

PRACTICAL

# ELECTRONICS

MAY 1984

90p

TEST  
GEAR

TEST  
GEAR

SPECIAL

SPECIAL

FREE!

LOGIC DESIGN CARD-Nº 3

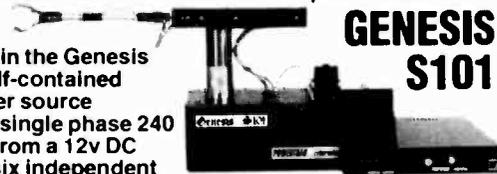


# Low-price robots from POWERTRAN

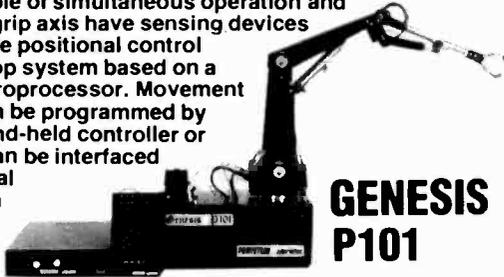
— hydraulically powered  
— microprocessor controlled

The UK-designed and manufactured range of Genesis general purpose robots provides a first-rate introduction to robotics for both education and industry. With prices from as low as £470, even the home enthusiast can aspire to his or her own robot.

Each robot in the Genesis range has a self-contained hydraulic power source operated from single phase 240 or 120v AC or from a 12v DC supply. Up to six independent axes are capable of simultaneous operation and all except the grip axis have sensing devices fitted to provide positional control by a closed loop system based on a dedicated microprocessor. Movement sequences can be programmed by means of a hand-held controller or the systems can be interfaced with an external computer via a standard RS232C link.



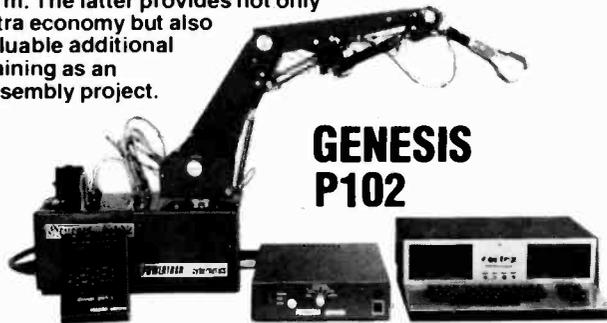
**GENESIS S101**



**GENESIS P101**

The top-of-the-range P102 has dual speed control, enhanced memory and double acting cylinders for increased torque on the wrist and arm joints. There is position interrogation via the RS232C interface, increasing the versatility of computer control and inputs are provided for machine tool interfacing.

All Genesis robots are available either ready-built or in kit form. The latter provides not only extra economy but also valuable additional training as an assembly project.



**GENESIS P102**

Cortex 16 bit microcomputer



**HEBOT II Turtle-type robot**

For a little over £100, Herbot II takes programming off the VDU and into the real world. Each wheel is independently controlled by a computer, enabling the robot to perform an almost infinite number of moves. It has blinking eyes, a two-tone bleep and a solenoid-operated pen to chart its moves. Touch sensors, coupled to its shell return data about its environment to the computer enabling evasive or exploratory action to be calculated.

The robot connects directly to an I/O port or, via the interface board, to the expansion bus of a ZX81 or other microcomputer.

## HEBOT II

Weight 1.8kg  
complete kit with assembly instructions £95  
Interface board kit £11

## MICROGRASP



A real programmable robot for under £300! Micrograsp has an articulated arm jointed at shoulder, elbow and wrist positions. The entire arm rotates about its base and there is a motor driven gripper. All five axes are motor driven and four of these are servo controlled giving positive positioning. The robot can be controlled by any microcomputer with an expansion bus—the Sinclair ZX81 being particularly suitable.

## MICROGRASP

Weight 8.7kg, max. lifting capacity 100g  
Robot kit with power supply £215.00

Universal computer interface board kit £57.00  
23 way edge connector £3.00  
ZX81 peripheral/RAM pack splitter board £3.50

## GENESIS S101

Weight 29kg, max. lifting capacity 1.5kg  
4-axis model (kit form) £470

5-axis model (kit form) £525  
5-axis complete system (kit form) £817

## GENESIS P101

Weight 34kg, max lifting capacity 1.8kg  
6-axis model (kit form) £750  
6-axis complete system (kit form) £1050

## GENESIS P102

Weight 36kg, max lifting capacity 2kg  
6-axis system (kit form) £1476  
Powertran Cortex microcomputer self-assembly kit £295.00



# POWERTRAN cybernetics Ltd.

PORTWAY INDUSTRIAL ESTATE, ANDOVER, HANTS SP10 3PE. TEL (0264) 64455

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Filesheet 15 NSC 800	

**OUR JUNE ISSUE WILL BE ON SALE FRIDAY, MAY 4th, 1984**

(for details of contents see page 15/4 of Micro-file)

\*The instruments featured on the front cover were kindly loaned to us by the House of Instruments, Global Specialties Corporation and Maplin Electronic Supplies

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# T.V. SOUND TUNER

**SERIES II BUILT AND TESTED** Complete with case. £26.50 + £2.00 p&p.

In the cut-throat world of consumer electronics, one of the questions designers apparently ponder over is "Will anyone notice if we save money by chopping this out?" In the domestic TV set, one of the first casualties seems to be the sound quality. Small speakers and no tone controls are common and all this is really quite sad, as the TV companies do their best to transmit the highest quality sound. Given this background a compact and Independent TV tuner that connects direct to your Hi-Fi is a must for quality reproduction. The unit is mains-operated.



Also available with built-in headphone amp. ONLY £32.50 + £2.00 p&p.

This TV SOUND TUNER offers full UHF coverage with 5 pre-selected tuning controls. It can also be used in conjunction with your video recorder. Dimensions: 10 1/2" x 7 1/2" x 2 1/2". E.T.I. kit version of above without chassis, case and hardware. £16.20 plus £1.50 p&p.

## PRACTICAL ELECTRONICS STEREO CASSETTE RECORDER KIT

COMPLETE WITH CASE

ONLY £34.50 plus £2.75 p&p.

- NOISE REDUCTION SYSTEM. • AUTO STOP. • TAPE COUNTER. • SWITCHABLE E.Q. • INDEPENDENT LEVEL CONTROLS.
- TWIN V.U. METER. • WOW & FLUTTER 0.1%. • RECORD/PLAYBACK I.C. WITH ELECTRONIC SWITCHING. • FULLY VARIABLE RECORDING BIAS FOR ACCURATE MATCHING OF ALL TYPES.

Kit includes tape transport mechanism, ready punched and back printed quality circuit board and all electronic parts. I.e. semiconductors, resistors, capacitors, hardware, top cover, printed scale and mains transformer. You only supply solder & hook-up wire. Featured in April P.E. reprint 50p. Free with kit.



## BSR RECORD DECKS

Auto-Changer model - takes up to 6 records with manual override. Supplied with stereo ceramic cartridge.

£12.95 plus £1.75 p&p.



3 speed, auto, set-down; with auto return. Fitted with viscous damped cue, tubular aluminium counter-weighted arm, fitted with ADC magnetic head. Ideally suited for home or disco use.

£25.95 plus £1.75 p&p.

Manual single play record deck with auto return and cueing lever. Fitted with stereo ceramic cartridge 2 speeds with 45 rpm spindle adaptor ideally suited for home or disco. 13" x 11" approx.

£14.95 plus £1.75 p&p.



**SPECIAL OFFER!** Replacement st. cassette tape heads. £1.80 ea. Add 50p p&p to order. Phillips st. mag. cartridge. £3.95 + 60p p&p.

PLINTH to suit BSR Record Player Deck (with cover). Size 16 1/2" x 14 1/2" x 2 1/2". Cover size: £14 1/2" x 13 1/2" x 3 1/2". Due to fragile nature, Buyer collect only. Price: £8.95.

## STEREO TUNER KIT

**SPECIAL OFFER!**

£13.95 + £2.50 p&p.

This easy to build 3 band stereo AM/FM tuner kit is designed in conjunction with P.E. (July '81). For ease of construction and alignment it incorporates three Mullard modules and an I.C. IF System. Front scale size 10 1/2" x 2 1/2" approx. Complete with diagram and instructions.



## 125W HIGH POWER AMP MODULES

The power amp kit is a module for high power applications - disco units, guitar amplifiers, public address systems and even high power domestic systems. The unit is protected against short circuiting of the load and is safe in an open circuit condition. A large safety margin exists by use of generously rated components, result, a high powered rugged unit. The PC board is back printed, etched and ready to drill for ease of construction and the aluminium chassis is preformed and ready to use. Supplied with all parts, circuit diagrams and instructions.

Accessories: Stereo mains power supply kit with trans. £10.50 + £2 p&p. Mono: £7.50 + £2 p&p.



### SPECIFICATIONS:

Max. output power (RMS): 125 W. Operating voltage (DC): 50 - 80 max. Loads: 4 - 16 ohm. Frequency response measured @ 100 watts: 25Hz - 20KHz. Sensitivity for 100w: 400mV @ 47K. Typical T.H.D. @ 50 watts, 4 ohms: 0.1%. Dimensions: 205x90 and 190x36mm.

KIT £12.00 + £1.15 p&p. BUILT £17.50 + £1.15 p&p.

## HI-FI SPEAKER BARGAINS

AUDAX 8" SPEAKER £5.95 + £2.20 p&p.

High quality 40 watts RMS bass/mid. Ideal for either HiFi or Disco use this speaker features an aluminium voice coil and a heavy 70mm dia. magnet. Freq. Res.: 20Hz to 7kHz. Imp.: 8 ohms.

AUDAX 40W FERRO-FLUID HI-FI TWEETER Freq. res.: 5KHz - 22KHz. Imp.: 8 ohms. 60mm sq. £5.50 + 60p p&p.

GOODMANS TWEETERS 8 ohm soft dome radiator tweeter (3 1/2" sq) for use in systems up to 40W. £3.95 ea + £1 p&p. £6.95 pr + £1.50.

## MONO MIXER AMP

Ideal for halls and clubs.

£45.00 + £2 p&p.

50 Watt, six individually mixed inputs for 2 pickups (Cer. or mag), 2 moving coil microphones and 2 auxiliary for tape tuner, organs etc. Eight slider controls - 6 for level and 2 for master bass and treble, 4 extra treble controls for mic. and aux. inputs. Size: 13 1/2" x 6 1/2" x 3 1/2" app. Power output 50 W RMS (cont.) for use with 4 to 8 ohm speakers. Attractive black vinyl case with matching fascia and knobs. Ready to use.



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# Are you as fast as a bullet?

WOULD YOU HAVE MADE A FIGHTER PILOT?  
NOW YOU CAN FIND OUT WITH THE NEW

## REACTION TESTER

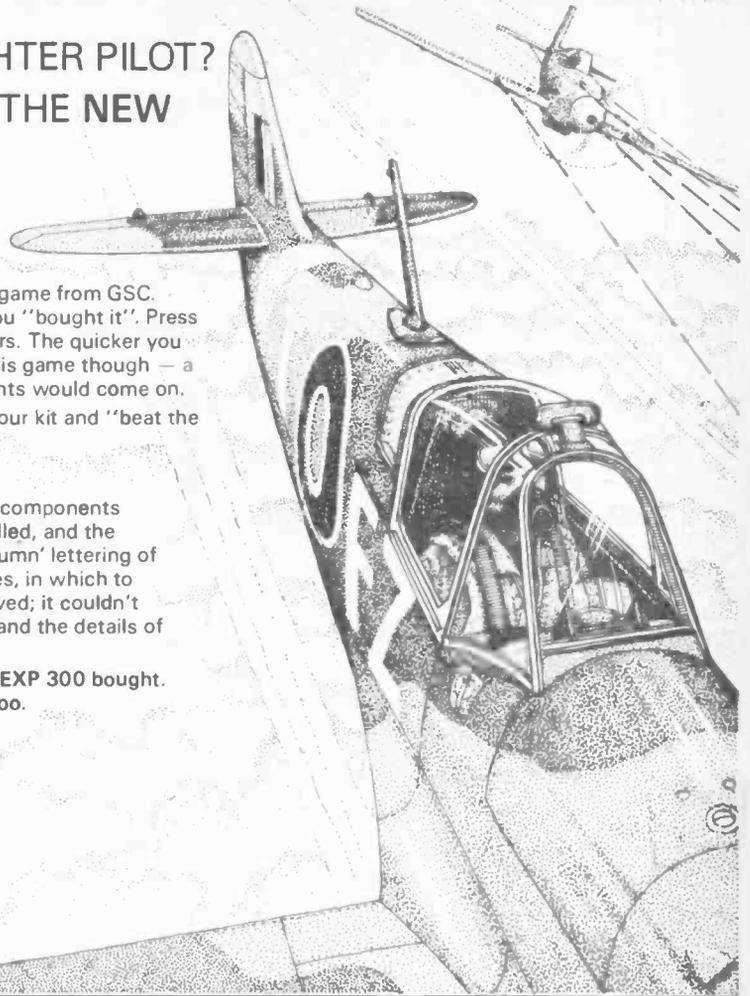
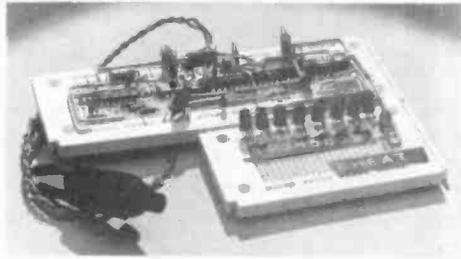
A FREE PROJECT FROM GSC

Split second timing is essential for this, the latest and fastest game from GSC. Find out how long you could have stayed "upstairs" before you "bought it". Press start switch, after a random time period, a moving light appears. The quicker you press the button, the longer you "stay alive". You can't fool this game though — a "cheat" light will tell everyone that you guessed when the lights would come on. Speed and concentration are the names of this game — build our kit and "beat the bullet".

### HOW DO YOU MAKE IT?

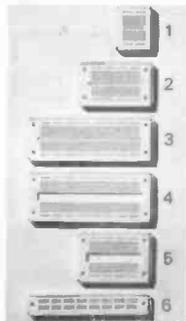
Our FREE project sheet gives you a large, clear diagram of the components layed out on an EXP 300 breadboard. Each component is labelled, and the values are given in a component listing. Even the 'row and column' lettering of our EXP 300 is shown to make the location of the correct holes, in which to push the components, easy to find. There's no soldering involved; it couldn't be easier! As an extra bonus, there's a full circuit description, and the details of a regulated power supply on the other side of the sheet.

"Clip the coupon" and get your FREE project sheet with each EXP 300 bought. AND a free catalogue! Just ask about our other free projects too.



### EXPERIMENTOR BREADBOARDS

The largest range of breadboards from GSC. Each hole is identified by a letter/number system. EACH NICKEL SILVER CONTACT CARRIES A LIFE TIME GUARANTEE. Any Experimentor breadboard can be 'snap-locked' with others to build a breadboard of any size.

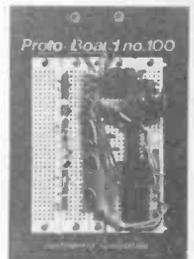
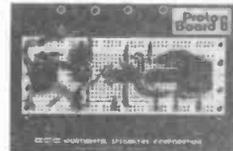


1. EXP 325 £2.00 The ideal breadboard for 1 chip circuits. Accepts 8, 14, 16 and up to 22 pin ICs. Has 130 contact points including two 10 point bus-bars.
2. EXP 350 £3.45 Specially designed for working with up to 40 pin ICs perfect for 3 & 14 pin ICs. Has 270 contact points including two 20 point bus-bars.
3. EXP 300 £6.00 The most widely bought breadboard in the UK. With 550 contact points, two 40 point bus-bars, the EXP 300 will accept any size IC and up to 5 x 14 pin DIPS. Use this breadboard with Adventures in Microelectronics.
4. EXP 600 £7.25 Most MICROPROCESSOR projects in magazines and educational books are built on the EXP 600.
5. EXP 650 £4.25 Has 6" centre spacing so is perfect for MICROPROCESSOR applications.
6. EXP 4B £2.50 Four more bus-bars in "snap-on" unit.

### PROTO-BOARDS

The ultimate in breadboards for the minimum of cost. Two easily assembled kits.

7. PROTO-BOARD 6 KIT £11.00 630 contacts, four 5-way binding posts accepts up to six 14-pin Dips.
8. PROTO-BOARD 100 KIT Complete with 760 contacts accepts up to ten 14-pin Dips, with two binding posts and sturdy base. Large capacity with kit economy.



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### MOTORIZED GEARBOX

These units are as used in a computerized tank, and offer the experimenter in robotics the opportunity to buy the electro-mechanical parts required in building remote controlled vehicles. The unit has 2 x 3V motors, linked by a magnetic clutch, and a gearbox contained within the black ABS housing, reducing the final drive speed to approx 50rpm. Data is supplied with the unit showing various options on driving the motors etc. £5.95. Suitable wheels also available: 79mm Dia plastic with blue tyre, drilled to push-fit on spindle. 2 for £1.30 (limited qty). 75mm dia aluminium disc 3mm thick, drilled to push-fit on spindle. 2 for 68p.

### COMPUTER GAMES

Z901 Can you follow the flashing light/pulsating tone sequence of this famous game? Supplied as a fully working PCB with speaker (no case) plus full instructions. Only £4.95

Z902 Probably the most popular electronic game on the market - based on the old fashioned pencil and paper battleship game, this computerized version has brought it bang up to date! We supply a ready built PCB containing 76477 sound effect chip, TMS1000 micro-processor chip, R's, C's etc. Offered for its component value only (board may be cracked or chipped, it's only £1.95. Instructions and circuit, 30p.

### "THE SENSIBLE 64"

David Highmores new book on the Commodore 64 now available £5.95.

### BULK BUYERS LIST

Send for our latest wholesale list - IC's from 5p, R's £2/1000, transistors 21p, C's 0.8p etc. Bargains galore!!

### PACKS PACKS PACKS

K517 Transistor Pack. 50 assorted full spec marked plastic devices PNP NPN RF AF. Type numbers include BC114, 117, 172, 182, 183, 198, 239, 251, 214, 225, 320, BF198, 255, 394, 2N3904 etc etc. Retail cost £7+. Special low price 275p

K523 Resistor Pack. 1000 - yes, 1000 1/2 and 1/4 watt 5% hi-stab carbon film resistors with pre-formed leads for PCB mounting. Enormous range of preferred values from a few ohms to a several megohms. Only 250p. 5000 £10; 20,000 £36.

K520 Switch Pack. 20 different assorted switches - rocker, slide, push, rotary, toggle, micro etc. Amazing value at only 200p

K522 Copper clad board. All pieces too small for our etching kits. Mostly double sided fibreglass. 250g (approx 110 sq ins) for 100p

### STORE CLEARANCE!!

We've bought so much surplus recently our stores are bulging at the seams! In order to clear some space, we're once again offering "Bargain Parcels" which have proved very popular in the past. They contain resistors, capacitors, switches, panels with transistors and IC's, screws and various hardware + all the odd bits and pieces which have accumulated over the years. Each parcel weighs 10lbs and costs just £8.00.

### TTL PANELS

Panels with assorted TTL inc. LS types. Big variety. 20 chips £1.00; 100 chips £4.00; 1000 chips £30.00.

### RIBBON CABLE

Special purchase of multicoloured 14 way ribbon cable - 40p/metre; 50m £18.00; 100m £32.00; 250m £65.00.

### NICAD CHARGERS

Versatile unit for charging AA, C, D and PP3 batteries. Charge/test switch, LED indicators at each of the 5-charging points. Mains powered. 210 x 100 x 55 mm £7.95.

Model A124. Unit plugs directly into 13A socket, and will charge up to 4 AA cells at a time. Only £4.80.

### NI-CAD BATTERIES

AA size 99p each; C size 199p; D size 220p; PP3 size 395p. SPECIAL!! 6 x D size. For only £11.00.

### PRECISION PCB DRILL

Small size, 35mm dia x 165mm long. 12V operation. Supplied with collet + 1mm bit 6000RPM. Only £7.50.

### 5000 COMPONENTS £25!!

Amazing variety of passive components - carbon, film oxide, wirewound resistors from 1W to 10W, ceramic, polystyrene, polyester and electrolytic capacitors in an extremely wide range of values and types from a few pF to 1000uF!! All parts are brand new, full spec devices. The best value components parcel offer around!! Cost of parts if bought individually would be well over £200!!

### CLOCK CASES

We must clear these to make more room in our store!! This attractive white plastic case with rear panel drilled for switches etc is oval in shape, 130x68x87mm. (no front panel). 4 (yes, four!!) for £1.00!!

### STABILIZED PSU PANEL

A199 A versatile stabilized power supply with both voltage (2-30V) and current (20mA-2A) fully variable. Many uses inc. bench PSU, Ni-cad charger, gen purposes testing Panel ready built, tested and calibrated. £7.75. Suitable transformer and pots, £6.00. Full data supplied.

### PUSH BUTTON BANKS

W4700 An assortment of latching and independent switches on banks from 2 to 7 way, DPCC to 6DPCC. A total of at least 40 switches for £2.95; 100 £6.50; 250 £14.00; 100 £45.00.

### SEAT BELT ALARM

Originally for sale at £8.95, these well made units 70 x 50 x 25mm provide both audible and visual alarms. Uses 2 IC's, PB2720 transducer, etc. Available ready built, with circuit and instructions for just £3.95. Also available as a kit, PCB + all components, box, wire, etc, together with instructions. Only £2.95.

### VEROBLOC £1 OFF!!

Our biggest selling breadboard on offer at a special price of £4.10.

### FERRIC CHLORIDE

New supplies just arrived - 250g bags of granules, easily dissolved in 500ml of water. Only £1.15, 10 for £8, 100 for £60. Also abrasive polishing block 95p.

### 1N5400 3A 50V RECTS

Bulk purchase enables us to offer these at special low prices: 25 £1.50; 100 £4.50; 250 £12; 1000 £43; 5000 £200.

### 5mm RED LED SCOOP!!

Full spec brand new devices at a low, low price!! 25 £1.95; 100 £6.

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5% tolerance from 0.0082 to 0.68uF in 400, 250 or 100V 26 values

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C.333 100Vdc 1.8-4700pF

B.37448 63Vdc 2.5mm PCM

0.068 and 0.1pF

B.37449 63Vdc 5mm PCM

0.68 and 0.1uF

**CERAMIC DISC**

1nF-10nF, 300Vac

**ELECTROLYTIC**

Axial in many from 1 to 10000uF, 10 to 100Vdc

Can in several values from 100 to 22,000uF, 16 to 350V

Reversible from 2 to 100uF

Low Leak, Almmn, 0.1-100uF, 17 values, 6-50Vdc

Radial 15 values up to 63Vdc

**TANTALUM BEADS**

In 18 values from 0.1-100uF, 3 to 35V

**POLYSTYRENE (Siemens)**

39 values 5pF to 18nF, 160Vdc.

The above ranges should meet the majority of current requirements. Mention P.E. when sending for our latest A-Z list showing very many more types.

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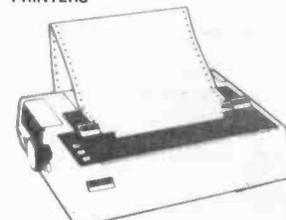
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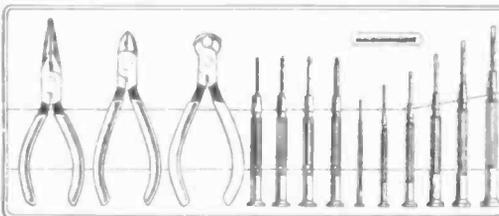
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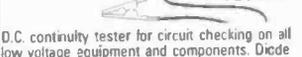
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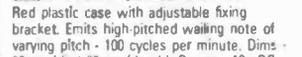
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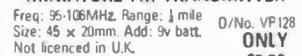
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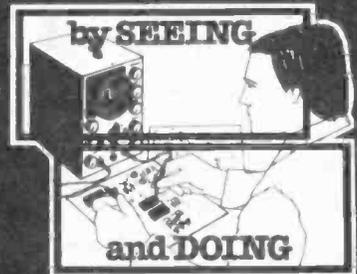
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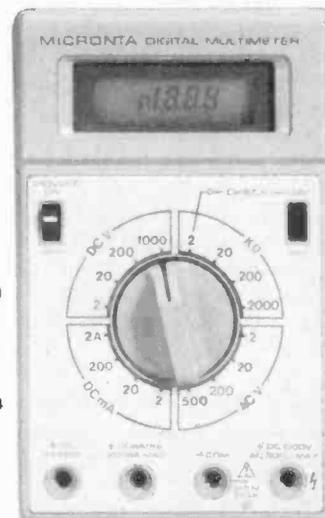
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## GUIDE

THE multimeter buyer's guide in this issue may be an eye opener to many readers. Obviously a number of meters are regularly advertised in our pages and many component suppliers carry a range in their catalogues. However, the sheer range size may come as something of a shock.

Unfortunately many suppliers do not show a great deal of interest in selling to hobbyists. Even though PE can claim a readership made up from pure hobbyists, students, teachers and professionals in the electronics industry of around 200,000 people, many companies remain unaware of the potential. One large international multimeter manufacturer recently announced its intention to enter the hobbyist field with special products but, apart from a press release sent out months ago, appear to have taken no steps to get this fact across to the buying public.

## COMPREHENSIVE

We do not claim that our buyer's guides are comprehensive. What we have attempted to do is take a substantial and representative selection of what is available, in an effort to provide readers with a reasonable choice. Just as one company approached us follow-

ing our *Monitors For Home Computers* guide in the February issue asking how we missed them, we expect multimeter suppliers to come out of the woodwork following this feature to ask why they have not been included. Our answer is simple: You must make us and our readers aware of your products, not expect someone to find your company.

We have attempted to do their marketing job for them and give readers basic information on the products available. Thankfully these comments do not apply to all companies. You will find some multimeter advertisements in this and other issues of PE and we commend these advertisers to you. They obviously want your business and are prepared to do something about it.

Next month we continue this theme in our pages with a look at oscilloscopes, p.s.u.s, function generators and logic probes. We are sorry to say that by the time you read this it will be too late to get any further material in. If your company has been missed may we suggest that you make sure we are aware of your products and PE readers know where to get them in the future!

## SEASONAL

Changing tack slightly may we urge you to make sure you continue to buy

the product you are reading. It is normal for us to start getting requests for back numbers just after the summer months, when some readers have been away and missed an issue, only to find that it contained an important feature or project. While we are pleased to supply back numbers, the quantity available is limited and you pay more for them (see foot of this page). So please save yourself all the hassle by placing an order for a regular copy with your newsagent—they will hold them for you while you lie on the beach in some exotic part of the world. Most newsagents also deliver them when you return, and want to catch up on technological innovations.

Of course, if supply of issues is a regular problem, we can offer you a subscription which will ensure your issue is posted to you every month (details at the foot of the page). Just to keep you interested we are planning features or projects relating to the following subjects during the summer months: photography, hi-fi, test gear, fibre optics, radio astronomy, computing, robotics and alarm systems.



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We are unable to offer any advice on the use or purchase of commercial equipment or the incorporation or modification of designs published in PE. All letters requiring a reply should be accompanied by a stamped, self addressed envelope, or addressed envelope and international reply coupons, and each letter should relate to one published project only.

Components and p.c.b.s are usually available from advertisers; where we anticipate difficulties a source will be suggested.

## Back Numbers and Binders

Copies of most of our recent issues are available from: Post Sales Department (Practical Electronics), IPC Magazines Ltd., Lavington House, 25 Lavington Street, London SE1 0PF, at £1 each including Inland/Overseas p&p. Please state month and year of issue required.

Binders for PE are available from the same address as back numbers at £5.50 each to UK or overseas addresses, including postage, packing and VAT where appropriate. State year and volume required.

## Subscriptions

Copies of Practical Electronics are available by post, inland for £13, overseas for £14 per 12 issues, from: Practical Electronics, Subscription Department, IPC Magazines Ltd., Room 2816, King's Reach Tower, Stamford Street, London SE1 9LS. Cheques, postal orders and international money orders should be made payable to IPC Magazines Limited. Payment for subscriptions can also be made using any credit card and orders placed via Teledata. Tel. 01-200 0200.

Items mentioned are available through normal retail outlets, unless otherwise specified. Prices correct at time of going to press.

# NEWS &

## HEAVY-DUTY CASSETTE

It is estimated that, even at home, a recorder coupled to a computer may go through more cycles of operation in a month than a recorder used only for audio does in a year. Commonsense companionship for a micro with a busy operator comes in the shape of this 'heavy-duty' recorder from Bell and Howell.

Unlike the majority of cassette recorders used for data transferral, the 3179CX is based on a recorder designed specifically for use in schools. The unit is aimed at the BBC machine primarily but is compatible with other personal computers.

The machine incorporates an internal electret microphone and an external microphone socket. Two headphone sockets are provided for private study, as well as a socket for remote control of the drive motor by the computer. In addition to conventional fast-forward and rewind a

'cue and review' mode is incorporated: This allows fast-forward or rewind to be done with the 'play' button depressed so that playback begins immediately the wanted section of the tape has been found.

Other features include auto-stop at both ends of the tape and mains or battery operation. Recording whether computer or audio can be done with either manual or automatic level control. For computers requiring a higher output from the recorder when loading such as the ZX Spectrum, the signal is taken from one of the headphone sockets. From these up to 4V is available from 'volume control' adjustment. The case, mechanism and circuit boards are exceptionally hard wearing and shock resistant.

A full list of micros compatible with the 3179CX is unfortunately not yet available. However, owing to the high output it is expected that most micro users will have little trouble with compatibility. The unit is expected to retail at around £39.95 inc VAT. For further information contact Brian Watkinson, Bell and Howell, Alport House, Bridgewater Road, Wembley, Middx. HA0 1EG. (01-902 8812).



## UK Sales Boom

The buoyancy of electronic equipment production in the UK was reflected in substantially increased demand for semiconductors in 1983, says the Electronic Components Industry Federation.

On the basis of ECIF returns and after fair allowances for the imports and production of others, it is calculated that the 1983 UK market for semiconductors attained a size of £600M, which is equivalent to a growth of 41% over 1982. It has now doubled in size in the last 4 years, with continuous growth throughout the recent recession.

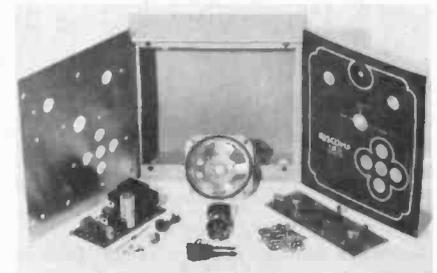
The Federation predicts that 1984 will see a growth of 38% in integrated circuits and 12% in discrete devices.

Beyond this the expectation is for 1985 to see further growth and the UK semiconductor market reaching a size of £1 billion for the first time.

## SONIC-ALARM

New from Riscomp, and complementing their existing range of modular alarm systems, is the 'stand alone' ultrasonic intruder detector kit, the CK 5063.

This unit generates an ear-piercing alarm signal in excess of 110dB when triggered. Although designed as a 'stand alone' unit, an external bell or siren can be connected. Simple soldering and assembly is all that is required along with a mains supply on completion.



The system incorporates digital circuit techniques and provides for three levels of discrimination against false alarms. A built-in exit-delay and fixed alarm time are incorporated as well as a selectable entrance-delay. A 'hold' position on the key-switch allows for 'walk-testing' the area to be protected.

Normally retailing at £42.55 inc VAT this kit is available on special offer in this issue of PE priced £37.95 inc VAT (see page 34).

## DOWN TO EARTH AWARD

A coveted Ideal Home Exhibition 'Blue Ribbon' has been awarded by the Daily Mail to B&R Electrical Products Ltd of Harlow for their unique range of 'PowerBreaker' products designed to prevent death or injury from electrical accidents. Invented and manufactured in Britain, the slim plugs and sockets incorporate an electronic residual current circuit breaker (RCCB) which protects in a way that fuses, miniature circuit breakers or double insulation never can.

The unique RCCB constantly monitors the flow of power to an appliance. If an accident occurs and current starts to flow to earth through a human body or other conductive material, 'PowerBreaker' senses the fault instantly and cuts off the current in a split second—well before accepted danger levels are reached.

Less than ¼ amp can kill or start a fire, but will not blow a fuse; double-insulation becomes ineffective if the cable is cut or an exposed metal part is made live because of



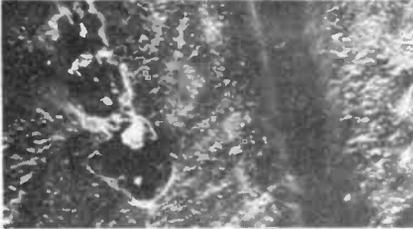
a loose connection. Users of portable electric tools and garden equipment such as electric lawnmowers and hedgecutters are particularly at risk because of the dangers of cut cables, as are users of electrical appliances in kitchens etc.

The 'PowerBreaker' range is available from the usual electrical outlets. The plug has a RRP of £24.15 and the socket £42.97, these prices include VAT. Details from B&R Electrical Products Ltd, Temple Fields, Harlow, Essex CM20 2BG. (0279 34561).

# MARKET PLACE

## ABLATIVE ETCHING

Laser etching, with all its promise in medical and photolithographic applications, suffers from the disadvantage of heating side effects, or charring. The photograph shows this (cut on the left) where a conventional visible infra-red laser was used.



The cut on the right was made using a new technique called ablative photodecomposition, and developed by IBM at its Thomas J. Watson research centre. It is seen how a laser can be made to cut biological or polymeric substances without heating up the surrounding material. The breakthrough takes advantage of a phenomenon of far-ultraviolet laser, which features an intensity threshold that, if exceeded, will eject molecules from the area, taking with them excess energy that would otherwise have been absorbed by the surrounding material (hence the term 'ablative').

In biological and dental applications, un-



precedented accuracy can be achieved because the geometry of the cut is controlled entirely by the shape of the light beam.

The lower photograph shows a scanning electron micrograph of commercial plastic film etched to a line width of five microns, demonstrating the technique's potential in the photolithographic fabrication of integrated circuits.



In recent weeks the PE office has received several suppliers' catalogues which may be of interest to readers:

**Greenweld's Components and Equipment Catalogue** (84 pages), the post-paid price of £1 is redeemable with a discount voucher against subsequent purchases, 70p to callers at: 443 Millbrook Road, Southampton SO1 0HX (0703 772501).

**Marshall's Component and Equipment Catalogue** (56 pages), costs 75p to callers or £1 post-paid (UK) £1.50 (Rest of World) from: 85 West Regent Street, Glasgow G2 2QD (041-332 4133).

**Marco Trading's Components and Equipment Catalogue** (109 pages), costs 65p post-paid and 65p to callers. A 30p discount voucher (included) is redeemable against subsequent purchases from: The Maltings, High Street, Wem, Shropshire SY4 5EN (0939-32763).

**Joe Distributions' Components and Equipment Catalogue** (48 pages) is free and can be obtained by sending a large s.a.e. to, or calling at: 43 Strathville Road, London SW18 4QX (01-870 0075). A counter-service is also available from: 267 Hanworth Road, Hounslow, Middx.

**Semiconductor Supplies International Components Catalogue** (178 pages) is free and can be obtained by sending a large s.a.e. to, or calling at: Dawson House, 128/130 Carshalton Road, Sutton, Surrey SM1 4RS (01-643 1126).

**Supercat Electronics' Test and Measuring Equipment Catalogue** (36 pages) is free and can be obtained by sending a large s.a.e. to: PO Box 201, St Albans, Herts AL1 4EN (0727-621711).

## Silicon News Corner

**Motorola** ♦ Introduces dual-chip, ultrafast rectifiers in TO-220 package to replace two axial lead 3A devices which normally require hand soldering to a heatsink. These switchmode rectifiers are MUR605CT, MUR610CT, MUR615CT & MUR620CT.

♦ 100MHz infrared fibre-optic emitters MFOE1201 & MFOE1202.

