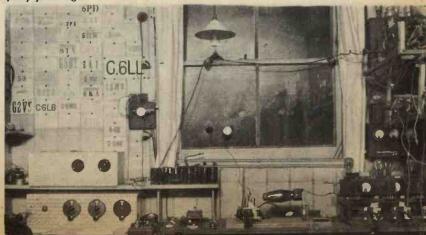
All in all, a climate of caution prevailed, created by the difficulty of seeing where the future of "wireless", developed immensely by war, truly lay. This caution was exhibited in a special degree as a phobia against "interference". Even the tranmitters of the British Broadcasting Company were under an obligation to close down at certain intervals lest they should jam "official" stations!

It was within this climate that young men in increasing numbers, fascinated by this quite new scientific thing, "the wireless", felt the desire to use it as a means to communicate with one another. It must be said to the credit of the Post Office of the time—and turbulent times they were, politically—that any young man who could show them that he took "wireless" seriously—that he had a convincing "line of experiment", generally with aerials, that justified permission to transmit—would be able to travel that far from royal road with a reasonable degree of hope.

Upon that confident note we could well leave the story of the young hopeful and Mr. Smith, were it not for the fact that one further phenomenon peculiar to the amateur radio world of the 'Twenties has not yet been described, and that is the "artificial aerial" transmitting permit. But this, and the overtones which it has produced in the amateur radio scene of today, must wait until next

time.

Mr James W. Mathews is one of the band of amateur radio pioneers who, though not professionally engaged in electronic engineering, made a considerable contribution towards the art of communication. Licensed in the Twenties, "G Six Double Ell", as he is generally known, opened up the 10 metre band at a time when its potentialities for world wide contacts were virtually unknown. In later years he was one of the first operators to use the 2 metre band when it was allocated to British amateurs after the war. Today in retirement in a Hertfordshire village, Mr Mathews continues to operate actively on several v.h.f. bands, with equipment very different in appearance from that shown in this picture taken of station 6LL when it was in Clapton, London, forty years ago.



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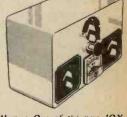
Tuning units are available to allow the system to be used for Medium Wave reception. Licensed amateurs all over the world are radiating excellent signals using the transmitting Joystick Systems and are also enjoying a considerable improvement in reception quality. In fact, the latest figures show that over 10,000 systems are now in use.

Hundreds and hundreds of enthusiastic testimonials are flowing into the Joystick office. These show that in particular users who have difficult locations, live in flats or EVEN IN A BASEMENT have experienced a remarkable increase in sensitivity and reception volume—many say they now hear signals that they did not know existed before they rigged up their Joystick System.

Patents have been applied for all over the world — and we recommend you to send for a brochure and full information immediately.

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WA2WOR/W4WFL, New York 23 says: 'Not only does the Joystick make it possible for me to operate on 160m. from my location in the centre of New York City, its performance on the higher frequencies is excellent; the Joystick is certainly the answer to the Antenna problem for apartment dwellers."



Above: One of the new JOY-MATCH|'EASY-TO-USE' units with the built-in RF indicator for transmission

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MARKET PLACE

Items mentioned in this feature are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned.

SAFETY FIRST

The first item this month is the Bulgin Security Alarm from A. F. Bulgin & Co. Ltd., Bye-pass Road, Barking, Essex, which provides protection to the average household at a reasonable cost of £12 17s 6d. The basic system, once installed as instructed, is very efficient and consists of six units: Latching Door Switch, having special one way operation; Keyswitch Control Box,



Security Alarm by Bulgin

which is the nerve centre of the system and keeps the bell ringing once activated; Battery Magazine; 4 in Underdome bell; Pressure Switch; and the system is completed by twin plastic coated wire, screws, tacks, keys and protective Door Striker Plates. There are many accessories available and seems well worth investigating.

A safety device of particular interest to the experimenter is the Rendar Safebloc available from DTV Group, 126, Hamilton Road, West Norwood, London, S.E.27 or by postfrom Guildford Mail Order, 6, Leapdale Road, Guildford, Surrey. This device provides a quick and safe method of securing 2-core or 3-core bare ended connecting wires to the

Another item which should be considered a must in the workshop or house is a fire extinguisher. The usual excuse for not having one is either that they are too expensive or too heavy, consequently not suitable



Rendar Safebloc mains connector

for the lady of the house. With the introduction of a new range of extinguishers from Firemaster Extinguishers Ltd., these arguments are no longer valid. Of the dry powder type, they are light, 2.2lb, powerful and easy to use and range from £2 19s 6d to £4 9s 6d. They are covered by a three year guarantee and there is a low cost replacement service for used extinguishers.

CONSTRUCTORS AIDS

A fairly new "electronic breadboard" that will appeal to the hobbyist is being marketed exclusively in the U.K. by Livingston Components Ltd., called the Develoboard it consists of a breadboard chassis assembly which employs solderless connectors, enabling transistor circuits to be made up rapidly and any circuit modifications can be made instantly—well almost.

Some time ago we used "Masterboxes" from Cockrobin Controls, in a series of constructional articles (issues now entirely out of print and unobtainable). These proved very successful in obtaining a good presentable finish. Now this firm is producing a series of four design sheets to help layout circuits and aid in choosing the best type of boxes to be used. Our photograph shows a model railway control panel which is a typical example of the type of unit that can be first laid out on these sheets.

Developoard marketed by Livingston



COMPONENTS

The basis of portable flash equipment for photography is the use of rechargeable low voltage batteries as a primary source of power with an electronic circuit charging a capacitor to a much higher voltage. Electrolytic capacitors are used because of their large capacitance for a given size coupled with low leakage currents, and to ensure proper charging after extended idling periods.

extended idling periods.

A specially designed capacitor for this application is the "Lectroflash" manufactured by TCC Division of Plessey and available from most good retailers. The capacitor is available with ratings from 200 µF to 1,750 µF. The discharge energy varies between 16 and 92 joules.

Whilst still on electronic flash guns we have in the past recommended Deac batteries. These batteries are now available direct from Deac (Great Britain) Ltd., Hermitage

Street, Crewkerne. Somerset.



Major 750 Firemaster extinguisher

A problem that seems to always confront us when building battery powered equipment is how best to mount the batteries? A spring clip mounted on one side of a cabinet is usually possible, but with equipment that is likely to be subjected to some form of vibration there is a tendency for the batteries to become dislodged. However, Bulgin are now producing a complete range of battery holders in various styles, base mounting, panel mounting, and types for fixing to chassis lugs. All have highly insulating moulded bodies, corrosion resisting metal tags and springs and reversed polarity prevention.

TOOLS

Three aids to wiring and soldering are the next components of interest. The first is a tool kit containing 18 tools in a neat zip fastened wallet.

The selection of tools include a 14mm magnifying mirror, a 30 watt soldering iron, a flexible screwdriver and a variety of miniature screwdrivers and tweezers. This kit is intended mainly for transistor circuits and is priced at 10 guineas from Henri Picard & Frère Ltd., 34/35, Furnival Street, London, E.C.4.

The second is a tweezer shaped in such a manner that it enables much steadier and positive use as indicated in the photograph. Available from J. A. C. Wilkinson Co., 5, Beeches Avenue, Carshalton, Surrey, this tweezer is known as the Rubis No. 5A, is Swiss made, and sells at 12s 9d for a standard carbon steel model and 14s 3d for a stainless steel version.

The third item is the well-known Model 8 wire-stripper from Multicore Solders Ltd., which cuts and strips most standard wires accurately. It



Henri Picard & Frère tool kit

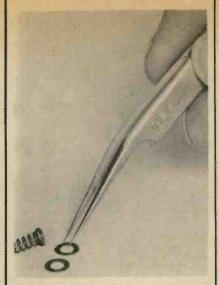
can be adjusted quickly to the wire thickness required by the special pre-set selector gauge, which is now conveniently marked at each setting with a letter for simple identification. At 8s 6d this seems to be a worthy addition for the tool box.

LITERATURE

Two of the most treasured items in our workshop have been the catalogues issued by Home Radio (Mitcham) Ltd., and Henry's Radio Ltd. The only trouble is that they keep disappearing and a frantic search follows until a voice casually mentions "Oh! I've got that, I borrowed it and took it home to do some research on a job I'm doing

There are quite a number of new items in the Home Radio Catalogue, price 7s 6d, which arrived in the office and has already disappeared

into the Editor's office.

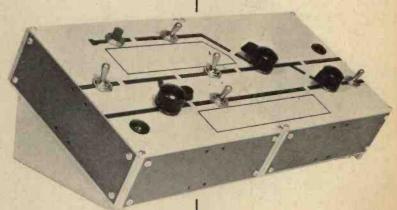


Rubis No. 5A tweezer

A third catalogue has just been added to the above list and we strongly recommend readers to obtain a copy for reference. It is part of a new service just started by Electroniques (Prop. STC Ltd.), Edinburgh Way, Harlow, Essex, specially for the home constructor and the smaller companies. The catalogue is called Electroniques Hobbies Manual and lists components and equipment from over 85 leading manufacturers. Priced 10s 6d it contains details of complete designs and kits, technical data, practical tips and formulae as well as the vast amount of stock parts required to construct electronic apparatus.

A new Brimar, Data List No. 33, valve booklet covering 542 valves and cathode ray tubes is available from Brimar Publicity Department, Thorn-AEI Radio Valves & Tubes Ltd., 7, Soho Square, London, W.1. No

price given.



Masterboxes Controls

from

Cockrobin

Model 8 wire-stripper from Multicore Solders



FINISHING TOUCH

How to finish off one's final project has always been a problem, particularly the front panel which either makes the equipment look professional or amateurish. With so many decorative plastics self-adhesive papers available (and not forgetting the well-known technique of rubbing an aluminium front panel with glasswool) the panel itself presents no real problem until you come to lettering the facia. This is where the trouble really starts, hand painting and labels are all right but do not really fulfil the requirements.

We have recently started using Letraset (Letraset Ltd., 195, Waterloo Road, London, S.E.1) instant lettering and find this is one of the best methods so far. The only drawback is that you have to lay the lettering on the panel before mounting any components. But provided the lettering is sprayed with Letracote protective coating it will withstand rough

handling and abrasion.

LAII these Constructional

CTRONICS

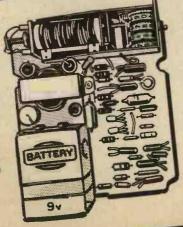
PROXIMITY DETECTOR



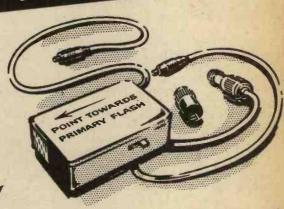
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Transistorised circuit drives a digital relay which displays the count from a halogen-quenched Geiger Muller tube. Suitable for determining the day-today change in cosmic radiation or for the accurate quantitative analysis of liquid samples.

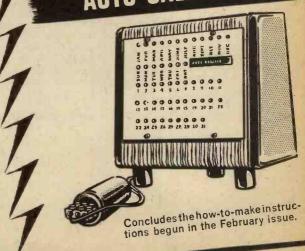


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REPEATER

by G.E. COUCHER

WILL probably seem obvious to the reader that, although the unit featured in this article was originally designed for the hard of hearing, it will find a use in most households with an inadequate bell system or while television is on.

The problem could be tackled in a variety of ways. A louder bell is the obvious solution, but this is often disturbing to the neighbours. The existing bell could be moved to the living room, but since this normally leads to confusion with bells included in the televised programme, it is not effective.

