

# PRACTICAL WIRELESS

OCTOBER  
1971

20p

**EXTRA INSIDE**

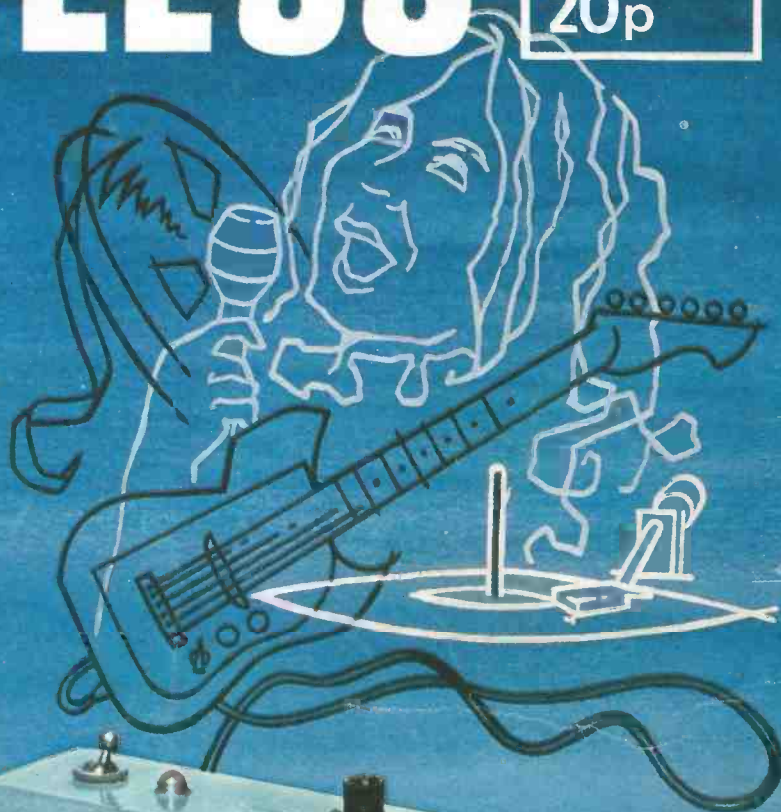
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**SMALL  
WORKSHOP  
TOOLS**

*plus*

Wall Chart

**CIRCUIT  
BUILDING  
BRICKS**



**MODULAR AUDIO MIXING SYSTEM**

# ADCOLA Soldering Instruments add to your efficiency

## THE NEW 'INVADER'

### ADCOLA L.646

for Factory Bench Line Assembly

A precision instrument—supplied with standard 3/16" (4.75 mm) diameter, detachable copper chisel-face bit\*.  
Standard temp. 360 c at 23 watts.  
Special temps. from 250°c—410 c.

**PRICE**  
**£1.85**



#### \*Additional Stock Bits (illustrated) available

##### COPPER

B 38  $\frac{1}{4}$ " — 3.2 mm CHISEL FACE

B 14  $\frac{3}{32}$ " — 2.4 mm CHISEL FACE

B 24  $\frac{1}{8}$ " — 4.75 mm SCREWDRIVER FACE

B 12  $\frac{3}{16}$ " — 4.75 mm EYELET BIT

B 58  $\frac{1}{4}$ " — 6.34 mm CHISEL FACE

##### LONG LIFE

B 42 LL  $\frac{1}{4}$ " — 4.75 mm CHISEL FACE

B 38 LL  $\frac{1}{4}$ " — 3.2 mm CHISEL FACE

B 14 LL  $\frac{3}{32}$ " — 2.4 mm CHISEL FACE

B 44 LL  $\frac{1}{4}$ " — 4.75 mm SCREWDRIVER FACE

Don't take chances. We don't. All our ADCOLA Soldering Instruments are of impeccable quality. You can depend on ADCOLA day after day. That's why they're so popular. You get consistent good service... reliability... from our famous thermally controlled ADCOLA Element and the tough steel construction of this ideal production tool.

\* Write for price list and catalogue



**ADCOLA PRODUCTS LTD.,**  
(Dept. M), ADCOLA HOUSE, GAUDEN RD., LONDON, S.W.4.  
Telephone: 01-622 0291/3 - Telegrams: Soljoint London Telex • Telex: Adcola London 21851



## for fast, easy, reliable soldering

Contains 5 cores of non-corrosive flux, instantly cleaning heavily oxidised surfaces. No extra flux required.

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Economically packed for general electrical and electronic soldering. 75ft. 18 gauge on plastic reel. Recommended retail price **75p**  
Size 12



### THIN GAUGE SOLDER, ESSENTIAL FOR

soldering small components and thin wires. High tin content, low melting point, 60/40 alloy, 170ft. 22 gauge on plastic reel. Recommended retail price **75p**  
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19A 60/40 18 18p\*

Size 5 (illustrated) Savbit 18 18p\*

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\*Recommended Price



### INVALUABLE FOR STRIPPING FLEX, THE NEW AUTOMATIC OPENING BIF WIRE STRIPPER AND CUTTER, easily

adjustable for all standard diameters. Plastic covered handles can also be used as wire cutter. Recommended retail price **50p**



From Electrical and Hardware shops. If unobtainable, write to: **Multicore Solders Ltd., Hemel Hempstead, Herts.**



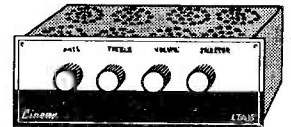
## RANGE OF SOLID STATE A.C. MAINS AMPLIFIERS

Employing only high grade components and transistors.

### LTA 15 WATT AMPLIFIER

HIGH FIDELITY OUTPUT SWITCHED INPUTS FOR GRAM, 'MIKE', TAPE, AND RADIO

Frequency Response 10-40,000 cps—3dB. Bass Control+17dB to—16dB at 40cps. Treble Control—17dB to—14dB at 14Kcs. Hum and Noise—80dB. Harmonic Distortion 0.2% at rated output. Output for 3-8-15 ohm Loudspeakers.



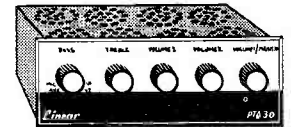
Recommended **£19**  
Retail Price  
Size 9½ x 3½ x 5½ in. approx.

### PTA30 HI-FI PUBLIC ADDRESS AMPLIFIER

A SUCCESSOR TO OUR POPULAR CONCHORD 30 WATT UNIT

Input Sensitivity 2 mv (max.)  
Output 30 watts.

Output Sockets for Loudspeaker or combination of Speakers with total impedance between 3 ohms and 30 ohms. Three individually controlled Inputs for mixing purposes. Housed in fully enclosed stove enamelled steel case. Controls Vol. (1) Vol. (2) Vol. (3) with mains switch, Treble 'lift', and 'cut'. Bass 'lift' and 'cut'.



Recommended **£24**  
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Size 12 x 3½ x 6 in. approx.

AN IDEAL UNIT FOR VOCAL AND INSTRUMENTAL GROUPS, SUITABLE FOR ANY KIND OF 'MIKE' AND INSTRUMENT PICK-UP, ALSO FOR RADIO, TAPE OR GRAM.

Please send a stamped addressed envelope for full descriptive details of above units.

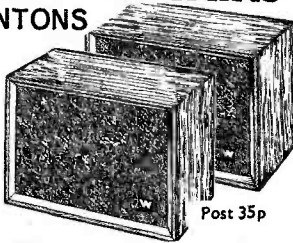
If required an attractive wood cabinet with veneer finish can be supplied for any model. **£3.50**  
Prices from

AVAILABLE FROM YOUR LOCAL HI-FI DEALER  
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**LINEAR PRODUCTS LTD,**  
Electron Works, Armley, Leeds

## SUPER SPEAKER BARGAINS WHARFEDALE DENTONS

A compact system sold in matched pairs for a perfectly balanced stereo system. Each Denton contains an 8in. bass unit with 3in. pressure unit, coupled by a Wharfedale crossover network. Rated input: 15 watts maximum. Frequency response: 65-17,000Hz. Impedance: 4/8 ohms. Cabinet 9 1/2in. x 14in. x 8 1/2in. These most attractive units are available in oiled teak, white or walnut and are small enough to blend in with most surroundings.



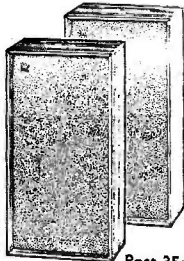
Post 35p

LIST PRICE £39.00 **£28.00** Walnut White

**£27.00** Teak

## WHARFEDALE TRITONS

A new and exciting addition to the Wharfedale range, this three speaker system will satisfy the most ardent Hi-Fi enthusiast. Shelf or floor standing—hand finished in oiled teak or polished walnut. Frequency response 55-22,000Hz. C.A.B. Dome pressure unit. Bass unit 8in. Mid-range unit 5in. Treble unit 2in. Impedance 8 ohms. Size 2 1/2in. x 9 1/2in. x 9in.



Post 35p.

LIST PRICE £59.90

**LASKY'S £36.00** Teak

**PRICE £38.00** Walnut White

## BSR McDONALD MP60

High precision low-mass counterbalanced pick-up arm, heavy balanced turntable, simple to operate controls, viscous cueing device, slide in cartridge carrier, 4 pole motor.

**LASKY'S PRICE £12.50** Post 35p



### BSR McDONALD UNITS & PACKAGES

A. Chassis only. B. Complete with Lasky's plinth and cover. C. Complete with Lasky's plinth, cover and AD76K cartridge. D. Comp. wired on BSR plinth with cover. E. As D plus AD76K cartridge.

MODEL	A	B	C	D	E
610	£15.45	£18.75	£22.50	£24.50	£28.50
510	£13.45	£16.95	£20.75	£22.00	£26.00
310	£9.95	£13.45	£17.25	£21.00	£23.50
MP60	£12.50	£15.75	£19.50	£21.50	£25.50

## GARRARD UNITS AND PACKAGES

### GARRARD SL 55B

Four speed autochanger

**LASKY'S PRICE £10.50** Post 35p



Garrard SP25 Mk. III	£11.50	Garrard SL40B	£9.95
Garrard SP25, Mk. III wired	£12.00	Garrard AP76 without cart.	£20.95
Garrard SP25 Mk. III with 9TA cart.	£13.95	Garrard 3000 with 9TA cart.	£10.50
		Garrard 2025TC with 9TA cart.	£9.85

### GARRARD PACKAGES

Post on packages 50p

Garrard AP76 with AD76K cart. and Lasky's plinth and cover	£35
Garrard AP76 with Shure M44E cart. and Lasky's plinth and cover	£40
Garrard SP25 Mk. III, AD76K cart. and Lasky's plinth and cover	£20
Garrard SP25 Mk. III, Micro M2100e cart. and Lasky's plinth and cover	£25

## LASKY'S NEW LOW NOISE CASSETTES FROM THE USA

Type	Singles	5	10	20
C-60	41p	£1.82	£3.41	£6.55
C-90	63p	£3.04	£5.78	£10.89
C-120	96p	£4.13	£7.43	£13.41

Post Each 5p. 5-20p. 10-25. 20-50p.

## SONY 8FC 59W SCOOP

### DIGITAL AM/FM CLOCK RADIO



Digital Alarm Clock Radio. The digital clock shows you the time minute by minute with matchless accuracy and once set the Digimatic will wake you up at the same time every morning without having to be re-set. The radio section features Sony's unique sleep button, you fall gently to sleep lulled by the sweet tone of the radio, which switches itself off at a predetermined time. Available in either black, white or red (8FC-59W). Frequency range 530-1,605KHz (AM); 87-108MHz (FM). Uses 8 transistors and 8 semi-conductors, built-in ferrite aerial and 3 1/2in loudspeaker. Power requirements: 230V AC 50Hz. Dimensions: 12 1/2in x 3 1/2in. x 5 1/2in.

LIST PRICE £30.00

**LASKY'S PRICE £22.50** Post free in U.K.

## KATONE AM/AIRCRAFT PORTABLE RADIO

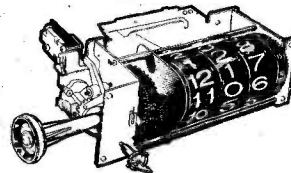
### BATTERY/MAINS

A combined battery and mains portable of exceptionally attractive design. Housed in a leatherette covered case, size 8 1/2in. x 5 1/2in. x 3 1/2in., fitted with an 8-section external telescopic aerial for FM and internal ferrite rod for MW wave bands, and clear easy-to-read dial with logging scale. Wave band coverage is FM 88-108MHz, AM 535-1,600KHz. A highly selective circuit using 9 transistors and 9 semi-conductors operating from either 4 x 1.5 volt torch batteries or direct from 230 volts 50Hz AC house mains, from a built-in mains unit. A socket is fitted for a personal earphone. Easy-to-use silver colour knobs, with "woodgrain" panel enhances the appearance of this fine radio.



**LASKY'S PRICE £9.95** Post 15p

## DIGITAL CLOCK SCOOP



EXCLUSIVELY FROM LASKY'S

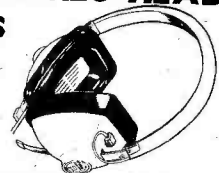
for you to mount into any housing. The clock measures 4 1/2 W x 1 1/2 H x 3 1/2 D (overall from front of drum to back of switch). SPEC.: 210/240V a.c., 50Hz operation; switch rating 250V 5A. Complete with instructions. HUNDREDS OF APPLICATIONS. COMPLETE WITH KNOBS.

- MADE ESPECIALLY FOR LASKY'S BY FAMOUS MAKER
  - MAINS OPERATION
  - 12-HOUR ALARM
  - AUTO "SLEEP" SWITCH
  - HOURS, MINUTES AND SECONDS READ-OFF
  - FORWARD AND BACKWARD TIME ADJUSTMENT
  - SILENT OPERATION SYNCHRONOUS MOTOR
  - SHOCK AND VIBRATION PROOF
  - BUILT IN ALARM BUZZER
- SPECIAL QUOTES FOR QUANTITIES

**LASKY'S PRICE £6.95** Post 18p

## TRIO HS.1 & HS.2 STEREO HEADPHONE BARGAINS

Models HS-1 and HS-2. Both these sets by TRIO offer really superb stereo reproduction in a lightweight, fully adjustable headset designed for optimum comfort. Listening fatigue is unknown with TRIO headphones. Brief spec. both models: Imp. 80 nominal (matching 4 to 80); max. input 0.5W; frequency response 20-19 kHz; output sensitivity at 1mW input; HS-1 118 dB, HS-2 111 dB; weight 0.66lbs. Identical in appearance—both models are finished in ivory with contrasting foam filled ear pads and head band.



LIST PRICE £8.40 **LASKY'S PRICE £6.75**

**HS.1 £5.20p HS.2 £4.15p** Post 18p

## Lasky's Radio Limited

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# RADIO CONSTRUCTOR



Special  
IN THIS ISSUE

# THE RADIO CONSTRUCTOR

## September Issue

Constructional Articles include

### SEMI-CONDUCTOR GATE-DIP OSCILLATOR

Bringing the grid-dip oscillator up to date with the aid of a modern low-cost field-effect transistor. The unit described is capable of operation from 4 to 145MHz.

### BRAKE LIGHT FAILURE INDICATOR

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Copies may also be obtained direct from the Publishers 24p including postage. Published by:  
Data Publications Ltd., 57 Maida Vale, London W.9

## ON SALE NOW 20p

### 4-STATION INTERCOM



£6.75

Solve your communication problems with this 4-Station Transistor Intercom system (1 master and 3 Subs), in de-luxe plastic cabinets for desk or wall mounting. Call/talk/listen from Master to Subs and Subs to Master. Ideally suitable for Business, Surgery, Schools, Hospital, Office and Home. Operates on one 9V battery. On/off switch. Volume control. Complete with 3 connecting wires each 6ft. and other accessories. P. & P. £0.40.

### MAINS INTERCOM

No batteries—no wires. Just plug in the mains for instant two-way loud and clear communication. On off switch and volume control. Price £13.95 P. & P. £0.25.

### INTERCOM/BABY ALARM



OUR PRICE ONLY £3.35

Same as 4-Station Intercom for two-way instant communication. Ideal as Baby Alarm and Door Phone. Complete with 6ft. connecting wire. Battery 13p. P. & P. £0.25.

### Transistor TELEPHONE AMPLIFIER



£2.98

Why not boost business efficiency with this incredible De-luxe Telephone Amplifier. Take down long telephone messages or converse without holding the handset. A useful office aid. On/off switch. Volume Control. Battery 13p. extra. P. & P. 20p. Full price refunded if not satisfied in 7 days.

WEST LONDON DIRECT SUPPLIES (P.W.S)  
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### The Unique MULTI-MINI TWIN-VICE



An extra "Pair of hands" for those tricky jobs

ASSEMBLY—SOLDERING—GLUING—WIRING—DRILLING ETC.

- INDEPENDENT ADJUSTMENT OF THE TWO VICE HEADS TO ANY ANGLE WITH POSITIVE LOCKING.
- JAWS WILL FIRMLY GRIP ROUND, FLAT, SQUARE, OR HEXAGONAL PARTS.

TWIN VICE: £5.90 (24p P & P)

ALSO AVAILABLE

SINGLE VICE: £3.37½ (20p P & P)

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### MAINS UNITS for all types of TRANSISTOR EQUIPMENT



### RUN YOUR TAPE RECORDER OFF A.C. MAINS

Mains unit supplied complete and ready to plug into your cassette recorder. (State voltage, model and plug required.)

£2.50 P. & P. 15p

### 12 VOLT CAR BATTERY UNIT

Enables you to run your cassette recorder off 12V. car battery. (State 6v or 7½v output, model and plug required.)

£2.00 P. & P. 15p

### PLUS-3 MAINS UNIT

Provides three separate switched output voltages 6v, 7½v and 9v. D.C. attractive case with indicator light, mains lead output socket, plug and lead. Size 4½ x 3½ x 2½ in.

£3.00 P. & P. 15p.



Extra lead with plug to fit your cassette recorder 50p. (State model and plug required.)

MAINS UNIT FOR ALL TRANSISTOR RADIOS, ETC., USING PP3 TYPE BATTERY. (ALSO AVAILABLE FOR 6V.)

£1.15 P. & P. 10p.

### MAIN UNITS

For single outputs, 6v, 9v, 12v, 18v, £2.00. For two separate outputs, 4½v + 4½v, 6v + 6v, 9v + 9v, £2.50. P. & P. 15p. per unit. (Please state outputs reqd.)

All units are completely isolated from mains by double wound transformer ensuring 100% safety.

R.G.S. PRODUCTS (RADIO) LTD.  
(Dept. P.W.), 31 Oliver Road, London, E17

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AC126	0-13	OC171	0-23
AC127	0-17	OC200	0-25
AC128	0-13	OC201	0-25
AC176	0-25	2G301	0-13
ACY17	0-15	2G303	0-13
AF239	0-37	2N711	0-50
AF186	0-50	2N1302-3	0-20
AF139	0-37	2N1304-5	0-25
BC154	0-25	2N1306-7	0-30
BC171 = BC107	0-13	2N1308-9	0-35
BC172 = BC108	0-13	2N3819FET	0-45
BF194	0-15		
BF274	0-15	<b>Power Transistors</b>	
BFY50	0-20	OC20	0-50
BSY25	0-57	OC23	0-30
BSY26	0-13	OC25	0-25
BSY27	0-13	OC26	0-25
BSY28	0-13	OC28	0-30
BSY29	0-13	OC35	0-25
BSY95A	0-15	OC36	0-37
OC41	0-13	AD149	1-30
OC44	0-13	AUY10	0-20
OC45	0-13	2S034	0-25
OC71	0-13	2N3055	0-63
OC72	0-13		
OC73	0-17	<b>Diodes</b>	
OC81	0-13	AA42	0-10
OC81D	0-13	OA95	0-19
OC83	0-20	OA79	0-99
OC49	0-13	OA81	0-99
OC140	0-17	IN9114	0-07

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## OUR VERY POPULAR 3p TRANSISTORS

FULLY TESTED & GUARANTEED

- TYPE "A" PNP Silicon alloy, metal TO-5 can. 25300 type, direct replacement for the OC200/203 range.
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- TYPE "F" NPN Silicon plastic encapsulation, low noise amplifier of the 2N3708, 9, 10, 11.

## BULK BUYING CORNER

- NPN/PNP Silicon Planar Transistors TO-18 mixed untested similar to 2N706-6A-8, BSY26-7A9-95A and BCY70 etc. £4-25 per 500. £8 per 1000.
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- OC44, OC45 transistors fully marked and tested 500 to 999, 8p each, 1000+ 6p each.
- OC71 transistors fully marked and tested, 500 to 999, 6 each, 1000+ 5p each.
- A amp miniature plastic diodes IN4001 at 500 to 999, 4p each, 1000+ 3p each. IN4004 at 500 to 999, 5p each, 1000+ 4p each. IN4006 at 500 to 999, 6p each, 1000+ 5p each. IN4007 at 500 to 999, 8p each, 1000+ 7p each.

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IC 709C Linear Opp. Amp.	2-00	1-95	1-80
A.E.I. Fully marked & tested Gates	50p	40p	35p
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Matched Sets 1-OC44, 2-OC45 Per set	5p	5p	4p
Matched Sets, OC45, 1st & 2nd I.F. Per set	25p	20p	15p
TIC45 Thyristors, 6A, 60V Texas	15p	12p	10p
OA47 Gold bonded Diodes, marked & tested	15p	15p	12p
1W Zener Diodes 6.8V, 7.5V, 24V, 27V, 30V & 43V	3p	3p	3p
10W Zener Diodes: 7.5V, 11V, 13V, 20V & 100V	5p	4p	3p
Micro Switches, S/P, C/O Popular size	20p	17p	15p
1 Amp Bridge Rectifiers 25V, RMS	25p	20p	15p

1 Amp Plastic Rectifiers. These are voltage, reverse Polarity and other rejects from the BY 127 range. Ideal for low voltage Power Units etc. Price £1 per 100.

## COLOUR T.V. LINE OUTPUT TRANSFORMERS

Designed to give 25kV when used with PL509 and PY500 valves. As removed from colour receivers at the factory.

ONLY £1 each Post and packing 23p.

## BUMPER BUNDLES

These parcels contain all types of surplus electronic components, printed panels, switches, potentiometers, transistors and diodes, etc.

2 LBS IN WEIGHT FOR £1 Post and packing 25p.

## NEW TESTED AND GUARANTEED PAKS

B2	4	Photo Cells, Sun Batteries. 0.3 to 0.5V, 0.5 to 2mA.	50p
B79	4	IN4007 Sil. Rec. diodes, 1,000 PIV lamp plastic	50p
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B99	200	Mixed Capacitors. Postage 13p Approx. quantity, counted by weight	50p
H4	250	Mixed Resistors. Postage 10p. Approx. quantity counted by weight	50p
H7	40	Wirewound Resistors. Mixed types and values. Postage 8p.	50p
H8	4	BY127 Sil. Recs. 1000 PIV. 1 amp. plastic	50p
H9	2	OC71 Light Sensitive Photo Transistor	50p
H12	20	NKT155/259 Germ. diodes, brand new stock clearance	50p
H18	10	OC71/75 uncoated black glass type PNP Germ.	50p
H19	10	OC81/81D uncoated white glass type PNP Germ.	50p
H28	20	OC200/1/2/3 PNP Silicon uncoated TO-5 can	50p
H29	20	OA47 gold bonded diodes coded MCS2	50p

## F.E.T. PRICE BREAKTHROUGH!!

This field effect transistor is the 2N3823 in a plastic encapsulation, coded as 3823E. It is also an excellent replacement for the 2N3819.

Data sheet supplied with device.

1-10 30p each, 10-50 25p each, 50+ 20p each.

Make a Rev. Counter for your Car. The 'TACHO BLOCK'. This encapsulated block will turn any 0-1mA meter into a linear and accurate rev. counter for any car. **£1 each**

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MINIMUM ORDER 50p CASH WITH ORDER PLEASE. Add 10p post and packing per order. OVERSEAS ADD EXTRA FOR AIRMAIL.

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Various Contacts and Coil Resistances. No individual selection. Post & Packing 25p

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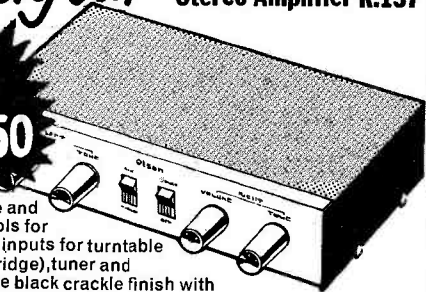
# JUST BEGINNING?

Then try out **8-Watt, 10-Transistor Stereo Amplifier R.137**

**ROC price**  
**£10.50**

Separate tone and volume controls for each channel, inputs for turntable (ceramic cartridge), tuner and tape. Attractive black crackle finish with brushed aluminium front. Frequency response: 70-20,000 Hz  $\pm$  3dB. Output: 4 watts per channel @ 8 ohms. Inputs: Phono 80mV; tuner/aux 80mV.

Normal retail price: **£14.70**

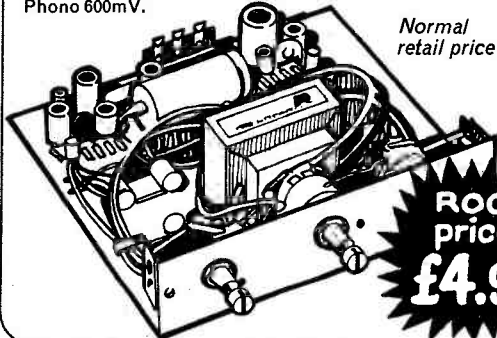


# FIRST STEP TO STEREO!

**5-Watt Transistor Stereo Amplifier Chassis R.123**

Completely self-contained, fully transistorised, mains-powered (240v AC) amplifier, needing only cabinet and knobs. Ideal for adapting mono players to stereo. Frequency response: 40-17,000 Hz  $\pm$  3dB. Output: 2.5 watts per channel @ 8 ohms. Input: Phono 600mV.

Normal retail price: **£7.30**



**ROC price**  
**£4.95**

# SOUNDS SENSATIONAL

**AM/FM/MPX Stereo Tuner Amplifier R.124**

A top quality amplifier with facility for receiving stereo broadcasts. Separate bass and treble controls, automatic frequency response, stereo headphone socket, output power: 8 watts. FM frequency range 88-108 MHz; AM frequency range 535-1605 K Hz. Inputs for turntable (ceramic cartridge) and tape. Frequency response: 50-10,000 Hz  $\pm$  3dB. Output: 4 watts per channel @ 8 ohms. Inputs: Phono 200mV, tape 100mV. FM: Sensitivity 20 $\mu$ V, stereo separation 26dB, image rejection 55dB. AM: Sensitivity 300 $\mu$ V.

Normal retail price: **£42.00**

**ROC price: £29.95**



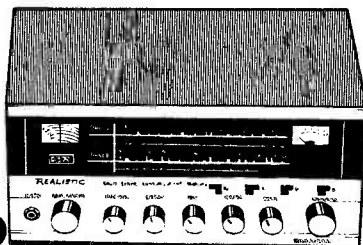
# World wide reception

**Professional Solid-state, Four-band Communications Receiver R.135**

Fully transistorised with continuous coverage from 555K Hz to 30 M Hz in four bands (with illuminated bandspread for 160-10 metres). Incorporates internal speaker, automatic noise limiter, SSB/AM/CW switch, AVC switch, S Meter, Receive and Standby switch, external socket for headphone or speaker, bandspread control, BFO control, on/off/AF gain, band selector, antenna trimmer and RF gain. Runs off 240 v AC, batteries or any 12 v DC negative ground source. Frequency ranges (in MHz): Band A, 535-1.6; B, 1.55-4.5; C, 4.5-13; D, 13-30. Sensitivity: 0.5 $\mu$ V @ 30mHz. Bandspread: 10-160 metres.

Normal retail price: **£65.00**

**ROC price: £45.00**

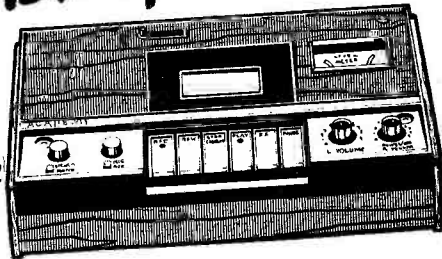


# AMAZING OFFER!

**Stereo Cassette Tape Unit R.142**

Complete stereo record and playback unit with line and microphone inputs. Fitted with tape counter, separate pause control, recording level metres for each channel, pop-up cassette ejection. Supplied complete with two pencil microphones. Wow & flutter better than 0.3%, frequency response 100-10,000 Hz. Tape speed: 1 1/2 IPS, 4.75 CMS. Rewind time: Better than 60 sec (C.60 cassette).  
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**ROC price**  
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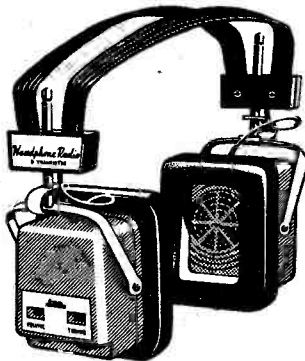


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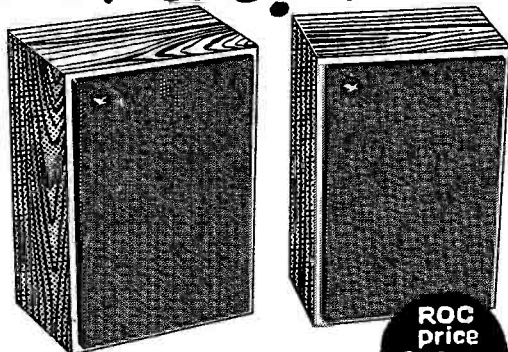


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For completely private listening without the distortion of the ordinary earphone adaptor. Battery operated; PP3. Fully transistorised. Frequency range: 535-1600 K Hz, Medium Wave Band. Maximum output: 300mW.

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# STEREO headphones

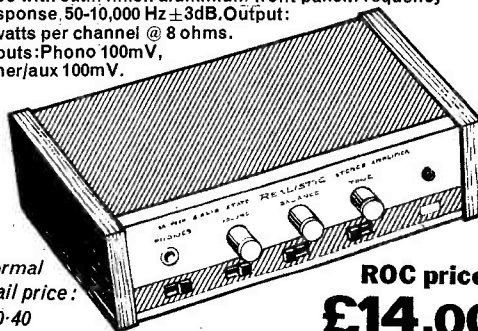
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Light and comfortable, with a frequency response of 30-15,000 Hz for real listening pleasure. Complete with jack plug, impedance 8-16 ohms.  
Normal retail price: £2.95

## Don't read this!

**10-watt Transistor Stereo Amplifier R.136**  
Ganged volume, balance and tone controls. Inputs for turntable (ceramic cartridge), tuner (see R.134) or tape. Oiled walnut case with satin finish aluminium front panel. Frequency response: 50-10,000 Hz ± 3dB. Output: 5 watts per channel @ 8 ohms. Inputs: Phono 100mV, tuner/aux 100mV.



Normal retail price: £20.40

**ROC price:**  
**£14.00**

## The Perfect match!



Matching unit to the R.136 amplifier. Covers AM and FM tuning bands with automatic stereo signal light. FM frequency range: 88-108MHz; AM frequency range: 535-1605kHz. FM: Sensitivity 5µV, stereo separation 25dB @ 1kHz, image rejection 50dB. AM: Sensitivity 250µV.

Normal retail price: £28.60

**ROC price**  
**£22**



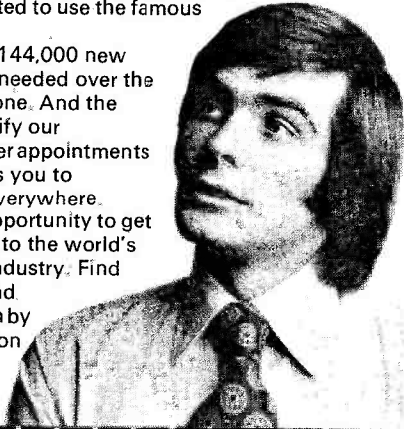
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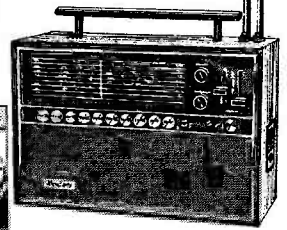
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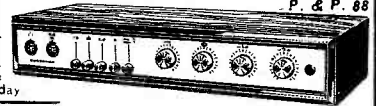
This system includes this elegantly styled solid state Teak finished cabinet tuner/amplifier. Covering VHF/FM, medium and long wavebands. The latest 4 Speed B.S.R. Mono/Stereo record changer with 2-10in. x 6in matching elliptical speakers. A complete Hi-Fi Stereo Radiogram at less than half normal price.

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P. & P. 88

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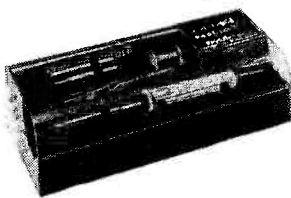
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£2.75



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Model CN 240/2  
- 15 watts  
- 240 volts

Fitted with nickel plated  $\frac{3}{32}$ " bit and packed in handy transparent box.

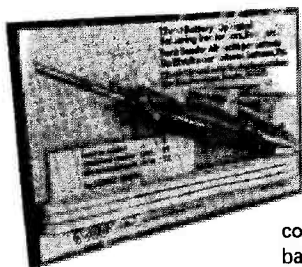
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ES240 D 25 watt  
soldering iron

In transparent display pack, fitted with long life iron-coated bit  $\frac{1}{8}$ " diam. Interchangeable spare bits  $\frac{3}{32}$ ",  $\frac{1}{16}$ ",  $\frac{1}{4}$ " (extra) available. Improved design to ensure strong and reliable high speed iron. Heats up in 2 minutes.

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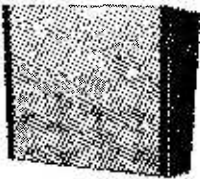


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Simple unit connects direct to amplifier and speakers to give attenuated headphone output, has 2 position switch to give headphones only—speakers only. Only £1.37 each P & P 12½.

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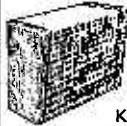
11" x 9½" x 5" deep, tapering to 3½" deep covered in Black Reseal and Mottled fawn Vynair £2.10 P & P 25p.

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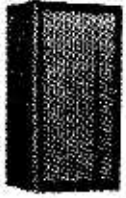
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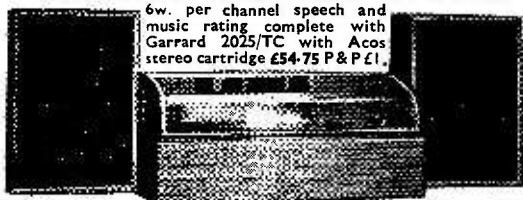


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6AM6	18	30L17	71	EBF89	81	GZ30	35	PL81	48	UCL83	35
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6X4GT	28	DAF91	22	EF80	23	PC85	27	R20	69	AF118	48
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12AU7	20	DK91	28	EH90	37	PCF86	45	U78	24	OC72	12
12AX7	23	DK92	42	EL33	55	PCF800	67	U91	80	OC75	13
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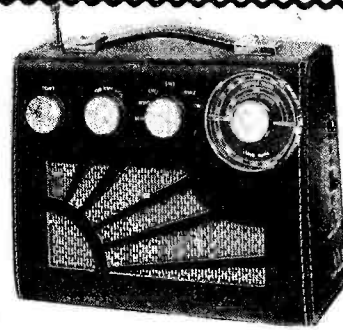
Built in Ferrite Rod Aerial for MW/LW. Retractable, chrome plated 7 section Telescopic Aerial, can be angled and rotated for peak short wave and VHF listening. Push Pull output using 600mw Transistors. Car Aerial and Tape Record Sockets. Switched Earpiece Socket complete with Earpiece. 10 Transistors plus 3 Diodes. 7in x 4in Speaker. Air Spaced ganged Tuning Condenser with VHF section. Volume on/off, Wave Change and Tone Control. Attractive Case in black with silver blocking. Size 9" x 7" x 4". Easy to follow instructions and diagrams. Parts price list and easy build plans 30p (FREE with parts).

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### ROAMER EIGHT Mk I



**NOW WITH SWITCHED TONE CONTROL**

7 Tunable Wavebands: MW1, MW2, LW, SW1, SW2, SW3 and Trawler Band. Built in Ferrite Rod Aerial for MW and LW. Retractable chrome plated Telescopic aerial for Short Waves. Push pull output using 600mW transistors. Car aerial and Tape record sockets. Selectivity switch. Switched earpiece socket complete with earpiece. 8 transistors plus 3 diodes. 7in x 4in. Speaker. Air spaced ganged tuning condenser. Volume/on/off, tuning, wave change and tone controls. Attractive case in rich chestnut shade with gold blocking. Size 9 x 7 x 4in. approx. Easy to follow instructions and diagrams. Parts Price List and Easy Build Plans 25p (FREE with parts).

Total building cost **£6-98** P. P. & Ins. 41p. (Overseas P. & P. £1)

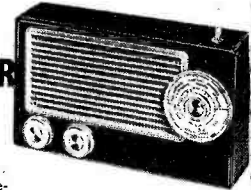
### ROAMER SEVEN MK IV



7 Tunable Wavebands: MW1, MW2, LW, SW1, SW2, SW3 and Trawler Band. Extra Medium waveband provides easier tuning of Radio Luxembourg, etc. Built in ferrite rod aerial for MW and LW. Retractable 4 section 24in. chrome plated telescopic aerial for SW. Socket for Car Aerial. Powerful push-pull output. 7 transistors and 2 diodes, including Micro-Alloy R.F. Transistors. 7 x 4in. P.M. speaker. Air spaced ganged tuning condenser. Volume/on/off, tuning and wave change controls. Attractive case with carrying handle. Size 9 x 7 x 4in. approx. Easy to follow instructions and diagrams. Parts price list and easy build plans 15p (FREE with parts). Earpiece with plug and switched socket for private listening, 30p extra.

Total building costs **£5-98** P. P. & Ins. 41p. (Overseas P. & P. £1)

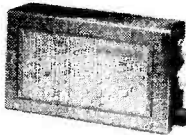
### ROAMER SIX



6 Tunable Wavebands: MW, LW, SW1, SW2, Trawler band plus an extra M.W. band for easier tuning of Luxembourg, etc. Sensitive ferrite rod aerial and telescopic aerial for Short Waves. 3in. Speaker. 8 stages—6 transistors and 2 diodes including Micro-Alloy R.F. Transistors, etc. Attractive black case with red grille, dial and black knobs with polished metal inserts. Size 9 x 5 1/2 x 2 1/2in. approx. Easy build plans and parts price list 15p (FREE with parts). Earpiece with plug and switched socket for private listening 30p extra.