♦ Four new r.f. power TMOS f.e.t. transistors for low band linear applications, are MRF148, MRF150 @ 30W & 150W respectively, and MRF138, MRF140 @ 30W & 150W respectively, the former being 50V, the latter, 28V.

♦ Optocoupler/7500V isolator requiring only 1mA input, is MOC8100.

♦ New series of high speed, single supply, quad op amps known as the MC34074 series run from 3 to 44V ( $\pm 1.5$  to  $\pm 22V$ ). Bipolar. 4.5MHz gain bandwidth product.

♦ New dual port memory unit (8-bit HCMOS) is MC68HC34.

♦ 3A voltage regulator series in voltages from 5V-24V, with up to 2% o/p voltage tolerance (A suffix) is MC78T00 series.

Motorola European Literature Centre, 88 Tanners Drive, Blakelands, Milton Keynes.

## Countdown . . .

Please check dates before setting out, as we cannot guarantee the accuracy of the information presented below. Note: some exhibitions may be trade only. If you are organising any electrical/electronics, radio or scientific event, big or small, we shall be glad to include it here. Address details to Mike Abbott.

**Life** (Fire protection) April 9-13. Olympia. S  
**Laboratory** April 11-12. New Century Hall, Manchester. E  
**Tectronica** April 16-18. Earls Court, London. T  
**Fibre Optics** May 1-3. Porter Tun Room, Whitbread Brewery. E  
**All Electronics/ECIF** May 1-3. Barbican, London. E  
**Biotech Europe** May 15-17. Wembley Conf. Cntr., London. O  
**DEC user** May 15-17. Cunard Int. Hotel, Hammersmith, London Q1  
**Micro City** May 15-17. Exhibition Complex, Bristol. F3  
**Scotex** June 5-7. Royal Highland Exhibition Halls, Ingliston, Edinburgh. O5  
**IBM System User Show** June 12-14. Wembley Conf. Cntr., London. O  
**Qualx** June 19-21. Corn Exchange, Brighton. D4

**Surface Treatment & Finishing Show** June 25-29. Birmingham. M  
**Leeds Electronics** July 3-5. University. E  
**Networks** July 3-5. Wembley Conf. Cntr., London. O  
**Cable** July 10-12. Wembley Conf. Cntr., London. O  
**Laboratory** Sept. 4-6. Barbican, London. E  
**Testmex** Sept. 11-13. Grosvenor Ho. Pk. Lane, London. E  
**Personal Computer World Show** Sept. 19-23. Olympia 2, London. M  
**Building & Home Improvement** Sept. 25-30. Earls Court, London. M  
**Computer Graphics** Oct. 9-11. Wembley Conf. Cntr., London. O  
**Software Expo** Oct. 16-18. Wembley Conf. Cntr., London. O  
**Drives, Motors & Controls** Oct. 24-26. Harrogate Exhibition Cntr. E  
**Computers In The City** Nov. 20-22. Barbican, London. O  
**Data Security** Nov. 20-22. Barbican, London. O

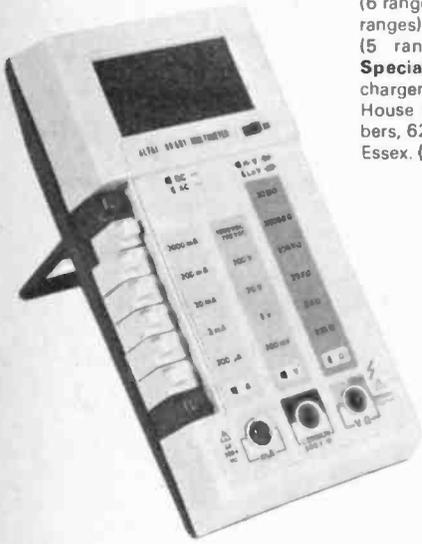
D4 Network ☎ 0280 815226  
E Evan Steadman ☎ 0799 26699  
F3 Tomorrow's World ☎ 0272 292156  
M Montbuild ☎ 01-486 1951  
O Online ☎ 01-868 4466  
O5 Institute of Electronics ☎ 0706 43661  
Q1 ☎ 01-242 8697  
S IFSSEC ☎ 01-387 5050  
T Trident ☎ 0822 4671



**Model:** BBC MA5D. **Ranges:** Voltage a.c./d.c. 300mV–1000V (5 ranges). Current a.c./d.c. 300 $\mu$ A–20A (6 ranges). Resistance 3k $\Omega$ –20M $\Omega$  (5 ranges). Capacitance 300nF–3000 $\mu$ F (5 ranges). Decibels (5 ranges). **Special Features:** Built-in battery charger. **Price:** £265.00. **Supplier:** House of Instruments, Clifton Chambers, 62 High Street, Saffron Walden, Essex. (0799 24922).



**Model:** Hung Chang HM101. **Ranges:** Voltage d.c. 10V–1000V (4 ranges). Voltage a.c. 10V–1000V (4 ranges). Current d.c. 0–100mA (1 range). Resistance 0–1M $\Omega$  (2 ranges). Decibel range. **Price:** £8.60. **Model:** HM102. **Ranges:** Voltage d.c. 250mV–1000V (8 ranges). Voltage a.c. 10V–1000V (5 ranges). Current d.c. 50 $\mu$ A–500mA (5 ranges). Resistance 0–6M $\Omega$  (4 ranges). Decibel range. **Price:** £13.22. **Supplier:** House of Instruments, Clifton Chambers, 62 High Street, Saffron Walden, Essex. (0799 24922).



**Model:** DD601 (YK32K). **Ranges:** Voltage d.c. 200mV–1000V (5 ranges). Voltage a.c. 200mV–750V (5 ranges). Current d.c. 200 $\mu$ A–2A (5 ranges). Current a.c. 200 $\mu$ A–2A (5 ranges). Resistance 200 $\Omega$ –20M $\Omega$  (6 ranges). **Special Features:** Diode test facility. **Price:** £42.50. **Supplier:** Maplin Electronic Supplies, PO Box 3, Rayleigh, Essex. (0702 554155).

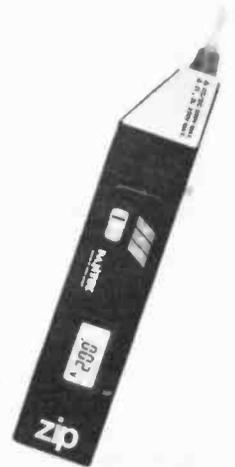
# MULTIMETERS buyer's guide

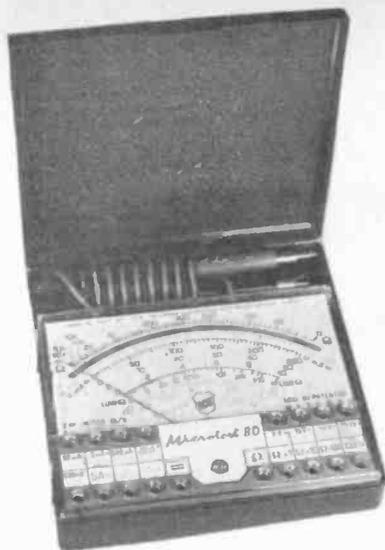
A multimeter is one of the most essential pieces of test equipment for the hobbyist. This buyer's guide has been designed to show you a selection of the meters currently available. Although it cannot cover all the models it should at least put you on the right road to the type of meter you require. Please note all the prices are inclusive of VAT but not p&p. Only one supplier is listed for each meter but many of the models are available from more than one source.



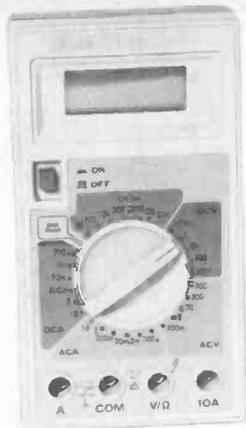
**Model:** Philips PM2544. **Ranges:** Voltage d.c. 0–1000V (4 ranges). Voltage a.c. 0–1000V (4 ranges). Current d.c. 0–10A (2 ranges). Current a.c. 0–10A (2 ranges). Resistance 0–10M $\Omega$  (5 ranges). **Special Features:** The PM2544 is also a signature analyser and timer/counter. **Price:** £983.25. **Supplier:** Pye Unicam Ltd., Sales Dept., York Street, Cambridge. (0223 358866).

**Model:** Pantec Zip. **Ranges:** Voltage a.c./d.c. 2V–500V (4 ranges). Resistance 2k $\Omega$ –2M $\Omega$  (4 ranges). **Special Features:** Auto-ranging. Direct entry probe allows one-handed operation. **Supplier:** Pantec, Carlo Gavazzi (UK) Ltd., 162–164 Upper Richmond Road, Putney, London. (01-785 9022).





**Model:** Microtest 80 (YB84F). **Ranges:** Voltage d.c. 0-1V-1000V (6 ranges). Voltage a.c. 1-5V-1000V (5 ranges). Current d.c. 50 $\mu$ A-5A (5 ranges). Current a.c. 250 $\mu$ A-2.5A (5 ranges). Resistance 500 $\Omega$ -5M $\Omega$  (5 ranges). Capacitance 1 $\mu$ F-25000 $\mu$ F (4 ranges). Decibels (5 ranges). **Price:** £27.00. **Supplier:** Maplin Electronic Supplies, PO Box 3, Rayleigh, Essex. (0702 554155).



**Model:** Metex 3000. **Ranges:** Voltage d.c. 200mV-1000V (5 ranges). Voltage a.c. 200mV-700V (5 ranges). Current d.c. 200 $\mu$ A-10A (6 ranges). Current a.c. 200 $\mu$ A-10A (6 ranges). Resistance 200 $\Omega$ -20M $\Omega$  (6 ranges). **Special Features:** Diode test facility and zero check. **Price:** £32.77. **Supplier:** House of Instruments. (0799 24922).



**Model:** Avometer 1001. **Ranges:** Voltage d.c. 240mV-1000V (7 ranges). Voltage a.c. 10V-1000V (5 ranges). Current d.c. 0-1mA-1A (5 ranges). Resistance 5 $\Omega$ -2M $\Omega$  (2 ranges). **Price:** £32.77. **Supplier:** House of Instruments.



**Model:** BBC M2012. **Ranges:** Voltage d.c. 200mV-650V (5 ranges). Voltage a.c. 200mV-650V (5 ranges). Current d.c. 2mA-2A (4 ranges). Current a.c. 2mA-2A (4 ranges). Resistance 2k $\Omega$ -20M $\Omega$  (5 ranges). **Price:** £102.92. **Supplier:** House of Instruments. (0799 24922).



**Model:** Pantec Dolomiti. **Ranges:** Voltage d.c. 150mV-1.5kV (9 ranges). Voltage a.c. 5V-1.5V (6 ranges). Current d.c. 50 $\mu$ A-5A (6 ranges). Current a.c. 5mA-5A (4 ranges). Resistance 500 $\Omega$ -50M $\Omega$  (6 ranges). Decibels (6 ranges). **Special Features:** Universal signal injector. **Price:** £57.61. **Supplier:** Alcon Instruments Ltd., 19 Mulberry Walk, London SW3 6DZ. (01-352 1897).



**Model:** DME1400. **Ranges:** Voltage a.c./d.c. 200mV-1000V. Current a.c./d.c. 200mA-1A. Resistance 200 $\Omega$ -20M $\Omega$ . **Special Features:** Autoranging or manual selection, low resistance 'bleeper' and sample hold function. **Price:** £270.25. **Supplier:** Telonic Instruments Ltd., 2 Castle Hill Terrace, Maidenhead, Berkshire. (0628 73933).



**Model:** Avometer Model 8 Mk 5. **Ranges:** Voltage d.c. 100mV-3000V (9 ranges). Voltage a.c. 3V-3000V (8 ranges). Current d.c. 50 $\mu$ A-10A (7 ranges). Current a.c. 10mA-10A (4 ranges). Resistance 2k $\Omega$ -20M $\Omega$  (3 ranges). Decibel range. **Special Features:** Automatic cut out. **Price:** £145.00. **Supplier:** House of Instruments. (0799 24922).



**Model:** YK375. **Ranges:** Voltage d.c. 0-25V-1000V (6 ranges). Voltage a.c. 10V-1000V (4 ranges). Current d.c. 25 $\mu$ A-10A (10 ranges). Resistance 2k $\Omega$ -20M $\Omega$  (5 ranges). Decibels (8 ranges). **Special Features:** Range doubler facility which enables readings to be taken at lower ranges. **Price:** £19.95. **Supplier:** Maplin Electronic Supplies, PO Box 3, Rayleigh, Essex. (0702 554155).

**Model:** BBC MA3E. **Ranges:** Voltage a.c./d.c. 100mV-1000V (9 ranges). Current a.c./d.c. 10 $\mu$ A-10A (7 ranges). Resistance 1 $\Omega$ -20M $\Omega$  (5 ranges). Decibels (9 ranges). **Price:** £112.20. **Supplier:** House of Instruments, Clifton Chambers, 62 High Street, Saffron Walden, Essex. (0799 24922).



**AVO 1001 £29.90**  
U.K. price only

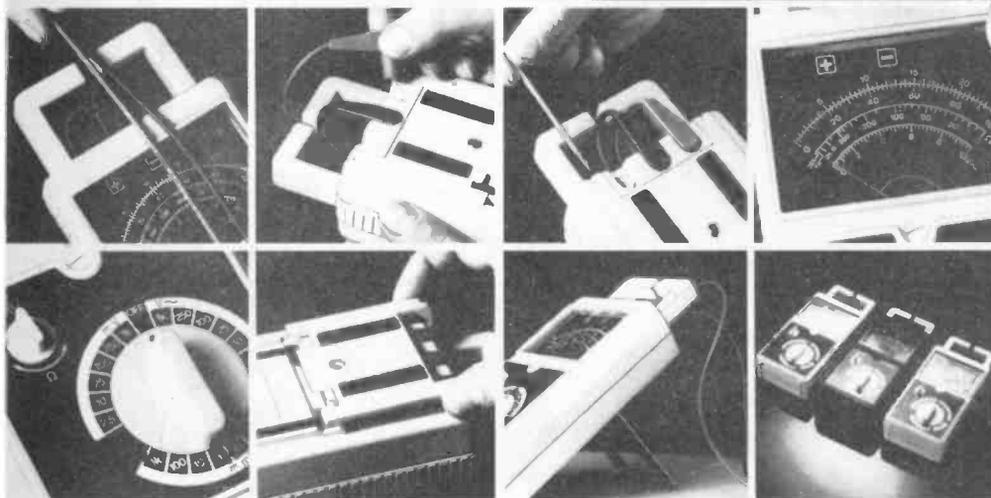
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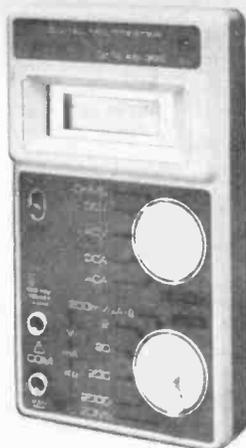
**THORN EMI Instruments Limited**

Archcliffe Road, Dover, Kent CT17 9EN. Telephone: 0304 202620. Telex: 96283

# MULTIMETERS buyer's guide



**Model:** Hitachi VR3525. **Ranges:** Voltage d.c. 200mV–1000V (5 ranges). Voltage a.c. 200mV–750V (4 ranges). Current a.c./d.c. 200 $\mu$ A–10A (5 ranges). Resistance 200 $\Omega$ –20M $\Omega$ . **Special Features:** Autoranging. Diode test. Continuity. Temp. –20°C to +700°C. **Price:** £120.75. **Supplier:** Reltech Instruments, New Road, St. Ives, Huntingdon, Cambridgeshire PE17 4BG. (0480 63570).



**Model:** ALT/AI KD30C. **Ranges:** Voltage d.c. 0–1000V (5 ranges). Voltage a.c. 0–700V (5 ranges). Current a.c./d.c. 0–1A (5 ranges). Resistance 0–20M $\Omega$  (6 ranges). **Price:** £37.95. **Supplier:** Semiconductor Supplies International Ltd., Dawson House, 128/130 Carshalton Road, Sutton, Surrey SM1 4RS. (01-643 1126).



**Model:** ALT/AI KD305. **Ranges:** Voltage d.c. 0–1000V (4 ranges). Voltage a.c. 0–750V (2 ranges). Current d.c. 0–10A (4 ranges). Resistance 0–2M $\Omega$  (4 ranges). **Price:** £32.20. **Supplier:** Semiconductor Supplies International Ltd., Dawson House, 128/130 Carshalton Road, Sutton, Surrey SM1 4RS. (01-643 1126).



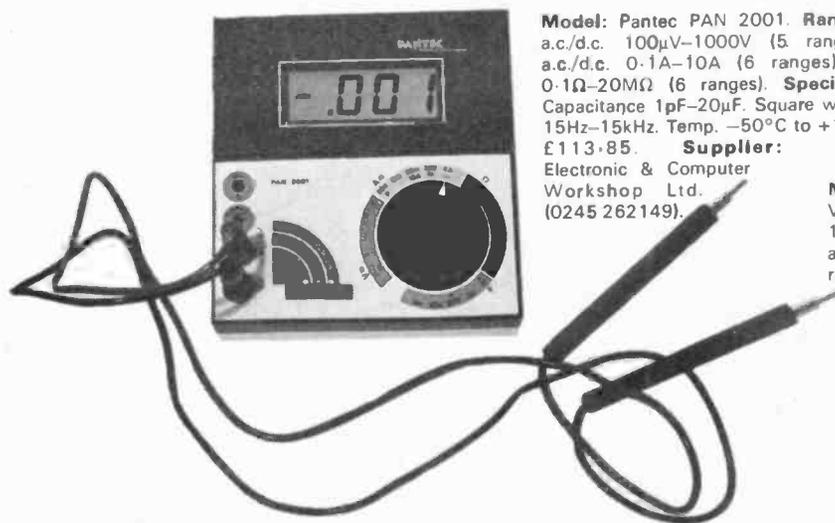
**Model:** Fluke JF73. **Ranges:** Voltage d.c. 0–1000V. Voltage a.c. 0–750V. Current d.c. 0–10A. Current a.c. 0–10A. Resistance 0–32M $\Omega$ . **Special Features:** Digital and analogue. Autoranging. **Price:** £74.75. **Supplier:** Electroplan Ltd., PO Box 19, Orchard Road, Royston, Herts SG8 5HH. (0763 41171).



**Model:** Miselco Electro Super. **Ranges:** Voltage a.c./d.c. 100mV–1000V (9 ranges). Current a.c./d.c. 100 $\mu$ A–6A (8 ranges). Resistance 0–1M $\Omega$  (3 ranges). **Special Features:** dB scale. **Price:** £56.00. **Supplier:** Alcon Instruments Ltd., 19 Mulberry Walk, London SW3 6DZ. (01-352 1897).



**Model:** Fluke 8026B. **Ranges:** Voltage d.c. 200mV–1000V. Voltage a.c. 200mV–750V. Current a.c. 2mA–2A. Resistance 200 $\Omega$ –20M $\Omega$ . **Special Features:** Diode test. Conductance: 2ms–200ns. **Price:** £207.00. **Supplier:** Electroplan Ltd., PO Box 19, Orchard Road, Royston, Herts SG8 5HH. (0763 41171).



**Model:** Pantec PAN 2001. **Ranges:** Voltage a.c./d.c. 100 $\mu$ V–1000V (5 ranges). Current a.c./d.c. 0.1A–10A (6 ranges). Resistance 0.1 $\Omega$ –20M $\Omega$  (6 ranges). **Special Features:** Capacitance 1pF–20 $\mu$ F. Square wave generator 15Hz–15kHz. Temp. –50°C to +150°C. **Price:** £113.85. **Supplier:** Electronic & Computer Workshop Ltd. (0245 262149).

**Model:** AVO 2001. **Ranges:** Voltage a.c./d.c. 200mV–1000V (5 ranges). Current a.c./d.c. 200nA–10A (6 ranges). Resistance 200 $\Omega$ –20M $\Omega$  (6 ranges). **Special Features:** Continuity. Diode test. **Price:** £98.21. **Supplier:** House of Instruments, Clifton Chambers, 62 High Street, Saffron Walden, Essex. (0799 24922).



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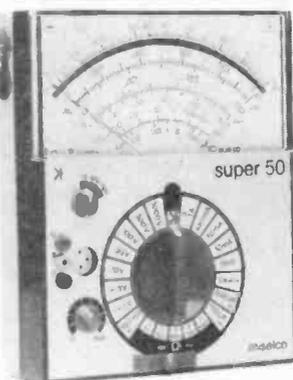
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**Model:** ISI DM3350. **Ranges:** Voltage d.c. 0-1000V (4 ranges). Voltage a.c. 0-600V (4 ranges). Current a.c./d.c. 0-10A (2 ranges). Resistance 0-2M $\Omega$  (5 ranges). **Special Features:** Autoranging, Continuity. **Price:** £51.75. **Supplier:** Semiconductor Supplies International Ltd., Dawson House, 128/130 Carshalton Road, Sutton, Surrey SM1 4RS. (01-643 1126).



**Model:** Beckman T90. **Ranges:** Voltage d.c. 200mV-1000V (5 ranges). Voltage a.c. 0-600V (2 ranges). Current d.c. 200 $\mu$ A-2A (5 ranges). Resistance 200 $\Omega$ -20M $\Omega$  (6 ranges). **Special Features:** Diode test. **Price:** £49.96. **Supplier:** Beckman Instruments Ltd., Mylen House, 11 Wagon Lane, Sheldon, Birmingham B26 3DU. (021-742 7761).



**Model:** Anders AMM301. **Ranges:** Voltage d.c. 60mV-300V (7 ranges). Voltage a.c. 6V-600V (5 ranges). Current d.c. 0.03mA-600mA (4 ranges). Resistance 0-2M $\Omega$  (4 ranges). **Special Features:** dB scale. **Price:** £29.33. **Supplier:** Anders Electronics Ltd., 48-56 Bayham Place, Bayham Street, London NW1 0EU. (01-387 9092).



**Model:** Beckman HD100. **Ranges:** Voltage d.c. 200mV-1500V (5 ranges). Voltage a.c. 200mV-1000V (5 ranges). Current a.c./d.c. 200 $\mu$ A-2A (5 ranges). Resistance 200 $\Omega$ -20M $\Omega$  (6 ranges). **Price:** £132.25. **Supplier:** ITT. (0279 29522).



**Model:** ALT/AI KD25C. **Ranges:** Voltage d.c. 0-1000V (4 ranges). Voltage a.c. 0-500V (2 ranges). Current d.c. 0-200mA (2 ranges). Resistance 0-2M $\Omega$  (4 ranges). **Price:** £27.60. **Supplier:** Semiconductor Supplies International Ltd., Dawson House, 128/130 Carshalton Road, Sutton, Surrey SM1 4RS. (01-643 1126).

**Model:** Hitachi VR3510. **Ranges:** Voltage d.c. 200mV-1000V (5 ranges). Voltage a.c. 2000mV-750V (4 ranges). Current a.c./d.c. 200 $\mu$ A-10A (5 ranges). Resistance 200 $\Omega$ -20M $\Omega$  (6 ranges). **Special Features:** Autoranging. More accurate than VR3525. Continuity. Diode test. Temp. -20°C to +700°C. **Price:** £155.25. **Supplier:** Reltech Instruments, New Road, St. Ives, Huntingdon, Cambridge PE17 4BG. (0480 63570).



**Model:** Soar ME-531. **Ranges:** Voltage d.c. 200mV-1000V (5 ranges). Voltage a.c. 2V-1000V (4 ranges). Current d.c. 200mA-10A (2 ranges). Current a.c. 200mA-10A (2 ranges). Resistance 200 $\Omega$ -2M $\Omega$  (5 ranges). **Special Features:** Autoranging. Continuity. Diode tester. **Price:** £56.20. **Supplier:** Maplin Electronic Supplies, PO Box 3, Rayleigh, Essex SS6 8LR. (0702 554155).

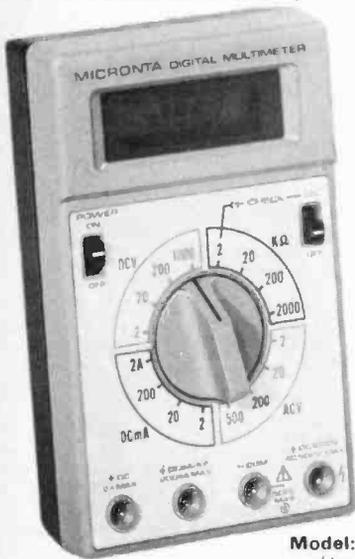
**Model:** Keithley 175. **Ranges:** Voltage d.c. 200mV-1000V (5 ranges). Voltage a.c. 200mV-750V (3 ranges). Current d.c. 200 $\mu$ A-10A (6 ranges). Current a.c. 200 $\mu$ A-10A (6 ranges). Resistance 200 $\Omega$ -200M $\Omega$  (7 ranges). **Special Features:** Autoranging.  $\mu$ P operated with memory (100 readings). IEEE bus. **Price:** £396.75. **Supplier:** Keithley Instruments Ltd., 1 Boulton Road, Reading, Berkshire RG2 0NL. (0734 861287).



# MULTIMETERS buyer's guide



**Model:** Keithley 179A. **Ranges:** Voltage d.c. 200mV–1200V (5 ranges). Voltage a.c. 200mV–1000V (5 ranges). Current a.c./d.c. 200µA–20A (6 ranges). Resistance 0–20MΩ (5 ranges). **Special Features:** Hi-lo range option, over-range indication. **Price:** £385. **Supplier:** Keithley Instruments Ltd, 1 Boulton Road, Reading, Berks RG2 0NL. (0734 861287).



**Model:** Micronta (Tandy). **Ranges:** Voltage a.c./d.c. 2V–1000V (4 ranges). Current a.c./d.c. 2mA–2A (4 ranges). Resistance 0–2kΩ (4 ranges). **Special Features:** Diode test facility, overload protection. **Price:** £34.95. **Supplier:** Tandy stockists.

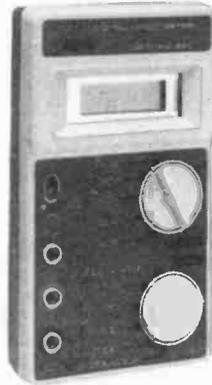


**Model:** Thandar TM451. **Ranges:** Voltage a.c./d.c. 200mV–1000V (5 ranges). Current a.c./d.c. 200mA–1A (2 ranges). Resistance 0–20MΩ (6 ranges). **Special Features:** Optional auto-ranging, diode test. **Price:** £184. **Supplier:** Thandar Electronics. (0480 64646).



**Model:** Lascar LMM/100 (LH95D). **Ranges:** Voltage a.c./d.c. 0.1mV–1000V (5 ranges). Current a.c./d.c. 0.1µA–2A (5 ranges). Resistance 0–20MΩ (5 ranges). **Special Features:** Overload protection, display 'hold'. **Price:** £88.61. **Supplier:** Maplin Electronic Supplies Ltd., P.O. Box 3, Rayleigh, Essex SS6 8LR. (0702 552911).

**Model:** ALT/AI KD55C. **Ranges:** Voltage d.c. 200mV–1000V (5 ranges). Voltage a.c. 200mV–700V (5 ranges). Current a.c./d.c. 200µA–10A (6 ranges). Resistance 0–20MΩ (6 ranges). **Special Features:** Overload indication. **Price:** £43. **Supplier:** Semiconductor Supplies International, Dawson House, 128/130 Carshalton Road, Sutton, Surrey. (01-643 1126).



**Model:** ALT/AI KD615. **Ranges:** Voltage d.c. 200mV–1000V (5 ranges). Voltage a.c. 0–750V (2 ranges). Current d.c. 200µA–10A. Resistance 0–20MΩ (6 ranges). **Special Features:** Overload protection, diode test facility. **Price:** £42.55. **Supplier:** Semiconductor Supplies International, 128/130 Carshalton Road, Sutton, Surrey. (01-643 1126).



**Model:** Miselco T20 'Super'. **Ranges:** Voltage d.c. 100mV–1000V (8 ranges). Voltage a.c. 0V–1000V (5 ranges). Current d.c. 50µA–10A (10 ranges). Current a.c./d.c. 3mA–10A (6 ranges). Resistance 0–50MΩ (5 ranges). Decibels –10 to +61 (5 ranges). **Special Features:** Diode test facility, overload protection. **Price:** £42.25. **Supplier:** Alcon Instruments Ltd., 19 Mulberry Walk, London SW3 6DZ. (01-352 1897).



**Model:** Thandar TM354. **Ranges:** Voltage d.c. 2V–1000V (4 ranges). Voltage a.c. 0–500V (2 ranges). Current d.c. 2mA–200mA (4 ranges). Resistance 0–2MΩ (4 ranges). **Special Features:** Diode test facility. **Price:** £45.95. **Supplier:** Thandar Electronics Ltd, London Road, St Ives, Huntingdon, Cambs. PE17 4HJ. (0480 64646).

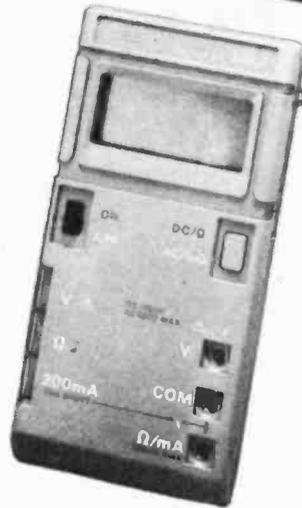




**Model:** Miselco 'Super' 50. **Ranges:** Voltage d.c. 150mV-1000V (8 ranges). Voltage a.c. 0-1000V (5 ranges). Current d.c. 20 $\mu$ A-3A (10 ranges). Current a.c. 3mA-3A (6 ranges). Resistance 0-50M $\Omega$  (5 ranges). Decibels -10 to +61 (5 ranges). **Special Features:** Diode test facility. **Price:** £50. **Supplier:** Alcon Instruments Ltd., 19 Mulberry Walk, London SW3 6DZ. (01-352 1897).



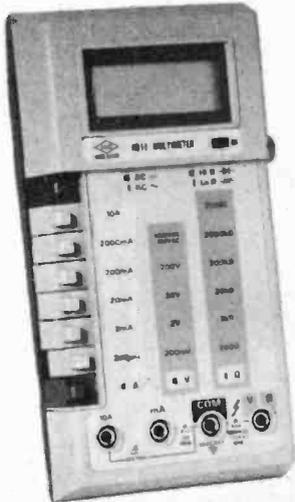
**Model:** Thandar TM356. **Ranges:** Voltage d.c. 200mV-1000V (5 ranges). Voltage a.c. 200mV-750V (5 ranges). Current d.c. 200 $\mu$ A-10A (6 ranges). Resistance 0-20M $\Omega$  (6 ranges). **Special Features:** Diode test facility. **Price:** £109.25. **Supplier:** Thandar Electronics Ltd, London Road, St Ives, Huntingdon, Cambs. PE17 4HJ. (0480 64646).



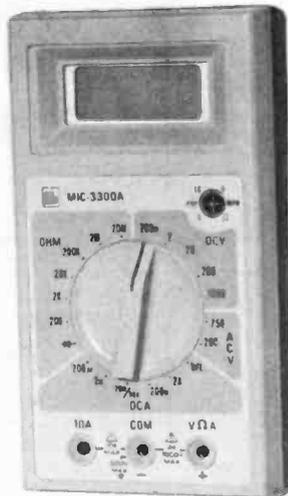
**Model:** DM 2350C. **Ranges:** Voltage d.c. 0.2V-1000V. Voltage a.c. 2V-600V. Current a.c./d.c. 200mA-20A. Resistance 0-2M $\Omega$ . **Special Features:** Auto-ranging, continuity 'buzzer'. **Price:** £67.85. **Supplier:** Semiconductor Supplies International Ltd., Dawson House, 128/130 Carshalton Rd., Sutton, Surrey SM1 4RS (01-643 0829).



**Model:** Levell TM11. **Ranges:** Voltage d.c. 150 $\mu$ V-50kV (18 ranges). Voltage a.c. 50 $\mu$ V-50kV (19 ranges). Current d.c. 150pA-50A (24 ranges). Current a.c. 50pA-50A (25 ranges). Resistance 0-10G $\Omega$  (7 ranges). Decibels -90 to +50 (15 ranges). **Special Features:** Diode test, temp. sensor (7 ranges), amp output. **Price:** £189.75. **Supplier:** Levell Electronics Ltd., Moxon St., Barnet, Herts. EN5 5SD (01-440 8686).



**Model:** Hung-Chang HC7030. **Ranges:** Voltage a.c./d.c. 100 $\mu$ V-1000V (5 ranges). Current a.c./d.c. 0.1 $\mu$ A-10A (6 ranges). Resistance 0-20M $\Omega$  (6 ranges). **Special Features:** Diode test facility, overload protection. **Price:** £49.95. **Supplier:** Ambit International, 200 North Service Road, Brentwood, Essex CM14 4SG. (0277 230909).



**Model:** MIC-3300A. **Ranges:** Voltage d.c. 200mV-1000V (5 ranges). Voltage a.c. 0V-750V (2 ranges). Current d.c. 200 $\mu$ A-10A (5 ranges). Resistance 0-20M $\Omega$  (6 ranges). **Special Features:** Diode test facility. **Price:** £48.30. **Supplier:** House of Instruments, Clifton Chambers, 62 High Street, Saffron Walden, Essex CB10 1EE. (0799 24922).



**Model:** Fluke '73'. **Ranges:** Voltage d.c. 320mV-1000V. Voltage a.c. 3.2V-750V. Current a.c./d.c. 32mA-10A. Resistance 0-32M $\Omega$ . **Special Features:** Auto-ranging, diode test facility, additional linear display feature. **Price:** £74.75. **Supplier:** Electroplan Ltd., P.O. Box 19, Orchard Rd., Royston, Herts. SG8 5HH. (0763 41171).



**Model:** Trio DL-705. **Ranges:** Voltage a.c./d.c. 1mV-1000V. Resistance 0-20M $\Omega$ . Current a.c./d.c. 10 $\mu$ A-200mA. **Special Features:** Hi-lo range option, semi-auto-ranging. **Price:** £123.91. **Supplier:** Supercat Electronics Ltd., P.O. Box 201, St Albans, Herts. (0727 62171).

# 66

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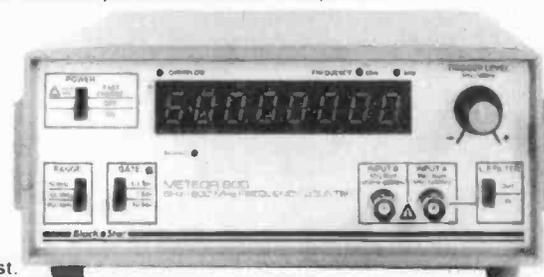
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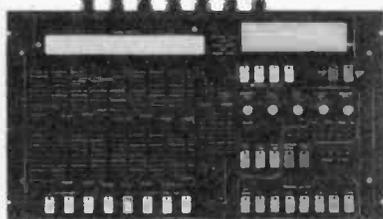
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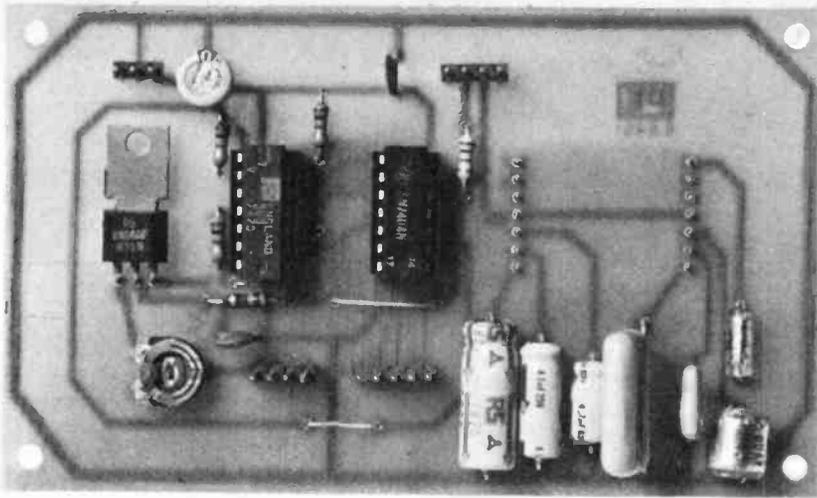
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# LOGIC SIGNAL GENERATOR

THIS month's Digital Project is devoted to the construction of a versatile signal source which will be invaluable for use in testing and fault diagnosis of digital circuits. The Logic Signal Generator provides four outputs which are fully TTL compatible. These consist of complementary square wave signals at both the nominal frequency ( $f$ ) and at twice this value ( $2f$ ). A fifth, variable amplitude, output of 1V peak maximum is also available. This output has a nominal 50 ohm impedance and is ideal for applications such as the calibration and general testing of both analogue and digital circuits.