The alternative is a visual indicator displayed in a prominent position, but the practical difficulties are rather more formidable than would at first be expected.

Firstly, if a bulb is used, the illumination period is restricted to the time that the bell is ringing, and if the bulb is not noticed at once its effect is lost, so that the illumination must be sustained.

Secondly, many bell systems are powered by a.c. mains via a suitable transformer, which is unsuitable for any form of standard timing circuit.

TIME DELAY

Both these problems are overcome by the circuit described. Only the transistor circuit of the unit need te operated on d.c. The bulbs may be run off the low voltage a.c. used to supply the bell.

The whole idea of using a transformer to power the bell is to save the frequent purchase of batteries, and to use batteries in this particular application seems at first to defeat the purpose of the transformer. Any rectifying circuit would have to be on continuously and include electrolytic capacitors, which have a habit of breaking down after a few months continuous use.

To offset the disadvantage of using batteries, both the quiescent and running currents have been kept to a minimum, being 25-60µA (depending on ambient temperature) and 45mA respectively at 9 volts.

The timing factor uses a slightly modified version of the better known type of delay circuit. Potential dividers have been eliminated in the quiescent state, and the time constant is derived from the charge time of a capacitor rather than its discharge, thus there are no capacitors across the battery supply.

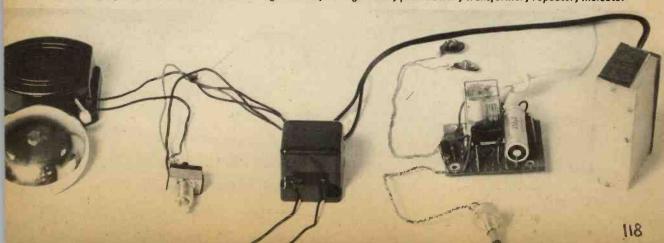
As can be seen in Fig. 1, a.c. is fed from the bell through D1; the consequent d.c. is smoothed by C2. This produces a few volts bias at the base of TR2, and switches it on operating the relay. The relay in the off position serves to "ground" the base of TR2 through R4, and TR1 through R3, thus keeping the quiescent current low. At the same time, it keeps C1 fully discharged. When the relay is operated RLA2 connects the indicator bulb across T1 secondary

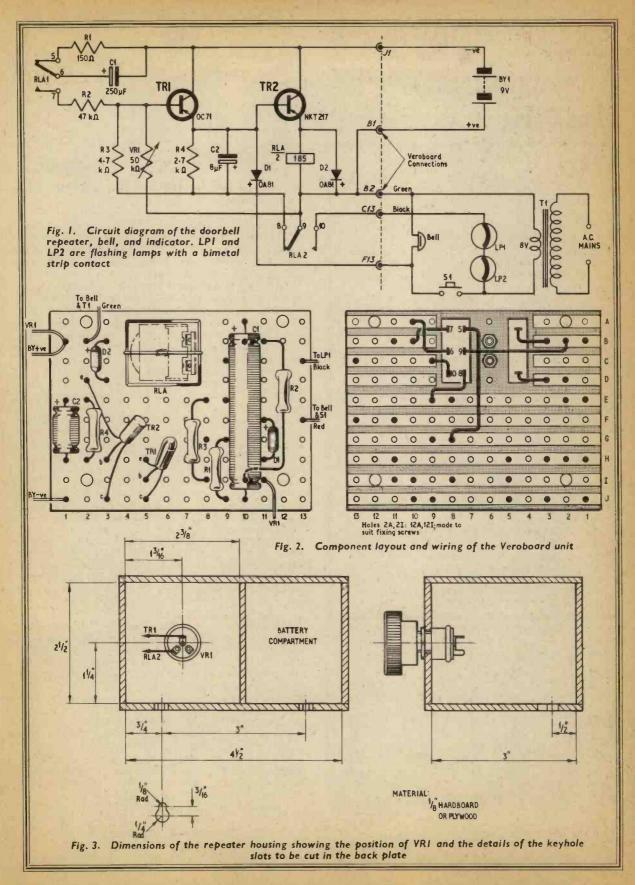
Contacts RLA1 connect C1 to the base of TR1 via R2. C1 charges through R2, VR1, and R3, and biases TR1 negative. TR1 conducts via the bell and D1 supplies a continuous negative bias to TR2, which sustains the relay. This condition continues until the charge of CI approaches a maximum when the bias at TR1 drops to a point where TR1 can no longer sustain TR2, and the relay drops out. C1 is then discharged by R1, and the transistors once more are "grounded"

The speed at which C1 charges is dependent on the setting of VR1, which may be adjusted to vary the time delay. If a short delay is required, a smaller value potentiometer should be used.

It is expected that one Ever Ready PP7 battery will operate this unit 1,800 times for a period of 2 minutes

Group photograph of the various units wired together. Left to right: bell, push button, transformer, repeater, indicator





per operation at 10 operations per day, or 3,600 operations using a PP9. It follows that this figure would be doubled at 1 minute periods.

Although the initial current is about 45mA at switch-on, this drops steadily to 4.5mA during illumina-

tion, at which point the relay drops out.

COMPONENTS . . .

Resistors R1 | 150Ω 1 R2 | $47k\Omega$ R3 | $4.7k\Omega$ R4 | $2.7k\Omega$ Potentiometer

VRI 50kΩ linear carbon

Capacitors
C1 250µF elect. 25V
C2 8µF elect. 15V

Transistors

TRI OC71 (Mullard) TR2 NKT217 (Newmarket)

Diodes
DI and D2 OA81 (Mullard)

Relay RLA 185 Ω with two sets of changeover contacts. Type MH2P with socket or type MH2 without socket (Keyswitch Relays)

Transformer
TI Primary 200-250V a.c.; Secondary 8V (Bell transformer)

BYI 9V (type PP7)

amps
LPI and LP2 6V 0.4A flashing bulbs (Pifco)

Switch
S1 Single-pole on/off push button
Miscellaneous

Veroboard 2 In × 2in, 0.15in hole matrix Electric bell 8V
Battery connectors, screws, wire Plywood for boxes (see diagrams)
M.E.S. batten lampholders (2 off)

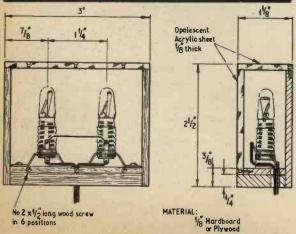
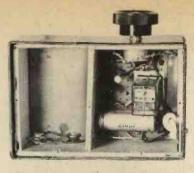
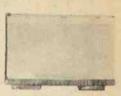


Fig. 4. Indicator lamps are haused in a small box with opalescent Perspex an two sides





The repeater unit and flashing indicator box. The battery has been removed

COMPONENTS

Veroboard construction is used for simplicity, and the device kept as small as possible. Layouts are shown in Figs. 2 and 3.

The relay is a plug-in type chosen for its high performance, clean action, and ease of replacement. If economy is important, an MH2 type may be used and directly mounted without a socket. If the socket is used, however, this should be ordered with the relay, and suitable holes should be cut in the Veroboard to accommodate it.

Supply voltage to the unit may be varied between 5-25V without serious deterioration of performance, but a high voltage is rather impractical in view of battery size.

None of the resistance values are critical, nor the capacitance of C2, as long as this is about 8μ F or more. Diodes D1 and D2 have a maximum current capacity of 150mA. This is important, as D1 has to supply about 40mA to the relay via the base-emitter junction of TR2 when the battery runs down. This switches the relay on and off twenty times per second, even without the battery supply and illuminates the bulb at half power. This automatically throws suspicion on the battery, and nothing else.

The indicators chosen were Pifco 6V flashing bulbs, which flash at a rate governed by a bimetal strip, situated near the filament. Because of their voltage rating, two must be used in series, but they are relatively inexpensive to run. The two may be displayed in the same room or in different parts of the house.

HOUSING

Size and appearance were borne in mind, since the unit will probably be mounted on a wall. Overall sizes of the two units are $3\frac{1}{4}$ in $\times 4\frac{3}{4}$ in $\times 2\frac{3}{4}$ in and 3 in $\times 2\frac{1}{2}$ in $\times 1\frac{1}{8}$ in. Two inverted "keyholes" were cut in the back of the large box for mounting on screws in the wall.

A partition 2\frac{1}{8} in wide made of plywood is used to separate the battery from the main assembly. A small gap is left between the base and partition to allow the battery leads access to the battery.

The Veroboard is secured to the base by four round-headed $\frac{1}{4}$ in screws, and pieces of plastics cable sleeving are used to space the board from the base. This prevents damage to the underneath wiring.

A hole should be cut in the side of the box to accommodate VR1 and another in the left-hand side for the connecting cable to pass through to the lamp unit. Blocks are eliminated, saving a great deal of space.

The whole unit is covered in decorative plastics laminate to give a pleasing appearance.



HI FI UNITS

Redesigned tuners and other transistorised units have been introduced by the Chapman Division of Derritron. Tuner model FM1000A, for f.m. only, is fitted with a stereo decoder and sells at £39 11s 3d when prepared for cabinet mounting. A shelf mounting version is obtainable and there is also an a.m./f.m. tuner type FM1005A for which outstanding signal-tonoise ratio and sensitivity are claimed. This latter model has entirely separate sections for a.m. and f.m.

Also new from Chapman is model 310 integrated stereo amplifier which, at £50, is supplied as a free standing unit in a wood case. Output rating is 10 watts per channel and there are the usual inputs for pick-ups (magnetic and crystal), radio tuners and tape recorders. The amplifier and control unit sections can be removed from the case if cabinet mounting is preferred.

Eagle products marketed by Adler (see Audio Trends, November) include a transistor stereo pre-amplifier which provides the extra stage of voltage amplification needed when a magnetic pick-up is used with an insufficiently sensitive amplifier. This little mains powered unit, type PRE302, costs £5 16s 6d. There is a mono version. Bookshelf speakers from this firm have a rosewood finish and are available in several sizes, the smallest of which is the MS40 (£8 10s 6d).

NEW SPEAKERS

A new bookshelf speaker by LNB of Loughborough is known as the Charnwood and sells at £21 16s 0d. The drive units are a Celestion h.f. radiator and an E.M.I. 13in by 8in elliptical for bass. This firm, well known for its small labyrinth enclosures has now restyled its Lab 8 model in a Mk3 version, which is priced at 14 guineas.

Nichols Acoustical Fitments, of Church Street, Bubwith, Yorks, offer a range of robust enclosures and supply drive units by leading makers. Advice is available on suitable combinations to meet individual needs. The Derwent Minster (£19) and Major (£15), the largest models, have characteristics which suit the Celestion 12in units. The Minor, at £11 10s, has a volume of 1.66cu ft and the Bookshelf (£5 5s) encloses 0.41cu ft.

Next a note for those who like to make a practical contribution to their speaker system. The Decca Kardioid, until now a ready-made speaker, has been introduced in kit form at 40 guineas. This is the system which incorporates the Kelly ribbon h.f. unit and an acoustical lens device. Also of interest is the revised Heathkit catalogue, now obtainable from Daystrom Ltd., Gloucester.

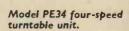
The Triaxiom 212c, a triple-element drive unit for high fidelity use, has been added to the Goodmans range. The basically similar 1220c, with a 20 watt rating, is already well established; the new version, rated at 15 watts and again of 12in diameter, costs £15 10s. This type of unit is essentially a twin-cone speaker with a horn loaded pressure tweeter mounted in the centre.

