

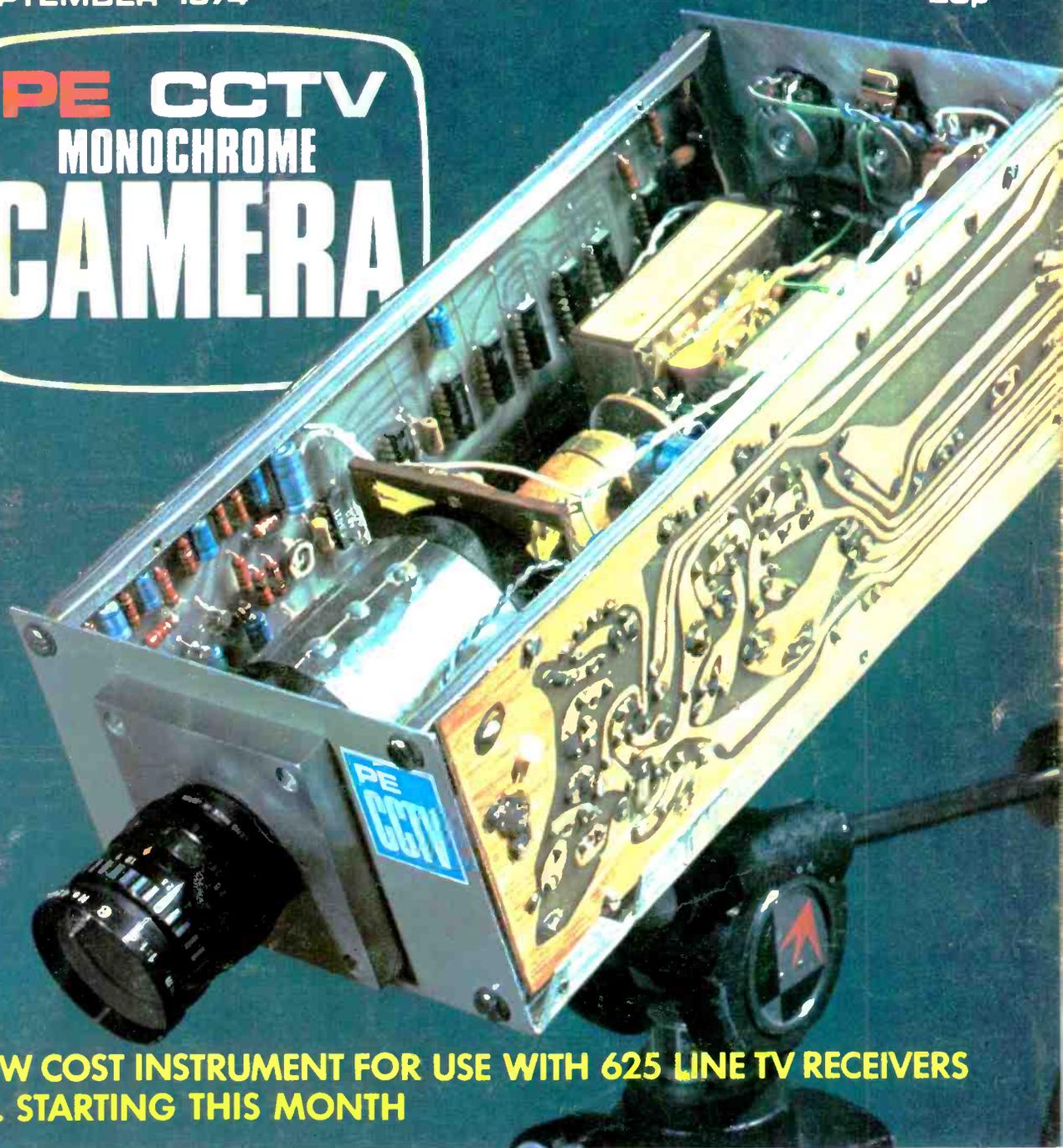
PRACTICAL

# ELECTRONICS

SEPTEMBER 1974

25p

**PE** CCTV  
MONOCHROME  
**CAMERA**



LOW COST INSTRUMENT FOR USE WITH 625 LINE TV RECEIVERS  
... STARTING THIS MONTH

**GAS DETECTORS** for •HOME•FACTORY  
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**BRITISH INSTITUTE OF ENGINEERING TECHNOLOGY**

# PRACTICAL ELECTRONICS

VOLUME 10 No. 9 SEPTEMBER 1974

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**Because of prevailing production problems, no firm publishing date can be announced for the October issue. Readers are advised to check regularly with their local supplier from mid-September onwards.**

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# Henry's

**DON'T RELY ON YOUR MEMORY  
BUY NOW AT BARGAIN PRICES**  
Hi Fi and Transistors - Up to date  
Brochures on request

## HENRY'S CATALOGUE

Due to rapid price changes, shortages of paper and raw materials, all prices in the existing catalogues no longer apply. Call or phone for latest prices. A new catalogue will be available for Aug/Sept. 1974

**UK's  
LARGEST RANGE  
OF KITS &  
GADGETS**

### TEST EQUIPMENT MULTIMETERS

(carr. etc. 30p)  
IT1-2 20K/Volt Slimline £5-95  
M210 (Case £1-25) 20K/Volt  
Slimline deluxe £6-75  
TLH33D 2K/Volt Robust £7-50  
U4323 (+1F BAF OSC) £7-00  
AF105 (Case £1-90) 50K/Volt 12-50  
U4313 20K/Volt AC current. Steel case 10-50  
U4341 Plus Built-in transistor tester 10-50  
Model 500 (Case £2-25) 30K/Volt 11-75



### OTHER EQUIPMENT

SE250B Pocket Signal Injector 2-25 carr. 15p  
TE15 Grid Dip meter 440kHz 280mHz 16-50 carr. 30p  
TE40 AC Millivoltmeter 1.2mHz 19-75 carr. 35p  
TE65 2B Range valve voltmeter 22-50 carr. 40p  
TE20D 120kHz-500mHz RF Gen. 18-95 carr. 40p  
TE22D 20Hz-200kHz Audio Gen. 19-95 carr. 40p  
SE350A Deluxe Signal Tracer 12-95 carr. 20p  
SE400 Volts/ohms/R-C sub./RF field/RF gen. 15-50 carr. 20p

### New Revolutionary Superstere 680R

680R Multi-tester £18-50

Accessories	
Transistor tester	11-00
Electronic voltmeter	18-00
Amplamp	11-95
Temperature probe	11-95
Gauss meter	11-95
Phase Sequence	5-95
EHT Probe	5-95
Shunts 25/50/100A	4-50



### A SELECTION OF INTERESTING ITEMS

C3025 Compact transistor tester 6-95 p & p 15p  
Q4002 Photoelectric System £13-70  
E1310 Stereo mag. cart. preamp. 4-80 p & p 25p  
Easiphone D1201 telephone amp 7-50 p & p 20p  
D1203 Telemp. with PU coil 4-95 p & p 25p  
LL1 Door Intercomm. and chime 8-40 p & p 25p  
9" Twin spring unit For 3-30 p & p 15p  
EHT Probe 6-85 p & p 25p  
U550 Ultrasonic Switch Trans/Rec £12-75  
C3041 1-250mHz £4-25  
C3043 SCH 1-300mHz £5-75  
VHF 105 Aircraft Band Converter 4-50 p & p 15p  
B2005 4 Ch. mic. mixer 4-20 p & p 15p  
B2004 2 Ch. Stereo mixer 6-75 p & p 15p  
PK3 Kit £1-95 p & p 20p

### EXCLUSIVE: SPECIAL OFFERS

MW/LW CAR RADIO PORTABLE CASSETTE TAPE PLAYER—for car or carry around. £7-25 c/p 20p. HANIMAX BC808 WITH % KEY. £28-95. HANIMAX BC811M MEMORY VERSION £33-75. \*BC807 % key £22-95. \*BC850 % key + memory £33-95. \*MAINS UNIT £3-25 EXTRA. HANIMAX H101 STEREO COMPACT RECORD PLAYER 2 7 watts. Complete with Speakers (List £54-50) Price £39-95. Plus free pair of stereo ette Recorder £12-75.

### BUILD THIS RADIO

Portable MW/LW radio kit using Mullard RF/IF module. Features MW—bandspread for extra selectivity. Slow motion tuning. Fibre glass PVC cabinet. 600MW output. All parts £7-98 (battery 22p), carr. etc. 32p.



FIBRE OPTICS  
0-01 diam. Mono Filament £5-50 per 100 metre reel  
0-13 diam. 64 Fibres Sheathed £1-00 per metre.  
SPRAYS 15mm diam. (Mare's Tail Spray £10-50)

### SPECIAL PURCHASES

#### UHF TV TUNERS CHANNELS 21 TO 64

Brand new transistorised geared tuners for 625 Line Receiver IF output. £2-50. Post 20p.



#### PUSHBUTTON UHF TV Tuner

New purchase of 4 button transistorised UHF tuners, £3-50, post 20p.

### EASY TO BUILD KITS BY AMTRON— EVERYTHING SUPPLIED

Model No.	£ p	Model No.	£ p
310 Radio control receiver	3-29	760 Acoustic switch	12-57
300 4-channel R/C transmitter	6-61	780 Metal Detector (Electronics only)	10-91
345 Superhet R/C receiver	6-61	790 Capacitive Burglar alarm	7-92
65 Simple transistor tester	1-66	835 Guitar preamp	4-99
115 8 watt Amplifier	4-50	840 Delay car alarm	6-99
120 12 watt amplifier	4-73	875 CAP Discharge ignition (for car engine (—Ve Earth))	13-99
125 Stereo control unit	6-01	80 Scope Calibrator	2-65
130 Mono control unit	4-16	255 Level Indicator	6-98
605 Power supply for 115	5-31	525 120-160mHz VHF timer	11-31
610 Power supply for 120	5-31	715 Photo cell switch	8-97
615 Power supply for 2 x 120	6-64	795 Electronic continuity tester	4-97
230 AM/FM aerial amplifier	3-29	860 Photo timer	15-51
240 Auto parking light	6-90	235 Acoustic Alarm for driver	8-61
275 Mic. preamplifier	6-98	465 Quartz XTAL checker	9-90
5705 LF generator 10Hz-1mHz	21-45	220 Signal Injector	2-30
5755 Sq. wave generator 20Hz-20kHz	19-77	390 VOX	15-50
590 SWR meter	9-47	432 Testakit	19-30
630 STAB Power supply 6-12V 0-25-0-1A	9-24	670 Buffer Battery Charger	6-55
690 DC motor speed Gov.	3-31	885 Capacitive Contact Alarm	6-25
700 Electronic Chaffinch	7-92	850 Electronic Keyer	18-75
		820 Electronic Digital Clock	58-50



ALL KITS OFFERED SUBJECT TO STOCK AVAILABILITY.  
Prices correct at time of preparation. Subject to change without notice.

### BUILD THIS TUNER ML3

MW/LW Radio Tuner to use with any amplifier. Features Mullard RF/IF module Ferrite aerial, built in battery. Excellent results. Size 7" x 2 1/2" x 3 1/2". All parts £5-25, carr. 15p.

#### MULLARD FM MODULES

LP1186 Tuning Heart Module  
LP1185 IF Module complete with data Price £9-00 pair

#### FM TUNER MODULE

FM5231 12v FM Tuner £7-95  
SD4912 Stereo Decoder £7-95  
SF62H 6v Stereo FM Tuner £14-95

#### TBA800 5 WATT I.C.

Suitable alternative to SL403D. 5/30 volt operated. 8/16 ohm 5 watt output. With circuits and data £1-50

Kit with printed circuit panel £2-70  
All kits available from stock.

#### STROBE TUBE

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ST2 (D32) DIAC 25p  
ZFS/40 SCR 45p  
ZFT8 £4-00

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#### PP9 ELIMINATOR KIT

Complete module kit 9v 100mA output £1-95 p & p 25p

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\*Sinclair IC12 6W IC £2-00  
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\*Ultrasonic Transducers £5-90 pr.  
\*3015F 75EG Indicator £1-70  
\*TIL 209 LED 24p each  
\*22p each per 10  
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GARRARD 2 speed 9 volt tape decks. Fitted record/play and oscillator/erase heads. Wind and rewind controls. Takes up to 4" spools. Brand new complete with head circuits. £9-50 carr. 30p.

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60mm stroke high quality controls complete with knobs (post, etc. 15p any quantity).

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Ganged Log and Lin 10K, 22K, 50K, 100K, 250K, 65p each.  
(Quantity discounts available)  
Complete with knobs.

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4 TRACK MONO or 2 TRACK STEREO  
"17" High Impedance £2-50  
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"36" Med. Impedance £5-00  
R730/R732 track mono Record/Erase low imp. 75p pair.  
Erase Heads for "17" "18" and "36" £1-00  
"63" 2 track mono. High Imp. £1-75  
"43" Erase Head for "63" 75p  
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AMPLIFIERS (carr. etc. 20p)  
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304, 3 watt 9 volt 3-95  
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410, 10 w 28 volt 4-45  
E1206, 30 w 45 volt 9-95  
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RE500, 5 watt IC mains operated Amplifier with controls 4-30  
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HC244B Stabilised version 5-50 carr. 30p  
P500 9 volt 500mA 3-20 post 20p  
P11 24 volt 500mA (chassis) 2-90 post 20p  
P15 26/28 volt 1 amp (chassis) 2-90 post 20p  
P1080 12V 1 amp (chassis) 4-70 post 20p  
P1081 45V 0-9 amp (chassis) 7-80 post 20p  
P12 4 1/2 volt 0-1 amp 7-15 post 30p  
SE101A 3 (6/9) 12 volt 1 amp (Stab.) 12-75 post 25p  
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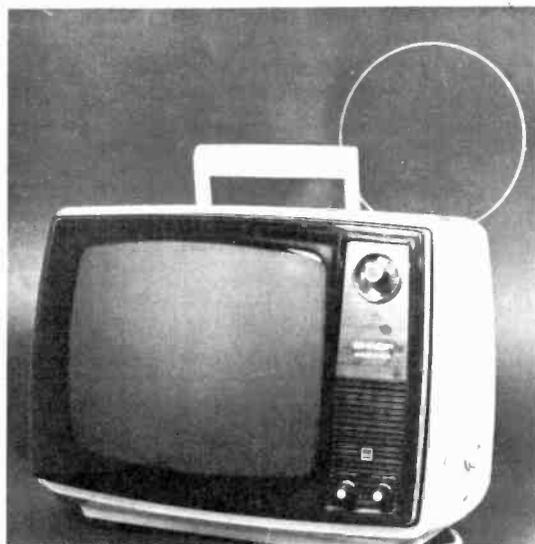
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- ★ GUARANTEED FOR 1 YEAR
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**BASF  
CASSETTE  
RECORDER**



- ★ THE LATEST HIGH QUALITY PRODUCT FROM THE RENOWNED GERMAN BASF COMPANY
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- ★ RECOMMENDED RETAIL PRICE £36.35 (Exclusive of V.A.T.)

OUR PRICE  
**£29.95**

## BASF CASSETTES (TYPE LH IN SNAP-PACK)

	C30	C60	C90	C120
PRICE EACH:	<b>47p</b>	<b>55p</b>	<b>76p</b>	<b>£1.13</b>

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**E12**  $\frac{1}{4}$  watt 10 $\Omega$  — 1M  
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- ★ MINIMUM ORDER 100 RESISTORS
- ★ MINIMUM PER VALVE 25

**75p/100**

IF EXACT VALVE IS OUT OF STOCK THEN NEAREST WILL BE SUPPLIED

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- ★ PRICES DO NOT INCLUDE V.A.T.
- ★ PAYMENT WITH ORDER ONLY
- ★ TOTAL PAYMENT = COST OF GOODS + P/P + 10% V.A.T.

**POSTAGE AND PACKING**  
TELEVISION—£1.25  
CASSETTE RECORDER—£1  
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**MOTEC**

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# ALL OUR PRICES INCLUDE V.A.T.

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Plays 12", 10" or 7" records. Auto or Manual. High quality unit backed by BSR reliability with 12 months' guarantee. AC 200/250V. Size 18 1/2 x 11 1/2 in. Above motor board 3 1/2 in. Below motor board 2 1/2 in. with STEREO and MONO XTAL £6.75 Post 45p.



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### 4 Transistor Mono Amplifier

Powerful 3 watt output, 15 ohm. AC mains operated with transformer. 3-Controls, volume, treble, bass and On/Off switch with knobs. Ready made on printed circuit board. Fused inputs and outputs. Famous make. Size 8 1/2 in wide x 4 1/2 in deep x 5 1/2 in high. Suitable 7 in x 4 in speaker, £1. £5.95 Post 25p



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Fitted with auto stop. Acos stereo/mono cartridge. Baseplate. Size 11 in x 8 1/2 in. Turntable. Size 7 in diameter. A/C mains. 200/250V motor has a separate winding 14 volt to power a small amplifier. Three speeds. Plays all records. £5.50 Post 25p

**METAL PLINTH AND PLASTIC COVER**  
Cut out for most Garrard or B.S.R. Most will play with cover in position. 12 1/2 x 14 1/2 x 7 1/2 in. Covered in black leatherette. £4.95 Post 45p

ALSO AVAILABLE IN SOLID NATURAL MAHOAGANY WAX POLISHED FINISH—£5.95

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Two full size loudspeakers 1 1/2 x 10 x 3 1/2 in. Player unit clips to loudspeakers making it extremely compact. Overall size only 13 1/2 x 10 x 3 1/2 in. 3 watts per channel, plays all records 33 r.p.m., 45 r.p.m. Separate volume and tone controls. 240V AC Mains. £25 Bargain Price 85p Carriage



Attractive Teak finish Weight 13 lb.

## SPECIAL OFFER! SMITH'S CLOCKWORK 15 AMP TIME SWITCH 0 TO 60 MINUTES

Single pole two-way surface mounting with fixing screws. Will replace existing wall switch to give light for return home, garage, automatic anti-burglar lights, etc. Variable knob. Turn on or off at full or intermediate settings. Fully insulated. Makers' last list price £4.50. Brand new and fully guaranteed. OUR PRICE £1.95 Post 25p



BLANK ALUMINIUM CHASSIS. 18 s.w.g. 2 1/2 in sides 6 x 4 in 45p; 8 x 8 in 53p; 10 x 7 in 65p; 12 x 8 in 85p; 14 x 9 in 90p; 16 x 6 in 90p; 12 x 3 in 50p; 16 x 10 in 81p. ALUMINIUM BOXES 3 x 3 x 3 in 60p; 4 x 4 x 4 in 70p; 6 x 4 x 4 in 80p; 9 x 4 x 4 in £1; 12 x 4 x 4 in £1.30. ALUMINIUM PANELS 18 s.w.g. 6 x 4 in 12p; 8 x 6 in 19p; 14 x 3 in 20p; 10 x 7 in 24p; 12 x 8 in 25p; 12 x 8 in 34p; 16 x 6 in 34p; 14 x 9 in 40p; 12 x 12 in 47p; 16 x 10 in 60p. PAKOLIN PANEL 10 x 8 in 20p. 1 1/2 inch DIAMETER VAVECHANGE SWITCHES, 45p ea. 2 p. 2-way, or 2 p. 6-way, or 3 p. 4-way. 1 p. 1. 2-way, or 4 p. 2-way, or 4 p. 3-way. TOGGLE SWITCHES, sp. 20p; dp. 25p; dp. dt. 30p. Sub-miniature, sp. 33p; dp. dt. 50p.

## BRITISH FM/VHF TUNING HEART

88 to 108 Mc/s British made. 2 Transistors ready aligned—requires 10.7 Mc/s I.F. Complete with tuning gang. Connections supplied but some technical experience essential. Our price £3.95 Post 20p

## R.C.S. STABILISED POWER PACK KITS

All parts and instructions with Zener Diode, Printed Circuit, Bridge Rectifiers and Double Wound Mains Transformer input 200/240V a.c. Output voltages available 6 or 9 or 12 or 15 or 18 or 20V d.c. at 100mA or less. £2.20 Post 20p  
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Ideal for Mike, Tape, P.U., Guitar, etc. Can be used with Battery 9-12V or H.T. line 200-300V d.c. operation. Size: 1 1/2 x 1 1/2 in. Response 25 c/s to 25 kc/s, 26 dB gain. Full use with valve or transistor equipment. £9.9p Post 10p  
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12 VOLT, 750mA. Complete with printed circuit board and assembly instructions. £2.95 Post 25p  
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2000mF 6V 25p; 25V 45p; 50V 57p.  
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TWIN GANG. "C-O" 20pF+176pF, 75p.  
Short wave trimmer 365pF+365pF with 25pF+25pF, 50p.  
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SHORT WAVE SINGLE GANG. Precision Silver Plated Gangable Tuning Condensers. 100pF. 50p each

NEON PANEL INDICATORS 250V AC/DC. Amber 30p.  
RESISTORS. 1/4W, 1/2W, 20% 1p; 2W, 5p. 10Ω to 10MΩ.  
HIGH STABILITY. 1/4W 2% 10 ohms to 6 meg., 10p.  
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## MAINS TRANSFORMERS ALL POST 25p each

Eagle MT12 12-0-12V 50mA ..... 90p  
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Primary 0-110-240V. Secondary 0-240V 3 amps 720 watt. Insulated terminals. Varnish impregnated. Fully enclosed in steel case with fixing feet. £10 Carr. 50p  
Famous make (Value £19) OUR PRICE £10 Carr. 50p  
Can be used as 800 watt auto transformers 240-110V.

## SET OF 3 MOTORS FOR COLLARO STUDIO 115 VOLT TAPE DECK

£2.50 Post 50p

## VOLUME CONTROLS 80 Ohm Coax 5p yd.

Long spindles. Midget Size 5 Kc. ohms to 2 Meg. LOG or LIN. L/R 20p. D.P. 35p. STEREO L/R 55p. D.P. 75p. Edge 5K. S.P. Transistor 25p.  
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DUAL CONCENTRIC TOP 500K LOG AND 500K LIN D.P. switch. Inner spindle 3 1/2 in; outer spindle 2 1/2 in 75p.

## E.M.I. 13 1/2 x 8 in. SPEAKER SALE!

With twin tweeters. £4.50  
And crossover. 10 watt. Size 3 or 8 or 15 ohm. As illustrated. Post 25p



With flared tweeter cone and ceramic magnet. 10 watt. Bass res. 45-60 c/s. Flux 10,000 gauss. Size 3 or 8 or 15 ohm. Post 25p £2.75

## LOUDSPEAKER FRONT GRILLES

Teakwood strips mounted on cloth backing, easily glued on to baffle to modernise cabinets. Size 19 1/2 in x 7 1/2 in. 45p  
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## E.M.I. 6 1/2 in. HI-FI WOOFER

8 ohm. 10W. Large ceramic magnet. Special Rubber cone surround. Frequency response 30-12,000 c/s. Ideal P.A. Columns. Hi-Fi. Enclosure Systems, etc. Suitable Cabinet 12 x 8 x 6 1/4 Suitable Tweeter £2



**ELAC CONE TWEETER**  
The moving coil diaphragm gives a good radiation pattern to the higher frequencies and a smooth extension of total response from 1,000 c/s to 18,000 c/s. Size 3 1/2 x 2 in deep. Rating 10W, 3 ohm. Crossover £1.25 £1.90 Post 20p.

## GOODMANS 8 in. WOOFER

8 ohm 12 watt. Deep cone. Heavy ceramic magnet. Bass resonance 35 cps. Frequency response 30-3,000 cps. Ideal bass unit for Hi-Fi system. £3.75



## SPECIAL OFFER LOUDSPEAKERS ALL BRAND NEW

3 ohm, 2 1/2 in; 2 1/2 in; 3 1/2 in; 5 in.  
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15 ohm, 3 1/2 in; 5 in; 6 x 4 in; 5 x 3 in; 7 x 4 in; 8 x 5 in.  
25 ohm, 2 1/2 in; 3 in; 5 x 3 in; 5 in.  
35 ohm, 2 in; 3 in; 5 in.  
80 ohm, 2 in; 2 in. 120 ohm 3 in. £1 EACH

LOUDSPEAKERS P.M. 3 OHMS. 7 x 4 in £1.95; 6 1/2 in £1.50; 8 x 5 in £1.60; 8 in £1.75; 10 x 6 in £1.90; 10 in £2.50  
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Complete with 12 ft. twin lead fitted with din speaker plug. Ready assembled with leads for speakers, bass, mid and tweeter. Crossover frequencies—850 cps and £1.95 3,000 cps.

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PUSH-PULL VALVE OUTPUT TRANSFORMERS. 50 watt ..... £12.50 100 watt ..... £15.00

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1.5V d.c. operation over 200 hours continuous on SP2 battery, fully adjustable swing and speed. Ideal display teaching electric magnetism or for metronome, 95p Post 20p.

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2 stage triode pentode valve. 3 watts output. Volume on/off and tone controls. Printed circuit A.C. mains complete and tested. £4.50 Post 25p  
Complete with speaker.

COAXIAL PLUG 10p. PANEL SOCKETS 10p. LINE 18 OUTLET BOXES, SURFACE MOUNTING 25p.  
BALANCED TWIN RIBBON FEEDER 300 ohms, 7p yd.  
JACK SOCKET Std. open-circuit 14p. closed circuit 23p.  
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## E.M.I. WOOFER AND TWEETER KIT £6-75

THE PAIR, Post 25p. (Available separately. Woofer £5-25; Tweeter £1-90)

Comprising a fine example of a Woofer 10 1/2 x 8 1/2 in. with a massive Ceramic Magnet, 44oz Gauss 13,000 lines. Aluminium Cone centre to improve middle and top response. Also the E.M.I. Tweeter 3 1/2 in square has a special lightweight paper cone and magnet flux 10,000 lines. Crossover condenser and full instructions supplied.

Impedance Standard 8 ohms  
Maximum power 12 watts  
Useful Response 35 to 18,000 cps  
Bass Resonance 45 cps

SUITABLE ENCLOSURE 20 x 13 x 9 in.  
MODERN DESIGN. TEAK WOOD FINISH.



£10-50 Post 75p

## ANOTHER R.C.S. BARGAIN!

ELAC 9 x 5 in. HI-FI SPEAKER TYPE 59RN  
This famous unit now available, 10 watts, 8 ohm.  
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## 8" or 10" x 6" ELAC HI-FI SPEAKER

Dual cone plasticised roll surround. Large ceramic magnet. 50-18,000 cps. Bass resonance 45 cps. 8 ohm impedance. 10 watts.

10 in version £4-50.

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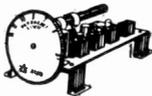
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LOUDSPEAKER CABINET WADDING 18 in wide, 20p ft.



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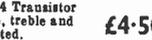
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Add musical highlights and sound effects to recordings. Will mix Microphone, records, tape and tuner with separate controls into single output. 9 volt battery operated. £4-50



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BARGAIN 3 WATT AMPLIFIER. 4 Transistor Push-Pull Ready built with volume, treble and bass controls. 18 volt battery operated. £4-50



## THE "INSTANT" BULK TAPE ERASER & HEAD DEMAGNETISER.

Suitable for cassettes, and all sizes of tape reels. A.C. mains 200/250V. Leaflet S.A.E. £3-50 Post 20p



## WAFER HEATING ELEMENTS

OFFERING 1001 USES for every type of heating and drying applications in the home, garage, greenhouse factory (available in manufacturing quantities). Approx size 10 1/2 x 8 1/2 x 1/4 in. Operating voltage 200/250V. a.c. 250 watts approx. Printed circuit element enclosed in asbestos fitted with connecting wires. Completely flexible providing safe Black heat. British-made for use in photocopyers and print drying equipment.

Ideal for home handymen and experimenters. Suitable for Heating Pads, Food Warmers, Convector Heaters, etc. Must be clamped between two sheets of metal or asbestos, etc., to make efficient clothes dryers, towel rails—ideal for airing cupboards. Ideal for anti-frost device for the garage—preventing safe Black heat. British-made for use in photocopyers and print drying equipment.

Use in greenhouse for seed raising and plant protection. Invaluable aid for bird houses, incubators, etc., etc. Can be used in series for lower heat. Or in parallel for higher heat applications.

ONLY 40p EACH (FOUR FOR £1-50)  
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## BAKER MAJOR 12" £9-90



Post Free  
30-14,500 c/s, 12in. double cone, woofer and tweeter cone together with a BAKER ceramic magnet assembly having a flux density of 14,000 gauss and a total flux of 145,000 Maxwells. Bass resonance 40 c/s Rated 20 watts. NOTE: 3 or 8 or 15 ohms must be stated.

Module kit, 30-17,000 c/s with tweeter, crossover, baffle and instructions. £12-50 Post Free

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Robustly constructed to stand up to long periods of electronic power. As used by leading groups. Useful response 30-13,000 cps. Bass Resonance 55 cps.

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12in 25 watt  
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15in 50 watt  
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## MAJOR 100 WATT ALL PURPOSE TRANSISTOR AMPLIFIER

All purpose transistorised. Ideal for Groups, Disco and P.A. 4 inputs speech and music. 4 way mixing. Output 8/15 ohm a.c. Mains. Separate treble and bass controls. Guaranteed. Details S.A.E.



£49 Carr. £1-00

CALLERS ONLY! DE-LUXE 100 WATT AMPLIFIER CHASSIS. 7 Valve version, 4 inputs, 10 wide range controls. For Mixes, Discos, Organs, Guitars, etc. 4, 8 and 15 ohm Loudspeaker matching. £69

## Q MAX CHASSIS CUTTERS

A die, punch and Allen Screw	
Sizes 1" .....	74p
" 1 1/2" .....	83p
Key "A" for above 6p	
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" 2 1/2" .....	22-30
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20 Watt 100 ohm Rheostat 2 1/2 in dia. Ceramic former screw terminals 1/4 in dia. spindle. 95p. Post 25p.

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British made. Ready aligned and tested. Complete with instructions. Size 3in x 2in. £6-95

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P50/20C 40p	RAEW 85p
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## DELUXE 4 POLE MOTOR

1,400 r.p.m. reversible 42 Watt, spindle 1 1/2 in x 7/32 in, size 3 1/2 in x 3 in. As illustrated. 240V a.c. mains. £2-25 Post 25p

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120V or 240V a.c. 2,400 rpm. 2-pole 70mA. Size 2 1/2 x 2 1/2 x 2 1/2 in. £1-00 Post 25p

## BAKER HI-FI SPEAKERS HIGH QUALITY—BRITISH MADE REGENT

### 12in. 15 watts

An inexpensive unit for the beginner in high fidelity and for general purposes. May be used to improve any Radio, Amplifier, Hi-Fi or Television receiver.

Bass Resonance 45cps  
Flux Density 12,000 gauss  
Useful response 45-13,000cps  
3 or 8 or 15 ohm models.

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Especially designed to provide full range reproduction at an economical cost. Suitable for use with any high fidelity system. Built-in concentric tweeter cone.

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A high quality loudspeaker, its remarkable low cone resonance ensures clear reproduction of the deepest bass. Fitted with a special copper drive and concentric tweeter cone resulting in full range reproduction with remarkable efficiency in the upper register.

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### AUDITORIUM 12in. 25 watts

A full range reproducer for high power. Electric Guitars, public address, multi-speaker systems, electric organs, Ideal for Hi-Fi and Discos-theques.

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Flux Density 15,000 gauss  
Useful response 25-18,000cps  
8 or 15 ohms models.

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A high wattage loudspeaker of exceptional quality with a level response to above 8,000 cps. Ideal for Public Address, Discotheques, Electronic instruments and the home.

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Flux Density 15,000 gauss  
Useful response 20-14,000cps  
8 or 15 ohms models.

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Hi-Fi Enclosure Manual containing 20 plans, designs, crossover data and cubic tables. 42p. Post Free.

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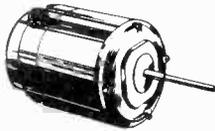
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Type SS15 These fine motors are easily reversed starting and stopping in less than 5 without electrical or mechanical braking. Simple relay circuit can

be applied to give DC to winding for a maximum holding torque of 300oz/in with 35v at 0.35 amps through winding. For AC (synchronous) operation at 120V, 50Hz. Speed 60 rpm at 60Hz, 72 rpm. STEPPING Holding torque at 50 steps per second—100 oz/in. Can be wired to give 100 or 200 steps per revolution with accuracy of 0.1° per step non-cumulative. Torque characteristics can be modified by simple R.C. circuits. Dimensions dia 4" body length 4 1/2" spindle length 2 1/2" dia Weight 6 1/2 lbs BRAND NEW in maker's packing. Offered at less than 1/2 maker's price.

OUR PRICE ONLY £15

### NORPLEX

Fibre-glass copper-clad laminate. Finest quality epoxy resin base. Heat resistant. Ideal for P.C.B. Size 12" x 12" 24" x 24" x 24" FULL SHEET 43" x 37" (11 sq ft). Single-sided Copper with thickness of 3/64". Also double-sided 3/64" x 3/64" £1 per sq ft. Cut sizes (1-10 sq ft) 25p P & P. Full Sheet £8 each. Carr £1 for 1st sheet plus 25p each additional sheet.



### SMITHS RINGER-TIMER

Reliable 15 minute times spring wound (concurrent with time setting) 15 x 1min divisions, approximately 1/2 between divisions. Panel mounting with chrome bezel 3 1/2" dia £1.40. 15p P & P.

### KNOWLE (U.S.A.) MINIATURE MICROPHONE CAPSULES

Impedance approx 200Ω output 60 or 80 DB at 1 Kc. As used in deaf aids, bugging device etc. Size (60 DB) 3/8" x 3/8" x 1/8" (80 DB) 1/2" x 1/2" x 1/8". Ex-equipment, all tested £1.20 each P & P FREE.

## Ultra PRECISION CENTRIFUGAL BLOWER by Air Control Ltd.



30 segments individually balanced in heavy cast alloy case. 2,300 r.p.m. 240 V a.c. Very powerful and silent running. 5 1/2" dia 3" Inlet dia. Outlet flange 3" x 2 1/2". Limited number only £8-95. P & P 40p.

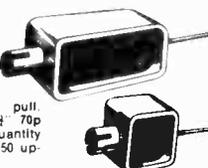
### MAINS SOLENOID

This little unit gives vertical lift of approximately 1" through hinged elbow. Bracket incorporates 2 fixing screws. Length of arm 2 1/2". 240V AC. Pull at coil is approximately 1lb. £1. FREE P & P. Special quotes for quantities.



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240AC type MM6 3lb pull. 2 1/2" x 1" x 1 1/2". Travel 1" 90p. each P & P 10p. 240AC type MM4 2lb pull. 1 1/2" x 1 1/2" x 1 1/2". Travel 1" 70p. each P & P 10p. Quantity discounts 10-50 10% 50 up-wards 25%.



### OPEN FRAME shaded pole GEARED MOTORS

(Dural gear case) 240 AC 28rpm NEW HIGH TORQUE, approx overall size 3 1/2" x 3 1/2" x 2 1/2". spindle 1/2" dia. as illustrated £2.70. P & P 30p. Similar to above. 19rpm £2.70. P & P 30p. 110rpm with pressed steel gear case (similar to above but SLIGHTLY SMALLER) £2.70. P & P 30p.



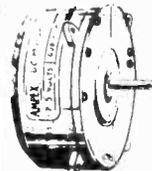
## SILVANIA MAGNETIC SWITCH

Now complete with reference magnet!



A magnetically activated switch, vacuum sealed in a glass envelope. Silver contacts, normally closed. Rated 3amp at 120v, 1amp at 240v. Size (approx) 1 1/2" long x 3/4" dia. Ideal for burglar alarms, security systems etc. and wherever non-mechanical switching is required. 10 for £2.10; P & P 15p. 50 for £8; 100 for £15.50. FREE P & P over 10.

## AMPEX 7.5V. D.C. MOTOR



An ultra precision tape motor designed for use in the AG20 portable recorder. Torque 450GM/CM. Stall load at 500ma. Draws 60ma on run. 600rpm = speed adjustment. Internal AF/RF suppression. 1/2" dia x 1" spindle. motor 3" dia x 1 1/2". Original cost £16.50. OUR PRICE £3.30. P & P 25p. Quantities available. Mu-metal enclosure available 75p each. FREE P & P.

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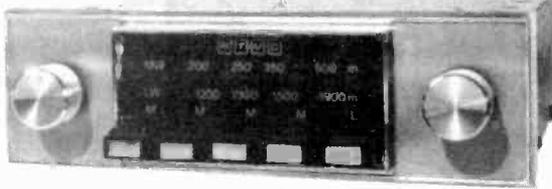
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# R T V C

## FOR AUDIO ON A BUDGET

### PUSH BUTTON CAR RADIO KIT

#### The Tourist II



**NO SOLDERING  
REQUIRED!**

#### NOW BUILD YOUR OWN PUSH BUTTON CAR RADIO

Easy to assemble construction kit comprising fully completed and tested printed circuit board on which no soldering is required. All connections are simple push fit type making for easy assembly. Fine tuning push button mechanism is fully built and tested to mate with printed circuit board.

Technical specification:

- (1) **Output** 4 watts R.M.S. output. For 12 volt operation on negative or positive earth.
- (2) **Integrated circuit** output stage, pre-built three stage IF Module.

Controls volume manual tuning and five push buttons for station selection, illuminated tuning scale covering full, medium and long wave bands.

Size chassis 7" wide, 2" high and  $4\frac{5}{16}$ " deep approx

**Car Radio Kit £7.70 + 55p. postage & packing**

**Speaker** including baffle and fixing strip **£1.65 + 23p. p&p.**

**Car Aerial** Recommended — fully retractable and locking

**£1.37 + 20p. postage & packing**

**Tourist Mk.1** kit still available—price **£6.60 + 55p. p & p.**

See July issue for full specification

## STEREO 21



### QUALITY SOUND<sup>(\*)</sup> FOR LESS THAN **£19.00**

Stereo 21 easy to assemble audio system kit. — no soldering required. Includes:—

**BSR 3 speed deck**, automatic, manual facilities together with ceramic cartridge.

**Two speakers** with cabinets.

**Amplifier module**. Ready built with control panel, speaker leads and full, easy to follow assembly instructions.

For the technically minded:—

**Specifications:**

Input sensitivity 600mV; Aux. input sensitivity 120mV; Power output 2.7 watts per channel; Output impedance 8–15 ohms. Stereo headphone socket with automatic speaker cutout.

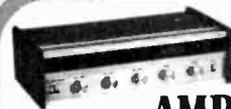
Provision for auxiliary inputs — radio, tape, etc., and outputs for taping discs. **Overall Dimensions**. Speakers approx.  $15\frac{1}{2} \times 8 \times 4$ ". Complete deck and cover in closed position approx.  $15\frac{1}{2} \times 12 \times 6$ ".

**Complete only £18.95**

**Extras if required.** £1.37 + £1.60 p & p.

Optional Diamond Styli **£1.37**

Specially selected pair of stereo headphones with individual level controls and padded earpieces to give optimum performance. **£3.85.**



### DISCO AMPLIFIER

Reliant Mk IV Mono Amplifier, ideal for the small disco or house parties.

Outputs 20 watts R.M.S. into 8 ohms (suitable for 15 ohms).

Inputs \* 4 Electrically Mixed Inputs \* 3

Individual Mixing controls. \*Separate bass and treble controls common to all 4 inputs

\*Mixer employing F.E.T. (Field Effect Transistors). \*Solid State Circuitry. \*Attractive Styling.

**INPUT SENSITIVITIES**

—Input—1.) Crystal mic. guitar or moving coil mic. 2, and 10 mV. (selector switch for desired sensitivity.—Inputs—2), 3), 4. Medium output

equipment—ceramic cartridge, tuner, tape recorder, organs etc.

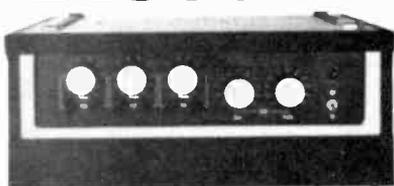
— all 250mV sensitivity.

AC Mains 240V. operation.