The Logic Signal Generator unit uses low-cost readily available components and is assembled on a small single-sided p.c.b. As with all of the projects in this series, power for the Logic Signal Generator is derived from the separate regulated d.c. supply module which was described in the March issue of PE.

## CIRCUIT DESCRIPTION

The complete circuit of the Logic Signal Generator is shown in Fig. 1. A Schmitt inverter, IC1f, forms a simple square wave oscillator where the frequency of operation is governed by switch selected capacitors, C1 to C7, together with the series combination of VR1 and R1. The capacitor values are selected to produce seven decade frequency ranges, and VR1 provides a continuously variable adjustment of the output frequency over a range of a little more than 10:1, thus ensuring a small overlap between switched ranges.

It should be noted that, although the output of this simple form of TTL oscillator has acceptably fast rise and fall times, the mark to space ratio is typically around 1:3. For most applications it is desirable to achieve as near unity a mark to space ratio as possible. In the Logic Signal Generator this is achieved by applying the oscillator output to an edge clocked bistable stage. Such a stage reacts solely to either the falling or the rising edge of its clock input, depending upon the particular i.c., and thus will generate a near perfect square wave regardless of the duty cycle of its input.

The oscillator output is buffered by means of IC1e and then taken to the JK bistable, IC2a, arranged as a binary divider with both J and K inputs taken to logic 1. The output of IC2a thus consists of a square wave of near unity mark to space ratio at exactly half the frequency of its clock input. Complementary outputs, Q and  $\bar{Q}$ , are taken to inverters, IC1b and IC1a, respectively. These gates act as buffers and help to minimise effects associated with loading at the output. A second bistable stage, IC2b, follows the first. This further divides the signal frequency to provide complementary outputs via IC1c and IC1d.

The  $\bar{Q}$  output from IC2b is applied to the source follower stage, TR1. This provides a low impedance output which is adjustable in amplitude by means of variable and pre-set resistors, VR2 and VR3 respectively. Distributed supply decoupling is provided at h.f. by means of C8 and C9 and at l.f. by means of C10.

## SPECIFICATION

### GENERAL

Waveform:	Square, unity mark to space ratio.
Frequency:	Seven switched ranges covering:—
1	0.3Hz to 3Hz
2	3Hz to 30Hz
3	30Hz to 300Hz
4	300Hz to 3kHz
5	3kHz to 30kHz
6	30kHz to 300kHz
7	300kHz to 3MHz appx.

### TTL OUTPUTS

Four fully TTL compatible outputs:  $f_{out}$ ,  $\bar{f}_{out}$ ,  $2f_{out}$ , and  $2\bar{f}_{out}$ .

### VARIABLE OUTPUT

Single output at  $f_{out}$  continuously variable in amplitude to 1V peak maximum.  
 Output impedance nominally 50 ohm.

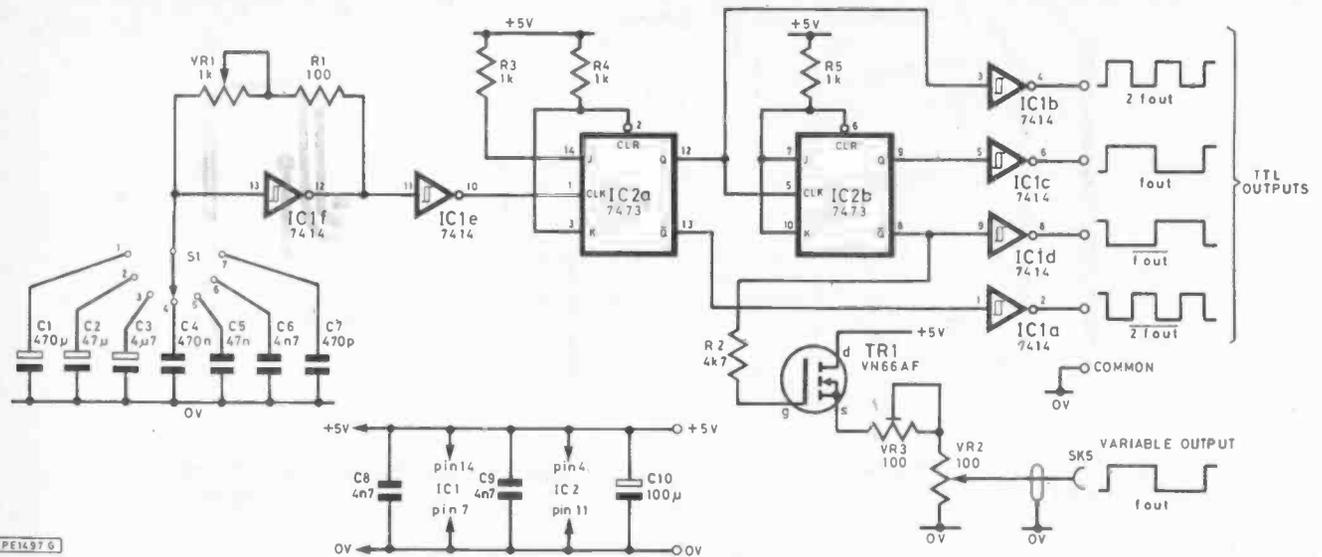


Fig. 1. Circuit diagram of the Logic Signal Generator

## CONSTRUCTION

The Logic Signal Generator is built on a single-sided p.c.b. measuring approximately 120 x 70mm, the copper foil layout of which is shown in Fig. 2. The corresponding com-

ponent layout on the top surface of the p.c.b. is shown in Fig. 3. Interconnections from the p.c.b. to the output sockets, potentiometers and power supply are all made via 0.1" matrix p.c.b. connectors, the wiring scheme for which is shown in Fig. 4.

Components should be assembled on the p.c.b. in the following sequence: d.i.l. sockets, p.c.b. connectors, links, resistors, capacitors, f.e.t., and rotary switch. Note that, unlike all of the other components, this last mentioned item is mounted on the copper track side of the p.c.b. Once assembly has been completed the underside of the p.c.b. should be carefully checked for solder splashes, bridges bet-

## COMPONENTS . . .

### Resistors

R1	100
R2	4k7
R3,R4,R5	1k (3 off)
VR1	1k carbon potentiometer
VR2	100 carbon potentiometer
VR3	100 miniature horizontal skeleton pre-set
All resistors 0.25W 5% carbon	

### Capacitors

C1	470µ 10V elect
C2	47µ 25V elect
C3	4µ7 63V elect
C4	470n polyester
C5	47n polyester
C6	4n7 polystyrene
C7	470p polystyrene
C8,C9	4n7 ceramic (2 off)
C10	100µ 16V PC elect

### Semiconductors

TR1	VN66AF
IC1	7414
IC2	7473

### Miscellaneous

- P.c.b.
- 14-pin d.i.l. sockets (2 off)
- 3-way 0.1" p.c.b. plug and socket
- 4-way 0.1" p.c.b. plug and socket (2 off)
- 5-way 0.1" p.c.b. plug and socket
- 1P 7W p.c. mounting rotary switch
- 2mm sockets (5 off; 4 red, 1 black)
- BNC socket

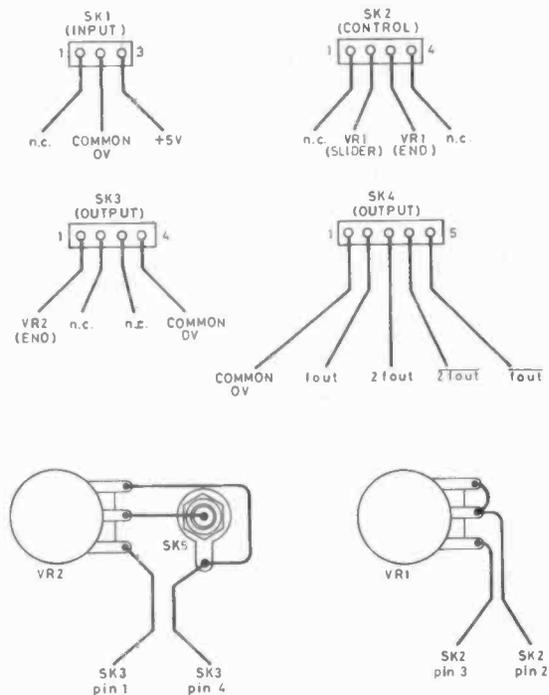


Fig. 4. Wiring interconnections

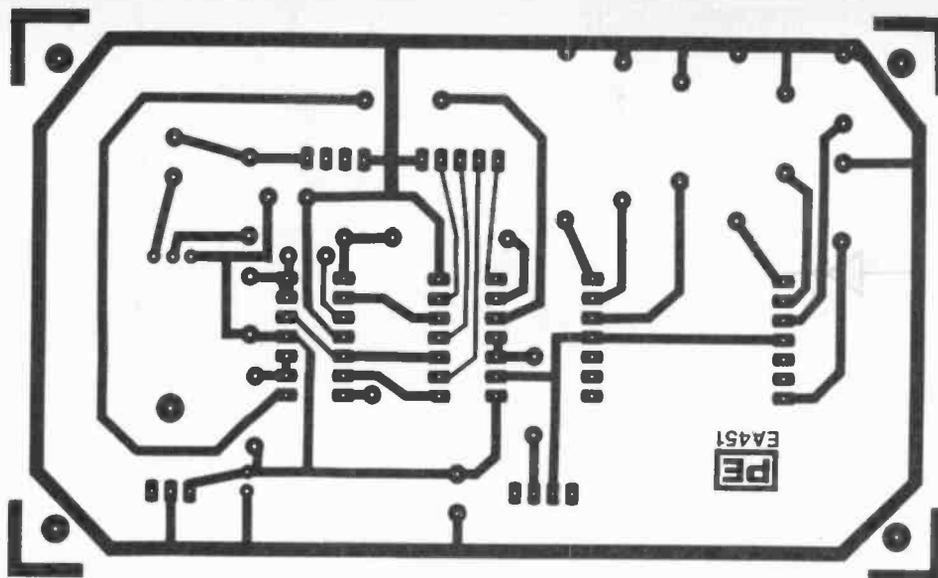


Fig. 2. P.c.b. design

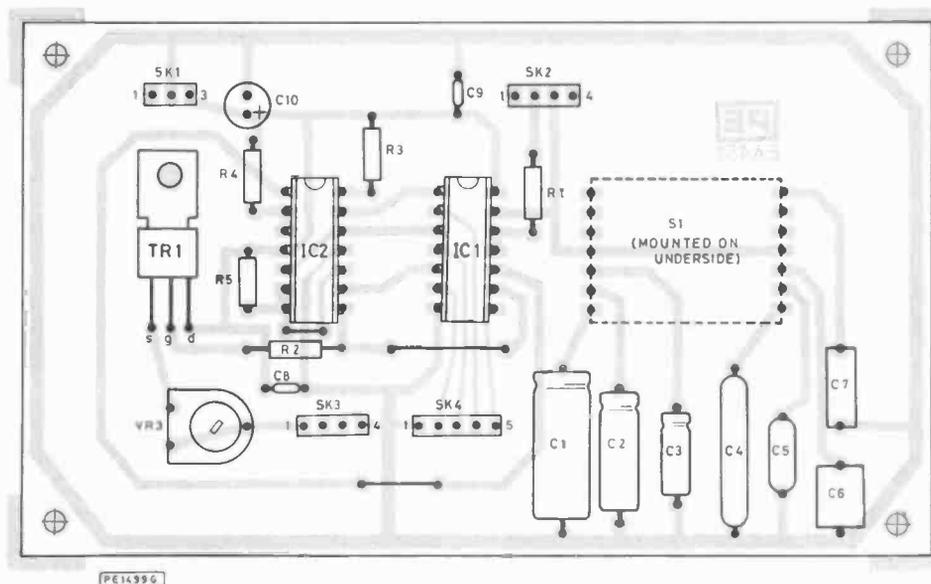


Fig. 3. Component layout

ween adjacent tracks, and dry joints. Finally, the i.c.s may be inserted in their respective holders, taking care to ensure the correct orientation of each device. Constructional details of the enclosure and off-board wiring have not been given since this will undoubtedly be a matter of preference for the individual constructor. Constructional details of a suitable power supply module were given in the March issue of PE.

### TESTING AND CALIBRATION

Two commonly available items of test equipment are required in order to fully test and calibrate the Logic Signal Generator. These are an oscilloscope (preferably a dual beam type) and a digital frequency meter. Calibration should initially be carried out with the unit switched to range 4 (300Hz to 3kHz), VR1 set to maximum (fully anti-clockwise). The Y1 input of the oscilloscope should be connected to dis-

play  $f_{out}$  and the timebase should be adjusted to display two to four cycles of this waveform. The Y2 input should then be connected to each of the other TTL outputs in turn, and the correct frequency and phase relationship should be checked by reference to the Y1 display. The amplitude of each of the TTL outputs should also be checked and this should be in the range 3.5V to 4.5V.

The oscilloscope Y2 input should now be connected to the variable output and VR3 adjusted until the amplitude of output signal is exactly 1V. Finally, the digital frequency meter should be connected to the variable output and VR1 adjusted for a reading of exactly 1kHz. The scale fitted to VR1 should then be marked appropriately at this and at other suitably chosen frequencies. This completes the testing and calibration of the Logic Signal Generator and the unit is now ready for use. ★



# sustain unit

R.A. Penfold



THE popular sustain effect for electric guitars is obtained using a form of compressor. Units of this type have fast attack and decay times so that they can respond with suitable rapidity to changes in the dynamic level of the signal from the guitar, and the compression characteristic gives an almost constant output level. This retains the fast attack each time a note is played, but the normal decay characteristic is eliminated, and a virtually constant volume level is maintained for the duration of each note. As a result, the normal, almost percussive sound of an electric guitar is modified to give a sound which is more like that of an organ.

Sustain units can be rather more complex than one might expect, and can have problems with noise levels. The noise results from the high gain that must be used to maintain the output at a suitable level once the input signal has substantially decayed. The gain (and noise) are at a maximum when there is little or no input signal, which, unfortunately, is when the noise is most noticeable.

This design is based on just one active device, and good noise performance is obtained by including a noise gate at the output. A useful additional feature is the ability to produce a good fuzz effect using the unit.

## NE571

The integrated circuit used in the unit is an NE571. This device is primarily intended for noise reduction systems where one section is configured as a 2 to 1 compressor and the other is used as a 2 to 1 expander. A straightforward 2 to 1 compression characteristic would give a reasonable sustain effect, but would be less than ideal. With this type of compressor any change in the input signal level gives only half as much change in the output level. For example, boosting the input signal by 20dB (10 times) would give a rise in the output level of only 10dB (about 3 times). This greatly restricts the dynamic range of the output signal, but ideally a sustain unit should give an almost constant output level from any input signal of adequate strength, and an effective dynamic range of only a few dBs.

The block diagram of Fig. 1a shows the standard NE571 compressor configuration.  $R_a$  to  $R_d$  are bias and feedback resistors, but due to the inclusion of decoupling capacitor  $C_c$

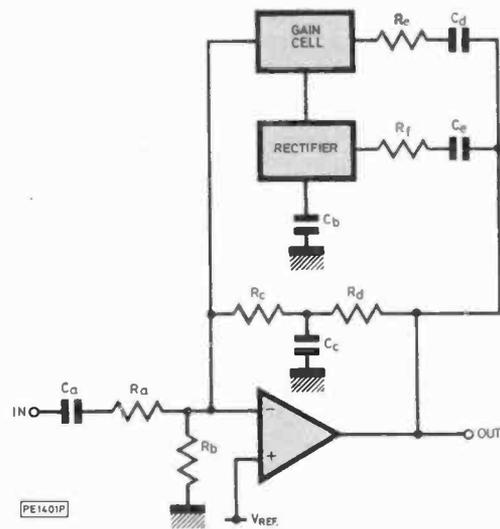


Fig. 1a. The normal NE571 compressor configuration

there is no negative feedback at audio frequencies, and the operational amplifier exhibits its full open loop voltage gain. However, there is a second feedback path through  $C_d$ ,  $R_e$ , and the gain cell. The latter is a form of voltage controlled resistor, and the greater the control voltage it receives, the lower its resistance. The control voltage is provided by the rectifier circuit, and this is driven from the output of the circuit.

Therefore, as the input signal is increased, the output level rises, giving increased control voltage to the gain block, which in turn provides more negative feedback. This feedback reduces the voltage gain of the amplifier, so that the rise in output level is limited, and the required compression is obtained.

There is an alternative form of compressor, and it is possible to reconfigure the NE571N to perform in this alternative mode. The block diagram of Fig. 1b shows this arrangement.

This is in most respects the same as the original set-up, and the only difference is that the rectifier circuit is driven from the input, not from the output. Previously, the output level of the circuit had to increase by a certain amount if there was a rise in input level, as some rise in output level was needed in order to increase the control voltage to the gain block and give a reduction in gain.

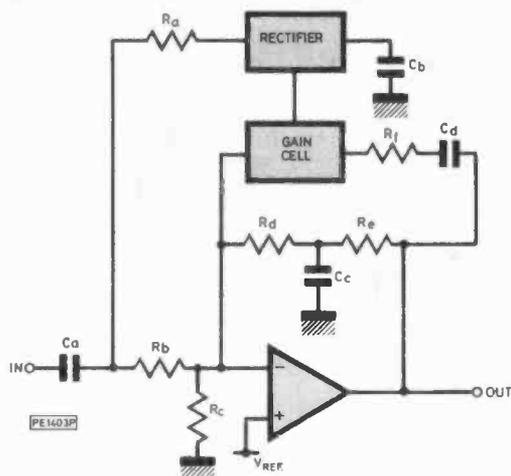


Fig. 1b. The compressor arrangement used in this design

With the second configuration this is not the case. An increase in the input amplitude reduces the gain of the amplifier, and the compression effect is independent of the output level. Low input levels have no significant effect on the gain block as the control voltage that is generated is too small, but above a certain threshold level a rise in input level causes a reduction in gain that stabilises the output at a constant level. In practice, there tends to be some variation in the output amplitude, but this can be kept to no more than a few dBs with careful circuit design, and the NE571N works well in this configuration.

## EXPANDER

The NE571N can operate as an expander using the arrangement shown in Fig. 1c. Here the gain of the amplifier is determined by the negative feedback network which is formed by  $R_a$ , the gain cell, and  $R_d$ . The lower the resistance of the gain cell, the higher the circuit gain.

The rectifier is driven from the input of the circuit, and the higher the input level becomes, the larger the control voltage and gain of the amplifier. This gives the 2 to 1 expansion characteristic.

In theory, using an expander of this type at the output of the circuit would give a high level of noise reduction without impairing the sustain effect. With only the noise output from the sustain circuit there would be only a low input level to the expander, and it would consequently have a low level of gain. In fact, it would provide considerably less than unity

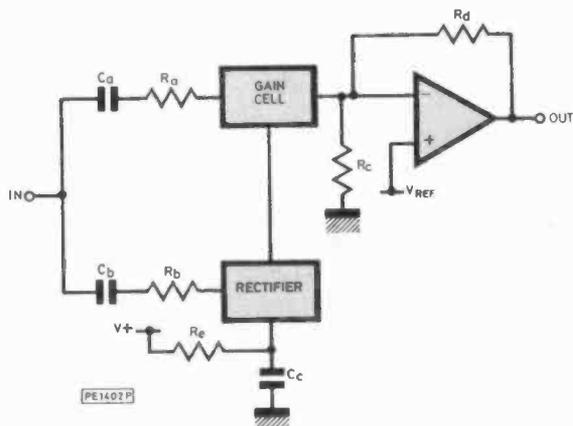


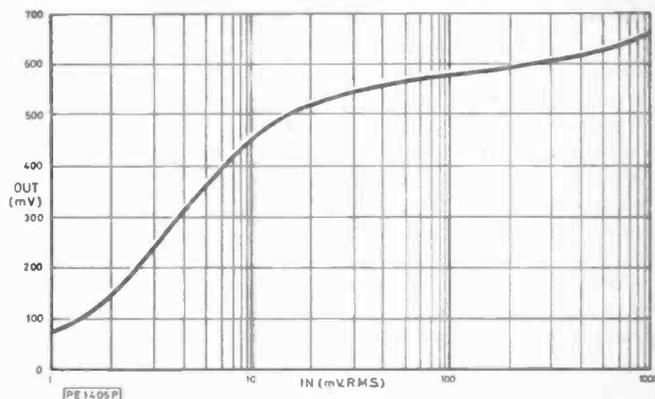
Fig. 1c. The NE571 as an expander

gain, and the noise would be attenuated. With a reasonably high signal level applied to the input of the sustain circuit, a high output level is produced, and the expander therefore has a comparatively high level of gain, so that the signal from the sustain circuit receives a degree of amplification.

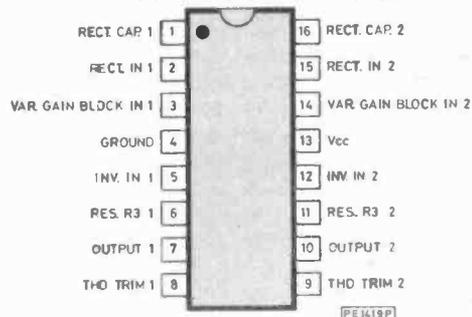
As stated earlier, in practice there is a small variation in the output level of the compressor as the input signal is increased above the compression threshold level. The expander would tend to exaggerate these variations and reduce performance. This problem can be overcome by using a less extreme expansion characteristic, but one which still gives sufficient expansion to give a useful degree of noise reduction. Resistor  $R_e$  provides a bias to the gain block which boosts the minimum gain of the circuit and gives a reduced amount of expansion. Strictly speaking, the circuit is an expander rather than a noise gate, as it does not simply gate the input signal on and off, but an expander used in this single-ended noise reduction role is often referred to as a noise gate.

A typical input/output characteristic of the sustain unit is shown in Fig. 2. As can be seen from this, a 40dB increase in the input signal (10mV to 1V) is compressed to a change in output of only about 3 to 4dB.

Fig. 2. Typical input/output characteristic of the sustain unit



## The NE571 pin connections



## THE CIRCUIT

The full circuit diagram of the unit is shown in Fig. 3, IC1a is used in the compressor/sustain circuit and the expander/noise gate is based on IC1b. These closely adhere to the configurations of Fig. 1b and Fig. 1c, but some of the resistors shown in these diagrams are integral components of IC1 and do not appear in Fig. 3.

Switch S1 is a (foot operated) bypass switch which enables the effect to be easily switched out. Switch S2 can be used to switch out the smoothing capacitor in the rectifier circuit of the compressor so that the input signal modulates itself. This produces severe distortion that gives quite a good

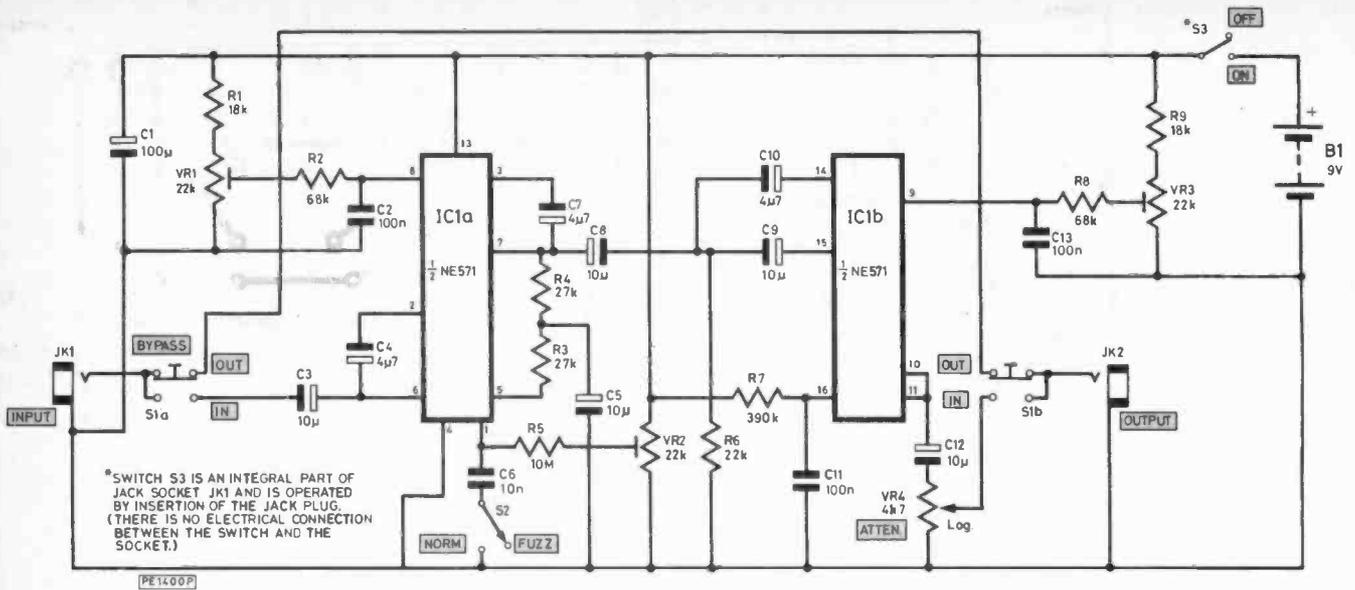


Fig. 3. The complete circuit diagram of the sustain unit

"fuzz" effect. The attack and decay times of the circuit need to be short, due to the rapid changes in the dynamic level of the input signal, but smoothing capacitors C6 and C11 must not be made too small or distortion performance suffers. It is, therefore, a matter of choosing values which give a good compromise between response time and distortion levels.

Potentiometer VR1 and its associated components enable the distortion performance of the compressor to be trimmed for optimum; VR3 is the distortion trim control for the expander. The gain of the circuit might be excessive for some guitars, and VR2 enables the gain of the compressor to be reduced by supplying a bias to the gain block; VR4 is the output level control.

Power is obtained from a small (PP3 size) 9 volt battery, and the current consumption is typically only about 3.5 milliamps. Switch S3 is the on/off switch, and this can be a set of isolated make contacts on the input socket, JK1.

### CONSTRUCTION

A diecast aluminium box is ideal as the housing for a guitar effects unit, as boxes of this type provide screening against electrical noise and are very tough. Bear in mind that bypass switch S1 is a heavy-duty push-button type that is foot or toe operated, and that a simple folded aluminium box might not be able to take the sort of stresses to which the unit will inevitably be subjected. A 150 by 80 by 50mm diecast aluminium box was used as the case for the prototype.

The two controls and two sockets are mounted on the front panel of the unit, which is one of the 150 by 50mm sides of the case. With effects units it is common for the on/off switch to be part of the input jack, so that the unit is automatically switched on and off when the guitar is plugged into the unit and disconnected from it. This is usually very convenient in use, but an ordinary jack socket and separate on/off switch can obviously be used if preferred. A jack socket having isolated d.p.d.t. contacts is specified for JK1 merely because a socket having a single make contact does not seem to be available. No connections are made to most of JK1's tags.

Details of the printed circuit board are shown in Fig. 4. The NE571 is not one of the cheapest integrated circuits, therefore it is advisable to use a (16 pin) d.i.l. i.c. socket for this component. Fit Veropins to the board at the places

## COMPONENTS ...

### Resistors

R1, 9	18k (2 off)
R2, 8	68k (2 off)
R3, 4	27k (2 off)
R5	10M
R6	22k
R7	390k
VR1, 2, 3	22k min skeleton pre-set (3 off)
VR4	4k7 log carbon
All fixed resistors are 0.25W 5% carbon	

### Capacitors

C1	100µ 10V axial elect
C2, 13	100n ceramic (2 off)
C3, 5, 8, 12	10µ 25V radial elect (4 off)
C4, 10	4µ7 63V axial elect (2 off)
C6	10n polyester
C7	4µ7 63V radial elect
C9	10µ 25V axial elect
C11	100n polyester

### Semiconductors

IC1	NE571
-----	-------

### Miscellaneous

S1	d.p.d.t. heavy-duty press-button switch
S2	Rotary on/off type switch
S3	Part of JK1
JK1	Standard jack socket with isolated d.p.d.t. contacts
JK2	Standard jack socket
B1	9 volt PP3 size

Diecast aluminium box, 150 x 80 x 50mm; printed circuit board; PP3 battery connector; two control knobs; Veropins; 16 pin d.i.l. IC socket; wire, etc.

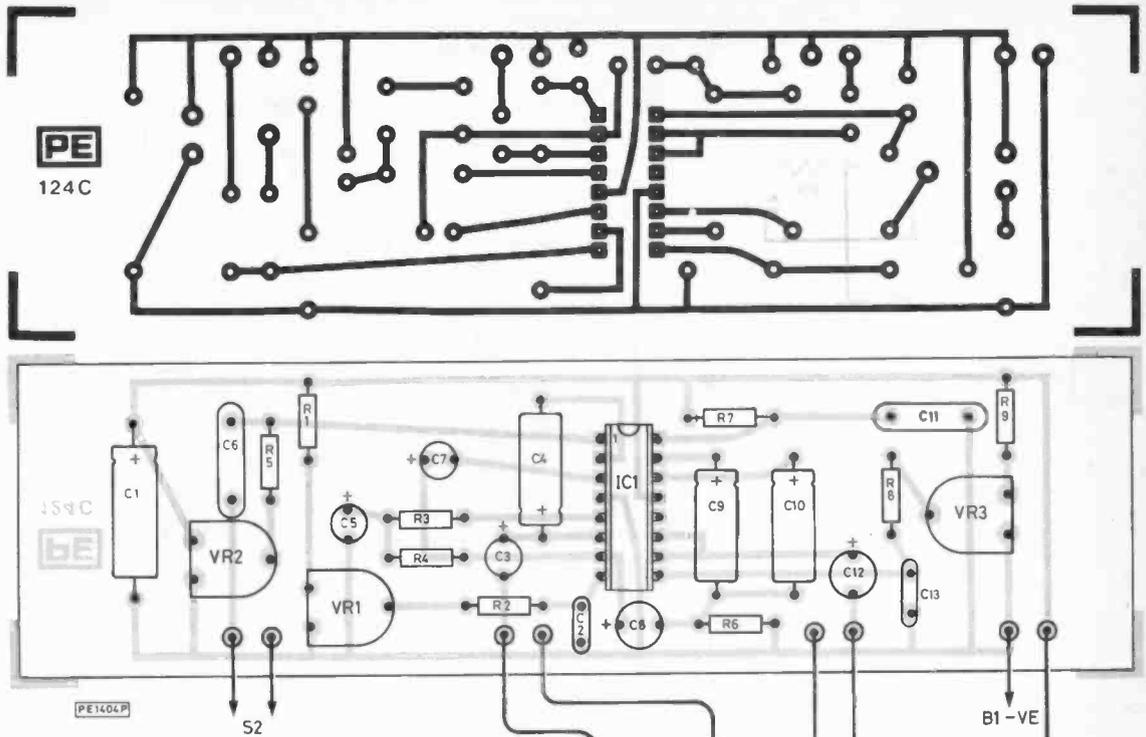


Fig. 4. Printed circuit board layout and wiring

where connections to the off-board components will be made. Once the board and wiring have been completed, the printed circuit is mounted in the case, and it simply slides into the set of guide-rails nearest the rear of the unit. There is plenty of space for the battery to one side of S1. It is advisable to fit a set of cabinet feet to the unit so that it does not slide around when S1 is operated.

#### ADJUSTMENT AND USE

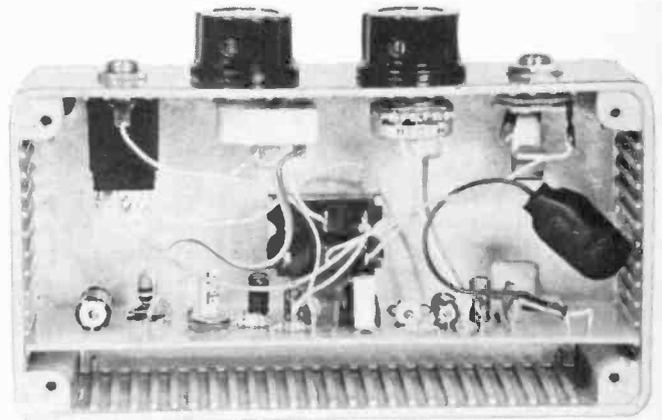
The guitar is connected to JK1 using a standard screened jack lead, and the output from JK2 is coupled to the guitar amplifier in the same way. Initially, all three preset potentiometers should be adjusted to a roughly mid-way setting. Using S1, it should then be possible to switch the sustain effect in and out, and with the effect switched in it should be possible to adjust the output level using VR4; this is adjusted so that the general volume obtained is much the same at both settings of S1. It is possible that a very high output guitar pick-up might give a slightly higher output than the sustain unit can provide, and the volume control of the guitar would then have to be backed-off slightly.

Potentiometers VR1 and VR3 are adjusted empirically to obtain optimum distortion performance. It is not essential to use sophisticated test equipment when doing this, and these presets can simply be adjusted to minimise audible distortion on the output. It is much easier to do this using a reasonably pure sinewave input rather than the signal from a guitar, but obviously any settings that give satisfactory results in practice can be used.

If the unit is used with a high output guitar, results will probably be better if VR2 is adjusted in an anti-clockwise direction. This reduces the gain of the circuit, which is otherwise almost certain to be excessive. A low output guitar will probably necessitate adjustment of VR2 in a clockwise direction to give a boost in gain. Otherwise, only a weak sustain effect is likely to be obtained. Really it is just

a matter of using trial and error to find the setting which gives the best subjective results.