AUDIO FURNITURE

Model S33 speaker enclosure by Design Furniture Ltd. measures 27in by 16in by 12in and is intended for use with various well known drive units. It is available in walnut, teak or mahogany finishes. A new equipment cabinet, model EQC18, has features which were determined to some extent by the results of a design competition held some time ago. For details write to the firm at Calthorpe Manor, Banbury, Oxfordshire.

There are two additions to the already extensive catalogue of Scandinavian audio furniture, a speciality of Howland-West. The "Viking Standard", 39in by 19½in by 12in, is an equipment cabinet finished in teak with matt black contrasting sections. The Perspex turntable cover runs in grooves and can be pulled to one side. This model costs 20 guineas and the solid teak plinth is an extra 6 guineas.

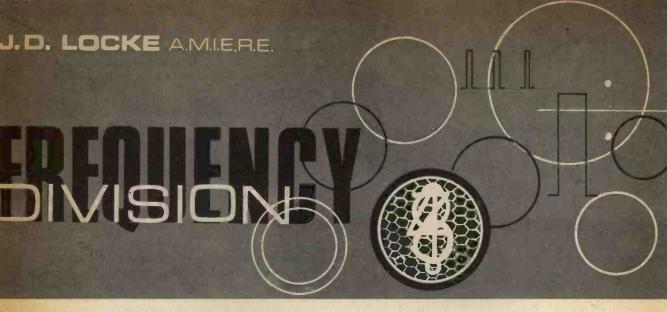
A similar "Major" model, 51in long, is priced at 24 guineas (plinth extra). The mounting board for the pick-up and turntable measures 19in by 18in. Model PE34 four-speed transcription turntable and arm, distributed in the U.K. by Howland-West, now retails at £30—considerably below the original price.





This firm is also importing Barzilay cabinet kits from the U.S.A. The imposing equipment consoles, substantial and built to luxury standards, are mostly expensive, but there are large (6cu ft) loudspeaker enclosures which sell at a little over £70 a pair. Hand finished, oiled walnut is standard for these cabinets.

A British firm making high class furniture of specialised type is Balmforth and Battye, The Forge, Marland, Rochdale. Elegant cabinets, made in two sizes, are supplied for practically any combination of hi fi units. A new venture is an efficient horn enclosure for Lowther PM6 or PM7 drive units. Priced at £22 the enclosure contains a folded horn of 9ft total length, but the external dimensions of the cabinet are quite moderate. The weight of this model, 56 pounds, gives an idea of the robust construction.



AST month, various pulse circuits for driving Dekatron clock counters were described. Here we go on to see how the divider circuits can be matched to a display.

NUMERICAL DISPLAY

There are two main types of numerical display: high voltage discharge tubes and low voltage incandescent lamp displays. In general, it is simpler to use the first group with decade counters and the second group with transistor counters and we will proceed on this assumption.

Now let us see what the display circuits of the clock have to do. We want a count of 0 to 9 and 0 to 5 to display the minutes and 1 to 12 to display the hours (or 0 to 23 on a 24-hour clock). Once again this means using frequency divider circuits. The only difference is that we want to know the state of the count at any instant.

Using binary circuits (the flip-flops already considered) there are two ways of doing this:

Method 1 (divide by 10 as an example)

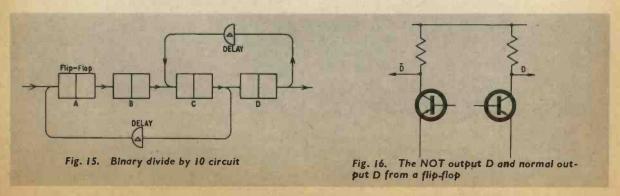
The binary divider shown in Fig. 15 divides by 10. A "truth table" is shown giving the output conditions of each divide by 2 circuit for each input pulse. A "0" signifies no output and a "1" signifies an output.

One has to be careful here; "0" output means that the output transistor is off, therefore the output voltage is highly negative; "1" output means that the output transistor is on therefore the output voltage is a very low negative voltage.

The conditions shown in this table must then be interpreted to light the appropriate number lamp; to light lamp 4 "A" must be on, "B" must be off, "C" must be on, and "D" must be off. This is expressed as $A \overline{B} C \overline{D}$. The bar over the B and D means "not B" and "not D". The "not" output is taken from the opposite transistor to that giving the normal output in the flip-flop. This is shown in Fig. 16.

Table I

Input Pulse	Output from					
Number	D	С	В	Α		
0	0	0	0	0		
1	. 0	0	0	1		
2	0	0	1	0		
2 3 4 5 6	0	0	1	-1		
4	0	1	0	1		
5	0	-	-1	0		
	0	-	- 1	-1		
7	1	1	0	1		
8	1	-	1	0		
9	- 1	-1	-1	1		



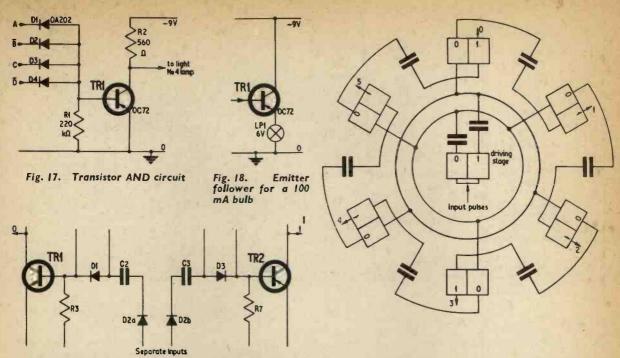


Fig. 20. Modified inputs (see Fig. 1) for the ring counter

Fig. 19. Ring counter for driving six lamps

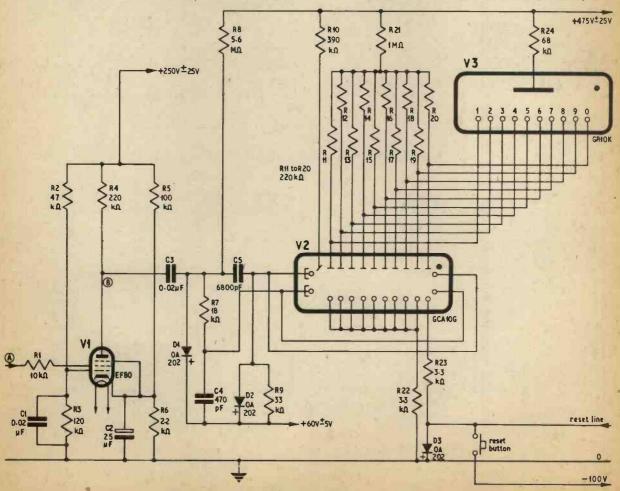
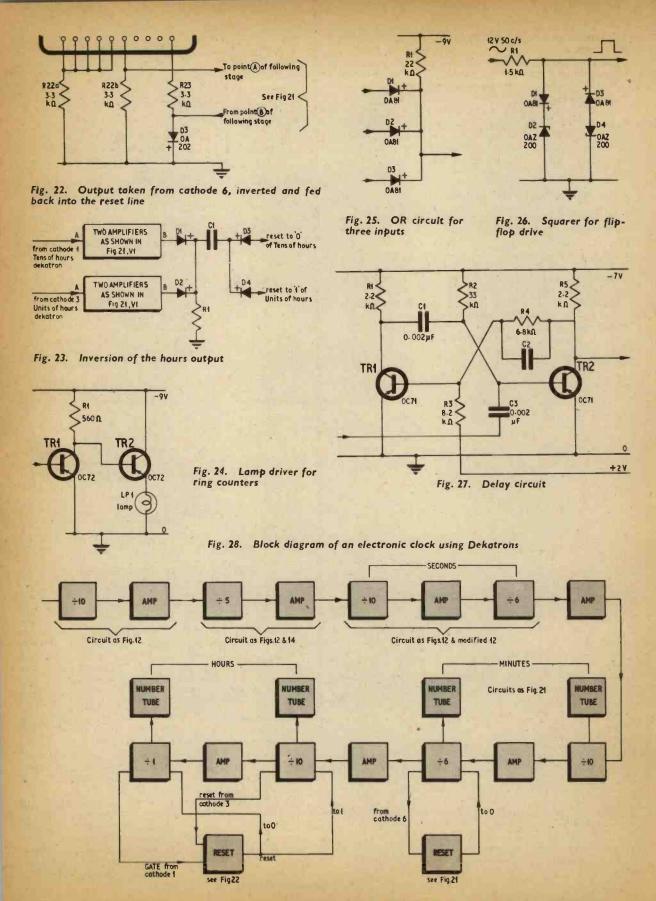


Fig. 21. Indicator drive stage using a Dekatron and Digitron



Having found which circuit conditions have to light the lamps, we have to find a circuit which will satisfy these conditions and also provide enough power to light the lamps. An AND circuit will do the first and an emitter follower will do the second. The AND circuit is shown in Fig. 17.

The transistor will be nearly cut off and its collector voltage will be high only if all the inputs are in the "1" condition. The output of the transistor is then fed to an emitter follower to give current amplification sufficient to drive a lamp (in this example 6V, 0.1A) (Fig.

RING COUNTER

The arrangement described above requires a large number of diodes, 112 for the AND circuits, but only 15 flip-flops for the display. There is an alternative method which uses more flip-flops but no extra diodes. This method is basically a ring counter made up of flip-flops, only one of which will be on for each lamp

An example of a ring counter, one for driving 6 lamps (0 to 5 for tens of minutes) is shown in Fig. 19. Notice that the inputs to all the outer flip-flops are split, i.e. separate inputs to each transistor. Thus the input to the circuit shown in Fig. 1 has to be modified as shown in the redrawn section, Fig. 20. The two outputs labelled "0" and "1" are the outputs from TR1 and TR2 respectively.

The operation of the ring counter is as follows: assume that stage 2 is on and all other stages are off. i.e. TR2 is in the "1" state and all the other stages are in the "0" state, including the driving stage.

The next input pulse switches the driving stage to "1". This feeds a pulse to the outer ring to drive all those connected to it to "0". The only stage to be affected is stage 2. This then produces an output from its "0" terminal which will switch on stage 3. The next input pulse switches the driving stage from "1" to "0", producing a pulse on the inner ring, which switches off stage 3 and in turn switches on stage 4. Once igain, a current amplifier is required to drive the

The final method of indicator drive is by using a Dekatron to drive a Digitron. This is shown in Fig. 21. This circuit is only suitable for counts from 0-9 and not for 0-5 and 1-12 as are also required for the clock display. For a count of 6, an output must be taken from cathode 6, inverted and fed on to the reset line,

as shown in Fig. 22.

In order to obtain a count of 12, a further stage is required. An output from cathode 1 of this extra stage is used to "gate" an input which is obtained from cathode 3 of the previous stage. The output of the gating circuit provides a reset pulse to reset the additional stage to "0" and the previous stage to "1". Thus as soon as the indicators try to go to 13 they are reset to read 01

Figs. 23 to 27 are supplementary circuits used in building up a complete clock such as shown in Fig. 28.

The circuits given will form a good basis for a clock but may need adjustments to get the best out of them.

Power supplies are not shown but are conventional and will be well within the compass of anyone attempting a project of this kind. It is stressed that the circuits given are only intended for guidance for the experimenter.

The estimated cost of the transistor version would be about £75, for the Dekatron version £25, excluding hardware.