Size approx.  $12\frac{1}{2} \text{ ins} \times 6 \text{ ins} \times 3\frac{1}{2} \text{ ins}$

**£15.00 + 60p. post & pack**

## DISCO 50



### 45 WATT R.M.S. MONO DISCOTHEQUE AMPLIFIER

Ideal for Disco Work. Output Power: 45 watts R.M.S. Frequency

Response 3dB points 30Hz and 18KHz. Total Distortion: less than

2% at rated output. Signal to noise ratio: better than 60dB. Bass

Control Range: 13dB at 60Hz. Treble Control Range: 12dB at

10KHz. Inputs: 4 inputs at 5mV into 470K. Each pair of inputs

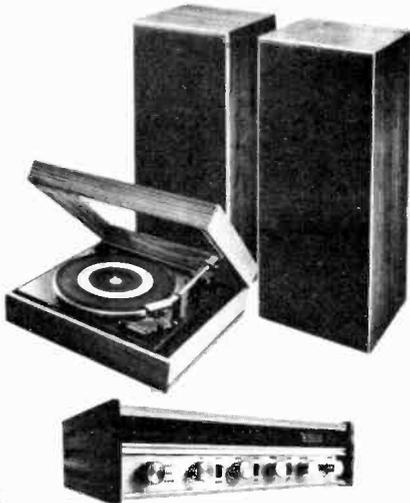
controlled by separate volume control. 2 inputs at 200mV into

470K. Size:  $19\frac{1}{2} \times 10\frac{1}{2} \times 8$  ins. approx. Amplifier **£27.50 + £1.50 p. & p**

**Special Offer:** Disco 50 plus two 15" E.M.I. speakers type 14A/780

(as illustrated on opposite page). **Complete £57.00 + £4.00 p&p.**

# COMPLETE(\*) STEREO SYSTEM



**£51.00**

**40 Watt Amplifier.**  
Viscount III - R102 now 20 watts per channel.  
System I includes:  
Viscount III amplifier - volume, bass, treble and balance controls, plus switches for mono/ stereo on/off function and bass and treble filters. Plus headphone socket.

**Specification**  
20 watts per channel into 8 ohms.  
Total distortion @ 10W @ 1kHz 0-1%. *P.U.1* (for ceramic cartridges) 150mV into 3 Meg. *P.U.2* (for magnetic cartridges) 4mV @ 1kHz into 47K. equalised within  $\pm 1$ dB R.I.A.A. *Radio* 150mV into 220K. (Sensitivities given at full power).  
Tape out facilities: headphone socket, power out 250mW per channel. *Tone controls and filter characteristics:* Bass: +12dB to -17dB @ 60Hz. Bass filter: 6dB per octave cut. Treble control: treble +12dB to -12dB @ 15kHz. Treble filter: 12dB per octave. *Signal to noise ratio:* (all controls at max.) -58dB.  
Crosstalk better than 35dB on all inputs.  
Overload characteristics better than 26dB on all inputs. Size approx. 13 $\frac{1}{2}$ " x 9" x 3 $\frac{1}{2}$ ".  
**Garrard SP25 deck**, with magnetic cartridge, de luxe plinth and hinged cover.  
**Two Duo Type II matched speakers** - Enclosure size approx. 17 $\frac{1}{2}$ " x 10 $\frac{1}{2}$ " x 6" in simulated teak. Drive unit 13" x 8" with parasitic tweeter 10 watts handling

**Complete System £51.00**

**£69.00**

**System II**  
Viscount III amplifier (As System I)  
Garrard SP. 25 (As System I)  
**Two Duo Type IIIA matched speakers** - Enclosure size approx. 31" x 13" x 11 $\frac{1}{2}$ ". Finished in teak veneer. Drive units approx. 13 $\frac{1}{2}$ " x 8 $\frac{1}{2}$ " with 3 $\frac{1}{2}$ " HF speaker. Max. power 20 watts, 8 ohms. Freq. range 20Hz to 20kHz.

**Complete System £69.00**

**PRICES: SYSTEM 1**  
Viscount III R102 amplifier £24.20 + £1 p & p  
2 Duo Type II speakers £14.00 + £2.20 p & p  
Garrard SP25 with MAG. cartridge de luxe plinth and hinged cover £21.00 + £1.75 p & p.  
total £59.20

**Available complete for only £51.00 + £3.50 p. & p.**

**PRICES: SYSTEM 2**  
Viscount R102 amplifier £24.20 + £1.00 p & p  
2 Duo Type IIIA speakers £39.00 + £4.00 p & p  
Garrard SP25 with MAG cartridge de luxe plinth and hinged cover £21.00 + £1.75 p & p.  
total £84.20

**Available complete for only £69.00 + £4 p. & p.**

## EMI SPEAKERS AT FANTASTIC REDUCTIONS



### 20 WATT SPEAKER SYSTEM

System consists of a 13" x 8" (approx) elliptical woofer unit with a 8" x 5" (approx.) mid range unit incorporating parasitic tweeter and crossover components.

#### Technical Specification:

**Bass Unit**  
Flux density-100 K, speech coil-1 $\frac{1}{2}$ ".  
Cone, Triple laminated paper with P.V.C. surround.  
**Mid Range Unit**  
Flux density-33K, speech coil-1" with parasitic tweeter.  
**Power Handling**  
20 watts R.M.S., impedance - 8 ohms, frequency response - 20 Hz to 18,000 Hz.

**OUR PRICE £6.60. Complete + 90p p & p.**

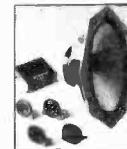


### 15" 14A/780 BASS UNIT

Bass unit on a rigid diecast chassis. Superior cone material handles up to 50 watts RMS, and is treated to give a smooth frequency response. Resonance 30 Hz. flux density 360,000 Maxwells. Impedance at 1 kHz is 8 ohms. 3" voice coil.

**Recommended retail price £40.80.**

**OUR PRICE £18.70 + £1.50 p & p + £1.50 p & p Special Offer.**



### 950 KIT

Five matched speakers and crossover unit for handling up to 45 watts, frequency response from 20 to 20,000 Hz. Huge 19" x 14" (approx.) high efficiency Bass-Speaker with 16,500-gauss magnet built on a heavy diecast frame. The four 10,000 gauss tweeters, each 3 $\frac{1}{2}$ " dia. approx., are fed by the crossover which critically adjusts signal for maximum fidelity. Impedance at 1 kHz is 8 ohms. Bass coil 2", others 0.5". Recommended list price £44.00.

**OUR PRICE £19.50**



## BUILD YOUR OWN STEREO AMPLIFIER(\*)

For the man who wants to design his own stereo - here's your chance to start with Unisound - pre-amp, power amplifier and control panel. No soldering - just simply screw together. 4 watts per channel into 8 ohms. Inputs: 120mV (for ceramic cartridge). The heart of Unisound is high efficiency I.C. monolithic power chips which ensure very low distortion over the audio spectrum. 240V. AC only.

**£7.64 + 55p. p & p**



## 8 TRACK CARTRIDGE PLAYER(\*)

Elegant self selector push button player for use with your stereo system. Compatible with Viscount III system, Unisound module and the Stereo 21

Technical specification Mains input. 240V, Output sensitivity 125mV  
Comparable unit sold elsewhere at £24.00 approx.

**Yours for only £10.95 + 90p. p & p**



Just write your order giving your credit card number  
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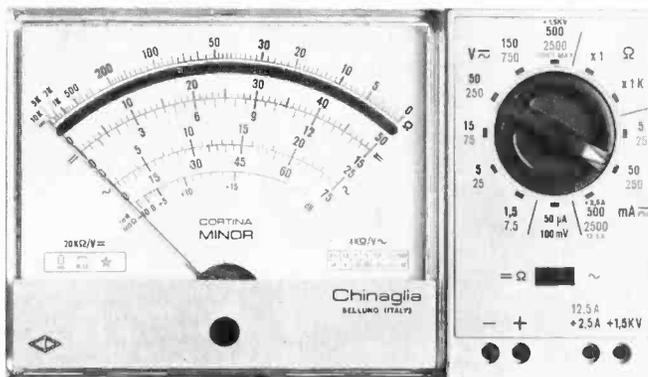


PROFESSIONAL QUALITY TEST EQUIPMENT FROM ONE OF ITALY'S LEADING MAKERS

One example from the big range of sophisticated instruments

**CORTINA MINOR**  
**33 RANGE POCKET MULTIMETER**

- SENSITIVITY 20,000Ω/VOLT (D.C.), 4,000Ω/VOLT (A.C.)
- ROBUST DIODE PROTECTED PRECISION MOVEMENT.
- 33 RANGES D.C. VOLTS 0-100mV, 1-5V, 5V, 15V, 50V, 150V, 500V, 1,500V, D.C. CURRENT 0-50μA, 5mA, 50mA, 500mA, 2.5A, A.C. VOLTS, 0-7.5V, 25V, 75V, 250V, 750V, 1,500V, A.C. CURRENT 0-25mA, 250mA, 2.5A, 12.5A, dB RANGES, -10 to +69, AF VOLTS RANGES 0-1,500V, RESISTANCE RANGES 10kΩ, 10MΩ F.S.D. CAPACITANCE RANGES 100μF, 1F F.S.D.
- ACCURACY—RESISTANCE, D.C. VOLTAGE AND CURRENT, 2-5%, A.C. VOLTAGE AND CURRENT 3-5%
- RESISTANCE RANGES POWERED BY INTERNAL BATTERIES.
- COMPACT SIZE: 150 x 85 x 40mm, 350gr.
- CLEARLY CALIBRATED DIAL WITH ANTI-PARALLAX MIRROR.
- PROFESSIONAL QUALITY COMPONENTS EMPLOYED THROUGHOUT.
- FULLY GUARANTEED FOR 12 MONTHS.
- AFTER SALES SERVICE AND SPARES FACILITIES.
- SUPPLIED WITH ADDITIONAL SHOCKPROOF PLASTICS CARRYING CASE, TWO HIGHLY INSULATED TEST LEADS AND INSTRUCTION BOOKLET.
- SPECIAL 30kV PROBE FOR D.C. MEASUREMENT AVAILABLE AS AN OPTIONAL EXTRA.



METER PRICE £15.40 (p & p 80p) PROBE £8.80 inclusive of V.A.T.

for further information on the "Cortina Minor" or other instruments from the exciting Chinaglia range write or telephone:—

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TRADE ENQUIRIES WELCOMED

**YATES ELECTRONICS**

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PLEASE ADD 10p TO ORDERS UNDER £2.

Catalogue sent free on request. 10p stamp  
appreciated

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**RESISTORS**

1/4W Iskra high stability carbon film—very low noise—capless construction  
1/4W Mullard CR25 carbon film—very small body size 7.5 x 2.5mm. 1/4W 2%  
ELECTROSIL TR5

Power watts	Tolerance	Range	Values available	Price
1/4	5%	4.7Ω-2.2MΩ	E24	1-3p
1/4	10%	3.3MΩ-10MΩ	E12	1-3p
1/4	2%	10Ω-1MΩ	E24	3-5p
1/4	10%	1Ω-3.9Ω	E12	1-3p
1/4	5%	4.7Ω-1MΩ	E12	1-3p
4	10%	1Ω-10Ω	E12	8p

Quantity price applies for any selection. Ignore fractions on total order.

**DEVELOPMENT PACK**

0.5 watt 5% Iskra resistors 5 off each value 4.7Ω to 1MΩ.  
E12 pack 325 resistors £2.40. E24 pack 650 resistors £4.70.

**POTENTIOMETERS**

Carbon track 5kΩ to 2MΩ, log or linear (log 1/2W, lin 1/2W).  
Single, 14p. Dual ganged (stereo), 49p. Single D.P. switch 28p.

**SKELETON PRESET POTENTIOMETERS**

Linear: 100, 250, 500Ω and decades to 5MΩ. Horizontal or vertical P.C. mounting (0.1 matrix).  
Sub-miniature 0-1W, 5p each. Miniature 0-25W, 7p each.

**SMOKE AND COMBUSTIBLE GAS DETECTOR—GDI**

The GDI is the world's first semiconductor that can convert a concentration of gas or smoke into an electrical signal. The sensor decreases its electrical resistance when it absorbs deoxidizing or combustible gases such as hydrogen, carbon monoxide, methane, propane, alcohol, North Sea gas, as well as carbon-dust containing air or smoke. This decrease is usually large enough to be utilized without amplification. Full details and circuits are supplied with each detector. Detector GDI, £2.

**SMOKE AND GAS DETECTOR KITS**

Mains operated with audible alarm, £5-60.  
Mains operated meter indicator, £7-90.  
Mains/battery gas leak detector, £12-60.  
12/24 battery operated, £8-40.  
12V battery operated two remote sensors, £12-80.

**NOTE**—The battery operated kits incorporate our patented circuit to minimise battery drain. Typically 120mA for 12V. These kits contain all parts required with the exception of case. Suitable case. Mains operated kit, £1-60. Battery operated kits, £5.

**MULLARD POLYESTER CAPACITORS C296 SERIES**

400V: 0.001μF, 0.0015μF, 0.0022μF, 0.0033μF, 0.0047μF, 3p, 0.0068μF, 0.01μF, 0.015μF, 0.022μF, 0.033μF, 3.3p, 0.047μF, 0.068μF, 0.1μF, 5p, 0.15μF, 6p, 0.22μF, 7.1p, 0.33μF, 11p, 0.47μF, 13p.  
160V: 0.01μF, 0.015μF, 0.022μF, 0.033μF, 0.047μF, 0.068μF, 3p, 0.1μF, 3.3p, 0.15μF, 4.1p, 0.22μF, 5p, 0.33μF, 6p, 0.47μF, 7.1p, 0.68μF, 11p, 1.0μF, 13p.

**MULLARD POLYESTER CAPACITORS C280 SERIES**

250V P.C. mounting: 0.01μF, 0.015μF, 0.022μF, 3p, 0.033μF, 0.047μF, 0.068μF, 3.3p, 0.1μF, 4p, 0.15μF, 5p, 0.22μF, 5p, 0.33μF, 6.1p, 0.47μF, 8.1p, 0.68μF, 11p, 1.0μF, 13p, 1.5μF, 20p, 2.2μF, 24p.

**MYLAR FILM CAPACITORS 100V**

0.001μF, 0.002μF, 0.005μF, 0.01μF, 0.02μF, 3p, 0.04μF, 0.05μF, 0.068μF, 0.1μF, 4p.

**CERAMIC DISC CAPACITORS**

100pF to 10,000pF, 2p each.

**ELECTROLYTIC CAPACITORS—MULLARD O15/617**

(μF/V) 1/63, 1.5/63, 2.2/63, 3.3/63, 4.7/63, 6.8/40, 8.8/63, 10/25, 10/63, 15/16, 15/40, 15/63, 22/10, 22/25, 22/63, 33/63, 33/16, 33/40, 47/4, 47/10, 47/25, 47/40, 68/63, 68/16, 100/4, 100/10, 100/25, 150/63, 150/16, 220/4, 220/63, 220/16, 330/4, 6p, 47/63, 100/40, 150/25, 220/25, 330/10, 470/63, 7p, 68/63, 150/40, 220/40, 330/16, 1,000/4, 10p, 470/10, 680/63, 11p, 100/63, 150/63, 220/63, 1,000/10, 12p, 470/25, 680/16, 1,500/63, 13p, 470/40, 680/25, 1,000/16, 1,500/10, 2,200/63, 18p, 330/63, 680/40, 1,000/25, 1,500/16, 2,200/10, 3,300/63, 4,700/4, 21p.

**SOLID TANTALUM BEAD CAPACITORS**

0.1μF 35V; 0.22μF 35V; 0.47μF 35V; 1.0μF 35V; 2.2μF 35V; 4.7μF 35V; 6.8μF 25V; 10μF 25V; 22μF 16V; 33μF 10V; 47μF 6.3V; 100μF 3V

**VEROBOARD**

24 x 33	0-1	0-15
26p	22p	22p
24 x 5	28p	28p
32 x 32	28p	28p
32 x 5	34p	34p
17 x 24	95p	77p
17 x 32	130p	108p
17 x 32 (plain)	36p	72p
17 x 24 (plain)	—	57p
24 x 5 (plain)	—	18p
24 x 32 (plain)	—	15p
Pin insertion tool	62p	62p
Sport face cutter	52p	52p
Pkt. 50 pins	20p	20p

**JACK PLUGS AND SOCKETS**

Standard screened	28p	2.5mm insulated	12p
Standard insulated	18p	3.5mm insulated	12p
Stereo screened	40p	3.5mm screened	18p
Standard socket	20p	2.5mm socket	10p
Stereo socket	30p	3.5mm socket	11p

**D.I.N. PLUGS AND SOCKETS**

2 pin, 3 pin, 5 pin 180°, 5 pin 240°, 6 pin, 7 pin  
Plug 12p, Socket 8p.  
4 way screened cable, 25p/metre.  
6 way screened cable 30p/metre.

**BATTERY ELIMINATOR**

£1-70  
9V mains power supply. Same size as PP9 battery.

**PRINTED BOARD MARKER**

97p  
Draw the planned circuit onto a copper laminate board with the P.C. Pen, allow to dry, then immerse the board in the etchant. On removal the circuit remains in high relief.

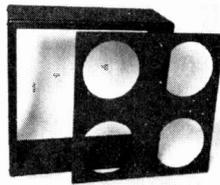
# CUSTOM CABINETS

328/30 The Banks, Rochester, Kent. Tel: Medway (0634) 404199

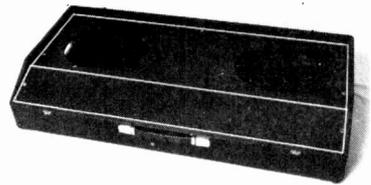
## SPEAKER CABINETS IN KIT FORM REPRESENT **HUGE SAVINGS**



2' x 12" Cabinet



4' x 12" Cabinet



Disco Console (includes lid not shown)  
Takes two slaves

For a long time now a large number of customers have asked us to produce cabinets in kit form, and above we show examples of cabinet styles and these are now available either fully built or in kit form ready for you to produce a professional finish in a very short time!

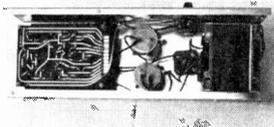
Kits are available in all specifications and all the kits contain everything you need as follows :-

- 1) 4 sides with handle cutouts, front edges rounded, 1 back with jack socket hole, and 1 baffleboard with speaker cutout
- 2) P.V.C. cut to size for frame and back, plus false front and back timbers, white front piping and speaker cloth
- 3) Recessed handles with fixing screws, jack socket, all fixing screws, corner plates, glue, and full instructions!

### PRICE & TYPE LIST

Type	Size	Price manufactured	Kit price
2 x 12" (illustrated above)	36" x 18" x 13" x 3/4"	£19.50	£12.50
4 x 12" (illustrated above)	31" x 31" x 13" x 3/4"	£24.50	£17.50
4 x 12" P.A. Column	48" x 27" x 13" x 3/4"	£30.00	£21.50
1 x 18"	31" x 31" x 13" x 3/4"	£24.50	£17.50
1 x 15" with two top horn cutouts	36" x 20" x 13" x 3/4"	£21.00	£13.50
Mini Disco (state deck cutout BSR, GARRARD etc.)	33" x 20" x 8" x 1/2"	£20.00	£13.00
Maxi Disco (illustrated) (state deck cutout BSR, GARRARD etc.)	42" x 20" x 10" x 1/2"	£25.00	£18.50

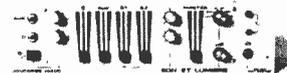
Please ask for quotation on any other type or size of cabinet you may require.



- \* 100 w RMS slave amp for Disco
- \* 100 w RMS continuous sine wave output
- \* Short and open circuit protection
- \* Built to highest industrial spec.
- \* Price £37.00 complete



- \* Stereo studio disco mixer
- \* Full PFL and Monitor facilities
- \* As used by John Peel, Mark Wesley, Paul Burnett, DLT, Dave Christian, Tony Prince
- \* Price £120.00

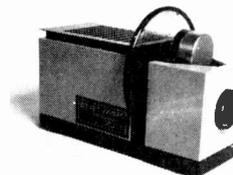


- \* Concorde mono M400 mixer
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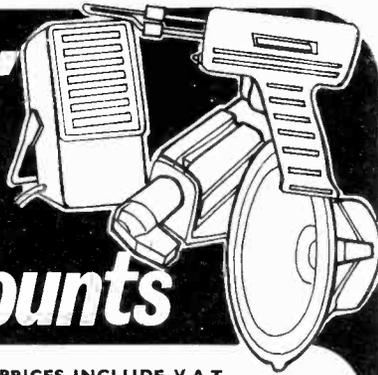
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EMI 13in x 8in 3, 8 or 15 ohm			GOODMANS 6in 8 ohm Dual cone	2-15
Plain	2-05		FANE, 7in x 4in, 3 or 8 ohm	1-00
With Co-Axial Tweeter	2-20		CELESTION 8in, 15 ohm	1-65
Twin Tweeter	3-70		ADASTRA 10in, 8 or 15 ohm.	10-40
Type 350, 8 ohm, 20W	7-50		10W	3-45
6in, 8 ohm, 10W	2-40		BAKER GROUP 25 12in, 8 or 15 ohm, 25W	7-50
8in, 8 ohm, 10W	3-75		5in, 8 ohm, C/Mag.	0-85
12in, 8 ohm, 20W	5-70		24in, 8 ohm or 64 ohm	0-50
Cone 5in, C/Mag. 5W	1-25		P. & P.	0-15
8in x 5in. Dual cone 8 ohm, 10W	2-45			
ELAC 8in 8 ohm Dual cone	2-25			

TWEETER AND CROSSOVER		£	Dome Tweeter 8 ohm, 30W	5-40
EMI 3 1/2in, 3 or 8 ohm C/Mag.	1-00		Crossovers CN23 (3 ohm), CN28 (8 ohm), CN216 (16 ohm)	1-10
Cone Tweeter 8 or 15 ohm, 10W	2-40		P. & P.	0-15
Cone Tweeter 8 ohm, 3W	1-45			
Horn Tweeter 8 ohm, 20W	6-40			

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VEENER, 12in x 12in x 6in with 8in, 8in x 6in or 6in and 3 1/2in cutout	2-45		18in x 11in x 9in with 13in x 8in cutout for EMI 350	4-25
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CM70 Planet stick metal, switch crystal	1-55		CONDENSER MIKE 600 ohm, uni-dir	9-85
DM160 Dynamic omni-dir, ball metal	3-85		Cassette Stick Mike with E. Control on/off switch (2-5 and 3-6mm J/Ply)	1-45
UD130 50K/600 ohm, uni-dir, ball metal	5-75		P. & P.	0-20

SOLDERING IRONS		£	spare Bib, etc.)	3-30
ANTEX CN240 15W	1-90		X25 25W (low leakage)	1-90
SKI Kit (15 watt iron, 2			P. & P.	0-10

CARTRIDGES		£	SX6H Stereo crystal <th>1-70</th>	1-70
ACOS GP91/38C or GP91/38C Stereo comp	1-00		SX6M Stereo crystal	1-70
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GP94/1 Stereo crystal	1-85		X5M Mono/stereo	1-40
GP95/1	1-35		GOLDRING G800	3-85
GP96/1	1-65		G850	2-95
GP101	0-80		G800E	7-15
GP104	1-65		STYLL FOR ABOVE P. & P.	0-10
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			P. & P.	0-05

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240V input 6, 7.5 or 9 300mA 12V d.c. input (please specify	2-75		P. & P.	0-15

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5in	50p	65p	85p	85p	P. & P. 1-3 each			0-09
5 1/2in	65p	80p	1-15p	4 or more lot				0-30

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C60	1-5	6-10	11-20	P. & P. 1-5 each	0-03
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PLASTIC LIBRARY CASES for		£	7in Reels	0-25
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Sub-miniature Axial lead electrolytic

Mfd	V	Price	Mfd	V	Price
1	63	6p	68	6.3	6p
1.5	63	6p	68	16	6p
2.2	63	6p	68	63	10p
3.3	63	6p	100	4	6p
4.7	63	6p	100	10	6p
6.8	40	6p	100	25	6p
6.8	63	6p	100	40	6p
10	25	6p	100	63	12p
10	63	6p	150	6.3	6p
15	16	6p	150	16	6p
15	40	6p	100	25	6p
15	63	6p	150	40	6p
22	10	6p	150	63	12p
22	25	6p	220	4	6p
22	63	6p	220	10	6p
33	6.3	6p	220	16	6p
33	16	6p	220	25	10p
33	40	6p	220	40	12p
47	4	6p	220	63	18p
47	10	6p	330	4	6p
47	25	6p	330	10	6p
47	40	6p	330	16	10p
47	63	6p	330	63	22p
47	63	6p	330	63	22p

## PLUGS AND SOCKETS



Item	Price	Item	Price
DIN PLUGS		RSR way chassis socket	68p
2 pin (1 flat)	8p	P360 3 pin 1.5A chassis plug with line socket	2p
3 pin	8p	Per pair	2p
4 pin	5 pin	SA 2190 3 pin 5A chassis plug	20p
(180°)	5 pin	SA 1862 Line socket for above	23p
(240°)	6 pin	10p	
DIN Sockets		JACK	
2 pin	6p	Std. 1/2" mono plug	13p
3 pin	4 pin	RPR 8 way chassis plug	52p
A (180°)	5 pin	Std. 1/2" stereo plug	18p
(240°)	7p	6 pin	9p
		Screened	21p
		Open socket	8p

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Rotary with adjustable stop 1 pole 2 to 12 way; 2 pole 2 to 6 way; 3 pole 2 to 4 way; 4 pole 2 or 3 way, each 32p.	
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Slide Sub-miniature DPDT 9p	
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High quality "sub-miniature" toggle switches.	
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PP3, 6, etc., battery clip dual min. 9p.	
PP1, 9, etc., battery clip separate per pair 6p.	
Pair crocodile clips, 1 red, 1 black insulated sleeve 10p.	
Solder Multicore 22 s.w.g. 10 metres 25p.	
Silicone grease in special dispenser 20ml 54p.	
Terminal Block 12-way 5A 14p.	
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Transformers	
LT700 min. output transformer Pri. 1.2kV Sec. 5.0 200mW 50p.	
Sub-main, Mains Transformer 6-0-6V 100mA 95p, 12-0-12V 50mA 95p.	
Size: Both approx. 30 x 27 x 25mm.	
Min. Mains Transformer Size: 46 x 31 x 38mm 0-12V 250mA 0-12V 250mA £1.36.	
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Mains Transformer MT206AT Pri. 200-220-240V Sec. 0-15-20V 1A 0-15-20V 1A £3.98.	
Hook-up wire, 7 strand 0.2mm PVC covered tinned copper wire for light general connexions up to 1.4A. 11 colours: black, blue, brown, green, grey, orange, pink, red, violet, white, yellow. 10 metres of any one colour 20p. Pack of 11 (1 of each colour) 10m coils £2.05.	
Single core screened 8p per metre.	
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High quality single screened 50n 100pF per metre, ideal for high grade audio connexions 154p per metre.	
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Rotary miniature carbon track 1/2" spindle	
Single gang Lin or Log 5k, 10k, 25k, 50k, 100k, 250k, 500k, 1M, 2M (and 1k Lin) 14p	
Dual gang (Stereo) without switch Log or Lin 5k to 2M as above 44p	
Single gang with DP switch 250V 2A Log or Lin 5k to 2M as above 29p	
PRESETS	
Sub-miniature 0-1W Vert or Horiz 100, 250, 500, 1k, 2.5k, 5k, 10k, 25k, 50k, 100k, 250k, 500k, 1M 6p	

## RESISTORS

Carbon Film 1/4W 5% 1Ω to 1M; 10% 1.2M to 10M E12 1p	
Carbon Film 1/4W 5% 1Ω to 10Ω; 10% 1.2M to 10M E12 1p	
Carbon Film 1/4W 5% 11Ω to 910k E12 & E24 1p	
Carbon Film 1W 5% 10Ω to 10M E12 3p	
Metal Oxide 1/4W 9% 10Ω to 1M E12 & E24 4p	
Wirewound 2 1/2W 10% 0.2ohms to 0.47ohms E12 12p	
Wirewound 2 1/2W 5% 1ohm to 270ohms E12 12p	
E12 values 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 and decades	
E24 values 11, 13, 16, 20, 24, 30, 36, 43, 51, 62, 75, 91 and decades	

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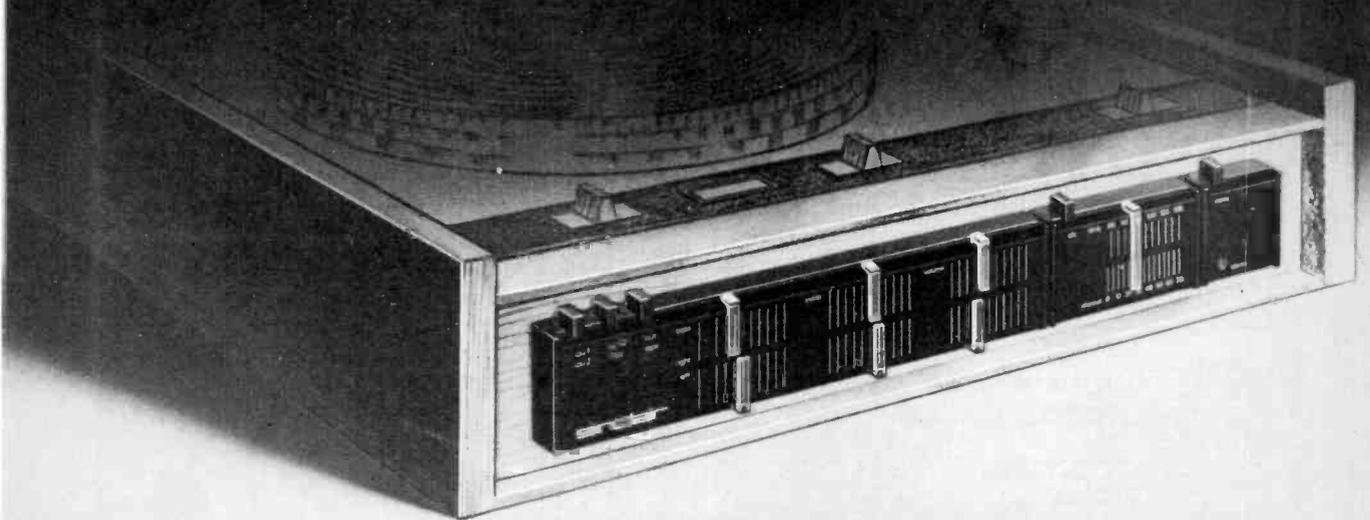
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a brilliant new concept in modular hi-fi



Project 80 is going to be the ultimate in modular hi-fi construction for a very long time to come. It combines the qualities most demanded of any modern domestic system – good circuitry, reliability and fine performance – with other features to be found nowhere else in the world. For example,

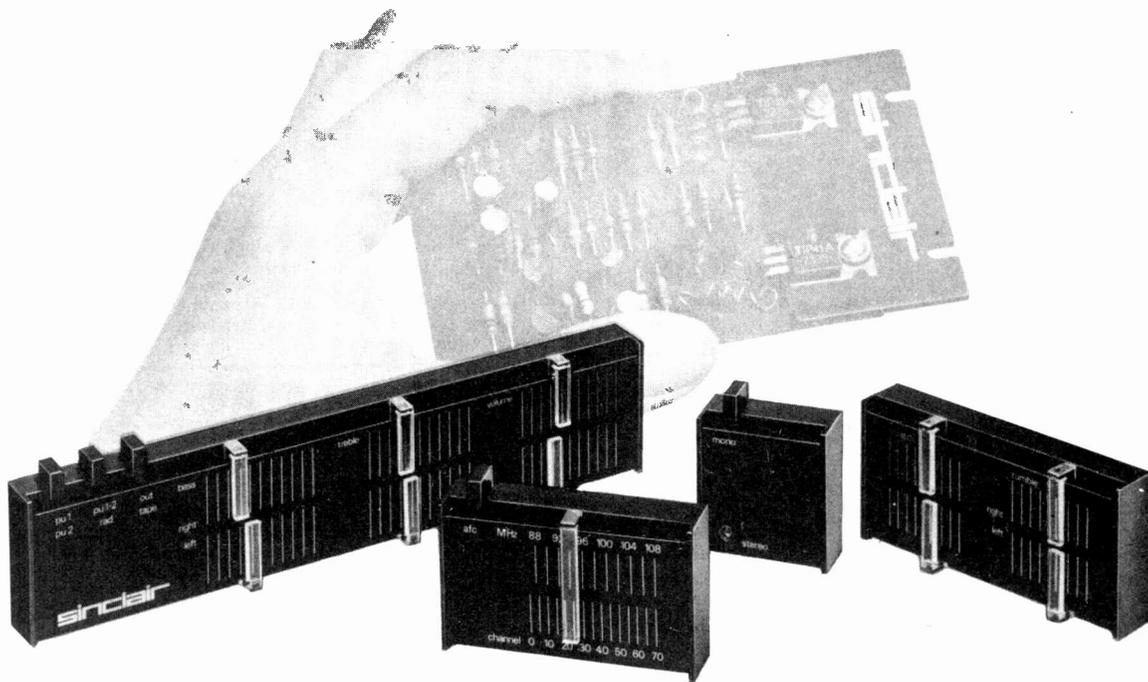
*compactness* – Project 80 control units are  $\frac{3}{4}$ " deep  $\times$  2" high, and each one is completely self-contained.

*Elegance* – all of Sinclair's design leadership has been concentrated on producing designs of outstanding functional elegance unsurpassed for styling and simplicity. *Flexibility* –

the size and styling of Project 80 modules makes them the most versatile units ever. Combine them how you will, where you will, the Project 80 System of your choice gives you the best.

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# Sinclair Project 80



## technically the world's most advanced

Project 80 gives you choice from a range of 9 different modules for combining in a variety of ways to suit your requirements. The Stereo 80 is a versatile pre-amp control unit designed to meet all domestic hi-fi requirements including tape monitoring, high sensitivity magnetic cartridge input, and of course, individual slide controls on each channel for precise output matching. By separating the F.M. tuner and stereo decoder, useful economies can be effected where stereo radio reception is not needed. Two power amplifiers – Z.40 (18 watts RMS continuous into 4 ohms using 35V) and Z.60 (25 watts RMS continuous into 8 ohms using 50V) are available with choice of 3 different power supply units. The PZ.8 with its virtually indestructible circuitry is particularly recommended. For the final word in system building, the Active Filter Unit puts the finishing touch of quality to what are easily the world's most technically advanced hi-fi modules. Any further units likely to be added to Project 80 range will be compatible with those already available.

### Guarantee

If, within 3 months of purchasing any product direct from us, you are dissatisfied with it, your money will be refunded on production of receipt of payment. Many Sinclair appointed stockists also offer this guarantee. Should any defect arise in normal use, we will service it without charge.

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Sinclair Radionics Ltd  
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Huntingdon PE17 4HJ  
Telephone  
St Ives (0480) 64646

### Stereo 80 Control Unit

Size – 260 · 50 · 20mm (10½ · 2 × ¾ins)  
Finish – Black with white indicators and transparent sliders  
Inputs – Magnetic pick up 3mV RIAA corrected. Ceramic pick-up 350mV Radio 100mV. Tape 30mV  
Signal/noise ratio – 60db Frequency range – 20Hz to 15KHz  
-1dB, 10Hz to 25KHz + 3dB Power requirements – 20 to 35 volts  
Outputs – 100mV · AB monitoring for tape Controls – Press button tape radio and P.U  
Sliders on each channel for volume bass treble R R P £11.95  
(add £1 19 V A T)

### Project 80 FM Tuner

Size – 85 · 50 · 20mm (3½ · 2 · ¾ins)  
Tuning range Dual varicap – 87.5 to 108MHz Detector – I.C. balanced coincidence  
One I.C. equal to 26 transistors Distortion – 0.2% at 1KHz for 30% modulation  
4 pole ceramic filter in I.F. section Aerial impedance – 75 Ω or 240 · 300 Ω  
Sensitivity – 5 microvolts for 30dB S/N ratio Output – 300mV for 30% modulation  
Power requirements – 25 to 35 volts R R P £11.95  
(R R P add £1 19 V A T)

### Project 80 Stereo Decoder

Size – 47 · 50 · 20mm (1¾ · 2 · ¾ins)  
One 19 transistor I.C. Channel separation greater than 30dB Power requirements – 25V Output 150mV per channel R R P £7.45  
(add 74p V A T)

### Active Filter Unit

Separate controls on each channel Size – 108 · 50 · 20mm (4½ · 2 · ¾ins)  
Voltage gain – minus 0.2dB Frequency response – 40Hz to 22KHz controls minimum Distortion – at 1KHz – 0.03%  
using 30V supply H.F. cut off (scratch) – 22 KHz to 5.5KHz 12dB/oct slope  
L F cut off (rumble) – 28dB at 20Hz, 9dB/oct slope R R P £6.95  
(add 69p V A T)

### Z.40 Power Amplifier

Size – 55 · 80 · 20mm (2½ · 3½ · ¾ins) 9 transistors  
Input sensitivity – 100mV Output 18 watts RMS continuous into 4 Ω (35V)  
Frequency response 30Hz 100KHz · 3dB S/N ratio – 64dB Distortion – at 10 watts into 8 Ω less than 0.1%  
Power requirements – 12 to 35 volts, built in protection against overload R R P £5.40  
(add 54p V A T)

### Z.60 Power Amplifier

Size – 55 · 98 · 15mm (2½ · 3¾ · ¾ins) 12 transistors  
Input sensitivity – 100 250mV Output – 25 watts RMS continuous into 8 Ω (50V)  
Distortion – typically 0.03% Frequency response – 15Hz to more than 200KHz · 3dB S/N ratio – better than 70dB  
Built in protection against transient overload and short circuiting Load impedance 4 Ω min. safe on open circuit R R P £6.95  
(add 69p V A T)

### Power Supply Units PZ.8

Stabilised Re-entrant current limiting makes damage from overload or even direct shorting impossible. Normal working voltage (adjustable) 50V R R P £7.98 · 79p V A T Without mains transformer PZ.6 35V stabilised R R P £7.98 · 79p V A T PZ.5 30V un-stabilised R R P £4.98 · 49p V A T

To Sinclair Radionics Ltd, St. Ives Huntingdon PE17 4HJ

Please send post paid \_\_\_\_\_

for which I enclose Cash/Cheque for £ \_\_\_\_\_ including V A T \_\_\_\_\_

Name \_\_\_\_\_

Address \_\_\_\_\_

PE8

# TRANSFORMERS

**SAFETY MAINS ISOLATING TRANSFORMERS**  
Prim. 120/240V. Sec 120/240V Centre Tapped and Screened  
ALSO AVAILABLE WITH 115/120V SEC. WINDING

Ref. No.	VA (Watts)	Weight lb oz	Size cm.	P & P £ p
07	20	1 8	7.0 x 6.0 x 6.0	2.35 30
149	60	3 12	9.9 x 7.7 x 8.6	3.79 36
150	100	5 8	9.9 x 8.9 x 8.6	4.17 52
151	200	8 0	12.1 x 9.3 x 10.2	7.39 52
152	250	13 12	12.1 x 11.8 x 10.2	9.25 67
153	350	15 0	14.0 x 10.8 x 11.8	11.35 82
154	500	19 8	14.0 x 13.4 x 11.8	13.20 *
155	750	29 0	17.2 x 14.6 x 14.0	21.20 *
156	1000	38 0	17.2 x 16.6 x 14.0	27.40 *
158	2000	60 0	21.6 x 15.3 x 18.1	49.25 *

## AUTO TRANSFORMERS

Ref. No.	VA (Watts)	Weight lb oz	Size cm.	Auto Taps	P & P £ p
113	20	1 0	5.8 x 5.1 x 4.5	0-115-210-240	1.34 22
64	75	2 4	7.0 x 6.7 x 6.1	0-115-210-240	2.64 30
4	150	3 4	8.9 x 7.7 x 7.7	0-115-200-220-240	3.18 36
66	300	6 4	9.9 x 9.6 x 8.6	...	6.19 52
67	500	12 8	12.1 x 11.2 x 10.2	...	8.33 67
84	1000	19 8	14.0 x 13.4 x 14.3	...	13.50 82
93	1500	30 4	14.0 x 15.9 x 14.3	...	17.50 *
95	2000	32 0	17.2 x 16.6 x 14.0	...	25.35 *
73	3000	40 0	21.6 x 13.4 x 18.1	...	32.80 *

## CASED AUTO TRANSFORMERS

115 500W enclosed transformer, with mains lead and two 115V outlet sockets. £9.49, P & P 67p. 20W version, £2.02, P & P 22p.