A point which has to be borne in mind when using any sustain unit is that it effectively boosts the gain of the guitar amplifier when the output of the guitar is at a low level. This increases the risk of problems with stray feedback, pick up of mains hum, etc., although in this case the built-in noise gate helps to minimise the risk of such problems. ★



# AUDIO SIGNAL GENERATOR



Sine, triangular and square waves  
Digital readout  
Sweep ranging  
Mains powered

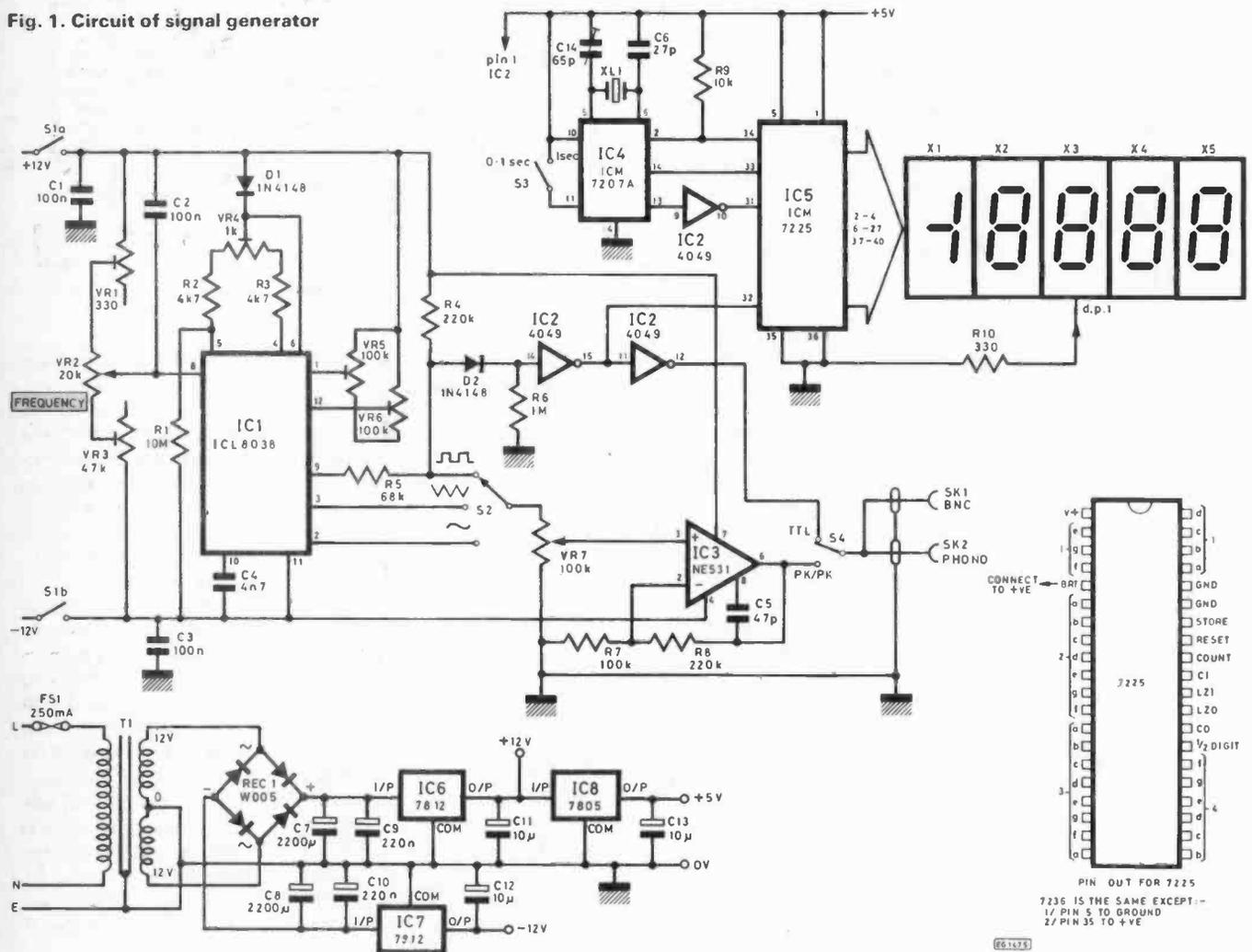
**STEPHEN IBBS**

THIS design provides gain control of sine, triangle and square waves via an op-amp buffer. It has a TTL output for logic applications, and gives digital readout accurate to  $\pm 1\text{Hz}$ . No switched ranges are used, the potentiometer giving a 1000:1 sweep range, and for this reason a multiturn pot is specified to enable accurate settings to be made easily. The unit is mains-powered, giving  $\pm 12\text{V}$  and  $+5\text{V}$ .

## HOW IT WORKS

The heart of the signal generator is the ICL8038 voltage controlled oscillator with the following excellent features: low frequency drift with temperature, low distortion and high linearity, wide operating range (possible 0.001Hz to 300kHz), variable duty cycle from 2%–98% etc. The three waveforms are available simultaneously at pins 2, 3 and 9.

Fig. 1. Circuit of signal generator



## COMPONENTS . . .

### Resistors

R1	10M
R2,3	4k7
R4,8	220k
R5	68k
R6	1M
R7	100k
R9	10k
R10	330
All 1/4W 10% carbon	

### Semiconductors

IC1	ICL8038
IC2	4049
IC3	NE531
IC4	ICM7207A
IC5	ICM7225
IC6	7812
IC7	7912
IC8	7805
D1,2	1N4148
REC1	W005

### Potentiometers

VR1	330 min preset
VR2	20k multturn lin
VR3	47k min preset
VR4	1k min preset
VR5,6	100k min preset
VR7	100k lin (with S1)

### Capacitors

C1-3	100n
C4	4n7 mica
C5	47p
C6	27p
C7,8	2200µ 25V elect
C9,10	0.22µ 25V tant
C11-13	10µ 15V tant
C14	5-65p trimmer

### Miscellaneous

- S1—D.p.s.t.
- S2—3 way rotary
- S3—S.p.d.t.
- S4—S.p.s.t.
- XL1—5.24288MHz crystal
- FS1—250mA fuse and holder
- SK1—BNC socket
- SK2—Phono socket
- Display bezel
- 5-digit CA multiplexed display (GL9R03)
- Centurion DX1 case
- T1—0-12V, 0-12V 3VA p.c.b. mounting transformer

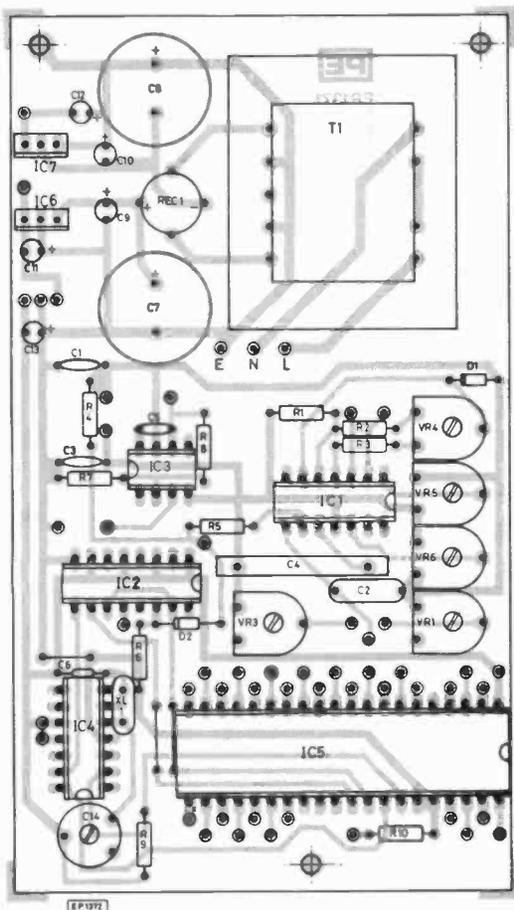


Fig. 2. Main board assembly

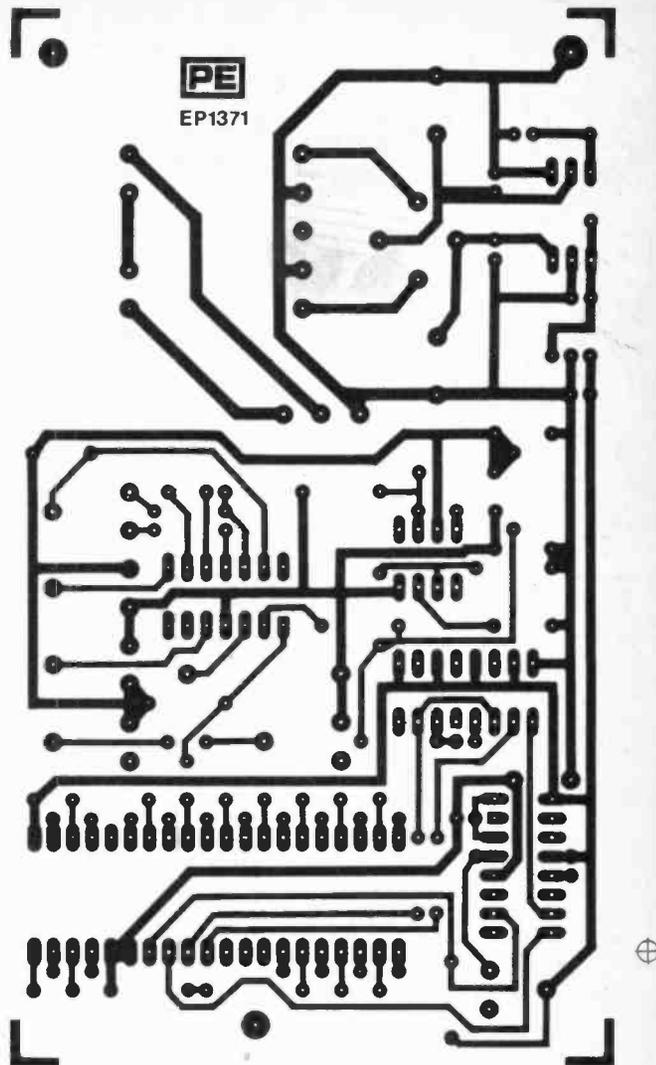


Fig. 3. Printed circuit of main board

The symmetry of the waveform can be affected by the external resistors on pins 4 and 5, and those readers who would like to vary the duty cycle to produce, e.g. short pulses or sawtooth waveforms, may like to experiment with these components. The frequency of the generator is a direct function of the voltage on pin 8, so by varying the potential divider formed by VR1, VR2, VR3, it is possible to obtain a 1000:1 sweep (i.e. 20-20,000Hz with the values selected). The presets are used to set the top and bottom limits. However, to obtain this sweep the voltage across R2 and R3 must decrease to nearly zero. This requires the highest voltage on pin 8 to exceed that at the top of R2 and R3 by a few hundred millivolts, and so D1 is included to lower the effective supply to the 8038. IC3 is included as an output buffer, and provides gain control by means of the potential divider at pin 3. The two presets on pins 1 and 12 minimise sine wave distortion, and according to the Intersil data it should be possible to reduce the distortion to 0.5% by adjusting these.

A split power supply is used because it enables all the waveforms to move symmetrically about 0V. The square wave is not committed, and so R4 is used as a load resistor. This output is also linked to two inverting gates of the 4049 which, being powered from the 5V line, gives a TTL compatible square wave signal available at the output terminals, and is used for the digital display.

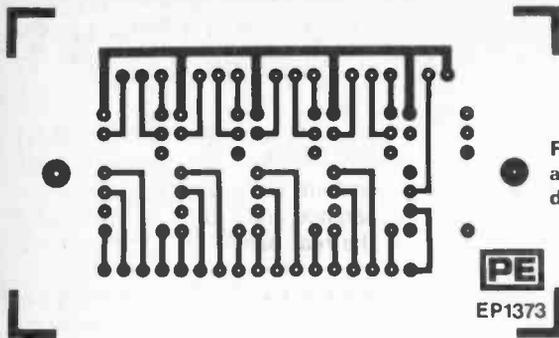
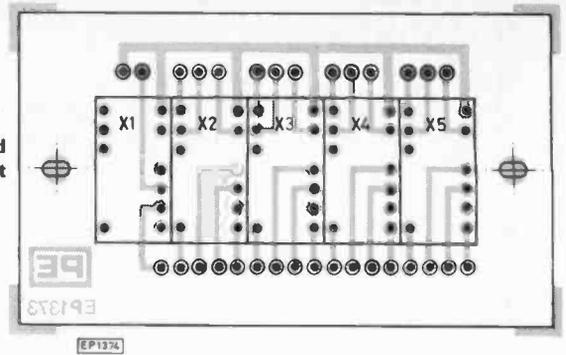


Fig. 4. Etched board and assembly of 5 digit display



An ICM7225 is used, being the simplest means of providing frequency readout. It drives a 4½ digit CA display direct, with the CA line to 5V, but needs its store, reset, and gating pulses in a specific sequence, and this is done by IC4, an ICM7207A designed for just such a purpose. This gives a 1s gate (0·1s if pin 11 is connected to 5V) to give readings of Hertz, and IC2 inverts the count inhibit output to provide the gating input to the 7225. For readers who wish to use a CC display (possibly the miniature FND357) the 7225 can be replaced with the 7236. Though the data sheets specify this as a device for driving vacuum fluorescent displays, it will also drive the CC type. The pin out is exactly the same as the 7225 except that pin 11 should be grounded and pin 35 (at present connected to 0V) should instead be connected to +5V. Otherwise simply connect the display segments as shown, and the CC line to 0V.

The power supply is straightforward and consists of a 3VA, 0-12, 0-12V transformer arranged in a 12-0-12V centre tapped configuration. The secondary a.c. is then rectified

and smoothed before being regulated by IC6 and IC7 to give ±12V controlled by S1. The 12V also feeds the 5V regulator which supplies IC2, 4, 5. This line is not switched because it would have meant that VR7, incorporating only a two-pole switch, could not be used. It is therefore made to power the decimal point of the least significant digit to show that the mains supply is on.

### CONSTRUCTION

The project uses two p.c.b.s, details of which are given in Figs. 3 and 4.

Mount the power supply components, making sure that the regulators are inserted the right way round. The 7805 is mounted on the rear panel.

After checking, attach a mains lead, switch on and make sure that ±12V and 5V appear at the 'out' pins. If all is well, switch off, and disconnect the mains before proceeding with the oscillator section. Two sets of holes are provided on the p.c.b. for C4 depending on whether polystyrene or silver

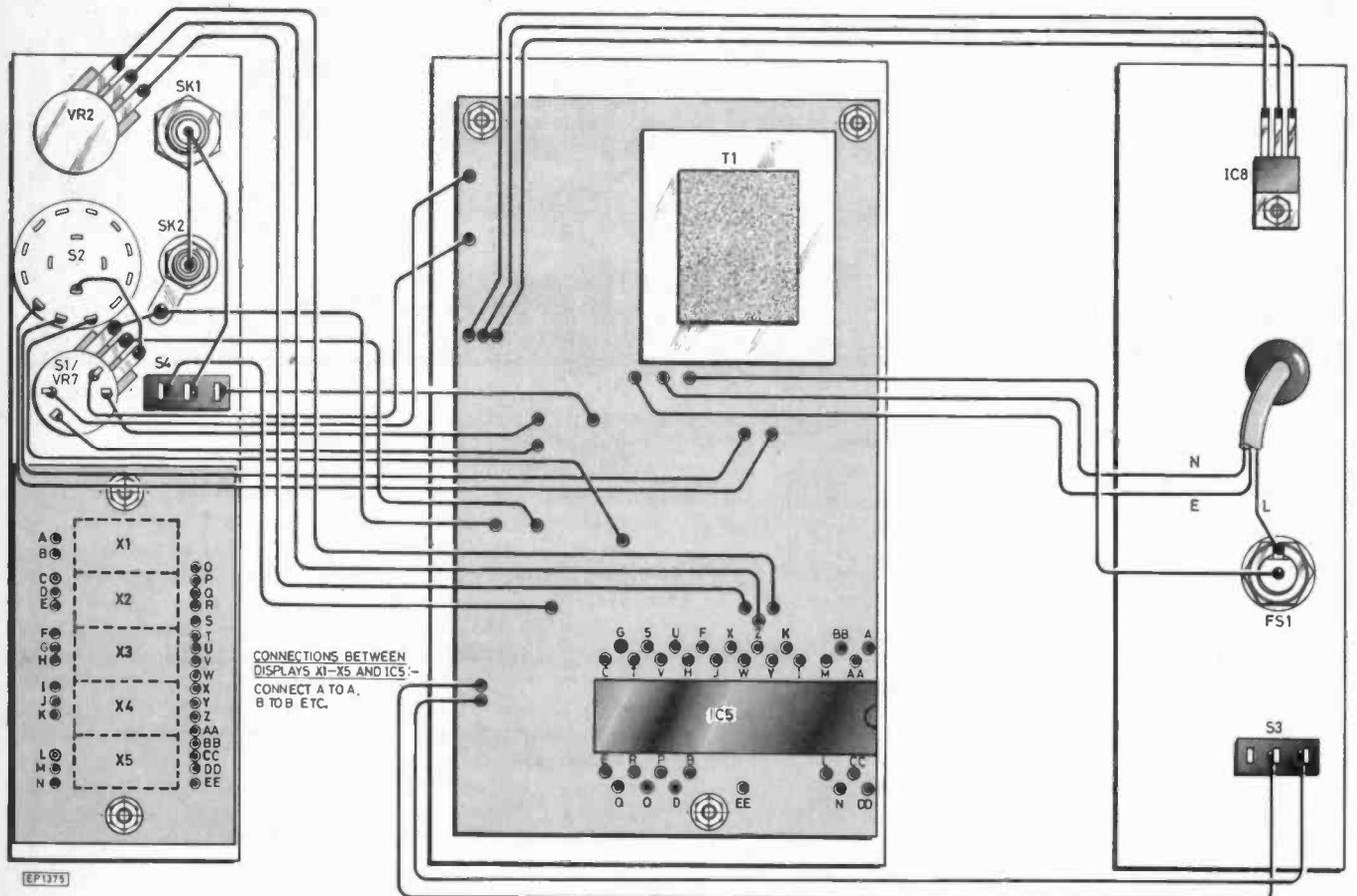


Fig. 5. Interwiring details of generator



mica is selected. This component needs to be of high stability to minimise frequency drift. Use Veropins for all interconnections to the p.c.b., and set all the presets to mid travel. Apply power and check, preferably with a scope, that the correct waveforms appear, and that adjusting the various presets causes some alteration to them. Check the TTL output on pins 15 and 12 of IC2 (one of them being an inversion of the other). Varying VR7 should alter the peak-to-peak level coming out of IC3 pin 6. Again if all is well, switch off, and insert the components associated with the digital readout. The digits are connected with ribbon cable to make possible fault-tracing easier. By monitoring pins 2, 13, 14 of IC4 it should be possible to see the count inhibit pulse switching at a 1Hz rate, and the reset and store pins producing short negative going pulses. Connecting pin 11 of IC4 to +5V will reduce the gate time to 0.1s, speeding up any change in reading, but this does reduce the resolution to

10Hz, and this can be included via a toggle switch if desired.

If everything is working satisfactorily, the p.c.b. can be bolted to the base panel of the Centurion DX1 case. It is a very tight fit, but the result is a neat compact unit.

A ten-turn pot was used for VR2 to make resolution easier but the author chose not to include a ten-turn dial, being superfluous with a digital readout. The display incorporates a bezel to improve the appearance and hide possible ragged edges. Drill two holes in the rear panel for the strain relief bush and mains fuse.

After a final check the unit can be calibrated by adjusting trimmer C14 with reference to a reliable source, but in practice it was found that setting it to mid travel was accurate enough for all but the most demanding purposes. VR5 and VR6 are adjusted to give a good shape to the positive and negative peaks of the sine wave, whilst VR4 alters the duty cycle, most easily set using the square wave output. VR3 is then adjusted to give a reading of 20kHz and VR1 a reading of 20Hz. These presets interact and repeated adjustments are necessary. Note that above 20kHz, the  $\frac{1}{2}$  digit will remain lit, and give misleading results, so the prototype was set with a top limit of 19500 to avoid confusion. When these adjustments are complete, the case can be screwed together, and any front panel markings, e.g. Letraset, added. If readers are concerned about the buffer being a d.c. amp, it can easily be modified to one of the standard a.c. op-amp configurations. ★

# RSGB National Amateur Radio Convention

National Exhibition Centre, Birmingham

Saturday 28th April 10am to 6pm Sunday 29th April 10am to 5pm

## FEATURING

-  Lectures on Propagation, VHF and Microwaves.
-  Introduction to Amateur Radio for Beginners
-  Annual RSGB HF Convention
-  Major Exhibition of Amateur Equipment & Components.

-  Forum for VHF and Repeater Enthusiasts.
-  RSGB stand with book sales and representation by many of the Society's committees.
-  Bigger Flea market as a result of last year's success.

**Entrance Fee £2 (Children  $\frac{1}{2}$  price) Car Parking Free**

Organised by the Radio Society of Great Britain



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A set of parts to build a complete stand-alone alarm system which may be mounted on the wall, or placed on a shelf or table. A few soldered joints and simple assembly is all that is required to complete this kit; an external horn or bell can be used with the unit. For further details of this advanced ultrasonic system, see 'News and Market Place' in this issue.

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**Indicator:** Red l.e.d.



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FILESHEET 15

NSC800

WE have now covered most of the common 8 and 16 bit multi-chip processor families, followed by their single-chip cousins, and the time has now come to take a look at the few remaining processors which either did not fit readily into those earlier categories or were not widely available when the series began.

In March we looked at the single-chip 8070 family, and I highlighted the uninspiring microprocessor track record of its manufacturer, National Semiconductor, which despite some very good ideas had not been able to shake the market stranglehold enjoyed by the Intel, Zilog, Motorola, "big-three". In the next two file articles we are therefore going to examine two other, fairly new, devices from the National stable which are expected by their sponsor to break the existing mould and to turn the "big-three" into the "big-four". See what you think!

First let's look at the National NSC800, an interesting 8 bit multi-chip design which is already beginning to take-off well in the expanding market for battery operated microprocessor systems where its low power CMOS technology gives it an instant advantage.

It all started with the development by National of a new CMOS processing technology which combined, for the first time, the functional density of NMOS with the low power requirements of CMOS. National called this technology P<sup>2</sup>CMOS, and set about the task of designing a new processor to make use of it.

In order that they might capitalise on their new technology as quickly as possible, before everyone else could catch up, National decided not to face the certain delays involved in a brand new architecture, but to use an existing architecture instead. The trouble was, National did not have a suitable 8 bit NMOS processor of their own since their indigenous 8060 (SC/MP) design was becoming obsolete and their other 8 bit processor, the 8080A, was just a second source to the Intel design which itself was well past its prime. National therefore examined all the offerings of their competitors and decided that the impressive success of the Zilog Z80 and its powerful instruction set was the act they wanted to follow. Unfortunately, they also felt that the un-multiplexed Z80 bus structure was not as neat as that of the multiplexed Intel 8085, and so they decided to use their P<sup>2</sup>CMOS technology to demonstrate that you *can* have a cake and eat it too, by building a CMOS Z80 with an 8085 bus interface. The NSC800 was born!

Of course there were CMOS microprocessors already available, particularly the RCA 1802, but these early devices had to pay quite a price for their low power consumption and suffered from low operating speeds and a primitive architecture. By having the capability to put the Z80 register and instruction set inside a package using the efficient 8085 bus interface, running at the full Z80 clock rates of up to 4MHz and with a low power consumption to boot, National felt they were bound to produce a winner.

To back up the impressive capabilities of the NSC800, National also designed two multi-function P<sup>2</sup>CMOS peripheral chips based on the Intel 8155 and 8355 devices, to allow the design of a system with 2K of ROM, 128 bytes of RAM, 42 I/O lines and two 16 bit programmable timers, but needing only three 40 pin chips.

The NSC800 and its support chips have been available for about 2 years now, and success has certainly been achieved to the extent that the National device has ousted the RCA 1802 from its position as the foremost CMOS processor, and has won ready acceptance in battery powered applications thanks to its powerful architecture and its ability to run the vast library of available 8080 and Z80 software, including the ubiquitous CP/M operating system.

Promising as this may be however, the NSC800 is unlikely to make National's fortune. For a start, the NSC800 is several times

more expensive than the NMOS Z80, making it a natural choice *only* for battery powered applications, which taken together are a relatively small fraction of the total microprocessor market. Secondly, other manufacturers, particularly in Japan, have now introduced their own CMOS versions of both the Z80 and the 8085 microprocessors, and these have the great advantage that they can be plugged straight into an NMOS Z80 or 8085 socket, often with little or no circuit change. The NSC800 cannot be used in this way, and is therefore mainly specified for brand new projects where its special blend of Z80 and 8085 features can be used to advantage.

We therefore have to ask ourselves whether National have got it wrong again, by designing an admittedly superior product which in the end will be less successful than microprocessors which are simpler and therefore less expensive.

Only time will tell, but after reading more about the technical features of this excellent chip I am sure you will agree with me that National do at least *deserve* to succeed!

## REGISTERS

The NSC800 has an almost identical register set to that of the Zilog Z80, which in its turn consists of a superset of the 8080/8085 registers. Register names remain the same as those used on the Z80, and anyone used to that processor, or even the earlier Intel 8080, will feel immediately at home with the NSC800.

Like the Z80, the NSC800 has two separate general purpose register banks each containing the AF, 8C, DE and HL register pairs, and it has the usual 16 bit index registers IX and IY in addition to the Stack Pointer and the Program Counter. You may remember that the Z80 also had two 8 bit registers, T and R, which provided the base address of the Interrupt vector table and a dynamic RAM refresh count respectively. These have been retained on the NSC800 with the R register now having a modification to enable it to provide a full 8 bit count value rather than the 7 bit count of the Z80. This is the only obvious difference between the register sets of the two processors, and it confers the useful ability to refresh the newer 64K bit DRAM chips some of which have become a problem for the Z80 since it is only directly able to refresh 16K bit devices unless additional external hardware is used.

As I pointed out on File Sheet 3, the Z80 has a more comprehensive register set than any of the other 8 bit multi-chip processors, and the NSC800 is therefore very well endowed in this respect.

The flags in the F register are also identical to those of the Z80, and consist of the familiar Carry, Add/Subtract, Parity/Overflow, Half Carry, Zero, and Sign bits.

## INSTRUCTION SET

The NSC800 has all the Z80 instructions, and, thank goodness, they all use the same mnemonics (for this reason we have not shown the instruction set here) so that any Z80 based machine with an assembler can easily be used to produce object code for the National processor.

Like the Z80, the NSC800 instruction set contains all of the 8080 instructions too, although as before, most mnemonics have been changed so that compatibility exists only at the object code level. The two additional 8085 instructions, RIM and SIM, which manipulated the Interrupt Mask and provided a serial I/O facility are missing from the NSC800 set however, and this is because the two serial I/O lines of the 8085, SID and SOD, have been sacrificed to provide the new NSC800 pin functions Refresh and Power Save.

Although the RIM and SIM instructions are not available, some functions of the additional Interrupt Mask Register of the 8085, which provided individual status and enable flags for the three fixed

# NSC 800 REFERENCE FILE SHEET

## GENERAL

The use of low power CMOS technology combined with an 8085 bus structure and the full Z80 instruction set makes the NSC 800 a unique and interesting processor. This device has become very popular for battery powered applications, but due to a higher price tag than that enjoyed by NMOS processors and some recent competition from CMOS pin compatible versions of the Z80 and 8085 it may not turn out to be the great success that National had hoped for. It is without a doubt however the most powerful 8 bit CMOS processor available and is ideal for "few-chip" battery powered systems.

## REGISTERS

The NSC 800 register set is identical to that of the Z80 except that the refresh counter register (R) is 8 bits (rather than 7 bits) long. This allows easy interface to the 64K RAM chips now available.

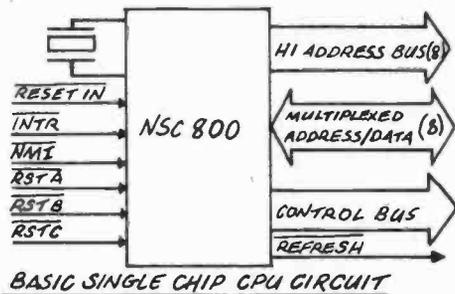
A (8)	F (8)	A' (8)	F' (8)
B	C	B'	C'
D	E	D'	E'
H	L	H'	L'
INTERRUPT VECTOR I	MEMORY REFRESH R	<b>ALTERNATE SET</b> Like the Z80, the main register bank can be swapped with the alternate bank by issuing an EXX instruction.	
INDEX REGISTER IX			
INDEX REGISTER IY			
STACK POINTER SP			
PROGRAM COUNTER PC			

## FLAGS

D7	D6	D5	D4	D3	D2	D1	D0
SIGN	ZERO		HALF CARRY		PARITY & OVERFLOW	SUBTRACT	CARRY

## INSTRUCTION SET AND SOFTWARE

The NSC 800 uses the full Z80 instruction set with no additions or deletions, and uses standard Z80 mnemonics so that any Z80 based system can be used for software development. It is upwards compatible with the 8080 and 8085 at the object code level apart from the two 8085 specials RIM & SIM. It is fully compatible with the CP/M O.S. and therefore has access to a very large software library.



## PERFORMANCE DATA

MEMORY ADDRESS RANGE :	64K
I/O ADDRESS RANGE :	256
CLOCK FREQUENCY :	2.5MHz*
POWER SUPPLIES :	+3 → +12V
INTERRUPTS :	INT, NMI, RSTA, RSTB, RSTC

\* NOTE: 4MHz version also available

## BENCHMARKS

ADD REGISTER TO ACCUM	1.6µs
OUTPUT ACCUM TO PORT	4.8µs
MOVE FROM MEMORY TO MEMORY	6.4µs

## NSC 800

A8	1	40	VCC
A9	2	39	PS
A10	3	38	WAIT
A11	4	37	RESET OUT
A12	5	36	BREQ
A13	6	35	BACK
A14	7	34	I/O/INT
A15	8	33	RESET IN
CLK	9	32	RD
X OUT	10	31	WR
X IN	11	30	ALE
A00	12	29	RD
A01	13	28	RFSH
A02	14	27	SI
AD3	15	26	INTA
AD4	16	25	INTR
AD5	17	24	RSTC
AD6	18	23	RSTB
AD7	19	22	RSTA
GND	20	21	NMI

## NSC 800 VERSUS Z80 AND 8085 A COMPARISON:

FEATURE	NSC 800	Z80	8085
1 SUPPLY VOLTAGE	3→12	5	5
2 CONSUMPTION	50mW	750mW	850mW
3 DYNAMIC RAM RFSH	YES	YES	NO
4 INTERRUPTS	5	2	5
5 ON CHIP CLOCK	YES	NO	YES
6 NO. OF INSTRUCTIONS	158	158	80
7 NO. OF REGISTERS	22	22	10
8 BLOCK INSTRUCTIONS	YES	YES	NO
9 TECHNOLOGY	CMOS	NMOS	NMOS
10 PACKAGE PINS	40	40	40

## MANUFACTURERS

ORIGINATOR : NATIONAL SEMICONDUCTOR

2ND. SOURCES : SMC, EUROTECHNIQUE

## SUPPORT CHIPS

THE NSC 800 PERIPHERAL CHIP FAMILY IS MODELLED ON THAT OF THE 8085 AND INCLUDES THE NSC 830 ROM, I/O (LIKE 8355) AND THE NSC 810 RAM, I/O, TIMER (LIKE 8155) BOTH IN LOW POWER CMOS. Z80 AND 8080 PERIPHERALS CAN ALSO BE USED IF REQUIRED.

vector interrupts, have been retained in the NSC800 via a special 4 bit Interrupt Control Register (ICR). This register is unique to the NSC800 and has to be accessed via an OUT instruction to I/O address 0BBH. Anyone who is familiar with the 8085 will soon find that the NSC800 RST A, B and C interrupts which are intended to be similar to the RST 5.5, 6.5 and 7.5 of the 8085, are in fact quite different in some respects, so be careful!

There is no need for me to examine the NSC800 instruction set in detail, since this was done quite adequately in the Z80 file article. Suffice to say that those useful bit Set, Test, and Reset, instructions, BCD Shifts and Block Moves are all alive and well.

Since all the instructions are the same you would expect the addressing modes to be the same too, although National have put their stamp on things by renaming the Extended mode of the Z80 as the Direct mode, which is an improvement, I suppose.

## SOFTWARE

With full 8080 and Z80 compatibility there is definitely no shortage of software for the NSC800 since it can share the huge existing library built up for those processors over the years. The CP/M disc operating system provides the easiest gateway to this library, although whether it is likely that the low power advantages of the NSC800 could ever be fully appreciated in a system which uses a couple of floppy disc drives is quite another question!

More important perhaps, is the possibility of using an existing Z80 based personal computer as a host development system for battery powered NSC800 target systems. Almost any Z80 system with an assembler and a PROM programmer could be used, including the humble Sinclair Spectrum, but a system with floppy discs and running the CP/M DOS would be ideal.

So far as I am aware, there are no personal computers which actually use an NSC800 CPU, but this is only of academic importance to the programmer.

## INTERFACING

The NSC800 is not pin compatible with either the Z80 or the 8085, although it most closely resembles the latter. Some of the 8085 pins which have similar functions on the NSC800 have been renamed by National to confuse the enemy, so that TRAP becomes NMI and Ready becomes Wait. Some other pins have changed not only their names but also their functions. In the 8085 two pins HOLD and HOLDA provide a handshake to permit other devices to request, and then use, the data and address buses. In the NSC800 these functions are provided by the aptly named BREQ and BACK but with the difference that the logic polarities have been inverted to be the same as those of the Z80.

The new function RFSH is also identical to the Z80 pin of this name, but with the previously mentioned advantage of an 8 bit refresh address being provided on the multiplexed bus. The PS input pin is unique to the NSC800 and complements the low power operation of the CMOS processor by invoking a very low power standby mode in which the processor clock is suspended to reduce consumption. Since it is intended that the processor itself should control this pin in most circumstances, it would seem more appropriate to provide this function via a special instruction rather than by external hardware, but in its present form it does also provide the useful facility of a single step mode when driven by a couple of external latches.

The P<sup>2</sup>CMOS technology of the NSC800 confers several other advantages in addition to low power consumption. Instead of the usual rigidly imposed 5 volt power supply voltage, the NSC800 can operate over a 3 to 12 volt range and does not need tight voltage regulation. Noise immunity too, can be better in CMOS systems, and the low internal heat dissipation makes it possible for some NSC800 versions to be specified for the very wide ambient temperature range of -55 degrees C to +125 degrees C.

The 8085 bus structure is a good choice for the NSC800 since it multiplexes the 8 low order address bits with the data bus to save package pins for other functions. In systems using standard peripheral components such as 27C16 CMOS EPROMs or 16K static CMOS RAM chips the bus has to be demultiplexed externally using an 8 bit CMOS latch such as the MM82PC12. An 8085-like Address Latch Enable (ALE) output is provided to capture this address information from the multiplexed bus.

For many applications however, it may not be necessary to use a

separate address latch since the two special I/O devices coded NSC810 and NSC830 contain internal demultiplexing circuitry for this purpose.

The NSC810 is a 40 pin P<sup>2</sup>CMOS device which features 128 bytes of static RAM, 22 parallel I/O lines and two programmable 16 bit timer/counters. In most respects this device is similar to the 8155 from the 8085 family but it differs in having two timer counters instead of one, each having superior features to the single 8155 circuit.

The NSC830 is also a 40 pin P<sup>2</sup>CMOS device, but in this case containing 2K bytes of masked ROM and 22 I/O lines. Masked ROM is of no use for low volume applications of course, but there is a companion device, the NSC831, which only has the I/O lines. Unfortunately there is no EPROM version equivalent to the 8755.

The NSC800 is particularly well endowed with interrupt inputs and modes, inherited from both the Z80 and the 8085 and providing a high level of compatibility with both devices.

There are four fixed vector interrupts, NMI, RSTA, RSTB and RSTC, all of which result in a direct vector to locations in low memory. NMI is of course non maskable, but the other three can be individually masked by clearing the appropriate bit in the Interrupt Control Register (ICR), or collectively masked by issuing a DI (Disable Interrupts) instruction. The NMI interrupt input is edge triggered but the other three are all level sensitive; while the input pin is pulled low an interrupt is continuously asserted.

In addition to the fixed vector interrupts there is a single multi-mode interrupt INTR, which operates in the same way as the Z80 input of that name. This input can be set up by the program instructions IMO, IM1 and IM2 to respond in one of three different modes depending on the system configuration and the peripheral devices.

Interrupt Mode 0 is similar to the standard 8080 interrupt which requires an interrupting device to respond to the Interrupt Acknowledge output (INTA) by placing a suitable instruction on the data bus (usually a 3 byte Call, but one could use the simpler 1 byte Restart). This mode is particularly useful when a number of vectored interrupts need to be handled and the system includes an interrupt controller chip such as the Intel 8259.

Interrupt Mode 1 is the simplest mode since it turns the general purpose INTR pin into an additional fixed vector input making a new total of five. This is the most useful mode for many all-CMOS systems, since as far as I can discover, there is no CMOS equivalent to the 8259, and there are no CMOS equivalents to the Zilog peripherals either.

Interrupt Mode 2 is the most powerful mode since in this case the INTA output is used to read a single byte vector from the interrupting device which is subsequently concatenated with the contents of the I register to form a 16 bit pointer into a 128 entry vector table which can be located anywhere in memory. Unfortunately, the external logic required to generate the appropriate response is quite complex, and neither of the two National peripherals (NSC810 and NSC830) have the necessary facilities to support this mode, a surprising omission. Perhaps National intend (or intended) to produce an interrupt controller which supports this facility, but without it the only easy way to use Mode 2 is to choose NMOS Zilog peripheral chips such as the PIO and CTC devices.