Total building costs **£3-98** P. P. & Ins. 26p. (Overseas P. & P. £1)

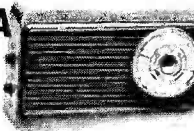
### POCKET FIVE



3 Tunable Wavebands: MW, LW, Trawler Band with extended M.W. band for easier tuning of Luxembourg, etc. 7 stages—5 transistors and 2 diodes, supersensitive ferrite rod aerial, fine tone moving coil speaker. Attractive black and gold case. Size 5 1/2 x 1 1/2 x 3 1/2in. Easy build plans and parts price list 10p (FREE with parts). Earpiece with plug and switched socket for private listening 30p extra.

Total building costs **£2-23** P. P. & Ins. 21p. (Overseas P. & P. 65p)

### TRANSONA FIVE

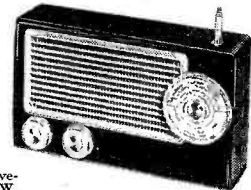


**NOW WITH 3in SPEAKER**

3 Tunable Wavebands: MW, LW and Trawler Band. 7 stage—3 transistors and 2 diodes, ferrite rod aerial, tuning condenser volume control, fine tone 3in. moving coil speaker. Attractive case with red speaker grille. Size 6 1/2 x 4 1/2 x 1 1/2in. Easy build plans and parts price list 10p (FREE with parts). Earpiece with plug and switched socket for private listening 30p extra.

Total building costs **£2-50** P. P. & Ins. 22p. (Overseas P. & P. 63p)

### TRANS EIGHT



6 Tunable Wavebands: MW, LW, SW1, SW2, SW3 and Trawler Band. Sensitive ferrite rod aerial for M.W. and L.W. Telescopic aerial for Short Waves. 3in. Speaker. 8 improved type transistors plus 3 diodes. Attractive case in black with red grille, dial and black knobs with polished metal inserts. Size 9 x 6 1/2 x 2 1/2in. approx. Push pull output. Battery economiser switch for extended battery life. Ample power to drive a larger speaker. Parts price list and easy build plans 25p (FREE with parts). Earpiece with plug and switched socket for private listening 30p extra.

Total building costs **£4-48** P. P. & Ins. 31p. (Overseas P. & P. £1)

## NEW! "EDU-KIT"

**BUILD RADIOS, AMPLIFIERS, ETC., FROM EASY STAGE DIAGRAMS. FIVE UNITS INCLUDING MASTER UNIT TO CONSTRUCT.**

**COMPONENTS INCLUDE:**

Tuning Condenser: 2 Volume Controls: 2 Slider Switches: 4"x2 1/2" Speaker: Terminal Strip: Ferrite Rod Aerial: 3 Plugs and Sockets: Battery Clips: 4 Tag Boards: Balanced Armature Unit: 10 Transistors: 1 Diodes: Resistors: Capacitors: Three 1" Knobs. Units once constructed are detachable from Master Unit, enabling them to be stored for future use. Ideal for Schools, Educational Authorities and all those interested in radio construction.

All parts including Case and Plans **£5-50** P. P. & Ins. 31p. (Overseas P. & P. £1)



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\* Open 10-1, 2.30-4.30 Mon.-Fri. 9-12 Sat.

## RADIO EXCHANGE CO

61 HIGH STREET, BEDFORD. Tel. 0234 52367

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ROAMER TEN  ROAMER SEVEN   
ROAMER EIGHT  TRANS EIGHT   
TRANSONA FIVE  ROAMER SIX   
POCKET FIVE  EDU-KIT

Parts price list and plans for .....

Name .....

Address .....

PW.34

## DISCOTHEQUE EQUIPMENT PACKAGE OFFERS

F.A.L. PHASE 50 MKII AMPLIFIER PR. FANE POP 25/2 SPEAKERS Terms: Deposit \$5.50 and 9 monthly payments of \$4.72 (Total \$47.98)	\$33.50 \$13.50 \$47.00	PACKAGE PRICE \$44 carr. \$1
F.A.L. PHASE 50 MKII AMPLIFIER PR. FANE POP 50 L/SPEAKERS Terms: Deposit \$10.50 and 9 monthly payments of \$5 (Total \$55.50)	\$33.50 \$21 \$54.50	PACKAGE PRICE \$49.50 carr. \$1
F.A.L. PHASE 100 AMPLIFIER PR. L125 50W L/S in cabinets Terms: Deposit \$22 and 9 monthly payments of \$11 (Total \$111)	\$61.95 \$59.90 \$121.75	PACKAGE PRICE \$110 carr. \$1.50
F.A.L. PHASE 100 AMPLIFIER 4 FANE POP 50 L/SPEAKERS Terms: Deposit \$14 and 9 monthly payments of \$10 (Total \$104)	\$31.95 \$22 \$103.95	PACKAGE PRICE \$94 carr. \$1.50

## F.A.L. DISCOTHEQUE CONSOLE



Incorporating twin Garrard SP25 Mk.III turntables and Goldring CS90 Ceramic Cartridges with diamond styli. Separate Vol. Bass and Treble controls for each turntable plus MONITORING FACILITIES. Black Rexine covered Cabinet with lid.

**£65** Carr. \$1.25 (Total \$71.80)

Terms: Deposit \$11 and 9 monthly payments of \$6.70 (Total \$71.80)

## AUDIOTRINE HI-FI SPEAKER SYSTEMS

Consisting of matched 12in. 11,000 line 15 Watt 15 ohm high quality speaker, cross-over unit and tweeter. Smooth response and extended frequency range ensure surprisingly realistic reproduction.

**£5.75** Carr. 30p

OR SENIOR 15 WATT INC. £6.75 Carr. 30p  
HF126 15,000 LINE SPEAKER carr. 35p

## AUDIOTRINE HIGH FIDELITY LOUSPEAKERS

Heavy construction. Latest high efficiency ceramic magnets. Treated Cone surround. "D" indicates Tweeter Cone providing extended frequency range up to 15,000 c.p.s. Impedance 3 or 8-15 ohms. Please state choice. Exceptional performance at low cost.

HF801D 8" SW £2.71 HF180D 12" 15W £4.75  
HF102D 10" 18W £3.40 HF128 12" 15W £5.60  
HF120 12" 15W £4.25 HF128D 12" 15W £5.90

## FANE 807 HIGH FIDELITY LOUSPEAKER

A full range 8in. 10 watt unit for excellent sound quality, in suitable enclosure. Cast chassis Roll P.T.C. cone surround and low throw voice coil to achieve very low fundamental resonance of 30 c.p.s. Tweeter cone is fitted to extend high note response. Frequency range 25 Hz to 15 KHz. Impedance 3 or 8-15 Ω. Gauss 10,000. Remarkable value.

**£3.50**

## HI-FI SPEAKER ENCLOSURES

Modern design. Teak veneer finish. Acoustically lined. All sizes approx. Carr. 30p. per enclosure  
JES Size 16 x 11 x 9in. Pressurised. Gives pleasing results with 8in. Hi-Fi speaker. **£5.35**  
SES For optimum performance with any 8in. Hi-Fi speaker. Size 22 x 15 x 9in. Ported. **£6.47**  
SE10 For outstanding results SE12 For excnt prfmanc with 12in. with 10in. Hi-Fi 'spkr' HI-FI speaker and Tweeter. **£7.87**  
Size 24x16x10in. P.t'd. Size 25 x 15 x 10in.

## R.S.C. BATTERY/MAINS CONVERSION UNITS

TYPE BML. An all-dry battery eliminator. Size 5 1/2 x 4 1/2 x 2in. approx. Completely replaces batteries supplying 1.5v and 90v, where A.C. mains 200/250v. 50c/s is available. Complete kit with diagram **£3** Assembled ready for use **£3.50**

## R.S.C. TA6 6 Watt HI-FI SOLID STATE AMPLIFIER

200-250v. AC mains operated. Frequency Response 30-20,000 c.p.s. -2dB. Harmonic Distortion 0.3% at 1,000 c.p.s. Separate Bass and Treble. Input selector switch. Output for 3-15 ohm spkrs. Max. sensitivity 5mV. Output rating I.H.F.M. Fully enclosed enamelled case, 9 1/2 x 2 1/2 x 6 1/2in. Attractive brushed silver finish fascia plate 10 1/2 x 3 1/2in. and matching knobs. Complete kit of parts with full wiring diagrams and instructions. **£7.50** Carr. 40p.

OR FACTORY BUILT WITH 12 MONTHS GUARANTEE **£9.75**

## R.S.C. A11 HI-FI 12-14 WATT AMPLIFIER

PUSH-PULL OUTPUT. Two input sockets with sep. vol. controls for mixing. High sensitivity, 5 valves. Bass and treble controls. Response ± 3dB 30-20,000 c/s. Hum level -60dB. Sensitivity 40 millivolts. For Crystal or Ceramic P.U.s. High Impedance "mikes". For Musical Instruments etc.

SAE A.C. mains. For 3 & 15 ohm spkrs. Complete kit. Full instructions and point-to-point wiring diagrams. Carr. 60p SAE for leadst. Twin handled metal cover **£1.75** Factory built **£14.75** or Dep. \$3 and 9 mthly pymts of **£1.60** (Total **£17.40**)

## R.S.C. COLUMN SPEAKERS

IDEAL FOR VOCALISTS AND PUBLIC ADDRESS

All types 15 Ohms covered in Rexine Vynair  
TYPE C4100 IS ALSO SUITABLE FOR BASS GUITAR OR ELECTRONIC ORGAN

**TYPE C485 25-30 WATTS**  
Fitted four 8" high flux 8 watt speakers.  
Overall size approx 48 x 10 x 5 in. Carr. 60p  
Terms: Dep £3 and 9 monthly payments £17.75

**TYPE C4125 50 WATTS**  
Fitted four 12" 11,000 line 15 watt speakers: Overall size approx 56 x 14 x 9 in. Carr. 75p  
payments £2 (Total \$81) **£27.50**

**TYPE C4100 100 WATTS** inc. four 12" 50 watt speakers for conservative rating. Extra heavy construction. Size approx 68 x 16 x 10" Acoustically filled and pressurized. Terms: Dep. £7.50 and 9 mthly. pymts. £6.45 (Total \$56.55). Carr. £1 **£50.50**

## 30 WATT HI-FI AMPLIFIER FOR GUITAR, VOCAL OR INSTRUMENTAL GROUP.

A 2 or 4 input, 2 vol. control HI-Fi unit with Separate Bass and Treble controls. Current valves. Peak output rating. Strong Rexine covered cabinet with handles. Attractive black/gold P.V.C. fascia. Neon indicator. For 200-250v. A.C. mains. For 3 or 15 ohm speakers. Send S.A.E. for leaflet.

Terms: Deposit £3.70 and 9 monthly payments of £2.10 (Total £22.60) **£19.95** Carr. 65p

## HIGH QUALITY LOUSPEAKER UNITS

IN TEAK VENEERED CABINETS

L13 13" x 8" 10 Watt L12 12" Also  
10,000 lines 3 or 15 25 WATT supplied  
ohms. State impedance 10,000 lines Rexine  
required. 15 ohms. covered

**£5.25** carr. 40p **£10.50** carr. 45p

L125 50 WATT  
Two tone Rexine and Vynair finish. Fitted pair of 12" 50 watt high flux speakers for conservative rating. Impedance 8-15 ohms. Or deposit £4 and 9 monthly payments of £3.35. Total £34.15 Carr. 75p **£31** Carr. 75p

## R.S.C. BASS REGENT 50 WATT AMPLIFIER

A powerful high quality all-purpose unit for lead, rhythm, bass guitar, vocalist, gram, radio, tape. Peak Output rating. Loudspeaker unit optional horizontal or vertical mounting. **£60**

★ Two extra heavy duty 12in. Loudspeakers. Carr. £1.50  
★ Four Jack inputs and two Volume Controls for simultaneous use of up to four pick-ups or "mikes". Bass and Treble controls. Send S.A.E. for leaflet. Credit Terms Deposit £16 and 9 monthly payments of £5.75 (Total £67.75)

## FAL PHASE 50 MKII AMPLIFIER 50W FAL PHASE 100 AMPLIFIER 100W

Solid state. 4 Separately controlled inputs. Plus master vol. control. Ind. Bass and Treble Controls. Protective circuit to guard against damage from accidental shorts. Output for Speaker/s 3-30 ohms. Size 17" x 7" x 7" 200-250v. A.C. mains. Output 60 watts music rating. Or deposit £6 & 9 monthly payments £33.50 Carr. 65p

Solid State. 4 Separately controlled inputs Plus master volume control. Ind. Bass and Treble Controls. Output for speaker/s 3-30 ohms. Protective circuit to guard against damage from accidental shorts. I.H.F.M. Output rating. Or deposit £12 & 9 monthly payments £61.95 Carr. 75p Send S.A.E. for leaflets.

## FANE ULTRA HIGH POWER LOUSPEAKERS

All power ratings are R.M.S. continuous. 2 YEARS' GUARANTEE  
High flux ceramic magnets. Heavy cast chassis. All carr. free.

<b>'POP' 100</b> 18" 100 Watt 14,000 gauss 8/15Ω <b>£22.05</b> Dep. £6 and 9 monthly payments £2-10 (Total £115)	<b>'POP' 60</b> 15" 60 Watt 14,000 gauss 8/15Ω <b>£12.90</b> Dep. £3.80 and 9 monthly payments. £1.80 (Total £115)	<b>'POP' 50</b> 12" 50 Watt 13,000 gauss 15Ω <b>£10.50</b> Dep. £2 and 9 monthly payments £1.16 (Total £12.85) Pair suitable all purposes
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FOR BASS GUITAR, ELECT. ORGAN, ETC.

## F A N E LOUSPEAKERS 'POP' 25/2

12in. 25 WATT  
Dual Cone 15 Ω (for uses other than Bass Guitar or Electronic Organ). **£6.75** Carr. free or Dep. £1 and 9 mthly payments 75p (Total £7.75)

## R.S.C. A10 30 WATT ULTRA LINEAR HI-FI AMPLIFIER

Highly sensitive. Push-Pull high output. Hum level -70dB. Response ±3dB 30-20,000 c/s. All high grade components. Valves 6F86, 6F66, EC638, 807, 807, GZ34. Separate Bass and Treble Controls. Sensitivity 35 millivolts. For High Impedance microphones. For Clubs, Schools, Theatres, Dance Halls, Outdoor Functions, etc. For Electronic Organ, Guitar, String Bass, etc. Gram, Radio or Tape. Two separate inputs with vol. controls permit such as "mike" and Pick-up etc. to be used for mixing purposes, 200-250 v. 50 c/s A.C. mains. For 3 and 15 ohm speakers. Complete kit of parts with wiring diagram and instructions. Twin-handled perforated cover **£15.75** Carr. 65p  
TERMS: Deposit £4 and 9 monthly payments of £2-10 (Total £22.80). Send S.A.E. for leaflet.

## RSC TRANSFORMERS, L.F. CHOKES & RECTIFIERS

FULLY GUARANTEED. Impregnated and Interleaved where necessary

Primaries 200-250v. 50c/s. Screened  
MIDGET GAMBUR TYPE 2 1/2 x 2 1/2 in. 99p  
250v. 60mA, 6.3V. 2a. £1.05  
250-0-250v. 60mA, 6.3V. 2a. £1.05  
FIXED SHROUDED UPRIGHT MOUNTING  
250-0-250v. 60mA, 6.3V. 2a., 0-5-6.3V. 2a. £1.40  
250-0-250v. 100mA, 6.3V. 4a., 0-5-6.3V. 3a. £2.20  
300-0-300v. 100mA, 6.3V. 4a., 0-5-6.3V. 3a. £2.20  
300-0-300v. 180mA, 6.3V. 4a., c.t., 6.3V. 1a. £2.45  
For Mullard 610 Amplifier £2.45  
250-0-250v. 100mA, 6.3V. 4a., 0-5-6.3V. 3a. £2.20  
350-0-350v. 150mA, 6.3V. 4a., 0-5-6.3V. 3a. £2.65  
425-0-425v. 200mA, 6.3V. 4a., c.t., 5v. 3a. £2.45  
425-0-425v. 200mA, 6.3V. 4a., 6.3v. 3a., 5v. 3a. £5.10  
450-0-450v. 250mA, 6.3V. 4a., c.t., 5v. 3a. £5.50  
TOP SHROUDED DROP-TYPE TYPE  
250-0-250v. 70mA, 6.3V. 2a., 0-5-6.3V. 2a. £1.35  
250-0-250v. 100mA, 6.3V. 3.5a. £1.55  
250-0-250v. 100mA, 6.3V. 2a., 6.3v. 1a. £1.60  
350-0-350v. 80mA, 6.3V. 2a., 0-5-6.3V. 2a. £1.65  
250-0-250v. 100mA, 6.3V. 4a., 0-5-6.3V. 3a. £2.20  
300-0-300v. 100mA, 6.3V. 4a., 0-5-6.3V. 3a. £2.20  
300-0-300v. 150mA, 6.3V. 4a., 0-5-6.3V. 3a. £2.20  
Suitable for Mullard 610 Amplifier £2.60  
350-0-350v. 100mA, 6.3V. 4a., 0-5-6.3V. 3a. £2.20  
450-0-450v. 100mA, 6.3V. 4a., 0-5-6.3V. 3a. £2.60

FILAMENT OR TRANSISTOR POWER PACK  
Types 6.3v. 1.5a. 49p; 6.3v. 2a. 54p; 6.3v. 3a. 76p;  
6.3v. 6a. £1.30; 12v. 1a. 55p; 12v. 2a. 62p;  
1.5a. £1.35; 0.9-1.8v. 1.5a. £1.10; 0.12-25-43v. 2a. £1.76  
CHARGER TRANSFORMERS 0-9-15v. 1 1/2a. 89p;  
2a. £1.10; 3a. £1.25; 6a. £1.45; 6a. £1.65; 8a. £2.00  
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0-110/120v. 200-250-250v., 60-80 watts £1-10;  
160 watts, £1.90 250 watts £2.75; 600 watts £6.75.  
OUTPUT TRANSFORMERS  
Standard Pentode 6.000 Ω or 7,000 Ω to 3 Ω 50p  
Push-Pull 8 watts EL84 to 3 Ω or 15 Ω 85p  
Push-Pull 10 watts 6V6, ECL86 to 3 or 3.5, 8 or 15 Ω £1.37  
Push-Pull EL84 to 3 or 15 Ω 10-12 watts £1.85  
Push-Pull Ultra Linear for Mullard 610, etc. £2.20  
Push-Pull 15-18 watts, sectionally wound 6L6, KT66, etc. for 3 or 15 Ω £1.99  
Push-Pull 20 watt high quality sectionally wound EL34, 6L6, KT66 etc. to 3 or 15 Ω £3.30  
SMOOTHING CHOKES 150mA, 7-10H, 250 Ω 70p; 100mA, 10H, 200 Ω 60p; 80mA, 10H, 350 Ω 60p; 60mA, 10H, 400 Ω 75p.  
SELENIUM RECTIFIERS F. W. (Bridged)  
All 6/12v. D.C. output. Max. A.C. input 18v.  
1a. 25p. 2a. 35p. 3a. 50p. 4a. 65p. 6a. 80p.

# Introducing R.S.G. MkIII SUPER 30 HI-FI STEREO AMPLIFIER

A COMPLETELY NEW DESIGN FURTHER IMPROVED IN BOTH APPEARANCE and PERFORMANCE. REPRESENTING VALUE FAR HIGHER THAN THE PRICES SUGGEST.

Only high grade components by leading manufacturers. COMPLETE KIT OF PARTS **£25** Carr. 65p

Or FACTORY BUILT with 12 months guarantee Dep. **£3-75** and 9 monthly payments **£3-50** (Total **£37-25**)  
Or FACTORY BUILT in cabinet as illustrated Dep. **£8** and 9 monthly payments **£3-88** (Total **£40-74**)

PRINTED CIRCUITRY, TWENTY SILICON TRANSISTORS. FOUR DIODES, FOUR RECTIFIERS. TECHNICAL DETAILS (Applying to each channel where appropriate) CONTROLS: PUSH-BUTTON SELECTOR (1) Disc (2) Radio (3) Tape (4) Mono L (5) Mono R (6) SPEAKER DIS. (7) Mains on/off. Bass, Treble, and Balance. Plus Ceramic/Mag P.U. Switch.



- ★ SATIN SILVER METAL FACIA with black lettering. Black edged knobs with bright silver centres.
- ★ PUSH-BUTTON SELECTOR SWITCHING
- ★ NEON INDICATOR
- ★ JACK SOCKET FOR HEADPHONES
- ★ CABINETED MODEL VENEERED IN SATIN TEAK, SUITABLE FOR ANY MODERN PICK-UP CARTRIDGE CERAMIC or MAGNETIC, REGARDLESS OF PRICE.
- ★ WE RECOMMEND USE WITH THE BEST ANCILLARY EQUIPMENT THAT CAN BE AFFORDED.

OUTPUT: 15 watts R.M.S. (Continuous) into 8 ohms. 10 watts R.M.S. (Continuous) into 15 ohms.  
HUM & NOISE - 75dB Min. Vol. - 65dB Full Vol. HARMONIC DISTORTION  
FREQUENCY RESPONSE: -3dB 7Hz to 70KHz 0.1% at 1000 Hz 10 Watts  
TREBLE CONTROL: +16dB to -12dB at 14KHz  
BASS CONTROL: +17dB to -16dB at 40Hz  
SENSITIVITIES: Disc Mag. 2.5mV. Ceramic 35mV. Radio 120mV. Tape 120mV.  
REAR PANEL SOCKETS ARE FOR 3 PAIRS OF INPUTS (1) P.U. (2) Radio. (3) Tape Amp. Plus pair for tape recorder signal take off and 2 pairs for speaker connections.

## R.S.G. HIGH FIDELITY STEREO PACKAGE OFFERS

- ★ Four fully wired units ready to 'plug in.'
  - ★ SUPER 30 AMPLIFIER (15 + 15 watt) in veneered housing
  - ★ GARRARD SP25 MKIII Turntable on Plinth with cover
  - ★ GOLDRING CS90 Ceramic Pick up Cartridge with diamond stylus
  - ★ PAIR OF STANWAY II Speaker Units
- £79-80**  
Total Price Carr. £1-50

Matching as recommended for optimum performance. Send S.A.E for coloured brochure showing other money-saving offers.



Package prices apply providing all individual units are purchased from any branch within 3 months. See leaflet.

ATTRACTIVE TEAK or AFROBROSIA VENEERED CABINETS and PLINTHS

- ★ TA12 AMPLIFIER 6.5 + 6.5 watt in veneered housing
  - ★ GARRARD SP25 MK III Player unit on Plinth
  - ★ GOLDRING CS90 Ceramic P.U. Cartridge with diamond stylus
  - ★ PAIR OF DORCHESTER Loudspeaker Units
- £58**  
Special Total Price Carr. £1-25

Or Deposit **£7-15** and 9 monthly payments **£6-35** (Total **£64-30**). Trans. Plastic Cover **£3-15** extra.

Package as above but with Garrard 8000 Auto-changer and Sonotone 9FA Ceramic Cartridge in lieu of SP25 and CS90 **£51-75** Carr. £1-25

Or Deposit **£6** and 9 monthly payments **£5-70** (Total **£57-30**) Trans. Plastic cover **£3-15** extra.

- ★ Super 30 Amplifier (15 + 15 watt) in veneered housing
  - ★ Goldring GL69 II Transcription Turntable on Plinth as illustrated
  - ★ Goldring Magnetic P.U. Cartridge.
  - ★ Pair of Stanway II speaker units
- £96-75**  
Special Total Price Carr. £1-50

### TERMS AVAILABLE ON ALL PACKAGE OFFERS

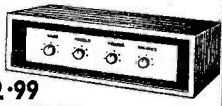
### 'YORK' HIGH-FIDELITY 3 SPEAKER SYSTEM

- ★ Moderate size only 25 x 14 x 10in. COMPLETE KIT **£22** Carr. 63p
- ★ Response 30-20,000 c.p.s. Impedance 15 ohms
- ★ Performance comparable with units costing considerably more. Consists of (1) 12in. 15 watt Bass unit with cast chassis, Roll rubber cone surround for ultra low resonance, and ceramic magnet. (2) 3-way quarter section series cross-over system. (3) 8 x 5in. high flux middle range speaker. (4) High efficiency tweeter. (5) Appropriate quantity acoustic damping material. (6) Handsome Teak veneered cabinet. (7) Circuit and full instructions. Terms: Dep. **£4-50** and 9 monthly payments **£2-25** (Total **£24-75**).

#### DEMONSTRATIONS AT ALL BRANCHES

### R.S.G. G66 6+6 WATT high quality STEREO AMPLIFIER

Individual Ganged controls: Bass, Treble, Volume and Balance. Printed circuit construction employing 10 Transistors plus Diodes. Output rating I.H.F.M. Frequency range 20-20,000 c.p.s. Suitable for Crystal Pick-ups, etc., and for loudspeaker output impedances of 3 to 15 ohms. For standard 200-250v A.C. mains operation. Attractive silver finished metal face plate & matching control knobs. COMPLETE KIT OF PARTS INCLUDING FULLY WIRED PRINTED CIRCUIT and comprehensive wiring diagram and instructions **£9-99** carr. 40p.  
Or FACTORY BUILT IN TEAK **£12-99**  
VENEERED CABINET as illustrated **£12-99**  
or dep **£2-50** and 9 mthly pymnts. **£1-45** (Total **£15-55**).



### HIGH FIDELITY LOUSPEAKER UNITS

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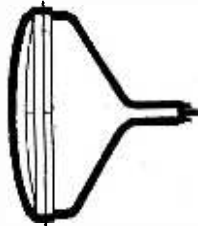
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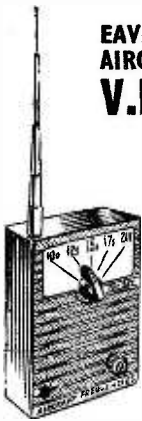
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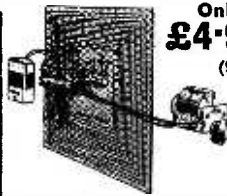
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**AMPEX 7.5v. D.C. MOTOR.** This is an ultra-precision tape motor designed for use in the AMPEX model AG20 portable recorder. Torque 450GM/CM. Stall load at 500ma. Draws 60 ma on run, 600rpm +5% speed adjustment. Internal AF/RF suppression  $\frac{1}{2}$ " dia.  $\frac{1}{8}$ " spindle, motor 3" dia.  $\frac{1}{2}$ ". Original cost £16.50. Our price £4.25. P. & P. 25p. Mu-metal enclosure available 75p each.

**SYNCHRONOUS MOTORS.** 220/380 v. 50/60 Hz. 250-300 rpm. 75p each.  
**MYCALEX MAINS.** Shaded pole, 1425 rpm,  $\frac{1}{8}$ " spindle. 2 for £1.25. Carriage Paid.

**MAINS INDUCTION MOTOR.** Open frame,  $\frac{3}{8}$ " spindle, weight  $\frac{1}{2}$  lb. Powerful. 88p each. P. & P. 12p.

**GEARED MOTORS** Shaded pole 240v. 50 Hz. 200 rpm. 10lb. in. £2.50. P. & P. 25p.  
**MYCALEX.** Open frame, shaded pole motors, 240v. 50 Hz. 7 rpm. 28 lb. in. 80 rpm. 12 lb. in. £2.25 each. P. & P. 25p.

**"CROUZET" TYPE 965.** 115/240v. 50 Hz. 47/68 watts. 50 rpm. Stoutly constructed. Size:  $2\frac{1}{4}$ " dia.  $\times$   $3\frac{1}{2}$ " long plus spindle  $1\frac{1}{2}$ "  $\times$   $\frac{1}{4}$ " dia. Anti-clock. £2.75. P. & P. 25p.

**TYPE 955.** Same as above, but 3 rpm. £3.00. P. & P. 25p.

**"M A L L O R Y" LONG LIFE BATTERIES.** Type A. RM12 cell 1.35v. 3,600 ma/h. CAP. 250/300 ma cont. current. Size:  $2\frac{1}{2}$ "  $\times$   $2\frac{1}{2}$ "  $\times$  1" for £1.00 or £2.00 per doz. Carr. Paid. Type B. Comprises 8  $\times$  RM 625 cells. Nom. volts. 1.35 each 10.5v. Overall, 350ma/H CAP. 20/25 ma cont. current. Size:  $2\frac{1}{2}$ "  $\times$   $1\frac{1}{2}$ "  $\times$  3" for £1.00 or £3.00 per doz. Carr. Paid.

**A.C./D.C. M/IRON AMMETERS.** 0-5 amps or 0-8 amps (suitable battery chargers etc.). Perspex front. Size:  $1\frac{1}{2}$ "  $\times$   $1\frac{1}{2}$ ". Any 2 for £1.10. Carr. Paid.

**ERNEST TURNER 800 $\mu$ A METER.** 160 $\Omega$  movement, 2" case elipic, plastic front. Green-Red-Green uncalibrated scale £1.50 each. Carriage paid.

**PAINTON BOURNS TRIMPOTS.** 1k, 2k, 2.5k, 5k, 10k, 20k, 50k, 500k. Other Trimmer pots in stock. RIL 10k. MORGANITE 1k. MEC 200  $\Omega$  (tubular) 50 $\Omega$ . Any 3 for £1.10 carr. paid.

**PROGRAMME TIMER BY HONEYWELL.** A bank of 15 micro-switches are each independently operated by 15 pairs of cams which in turn are individually adjustable to give switching periods of zero to 12 seconds with infinitely variable combinations. A mains synchronous motor drives the cam shaft at 1 rev. per 12 seconds (5 R.P.M.). Originally cost £15.00 plus. Many applications, such as lighting effects etc. New in original makers cartons. First class value at £5.75 plus 25p. P. & P.



**PRECISION FAN CO. (SMITHS INDUSTRIES) DOUBLE ENTRY CENTRIFUGAL FAN/BLOWER.** This is a beautifully balanced, particularly quiet running unit giving approx. 90 cubic ft./min. The motor is a 2 pole shaded pole Mycalox, drawing only 240ma on run. Weight 2 $\frac{1}{2}$  lbs. Sizes: case dia. 3.1 ins. width (case only) 3.125 ins. Width overall (inc. 5.25 ins. Aperture 3.125 ins  $\times$  1.85 ins. Offered well below makers price at £2.95. P. & P. 25p.

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**SLIDER SWITCHES.** 3 amp. type P.D.P.T. 1"  $\times$   $1\frac{1}{2}$ "  $\times$   $1\frac{1}{2}$ " deep. 1 amp. type P.D.T. 1"  $\times$   $1\frac{1}{2}$ "  $\times$   $1\frac{1}{2}$ " deep. £1.25 per doz. Either type or mixed as required. Carr. Paid.

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Prim 200/240v Sec 0-1-55-58-60 at 3-5 amps plus 0-90 at 100 ma. wax impregnated with screw term blocks. Weight 10 lbs £3.60 plus 40p P. & P.

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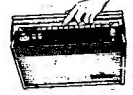
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Garrard SP25 Mk. III with MAG. cart ridge plinth and cover	£23.00+£1.50 p&p
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Viscount R101 amplifier	£22.00+90p p&p
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Viscount III Amplifier R100	£17.00+90p p&p
2 x Duo Type II speakers, pair	£14.00+£2 p&p
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### SPEAKERS Duo Type II

Size 17" x 10½" x 6½". Drive unit 13" x 8" with parasitic tweeter. Max. power 10 watts, 3 ohms. Simulated Teak cabinet. £14 pair+£2 p&p.

Duo Type III Size 23½" x 11½" x 9½". Drive unit 13½" x 8½" with H.F. speaker. Max. power 20 watts at 3 ohms. Freq. range 20Hz to 20kHz. Teak veneer cabinet. £32 pair+£3 p&p.

### SPECIFICATION R100/101

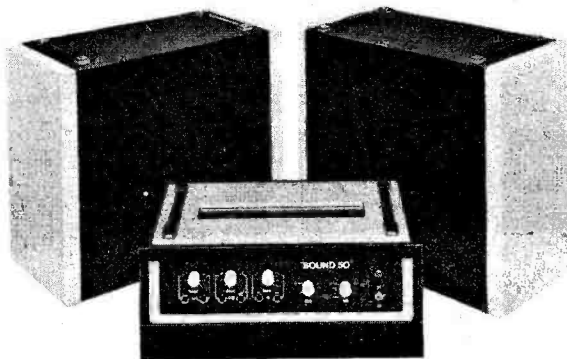
14 watts per channel into 3 to 4 ohms. Total distortion @ 10W @ 1kHz 0.1%. P.U.1 (for ceramic cartridges) 150mV into 3 Meg. P.U.2 (for magnetic cartridges) 4mV @ 1kHz into 47K, equalised within ± 1dB R.I.A.A. Radio 150mV into 220K. (Sensitivities given at full power). Tape out facilities; headphone socket, power out 250mW per channel. Tone controls and filter characteristics. Bass: +12dB to -17dB @ 60Hz. Bass filter: 6dB per octave cut. Treble control: treble +12dB to -12dB @ 15kHz. Treble filter: 12dB per octave. Signal to noise ratio: (all controls at max) R101—P.U.1 and radio—65dB. P.U.2. -58dB. R100 same as R101 but P.U.2 (for crystal cartridges) 450mV into 3 Meg. Cross talk better than -35dB on all inputs. Overload characteristics better than 26dB on all inputs. Size 13½" x 9" x 3½".

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**COMPLETE SYSTEM £50** Plus £6 P. & P.  
Sound 50 amp and 2 speakers

or available separately. Amplifier £28.50 plus £1.50 P. & P.  
Speakers £12.50 each plus £2.25 P. & P.

## THE ELEGANT SEVEN Mk. III

(350m W Output)



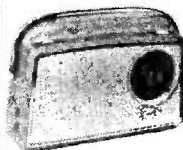
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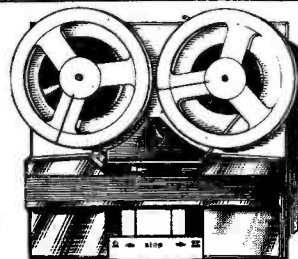


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R.C. 74 tape deck. Three speeds—7½, 3½ and 1½ ips.

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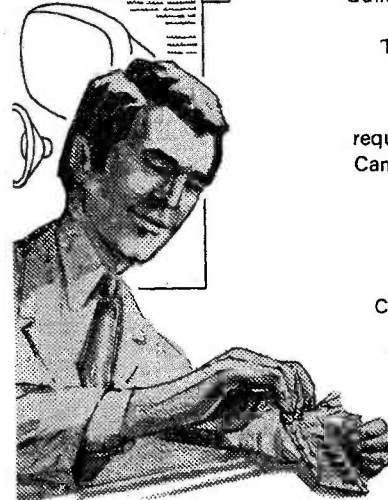
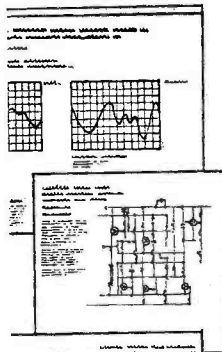
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BP01 = 7401	Quad 2-input pos. NAND gate (with open collector output)	0-15	0-14	0-12
BP02 = 7402	Quad 2-input pos. NOR gates	0-15	0-14	0-12
BP03 = 7403	Quad 2-input pos. NAND gates (with open collector output)	0-15	0-14	0-12
BP04 = 7404	Hex Inverters	0-15	0-14	0-12
BP05 = 7405	Hex Inverter (with open collector output)	0-15	0-14	0-12
BP10 = 7410	Triple 3-input pos. NAND gates	0-15	0-14	0-12
BP13 = 7413	Dual 4-input Schmitt trigger	0-29	0-28	0-24
BP20 = 7420	Dual 4-input pos. NAND gates	0-15	0-14	0-12
BP30 = 7430	8-input pos. NAND gates	0-15	0-14	0-12
BP40 = 7440	Dual 4-input pos. NAND buffers	0-15	0-14	0-12
BP41 = 7441	BCD to decimal mixer driver	0-87	0-84	0-58
BP42 = 7442	BCD to decimal decoder (4-10 lines)	0-87	0-84	0-58
BP46 = 7446	BCD-to-seven-segment decoder/driver	2-00	1-75	1-50
BP47 = 7447	BCD-to-seven-segment decoder/drivers (15V outputs)	0-97	0-94	0-88
BP48 = 7448	BCD-to-seven-segment decoder/driver	0-97	0-94	0-88
BP50 = 7450	Expandable dual 2-input and-or-invert	0-15	0-14	0-12
BP51 = 7451	Dual 2-wide 2-input and-or-invert gates	0-15	0-14	0-12
BP53 = 7453	Quad 2-input expandable and-or-invert	0-15	0-14	0-12
BP54 = 7454	4-wide 2-input and-or-invert gates	0-15	0-14	0-12
BP60 = 7460	Dual 4-input NAND	0-15	0-14	0-12
BP70 = 7470	Single-phase J-K flip-flop	0-29	0-28	0-24
BP72 = 7472	Master slave J-K flip-flop	0-29	0-28	0-24
BP73 = 7473	Dual Master slave J-K flip-flop	0-37	0-35	0-32
BP74 = 7474	Dual D type flip-flop	0-37	0-35	0-32
BP76 = 7476	Quad latch	0-47	0-45	0-42
BP78 = 7478	Dual J-K with pre-set and clear	0-43	0-40	0-38
BP80 = 7480	Expand full adders	0-67	0-64	0-58
BP81 = 7481	16-bit read/write memory	0-97	0-94	0-88
BP82 = 7482	2-bit binary full adders	0-97	0-94	0-88
BP83 = 7483	Quad full adder	1-10	1-05	0-95
BP86 = 7486	Quad 2-input exclusive NOR gates	0-32	0-30	0-28
BP90 = 7490	BCD decade counter	0-67	0-64	0-58
BP91 = 7491	8-bit shift registers	0-87	0-84	0-78
BP92 = 7492	Divide-by-twelve counters	0-67	0-64	0-58
BP93 = 7493	4-bit binary counters	0-67	0-64	0-58
BP94 = 7494	Dual entry 4-bit shift register	0-77	0-74	0-68
BP95 = 7495	4-bit up-down shift register	0-77	0-74	0-68
BP96 = 7496	5-bit parallel in parallel out shift register	0-77	0-74	0-68
BP100 = 74100	8-bit bistable latches	0-77	0-74	0-68
BP104 = 74104	Single J-K flip-flop equivalent 9000 series	1-75	1-65	1-55
BP105 = 74105	Single J-K flip flop equivalent 9001 series	0-97	0-94	0-88
BP107 = 74107	Dual Master slave flip-flops	0-40	0-38	0-36
BP110 = 74110	Gates master-slave flip-flops	0-55	0-53	0-50
BP111 = 74111	Dual data lock-out flip-flop	1-25	1-15	1-00
BP118 = 74118	Hex set-reset latches	1-00	0-95	0-90
BP119 = 74119	Hex set-reset latches, 24-pin	1-35	1-25	1-10
BP121 = 74121	Monostable multivibrators	0-67	0-64	0-58
BP141 = 74141	BCD-to-decimal decoder/driver	0-67	0-64	0-58
BP145 = 74145	BCD-to-decimal decoder/driver O/C	1-50	1-40	1-30
BP150 = 74150	16-bit data selector	1-80	1-70	1-60
BP151 = 74151	8-bit data selectors (with strobe)	1-00	0-95	0-90
BP153 = 74153	Dual 4-line-to-1-line data	1-20	1-10	0-95
BP154 = 74154	4- to 16-line decoder	1-80	1-70	1-60
BP155 = 74155	Dual 2- to 4-line decoder	1-40	1-30	1-20
BP156 = 74156	Dual 2- to 4-line decoder O/C	1-40	1-30	1-20
BP160 = 74160	Sync. decade counter	1-80	1-70	1-60
BP161 = 74161	Sync. 4-bit binary counter	1-80	1-70	1-60
BP190 = 74190	Sync. up-down BCD counter	3-50	3-25	3-00
BP191 = 74191	Sync. binary up-down counter (single clock line)	3-50	3-25	3-00
BP192 = 74192	Sync. up-down decade counter	2-10	1-95	1-75
BP193 = 74193	Sync. binary up-down counter (two clock lines)	2-10	1-95	1-75
BP196 = 74196	Pre-settable 50MHz decade counter	1-80	1-70	1-60
BP197 = 74197	Pre-settable 50MHz binary counter	1-80	1-70	1-60
BP198 = 74198	8-bit parallel L-R shift register	5-50	5-00	4-00
BP199 = 74199	8-bit parallel access shift register	5-50	5-00	4-00

D devices may be mixed to qualify for quantity price. Larger quantities—prices on application (DTL 74 Series only).