## LOW VOLTAGE SERIES (ISOLATED)

Ref. No.	Primary Amps	Weight lb oz	Size cm.	Secondary Windings	P & P £ p
111	0.5	0.25	8	4.8 x 2.9 x 3.5 0-12V at 0.25A x 2	1.34 22
213	1.0	0.5	1 4	6.1 x 5.8 x 4.8 0-12V at 0.5A x 2	1.58 22
71	2	1 12	7.0 x 6.4 x 6.1 0-12V at 1A x 2	2.09 22	
18	4	2 12	8.3 x 7.7 x 7.0 0-12V at 2A x 2	2.95 36	
70	6	3 8	8.9 x 8.0 x 7.7 0-12V at 3A x 2	3.52 42	
108	8	4 8	9.9 x 8.9 x 8.6 0-12V at 4A x 2	3.96 52	
72	10	5 6	9.9 x 8.9 x 8.6 0-12V at 5A x 2	4.67 52	
116	12	6 12	9.9 x 10.2 x 8.6 0-12V at 5A x 2	5.61 52	
17	16	8 8	12.1 x 9.9 x 10.2 0-12V at 8A x 2	7.22 52	
115	20	10 11	14.0 x 9.6 x 11.8 0-12V at 10A x 2	9.20 67	
187	30	15 15	14.0 x 12.1 x 11.8 0-12V at 15A x 2	16.94 82	
226	60	30 32	17.2 x 15.3 x 14.0 0-12V at 30A x 2	22.50 *	

## 30 VOLT RANGE

Ref. No.	Amps	Weight lb oz	Size cm.	Secondary Taps	P & P £ p
112	0.5	1 4	6.1 x 5.8 x 4.8	0-12-15-20-24-30V	1.56 22
79	1.0	2 4	7.0 x 6.7 x 6.1	...	2.11 36
3	2.0	3 4	8.9 x 7.7 x 7.7	...	3.18 36
20	3.0	4 8	9.9 x 8.3 x 8.6	...	3.96 42
21	4.0	6 4	9.9 x 8.6 x 8.6	...	4.67 52
51	5.0	6 12	12.1 x 8.6 x 10.2	...	5.67 52
117	6.0	8 0	12.1 x 9.3 x 10.2	...	6.94 52
88	8.0	12 0	12.1 x 11.8 x 10.2	...	9.00 67
89	10.0	13 12	14.0 x 10.2 x 11.8	...	11.36 67

## 50 VOLT RANGE

Ref. No.	Amps	Weight lb oz	Size cm.	Secondary Taps	P & P £ p
102	0.5	1 12	7.0 x 6.4 x 6.1	0-19-25-33-40-50V	2.09 30
103	1.0	2 12	8.3 x 7.4 x 7.0	...	3.08 36
104	2.0	5 8	7.9 x 8.9 x 8.6	...	4.26 42
105	3.0	6 12	9.9 x 10.2 x 8.6	...	5.79 52
106	4.0	10 0	12.1 x 10.5 x 10.2	...	7.69 52
107	6.0	12 0	14.0 x 10.2 x 11.8	...	11.38 67
118	8.0	18 0	14.0 x 12.7 x 11.8	...	12.40 97
119	10.0	25 0	17.2 x 12.7 x 14.0	...	18.62 *

## 60 VOLT RANGE

Ref. No.	Amps	Weight lb oz	Size cm.	Secondary Taps	P & P £ p
124	0.5	2 4	7.0 x 6.7 x 6.1	0-24-30-40-48-60V	2.12 36
126	1.0	3 4	8.9 x 7.7 x 7.7	...	2.97 36
127	2.0	6 4	8.9 x 9.6 x 8.6	...	4.67 42
125	0	6 12	12.1 x 9.9 x 10.2	...	7.11 52
123	4.0	13 12	12.1 x 11.8 x 10.2	...	9.20 67
40	5.0	12.00	14.0 x 10.2 x 11.8	...	10.83 67
120	6.0	15 8	14.0 x 12.1 x 11.8	...	13.35 82
121	8.0	25.00	14.0 x 14.7 x 11.8	...	15.01 *
122	10.0	25 0	17.2 x 12.7 x 14.0	...	19.60 *
189	12.0	29.00	17.2 x 14.0 x 14.0	...	21.60 *

## MINIATURE TRANSFORMERS WITH SCREENS

Ref. No.	mA	Weight lb oz	Size cm.	Volts	P & P £ p
238	200	2	2.8 x 2.6 x 2.0	3-0-3	1.44 10
212	1A, 1A	1 4	6.1 x 5.8 x 4.8	0-6, 0-6	1.67 22
13	100	4	3.9 x 2.6 x 2.9	9-0-9	1.22 10
235	330, 330	4	4.8 x 2.9 x 3.5	0-9, 0-9	1.27 10
207	500, 500	1 00	6.1 x 5.4 x 4.8	0-8.9, 0-8.9	2.23 22
208	1A, 1A	1 12	7.0 x 6.4 x 6.1	0-8.9, 0-8.9	3.00 30
236	200, 200	4	4.8 x 2.9 x 3.5	0-15, 0-15	1.67 10
214	300, 300	1 4	6.1 x 5.8 x 4.8	0-20, 0-20	1.76 22
221	700 (d.c.)	1 8	7.0 x 6.1 x 6.1	20-12-0-12-20	1.55 30
206	1A, 1A	2 12	8.3 x 7.7 x 7.0	0-15-20, 0-15-20	4.05 38
203	500, 500	2	8.3 x 7.0 x 7.0	0-15-27, 0-15-27	3.10 38
204	1A, 1A	3 4	8.9 x 7.7 x 7.7	0-15-27, 0-15-27	3.15 38

\*Carriage via B.R.S.

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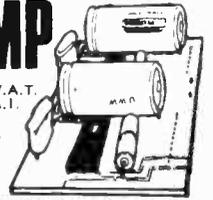


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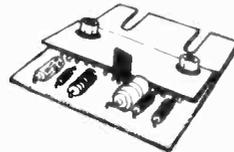
incl. P. & P. and V.A.T. Order Code I.C.A.1.



On P.C. Board with all components or 2 on one board for £2.86. Order Code I.C.A.1/S.

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ACY39	55p	BCY72	25p	MH1613	43p	OC81	25p	IN659	4p	2N3225	95p
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AD161	40p	BD131	75p	(2N5457)	35p	OC140	30p	IN4002	8p	2N3705	12p
AD162	40p	BD132	75p	MPF104	45p	OC170	25p	IN4003	8p	2N3706	12p
AF114	25p	BD153	75p	(2N5458)	35p	OC171	30p	IN4004	10p	2N3707	12p
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BC107	12p	BFY08	30p	NKT773	30p	TIP41A	75p	2N1132	25p	2N4060	12p
BC108	12p	BFY10	35p	NKT774	25p	TIP42A	90p	2N1302	16p	2N4061	12p
BC109	12p	BFY40	50p	OA5	20p	TIP29B	50p	2N1303	18p	2N4080	12p
BC146	12p	BFY51	25p	OA10	20p	TIP30B	60p	2N1304	25p	2N4126	17p
BC148	12p	BFY52	25p	OA17	20p	TIP31B	70p	2N1305	25p	2N4286	15p
BC149	12p	BFY52	25p	OA70	12p	TIP32B	82p	2N1306	25p	2N4287	15p
BC153	15p	BFY53	25p	OA79	12p	TIP33B	£1-12	2N1307	25p	2N4288	15p
BC157	14p	BFY90	80p	OA8	10p	TIP34B	£1-88	2N1308	25p	2N4289	15p
BC158	15p	BSW63	85p	OA80	10p	TIP35B	£2-81	2N1309	25p	2N4290	15p
BC159	15p	BSW68	80p	OA91	10p	TIP36B	£3-04	2N1613	25p	2N4444	£1-80
BC169C	14p	BSY95A	12p	OA200	10p	TIP41B	83p	2N1711	25p	2N4871	35p
BC182	14p	C111	50p	OA202	10p	TIP42B	98p	2N2147	70p	2N4920	80p
BC183	14p	C206	40p	TIP30C	71p	2N2160	75p	2N5191	60p	2N5192	60p
BC184	14p	BY100	20p	OA211	36p	TIP30C	78p	2N2217	70p	2N5193	60p
BC212	14p	BY126	20p	OC16	80p	TIP31C	85p	2N2218	25p	40360	50p
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AB13	6
AB14	7
AB15	8
AB16	10
AB17	10
AB18	12
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TRANSFORMER  
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PIN INS TOOL	72p	72p
SP F CUTTER	52p	52p
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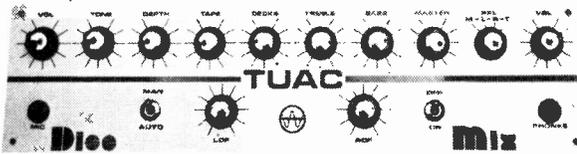
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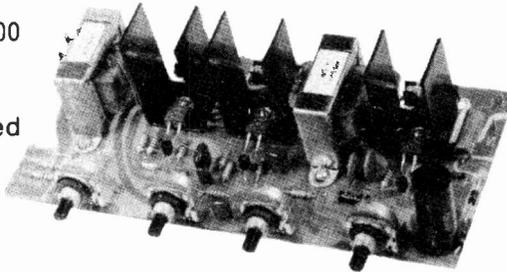
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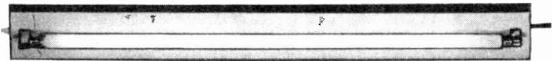
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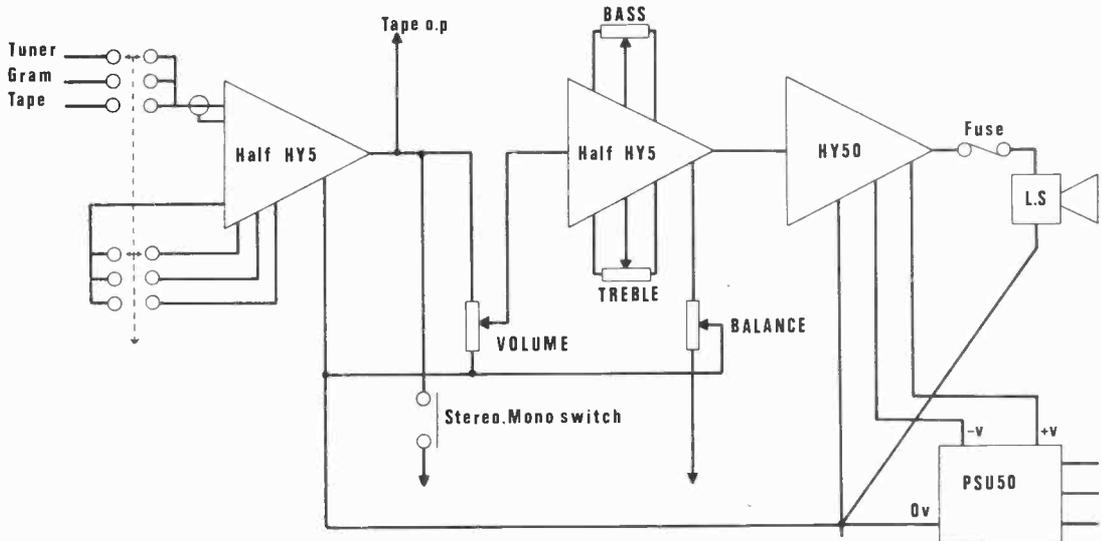
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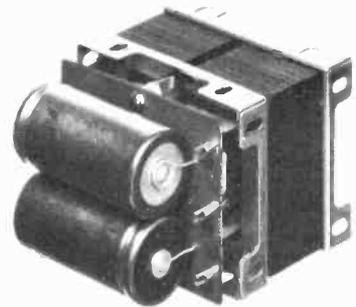
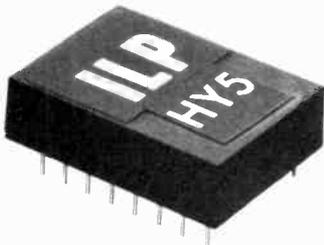


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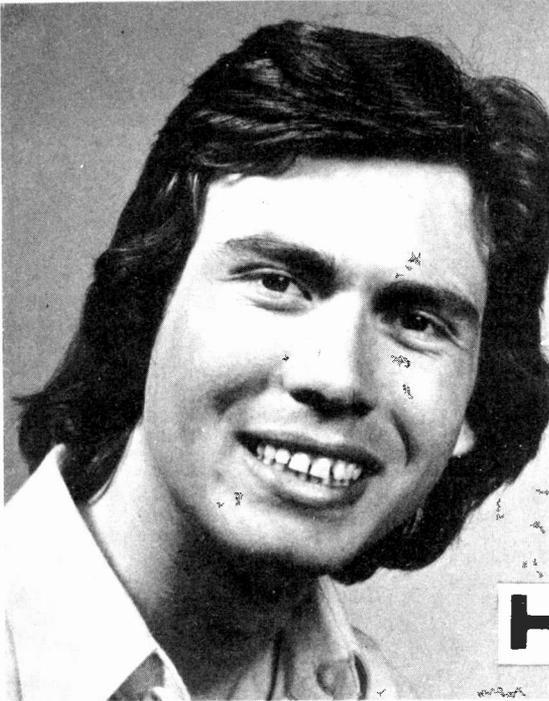
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## SORRY FOR THE DELAY

**F**IRST a word or two of explanation and apology. Like our weather this summer, the economic and industrial climate has been unsettled and changeable over the whole country. And the Publishers of this magazine have had their share of problems, as many readers will have guessed. We can only apologise to all our readers and advertisers who regularly support us for any disappointment, perplexity and inconvenience they may have experienced by the delayed appearance of some recent issues of PRACTICAL ELECTRONICS.

Because of continuing production problems erratic publication dates must be expected for the next few issues, also. But we hope soon everything will be restored to normal. In the meantime, while writing, we have to admit not knowing just when this particular issue will appear on the book-stalls. It may be during the second half of August, but more probably during the first half of September (yes, we did try ESP, but alas to no avail).

## A NEW SEASON—AND A NEW VIEW

In any event, September is a significant turning point in the year so far as hobbies are concerned. It is a month when those typically summer activities start to fade and become overshadowed by the different prospects that lie just ahead for the autumn and winter—the period when indoor activities really come into their own. Now the electronics constructor faces his most productive period of the year and starts to think again of projects long intended, but not so far realised. A foraging amongst back numbers of periodicals probably brings to light some design ear-marked long ago for the earliest possible attention. And there is the constant flow of new ideas that come from sources such as this magazine regularly each month (normal conditions prevailing).

Some constructors like a reasonably large and involved project to get their teeth into, and something which will keep them usefully occupied over several months. This kind of need will be satisfied in many instances by the P.E. Closed Circuit Television Camera. Although CCTV systems are common enough in commercial and industrial fields, this particular type of instrument has not yet come into general use. Since most homes possess the necessary monitor in the form of the normal TV set, it is a pity that a private, personal CCTV facility is not more readily available. With our specially commissioned design for a camera, this does now become a reasonable and economic proposition for the average constructor, and permits him to extend his technical knowledge and experience by acquiring new skills in video work which can be applied to instruct or entertain his own family or circle of friends, in a multitude of ways.

Of course, some constructors prefer smaller and less complicated designs. We don't neglect or ignore them. There is always a wide choice of subjects in P.E. each month.

Whatever the individual choice may be, of this there is no doubt: by becoming immersed in his hobby the electronics constructor can forget for a while some of the more gloomy news which seems to provide a constant background to present day affairs.

F.E.B.

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# PE CCTV MONOCHROME CAMERA

BY A.V. FLATMAN \* B.Sc.

**M**OST commercially available closed circuit television equipment is of semi or fully professional quality and is therefore financially prohibitive to a large group of potential users. This project describes an economical and relatively simple, black and white, amateur grade CCTV Camera.

The constructor should, without the use of specialised test equipment, be able to build this interesting and extremely useful item for less than £60—the cost being controlled to a large extent by the lens used with the camera.

## GENERAL DESCRIPTION

The greatest economy is made by basing the design of the camera unit on an amateur grade one inch diameter Vidicon (namely the EMI 9677). This device may be obtained, together with its scan coil assembly and pin connector, from EMI Electron Tube Division, 243 Blyth Road, Hayes, Middlesex UB3 1HJ.

7400 family logic is utilised to generate the complex synchronisation signals required within the camera system. This feature renders the widely used, discrete component equivalent obsolete and enables a cheaper, more compact and less power consuming replacement. The hybrid nature of the circuitry, due to the combination of digital integrated circuits and transistors, will, it is hoped, give the constructor some interesting examples of how these contrasting components may live together in harmony.

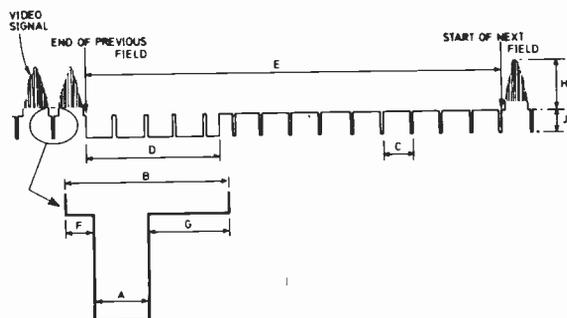


Fig. 1.1. CCIR 625/405 line TV Standards

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The camera, whose circuitry is mounted on two printed circuit boards and is compatible to either 625 or 405 line TV standards (by a simple adjustment), may be coupled to a remote TV monitor via a single coaxial link. Alternatively, the unit may be used in conjunction with a standard domestic 625 line TV receiver with the aid of a u.h.f. modulator. This will enable the video information from the camera to be injected into the receiver aerial socket.

A strong aluminium case houses the mains-powered camera in a compact yet accessible manner and caters for the attachment of a standard photographic tripod.

## BRITISH TV STANDARDS

A television picture is made up of a series of merging horizontal lines. One complete picture or frame is scanned out every 1/25 second, and is "enhanced" by the tube phosphor for a very short time—thus enabling following frames to be scanned-out to give a flicker free and lifelike appearance to the moving picture.

If one visualises a picture being sliced into thin horizontal strips, which are linked end-to-end to form a long chain, then it is not a difficult conception to understand how the information is conveyed from a TV camera to its monitor. Reconstruction of the "mutilated" picture in the above example requires knowledge of the exact location of each strip, and introduces the need for two groups of

Table 1-1		625-Line	405-Line
A	Line sync pulse	4 $\mu$ s	8 $\mu$ s
B	Line blanking period	12 $\mu$ s	18 $\mu$ s
C	Line period	64 $\mu$ s	98 $\mu$ s
D	Field sync pulse	250 $\mu$ s	350 $\mu$ s
E	Field blanking period	1.28ms	1.4ms
F	Front porch	2 $\mu$ s	2 $\mu$ s
G	Back porch	6 $\mu$ s	8 $\mu$ s
H:J	Video: Sync ratio	7:3	7:3
H + J	Composite video level	IV pk/pk	IV pk/pk

\*North Staffordshire Polytechnic

information—video and synchronisation. For convenience, both groups of information are then compressed into a composite signal to enable single channel conveyance.

Approximate CCIR 405/625 line TV standards are shown in Fig. 1.1. Video and sync information are easily distinguished by their respective positive and negative-going directions. Most aspects of the composite video waveform shown may be summarised as follows.

**Line Sync Pulse** The leading edge of the line sync pulse marks the end of a line scan and initiates a beam flyback in the scanning process. Inaccuracy in the generation of these sync pulses will give rise to line slip or the breaking up of the monitored picture—they must therefore be inserted precisely in time with fast vertical edges.

**Line Blanking Period** The electron beam in any TV system requires a finite time to traverse the face of the tube. To allow for this flyback time, and to prevent the action of beam flyback from interfering with the intended scanning process (by retracing itself), a line blanking period is employed. This period blanks-off the video signal and starts slightly before the line sync pulse, ending some microseconds after its completion and accounts for up to 15 per cent of the total available line time.

**Front Porch** This period allows time for the video signal voltage to fall to the blanking level before the action of the line sync pulse.

**Back Porch** Composite video signals are often processed by amplifiers having no d.c. coupling facilities. This unfortunately allows the video levels to drift and give a mean voltage level coincident with zero volts d.c. D.c. restoration is simply achieved in the TV monitor/receiver by clamping the reference level to the back porch for the duration of the following line. All picture half tones are thus faithfully reproduced.

**Field Sync Pulse** The leading edge of the field sync pulse marks the end of a complete field and initiates a beam flyback. As field deflection coils are generally more inductive than line deflection coils, the time taken for a flyback operation is understandably longer (as  $t = L/R$  seconds). The energy in the field sync pulse must then be correspondingly larger than that in the line sync pulse. Pulse energy is calculated as the product of its height (volts) and its width (seconds) and is, in this case, more conveniently controlled by its width. A field sync pulse of  $160\mu\text{s}$ – $300\mu\text{s}$  width performs the required task admirably, at the same time making it easily differentiated from the line sync pulse.

A frame sync pulse of at least  $150\mu\text{s}$  duration would obliterate several line sync pulses and momentarily inhibit the operation of the line generator in the monitor/receiver. It is preferable to maintain the free-running of the line generator due to its difficult fast-starting properties. For this reason, the long field sync pulse is broken up into a series of broad pulses, enabling the delivery of a pulse whenever the line generator expects one.

In more sophisticated TV systems, the field sync pulse is the most complex signal of them all. This is to cater for the fully synchronised interlacing;

whereby in 625 line standards, for example, field 1 would commence scanning at the top left hand corner and comprise 312.5 lines, whilst field 2 would start scanning the inter-leaved remainder of the 625 lines halfway along the top line. Interlaced scanning is accurately achieved in this way but is unfortunately costly in circuitry. The alternative to fully synchronised scanning will be explained shortly.

**Field Blanking Period** Blanks the video signal whilst field flyback is performed, taking about 20 line periods.

**Composite Video Bandwidth** The theoretical maximum frequency of the signal from a TV Camera is given by:

$$f_{\text{max}} = \frac{a N^2 P}{2}$$
 where N is the number of lines in a picture frame, P is the number of frames/second and  $a = \frac{4}{3}$  the picture aspect ratio.

For 625 lines  $f_{\text{max}} = 6.5\text{MHz}$ ; for 405 lines  $f_{\text{max}} = 2.74\text{MHz}$ .

The theoretical maximum bandwidth assumes equal horizontal and vertical resolution. In practice this is not so and lower working bandwidths are possible—5MHz for 625 line standards.



## RANDOM INTERLACING

The CCIR system of field sync pulses required to generate fully synchronised interlacing requires costly additional circuitry, which would therefore defeat the object of producing a compact, low-cost TV camera. For this reason alone, the above system is not incorporated and will not be summarised in this preamble.

If the field and line sync pulses were generated separately and not synchronised to one another in any way, a system of random interlacing would be obtained. To use random interlacing to its fullest potential, the line generator must generate exactly half the number of lines in a picture frame per field, thus positioning the interlaced field accurately within the first field.

In practice, the frequency of a simple line generator will have a limited stability—and will thus impair the accurate positioning of interlaced fields. Alternate fields will randomly vary in position to give a maximum possible resolution of 625 lines/frame—and a mean resolution of slightly less than 625 lines/frame.

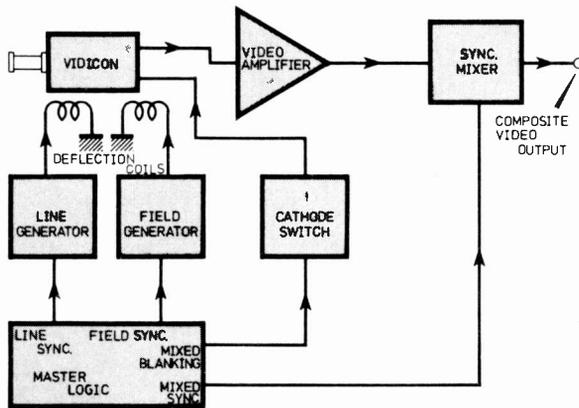


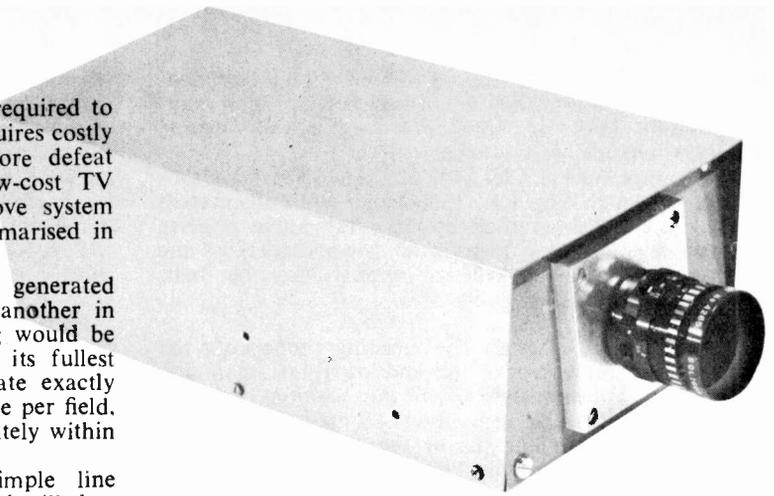
Fig. 1.2. CCTV camera system block diagram

## TV CAMERA SYSTEM

The schematic diagram of the TV Camera is shown in Fig. 1.2. All the sync signal timing and generation is performed by the Master Logic, which may be thought of as the system heart. Each of the control pulses is then directed to its appropriate location.

Scanning within the Vidicon camera tube is made possible by driving the deflection coils with current waveforms, which are synchronised to the line and field sync pulses and generated by the Line and Field Generators. Actual width and height of the scanned area are set within the Line and Field Generator circuitry.

The scanning beam of the Vidicon is switched off by the Cathode Switch to inhibit the video signal during blanking periods. The video signal is amplified up to the required level and mixed with the line and field sync pulses—driving composite video into a 75 ohm load.



## MASTER LOGIC

Examination of the Table 1.1 of the CCIR TV standards shows that the shortest period involved is  $2\mu\text{s}$  (625 line front porch). A convenient and accurate technique of obtaining a great proportion of the pulses required within the Master Logic would be to generate a  $2\mu\text{s}$  pulse chain from a 250kHz clock and successively divide it down in time using a binary counter. A 4-stage binary counter, using SN7473's, would count to 16 negative going pulse edges before repeating itself, giving a repeat time of  $16 \times 4 = 64\mu\text{s}$ , or the line time of a 625 line picture. Within this  $64\mu\text{s}$  repeat time, logic gates could easily construct pulses of various durations from any combination of the available  $2\mu\text{s}$  "time slots".

Fig. 1.3 shows the Master Logic circuit diagram and Fig. 1.4 its relevant waveforms.

A 4-stage divider, comprising BS1, 2, 3 and 4, is driven from a variable frequency clock to give pulse chains A, B, C, D and E, and their inverted complements. The clock is basically two cross-coupled NAND gates, G3 and G4, which means that either output A or  $\bar{A}$  is high (+5V) at any one time. If A is high, then D2 becomes reverse biased and C2 is allowed to charge via the input resistance of G2. The output of G2 will subsequently become low (0V) and  $\bar{A}$  high, causing D2 to conduct and rapidly discharge C2. The repeat of this procedure will occur now in the other half of the clock (concerning G1, D1 and C1), thus completing the loop and maintaining repetitive generation of  $2\mu\text{s}$  pulses. R1 and VR1 control the capacitor charge rate (clock frequency), and G5 is simply a self starting gate, ensuring the output of G2 to be low immediately after switch-on.

Remembering that all inputs of a NAND gate must be high for its output to be low, the selection of line sync and blanking pulses may now be understood. The first six  $2\mu\text{s}$  time slots are selected by G6 and G7 to represent a line blanking period of  $12\mu\text{s}$ . The first  $2\mu\text{s}$  time slot represents the front porch, whilst the second and third are selected by G8, G9, G10 and G11 to represent a line sync period of  $4\mu\text{s}$ . This latter pulse is inverted by G12 to give it the correct positive going direction.

## FIELD CONTROL SIGNALS

Concentrating now on the field control signal generation, we move to the waveform shaper. When the high gain stage comprising TR1, R2 and R3

amplifies the Vidicon heater voltage, which is already 6.3V a.c. or 18V pk/pk, the resultant will be the square shaped waveform with 20ms cycle time, as shown by H. D3 simply protects TR1 against the high reverse  $V_{be}$ . C3 and R4 will further act to differentiate this square-shaped signal to present negative edges to Monostable 1 input every 20ms. Monostable 1 will then generate the field blanking pulse of 1.2ms and Monostable 2 the field sync pulse of 250 $\mu$ s—both Monostables being effectively triggered by the negative-going edges J.

The operation of both monostables is understood from the description of the clock, which is basically two monostables itself. Again, the values of C4 and

C6 determine the widths of the generated pulses, which are available together with their complements at the outputs of the monostable.

Line and field blanking pulses, F (12 $\mu$ s) and K respectively, are mixed in G16 and inverted by G17 to give the correct negative going direction.

The mixing of line and field sync pulses is not so straightforward. In the absence of a field sync pulse, line sync pulses are routed through G13 and G15 to be outputted as positive going signals. However, in the presence of a field sync pulse, the mixed sync output is made high, whilst line sync pulses are routed through G14 and G15 to be effectively inverted at the output. In this way, the long field

## MASTER LOGIC CIRCUIT

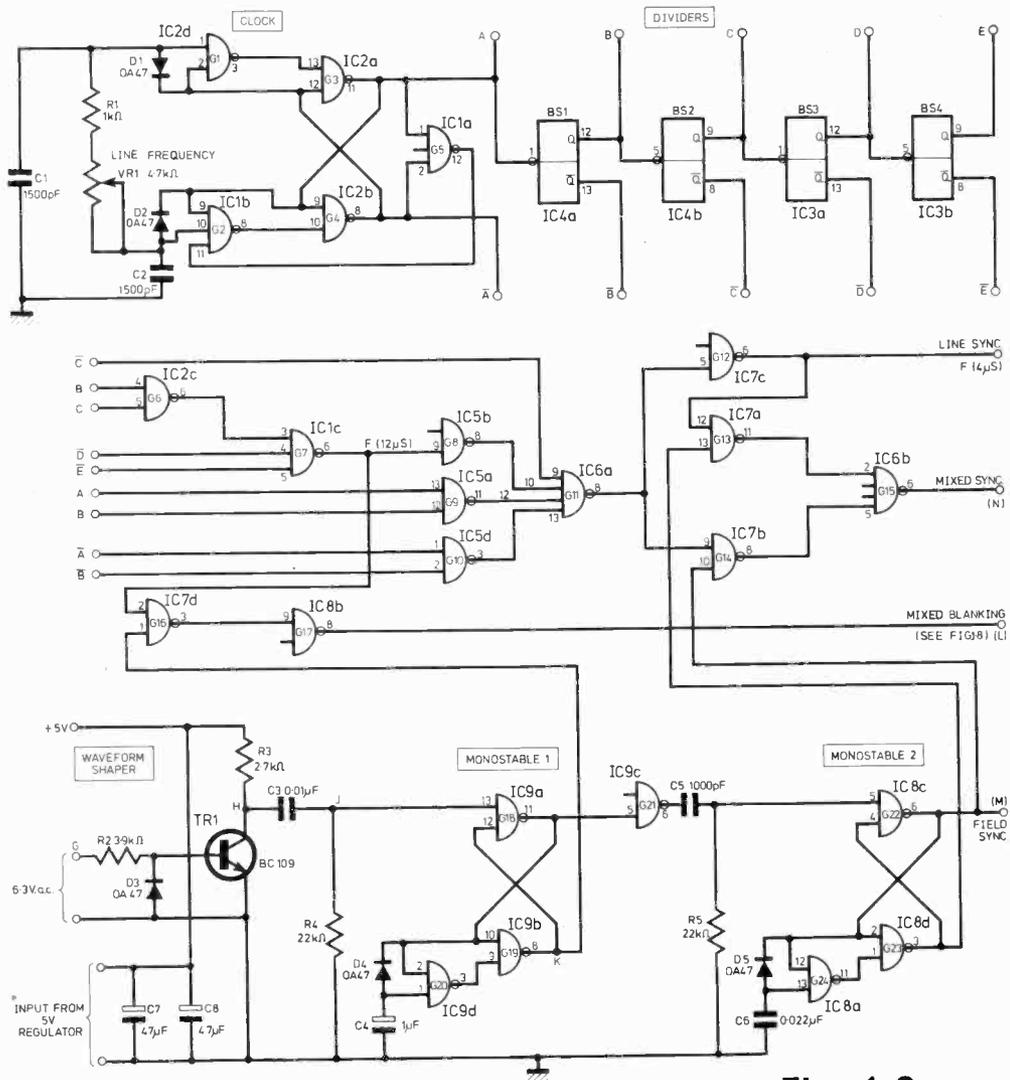


Fig. 1.3

sync pulses are divided into a series of broad pulses and line sync pulses are still conveyed.

VR1 is adjusted for 625-line operation by setting the clock frequency to 250kHz ( $2\mu\text{s}$  time slots), or for 405-line operation by setting the clock frequency to 162kHz ( $3.1\mu\text{s}$  time slots).

As previously stated, the master logic is the heart of the TV camera system and controls the timing of all control signals. Tremendous flexibility is obtained by the use of a master clock, which, by the adjustment of a single control, enables the alteration of all the required control signals to suit almost any TV standards.

## THE VIDICON

A cross sectional view of the Vidicon, given in Fig. 1.5, shows how a scene is imaged onto the photoconductive target by an optical lens. The focused image, which the human eye knows to be a complex light pattern, is then converted into an electrical charge pattern by the photoconductive target.

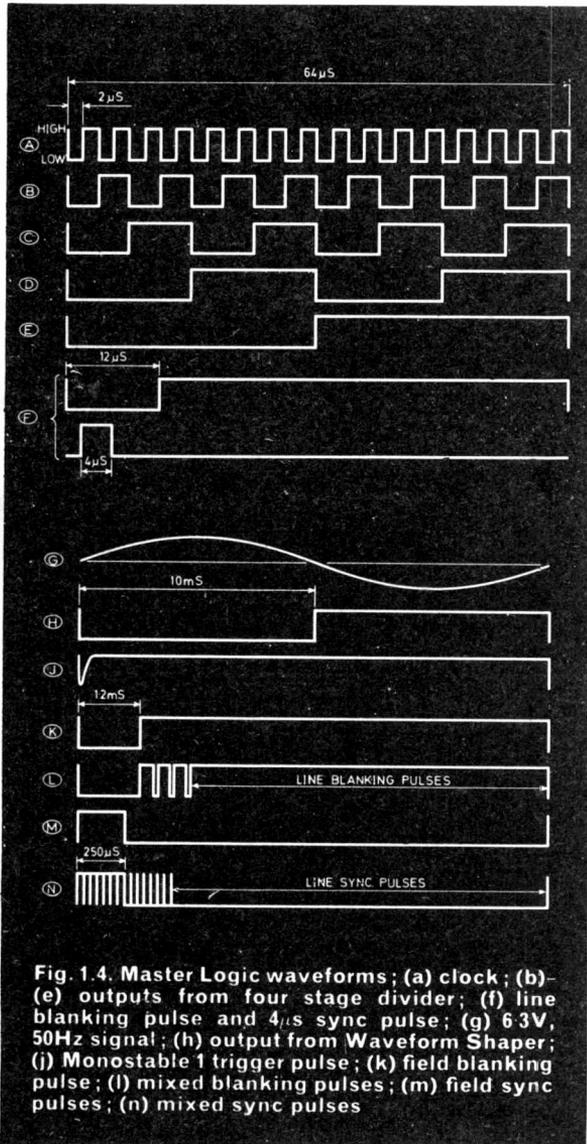


Fig. 1.4. Master Logic waveforms; (a) clock; (b)-(e) outputs from four stage divider; (f) line blanking pulse and  $4\mu\text{s}$  sync pulse; (g) 6.3V, 50Hz signal; (h) output from Waveform Shaper; (j) Monostable 1 trigger pulse; (k) field blanking pulse; (l) mixed blanking pulses; (m) field sync pulses; (n) mixed sync pulses

An electron beam is generated by the Vidicon electron gun (comprising cathode, control grid G1 and limiter anode G2) and focused into a fine spot on the rear surface of the target. Suitable beam deflection, made possible by the scan coils, will then scan the beam in a raster fashion to cover the required area of the focused image. The beam current is adjusted to neutralise the electrical charge pattern during the scanning process and enables yet another conversion; this being the conversion of electrical charge into current. We now have a complex current pattern which resembles the initial light pattern of the focused image, and, although the

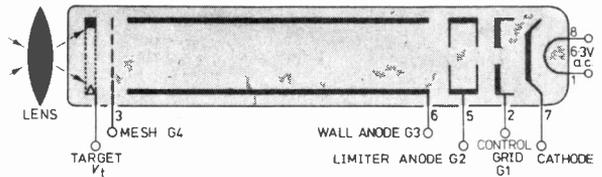


Fig. 1.5. The EMI 9677 1in Vidicon

range of target current is small, it is now in a form found most convenient for electronic processing (i.e. amplification).

A potential  $V_t$  is applied to the target in order to enable the electron beam to reach its rear surface (just as in valve theory we have to apply positive anode potentials to enable current flow from the cathode). This potential roughly determines the operational sensitivity, higher values of  $V_t$  giving a more efficient conversion (more target current per level of light intensity). Typical values of  $V_t$  are + 50V for low-light conditions, and + 20V for bright-light conditions. One point to remember is that operation at high values of  $V_t$  gives correspondingly higher "black" currents (target current representing black or unlight areas of the image), resulting in a "grey" reproduction of the shade black.

Sensitivity may also be controlled to some extent by the electron beam current. Beam current is simply controlled by the control grid potential  $V_{G1}$ , higher currents being obtained from less-negative value of  $V_{G1}$ . The beam current is adjusted to neutralise or discharge the electrical charge pattern established on the target; a typical value of  $V_{G1}$  being + 20V with respect to the cathode. It must be appreciated that operation at high beam currents will correspond to a larger focused spot—and a lower picture resolution.

## VIDEO SIGNAL CURRENT

Assuming the Vidicon camera tube to be suitably adjusted (i.e. correct electrode potentials are applied) for the capture of a well illuminated scene, the video signal current from the target will range from approximately 10nA, representing the black level, and 300nA, representing the full white level. This range of currents must be suitably amplified to give a working level of 700mV pk/pk.