Although National have not produced many CMOS LSI peripheral devices for the NSC800, they have performed much better in the provision of CMOS "glue" ports, since a useful range of gates, decoders and latches is available, all fabricated in P<sup>2</sup>CMOS.

## APPLICATIONS

The NSC800 should be considered for all battery powered microprocessor applications since it offers a powerful architecture and instruction set, an excellent bus structure, and all the low power advantages of CMOS technology. If the need is to convert an existing NMOS8085 or Z80 system for a low power application, however, it may be easier to use one of the pin compatible CMOS versions of those processors (80C85, Z80C) which are now becoming available.

If the intended application is to be mains powered, then it is unlikely that the NSC800 could be considered cost effective unless the reduced cooling requirements or the particular attractions of a Z80 architecture and an 8085 bus are dominant factors.

A nice try National, but perhaps you should listen more closely to the market research team rather than allow those bells-and-whistles engineers to call the shots!

all in your **JUNE** issue!

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# **ELECTRONICS**

JUNE ISSUE ON SALE FRIDAY 4th MAY 1984

# VERNON at TRENT Large!

*V.T.'s views and opinions are entirely his own and not necessarily those of PE*

THE late David Cohen came into the radio business in Birmingham before the second world war. He began, as so many of the old pioneers did, by offering a battery-charging service. He then gradually extended his business into the retail and mail order equipment supply areas. His avowed policy—and you can't have better roots—was to sell competitive goods of a quality commensurate with what the man in the street could afford.

As well as being an ambitious man of business, David Cohen was also a patriot—which may seem a bit old-fashioned by today's cynical standards. So when Hitler got up to his tricks—which eventually, as we know, did him no good at all—David wound up his business, moved to London and offered to do whatever he could to help the war effort.

His son, Les, who now runs the firm which is still called Radio & Television Components Ltd., said: "My father, who was entirely self-taught, got a job as an inspector with EMI, then called The Gramophone Company. And I'm convinced he did a good job, because he was that sort of man. But when the end of the war came he was given the push. This is no criticism of EMI, with whom we still have friendly ties. It was the vogue. In those days, anyone who had a disability which prevented them going into the services, as in my father's case, tended to be regarded as a second-class citizen."

But, disability or not, the drive was still there. David launched himself into the Government surplus business. He built and marketed radio receivers made from broken-down Government equipment and housed in cabinets made out of ammunition boxes. Another venture, on the components side, was to acquire a consignment of dried-out Mullard electrolytics at 2/6d (12½p) each. He discovered a method of reforming them and sold them at £1 a time. The Cohen enterprise at that time was being run from the family's back garden and neighbours were not happy about the situation. So David took over premises in Acton, West London, and from there he edged his way into other spheres. One of them was stereo, using for the first time, Les claims, an integrated circuit.

Although the firm now concentrates on the retail and mail order trade—with the accent on the former—from the Acton branch and another in London's Edgware Road—it still manufactures such items as TV sound tuners, stereo cassette players in kit form and 125W power amplifiers.

Les, who literally learned the game at his father's knee, recalls how from his earliest years he was totally involved in the operation. "I was weaned on electronics," he says. "Just after the war there were very few toys about. At that time, with my father knee-deep in the Government-surplus trade, I never had such a thing as a train set for Christmas. Instead, I

had a rubber dinghy. Or an ex-WD box-kite (used for meteorology) or a transmitter/receiver. My destiny was plain to see.

"The fascination of electronics," he continued, "is that there is always something new and exciting round the corner. But it is a matter for regret that so many of our young constructors lack the ability or interest to keep up with the pace. Why, some of them don't even know how to solder!"

Another of the tragedies of our time, thinks Les, is that 90 per cent of electronic equipment in use today is made outside the UK. "To think," he said, "that at one time we had it all in the palm of our hand. There were the great names like Murphy, Bush, Leak and a whole host of others, now dead and gone. And why? Poor marketing, perhaps? Complacency? Who knows? You know, someone once said that the perfect product would be designed by the British, made by the Germans and marketed by the French. How valid that is I don't know. But perhaps we're not as

## "Curiouser and curiouser"

European in our thinking as we ought to be.

"Deep down I like to think that I'm a good European. But now and then I can't help reminding myself that it's that strip of water between Dover and Calais that's saved our rather special way of life so many times. You just can't ignore that.

"Once upon a time we had a strong Commonwealth market that would take everything—including all the rubbish—we had to offer. And then when we went into the Common Market we lost a lot of friends.

"Today we seem to lack a sense of purpose. Go into any factory and you'll see people running around doing nothing. People just haven't come to terms with reality. The good times we knew in the past are, for goodness sake, over. It's now a matter of the survival of the fittest. Management don't, in the main, look far enough ahead. That's why we've lost out in so many markets. Our ceramics industry—once the envy of the world—has virtually gone. Our cutlery—once universally unrivalled—has gone. Our motor cycle industry has been killed stone dead.

"It would be foolish, of course, to deny that the Japanese goods which flood our markets are anything but excellent. But why is this so? Is it because of their total dedication to corporate objectives which, possibly because of differences in national outlook and temperament, we lack? Alright, this may be so. But what is more significant, I think, is that whereas, when we find a successful

product we go on to discontinue it and put something we feel is even better in its place, the Japanese push and push and, only when they have completely captured that particular market, do they go on to update. Really, it's all so simple. In the audio area, for instance, it costs the same to make something within 1000th of an inch as a half-inch."

Napoleon designated the British as a nation of shopkeepers. Les thought it was Hitler, but I forgave him because he's a young man who probably didn't care much for history as a schoolboy—he was too tied up with electronics. But if Napoleon was right, isn't it time we did something about changing that image? It is laudable to be an efficient supplier. But it is even more laudable—and essential to ensure our economic future—that we should be a good salesman as well.

My goodness, Les. You *have* thrown the cat among the pigeons.

★ ★ ★

Electronics and its applications knows no bounds. Hotelier Peter Rudd, according to reports reaching my ears, is offering cut-price weekends at his Norfolk establishment for chronic snorers. Apparently he is prepared to give them accommodation in a special (sound proof?) wing, where their nocturnal snortings will be monitored and measured by night porters equipped with decibel meters. And there will be prizes for those generating the most ear-splitting row.

He goes even further than that, if my informant is to be believed. To ensure that the participants are worked up to maximum pig-noise capacity by night, he takes them on daytime visits to the neighbouring villages of Great and Little Snoring.

But it is clear that this lively inn-keeper is setting a trend which could spread. What about a similar facility for those who are prone to talking in their sleep? It is a well-known fact that the truth, the whole truth and nothing but the truth tends to emerge during mutterings in the wee small hours and it is important that this soul-baring should be handled in a controlled way. So why doesn't Mr. Rudd organise weekends for those with something on their minds? In the secure atmosphere of his hotel they would be able to babble away to their heart's content and purge their systems of what could otherwise be a death blow to marital harmony.

Whether such revelations should be taped by the prowling porters is quite another matter. But certainly a playback session—with immediate destruction of the recordings afterwards—would be a much more entertaining diversion than Monopoly.

★ ★ ★

Here's an odd remark attributed to Patrick Cody, managing director of STV, when announcing his company's plans. He's quoted as saying "we specialise in entertainment. *We make no pretence or apology for that.*"

Now, what did the gentleman mean? Surely, entertainment is what people are paying out their pounds for. So why should anyone pretend anything else? And why should an apology be forthcoming for a pledge to deliver the goods the client rightly looks forward to? As Alice said: "Curiouser and curiouser..."

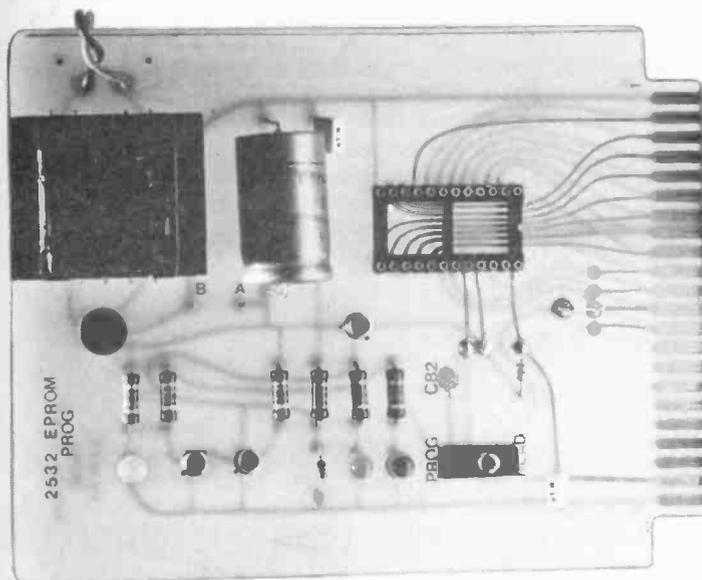
# VIC 20

## EXPANDING THE



PART SEVEN SAM WITHEY

### 2532 EPROM PROGRAMMER . . .



FOR AROUND £8

SINCE the Vic 20 ROM board described in Part 1 of this series is designed to accommodate 2 x 2532 EPROMs it was decided that there was little point in building a complex programmer for use with the Vic 20, even though it is possible to use 2716 EPROMs. Further to this, the falling cost of the 4K ROM is conducive to adopting it as a standard instead of the 2716. The programmer described here uses the minimum of components required to fulfil the necessary operations needed to test, read, program and verify a 2532 EPROM, instructions to the operator and other functions being carried out under software control. Unlike most microcomputers, the Vic 20 has address and data lines available at the expansion port, cutting the components count of the EPROM programmer by several costly i.c.s.

#### EPROM PROGRAMMING

When "clean" every bit in the memory matrix of an EPROM is set *high* and since these are presented on the screen of a computer in bytes, each byte has the Hex value FF (1111 1111). To program the EPROM, some of the bits are brought *low* to logic "0". The Hex value CA would be represented by the bit pattern 1100 1010. In order to bring the required bits *low*, a high voltage pulse of 50ms duration has to be applied to the bit in question. This is carried out by first of all applying a *high* (25V) voltage to Vpp (pin 21) and then applying the 50ms pulse at CE (pin 20) when pointing

to the particular memory bit to be brought *low*. This is carried out sequentially throughout the 4096 bytes (32768 bits) contained in the 2532.

Programming is carried out in four stages. The first function of a programming sequence should be to check that the EPROM is clear, i.e. all bits set *high*. This is carried out in the Read mode. The second stage sets the programmer circuit to Program mode. Next is the actual programming, consisting of comparing with a 4K byte section of RAM bit by bit and bringing bits *low* where required. The third stage compares, or Verifies the programmed EPROM with the RAM section, indicating any bits left *high* that should have been brought *low* and listing them, before announcing that the operation is finished. Finally the EPROM board is returned to the Read mode before removal of the EPROM from its socket. Reading EPROMs is similar to Verification. For those possessing Vicmon, this has a facility built in. Because of the vast quantity of information being processed, it is usual to program in machine code, the whole sequence described above taking between 3 to 5 minutes for a 2532. Again, those who have Vicmon will find many subroutines in this package that they can use.

A typical programming sequence would follow these lines:

- (a) Set Prog/Read switch to Read - Check
- (b) Insert EPROM in socket - Check pin orientation
- (c) Has Data been entered into RAM - Check
- (d) Define Start and End of RAM area - Check
- (e) Define Start and End of ROM area - Check
- (f) Will total RAM fit into ROM?
- (g) Check that ROM is clear. All bytes set at FF Hex
- (h) Check that EPROM space is free of Data held in RAM
- (i) Set Prog/Read switch to Prog. Apply 26V to Vpp
- (j) Program - output bit pattern to start address - toggle CB2, 50ms pulse
- (k) Output bit pattern to Start + 1 - toggle CB2
- (l) Repeat until program count is complete
- (m) Set Prog/Read switch to Read
- (n) Verify that Data in EPROM is same as Data in RAM
- (o) If correct - End
- (p) If not, List Bytes that do not agree
- (q) Do you want to re-run from (i)?
- (r) If Yes, go to (i), otherwise - End
- (s) If Verification now correct - End

EPROMs can be checked for "clear" by verifying with a RAM area set to FF Hex. They can be Read by POKEing Data into RAM instead of comparing as at the Verification stage. Note that the RAM address is not usually the address where the EPROM will normally reside when in use.





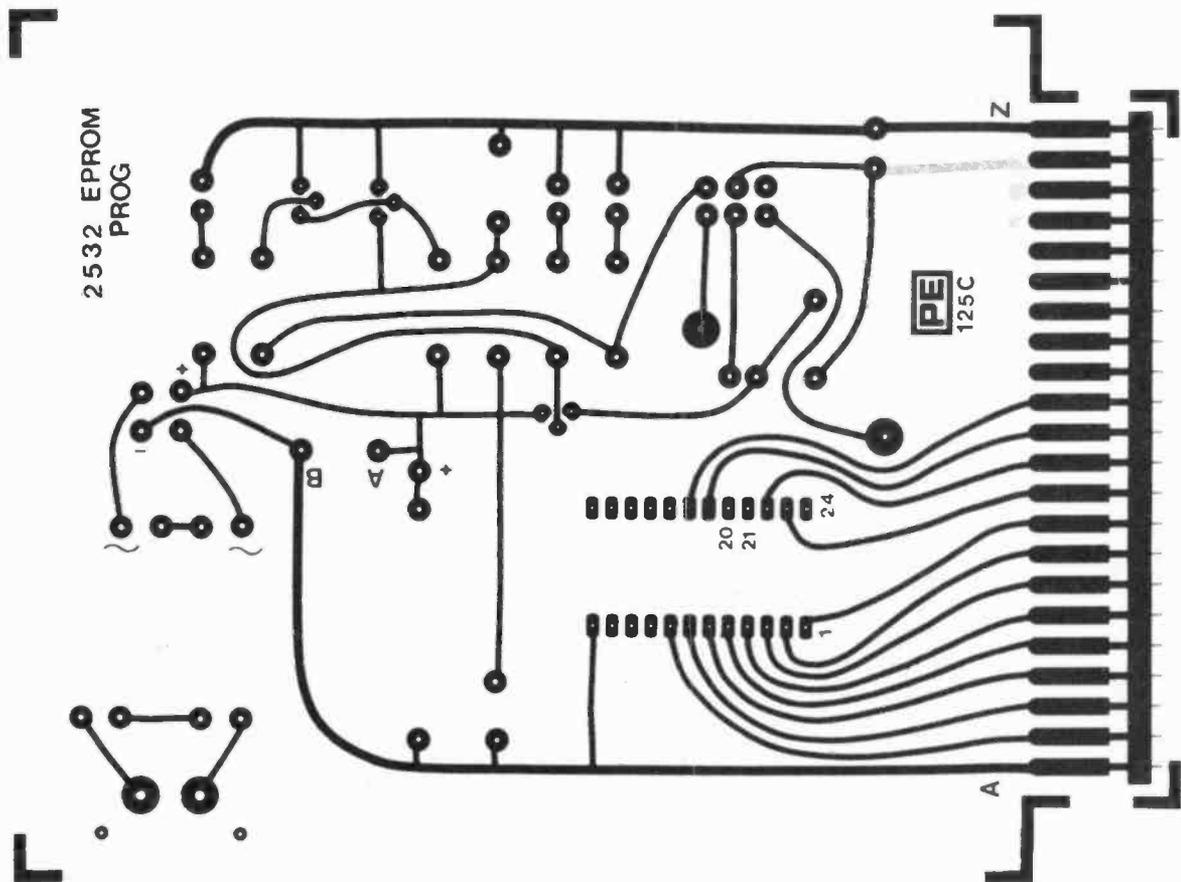


Fig. 7.3. P.c.b. component-side pattern (actual size)

at BLOCK 1 for the BASIC program to use and for storage of the data to be burnt into ROM. If most of the programming functions are to be carried out in machine code, these routines can reside in the onboard RAM. Capacitor C1 provides smoothing at the power supply, and whilst it is necessary to have an electrolytic with a working voltage of 50V to 63V, the capacitance value is not critical, 220 $\mu$  being a suitable minimum value. Two holes are provided at the positive end because of varying shapes and sizes. For the use of the programmer in schools, where mains supplies are not allowed, batteries can be connected at points A, positive and B, negative. Four PP3 batteries in series make a suitable supply and these should last for years. Three PP3 are not sufficient as the supply must be above the Zener voltage (27V). If difficulty is experienced in buying PP3 connectors, these can be made from expended batteries.

The mains supply must be shrouded at the transformer for the safety of operator and equipment. Since it is necessary to raise the rear end of the programmer to the height of the mother board, a spacing block made from an audio cassette case is ideal for starters.

Capacitors C2 and C3 are included for noise suppression and may not be needed.

Connection of CB2 is to pin M on the User Port. The author identified this with a marker and connected up with a small croc-lead, insulated at the top side of one end with tape.

## COMPONENTS . . .

### Resistors

R1	470
R2,R3	47k (2 off)
R4	2k2
R5,R6	4k7 (2 off)

### Capacitors

C1	220 $\mu$ 63V elect.
C2	100n
C3	220n (see text)

### Semiconductors

TR1-3	BC107 (3 off)
BR1	1A 50V rectifier stack
D1	Red l.e.d. (0.2")
D2	BZY88 27V Zener
D3	Green l.e.d. (0.2")
D4	1N4148 (or 914)
D5	Yellow l.e.d. (0.2")

### Miscellaneous

- S1 Miniature DPDT switch
- 24-way i.c. socket
- P.c.b. mounting transformer (RS 207-835)
- Printed circuit board (or stripboard)





# SEMICONDUCTOR CIRCUITS

TOM GASKELL BA (Hons) AMIEE

## GAIN CONTROLLED PREAMPLIFIER (SL 6270C)

THE range of signal levels which can be obtained from modern microphones is very large indeed, varying from a few microvolts to several hundred millivolts. The differences in sensitivities of the microphones account for some of this signal range, although for any specific type of microphone the difference in signal level produced by a whisper several metres distant and a shout directly adjacent to the microphone is vast; ratios of thousands to one are typical. Because of the practical constraints of audio system design, we need to provide the means to control the gain of microphone amplifiers, such that the system can be optimised for most circumstances in which the microphone is likely to be used. The majority of audio systems have manual adjustment of microphone level, allowing the owner or operator of the system to decide on the optimum gain setting at any given moment.

Some form of automatic control, on the other hand, is an attractive concept in simpler systems. While such an arrangement may lack sufficient quality or sophistication for very high fidelity audio, it is ideal for such applications as cassette recorders, public address equipment, intercoms, etc. The Plessey SL 6270C gain controlled preamplifier (sometimes known as a Voice Operated Gain Adjusting Device, or VOGAD) is a very easy and economic way to provide such an automatic gain control facility. Fig. 2 shows a block diagram of the i.c.

The pre-amp has a balanced low impedance input, specifically designed to match low impedance microphones with an impedance of 300 ohms (typically) or less. The microphone MUST be a.c. coupled to the inputs, hence the use of C1 and C2. The output of the preamplifier is fed via an internal 680 ohm resistor, and the external capacitor C3 (to ensure a.c. coupling between stages), to an inverting main amplifier, the output of which is fed to the automatic gain control (AGC) detector. The output of this, in turn, is fed back to the gain controlling input of the pre-amp via an internal 2k resistor. Hence, if a large signal is generated by the microphone, the AGC 'loop' turns the gain of the pre-amp down, and if a small signal is generated the AGC loop turns the gain of the pre-amp up. As a result of the constantly changing gain of the preamplifier, the main amplifier output level tends to remain constant.

### AGC PARAMETERS

Normally, the i.c. will be required to respond very quickly to large input signals, decreasing the pre-amp gain to minimise overload of the input stage. When the signal from the microphone drops to a low level again the AGC is allowed to increase the gain, but only relatively slowly in case other large signals are about to be generated. Without this

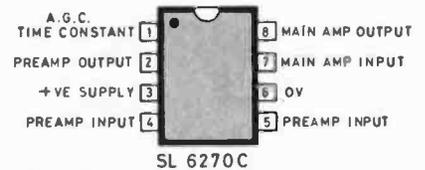


Fig. 1. Pinout and specification

Characteristic	Notes	Minimum Value	Typical Value	Maximum Value	Units
Supply Voltage	(All spec's measured at +6V, with input frequency = 1kHz)	4.5	6	10	V
Quiescent Current			5	10	mA
Temperature Range		-30		+85	°C
Input Impedance	Pin 4 or Pin 5		150		Ω
Input Impedance, total	Differentially between pins 4 & 5		300		Ω
Voltage Gain	72μV r.m.s. input to pin 4	40	52		dB
Output Level	4mV r.m.s. input to pin 4	55	90	140	mV <sub>r.m.s.</sub>
Distortion (t.h.d.)	{ 90mV r.m.s. input to pin 4 10mV r.m.s. input to pin 4		2 0.3	5	% %
Load Impedance	(Load of I/P of next stage) at pin 8	1.0			kΩ

slow 'decay' the system can sound very unpleasant, with a 'sucking' or 'pumping' effect on the audio signal as the gain is constantly changed. The time taken to turn the gain down after receipt of a large signal is known as the

'attack' time, and is determined by the value of C4. It approximates to:

$$\text{Attack Time} = 0.4\text{ms per microfarad.}$$

For a 47μF capacitor, this gives a 20ms attack time. The 'decay' time is the time taken to

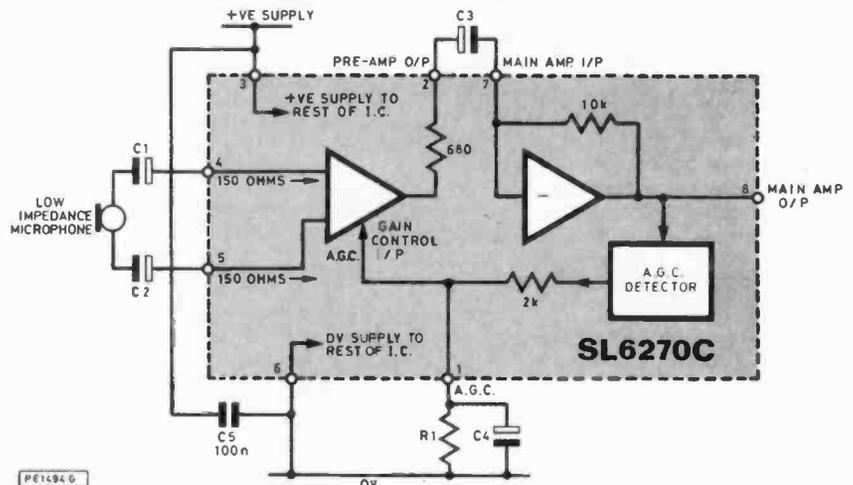


Fig. 2. Block diagram of the SL6270C

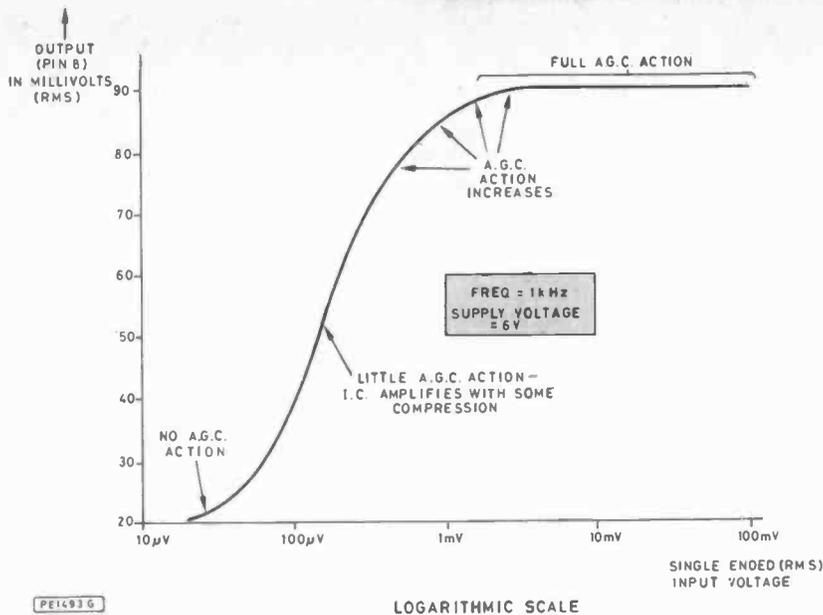


Fig. 3. Graph showing input against output (unbalanced input)

turn the gain back up again after the input signal level has dropped to its earlier level. This is determined by the combination of R1 and C4. For 1 megohm and 47 microfarads the decay is 20dB (a gain increase of  $\times 10$ ) per second, which should suit most applications. If required, the values of R1 and C4 can be altered to change these time constants.

Input signals of up to several tens of microvolts are amplified normally by 52dB (typically), as indicated in the specification of Fig. 1. As the level increases the AGC action gradually takes over, to eventually hold the output at a nominal 90mV (for a 6V supply) over an input range of over 50dB. Reducing the main amplifier gain will reduce both the dynamic range of the system and its sensitivity. Connecting an external resistor between pins 7 and 8 will reduce the gain; for a 1k resistor the reduction will be 20dB. Values of external resistor less than 680 ohms are not advisable. Full AGC action comes in at around 1mV for the standard circuit and 8mV with the external 1k resistor fitted. Fig. 3 shows a graph of input vs. output for the i.c.; note that there is some compression of the signal (i.e. the output variation is less than the input variation) prior to full AGC action. This also helps to keep the output signal reasonably constant in level.

### PRACTICAL CONSIDERATIONS

There are many factors which affect the operation of this i.c. in practical systems. The first of these is frequency response; the SL 6270C has an open loop response of several megahertz, but it is normally intended for use in speech bandwidth systems. The frequency response is primarily defined by C3 and by a capacitor connected between pins 7 and 8 (C7 in Fig. 4). With the circuitry shown, and the values of 1 $\mu$  and 4n7 for C3 and C7, the bandwidth is approximately 240Hz to 3.4kHz. The values of C1 and C2 can also affect the frequency response, so these are usually made quite large in value to ensure that only C3 affects the lower frequency limit.

Although a wide range of supply voltages can be tolerated, the supply itself must remain constant in voltage during operation of the circuitry. The AGC circuit is dependent on the supply voltage; change that voltage, and the AGC will clamp the output at a different level from the nominal 90mV specified at 6V supply. Hence, any ripple on the supply will modulate the output, and could lead to instability. Although the specification of Fig. 1 paints a pessimistic view of the distortion performance at higher input levels, the lower levels will be the norm, where the distortion is considerably less than 1%.

Finally, care must be taken with the inputs to the i.c. These should normally be a.c. coupled; if d.c. coupling is used the resistance between pins 4 and 5 must be less than 10 ohms. The inputs are arranged differentially to suit balanced microphones, although unbalanced signals can also be accommodated. Because of the low input impedance, crystal or high impedance microphones are not suitable for use with this i.c. Microphones supplied with many cheap cassette recorders, however, can often be ideal.

### APPLICATIONS CIRCUIT

The circuit diagram of a 'baby alarm' is shown in Fig. 4; basically a one-way intercom used to monitor a child in a distant room. IC1 is an SL 6270C set up as previously described. C7 ensures stability by rolling off the gain of the main amplifier of IC1 at high frequencies. D1, R2, C5, and C6 decouple the power supply to IC1. Without this, the power amplifier, IC2, modulates the supply rail sufficiently to cause instability in the system. R3 is included to provide a small offset at pin 5 with respect to pin 4, again helping to prevent internal instability within IC1.

### POWER AMP

IC2 is a simple power amplifier in a standard configuration. Note that the 'M' package (i.e. TBA 820M) should be used, since the TBA 820 has a different package type, incompatible with the given layout in Fig. 5. R6 and C14 provide bootstrapping, C13 provides frequency compensation, C11 reduces the effects of supply ripple, and C15 decouples the loudspeaker. C12 and R5 form a 'zobel' network, which helps to ensure stability when driving into reactive loads, and R4 sets the gain of the power amplifier, decoupled by C10. Finally, VR1 controls the gain of the system, and C9 decouples the power supply.

The circuit is designed to be powered by a 9V battery for safety and convenience, via D2 to protect against incorrect connection. Any type of loudspeaker will suffice, although its impedance should be at least 4 ohms, and preferably 8 ohms or more. A 0V feed for the microphone is provided if required for screening, etc. The microphone should be connected between the two inputs as shown, or between one input and 0V, in which case the unused input should be taken via its input capacitor to 0V. (Never connect pin 4 or 5 directly to 0V; always use a capacitor.) No heatsinking is normally required for IC2. In the interests of stability, it is strongly urged that the layout shown in Fig. 5 is closely adhered to. If the circuit still oscillates, and it isn't because of simple 'howlround' or acoustic feedback, try increasing the values of C6 and C9, change R2 to 330 ohms, and try a new battery in place of the old one. Note that all capacitor values are shown at 25 volt rating; in practice, 16 volt types are equally acceptable.

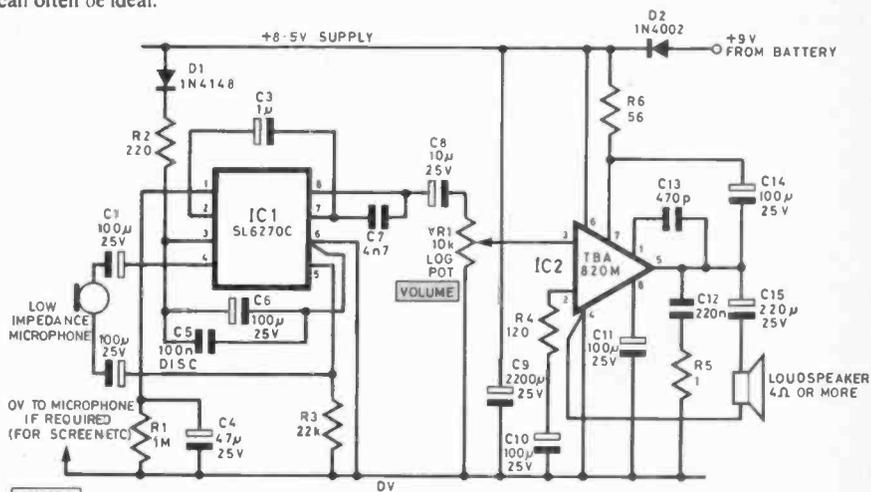


Fig. 4. Circuit diagram of the Baby Alarm

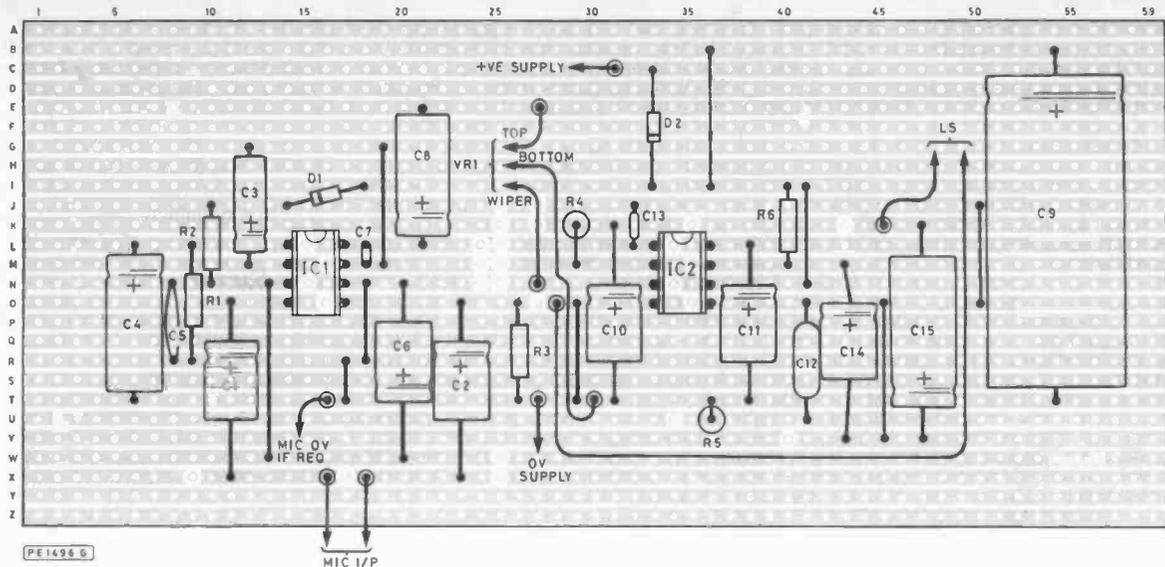


Fig. 5. Veroboard layout for the Baby Alarm

In use, the microphone is normally placed in the child's room, and is connected via screened cable to the unit in the required room; usually this is a kitchen, lounge, or parents' bedroom. The AGC action ensures that the child can be clearly heard, whether he

or she is quietly complaining or shouting the house down! If required, the unit can be operated with the microphone local to the circuitry, and the speaker remote, although the volume will have to be preset, of course.

The SL 6270C will find many uses in public

address, tape recording, and simple telecommunications projects. It can be obtained from **Watford Electronics**, and the TBA 820M can be obtained from **Cricklewood Electronics Ltd.**, 40 Cricklewood Broadway, London NW2 3ET.

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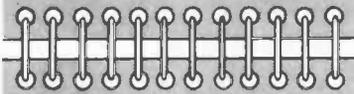
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# INDUSTRY NOTEBOOK

By Nexus



## ET

Convergence was a fashionable catchphrase a few years ago. It foresaw a coming together of discrete electronic technologies to provide powerful integrated systems. The most obvious outcome is Information Technology (IT) which integrated display technology, telecommunications and data processing to spawn a whole new sector of the electronics industry, of which more later.

In the defence field a newly fashionable in-phrase is Emerging Technology (ET) which is viewed by some military experts as a miracle alternative to theatre nuclear weapons. It has always been accepted that NATO forces would be outnumbered in manpower, tanks, guns and aircraft in the event of conflict. As a last resort to prevent catastrophic defeat it would be necessary to use tactical nuclear capability with the consequent risk of escalation to full rather than limited nuclear war.

It has also been argued that numerical advantage of men and materials of the potential enemy ought to some extent be counterbalanced by higher efficiency and technological superiority in one's own forces. ET would stretch this notion to its fullest extent. The brute force of the enemy would be blunted by super-sophisticated weapons of the conventional type.

It sounds good news for the industry. The giants in the defence sector such as Ferranti, GEC, Plessey and Racal together with dozens of smaller companies all stand to gain by a new impetus towards even more advanced systems. Again we see convergence, to integration in a single system of sensors for target acquisition, data processing for analysis, and terminal guidance for liquidation of threat.

Much of the technology is already available and is, in fact, in service. An example is Thermal Observation and Gunnery System (TOGS) being fitted to Britain's Chieftain and Challenger tanks. TOGS provides the ability to detect, track and engage targets by day or night in any

weather without disclosing one's own position. At longer range there are precision guided munitions for artillery, and airborne stand-off weapons with fire-and-forget terminal guidance. Data processing is already commonplace in all the armed services in operational, logistical and administrative duties.

In a sense ET has already emerged but its supporters want it to emerge even more. The danger could come from oversophistication and misplaced confidence in reliability. And while the push-button war might be effective in large set-piece battles, technical superiority was ineffective against a peasant army in Vietnam, remains so in Afghanistan and would be equally so in any brush-fire conflicts involving infiltration, fifth-column support and street fighting.

Whatever the military merits, ET is a short-term political winner. If it led to a nuclear freeze the anti-nuclear doves would be mollified without damaging the morale of the hawks. My own guess is that the nuclear option will be maintained but not expanded while ET will receive a modest boost. But much will depend on the attitude of the new leaders in the Soviet Union and the result of the presidential election in the United States.

## IT

Whereas ET for defence is of relatively low volume and very highly priced, the reverse is true for IT where high volume production and tumbling prices is now the name of the game.

That the great publicity drive for IT has been a staggering success is high-lighted in the nominations for this year's TOBIE Awards. The winners, chosen by ballot among readers of Electronics Times, are to be announced at the All Electronics Show Dorchester Ball on May 2.

Acronym composers at Imperial College must have had quite a struggle to arrive at ALICE (Applicative Language Idealised Computing Engine), an advanced computer nominated in the 'Research Achievement' category. Her distinctive feature is a high degree of parallel, as distinct from serial, processing to give very high operating speeds. ALICE uses the Inmos transputer.