Data is available for the above series of I.C's in booklet form. Price 13p.

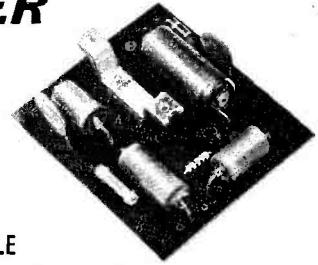
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UIC02 = 12 x 7402N	UIC51 = 12 x 7451N	UIC83 = 5 x 7483N
UIC03 = 12 x 7403N	UIC60 = 12 x 7460N	UIC86 = 5 x 7486N
UIC04 = 12 x 7404N	UIC70 = 8 x 7470N	UIC90 = 5 x 7490N
UIC05 = 12 x 7405N	UIC72 = 8 x 7472N	UIC92 = 5 x 7492N
UIC10 = 12 x 7410N	UIC73 = 8 x 7473N	UIC93 = 5 x 7493N
UIC20 = 12 x 7420N	UIC74 = 8 x 7474N	UIC94 = 5 x 7494N
UIC40 = 12 x 7440N	UIC75 = 8 x 7475N	UIC95 = 5 x 7495N
UIC41 = 5 x 7441AN	UIC76 = 8 x 7476N	UIC96 = 5 x 7496N

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\*Supply voltage (Vs) = 24V 15ohm load.

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LOGIC Type No.	Function	DTL 930 SERIES	IC's
BP930	Expandable dual 4-input NAND	1-24	25-99 100 up
BP932	Expandable dual 4-input NAND buffer	12p	11p 10p
BP933	Dual 4-input expander	13p	12p 11p
BP935	Expandable Hex Inverter	13p	12p 11p
BP936	Hex Inverter	13p	12p 11p
BP944	Dual 4-input NAND expandable buffer without pull-up	13p	12p 11p
BP945	Master-slave JK or RS	25p	24p 22p
BP946	Quad, 2-input NAND	12p	11p 10p
BP948	Master-slave JK or RS	25p	24p 22p
BP951	Monostable	65p	60p 55p
BP962	Triple 3-input NAND	12p	11p 10p
BP9098	Dual Master-slave JK with separate clock	40p	38p 35p
BP9094	Dual Master-slave JK with separate clock	40p	38p 35p
BP9097	Dual Master-slave JK with Common Clock	40p	38p 35p
BP9099	Dual Master-slave JK Common Clock	40p	38p 35p

Devices may be mixed to qualify for quantity price. Larger quantity prices on application. (DTL 930 Series only).

### BRAND NEW LINEAR I.C's—FULL SPEC.

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BP 201C—SL201C	TO-5	8	G.P. Amp	1-24 25-99 100 up
BP 701C—SL701C	TO-5	8	G.P. Amp	63p 53p 45p
BP 702C—SL702C	TO-5	8	OP Amp Direct OP	63p 50p 45p
BP 702—72702	D.I.L.	14	G.P. OP Amp (Wide Band)	53p 45p 40p
BP 709—72709	D.I.L.	14	High OP Amp	53p 45p 40p
BP 709F—7A709C	TO-5	8	High Gain OP Amp	58p 45p 40p
BP 711—7A711	TO-5	10	Dual comparator	58p 50p 45p
BP 741—72741	D.I.L.	14	High Gain OP Amp (Protected)	75p 60p 50p
7A 703C—7A703C	TO-5	6	R.L.F. Amp	45p 35p 27p
TAA 262—	TO-72	4	A.E. Amp	70p 60p 55p
TAA 293—	TO-74	10	G.P. Amp	90p 75p 70p

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# PRACTICAL WIRELESS

VOL 47 NO 6

Issue 776

OCTOBER 1971

## Who makes what?

**W**ELL, of course, that's easy! When you buy a radio set, hi-fi amplifier or piece of electrical equipment, the trade mark tells you that. Or if the mark is an unfamiliar one you can find the piece moulded on the cabinet or printed on the carton which says 'Made in Outer Mongolia' or whatever.

People are interested in where products are made for a variety of reasons. The possible standard of workmanship, value-for-money, reputation, reliability, the position of after-sales service, availability of spare parts—or even personal political motives—are all valid reasons why a purchaser would want to know who makes what, and where.

From November 30th, however, the Merchandise Marks Act comes to an end and from that date it will no longer be obligatory for imported goods to bear a 'country-of-origin' mark. The casual customer will therefore not be sure if he is buying a radio set made in Birmingham or Baluchistan, or an amplifier which is a Chinese-copy of an American design made in Hong Kong or Japan.

Of course, there will still be trade marks which proclaim that the goods are true-blue British or come from well-respected foreign companies. Sadly, though, things are not always what they seem for many tape recorders, radio and TV receivers, bearing the names of old-established British manufacturers have for some time been made overseas and imported for the home market.

From November 30th, protection of the consumer has been thrown at the retailer who, when asked, will be expected to disclose where a particular product is made. Unfortunately in many cases he will have no way of giving the required information. For instance, 'household-name' UK companies are none too keen to admit that some of their goods are being made in low-cost labour countries. Moreover, if a retailer does not know the country of origin, or (even inadvertently) gives the wrong answer, he will be at risk under the Trade Descriptions Act!

Apart from the factors mentioned earlier, which allow a customer to assess the advisability or otherwise of making a purchase, a particularly disturbing aspect of electrical goods (notably electric blankets and appliances) is that safety specifications may fall far short of those imposed on British-made goods and expose the user to potential hazards.

So, together with the British Radio Equipment Manufacturers' Association, the Radio and Television Retailers' Association and the Association of Manufacturers of Domestic Appliances, we beg the Secretary for Trade and Industry to think again. And to would-be purchasers after November 30th we can only say, most emphatically *caveat emptor!*

W. N. STEVENS—*Editor.*

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**NOVEMBER ISSUE WILL BE  
PUBLISHED ON OCTOBER 8th**

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# NEWS... NEWS... NEWS...

## Viscount value



The Viscount III Audio System is the first of a range of audio equipment marketed in the UK by R+TV Components (Acton) Ltd. under the Viscount brand name.

The complete system includes a choice of two amplifiers, a Garrard SP25 Mk III turntable and two Duo type II or type III speakers.

Amplifier RT100 is for ceramic cartridges and model RT101 which has an additional input stage accepts magnetic types. Both amplifiers incorporate f.e.t.'s giving excellent signal to noise ratios.

Prices are: RT100, £17; RT101, £22; Garrard SP25 with ceramic cartridge, £21 or with magnetic cartridge, £23. Duo type II speakers cost £14 the pair and Duo type III, £32.

Savings can be made by buying complete systems.

## Impex cases

In last month's issue we stated the following about Impex instrument cases:

"At no additional cost, Impex cases can be supplied with all or some of these specifications: alternative colours of blue or bronze; no hood; no ventilating slots or back/front anodised front/rear panels".

What we should have mentioned is that these additions can only be supplied free of charge for quantities over 24.

## NHK's anniversary

June 1 saw the anniversary of the Radio Japan Service. Thirty-six years ago NHK commenced this service in commemoration of the 10th anniversary of radio broadcasting in Japan and the attainment of 2 million licensed subscribers.

From June 1934 to 1945, NHK broadcast its domestic programmes to Korea, Taiwan and Manchuria, then Japan's outlying territories, utilising telephone channels of the International Telephone Company. Shortwave broadcasts were received in various parts other than the areas directed, and reception reports

began to come to NHK from Japanese residing abroad and from large numbers of overseas people. In those days, Japanese living in various parts of the world totalled nearly two million. These people raised their voices requesting the establishment of an overseas broadcasting service. In Japan, too, commencement of an overseas broadcasting service was also strongly desired, since this country had been isolated after her withdrawal from the League of Nations and was in need of reinforcing its public relations abroad. At first the service was known as Radio Tokyo (Radio Japan was first used in 1952).

## Avo wall chart

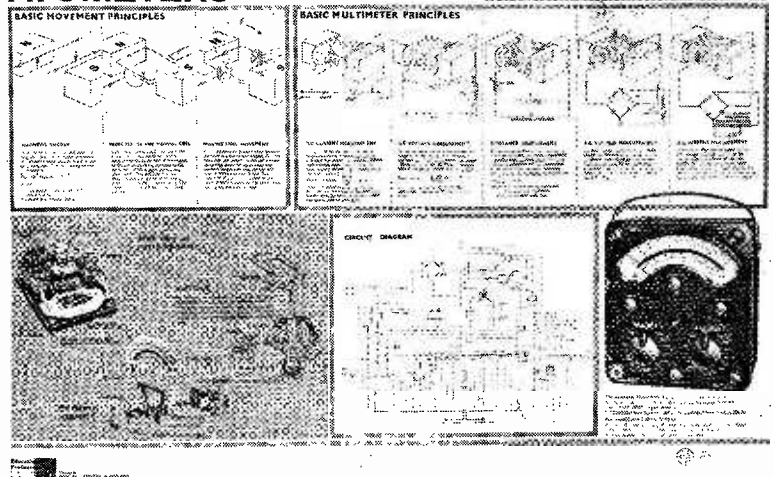
Avo Limited (Thorn Group) announce a new wall chart featuring the latest Mark 4 version of the Avometer Model 8. The design and layout is such that it will prove of great interest not only to Avometer users but also to technical schools and general education establishments as a teaching aid.

Information is presented in a clear, logical manner and the theoretical and practical information is both concise and easy to understand. Magnetic theory is developed pictorially to outline the operation of the moving coil movement whilst a mathematical treatment is used to derive the various ranges of a multimeter.

Illustrations of the interior of the instrument include an exploded view of the movement to simplify the constructional detail and a circuit diagram provides an introduction to standard symbols and references.

The Avometer chart (size 20×30in., 508×762mm.) is ideal for black-board or wall presentation and is available from *Spares Dept., Avo Limited, Avocet House, Dover*, at 75p per copy, including post and packing.

## AVOMETERS



# NEWS... NEWS... NEWS...

## Windermere VHF

The v.h.f. radio services from the Windermere relay station started on August 7. Radio 2 is on 88.6MHz, Radio 3 on 90.8MHz and Radio 4 on 93.0MHz, all with horizontal polarization.

The v.h.f. radio transmissions from this new relay station, which is situated on Claife Heights, above the western shore of Lake Windermere, will serve Ambleside, Windermere town, Bowness-on-Windermere, and an area around the northern shores of the lake.

## Stereo from Rowbridge

The necessary equipment has now been installed at Rowbridge to enable the Radio 3 transmitter (90.7MHz) to broadcast stereo-phony. This is being brought into use immediately, so that listeners can hear the Promenade Concerts in stereo—all except four of the concerts will be broadcast stereophonically in Radio 3. The stereo transmissions from Rowbridge will initially be on an engineering test basis; every effort will be made to maintain them, but there may be occasions when it will be necessary to revert to monophonic transmissions. The date for the start of the full stereophonic service will be announced later.

## Miniature Electric Tools

A range of battery-operated miniature tools has been introduced by Expo (Drills) Ltd., 62 Neal Street, London, W.C.2.

Two basic models are available. The 'Reliant' is designed for lighter work such as model making, and has a full load current of 1.5A. Its rated torque is 1.38oz. in. (100 gm.cm.). For jobs requiring a more powerful tool and for professional applications the 'Titan Super' is rated at 3.5A on full load. It has a rated torque of 350cmp operating at 4000-9000rpm. An extremely large range of accessories is also available for both models. Various collets and accessories are supplied with the different models, which range in price from £3 to £5.50.

## Lectures

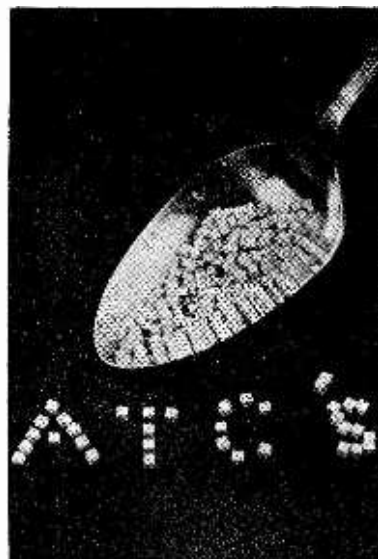
THE Polytechnic of North London Department of Electronic and Communications Engineering is running a course on Audio and Acoustic Measurements on Thursdays 6.30-8.30 p.m. 1971/2. 1971: Oct., 28, Parameters and Standards of Measurement R. N. Baldock, B.Sc., F.B.K.S.T.S. Nov. 4, Measurement of Microphone Performance, H. D. Harwood, B.Sc., B.B.C. Research; 11, Electrical and Mechanical Measurements in Tape Recording, R. L. West, B.Sc., C.Eng., F.I.E.R.E.; 18, Measurements in Professional Recording, Angus McKensie; 25, Electrical and Mechanical Measurements on Disc, Pickups and Accelerometers, S. Kelly, C.Eng., F.I.E.R.E. Dec. 2, Measurement of Loudspeaker Performance I, R. L. West; 9, Measurement of Loudspeaker Performance II, R. C. Driscoll, M.Sc.; 16, Measurement of Studio Characteristics, R. C. Driscoll, M.Sc. 1972: Jan. 13, Measurement of Noise Transmission, J. Moir C.Eng., F.I.E.E.; 20, Assessment of Noise Nuisance, J. Moir, C.Eng., F.I.E.E.; 27, Visit to A.I.R.O. Laboratories, Hemel Hempstead, G. Berry, B.Sc., C.Eng., M.I.Mech.E. and Assocs.

## Grand Junk Sale

The Star Short Wave Club, G3ZWA, is holding a "Grand Junk Sale" in aid of Radio Amateur Invalid Bedfast Club funds. It is to be held at the New Inn Hotel, Bramley Town Street, Bramley, Leeds 13. The date is Wednesday September 15th and time 7.30.

If any readers have any junk, the Star Club will collect within a radius of 25 miles from Leeds. Please contact Mr. T. Leeman, G8BUU, 115 Asket Drive, Seacroft, Leeds, LS14 1HX.

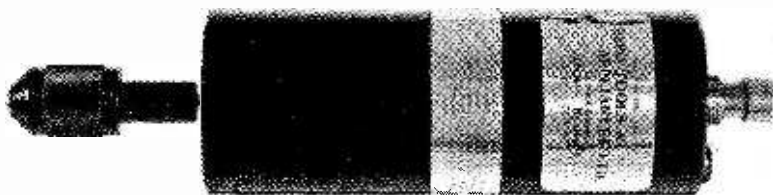
## Chip "C's"

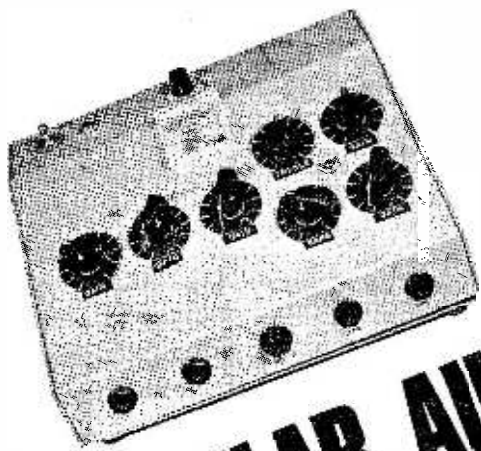


Featuring a very low insertion loss, a very high Q and high capacitance-to-volume ratios, a new range of ceramic and porcelain chip capacitors from Guest International Limited is ideal for u.h.f. and microwave applications. Apart from the basic pellet and chip, there is a wide choice of lead variations: stripline, axial and radial wire, axial and radial ribbon.

ATC 100 series are porcelain chips with an insertion loss of 0.03dB, a Q of over 10,000 and a capacitance range of 0.1 to 1000pF. In a case size of only 0.110in.square, the working voltage is up to 500V d.c.

ATC 200 series are ceramic chips with an insertion loss of 0.05dB. The capacitance range is 10pF to 1.2µF and chips are available in case sizes 0.050, 0.110 and 0.250in.square, depending on the value and the working voltage.





# MODULAR AUDIO MIXING SYSTEM

F.C. JUDD



So many audio sources are now in common use that an article describing a specific design would meet the needs of only a few. This problem is overcome here by giving circuits for virtually all sources and care in design has made possible a large number of permutations so that a custom built audio mixer is possible even for those readers unable to design their own. The clever constructional method employed also allows for rapid modification to meet any mixing need.

**A** STUDY of the four block diagrams in Fig. 1 will show how the various signal preamplifiers, the tone control unit and line amplifier etc. can be used to build audio signal mixing systems to cater for tape recording, public address, discotheque and even Hi-Fi applications. The combinations given are but a few of the permutations which can be extended for stereo use simply by duplication.

Each signal preamp has the same output level, 100mV, and will match directly into either the tone control unit or the line amplifier, both of which are designed to accept a signal level of 100mV. The tone control has unity gain so this provides 100mV output to match into the line amplifier. Any group of signal preamplifiers can therefore be coupled directly to the line amplifier or via the tone control unit and then to the line amplifier. This allows any of the signal preamplifiers to be used with or without the tone control unit.

The line amplifier has a nominal output of 1V r.m.s. at a fairly low impedance and can be used to drive a power amplifier module requiring between 500mV. to 1V input, or it can be coupled to a tape recorder or radio input, or to a public address or music amplifier with inputs rated for 500mV to 1V. Groups of the preamplifiers and line amplifier can be run from batteries or from an 18V mains power supply.

## COMBINATIONS

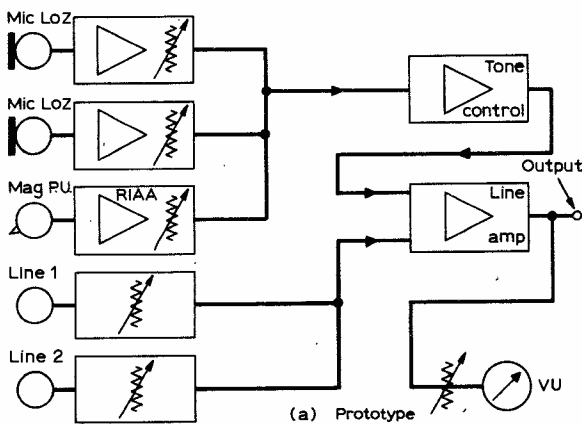
A fairly simple arrangement is shown in Fig. 1a and is intended for use as a general purpose signal mixer as shown on the front cover. This would be suitable for tape recording, as it has two microphone inputs, one input for low impedance pick-up (with R.I.A.A. correction), and two line level (200mV to over 1V) inputs. The tone control operates for the mic. and pickup inputs, whilst the line inputs go directly to the line amplifier. The system also includes a VU meter with variable control so that the meter can be set to read with the level meter on a tape recorder.

The combination shown in Fig. 1b has the same input channels but no tone control unit. The arrangement in Fig. 1c might be suitable for a small discotheque with one mic. input, two pickup inputs both via a tone control unit and one line input, suitable for the output from a tape recorder. For music application, Fig. 1d provides two mic. and two guitar inputs with separate tone control units for each guitar input. In each case the VU meter is optional but can be used as an overload indicator as will be shown later.

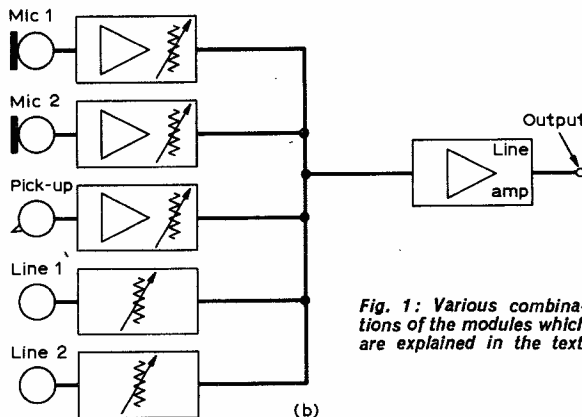
## PERFORMANCE SPECIFICATIONS

Seven preamplifiers will be described, each catering for specific signal sources as follows:—

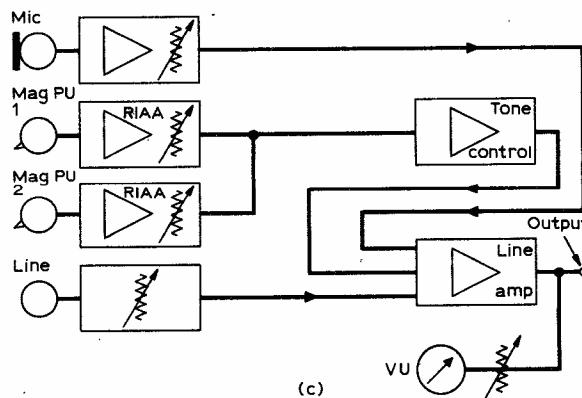
1. **LOW IMPEDANCE MICS.** (25 to 600 $\Omega$ ). Direct input, no transformer required. Input sensitivity 50 $\mu$ V. Output 100mV. Frequency response  $\pm$ 1dB. 30 to 30,000Hz. Signal-to-noise -50dB. (Code: **Mic. Lo-Z**).
2. **FOR MICROPHONES WITH BUILT-IN TRANSFORMERS.** Medium to high impedance. Input sensitivity 1mV. Output 100mV. Frequency response  $\pm$ 1dB 20 to 30,000Hz. Signal-to-noise -60dB. (Code: **Mic. Hi-ZT**).
3. **FOR CRYSTAL MICS.** High impedance. Input sensitivity 2mV. Output 100mV. Frequency response  $\pm$ 1dB 30 to 12,000Hz. Signal-to-noise -50dB. (Code: **Mic. Hi-ZX**).
4. **MAGNETIC PICKUP.** Impedance 56k $\Omega$ . Input sensitivity 5mV. Output 100mV. Frequency response to R.I.A.A. as shown in Fig. 2. Signal-to-noise -60dB. (Code: **PU Mag.**)



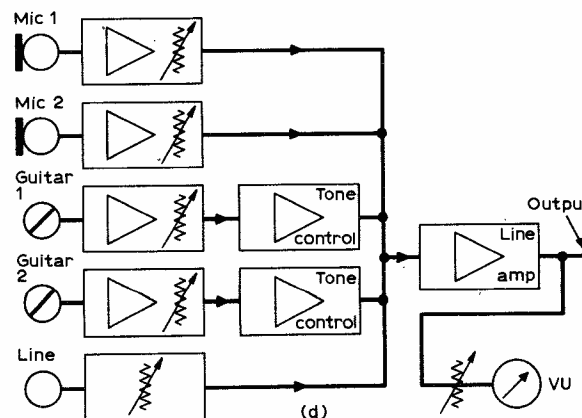
(a) Prototype



(b)



(c)



(d)

Fig. 1: Various combinations of the modules which are explained in the text.

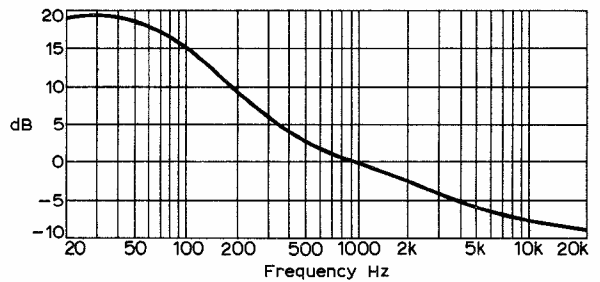


Fig. 2: The RIAA response curve incorporated in the magnetic pickup module.

5. CERAMIC PICKUP. Input impedance 2MΩ. Input sensitivity 60mV. Output 100mV. Frequency response approximately 20 to 20,000Hz ±1dB. Equalisation automatic due to high input impedance. Signal-to-noise -50dB. (Code: PU Cer.)
6. CRYSTAL PICKUP. Input impedance about 1MΩ. Input sensitivity 850mV. Output 100mV. Frequency response approximately 20 to 20,000Hz ±1dB. Equalisation automatic due to high input impedance. Signal-to-noise -60dB. (Code: PU Xtal.)
7. GUITAR PREAMP. Input impedance medium, 10 to 100kΩ. Input sensitivity variable. 50 to 100mV. Output 100mV. Frequency response ±1dB 20 to 30,000Hz. Signal-to-noise -50 to -60dB. (Code: G.)

The tone control unit will take the output from any of the preamps and provides 100mV output so that it can be coupled directly to the line amplifier. Its performance is as follows:— With tone controls neutral the flat response is 10 to 80,000Hz ±1dB. The response of the bass and treble controls is shown in Fig. 3 providing 15dB lift and 12dB cut at 40Hz and 15dB lift to 12dB cut at 20,000Hz The signal to noise performance is better than -90dB. (Code: TC.)

The line amplifier unit will accept the output from any of the preamps or the tone control unit and therefore has an input sensitivity of 100mV. The output signal level available is 1V r.m.s at an impedance of approximately 600Ω. The frequency response is flat from 10 to nearly 100,000Hz and the signal-to-noise performance -80dB. The output can be fed simultaneously to one or more tape recorders and/or amplifiers via series output resistors as will be shown. The overall gain of the line amplifier is adjustable i.e., the input sensitivity can be increased. (Code: LA.)

The line inputs do not require separate pre-amplifiers as these are arranged in passive network coupling directly to the line amplifier. The input sensitivity will be 200mV to over 1V r.m.s. at approximately 10kΩ impedance. (Code: L input.)

## CONSTRUCTION

The construction of each of the preamplifier modules is such that the circuit board is mounted on a small screen this, in turn, being secured to the fixing bush of the gain control (VR1 in each circuit). The complete preamp can therefore be secured to a front panel by the lock nut of the gain control. The tone control unit is similar except that there are two potentiometers and both are mounted on the small screen and then secured to the panel. The line amplifier can be simply mounted on a piece of aluminium angle (3/8 x 3/8 in) or on stand-off pillars as convenient. It need not be fixed to a panel but must

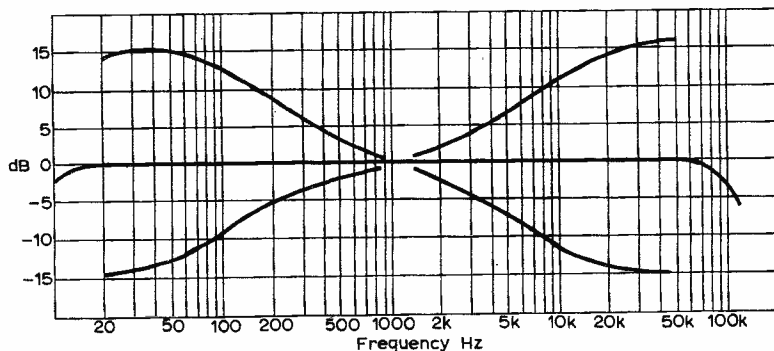


Fig. 3: Response curves of the tone control module.

be fairly well clear of mains power supply components. The input sockets for all inputs must be insulated from the front panel and earthed only at the common earthing point on the preamplifier board. If the mixing unit is to be mains powered, the components for the power supply must be kept as far away from the amplifier boards as possible and preferably with a screen around them.

The seven preamplifier boards are exactly the same and details for construction are given in Fig. 4. In each case the gain control (VR1) is fitted as shown

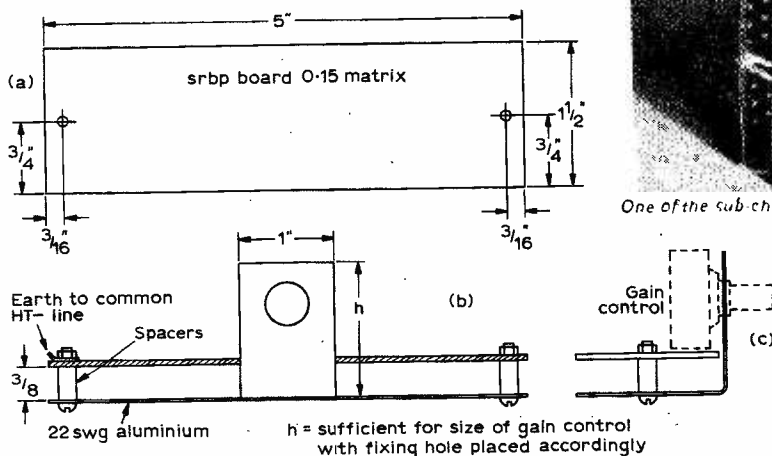
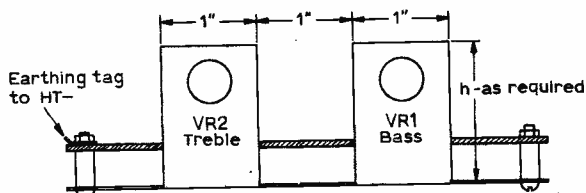


Fig. 4: Details of the sub-chassis used for each module.

in Fig. 4c. The construction of the tone control board is similar except that two controls have to be fitted so the screen has two flaps as shown in Fig. 5. The height of each flap and the position of the fixing hole will depend on the physical size of the potentiometers used.

## CIRCUITS AND ASSEMBLY OF THE MODULES

Each of the amplifier modules and the tone control



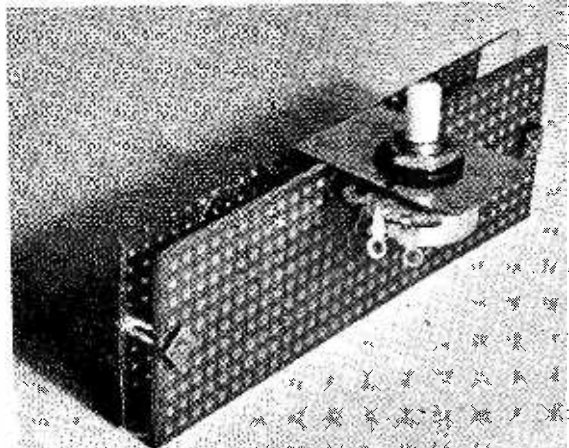
Controls mounted as in Fig. 4 (c)

Fig. 5: Modified sub-chassis for the tone control module.

can be tested separately by operating them from an 18V battery (two 9V units) and by checking each one with an audio signal generator and audio voltmeter or by connecting an appropriate input signal source and feeding the output to an amplifier.

## LINE AMPLIFIER

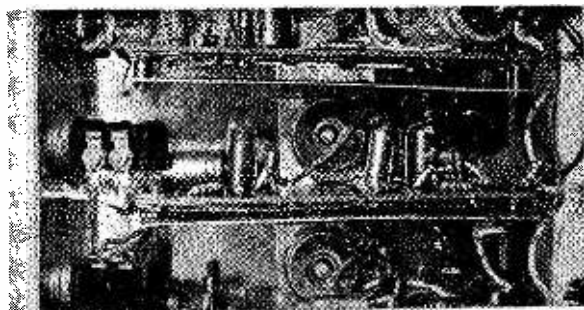
The best order of construction is to build the line amplifier (code: LA) first so that the preamps can be tested with it as each is completed. The circuit is given in Fig. 6 and the board layout in Fig. 7. As



One of the sub-chassis before the components are fitted; dimensions are given in Fig. 4.

with all the circuits except the tone control unit only one type of transistor is used—the BC109 silicon NPN—which is readily available and inexpensive. The line amplifier employs three of these beginning with Tr1 as an emitter follower input stage with Tr2 as the amplifier.

Negative feedback between Tr2 and Tr1 via the pre-set PR1 ensures a linear response and some adjustment over total gain. The pre-set should be adjusted so that with a 100mV input signal the output at C6 is exactly IV. If a signal generator and audio voltmeter are unavailable, set PR1 to mid-way position. The output transistor Tr3 operates as an emitter follower and provides a low impedance



An internal view of the prototype showing one of the modules. The input jack is on the left with the common wiring on the right.

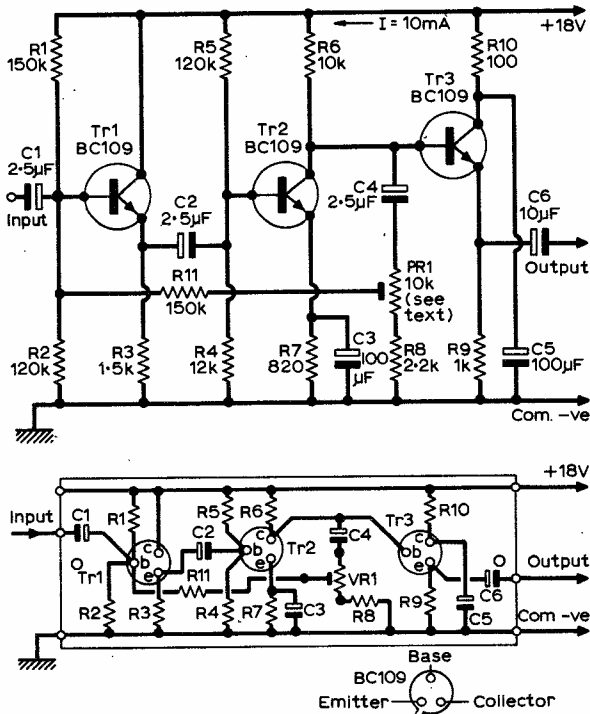


Fig. 6: (above) and Fig. 7 (below): The circuit and layout of the line amplifier module.

output. Details for feeding more than one power amplifier and/or tape recorder from the line amplifier output will be given later.

### MICROPHONE PREAMP (Mic Lo-Z)

The circuit is given in Fig. 8 and the board layout

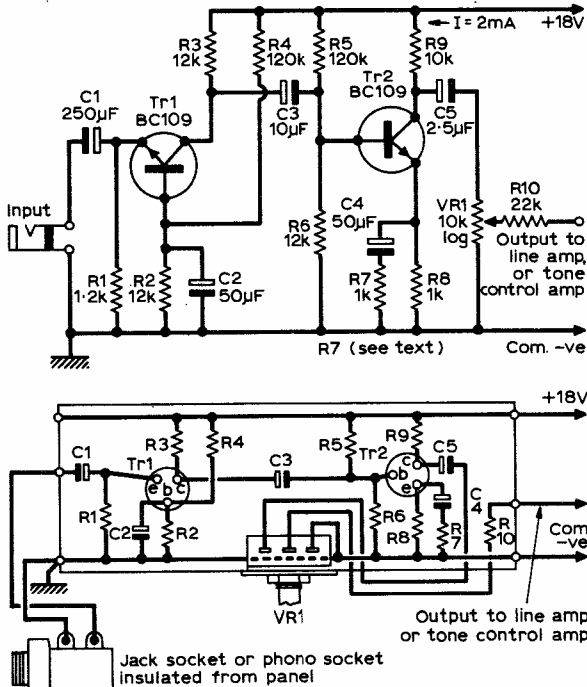


Fig. 8 (above) and Fig. 9 (below): The circuit and layout of the low impedance microphone preamplifier module.

## ★ components list

### Amplifier Modules Circuit Boards

1/16" MATRIX s.r.b.p. board to sizes given. 22 g. w.g. aluminum for module screens to sizes given.

#### Line Amplifier (LA)

Tr1, Tr2, Tr3 BC109  
PR1 10kΩ Miniature carbon pre-set

#### Resistors

R1	150kΩ	R6	10kΩ
R2	120kΩ	R7	820Ω
R3	1.5kΩ	R8	2.2kΩ
R4	12kΩ	R9	1kΩ
R5	100kΩ	R10	100Ω

All 1/4W, 10% types

#### Capacitors

C1	2.5μF	25V	C4	2.5μF	25V
C2	2.5μF	25V	C5	100μF	25V
C3	100μF	25V	C6	10μF	25V

#### Microphone Pre-amplifier (Mic. Lo-Z)

Tr1, Tr2 BC109  
VR1 10kΩ Log. Potentiometer

#### Resistors

R1	1.2kΩ	R6	10kΩ
R2	15kΩ	R7	1kΩ
R3	12kΩ	R8	1kΩ
R4	12kΩ	R9	10kΩ
R5	120kΩ	R10	22kΩ

All 1/4W, 10% types

#### Capacitors

C1	250μF	25V	C4	50μF	25V
C2	50μF	25V	C5	2.5μF	25V
C3	10μF	25V			

#### Power Supply

Transformer T1 18V Secondary Henry's Radio Type MT95  
Bridge Rectifier MR1 Henry's Radio Type LT118

C1	250μF	25-30V
C2	5000μF	25-30V
R	1W	see text

On/Off main toggle switch.  
Panel neon indicator.  
All electrolytics used in the amplifier circuits should be rated for at least 25V working.  
Each pre-amplifier will require an input jack socket or phono socket of the type that can be insulated from the panel on which they are mounted.