The most convenient way of amplifying this signal would be to convert it to a voltage signal prior to amplification. To do this, various points must be

# COMPONENTS . . .

## Resistors

R1	1k $\Omega$	R26	1k $\Omega$
R2	3.9k $\Omega$	R27	1k $\Omega$
R3	2.7k $\Omega$	R28	1.5k $\Omega$
R4	22k $\Omega$	R29	1k $\Omega$
R5	22k $\Omega$	R30	470 $\Omega$
R6	220k $\Omega$	R31	220 $\Omega$
R7	6.8k $\Omega$	R32	1k $\Omega$
R8	47k $\Omega$	R33	5.6k $\Omega$
R9	1k $\Omega$	R34	1.2k $\Omega$
R10	470 $\Omega$	R35	10k $\Omega$
R11	470 $\Omega$	R36	100 $\Omega$
R12	2.7k $\Omega$	R37	150k $\Omega$
R13	470 $\Omega$	R38	100k $\Omega$
R14	3.9k $\Omega$	R39	2.8k $\Omega$
R15	6.8k $\Omega$	R40	100k $\Omega$
R16	1k $\Omega$	R41	15 $\Omega$
R17	180k $\Omega$	R42	390k $\Omega$
R18	18 $\Omega$	R43	1k $\Omega$
R19	2.2k $\Omega$	R44	680 $\Omega$
R20	470 $\Omega$	R45	470 $\Omega$
R21	2.2k $\Omega$	R46	100 $\Omega$ 5% 2 watt
R22	10k $\Omega$	R47	2.7k $\Omega$
R23	82 $\Omega$	R48	270 $\Omega$
R24	82 $\Omega$	R49	390 $\Omega$
R25	470 $\Omega$	R50	100 $\Omega$ 5% 1 watt

All 5%  $\frac{1}{2}$  watt carbon except where otherwise stated

## Capacitors

C1	1,500pf Ceramic
C2	1,500pf Ceramic
C3	0.01 $\mu$ F Polyester (Mullard C280)
C4	1 $\mu$ F Elect. 10V
C5	1,000pF Ceramic
C6	0.022 $\mu$ F Polyester (Mullard C280)
C7	47 $\mu$ F Elect. 10V
C8	4.7 $\mu$ F Elect. 10V
C9	1 $\mu$ F Elect. 63V
C10	1 $\mu$ F Elect. 63V
C11	47 $\mu$ F Elect. 25V
C12	10 $\mu$ F Elect. 25V
C13	10 $\mu$ F Elect. 25V
C14	4.7 $\mu$ F Elect. 25V
C15	4.7 $\mu$ F Elect. 25V
C16	10 $\mu$ F Elect. 25V
C17	4.7 $\mu$ F Elect. 25V
C18	47 $\mu$ F Elect. 25V
C19	100 $\mu$ F Elect. 25V
C20	470pF Ceramic
C21	4.7 $\mu$ F Elect. 25V
C22	470 $\mu$ F Elect. 10V
C23	1,000 $\mu$ F Elect. 25V
C24	16 $\mu$ F Elect. 350V
C25	16 $\mu$ F Elect. 200V
C26	32 $\mu$ F Elect. 200V
C27	0.22 $\mu$ F Polyester (Mullard C280)
C28	1,000 $\mu$ F Elect. 25V
C29	470 $\mu$ F Elect. 10V
C30	470 $\mu$ F Elect. 10V
C31	220 $\mu$ F Elect. 10V

## Transistors

TR1-TR10	BC109 (10 off)
TR11	BF178
TR12	BC109
TR13	2N4060
TR14	2N5245
TR15-TR16*	BFY51 (2 off)
TR17	BC109
TR18*	BFY51
TR19	BC109

\* transistors must include clip-on heatsinks

## Integrated Circuits

IC1	SN7410
IC2	SN7400
IC3-IC4	SN7473 (2 off)
IC5	SN7400
IC6	SN7420
IC7-IC9	SN7400 (3 off)

## Diodes

D1-D5	OA47 (5 off)
D6	OA202
D7	BZY88 400mW 5.6V Zener
D8-D11	IN4001 (4 off)
D12	IN4007
D13	IN4005
D14	BZY88 400mW 5.6V Zener
D15	BZY88 400mW 3.9V Zener

## Potentiometers

VR1	4.7k $\Omega$ miniature skeleton
VR2	100 $\Omega$ miniature skeleton
VR3	470 $\Omega$ miniature skeleton
VR4	1k $\Omega$ miniature skeleton
VR5	4.7k $\Omega$ miniature skeleton
VR6-VR7	50k $\Omega$ linear (2 off)
VR8	470 $\Omega$ miniature skeleton
VR9	100 $\Omega$ miniature skeleton
VR10	100 $\Omega$ 1W wire wound

All skeleton pots are horizontal mounting type

## Transformers

T1	Type 634 Pri-250V, Sec. 17.5V @ 1.6A (R.S. Components)
T2	Midget mains Pri-245V, Sec. 125-0-125V @ 50mA; 6.3V @ 1.2A (R.S. Components)

## Inductors

L1, L2	150 and 85 turns respectively of 36 s.w.g. enamelled copper wire on Mullard FX2239 ferrite cores
L3	Focus coil
L4-L5	Line scan coils
L6-L7	Field scan coils

EMI,  
243, Blyth Road,  
Hayes, Middlesex

## Vidicon Tube

V1	9677 Vidicon (EMI) (see text) †
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## Camera Lens

Soligor television lens, f1.9, 25mm focal length (Dixons Photographic)

## Miscellaneous

Flush-mounting Coax Socket  
D.p.s.t. Mains toggle  
3 knobs  
Assorted 6BA, 4BA and 2BA nuts and bolts  
 $\frac{1}{4}$ in  $\times$   $\frac{1}{4}$ in steel rod  
Eight 2BA chrome-head screws  
Length of 3-core Mains lead  
Sheet 18 s.w.g. aluminium 18in  $\times$  6 $\frac{1}{4}$ in  
Sheet 20 s.w.g. aluminium 11 $\frac{3}{4}$ in  $\times$  12 $\frac{1}{2}$ in  
1in  $\times$   $\frac{1}{4}$ in aluminium 3 $\frac{1}{2}$ in long  
2 $\frac{1}{2}$ in  $\times$  2 $\frac{1}{2}$ in  $\times$   $\frac{1}{2}$ in aluminium block  
Rubber grommet  $\frac{1}{4}$ in  $\times$   $\frac{1}{2}$ in  
6.3V Pilot lamp (panel mounting)

considered. Let us firstly examine the equivalent input network required to convert the video current to a voltage signal, which will subsequently be presented to the Video Amplifier input. Such a network is shown in Fig 1.6.

The output of the Vidicon may be considered as being a current source (i.e. having infinite shunt resistance). Conversion of signal current to voltage is then simply achieved by passing  $I_1$  through  $R_{in}$ , the input resistance of the Video Amplifier. Now, by Ohm's law,  $V=I_1 \times R_{in}$ , and the magnitude of the voltage available at the Video Amplifier input will be proportional to the value of  $R_{in}$ . Unfortunately, however, there exists an equivalent shunt capacitance,  $C_{in}$ , which is made up from the output capacitance of the Vidicon and the input capacitance, of the Video Amplifier.  $C_{in}$  will, in conjunction with  $R_{in}$ , determine the frequency response of the input network by:

$$f_{max} = \frac{1}{2\pi C_{in} R_{in}} \text{ Hz}$$

Therefore, as  $C_{in}$  is essentially fixed,  $R_{in}$  must be limited to a value giving the 5MHz maximum working frequency required for 625-line operation.

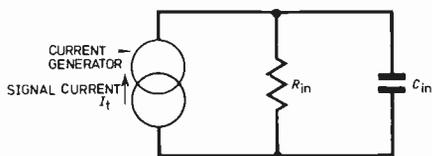


Fig. 1.6. Equivalent input network of the Video Amplifier

### VIDEO AMPLIFIER

The Video Amplifier circuit diagram is shown in Fig. 1.7. Due to the application target, the first stage potential,  $V_1$ , to the Vidicon target, the first stage of the Video Amplifier is a.c. coupled via C10.  $V_1$  is then simply conveyed to its destination by R6

after being decoupled by C9 to prevent any unwanted signals breaking through to the extremely sensitive amplifier input.

As a common emitter stage presents a relatively low impedance at its input, we are presented with two alternatives in design. Either overall negative feedback is applied to the amplifier to increase its input impedance, or an emitter follower front end is used. Overall negative feedback tends to create instability in wideband amplifiers, whilst an emitter follower stage inherently presents a relatively high input impedance. The first stage is therefore chosen to be an emitter follower or impedance converter of unity voltage gain.

The equivalent shunt input capacitance,  $C_{in}$  is 6pF. Now, for 5MHz bandwidth, commanded by 625 line TV standards, the total shunt input resistance,  $R_{in}$ , may be calculated as:

$$R_{in} = \frac{1}{2\pi C_{in} f_{max}} = 5.3k\Omega$$

In practice,  $R_{in}$  is made up from resistors R6, R7 and R8, which are designed to give an equivalent shunt resistance of 5.3kΩ. The input resistance of TR2 is very high and may be neglected in the above calculation.

From knowledge of the maximum signal current,  $I_{(max)}$ , the input voltage developed across  $R_{in}$  may be found as:

$$V_{in(max)} = I_{(max)} \times R_{in} = 300nA \times 5.3k\Omega = 1,590\mu V \text{ pk/pk}$$

A Video Amplifier gain of 440 is therefore required to produce the required 700mV of video signal at the output. Additional gain will also be made available for increased sensitivity if required.

Most of the signal gain is achieved by the second stage, which is a cascode amplifier, comprising TR3, TR4 and associated components.

Low-noise BC109's are used in this novel mode to enable high gain, wideband amplification. Stage 2 is directly coupled from stage 1 and achieves a voltage gain of 70.

The output signal from the cascode stage is taken to the next voltage gain stage via an emitter follower. This emitter follower, TR5 and R16, is directly coupled to the cascode stage and establishes a low

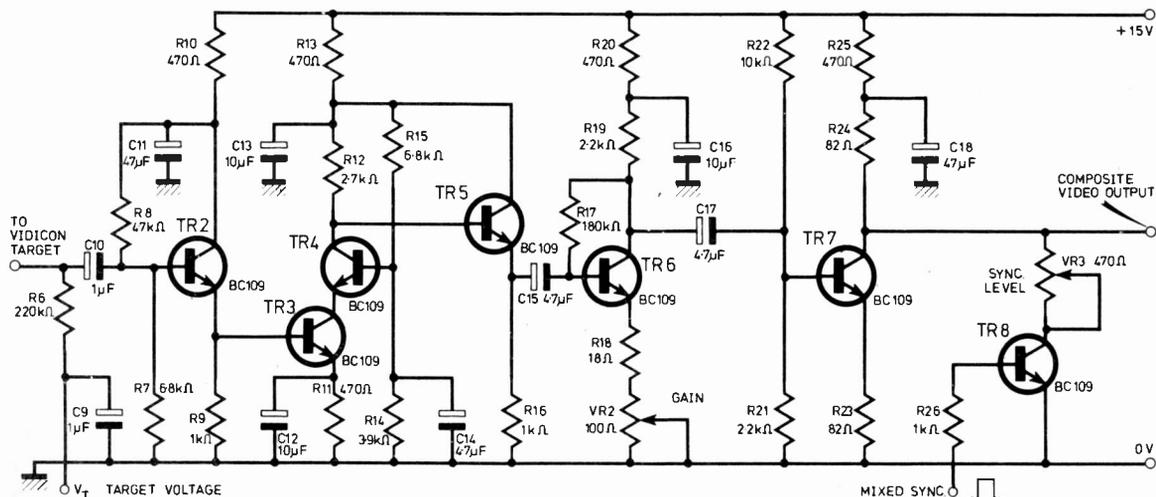


Fig. 1.7. Video Amplifier and Sync Mixer

impedance drive into the capacitive input of the common emitter stage built around TR6. Wideband amplification is ensured by the use of this accepted technique.

Local negative feedback is applied to TR6 to control its stage gain, VR2 giving the required range of amplification of between 6 and 40. Sufficient gain has now been contributed to the Video Amplifier to give 700mV of video signal.

Two further functions are to be facilitated in the video amplification—180 degree phase shift to give a positive going video waveform, and impedance conversion to give 75 ohm output impedance. The final stage of TR7 and associated components is a common emitter amplifier with approximately 75 ohms load in both collector and emitter circuits and therefore performs the impedance conversion and acts as a unity-gain signal inverter.

A.C. coupling has been utilised in the Video Amplifier via C10, C15 and C17. Each value of capacitance is designed to pass the lowest frequency component of the video signal—that being the field repetition frequency of 50Hz.

The supply to each stage is individually decoupled to prevent unwanted breakthrough (feedback) of the various signals within the TV Camera system.

### SYNC MIXER

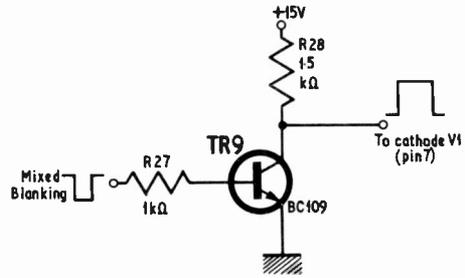
Mixed sync pulses are used to switch TR8, which in turn will switch the d.c. level of the collector of TR7 negatively by a controlled amount. VR3 is adjusted to enable 0.3V negative sync pulses to be superimposed on the video signal.

### CATHODE SWITCH

Blanking is facilitated by the Cathode Switch, whose circuit diagram is shown in Fig. 1.8.

The Vidicon electron beam current may be cut off by either applying a large negative potential to the control grid G1, or conversely, a large positive potential to the cathode. Arguing for and against these two methods, beam cut off control via the cathode seems to be most convenient.

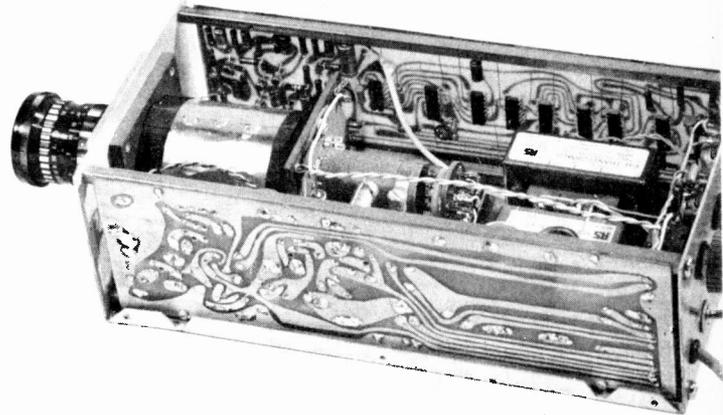
As all Vidicon electrode potentials are measured with respect to the cathode, alteration of the cathode potential therefore controls several mechanisms



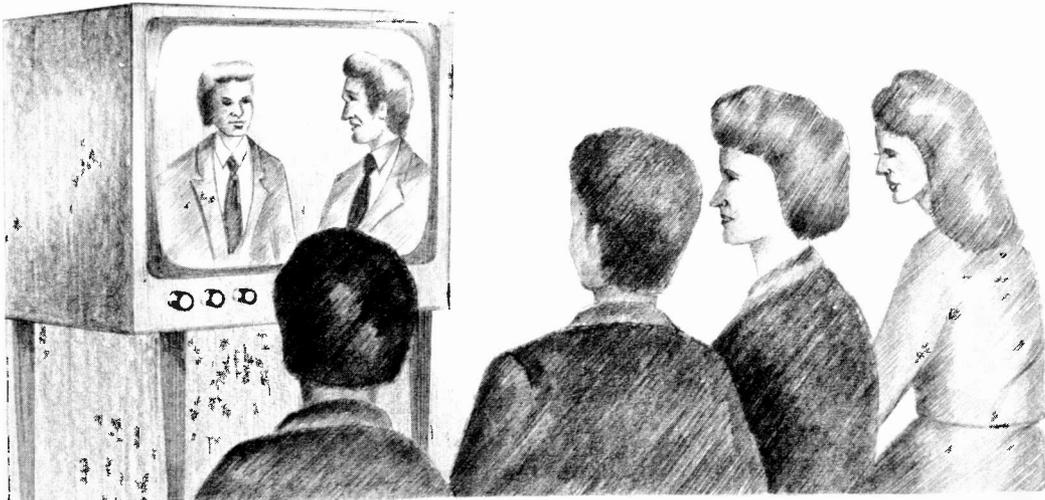
within the tube. The beam current is reduced and a limited number of electrons reach a less positively biased target with the application of +15V to the cathode.

Mixed blanking pulses are used to switch TR9 and apply the Vidicon cathode with one of two potentials—0V to make the required beam current available for scanning, and +15V to blank or switch off the beam during flyback periods.

The video signal is now blanked and sync pulses added accordingly to produce the composite video waveform.



Next month: P.C.B. construction and more camera electronics



# FIRST STEPS IN CIRCUIT DESIGN

# 6

By A. P. Stephenson

*This series, specially written for the beginner, takes you step-by-step through transistor circuit design in a simple, non-mathematical way.*

*Design of a small signal amplifier will be followed by a Class B amplifier and the series will conclude with a constructional project so that your theoretical knowledge can be put into practice.*

**S**TABLE and predictable power amplifiers are not easy to design and it is only fair to warn would-be designers of the danger of increasing the bank overdraft!

A miscalculation in a resistor value, a too hasty twiddle of a preset, or a loose nut on a heatsink, can often be enough to trigger off an avalanche of disaster.

A typical sequence of events would commence with a slight rise in the temperature in the output

transistors; this increases the drive current which in turn increases the temperature and so on. Eventually (usually after a few milliseconds) bang go the outputs, the drivers and, if you are particularly unlucky, the loudspeaker cones.

In fact the writer's experience suggests that the fuse is the hardest component in the chain.

Strictly speaking, the power amplifier should be left in the hands of the professional.

## 6.1. POWER AND VOLTAGE AMPLIFIERS COMPARED

If one's aims are moderate, in the sense of only a few hundred milliwatts rather than tens of watts, there is no reason for not trying one or two circuits if only to get the feel of the beasts. The best way to start is to list the problems of power amplifiers in comparison with voltage amplifiers.

Voltage amplifiers normally operate with relatively small signal swings well within the available limits of ground and supply rail.

Thus distortion due to non-linearity is not too serious because the small part of the transistor characteristic used is almost a straight line.

Power amplifiers, in order to operate efficiently, must use all the available voltage swing, giving rise to distortion levels which would be unacceptable without circuit sophistication.

The power output transistors require large currents, sometimes many amps. This means considerable heat production which tends to be cumulative because

- (a) Leakage current is no longer negligible.
- (b) Base to emitter voltage ( $V_{BE}$ ) can no longer be taken as 0.6V because of the relation to temperature ( $V_{BE}$  falls by 2mV for every degree C rise).
- (c)  $h_{FE}$  is dependent on temperature, rising as temperature increases. Thus the drive increases with temperature.

High power transistors have a much lower  $h_{FE}$  — 20 or 30 instead of 200 or 300.

## 6.2. BASIC CIRCUIT OUTLINES

Class B push-pull is used almost exclusively for power output stages but, unlike the old valve circuits, modern circuits dispense with transformers.

There are many possible permutations as will be seen in the following selection. No intricate details will be shown, merely the outlines.

### PURE COMPLEMENTARY PUSH-PULL

Figs. 6.1 and 6.2 show two complementary push-pull circuits which have the merit of neatness, balance, low impedance output, and high, equal drive impedances.

There is one practical disadvantage—it is difficult to match high power *pnp* and *npn* transistors. So-called “matched pairs” are available on the market but are quite expensive if close matching is required.

### QUASI-COMPLEMENTARY PUSH-PULL

Because it is easier to match transistors of the same type, particularly *npn* pairs, the arrangements shown in Figs. 6.3 and 6.4 are very popular.

There are two snags however: one transistor is an emitter follower and the other is grounded emitter. The other snag is the input phasing which means that a pair of anti-phase signals are necessary.

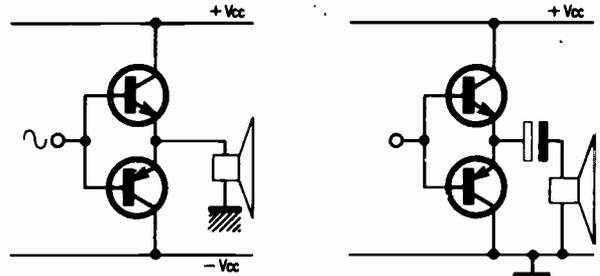


Fig. 6.1. Complementary push-pull circuit using a centre-tapped supply rail and Fig. 6.2. using a single supply rail

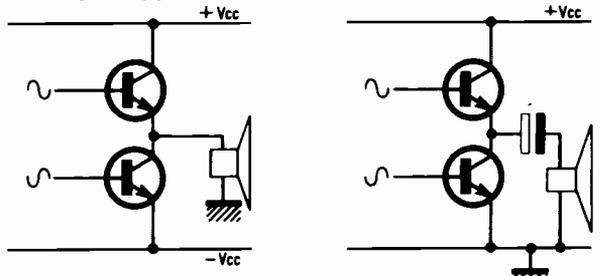


Fig. 6.3. Quasi-complementary push-pull circuit with a centre-tapped supply and Fig. 6.4. using a single supply rail

## 6.3. QUIESCENT CURRENT IN CLASS B

The virtue of pure Class B can be stated in one word—efficiency.

With the volume control turned down (i.e. no drive signal) the power-hungry output stages are also off and draw no current. Thus the power consumed by the output stages is proportional to the input signal.

In Class A the output stages are permanently consuming power without an input signal.

### CROSSOVER DISTORTION

Unfortunately we are unable to use pure Class B with transistor pairs because of the rather disagreeable “crossover distortion”.

Consider what happens if we apply a signal to a pair of complementary outputs whose bases are tied together (see Fig. 6.5).

The top waveform is the input signal voltage which drives TR1 to conduction on the positive

input cycles and TR2 on the negative. Thus the load receives its current only from one transistor at a time, because the other is cut off.

The bottom waveform shows the current through the respective transistors and the distortion due to “crossover”.

From zero volts to +0.6V there is no current in TR1 and from zero volts to -0.6V there is no current in TR2. Thus we have discontinuities in the current waveform in the vicinity of the crossover point at zero volts.

To overcome this, the transistors are usually operated with a small forward bias so that, in the absence of an input signal, they are both slightly conducting.

The value of this current is called the “quiescent current” and is, in practice, a rather trial and error affair being a compromise between acceptable crossover distortion and acceptable quiescent dissipation.

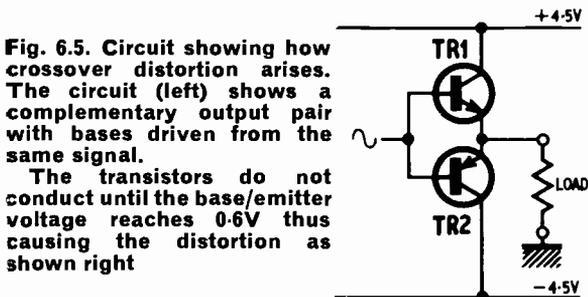


Fig. 6.5. Circuit showing how crossover distortion arises. The circuit (left) shows a complementary output pair with bases driven from the same signal.

The transistors do not conduct until the base/emitter voltage reaches 0.6V thus causing the distortion as shown right

## 6.4. THE DRIVER STAGE

A simple driver stage can be used to serve two purposes: to provide some voltage gain; and to develop the 1.2 volts needed to ensure that both bases are slightly forward biased at zero signal.

Fig. 6.6 shows a simple but quite workable little circuit which is worth studying.

Note carefully the following points:

(a) The d.c. voltage drops are the quiescent values (zero signal).

(b) To avoid a centre tapped supply, the loudspeaker is connected via a d.c. blocking electrolytic capacitor to ground—a well-established practice although alternatively it could be returned to the positive rail, with the capacitor polarity reversed.

(c) The diode is not absolutely necessary, but does help to compensate for  $V_{BE}$  changes in the output transistors.

In theory, we could have two diodes and scrap VR1 altogether, because the two together would give us the 1.2V needed to turn on the bases of TR1 and TR2. However, this assumes that the temperature coefficients of both diodes and transistors are identical.

By using one diode and a "twiddler" we can make a fine adjustment in quiescent current.

(d) The bias current for TR3 is bled from the output line via R2 which introduces heavy d.c. negative feedback and keeps the output locked at midpoint (4.5V).

There is no signal negative feedback so the gain is not affected.

(e) The "voltage gain" of the circuit is a figure whose calculation can easily be tackled from the wrong lines.

Superficially we may be tricked into thinking that TR3 is an ordinary voltage amplifier stage with a gain equal to  $R_C/r_e$  where  $R_C$  is R1.

There is nothing wrong with the equation but it is erroneous to think that R1 in the diagram is the collector resistor since it is swamped by the  $R_{IN}$  of the output transistors.

The effective signal load of TR3 is the input resistance of an emitter follower stage which is

$$R_{IN} = h_{FE} R_L$$

where  $R_L$  is the loudspeaker impedance.

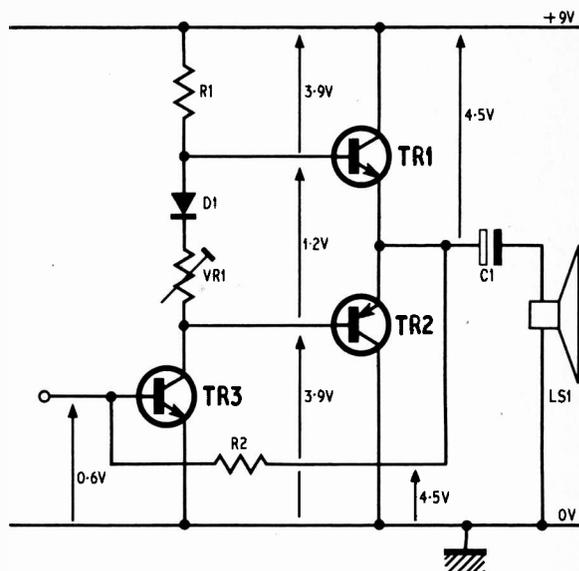


Fig. 6.6. Complementary output stage with a simple driver circuit using single diode for base/emitter voltage stabilisation

### EXAMPLE

Assume the  $h_{FE}$  of the output transistors is 50, the collector current of TR3 1mA, and the speaker impedance 8 ohms.

The voltage gain from the base of TR3 to speaker is

$$A = R_C/r_e \text{ where } r_e = 25/I_C \text{ (mA)} = 25 \text{ ohms}$$

$$\text{and } R_C = h_{FE} R_L = 50 \times 8 = 400$$

$$\text{Hence gain} = 400/25 = 16.$$

(f) The input resistance ( $R_{IN}$ ) of TR3 is

$$h_{fe} \times r_e \text{ in parallel with } R_2/A$$

If this seems strange, remember that the method of obtaining the bias is fundamentally "collector-to-base feedback" which was discussed in section 4.1.

The gain of the emitter followers being unity means that, although R2 is taken from the output stages, it is effectively taken from the collector of TR3.

## 6.5. LIMITATIONS OF THE SIMPLE CIRCUIT

The high frequency response of the circuit described is poor mainly due to the capacity of the collector-base diode of TR1. When TR1 is off the capacity is across R1.

To reduce this effect we can bootstrap R1 by splitting it in two and connecting the output to the junction via a large blocking capacitor.

This has the effect of making R1 higher by a factor equal to the reciprocal of one minus the voltage gain of the output transistor ( $\alpha$ ).

$$R1' = \frac{R1}{1 - \alpha}$$

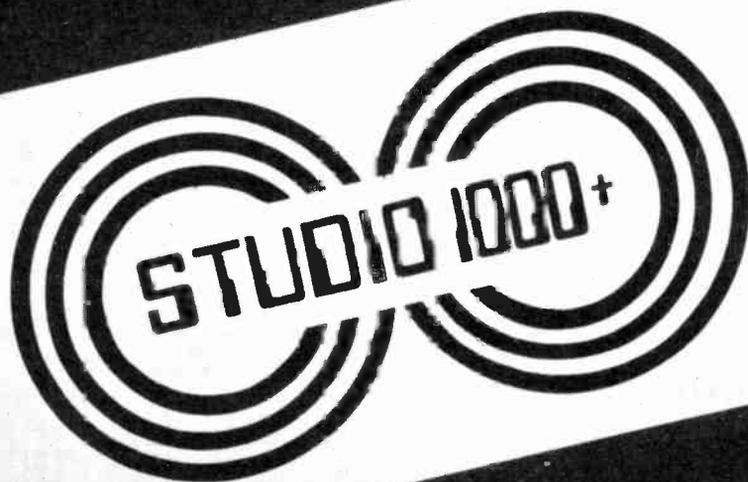
This does however introduce some positive feedback.

Another advantage of this bootstrapping technique is that the current through TR3 is virtually constant since the voltage across R1 is kept constant.

Thus the drive to the output transistors is via a constant current source which decreases the non-linearity of the  $V_{BE}$  characteristic of the output stages.

**Next month: Concluding article and special constructional project linked to this series**

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MM5375	6 digit alarm, Sperry drive	TBA	24
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BC184	0-10	OC44	0-20	TIP41A	0-85	2N3053	0-18	2N3442	1-45
BC212	0-12	OC45	0-20	TIP42A	0-90	2N3054	0-48	3N140	0-98
BC213	0-12	OC71	0-13	2TX304	0-28	2N3055	0-46	3N141	0-66
BC214	0-12	OC84	0-25	2TX504	0-35	2N3391	0-29	3N142	0-65

Electrolit TR5 resistors 2%, 2p; TR6, 3p; TR4, 4p. Wirewound resistors, all values 2-5W, 10p; 6W, 10p; 9W, 12p; 12W, 15p. Diecast boxes 4pin x 2pin x 1in. 40p; 4pin x 2pin x 2in. 50p; 7pin x 4pin x 2in, £1-25. Solder 18 s.w.g., £1-30/lb. Dalo pen, 75p. Litesold Irons, 10W, £1-75; 25W, £1-75; spare bits, 5p. Fibreglass P.C.B., cut to size, 1p per sq.in. Presets, 5p. Disc ceramics, all values, 3p. Tantalum beads, all at 13p. I.C. sockets, 8-pin, 18p; 16-pin, 18p; 14-pin, 15p. BZY88 series zeners, Full range, 400mW, 10p; 20W, 90p. Siemens polycarbonate capacitors, full range, 4p up to 0-1/250V. Bulgin miniature 3-pin mains sockets, 17p, plugs, 16p. Mullard LP1186 F.M. module, £5-05. SBA750A, £1-80; SL3045, £1. Full specification devices discounts for quantity—Many more items available. Send for lists, etc. Cash with order. Mail order only. P. & P. 12p.

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BY FRANK W. HYDE

## RESULTS FROM JUPITER

The data returned from *Pioneer 10* about Jupiter will take a great deal of time to analyse and correlate. However, there is now emerging some early interpretation of the data.

When the study of the radio radiations began, with the discovery in 1955 of the intense outbursts of energy from the planet, it was clear that for this effect to occur it required an intense magnetic field to be present. This is because high electron energy, more than 3MeV, is needed to produce synchrotron radiation.

The Earth-based results had indicated that the magnetic field was more intense than that of the Earth, as high as 8/10 gauss, and it was suggested that the magnetic field was in fact  $11^\circ$  off centre and at a meridian of about  $220^\circ$ . These theories were based on the radio rotation period of Jupiter.

It was also suggested that because the pole of the magnetic field was so far inclined from the rotation axis, it produced a variability which gave rise to the radiation.

## ANALYSIS RESULTS

An analysis of the whole matter by using both the geographical axis and the magnetic axis gave results which indicated that Jupiter's satellite Io had a profound effect on the times of the radio radiations. In tests carried out by the writer and others as part of a NASA project under the leadership of C. H. Barrow this effect was found to be correct for about 60 per cent of the events. The events not lining up with this can now be explained as a result of the *Pioneer* findings.

The in situ measurements that were made by the spacecraft have shown that there are two areas of magnetic effect. One is the field of 4 gauss, which extends to a distance of 20 Jupiter radii, and the other a non dipole field which extends to 108 Jupiter radii. In the latter field the lines seem to be centred near the equator. This displaced relative to the magnetic equator is about 0.1 Jupiter radius north. The longitudinal position is about  $174^\circ$ .

At the central region of the magnetic field the magnetosphere seems to behave in the same way as that of the Earth. In the region beyond this protons and electrons are concentrated near to the equator. This seems to be emphasised on the dawn side.

It is clear that the satellites Amlthea, Io, Europa and Ganymede are "absorbers" of electrons. Thus, there is an explanation for the variations in the Jupiter radiations.

It also raises the question of Saturn which though of a similar composition chemically and physically shows no observable magnetic field. It could be that the presence of the rings of the planet inhibit the formation of a magnetic field. This should be cleared up by *Pioneer 11* which is to pass inside the rings.

Meanwhile *Pioneer 10* is leaving the Solar system at the rate of 280 million miles a year. At present it continues to send back data of its environment.

## SATELLITES ON CALL

The call for satellite assistance is now beginning to be a part of the peaceful economic use of space technology.

The Australian Government sought the assistance of NASA to photograph Lake Eyre during the recent serious flooding. The photographs are required in order to see what were the reasons for the immense amount of water flowing in formally dry watercourses in Australia's most arid regions. Lake Eyre is at the present time covering an area of 300 square miles and the satellite pictures will enable a plan to be formulated in case of future floodings.

Water is pouring in from as far away as Western Queensland and it is thought that if the level of the lake can be kept high, then the rainfall can be increased in areas as far apart as South Australia, New South Wales and Western Australia.

It is also being suggested that pumping sea water into the area could have a profound effect on the environment. It is a new economical possibility that Australia must consider.

## SUNSPOTS AND THUNDERSTORMS

It has long been a joke that almost anything can be predicted by sunspot cycles, from birth incidence to car sales. However, some of the correlations are now receiving special attention and one of these is the event of the thunderstorm.

Using the 11 years sunspot cycle there does appear to be a positive link between the sunspots and thunderstorms. Data produced by M. F. Stringfellow working at the Electricity Council's research centre, who examined records from 1930 to 1973, based on the number of faults induced in overhead lines, taken together with the number of thunderstorm days has revealed a formula.

It is claimed that the events are related in that the number of lightning flashes is proportional to the square of the mean number of events. This can be applied in a predictive form to provide warning in advance. It is certain this cyclic variation is consistent and had an amplitude of  $\pm 30$  per cent of the mean.

The next solar maximum is predicted to have a two-fold increase on 1973.

## BEADS FROM THE MOON

The minute and almost spherical glass beads, returned from *Apollo 12*, found in the Lunar regolith to the extent of 1 per cent have been studied by B. Scarlett and R. E. Buxton of Loughborough University of Technology. Results have shown that they are the product of the break up of liquid jets of rock. These delicate jets are produced when a meteorite impacts the Lunar surface.

The beads vary in size and composition from 0.1 micrometres to 1.0mm. They are coloured red, yellow, silver, grey or just opaque. It is this variance which suggest meteoritic bombardment as the source rather than the well mixed volcanic mixture. The sizes indicate that the temperature formation is not less than  $1,450^\circ\text{K}$  and probably in excess of  $2,000^\circ\text{K}$ .

The two researchers offer certain conclusions about the beads and "balloons". One of these larger spheres was some 260 micrometres in diameter with a wall thickness of 5 micrometres. These are probably blown up because of the volatilisation of some of the lighter constituents like sodium and magnesium.

Calculations show that if these particles are formed as Scarlett and Buxton suggest, the maximum size cannot exceed 1mm. Surface tension would fix a lower limit of size at about  $10^{-2}$  micrometre.



**WE** are going through a patch at the moment not too dissimilar to that experienced by the early classical composers in Mannheim during the eighteenth century. These men discovered the expressive power of the orchestra and spent their time composing symphony after symphony which used dramatic contrast between wind and string timbres, carefully controlled gradations of dynamics, incredible (for the time) finesse in melodic phrasing and demanded an extremely professional approach to ensemble playing. Previous ages had not regarded shades of attack, decay, dynamics or phrasing as necessary to the overall musical effect, so it was quite natural that these new experiences were shunned by some and extolled by others.

About a hundred and fifty years later the orchestra, much augmented, had reached the peak of its achievement in symphonic works like Mahler's Ninth Symphony, Strauss' "Also sprach Zarathustra" (from which BBC TV took its theme music for the Apollo space shots), Stravinsky's "Rite of Spring" and Debussy's "La Mer".

Here, in 1974, we are at the beginning of a new phase, but it is so new that we cannot see where it is all leading. We have at our disposal electronic equipment whose potential is beyond imagination, acoustic instruments which are widening their scope, and yet we are still grovelling in the primeval mud waiting for the particles to settle.

The Mannheim composers churned out symphony after symphony, yet out of this vast acreage of manuscript paper and man-hours there is little of musical value left. Until Mozart and Haydn

arrived and saw a way through there was little in the way of substance but a heck of a lot of mannerisms and repetitive sound effects. What they did not appreciate was that sound effects do not necessarily constitute a satisfactory piece of music.

We are in that same position. The Synthesiser can produce an incredible range of effects, but let us never forget that effects, noises, sounds—call them what you will—are meaningless abstractions in themselves; until they are laid before our ears with some kind of structure—albeit apparently random—they might as well not exist at all.

#### Pitch systems

Until comparatively recently art-music (as opposed to popular or folk music) was indulged in only by those who had some standing in society or who were educated sufficiently to be able to read and write. In early Christian Europe the priests acquired literacy in order to propagate the faith and their written music set the trend for future generations. In order to remember melodies set to specific liturgical texts a new script had to be devised, and it is from this early notation that we know what sort of pitch system they employed. All the chants were based on a series of scales (of Greek origin) containing seven notes to the octave.

These 'modes' took as their key-note (i.e. the note which was a point of focus or of rest) the first pitch in the ascending scale. If one plays the white notes on a modern keyboard starting from D and ending on the D an octave above the Dorian mode will be heard, D being its key-note. It so happens that seven modes were employed, equivalent to playing an ascending sequence of seven notes from any of the seven white notes of a keyboard.

By the sixteenth century some of these modes had proved more popular than others and certain coincidental chords had gained wide acceptance. A hundred or so years later the number of modes had dropped to two and become the major and minor scales, with certain chords from within them predominating. From this point on the whole focus of music has been on the two modes; any elaboration, including excursions into so-called 'chromatic' notes (i.e. discrete pitches not contained in the modes themselves), was largely decorative.

#### Rhythm changes

Rhythm has undergone similar changes. In the Middle Ages poly-rhythm was not unknown; there

are numerous examples of pieces in three melodic lines performed simultaneously which differ from each other in rhythmic phrasing, metre and accentuation as well as language! But the introduction of the bar-line killed that. Originally brought in to aid the performer's eye across the page by grouping rhythmic pitches together, the bar-line became a rigid constraint; underlying pulses were largely grouped into continuous repetitions of 2, 3, 4 or 6 beats at a time with strong accentuation at the beginning of each bar.

In the less clearly-defined area of timbre ideas have changed too. In most early music vocal or instrumental timbre was unimportant. Even as late as the Baroque period (roughly 1650 to 1750) the choice of musical instruments for a given piece was fairly arbitrary, given that the violin family held sway anyway, and instrumental effect, beyond a few acceptable techniques, was negligible. The nineteenth century saw the growth of the orchestra into a mammoth acoustic synthesiser, yet, because of the rhythmic and tonal restrictions imposed on the notes themselves, orchestration tended to represent the icing on the cake.

Schoenberg reached breaking point with the old hierarchical structure of pitch relationships around 1910 when he realised that decorative chromaticism was clogging up the works; he eventually structured chromaticism. Stravinsky and Bartok rebelled against the rigidity of the bar-line at about the same time. In the 1920s Varèse upset the whole works by putting pitch, timbre, rhythm and structure on an equal and totally new footing.

#### Towards emancipation

And now, in the (emancipated?) second half of the twentieth century, electronic technology, though not geared specifically to music, has allowed us to widen our horizons beyond the 'natural'. The aural universe is now apparently boundless and open to everyone, and with the lead given us by Schoenberg and others our ears should be cleansed and our endeavours positively bursting with euphoric enthusiasm. We can now accept or reject the old order of pitch relationships, even 'play between the cracks' of the twelve-note keyboard; we can move into rhythmic patterns unperformable by a human being (though conceived by one); we can choose our dynamics from the inaudible to the painful; we can order timbre to taste; we can utilise the space around the listener; we can be as strict or as free as our imagination permits; the rules are the ones we make ourselves.

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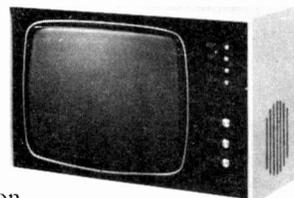
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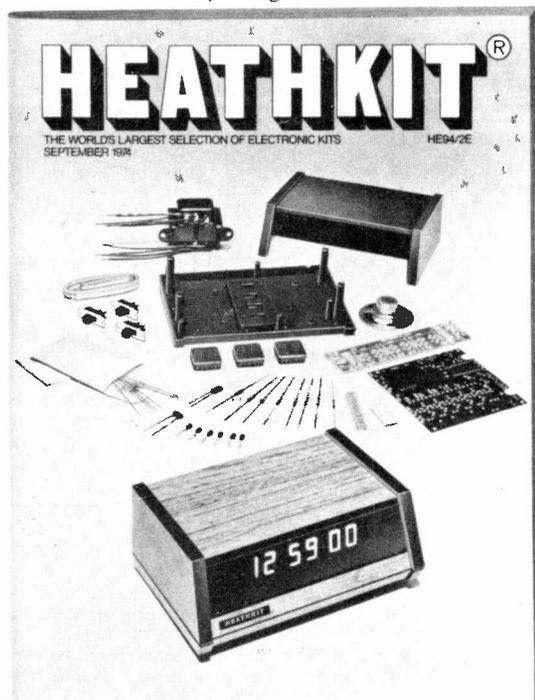
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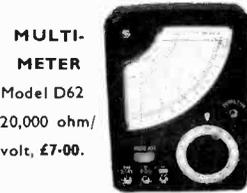


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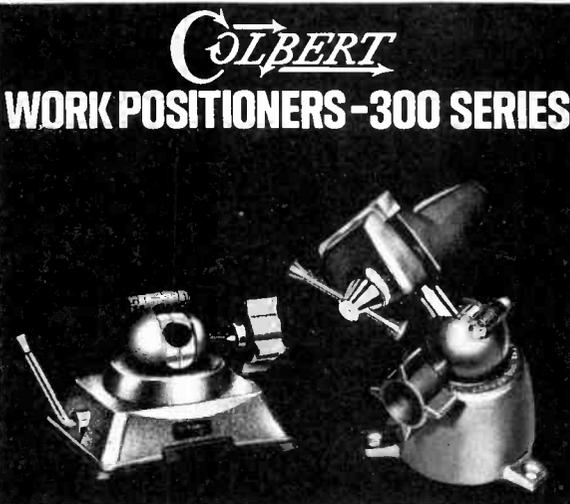
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## Learning by Experience

By now many readers are probably thinking that my presentation of the subject shows rather much bias, considering that I have said more than once that I am not easily convinced. If this is so, I can only repeat that I constantly seek proof that a phenomenon is not explainable by *normal* means, but here it must be clearly understood what we mean by *normal*.