Competing against ALICE are Project Universe, an expanded form of local area networks and an array processor which enables robots to 'see' what they are doing and perform more intelligently.

These are just a sprinkling of the 21 TOBIE contestants but the general thrust is clear. Every product or system is aimed at higher speeds, lower costs, greater productivity. In short, the regeneration of British industry or, from another viewpoint, a further threat to jobs.

But the IT revolution does provide extra work and more jobs. There is plenty of investment and new job opportunities in Scotland's Silicon Glen and reports from the United States suggest a strong black market in some semiconductor devices. Delivery times have lengthened from a few days into months and some short-supply items are said to be commanding as much

as 20 times their list value. Speculative buying in the hope of big profit on re-sale is suspected. Monolithic Memories is but one firm with record order books who are monitoring all incoming orders to determine whether speculators might be distorting their usual projection of future demand. But MM have concluded that order growth is genuinely through demand.

## Big Sister

Social conscience is a burden made even heavier when, after a quick check, I discovered that the Nexus home is nothing less than sexist. The total number of male plugs on my household and workshop appliances outnumber the demure female sockets with which they mate by over three to one.

A ridiculous assertion, of course, but no more silly than many calls for sexual equality from the Equal Opportunities Commission. In terms of numbers, electronic equipment manufacturers have always employed far more women than men, albeit in repetitive assembly work. But if we look in the R & D labs, at installation and commissioning engineers, and at management, males are predominant.

This year's WISE (Women in Science and Engineering) campaign hopes to get more girls in at professional level. At present of all our chartered engineers only one in a hundred is female. Of the new generation of engineering undergraduates at universities only 8.6 percent are female, in polytechnics only 3.2 percent.

Of course these figures cover all engineering disciplines. In electronics there is every reason to suppose that a better balance will be achieved naturally. The possibility of positive discrimination is unhealthy and I feel sure that thinking feminists would prefer employment by merit rather than by quota. So it's really up to the girls themselves. Electronics is a 'natural' for them, the opportunities are there and they only need to work hard at it to increase their numbers. Equal opportunity has existed for years and a *Big Sister* to force the issue is totally unnecessary.

## The Old and the New

Professor Eric Laithwaite, famous for his work on magnetic levitation, has always contended that nature is more skilled at engineering than man. In fact he gets much of his engineering inspiration from the study of evolution, the continuous refinement of living structures over millions of years.

His example reminds us that we should never dismiss or discard earlier work. For instance the 'new' design of satellite communications aeriels now being installed at Ealing and Madley don't use the conventional geometry. Instead they use the Gregorian, found to be more efficient in smaller sizes of dish. The principle is exactly that developed for an optical telescope by James Gregory, a Scottish mathematician who lived in the 17th century.

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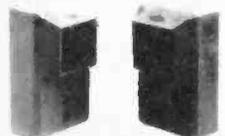


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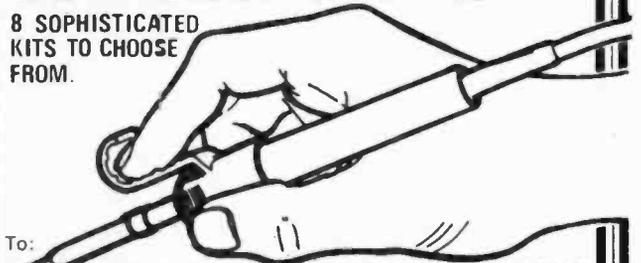
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# Patents Review

Copies of British Patents can be obtained from: The Patent Office, Sales, St. Mary Cray, Orpington, Kent (£1.75); and copies of Foreign Patents can be obtained from The Science Reference Library, 25 Southampton Buildings, London, WC2A 1AJ. (Prices on application.)

## RF KEY-FINDER

European patent item 089667, from Thomas William Nyiri of San Marino, California is a quaint idea with interesting possibilities. The idea is to track down lost keys, purses and wallets by fitting them all with a miniature receiver that produces an audible or visible signal when triggered by a transmitted search signal. Fig. 1 shows the transmitter, which will usually be a handheld battery powered gadget like a TV remote control. Chip 3 produces an r.f. signal on either CB or model-control frequencies. Encoder 4 chops the signal in a pre-arranged code. When the first stage of the receiver shown in Fig. 2 picks up a signal of correct frequency it triggers f.e.t. 9 to switch battery power 10 into the rest of the receiver. Decoder 12 distinguishes between random CB or model transmissions and a wanted search signal. It outputs to amplifier 13 and sound or light generator 14. The idea, of course, is to make the receiver small enough to attach to whatever it is you think you are going to lose. By using different transmission frequencies, or codes, one transmitter can search independently for several lost ob-

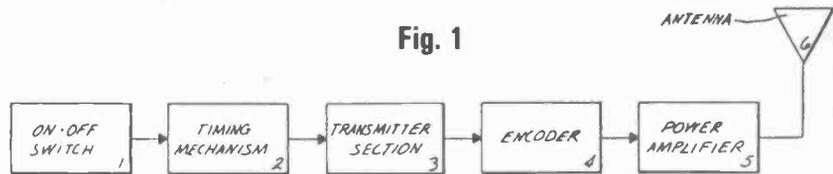


Fig. 1

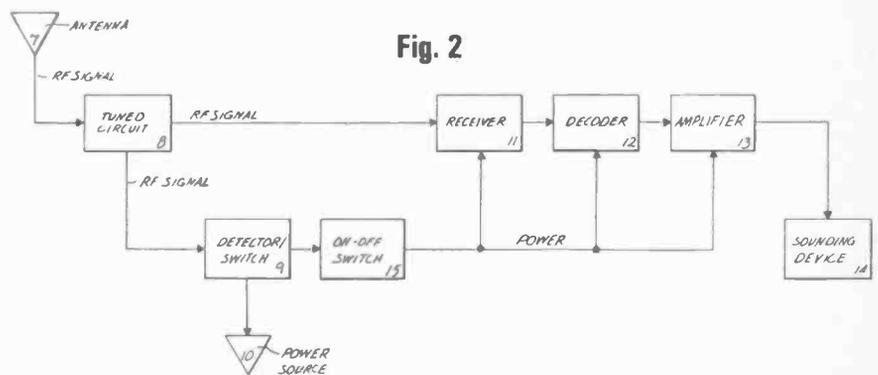


Fig. 2

jects. The patent is rather short on detail but if the gadget could be made cheaply and small enough it would undoubtedly sell

to anyone who routinely loses their car keys five minutes before they are due to leave home.

## WRIST-WATCH THERMOMETER

A new British patent application 2118307 from the Citizen Watch Company of Tokyo suggests that wrist-watches with thermometers built-in may be the next consumer gimmick. A combined watch and thermometer can easily log temperature over a pre-set period of time, storing averages and maximum and minimum values. The snag, say Citizen, is finding an electrical element to measure temperature that is cheap, accurate and reliable. Thermocouples, for instance, are too expensive. A thermistor, a resistor which changes value with temperature, is cheap but difficult to use because the resistance changes value exponentially. Complicated circuits are needed to provide a linear readout. Citizen, in this very lengthy and detailed patent, explain how linearity may be quite simply achieved by using the thermistor to control the frequency of an oscillator circuit.

Fig. 1 shows a CR oscillator circuit, with thermistor 1, capacitor 2, two CMOS inverters 3 and 4 and CMOS NAND gate 5. A

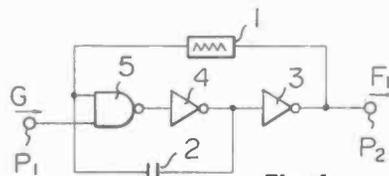


Fig. 1

control signal G is applied to input P1. When signal G is low CR oscillator is switched off. When signal G goes high, CR oscillates to produce pulse signal F1 at terminal P2 of frequency determined by resistance R of thermistor 1. The temperature value can be derived from the pulse rate, but correction is needed to compensate for the non-linear change of resistance. Fig. 2 shows the circuit. The CR oscillator of Fig. 1 is shown at 6, receiving control signals G from circuit 7 and outputting oscillator pulses to frequency divider circuit 8. The division ratio of circuit 8 is varied according to the cumulative number of pulses counted at 9. Variations in the ratio are set at 9 to compensate for the exponential characteristic of the thermistor. So the total pulse count at the end

of a fixed time interval is directly proportional to temperature and is displayed at 11.

Readout will usually be on an LCD which also displays time. Citizen say that this circuit can be manufactured at "very low cost" and with a memory it is possible to arrange for ambient temperature to be measured and memorized at a fixed time each day, along with maxima and minima. The temperature readings taken can also be used to generate temperature compensation data for the clock circuits, to improve time-keeping accuracy.

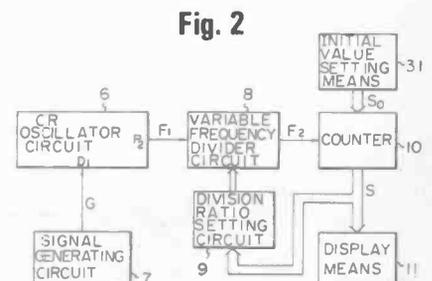


Fig. 2

# TECHNOLOGY UPDATE: SO SMDs

tomorrow's new breed of electronic component

## ARE TODAY'S ELECTRONIC COMPONENTS LIKE THE DINOSAUR—TOO LARGE TO SURVIVE?

IT IS common knowledge that all electronic components, no matter what shape or size, have leads protruding from them . . . *isn't it?* After all, how else can they be soldered to a printed circuit board?

The answer to this question is investigated here, and it reveals a direction in equipment manufacture which is *not* common knowledge. A new technique is emerging; it's called SMA (Surface Mounted Assembly), and with it grows an army of leadless components called SMDs (Surface Mounted Devices). This development was spawned by the electronics industry in the face of fierce competition, and its urgent need to reduce assembly costs. In fact, components as we know them today will not allow further miniaturisation. Conventional devices represent a dead end.

### SURFACE MOUNTED DEVICES

Leadless, surface mounted capacitors and resistors, commonly (and confusingly) called "chips", consist of small rectangular packages. These are of either plastic or ceramic construction, and are metallised at each end. Diodes, although they have a more recognisable body, also have metallised ends instead of leads, and all these devices are soldered by their metallised ends, directly to the *top surface* of the p.c.b.

SMDs have numerous advantages. They are smaller (allowing typically twice the p.c.b. packing density of conventional components), they are cheaper to use in end-product terms, and they are more reliable. Also, the absence of wire leads eliminates the radiating antenna effect that downgrades high frequency/switching performances in conventional components.

A high-performance car radio might comprise well over 500 components, and with such numbers it is easy to see why the SMD's high packing density and low profile appeals to forward-looking equipment manufacturers. Circuit board assembly costs can be as much as 50% lower than those for conventional "inserted" devices, so Mullard claims. The claim that SMDs are very much more reliable is nothing to do with their fabrication technology, but because they do not have to have leads or tags added, and because no lead-bending or cropping takes place during assembly—stages which frequently cause damage.

The Mullard SMD product line already covers some 80% of all component types which, according to the company, account for nearly all potential applications in the emerging digital era.

Who knows, in fifteen years' time, the hobbyist may need a magnifying glass and tweezers to handle components; components which it is already known, will be *too small* to accommodate printed values or colour codes. The development engineer too, will be forced into modular applications, rather than a breadboard approach to design. What else might the hobbyist one day need? A pot of glue!

### GLUE?

The "pick-and-place" machinery used in automated SMA has to include a method of making the devices stay put until soldered. For without leads passing through to the other side of the p.c.b., these tiny devices would slide around during conveyance to the soldering station. The answer is glue. The pick-and-place must first daub a spot of glue on the underside of each component to be mounted, or drop a spot of glue on the p.c.b. itself. These special epoxy adhesives have been developed for short cure time (the boards are passed through an oven prior to soldering) and adequate viscosity.

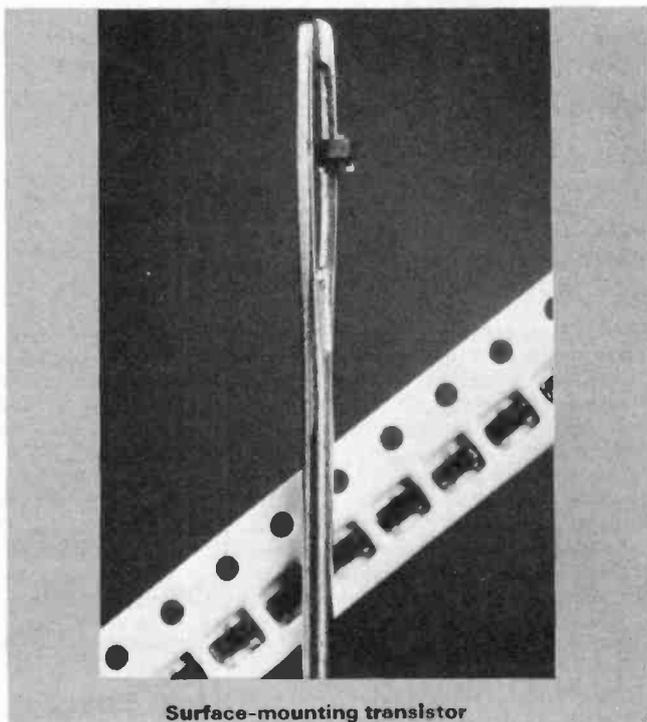
### SURFACE MOUNTED ASSEMBLY

At the heart of the pick-and-place assembly machine is the "pipette". The Mullard system comprises a mechanical jaw for clamping the component to be placed (the terms "place" and "insert" have a sharp distinction now that leadless devices exist). The pipette also incorporates a vacuum sensor which uses an embodied microphone to verify the presence of the component being handled.

These production machines are extremely fast, and may be software or hardware controlled. Reliability is higher here too, it is claimed. A run of 100,000 component placements before a single error occurs is quoted by Mullard as typical, this being 10 p.p.m. as opposed to an often quoted error figure of 1000 p.p.m.

SMDs are supplied on reels of tape containing blister packs, and partial standardisation is already achieved in this area.

Real-estate savings to the manufacturer are considerable, too. SMA machinery occupies far less factory floor space.



Surface-mounting transistor

## TERMINOLOGY

Over the last three or four years these new phrases have crept into the electronics press: "leadless chip carriers", "surface mounted devices" and "SO" devices. The "SO" package for i.c.s was defined by Philips (Mullard's parent company) back in 1967, and it then stood for "Swiss Outline", although the contemporary interpretation is "Small Outline".

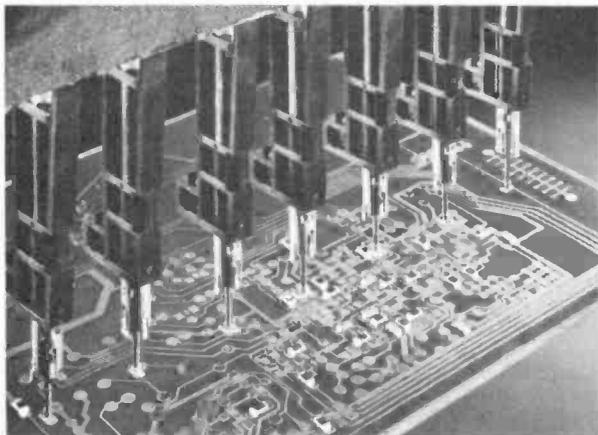
At one time the surface mounted device and the leadless chip carrier were envisaged as exclusively the same thing, but in practice it will be found that surface mounting i.c.s have tabs on them for soldering. The same applies to transistors, although passive components *are* without leads.

## MULLARD

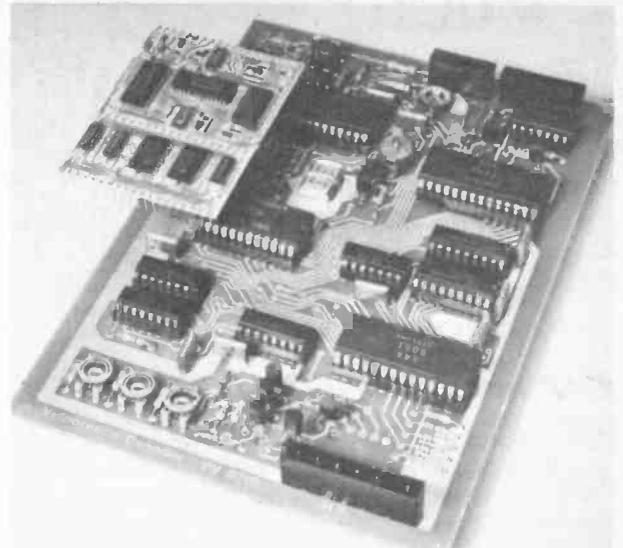
As the reader may have begun to suspect, Mullard has a major involvement in this development. As the UK's largest electronics component manufacturer, its activity in the area of SMD and SMA equipment manufacture virtually represents Europe's only horse in this race, in which Japan looks set for an unassailable lead (the Japanese are said to be producing 6 billion surface mounted resistors a year). Whilst it is not too surprising to learn that in Japan 40% of all electronic equipment already makes use of the technology, nor that Europe is only just beginning to look seriously at it, it is surprising to find reports that the US is still further behind. Now, at least, a source of expertise and hardware, from the devices themselves through to the automatic placement machinery is, in the shape of Mullard Ltd., available in Europe.



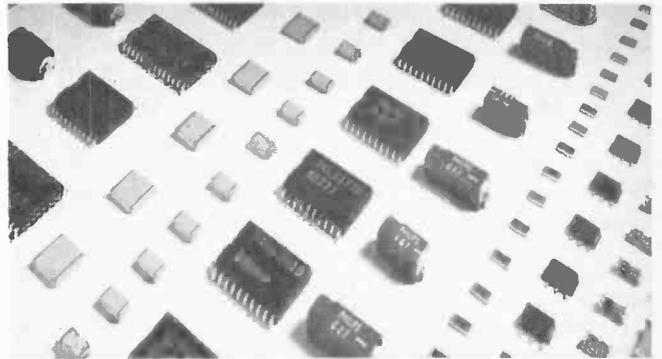
MCM III is a hardware-automatic placement machine accommodating up to 12 placement heads. A typical handling capacity is 200,000 component placements per hour. Photograph courtesy of Mullard Ltd.



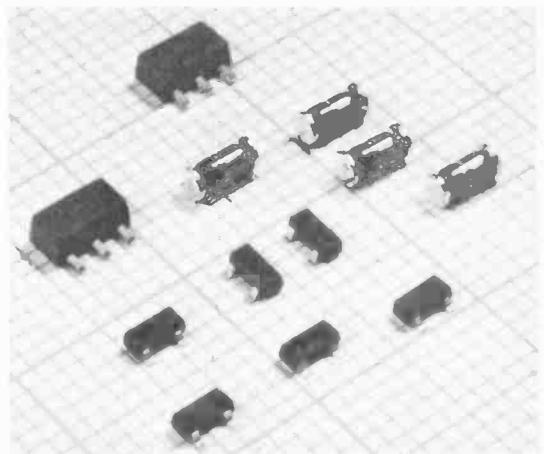
The unique pipettes of the Philips MCM range of automatic SMD placement machines



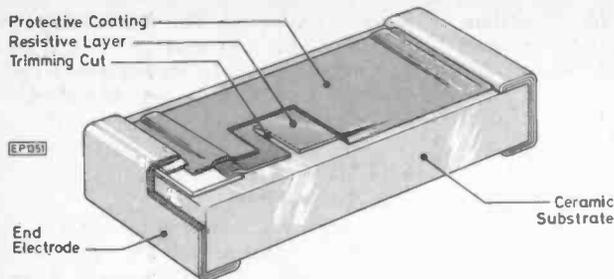
These boards fulfil identical functions. Generally, SMDs require only a third of the board space needed by conventional components. Photograph courtesy of Mullard Ltd. P.c.b. drilling is entirely eliminated



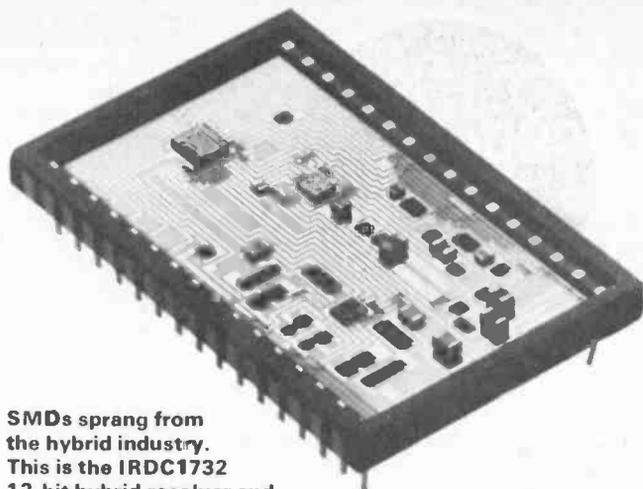
Examples of Mullard range of SMDs, including "chip" resistors, diodes, SOT package transistors, and i.c.s. All these miniature "chip carrier" outlines conform to international standards



A closer look at the SO transistors and diodes



Structure of a SMD, laser trimmed resistor



SMDs sprang from the hybrid industry. This is the IRDC1732 12-bit hybrid resolver and Inductosyn™-to-digital converter (for digital representation of angular or linear measurement). Photograph supplied by Analog Devices Ltd.

## SOLDERING

One of the first questions to spring to mind when looking at a board full of SMDs is, how are they production-soldered when the connections, and the devices, are on the same side? The assembled p.c.b.s shown to the press by Mullard were wave-soldered in the conventional way, but of course the components, it was explained, are designed to survive the wave of solder too. An interesting, and obvious outcome of all this, is that a p.c.b. can be double-sided in terms of both copper tracks and components!

New techniques in wave-soldering have had to be developed because, for example, the components tend to cast a "shadow" in the wave, possibly leaving themselves unsoldered at one end.

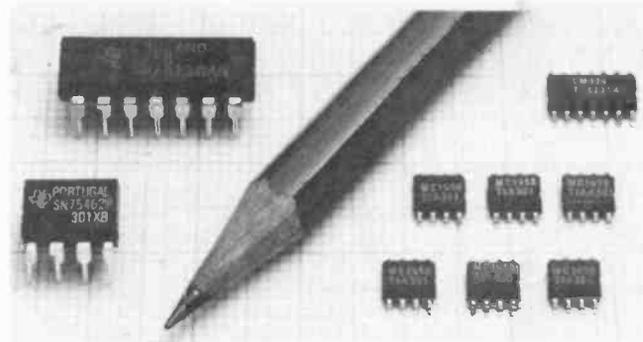
## COST FACTORS

It is all very well the electronics industry concentrating progress on the integrated circuit; moving from MSI to LSI to VLSI etc., but i.c.s apparently account for around only 5% of the total equipment cost in current designs. Interconnect components (approximately 30 passives for each i.c. on average), on the other hand, are reported to account for nearly 25%. Mullard's specialists point out that if the trend towards miniaturisation, lower cost and failure rate, remains focused on i.c.s, a disproportionate cost relationship will soon arise.

It is obviously now necessary to develop the SMD, which, incidentally, was originally devised by the hybrid manufacturing industry for mounting on the surface of substrates, to rationalise equipment costs in the future. Moreover, new products will be possible only because of SMA—portable video equipment already depends heavily on the technique.

## FUTURE

The development is important to industry now, the hobbyist later. But then, a glance through a late sixties copy of PE will reveal life at the dawn of the i.c. Not that long ago really, and today's hobbyist is not so far behind industry.



These SO i.c.s, launched by Texas Instruments less than a year ago, are shown compared to their d.i.l. counterparts. They take up one-third of the board space, and are available in alternative packages to many of TI's more popular i.c.s. These SO packages started life at 1.6 times the cost of their conventional alternatives, but may already be on a price parity

Industry sources suggest that by next year one-quarter of all equipment manufactured will contain SMDs. Another five years, and this figure will be one-half, which represents around 100 billion SMDs worldwide. ★

# BAZAAR

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**SCOPE** Gould 05245A 10MHZ Dual trace hardly used. Probes instr. manual £130. Tel: 0202 886943/887240. R. Tarling, 35 High Street, Wimborne, Dorset BH21 1HR.

**WANTED** manual for Solatron Scope Model CD 1014.2. J. McMahon, 7 The Meade, Chorltonville, Manchester M21 2EA. Tel: (881) 2714.

**ZX-81** 16K RAM, Programs manuals and leads. Open to offers. Tel: Egremont (0946) 821521. Graeme Hodgson, 20 Chaucer Avenue, Orgjill, Egremont, Cumbria CA22 2HB.

**AVO DA.** 116 Digital Multimeter. Hardly used. £65. o.n.o. Buyer collects. B.E. Hull, 21 Courtenay Road, Wantage, Oxon. OX12 7DW. Tel: Wantage 3372.

**BUY:** Acorn Atom disc pack or controller card. Send details to: Tony Dale, 30 Cuffs Road, Christchurch 6, New Zealand.

**ZX-81** 16K with assembler, MCTT monitor, forth, toolkit, flight simulator. £55. Tel: 051-608 8617. D. Stephens, 411 Woodchurch Road, Birkenhead, Merseyside L42 8PF.

**HALL** effect K/Board 83 keys parallel ASCII output metal framed p.c.b. New, unused. £35 inc. (0782) 550684. N. L. Smith, 31 Meadow Avenue, Wetley Rocks, Stoke-on-Trent ST9 0BD.

**HI-RES** graphics board for use with UK101 wanted. Preferably the kind produced by CUA. Hans-Petter Naas, 2450 Rena, Norway.

**TELEQUIP** 43 CRO with manual. Offers. 01-977 1549. John Petherick, 41 Somerset Road, Teddington, Middlesex TW11 8RT.

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## Space Watch...

### THE ISAAC NEWTON TELESCOPE

British astronomers are celebrating 'first light' at the new observatory which is being constructed on the island of La Palma, one of the Canary Islands group. The Isaac Newton 2.5 metre telescope, currently the largest optical telescope that Britain has, is now operational, it is one of a trio of British telescopes now being installed at La Palma; they are being funded by the Science and Engineering Research Council (SERC). These telescopes form the core of a new International Observatory. The official name for the installation is the 'Observatorio del Roque de los Machachos.'

The Isaac Newton telescope was first installed at Herstmonceux, Sussex at the site of the Royal Greenwich Observatory in the late sixties. In the 1970's it was decided by the SERC that the best place for the telescope would be in the northern hemisphere and in 1979 entered into an international agreement with Spain, the United Kingdom, Denmark and Sweden to build telescopes on the Spanish site at La Palma. As part of this agreement Spain was to provide a road to the peak, staff accommodation, power and telephone lines. In return the Spanish astronomers are guaranteed 20 per cent of the observing time. Also to share are the Dutch who are to have 20 per cent of the time on the three British telescopes. The Irish are also partners and would have 27 nights per year on the one metre telescope.

The two telescopes presently installed are a 'one metre' and the Isaac Newton. The third telescope is the William Herschel which has a primary mirror diameter of 4.2 metres, the mirror has just been completed at Grubb Parsons, the famous telescope manufacturers based in Newcastle-on-Tyne. This will be operational in 1986 on La Palma. There are other telescopes at the observatory. The Swedes have installed a 0.6 metre reflector and a solar telescope. There is also an Anglo-Danish transit circle for accurate star positioning.

The new telescopes on La Palma will re-establish the United Kingdom's leading role in optical astronomy and so complement the world-leading position it holds in most of the major branches of astronomy. This applies especially to radio, infra-red, X-ray and theoretical research. For more than three centuries now the Royal Greenwich Observatory has been a centre of excellence in astronomical research. Originally its purpose was to study

the position and apparent motion of the stars. These observations were required to ascertain the longitude on the Earth and Time measurement data.

Since the end of the last century activities were widened to include astrophysics and much ground has been covered since. Indeed several volumes would be needed to give even notes of the work done. It was the inevitable expansion that finally led to the need for the Isaac Newton telescope. The changing emphasis finally led to the transfer of the Royal Greenwich Observatory from the Admiralty to the Science and Engineering Research Council in 1965. Later the Observatory was transferred to Herstmonceux Castle, Sussex. It has of course retained the title of Royal Greenwich Observatory. This extended the telescope facilities throughout the whole of the astronomical community.

The results have been quite outstanding, the extended facilities have helped to develop some of the world's most sensitive detectors of light for use on telescopes, providing a continuity of development that university research departments cannot always maintain. Of the contribution to astrophysics of course there is a formidable record. In recent years astrophysicists have become interested in objects which are very faint optically. Much of this work has appeared in *Spacewatch*. Many have been found by radio astronomy, satellites and probes. Sometimes this is because the sources, such as quasars, are so far away or because they are so faint, the optical telescope constantly needs updating.

Of course most observations of very dim objects have to be carried out using large telescopes. Many of the observations have been made with telescopes in the USA and in Australia. An Anglo-Australian telescope is based in New South Wales. There is still work to be done by large earth-based telescopes but they must be at suitable sites. The particular demands that are determined by the nature of the research must be observed if the results are to be valid. In many cases satellites have confirmed the accuracy of data gathered on Earth. With the aid of the sophisticated techniques available to earth-based telescopes, whose sensitivity has been enhanced thereby, there is the benefit of extra-terrestrial back-up.

The 4.2 metre William Herschel telescope was designed for La Palma. This telescope has special light detectors which have been supplied by the Royal Greenwich Observatory and will ensure a sensitivity second to none. This is one of the reasons that the SERC are funding this project. The decision to make this site available to all researchers, from anywhere in the world, is the truly democratic way of knowing more about our place in the Universe.

It is to this end also that the new large infra-red telescopes have been funded. These have the Island of Hawaii as their site. The parent organisation of the large infra-red instrument, the Royal Observatory of Edinburgh, has already shown its worth and has also demonstrated how the techniques of remote control can be such that the researcher does not have to be present at the telescope site. The control and remote viewing can be done from the comfort of the home station. Much of this has been described in detail in previous

issues of *Spacewatch*. The other telescope at Hawaii is the 'millimetre-wave' telescope. This will help to resolve the unexplored area of the spectrum between infra-red and radio wavelengths.

### EXTRA-TERRESTRIAL OBSERVATION

It is necessary to make proper reference to the extra-terrestrial activity. The observations from the Earth are complemented by instruments above the atmosphere. This covers a whole new field because the absorption by the atmosphere is no longer an obstacle. The SERC has supported the researchers in universities. This has been put into effect at Leicester University and University College, London. These two have contributed very well as pioneers in X-ray astronomy.

British astronomers have also a large stake in satellites investigating the Universe in the infra-red and ultra-violet. This was the IRAS and the International Ultra-Violet Explorer. The data from IRAS, which has now ceased its mission, will take a decade to analyse.

On the interpretive side university astronomers and researchers of the RGO and the ROE are keeping the UK at the forefront in theoretical astronomy especially cosmology which deals with galaxies, quasars within them and more recently the black holes. So the new International Observatory will take learning into the next century.

### THE WILLIAM HERSCHEL TELESCOPE

This was named after the Musician/Astronomer. He was the remarkable man who in 1781 discovered the planet Uranus. Of course originally it was called Herschel, after its discoverer. His skill as a telescope maker was quite exceptional. The telescope that bears his name in commemoration is very much larger than those which he made. The present telescope has a primary mirror which is 4.2 metres in diameter. It is the third largest in the world. So the man who should be called the father of observational cosmology will be honoured again in tribute by the users of this instrument. The exceptional viewing site together with the use of the most modern light detectors will give this telescope the advantage over others. Although its mirror is smaller than those of the American or Russian telescopes it will be able to see farther than either.

The telescope itself, which was once the only step between the observer and his target, has to use intermediate apparatus for research purposes. Again modern techniques dispense with the human being and give the human a more accurate picture of what is taking place. This instrumentation is superior indeed to the human. It does however furnish data which enables the human to think with reliable 'known' information. So it is now possible to determine a situation without the need to 'see' directly. Fortunately it is possible to expound a good deal about these techniques, they will be explained more fully in a forthcoming issue of *Spacewatch*.

## Frank W. Hyde

# INTRODUCTION TO DIGITAL ELECTRONICS

MICHAEL TOOLEY BA DAVID WHITFIELD MA MSc CEng MIEE

## O & A Level Part Eight

WE shall begin this month with a practical example of the use of J-K bistables and logic gates in the form of a traffic lights simulator. For simplicity we shall only concern ourselves with the most basic form of traffic lights once encountered at road works, i.e. those which consist of two lights only; red and green. This is a system with which most of us are all too familiar. Even so, it is worth reminding ourselves of the sequence of events in such a system.

Let us assume that the traffic lights are labelled TL1 and TL2. The sequence of operation of the lights should follow the pattern:—

TL1	TL2
red	red
red	green
red	red
green	red
red	red
etc.	etc.

In fact there will be two lamps fitted in each traffic light unit. If we refer to these separately as TL1(red), TL1(green), etc. and use a 1 to denote 'light on' and a 0 to denote 'light off', we arrive at something which is more akin to a truth table as shown in Table 8.1.

TL1		TL2	
RED	GREEN	RED	GREEN
1	0	1	0
0	1	1	0
1	0	1	0
1	0	0	1
1	0	1	0
etc	etc	etc	etc

Table 8.1. Truth table for the Traffic Lights

There are two things to note from this:—

1. The red and green lamps in either traffic light are always complementary. Thus:

$$TL1(\text{red}) = \overline{TL1(\text{green})}$$

$$TL2(\text{red}) = \overline{TL2(\text{green})}$$

2. The sequence of operation consists of four distinct states repeated over and over again.

For the purpose of this example we shall assume that each state occupies the same time interval. In practice, and dependent upon the traffic flow and separation of the traffic lights, this may not be the case. In any event, we shall require a clock in order to define our basic unit of time, i.e. the time interval for any one of the states in the sequence. The clock can take the form of any one of the several circuits previously described but, for convenience, we shall use the clock oscillator provided within the Logic Tutor. This will give us a basic time interval (clock period) of approximately 1 second: long enough for us to see what is happening, but far shorter than would be acceptable in practice!

The four logic states, corresponding to those shown in the Table 8.1, can be generated by two J-K bistables in conjunction with some additional logic. The J-K bistables operate as binary dividers (as discussed in Part Seven), and the additional logic is used to decode the bistable outputs (Q and  $\bar{Q}$ )

into the required logic 1 and logic 0 states to activate the four lamps: TL1(red), TL1(green), TL2(red), and TL2(green). The basic arrangement of the logic control system is shown in Fig. 8.1.

The four states produced by the two bistables will follow the normal binary counting sequence. If the bistable outputs are labelled Q1 (LSB) and Q2 (MSB) we arrive at the sequence:—

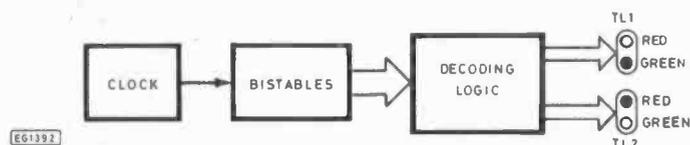
Q2	Q1
0	0
0	1
1	0
1	1

Combining this sequence with the truth table which we saw earlier gives the complete truth table shown in Table 8.2. Here we have shown 'inputs' from the simple binary counter and 'outputs' required from the decoding logic. Now we are confronted with the problem of what must go into the decoding box!