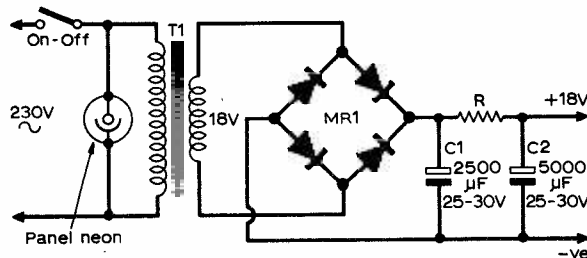
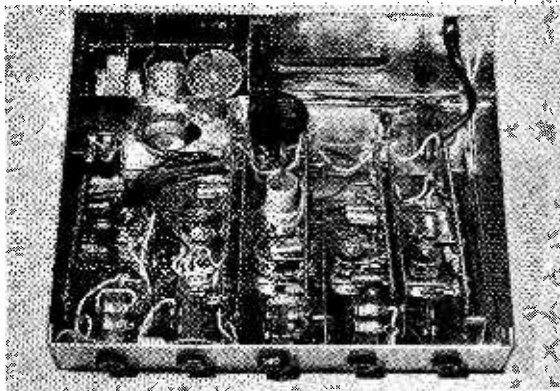


Fig. 10: Suggested circuit for a mains power supply to power the mixer.

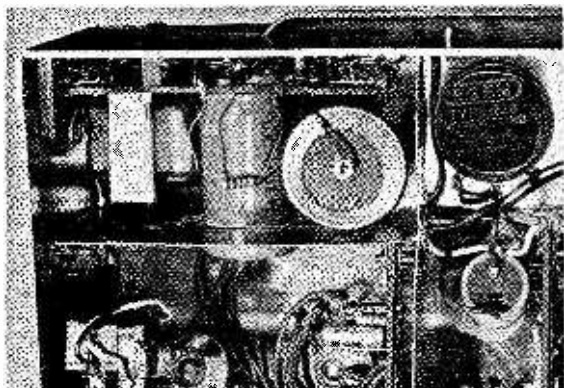
in Fig. 9. The input transistor Tr1 operates as a grounded base amplifier and provides a very low impedance input. Tr2 is a signal amplifier with negative feedback introduced by R7 in series with the emitter by-pass capacitor C4. This resistor can be reduced a little in value to obtain more gain for very low output microphones, although it should not be less than 680Ω otherwise the noise level will rise excessively. As with all the preamplifiers the output is taken to the gain control VR1 and thence via the series resistor (R10) which becomes part of the passive mixing network common to all the preamps.

## MAINS POWER SUPPLY

The current consumption of the preamplifiers at



*Internal view of the completed prototype.*



*The power supply should be properly screened as shown.*

18V varies between about 2 and 5mA. The line amplifier takes 10mA and the tone control unit 5mA. Four preamplifiers, a line amplifier and say one tone control unit, would require about 25mA which could be drawn from an 18V battery with reasonable economy. Two PP9 batteries would be ideal. Larger mixing units, particularly if built for stereo use and requiring duplication of preamps etc. are best operated from a mains power supply. One that will provide well over 100mA is given in Fig. 10 (see components list for transformer and rectifier details). The resistor R will be around 1kΩ for low current drain and of lower value for higher current drain. With the mixing circuits running, adjust R to obtain 18V across C2.

Part 2 next month, will deal with the rest of the preamplifier modules.

**TO BE CONTINUED**

CHARLES MOLLOY

# THE Medium Wave Column

**A** NEW 1000kW station on 1457kHz located near Tirana in Albania is being heard in this country as a background to BBC Radio 4, (South and West). It relays Radio Peking and has been heard at 2100hrs GMT with the identification 'Govarit Peking' followed by programmes in Russian. An increasing number of superpower broadcasters are appearing on the medium waves. Urumchi in Western China (2000kW) is audible all evening on 1525kHz; listen between Prague 1520kHz and Vatican Radio 1529kHz for Russian speech plus jamming. Libya has two megawatters—El Beida on 1124kHz and Tripoli on 1250kHz. El Beida is the stronger of the two; it is heard with EAJ15 Barcelona on the same frequency throughout the evening. Tripoli suffers from interference from Dublin/Cork until 2245hrs when the latter close down, leaving the channel clear. Further east, Riyadh (1200kW) in Saudi Arabia is on 587kHz and has been logged before midnight with Arabic programming.

Calcutta 1130kHz (1000kW) was heard frequently last winter before sign-off at 1700hrs. It is now on extended schedule and has been several times during the summer at 2230hrs GMT, as it changes from Chinese to Indian programming. There are three Voice of America stations in the Far East, each with 1000kW, all of which have been heard in the U.K. Bangkok, Thailand 1580kHz was logged at the end of September last year at 2200hrs GMT while Poro 1140kHz in the Phillipines and Okinawa 1178kHz in the Ryuku Islands are both heard in winter before sign-off at 1700hrs.

'Book of the World 1971' is the title of an unusual paperback now on sale in the bookshops. Sections deal with 181 different countries, each with a map plus details of the type of government, languages spoken, religions and currency. As well as providing the DXer with a valuable aid to station identification, this book gives background information on countries logged and adds interest to the hobby.

Broadcasts in English on the medium waves can be heard from a number of unexpected places during the late evening. Timisoara, Rumania on 755kHz has a programme in English, French and German at 2250hrs GMT, which should not be confused with the Voice of the West, in Portugal, also on 755, which starts its English programmes at 2245hrs. The Voice of America in Rhodes is 1259kHz is heard regularly in English between 2100hrs and midnight, with some interference from Wroclaw in Poland. Rhodes is one of the Dodecanese Islands situated near the coast of Turkey, which are usually counted as a separate country by DXers. The VOA is also heard in English from Thessalonika, Greece 791kHz between 2100hrs and 2130hrs. Enugu, Nigeria 1320kHz, although only 10kW, is a weak but consistent signal at 2300hrs GMT when it carries it's final news in English before closing down. ELBC Monrovia, Liberia on 629kHz has English programming and is usually logged between 2330hrs and sign-off at 0045hrs.

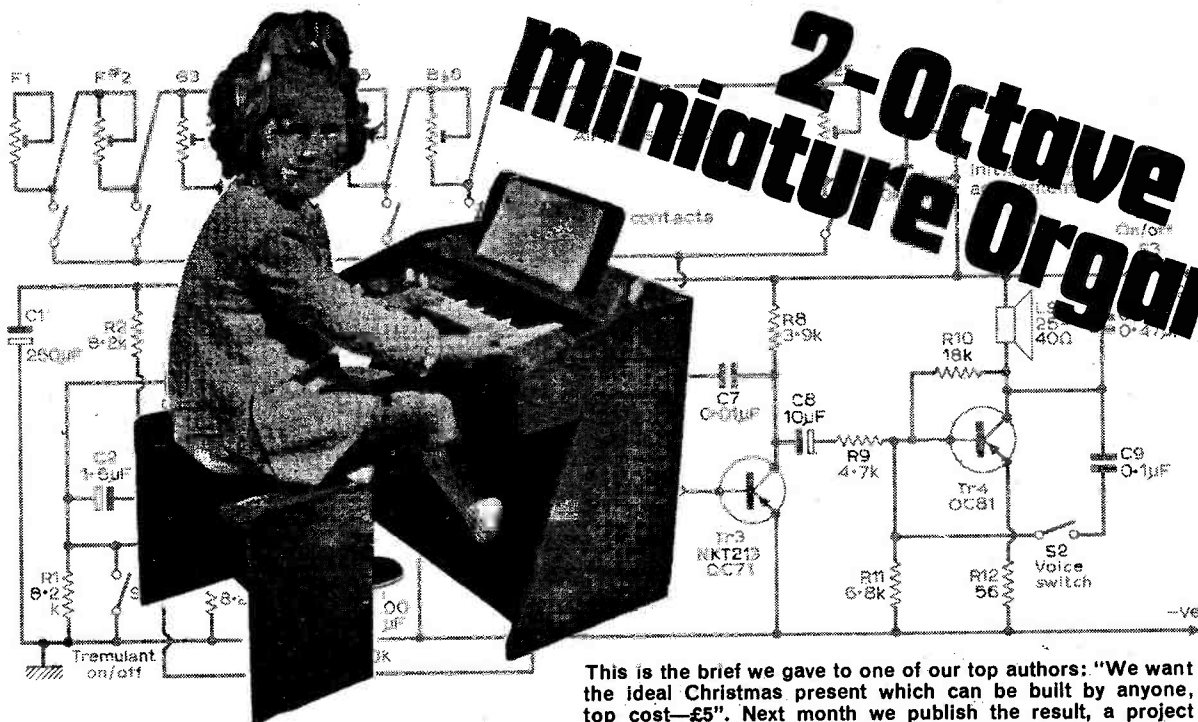




# IN NEXT MONTH'S

# PRACTICAL WIRELESS

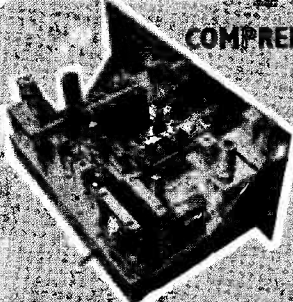
## 2-Octave Miniature Organ



### Special Feature

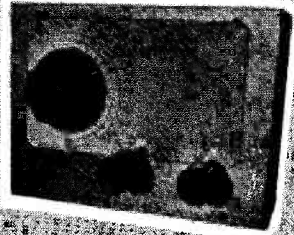
This is the brief we gave to one of our top authors: "We want the ideal Christmas present which can be built by anyone, top cost—£5". Next month we publish the result, a project which will go down as one of the all-time 'greats', a **2-Octave Miniature Organ**—complete with voicing and tremulant. The electronics is dead simple (just look at the circuit sketch above!) and the cabinet woodwork can be built by anyone who can use a saw. The £5 cost includes everything—just as you see it.

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**COMPREHENSIVE MULTI-BAND RECEIVER**

Do you want to build a communications receiver in easy stages? This design initially provides a basic 3 valve receiver, complete in itself, covering 550kHz to 30MHz with full bandwidth. At your leisure add an RF stage, a simple crystal filter, a carrier oscillator/product detector for receiving SSB/CW and finally a crystal marker. Full constructional details.



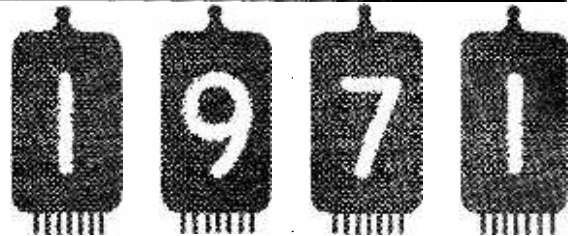
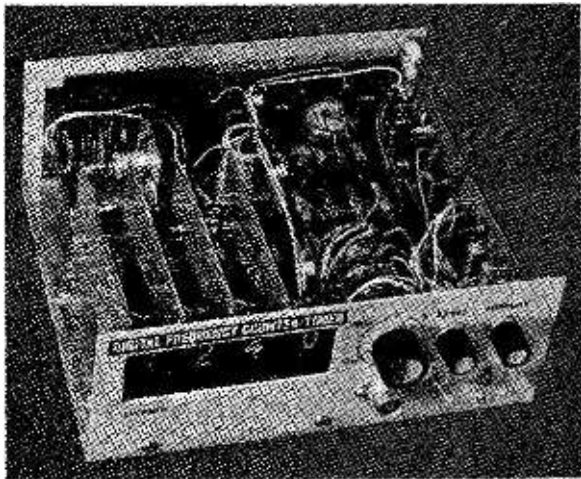
**BASIC SIGNAL GENERATOR**

A signal generator is essential for the testing, alignment and calibration of receivers and for quick tests of audio circuits. For the beginner or occasional dabbler, this basic design should prove ideal, with modulated or unmodulated outputs from 150kHz to 1.6MHz, plus a direct audio source; all outputs are fed via a variable attenuator.

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# DIGITAL FREQUENCY COUNTER/TIMER



J. THORNTON-LAWRENCE GW3JGA

## PART 2 (continued from the September issue)

This negative going step is passed by C5 to Tr7 base which moves by  $-5$  volts thus cutting off Tr7 and allowing the collector of Tr7 to rise to  $+5$ V.

The current through VR2 and R14 discharges C5 so that the negative voltage on Tr7 base rises exponentially until Tr7 conducts. The rate is determined by the setting of VR2, the DISPLAY control.

When Tr7 conducts, its collector voltage starts to fall, turning off Tr6 and thus increasing the base current to Tr7 and producing a fast negative going voltage at Tr7 collector. This voltage step is differen-

tiated by C7, R16 and R17 and inverted by IC2d to give a positive pulse of  $200\mu\text{s}$  duration.

The positive going edge of this pulse resets the counter to zero and the negative going edge sets the JK flip-flop IC1a and causes the cycle of operation to be repeated. The time for which the reading is displayed is controlled by the DISPLAY control and this is adjustable from about 0.5 second to 2 seconds.

### NOTE

Several wiring connections were omitted from figure 6 in the September issue. Pin 10, on IC's 3, 4, 5, 6 and 7, should be shown connected to the OV rail. Pins 1 and 12 on IC's 9, 11, 13 and 15, should be shown joined.

On IC1, pin 4 is the  $+5$ V supply rail and pin 11 is OV supply rail. On IC2, pin 14 is  $+5$ V supply rail and pin 7 OV supply rail. These latter connections were omitted from figure 6 for clarity.

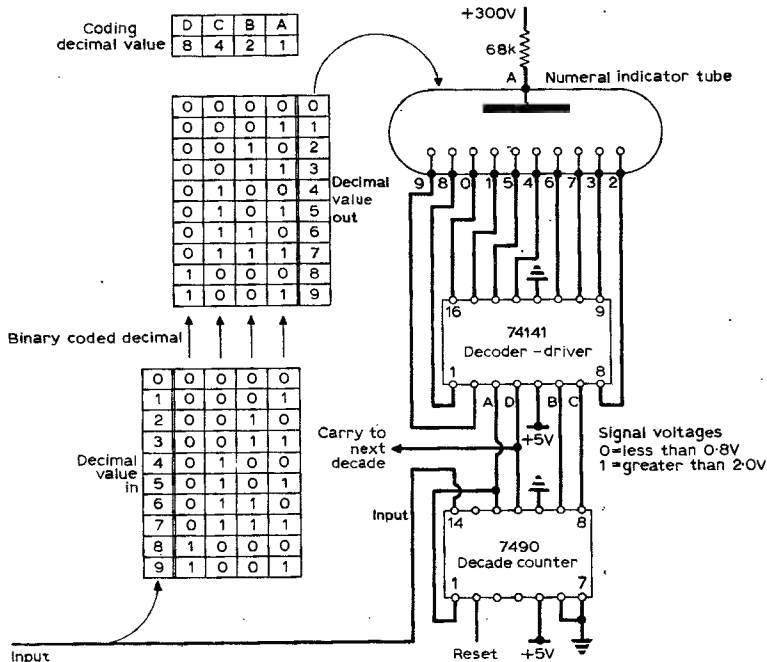


Fig. 9: Table showing the operation of the decade counter and decoder-driver.

## Counter and Display

The counter and display has four decades, each decade operates in the same way. The output of one decade is linked to the input of the next higher decade to perform the 'carry' operation and a reset connection is common to all decades.

The input to the counter is a series of pulses. The counting has to be carried out in binary form and then decoded into decimal form for display.

This is done using a decade counter I.C. type SN7490N, which consists of 4 master-slave flip-flops forming a  $\pm 2$  counter and a  $\pm 5$  counter.

The input signal goes to the input of the  $\pm 2$  counter (pin 14) and the output of this (pin 12) is linked externally to the input of the  $\pm 5$  counter (pin 1).

The outputs of the four flip-flops are called A, B, C, D and have a decimal value of 1, 2, 4, 8 respectively. The table showing the operation of the decade counter is included in Fig. 9.

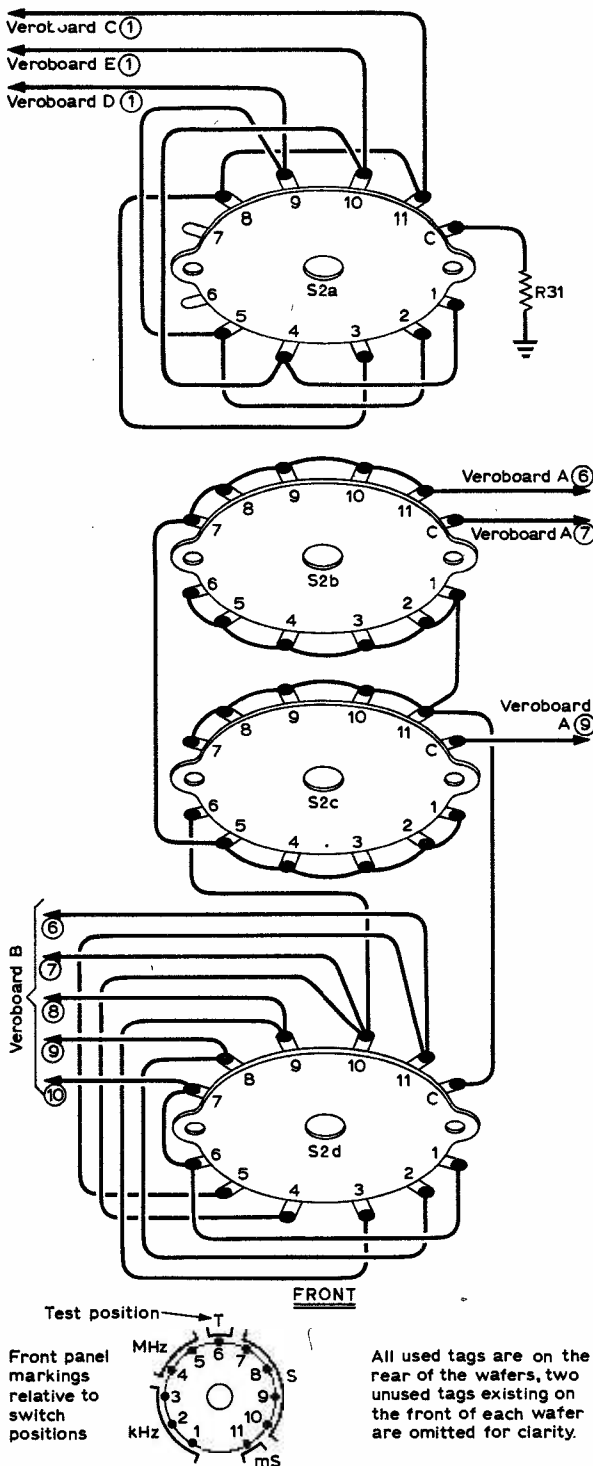


Fig. 10: Exploded view of the function switch S2, viewed from the front.

The counter can be reset to zero at any time by the application of a positive pulse to pin 2.

The binary coded decimal output from the counter, A, B, C, D is connected directly to the inputs of the decoder/numeral tube driver I.C. type SN74141N. Here the inputs are decoded back into decimal form

for driving the numeral tube (Hivac Type XN13).

The numeral tube contains neon gas at low pressure and has an anode and 10 wire cathodes in the form of numerals, 0-9.

With the anode connected to HT+ through a current limiting resistor, any cathode which is connected to 0V will be surrounded by a glow showing up the shape of the number.

The outputs of the decoder-driver are collector circuits of high voltage transistors which, when made to conduct, effectively connect the appropriate cathode to 0V. For example, suppose the input to the decade counter receives 5 pulses or cycles of input signal. The output will be D low, C high, B low, A high, representing a binary number of 0101. This number is decoded in the decoder/driver to figure 5 and the figure 5 output (pin 14) becomes switched to 0V causing the figure 5 to be displayed in the numeral tube.

Each counter, decoder/driver and tube is built on a Veroboard panel and the inter connection of these panels is shown in the main diagram Fig. 6.

The decimal indication is provided by miniature wire ended neon indicator lamps mounted between two numeral tubes and these are switched by the function switch S2a.

## Function Switch

The function switch S2 is made up from Radiospares Miniature 'Maka Switch' parts and consists of a shafting unit and 4 break-before-make 1 pole 12 way wafers. The wafers are spaced by 2 spacers on each side. Only 11 positions are used and the stop on the indexing mechanism is adjusted accordingly.

The wafers are lettered a, b, c and d, starting at the rear and working towards the indexing mechanism. Wafer 'a' controls the decimal point neon lamps, wafer 'b' the clock period input to the gate, wafer 'c' the signal input to the gate and wafer 'd' the output from the clock divider.

In the frequency positions 1 to 5, the output from the input stage is fed to the 'Signal Input' of the gate and the appropriate clock signal is fed to the 'Clock Period Input' of the gate. In the time positions, 7 to 11 of the switch, the output from the input stage is fed to the 'Clock Period Input' of the gate and the appropriate clock signal is fed to the 'Signal Input' of the gate.

A test position is provided in position 6 where the 1kHz clock output is counted for a period of 1 second to give a reading of 1,000. The test position only serves to check that the gate, counter and display are functioning, it does not provide a check of the crystal oscillator frequency.

The wiring and connections to the switch are shown in Fig. 10. The method of assembly is as follows:

1. On the shafting unit, check that the lengths of studding are screwed fully into the indexing mechanism plate and remove the end nuts and washers.
2. Rotate the switch spindle to the fully anti-clockwise position (as viewed from the front). The flats on the wafer end of the spindle should be in line with the studding. This is position "1".
3. The switch should now be held so that the lengths

of studding are at each side and the control knob end of the spindle is towards you, as shown in Fig. 10.

4. Take a 1 pole 12-way wafer and hold this with the side having the majority of tags, away from you and with the two tags that are facing you positioned in the top right hand segment. Rotate the rotor section until the common or rotor contact is making contact with tag 1. The slot in the rotor should now be horizontal.

5. Assemble the wafer on to the shafting assembly, keeping the side with the majority of tags facing away from the indexing mechanism. This wafer is now wafer "d" in Fig. 10.

6. Fit 2 spacers on each piece of studding.

7. Fit another wafer as described in operation 4 and 5 (wafer "c").

8. Repeat operations 6 and 7 until four wafers have been fitted (wafers "b" and "a").

9. Fit washers and fixing nuts to the studding.

10. The rotation of the switch should now be checked to see that all parts operate smoothly.

11. The rotatable stop plate, which is located on the face of the indexing mechanism, should now be set to give 11 positions, working clockwise and commencing from the maximum anti-clockwise position. This is the position at which all the wafers have been set. The stop plate may be held in place temporarily by the mounting nut, ready for assembly to the front panel.

12. The wiring of the switch may now be carried out as shown in Fig. 10. 22 s.w.g. tinned copper wire is used for wiring from tag to tag, sleeving being necessary only when crossing between wafers.

13. The correctness of the wiring can be checked by using an ohm or continuity meter and measuring between the appropriate tags whilst the switch is rotated, e.g. S2b/C is connected to S2d/C in positions 1, 2, 3, 4, 5 and 6.

## Power Supply

The power supply consists of a Radiospares Midget Mains transformer which with its associated rectifiers smoothing and regulators provides

+300V at 10mA	Unregulated
+5V at 350mA	Regulated
-5V at 5mA	Regulated

The output from the 250 volt secondary winding is rectified by D7 and smoothed by C12 to give about +300V output. The negative return is through R24 and D9 to 0V. The negative supply derived in this way is smoothed by C13 and regulated by the zener diode D9 to give -5V. The I.C. logic requires about 350mA at +5V and this is provided by the 6.3 volt filament winding on the transformer.

The 6.3 volt output is full wave bridge rectified to give about +7.5 volt across the reservoir capacitor C14. This feeds the zener diode D6 and the power emitter follower Tr11 to give the required 5V output.

## Veroboard Panels

The layout drawings of the 0.1x0.1in matrix Veroboard show the copper strip side of the panel the components on the reverse side being "seen through" the copper strips.

Each copper strip is given a letter code and each

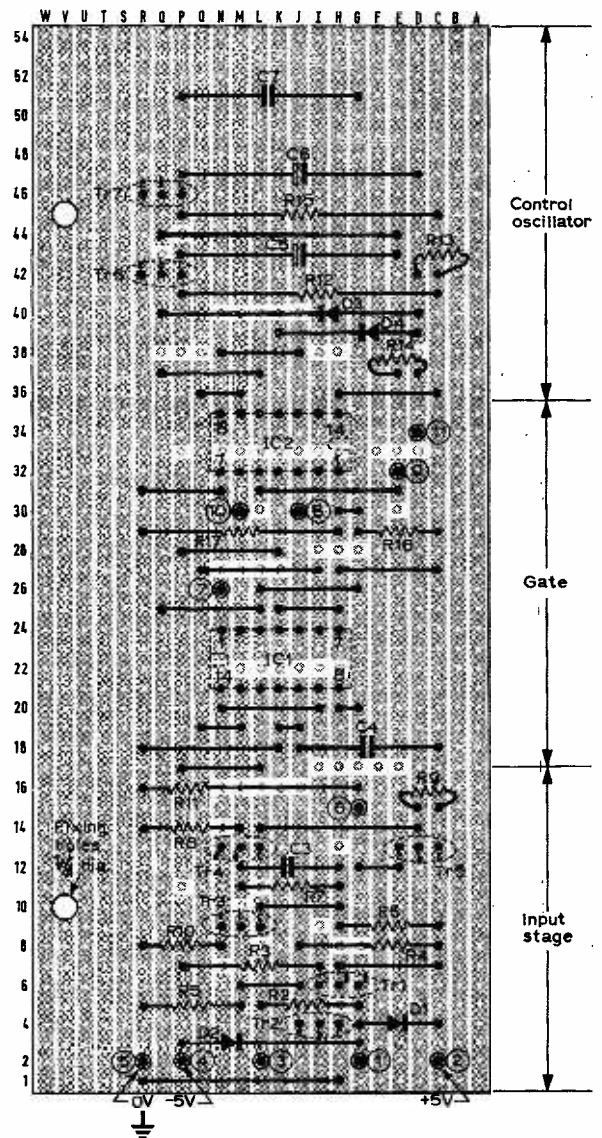


Fig. 11. Veroboard panel A. Input stage, gate and control oscillator. Viewed from copper side. Note correct orientation of integrated circuits when fitting. The integrated circuits and their holders are indented at one end to assist orientation.

horizontal row of holes, a number.

All solid horizontal lines represent wire links which connect one strip to another.

The orientation of integrated circuits and transistors should be noted carefully, some transistors may have unusual lead positions and these may have to be crossed over for the connections to be correct. Assembly of the components, etc., must be carried out in a systematic manner or errors will result. A suggested method is as follows:

1. Cut the Veroboard to the correct dimensions using a fine toothed saw and working from the copper side. Apart from checking the physical dimensions, also check that the correct number of holes appear in each direction.

2. Fix strips of masking tape on all four edges of the Veroboard panels. Also fix masking tape to the same edges on the reverse (copper) side of the board.

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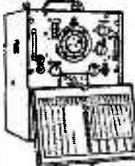
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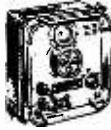
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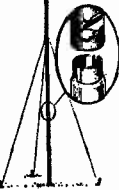
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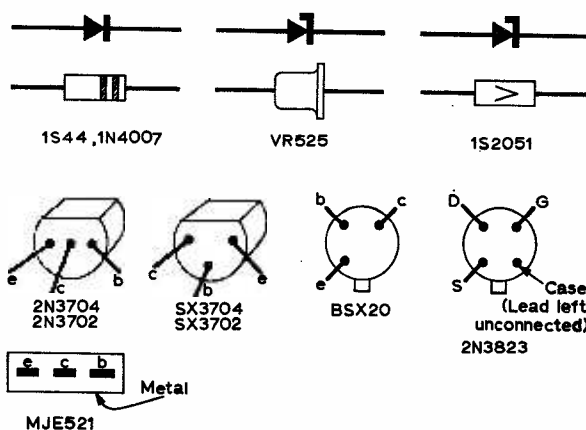


or solder to bridge the 0.025in gap between the copper strips.

8. Connections to the Veroboard panel are made to pins inserted in the appropriate places and soldered to the copper strip. These pins are Vero type TP 11032 or similar.

An insertion tool for this pin is Vero part No. IT 2151.

9. Tick off each break, link, component and pin on the drawings as they are fitted, this will identify any items which otherwise might be missed.

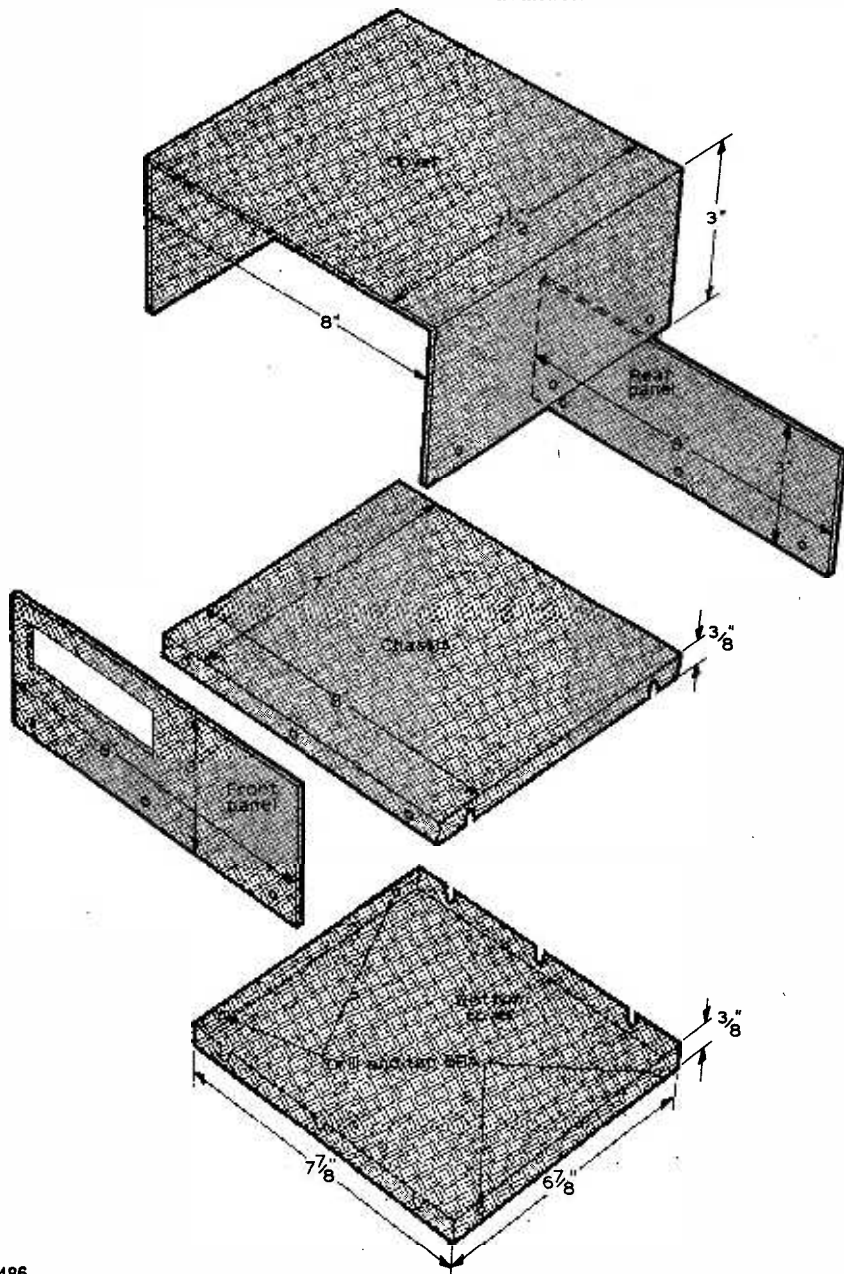


## Semiconductors

The 3702 and 3704 transistors are specified in the components list as being the '2N' types, these are the most popular version and are readily available.

The 3702 and 3704 transistors are also available

Fig. 14 (left) Cabinet and chassis construction.



in an 'SX' version. The lead connections for these types are all different from each other and are shown in the diagram above.

It should be noted that on the Veroboard panels, the connections run e.b.c. and when the '2N' version is used, the collector and base leads will have to be crossed over to line up with the appropriate holes in the Veroboard panel.

## Sockets for Integrated Circuits

Sockets are used for all the integrated circuits and although this increases the overall cost and is not essential for the operation of the instrument, it does provide the facility for disconnecting or changing an I.C. should a fault condition exist, also it does allow various parts of the instrument to be tested without incurring the expense of buying all the I.C.'s at once, 16-way sockets are required for I.C.8, 10, 12 and 14 and 14-way sockets for all the others.

The instrument is built using a simple aluminium chassis, panel and cover type of construction, as shown in Fig. 14. The finished chassis size is 8x7x3/8in deep and has a front and rear panel, each size 8x3in, fastened to the front and rear edges with 6BA screws and nuts.

(To be continued)



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40362	68p	2N2906A	47p	2N4292	15p	BC149	10p	BFX88	26p
2N696	17p	2N2974	20p	AC107	48p	BC153	19p	BFY50	28p
2N706	18p	2N2926	22p	AC126	20p	BC154	20p	BFY51	28p
2N790	12p	2N2926	11p	AC127	20p	BC157	12p	BFY52	28p
2N1131	29p	2N3053	27p	AC128	20p	BC158	11p	B8X20	16p
2N132	29p	2N3055	60p	AC153K	22p	BC159	12p	C407	17p
2N1302	19p	2N3702	18p	AC176	16p	BC167	11p	MO140	25p
2N1303	19p	2N3703	13p	ACY20	20p	BC168	10p	MP85531	35p
2N1304	28p	2N3704	13p	ACY22	16p	BC169	11p	MP85534	30p
2N1305	28p	2N3705	13p	AD140	63p	BC177	14p	NKT211	25p
2N1306	33p	2N3706	13p	AD142	50p	BC178	13p	NKT212	25p
2N1307	33p	2N3707	13p	AD149	55p	BC179	14p	NKT214	25p
2N1308	36p	2N3708	10p	AD161	33p	BC182L	11p	NKT274	45p
2N1309	36p	2N3709	11p	AD162	39p	BC183L	10p	NKT409	55p
2N1313	28p	2N3710	13p	AF114	24p	BC184L	11p	NKT405	75p
2N1711	36p	2N3711	13p	AF115	24p	BC212L	16p	OC71	38p
2N1893	54p	2N3819	23p	AF117	22p	BC213L	16p	OC81	25p
2N2147	95p	2N3904	35p	AF124	24p	BC214L	16p	OC81D	25p
2N2218	34p	2N3906	35p	AF127	22p	BCY70	18p	ZTX300	14p
2N2218A	44p	2N4058	13p	AF139	33p	BCY79	38p	ZTX301	16p
2N2219	38p	2N4059	10p	AF339	36p	BCY72	15p	ZTX302	22p
2N2219A	53p	11 ASY26	27p	BF115	23p	BF115	23p	ZTX303	22p
2N2270	62p	2N4061	11p	ASY28	27p	BF172	19p	ZTX304	27p
2N2369A	19p	2N4062	12p	BC107	12p	BF173	19p	ZTX500	18p
2N2483	35p	2N4124	18p	BC108	11p	BF194	14p	ZTX501	21p
2N2484	35p	2N4126	27p	BC109	12p	BF195	15p	ZTX502	25p
2N2484A	42p	2N4284	15p	BC125	15p	BFX85	25p	ZTX503	22p
2N2646	47p	2N4286	15p	BC128	22p	BFX86	25p	ZTX504	52p
2N2904A	42p	2N4289	15p	BC147	10p	BFX85	32p		

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C	1/20W	5%	82Ω-220KΩ	E12	9	8	7
C	1/8W	5%	47Ω-470KΩ	E24	1	0-8	0-7
C	1/4W	10%	47Ω-10MΩ	E12	1	0-8	0-7
C	1/2W	5%	47Ω-10MΩ	E24	1-2	1	0-9
C	1W	10%	47Ω-10MΩ	E12	2	1	0-9
MO	1/2W	2%	10Ω-1MΩ	E24	4	3-5	3
WW	1W	10% ± 1/20Ω	0.22Ω-3.9Ω	E12	7	7	6
WW	3W	5%	12Ω-10KΩ	E12	7	7	6
WW	7W	5%	12Ω-10KΩ	E12	9	9	8

Codes: C = carbon film high stability low noise MO = metal oxide Electrostrict TR5 ultra low noise WW = wire wound Pleseeey.

Values: E12 denotes series: 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 and their decades. E24 denotes series: as E12 plus 11, 13, 15, 20, 24, 30, 36, 43, 51, 62, 75, 91 and their decades.