My own belief is that ESP covers a number of presently little-known phenomena, as well as completely unknown ones. But let me give a simple example. Most of us can drive a car or motor-cycle, or at least a bike. Whatever you can drive or ride, cast your mind back to the early day of mastering your vehicle. Remember how you used to panic and force the gear into reverse at about 30 m.p.h., or steer the handlebars to the left when you were falling to the right.

But whatever the mistake, you knew better at the time, but your conscious mind was panicked into doing either the wrong thing, or the right thing too late. But how many times do you find yourself doing silly things like that now? Not very often, if at all. This is mainly because you have conditioned yourself to take the proper course *automatically*. But how?

Well, we cannot be certain exactly, but we do know that practice makes perfect, and that we do not have to think out reasons for doing some things once experience has taught us they are the right things to do at particular times.

The examples above are concerned with facts that conscious learning has precipitated into our sub-conscious mind, and are treated as facts which are known to be true, so our conscious mind can conveniently forget about the experience that taught them to us.

## Subconscious Learning

But it is not only conscious learning that can take place. Experiments using lower forms of animal life, where conscious thinking is absent or near-absent, show that experience is learned at a different level, but certainly learning takes place. When assessing results of experiments concerning ESP we must always look for this kind of learning. Not that it will preclude the existence of ESP altogether but simply that it enables us to categorize what is responsible. At present, it would consider the subconscious learning process as a legitimate ESP phenomenon, because it cannot be placed in the group of experiences using the five senses.

Subconscious learning is a very useful asset, and it is a good idea

to try to cultivate it. I first discovered it after trying to find out what it was that certain successful people had in common. To me it appeared that people I knew who seemed to "get on" did so without flustering and without going about everything deliberately. They seemed to have a curious quality of being able to stay in top gear in everything and very rarely had to change down. Was it, I wondered, that their success made them carefree, or could it be that they owed their success to the state of mind of keeping their cool?



Many years taught me a lot about this. I tried to take things more lightly whenever I could, and if I met obstacles which seemed unsurmountable, I just passed them over and left them for another time, rather like you are told to do in an examination when you don't understand a question. Come back to it later. By this means, you would expect to get along all right on all the easy stuff, but later on you would expect to be faced with a mountain of insoluble problems.

## Limitations of Logic

Logically, this would be true. But statistically, the experience is quite different. In the intervening time, each problem seems to have turned itself around, to show a quite different side, which then looks so simple that you wonder why you did not turn it round in the first place. But you couldn't, because your conscious mind is logical, and logic is certainly not the solution to all problems.

Of course, the problem itself had not altered, but ever since the time that you looked at it initially your subconscious has been working, unbeknown to your conscious mind, on the problem, and has presented the facts, probably quite randomly, and arranged them in a way that logic would not have led you to on its own. Hence, you suddenly see a chink of light and this could be the very thing which leads to the solution you require.

I must stress that some of the above is based on suppositions, as I doubt if any true analysis has been carried out (or even could be) on the actual workings involved.

If you are doubtful about the validity of what I have written, why not try out a few exercises for yourself. Select a few jobs which are not vitally important for starters, of course, or even invent an experiment or two. For instance, try your friends at judging quantities of small identical items, such as beads, beans or dried peas. You will be amazed how accurate some become at selecting say, 30, 50 or 100. Now, if in your first attempts someone arrives at EXACTLY the right number, then you may (or may not) have reason to question whether another form of ESP has crept in, as experience, conscious or subconscious, cannot be seen to be involved.

## Decision Makers

You may well wonder why I have dwelled upon the subject this month, in the form I have chosen. But I assure you, it is very relevant to what I wish to present now and later. Firstly, it has now been established that many people in top managerial positions make decisions which they cannot at the time justify by any particular logical or statistical data. Naturally, it is hard to get an admission out of such people, as admissions to this sort of thing would appear most unscientific. But such decisions later prove to be right, against all evidence of facts available at the time.

A detailed analysis was made of results of some special experiments and is covered in detail in Vol. 1 No. 7 of the *Journal of Paraphysics*, in an article by Prof. John Mihalosky, Newark College of Engineering.

This article is of great interest, and I am going to quote here a few extracts from its text. A number of top decision-makers were asked how they came up with the particular decisions they had to make, many upon which millions of pounds profit or loss might hinge, and the answers were: "I don't think businessmen know how they make decisions. I know I don't" and "You don't know how you do it; you just do it" and "There are no rules"; and "It is like asking a baseball player to define the swing that has always come natural to him" or, as one put it, "Whenever I think, I make a mistake". One even said, "I have found that some of the most horrible mistakes we have made came after I ignored my intuition under the pressure of what looked at the time like unshakeable evidence".

Well, what do you think?

# DEVICES ...APPLICATIONS

## PROTECTED POWER TRANSISTOR WITH A GAIN OF A MILLION

THE NEW LM395 series of devices available from National Semiconductor look like a normal TO3 power transistor, but are actually integrated circuits which behave like fast *npn* power transistors with a current gain of the order of a million. They contain some fifty internal components, including 21 transistors.

The protective circuits incorporated in these devices are one of their most important features. If the temperature of the chip exceeds 165°C, the power output stage is shut down. This enables a much smaller heat-sink to be used with safety than would otherwise be possible. In addition, a current limiting circuit prevents damage to the device by excessive current.

Any number of the devices can be connected in parallel to increase the current capacity, since no device will pass more than the limiting value of the current.

### THE LM395

The LM395 is the most economical device in the series, the price being about four times that of the well-known 2N3055 power transistor. The LM195 and LM295 are similar to the LM395, but can operate over a wider temperature range and have the higher maximum operating voltage of 42V.

The LM395 may be destroyed if the maximum permissible voltage rating (36V) is exceeded, but it is almost impossible to destroy it in any other way.

Even if this device is destroyed by the application of an excessive voltage, it will become open circuited

and will protect other devices in the circuit. (A normal power transistor becomes short circuited if an excessive voltage is applied to it.)

### CONNECTIONS

The connections to the LM395 series of devices are shown in Fig. 1. It should be noted that the case of the device is connected to the emitter electrode. It is expected that the same type of device will be available in the smaller TO5 package in due course.

The typical base current is quoted as 3µA. If a current appreciably greater than this is fed into the base, the collector voltage will fall to its saturation value of about 1.8V for collector currents of up to 1A.

It was found that the device conducted when the base was open circuited, but became non-conducting when the base was connected to the emitter.

The switching time is typically 500ns.

### TYPICAL APPLICATIONS

#### 1. Simple current limiter

The circuit of Fig. 2 forms a very simple current limiter. The internal circuit of the device limits the collector to emitter current to about 2A (minimum 1A at 15V). When no heatsink was used with an LM395 in this circuit with a 6V supply, the current fell to about 0.5A after a short time as the device became hot.

If the base connection is switched from the collector to the emitter of the device, the collector current will fall to the quiescent value of a few milliamps.

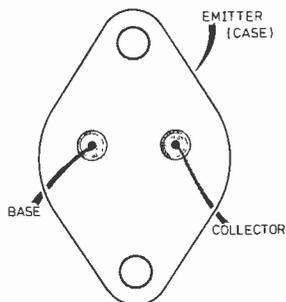


Fig. 1. Connections of the LM395 series of devices (looking at underside)

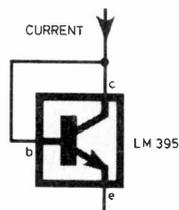


Fig. 2. A simple current limiter circuit using the LM395

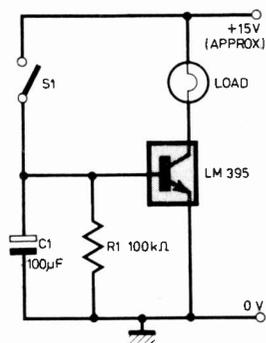


Fig. 3. A simple time delay circuit

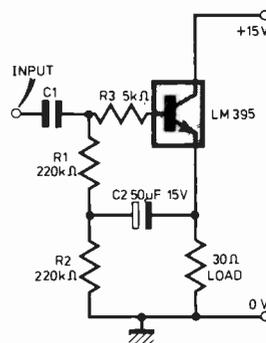


Fig. 4. A very high impedance emitter follower circuit

The base current which must be switched is very small and one could, for example, use the output from a TTL circuit to control a current of at least 1A in the emitter-collector circuit.

## 2. Time Delay

A very simple time delay circuit is shown in Fig. 3. When S1 is opened, C1 discharges through R1. The LM395 remains fully conducting until the voltage between the base and emitter falls below 1V. When the values of R1 and C1 shown are used, the current in the load begins to fall about ten seconds after S1 is opened.

The load shown in Fig. 3 is a lamp, but other types of load may be used. The maximum current is about 2A and this will not be exceeded even if the load is accidentally shorted.

## 3. Emitter Follower

An LM395 emitter follower circuit with a very high input impedance is shown in Fig. 4. The output voltage is fed back to the junction of R1 and R2 so that the voltage across R1 remains almost constant.

This feedback arrangement ensures that the input impedance is very high. The resistor R3 is required to prevent possible oscillation and should be used in all LM395 emitter follower circuits.

The circuit of Fig. 4 can be used to control a current of over 1A in the load using a control signal of high impedance.

## 4. 1A Regulator

The circuit of a voltage regulated supply which can deliver up to 1A is shown in Fig. 5. The output can be set anywhere in the range of 4.5V to 30V by adjusting VR1. The output current is automatically limited by the circuits inside the LM395.

The LM305 device is a voltage regulator which accepts an unregulated input at pins 2 and 3 and provides a regulated output from pin 8. The latter controls the LM395 which is connected as an emitter follower.

The voltage controlling signal is taken from the tapping on the load in the emitter circuit.

## 5. Power pnp transistor

If one requires a *pnp* circuit which is equivalent to the LM395, one may use the arrangement shown in Fig. 6. When a current is taken from the base lead through R1, the transistor TR1 conducts and supplies base current to the LM395.

This circuit has the same thermal overload protection and current protection as the LM395 itself. It may be used in the same way as an LM395 with all polarities reversed.

The LM395 can also be used in operational amplifier circuits which must provide a high output power, in high power oscillators at frequencies up to 1MHz, in switches with optical isolation, etc.

Further details on the LM395 series of devices are available from National Semiconductor, The Precinct, Broxbourne, Hertfordshire.

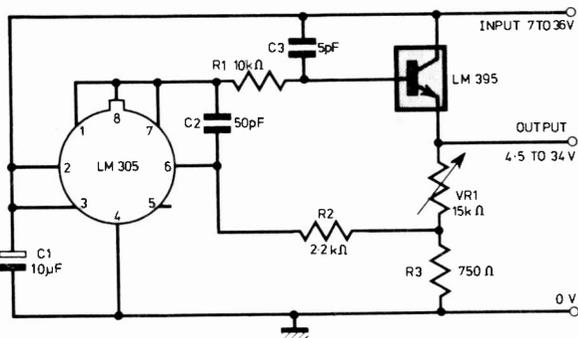


Fig. 5. A one amp voltage regulator with current limiting

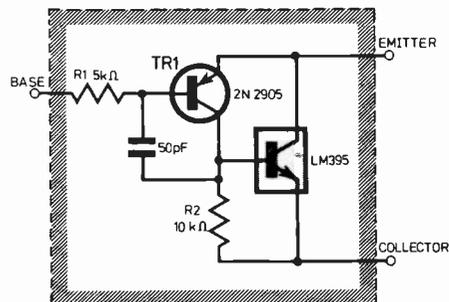
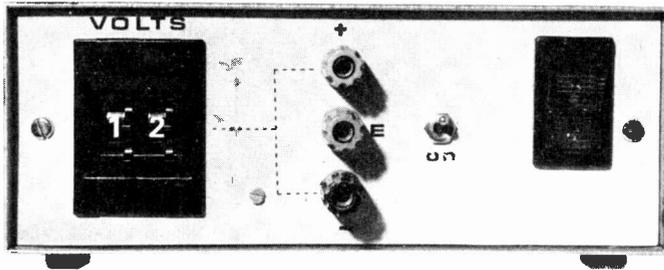


Fig. 6. A *pnp* circuit for a power transistor with thermal overload and current limiting



# BENCH POWER SUPPLY

By D.W. LLOYD

**T**HIS article describes a bench power supply using the minimum of components without sacrificing performance. Normally power units with similar specifications cost anything up to £30; this unit should cost much less than that.

One of the items that makes power supplies costly is the meter which so many people rely on for accuracy when setting up the output voltage. This device however is inaccurate or, to be more correct, will only typically be 2 per cent accurate or worse, which is the tolerance on most meters.

The power unit described here uses no meter and is as accurate as the tolerance on a chain of switched fixed resistors with which the voltage can still be read directly. As can be seen from the illustrations the output voltage is set up by the use of thumb wheel switches and on the particular unit shown the output voltage is in fact controllable from zero volts up to 19V in 1V steps.

## BASIC CIRCUIT

The basic circuit is shown in Fig. 1 from which it can be seen that the mains supply transformer is provided with two secondary windings. One, identified A, is the power supply source proper, whilst the second is a low current winding which powers the regulator chip IC1. This floating mode of powering for the chip allows the sweep of voltage fed to the error amplifier in the regulator to be increased beyond the limits of the voltage of the main power supply.

In this way it is possible to control output voltage from 0 volts to full voltage from winding A.

In addition to allowing full sweep of the output voltage, the use of this floating independent supply for the chip also assists in regulation. Clearly the regulator supply will not vary in the same way that the main supply will as the load is varied.

The circuit is simple and effective in regulation and has the added advantage of being flexible on the current front. By selection of the series regulating transistor the unit can be preset to supply up to 250mA, 1A or 2A whilst using the same control board. The only other basic alteration to increase current output is of course the provision of a suitably rated transformer.

## SPECIFICATION . . .

<b>Supply</b>	230V $\pm$ 20V, 50/60Hz
<b>Output Voltage</b>	Up to 0 to 19V in 1V steps or as required (see text)
<b>Output Current</b>	250mA, 1A or 2A
<b>Output Regulation</b>	0.08 per cent
<b>Line Regulation</b>	For 10 per cent line variation is 0.05 per cent
<b>Ripple</b>	3mV
<b>Output Resistance</b>	10m $\Omega$
<b>Temperature Coeff.</b>	0.02 per cent

The voltage regulator used in the circuit is the 723, generally available from several manufacturers. This chip contains an accurate reference source, an error amplifier and a controlled output with current limit facilities.

Operation of the output is effected as a result of variations in the measured voltage, in this case the output of the main power supply, being fed to the error amplifier which then controls the output to maintain the main voltage at a constant level.

Current limit is achieved by placing a known low value resistor, in the present case R1, in the regulated supply line and making use of the voltage developed across it (which is proportional to current through it) to operate a limit on the current allowed through the main supply. Frequency compensation is provided on the chip through a feedback link to pin 13 via capacitor C4.

## OPERATION

The regulator supply, winding B, is rectified by bridge rectifier D2 and smoothed by C2 before passing to pins 7 and 12 of the i.c.

Similarly, the output of winding A is rectified by diode bridge D1, smoothed by capacitor C1 and then subjected to regulation as a result of the output current and voltage requirements. Control is effected mainly by the series transistor TR1 in the case of 250mA output or TR2/TR3 in the case of 1 or 2A outputs. Connections for the three forms of circuit are shown in Fig. 1.

Resistors R2 and R3 are used either in parallel or associated with TR2 and TR3 which are run in parallel. Thus they present a 1.1Ω series resistance.

The main sensing and control signal is obtained from the series chain R4, VR2 and R6, being tapped from this chain and fed via R5 to pin 4 of the regulator i.c. Resistor R4 determines the output voltage and can be made up in a number of ways.

In the prototype R4 is formed of a series of discrete resistors selected to give unit and decade switching of the output voltage from 0V to a maximum dependent on the output of winding A. In the prototype this is 19V. Selection of the resistors is by means of two thumbwheel switches S3 and S4 connected between points P3 and P4 of the circuit although of course rotary switches or, for that matter a 10-turn potentiometer, could be used if desired.

In order to allow the controlled voltage to be swung down to zero volts the non-inverting input of the error amplifier in the regulator chip is connected to the negative output rail whilst the inverting input is connected to the sensed voltage. In this way the

negative supply to the i.c. from winding B is negative with respect to the negative of the main output by the same value as the reference voltage.

Any variations in the main output are fed back into the regulator and serve to control the output in the opposite sense, thus giving stabilisation. The chain including VR2, R6 and R4 serves to set the point about which stabilisation occurs.

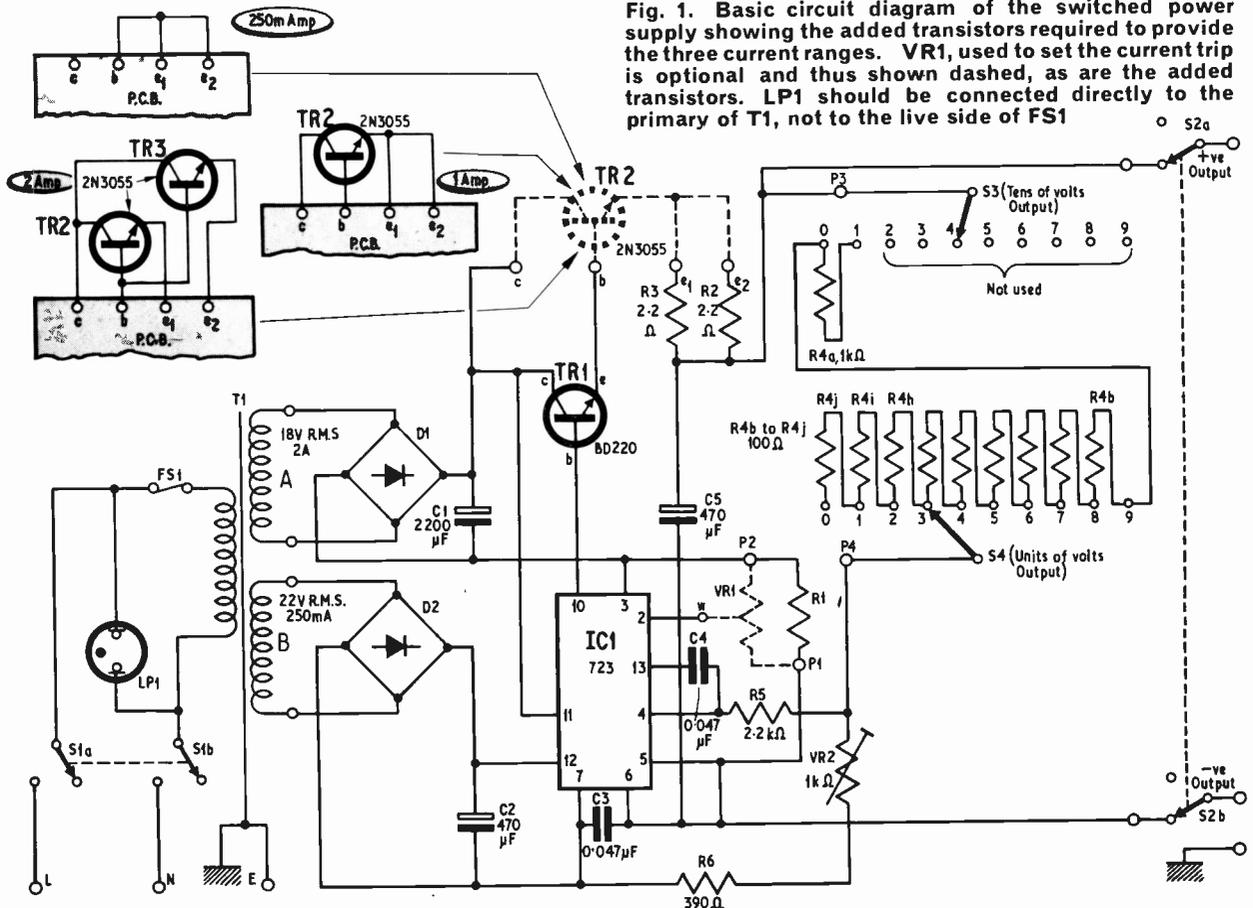
Preset potentiometer VR2 serves to ensure that the current through the chain is 10mA, a value at which the values of the step resistors selected by S3 and S4 can thus become 1kΩ and 100Ω respectively for steps of 10V and 1V respectively. In this way the output voltage control is as accurate as the resistors selected so that 1 per cent resistors give a control function to 1 per cent and 0.1 per cent to the same 0.1 per cent level.

### EARTHING

It will be seen that neither side of the output is earthed to the chassis or to an output earth point. This allows the unit to be used in any configuration of other units; to supply, for example, the positive or the negative half of a double supply or perhaps even be used in series with another supply to uprate the output voltage.

An earth terminal connected to the unit case is mounted on the front panel and can be connected externally as required to either rail.

Fig. 1. Basic circuit diagram of the switched power supply showing the added transistors required to provide the three current ranges. VR1, used to set the current trip is optional and thus shown dashed, as are the added transistors. LP1 should be connected directly to the primary of T1, not to the live side of FS1



# Components . . .

## Resistors

- R1 1Ω 1W, wire-wound (n.i.) for 1A version
- R2 2.2Ω 2W
- R3 2.2Ω 2W
- R4a 1kΩ or as required, see text; 1% or better
- R4b to j 9 × 100Ω or as required, see text, 1% or better
- R5 2.2kΩ 2%
- R6 390Ω 2%

## Potentiometers

- VR1 100Ω pre-set
- VR2 1kΩ pre-set

## Semiconductors

- D1 10DB1A bridge rect.
- D2 10DB1A bridge rect.
- TR1 BD220
- TR2 2N3055
- TR3 2N3055
- IC1 723 d.i.l. stabiliser i.c.

## Capacitors

- C1 2,200μF, 25V
- C2 470μF, 50V
- C3 0.047μF
- C4 0.047μF
- C5 470μF, 25V

## Switches

- S1 D.P.D.T. mains switch
- S2 D.P.D.T. miniature 2A d.c. toggle
- S3 Digital Thumbwheel (Birch Stolec Ltd.)
- S4 Digital Thumbwheel (Birch Stolec Ltd.)

## Transformer

- T1 240V, 50Hz 1/P, 18V r.m.s. @ up to 2A and 22V at 250mA O/Ps. Type 1069, £3.85, Zeta Windings, 26 All Saints Rd., London, W.11; Toroidal form is Type T1182 from Siga Electronics Ltd., Sandy, Beds.

## Miscellaneous

- Case, terminals, p.c.b., 1A fuse (FS1) and holder



Fig. 2. Printed circuit master for the power supply

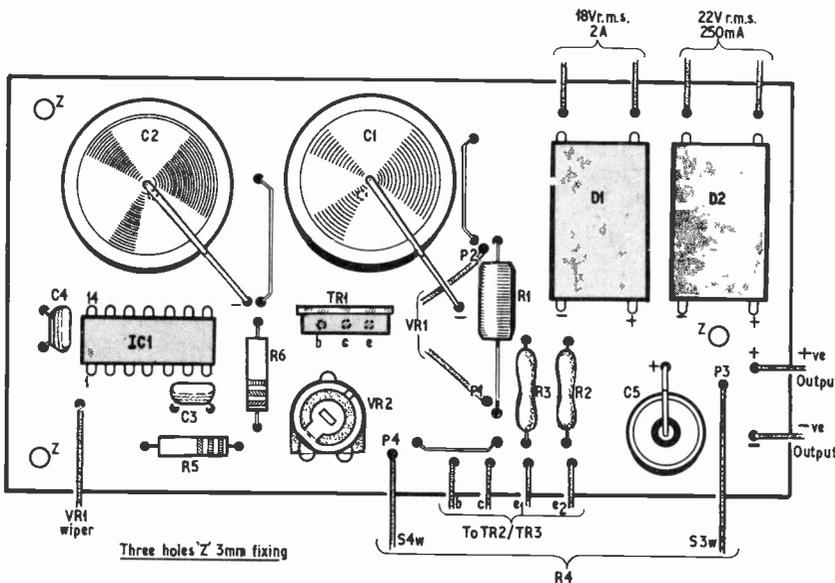


Fig. 3. Layout of components on the circuit board of Fig. 2 identifying the flying leads to other circuit devices

## CONSTRUCTION

As can be seen from the illustrations, construction is simple and in fact is quite flexible since some of the options used in the prototype can be altered to suit individual requirements.

For example, whilst the printed circuit board and layout shown in Fig. 2 and Fig. 3 includes only the main components of the circuit, with the transformer and switched resistors mounted elsewhere, some constructors may wish to have a much larger board and mount all or most of the components thereon.

As has been noted, switch S3/S4 could be replaced by a rotary unit or even by a potentiometer if required or even by a fixed value resistor if only one output voltage is required. It should be remembered that any deviation from the electrical arrangement suggested might degrade the performance by introducing errors so alterations in this part of the circuit should be viewed with some care.

A single-throw mains switch with self-contained neon indicator was used in the prototype but of course any suitable arrangement can be used here as in the switching of the d.c. rail by switch S2. This latter is included in the circuit so as to avoid build-up and decay time problems which occur when switching the mains supply. The latter being switched ON most of the time and supply switching being effected in the d.c. rail.

There is no particular problem with the remainder of the assembly except perhaps with the power transistors used at TR2 and TR3 where these are needed. In the prototype the output was set to 1A so that only TR2 was required. The (or each) device is mounted on the back panel of the unit using the mica insulating washer supplied with the transistor so as to avoid shorting the transistor to earth.

## MAINS TRANSFORMER

A toroidal transformer was used in the prototype as one was to hand and in any case is smaller than its more normal counterpart, thus allowing a smaller case to be used. Using a toroidal transformer the radiated magnetic field is also smaller than with a conventional device, but either may be used if required.

The square holes in the front panel for the thumb-wheel switches were cut by first drilling and then filing. If some other form of switching is used then obviously this step is avoided.

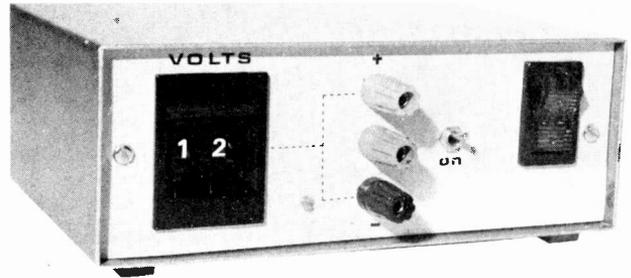
Finishing touches have been added using Letraset over the top of a coat of paint followed by fixing varnish to give a professional appearance.

## TESTING

After assembly the first thing to check is the isolation of the power transistor/s case/s. A simple resistance check here and at the mains input lines to ensure that nothing is shorted to chassis or elsewhere is always valuable at this stage.

Switching on the supply should now illuminate the mains neon indicator and of course produce voltages in the circuit. Check that the voltage across C1 is not less than 22V. That across C2 should be not less than 28V and not more than 40V.

The output level is set quite simply by placing a voltmeter across the output, setting the switches to give a 1V output and then adjusting VR2 until the output is indeed 1V.



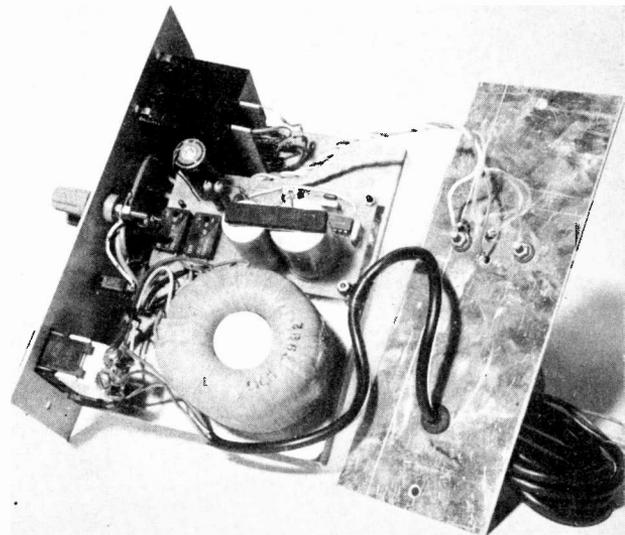
## CURRENT LIMITING

It is quite simple to set the current limit to the required value. Take the case of a 1A unit. Set the output switches to the 10V position and connect a 10 $\Omega$  load so that a 1A current flows. Monitoring the output voltage, adjust an added current limiting potentiometer VR1 between points P1 and P2 (shown dotted in Fig. 1) till the output voltage just starts to fall. Turn the potentiometer back a little so that the supply is operating in the regulated portion of its curve and the output is now set to limit at just over 1A. The potentiometer may now be replaced by fixed resistors if required. If VR1 is not used at all and the load current determined by R1 alone then points W and P1 on the circuit should be shorted together.

A simple way of testing this is to leave the meter connected, remove the load and then to switch on with the meter switched to a range greater than 2A. In this case the meter forms its own load and the reading should be just over 1A.

A check of the voltage over the load (meter) will show that this has dropped to a very low level. This illustrates the way in which this design acts to protect load circuitry connected to the output when shorts exist in that load. ★

**Exploded view of the prototype power supply showing the use of a toroidal mains transformer, digital thumbwheel switches and the power transistor mounted on the rear panel**



# INGENUITY UNLIMITED

A selection of readers' suggested circuits. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought. This is YOUR page and any idea published will be awarded payment according to its merits.

## A SIMPLE CONTINUITY TESTER

FIG. 1 shows three gates of the familiar 7400 connected via R1 and C1 to form a relaxation oscillator continuity tester. The output is fed through the remaining gate, which acts as a buffer amplifier, to LS1, a miniature earphone. With the values shown for R1, C1 and LS1 the frequency is about 800Hz. Virtually any earphone or loudspeaker can be used. If one of a lower resistance is chosen the signal may be unacceptably loud, but can be reduced to any level by inserting a suitable series resistor.

The test leads can be in either positive or negative supply. When they are joined the note will sound and the current flowing will be about 8mA. The oscillator will continue to sound until the battery has run down to three volts or less.

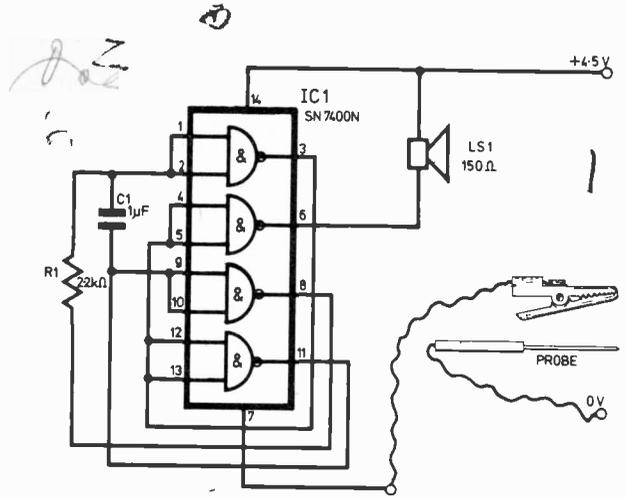


Fig. 1. Integrated circuit continuity tester

When the test leads are connected across a resistance a higher note is produced. The device is useful up to some 400 ohms or so and is just audible across 1 kilohm. The smallest resistor which can be distinguished from no resistance at all is about 4 ohms.

Diodes, if tested so that they are reverse biased, do not of course make the oscillator sound. If forward biased the note is about a third, musically speaking, higher than when the leads are shorted.

The polarity of the test leads should therefore be marked. Capacitors of 40μF and up give a chirp as they charge.

R. Parfitt, Croydon.

## TOUCH START OF AUTOMATIC RHYTHM DEVICE

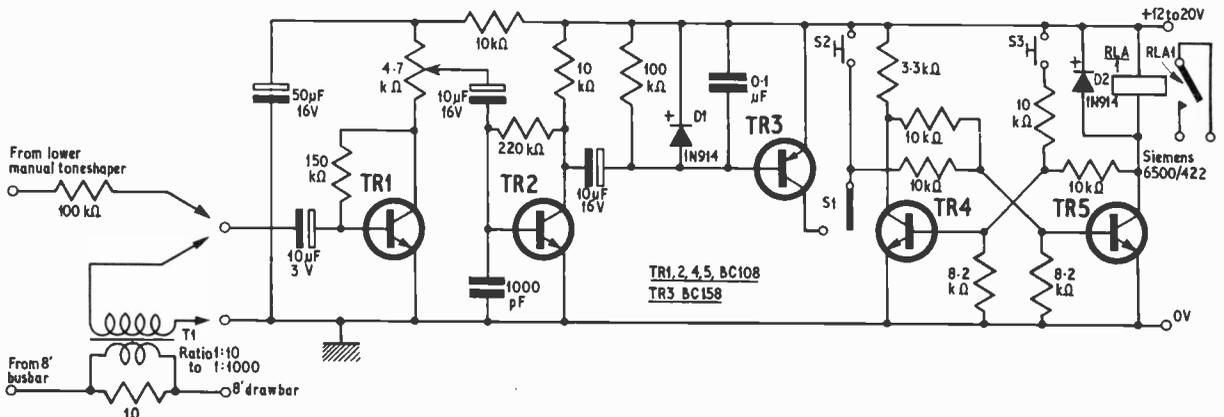
VERY few electronic organs manufactured before 1970 are equipped with facilities for remote control of an automatic rhythm device. This circuit is activated by an audio signal from the lower manual (or pedal), making it possible for the performer to play the prelude on the upper manual and the pedal, and when the first note is played on the lower manual, the rhythm accompaniment is started.

At the front end of the circuit two alternatives are shown; a high impedance input for connection to the lower manual toneshaper output of an electronic organ, and an electromechanical Hammond

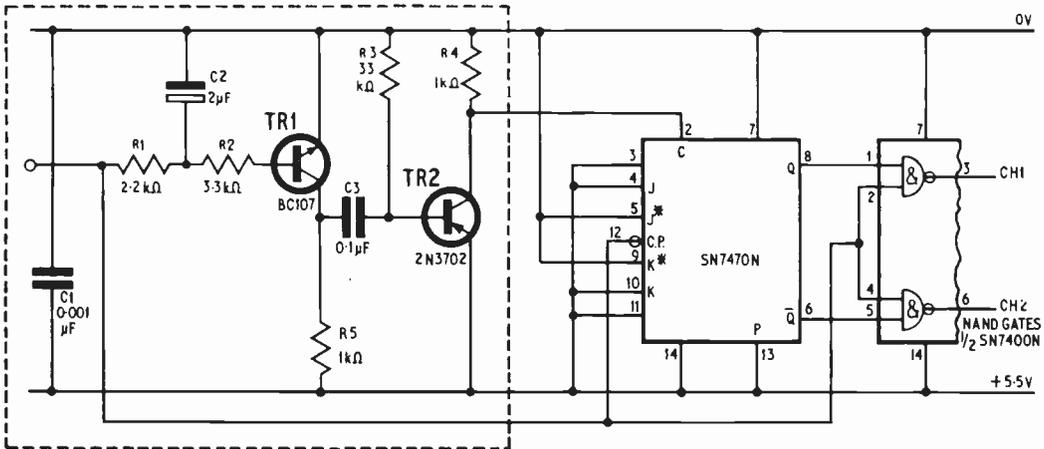
organ connection using a transformer and a series resistor.

The transformer could be any output transformer for use in portable radios with a ratio of 1 : 10 to 1 : 1,000. An incoming signal will be amplified through TR1 and TR2, and turn on TR3. If S1 is closed, a current will pass through to TR5, triggering the bistable, causing the relay to pull in. S2 and S3 are used for manual start and stop.

K. B. Sorensen, Copenhagen, Denmark.







THE circuit of Fig. 1 shows a decoder capable of dealing with a two-channel system. It was developed as a result of work carried out with the Radio Control System described in P.E. in December 1971 and the following two issues.

The section of the circuit enclosed in a dashed line replaces the re-triggerable monostable and associated components of the earlier system and can be used in its place to supply the clear pulse to the shift register for more than two channels if required.

Positive pulses are fed from the receiver (if negative then they can be inverted by a spare gate).

TR1 is held on by the input voltage whilst the pulses are being received and remains on for a short time after the second pulse.

When TR1 turns off a positive pulse through C3 turns TR2 off for a short time. It is normally held on by R3 connected to the 0V rail. This produces the required negative-going clear pulse.

The outputs from the edge-triggered flip-flop are fed to two gates along with the input signal and the separate outputs are obtained. The unused J and K inputs are connected to positive to give better noise immunity. A. Sansome, Sutton Coldfield.



# BOOK REVIEWS

## EFFECTIVE TECHNICAL WRITING AND SPEAKING

By Barry T. Turner

Published by Business Books Ltd.

206 pages, 9½in × 6½in. Price £4.75

THE so-called "communications explosion" places greater and heavier responsibilities upon all communicators, whether they be scientists, engineers, technical writers in industry, or contributors to the technical press.

This book has been prepared to help those who may be called upon to present technical information through the medium of the printed or spoken word. The author is Professor of Industrial Management, University of Newcastle-upon-Tyne. The work is an excellent textbook covering the special requirements and practices involved in the many forms that communication can take.

Technical report and article writing, technical business correspondence, preparation of specifications and standards, handbooks and manuals, and patent writing receive individual expert consideration.

On the aural side, the preparation and delivery of talks and lectures, and the running of meetings receive detailed treatment.

As would be expected, this book is itself a good example of the doctrine it preaches; clear exposition of facts, good division and arrangement of contents, supported by many useful references for "Further Reading," and finally nicely rounded off with an extensive and valuable collection of appendices.

An indispensable companion for all who, whether in the course of duty or by choice, have at times to perform in the role of a communicator of technical information. F.E.B.

## SEMICONDUCTOR DEVICES:

### Testing and Evaluation

By C. E. Jowett

Published by Business Books Ltd.

134 pages, 9½in × 6½in. Price £5.00

THIS is a specialist's book, and is probably unique.

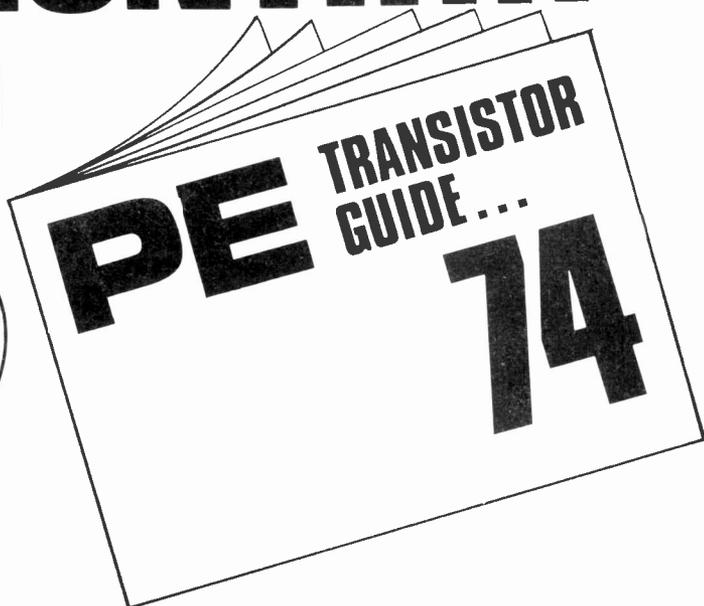
It deals with the subject of standard comprehensive testing of semiconductor devices within industry. Thus its appeal will be chiefly to those engaged professionally as designers or technicians and to college and university students. To such readers, this volume will no doubt constitute a definitive source of reference, and its recommendations and procedures are thus likely to become widely adopted.