INPUTS TO DECODER		OUTPUTS FROM DECODER			
Q2	Q1	TL1 (RED)	TL1 (GREEN)	TL2 (RED)	TL2 (GREEN)
0	0	1	0	1	0
0	1	0	1	1	0
1	0	1	0	1	0
1	1	1	0	0	1

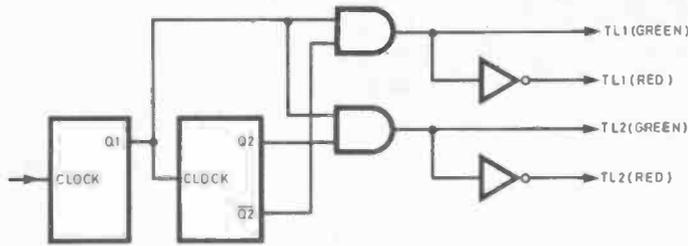
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Table 8.2. Complete truth table

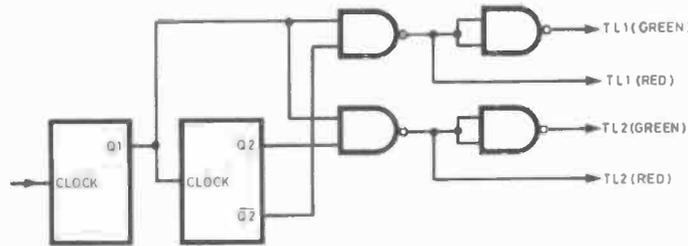


EG1392

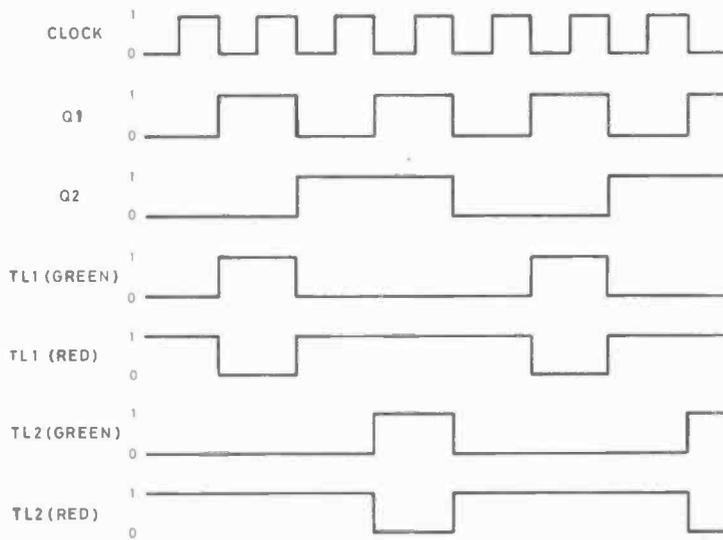
Fig. 8.1. Basic block schematic of the traffic light simulator



**Fig. 8.2. Logic arrangement of the traffic light simulator**



**Fig. 8.3. Improved version of Fig. 8.2**



**Fig. 8.4. Timing diagram for the traffic light simulator**

If we concentrate on the green lamps only (remember that the red lamps are always the opposite) we can readily develop the Boolean expressions from the truth table:—

$$TL1(\text{green}) = Q1 \cdot \overline{Q2}$$

and

$$TL2(\text{green}) = Q1 \cdot Q2$$

The red lamps are simply the complement of the above:—

$$TL1(\text{red}) = Q1 \cdot \overline{Q2}$$

and

$$TL2(\text{red}) = \overline{Q1} \cdot Q2$$

Again, concentrating on the green lamps initially, TL2(green) can be generated very easily by applying the Q1 and Q2 outputs to an AND gate.

For TL1(green), however, we will require Q1 to be AND'ed with  $\overline{Q2}$ . Happily, this is no great problem since our J-K bistable provides us with a  $\overline{Q}$  output! We can now, tentatively at least, sketch out the logic arrangement of our traffic lights controller, adding inverters between the red and green outputs. This arrangement is shown in Fig. 8.2.

Rather than use a mixture of AND gates and inverters (which would require two integrated circuits in the decoding section) we could just use one quad two-input NAND i.c., as shown in Fig. 8.3.

The circuit can now be assembled on the Logic Tutor. Insert the 7473

dual J-K bistable into socket A and the 7400 quad two-input NAND into socket B. Carefully ensure that pin 1 aligns with socket 1 in each case. The following links should then be connected:—

- A1 to clock (clock input)
- A2 to A3
- A3 to A16
- A4 to +5V (supply)
- A5 to A14 (Q1)
- A6 to A7
- A7 to A12
- A10 to B14 ( $\overline{Q2}$ )
- A11 to B2 (Q2)
- A12 to logic 1
- A13 to 0V (supply)
- A14 to B1
- A16 to logic 1
- B1 to B15
- B3 to B4
- B4 to B5
- B5 to D4 (TL2(red))
- B6 to D3 (TL2(green))
- B7 to 0V (supply)
- B10 to D1 (TL1(green))
- B11 to D2 (TL1(red))
- B12 to B11
- B13 to B12
- B16 to +5V (supply)

Total of 24 links.

The keen student will doubtless wish to further develop the simulator. The following exercises are suggested:—

1. Incorporate extra gating so that a red warning light is available to the workmen which indicates that either one of the traffic lights is showing green.
2. Improve the operation of the lights by increasing the period for which a green light shows. Make this equivalent to two clock cycles. (Hint: It will be necessary to use a further 7473 J-K bistable).
3. Devise a system for controlling three lamps in each traffic light obeying the following sequence:—

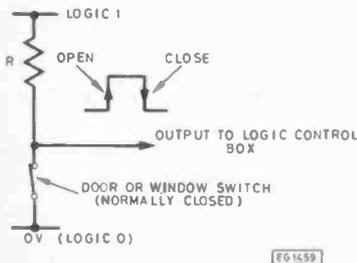
TL1	TL2
red	green
red/amber	amber
green	red
amber	red/amber
red	green
etc.	etc.

4. Devise an arrangement for controlling a 'Pelican' pedestrian crossing. This type of crossing uses a conventional three-lamp traffic light to control vehicles and a two-lamp light to control pedestrians, with an audible output during the period for which the pedestrian light is a continuous green.

## INTRUDER ALARM FOR THE ELECTRONIC SHOP (A practical design example)

As a 'grand finale' in the use of TTL, we have included an example of the design of a simple intruder alarm for the electronic shop which we first met in Part Two. This example has been chosen so that it illustrates many of the logic elements and techniques previously discussed.

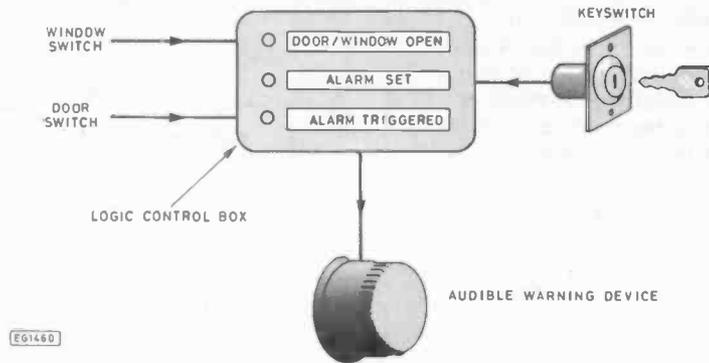
Let us imagine that the owner of the shop requires an intruder alarm to protect the premises during the hours in which the shop is closed. The shop is to be fitted with magnetic window and door switches. For the purpose of this example we will assume that only two switches have been fitted, although in practice it would be a fairly simple matter to add as many additional switches as required. The switches are a type which open whenever the door or window is open, and close whenever the door or window is closed. These "normally closed" switches can be arranged to generate a 0→1 edge whenever the respective door or window is opened by means of the arrangement shown in Fig. 8.5.



**Fig. 8.5. Method of generating a pulse when a window or door is opened**

The intruder alarm is to have a control panel located just inside the door (so that it remains visible from the outside), and a keyswitch is to be placed in the wall adjacent to the door. The shopkeeper requires that a warning light be incorporated in the control panel to remind him that either the door or the window has been left open, thus enabling him to check the state of the premises at the end of the day before locking the door and setting the alarm.

Once triggered by an intruder, the alarm is to activate an audible warning device which is to be repeatedly pulsed on and off. For test purposes, when the audible warning device is temporarily disconnected, a further warning light is to be incorporated into the control panel to show that the alarm has been



**Fig. 8.6. Essential components of the intruder alarm for the electronic shop**

set off. The exterior keyswitch is used to set the alarm to the active state and to reset or disable it before entering the premises. The switch is connected to produce a logic 1 in the set/active condition and logic 0 in the reset/disabled position. The keyswitch is to activate a further warning light so that the shopkeeper is aware of the state of the alarm before unlocking the door.

The essential components of the system are shown in Fig. 8.6. Having established the operational features and nature of the external components, we shall now concentrate on the contents of the logic control box. This is where our experience in digital electronics can really be put to the test! In order to keep things simple we shall follow the design process through stage by stage and readers may wish to use the Logic Tutor to verify each section in turn. We shall start by combining the window and door switches but, before we do, it is a good idea to list the functions of the various switches and indicators that we will be using on the Logic Tutor:

S1	window switch	(logic 1 when window open)
S2	door switch	(logic 1 when door open)
S3	alarm set/reset	(logic 1 to set, 0 to reset)
D1	door/window open	
D2	alarm set (active)	
D3	alarm triggered	

The logic outputs from the window and door switches, S1 and S2 respectively, need to be combined in an OR gate in order to provide a logic 1 output whenever either or both of them is open. This could be carried out quite

simply using a single two-input OR gate, as shown in Fig. 8.7.

Before making a final decision as to which type of gate we should employ, it is worth considering the requirements of the next stage in the logic system. This would have to be a



**Fig. 8.7. Method of combining window and door open signals**

bistable element simply because an essential property of an intruder alarm is that it "remembers" that it has been triggered, providing a warning until someone arrives to disable it. Almost any type of bistable which has a CLEAR or RESET input would be suitable. We shall settle for a simple 7474 D-type. Remember that, with a D-type bistable, data (in the form of a logic 0 or logic 1) is transferred into the bistable when there is a change of state at the clock input. Such a change can either be positive going (0→1) or negative going (1→0), depending upon the internal logic of the bistable. With the 7474 clocking occurs on a rising clock edge, and thus a 0→1 transition is required from the previous logic gate.

An OR gate produces a 0→1 output whenever either one of its inputs is taken to logic 1. A NOR gate, on the other hand, produces an opposite, 1→0, transition under similar circumstances. Thus the OR gate is to be preferred.

Now we shall turn our attention to the bistable stage itself. The state of the Q output indicates whether, or not, the alarm has been triggered and thus, initially at least, the Q output should be logic 0. To ensure that it is, we can use the CLEAR input; this is simply connected directly to the keyswitch which provides logic 0 to reset the alarm.

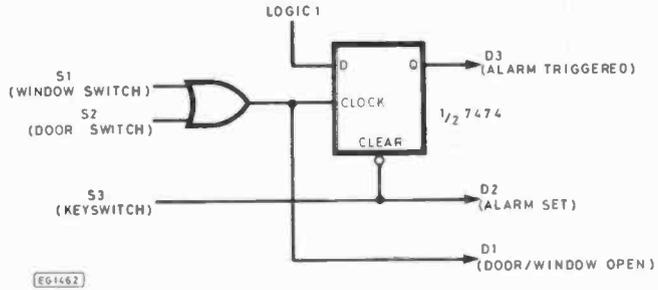
(Note that the 7474 has a CLEAR input which is "active low"). The DATA input must be connected to logic 1 so that a logic 1 will be transferred to the Q output whenever a negative going clock input appears (i.e. when a window or door is opened).

The 'alarm set' indicator, D2, can simply be connected to the output of the keyswitch, S3, whilst the 'alarm triggered' indicator, D3, is taken directly from the Q output of the bistable. In a practical circuit, due to current sourcing limitations, such an indicator should be connected between the positive supply and  $\bar{Q}$  output. The Logic Tutor's indicator diodes (D1 to D4) are, however, already buffered and may be used directly. The arrangement thus far is shown in Fig. 8.8.

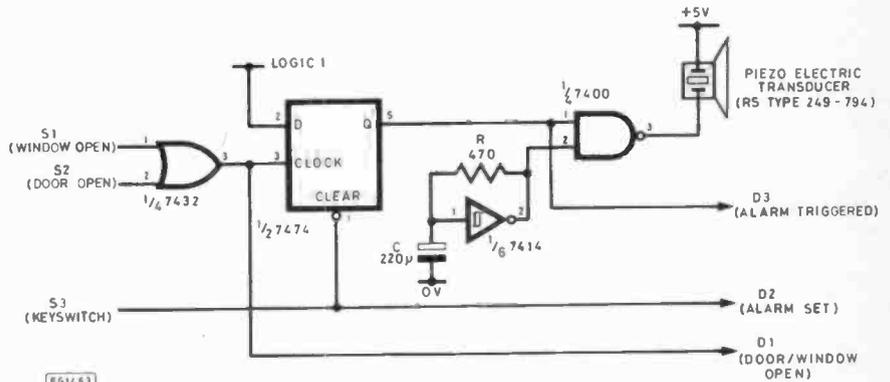
The final stage is to provide an audible warning indication which is capable of being pulsed on and off. On the Logic Tutor we shall use a simple piezoelectric transducer to simulate such a device. Low power transducers, particularly those which are p.c.b. mounted, consume currents as low as 10mA or less from a nominal 5V supply, and may thus be connected directly to the output of a conventional TTL gate. In this respect, they should be treated in the same manner as an l.e.d. load, i.e. connected from the +5V supply to the output of the gate. In a practical circuit, a buffer would be required in order to sink sufficient current to activate a high output alarm transducer.

At this point our design strategy can be usefully changed so that we now work backwards from the output to the bistable stage. The transducer will be connected between the output of the final gate and the positive supply, thus a logic 0 output from the gate will be necessary in order to activate the alarm. The final gate must therefore be an inverting type (unless we use the  $\bar{Q}$  output from the bistable!). If the gate is a two-input NAND, one input can be taken from the Q output of the bistable and the other can be supplied from a simple Schmitt TTL oscillator of the type which we met in Part Six. The timing components (resistor and capacitor) can be chosen so as to produce an output at an appropriate frequency in the range 1Hz to 4Hz.

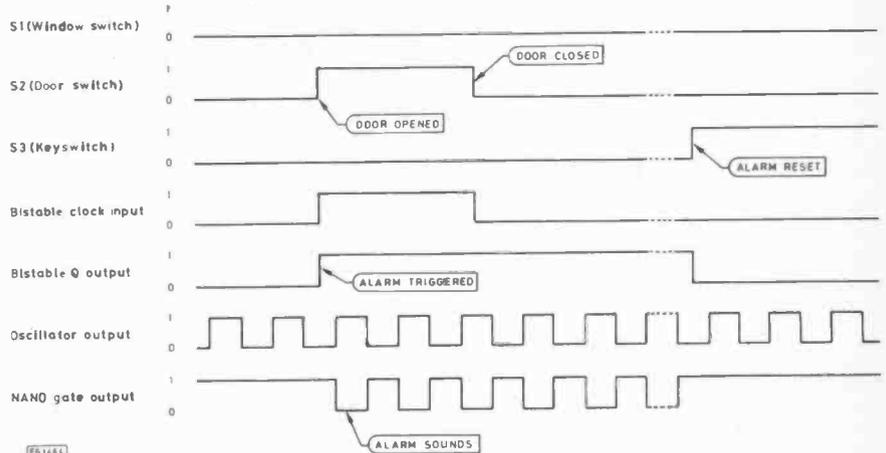
The final circuit of the intruder alarm is shown in Fig. 8.9 and the relevant timing diagram has been shown in Fig. 8.10. It must be stated that the alarm does not provide all of the functions which one might expect to be present on a proprietary security system.



**Fig. 8.8. Intruder alarm bistable arrangement**



**Fig. 8.9. Final circuit of the intruder alarm**



**Fig. 8.10. Timing diagram for the intruder alarm**

To simulate the complete intruder alarm system, insert 7432, 7474, 7400 and 7414 i.c.s respectively in sockets A, B, C and E of the Logic Tutor. In each case check that the device has been inserted with the usual orientation, i.e. pin-1 to socket 1. The following links are now required:

- A1 to S1 (window switch)
- A2 to S2 (door switch)
- A3 to B3
- A7 to 0V (0V)
- A16 to +5V (positive supply)
- B1 to S3 (alarm set/reset)
- B2 to logic 1
- B3 to D1 (door/window open indicator)

- B4 to logic 1
  - B5 to D3 (alarm triggered indicator)
  - B7 to 0V (0V)
  - B16 to +5V (positive supply)
  - C1 to B5
  - C2 to E2
  - C3 to piezoelectric transducer (-ve)
  - C7 to 0V (0V)
  - C16 to +5V (positive supply)
  - E1 to E2 via 470 ohm resistor
  - E1 to 0V via 220µF capacitor
  - E7 to 0V (0V)
  - E16 to +5V (positive supply)
  - S3 to D2 (alarm set indicator)
  - +5V to piezoelectric transducer (+ve)
- (Total of 23 links)

# DIGITAL ELECTRONICS

Readers may like to develop and extend the circuit incorporating some, or all, of the following suggested modifications:

1. Re-design the logic arrangement in order to replace the OR gate with the three unused NAND gates.
2. Add an input from a pressure sensitive mat to be placed behind the door. Assume that the mat has a 'normally open' switch. One of the unused inver-

ters may be useful here!

3. Add an extra switch (to be located on the logic control panel) which allows the alarm to be tested without having to disconnect the audible warning device. The switch is to be a pushbutton type and should be used in conjunction with the unused bistable.
4. Add an extra output to activate an external alarm bell via a relay. The alarm bell is to be

operated from a 12V battery (also external) and is to continue to operate in the event of an intruder gaining access to the premises and cutting the alarm bell connection to the control box.

**Although this is the final part of our course, to complement the series, we'll be looking at CMOS devices next month and another Digital Project, the Oscilloscope Calibrator.**

## QUESTIONS

If you have any questions or queries you would like answered regarding our Digital Electronics series we would be pleased to receive them at our Editorial offices. All questions must be related to the course and we will publish as many questions and answers as possible. Also if you have any comments or observations about any part of the course we would be pleased to receive them.

The address to write to is: Practical Electronics, Digital Electronics Questions, Westover House, West Quay Road, Poole, Dorset BH15 1JG.

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# MICRO-BUS

## and MICROPROMPT

Appearing every month, Micro-Bus now presents ideas, applications and programs for the most popular micro-computers and all micro-related projects so far published in PE. Ideas must be original, and payment will be made for any contribution featured.

### NEW LOGIC TESTER

Sir — I am a regular reader of *Practical Electronics* and followed the early series of articles on interfacing the CompuKit with great interest. One of the programs (UK 101 Logic Tester) given back in the February '81 issue proved quite helpful in getting to grips with the PIA. However, after a while a number of shortcomings became apparent, namely that it only polled port A, and the rate at which it did this was fairly low. The program enclosed solves both problems in that it polls both ports, and because it is in machine code, polls the ports very rapidly and displays the inputs on the screen.

The program, which operates under a 'Cegmon' monitor, fits neatly into page two from 0236 and leaves seven free bytes below the basic workspace. The program once loaded into memory is run by typing '0236G'. The sequence of events is then: the screen is cleared and the words 'PORT A' and 'PORT B' are displayed, the PIA is then configured so that all of the lines are set to input, next the input at port A is stored and each bit displayed (as with the basic program), the same is done for the input at port B, then checks for 'CTRL C' and 'CTRL A' are made before looping back to poll port A. By pressing 'CTRL C' the program may be stopped, and by pressing 'CTRL A' the PIA may be reconfigured; this may be useful if the reset button on the decoding module had been pressed.

As the program uses a number of sub-routines peculiar to 'Cegmon', it will not, without modification, run under another monitor. However, should anyone require a fully portable version located at 0300 onwards, I would be pleased to send them a copy of the listing. (via the editor of PE).

As an extra, altering the contents of location 029F will change the rate at which the ports are polled.

Joseph Arrowsmith,  
London

### CEGMON PIA LOGIC TESTER

```

0235
0236 20 59 FE JSR FE59
0239 A9 50 LDA 50
023B 8D 12 D2 STA D212
023E 8D 92 D2 STA D292
0241 A9 4F LDA 4F
0243 8D D2 STA D213
0246 8D 93 D2 STA D293
0249 A9 52 LDA 52
024B 8D 14 D2 STA D214
024E 8D 94 D2 STA D294
0251 A9 54 LDA 54
0253 8D 15 D2 STA D215
0256 8D 95 D2 STA D295
0259 A9 41 LDA 41
025B 8D 17 D2 STA D217
025E A9 42 LDA 42
0260 8D 97 D2 STA D297
0263 A9 00 LDA 00
0265 8D 9D EF STA EF9D
0268 8D 9F EF STA EF9F
026B 8D 9C EF STA EF9C
026E 8D 9E EF STA EF9E
0271 A9 FF LDA FF
0273 8D 9D EF STA EF9D
0276 8D 9F EF STA EF9F
0279 A9 18 LDA 18
027B 8D F1 02 STA 02F1
027E 20 94 FB JSR FB94
0281 AD 9C EF LDA EF9C
0284 8D 35 02 STA 0235
0287 A0 10 LDY 10
0289 20 BF 02 JSR 02BF
028C A9 98 LDA 98
028E 8D F1 02 STA 02F1
0291 A0 10 LDY 10
0293 AD 9E EF LDA EF9E
0296 8D 35 02 STA 0235
0299 20 BF 02 JSR 02BF
029C 98 TYA
029D 48 PHA
029E A0 08 LDY 08
02A0 20 E1 FC JSR FCE1
02A3 68 PLA
02A4 A8 TAY
02A5 A9 FE LDA FE
02A7 8D 00 DF STA DF00
02AA 2C 00 DF BIT DF00
02AD 70 0D BVS 02BC
02AF A9 FD LDA FD
02B1 8D 00 DF STA DF00
    
```

Store for port inputs.

Clear screen.

Put 'PORT A' and 'PORT B' on the screen.

Access data direction register on port A.

Access data direction register on port B.

Set data direction for input on port A.

Set data direction for input on port B.

Code for peripheral register A.

Code for peripheral register B.

Alter subroutine to print up contents of port A.

Do 'CTRL C' check.

Collect input on port A.

Store input at 0235.

Go to subroutine to determine which bits are on.

Alter subroutine to print up contents of port B.

Collect input on port B.

Store input at 0235.

Go to subroutine to determine which bits are on.

Transfer Y register to Accumulator.

Push Accumulator onto stack.

Y register holds delay length.

Do 'DELAY2'.

Pull Accumulator off stack.

Transfer Accumulator to Y register.

Check for 'CTRL A', if not pressed JMP 0279, if pressed do JMP 0263 to reconfigure ports.

02B4	2C	00	DF	BIT	DF00	
02B7	70	03		BVS	02BC	
02B9	4C	63	02	JMP	0263	
02BC	4C	79	02	JMP	0279	
02BF	20	EB	02	JSR	02EB	Display Bit 0.
02C2	6A			ROR	A	Move Bit 1 to Bit 0.
02C3	20	EB	02	JSR	02EB	Display Bit 1.
02C6	6A			ROR	A	Move Bit 2 to Bit 0.
02C7	6A			ROR	A	
02C8	20	EB	02	JSR	02EB	Display Bit 2.
02CB	6A			ROR	A	Move Bit 3 to Bit 0.
02CC	6A			ROR	A	
02CD	6A			ROR	A	
02CE	20	EB	02	JSR	02EB	Display Bit 3.
02D1	6A			ROR	A	Move Bit 4 to Bit 0.
02D2	6A			ROR	A	
02D3	6A			ROR	A	
02D5	20	EB	02	JSR	02EB	Display Bit 4.
02D8	2A			ROL	A	Move Bit 5 to Bit 0.
02D9	2A			ROL	A	
02DA	2A			ROL	A	
02DB	2A			ROL	A	
02DC	20	EB	02	JSR	02EB	Display Bit 5.
02DF	2A			ROL	A	Move Bit 6 to Bit 0.
02E0	2A			ROL	A	
02E1	2A			ROL	A	
02E2	20	EB	02	JSR	02EB	Display Bit 6.
02E5	2A			ROL	A	Move Bit 7 to Bit 0.
02E6	2A			ROL	A	
02E7	20	EB	02	JSR	02EB	Display Bit 7.
02EA	60			RTS		Return to main program.
02EB	29	01		AND	01	Mask off top 7 Bits.
02ED	18			CLC		
02EE	69	30		ADC	30	Add ASCII character offset.
02F0	99	18	D2	STA	D218,Y	Print to screen.
02F3	88			DEY		Point STA D218,Y to the next print location.
02F4	88			DEY		
02F5	AD	35	02	LDA	0235	Collect input data from storage at 0235, and return to main subroutine.
02F8	60			RTS		
02F9	00			BRK		
02FA	00			BRK		

## BASIC LISTING

10 DATA 32,89,254,169,80,141,18,210  
 20 DATA 141,146,210,169,79,141,19,210  
 30 DATA 141,147,210,169,82,141,20,210  
 40 DATA 141,148,210,169,84,141,21,210  
 50 DATA 141,149,210,169,65,141,23,210  
 60 DATA 169,66,141,151,210,169,0,141  
 70 DATA 157,239,141,159,239,141,156,239  
 80 DATA 141,158,239,169,255,141,157,239  
 90 DATA 141,159,239,169,24,141,241,2  
 100 DATA 32,148,251,173,156,239,141,53  
 110 DATA 2,160,16,32,191,2,169,152  
 120 DATA 141,241,2,160,16,173,158,239  
 130 DATA 141,53,2,32,191,2,152,72  
 140 DATA 160,8,32,225,252,104,168,169  
 150 DATA 254,141,0,223,44,0,23,112  
 160 DATA 13,169,253,141,0,223,44,0  
 170 DATA 223,112,3,76,99,2,76,121  
 180 DATA 2,32,235,2,106,32,235,2  
 190 DATA 106,106,32,235,2,106,106,106  
 200 DATA 32,235,2,106,106,106,106,32  
 210 DATA 235,2,42,42,42,42,32,235  
 220 DATA 2,42,42,42,32,235,2,42  
 230 DATA 42,32,235,2,96,41,1,24  
 240 DATA 105,48,153,24,210,136,136,173  
 250 DATA 53,2,96,0,0,0,0  
 260 FORX=566TO762:READA:POKEX,A:NEXT  
 270 POKE11,54:POKE12,2:X=USR(X)

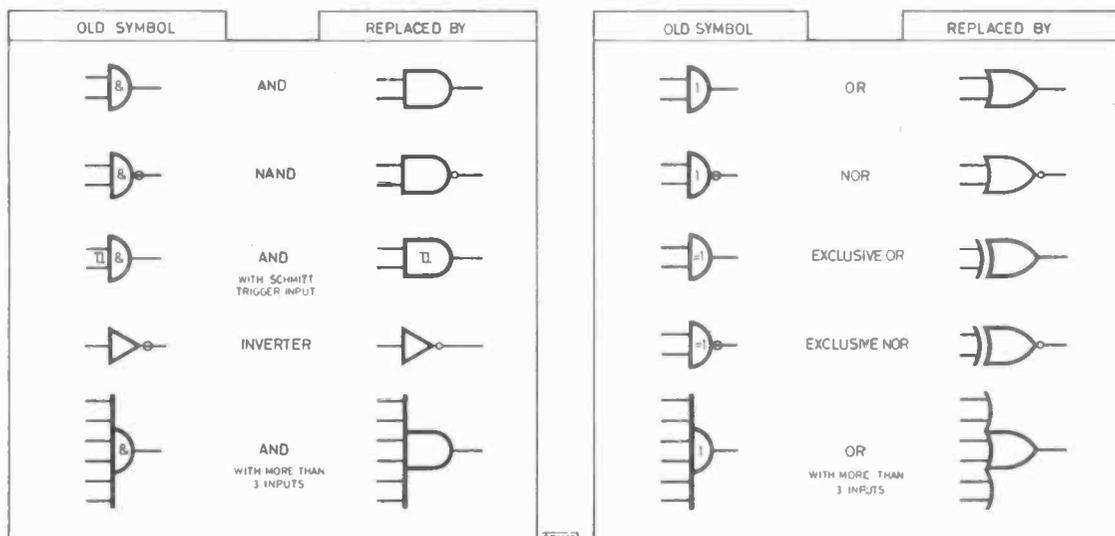
### CONTROLS

- 1) To start the program enter the monitor and type "0236 G".
- 2) Pressing "CTRL C" at any time will cause a warm start.
- 3) Pressing "CTRL A" at any time will cause the PIA to be configured for input. This may be used after the PIA has been reset.
- 4) The sampling rate may be changed by altering the value stored at location 029F. '00' gives a high sample rate whereas 'FF' gives a low rate.

It is emphasised that material presented in Micro-Bus has not necessarily been proved by us. Neither can compatibility with all generations of the computer equipment to which it relates be guaranteed.

Software and hardware designs submitted should be accompanied by a declaration to the effect that it is the original work of the undersigned, and that it has not been accepted for publication elsewhere.

## LOGIC SYMBOLS



# Simple PSU

STEPHEN IBBS

WHEN designing this power supply, I considered adding over-voltage protection, various forms of current limiting and alarms, but experience has shown that these can be more trouble than they are worth. Thus the design offered here has no embellishments, nor is it a revolutionary design. What it does offer is a simple to build, relatively cheap, simple to use power supply with some options open for variation.

Over a period of time it was found that the voltage range most used is 5 to 12 volts, with occasional drops to 2V to test i.e.d.s. Current requirements rarely exceeded 1 amp, so with these criteria in mind, various regulators were looked at, and finally the LM317 was settled upon. I selected the 317K which is capable of delivering 1.5A, but the p.c.b. has been designed to accommodate the 317M as an alternative, which will give 500mA for readers who require a less substantial power supply. The transformer can then be down-rated. Both regulators have built-in fold-back current-limiting and thermal protection.

A 12 volt transformer was used simply because I already had one, but if constructors want to be able to draw 15V at full current rating, the transformer should be upgraded to 15V or 17.5V. By limiting the range of the power supply it was possible to use two large clear meters to give voltage and current readings without having to resort to switched ranges etc.

## HOW IT WORKS

The secondary a.c. voltage is bridge rectified by REC1 and smoothed by C1. The resultant unregulated d.c. enters the IN pin of the 317, with C2 and C4 included to aid the stability of the regulator. The action of the i.c. is such that the output pin produces a voltage 1.25V higher than that on the ADJ pin, which is variable by means of the ratio between R1 and VR1. The circuit as described so far has a ripple-rejection factor of approx 65dB, but by adding a bypass capacitor C3 and a protection diode D1, this can be in-

creased to approx 80dB. D1 is needed to provide a discharge path for C1 under output short-circuit conditions to prevent the capacitor discharging back into the i.c. For those readers who may be worried about the possibility of an input short circuit condition, another diode, D2, can be included to restrict the output to input reverse voltage. The d.c. regulated voltage then goes via the meter and the switch to the output terminals. A third socket for earth is also included.

## CONSTRUCTION

It was decided for various reasons to use a Centurion case (WX3) and the finished result looks extremely professional. Once the case had been decided upon, the largest meters possible were selected to make readings easy, and the ML52 series fitted the bill perfectly.

Though few components are involved, it is recommended that for ease of construction a p.c.b. be used, and a suggested design is given in Fig. 2. A mains fuse is included and for safety reasons should not be omitted. Insert the components, including the i.c. if the 317M has been chosen (metal tab to the edge of the p.c.b.). Otherwise insert three Veropins for connection to the 317K, and Veropins for all other connections. Mount the p.c.b. in the case (in such a position that the 317M if used can be bolted via a mica washer to the rear panel). The 317K should be mounted on the rear panel, also with an insulating kit.

Theoretically a 2.2k potentiometer should produce a voltage output from 1.25V to 12.5V, but variable pots of this value are rare, 5k being much more common, so to avoid a cramped first half and a useless second half of the knob's travel, a 5.6k resistor is connected in parallel to make the effective resistance 0-2.6k approximately. This was then mounted, along with the other components on the front panel, which had been drilled and cut to suit. Mount the transformer, incorporating a solder tag for the earth wire, and drill a hole in the rear panel for the strain-relief bush. Next make all the necessary interconnections according to

WITH SIMULTANEOUS  
CURRENT AND VOLTAGE  
METERING



# TEST GEAR PROJECT

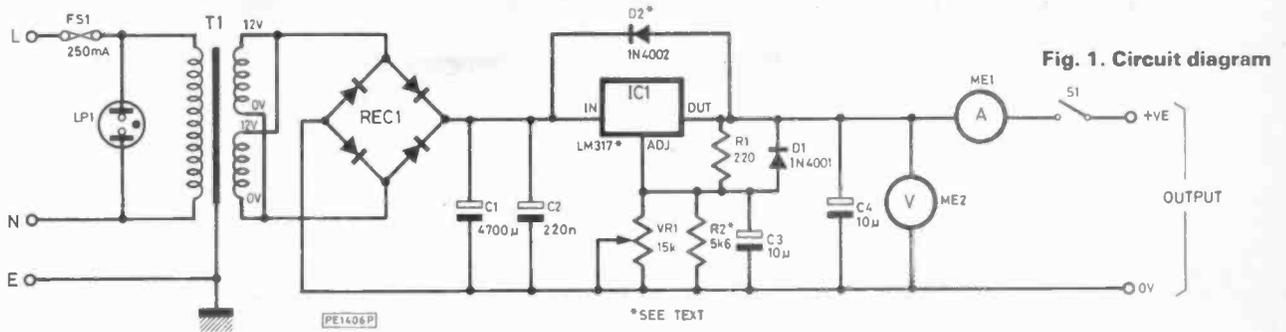


Fig. 1. Circuit diagram

## COMPONENTS . . .

### Resistors

R1	220 $\frac{1}{4}$ W 5%
R2	5k6 (see text)

### Capacitors

C1	4700 $\mu$ 25V elect.
C2	220n 25V tant.
C3, 4	10 $\mu$ 25V tant. (2 off)

### Semiconductors

D1(D2)	1N4002
IC1	LM317K or LM317M (see text)

### Miscellaneous

Centurion case WX3  
 ML52 meter 0-15V } Ambit  
 ML52 meter 0-1A }  
 BR1 SO4  
 Terminal posts: red, black, green  
 Fuseholder and fuse 250mA (20mm)  
 SPST toggle switch  
 Neon  
 Nuts, bolts etc.