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6BW7	55	DC90	80	ECC80	27	EZ80	21	PLC86	38	UCC85	34
6E1	60	DF91	14	ECC82	26	EZ81	22	PFL200	52	UCH81	30
6F28	89	DF96	35	ECC85	27	EL37	34	PL81	45	UCL82	56
6P25	55	DK91	28	ECH81	27	KT66	80	PL81	45	UCL83	48
6N7GT	28	DK92	40	ECL80	31	N78	85	PL82	30	UFB89	29
25L6GT	20	DK96	36	ECL82	30	PC86	47	PL83	32	UL84	31
30C15	60	DL92	26	ECL86	36	PC88	47	PL84	30	UY85	26
30C18	62	DL94	37	EF99	36	PC97	38	PL500	62	Z77	18
30E7	97	DL96	36	EF80	23	PC900	32	PL504	63		
30FL1	60	DY86	24	EF85	23	PC984	30	PY81	24		
30FL14	69	DY87	24	EF86	30	PC989	45	PY82	22		
30L15	58	DY802	38	EF89	24	PCC189	48	PY800	33		

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# TESTING

R A BUTTERWORTH



# surplus transistors

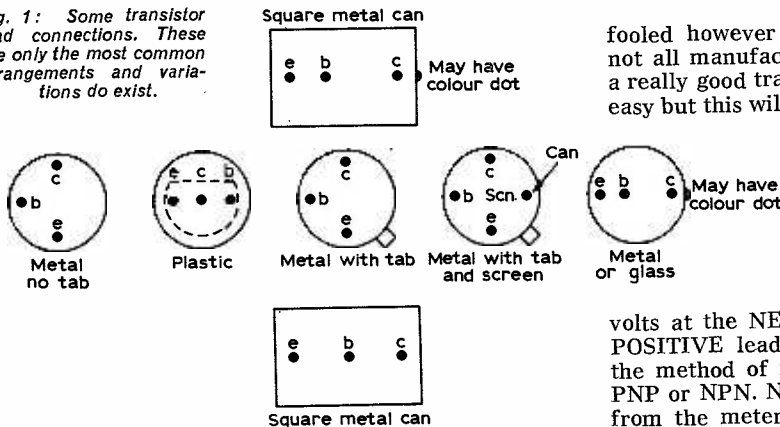
THE technical press offer so many transistor projects that many of us have bought and acquired a fair stock of transistors gathered from bargain packs or labouriously removed them from surplus computer boards. We then go through them only to find that many are un-marked, indecipherable, or have some queer markings not contained in any lists. The manufacturers are reluctant to supply data because they have been made to "customer requirements". A few hours spent in sorting these into NPN or PNP and grading them into four categories will save a lot of time, patience and money on the next project development. The methods of grading are only approximate and there are only four grades:—

1. RF types.
2. Low gain types.
3. High gain types.
4. All others which do not pass the tests described.

## PRELIMINARY TESTING

First do a thorough visual examination and sort the transistors into *known* and *unknown*. The *knowns*, however, should be put through the tests since they may be blown or below spec. If your collection contains transistors removed from computer boards, the leads will be short. Fortunately when these boards are assembled, small plastic

Fig. 1: Some transistor lead connections. These are only the most common arrangements and variations do exist.



spacers are fitted, in most cases to comply with manufacturer's recommendations as to bending and heat dissipation. The makers also usually bend over about  $\frac{1}{8}$  in on the solder side with the result that the lead lengths are in a safe condition. Any that are too short should be thrown away. Figure 1 shows the bases of seven categories into which these recovered units fall. Some may have a coloured dot, usually red or white, indicating the collector lead, also some are internally connected collector-to-can. Do not be

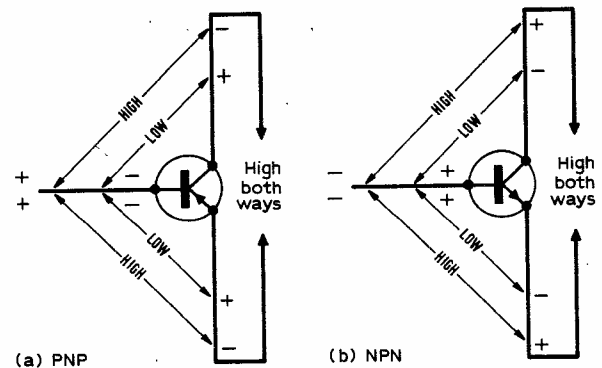


Fig. 2: Resistance readings found on a good transistor—see text for details.

fooled however by coloured sleeving on the leads; not all manufacturers use the same code. Of course a really good transistor checker can make things very easy but this will cost a good deal of money.

## IDENTIFYING THE LEADS

The first checks, sorting the PNP and NPN types and the leads are done with a multimeter on its low ohms range. A word of warning first about that multimeter. Most meters on the ohms range give positive volts at the NEGATIVE LEAD and negative at the POSITIVE lead, so check first. Figure 2 illustrates the method of finding out whether the transistor is PNP or NPN. Never be scared of reversing the leads from the meter; with about 1.5V, which is usually

available from the meter on low ohms ranges, you won't do any harm. Should you get a low resistance reading both ways between base and either of the other connections you can be fairly certain that there is an internal short. If you get a low reading between the base and one lead and a high at the other it is either bad or you are not on the base. It is probable that you will meet with marginal readings at times, so make tests as follows with reference to Fig. 3.

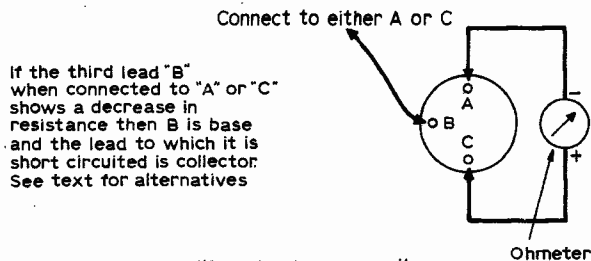


Fig. 3: Tests for identifying the base connections.

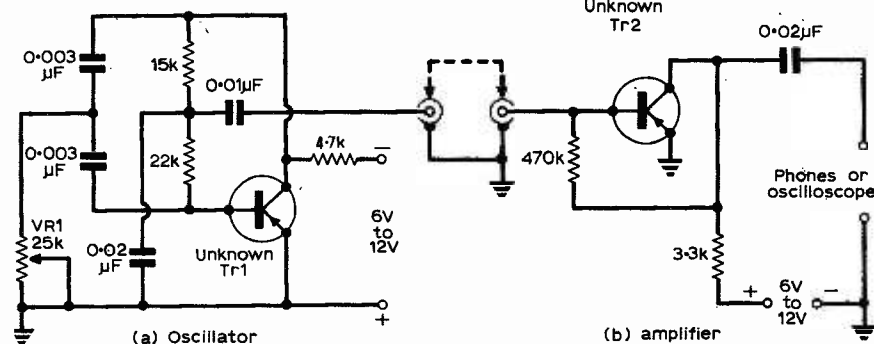


Fig. 4: The circuit used for the gain and amplification tests. Note that for NPN devices the battery polarity must be reversed.

Draw a base diagram of the base of the transistor and mark them 'A', 'B', 'C'; you are now faced with three permutations, of pairs 'AB', 'AC' 'BC'. Now take any pair and connect to the ohmmeter on low ohms range, then connect the other lead to each lead in turn: if the resistance falls the unpaired lead is the base lead and the lead to which the base was shorted is the collector. Check to see if this lead is connected to the metal can, this could confirm that it is the collector. If you do not get these results then check each of the three pairs using the same procedure. If the base cannot be identified for certain and there is high resistance both ways it is most probable that the third lead is base. To check, assume this is base and check with the meter whether it is a PNP or NPN in Fig. 1. You should then have established the base connection; the emitter and collector connections will be identified by reversing the leads in the grading test.

#### TESTING FOR GAIN

To test for gain two simple circuits are required as shown in Fig. 4. Good quality transistor sockets are essential since we are most likely dealing with short leaved transistors and soldering in and out will become tedious. The assembly of the the circuits is an individual choice, though the author used 'S-Dec' and found it ideal. When the test rig is assembled, put in two good known transistors, say an OC44 or OC45 for Tr1 and an OC70 or OC72 for Tr2, connect up the battery and headphones. If you can use a

'scope, all the better. Now adjust VR1 until a tone (or trace) is observed, then start to substitute the unknowns for Tr1. If a tone is present the gain will be more than 30, if no oscillation occurs then it is less than 30. At this point those transistors which have connections which are difficult to identify can be checked and identified by insertion, keeping the assumed base connection and reversing the other two unknown leads in the socket. If no oscillation occurs, keep it for the two further tests. Do not be afraid to reverse leads even at this higher voltage; if it blows then it was probably useless anyway.

#### AMPLIFICATION TEST

Now replace the original test transistor i.e. the OC44/45 (or one of the good ones known to oscillate) and then one by one test all those which failed the high gain test by substitution in the Tr2 position. The note heard in the headphones will tell you if it will amplify at all. If it is possible to use an oscilloscope, a little more information will be gained on this last test which is for low gain. By means of the trace shown on the 'scope, you can classify some transistors in the large signal class because the waveform will be distorted or clipped. The assumption in the tests up to now has been that the surplus transistors are in the small signal group.

#### R.F. TESTS

All the transistors available should be put through the r.f. test, irrespective of whether they have passed the previous tests. The r.f. test circuit is shown in Fig. 5. Here the reader will have to arrange for the crystal, Tr1, L1 and C1, according to what he has available, to check frequency. As a guide, with a 20MHz overtone crystal, an OC170, L1 being eight turns of 18s.w.g. on a 1/2in former, tuned with a 50pF capacitor. the circuit will cover the range up to

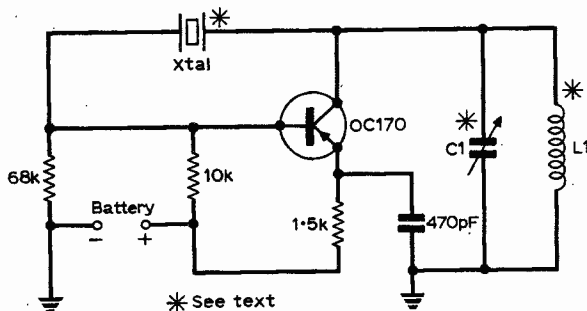


Fig. 5: The r.f. test circuit. For NPN devices the battery polarity must be reversed.

30MHz. Here a receiver or G.D.O. is necessary to detect the oscillation. Once oscillation is established it is merely a matter of substituting as before.

With your collection graded, as outlined, it is simply a matter of substitution of various types within that grade for optimum results in a particular project. The methods described are by no means comprehensive but at least you will have got a little order out of chaos and the building of many projects will be made much easier.

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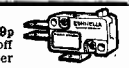
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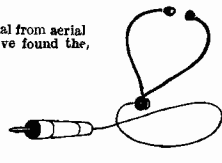
Designed to operate transistor sets and amplifiers. Adjustable output 8v., 9v., 12 volts for up to 500mA (class B working). Takes the place of any of the following batteries: P1, P3, P4, P6, P7, P9 and others. Kit comprises: mains transformer rectifier, smoothing and load resistor, condensers and instructions. Real snip at only 89p, plus 18p postage.

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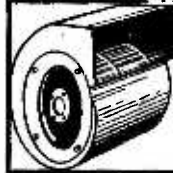
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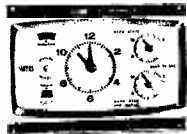
**DISTRIBUTION PANELS**

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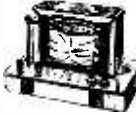
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# GENERAL PURPOSE

# power supply

M. WALLIS

**I**N the "good old days" of valves, power supplies were simple. Some 90 per cent of equipment operated with an h.t. supply of about 300V and the heaters were nearly all 6.3V. A single power supply would operate the vast majority of equipment that one was experimenting with. Today the semiconductor rules the day and power supplies are very much less standardised. Checking through a recent copy of *Practical Wireless* showed that there were six circuits given—and five different supply voltages were specified, ranging from 6V to 30V. Batteries can cope with a number of these, especially the most common 9V supply, but even the most half-hearted experimenter needs quite a range of batteries to pursue his hobby—even for quick lash-ups.

One can of course build a sophisticated, stabilised power supply with variable output covering quite a large range but such circuits are expensive, are by no means simple in their construction and most of the time the sophistication is not required.

By incorporating a simple two-pole, six-way rotary switch into the circuit of a standard power supply, it is possible to build a power unit with six different outputs—all with low internal impedance—and which will simulate exactly the supply that you finally build into the equipment.

A few refinements can be incorporated into such a power supply such as an indicator neon and fuse protected output which are not always necessary on the final supply which is fitted permanently but which make life simpler (and cheaper!) while experimenting.

## the circuit

The wide proliferation of supply voltages needed for semiconductor designs has brought about the introduction of mains transformers with a wide range of secondary windings and it is simply by selecting the appropriate ones of these that various output voltages can be obtained.

The transformer specified in the components list is a good one to use but other types with multiple secondaries can be adopted.

This one is fitted with 12, 15, 20, 24 and 30V windings (these of course refer to a.c. r.m.s. volts)

TABLE 1

VOLTS (d.c.)	VOLTS (a.c.)	Connections from which derived
4.5	3	12-15
6	4	20-24
7.5	5	15-20
9	6	24-30
12	8	12-20
13.5	9	15-24
15	10	20-30
18	12	0-12 or 12-24
22.5	15	0-15 or 15-30
27	18	12-30
30	20	0-20
37.5	24	0-24
45	30	0-30

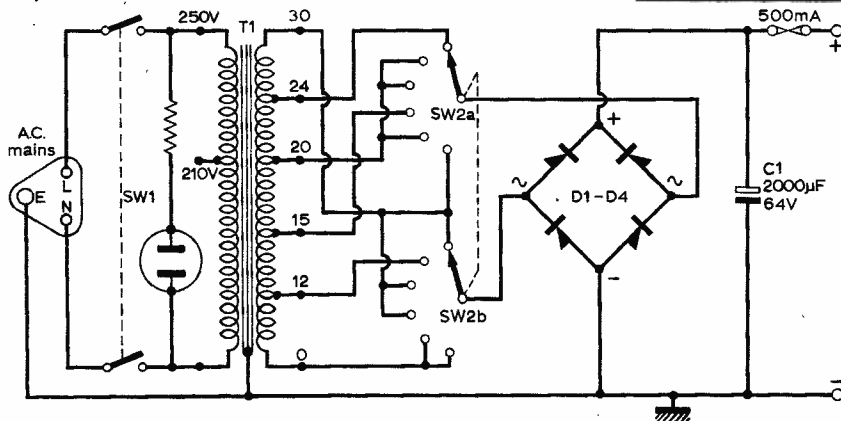


Fig. 1: The circuit of the general purpose power supply.

and a total of 13 different voltages can be selected from this as shown in the table. Those shown in the drawings, and for which the wiring is done, tend to be the higher voltages as batteries are still the best bet up to about 9V but it is a matter of personal choice which are selected.

Note that the d.c. voltages are those which should be read with no loading and are only approximate. In any case it has been found by

## ★ components list

T1	Mains transformer, 250V primary, 500V multiple secondary, or 250V/500V Douglas Type MT12AT or similar.
D1-D4	Silicon Bridge Rectifier, BY164 or similar.
C1	2000µF 64V
SW1	Double pole on-off switch.
SW2	2-pole, 6-way rotary switch.
	Panel neon with built-in resistor.
	Robert Electronics Fuse.
	Plastic encapsulated terminals.
	Tap wire for switch.
	Capacitor clamp.
	Aluminium chassis, 6" x 4" x 1/2", K. L. Smith, Ltd., 287 Edgware Rd., London W2.

experience that the secondary taps are by no means always accurate and quite large differences have been measured from the theoretical voltage but as exact voltages are rarely needed, variations are allowable.

The output voltage from the prototype, which can be seen marked on the chassis, are those measured, not those calculated, and these discrepancies can only be due to winding inaccuracies as it is wired up exactly as in Fig. 1.

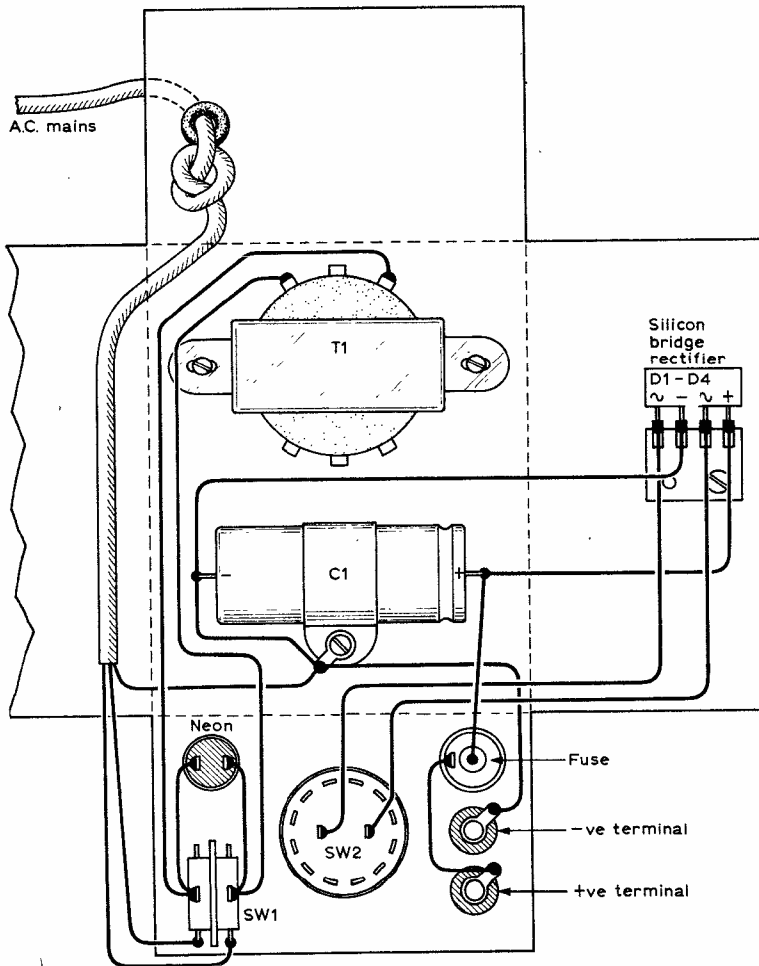


Fig. 2: The component layout and wiring details.

The current rating required from a general purpose power supply will depend on the uses to which it is put. Only power amplifiers at peaks take more than about 500mA and that was the rating chosen; it is sufficient for nearly all experimental work.

More than one company makes transformers with the voltage taps used here, but the most widely available is possibly the Douglas MT12AT. The same transformer with a 2A rating is coded MT3AT and although it will just fit into the chassis shown, it is a tight fit and a larger one is recommended.

The mains supply is connected to the correct primary (either 210V or 250V) of the transformer via a double-pole switch. A panel neon, connected

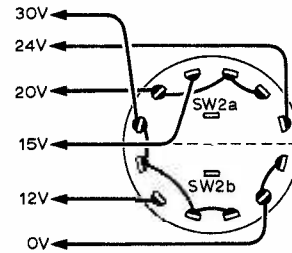


Fig. 3: The switch wiring used on the prototype.

across the primary is very useful. Today most neons are supplied with a built-in resistor but if one is not fitted, a 220kΩ should be wired in series as shown in the circuit.

The earth line is shown connected to the negative line but may equally well go the positive if used in conjunction with PNP type equipment which is earthed by some other means. Whatever happens the aluminium chassis should be earthed for safety reasons.

The various connections to the voltage selector switch are taken from the appropriate tapings and the switch wipers are connected directly to the bridge rectifier a.c. contacts. Plastic encapsulated silicon bridge rectifiers are widely available at reasonable prices and come under a variety of codings. The ratings must be 50V peak, 1A. The Mullard BY164 is suitable here.

Adequate smoothing for all purposes is provided by the 2000µF capacitor; the voltage rating of this should be well above the 45V or so applied and a 64V type was used in the prototype.

To provide a measure of protection, a 500mA fuse should be connected in the supply as shown.

## construction

The prototype was built in a

small aluminium chassis size  $5 \times 4 \times 2\frac{1}{2}$  inches, fitted with a drop-in lid. These chassis are available from H. L. Smith Ltd., the address is given in the components list.

The layout of the components is shown in Fig. 2 and can be seen in the photograph.

The bridge rectifier can be mounted on a small lag strip on one long side. the transformer and the

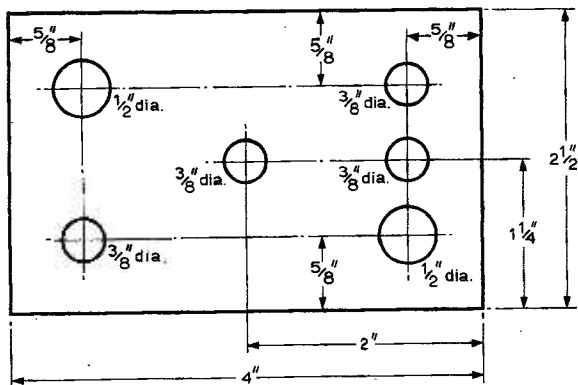
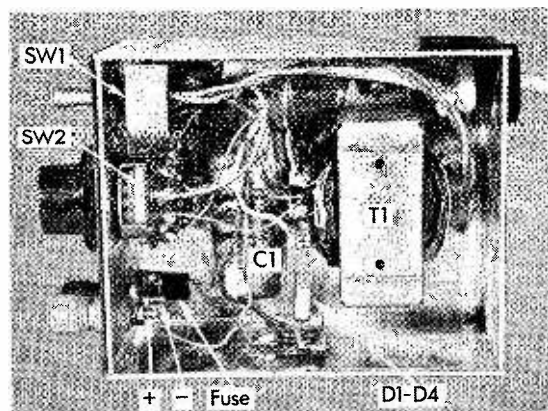


Fig. 4: The front panel drilling details.

capacitor on the base, with the remaining components on the front panel.

The switch wiring needs quite a lot of planning unless that used in the prototype is copied exactly, this is shown in Fig. 3. If other voltages, selected from the table, are required, the wiring should be planned carefully first of all. It is far easier to do the wiring on the switch leaving a few inches of wire which will finally be wired to the transformer.

When all wiring is completed a thorough check should be made to see that there is no possibility of



Internal view of the prototype showing component siting. Compare this with Fig. 2.

mains being applied to the case and that no bare wires can touch each other.

Connect a voltmeter to the terminal sockets and switch on, ensuring that a voltage reading is obtained in each switch position. Wrong wiring on a switch of this sort can lead to a direct short of the secondary and—unless noted very quickly—unpleasant things can happen to both the transformer and the switch.

There may be a very small amount of sparking while switching but this does no harm. The prototype has been in use continuously for several months with no ill effects.

There is just one point that must be made. The charge stored in a smoothing capacitor of this size lasts for a long while and if the power supply has been on a high range the capacitor should be shorted out (with the mains switch off) before being applied to a circuit where a high voltage could cause damage. This should be done through a resistor, not directly, as the fuse may blow otherwise.

If, due to the nature of the experimenting, a considerable amount of switching is envisaged, a resistor can be wired permanently between the output terminals so that a small current is drawn at all times and the capacitor will then settle down very quickly to the applied voltage. A  $4.7k\Omega$  resistor with a  $\frac{1}{2}W$  rating will serve this purpose.

## CROSSWORD No.2 WINNERS and SOLUTION

The Practical Wireless Crossword Competition No. 2, published in the June 1971 issue, has now closed and the prizes of £10 vouchers, exchangeable with any advertiser in Practical Wireless have been awarded to:

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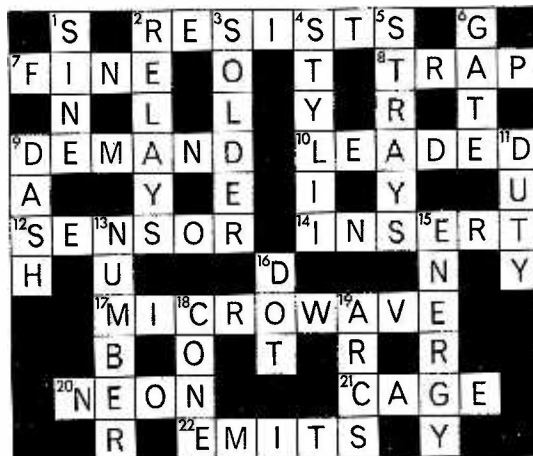
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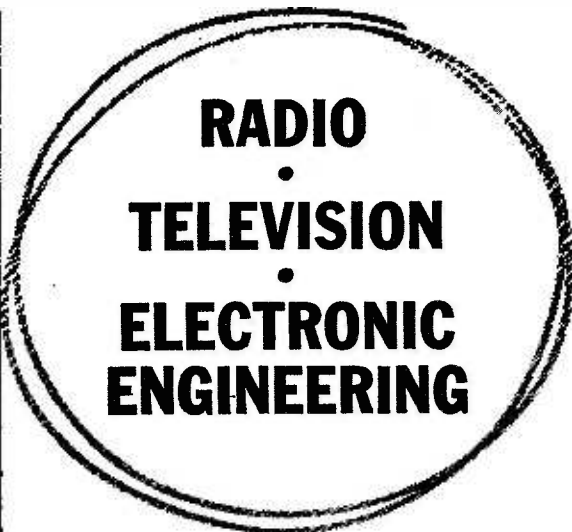
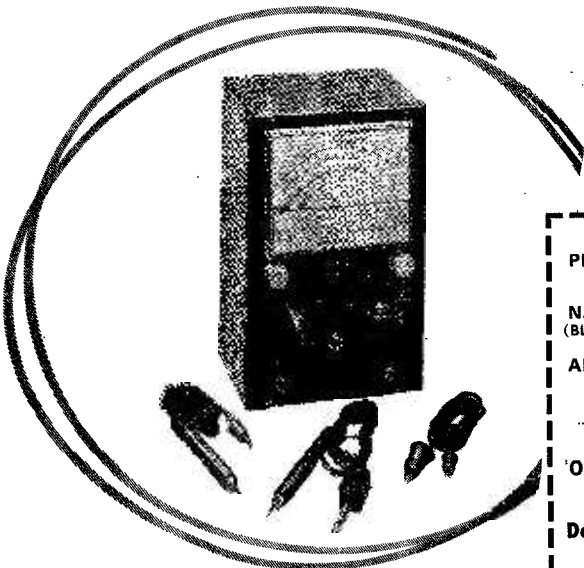
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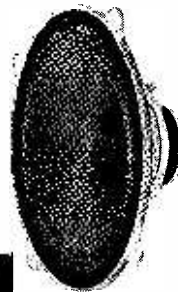
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PRACTICAL WIRELESS  
SUPPLEMENT  
OCTOBER 1971



Choosing

## SMALL WORKSHOP TOOLS S. YEATMAN

**S**INCE YOU ARE reading Practical Wireless the chances are that you have already tried your hand at constructing one of our projects. If you are already well fitted out with tools or have access to workshop facilities the bending up of a piece of aluminium to make a chassis or the punching and drilling of various holes would not have presented you with much of a problem. But if you are a newcomer to home electronics you have probably employed 'knife and fork' techniques, utilising kitchen knives and similar tools!

This really is doing things the hard way and the effort involved can put a considerable damper on anyone's enthusiasm for home construction, apart from any ensuing domestic problems when the lady of the kitchen discovers that her best kitchen knife now looks like a hacksaw blade!

If you are really taken with the idea of constructing electronic gear then be prepared to start off properly by buying a few good essential tools designed for the job in hand. Forget Dad's woodworking screwdriver with its  $\frac{1}{2}$ " wide blade filed so thin that it seems to fit any screw head from 8BA upwards! Very convenient, of course, but what a mess it makes of screw heads! Dad's pliers, too, are very handy—they 'fit' any size of nut you like to mention but by the time they have slipped a couple of times that nut looks pretty sorry for itself.

When you find out what fun these electronic projects can be you will begin to take pride in the finished job and Mum's knives and Dad's tools just won't be good enough. So, start off on the right foot by getting the proper tools and remember that, like most 'bargains', cheap tools can turn out to be expensive in the long run. Spend a little more on tools from manufacturers of repute and scorn imported tools made of inferior materials.

The following review lists small workshop tools more or less in the order of necessity bearing in mind the requirements of the home constructor. The soldering iron takes precedence since even the simplest bought kit of parts needs the odd soldered joint or two.

In a review of this kind only general reference can be made to the great variety and range of tools that are available today. Specific recommendations are impossible without some knowledge of the amount of money it is intended to spend and the precise nature of the work to be undertaken in the workshop.

Workshops tend to 'just grow' from a few simple tools. As the limitations of these tools become apparent so more tools are bought to fill the gaps, thus it can be seen that a large initial outlay is not necessary.

Spreading the cost over a period allows emphasis to be made here on the requirement to buy quality, a policy which, if followed, will not be regretted.



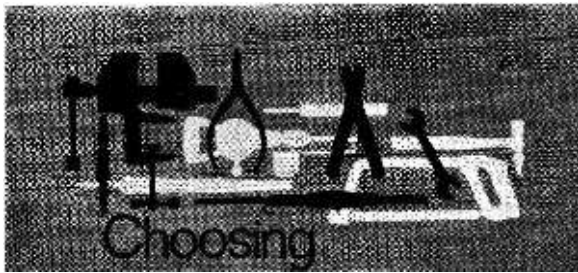
**SOLDERING IRONS.** There is a wide variety of electric soldering irons available today, the main problem being the selection of one of a suitable wattage for the home constructor of radio gear. For the average Practical Wireless project a 25 watt iron should prove satisfactory but if a lot of work is likely to be done on printed circuit boards a 15 watt iron would be more appropriate. These circuit boards often contain many small components fitted quite close together and thus vulnerable to the heat of a soldering iron. Excessive heat can also damage the copper strips of the board itself.

With these irons goes a wide range of copper bits of differing diameters, some straight and some angled. Initially a straight bit  $\frac{1}{8}$ " or  $\frac{3}{16}$ " in diameter can be chosen for general purpose work with an angled bit for the awkward spots. At a little extra cost special bits are available which contain additives to the copper designed to prolong the life of the bit.

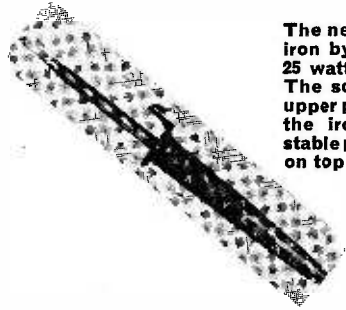
For home use a soldering iron operating directly from the 230 volt mains supply is usual but, for anyone who might feel a little happier with a lower working voltage, irons are available to work from as low as 6 volts via a mains isolating transformer.

When wiring an electric iron to its mains plug ensure that the instructions supplied with the iron are strictly adhered to so that the iron is properly earthed. This is a very important point for the builder of electronic equipment when wiring in transistors and other solid-state devices. Irreparable damage can be caused to these devices by stray earth currents if the soldering iron is not properly earthed.

Advancing rapidly in popularity are the soldering guns or 'heat guns', as they are sometimes known. The copper bit is, in fact, part of a low voltage secondary winding of the built-in transformer. Exaggerated claims are sometimes made concerning the short heat-up time for these guns,



## Choosing SMALL WORKSHOP TOOLS

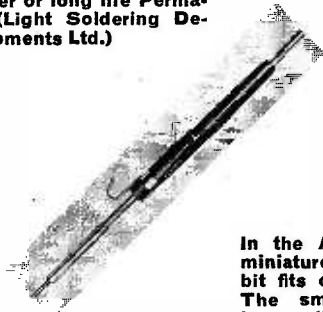


The new Invader soldering iron by Adcola is rated at 25 watts and has a  $\frac{1}{16}$ " bit. The square styling of the upper part of handle causes the iron to remain in a stable position when placed on top of the workbench.

One of the Litesold range of irons available in ratings from 10 to 60 watts, covering all requirements in



electronic soldering. Various tips are obtainable in copper or long life Perma-tip. (Light Soldering Developments Ltd.)



In the Adamin series of miniature irons the copper bit fits over the element. The smallest, Model 6, has a rating of only 6 watts at 6 volts. (L.S.D. Ltd.)



This soldering iron bench stand guards against accidental burns or even fires. The iron maintains its normal operating temperature while in the stand. A bit cleaning pad is fixed to the front of the stand. (L.S.D. Ltd.)

typically 10 seconds, but the better known makes can be relied upon in this respect.

The trigger style on-off switch on these guns often has two positions, for fast heat-up and for running heat, thus giving a dual-heat facility. Sometimes other types of bit are available which can be used to cut sheet plastics or to weld plastic sheet and so on.

Solder today, as used on electronic work, invariably has several cores of flux to ensure better distribution of the flux around the joint and consequently a better joint. The solder contains tin and lead in varying proportions which affect the temperature at which the solder will melt. The usual ratio of tin to lead is 60/40 for radio work and the diameter of the solder can be between 18 and 22 s.w.g. depending upon the fineness of the work being done.

While short lengths of solder can be bought for a few pence the  $\frac{1}{2}$  or 1lb. reel will be found to be more economical for the home constructor. If however he wishes to experiment with various solders he will find many easy-to-use dispensers and handy-packs available with different types of solder such as 40/60 or 60/40 tin-lead alloys as well as solders containing a small amount of copper which is calculated to reduce the amount of wear on the copper soldering bit.

Although soldering irons are usually fitted with a hook of some kind so that they can be hooked onto a convenient point it is a good policy to provide some kind of metal stand for use on top of the bench. Such a stand can be easily made out of an odd piece of aluminium or tinplate.

Soldering iron manufacturers naturally produce their own stands or 'protective shields' for their irons and these are designed to ensure that the iron does not overheat when the iron is not being used but is still switched on. For convenience a cleaning pad for the bit may be incorporated and possibly a holder for a reel of solder.

A 'must' in soldering is a sharp pick or long needle for clearing out holes in soldering tags and removing surplus solder. Commercial versions are usually made of aluminium, to prevent the solder sticking to the needle, and with a plastic handle or covering. One end may be pointed and the other end split to enable wires to be unravelled from tags etc., while the solder is molten.

Another de-soldering aid available is in the form of copper wire braid. When the end of the braid is touched on a hot soldered joint surplus solder travels up the braid by capillary action. The end of the braid is snipped off ready for the next joint.



**PLIERS AND CUTTERS.** Again a very large field of choice and again the rejoinder to pay a bit extra to get quality. Two pairs of pliers will suffice for most constructional work, a long-nosed pair with tapered jaws coming to a reasonable fine point and a heavier pair with stocky jaws, maybe  $\frac{1}{2}$ " wide, and probably incorporating a pair of sidecutters.

The long-nosed pliers will always be in the hand of the electronics constructor, for twisting wires round tags and forming the wire ends of components before soldering them into position. Don't forget that a wiring joint should always be mechanically sound before it is finally soldered, although the true experimenter will not go along with this principle because he will want to use the same components time and again!

Variations on the pliers theme include those with angled

jaws of various lengths, round jaws and flat narrow jaws rather than pointed ones. When buying pliers see that the opening and closing action is not too loose or the jaw tips will not close together properly and it will be difficult to get hold of fine wires when wiring up.

Wirecutters will be used as often as the pliers so, again, only the best must be chosen. They should be about the same size as the long-nosed pliers with the cutting edges at an angle to the body. Other types have the cutting edges across the top or parallel with the body.

When buying sidecutters hold them up to the light and see that the cutting edges come together cleanly and evenly throughout their length. Try this test with a cheap imported pair of cutters and see the difference! The previous remarks concerning the action of pliers applies just as much to sidecutters. A loose action and the cutting action will be greatly impaired. On the other hand, there is nothing more annoying than a pair of cutters or pliers that need two hands to open them!

**WIRESTRIPPERS.** Different people have different ways of stripping the insulation from wire, varying from the use of the front teeth to an old kitchen knife! If the wire is nicked, and it often is, it will eventually break if it is subject to vibration or flexing. The ordinary sidecutters are frequently pressed into service as wirestrippers mainly because they will have just been used to cut off a piece of wire and are still in the hand! However there are plenty of wirestrippers on the market designed for the job so there is no excuse for improvisation.

Wirestrippers usually have some means of adjustment to cater for different size wires. It is important not to try to strip wires of a larger gauge than that for which the wirestripper has been set, or the wire will be nicked. One of the latest style wirestrippers on the market has a four position cam that can be adjusted immediately to another gauge of wire, while still held in the hand. Incidentally, this model also has wire cutters which have ground edges, a great improvement.

A feature on some types of wirestrippers, which the author considers of great importance, is the provision of a spring that keeps the cutters normally open, the cutting action taking place against the spring.

**SCREWDRIVERS.** Strictly speaking, every different sized screw needs its own screwdriver, if the blade is to fit the screw slot properly, but not many of us are likely to go to that extreme. The width of the blade should be about the diameter of the screw head or wider, rather than narrower. For electronic construction work it is best to buy a set of screwdrivers with blade widths from about  $\frac{1}{8}$ " up to  $\frac{1}{4}$ " or  $\frac{5}{16}$ ". Three screwdrivers should be sufficient. A useful addition is one for the Philips style screws, that is the screws with crossed slots.

Screwdriver sets are available consisting of several blades that can be fitted to a common handle. Although these may be cheaper than individual screwdrivers they are less convenient in practice.

The screwdriver blade itself should be about 6" or so long depending upon the blade width. One very useful size of blade is one about  $\frac{3}{8}$ " wide for use with knob setscrews. The blade should be as long as possible so as to reach a knob in spite of the clutter of other knobs, dials etc. on a panel.

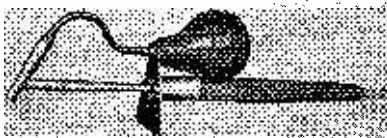
Don't take any notice of the markings on some screwdrivers that seem to indicate that one can use them with safety on 10000 volt circuits! Anyone having that sort of voltage around should know the precautions he should take. They would not include the use of a screwdriver on 10000 volts!

Variations on the basic screwdriver include the ratchet

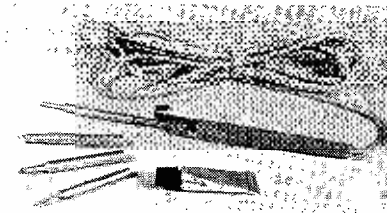
A most useful de-soldering aid is a reel of specially treated copper braid which will completely remove unwanted solder from a joint by capillary action.



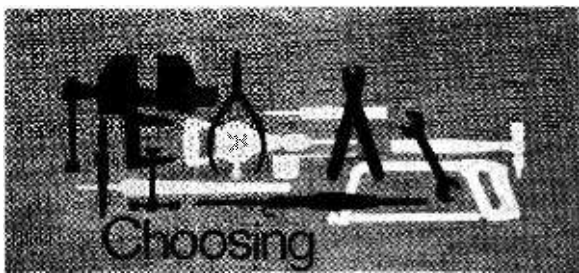
The Adcola protective shield is intended for wall or bench mounting and has slots for a spindle carrying a reel of solder.



This de-soldering tool (L.S.D. Ltd.) could be invaluable when stripping components from surplus equipment. It is self-contained and simple to operate and may be used as a conventional soldering iron.

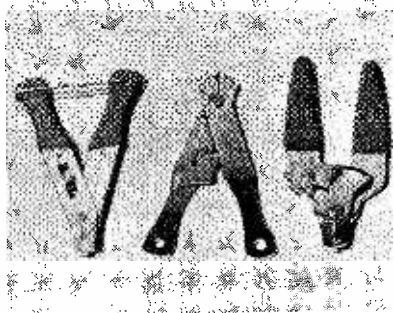


The Adamin miniature iron, Model 15, can be obtained complete with a set of four bits of differing size. The tube of special lubricant is used to prevent the bits from sticking to the heating element.

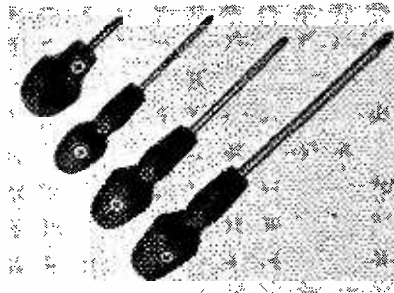


Choosing

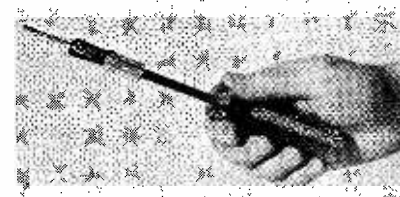
## SMALL WORKSHOP TOOLS



Three of the Bib range of wirecutter, strippers by Multicore Solders Ltd. The latest, centre, is the Model 3A with an instantly adjustable cam enabling the strippers to deal with most wire sizes. The cutters have ground cutting edges. The ends of the arms are, in fact, flat spanners for 4 and 6BA nuts, a most unusual feature.