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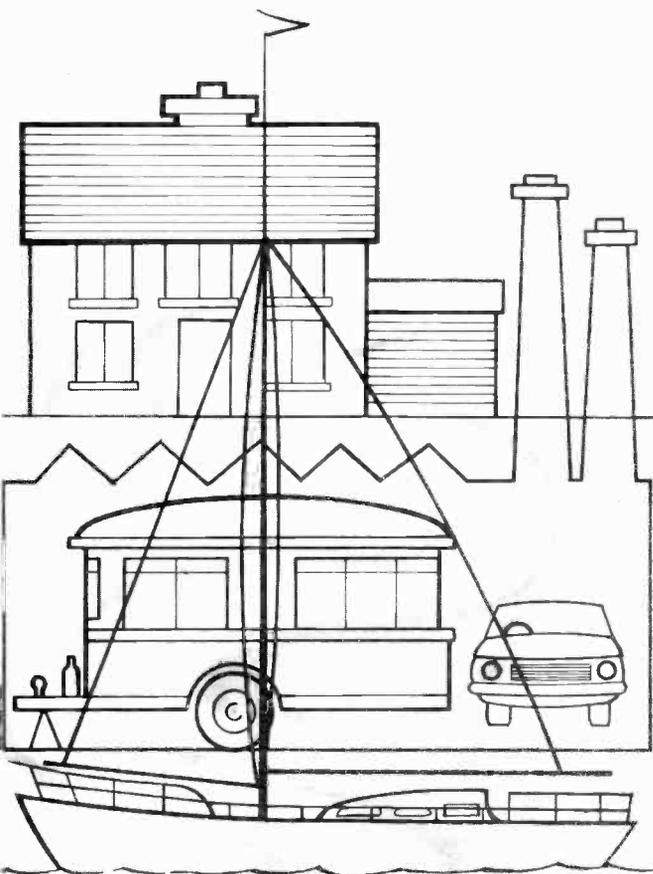
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# PRACTICAL ELECTRONICS

Because of prevailing production problems, no firm publishing date can be announced for the October issue. Readers are advised to check regularly with their local supplier from mid-September onwards.



# GAS DETECTORS

... FOR HOME · FACTORY  
CARAVAN · BOAT

By J. C. PERRETT

*Several circuit variations using state-of-the-art catalytic gas/smoke detectors to indicate the presence of such dangerous materials as methane, propane or butane*

**T**HE increasing use of portable gas stoves in caravans and boats each year brings its own crop of accidents, so that any instrument which might give adequate warning of a dangerous situation must be considered useful, particularly if it is easy to build and use.

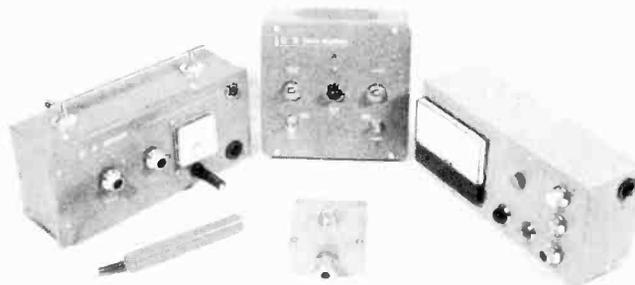
The various circuits described in this article meet this sort of demand, and may be used either as alarms or monitors for changing levels of gas or smoke in the home, boat, caravan and even industrial environment. A total of six circuits are shown. The first is a general test circuit which allows the user to ascertain the performance of the sensor used with any type of gas or smoke.

Other circuits include mains driven units which may trigger audible alarms or lamps, and a portable battery/mains unit which allows operation from dry batteries, suiting the circuit to leak detection of gas from pipes or tanks. The sensor is remote from the instrument.

The penultimate circuit discussed is that of a twin station unit designed specifically for use in boats from either 12 or 24V. A multi-station unit is discussed as an experimental project.

## THE SENSOR

The systems proposed use one or other of the Figaro Engineering sensors described in the July and September 1973 issues of Practical Electronics. When the sensor is exposed to fresh air it assumes a high resistance state but as it absorbs de-oxidising or combustible gases such as hydrogen, carbon monoxide, methane, propane, butane, alcohol, or the carbon dust contained in smoke, the resistance decreases.



The devices vary in characteristic. Type 308 sensor has a very long warm up time of between 5 and 10 minutes and is, therefore, better suited for use where only occasional turning off or on is required. However, the device is very sensitive to carbon monoxide and smoke.

Three other types of sensor are available and are suited for high voltage use up to 100V. These are the type 109 general purpose detector requiring a 1V heater and a 4k $\Omega$  load which takes 2 to 3 minutes to warm up and the 105 which has a warm up time of approximately 1½ minutes.

Finally, the type 102, suitable for carbon monoxide and smoke detection, has a 1V heater and requires 5 to 10 minutes warm up time.

The life of all devices is approximately two years with normal use.

## CIRCUITS

Fig. 1 shows a basic experimental circuit which will allow a reader to determine for himself the reactions of the transducer to various stimuli if VRL is plotted against concentration of the stimulus in air.

An alarm may constitute almost anything, though a 6V bell is used in the most simple prototype. Because the current for the bell (Fig. 2) is fed through a thyristor, the bell becomes polarity conscious. This unit may be simply built on a piece of tag strip and is useful for permanent site monitoring of environments where gas appliances are used.

The components to the left of the line Z-Z in Fig. 1 constitute a mains power supply and is repeated in some following circuits and denoted by the reference to Z-Z in those figures.

The circuit of Fig. 3, the first prototype, is also mains operated, but includes meter monitoring and a light which gives visual warning of a pre-determined level of gas.

The alarm is driven by monitoring the voltage across transducer using the meter bridge circuit, D1 to 4. This voltage is also applied to the base of TR1. The 1kΩ VR2 is the alarm sensitivity control which attenuates the voltage available to drive the base

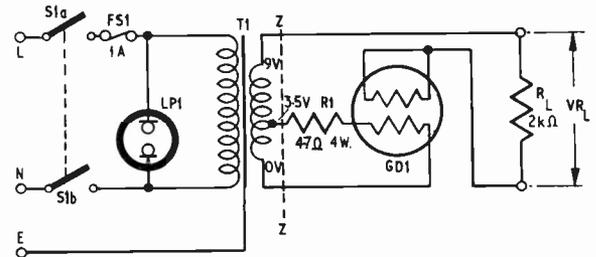


Fig. 1. Test circuit for examining the characteristics of the Figaro gas detectors

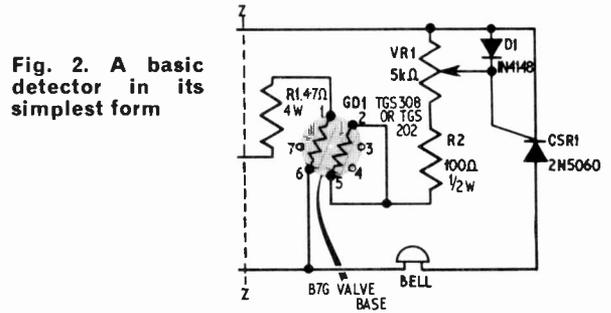


Fig. 2. A basic detector in its simplest form

## COMPONENTS . . .

### Resistors

- R1 4.7Ω 4W
- R2 1.8kΩ ½W
- R3 1.8kΩ ½W
- R4 470Ω

### Potentiometers

- VR1 5kΩ Lin.
- VR2 1kΩ Lin.

### Semiconductors

- D1 to 4 OA91 (4)
- D5 1N4001
- TR1 BC107
- TR2 BFY50

### Miscellaneous

- F2 2A fuse and holder
- GD1 TGS 308 or TGS 202 and B7G valve holder
- LP2 6V bulb and SL90 holder
- LP3 6V bulb and SL90 holder
- ME1 1mA moving coil meter
- Case AB17 aluminium box, 10 × 4.5 × 3in

## MAINS GAS/SMOKE DETECTOR

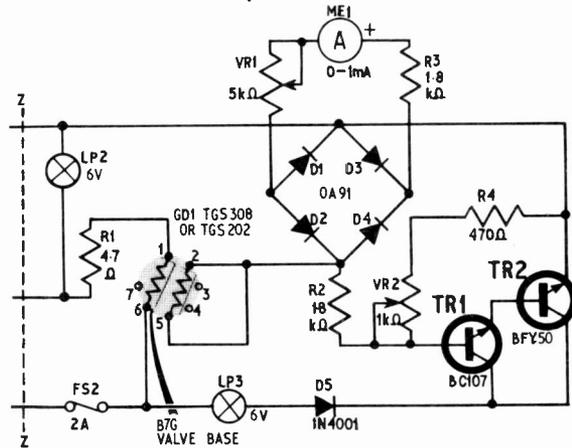
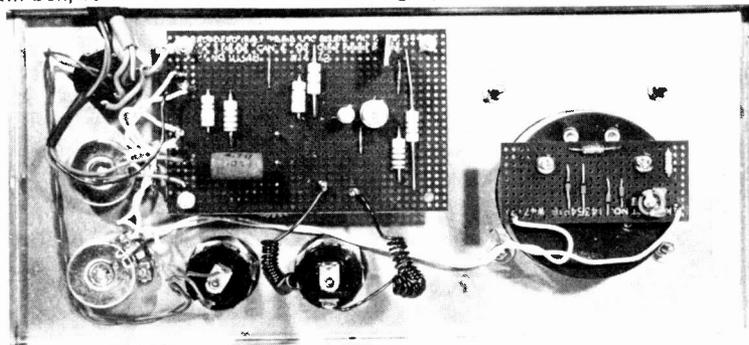


Fig. 3. The prototype mains operated version of the gas/smoke detector

Rear view of the front panel of the mains unit showing location of the various components, Veroboard and meter. The detector socket is mounted in the panel behind the Veroboard



of TR1. The inclusion of diode D5 prevents the base/collector junction of TR1 becoming forward biased during the time when the emitters of TR1 and TR2 become positive.

The detector itself may be neatly mounted using a B7G valve base, as shown in the illustrations; the heater becoming pins 1 and 6. The sensors may be fitted either way round, in pins 1, 6, 2, 5 of the valve base. Such a circuit is simple and may easily be assembled onto Veroboard.

It is possible for the detector to be used remote from the main circuit board by using a 3-core mains lead of at least 5A capacity. If a very long length of lead is used the resistance of the cable connected to pins 1 and 6 of the B7G base should be subtracted from the 4.7Ω ballast resistor R1 so that the heater voltage remains correct for the type of sensor fitted.

The circuit of Fig. 3 is one of the non-latching type and will automatically stop showing an alarm condition when the gas concentration falls below the level set by the alarm sensitivity control VR2.

## PORTABILITY

The low voltage heater used in the transducer makes battery operation difficult, the problem being aggravated by the dependence of the sensitivity of GD1 on the heater voltage. If batteries are used directly, stabilisation of the heater supply will be required, but most methods of doing this are very inefficient due to the high power loss in the regulator section of the instrument.

To overcome this a chopper supply has been proposed in Fig. 4, and this circuit will allow the unit to be used from HP11 torch batteries.

To understand the circuit we first must study the power requirements for the gas detector. The heater requires 1.5V and the heater resistance (cold) is approximately 2Ω. In normal use a current of 0.5A is required.

Thus the power requirement is 0.75W.

From this point forward we are only interested in the power requirement of the device. Assume

that the use of a 10V supply is convenient; if the 10V supply is connected across the heater the power dissipated would become

$$\frac{V^2}{R} = \frac{100}{2} = 50W$$

It is quite obvious that if current continued to flow the device would be destroyed.

This problem is overcome by pulsing the supply voltage to reduce the average power dissipation to 0.75W. To calculate the mark/space ratio required to reduce the heater power from 50W to 0.75W use the formula:

$$\begin{aligned} \text{Mark/space ratio} &= \frac{\text{Max peak power (instantaneous)}}{\text{Average power dissipation required}} \\ &= \frac{50}{0.75} = 66 : 1 \end{aligned}$$

In the circuit of Fig. 4, a mains or battery version designed for portability, the multivibrator comprising TR1, TR2, TR3 is capable of providing a 100 to 1 mark/space ratio. The output of the oscillator appears at the emitter of TR3 which is connected to base of TR4, this transistor acts as a switch which connects the detector to the supply voltage. The oscillator frequency is not critical and runs at a few hundred hertz.

In practice a 0.5Ω resistor is connected in series with the sensor to reduce the peak current and increase circuit flexibility. This somewhat lowers the overall efficiency but is worthwhile. The inclusion of this resistor modifies the drive requirement for the sensor. The equivalent circuit is now a 0.5Ω resistor, the detector and TR4 in series across the supply.

Ignoring TR4  $V_{sat}$  the voltage across the detector now becomes 8V providing a peak power of 32W. This gives a mark/space ratio of 42 : 1. Thus total battery drain, maximum current divided by the mark/space ratio is 0.095A.

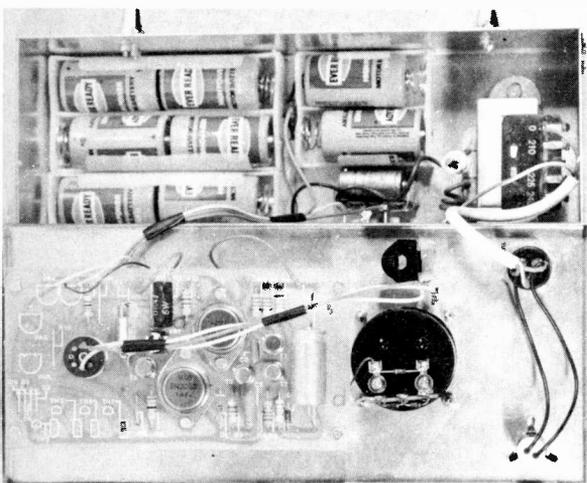
For this current approximately 0.025A should be added to allow for circuit operation. Thus the total requirement is 120mA.

The capacitor C1 supplies the high current pulses required during the time when TR4 is conducting. When TR4 is off C1 charges from the supply transistor TR5.

## BATTERIES

If the completed unit is to be used as a portable instrument it may be powered by heavy duty HP11 batteries. The gas concentration meter can also double as a voltmeter which may be switched to monitor the supply. To allow the sensor to be used as an alarm its performance must be predictable, even if the supply voltage changes. For this reason a power regulator circuit is recommended.

Due to the long mark/space ratio required, a high current consumption is normally drawn by the multivibrator which reduces circuit efficiency. To overcome this problem TR1 is included to give extremely rapid charging of C2. During the time when TR2 is conductive, C2 turns off TR3, the collector of TR3 is therefore at full supply potential. Supply is placed on the base of TR1 via R4, making it non-conductive and R1 is now the feed resistor for TR2.



The portable mains/battery version opened up to show location of the main component parts. Note the use of battery holders and only part of the p.c.b. circuitry

# PORTABLE GAS/SMOKE DETECTOR

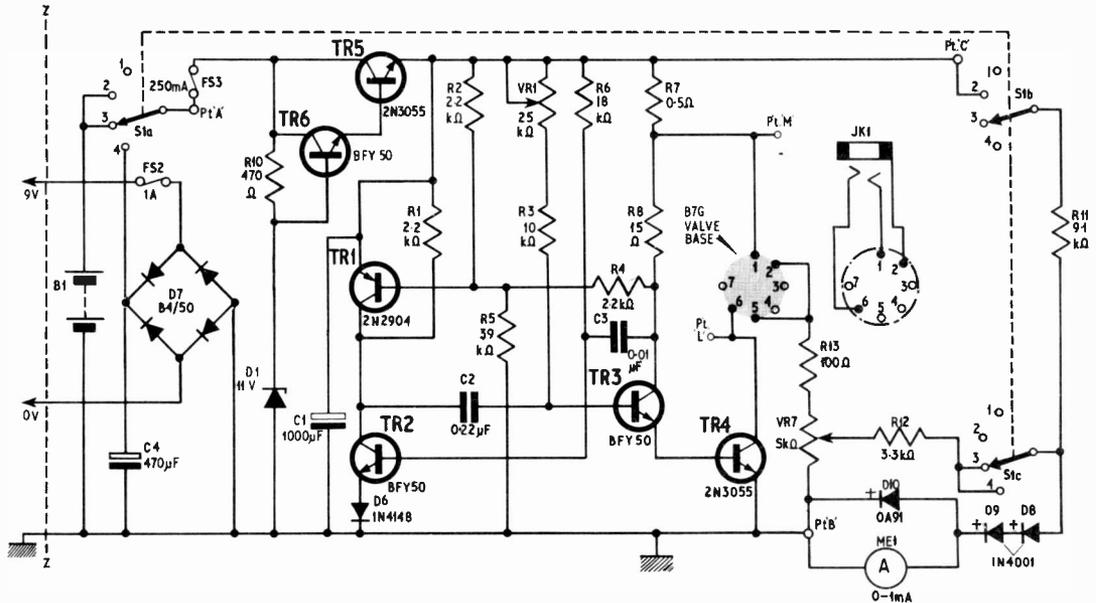
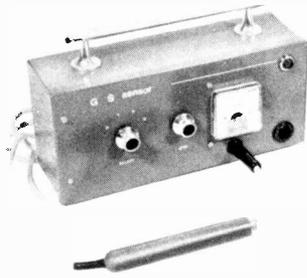


Fig. 4. The portable battery/mains detector using a plug-in head which connects with the instrument via a stereo jack plug and socket

## COMPONENTS . . .

R1 2.2k $\Omega$	R7 0.5 $\Omega$ 4W
R2 2.2k $\Omega$	R8 15 $\Omega$
R3 10k $\Omega$	R10 470 $\Omega$
R4 2.2k $\Omega$	R11 9.1k $\Omega$
R5 39k $\Omega$	R12 3.3k $\Omega$
R6 18k $\Omega$	R13 100 $\Omega$

All  $\frac{1}{2}$ W unless otherwise specified

### Potentiometers

VR1 25k $\Omega$ pre-set
VR7 5k $\Omega$ Lin.

### Capacitors

C1 100 $\mu$ F, 25V
C2 0.22 $\mu$ F
C3 0.01 $\mu$ F
C4 470 $\mu$ F, 25V

### Diodes

D1 11V, 400mW Zener
D6 1N4148
D7 B 4/50 Bridge rectifier
D8 1N4001
D9 1N4001
D10 OA91

### Transistors

TR1 2N2904	TR4 2N3055
TR2 BFY50	TR5 2N3055
TR3 BFY50	TR6 BFY50

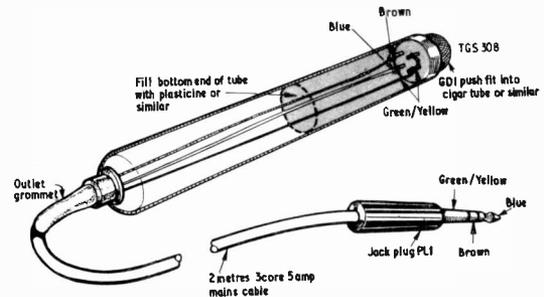


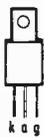
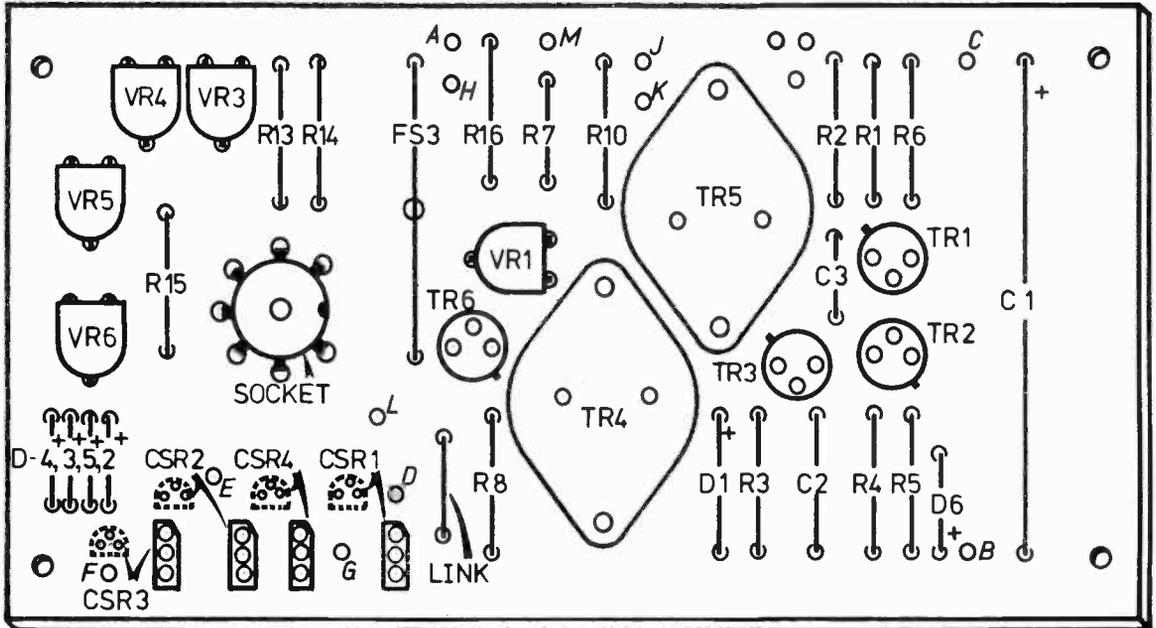
Fig. 5. Detector head made up from an old cigar tube, mains lead and stereo jack plug

### Miscellaneous

GD1 TGS308
M1 1mA moving coil meter
S1 3-pole 4-way selector switch
F2 1A mains fuse
F3 250mA fuse

Printed circuit board, batteries and holder, case AB17, 10 x 4.5 x 3in, Bulgin 1.5A chassis plug, socket, knobs, fuseholders, stereo jack PL1 and socket JK1, and power supply section from Fig. 1.

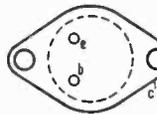
# MASTER PRINTED CIRCUIT BOARD



TIC106



SN5060  
SN5064



2N3055  
2N2904



2N2904  
BFY50

Fig. 7. Printed circuit board component layout suitable for all versions

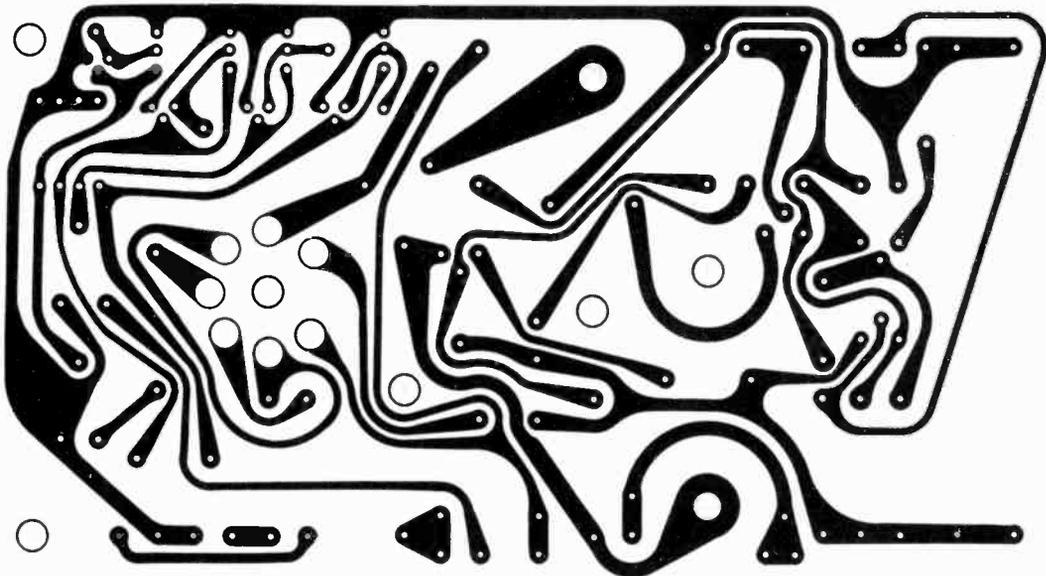


Fig. 8. Printed circuit master (full size) suitable for all versions of the gas/smoke sensors

As C2 discharges through R3-VR1, TR3 comes into conduction and the collector voltage falls. This falling voltage via C3 turns off TR2, at the same time the voltage on the base of TR1 is reduced, which causes TR1 to saturate; this connects the left hand side of C2 to the supply line, causing it to rapidly charge. The circuit will remain in this condition until C3 discharges through R6.

The output of the oscillator is taken from the emitter of TR3 to ensure sufficient drive to make TR4 saturate. Waveforms for the circuit are given in Fig. 6 and details of the head mounting are in Fig. 5.

## INDICATION

The meter ME1 is driven from the slider of VR7, the sensitivity attenuator control. Overall sensitivity is set by the value of R13. Two diodes D8, D9, in series with the meter allow a suppressed zero effect to be obtained without attenuation of the signal and D10 provides some degree of overload protection for the meter.

Switch S1 provides four switch functions. Position 1 is off. 2 allows the regulated supply voltage to be measured, normally 9.5V on load. Position 3 allows the instrument to run from the batteries, and position 4 is for use from the mains. Note that it is not possible to turn off mains power without removing the plug from the front panel. Connection to the mains is indicated by the neon lamp LPI.

## CONSTRUCTION

Any well ventilated case may be used to house the circuit of Fig. 2, and the components may be mounted on tag strip. The thyristor CSR1 is suitable for alarm currents up to 0.8A.

The prototype of Fig. 3 is shown built inside an AB17 case, the circuit built on Veroboard, part of which is fixed to the rear of the meter.

A printed circuit layout is shown (Figs. 7 & 8) of the portable version of Fig. 4, for those people who like to make their own p.c.b. The board holds most of the components. The attenuator control (pre-set) should be left off the board, taking two wires from the board to connect to the remote 5kΩ pot on the front panel.

The p.c.b. has room for extra components not listed for this circuit. These are made use of in further versions. In addition, the p.c.b. can accept two sizes of thyristor, the TIC 106 and the 2N5060 to 2N5064 series. The former will switch up to 4A with a sink whilst the latter will only cope with lamp circuits up to about 0.8A. Clearly the constructor may decide which he prefers to use dependent on external loads he might wish to apply.

Wiring details of some of the off-board components is shown in Fig. 5. The jack socket must be of the insulated type to avoid supply to chassis shorts as this may well destroy the detector.

The latter is fitted into a discarded cigar tube and should be a good push fit. A hole drilled in the other end allows the 5A, 3-core cable to enter. A rubber sleeve must be fitted to stop cutting of the wire. As the cigar tube is very light, Plasticine may be added to the inside to give the unit a better balance.

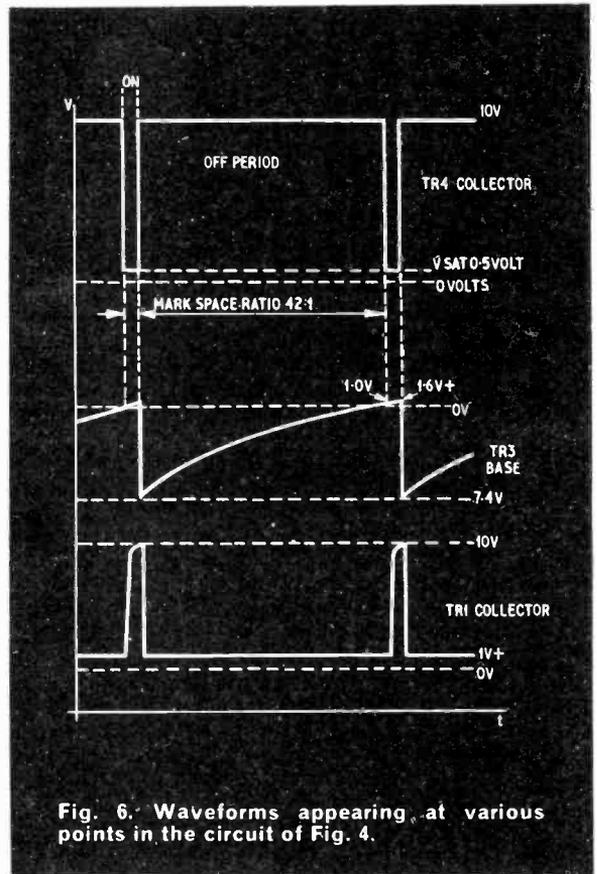
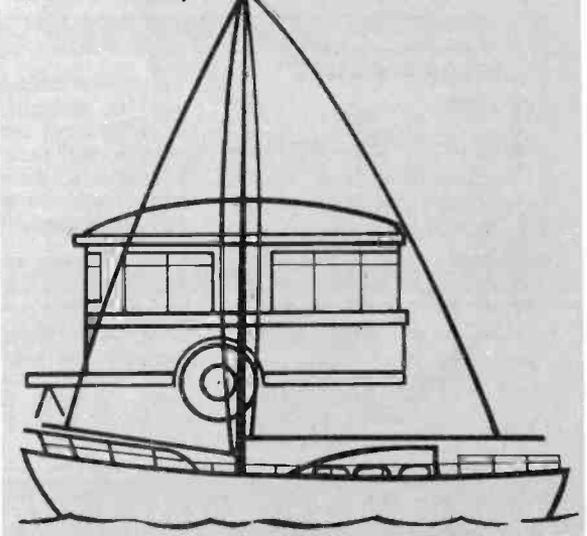


Fig. 6. Waveforms appearing at various points in the circuit of Fig. 4.

Ensure that both the lid and the case are correctly earthed to the earth pin of the mains socket. If required an I.e.d. circuit may be added to the unit, to give warning of inadvertently leaving the device switched on. This will, however, increase battery drain current by approximately 10mA.

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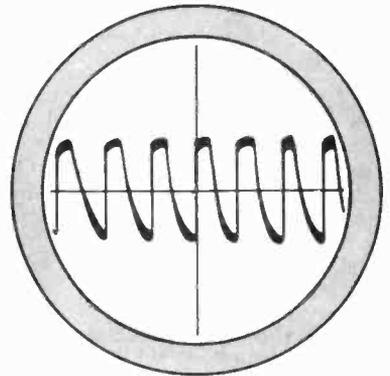


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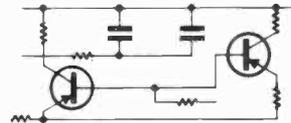
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## MOBILE THOUGHTS

The Chairman of the Mobile Radio Committee of the Electronic Engineering Association, J. R. Brinkley, as well as being Managing Director of Redifon Telecommunications Ltd., is no mean hand at deploying an argument. At the recent Communications 74 Exhibition and Conference at Brighton he gave some startling statistics on what it costs to run Europe's road transport and how much could be saved if the 90 million vehicles all had two-way radio.

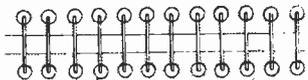
The UK share of this mammoth fleet is 16.5 million vehicles which have an annual running cost, excluding manpower, of £8,000 million. This, says Brinkley, is equal to the total revenue from income tax or twice the national defence budget or three times the cost of the national health service. So even a one per cent saving would yield £80 million and a ten per cent saving £800 million.

He argues that the 200,000 vehicles already fitted with radio-telephones in the UK give them a 20 per cent edge on efficiency compared with unfitted vehicles. In other words four vehicles fitted with radio will do the work of five without. But to date, only one per cent of all vehicles are so fitted and these generally work privately with their own base stations in a small radius of 10-20 miles. What is really needed is a sort of national grid with all vehicles being tied in by radio to the public telephone network.

Such schemes are already being planned in the USA with adequate frequency allocation in the 900MHz region. We use this band partly for TV in Europe but Brinkley sees the present Band III 405-line TV allocation, due to close down in the UK in five years' time, as a promising alternative.

Of course, we already have a public system but costs are relatively high. A mammoth increase in utilisation would bring prices tumbling down. To equip, say, ten per cent of all cars would mean big production lines with consequent economy of scale which would be expected to result in a rental charge per vehicle of £2 a week, plus calls charged on a time basis. With petrol at over 50p a gallon and time in excess of £1 per hour the system could be a bargain for the user.

Meantime, the mobile radio market is still running at 15 per cent growth rate. Pye, the brand leader in the UK, has been pushing exports with a floating exhibition and seminar on the River Rhine taking in France, Switzerland, Germany and the Netherlands. There is no nicer way of doing business and the trip netted over £500,000 of orders confirmed with the prospect of more to come.



# INDUSTRY NOTEBOOK

*By Nexus*



## CONSUMER ICs . . .

The Philips Group is determined to consolidate its leading position in consumer i.c.s. No less than 26 new devices, most of them of considerable complexity and all real state-of-the-art are due for production next year and will be in TV, radio, hi-fi and tape equipment from then on.

To get set manufacturers acquainted with the new circuits Philips invited 300 engineers from 13 countries for a full-scale seminar in Eindhoven. Sixteen of the new circuits are for TV and ten for radio/audio equipment.

The designs are truly international and originate from Mullard experts in the UK and from Philips' men in Holland and Germany. Production technology is to be that already proven on the existing range so there should be big yields (therefore, low prices) from the start, but the chips are larger to accommodate many more functions.

The philosophy behind the new circuits is mainly to reduce the number of external peripheral components and the number of factory adjustments. For example, on a typical colour TV, Philips say the number of peripheral components can now be halved from 320 to 160 and the adjustments reduced from 20 to 10.

It's hard to pick out specific examples but typical of the new thinking is a complete recorder using only three i.c.s. One has the pre-amplifier, level control and recording and playback amplifier, another incorporates motor speed control, automatic stop, and erase oscillator, and the third the complete power amplifier.

More circuits are in development including one for search tuning in which a band of frequencies is electronically scanned and each receivable station is given 1.5 seconds playing time so that the listener can have a quick listen to see what programmes are on offer.

## . . . AND AVIONICS

With Philips so strong in consumer electronics it is only too easy to forget the Group's potency in professional equipment and not least in avionics. The Group is planning a major sales drive at the Farnborough Air Show next September with no less than seven companies based in the UK, Holland, France, Sweden and Canada taking part.

The British effort from MEL at Crawley includes airborne weather and ground-mapping radars for civil use and the very advanced tactical radar fitted in Sea King helicopters of the Royal Navy and a number of other navies. On the ground MEL scored a big hit with MADGE, a NATO award-winning portable microwave tactical approach aid and then, of course, there is direct involvement with the Clansman project where MEL is responsible for transmitter/receivers in the range 1.5-30MHz with powers up to 400 Watts.

Quite apart from selling individual pieces of equipment Philips has both the economic and technical strength to undertake large turnkey projects. One of these is for Zaire where 40 airfields are involved for a contract price of £35 million.

## ENERGY

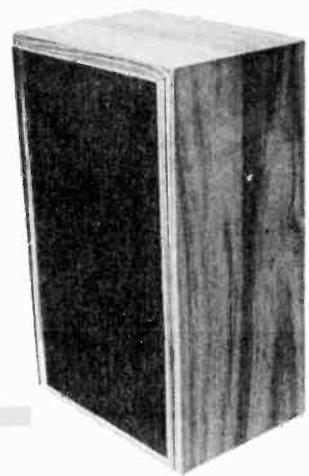
At the turn of the year we were all sick with fear over the energy crisis. Now it seems we have slipped back into easy acceptance that provided we pay over 50p a gallon for petrol and, perhaps, £40 a ton for coal we shall remain mobile and warm and in business. I think this is a poor attitude, probably encouraged by the prospect of North Sea Oil. We should still be looking for economies.

An exciting development is the electric bicycle for which Cambridge Consultants contributed the idea of an electronic throttle working on pulse width modulation to give smooth speed control without recourse to gear changing.

Radius of action is 20 miles (i.e. a 40 mile round trip) before recharging which costs about 2p. With pump petrol selling at 50p this gives personal mobility at an equivalent of 1,000 m.p.g. with the added bonus that there is no exhaust fume pollution of the atmosphere.



# REMOTE VOLUME CONTROL



BY R. WHITAKER

## A WIRED-IN SYSTEM WITH MANY APPLICATIONS

**T**HIS design was developed to give a method of balancing a stereo amplifier from a distance but in fact it has many other uses. In particular it can be used when testing other circuits with a general purpose amplifier as the amplifier volume control may be placed close to hand. The circuit is remarkably simple and is fairly cheap to construct.

### DESIGN CONSIDERATIONS

The circuit uses a field effect transistor (f.e.t.) in a conventional amplifier stage. The characteristics of an f.e.t. are shown in Fig. 1 and it can be seen that the slope or gradient of the graph of  $I_d$  or drain current against  $V_{gs}$  or gate voltage varies according to the value of the gate-source voltage  $V_{gs}$ . This is the basis of the remote operated volume control.

In fact the slope of the graph is called the  $g_m$  or the mutual conductance of the f.e.t., a term borrowed from valve technology.

If we look at the basic f.e.t. amplifier circuit shown in Fig. 2 then the voltage gain can be shown to be  $g_m \times RL$ . Thus by varying  $V_{gs}$ ,  $g_m$  is changed and so the gain can be varied.

One way of varying  $V_{gs}$  is to make R2 variable since the voltage drop across R2 is in fact the way in which  $V_{gs}$  is produced. The current through R2 depends on  $V_{gs}$  and this means that  $V_{gs}$  can never be made to be  $V_p$  the pinch-off voltage of Fig. 1. This means that the volume cannot be faded to zero but only to a very low level. To overcome this, a potential divider is used for R2 and in this way  $V_{gs}$  can be varied from 0V to  $V_p$  or even higher to ensure cutoff.

### THE CIRCUIT

The circuit has only two main design criteria. The first is to decide the working point A of Fig. 1.

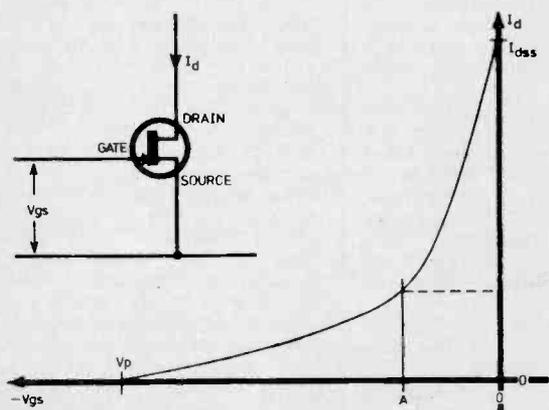


Fig. 1. The characteristics of an f.e.t. and the circuit symbol of the device

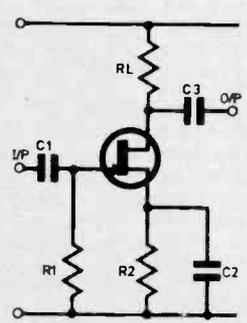


Fig. 2. A basic f.e.t. amplifier

# COMPONENTS

## Resistors

R1 2.2M $\Omega$ Metal Oxide	R3 2.2k $\Omega$ (5-6k $\Omega$ for 2N3819)
R2 100k $\Omega$ Metal Oxide	R4 270 $\Omega$
All $\frac{1}{4}$ or $\frac{1}{2}$ W, 5% carbon	R5 56k $\Omega$ (6.8k $\Omega$ for 2N3819)

## Capacitors

C1 0.01 $\mu$ F	C3 100 $\mu$ F
C2 0.01 $\mu$ F	C4 0.01 $\mu$ F

## Transistors

TR1 BW42 or 2N3819 (Most n-channel f.e.t.s suit on selection)

## Potentiometer

VR1 10k $\Omega$  linear carbon

## Miscellaneous

Veroboard, wire, screened cable for feed, cable to VR1, suitable mono or stereo jack plug and socket

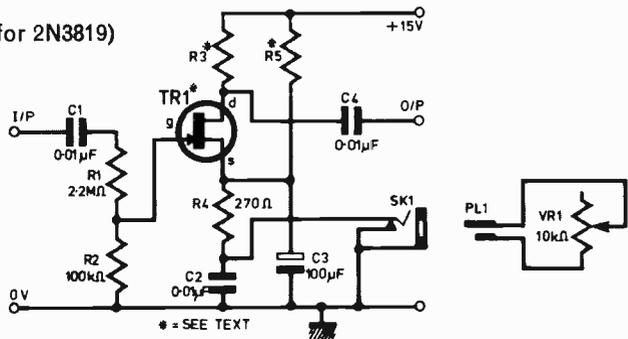


Fig. 3. Practical circuit of a remote volume control

The second is to make sure that the potential divider can produce a high enough voltage to turn the f.e.t. off.

Looking at Fig. 3, a practical version of the control circuit, the resistors R1 and R2 form the input impedance of the amplifier and also reduce the amplitude of the input so that there is slow distortion in the circuit. R3 is chosen so that the gain of TR1 makes up for the loss due to R1 and R2 giving a circuit with a voltage gain of one when it is not acting as an attenuator.

Thus the circuit can be inserted directly into a reproduction chain without any loss.