Book reviews

RAPID SERVICING OF TRANSISTOR EQUIPMENT By Gordon J. King

Published by George Newnes Ltd. 151 pages, 8\frac{3}{2}\text{in.} \times 5\frac{1}{2}\text{in.} \text{ Price 30s}

A LTHOUGH this book is aimed primarily at first year students, service technicians, and enthusiastic amateurs, the author avoids the usual lengthy comparisons between valve and transistor circuits, thereby saving valuable space for a more direct treatment of up-to-date equipment. The emphasis, as the title suggests, is on fault finding, but there is a great deal of general information in the text to interest the casual reader.

The contents are as follows; transistor fundamentals, d.c. tests, signal condition testing, audio amplifiers with a disappointingly short section on video amplifiers, a good chapter on r.f. testing which includes u.h.f. tuners and boosters, tape bias/erase and other lowish frequency oscillators, radios, and a brief look at hi-fi amplifiers. Some of the circuit examples have component values and five fault diagnosis charts are provided. The concluding chapter, after a discussion of test equipment, becomes severely practical with printed circuit and soldering advice, and a list of "don'ts" for the unwary.

The index does little to help the reader, but clear paragraph headings will make a search for information more rapid than the time it takes to cure a fault. book is well produced on semi-glossy paper with a durable cover, and it contains photographs.

COMPUTER BASICS—INTRODUCTION TO **ANALOGUE COMPUTERS** Published by Foulsham-Sams

288 pages, $8\frac{3}{4}$ in $\times 5\frac{1}{2}$ in. Price 30s

HIS VOLUME, which is of U.S. Navy origin, is only the first of a series of five books and this may explain some otherwise inexplicable peculiarities. Certainly, it came as a slight shock to find a book, supposedly on computer design, which did not contain a single circuit diagram of any sort. Throughout the book the emphasis is almost exclusively on mechanical means of calculation with lengthy discussions on the wheel-anddisc integrator, differential gear systems, the cam, and related devices. Apart from the occasional mention of electrical-mechanical analogies the subject of electronic calculation is left untouched. In fairness, though, it would seem that this deficiency is at least partly corrected in Book 2, the contents of which include a chapter on electronic calculating devices.

In addition to the descriptions of purely mechanical calculators there are chapters on basic and advanced computer mathematics which in some places become

very advanced indeed.

By itself this book is of little value to those wishing to learn about the principles of electronic analogue computers, although coupled with Book 2 it would probably be appreciably better. On the other hand for anyone wishing to investigate the properties and capabilities of mechanical analogue devices it should be of considerable use and can be recommended.

ST.A.



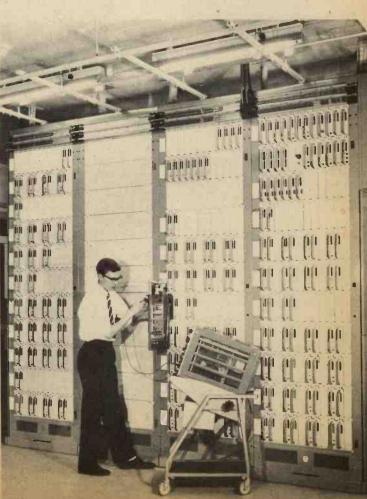
cuitry, reducing both capital and operating costs. Electronic Exchange in Service

THE first production electronic telephone exchange, Pentex TXE 2, was brought into public service on December 15 at Ambergate, Derbyshire, by the Postmaster-General. This new system relies on reed relay switches instead of the conventional types. It vastly cheapens relay production and improves reliability. However, this lower cost is offset by using sophisticated pulse circuitry which gives higher speed line location.

Dialled digits are stored until the final digit is registered, then the complete code finds the required line in 50 milliseconds. Faults are detected automatically and the exchange finds another path and prints out the fault on paper tage for servicing engineers.

paper tape for servicing engineers. It is possible in electronic PABX installations that the caller can dial direct into the required extension. Although Ambergate carries only about 900 lines at present, a "large" exchange version (more than 2,000 lines) is expected to be ready later this year.

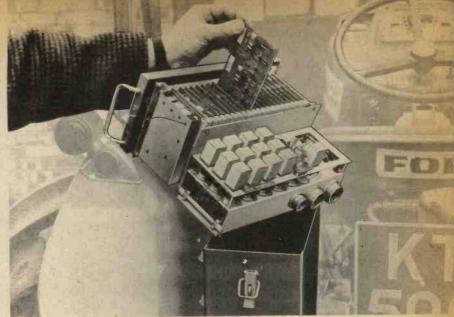
The equipment is built by Ericsson Telephones, one of the Plessey Group of Companies, to Post Office specification.

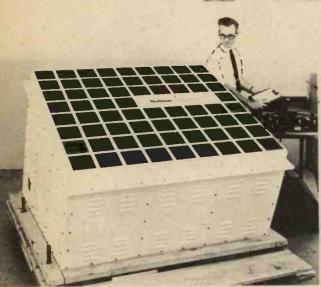


Ghost Tractor

New development in farming in this country is this remote control farm tractor. The unit here has been lifted out of its housing on the back of a tractor to show a 28-channel digital receiver built up on plug-in Veroboards.

Information is transmitted in binary code by on/off bursts of carrier. A memory store retains any required operation in the "on" or "off" state until a "change" signal is received. The electronic control system is the work of C. & L. Developments of Weybridge in conjunction with the Ford Motor Company.





Solar Cell Television

THE FIRST sun powered television translator to cover areas where a signal is weak or non-existent is being installed in Jamaica. It is designed by T.I.E. (Communications) Limited using components manufactured by Hoffman Electronics Corporation, Marconi Company Limited, and Nife Limited.

The first installation has been deliberately located in an accessible area so that data from its operation can be easily received and evaluated. Subsequent installations will tend to be in remote areas, where mains electricity does not exist and where the provision of fuel and maintenance for engines is both difficult and expensive.

The Jamaica installation, opened in December, demonstrated for the first time that a television picture can be made available for some eight hours a day, or more, relying

on sunlight as the only source of power.

Missile Use Teleprinters

A Row of advanced communications equipment bearing a resemblance to a line of slot machines are seen here at the Aerojet-General plant in California. The devices are actually teleprinters awaiting assembly into flight communication systems for installation at U.S. Air Force Minuteman ballistic missile launch sites.







Classic

Origin

WHEN in 1940 the new R1155 receiver (with its companion T1154 transmitter) was released in small numbers to units of the R.A.F., its advent was greeted with surprise delight by signals personnel, for nothing quite like this had been seen (or heard) before. Offering one-knob operation allied to high performance, it brought about a revolution in the technique of air to ground communication, hitherto performed largely with the TR1082/1083 combination that used a t.r.f. receiver with adjustable reaction and 2 volt battery valves!

In later years the R1155 came under the shadow of receivers more recently developed and offering such improved facilities as greater audio output and a crystal filter. This situation, although depressing the post war selling price of the R1155, has added to the attractiveness of the receiver to persons desiring to embark on short wave reception at minimum cost.

Like most classic communication receivers the R1155 went through many "marks" of which the most important from the private listener's point of view is the R1155N, a variety introduced for air to surface vessel communication. Because this version covers the 160 metre amateur band it generally fetches a pound or two more than other varieties. On the "N" version the four most populated amateur bands occur, namely, 1.8Mc/s, 3.5Mc/s, 7Mc/s and 14Mc/s. For the 21 and 28Mc/s bands an external converter(s) would be needed, as also for the v.h.f. bands (see important note under "Modifications" below).

Basic Circuit

One r.f. amplifier	VR100	(KTW63)
Mixer	VR99	(X65)
Two i.f. amplifiers, both	VR100	(KTW63)
Beat oscillator and a.g.c. diode		(DL63) '
Demodulator and audio amplifier	VR101	(DL63)
Tuning indicator	V1103	(Y61)

COMMENT: If the R1155 is purchased unmodified three valves additional to the above will be found on the chassis. These are associated with the direction

finding facility and have little or no value for amateur band reception. Their removal provides enough space for a small transistorised v.h.f. converter to be installed, or a 100kc/s calibration oscillator. Although all valves are conveniently 6·3 volt types it is well to check through all heater lines to ensure that none are in series-parallel modes.

Waveranges Covered

(Standard version) 75kc/s to 200kc/s. 200kc/s to 500kc/s. 600kc/s to 1,500kc/s. 3,000kc/s to 7,500kc/s. 7,500kc/s to 18,500kc/s.

Intermediate Frequency

560kc/s (It will be noted that a gap has been left for the i.f. in the above tuning ranges).

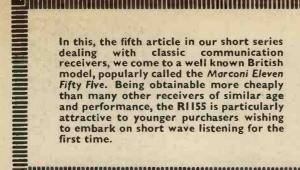
Power Requirements

A small power unit delivering 60mA at 220 volts and 2.5A at 6.3 volts will be adequate if the receiver is used "as is" but with the three D/F valves removed. If an output stage is added for loudspeaker operation the power requirements will rise to about 3A l.t. and 100mA h.t.

SPECIAL NOTE: The h.t. negative rail of the R1155 is not at chassis level, a biasing resistor being interposed. A separate h.t. negative point is on the 8-way power input plug on the front panel and any power unit used externally should be connected to this.

Controls

It is the big crescent shaped tuning scale that gives the R1155 its immediate recognizability. All bands are visible at a glance, and the big pointer may be set at once with a direct drive knob to the area it is desired to tune. A second concentric knob gives slow motion tuning of that area. For quick frequency setting this receiver has advantages over certain other subsequent sets in which laborious winding of the tuning knob is necessary to reach a desired frequency area.



Readers acquiring this model are recommended once again, as in previous articles in this series, to obtain at the time of purchase at least a circuit diagram together with as much other technical literature about the receiver which the vendor is able to provide.

It should be noted that handbooks for receivers featured in this series are often

available from advertisers.

COMMUNICATION RECEIVERS

COMMENT: Unfortunately, the amateur bands, which will be the main preoccupation of most users of the R1155, are rather cramped and can be passed over with only a few turns of the slow motion drive. There is certainly a case for utilising external converters for all bands except "160" and "80", and using the set solely as an i.f. strip to give improved bandspreading. And because "160" occurs only on the R1155N an external converter for that band, too, may be worth considering.

Apart from the tuning control and wavechange switch, the only other controls requiring attention are the volume control, the b.f.o. pitch control (a trimmer just above the main scale), the master switch bottom right, which selects a number of functional operations, of which only the "AGC ON" and "AGC OFF" are of importance to the amateur user, and the audio filter, bottom left.

Recommended Basic Modifications

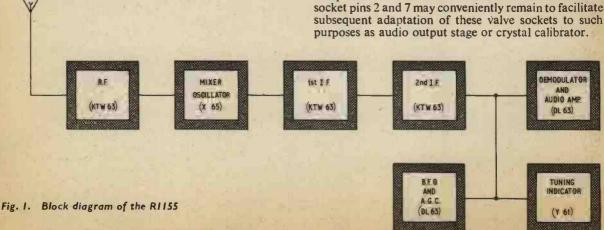
Additional Audio: In its airborne applications the R1155 was required only to feed aircrews' headphones. If a 6V6 output stage is built into the case to furnish high level audio it can conveniently occupy one of the redundant D/F valve sockets, suitably rewired.