A set of Stanley 'Pozi-drive' screwdrivers enabling Philips type screws to be reached in the most awkward corners.



The Stanley range of 'Spee-D-Grip' screwdrivers incorporating a spring clip which holds screws in position for starting in inaccessible places.

types which remove the necessity of continually lifting the screwdriver from a screwhead thus, incidentally, reducing the risk of the blade slipping and doing damage. Of course, if one used a screwdriver properly, the blade should never leave the slot, but this seldom happens!

A most valuable addition to a set of screwdrivers is one having a spring attachment at the tip of the blade to firmly hold a screw while it is being inserted into place. Its value in awkward spots is inestimable. Such an attachment can sometimes be bought separately for use on almost any screwdriver.

**SPANNERS.** There is always a temptation to use a pair of pliers on any nut that needs tightening, usually because the pliers are ready to hand. It should be remembered that the opposite faces of a nut are parallel to each other where-as the jaws of a pair of pliers are only parallel when they are closed. That's why the pliers always slip off the nut and cause damage.

First of all, get a set of box spanners covering 0 to 8BA either single or double ended. The single ended ones with a wooden or plastic handle are recommended. Just two, for 4 and 6BA, are worth their weight in gold in a workshop. Having long stems they are invaluable for placing nuts into odd corners where fingers or pliers cannot reach.

It is always good practice, wherever possible, to tighten a nut on to a screw rather than use a screwdriver on the screwhead. This is particularly important where the screwhead is visible such as on the front panel of a piece of equipment where a damaged slot on a screw would be an eyesore.

Another requirement in the spanner line is a set of flat spanners, again covering the BA sizes, possibly 0 to 8BA. These can very well be double ended ones since the length of the spanners is not of much importance.

Some sets are single ended but bolted together at one end so that one can be selected and the others swung out of the way, rather like a set of feeler gauges.



**DRILLS.** In the past a hand drill would have been a first acquisition in a workshop, followed by an electric drill when the money was available. Today the cost of electric drills is such as to justify buying one from the outset.

The simple electric drill will have a single speed and accommodate drills up to  $\frac{1}{4}$ " in diameter, ('twist drill' is really the proper name for the bit that does the cutting). This model will perform just about all the routine drilling jobs in a workshop where electronic projects predominate. A chuck adaptor to take drills up to  $\frac{3}{8}$ " in diameter is highly desirable, enabling the usual holes for mounting potentiometers etc. to be drilled without having to resort to files or reamers.

If the drill is likely to be used for other duties around the house then the two speed drill with a chuck taking drills up to  $\frac{1}{2}$ " in diameter can be considered. A popular accessory for the electric drill is the speed controller which is an electronic device enabling the speed to be varied continuously from a few r.p.m. to maximum speed. Such controllers are available in kit form or ready assembled.

If a lot of drilling is anticipated, particularly on chassis work, a drill stand will prove a boon. Most electric drill manufacturers have such stands but their design is such that they will accommodate most makes of drill. Such

stands ensure that holes are drilled vertically, which may not be very important on sheet metal work but could be critical with a deep hole. Holes will be more accurate both in size and positioning when drilled on a stand rather than with a hand held electric drill.

When using drill adaptors enabling, say, a  $\frac{3}{8}$ " drill to be used in a chuck of nominal  $\frac{1}{4}$ " capacity, remember not to overload the motor by exerting excessive pressure on the drill especially in hard materials.

Hand operated drills suitable for the small workshop range from the simplest single speed ones with a  $\frac{1}{4}$ " capacity to those taking drills up to  $\frac{1}{2}$ " and having an integral gearbox providing either a low speed or a high speed at the chuck. A little extra spent on a good hand drill will be a worthwhile investment. In particular the gears will run more smoothly and require less energy and the chuck will be of a better quality.

Now, what about the twist drills themselves? These are bought singly, as required, or, if starting more or less from scratch, then in a set complete with a stand for use on top of the bench. They may be had in sizes from about  $\frac{1}{32}$ " to  $\frac{1}{4}$ " in diameter or in a numbered range from No. 80 (0-0135") to No. 1 (0-228"). Letter drills carry the range on upwards from 'A' (0-234") to 'Z' (0-413").

For many years the author has had just four drills always to hand, No's 12, 24, 32 and 43. These will cover the drilling of holes for tapping or clearing for 2, 4 and 6BA screws.

As far as the quality of twist drills is concerned, it is necessary to take a little more care over their selection than with other tools since there are a lot of drills on the market that seem to be made of little more than soft iron! So once again beware of cheap imitations and if the pocket will stand it, buy a small set of genuine high speed drills. These will last for ever and seldom need sharpening if not abused.

**PUNCHES.** Whenever it is required to drill a hole in a chassis, or anywhere else for that matter, it is essential to use a centre punch to mark the spot where the hole is required. Otherwise it is almost certain that the drill will wander off the spot, scratching or damaging the surface being drilled. This particularly applies to hard surfaces and when using a hand held electric drill especially if care is not taken to keep the drill vertical.

There's not much to say about centre punches. A good one will be of tempered steel with a sharp round point, usually machine ground. Spring loaded punches are available which obviate the need for a hammer, so these punches are very convenient and the extra cost well justified.

Chassis punches are a necessity although the number bought for a small workshop will probably depend upon the funds available. These punches will cut holes ranging from  $\frac{3}{8}$ " to 3" in diameter but it is recommended that at least two be obtained,  $\frac{3}{8}$ " diameter for B7G valveholders and  $\frac{1}{2}$ " diameter for B9A valveholders. These punches require a suitable Allen key to operate them and their cutting limit is about 16 s.w.g. mild steel. They will cut through the usual 16 s.w.g. aluminium sheet like the proverbial knife through butter, thus saving a great deal of time and energy.

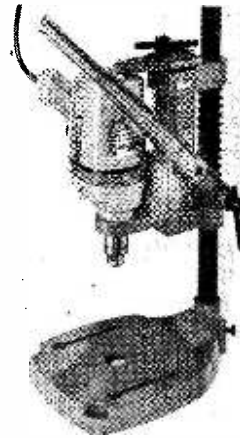
A useful tip . . . the resulting hole will have a burr on one side so place the cutting part of the punch on the side of the panel or chassis that might be of some importance from the point of view of appearance.

Other chassis cutters are available that will cut square or rectangular shaped holes but the infrequent need for such cutters does not justify their purchase.

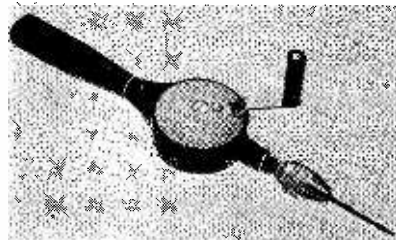
The predecessor of the chassis cutter was the tank cutter. This had an adjustable cutting bar for different diameters of hole, but unless used in a lathe or drill press,



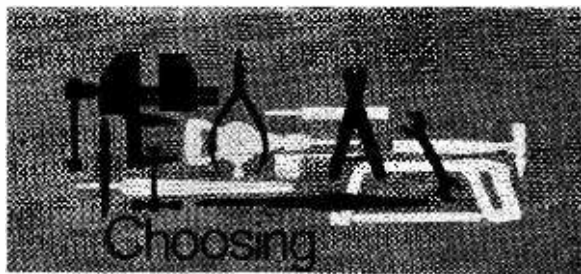
This bench clamp enables a portable electric drill to be used with grinding, polishing or other attachments (Wolf). The drill is a Wolf Sapphire 73.



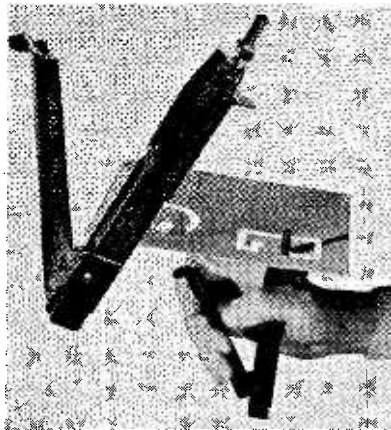
For precision drilling a bench drill stand is essential. The spring loaded press magnifies the hand pressure some ten times. (Wolf)



The old-fashioned hand drill now has a streamlined appearance. In this Stanley drill the gears are completely enclosed protecting them from dirt, swarf etc. and obviating nipped fingers!



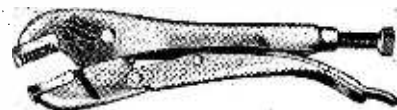
## Choosing SMALL WORKSHOP TOOLS



Requiring only a  $\frac{1}{8}$ " hole to begin operations this Adel nibbling tool will cut a hole of any shape or size in sheet steel up to 18 gauge steel or aluminium up to 16 gauge. (West Hyde Developments Ltd.) The punch and die action cuts without distorting the metal.



This precision made Mole 'Supercut' tool has a powerful action capable of cutting long straight lengths, curves or angles in sheet materials such as steel, aluminium, plastic laminates etc. A replacement blade can be fitted very easily.



The standard Mole wrench has many uses in the small workshop. In spite of its immense gripping power it can be opened at a touch on the release lever.

the resulting hole could be a little rough in appearance. A slow cutting speed was essential and for this a carpenter's brace was ideal.

Other hand tools for cutting holes in sheet metal include the family of 'nibblers'. A small hole is first drilled in the sheet metal, the nibbler inserted and the action of the tool nibbles the material away to form a hole of almost any shape desired. The hole can be finished off with the usual files.

Shears, or tinsnips, will be needed for cutting sheet metal and a 10" pair with straight jaws should suffice for general work. The will make a straight cut in sheet metal for a limited distance although the 'goosebill' type will usually prove better for this work.

**TAPS.** Now and again the necessity will arise to tap a thread in a hole and for this two taps for each size thread are required, together with a tap wrench. The first tap is tapered, to start the thread, and the second tap is full size. Sometimes a third tap of intermediate taper is used but this is not really required for small threads.

The tap sizes most likely to be required are the usual 2, 4 and 6BA. Taps can be broken off relatively easily and for this reason a proper tap wrench is strongly recommended.

The simplest and probably the best tap wrench is the bar type with a screw grip on to the tap. The chuck model is more expensive but it does enable the tap to reach positions that would be inaccessible with the bar type wrench.



**FILES.** For finishing off the edges of metalwork and suchlike a 10" flat file will be quite adequate. That known as 'second cut' will prove best being neither too coarse nor too fine for work on soft metals. A similar sized half round file is very useful for finishing off large holes such as those required for meters. While smaller holes, for valveholders etc., can be cut with chassis punches the cost of similar punches for large meter holes tends to be prohibitive, especially as they are used relatively infrequently. Such large holes can be made by drilling a circle of small holes, then knocking out the disc of metal and finishing the work with a half round file.

A  $\frac{1}{4}$ " round file completes the essential complement of files. This will find most use in enlarging small holes in the absence of a reamer or for 'drifting' holes that are not quite where they ought to be! Perhaps the spot was not properly spotted with a centre punch before drilling!

With the advent into common use of slide switches on electronic equipment the need has arisen for a couple of small needle files, one round and the other square, for finishing off the rectangular holes required in panels for these switches. If a set of needle files can be managed then so much the better as these sets contain files of circular, triangular and flat sections as well as those already recommended.

When buying files get suitable wooden handles for them at the same time. Don't try to use a file without a handle or there will be a grave risk of the tang of the file entering the wrist if the file should jam or stick in the work.

**HAMMERS.** As far as hammers are concerned the small workshop should have one with a plastic or rubber head for bending sheet metal, without causing undue marking of the metal. A second hammer should be a light



one of the 'ball-pein' variety for general work around the place. A good make is advisable to ensure that the hammer-head is properly attached to the shaft as a hammerhead in orbit around the workshop is not funny!

**REAMERS.** During the construction of a piece of electronic equipment one always seems to need to drill a hole that is between the sizes of the drills available. In such a case a tapered reamer can be invaluable, as an alternative to filing out the hole with a round file, a process that does not endear one to one's family, if they are within earshot!

A pair of reamers can deal with holes between  $\frac{1}{8}$ " and 1" in diameter producing a clean circular hole with little or no burr. They are usually intended for use in a hand brace but can on occasion be held in the hand.

**VICES.** If a bench or table is permanently available for constructional work then a vice of some sort will prove to be a great boon especially when fabricating metal work. While smaller sizes are obtainable, an engineer's vice with 4" wide jaws should be the smallest size to be considered. Such a vice is extremely rugged and will take a lot of punishment, including using it as an anvil!

Since the vice jaws are made of hardened steel, and serrated at that, it is essential to make up a pair of soft jaws to protect work held in the vice. These jaws can be made from pieces of aluminium or other soft metal. Other vices have clip-on jaws which are plain, serrated or slotted to hold tubing or round material more securely. Another model of vice has a separate mounting plate that can be attached to almost any flat surface by means of a suction pad.

A carpenter's vice with 6" or 8" jaws is even better for sheet metal work since the jaws can be opened to a far greater extent than those of an engineer's vice. However the space needed to permanently mount a carpenter's vice, especially below and behind the vice, is considerably more than that needed for an engineer's vice. However, there are some portable vices on the market that seem to combine the best points of both types.

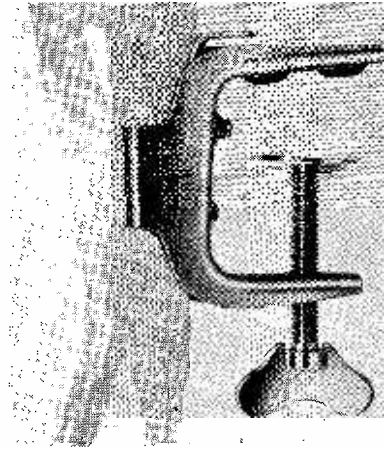
Although one may possess a bench vice there is always a need for a portable clamping or holding device and this is where the wrench comes in very handy.

The modern version of the wrench has an easily operated lever that allows the wrench to be locked on to the work and just as easily released. A clamp to hold the wrench is also available, which can be fitted to a table or bench top with a single clamping screw, thus providing a fixed vice if necessary. The jaw opening of the wrench can be adjusted over a wide range by a single screw fitting.

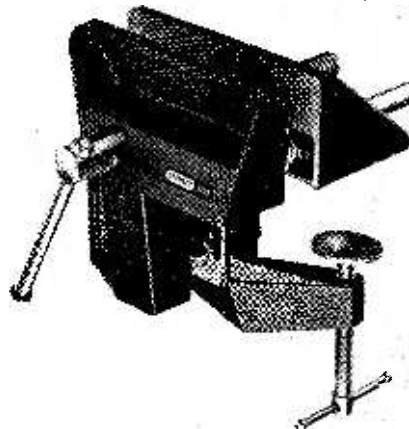
**RULES.** For marking out on sheet metal a rule and a square (trysquare) will be required, if an accurate job is to be done. A 12" rule is good enough and although it would seem that choosing such a simple tool would be no problem, the choice is, in fact, very wide indeed, ranging from rather inaccurate wooden rules, with printed graduations, to engraved steel ones.

Although a 6" square can be bought separately it really pays to buy a combination square since this incorporates a rule and square, usually of reasonable quality.

**HACKSAWS.** The hacksaw will come in for quite a bit of use in the small workshop, mainly for cutting sheet metal to size before forming into a chassis. Some of the cheaper hacksaw frames will be found to twist when the blade is tightened up, so a good quality frame will be a sound buy. The adjusting nuts, too, can be difficult to turn owing to poorly formed threads.



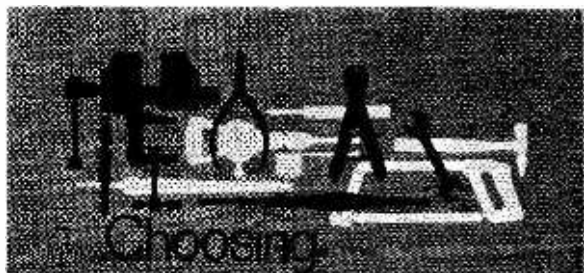
The versatility of the Mole wrench can be greatly increased by the use of this table or bench clamp, converting the wrench into a portable vice.



This Stanley aluminium portable vice has 5" jaws and can be clamped to any convenient surface. It is eminently suitable for bending sheet metal into chassis etc.



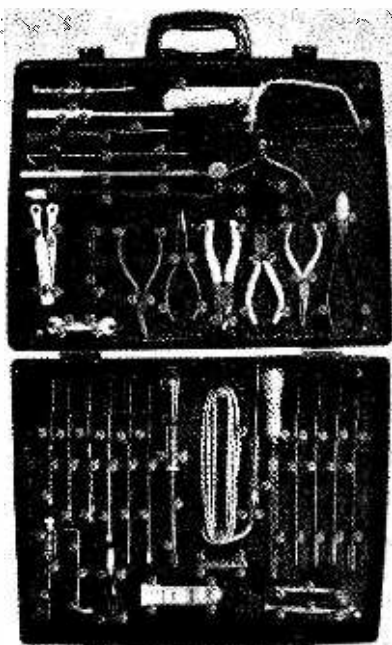
The Mini-Mole is just 5" long and very useful for getting into those tight corners, inaccessible to its 'big brother'. The curved jaws provide maximum contact with round or irregular shapes.



## SMALL WORKSHOP TOOLS



This set of Philips trimming tools and adaptors will cover every conceivable requirement when aligning electronic equipment. The compact packaging makes the set particularly useful to the service engineer. (Combined Electronic Services Ltd.)



If you don't feel like tramping around the tool shops to gather together your collection of small workshop tools then this very comprehensive tool kit may be the answer. It has a wide variety of spanners, screwdrivers, pliers, cutters, a soldering iron and solder, and even an angled mirror for viewing components tucked away in tight corners. (C.E.S Ltd.)

A frame to take 10" or 12" blades is big enough and the blades themselves can be of the low tungsten flexible type. These will deal with general cutting of mild steel, brass and aluminium etc. and absorb a lot of misuse without breaking. For maximum performance high speed flexible blades are to be preferred although they are a little more expensive.

For maximum efficiency the size of the teeth on the blade must be related to the material being cut. For soft metals, such as aluminium, a coarse blade is desirable to prevent the teeth from clogging, but on harder metals such as brass or on thin sheet metal a finer toothed blade is required. The number of teeth per inch of blade normally runs from 14 to 32 for hand held saws.

A very useful addition to the standard hacksaw is the 'junior' or bow-frame saw in which the blade is held under tension by the bow. The standard blade is 6" long with fine teeth. This saw is very handy for the smaller, finer jobs where the standard hacksaw would prove clumsy. In the electronic workshop the bow saw will be used a great deal for shortening the spindles of potentiometers, capacitors etc. Remember to hold the unwanted end of the spindle in the vice while cutting, rather than the component itself.

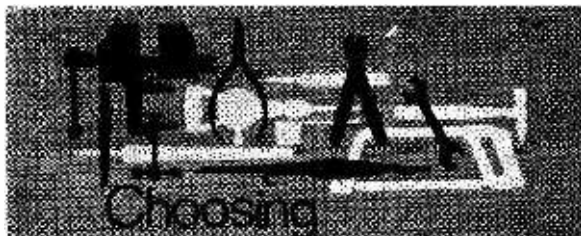
**TRIMMING TOOLS.** Although perhaps it is wandering into the realms of servicing it is not inappropriate in this review to mention trimming tools for electronic equipment. After all, having built a lovely radio set in our nice new workshop, it won't be of much use unless the tools to align it are to hand.

These trimming tools can be bought individually, as needed, but preferably they ought to be obtained as a kit. This will prevent the use of ordinary screwdrivers for adjusting iron cores which can only cause damage in the long run.

A kit may consist of one basic tool holder with several types of trimming tool that can be fitted into the holder or, in the more expensive kits, a complete trimmer for each purpose, such as adjusting iron cores, capacitors and special types of capacitors, such as the Philips pre-set beehive capacitors, which are met with quite frequently.

In conclusion it should be pointed out that for every basic tool mentioned in this review there are a dozen or more variations on the market. Like women, there are short ones, tall ones, thin ones and fat ones! Each one to his own fancy! The average D.I.Y. or tool shop is sated with gadgets that promise to relieve us of the tedium and work required to do a particular job. Few succeed, and those that do probably take twice as long to set up to do the job as one would take using basic tools alone.

It's surprising how often one resorts to basic methods and tools in the workshop. If funds are limited then put them to good use by buying only the best in tools from reliable manufacturers. If their names happen to be a household words they would not have reached those dizzy heights by selling rubbish.



## SMALL WORKSHOP TOOLS



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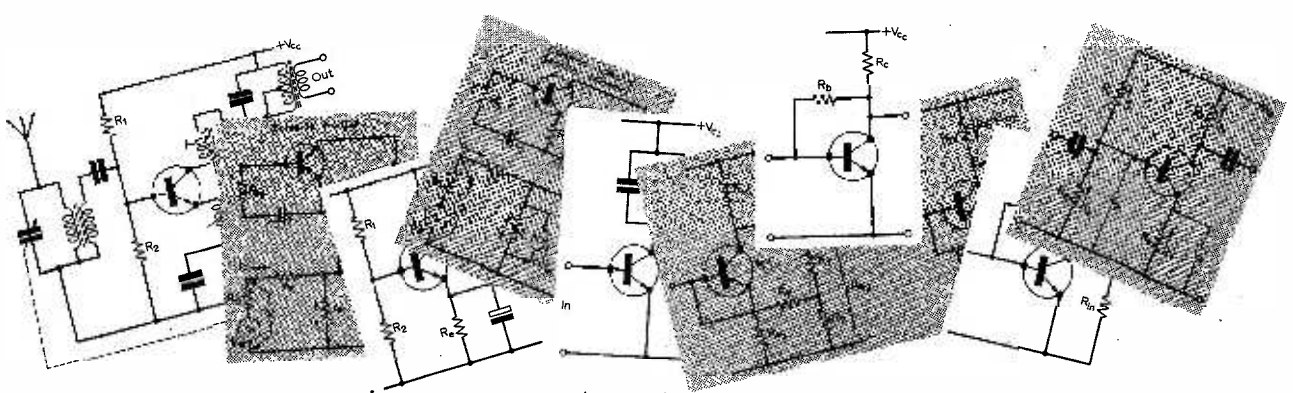
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# TRANSISTOR CIRCUITRY for beginners'

PART 1 H.W.HELLYER

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WHEN the idea for this series was first broached, everything seemed straightforward and simple. We would entitle the wallchart 'Building Bricks,' said the Editor, in an inspired moment, and the articles would take up each 'brick' and develop it so that newcomers to transistor circuitry could understand what was happening inside those inscrutable black boxes.

Which was all very fine—but it completely overlooked the fact that any beginner worth his salt is going to say 'But Why???'

No good my declaring '... an input signal to the base of Tr1 turns it on, which causes Tr2 to turn off and Tr3 and Tr4 to return to the stable mode, releasing Tr5, which now bottoms and allows ... etc.' It would sound like a paragraph from Henry!

To understand transistor action, it is imperative that we begin by understanding what makes the darned things tick. That means going back to pure physics, not too deeply, preferably without mathematics, and then progressing to the methods of construction and the reasons why there are essential parameters—rules of operation, if you like—and this is what we shall begin with.

## Semiconduction

As the name implies, the semiconductor is neither pure insulator nor electrical conductor, but something in between. Its resistivity lies roughly midway between that of conductors and insulators. This resistivity, moreover, decreases with increase of temperature (the resistance of a conductor increases slightly as the temperature is raised). This is one important difference between semiconductors and conductors.

Next, perhaps more important, is the way in which current flows in a semiconductor. There can be two processes; either a flow of negative electrons, as in the case of a conductor, or a flow in the opposite direction of positive 'holes'. The concept of hole flow is so vital to the understanding of transistor operation that we must begin with a simple discussion of atomic structure in order to get a grasp of it.

## Atomic Structure

An atom consists of a central nucleus containing positively charged protons with a number of negatively charged electrons orbiting around it. The negative charge carried by an electron is equal to, and exactly opposite to, the positive charge of a proton. In a neutral atom, the numbers of each are equal.

Different elements have atoms containing different numbers of electrons, orbiting at different distances from the nucleus. The electrons close to the nucleus are tightly bound to the nucleus, but those circling in the outer orbits are more loosely bound, and are easier to dislodge from the parent atom. The outer ring is called the **valence ring**, and the valence electrons are those with which we are mainly concerned in this work. The looser they are bound to the atom—in any material—the better a conductor a piece of that material will make. This is because loosely bound valence electrons are free to be attracted by a positive charge, such as a voltage applied across a conductor by means of a battery.

Electrons flow out of the conductor into the battery at the positive connection, but an equal number pass from the negative connection of the battery into the conductor at the negative terminal, keeping the overall total of electrons the same.

Conversely, an insulator is a material in which all electrons are tightly bound to the nucleus, so that a large amount of energy is needed to break any loose to make a current flow.

## Crystal Structure

The structure of a crystal of germanium or silicon is depicted in Fig. 1. It can be seen that there are four valence electrons in the outer ring and these are balanced in the nucleus by four positively charged protons, as indicated. In the three-dimensional structure that exists in reality, every atom is equi-distant from four other atoms and each valence electron forms a pair with one from an adjacent atom.

In two-dimensional form this can be shown as in Fig. 1, with pairs of electrons forming co-valent

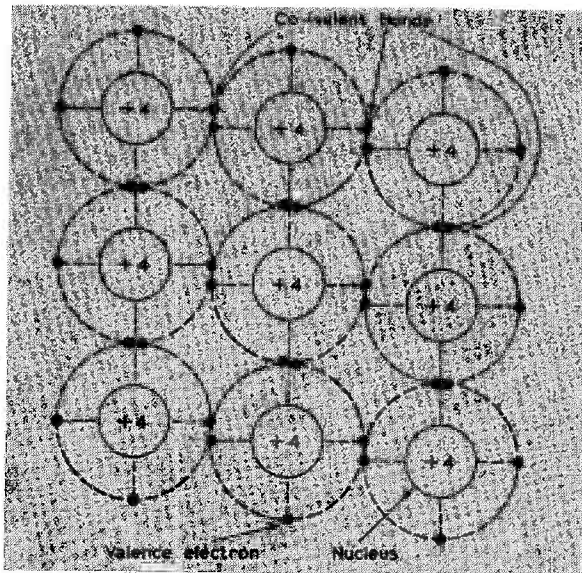


Fig. 1: Illustrating the structure of a germanium or silicon crystal.

bonds. This is a perfect crystal, with no impurities; and no electrons are dislodged from their atoms. This is, in fact, the basic structure of a perfect insulator, at absolute zero temperature, but as temperature increases, the energy of each atom is increased and some electrons can break away. If a voltage is applied, these free electrons are attracted to the positive pole and a current flow results. The space left in the crystal structure by a dislodged electron is termed a 'hole' and this represents a net positive charge.

We can therefore think of a movement of negative electrons toward the positive voltage terminal and a virtual movement of positive 'holes' (as successive electrons move to fill the vacant spaces) toward the negative pole.

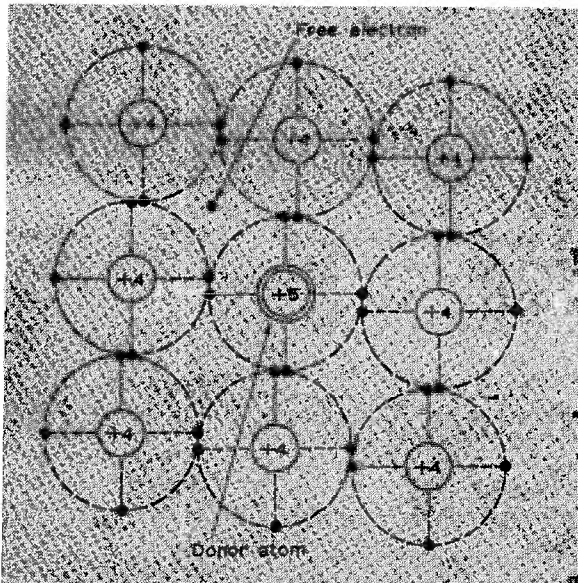


Fig. 2: Adding a 'donor' atom producing an excess free electron. N-type crystal.

## N- and P-Type Semiconductor

This is a simplified explanation, but suffices to show the principle of hole movement. In a pure semiconductor there must be one hole for each free electron. Such a pure semiconductor is termed an **intrinsic material**. However, if an element of impurity is added to the intrinsic material an imbalance is obtained. If, for example, a "donor atom" having five valence electrons is added to the crystal, as in Fig. 2, there is an excess free electron. Four of the donor atom's valence electrons form co-valent bonds, in the manner previously described, but the free atom cannot do so and orbits loosely.

Some materials with a valency of five are antimony, arsenic and phosphorus. These can be added to the germanium or silicon crystal in proportions of as little as one part in a hundred million and reduce the resistivity of the germanium from 70 ohms/cm to 1 ohm/cm. Because the donor atoms in such a material contribute free electrons, which carry a negative electric charge, a material "doped" in this

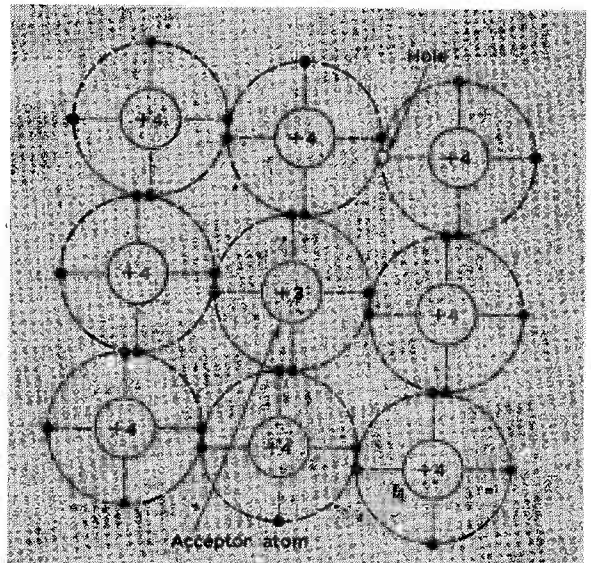


Fig. 3: In this case, an 'acceptor' atom creates a 'hole'. P-type crystal.

way is called an **n-type** semiconductor (i.e. it possesses an excess of negative current carriers).

The opposite process takes place if indium, borium or aluminium atoms are added to the basic semiconductor material, germanium or silicon. These materials have three valence electrons, and the addition of them creates holes in the semiconductor material, as shown in Fig. 3. The resultant semiconductor material has an excess of positively charged holes and is termed **p-type**.

## Minority Carriers

Minority carriers are another important factor of semiconductor physics. If a few electrons are injected into p-type material they are called minority carriers (the majority of current carriers in p-type material being, as we have seen, holes). Recombination takes place as the electrons move to fill the holes.

Similarly, holes injected into an n-type material

form minority carriers in this type of material, and small currents arise as recombination takes place. The time this takes to happen, termed the minority carrier lifetime, is an important property of a semiconductor material and the operation of most transistors depends on the movement of minority carriers.

## PN Junction

A single piece of p-type or n-type semiconductor material is purely resistive: reversing the applied voltage does not alter the current flow. But if p-type and n-type regions are formed in a piece of semiconductor material, with the regions adjoining each other, a rectifying device is formed: when voltage is applied in one direction, current flows, but in the other direction little or no current flows. Such an arrangement is termed a pn junction.

In Fig. 4, the region to the right of the centre line is n-type, possessing a certain density of free electrons. To the left of the line is a region of p-type material possessing a number of positively charged holes. When the junction is first formed, it becomes an area of activity for a short period as free electrons tend to cross into the p-type region and holes move over to the n-type region.

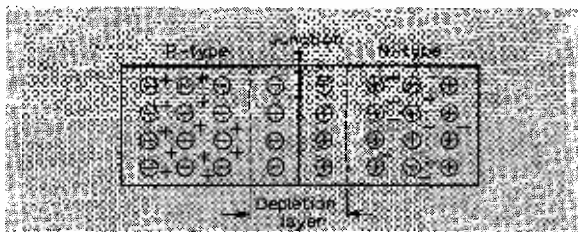


Fig. 4: Showing the charges existing in an unbiased PN junction.

This process of diffusion results in a potential building up across the junction, as the p-region gains a net negative charge with respect to the n region in the vicinity of the junction, and vice-versa, and this potential prevents further diffusion. This potential is termed the barrier potential and the region in the immediate vicinity of the junction, where there are very few free current carriers remaining after the initial diffusion, is termed the depletion layer or region, as shown in Fig. 4.

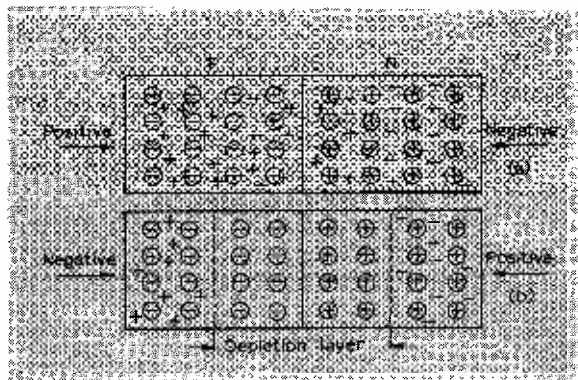


Fig. 5(a): Position of the charges with forward biasing and Fig. 5(b): with reverse biasing.

## Forward and Reverse Biasing

We now have a piece of material with pronounced non-linear characteristics: when an external voltage is applied, current will flow in one direction only. If the p-type side is made positive with respect to the n-type (see Fig. 5(a), forward biasing), the effect is that the barrier potential is reduced. Majority carrier holes will diffuse across to the n-type (where they become minority carriers), and majority carrier electrons will move in to the p-type region. A relatively large current can flow across the junction in this way.

Reversing the bias, i.e. applying it as shown in Fig. 5(b), increases the barrier potential (since the external voltage adds to that across the depletion layer already) so that current flow is made very low—in fact virtually nil. However, due to the effect of temperature a number of holes and free electrons will be generated on either side of the junction—this happens even at room temperatures—and this will give the effect of a small reverse current flowing across the junction. The forward current may be quoted in milliamps but the reverse current only in microamps.

## Characteristics of PN Junction

Fig. 6 shows the characteristics of a pn junction. As the forward voltage is increased from zero, the forward current increases slowly at first until the junction barrier is overcome, then rises rapidly. (In alternative terms, it can be said that the resistance of the forward biased junction is low.) In the reverse direction, the current remains low and practically

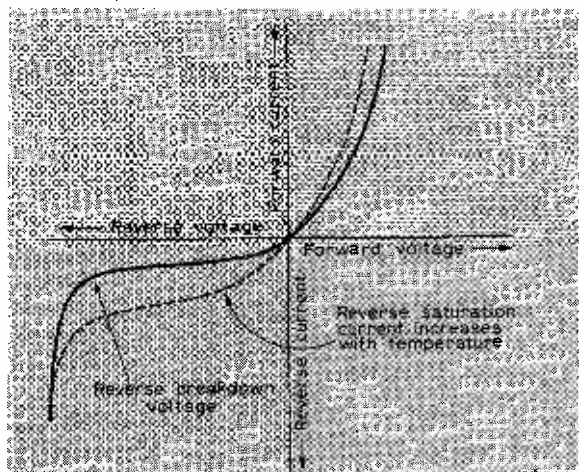
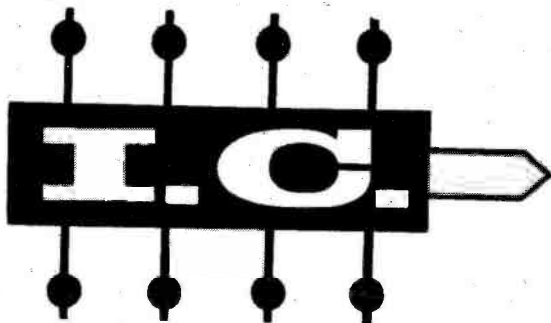


Fig. 6: The electrical characteristics of a PN junction.

constant as voltage is increased, i.e. reverse resistance is very high. Eventually, however, a point is reached where the reverse voltage accelerates the reverse current carriers to such a speed that they break down covalent bonds in the crystal structure, thereby releasing more carriers and producing an avalanche breakdown (when the junction may be destroyed). The value of voltage at which this occurs depends on the resistivity of the material.

As the reverse saturation current is due to the effect of heat, it increases with temperature, giving

—continued on page 512



# OF THE MONTH

L.A.J. IRELAND

## Number 24 LM373 Multiple-mode Detector

SOME months ago these notes described the Motorola MC1596 balanced mixer integrated circuit and outlined its operation as a multiple-mode detector in receiver circuits. The unit discussed now goes further; full i.f. amplification facilities, at any chosen frequency up to 12MHz., are incorporated, as well as multiple-mode detection. It is the National Semiconductors (U.S.A.) type LM373, available in the U.K. from: Athena Semiconductor Marketing Co. Ltd., 140 High Street, Egham, Surrey: or Rastra Electronics Ltd., 275 King Street, Hammersmith, London W.6.