### Transformer

T1	0-12, 0-12V 25VA
----	------------------

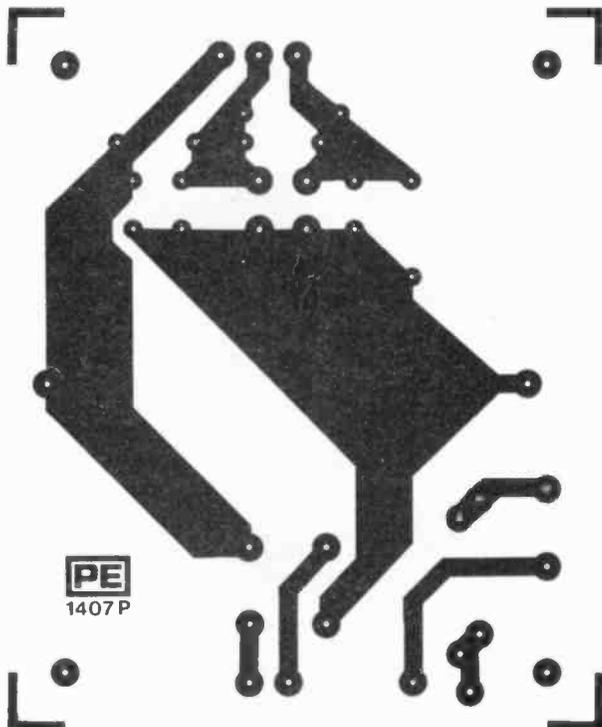


Fig. 2. Printed circuit board (actual size)

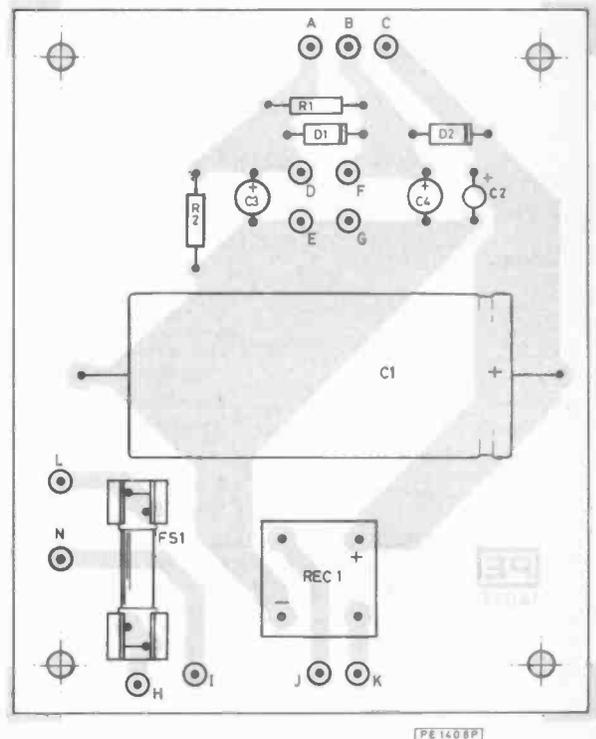


Fig. 3. Component layout

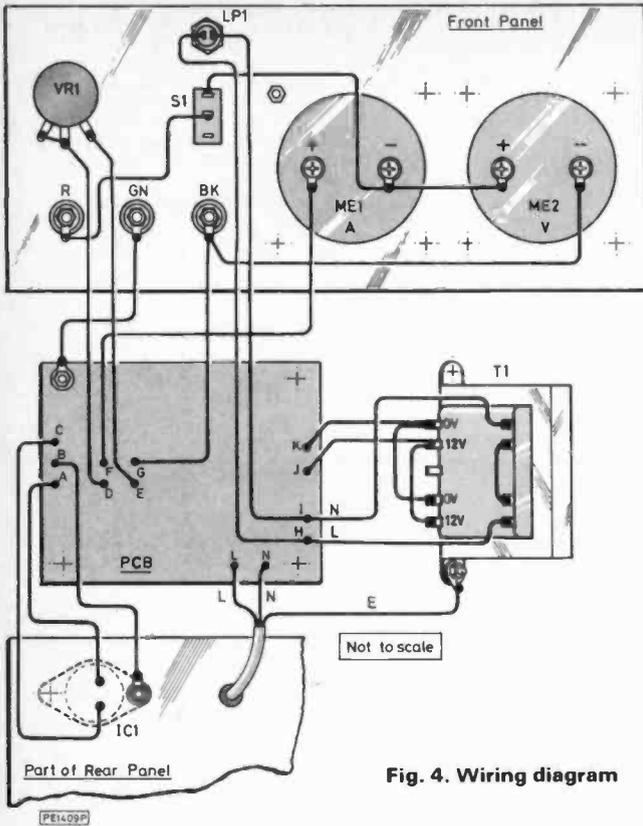


Fig. 4. Wiring diagram

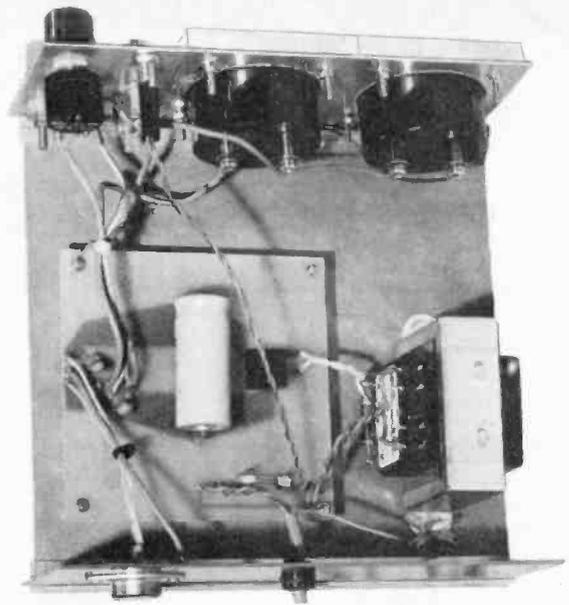


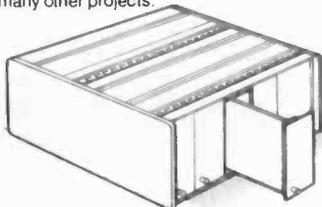
Fig. 4 and use thicker than normal wire for the output connections to avoid unnecessary voltage drops caused by lead resistance. Take care with the mains connections, particularly those to the neon as these can be easily touched inadvertently. After a final check the case can be bolted together and a useful piece of equipment added to the workbench. ★

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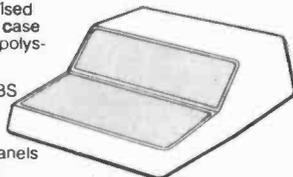
Half size eurocards (100 x 80mm) mounted vertically included as part of all front panel kits (except 35TE), with connector included.

### Hi-Style Desk Top Case

Designed to house keyboards and displays on two 1.6mm silver anodised aluminium panels. The light brown case is manufactured from high impact polystyrene and has a textured finish.

- Casing-High impact textured ABS

- Colour-Brown, front and base panels 1.6mm satin anodised aluminium



### Hand Held Box



This box is moulded in two sections and has a textured finish. The battery compartment accepts a PP3 or nickel cadmium stack 25 x 45mm long. A circuit board 56 x 105mm may be mounted on three pillars in the base, location being provided by a 3mm spigot. The top moulding will accept a circuit board 71 x 107mm.

- Material-Textured ABS
- Colour-Dark brown

### Plastic Boxes

#### Type A

Plastic boxes consisting of a top and bottom moulding with front and rear aluminium panels, positively retained in the two halves.

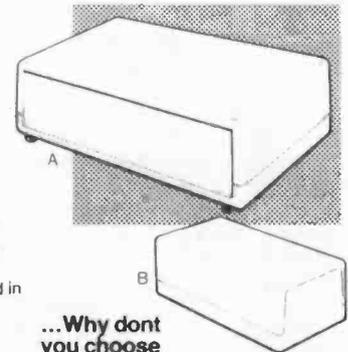
- Top and bottom moulding-High ABS.
- Colour-Light grey top: dark grey base.
- Front and rear panels-Satin anodised aluminium 1.6mm thick.

#### Type B

Constructed of high impact polystyrene, these handsome two-toned grey boxes are suitable for wall mounting and free standing instruments. The two halves of the box are held together by screws inserted from the base.

- Material-High impact polystyrene
- Colour-Top light grey: base dark grey
- Panels-Satin anodised aluminium

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Articles submitted for publication should conform to the usual practices of this journal, e.g. with regard to abbreviations and circuit symbols. Diagrams should be on separate sheets, not in the text.

## INTRUDER ALARM

THE circuit is described in its simplest form in order to show how very easy it is to construct a reliable alarm system for your home, or workshop, at almost negligible cost. Some commercial products are cloaked in an air of mystery (particularly with regard to the prices) and talk is of infra-red, doppler and vibration detection systems, but with scant reference to false alarms, which seem to occur with increasing frequency as the circuitry grows more sophisticated.

My simple 'Intruder Alarm' (PE Mar 83 issue) was designed primarily for 'unattended' operation in boats and caravans, so a time and re-set circuit had to be provided, and although it could also be installed in the home, a 'closed-loop' system gives somewhat greater protection. The present circuit employs the absolute minimum of components and operates continuously when triggered, but a suitable timer circuit could be included to provide switch-off after a few minutes if desired.

The unit can be constructed on a small piece of stripboard and requires only two components plus the relay. (Although it is recommended that a small diode should be connected across the relay coil to protect the transistor from the back EMF's generated during operation). From Fig. 1 it will be seen that the transistor current will close the relay contacts until the base is connected to ground (shown dotted)

whereupon conduction will cease. Nothing more is therefore required to produce a comprehensive and reliable system than this elementary circuit, together with a continuous loop shorting the base to ground, which would cause the unit to operate if it is broken at any point.

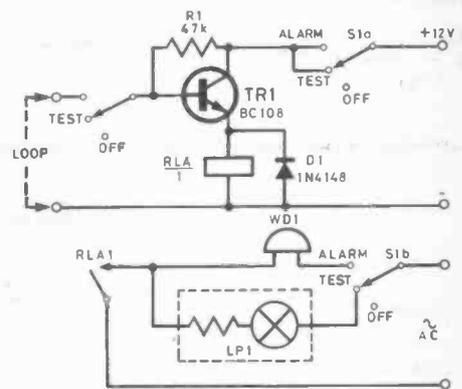
Consisting of a single wire fed around the property, possibly tucked under the edge of carpets, the loop is completed at opening windows and doors by magnetic latches, and by metal foil on the fixed glass. This self-adhesive tape can be arranged, for neatness, around the edge rather than across the panes if preferred; and some attention should be paid to the routing of this wiring in order to keep the total loop length as short as possible for efficiency as well as for economic reasons.

The reed switches are of the 'normally-open' type, whose contacts are held closed by the magnets. If a window is forced open, or the metallic tape torn by the glass being broken, the loop will no longer be complete and the relay will operate the alarm.

Since the circuit in its dormant state draws less than 1 milliamp, battery operation is perfectly acceptable, the 12V being derived from 'AA' 1.5V pen cells in two 4-cell plastic holders, although the unit will in many cases work quite successfully from a 9V PP3.

The alarm itself is largely a matter of choice and can range from a conveniently sited doorbell, to a mains-operated gong with, possibly, some of the house lights switching on at the same time. A 'test' circuit is a useful addition and Fig. 2 shows the switching arrangement with a mains bell and neon indicator. A 3-pole 3-way rotary switch is used providing 'Off', 'Test' and 'Alarm' positions. Section S1a is the On/Off, S1b switches off mains, or connects it to either the neon or bell and S1c joins the external loop to the transistor

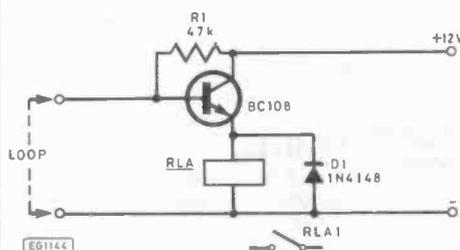
base in the 'Alarm' position. The Test setting shows that both battery and mains supplies are good and that the circuit is operating correctly (since the loop is open-circuit).



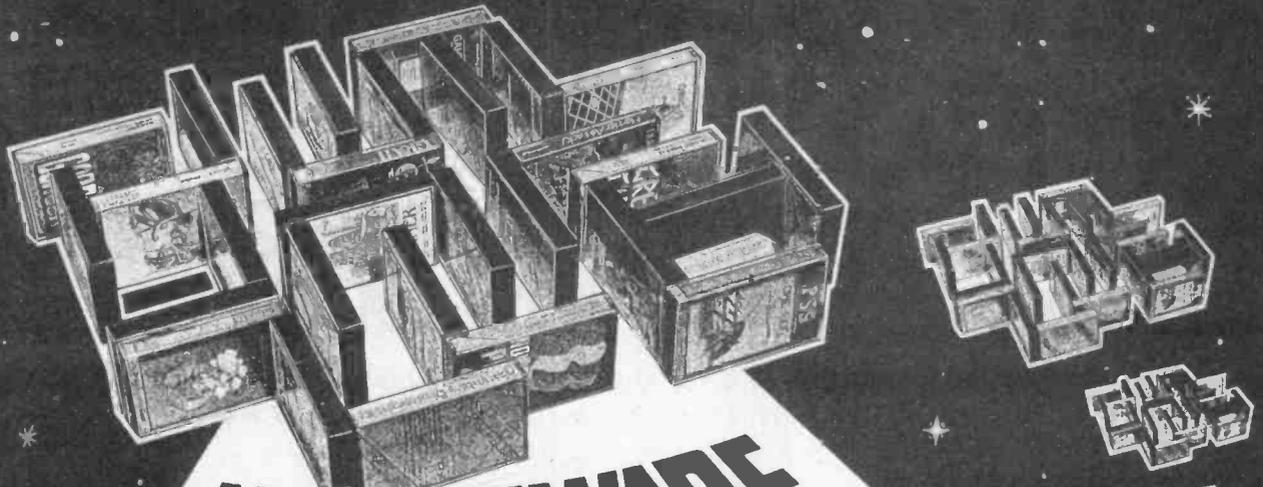
EG1145

The basis of operation—or rather, non-operation—relies upon the transistor base being firmly grounded, so it is important to ensure that there are no poor connections in the loop. If the foil is damaged during installation, *replace it*. Magnetic switches, window foil and all accessories for making the loop are readily available from advertisers and in many cases, these days, from local shops. Special connectors for joining the foil to the wiring are on the market, but quite satisfactory use has been made of standard strip-connectors, although needing a little more patience. If a 4-pole switch wafer is used, the spare tags can be connected in parallel with those of S1b so as to increase the current capacity of the switch if heavier loads are going to be used in the alarm circuit.

P. E. Mackrell,  
Lytham St Annes,  
Lancashire.



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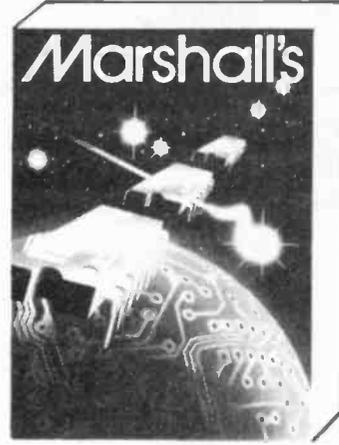
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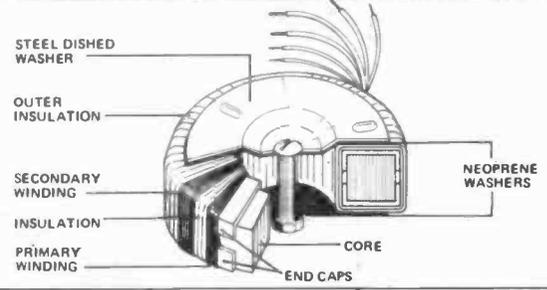
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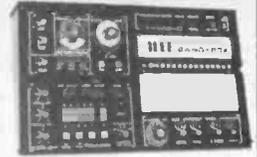
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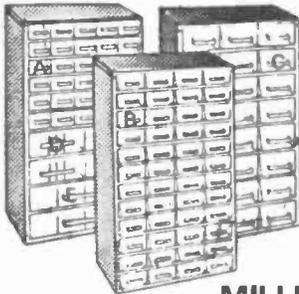
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CARBON FILM	7492	74S162	4073	15p	7905T 57p	40673	70p	BC441	32p	BFV52	30p	ZX502	14p	Square with hole	SL480	2.9p	100 = 160 2.10
5% HI STAB	7493	74S164	4074	15p	7912T 57p	40674	1.00	BC460	32p	BFV53	30p	ZX503	17p	R04 1000 3.2p	SN76003	2.9p	100 = 220 2.80
LOW NOISE	7494	74S166	4075	15p	7915T 57p	40675	1.00	BC461	32p	BSK19	24p	ZX504	24p	PW02 300i 95p	SN76013	2.9p	203 = 114 2.40
100 TO 10MΩ	7495	74S168	4076	45p	7924T 57p	40676	1.00	BC462	32p	BSK20	24p	ZX505	24p	PW04 1000i 30p	SN76023	2.9p	233 = 220 6.20
100 TO 10MΩ	7496	74S170	4077	15p	7924T 57p	40677	1.00	BC463	32p	BSK21	40p	ZX506	24p	PW06 1600i 1.3p	SN76033	2.9p	233 = 220 6.20
100 TO 10MΩ	7497	74S172	4078	15p	7924T 57p	40678	1.00	BC464	32p	BSK22	40p	ZX507	24p	PW08 1600i 1.3p	SN76043	2.9p	233 = 220 6.20
100 TO 10MΩ	7498	74S174	4079	15p	7924T 57p	40679	1.00	BC465	32p	BSK23	40p	ZX508	24p	PW10 1600i 1.3p	SN76053	2.9p	233 = 220 6.20
100 TO 10MΩ	7499	74S176	4080	15p	7924T 57p	40680	1.00	BC466	32p	BSK24	40p	ZX509	24p	PW12 1600i 1.3p	SN76063	2.9p	233 = 220 6.20
100 TO 10MΩ	7500	74S178	4081	15p	7924T 57p	40681	1.00	BC467	32p	BSK25	40p	ZX510	24p	PW14 1600i 1.3p	SN76073	2.9p	233 = 220 6.20
100 TO 10MΩ	7501	74S180	4082	15p	7924T 57p	40682	1.00	BC468	32p	BSK26	40p	ZX511	24p	PW16 1600i 1.3p	SN76083	2.9p	233 = 220 6.20
100 TO 10MΩ	7502	74S182	4083	15p	7924T 57p	40683	1.00	BC469	32p	BSK27	40p	ZX512	24p	PW18 1600i 1.3p	SN76093	2.9p	233 = 220 6.20
100 TO 10MΩ	7503	74S184	4084	15p	7924T 57p	40684	1.00	BC470	32p	BSK28	40p	ZX513	24p	PW20 1600i 1.3p	SN76103	2.9p	233 = 220 6.20
100 TO 10MΩ	7504	74S186	4085	15p	7924T 57p	40685	1.00	BC471	32p	BSK29	40p	ZX514	24p	PW22 1600i 1.3p	SN76113	2.9p	233 = 220 6.20
100 TO 10MΩ	7505	74S188	4086	15p	7924T 57p	40686	1.00	BC472	32p	BSK30	40p	ZX515	24p	PW24 1600i 1.3p	SN76123	2.9p	233 = 220 6.20
100 TO 10MΩ	7506	74S190	4087	15p	7924T 57p	40687	1.00	BC473	32p	BSK31	40p	ZX516	24p	PW26 1600i 1.3p	SN76133	2.9p	233 = 220 6.20
100 TO 10MΩ	7507	74S192	4088	15p	7924T 57p	40688	1.00	BC474	32p	BSK32	40p	ZX517	24p	PW28 1600i 1.3p	SN76143	2.9p	233 = 220 6.20
100 TO 10MΩ	7508	74S194	4089	15p	7924T 57p	40689	1.00	BC475	32p	BSK33	40p	ZX518	24p	PW30 1600i 1.3p	SN76153	2.9p	233 = 220 6.20
100 TO 10MΩ	7509	74S196	4090	15p	7924T 57p	40690	1.00	BC476	32p	BSK34	40p	ZX519	24p	PW32 1600i 1.3p	SN76163	2.9p	233 = 220 6.20
100 TO 10MΩ	7510	74S198	4091	15p	7924T 57p	40691	1.00	BC477	32p	BSK35	40p	ZX520	24p	PW34 1600i 1.3p	SN76173	2.9p	233 = 220 6.20
100 TO 10MΩ	7511	74S200	4092	15p	7924T 57p	40692	1.00	BC478	32p	BSK36	40p	ZX521	24p	PW36 1600i 1.3p	SN76183	2.9p	233 = 220 6.20
100 TO 10MΩ	7512	74S202	4093	15p	7924T 57p	40693	1.00	BC479	32p	BSK37	40p	ZX522	24p	PW38 1600i 1.3p	SN76193	2.9p	233 = 220 6.20
100 TO 10MΩ	7513	74S204	4094	15p	7924T 57p	40694	1.00	BC480	32p	BSK38	40p	ZX523	24p	PW40 1600i 1.3p	SN76203	2.9p	233 = 220 6.20
100 TO 10MΩ	7514	74S206	4095	15p	7924T 57p	40695	1.00	BC481	32p	BSK39	40p	ZX524	24p	PW42 1600i 1.3p	SN76213	2.9p	233 = 220 6.20
100 TO 10MΩ	7515	74S208	4096	15p	7924T 57p	40696	1.00	BC482	32p	BSK40	40p	ZX525	24p	PW44 1600i 1.3p	SN76223	2.9p	233 = 220 6.20
100 TO 10MΩ	7516	74S210	4097	15p	7924T 57p	40697	1.00	BC483	32p	BSK41	40p	ZX526	24p	PW46 1600i 1.3p	SN76233	2.9p	233 = 220 6.20
100 TO 10MΩ	7517	74S212	4098	15p	7924T 57p	40698	1.00	BC484	32p	BSK42	40p	ZX527	24p	PW48 1600i 1.3p	SN76243	2.9p	233 = 220 6.20
100 TO 10MΩ	7518	74S214	4099	15p	7924T 57p	40699	1.00	BC485	32p	BSK43	40p	ZX528	24p	PW50 1600i 1.3p	SN76253	2.9p	233 = 220 6.20
100 TO 10MΩ	7519	74S216	4100	15p	7924T 57p	40700	1.00	BC486	32p	BSK44	40p	ZX529	24p	PW52 1600i 1.3p	SN76263	2.9p	233 = 220 6.20
100 TO 10MΩ	7520	74S218	4101	15p	7924T 57p	40701	1.00	BC487	32p	BSK45	40p	ZX530	24p	PW54 1600i 1.3p	SN76273	2.9p	233 = 220 6.20
100 TO 10MΩ	7521	74S220	4102	15p	7924T 57p	40702	1.00	BC488	32p	BSK46	40p	ZX531	24p	PW56 1600i 1.3p	SN76283	2.9p	233 = 220 6.20
100 TO 10MΩ	7522	74S222	4103	15p	7924T 57p	40703	1.00	BC489	32p	BSK47	40p	ZX532	24p	PW58 1600i 1.3p	SN76293	2.9p	233 = 220 6.20
100 TO 10MΩ	7523	74S224	4104	15p	7924T 57p	40704	1.00	BC490	32p	BSK48	40p	ZX533	24p	PW60 1600i 1.3p	SN76303	2.9p	233 = 220 6.20
100 TO 10MΩ	7524	74S226	4105	15p	7924T 57p	40705	1.00	BC491	32p	BSK49	40p	ZX534	24p	PW62 1600i 1.3p	SN76313	2.9p	233 = 220 6.20
100 TO 10MΩ	7525	74S228	4106	15p	7924T 57p	40706	1.00	BC492	32p	BSK50	40p	ZX535	24p	PW64 1600i 1.3p	SN76323	2.9p	233 = 220 6.20
100 TO 10MΩ	7526	74S230	4107	15p	7924T 57p	40707	1.00	BC493	32p	BSK51	40p	ZX536	24p	PW66 1600i 1.3p	SN76333	2.9p	233 = 220 6.20
100 TO 10MΩ	7527	74S232	4108	15p	7924T 57p	40708	1.00	BC494	32p	BSK52	40p	ZX537	24p	PW68 1600i 1.3p	SN76343	2.9p	233 = 220 6.20
100 TO 10MΩ	7528	74S234	4109	15p	7924T 57p	40709	1.00	BC495	32p	BSK53	40p	ZX538	24p	PW70 1600i 1.3p	SN76353	2.9p	233 = 220 6.20
100 TO 10MΩ	7529	74S236	4110	15p	7924T 57p	40710	1.00	BC496	32p	BSK54	40p	ZX539	24p	PW72 1600i 1.3p	SN76363	2.9p	233 = 220 6.20
100 TO 10MΩ	7530	74S238	4111	15p	7924T 57p	40711	1.00	BC497	32p	BSK55	40p	ZX540	24p	PW74 1600i 1.3p	SN76373	2.9p	233 = 220 6.20
100 TO 10MΩ	7531	74S240	4112	15p	7924T 57p	40712	1.00	BC498	32p	BSK56	40p	ZX541	24p	PW76 1600i 1.3p	SN76383	2.9p	233 = 220 6.20
100 TO 10MΩ	7532	74S242	4113	15p	7924T 57p	40713	1.00	BC499	32p	BSK57	40p	ZX542	24p	PW78 1600i 1.3p	SN76393	2.9p	233 = 220 6.20
100 TO 10MΩ	7533	74S244	4114	15p	7924T 57p	40714	1.00	BC500	32p	BSK58	40p	ZX543	24p	PW80 1600i 1.3p	SN76403	2.9p	233 = 220 6.20
100 TO 10MΩ	7534	74S246	4115	15p	7924T 57p	40715	1.00	BC501	32p	BSK59	40p	ZX544	24p	PW82 1600i 1.3p	SN76413	2.9p	233 = 220 6.20
100 TO 10MΩ	7535	74S248	4116	15p	7924T 57p	40716	1.00	BC502	32p	BSK60	40p	ZX545	24p	PW84 1600i 1.3p	SN76423	2.9p	233 = 220 6.20
100 TO 10MΩ	7536	74S250	4117	15p	7924T 57p	40717	1.00	BC503	32p	BSK61	40p	ZX546	24p	PW86 1600i 1.3p	SN76433	2.9p	233 = 220 6.20
100 TO 10MΩ	7537	74S252	4118	15p	7924T 57p	40718	1.00	BC504	32p	BSK62	40p	ZX547	24p	PW88 1600i 1.3p	SN76443	2.9p	233 = 220 6.20
100 TO 10MΩ	7538	74S254	4119	15p	7924T 57p	40719	1.00	BC505	32p	BSK63	40p	ZX548	24p	PW90 1600i 1.3p	SN76453	2.9p	233 = 220 6.20
100 TO 10MΩ	7539	74S256	4120	15p	7924T 57p	40720	1.00	BC506	32p	BSK64	40p	ZX549	24p	PW92 1600i 1.3p	SN76463	2.9p	233 = 220 6.20
100 TO 10MΩ	7540	74S258	4121	15p	7924T 57p	40721	1.00	BC507	32p	BSK65	40p	ZX550	24p	PW94 1600i 1.3p	SN76473	2.9p	233 = 220 6.20
100 TO 10MΩ	7541	74S260	4122	15p	7924T 57p	40722	1.00	BC508	32p	BSK66	40p	ZX551	24p	PW96 1600i 1.3p	SN76483	2.9p	233 = 220 6.20
100 TO 10MΩ	7542	74S262	4123	15p	7924T 57p	40723	1.00	BC509	32p	BSK67	40p	ZX552	24p	PW98 1600i 1.3p	SN76493	2.9p	233 = 220 6.20
100 TO 10MΩ	7543	74S264	4124	15p	7924T 57p	40724	1.00	BC510	32p	BSK68	40p	ZX553	24p	PW100 1600i 1.3p	SN76503	2.9p	233 = 220 6.20
100 TO 10MΩ	7544	74S266	4125	15p	7924T 57p	40725	1.00	BC511	32p	BSK69	40p	ZX554	24p	PW102 1600i 1.3p	SN76513	2.9p	233 = 220 6.20
100 TO 10MΩ	7545	74S268	4126	15p	7924T 57p	40726	1.00	BC512	32p	BSK70	40p	ZX555	24p	PW104 1600i 1.3p	SN76523	2.9p	233 = 220 6.20
100 TO 10MΩ	7546	74S270	4127	15p	7924T 57p	40727											

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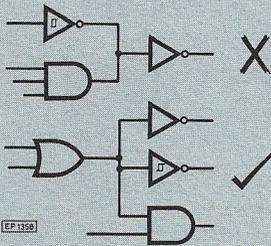
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## CONNECTING GATES

A standard ('totem-pole') TTL gate output to be connected to the input of any other TTL gate. The use of standard logic levels and common power supplies ensures that such signals will be compatible. There are many cases, however, where more than just two gates are involved in processing a signal. The rule then for connecting multiple standard gates (illustrated below) is that a single TTL output may be connected to more than one input, but not vice versa.



## FAN-IN AND FAN-OUT

The output of a TTL gate may be connected to the input of one or more gates. The drive capability of a gate is known as its fan-out, and is usually expressed as the number of standard loads (usually ten) which can be driven by the gate. The fan-in of a gate indicates its loading effect on a gate output, and is usually expressed as the number of standard loads (usually one) that it represents. It is unusual for more than ten loads to be connected to a single output, but if the fan-out is exceeded, the voltage and current swings may become too small to drive all of the loads reliably.

As a general rule, the fan-out within a TTL sub-family is 10 (20 for LS), and the majority of inputs have a fan-in of one. The general rules for fan-in and fan-out for the commonly encountered TTL sub-families are summarised in Table 1.

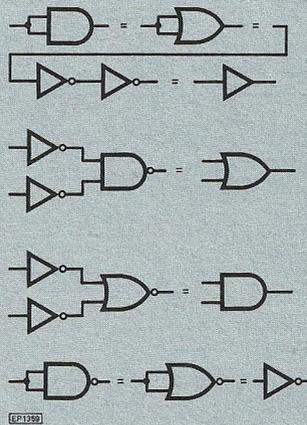
## INPUT AND OUTPUT CURRENT

The limits on fan-out are caused by the currents which must flow to hold the input of a gate at logic 0 and at logic 1. In TTL, the logic 0 currents usually predominate in determining fan-out. A standard gate input requires 1.6mA to flow between the input and 0 volts to establish a logic 0. Thus, to support a fan-out of 10, the corresponding gate output must be capable of 'sinking'

16mA. In the logic 1 state, the current flow is in the opposite direction, and is substantially smaller. Standard TTL inputs are typically able to 'source' 800µA, while typical inputs only require 40µA each in the logic 1 state. The source and sink currents for standard gates are shown in Table 2.

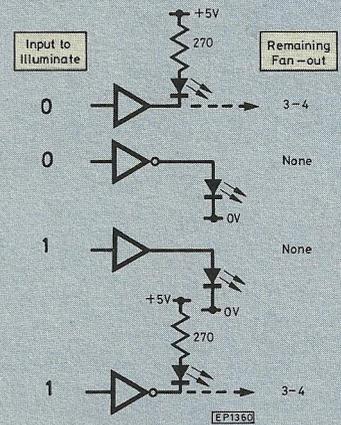
## CIRCUIT EQUIVALENTS

There are a number of arrangements of logic gates which are very useful in building real logic circuits. These are particularly useful when trying to use the minimum number of i.c.s in the circuit. Some useful equivalents are shown below.



## DRIVING LEDs

A typical red l.e.d. requires a current of around 10mA to flow through it in order to provide a reasonably bright display. There are a number of ways to drive an l.e.d. from a TTL gate output. The actual method chosen depends on whether the diode is to be illuminated for a gate output of 0 or 1, and whether the gate is required to drive any other logic gates in addition to the diode. The various techniques are shown below, together with the logic input/output states required to illuminate the l.e.d., and the fan-out remaining to drive other gates. Although specific gates are shown, any logical equivalent may also be used.

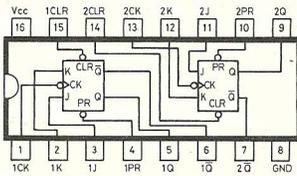


Driving Gate	Max. Number of Inputs Driven				
	74	74L	74H	74S	74LS
Standard TTL (74)	10	40	8	8	20
Low-Power (74L)	2	10	1	1	5
High-Power (74H)	12	40	10	10	25
Schottky (74S)	12	40	10	10	50
L-P Schottky (74LS)	5	20	4	4	20

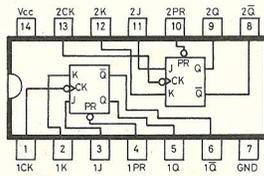
Table 1

Gate Type	High I/P (µA)	Low I/P (mA)	High O/P (µA)	Low O/P (mA)
74	40	-1.6	400	-16
74L	10	-0.18	100	-3.6
74H	50	-2	500	-20
74S	50	-2	1000	-20
74LS	20	-0.4	400	-8

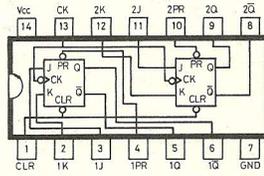
Table 2



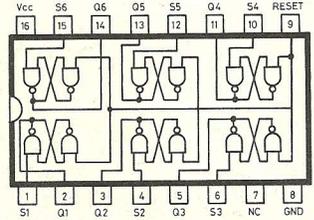
**74112 Dual**  
J-K preset and clear



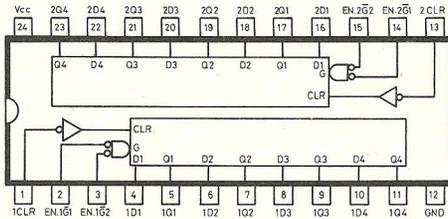
**74113 Dual**  
J-K with preset LS



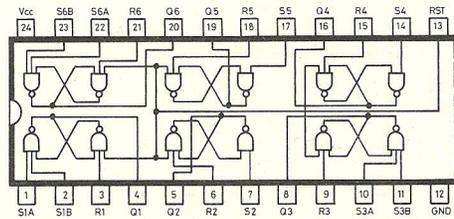
**74114 Dual**  
J-K preset and clear LS



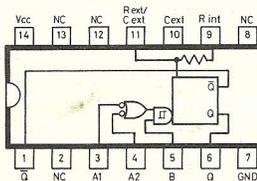
**74118 Hex**  
S-R latch with single reset



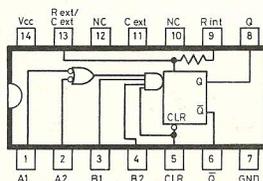
**74116 Dual** 4-bit latch  
with enable and clear



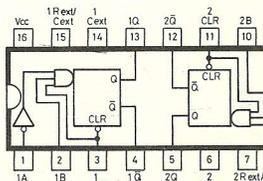
**74119 Hex**  
S-R latch



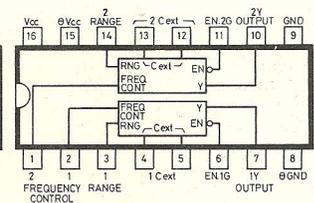
**74121**  
Monostable



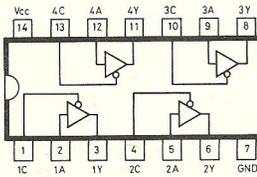
**74122 Retriggerable**  
mono with clear



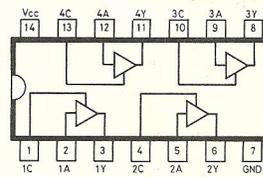
**74123 Dual Retriggerable**  
mono with clear



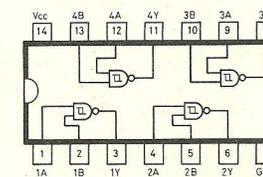
**74124 Dual**  
Voltage-controlled osc LS



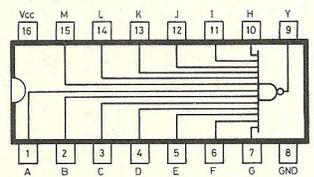
**74125 Quad**  
buffer tri-state



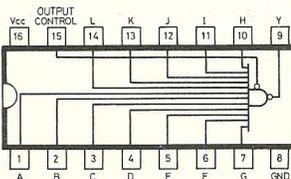
**74126 Quad**  
3 state buffer



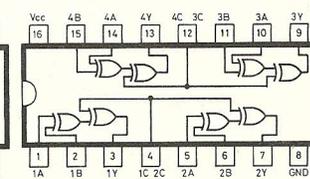
**74132 Quad**  
2-input NAND Schmitt



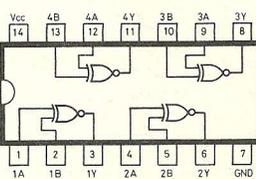
**74133**  
13-input NAND LS



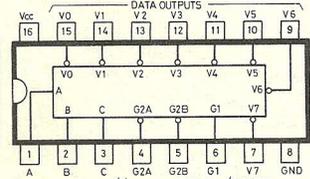
**74134**  
12-input 3 state NAND



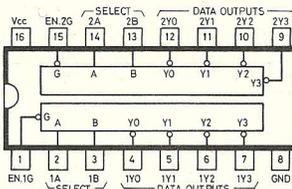
**74135 Quad**  
exclusive OR/NOR



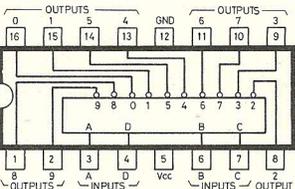
**74136 Quad**  
2-input Ex-OR



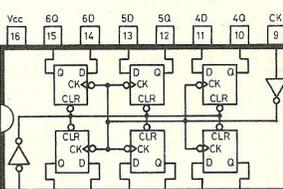
**74138 3-line to 8-line**  
decoder/demultiplexer



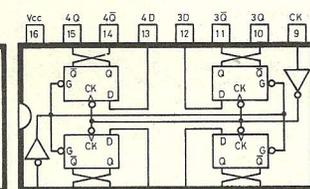
**74139 Dual** 2-line to 4-line  
decoder/demultiplexer



**74141 BCD decimal**  
decoder/driver



**74174 Hex D-type**



**74175 Quad D-type**