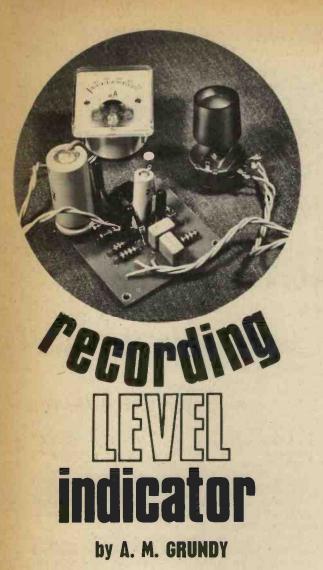
Aerial Input: In Service applications pin 2 received a long wave aerial, and may be ignored. For short wave reception pin 1 of the front panel 8-way socket is the correct one to use. If external converters are to be employed it will be desirable to trace back the lead from pin 1 to its tapping on the r.f. stage grid input coil, and to substitute for it a length of 80 ohm coaxial cable brought to a panel mounting coaxial socket on the front. Only by this means will it be possible to minimise i.f. breakthrough caused by reception on the receiver's main tuning range.

Mute Switch: It is desirable to fit a toggle switch on the front panel to cut the h.t. positive line; or if the set is to be used alongside a transmitter a small relay can be fitted inside the case, arranged for the contacts to be closed to apply h.t. during receive periods.

Separating the Gain Controls: Many users like to do this in order to facilitate reception of single sideband The existing ganged r.f. and a.f. controls can be readily separated; or one of them put out of commission, its leads wired to a new gain control of like value mounted on the front panel.

Redundant D/F Valves: If these and their associated components are removed the heater connections to socket pins 2 and 7 may conveniently remain to facilitate subsequent adaptation of these valve sockets to such purposes as audio output stage or crystal calibrator.





A LTHOUGH recording level meters are standard equipment on some of the more expensive tape recorders, many cheaper, and older recorders still use the magic eye to perform this function. It is true with some older machines that after long periods of use, the "eye" suffers from low emission and becomes dull.

Peering at the small segments of, for example, an EM34 can be rather trying and one longs for the clear indication of a meter. A meter is useful for giving reference levels of the matter to be recorded. The unit described here is a simple circuit for fitting in any tape recorder.

CIRCUIT

The circuit diagram is shown in Fig. 1. The first stage is an emitter follower, to give the unit a high input impedance so that it will not in any way affect the recorder circuit with which it is used.

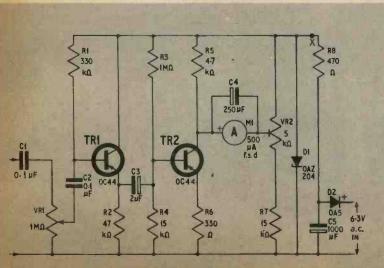
The second stage is, at first sight, an ordinary common emitter amplifier. Closer inspection reveals that R3, the base bias resistor, is of a high value, 1 megohm. This means that TR2 is only just conducting; the base-emitter junction is acting as a diode, rectifying the a.c. input from TR1 and giving a d.c. output at TR2 collector.

Zero drift is slight, and may only be caused by changes in ambient temperature, as the voltage is stabilised by the Zener diode D1. However, a "setzero" control, VR2, is supplied to make any adjustment to the zero calibration if this becomes necessary.

The time constant of the meter is the time t taken for the meter to fall to 0.37 of its initial value, as shown in Fig. 2, and is dependent on the value of the internal resistance of the meter $R_{\rm m}$ and C_4 . The relationship is given by the formula $t = C_4 R_{\rm m}/10^6$ seconds, where $R_{\rm m}$ is in ohms, and C_4 is in microfarads.

Using a typical 500μ A movement, with an internal resistance of 500 ohms, and C_4 at 250μ F, the time constant is 0.125 seconds (nominal). The tolerance of the meter and the capacitor will modify this slightly.

It was found that this value was the most satisfactory, as it gave indication of sharp music transients, without flicker at low frequencies. Other designs investigated



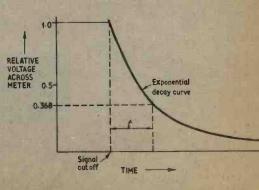


Fig. 1. Circuit diagram of the recording level indicator

Fig. 2. Time constant characteristic of the meter

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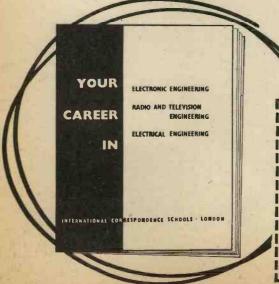
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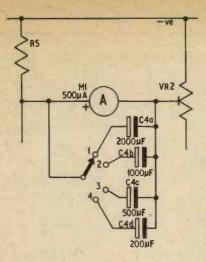


Fig. 3. A pre-selected switching arrangement providing four different time constants. Table I

by the author had much larger time constants. If this is found desirable the value of C4 can be modified to suit. Table I gives values of C4 for some different values of t, for a 500 ohm meter.

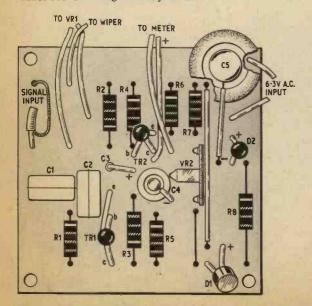
Ta	able I.	Rn	1 = 5	00 ohn	ns	
t (sec.) C ₄ (μF)	0·1 200			0·75 1500		

If a meter of different resistance is to be used, or if t is not covered by Table 1, the value of C4 may be calculated by the formula,

$$C_4 = \frac{10^6 t}{R_{\rm m}} \, \mu \text{F}$$

 $C_4 = \frac{10^6 t}{R_{\rm m}} \, \mu {\rm F}$ where t is in seconds and $R_{\rm m}$ is in ohms.

Fig. 3 shows a method of wiring in a selection of values for C4 using a rotary switch.



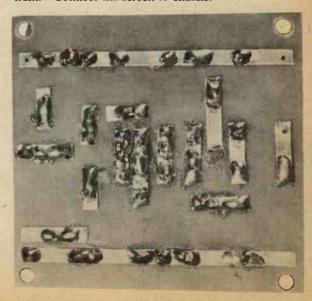
Component layout on s.r.b.p with connections to Fig. 4a. the input, VRI, and 6.3V a.c. supply

Components . . .

$\begin{array}{cccccccccccccccccccccccccccccccccccc$
Potentiometer VRI IM Ω log. carbon VR2 5k Ω linear, preset carbon skeleton
Capacitors C1 $0.1\mu\text{F}$ polyester 250V C2 $0.1\mu\text{F}$ polyester 250V C3 $2\mu\text{F}$ elect. 15V C4 $250\mu\text{F}$ elect. 6V (see text) C5 $1000\mu\text{F}$ elect. 15V
Transistors TRI, TR2 OC44 (2 off) (Mullard)
Diodes DI OAZ204 (6-2V Zener) (Mullard) D2 OA5 or OA10 (see text)
Meter MI 500μA moving coil
Miscellaneous Cir-kit adhesive copper kit (see page 96) Screened cable for input P.V.C. wire

CONNECTING TO THE RECORDER

The take-off point from the recorder to the unit can be the grid tag of the magic eye valveholder but, if preferred, it can be the anode or grid of the output valve which feeds the recording head. Screened wire is recommended to avoid misleading readings due to hum. Connect the screen to chassis.



Cir-kit is stuck to the underside in strips to give Fig. 4b. the required connections between components

The unit has a high input impedance and plenty of sensitivity (0.6V minimum for f.s.d.). If the signal is taken from the anode, a setting of only a quarter of f.s.d. is needed. The frequency response is substantially

flat from 10c/s to above 50kc/s.

Power for the meter circuit can be obtained from a simple half-wave rectifier, which is run off the 6.3V a.c. heater line. The voltage is stabilised by D1, a Zener, to avoid mains voltage variations affecting the sensitivity. Alternatively, the unit may be powered from a 6V battery, such as PP1 or four-pen cells. The life of a battery will almost equal its shelf life, since the current drain is only about 2mA.

Diode D2 is given in the components list as an OA5 or OA10; however, the base-emitter or the base-collector junctions of a transistor such as an OC72 may be used,

the base being the cathode.

CONSTRUCTION

Having located suitable signal, earth and heater take-off points (a circuit diagram of the recorder is useful here), if a continental D.I.N. pattern 3 or 5 way socket can be added to the recorder, then the level meter may be connected via twin screened microphone cable. The prototype was finally fitted into the recorder, but any suitable case will suffice.

The circuit was built up using the Cir-kit technique (see page 96); the layout diagrams are shown in Fig. 4.

SETTING UP

Having connected up the unit to the recorder, set VR1 to the earthy end of its track, and VR2 to the negative end of its track. Switch on the recorder and check the voltage on the negative line (point X on Fig. 1). This should read about 6V. The meter M1 should read around 100 to 150, providing VR2 is set in the above condition.

Adjust the set zero control VR2 to bring the pointer to zero and then set the recorder controls to "record". Inject, at the recorder input, an audio tone of about 400c/s from a signal generator, being careful not to overload the pre-amplifier stage, and adjust the recording level control, so that the vanes on the magic eye indicate maximum signal level. Then adjust VR1, so that M1 reads 400.

On normal recordings of speech and music the needle should not rise above this. If desired, a red line may be painted on the meter scale at 400, to indicate the

The instrument could be used as the basis of an a.c. millivoltmeter.

— INDEX -

An index for Practical Electronics volume two (January 1966 to December 1966) is now available price Is 6d inclusive of postage.

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Meetings . . .

INSTITUTION OF ELECTRICAL AND **ELECTRONICS TECHNICIAN ENGINEERS**

LONDON

Date: January 16

Title: Semiconductors for Power

K. G. King, D.F.H., C.Eng., M.I.E.E. Time:

Address: I.E.E. Lecture Theatre, Savoy Place,

London, W.C.2.

BRISTOL

Date: January 31

The Future of Telecommunications Title:

D. A. Barron, C.B.E., M.Sc., C.Eng.,

F.I.E.E. 7.45 p.m. Time:

Address: Large Conference Room, Council House,

Bristol.

SOCIETY OF ELECTRONIC AND RADIO **TECHNICIANS**

BIRMINGHAM

Time:

Date: January 17

Title: Post Office Tower, London

K. J. Lonnon 7.15 p.m.

Address: University of Aston in Birmingham,

Gosta Green, Birmingham, 4.

INSTITUTION OF ELECTRONIC AND RADIO **ENGINEERS**

LONDON

Date: January 17

Title: Symposium on "Radio Microphones"

M. L. Gayford, G. R. Pontzen and R. W.

Swain

Time: 6 p.m.

Address: London School of Hygiene & Tropical Medicine, Keppel Street, Gower Street, London, W.C.1.

HORNCHURCH

Time:

Date: January 26

Some Applications of Electronics Title:

Oceanography A. M. East 6.30 p.m.

College of Further Education, Ardleigh Address:

Green Road, Hornchurch.

SOUTHAMPTON

Date: January 17

Colour Television, S. M. Edwardson Title:

Time: 6.30 p.m.

Address: Theatre, of Lanchester University

Southampton.

(Sponsored by the I.E.R.E. and I.E.E.)

STAFFORD

Date: January 17

Title: Electronic Exchanges, E. S. Grundy

Time: 7.15 p.m.

Address: Stafford College of Further Education,

Tenterbanks.

IOINT MEETING

Date: January 31

Colloquium on "Adaptive Control For Title:

Aircraft" 2.30 p.m.

Address: I.E.E., Savoy Place, London, W.C.2.
This is a joint conference sponsored by I.E.R.E., R.Ae.S. and I.E.E. Tickets are available from I.E.E., Savoy Place, London, W.C.2.