### Uses

The unit is intended, not just to operate in each mode, but to make it possible to design a receiver in which intermode switching would be simple without reduction of performance. As well as the standard a.m. and f.m. modes, as used for broadcast entertainment in the m.f. and v.h.f. bands, the LM373

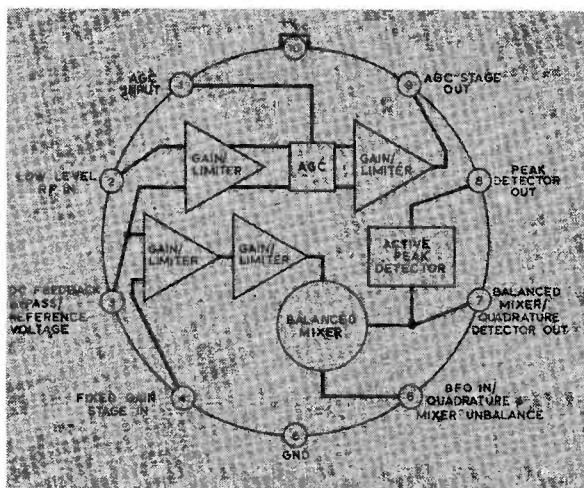
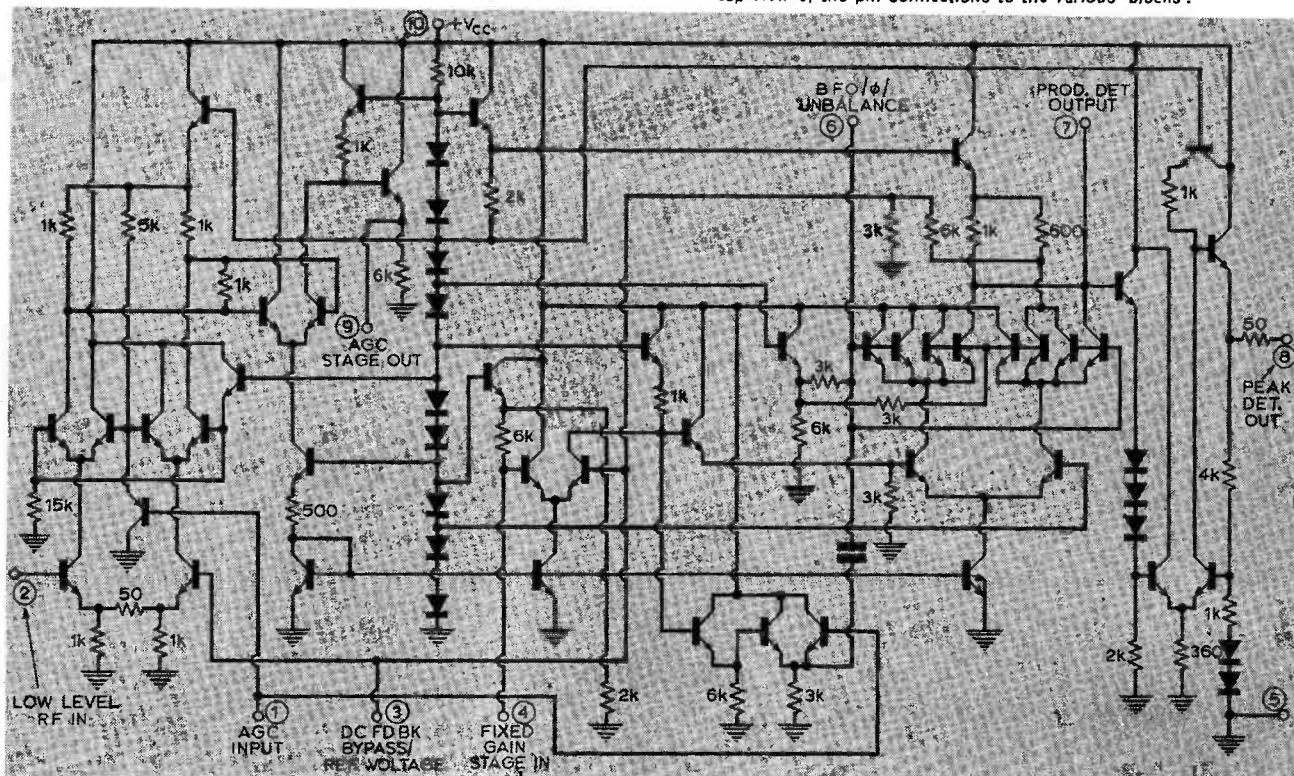


Fig. 1: The equivalent circuit of the LM373 (below) with (above) the top view of the pin connections to the various 'blocks'.





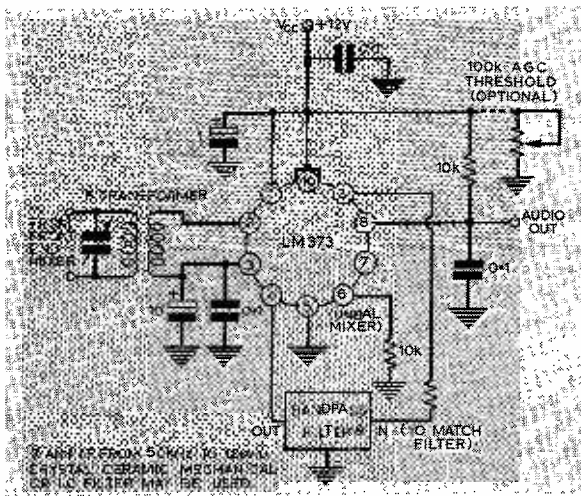


Fig. 2: External circuitry required for the LM373 when used as an AM IF strip.

can handle n.b.f.m. (narrow-band frequency modulation) increasingly used in mobile radiotelephone systems, and s.s.b. (single sideband suppressed carrier) transmissions of commercial or amateur origin.

### Design

Considerable ingenuity is exercised in the design of the i.c. to reconcile the conflicting demands of each transmission system with the minimum of intermode switching in the receiver. A.M. and s.s.b. receivers must have a linear amplitude response, maintained, despite the wide range of signal strength received off the air, by an automatic gain control subcircuit. An f.m. i.f. amplifier strip, on the other hand, is essentially nonlinear, in that any input signal is amplified to a limiting level before application to the detector stage. It follows that automatic gain control has no place in such a system.

To provide the facilities indicated, the LM373 incorporates four gain blocks, which can be operated in a limiting mode, as well as an automatic gain

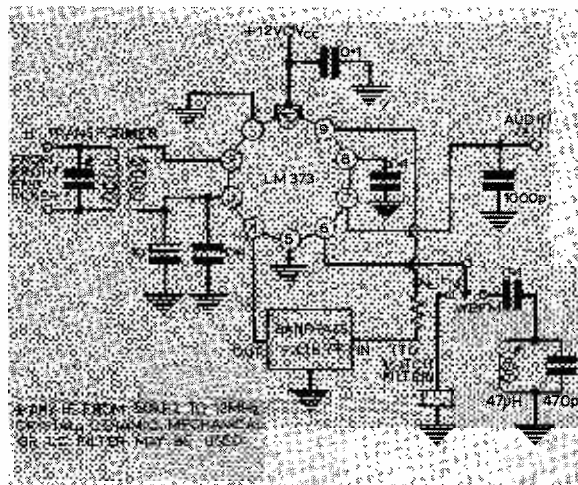


Fig. 3: The LM373 in its role of an FM IF strip suitable for narrow or wideband reception.

control system and two detectors, one a balanced mixer similar to that in the Motorola circuit already mentioned, and the other a peak detector for a.m. operation. The equivalent circuit and pin diagram given in Fig. 1 allows these sections to be identified.

### Operation

Some discussion of the circuit would appear necessary. Each gain block is essentially the familiar differential amplifier, which can be operated in its linear region when the circuit is used for a.m. or s.s.b. reception, or driven to full gain as a limiter for f.m.

The automatic gain control characteristic is secured through a pair of transistors shunting the differential interstage coupling components. When no a.g.c. voltage is applied, these transistors are cut off, but as the control voltage is increased, they draw off an increasing fraction of the signal current; finally the point is reached where the signal from

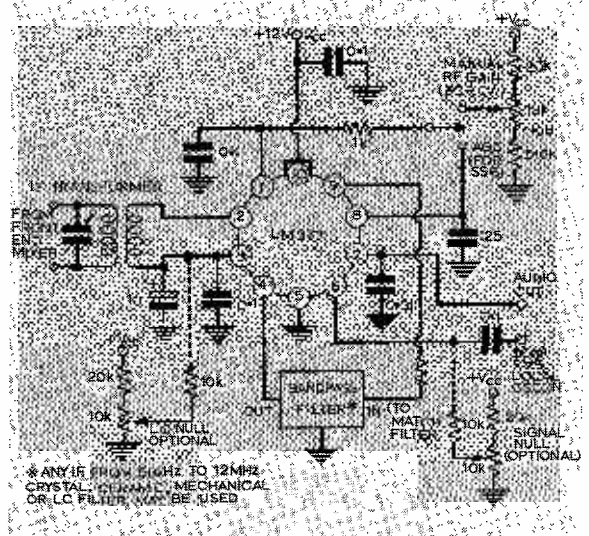


Fig. 4: The SSB/CW IF strip shown here further demonstrates the versatility of the LM373.

the first gain block is shorted out, and coupling to the second is merely through stray capacitance.

This approach secures the unusual a.g.c. range of over 70dB., enabling linear a.m. detection to be attained with input signals from 40 microvolts up to 200 millivolts. The string of reference diodes and emitter follower transistors from the d.c. +ve. line provide power supplies with decoupling to each stage of the amplifier strip, together with appropriate bias voltages to set the operating point of each element. As well as simplifying the external decoupling requirements of the circuit, these imply that each stage essentially has its own regulated supply, so minimizing the effects of power line variations.

The balanced mixer stage is easily identified by the cross-coupling of its component transistors. For f.m. it operates as a quadrature detector, a system outlined when describing the MC1496, as was the product detector system used for s.s.b. In a.m. operation, this section is deliberately unbalanced by an externally applied bias, leaving only one side of

the differential system connected to its load effectively.

N.b.f.m. demodulation requires a quadrature element of a higher Q factor, i.e. more rapid change of phase with frequency, and therefore a quartz crystal is substituted for the more familiar l.c. circuit. The final section is the peak detector, acting as a.m. detector and a.g.c. voltage source for linear a.m. and s.s.b. operation.

A few precautions are necessary for successful operation. The a.g.c. stage output at pin 9 has a very low impedance, being taken from an emitter follower. A value of 70 ohms is quoted, so that if a high Q crystal filter is employed here a series resistor is advocated, so that the resonance peak of the component will not be damped. The manufacturer of the crystal in question will quote a recommended source impedance, allowing selection of an appropriate resistor.

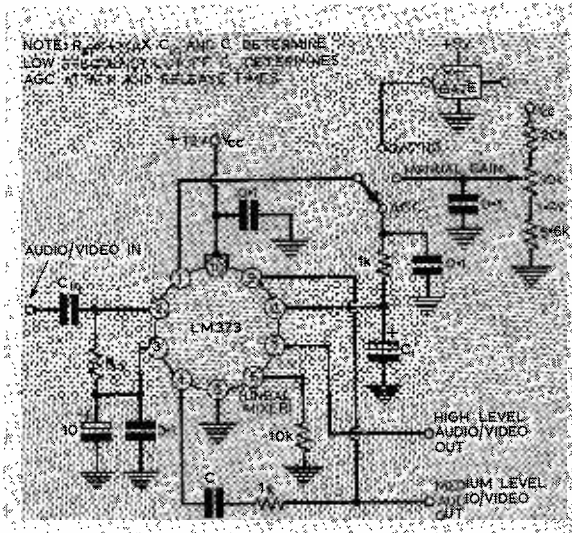


Fig. 5: In TV circuitry the LM373 can be used as an audio/video amplifier with a.g.c., manual gain control or gating.

The d.c. feedback loop at pin 3 must be carefully bypassed, since the decoupling must be effective throughout the passband of the LM373; an electrolytic or tantalum capacitor, as used for a.f. decoupling, has too high a reactance at high frequencies to be effective alone, so a small disc ceramic or silver mica is added.

For s.s.b., bypassing of r.f. at pin 7 is particularly important, as any local oscillator component reaching the peak detector would increase the a.g.c. voltage generated, and lead to an unnecessary reduction of system gain. The optional nulling circuits may be used to maximise gain should that prove necessary (an unlikely event).

Figs. 2-5 indicate the circuitry in which the LM373 may be employed, and it should be noted that the communications receiver applications for which it was designed do not exhaust the potential of this versatile unit, as is indicated by the circuit for a wideband amplifier indicated in Fig.5. Other reported applications have included use as an amplitude-modulated r.f. oscillator, an s.s.b. generator, or indeed any of the applications open to the balanced mixer circuit in which extra wideband gain is useful. So presumably more will be heard of the LM373!

## TRANSISTOR CIRCUITRY FOR BEGINNERS

—continued from page 509

the effect shown by the dotted line in Fig. 6.

Junction devices of this type are known as diodes, and widely used in radio, television and other electronic applications. The diode is essentially a one-way valve, as we have seen from the forward and reverse bias characteristics.

Germanium diodes were the first types developed for commercial use, but the current-handling capacity of these devices was limited, and it was not until research provided a means of treating silicon that power rectifier semiconductors became a practical proposition. Silicon is more difficult to melt and purify than germanium, but can be doped with donor and acceptor impurities in the same way as germanium, is less sensitive to temperature, and will handle higher powers more efficiently. Common types pass currents of half-an-ampere and more with a practically negligible forward resistance. Silicon diodes have a high reverse voltage rating. (On the other hand, a germanium has greater efficiency at low voltages and at higher frequencies, and is thus retained for signal circuits.)

The pn junction forms the basis of most forms of semiconductor diode and transistor. One other form of construction is important in connection with diodes—the point contact type. In this the rectifying property is possessed by a contact between a thin metal wire and a piece of semi-conductor material. Though junction devices predominate today, point contact diodes are still much used as detectors in radio equipment. Their characteristic is similar to that of the pn junction, shown in Fig. 6, except that as the reverse current increases beyond the reverse breakdown point, reverse voltage tends to fall.

TO BE CONTINUED

# TELEVISION

SEPTEMBER

## TV INTEGRATED CIRCUITS

Integrated circuits are beginning to appear in the new TV chassis in increasing numbers, particularly in colour receivers. The types used have been specifically developed to fulfil the signal processing requirements of TV sets but nevertheless bring with them numerous new techniques. In a new series starting this month we shall be examining these new i.c.s. to familiarise readers with the various changes in TV set design they involve.

## SERVICING TV RECEIVERS

Recent articles have concentrated on fairly up-to-date chassis. This month however we are going back to a widely distributed "625-line convertible" chassis, the Sobell ST195/ST282 series. This will give us an opportunity to examine the faults common in older sets.

PLUS ALL THE REGULAR FEATURES

ON SALE NOW

# SERVICING

## AN INTRODUCTION TO FAULT-FINDING

### PART 6

G. J. KING

**THIS MONTH G. J. KING RETURNS TO THE SERIES TO ELABORATE ON AUDIO MATTERS, DEALING WITH CONVENTIONAL VALVE AMPLIFIERS AS WELL AS TRANSISTORISED HI-FI EQUIPMENT.**

**N**OW that colleague Hellyer has cleared the decks on alignment, superhet theory and f.m. stereo, it is my turn to have a go on audio equipment.

#### GRAM AUDIO STAGES

An ordinary radiogram differs little at the pre-audio stages from a radio receiver, so much of the information presented earlier will also be applicable here. However, most contemporary radiograms are equipped for f.m. reception, possibly with a decoder to abstract the stereo information and to direct the left and right channel signals separately to the corresponding audio channels. Thus, many radiograms and record reproducers feature a pair of audio channels and speaker systems. These are very much twin partners, the design of one following very closely the design of the other.

A mono radiogram has just the single audio channel and speaker system (though some designs employ more than one speaker unit, the mono signal being applied to them all in suitable frequency division). Whether mono or stereo, the f.m. front-end is a fairly common factor, the demodulator these days usually being the ratio detector in unbalanced or (in better quality equipment) balanced mode.

However, while the f.m. detector in a mono receiver feeds the audio channel direct (via the  $50\mu\text{S}$  de-emphasis), the f.m. detector in a stereo receiver delivers the multiplex signal to the stereo decoder, the function of which is to process the sidebands of the stereo information (the difference signal) in conjunction with the mono information and the 38kHz reference signal (derived by frequency multiplication from the 19kHz pilot tone) to retrieve the left and right transmitted audio signals in the best isolation (e.g., with the least crosstalk).

De-emphasis and sometimes subchannel suppression (deleting the residual 19kHz and 38kHz multiplex components which can interfere with the audio section and add whistles to tape recordings) are engineered into the left and right audio channels, prior to the power amplifiers.

I shall be having something to say about f.m. front-ends, i.f. channels and stereo decoders later, but for now let us concentrate on the audio channels.

The simplest audio channel is designed round the triode-pentode valve, the triode receiving the detector's signal, amplifying it and then passing it to the control grid of the pentode for power amplification, Fig.1. Quite a lot of valve radiograms are equipped with this kind of audio section, as also are the inexpensive species of record reproducers. These were in fashion when stereo started, so early stereo models boast two such audio sections.

The advent of stereo was concurrent with the development of transistor equipment, which was fortunate for the receiver designers, so the audio channels we now find in stereo equipment are mostly transistorised.

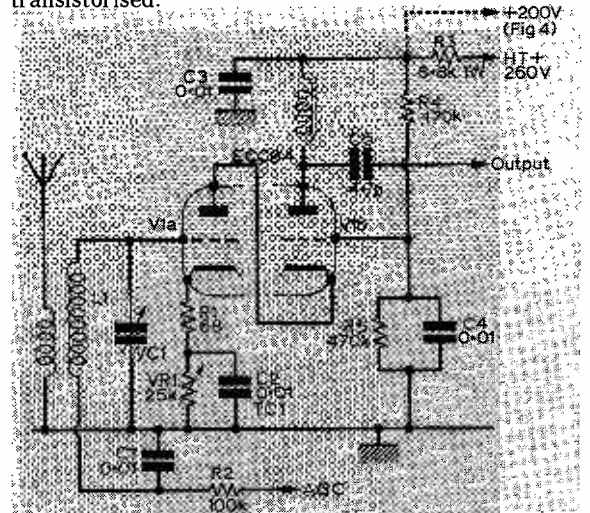


Fig. 1: A typical mono audio amplifier using a single triode-pentode valve.

Some designers favoured the use of a triode voltage amplifier (often one section of a double-triode valve) followed by a separate power pentode. This allows for greater audio power than generally possible from the pentode section of a triode-pentode valve, particularly so far as the early triode-pentode valves are concerned. Such a circuit is shown in Fig. 2, which will be seen to have much in common with that in Fig. 1.

Better quality receivers have been made with a pair of triode-pentodes in each channel to provide push-pull working. In this type of circuit the two pentodes are the push-pull output valves, while the two triodes are arranged as phase splitters supplying the anti-phase drives to the pentodes. However, since few receivers like this are in the field, there is not much point in detailing the circuit, but it is worth bearing in mind.

Let us return to Fig. 1. The audio signal from pickup or radio detector is coupled by C1 to the top of the volume control VR1, the selected level of signal then being applied via C2 to the triode grid. Note that the grid is returned to chassis through R1 (10M $\Omega$ ) and that the cathode of the triode is returned direct to chassis. This is a common trick to secure grid bias for the triode. Contact potential in the valve causes a minute current to flow through R1, and because of the high value of this resistor a small

potential developed across it, and since it is negative at the grid it serves as grid bias. It requires an electronic testmeter to measure this bias (since a normal meter would swamp the 10M $\Omega$  with its own resistance).

A common cause of distortion in this kind of circuit stems from a faulty triode, the fault resulting in excessive grid current and hence a potential across R1 in opposite polarity to that of the bias. The triode anode current rises, and often the valve tends to overheat.

R2 is the triode anode load, with R3 and C3 the decoupling components. The signal across R2 is coupled by C4 to g1 of the pentode, which is biased by the voltage drop across the cathode resistor R4, the grid being returned to chassis through R5. C5 is the cathode bypass capacitor (always an electrolytic in audio output stages).

The anode of the pentode is loaded by the low impedance speaker via the output transformer T1. C6 across the primary attenuates high-order harmonic distortion and makes the reproduction more palatable, as there is no negative feedback and no cancellation of second-harmonic distortion by any push-pull action.

## FAULTS

Owing to the simplicity of this circuit, (Fig. 1) faults are not generally very difficult to define or locate. A cause of bad distortion is poor insulation of the coupling capacitor C4. This would permit a positive potential to exist at the control grid of the pentode with a consequent counteracting of the negative bias. It would be accompanied by excessive positive voltage at the cathode of the pentode, which could result in the failure of C5. The valve would also

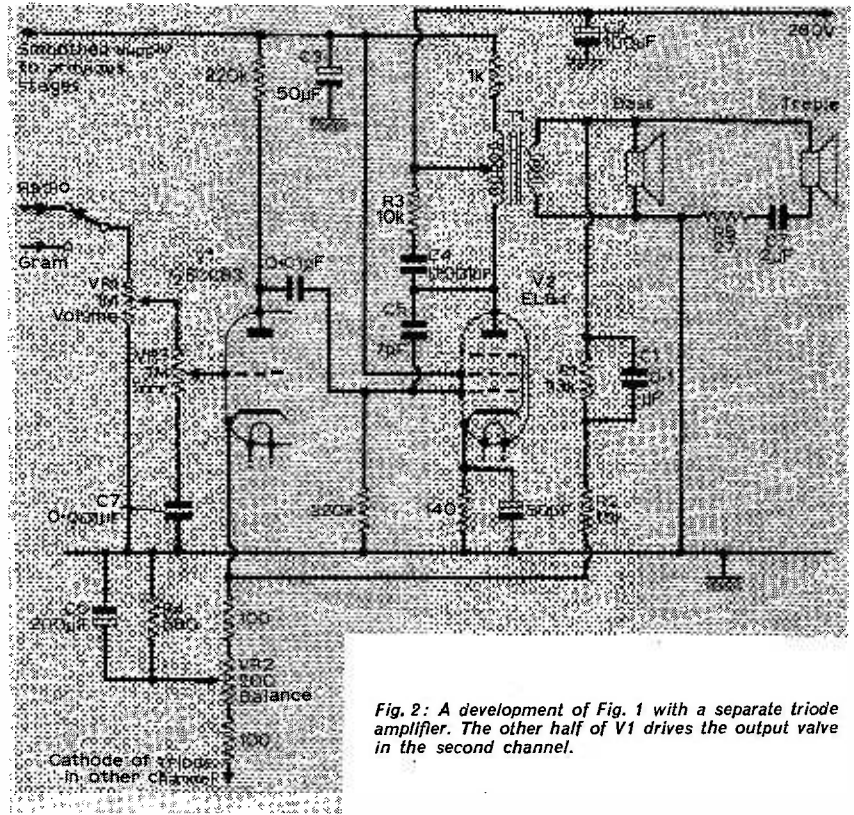


Fig. 2: A development of Fig. 1 with a separate triode amplifier. The other half of V1 drives the output valve in the second channel.

run very hot, possibly with the pentode anode glowing red.

Complete failure (e.g., audio drive at the top of the volume control VR1, but no speaker output) should first lead to a valve test, followed, if necessary, by voltage checks on the appropriate electrodes. C6 is subjected to audio voltage peaks which sometimes result in it shorting. This would cut the output completely, of course, but without affecting the pentode anode voltage much, so look out for this if the valve and electrode voltages seem to be normal.

Open-circuit of T1 primary deletes the pentode anode voltage, a fault condition which is often revealed by the screen grid (g2) of the pentode glowing red hot.

Low gain or volume at maximum volume control setting, assuming normal audio drive from the detector or gram pickup, is not uncommonly caused by C5 going open-circuit or low in value. This results in negative current feedback from the audio then developed across R4. The quickest way of checking this is by shunting an electrolytic across C5.

The symptom can also be caused (possibly accompanied by distortion) by the triode anode load R2 going high. If R3 goes high or C3 becomes electrically 'leaky,' the voltage at the top of R2, and hence the triode anode voltage, will drop, which again will cause low gain and possible distortion.

Before going on to more modern transistor circuits, let us have a look at some possible fault conditions in the valve circuit in Fig. 2. The faults described for Fig. 1 circuit would also be applicable here, with one or two qualifications. First, there are two separate valves involved, the triode voltage amplifier in this case being one section of a double-triode, the other triode serving as the voltage amplifier of the partnering stereo channel (not shown).

If one channel only is in trouble one can easily compare the voltages, etc. with those at the same points in the active channel, which is a quick way of bringing the fault to light. It is also possible to substitute the same type of valves (V2, for example) between the two channels, which would tell conclusively whether the valve is responsible.

There are refinements in Fig. 2, not found in Fig. 1 circuit. For example, voltage negative feedback is applied from the secondary of the output transformer T1 to the cathode of the voltage amplifier V1, and for this to happen one side of the secondary has to be connected to chassis. The amount of feedback is determined by R1 and R2, while C1 in parallel with R1 corrects the phase of the feedback signal, ensuring that it remains substantially negative over the audio spectrum. Thus, if there is a significant rise in gain (e.g., full output at a low setting of the volume control VR1) and abnormally high distortion, then R1 and R2 should be checked for value.

C1 open-circuit could encourage instability at certain frequencies, and this is sometimes 'triggered' by transients of the music. The oscillation could be at a frequency above audio, and the only way to prove this is by connecting an oscilloscope across the secondary of the output transformer T1, preferably when the amplifier is driven by a sinewave signal from an audio generator. The oscillogram in Fig. 3 gives some idea of what the spurious signal could look like on the sinewave. The audio generator would be coupled to the grid of the triode, of course.

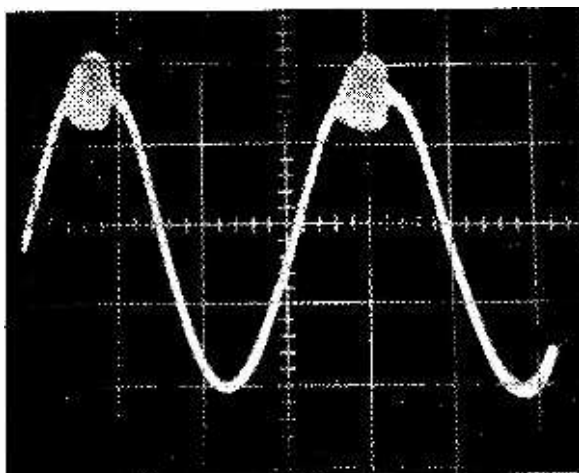


Fig. 3: This oscillogram shows spurious oscillation triggered off by transients in the signal

If the earth and feedback connections are reversed on the transformer the feedback would be positive and the amplifier would turn into a violent oscillator! Take care, therefore, when fitting a replacement transformer! Moreover, designs like this are geared to an output transformer of specific characteristics, so if it becomes necessary to replace the transformer, and the exact type is not available, then it might be necessary to alter the feedback resistors and the phase-correcting capacitor so that the values provide the correct conditions of feedback.

An interesting feature of the circuit is the tap on T1 primary. An output transformer of this kind serves both for speaker coupling and for 'smoothing' the h.t. supply fed to the earlier stages. In fact, it acts in part rather like a smoothing choke. In the

circuit, C2 is the reservoir capacitor across the power supply output and C3 is the main smoothing electrolytic.

R3 and C4 series combination across the signal part of T1 primary attenuates the higher-frequency distortion components while, with C5, providing a degree of corrective phase shift.

The triode V1 in this circuit is cathode-biased, the main cathode resistor being R4, decoupled by C6. VR2 is the stereo balance control, which feeds either side the 100-ohm resistors (one to the cathode circuit of the partnering channel). The 100-ohm resistors provide a small degree of negative current feedback since they are out of the decoupling influence of C6. The voltage developed either side of VR2 relative to the slider also contributes to the feedback. Thus it will be appreciated that by adjusting VR2 from its centre setting, the feedback on one channel will decrease, while increasing on the other channel. This, therefore, allows the gains of the two channels to be adjusted relatively for the most desirable stereo effect.

VR3 is a simple 'tone' control which works as a reactive potential-divider in conjunction with C7. With increasing frequency the reactance of C7 falls, which means that as the slider of VR3 is turned towards this end of the track the bass is lifted and the treble diminished.

It will also be seen that two speaker units are employed. That for bass is connected directly across the secondary of T1, while the treble unit receives drive via R5 and C7. R5 reduces the power, while C7 passes only the higher frequency signals. This is a very simple frequency-divider, which cannot be regarded as 'hi-fi.'

## HI-FI CIRCUIT

One channel of a slightly different circuit which, possibly differing in detail, is found in some hi-fi equipment. This is the power amplifier department only, Fig. 4, where Tr1 is the input transistor, coupling to the d.c.-coupled pair Tr2/Tr3 via C1. The coupling is from Tr1 emitter (the collector 'earthed' to signal through C2). The stage is thus an emitter-follower, which has a relatively high base input impedance, giving the correct match from the control section.

Tr4/Tr5 constitute a complementary driver pair (complementary because one is n.p.n and the other p.n.p.). These drive the push-pull output transistors Tr6/Tr7 alternatively into conduction and cut-off on each half-cycle of signal. It will be noted that the base of Tr4 is fed from the same source (e.g., Tr3 collector) as the base of Tr5. Thus on a positive half-cycle Tr4 conducts and pushes a positive half-cycle into Tr6 base. At the same time Tr5 is driven downwards and since Tr7 base is connected this time to Tr5 collector a negative half-cycle appears at Tr7 base, pushing this transistor into cut-off. On a negative half-cycle of drive the conditions reverse, so that Tr6 is driven into cut-off and Tr7 into conduction.

The two half-cycles are reconstituted as a complete waveform in the load comprising the speaker, coupled through C3.

C4 is a bootstrapping capacitor which applies feedback in such a way as to increase the driver input impedance. A.C. negative voltage feedback is applied to Tr2 emitter circuit from the push-pull pair, via C5

Fig. 4: Circuit of one channel of a transistorised hi-fi stereo amplifier.

and R1. Feedback of 60dB is a common hi-fi value, which reduces the output impedance to a fraction of one ohm.

D.C. coupling exists right through to the output transistors from Tr2, so by adjusting the d.c. conditions, both the drive 'balancing' and the quiescent current of the output transistors are affected. Some circuits have no means of adjusting these parameters, so if the value of a critical component alters, so might the quiescent current and balancing.

However, in Fig. 4 VR1 adjusts the balancing and VR2 the quiescent current, which leads us neatly to hi-fi equipment fault-finding and tests. But before going on to this it is noteworthy that temperature stabilisation is often provided in or around VR2 circuit to hold the quiescent current steady with increase in temperature of the transistors. The 'thermal element,' TH1 in Fig. 4 provides this function.

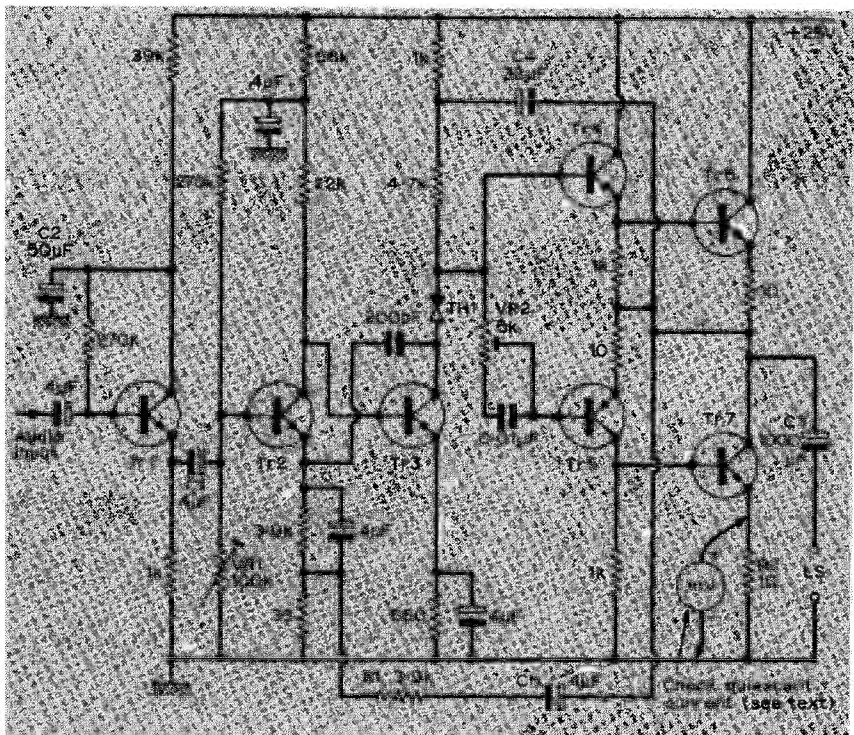
### AMPLIFIER TESTS AND FAULT FINDING

For detailed testing in audio circuits, especially high quality circuits in which transistors are employed, we require an audio signal generator, audio millivoltmeter and an oscilloscope, at least. For distortion tests, we require in addition a distortion factor meter or similar instrument.

If it is assumed that the radio or pickup source signal is reaching the input of the amplifier and there is no output from the speaker, then we should check as far as possible into the amplifier with a signal tracer (e.g., pair of headphones, etc.—see Part 3, PW July 1971). In Fig. 4, for example, we could get to the base of Tr2, but possibly not any further owing to the d.c. couplings of the subsequent stages. Indeed, it is often necessary to consider the power amplifier proper as a complete circuit from the testing point of view. This is because a faulty transistor or component in one stage could reflect fault conditions into the other stages as a result of the d.c. couplings. This possibility is often overlooked when testing in circuits of this kind.

When we reach the point where the signal disappears, therefore, we may have to continue the exercise in terms of voltage measurements at the electrodes of the various transistors, comparing them with the correct values given in the service manual or on the circuit. Complete failure commonly implies significant change in the d.c. conditions, so the fault area should soon be revealed by voltage testing. If a coupling capacitor has failed, then signal tracing should reveal this without much trouble.

More difficult faults to locate are those resulting in low gain, intermittent crackling and distortion at all powers or only at high power. Starting first with distortion, a preliminary test should be that of



quiescent current (assuming the amplifier to be 'Class B,' which it usually is in these days of transistors).

If possible, one should avoid connecting a milliammeter in series with the output pair for this test, owing to the resistance of the meter movement. In a circuit like that in Fig 4, the voltage across the emitter resistor (R2) of Tr7 should be measured on a d.c. millivoltmeter. The voltage will be very low because R2 is only 1 ohm! Anyway, suppose we measure 25mV, then by Ohm's law we can calculate that the current is 25mA (1 ohm resistor, since  $I=V/R$ , where I is in mA when V is in mV). A current of 25mA is, in fact, a common quiescent current value, and it can be adjusted accurately by a preset such as VR2.

If there is no preset and the current is way out, the values of the resistors associated with this part of the circuit should be measured (also the thermistor, etc., if used). Excessive quiescent current will cause the output transistors to run hot and limit the output

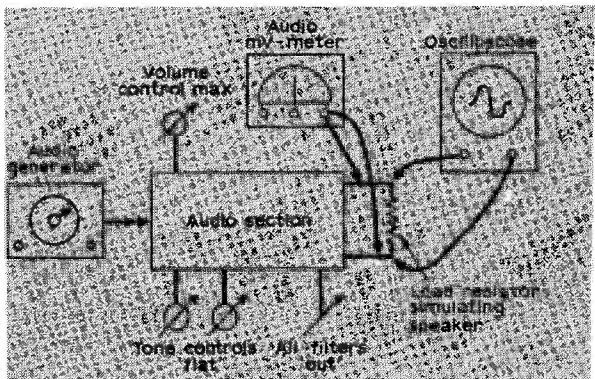


Fig. 5: Equipment set-up required to check the balance of output transistors.

power, while too low a value will precipitate high distortion (crossover distortion) at low volume.

Balancing requires an oscilloscope to monitor the output sine wave fed from an audio generator. The setup is shown in Fig. 5 where it will be seen that the speaker is replaced by a load resistor of suitable power rating (to match the steady-state power of the amplifier). The volume control should be fully advanced, and the generator signal increased until the tips of the displayed waveform commence to clip. When the balancing is correct both tips will clip together. If one clips before the other then the balancing preset (such as VR1 in Fig. 4) should be adjusted for symmetrical clipping. The waveforms are shown in Fig. 6.

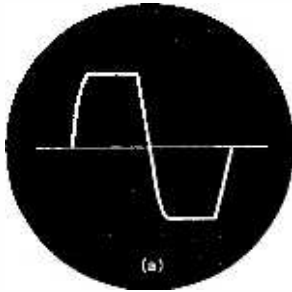


Fig. 6(a) Symmetrical clipping of the waveform when the gain is advanced indicates correct balance.

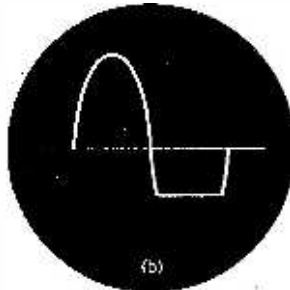


Fig. 6(b) Output waveform with an unbalanced stage.

We can use the setup in Fig. 5 to measure the steady-state power of the amplifier. For this test the oscilloscope should either be accurately calibrated in peak-to-peak voltage (so that the r.m.s. voltage of the waveform can be determined by multiplying the peak voltage—i.e., half p-p voltage—by 0.7) or an r.m.s.-reading audio millivoltmeter should also be connected across the load, as shown in Fig. 5.

The load voltage just prior to the clipping point should be noted, and the steady-state power in watts is equal to the load voltage squared divided by the load value in ohms (i.e.,  $W = V^2/R$ ). The power is usually taken at 1kHz, but the power bandwidth can be appraised by noting the reduction in power at the low and high frequency ends of the spectrum.

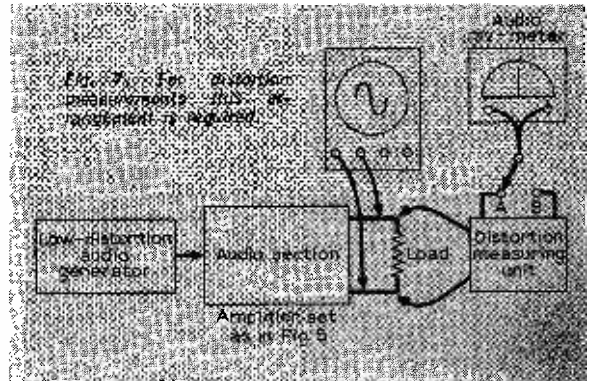
Low power, but good waveshape often signifies low supply rail voltage, and this can result from low mains voltage or incorrect mains voltage tapping.

## DISTORTION TEST

Finally, total harmonic distortion testing. For this we require either a complete distortion factor meter or the set-up in Fig. 5 with a distortion measuring unit which, as was noted in the Test Instrument supplement, April 1971, is a 'notch filter' which

tunes out the fundamental frequency of the output signal, leaving only the harmonic components, the voltage sum of which is compared in ratio with the voltage of the fundamental frequency across the load, to give the dB or percentage total harmonic distortion.

The complete set-up is shown in Fig. 7. The voltage across the load is first measured at the required power (use the oscilloscope for maximum power test to indicate the clipping level) with the switch in position A, then switching to position B, allowing the audio millivoltmeter to read the voltage of the summed harmonics. For this to happen, however, the distortion measuring unit needs to be very accurately tuned and balanced for the least indication on the audio millivoltmeter, which requires the range of the millivoltmeter progressively to be stepped down. The total harmonic distortion is the voltage ratio between the readings at switch positions A and B.