R4 is used to set the maximum drain current (i.e. point A on Fig. 1) and VR1 is used to alter the gain. At VR1 = 0 $\Omega$  the gain is maximum and at VR1 = 10k $\Omega$  the f.e.t. is cut off. C2 is used to short circuit high frequencies which may be picked up on the leads to VR1. C3 is a bypass capacitor and its value determines the low frequency gain of the amplifier. R5 together with VR1 and R4 set the maximum voltage at the source of the f.e.t. to ensure it is cut off.

This circuit, using a BW42 n-channel f.e.t., has a flat frequency response from below 20Hz to about 10kHz and is 3dB down at 20kHz. It has a high input impedance and a relatively low output impedance. Indeed the author's prototype used two such circuits as a remote stereo volume control. The resistor VR1 was chosen at 10k $\Omega$  to give a voltage swing at the source of the f.e.t. of 0.6V to 1.6V since the devices selected had a pinch-off voltage  $V_p$  of 1.6V.

In fact f.e.t.s do have a rather large spread of  $V_p$  from one device to the next, even of the same type number. 2N3819s could be used, but the ideal thing would be to plot the  $V_{gs}$ ,  $I_d$  characteristic for a device which you have and then alter the circuit to suit.

## DESIGN PROCEDURE

The design procedure is simple. First of all the characteristic of the devices to be used is plotted using the circuit shown in Fig. 4. Only one meter is needed really although two are shown.

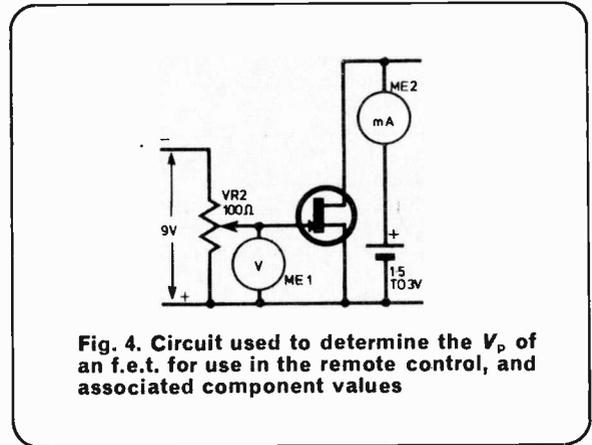
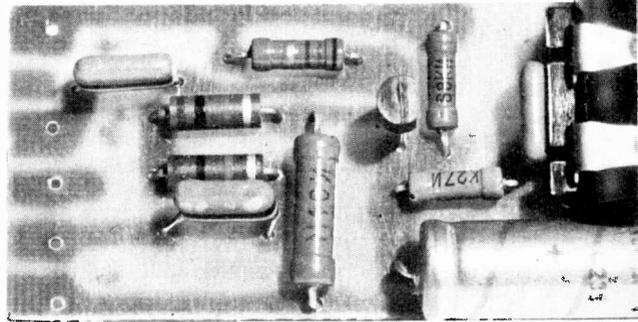


Fig. 4. Circuit used to determine the  $V_p$  of an f.e.t. for use in the remote control, and associated component values

First set the voltage, then measure the current for several values of voltage. It might be as well to first vary VR2 until no current is read on the meter ME2 then bring VR2 back to just where the current begins to flow. Measure this voltage, it is  $V_p$ .

Choose a suitable working point A considering that the gain does not vary over straight parts of the graph. Calculate R4 to drop the value of  $V_{gs}$  chosen. Select R3 to give the required gain, bearing

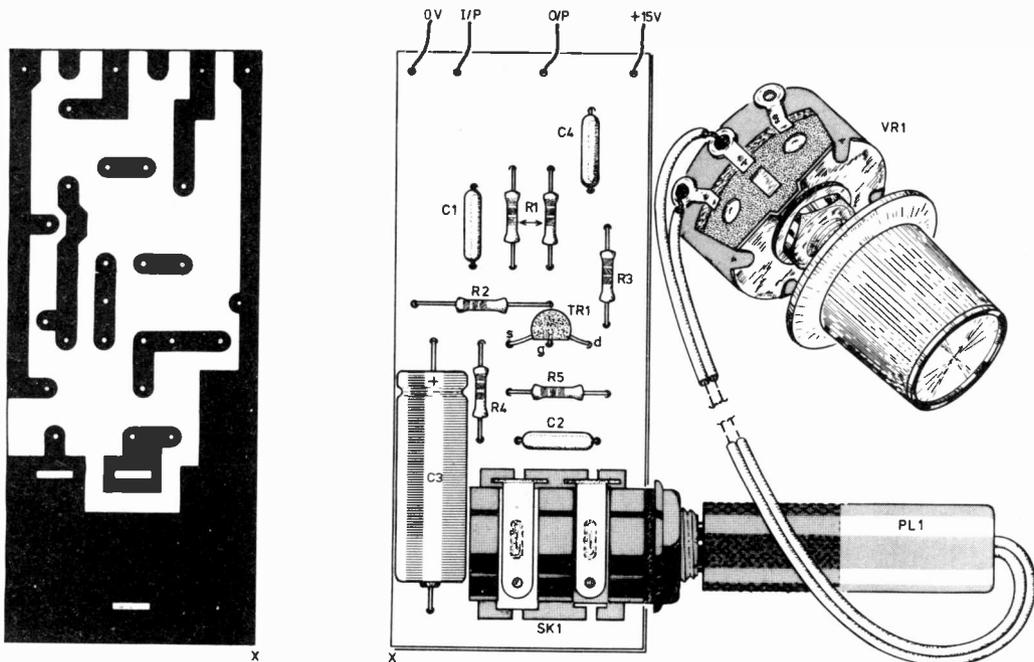


Fig. 5. Printed circuit pattern (full size) and component layout for the remote volume control

in mind the earlier comments on unity gain.  $g_m$  can be found from the tangent to the graph at the working point, then gain =  $g_m \times R_L$ .

Make certain that  $R_L$  does not drop so much voltage that there is less than 3V across the drain and source of the f.e.t., remembering that  $R_4$  will be dropping some voltage (i.e.  $V_{gs}$  chosen).

Since at cut-off the drain current  $I_d$  is zero, choose the value of  $VR_1$  and  $R_5$  to give a voltage greater than  $V_p$  at their junction. The only current flowing in them at this time will be that through them. None flows through the f.e.t.

It is suggested that the same values of  $R_1$  and  $R_2$  as in Fig. 3 be used as they are suitable for inputs of up to 1V r.m.s. Also, use the same capacitor values.

### VOLTAGE CONTROL

The circuit can in fact be voltage controlled by applying a variable voltage from 0.6V to 1.6V in place of  $VR_1$ . This could form the basis of a talk-over circuit for a discotheque or an automatic fader.

The leads to  $VR_1$  can be as long as required and do not have to be screened.

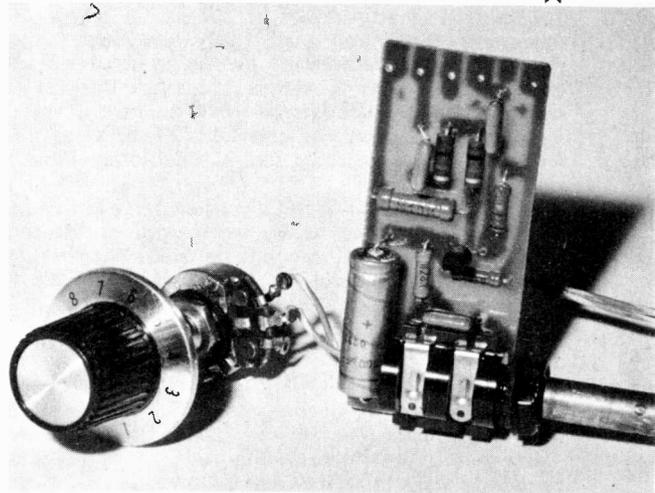
The prototype used a stereo switching jack to connect the control into the amplifier with the two control circuits mounted in the amplifier and powered from its supply. The amplifier controls can be used to preset maximum volume. The jack contacts were arranged so that the gain was 1 when the jack was unplugged.

The circuit works well, but if two are to be used for stereo then it is best to get two matched f.e.t.s.

### CONSTRUCTION

Each circuit was constructed on a printed circuit board, see Fig. 5. Layout is not critical, but the leads to  $R_1$  should be screened since the input impedance is high. The f.e.t. should be soldered in last so that it has least chance of being affected by the heat of soldering.

Two values of some components are given in the components list. The first is for use with a BW42 device and the second for a 2N3819. The single values are common to both circuits. The 2N3819 version exhibits a slightly lowered performance, being 3dB down at 25Hz. ★



# PATENTS REVIEW

## IMPROVING TREBLE CONTROL

In BP 1 337 284 from General Electric Co of New York is a typical British patent specification of USA origin. For legal reasons in the States it is essential for every last nut, bolt and blob of solder to be described in minute detail and for convenience the same text is often used for both countries. This makes for tedious reading and difficulty in sorting out where the novelty of the real invention lies, but it also provides masses of detailed background information.

The GEC patent concerns modifications in treble tone control circuits for audio amplifiers and to highlight the modifications, the inventors first of all describe and draw a conventional audio amplifier (complete with component values) for which no patent protection is claimed.

Although bass tone control, contour or loudness circuit, bass boost circuit and a volume control all operate exactly as in conventional amplifiers, the main difference and invention lies in the treble tone control circuit, see Fig. 1.

The mid-band attenuation has been reduced and the emitter bypass circuit, shown dotted in Fig. 1, is removed. The modified treble control circuit includes capacitors C1, C2 and C3.

When the wiper of the treble control potentiometer is at minimum, capacitor C1 effectively shunts to provide treble cut. When the wiper is at maximum, the shunting effect of C1 is minimised

and treble frequencies are boosted. Also, when the wiper is at maximum, C2 passes h.f. audio signals and an additional path for these components is provided, via C3, to boost treble when the volume control is below maximum.

When the treble tone control is turned towards its minimum position, not only is the shunting effect of C1 increased to provide high frequency roll-off but also the treble boosting effect of the capacitors C2 and C3 is reduced.

Graphs are given to show how control of this type can have considerable effect on the upper frequencies, including a 4dB increase between the maximum and minimum treble settings over conventional circuits at 10kHz and a 5dB increase at 20kHz.

## TEMPERATURE SENSITIVE OSCILLATOR

A clever use for a threshold glass switch is described by Standard Telephones and Cables in BP 1 341 172. The switch is constructed by embedding a pair of conductive wires in a bead of vitreous material, the device switching to conduction when a critical voltage is exceeded and returning to a high resistance state when the current is reduced below a critical holding current.

In the simple circuit of Fig. 1 C1 is charged from a constant voltage supply via VR1. When the voltage across the capacitor reaches the switching voltage of

BP 1 341 172

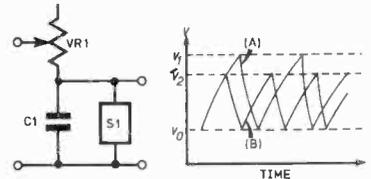


Fig. 1.

Fig. 2.

the glass switch S1, the capacitor discharges through it. The discharge continues until the current through the switch falls below the critical holding current. The switch then returns to its high resistance state and the next charge/discharge cycle commences.

In the graph of Fig. 2 the voltage waveform across the switch at a given temperature is represented by (A), the switching voltage being  $V_1$ . The voltage at which the current through the switch falls below the critical holding current varies only slightly with temperature, but the critical voltage varies significantly. Thus if the temperature of the switch is raised the critical voltage falls to  $V_2$  (Fig. 2) and the voltage across the switch produces the higher frequency waveform (B).

In practice the error due to changes in value of the R/C components with temperature are small compared to the significant change per degree centigrade.

The circuit may be arranged so that at 37 degrees centigrade (body temperature) the frequency of the waveform is 10kHz. If the output of the circuit is compared with a 10kHz locked frequency signal (e.g. from an oscillator) then an audio frequency signal can be generated as a beat frequency as the temperature of the switch is varied up or down from 37 degrees centigrade. In this and other ways the circuitry may be used to signal changes of temperature around a notional norm, such as the 37 degree centigrade level. The adjustment necessary at resistor VR1 to zero the beat can be used to indicate the temperature change that has occurred.

BP 1 337 284

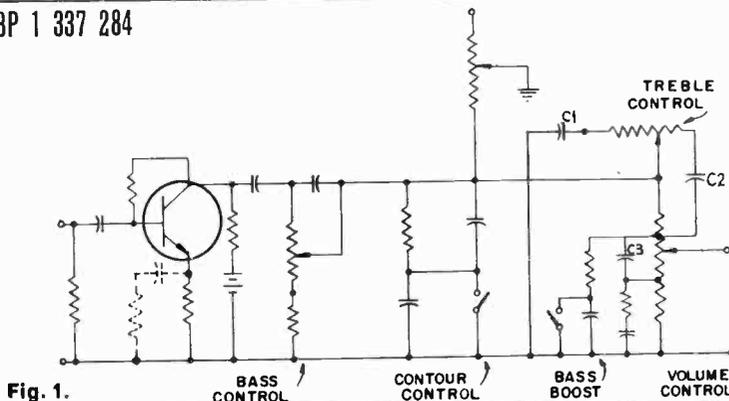


Fig. 1.

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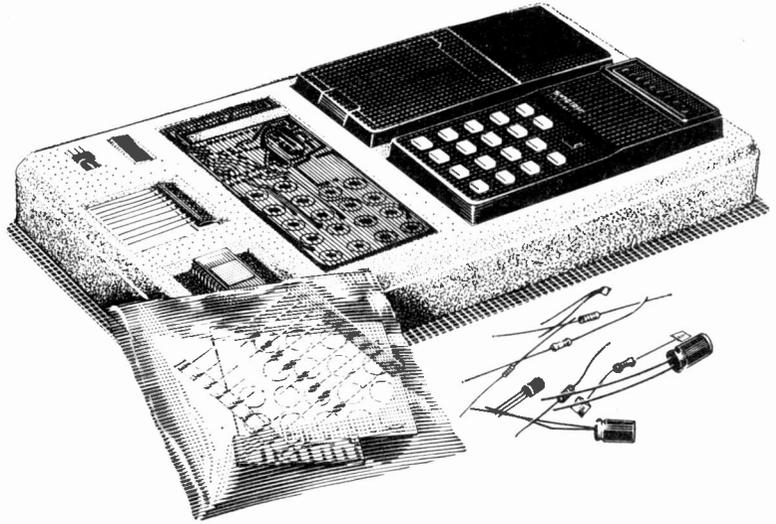


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PE/9/74

PLEASE PRINT

# MARKET PLACE

Items mentioned in this feature are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned. All quoted prices are those at the time of going to press.



**Tourist II  
Car Radio from R&TV  
Components**

## CAR RADIO KIT

It is unfortunate that this magazine cannot make awards to manufacturers for designs and service to readers' interests. If we did then **Radio & TV Components Ltd.** would certainly be top of our list for service to readers and probably very close to Sinclair's for top honours for design.

Although R&TV have had tremendous success with their unit audio systems and car radio kits, they have decided that because some of their clients are not too hot on soldering a new range of "solderless" units is required.

The first of these items is the Tourist Two car radio which dispenses entirely with soldering in its construction. Instead, all electrical connections are made through press-on tags and it is claimed that the kit can be assembled in less than two hours by any "do-it-yourselfer".

By utilising an integrated circuit and a printed circuit board allied to tested sub-assemblies, construction is simply a matter of fixing the various component assemblies to the chassis using the screws provided, and completing the electrical circuit by means of colour coded press-on tags.

The Tourist Two radio has five pushbuttons which can be tuned to any preselected station. Four of the buttons operate on the medium band and the other on the longwave band. The finished radio will slot into the standard car radio aperture.

The technical features of the kit include permeability tuning and longwave coils to ensure good sensitivity and selectivity on both wave bands. The r.f. sensitivity at 1MHz is claimed to be better than 15µV and the power output into 30 ohms is claimed to be 4W. The output stage is short circuit proof for added safety.

Both the i.f. module and tuner are pre-aligned and the kit is suitable for 12V positive or negative earth operation.

Complete with step by step instructions, including details for installing in the car, the Tourist car radio is available by post or direct from **Radio & TV Components Ltd.**, 21 High Street, Acton, London, W.3, price £7 plus VAT. Postage and packing is 55p.

Additional extras include a speaker with baffle and fitting strips, £1.65 plus 23p postage and packing, and a matched fully retractable locking aerial, £1.37 plus 20p postage and packing.

## DIGITAL ALARM CLOCK CHIP

Readers who like to experiment with clock circuits may find a new integrated circuit chip available from **Sintel** of particular interest.

Known as the Mostek MK50250N, the 28-pin device may be used to construct a 24-hour digital alarm clock, with the addition of only a single power supply, display and standard interfacing components.

Special features of the device are that when the "snooze" button is operated it will temporarily turn off the alarm signal to allow an additional 10 minutes' sleep. The "bleep" alarm is generated within the chip and there is no need for an external oscillator circuit.

## CHANGE IN VAT

Owing to the change from 10 per cent to 8 per cent in the rate of VAT, occurring as this issue closed for press, it has not been possible to alter all prices shown in advertisements.

If a low house voltage condition occurs, the a.m./p.m. indicator will flash at a 1Hz rate to signify an incorrect time display.

The 6-digit multiplexed outputs make the chip compatible with gas discharge or l.e.d. displays. An additional facility allows the use of an economical 4-digit display, hours and minutes, to be used if required.

The cost of the MK50250N is £8.36 including VAT and full technical details can be obtained from **Sintel**, 53 Aston Street, Oxford, OX4 1EW.

## DISCO CONSOLES

It is well known that noise is debilitating. With many discotheques distortion components generated through poor equipment can contribute to this unmusical sound providing cumulative discomfort.

With this in mind it is nice to record a new range of disco consoles from **Citronic Ltd.**, with a hi fi specification. The Stateline range includes one mono and three stereo units covering a basic range of 75 to 150W r.m.s.

A feature of the consoles is the modular assembly typified in the

four and six channel mixer/pre-amplifiers which can, in fact, be purchased as separates.

The power amplifier module provides a basic 75W r.m.s. which is compounded to provide the high outputs.

Top of the Stateline range is the Texas console which, in its quadruple amplifier configuration, is believed to be the most powerful self-contained disco unit on the U.K. market, giving 300W r.m.s. or approximately 500W music power. The Texas is equipped with two standard or transcription quality record decks and a cassette tape unit. If required an eight-track cartridge player may be incorporated as well. The Iowa, five inches shorter and without the option of quadruple amplifiers, may also include a cartridge unit.

At the lower cost end of the range the Delaware and Kansas units, mono and stereo respectively, have two record decks and give 75W mono or 150W as the stereo equivalent. The Delaware also has a dual-amplifier option.

Other optional extras include the stand, transcription quality record decks and electronic lighting effect control units.

Information and price list of the complete range of Stateline consoles may be obtained from **Citronic Ltd.**, Melksham, Wilts.

## PRINTED CIRCUIT KIT

A new professional printed circuit kit, providing all the necessary tools and equipment for producing good prototype printed circuits quickly, efficiently and at an economic price, has been introduced by **GSPK (Electronics) Ltd.**

Ideal not only for the electronics enthusiast but for engineers and students, it is claimed that a complex circuit board layout can be produced in a few minutes.

The Professional Kit contains six pieces of single sided laminate, a box of etchant, measuring scoop, steel rule, cutting knife, hand drill, etchant dish and printed circuit board marking pen.

Available from **GSPK (Electronics) Ltd.**, Hookstone Park, Harrogate, Yorks, each kit contains full instructions and the recommended retail price is £8.40 including VAT, postage and packing being extra.



**Stateline Iowa  
Disco Console  
from Citronic**

# Readout —

## A SELECTION FROM OUR POSTBAG

Readers requiring a reply to any letter must include a stamped addressed envelope. We regret that we cannot answer any technical queries on the telephone.

### Professional manner

Sir,—Mr. Kitchen's recent letter under the heading "Good Olde Days" (*Readout*, July), expresses sentiments which have been expressed by every generation on all matters.

Mr. Kitchen obviously enjoyed messing around with, and being bitten by those frightful, hot, glass bottles which imposed appalling restrictions on any constructor, but he must be very naive to think that all the fun has gone. The proof that there are a very large number of constructors, who I assume enjoy their hobby, is the very existence of *Practical Electronics* and many other magazines.

The advantages that transistors and integrated circuits have brought us are numerous: ease of handling, lower dissipation, smaller size, improved performance, etc. These advantages have opened up new areas of design, which were not possible with valves, and present designs cover all facets of everyday life. I would agree that 10 or 20 years ago chassis had to be "bashed out", but I can assure Mr. Kitchen that there are many who still "bash their own chassis".

Construction has been simplified, in some respects, by printed wiring and other methods, and basic circuit design is probably dying, although i.c. manufacturers haven't got all the answers. In its place we build our own "tag-boards" using copper clad insulating board and ferric chloride (far more skilful than buying tag-boards and insulating pillars); and we have application design which requires as much skill as circuit design, as we firstly have to interpret the design data sheets, which use terms like "on-chip address decoding, tri-state outputs, slew rate, propagation delay", and secondly wonder why the 40 legged monster does its nut when we can see nothing in its input (35 nano-second nasties can be a bit trying!)

I suggest Mr. Kitchen tries constructing a digital clock similar to the one described recently in P.E., but using techniques and components of 20 years ago. If he can get no enjoyment from constructing such a device using i.c.'s and on switch-on finding a mass of numbers rolling round then I pity him.

I think we should be thankful for present day technology in taking the shackles off us and allowing us to construct items which are not only rewarding to design and construct, but which can be useful and built in a professional manner.

Peter Seddon,  
Rugby.

### Psycho . . .

Sir,—Regarding Mr. Watson's letter on "Psycho-sensitive semiconductors" and their possible existence (*Readout*, July) I would like to say how interested I was to read these comments, particularly as it takes us out of the superstition that P.K. (psycho kinetics) can only be effected from living being to living being. Though the latter is considered the most common, I am sure it is not the only method of proving the power of P.K., and I add to this the results obtained by Uri Geller, who is able to bend objects without even touching them! O.K., I know this is a matter of controversy among (so-called) scientists at present, but I venture to add that I am willing to accept the evidence.

I would venture to state that mind over matter is a fact, and that it operates at a sub-microscopic level, possibly at atomic level, which results in a cumulative effect to create perceptible consequences. At this time I have certain facts at my disposal which suggest that non-biological material is affected equally well as plant or animal cells, but I have to await certain results for my own satisfaction.

The point Mr. Watson mentions about molecules of magnetic material being affected by mind power may well be true, but I would prefer not to be as specific on this point for one good reason at least. Experimenters in the field of P.K. have so far indicated that they find the effect is not diminished by distance between "transmitter" and "receiver".

As we know from basics, magnetic effects, light and radio waves included, are subject to attenuation on an inverse square law with distance. Hence, one would expect one of two things to happen with distance. Firstly, as in the case of

amplitude modulation, definition would be lost with increasing distance, or in the case of f.m. the effect may be sudden loss at a specific distance when carrier was lost into background noise. Secondly, if pulse-width modulation, or mark/space ratio modulation of some kind were used, the effect of distance would be greatly reduced, but again, a point should be reached where intelligibility would cease.

Nature uses a system similar to the latter in conveying information of an analogue type to muscles in the body, and it may be fair to assume a similar principle is involved in P.K. If so, it seems that distance has not defeated any known experiment as yet, unless the results of the Americans' space experiments in P.K. found that there was an attenuation. And it is unlikely that we shall hear much of those experiments . . . particularly if successful!

Meanwhile, it is surely up to all of us keen experimenters to delve deeper into the subject.

Brian H. Baily,  
Dorset.

### . . . theory

Sir,—I have just read the letter by Mr. P. Watson in the July issue of P.E. I should like to point out to Mr. Watson that the head of the chlorophyll molecule will probably not be magnetic as it contains an atom of magnesium (Mg) not iron (Fe).

However, there are compounds present in the plant cell which contain an atom of iron, e.g. cytochromes. I do not, however, see the advantage the plant would gain in aligning itself up with the lines of force of the magnetic field. This does not disprove Mr. Watson's theory of a magnetic field interacting with iron containing molecules.

I would now like to put forward my own theory. There is a class of compounds present in plant cells which initiate movements in plants when they are acted on by certain external stimuli, e.g. light and water. These compounds are called auxins and the movements they produce are called tropisms. The plant has no control over these movements, once the auxins have been produced they begin to act. One such tropism known as geotropism occurs in plant roots, in this an auxin is produced in one side of the roots causing them to bend downwards towards the centre of the earth.

It is known that strong magnetic forces radiate from the centre of the earth, could not these magnetic forces cause a concentration in the lower side of plant roots causing them to bend downwards?

P. Crilly,  
Reid Kerr College,  
Paisley, Scotland

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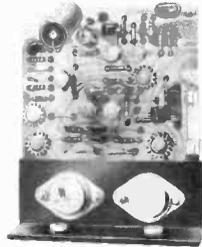
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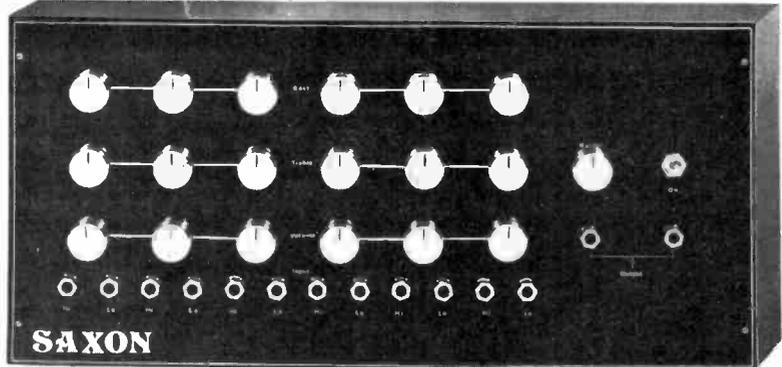
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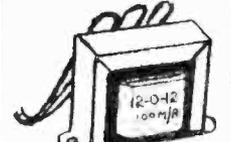
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This fantastic little box approx. 4" x 3" x 2 1/2" when connected to the output of a sound source from 1 to 100 watts produces a psychedelic light display of up to 1000 watts. Complete with a sensitive level control the unit is fused and cannot harm your amplifier. A Bargain at £7.50 plus 10p.

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Varnish Impregnated  
Size 46mm x 36mm x 31mm



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Sec	3.0-3	100mA
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Enables you to work your Transistor Radio, Amplifier or Cassette, etc. from the a.c. mains through this compact Eliminator. Just by moving a plug you can select the voltage you require, 6, 7 1/2 or 9 volt. This means all your transistor power pack applications can be handled by this one unit. Approx. size 2 1/2" x 2 1/2" x 3 1/2". Our Price £2.75 plus 10p P. & P. Same model suitably wired for the Philips Cassette £3 plus 10p P. & P.

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0.5mA—ME10	0.300V a.c.—ME17
0.10mA—ME11	8 meter—ME18
0.50mA—ME12	V.U. meter—ME19

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5 transistor amplifier complete with volume control, is suitable for 9V d.c. and a.c. supplies. Will give about 1W at 8 ohm output. With high IMP input this amplifier will work as a record player, baby alarm, etc., amplifier.  
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BC167 15p; BC168 14p; BC169 13p each } npn  
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AC128 17p; AF117 37p

BFY51 23p

Full lists and technical data will be found in Catalogue No. 7.

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Code	Watts	Ohms	1 to 9	10 to 99	100 up
(see note below)					
C	1/3	4.7-470K	1-3	1-1	0.9 nett
C	1/2	4.7-10M	1-3	1-1	0.9 nett
C	3/4	4.7-10M	1-5	1-2	0.97 nett
C	1	4.7-10M	3-2	2-5	1.92 nett
MO	1/2	10-1M	4	3-3	2.3 nett
WW	1	0.22-3.9	11	10	8 nett
WW	3	1-10K	9	8	6 nett
WW	7	1-10K	11	10	8 nett

## Codes:

C = carbon film, high stability, low noise.  
MO = metal oxide, ElectroSil TR5, ultra low noise.  
WW = wire wound, Pleesley.

Values: All E12 except C  $\frac{1}{2}$ W, C  $\frac{3}{4}$ W, and MO  $\frac{1}{2}$ W.  
E12: 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82  
and their decades.

E24: as E12 plus 11, 13, 16, 20, 24, 30, 36, 43, 51,  
62, 75, 91 and their decades.

## Tolerances:

5% except WW1 10%  
±0.05Ω below 10Ω and MO  $\frac{1}{2}$ W 2%  
Prices are in pence each for quantities of the same ohmic value and power rating. NOT mixed values. (Ignore fractions of one penny on total value of resistor order.) Prices for 300 up in units of 100 only.

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GIRO ACCOUNT No. 38/671/4002

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### DALY ELECTROLYTIC

in cons. plastic sleeved  
1,000mF/25V, 28p; 5,000mF/25V, 62p; 1,000mF/50V, 41p; 2,000mF/50V, 57p; 5,000mF/50V, £1-18;  
50,000mF/100V, £2-91; 2,200mF/100V, £1-56.

### POLYESTER TYPE C280

Radial leads for P.C.B. mounting. Working voltage 240V d.c.  
0.01 0.015, 0.022, 0.033, 0.047, 3p each; 0.068, 0.1, 0.15, 4p each; 0.22, 5p; 0.33, 7p; 0.47, 8p; 0.68, 11p; 1.0, 14p; 1.5, 21p; 2.2, 24p.

### SILVERED MICA

Working voltage 500V d.c.  
Values in pF—2.2 to 820 in 32 stages, 6p each; 1,000, 1,500, 7p each; 1,800, 8p; 2,200, 10p; 2,700, 3,600, 12p each; 4,700, 5,000, 15p each; 6,800, 20p; 8,200, 10,000, 25p each.

### TANTALUM BEAD

0.1, 0.22, 0.47, 1.0mF/35V, 14p each. 2.2/16V, 2.2/35V, 4.7/16V, 10/6-3V, 14p each. 4.7/35V, 10/16V, 22/6-3V, 18p each. 10/25V, 22/16V, 47/6-3V, 100/3V, 6.8/25V, 15/25V, 20p each.

### POLYCARBONATE TYPE B32540

Working Voltage 250V.  
Values in mF: 0.0047, 0.0068, 0.0082, 0.01, 0.012, 0.015, 3p each. 0.018, 0.022, 0.027, 0.033, 0.039, 0.047, 0.056, 0.068, 0.082, 0.1, 4p each.

### CERAMIC PLATE

Working voltage 50V d.c.  
In 26 values from 22pF to 6,800pF, 2p each.

## ELECTROLYTIC Axial Leads

uF	3V	6.3V	10V	16V	25V	40V	63V	100V
0.47	—	—	—	—	—	—	—	—
1.0	—	—	—	—	—	11p	—	—
2.2	—	—	—	—	—	—	8p	9p
4.7	—	—	—	11p	—	—	8p	9p
10	—	—	—	—	8p	9p	8p	8p
22	—	—	8p	—	9p	8p	8p	10p
47	8p	—	9p	8p	8p	8p	10p	13p
100	9p	8p	8p	8p	9p	10p	12p	19p
220	8p	8p	9p	10p	10p	11p	17p	28p
470	9p	10p	10p	11p	13p	17p	24p	45p
1,000	11p	13p	13p	17p	20p	25p	41p	—
2,200	15p	18p	23p	26p	37p	41p	—	—
4,700	26p	30p	39p	44p	58p	—	—	—
10,000	42p	46p	—	—	—	—	—	—

## POTENTIOMETERS

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Double wipers for good contact and long working life.  
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3-circuit with 3 break contacts, S3/BBB 20p  
2 circuit with chrome nut and black/white/red/green or grey unswitched, S5/SS 14p  
2 circuit with chrome nut and black/white/red/green with 2 break contacts, S5/BB 17p  
Miniature, 3.5mm, 2-circuit (black), 2 br. cont., S6/BB 8p

### Plugs

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2 circ. screened, side entry, SEPI 36p  
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3-circuit, unswitched, bl/grey/wh, P.4 48p  
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3-circuit, screened, top entry, P.3 53p  
3-circuit, screened, side entry, SEP3 55p  
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C9	3	Micro Switches	0-55
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PS 6 D.I.N. 6 Pin 0-17  
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PS 9 Jack 3.5mm Plastic 0-12  
PS 10 Jack 3.5mm Screened 0-18  
PS 11 Jack 1" Plastic 0-15  
PS 12 Jack 1" Screened 0-22  
PS 13 Jack Stereo Screened 0-36  
PS 14 Phono 0-10  
PS 15 Car Aerial 0-22  
PS 16 Co-Axial 0-15

## INLINE SOCKETS

PS 21 D.I.N. 2 Pin (Speaker) 0-14  
PS 22 D.I.N. 3 Pin 0-20  
PS 23 D.I.N. 5 Pin 180° 0-20  
PS 24 D.I.N. 5 Pin 240° 0-20  
PS 25 Jack 2.5mm Plastic 0-16  
PS 26 Jack 3.5mm Plastic 0-16  
PS 27 Jack 1" Plastic 0-30  
PS 28 Jack 1" Screened 0-35  
PS 29 Jack Stereo Plastic 0-30  
PS 30 Jack Stereo Screened 0-38  
PS 31 Phono Screened 0-18  
PS 32 Car Aerial 0-22  
PS 33 Co-Axial 0-22

## SOCKETS

PS 35 D.I.N. 2 Pin (Speaker) 0-08  
PS 36 D.I.N. 3 Pin 0-11  
PS 37 D.I.N. 5 Pin 180° 0-11  
PS 38 D.I.N. 5 Pin 240° 0-11  
PS 39 Jack 2.5mm Switched 0-12  
PS 40 Jack 3.5mm Switched 0-12  
PS 41 Jack 1" Switched 0-20  
PS 42 Jack Stereo Switched 0-38  
PS 43 Phono Single 0-08  
PS 44 Phono Double 0-10  
PS 46 Co-Axial Surface 0-10  
PS 47 Co-Axial Flush 0-20

## LEADS

L8 1 Speaker Lead 2 pin D.I.N. plug to open ends approx 3 metres long (codel) 0-20

## CABLES

CP 1	Single Lapped Screen	0-07
CP 2	Twin Common Screen	0-11
CP 3	Stereo Screened	0-12
CP 4	Four Core Common Screen	0-23
CP 5	Four Core Individually Screened	0-30
CP 6	Microphone Fully Braided Cable	0-10
CP 7	Three Core Mains Cable	0-09
CP 8	Twin Oval Mains Cable	0-07
CP 9	Speaker Cable	0-05
CP 10	Low Loss Co-Axial	0-18

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VC 2 Single D.P. Switch 0-28  
VC 3 Tandem Less Switch 0-48  
VC 4 1K Lin Less Switch 0-15  
VC 5 100K anti-Log 0-48

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Type	Amps	Price	P. & P.
MT50/1	1	£1.93	30p
MT50/1	1	£2.42	35p
MT50/2	2	£3.30	40p

## CARTRIDGES

AC08  
GP91-18C 300mV at 1.2cm/sec £1.35  
GP93-1 280mV at 1cm/sec £1.85  
PC5 1100mV at 1cm/sec £2.80  
J-2005 Crystal/Hi Output £1.05  
J-2010C Crystal/Hi Output Compatible £1.20  
J-2006S Stereo/Hi Output £1.75  
J-2105 Ceramic/Med Output £1.95  
J-2203 Magnetic 5mV/5cm/sec, including stylus £4.95  
J-2203S Replacement stylus for above £3.00  
AT-55 Audio-technica magnetic cartridge 4mV/5cm/sec £3.30

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The E12 Range of Carbon Film Resistors, £ watt available in PAKS of 50 pieces, assorted into the following groups:  
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R2 50 Mixed 1kΩ-8.2kΩ 50p  
R3 50 Mixed 10kΩ-82kΩ 50p  
R4 50 Mixed 100kΩ-1MΩ 50p  
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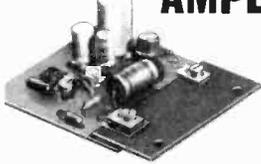
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### AL10/AL20/AL30 AUDIO AMPLIFIER MODULES



The AL10, AL20 and AL30 units are similar in their appearance and in their general specification. However, careful selection of the plastic power devices has resulted in a range of output powers from 3 to 10 watts R.M.S. The versatility of their design makes them ideal for use in record players, tape recorders, stereo amplifiers and cassette and cartridge tape players in the car and at home.

Parameter	Conditions	Performance
HARMONIC DISTORTION	Po = 3 WATTS f = 1KHz	0.25%
LOAD IMPEDANCE	—	8-16 Ω
INPUT IMPEDANCE	f = 1KHz	100 k Ω
FREQUENCY RESPONSE -3dB	Po = 2 WATTS	50 Hz-25KHz
SENSITIVITY for RATED O/P	Vs=25V. R1=8Ω f=1KHz	75mV. RMS
DIMENSIONS	—	3" x 2 1/4" = 1"

The above table relates to the AL10, AL20 and AL30 modules. The following table outlines the differences in their working conditions.

Parameter	AL10	AL20	AL30
Maximum Supply Voltage	25	30	30
Power out for 2% T.H.D. (RL = 8Ω f = 1KHz)	3 watts RMS Min.	5 watts RMS Min.	10 watts RMS Min.

#### AUDIO AMPLIFIER MODULES

AL 10. 3 watts	£2-19
AL 20. 5 watts	£2-59
AL 30. 10 watts	£3-01

#### POWER SUPPLIES

PS 12. (Use with AL10, AL20, AL30) 88p	
PS 30. (Use with AL60)	£3-25
FRONT PANELS PA 12 with Knobs	£1-00

#### PRE-AMPLIFIERS

PA 12. (Use with AL10 & AL20)	£4-35
PA 100. (Use with AL30 & AL60)	£13-15

#### TRANSFORMERS

T461 (Use with AL10)	£1-38 P & P 15p
T538 (Use with AL20, AL30)	£1-93 P & P 15p
BMT80 (Use with AL60)	£2-15 P & P 25p

#### PA12 PRE-AMPLIFIER SPECIFICATION

The PA12 pre-amplifier has been designed to match into most budget stereo systems. It is compatible with the AL 10, AL 20 and AL 30 audio power amplifiers and it can be supplied from their associated power supplies. There are two stereo inputs, one has been designed for use with Ceramic cartridges while the auxiliary input will suit most Magnetic cartridges. Full details are given in the specification table. The four controls are, from left to right: Volume and on/off switch, balance, bass and treble. Size 152mm x 84mm x 35mm.

Frequency response—  
20Hz-50KHz (-3dB)  
Bass control—  
± 12dB at 60Hz  
Treble control—  
± 14dB at 14KHz  
\*Input 1 Impedance  
1 Meg. ohm  
Sensitivity 300mV  
†Input 2 Impedance  
30 K ohms  
Sensitivity 4mV

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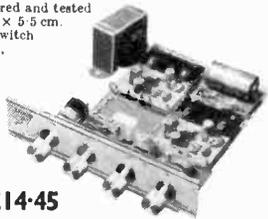
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## The STEREO 20

The "Stereo 20" amplifier is mounted, ready wired and tested in a one-piece chassis measuring 20 cm x 14 cm x 5.5 cm. This compact unit comes complete with on/off switch, volume control, balance, bass and treble controls, transformer, Power supply and Power amps. Attractively printed front panel and matching control knobs. The "Stereo 20" has been designed to fit into most turntable plinths without interfering with the mechanism or, alternatively, into a separate cabinet. Output power 20w peak. Input 1 (Cer.) 0.0mV into 1M. Freq. res. 25Hz-25KHz. Input 2 (Aux.) 4mV into 30K. Harmonic distortion. Bass control ± 12dB at 60Hz typically 0.25% at 1 watt. Treble control ± 14dB at 14KHz.

£14-45



#### FC20 TEAK VENEERED CABINET

For Stereo 20 (front board undrilled) Size 10 1/2" x 8 1/2" x 3", £3-95 plus 30p postage.

#### 3HP80 STEREO HEADPHONES

-16 ohms impedance. Frequency response 20 to 20,000Hz. Stereo/mono switch and volume controls, £4-95

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- Distortion better than 1% at 1KHz
- Supply voltage 10-35 volts

- Thermal Feedback
- Latest Design Improvements
- Load — 3, 4, 8 or 16 ohms
- Signal to noise ratio 80dB
- Overall size 63mm x 105mm x 13mm

Especially designed to a strict specification. Only the finest components have been used and the latest solid state circuitry incorporated in this powerful little amplifier which should satisfy the most critical A.F. enthusiast.