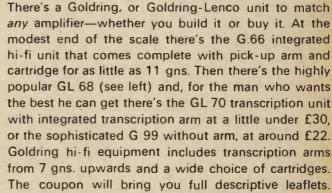
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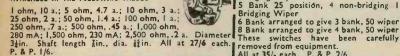
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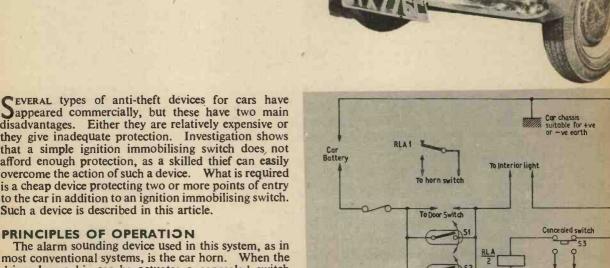


Fig. 1. Complete circuit diagram of the mercury switch (SI and S2) alarm system

disadvantages. Either they are relatively expensive or they give inadequate protection. Investigation shows that a simple ignition immobilising switch does not afford enough protection, as a skilled thief can easily overcome the action of such a device. What is required is a cheap device protecting two or more points of entry to the car in addition to an ignition immobilising switch. Such a device is described in this article.

most conventional systems, is the car horn. When the driver leaves his car he actuates a concealed switch outside the car, which engages the alarm system. The alarm can be set off in several ways, as detailed below:

(a) If the thief forces open a window this tilts the car sufficiently to actuate one of several criticallyplaced mercury switches.

(b) If a skeleton key is used to open any door, the interior light switch closes and sets off the alarm. (c) If the car is disturbed in any way (i.e. in a hit-

and-run accident) the alarm is set off.

Any attempts to stop the alarm by getting out of the car or closing the door will be foiled by the action of a set of hold-on relay contacts in the system. The only disadvantage of this system may appear to occur if the car is parked on a hill. In practice, however, this does not arise, as the mercury switches are arranged in such a way that they are actuated only by sideways movement, as a car is rarely parked broadside on to a slope.

CIRCUIT DESCRIPTION

The only components used in the system are two or three mercury switches as required, a two-pole changeover relay, and a concealed switch of suitable type.

The circuit diagram is shown in Fig. 1, and the system operates as follows. When the car is left and the concealed switch S3 is actuated, the coil of the relay RLA is effectively connected, in series with the interior light (door) switch, across the car battery. The mercury switches S2, S3 etc. shunt the interior light switch, and to make the system completely foolproof a normally open relay contact (RLA2) is also connected in parallel with these switches. The mercury switches are normally "open", as is the interior light switch when the door is closed.

If the concealed switch S3 has a double-throw changeover contact, the open contacts can be connected in series with the ignition lead to the key switch on the dashboard. This effectively immobilises the vehicle when the alarm system is engaged, and makes the system even more satisfactory in operation.

To Ignition.switch

RLA shown in de-energised condition.

One advantage of this system is that it uses no current whatsoever unless the alarm is actually operating.

When the alarm has been set off, the only way it can be silenced is by operation of the concealed switch S3, due to the action of the hold-on relay contact RLA2.

CONSTRUCTION

It is recommended that the alarm unit is built in a reasonably sturdy metal box secured in the engine compartment of the car. The box will house the relay and one mercury switch. Most electrical connections can be made here, with the possible exception of the horn switch contacts and, of course, the interior light lead. The connections to and from the unit can be made via an octal plug and socket with a suitable cable harness. If several mercury switches are required, these can be fitted outside the box and connected via the cable harness. The box will then function more or less as a convenient junction box for all the leads.

SETTING-UP PROCEDURE

The mercury switches (which can be obtained quite cheaply on the surplus market) are best mounted in Terry clips. The switches should be fitted across the car so that they are almost making contact under normal conditions. When the car is rolled, they will then operate. If, however, roads with a steep camber cause

COMPONENTS . . .

Switches

- S1, S2 (etc.) Miniature mercury switches
- S3 Double-pole, changeover switch, or as described in text

Relay

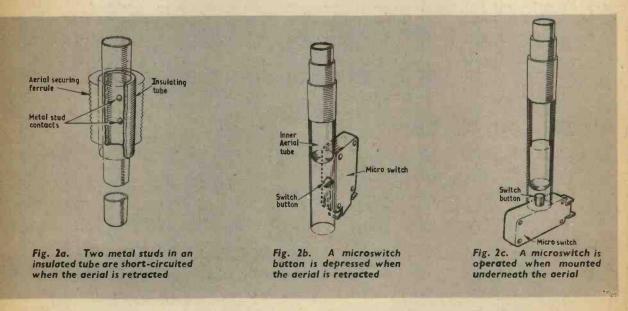
RLA Relay, 12V coil; 2 pole changeover contacts

Miscellaneous

Suitable metal box, e.g. 6in × 4in × $2\frac{1}{2}$ in aluminium chassis with top plate. Octal plug and socket. Terry clips.

cannot be confused. A very ingenious type of switch will now be described, based upon a car radio aerial.

Certain types of fully-retractable car radio aerials have non-metallic tubes into which the aerial collapses. As the car radio (if fitted) will not be used with the aerial retracted, it is a simple matter to arrange a pair of contacts which close when the aerial is fully retracted.



problems, the mercury switches may be mounted longitudinally at the expense of being unable to use the alarm when parked on steep hills.

An alternative system is to attach the mercury switch to the inside of the boot lid, to protect this in the event of a break-in. In this case there is less likelihood of a slight disturbance setting off the alarm accidentally. This setting-up is rather critical and may take a few minutes to achieve the optimum setting.

THE CONCEALED SWITCH

Any form of switch can be used for S4, but it is advisable to use a type in which the on and off positions

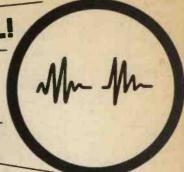
A number of systems of this type are shown in Fig. 2.

With such a system, the driver, when he leaves his car, simply retracts the aerial, thus engaging the system. Before re-entering the vehicle heraises the aerial with the special key which is supplied with such aerials. There is no reason why an aerial should not be used as a switch even if a car radio is not used, as few car thieves would suspect an aerial (especially retracted) of concealing the master switch of a highly efficient burglar alarm system.

This "aerial type" of switch is of course a simple single pole on/off device, and no provision can be made for connecting up to the ignition circuit in this case.



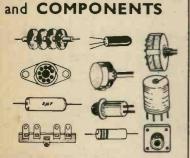
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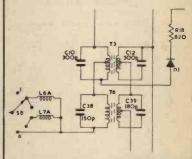
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Silicon Planar TRANSISTORS

by G. Wareham

SILICON planar transistors are now becoming almost as cheap as germanium transistors. They are extremely versatile. The same type is often useful for both audio and radio frequency applications. But these new maids-of-all-work do differ in certain respects from the more familiar germanium transistors, and to get the best out of them these differences must be taken into account. This article is a brief guide to practical applications.

MANUFACTURING TECHNIQUES

Silicon planar transistors are made by techniques in which the flat, polished surface of a silicon "chip" is treated so that selected areas are modified to produce the base, emitter, and collector. In the transistor factory, the percentage of "good" transistors (the yield) is high, partly because the fabrication techniques are more precise than the old fashioned alloying process, and partly because the surface of the silicon is protected, during and after manufacture, by a layer of silicon oxide.

This layer gives the transistor such good protection against chemical attack that it is possible for most purposes to dispense with the usual vacuum-tight hermetically sealed encapsulation and simply embed the transistor in synthetic resin. This, again, makes for cheapness, and so we find that, despite the fact that transistor-grade silicon is extremely expensive, these "epoxy transistors" can still be sold for a few shillings each.

WORKING CONDITIONS

A glance at the collector characteristics (see Fig. 1) of a typical silicon planar transistor shows nothing which differs substantially from the familiar germanium transistor characteristics. A closer look shows that one curve is apparently absent: the curve for $I_B = 0$. The reason is simple: a germanium transistor with no base current still passes enough collector current to show up on the curves, because of internal leakage. But in silicon transistors the leakage is so small that the curve for $I_B = 0$ virtually coincides with the X axis, until a certain critical collector voltage is reached. Then, as the curves show, the collector current tends to rise indefinitely. A sharp rise of collector current takes place for other values of I_B . This tendency to pass large collector currents at large collector voltages is obviously not healthy for the transistor and the only thing to do is avoid high collector voltages.

A good rule of thumb is: do not work the transistor at more than half the absolute maximum voltage quoted in the manufacturer's data. Thus a transistor with V_{CE} max = 18V will generally be all right at a battery voltage of 9V. The important exception is when the load is inductive. In this case, if the transistor is cut off abruptly, the collector voltage may rise far above the battery voltage. The situation is familiar to people who use transistors to operate relays, and the usual remedy is to connect a diode across the relay, so that it conducts and short-circuits the high-voltage "spike" which occurs on switch-off.

(There is nothing peculiar to silicon transistors here. Germanium transistors behave in the same way. But it is worth making the point again.)

EMITTER-BASE VOLTAGE

The curves of Fig. 1 do not show the one circuit voltage which is quite different from the corresponding one in germanium transistors. This is the base-emitter voltage $V_{\rm BE}$ which exists when the transistor is passing a given collector current. It is much bigger (0.5-1V) in silicon than in germanium transistors (0.1-0.3V).

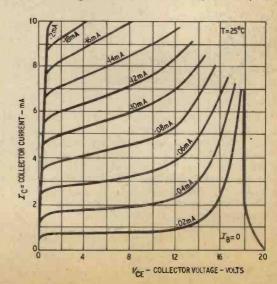


Fig. 1. Characteristic curves of typical silicon planar transistor

This has two practical results. One, not usually important, is that silicon transistors will not work from quite such low voltages as germanium ones, since there must always be enough voltage to provide the working $V_{\rm BE}$, and this means, say, 0.6V minimum, whereas many germanium transistors will work with lower

voltages than this.

However, the high $V_{\rm BE}$ can be turned to good advantage, and this is the second and more important result. A particularly simple and effective biasing system is possible with silicon transistors. This is shown in Fig. 2. Two resistors $R_{\rm f}$ and $R_{\rm b}$ form a potential divider across the collector-emitter circuit. Their values are selected so that the required $V_{\rm BE}$ is set up across $R_{\rm b}$. A method of calculating the required values is shown on the diagram, but readers might be interested to know the reasoning behind it.

The important thing is that the bias resistors should not shunt the base input impedance of the transistor too heavily, and so cause a loss of input-signal current, but, on the other hand, they should stabilise the working conditions against variations in temperature and transistors. The first condition—not to shunt the input—calls for high values of R_b and R_f and the second—good stabilisation—for low values. These conditions are incompatible, and the system seems a bad one, until one takes some actual examples.

The d.c. or large-signal input resistance of the transistor is simply $V_{\rm BE}/I_{\rm B}=R_{\rm IN}$. The a.c. or small-signal input resistance is 25 $h_{\rm te}/I_{\rm E}=r_{\rm in}$. Now, $I_{\rm B}=I_{\rm C}/h_{\rm FE}$, where $h_{\rm FE}$ is the large signal current amplification factor, so $R_{\rm IN}=V_{\rm BE}$ $h_{\rm FE}/I_{\rm C}$. Taking the ratio of small-signal to large-signal input resistances we have:

$$\frac{r_{\rm in}}{R_{\rm IN}} = \frac{25h_{\rm fe}}{I_{\rm E}} \times \frac{I_{\rm C}}{V_{\rm BE} \cdot h_{\rm FE}}$$
 (mA, mV)

Now, if $h_{\rm FE}$ is large, $I_{\rm C}$ is very nearly equal to $I_{\rm E}$. Also, under typical operating conditions, $h_{\rm fe}$ and $h_{\rm FE}$ are about equal. In this case,

$$\frac{r_{\rm in}}{R_{\rm IN}} \approx \frac{25}{V_{\rm BE}}$$

In a typical planar transistor used in the type of circuit in question, $V_{\rm BE}$ is not likely to be very different from 625mV, and so

$$\frac{r_{\rm in}}{R_{\rm IN}} \approx \frac{1}{25}$$

The a.c. input resistance is only 4 per cent of the d.c. resistance. Thus a bias network which shunts the d.c. input resistance heavily does not necessarily shunt the a.c. input signal heavily. This is precisely what we want for good stabilisation combined with small signalloss. A satisfactory compromise is to make R_B five times the a.c. input resistance. It is then typically one-fifth of the d.c. input resistance. In a germanium transistor, with $V_{\rm BE} = 150 {\rm mV}$, the ratio $r_{\rm in}/R_{\rm IN}$ would have been 1/6 and the best compromise factor $\sqrt{6} = 2.5$.

Bias circuits designed by this technique have the effect of compensating for the effects of differences in the gains of transistors on the working point. By calculating R_C , R_F and R_B for an average transistor we arrive at values which can be used for any transistor. It is necessary, if the system is to work really well, for the current gain to be high. Fortunately, the general-purpose planar transistors now coming on the market do usually have high gains ($h_{EE} = 50-300$) so this condition is easily met.

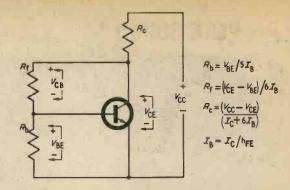


Fig. 2. The two-resistance bias circuit for RC amplifiers using high-gain silicon transistors. This compensates for both temperature and transistor variations and uses no electrolytic capacitors

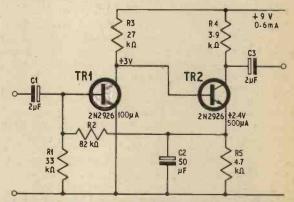


Fig. 3. General-purpose audio pre-amplifier. Both transistors may be high-gain 2N2926 (he over 50)

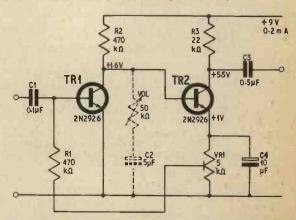
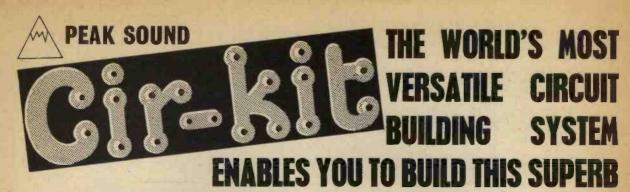


Fig. 4. In this "starved" amplifier TRI passes only about 10 micro amps, and therefore generates very little noise. Amplifiers like this can often be incorporated into existing valve amplifiers, since they require very little current and the polarity of the supply voltage is the same as that of the existing high tension supply

LOW-NOISE AUDIO CIRCUITS

Silicon planar transistors are often noisier than their germanium counterparts at audio frequencies, yet they make excellent low-level audio amplifiers. The explanation of this paradox lies in the behaviour of the transistors at low collector currents. In general, reducing the collector current reduces the noise. But it also reduces the gain, so there is a limit below which reducing current serves no useful purpose.



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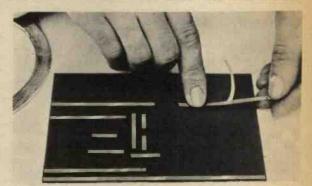
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UNIQUE DOUBLE SIDED TAPE OR 5% reels. Superb quality used in normal way. Aleal for experimenters too. 650' 9/-: 600' 8/6 (p/p 1/-per single reel, 6d. for each additional).

Established 1949

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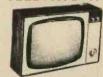
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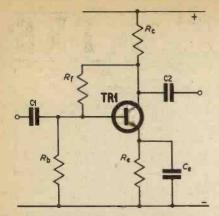


Fig. 5. In wide-band RC amplifiers an emitter resistor and capacitor provide high-frequency compensation

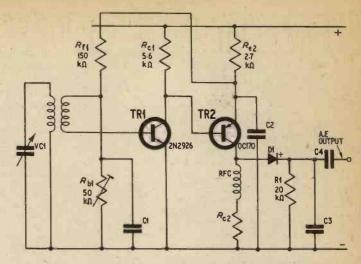


Fig. 6. Silicon npn transistors can readily be used in conjunction with germanium pnp transistors. In this circuit TRI and TR2 form an untuned r.f. amplifier feeding a detector

In the case of a germanium transistor, the gain usually falls off rapidly below about $0.5 \,\mathrm{mA}$. But comparable silicon planar transistors usually work quite happily down to $0.1 \,\mathrm{mA}$, and a high proportion still have useful gains (h_{10} over 10) at $0.01 \,\mathrm{mA}$ (10 microamps). By taking advantage of this good low-current performance we can achieve lower noise with silicon than with germanium. The input resistance goes up as $I_{\rm C}$ goes down, and this can be useful for matching the impedance of the signal source.

Using cheap epoxy transistors such as the 2N2926 series, amplifier circuits are "designable" with $I_C = 100\mu$ A, in the sense that fixed values of resistance are adequate. At lower currents, it is advisable to include one adjustable resistance to provide for variations from transistor to transistor. Two typical amplifier circuits are shown in Figs. 3 and 4.

RADIO FREQUENCY CIRCUITS

Radio frequency circuits are no different in principle from germanium transistor circuits. The cut-off frequency of a typical small planar transistor, particularly if it is of the epitaxial type, is likely to be high—a few hundred Mc/s. Special u.h.f. types go to 1,000Mc/s or higher. Ideally, one would like to operate well below cut-off, e.g. one-tenth of the cut-off

frequency. In practice, transistors must often be used at frequencies close to cut-off. In this case the gain is inevitably low, but may still be useful.

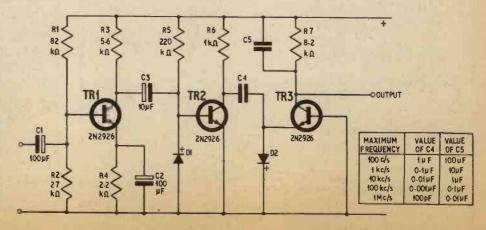
Whether neutralisation is necessary in a tuned amplifier depends partly on the stage gain and partly on the size of the collector-base capacitance $C_{\rm OB}$. In the cheaper transistors, with $C_{\rm OB}$ around 10pF, neutralisation is probably required. Special r.f. types, with $C_{\rm OB}$ less than 1pF, are just coming on the market, and are suitable for use without neutralisation.

The cut-off frequency is generally reduced if the transistor is operated at lower or higher collector currents than those for which the value of f_T is specified. Collector voltage should be reasonably large (5V) for high-frequency working.

WIDE-BAND AMPLIFIERS

There is no difficulty in making amplifiers with useful gains at frequencies of several megacycles. The main problem is keeping the gain reasonably constant over the full bandwidth—there is a natural tendency to get more gain at the lower frequencies. One simple technique is to include some resistance in the emitter circuit, and to bypass this at h.f. with a capacitance (Fig. 5). The required values are best found by trial and error, but are often in the range 100-1,000 ohms and 100-1,000 pF.

Fig. 7. Frequency to voltage converter. Here TR2 squares the waveform, and C4 differentiates it. result is to make TR3 pass a current proportional to the input frequency. The voltage across R7 is likewise proportional to frequency. Capacitor C4 sets the range and C5 smoothes the output. If the circuit is used as a frequency meter C5 should be large, while for use as a discriminator it should bypass the carrier frequency but not the audio output



Assuming a low-impedance signal-source ("voltage drive") the mutual conductance of the transistor with emitter resistance Re is roughly 1/Re, and this holds good for Re of 100 ohms or more at collector currents of 1mA or more. As with all wide-band circuits, the stage gain must be reduced (by using smaller Rc) as the bandwidth is increased. The bandwidth is always less than f_T , since at this frequency the "gain" is unity.

MIXED NPN AND PNP CIRCUITS

Constructors who are accustomed only to pnp circuits are often worried about the prospect of mixing pnp and npn transistors. In practice this is no problem,

and often results in cheaper circuitry.

A typical case is shown in Fig. 6. Here the two transistors form a wide-band amplifier feeding a detector diode. The input is from a ferrite rod aerial, and the whole circuit is a simple t.r.f. receiver "front end". Note that R_{E_2} is bypassed to the negative line. (If it were bypassed to positive this would create a lowimpedance path for h.f. disturbances on the positive line to R_{F1} and enough might get back to the base of V1 to cause instability. Resistor Rc_2 is included to provide d.c. bias to the detector. (In practice, the resistance of the choke is often adequate). Essentially the same pnp-npn technique can be used in the audio stages.

NON-LINEAR CIRCUITS

Planar transistors may be used in the usual switching and waveform-shaping circuits, but one or two special features should be borne in mind. Unlike alloy transistors, planar transistors have practically no gain in the "inverted" condition, i.e. with collector and emitter connections reversed. This is because the base is small. For the same reason, the base will not pass large

The reverse base-emitter breakdown voltage for a planar transistor is usually about 6V. If there is danger of exceeding this, a diode must be connected in the base lead so that, when the base voltage is such that the transistor is cut-off, the diode is reverse biased. In this condition the diode absorbs most of the reverse voltage and the transistor is protected.

A typical wave-shaping circuit, due to Marconi Instruments, is shown in Fig. 7. This is a frequency-tovoltage converter, and it could be used as a frequency meter or pulse-counting f.m. discriminator up to

about 1Mc/s.

PRACTICAL WIRELESS

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NEWS BRIEFS

Solid State Physics on TV

A NEW BBC1 television series on modern solid state electronic devices called "The New Electronics" started on January 8. Integrated circuits, Gunn oscillators, silicon-controlled rectifiers, field effect transistorsthese are some of the newest devices in a technology which was almost unknown ten years ago. They are all semiconducting devices. They all depend on the production of very pure solids in very exact crystalline forms. Impurities are added to these in amazingly small concentrations to make the p-type and the n-type materials which are the basis of the devices themselves

These ten programmes which are intended for electrical engineers, teachers in schools and colleges, undergraduates and sixth forms explain how the devices are made, how

they work and some of their uses.

GBR Returns to the Air

HE historic call sign GBR can once again be heard on the HE historic call sign GBR can once again very low frequency of 16kc/s (18,750 metres) after an

absence of 12 months.

Originally designed and built in the early 1920's by G.P.O. engineers, the Rugby Radio Station made history as the world's most powerful transmitter using valves. Now the old transmitter has been completely re-designed. The most striking changes are in the main amplifier stages where 54 water-cooled valves have been replaced by nine vapour-cooled amplifier valves; and in the modulator which can generate precision frequency-shift signals as well as the original c.w. signals at speeds up to 72 bauds. Transistors are employed in the driver stages.