### STABILISED POWER MODULE SPM80



SPM80 is especially designed to power 2 of the AL60 Amplifiers, up to 15 watt (r.m.s.) per channel simultaneously. This module embodies the latest components and circuit techniques incorporating complete short circuit protection. With the addition of the Mains Transformer BMT80, the unit will provide outputs of up to 1.5 amps at 35 volts. Size: 63mm x 105mm x 30mm. These units enable you to build Audio Systems of the highest quality at a hitherto unobtainable price. Also ideal for many other applications including:—Disc Systems, Public Address, Intercom Units, etc. Handbook available 10p

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TRANSFORMER BMT80 £2-15 p. & p. 28p

### STEREO PRE-AMPLIFIER TYPE PA100

Built to a specification and NOT a price, and yet still the greatest value on the market, the PA100 stereo pre-amplifier has been conceived from the latest circuit techniques. Designed for use with the AL60 power amplifier system, this quality made unit incorporates no less than eight silicon planar transistors, two of these are specially selected low noise NPN devices for use in the input stages. Three switched stereo inputs, and rumble and scratch filters are features of the PA100, which also has a STEREO/MONO switch, volume, balance and continuously variable bass and treble controls.



#### SPECIFICATION

Frequency Response 20Hz-20KHz ± 1dB  
Harmonic Distortion better than 0.1%  
Inputs: 1. Tape Head 3-25 mV into 50K Ω  
2. Radio, Tuner 75 mV into 50K Ω  
3. Magnetic P.U. 3 mV into 50K Ω

All input voltages are for an output of 250mV. Tape and P.U. inputs equalised to RIAA curve within ± 1dB. from 20Hz to 20KHz.

Bass Control ± 15dB at 20Hz  
Treble Control ± 15dB at 20KHz  
Filters: Rumble (High Pass) 100Hz  
Scratch (Low Pass) 8KHz  
Signal/Noise Ratio better than -65dB  
Input overload + 26dB  
Supply + 35 volts at 20mA  
Dimensions 292mm x 82mm x 35mm

ONLY £13-15

#### MK 60 AUDIO KIT

Comprising: 2 x AL60, 1 x SPM80, 1 x BTM80, 1 x PA 100, 1 front panel, 1 kit of parts to include on-off switch, neon indicator, stereo headphone sockets plus instruction booklets. Complete Price: £28-75 plus 30p postage.

#### TEAK 60 AUDIO KIT

Comprising: Teak veneered cabinet size 16 1/2" x 11 1/2" x 3 1/2", other parts include aluminium chassis, heat sink and front panel bracket, plus back panel and appropriate sockets, etc. Kit price: £29-95 plus 30p postage.

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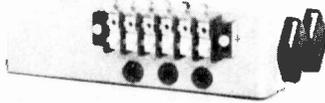
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- \* Construction manual available separately 25p.

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Conversion kit from Mk. 1 to Mk. 2. For constructors already possessing Mk. 1 Kits.—Miniature P.C. assembly £1 incl. carr. and ins. With full conversion instructions.

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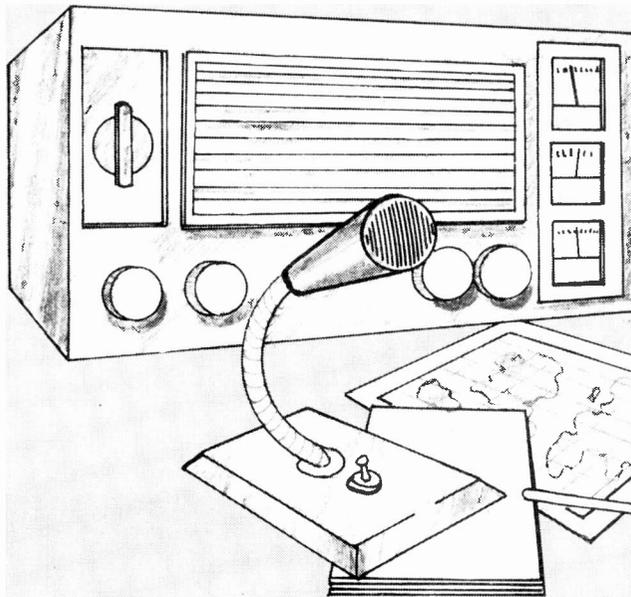
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2N696	0-22	2N3712	0-86	AF116	0-25	BC337	0-19	BFY60	0-60
2N697	0-22	2N3713	1-00	AF117	0-20	BC338	0-19	BFY39	0-23
2N698	0-40	2N3714	1-33	AF118	0-50	BCY30	0-43	BC104	1-42
2N699	0-45	2N3715	1-50	AF124	0-24	BCY31	0-52	BC105	2-25
2N706	0-20	2N3716	1-80	AF125	0-20	BCY32	1-15	BC106A	0-46
2N706A	0-18	2N3717	2-20	AF126	0-19	BCY33	0-34	BC106B	0-55
2N708	0-20	2N3712	1-80	AF127	0-20	BCY34	0-37	BC106D	0-65
2N709	0-45	2N3713	2-65	AF129	0-38	BCY38	0-53	BC106E	0-43
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2N1303	0-19	2N3903	0-24	AF280	0-54	BCY89	0-97	T099	0-48
2N1304	0-24	2N3904	0-27	AL102	0-75	BD115	0-75	BD11	0-38
2N1305	0-24	2N3905	0-24	AL103	0-70	BD116	0-75	LD11L	0-38
2N1306	0-31	2N3906	0-27	BC107	0-16	BD121	0-75	LM723C	0-75
2N1307	0-22	2N4036	0-63	BC108	0-15	BD123	0-32	LM741	0-40
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2N1309	0-36	2N4038	0-46	BC110	0-15	BD124	0-40	BD11	0-48
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2N1671A	1-54	2N4060	0-11	BC116	0-15	BD135	0-43	LM747	1-00
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2N2192	0-40	2N4923	0-83	BC134	0-11	BF117	0-43	MJ480	0-79
2N2192A	0-40	2N5172	0-12	BC135	0-11	BF119	0-58	MJ481	1-14
2N2193	0-58	2N5174	0-22	BC136	0-15	BF121	0-25	MJ490	0-98
2N2193A	0-61	2N5175	0-26	BC137	0-15	BF123	0-27	MJ491	1-38
2N2194	0-73	2N5176	0-32	BC138	0-24	BF125	0-25	MJ6340	0-42
2N2194A	0-30	2N5190	0-92	BC140	0-34	BF152	0-20	MJ2955	1-12
2N2218A	0-60	2N5191	0-95	BC141	0-29	BF153	0-21	MJ3005	1-12
2N2219	0-45	2N5192	1-24	BC142	0-23	BF154	0-20	MJ3005	1-12
2N2219A	0-60	2N5195	1-24	BC143	0-21	BF158	0-23	MJ3005	1-12
2N2220	0-45	2N5196	0-43	BC145	0-13	BF157	0-27	MP8111	0-48
2N2221	0-41	2N5197	0-49	BC147	0-12	BF160	0-23	MP8112	0-40
2N2221A	0-40	2N5198	0-45	BC148	0-13	BF161	0-42	MP8113	0-47
2N2222	0-40	2N5199	0-49	BC149	0-12	BF163	0-32	MP102	3-99
2N222A	0-50	40861	0-48	BC153	0-18	BF166	0-32	MP8A05	0-25
2N2368	0-31	40862	0-50	BC154	0-18	BF167	0-21	MP8A06	0-26
2N2369	0-37	40863	0-61	BC157	0-14	BF173	0-24	MP8A55	0-26
2N2369	0-41	40864	0-61	BC158	0-13	BF175	0-29	MP8A56	0-27
2N2646	0-77	40894	0-56	BC159	0-14	BF178	0-35	NK555V	0-90
2N2647	1-12	40895	0-65	BC160	0-37	BF179	0-43	NK590	4-48
2N2904	0-40	40406	0-44	BC167B	0-13	BF180	0-35	NK591	4-48
2N2904A	0-45	40407	0-33	BC168B	0-13	BF181	0-34	NK595A	4-48
2N2905	0-48	40408	0-50	BC169C	0-11	BF182	0-40	OC23	0-56
2N2905A	0-50	40409	0-52	BC169H	0-13	BF183	0-40	OC28	0-76
2N2906	0-31	40410	0-52	BC169H	0-13	BF184	0-30	OC35	0-60
2N2906A	0-37	40411	2-00	BC170A	0-11	BF185	0-17	OC42	0-35
2N2907	0-40	40414	3-55	BC171	0-13	BF194	0-16	OC45	0-32
2N2907A	0-45	40430	0-85	BC172	0-11	BF195	0-17	OC71	0-12
2N2924	0-14	40433	0-23	BC182	0-12	BF196	0-15	OC72	0-13
2N2925	0-17	40601	0-67	BC182L	0-12	BF197	0-15	OC81	0-20
2N2926	0-16	40602	0-46	BC183	0-09	BF198	0-18	OC82	0-20
Green	0-12	40603	0-53	BC184L	0-09	BF199	0-18	OP1P2	0-50
Yellow	0-11	40604	0-56	BC184	0-11	BF200	0-40	SC35D	1-68
Orange	0-11	40606	1-00	BC184L	0-11	BF225J	0-19	SC36D	1-46
0-11	40609	1-00	BC186	0-25	BF237	0-22	SC40D	1-89	
2N3053	0-25	40673	0-70	BC187	0-27	BF238	0-22	SC41D	1-32
2N3054	0-60	AC107	0-25	BC207	0-12	BF244	0-16	SC45D	1-89
2N3055	0-75	AC113	0-13	BC208	0-16	BF245	0-16	SC49D	1-86
2N3390	0-26	AC117	0-20	BC212K	0-10	BF246	0-43	SC50D	2-60
2N3391	0-23	AC126	0-25	BC212L	0-16	BF247	0-49	SC51D	2-39
2N3391A	0-23	AC127	0-25	BC214L	0-16	BF254	0-16	SL414A	1-80
2N3392	0-13	AC128	0-25	BC237	0-09	BF255	0-17	SL623	4-59
2N3393	0-13	AC151V	0-25	BC238	0-09	BF257	0-46	TAA263	0-70
2N3394	0-13	AC152V	0-17	BC239	0-09	BF259	0-59	TAA550	2-10
2N3402	0-18	AC153	0-26	BC264	0-11	BF255	0-55	TAA621	0-62
2N3403	0-18	AC153S	0-33	BC252	0-18	BF254	0-35	TAA661B	1-20
2N3440	0-59	AC154	0-20	BC253	0-23	BF258	0-22	TAD100	1-50
2N3441	0-97	AC176	0-23	BC257	0-09	BF261	0-27	TAD100	1-50
2N3442	1-25	AC176K	0-33	BC258	0-09	BF269	0-20	Fiber	0-70
2N3414	0-20	AC187K	0-23	BC259	0-13	BF269	0-30	TAA271	0-84
2N3415	0-21	AC188K	0-34	BC261	0-20	BF260	0-25	TAA641B	1-20
2N3416	0-34	AC193	0-26	BC262	0-20	BF264	0-35	TAA692	2-25
2N3417	0-24	ACY19	0-27	BC263	0-23	BF263	0-28	TAA800	1-50
2N3638	0-15	ACY20	0-22	BC300	0-36	BF268	0-30	TBA810	1-50
2N3638A	0-15	ACY21	0-22	BC301	0-34	BF268A	0-24	TLC209	0-35
2N3639	0-27	ACY28	0-20	BC302	0-29	BF265	0-30	TLP29A	0-49
2N3641	0-17	ACY30	0-42	BC303	0-54	BF266	0-38	TLP30A	0-58
2N3702	0-12	AD142	0-50	BC307	0-11	BF268	0-25	TLP31A	0-62
2N3703	0-13	AD143	0-60	BC308	0-11	BF269	0-41	TLP32A	0-74
2N3704	0-14	AD149V	0-58	BC308	0-12	BFY18	0-35	TLP33A	1-01

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Power W	Tol	Price	Tantalum Bead	Value	Price
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1/2	5%	1.5p		22/35v	14p
1	5%	2p		47/35v	14p
2	10%	6p		1p/35v	14p
2 1/2	5%	7p		2-2/35v	14p
5	5%	9p		4-7/35v	16p
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200 .. £5-58 £0-38  
500 .. £9-50 £0-67  
1000 .. £15-92 £0-92  
2000 .. £29-70 £1-50

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0-100 micro A. 580 0-100 micro A. 730  
0-500 micro A. 170 0-500 micro A. 200  
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0-5 mA 170 0-5 mA 200  
0-10 mA 6 0-10 mA 6  
0-50 mA 0-5 0-50 mA 0-5  
0-100 mA 0-5 0-100 mA 0-5  
0-500 mA 0-5 0-500 mA 0-5  
0-1 AMP 0-5 0-1 AMP 0-5  
0-2 AMP 0-5 0-2 AMP 0-5  
0-25 Volt 15K 0-25 Volt 15K  
0-50 Volt 50K 0-50 Volt 50K  
0-300 Volt 300K 0-300 Volt 300K  
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Vt Meter 5250 Vt Meter 5250  
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350	153	14-00	11-44
500	154	15-80	13-20
1000	156	30-70	27-46
2000	158	80-95	55-44
3000	159	79-53	72-49

**50 Volts**

Prim. 200-240V. Sec. 19, 25, 33, 40, 50V.

Amps	Type	Price	Post
0-5	102	£2-11	£0-30
1	103	3-08	0-38
2	104	4-29	0-42
3	105	5-77	0-52
4	106	7-48	0-52
6	107	11-00	0-67
8	118	14-19	0-97
10	119	17-60	0-97

**60 Volts**

Prim. 200-240V. Sec. 24, 30, 40, 48, 60V.

Amps	Type	Price	Post
0-5	124	£2-10	£0-38
1	126	2-97	0-38
2	127	4-77	0-42
3	125	7-15	0-52
4	123	9-35	0-67
5	40	11-55	0-67
6	120	13-57	0-82
8	121	18-00	1-00
10	122	19-40	1-00
12	189	£1-62	1-10

**12 & 24 Volts Prim. 200-240V.**

Amps	24V	Type	Price	Post
0-3	0-15	242	1-34	0-22
0-5	0-25	111	1-34	0-22
1	0-5	213	1-59	0-22
2	1	71	2-09	0-22
4	2	18	2-75	0-38
6	3	70	3-58	0-42
8	4	108	3-96	0-52
10	5	72	4-87	0-52
12	6	116	5-67	0-52
16	8	17	6-84	0-52
20	10	115	10-29	0-69
30	15	187	13-75	0-97
40	20	232	17-25	1-06
60	30	226	22-52	1-10

**30 Volts**

Prim. 200-240V. Sec. 12, 15, 20, 24, 30V.

Amps	Type	Price	Post
0-5	112	£1-58	£0-22
1	79	2-20	0-38
2	3	3-19	0-38
2	20	3-98	0-42
4	21	4-68	0-52
5	51	5-80	0-52
6	117	6-93	0-52
8	88	9-00	0-67
10	89	10-00	0-67

**MINIATURE AND EQUIPMENT**

Prim. 240V with screen.

Sec. 1	Sec. 2	Sec. 3	Milliamps	Type	Price	Post
3-0-3	—	200	238	1-23	£0-10	
0-6	0-6	500	500	234	1-30	
0-6	0-5	1000	1000	212	1-68	
9-0-9	—	100	—	13	1-23	
0-9	0-9	330	330	235	1-48	
0-8-9	0-8-9	500	500	207	2-28	
0-8-9	0-8-9	1000	1000	208	3-03	
15-0-15	—	40	—	240	1-23	
0-15	0-15	200	200	236	1-30	
20-0-20	—	30	—	241	1-23	
0-20	0-20	150	150	237	1-30	
0-15-20	0-15-20	500	500	205	2-97	
0-20	0-20	300	300	214	1-76	
0-20	—	3500	(No screen)	1116	3-00	
20-12-0-12-20	—	700 (D/C)	—	221	1-55	
0-15-20	0-15-20	1000	1000	206	3-80	
0-15-27	0-15-27	500	500	203	3-08	
0-15-27	0-15-27	1000	1000	204	3-24	

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200 P.I.V. 28p	200 P.I.V. 45p	400 P.I.V. 85p	200 P.I.V. 80p
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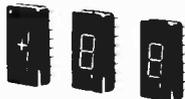
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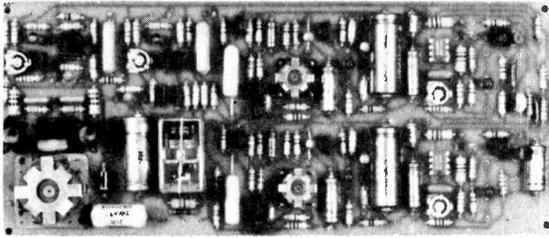
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(PE Sept 72/Jan 73) Details in lists

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(PE Nov 70/Mar 71) Stereo Sets and PCBs Pre-amp—Rs. Ca. Pots. Sw s—with jW MO Rs £14.18—with jW CF Rs. £10.40. PCB as published. £2.20. Main Amp—Rs. Cs. Pots. £5.88. PCB (3 1/2in x 5in). £1.28 Power supply—Rs. Cs. Pot. £4.56. PCB (2in x 4in). 65p.

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**SOUND SYNTHESISER**

(PE Feb. 73/Feb. 74)

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(PE May 74)

*Details of all these in List*

**REVERBERATION UNIT**

(PW Nov/Dec. 72) S/c's. Rs. Ca. T/former—with Rotary Pots. £8.44. PCB (2in x 1 1/2in). £1.40. Spring unit excluded

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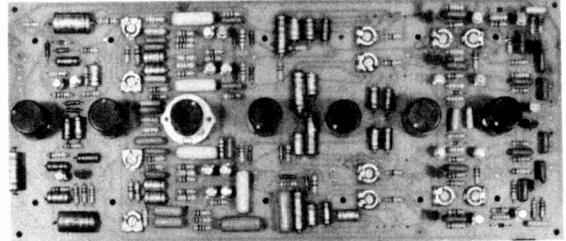
(PW Oct 73/Jan 74) Multisystem Quadrasonic Decoder. S/c's. I/c's. Rs. Ca. Pots. Makeswitches. £13.74. PSU. £3.17. Set of PCBs. £2.60.

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(PE Sept 73) S/c's. Rs. Ca. Pots. PCB (1 1/2in x 2 1/2in). £2.20.

**RONDO**

(PE Sept 73/Feb 74) Details in List



**AURORA**

(PE Apr/Aug 71) Multichannel Sound Controlled Light. S/c's (Excl. SCRs). Rs. Ca. Pots. Cores—Pre-amp. Sync Generator and 4 Chans. £10.97; 4 extra chans. £8.35. Reg. PSU. £4.32. PCB (4 1/2in x 10 1/2in) for Pre-amp and 4 Chans (also holds pots). £2.50. PCB (4 1/2in x 5in) for Sync. Gen. PSU. 8 cores. 8 SCRs. £1.25.

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2 Variable Frequency Strobe Generators and 4 Variable Amplitude Frequency Generators S/c's. Rs. Cs. Pots. PCB (3 1/2in x 5 1/2in). £4.87.

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(PE Oct 73) S/c's. Rs. Ca. Pots. Make-switches Sub-assembly PCB. £8.04.

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(PE Feb 72) S/c's. Rs. Cs. Pot. Sw. PCB (1 1/2in x 3in). £2.30. Reg. PSU and PCB (1 1/2in x 2 1/2in). £4.40.

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**SEMICONDUCTORS**

AC128	28p	2N2905	27p	0 47 63	6p	100 10	6p	0 01	3p
AC176	28p	2N2907	22p	1 0 63	6p	100 25	6p	0 015	3p
AO161	48p	2N1702	12p	2 2 63	6p	100 40	7p	0 022	3p
BC107	13p	2N3703	12p	4 7 35	6p	100 63	12p	0 033	3 1/2p
BC108	13p	2N3704	12p	4 7 63	6p	150 16	6p	0 047	3 1/2p
BC109	13p	2N3819	35p	6 8 40	6p	150 63	12p	0 068	3 1/2p
BC147	12p	2N5832E	39p	10 63	6p	220 16	6p	0 1	4p
BC148	12p	2N4871	36p	15 40	6p	220 25	6p	0 1	4p
BC149	12p			22 10	6p	220 63	12p	0 22	5p
BC157	12p	1N916	4p	22 25	6p	220 83	12p	0 33	7p
BC158	12p	1N4001	6p	33 6 3	6p	330 10	6p	0 68	11p
BC182L	12p	1N4002	7p	33 16	6p	470 6 3	6p	1 0	14p
BC224	14p	1N4004	8p	33 40	6p	470 10	10p		
BC209C	14p	1N4005	8p	33 50	6p	470 25	14p		
BC212L	15p	BA145	23p	47 25	6p	500 64	46p		
BC711	15p	OA91	7p	47 40	6p	680 5	3p		
BF950	22p	OA200	8p	47 63	7p	880 5	3p		
BF952	23p	1G7P	12p	50 6 4	6p	880 25	28p		
BS195A	15p	15J50	11p			1000 10	14p		
MJE2955	119p					1000 16	25p		
MJE3055	75p					1000 25	25p		
NK70033	112p					1000 25	25p		
OC28	65p					1000 40	48p		
OC71	14p	709 TOS	40p	7447	175p	2200 25	45p		
OC84	25p	723 TOS	55p	7473	44p	2200 40	50p		
ORP12	55p	741 8P DIL	40p	7489	432p	2800 100	350p		
TIS43	38p	747 14P DIL	115p	7815 TO220	226p	3300 63	133p		
2N106	13p	748 TOS	63p	CA3046	69p	3300 100	350p		
2N107	13p	7400	20p	PA263	168p	4700 16	80p		
2N104	22p	7402	20p	SU3402N	189p	4700 25	75p		
2N1304	22p	7420	20p			4700 40	83p		
2N219	27p	7420	20p						

**ELECTROLYTIC (uF/V)**

100 10	6p	100 10	6p
100 25	6p	100 25	6p
100 40	7p	100 40	7p
100 63	12p	100 63	12p
150 16	6p	150 16	6p
150 63	12p	150 63	12p
220 16	6p	220 16	6p
220 25	6p	220 25	6p
220 40	7p	220 40	7p
220 63	12p	220 63	12p
330 10	6p	330 10	6p
470 6 3	6p	470 6 3	6p
470 10	10p	470 10	10p
470 25	14p	470 25	14p
500 64	46p	500 64	46p
680 5	3p	680 5	3p
880 25	28p	880 25	28p
1000 10	14p	1000 10	14p
1000 16	25p	1000 16	25p
1000 25	25p	1000 25	25p
1000 40	48p	1000 40	48p
2200 25	45p	2200 25	45p
2200 40	50p	2200 40	50p
2800 100	350p	2800 100	350p
3300 63	133p	3300 63	133p
3300 100	350p	3300 100	350p
4700 16	80p	4700 16	80p
4700 25	75p	4700 25	75p
4700 40	83p	4700 40	83p

**POLYESTER (uF)**

0 1 35	12p
0 2 25	12p
0 47 35	12p
0 10 35	12p
0 22 35	12p
0 47 35	12p
0 10 35	12p
0 22 35	12p
0 47 35	12p
0 10 35	12p
0 22 35	12p
0 47 35	12p
0 10 35	12p
0 22 35	12p
0 47 35	12p
0 10 35	12p
0 22 35	12p
0 47 35	12p
0 10 35	12p
0 22 35	12p
0 47 35	12p

**TANTALUM BEAD (uF/V)**

0 1 35	12p
0 2 25	12p
0 47 35	12p
0 10 35	12p
0 22 35	12p
0 47 35	12p
0 10 35	12p
0 22 35	12p
0 47 35	12p
0 10 35	12p
0 22 35	12p
0 47 35	12p
0 10 35	12p
0 22 35	12p
0 47 35	12p
0 10 35	12p
0 22 35	12p
0 47 35	12p

ADD 15p P & P.  
ADD 10% VAT to total cost (including P & P)  
SEND S A E (Stamped Addressed Envelope) for Free Itemised List (and with all enquiries please!)  
OVERSEAS COSTS P & P will be charged at cost (most kit weights and postal rates are shown in list) Send International Reply Coupon for Free List & with all enquiries.  
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COLOUR CODE identification supplied with most kits and as part of list  
PCBs are Fibreglass, Drilled, Tinned, and designed by Phonosonics unless stated as published  
PCB Layout and Circuit Diagram supplied free with Phonosonics-designed PCBs  
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Ready Made Unit £14.75 inc. VAT and p & p.  
State 6V or 12V system.

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Part No.	Price																				
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1N23	0-85	AFZ12	0-90	BY210	0-80	0AZ206	0-45	ZB271	0-18												
1N85	0-88	ASX28	0-85	BYZ11	0-40	0AZ207	0-45	ZT21	0-80												
1N263	0-40	ASX27	0-80	BYZ12	0-40	0AZ208	0-40	ZT43	0-85												
1N265	0-50	ASX28	0-25	BYZ13	0-35	0AZ209	0-40	ZTX107	0-12												
1N645	0-16	ASX29	0-80	BYZ15	1-85	0AZ210	0-40	ZTX108	0-10												
1N725A	0-90	ASX30	0-85	BYZ16	0-60	0AZ211	0-40	ZTX300	0-14												
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2G371	0-40	ASX66	0-88	C84B	1-90	0AZ244	0-25														
2G381	0-22	ASZ21	1-00	CS104	3-00	0AZ246	0-15														
2G414	0-30	ASZ23	1-50	DD000	0-15	0AZ290	0-38														
2G417	0-25	AU101	1-00	DD003	0-15	OC18	1-00	7400	0-30												
2N404	0-28	AU100	1-00	DD006	0-25	OC18T	1-00	7401	0-30												
2N497	0-15	BC107	0-12	DD007	0-40	OC19	1-50	7402	0-30												
2N698	0-30	BC108	0-12	DD008	0-88	OC20	2-00	7403	0-30												
2N706	0-10	BC109	0-12	D3	3-88	OC22	1-00	7404	0-30												
2N706A	0-12	BC113	0-16	GD4	0-10	OC23	1-25	7405	0-20												
2N708	0-16	BC115	0-20	GD5	0-38	OC24	0-40	7406	0-40												
2N709	0-40	BC116	0-20	GD8	0-85	OC25	0-40	7407	0-40												
2N1091	0-55	BC118A	0-28	GD12	0-10	OC28	0-40	7408	0-25												
2N1132	0-25	BC118	0-28	GET102	0-50	OC28	0-70	7409	0-38												
2N1302	0-18	BC121	0-20	GET103	0-40	OC29	0-65	7410	0-38												
2N1303	0-18	BC122	0-20	GET113	0-35	OC30	0-40	7412	0-28												
2N1304	0-22	BC125	0-65	GET116	0-75	OC36	0-55	7413	0-30												
2N1305	0-22	BC140	0-55	GET116	0-85	OC41	0-35	7416	0-30												
2N1306	0-28	BC147	0-12	GET120	0-50	OC42	0-40	7417	0-30												
2N1307	0-28	BC148	0-10	GET872	0-30	OC43	0-70	7420	0-30												
2N1308	0-28	BC149	0-12	GET875	0-40	OC44	0-18	7423	0-40												
2N2147	0-75	BC157	0-14	GET890	0-50	OC44M	0-17	7426	0-37												
2N2148	0-80	BC168	0-12	GET881	0-25	OC48	0-18	7427	0-37												
2N2160	1-00	BC169	0-68	GET882	0-35	OC48M	0-18	7428	0-37												
2N2218	0-28	BC169	0-14	GET886	0-40	OC46	0-27	7430	0-38												
2N2219	0-85	BCY31	0-45	GEX44	0-08	OC57	0-60	7432	0-27												
2N2389A	0-16	BCY32	1-20	GEX45/1	0-45	OC58	0-60	7433	0-48												
2N2444	1-99	BCY33	0-85	GEX341	0-45	OC59	0-60	7437	0-48												
2N2613	0-28	BCY38	0-55	GJ3M	0-55	OC68	0-60	7438	0-48												
2N2646	0-16	BCY38	0-55	GJ4M	0-50	OC70	0-18	7440	0-30												
2N2909	0-20	BCY39	1-00	GJ5M	0-85	OC71	0-15	7440	0-20												
2N2904A	0-25	BCY40	0-80	HG1005	0-50	OC72	0-25	7441A	0-85												
2N2906	0-80	BCY42	0-20	HG1005	0-50	OC73	0-50	7450	0-30												
2N2907	0-28	BCY70	0-15	HG100A	0-80	OC74	0-80	7451	0-30												
2N2924	0-18	BCY71	0-80	MA100	0-20	OC76	0-20	7453	0-30												
2N2925	0-15	BCZ10	0-60	MAT101	0-25	OC76	0-20	7453	0-30												
2N2926	0-10	BCZ11	0-60	MAT120	0-80	OC77	0-50	7454	0-30												
2N3054	0-60	BD121	1-00	MAT121	0-25	OC78	0-25	7460	0-30												
2N3056	0-60	BD123	1-00	MJE520	0-65	OC79	0-80	7472	0-38												
2N3702	0-11	BD124	0-80	MJE2955	1-10	OC81	0-28	7473	0-44												
2N3705	0-15	BF115	0-22	MJ3055	0-70	OC82	0-28	7474	0-48												
2N3706	0-13	BF117	0-20	MPE102	0-40	OC81M	0-18	7476	0-59												
2N3707	0-13	BF167	0-55	MPP103	0-80	OC81Z	0-45	7476	0-46												
2N3709	0-10	BF173	0-28	MPP104	0-85	OC82	0-28	7482	0-57												
2N3710	0-11	BF181	0-85	MPP105	0-46	OC82D	0-25	7483	1-30												
2N3819	0-25	BF184	0-22	NKT128	0-45	OC83	0-25	7484	1-00												
2N4289	0-20	BF191	0-18	NKT129	0-80	OC84	0-20	7486	0-50												
2N5027	0-28	BF194	0-13	NKT211	0-25	OC114	0-85	7489	0-75												
2N5089	0-28	BF195	0-18	NKT213	0-85	OC122	1-00	7490	0-75												
2B301	0-59	BF196	0-15	NKT214	0-24	OC123	1-10	7491A	1-10												
2B304	1-15	BF197	0-15	NKT218	0-40	OC139	0-40	7493	0-75												
2B501	0-75	BF861	0-85	NKT217	0-45	OC140	0-65	7494	0-85												
2B703	1-00	BF896	0-85	NKT218	1-15	OC141	0-80	7495	0-85												
AA129	0-20	BFX12	0-20	NKT219	0-28	OC170	0-85	7496	1-00												
AAZ12	0-75	BFX13	0-25	NKT222	0-80	OC171	0-80	7497	4-82												
AAZ13	0-10	BFX29	0-28	NKT224	0-25	OC171	0-80	7497	4-82												
AC107	0-85	BFX30	0-28	NKT261	0-24	OC200															

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115/230-230/230 volts. Screened. Primary two separate 0-115V for 115 or 230 volt. Secondary two 115V at 150 VA each for 115 or 230 volt output. Can be used in series or parallel connections. Fully tinned, Length 13.5 cm. Width 11 cm. Height 13.5 cm. Weight 15 lb.  
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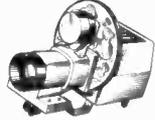
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Col. (1)	58	5-9	6 c/o	80p
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Price	700	16-24	4 c/o	80p
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Incl. Base	2,500	31-43	2 c/o HD	50p
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Each bank comprises a c/o rated at 10amps 240V. A.C. Black knob 1in. Fixing hole 1/2 in. ONE bank 30p; TWO bank 40p; THREE bank 50p. Quote for quantity.



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I/C Timer	NE555V	0-80
Dual I/C Timer	NE556A	1-40
High Phased Locked Loop	NE560B	4-20
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Decade Counter, Latch, Driver	AY-5-4007D	8-35
<b>Organ Circuits:</b>		
7 Stage Generator	AY-1-0212	5-55
7 Stage Divider	AY-1-5050	2-35
4 Stage Divider	AY-1-5051	1-20
5 Stage Divider	AY-1-6721/5	1-30
6 Stage Divider	AY-1-6721/6	1-45
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Static Shift Register	SL6-4032	4-00
Static Shift Register	SL5-2128	3-45
Static Shift Register	SL7-2128	3-80
Static Shift Register	SL7-4056	3-45
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Radio Receiver	ZN414	1-20
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Data sheets are supplied.

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- £1 30 Plastic Power NPN transistor TO220 case like 2N3055. U/tested
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- £1 200 mixed capacitors.
- £1 500 mixed resistors.
- ☆ Any 5 packs £4-50 ☆ Post/package 10p per pack

<b>SEMICONDUCTORS</b>			
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AC127 16p	OC45	10p	
AC128 15p	OC71	11p	22p
AC141K 26p	OC81	12p	200V 24p
AC142K 26p	2N706	14p	600V 27p
AC176 18p	2N1131	24p	
AC187 24p	2N1132	28p	
AC188 24p	2N2904	20p	1 Amp
AC187K 23p	2N2926	11p	50V 29p
AC188K 23p	2N3053	26p	100V 32p
AD149 49p	2N3054	55p	200V 34p
AD161 33p	2N3055	49p	400V 44p
AD162 40p	2N3702	14p	3 Amp
AF114 20p	2N3703	13p	50V 39p
AF115 20p	2N3704	14p	100V 44p
AF116 20p	2N3705	13p	200V 48p
AF117 20p	2N3706	12p	400V 66p
BC107 13p	2N3707	13p	5 Amp
BC108 12p	2N3708	11p	50V 46p
BC109 13p	2N3709	12p	100V 57p
BC147 13p	2N3710	12p	200V 66p
BC148 13p	2N3711	12p	400V 77p
BC149 13p	2N3819	35p	2 Amp
BC182 13p	40361	55p	100V 33p
BC183 11p	40362	55p	100V 33p
BC184 14p	40636	69p	200V 55p
BC212 13p	1N914	8p	400V 77p
BC213 13p	1N916	8p	6 Amp
BC214 13p	1N4001	7p	100V 66p
BD131 68p	1N4002	8p	200V 88p
BD132 90p	1N4003	10p	400V 99p
BF194 16p	1N4004	10p	10 Amp
BF195 17p	1N4006	15p	100V 99p
BF244 27p	1N4148	6p	200V 1-32
BFY50 18p	1N5400	16p	400V 1-43
BFY51 18p	1N5401	17p	400mW
BFY52 17p	1N5402	19p	ZENER
MPR111 36p	1N5404	24p	DIODES
OC28 50p	1N5406	28p	3-3 to 33
OC26 50p			volt 11p each

See advertisement to Practical Wireless for full range of TTL integrated circuits

## Resistors

½ watt 5% carbon	1p
½ watt 5% carbon	1p
1 watt 10% carbon	3p
range 10 ohms to 4.7 megohms.	
½ watt m/o 2%	4p
range 10 ohms to 1 megohms.	

## VEROBOARD

24 x 34	0-1	0-15
24 x 5	24p	19p
34 x 34	27p	23p
34 x 5	27p	23p
17 x 24	31p	31p
17 x 34	82p	63p
17 x 5 (Plain)	£1-10	87p
Pin insertion tool	57p	57p
Spot face cutter	46p	46p
Sk. 36 Pins	20p	20p

## Electrolytic Capacitors

<b>6.3 VOLT</b>	220µF 9p	<b>40 VOLT</b>
68µF 61p	680µF 17p	47µF 61p
150µF 61p	1000µF 17p	100µF 9p
470µF 11p	1500µF 25p	68µF 10p
680µF 13p	2000µF 43p	220µF 11p
1500µF 18p		470µF 19p
2200µF 18p		680µF 25p
3300µF 26p		1000µF 25p
		2200µF 44p
<b>10 VOLT</b>	10µF 61p	<b>63 VOLT</b>
47µF 61p	22µF 61p	1µF 61p
100µF 61p	47µF 61p	2-2µF 61p
220µF 8p	100µF 8p	4-7µF 61p
330µF 10p	150µF 8p	6-8µF 61p
470µF 10p	220µF 10p	10µF 61p
1000µF 11p	470µF 13p	22µF 61p
1500µF 20p	680µF 20p	68µF 10p
2200µF 24p	1000µF 22p	100µF 11p
	2200µF 39p	150µF 13p
	5000µF 68p	220µF 19p
<b>16 VOLT</b>		33µF 61p
15µF 61p		150µF 61p
33µF 61p		470µF 26p
150µF 61p		1000µF 44p
150µF 8p		

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**Potentiometers**  
Carbon track 500Ω to 2.2MΩ  
Log or Linear.  
Single 13p. Dual gang (stereo) 44p.  
Single type with D.P. switch 13p extra.

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### C296 SERIES

400V: 0-001µF, 0-0015, 0-0022, 0-0033, 0-0047 3p, 0-0068, 0-01, 0-015, 0-022, 0-033 34p, 0-047, 0-068, 0-1 44p, 0-15 61p, 0-22 84p, 0-33 12p, 0-47 14p, 0-68, 0-1µF, 0-15, 0-22 54p, 0-33 7p, 0-47 94p, 0-68 12p, 1µF 14p, 1-5µF 22p, 2-2µF 24p.



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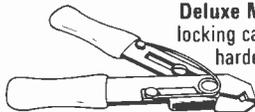
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Also available in 8 ohm with EMI 13in  $\times$  8in. bass speaker with parasitic tweeter. **£7.15**, Carr. 75p.

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LIMITED number of BSR 0123 Auto Charger De Luxe with lightweight tubular arm and stereo cartridge. Brand new. **ONLY £3.00** + P. & P. 60p.

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NEW FURTHER IMPROVED MODEL WITH HIGHER OUTPUT AND INCORPORATING HIGH QUALITY READY DRILLED PRINTED CIRCUIT BOARD WITH COMPONENT IDENTIFICATION CLEARLY MARKED FOR EASIER CONSTRUCTION

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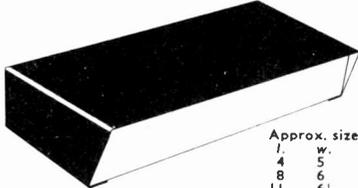
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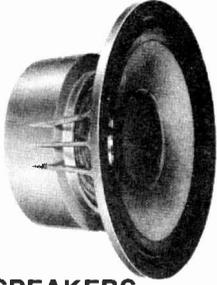
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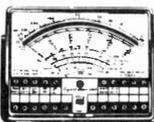
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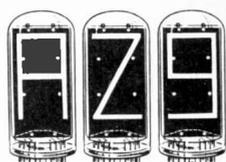
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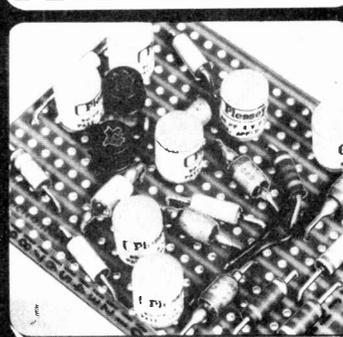
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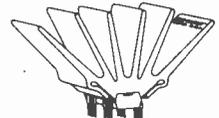
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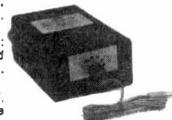
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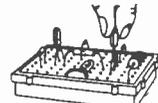
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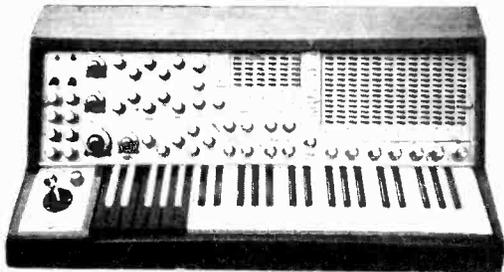
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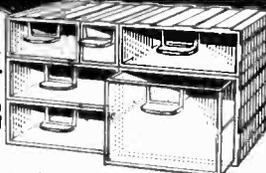
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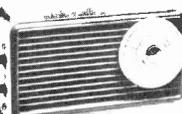
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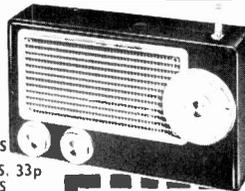
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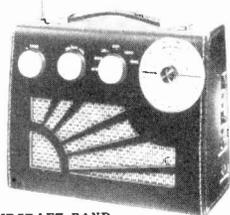
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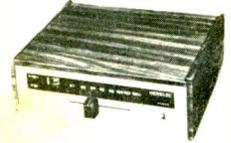


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