At an opening ceremony on November 30, GBR was switched on by Capt. C. B. H. Wake-Walker R.N., Director of Naval Signals. The new transmitter is now in regular use for naval traffic and time signal emissions. It can be received by warships and submarines in all parts of

the world.

The output power is 450-500kW and the radiated power from the large aerial array (a prominent landmark in the midlands) exceeds 60kW.

Mr. E. K. Cole

News of the death of Mr. E. K. Cole last November will have brought back memories of the early days of

broadcasting to many readers.

A pioneer of the mains operated radio set and founder of a large radio and electrical firm, Ekco, Mr. Cole made his first mains set in 1925. He was then working as an electrical engineer at Southend. His company, which grew to become one of the foremost in the industry, was merged into Pye of Cambridge a few years ago. Mr. Cole was 65.

New IEE Grading Structure

To conform to an agreed scale of membership grades, on which constituent institutions of the Council of Engineering Institutions are collaborating, the Institution of Electrical Engineers has changed its membership structure.

Full members are now designated Fellows; associate members are now members; graduates and associates are

now associate members.

Applications to the old class of associate have now been abolished. A new grade of associates is open to those applicants in other professions who are interested in or associated with the activities of the I.E.E. These may include doctors concerned with medical electronics, architects, teachers, and technicians who do not qualify for other grades of membership.

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MULTIMETERS TK.20A 1,000 o.p.v. TK.25 1,000 o.p.v. EP.10K 10,000 o.p.v. EP.10KN 10,000 o.p.v. £2.15.6 £2.15.6 £4.17.6 £5.8.0 £5.19.6 £6.8.0 EP.20K 20,000 o.p.v. EP.20K 20,000 o.p.v. EP.30K 30,000 o.p.v. EP.30K 30,000 o.p.v. EP.50KN 50,000 o.p.v. EP.100KN 100,000 o.p.v. £7 19 6 £11.19.6 £14.19.6

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TE-188. RF S!GNAL GENERATOR A stable while range signal generator with a range of 120 Kc/s-260 Mc/s on 6 hands. Features a large 4tm. vernier tuned, etched circular dial for easy accurate frequency adjustments £20.15.0

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As well as this beautifully designed speaker there are two other models M865. 10 watts RM8 at £12,12.0 and M840 5 watts RM8 £8,10.0.

All three speakers are finished in magnificent rosewood and the entire cabinet filled with acoustic damping material.

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MAGNETIC STEREO CARTRIDGES
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Response: 20-20,000 cps
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44 GDS

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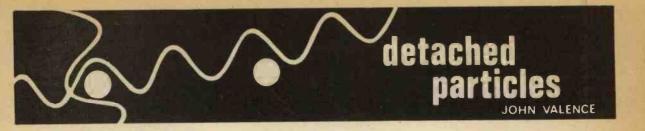
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Switch contacts 15 amp. 250 v. A.C., complete with chrome bezel and control knob. Min. operation time, 30 seconds, max. 4 minutes, brand new 17/6, p.p. 2/6.



FOG CONQUERED

Down at London airport great strides are being made in overcoming the fog problem. The Autoland system came through the latest tests earlier this winter with flying colours. A BEA Trident airliner made a number of landings in thick fog and the aircraft touched down within 3ft of the runway centre line, on each occasion.

This is an achievement of distinction, a credit to the designers and manufacturers of this equipment and also to the airline authorities for pursuing this idea so fervently. Conquest of the fog menace is one of the biggest challenges presented by nature. It is nice to know that in this field, Britain is well to the fore, if not way out ahead of other countries. Certainly London airport is at present unique in that it is equipped for blind landings.

Technically proved, the system has yet to receive official blessing so permitting its use for normal passenger flights. But the latest tests under extremely limited visibility must have hastened the day when automatic landing becomes fully operational.

BUT HERE . . . FOG PERSISTS

While the technocrats are winning the battle against fog at London airport, we find the bureaucrats at Westminster resolved on maintaining the "fog" which engulfs their proceedings so far as the public is concerned.

Rejection of the proposal to have trial sound and vision recordings made in the House during sessions seems to me most regrettable. Quotations I read from time to time in newspaper reports of Parliamentary debates do of course go some way to explaining the reluctance of our elected representatives to allowing a wider audience to listen or look in!

One of the greatest attributes of electronic science is surely the power to enable man to communicate with his fellow. To spurn modern innova-

tions without good reason suggests an unawareness of the realities of present times.

THE SAX IS BACK

Are our ears about to be assailed by yet another "new sound" from the jazz and popular music world?

I learn that the electronic saxophone has just been launched on the American market. Probably by now this latest creation is on its way to these shores, and soon the air will be filled with soft cooing sounds reminiscent of the mid '20's.

With this "Varitone" electronic unit, the characteristic tone of the saxophone can be modified with tremolo and reverberation effects. Those who do not like playing alone can produce an accompaniment by the flick of a switch—a frequency dividing circuit does the rest.

So this is the long awaited American reply to the Beatles!

ANOTHER DEPENDENT RELATIVE

When I refer to AUNTIE, you probably think I am alluding to that much maligned old soul who resides in Portland Place. But you would be wrong. The Auntie in question is another computer. (What fun it must be devising these names).

If the suggestions made by the Conservative Political Centre ever come to fruition, this particular machine (Automatic Unit for National Taxation and Insurance) will know all facts about our incomes and any social benefits we may be entitled to receive and would produce a single statement showing the balance due to (or from) the State.

The logic of having this kind of system is hard to deny. In fact I feel sure that this is inevitable in time, and the facilities of the computer will be extended to cover other personal particulars.

Yes, even dog, car, and television licences! And what a boon the latter would be to our other Auntie in her present straitened circumstances.

NO LOGIC AT ALL

One can dwell on the subject of computers, imagining all kinds of applications to exercise their nimble brains. As servant of the Government the computer might be thought as hastening the arrival of the Brave New World.

Perhaps this is rather frightening.

Turning to private enterprise, one application that seems to have quite a future is the "match-making" business. There have been many accounts of computers being used to match up compatible couples, but these were usually light hearted exercises conducted for the amusement of the operators between more serious stints.

However, the professional match makers have not been slow to appreciate the possibilities of this electronic tool, as a recent court case revealed.

Multifarious and marvellous are the tasks performed by the electron. It can guide a satellite-carrying rocket far out in space, it can solve a quadratic equation in a minute fraction of a second; but is it not rushing in where angels fear to tread when it tries to couple up for life two of nature's most imponderable creatures? There's really no logic in it at all. . . .



"I had a nice little number before the shakeout"

REGULOTIC— A SELECTION FROM OUR POSTBAG

Stereo amplifier

Sir—With reference to your article in PRACTICAL ELECTRONICS on the Integrated Stereo Amplifier. Having had great difficulty in trying to obtain the OA99 diodes as specified, I have been informed that these diodes are not in production and therefore unobtainable. Would you therefore inform me if any alterations to the circuit are required.

I also note that in the same article no switches are given in the

components list.

Although I know that this amplifier is of top quality design and up to your usual very high standard, is it not pointless to specify something which is unobtainable from normal suppliers and which can cause the amateur a great deal of trouble when he finds he cannot obtain components?

P. G. Dunstan, Mill Hill, London, N.W.7.

Our apologies for the omission of the switches. SI is 4-pole 3-way; S2 single-pole on/off or changeover; S3 double-pole on/off. As stated in last month's issue the diodes should be OA95. TR3a and b can alternatively be NKT0003

Alpha-radioactivity

Sir—Comments from many leading research scientists indicate that my suggestion of alpha-radioactivity influencing generation of thunderstorm electricity (P.E. October 1966) are considered probably correct and very important.

Of all the processes previously proposed to explain thunderstorm electricity, the one put forward by Mason has long been the favourite. It is based on the fact that defect protons (analogous to defect electrons in conventional semicon-

ductors) drift towards the colder regions of ice, crystals, charging them positively there.

Most of the precipitation of thunderstorms is produced via soft hailstones which grow by accretion of supercooled water droplets and then melt in the cloudbase to produce the heavy raindrops. Each water droplet thus captured by a growing hailstone first forms a thin skin of ice which bursts and releases numerous ice splinters during further freezing of the drop. Originating from the coldest parts, the ice splinters will be carrying the drifted protons and are thus positively charged. They are rapidly blown to the crown of the thundercloud, whereas the much larger hailstone continues to fall.

This convincing process definitely takes place in all thunderstorms, but was so far not recognised as the final explanation of thunderstorm electricity because it is too weak by a factor of 5 to 25 compared to the requirements of numerous intense storms. It is easy to see that its electric yield will be proportional to the number of defect protons

available in the ice.

I already showed in my thunderstorm article, that the ionisation current yield of the total alpharadioactivity in a thundercloud is quite adequate to supply the currents involved in all thunderstorms. It now seems evident that this ionisation current will actually appear as copious additional defects. Thus it will be coupled efficiently to the turbulence, for large-scale electric charge separation in the manner described.

Turning to a related question, I would like to reply to Mr C. B. Sibley regarding possible thunderstorms on Jupiter which he commented in his Radio Astronomy feature (P.E. August 1966). Thunderstorms of the required ferocity to account for radio signals received from Jupiter are indeed possible if a Mason-

Michaelis process operates on liquid and solid ammonia instead of water and ice.

The jovian atmosphere is believed to contain ammonia and also possesses suitable daytime temperatures around -100°C which would be necessary for an ammonia thunderstorm. Radioactive emmanations would doubtless be present just as on earth, and the chemical properties of liquid and solid ammonia would suggest much greater proton semiconductivity in response to alpha-radiation, than that obtainable with ice under terrestrial conditions.

M. L. Michaelis, M.A.

Dr B. J. Mason will be giving a talk on "The Generation of Cloud Electricity" at the I.E.E., Savoy Place, London, W.C.2 on January 18, 6.30 p.m.

Forthcoming . . .

Sir—I am interested in building a trace doubler.

I would like to know if you could perhaps send me a circuit or let me know if you will be printing one in any later issues.

Any information you can give me on this equipment will be a

great help to me.

G. G. Redding, Rogerstone, Mon.

A trace doubler will be appearing in the near future.

. . attractions

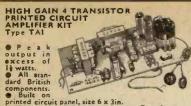
Sir—I would appreciate information of any kind, concerning the construction of a radio telescope.

We have a group of members interested in electronics, and would like to purchase blueprints, and equipment.

I trust you will be able to assist us, or at least direct us to a supplier.

J. W. Norton, Immingham Youth Centre, Immingham.

Although we have not so far published any constructional information in this field, we are sure you will be interested to learn that very shortly we will be commencing a short series on this subject by a well-known authority on radio astronomy. This series will include details of a simple station that can be set up for observation of the sun.



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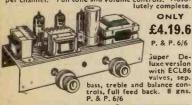
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Carr. 6/6 on each. GARRARD ATE £9.10.0. All the above units are complete with t/o mono head and sapphire styli or can be supplied with compatible stereo head for 12/6 extra.

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.M.I. PLASTIC CONED TWEETER. §". 3 ohm. Limited number: 12/6 each, P. & P. 1/6.

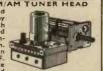
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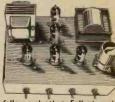
* Heavy duty doublewound mains transformer
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* Separate Bass, Treble
and volume controls, giving
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loss. * Heavy negative
feedback loop over 2 stages
ensures high output at
excellent quality with very low distortion factor.

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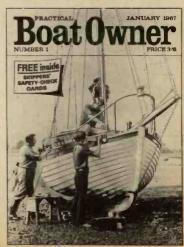
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