For example, if voltage A is 9V (which across 8 ohms would correspond to about 10W) and voltage B is 90mV, the ratio would be 100:1 or 40dB, corresponding to 1% t.h.d. With 9mV at B it would represent a ratio of 1000:1 or 60dB, corresponding to 0.1% t.h.d.

Remember, though, that a simple distortion measuring set 'notches out' only the fundamental, leaving wideband noise as well as t.h.d. components, so the distortion readout will include noise. Residual hum is generally removed by a high-pass filter in the test set-up, but such filtering, of course, cannot be used for distortion measurements at low-frequency for obvious reasons.

## END OF PART SIX

### Back Numbers Important Announcement

We regret to inform readers that owing to the closure by the Company of the department concerned it will no longer be possible to supply back numbers of **Practical Wireless** and **Television**.

To ensure obtaining regular copies of these magazines readers are strongly urged to place a regular order with their local newsagent, or to take out an annual postal subscription.

Reference to past issues of the magazines may sometimes be obtained at certain public libraries who may hold bound volumes. A few libraries are said to offer a photostat service. Alternatively, we are always willing to insert a free request for specific back numbers in our "CQ" column which appears in most issues.

# practically wireless

## commentary by HENRY

Ted  
and  
Lid

NO, not *that* Ted. Henry is not taking the lid off political chicanery—leave that to out-of-office politicians. TED, or, more properly, T.E.D., is a beautiful phrase I heard during a broadcast interview recently. That ubiquitous character, A. Spokesman, was defending the Post Office in the face of polite but relentless attacks from the BBC, who were following up listeners' complaints about crossed lines.

'How does it happen,' came the suave question, *'that we pick up our telephone and find our conversation interrupted by a pair of drooling lovers or an irate customer who has lost his laundry?'*

Ah, well, our indefatigable spokesman countered, that is probably caused by a Transient Equipment Defect. Isn't that lovely? Imagine, Joe, when wifey grumbles about the birdies that chirp unwantably during her 'Housewives' Choice', being able to say airily: *"Can't do much about that, I'm afraid. That's TED."*

The point is that the faults are not just short-lived, ephemeral, unidentified phenomena—giving them a name has fixed them, preserved them for posterity, entered them on the list of recognisable bugbears.

Wireless work is full of such



We cheer when we get a half-scale reading . . .

instances; for example, the intermittently blowing fuse. We pursue diligent tests before replacing the offending glass tube. We measure resistance, cheer when we get a half-scale reading, then remember that we intended to change the battery of the meter last time we used it.

Baffled by the lack of short-circuits we decide to beat the brute by checking the current. Meter in series—ah, which way round? Switch on. No, the other way around: *is that pointer bent?* But the reading is no greater than expected, and certainly less than the rating of the fuse, which we refit. Perhaps it is the result of overheating. We cover the now smug-looking set with our jacket and wait.

It is a bad habit of some manufacturers to let dirty great heat-sinks jut out at the back, and the fallacy about cool-running transistors is shattered as we smell singeing Harris Tweed and realise we have a Class A output to contend with.

Touching the fins to confirm our nose, we snatch fingers back with a howl and, sucking them, muse that the problem could not have been temperature at all. And the fuse still holds.

Obviously, TED has been at work. He is only waiting for us to settle comfortably with a book and a glass at our elbow before blowing the fuse again. Or, more likely, lulling us into a false sense of security, will allow us the whole evening's listening, then, while we sleep through the small CQ hours, will sneakily contract that vulnerable thread of wire again so that rising betimes, we gaily throw the switch and get: silence!

TED is no fool. That Post Office bloke urged 'sweet reasonableness' upon subscribers when their lines were crossed. The inference was that if we pretended not to notice the fault it would go away. Any PW reader could have told him that is the wrong approach.



. . . and we snatch our fingers back with a howl.

How many times have you had a piece of equipment propped up on the bench, festooned with test leads, bedizened with warning lights, burbling away in the corner of your mind, and leaped into the breach as the expected fault occurs, only to be greeted with a return to normality the moment you touch the chassis?

Tracking down TED is the work of an expert. One tests piecemeal. One uses not sweet reasonableness, but bitter reason. Diagnosis, as our soon-to-finish series on Servicing has emphasised, is the secret of success. And for *diagnosis*, where TED is concerned, read *inspired guesswork*. This is where LID comes in. LID is one of those contractions I am no longer likely to forget, since talking to Bob Stockwell, publicity manager of Bang & Olufsen, the day after an exhausting exhibition.

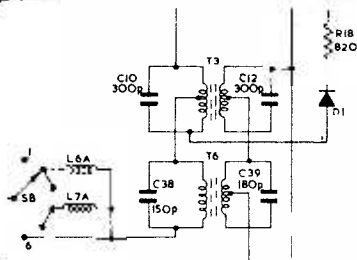
'How do you manage to organise it?'

'It's not easy,' he said, *'but we begin by catering for the Largest Imaginable Disaster and take it from there. . . .'*

That is the secret of dealing with TED. Put the LID on him: when the fuse blows, imagine the worst that could happen and assume that it has! But don't try to telephone the repairman—you will probably get the laundry company again.



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**1**

We provide a full range of components and sub-assemblies, with details of what they do, so that you learn to recognise all the 'bits and pieces'. Using some of these you are instructed in how to build this oscilloscope, simply and quickly.

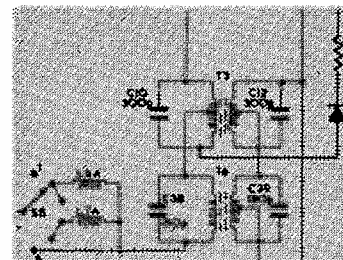
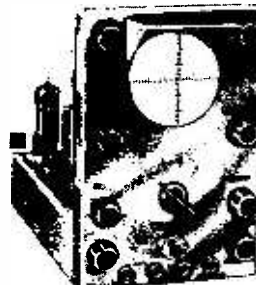
**2**

You are shown how to read and understand circuit diagrams so that you can later build more advanced equipment or draw your own diagrams.

**3**

You can construct over 40 kits, including:—

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- Transistor experiments
- Amplifiers
- Oscillators
- Signal tracer
- Photo electric circuit
- Computer circuit
- Basic radio receiver
- Electronic switch
- Simple transmitter
- a.c. experiments
- d.c. experiments
- Simple counter
- Time delay circuit
- Servicing procedures



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# ELECTRONIC VALVES

0A2	0-88	6L7GT	0-85	DY87	0-85	PC88	0-55
0A3	0-45	6F9GT	0-85	EF82	0-60	PC89	0-60
0B2	0-35	88Q7	0-40	EB8C3	0-65	PC89	0-55
0B3	0-60	68R7	0-40	EL80F	0-95	PC8065	0-85
0C3	0-58	6T8	0-35	EB10F	0-90	PC8066	0-80
0D3	0-35	6U4GT	0-60	EAB2C8	0-35	PCF80	0-30
138GT	0-38	6V8A	0-40	EAF42	0-55	PCF82	0-35
1CP31	0-60	6X6T	0-38	EB8C33	0-50	PCF84	0-60
1R4	0-20	6BC41	0-65	EB841	0-55	PCF87	0-80
1R4	0-85	6K5GT	0-85	EB8C81	0-50	PCF87	0-85
1R5	0-35	6K5	0-55	EBF80	0-40	PCF801	0-50
1S4	0-27	6Y6G	0-65	EBF83	0-40	PCF802	0-50
1S5	0-26	7Y4	0-60	EBF89	0-30	PCF805	0-75
1T4	0-25	9BW6	0-60	EC53	0-50	PCF806	0-70
1U4	0-27	10C1	0-50	EC86	0-60	PCF806	0-75
1U5	0-60	10D1	0-50	EC60	0-60	PCF806	0-70
1V2	0-45	10D2	0-40	EC90	0-38	PCL81	0-50
1X2B	0-40	10F1	0-60	EC91	0-50	PCL82	0-55
2D21	0-35	10F9	0-50	EC92	0-35	PCL83	0-65
3A4	0-35	10F18	0-45	EC93	0-50	PCL84	0-45
3Z8	2-15	10L1	0-45	EC8010	2-25	PCL85	0-40
3ZF1	2-75	10LD11	0-60	EC8011	2-40	PCL86	0-45
3Q4	0-40	10P13	0-55	EC831	0-38	PCL88	0-90
384	0-55	10P14	1-10	EC82	0-30	PCFL80	0-98
3V4	0-45	12AB5	0-60	EC83	0-30	PCFL801	0-70
5B4GY	0-60	12AC8	0-40	EC84	0-30	PD500	1-50
5Y4G	0-35	12AL5	0-45	EC85	0-40	PR86	0-60
5U4G	0-35	12AQ3	0-45	EC86	0-40	PR88	0-85
5V4G	0-40	12AT8	0-45	EC89	0-60	PFL200	0-70
5Y3GT	0-32	12AT7	0-38	EC91	0-90	PL3	0-85
5Z3	0-50	12AU6	0-30	ECC189	0-60	PL36	0-65
5Z4G	0-40	12AU7	0-30	ECC80	0-35	PL81	0-50
6/30L2	0-75	12AV6	0-38	ECCF82	0-35	PL82	0-45
6AD4	0-25	12AV7	0-50	ECCF86	0-65	PL83	0-45
6AD4A	0-25	12AX7	0-80	ECCF84	1-50	PL84	0-40
6AG7	0-40	12AX7	0-70	ECH42	0-70	PL302	0-80
6AH6	0-50	12BA4A	0-65	ECH81	0-30	PL504	0-80
6AJ2	0-30	12BA6A	0-35	ECH83	0-40	PL508	0-90
6AK5	0-30	12BA7	0-35	ECH84	0-45	PL509	1-30
6AK6	0-57	12BE6	0-35	ECH90	0-40	PL801	0-80
6ALS	0-43	12BH7	0-40	ECL1	0-45	PM84	0-50
6AL5	0-35	12BX7	0-35	ECL2	0-45	PM84	0-50
6AM5	0-32	12K5	0-55	ECL83	0-45	PY83	0-38
6AM6	0-38	12K7GT	0-38	ECL84	0-55	PY80	0-35
6AQ5	0-35	12Q7G	0-30	ECL85	0-55	PY81	0-30
6AQ6	0-55	12R7	0-35	ECL86	0-40	PY82	0-30
6AR5	0-35	1487	0-80	ECL89	0-60	PY83	0-38
6AR6	0-40	14D1	0-60	ECL89	1-50	QY81	0-40
6AR11	1-25	20L1	1-10	EF73A	0-60	PY800	1-50
6AS5	0-35	20P1	0-50	EF87A	0-40	PY801	0-50
6AS7G	0-30	20P4	1-10	EF40	0-50	PY801	0-50
6AT6	0-30	20P5	1-20	EF41	0-65	PZ80	0-35
6AU5	0-25	25C5	0-30	EF42	0-70	QQV2-6	2-15
6AV6	0-30	25L6GT	0-45	EF80	0-25	QQV8-10	2-25
6AW8A	0-55	25Z4G	0-60	EF83	0-35	QQV8-10	2-15
6BA4	0-25	25Z6GT	0-65	EF85	0-35	QQV3-20A	3-55
6BE6	0-30	30A5	0-45	EF86	0-30	QQV3-20A	3-55
6BF5	0-30	30AE3	0-40	EF89	0-28	QQV6-4A	5-50
6BF6	0-50	30C1	0-30	EF91	0-33	TT21	2-65
6BH5	0-45	30C15	0-80	EF92	0-40	TT22	2-85
6B7B	0-45	30C17	0-45	EF95	0-30	U18/20	2-75
6BK7A	0-55	30C18	0-75	EF97	0-65	U25	0-75
6BN6	0-43	30F5	0-85	EF98	0-65	U26	0-75
6BQ6	0-25	30FL1	0-70	EF183	0-30	U31	0-45
6BQ5	0-25	30FL12	0-98	EF184	0-35	U37	1-50
6BR8	0-65	30FL14	0-75	EF800	1-00	UT2	0-85
6BS7	1-30	30L7	0-45	EF804	1-25	UT2	0-85
6BW6	0-55	30L15	0-85	EK90	0-30	U76	0-30
6BX6	0-25	30L17	0-80	EL33	1-25	U78	0-30
6BX6	0-25	30P12	0-80	EL34	0-50	U191	0-75
6BX6	0-25	30P19	0-80	EL36	0-50	U201	0-85
6C4	0-38	30FL11	0-70	EL37	1-25	U281	0-40
6C5GT	0-45	30FL13	0-85	EL38	1-50	U32	0-40
6CB6	0-30	30FL14	0-90	EL42	0-68	U801	0-40
6CD6A	1-15	35A3	0-55	EL81	0-55	U403	0-50
6CQ7	0-50	35A5	0-75	EL82	0-42	U404	0-40
6C86	0-55	35B5	0-65	EL84	0-25	U801	1-30
6CLO	0-50	35C5	0-40	EL85	0-48	UACB80	0-85
6CW4	0-80	35D5	0-60	EZ86	0-50	UAF1	0-50
6CXY5	0-45	35L6GT	0-50	EL90	0-35	UAF42	0-55
6C7	0-68	35W4	0-30	EL96	0-85	UBC41	0-50
6D3	0-45	35Z3	0-30	EL803	1-00	UBC81	0-40
6D6G	0-75	35Z4G	0-60	EL821	0-55	UBF80	0-40
6D8	0-45	35Z6GT	0-40	EL822	0-90	UBF89	0-35
6DQ6B	0-65	35A5	0-50	EZ86	0-75	UBLA	0-50
6DS4	0-75	50R5	0-45	EM34	0-90	UBL21	0-60
6EA8	0-58	50C5	0-40	EM71	0-75	UC92	0-35
6ER7	0-60	50CD6G	1-65	EM80	0-40	UC85	0-40
6EJ7	0-35	50L6GT	0-50	EM81	0-80	UCF80	0-55
6FV6	0-55	85A2	0-40	EM84	0-35	UCM21	0-60
6F1	0-70	90A6	2-40	EM85	1-00	UCF42	0-70
6F5	0-50	90AV	2-50	EM87	0-55	UCH43	0-75
6FG6	0-30	90C1	0-60	EN91	0-85	UCH81	0-35
6F11	0-38	90CV	1-25	EY61	0-40	UCL81	0-60
6F13	0-38	807	0-50	EY80	0-45	UCL82	0-35
6F14	0-65	813	3-75	EY81	0-40	UCL83	0-80
6F15	0-85	809B	0-50	EY83	0-55	UFA1	0-60
6F18	0-45	5642	0-65	EY86	0-40	UFA2	0-60
6F23	0-80	6080	1-50	EY87	0-43	UFA3	0-65
6F24	0-75	6146	1-50	EY88	0-43	UFS8	0-80
6F25	0-75	6386	1-25	EZ40	0-45	UF85	0-40
6F26	0-35	6870	2-50	EZ41	0-45	UF89	0-35
6F28	0-60	7199	1-15	EZ50	0-85	UL41	0-60
6J4	0-30	7199	0-75	EZ51	0-28	UM84	0-30
6J5GT	0-80	7360	1-80	GY501	0-80	UM84	0-20
6K7	0-45	7586	1-25	GZ30	0-40	UY1N	0-50
6K6GT	0-55	7885	1-25	GZ31	0-33	UY11	0-65
6K7	0-35	9002	0-35	GZ32	0-48	UY41	0-45
6K6G	0-55	9003	0-50	GZ33	0-70	UF83	0-60
6K25	0-75	AZ1	0-48	GZ34	0-60	UY86	0-30
6L6GT	0-45	AZ31	0-55	HABC80	0-40	WT29	0-60
6L7	0-40	CB11	0-80	HK90	0-35	ZT59	1-85
6L18	0-45	CB13	0-90	KT66	2-05	Z803U	0-90
6LD20	0-40	CY31	0-35	KT88	2-00		
6N7GT	0-40	DAF96	0-42	N78	1-45		
6P4	0-60	DF96	0-42	PACB60	0-40		
6P25	1-25	DK40	0-55	PC86	0-60		
6P28	0-65	DK92	0-50	PC88	0-60		
6Q7	0-40	DK96	0-42	PC97	0-50		
68A7	0-40	DL96	0-42	PC90	0-48		
68G7	0-35	DM160	0-65	PC84	0-40		
68K7	0-35	DY86	0-38	PC85	0-40		

# STEPHENS

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### SEMICONDUCTORS BRAND NEW MANUFACTURERS MARKINGS NO REMARKED DEVICES

2N388A	62p	2N3702	17p	ACY18	25p	AF127	17p	BC184	22p	BFY52	22p
2N614	30p	2N3704	22p	ACY19	25p	AF139	37p	BC187	22p	B8X21	37p
2N697	20p	2N3705	20p	ACY20	25p	AF178	45p	BC23L	22p	OC25	25p
2N698	20p	2N3711	20p	ACY21	25p	AF179	45p	BCY32	37p	OC26	32p
2N706	12p	2N3819	35	ACY22	20p	AF180	52p	BCY58	22p	OC28	62p
2N706A	12p	2N3826	30p	ACY28	20p	AF181	42p	BCY70	20p	OC29	75p
2N706B	12p	2N3895	37p	ACY40	20p	AF186	66p	BD115	78p	OC35	40p
2N739	32p	2N3914	P.A.	ACY41	25p	AF239	42p	BD129	82p	OC42	25p
2N1132	27p	R.C.A.	47p	ACY74	40p	AS728	25p	BD132	82p	OC44	30p
2N1303	17p	R.C.A.	47p	ACY74	40p	BC107	15p	BD132	82p	OC45	32p
2N1305	25p	40253	P.A.	AD140	40p	BC109	15p	BD132	82p	OC46	15p
2N1306	25p	40298	P.A.	AD142	58p	BC108	15p	BD131	87p	OC45	15p
2N1307	25p	40454	P.A.	AD149	57p	BC109	15p	BD132	82p	OC46	15p
2N1711	25p	2N4061	22p	AD150	62p	BC113	27p	BF115	25p	OC70	15p
2N1747	78p	2N4082	22p	AD161	37p	BC114	37p	BF117	47p	OC71	12p
2N2160	57p	2N4286	17p	AD162	37p	BC115	32p	BF180	P.A.	OC72	12p
2N2614	30p	2N4281	17p	AF102	85p	BC116	62p	BF181	P.A.	OC74	32p
2N2646	57p	AC107	30p	AF106	42p	BC116A	37p	BF188	P.A.	OC75	22p
2N2905	40p	AC117	80p	AF114	25p	BC117	39p	BF187	25p	OC76	22p
2N2926	40p	AC126	20p	AF115	30p	BC118	32p	BF173	32p	OC77	27p
Green	12p	AC127	25p	AF116	25p	BC134	57p	BF178	35p	OC78	25p
Yellow	12p	AC128	20p	AF117	25p	BC135	P.A.	BF179	72p	OC81	20p
Orange	12p	AC154	25p	AF118	60p	BC136	P.A.	BF180	85p	OC81D	20p
2N3053	27p										

# SHORT WAVES

## MONTHLY NEWS FOR DX LISTENERS

**T**HE first report this month comes from a new reporter D. A. Hairon from Jersey in the Channel Islands. The equipment used was a Codar CR70A receiver, a 50ft long wire and a 19 metre band dipole. This combination enabled him to hear the following stations:—

- 9480 Radio Peking in English at 0130.
- 9625 CBC, Canada in English at 0200.
- 11710 R. Nacional de Espana in Spanish at 0130.
- 11720 CBC, Canada in English at 0200.
- 11730 R. Nederland, Bonaire, English at 0200.
- 11745 HCJB, Quito, Ecuador, English at 0000.
- 11775 TWR, Bonaire in Spanish at 0215.
- 11810 RAI, Rome in English at 0100.
- 15195 R. Ankara, Turkey, Turkish at 1600.
- 15250 RSA, South Africa in French at 1856.
- 15300 HCJB, Quito, Ecuador in Spanish at 2145, and in Portuguese at 0000.
- 15305 SBC, Switzerland in English at 1315.
- 15345 Radio Kuwait in English at 1630.
- 15355 ABC, Australia in English at 0530.
- 17655 R. Cairo, U.A.R. in English at 1730.
- 17715 ABC, Australia in French at 2315.
- 17810 R. Nederland, Bonaire in Spanish at 2130.
- 17830 R. Lebanon in English at 1830.
- 17825 NHK, Japan in English at 0800.
- 21525 WNYW, U.S.A. in English at 1800.
- 21640 R. Nederland, Bonaire, English at 1830.
- 25730 R. Norway in English at 1200.

Ray Warren of Bury St. Edmunds has used his Koyo 1661 receiver to good effect and heard the following:—

- 3980 Voice of America in English at 1720.
- 5970 R. Free Europe, Germany at 1450.
- 6075 WNBC, New York, news at 1630.
- 6085 R. Nederland in English at 0930.
- 9030 R. Peking in English at 2050.
- 9390 R. Tirana, Albania in English at 1530.
- 9750 SBC, Switzerland, news in English, 1540.
- 15300 HCJB, Quito, Ecuador, English news, 1410.

Peter Hall of Pocklington, Yorkshire, has a Meridian 10 transistor superhet and a 50 foot aerial which enabled him to hear:—

- 6070 R. Sofia, Bulgaria in English at 1930.
- 6130 HCJB, Quito, Ecuador in English at 0800.
- 7275 RAI, Rome in English at 1940.
- 9550 Radio Finland in English at 1815.
- 9580 BBC, Ascension Island relay at 2115.
- 9620 R. Belgrade, Yugoslavia at 1800.
- 9625 Israel B.C. in English at 2045.
- 9630 R. Trans Europe, Portugal at 2100.
- 9700 R. Sofia, Bulgaria in English at 2140.
- 11620 AIR, Delhi in English at 2010.
- 11672 R. Pakistan in English at 2030.

## THE BROADCAST BANDS

Malcolm Connah

Frequencies in kHz ● Times in GMT

- 11755 R. Finland in English at 0930.
- 11915 BBC, Cyprus relay at 1645.
- 11965 TWR, Monaco in English at 1700.

Ross Pullen of Crawley used his Murphy A72 communications receiver and a 100 foot long-wire to hear some interesting stations:—

- 6015 VOA, Rhodes, music and talk at 2200.
- 6145 R. Nacional, Brazil in Spanish at 2245.
- 9510 R. Noumea, New Caledonia, French at 0910.
- 9605 HCJB, Quito, Ecuador, English at 0730.
- 9745 R. Baghdad, Iraq in English at 2015.
- 9775 R. Diffusion-Television Nationale Congolaise, African music at 2200.
- 11672 R. Pakistan, English at 2002.
- 11965 Rwanda relay of Deutsche Welle at 2037.
- 17705 R. Havana, Cuba, Spanish news at 2015.

F. Wall of Walthamstow, London, E.17, has a homebrew 5-valve superhet and a 20 foot wire aerial, this equipment enabling him to hear:—

- 6035 R. Warsaw with Polish news at 1620.
- 6070 R. Sofia, Bulgaria in English at 1930.
- 9912 AIR, Delhi English news at 2000.
- 9630 R. Sweden 'Calling DXers' at 1230.
- 9660 R. Trans Europe in English at 1250.
- 9833 R. Budapest, Hungary, requests at 1945.
- 11735 R. Belgrade, Yugoslavia, English at 1530.
- 11740 ABC, Australia at 1530.
- 11755 R. Finland in English at 1500.
- 11765 ABC, Australia, sports programme at 0830.
- 11955 BBC, Malaysian relay at 1815.
- 15325 CBC, Canada, sports news at 1200.
- 21460 HCJB, Quito, Ecuador sign-on in French at 2015.
- 21535 RSA, South Africa, English news at 0930.
- 21595 CBC, Canada with news at 1910.
- 25790 RSA, South Africa, English news at 1500.

Stephen Mathews of Hull with his Bush 4-valve domestic receiver and 90 foot loft aerial heard the following:—

- 9660 YVLM Radio Rumbos, Venezuela at 0320.
- 9833 R. Espana Independiente, clandestine at 2230.
- 11765 ZYB8, R. Diffusion, Brazil at 0220.
- 11795 WINB, Red Lion, U.S.A. English at 2100.
- 11815 ZYW24, R. Brazil Central at 0045.
- 15260 FEBA, Seychelles testing at 1700.
- 17890 BED-40, Taiwan, weak at 0330.
- 21690 WIBS, Grenada in English at 1945.
- 21720 R. Ghana in English at 1445.

Reports should arrive by the 15th of the month and be addressed to the author at 5 Ranelagh Gardens, Cranbrook, Ilford, Essex.

# SHORT WAVES

## THE AMATEUR BANDS

David Gibson, G3JDG

Frequencies in kHz • Times in GMT

**H**IGH noise levels have been the main complaint this past month with many people confessing to giving up and going off to watch television (sacrilege!). Despite these conditions there was still a large number of listeners who persisted, despite the noise, and managed to log some worthwhile DX as reward for their labours. Just goes to show, while you are busy moaning about the QRM and QRN, someone else is just getting on with it and working half the world.

News that G5ZT has received slow-scan television pictures from FG7XT in Guadeloupe makes you think. Many people would be only too pleased to hear an FG7 on c.w. **John Rimmer** (Deal) warns that VS9MF is on from Gan—a small island in the Maldive group of islands. Listen on 14 and 21MHz; sorry, no specific freqs given.

No activity reported on ten metres this month and it rather looks as though everyone has migrated to 14MHz. This latter band is an early morning/late night affair nowadays with everything dying out from mid-morning to late afternoon. On fifteen metres the same remarks apply, although occasionally South American stations appear during the daytime. For those who would like to persist on 28MHz, suggested time for a listen is from 1400 to 1600hrs.

Incidentally, this is one of the best bands on which to play with aerials since these normally work out to a very reasonable size. A quarter wave vertical is only around the 8ft. 6in. mark, exact size depending upon frequency since ten metres is one of the widest bands we have among those l.f. of 144MHz. If sunspot counts are any indication, then September would be a very good time for ten metres.

A few contests this month just to get your ears in trim for the long winter evenings. September 11 and 12, WAE phone contest; 12, 3.5MHz Field Day; October 2 and 3, u.h.f./s.h.f. Field Day; 2 and 3, Oceania contest—a chance to bag a nice list of VK/ZL callsigns; 2 and 3, IARU Region 1 u.h.f./s.h.f. contest. Don't forget the Cumulative Activity on 70MHz from October 9 to December 30. This is our "use or lose" band and all support is very welcome, if not essential. You might try listening for some of the RAEN activity on four metres. The Radio Amateur Emergency Network has numerous "local" groups and the favourite band is 70MHz. How about listening out for your local group, or perhaps even joining them? Name and address of the Secretary of RAEN is; E. Bassett, 57 Upper St Helen's Road, Hedge End, Southampton, SO3 4LG.

## Logs

A solitary log for two metres arrived this month from **David Sheekay** (Ashford). Gear is a super-regen using three transistors and an i.c. audio amplifier, homebrew, and antenna is described as "telescopic". Stations logged include; G2JF, G2VB, G3EFX/P, G3JXN, G3LTF, G3TDP/M, G3UNT,

G4AAR, G4AAZ/M, G5OX, G8BYC, G8CCO, G8EBV, G8ELW and F0UJ. What about it all you converter and superhet types—you can't let a super-regen show you up, or can you?

**Richard Mortimore** (Cardiff), is now up to 20 w.p.m. at c.w. and says that he recommends all s.w.l.s to learn morse. Small sample from his list of c.w. pickings on 21MHz includes; CR6ID, JA3IL, KZ5BB, PY2EYE, PY4UK, W4NZK, WB4QVQ.

**Mark Marsden** (Ilford) uses a cassette tape recorder which has its input wired in parallel with the headphones. He claims this is very useful for checking calls heard against calls logged afterwards. Seems a very good idea. Calls heard, checked, recorded and logged on 14MHz include signals from; CE5ID, JA3JH, KV4HE, KZ5JF, PY2ZAC, PY4AEB, SV0WZ, VK3ART, VK4PJ, VP2AA, WA1DYR/MM, WB6YIY/MM, YV5CPA, YN2SC, ZL5ISJ, 4X4JU, 4X4OC, 9Q5IA.

"My uncle has given me all the PWs he can spare", writes **Kevin Davies**. Receiver is an R107 and the antenna 120ft. l.w. The following were in evidence on 14MHz s.s.b.; CT1ZE, EA3KO, EA4LM, EL2C, EL4A, HR3VSJ, JA1VK, K1WPS/CT1, LU4DMG, W1CMG/P1, W1MYA/MM, WA5KHM, WB6YIY, 4U1ITU, 4X4HT.

**Paul Newman** is at a new QTH which is some 680ft. a.s.l. Antenna at present is an 80ft. end fed and the receiver a modified BC348R ex G3HXS. With this gear, and from his lofty perch at Aylesbury, Paul bagged these on 14MHz; OD5BV, PY6AT, PY8LM, (Sao Luis Island), WA5STY/P/YV5 (Caracas) 4X4BL, 4X4GV, 5Z4KL, 9K2AL.

**Jim Martin** says that as it's the start of his holidays he thought he'd send in a report. (May the sun shine on your antenna, Sir.) His recently-purchased HA500 is nourished with an inverted V and rewards on 14MHz were; CR6EF, CR7IK, EL2CY, FP8CS, HC6CB, JA3IXL, JA4EDY, JA6FUV, JY9XL, KG4AN, KH6FP, KH6BB (Kure Island), KL7DIV, KR6US, KV4AD, KZ5AO, LG5LG, MP4MBC, PY1FN, PJ2MI, PZ1AD, PZ1AW, TG9GF, VK3JS, VP2MO, VQ9R, VS5CB, VS9MT, VU2BEZ, YV5EC, ZE1DO, ZP5GU.

On 3.5MHz c.w. it was UA1YUZ. Up on 7MHz, signals came from CX6CG, LX1BJ, PYCVX, PZ1AX, UW3NG, ZB2A, and ZP5AR. Gear is a JR500SE with 132ft. end fed. Operator's ears belong to **Julian Iredale** (Llandudno), and up on 14MHz s.s.b. Julian heard CR6GA, HV3SJ, OG5A, (Finnish Field Day prefix), PY2ZAC, PY4ATL, PZ1DL, TI2J, 5A4DL.

**P. McKay** advises that he never notices any logs for 7MHz in the Amateur Bands, and sends in a list of G-stations heard on this band. Well, the G's must have been working someone, so how about a listen this month?

*Logs, in alphabetical order please, to arrive by the 15th of the month to:*

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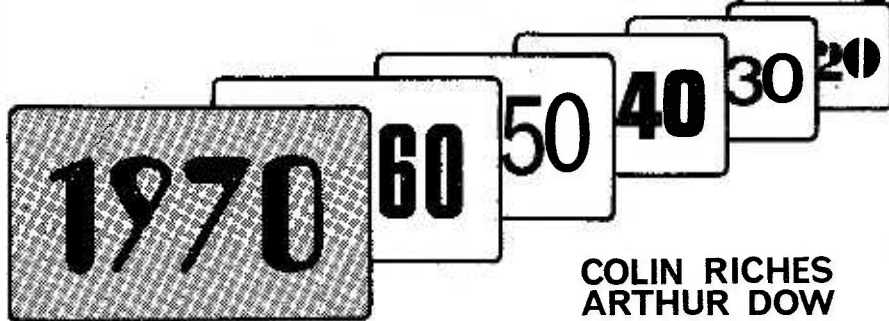
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# GOING BACK...



COLIN RICHES  
ARTHUR DOW



**M**ANY readers have written to ask us if we can suggest any gramophone records that may help them to bring alive even more vividly the days of vintage radio. After a certain amount of research we have discovered that Fountain Press, the book publishers, have now announced a new "Fountain" record label of Vintage Jazz music. The first 12in. LP releases feature historic jazz and blues recordings but future plans include Music Hall, Opera and other music of the "Good Old Days".

The records are housed in attractive double sleeves which open, displaying an authentically documented note section with accurate historical background information and photographs.

The first two releases are: "Original Dixieland Jazz Band and the Louisiana Five"—from the extremely rare Aeolian sessions of 1917 (catalogue number FJ-101). "Ladds Black Aces—Vol. 1"—the first 16 sides recorded by another pioneer white jazz band during 1921-1922 (Cat. No. FJ-102). Following soon are "Naylor's Seven Aces" (c 1923-4). "Jelly Roll Morton" 1923-4 piano solos. "Lovie Austin's Blues Serenaders" (1924-6), and "Annette Hanshawe. Vol. 1"—Miss Hanshawe enjoyed public acclaim as a singer of popular songs in the 1920's and 1930's and her records are great collectors' items today.

These records are available from record shops at £2.10 or direct at £2.25 which includes post and packing, from *Fountain Records, 46 Chancery Lane, London WC2A 1JU.*

If you have any questions or queries on these records or any other Vintage records or performers please write to us at *Practical Wireless* and we'll do our best to help you.

## The Mystery of the ST.200

We would, at this point, like to thank the many enthusiasts who have been kind enough to write and help us try to clear up the mystery of the missing John Scott Taggart design "ST.200" mentioned in "Going Back", August 1971.

One theory put forward by **Mr. F. W. Snow**, Belper, Derby, is that there never was a design called the ST.200 but one called "The ST Twin"—a 2-valve reflex. It was published in *The Wireless Constructor* and not the *Popular Wireless* magazine during the late 1924's and early 1925's.

**Mr. J. Crossley** hailing from Failsworth, Manchester, also maintains that the ST.200 never existed. He

says that J.S.T. visited the United States just after the advent of the ST.100. On his return, he was full of enthusiasm about a gentleman by the name of Armstrong, and *Popular Wireless* published a circuit by this man which J.S.T. had brought back with him. It was the "Armstrong Regenerative Circuit". J.S.T. then went on to publish the ST.300 design, so it appears that Armstrong's receiver may have taken the place of the missing ST.200.

**Mr. A. H. Jenkins**, Dringhouses, York, writes to say that as far as he recollects, the ST.200 may well have been just a mains-operated version of the ST.100 and therefore did not differ operationally from that design. It did however, need an extra valve. Mr. Jenkins also informs us that the S.T. series did not start at ST.100, although this was the most famous. He says that he used to have a limp covered book of J.S.T. circuits which started at crystal sets and worked up through one valvers. He seems to remember an ST.37 which was quite well-known at the time.

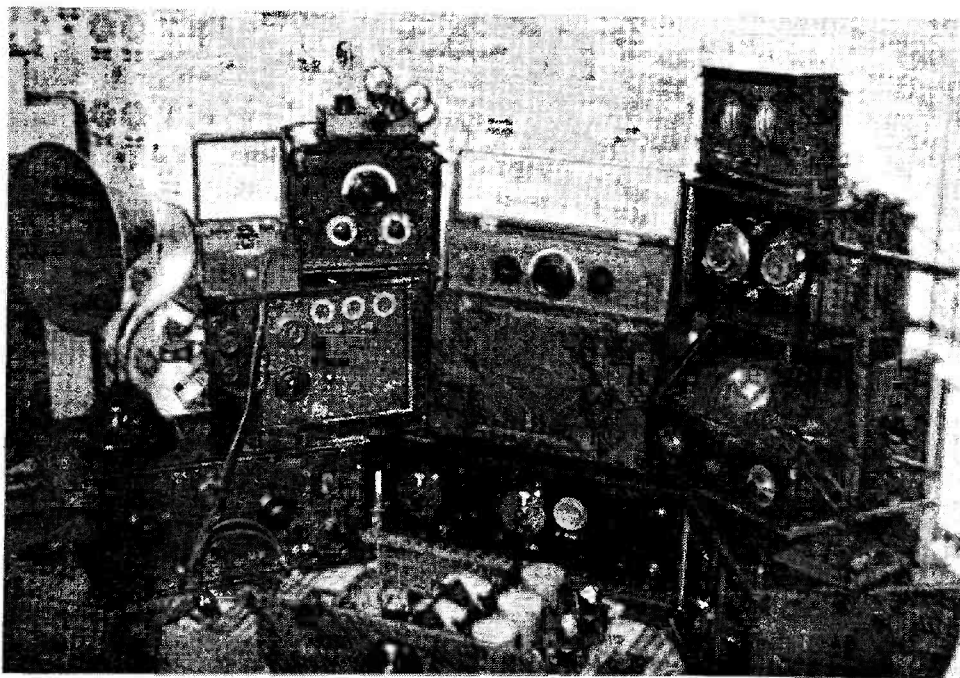
## Vintage Sets

**Mr. William Pozniak**, from 37 Manley Road, Oldham, Lancashire, has loaned us some photographs. He says that for three years he has been routing through old cellars and derelict radio shops throughout the North (we hope you came out for food now and again, Mr. Pozniak) and has produced the collection of Vintage gear shown in the first picture. He says that it takes him most of his time to strip down and restore these sets to as near as possible their original condition. The sets he has are as follows: The Burndept Screened Four, The Burndept Portable Five, the Burndept Ethophone Five and the Burndept Ethophone Two.

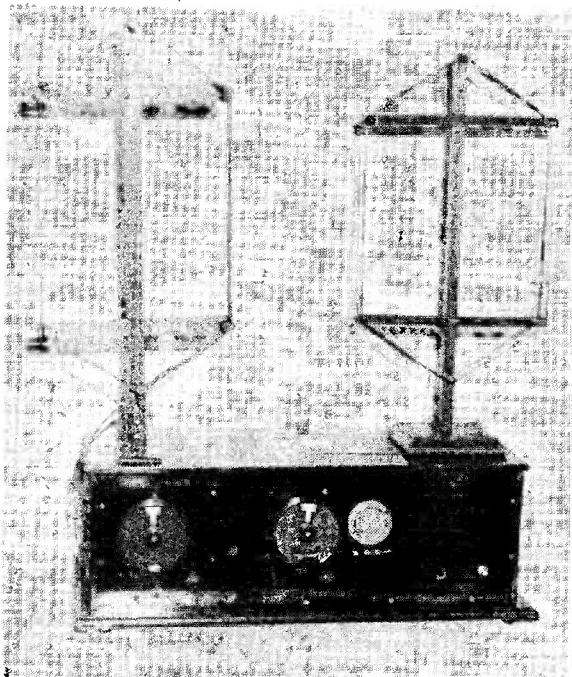
Mr. Pozniak believes there were about 20 Burndept receivers. This figure is agreed by Mr. Keith Lancaster who we mentioned some time ago as wanting to start a Vintage Radio Club. Incidentally, response has not been too good and if readers are interested in such a Club, would they please contact *Keith Lancaster, 40 Great Gardens Road, Hornchurch, Essex.*

The rest of Mr. Pozniak's collection contains a Marconiphone Type 32 three valver, a domestic Cossor two valver, a small set in a metal case named a GECOPHONE Victor 3 and a few home-constructed receivers.

The receiver shown in the second picture is a



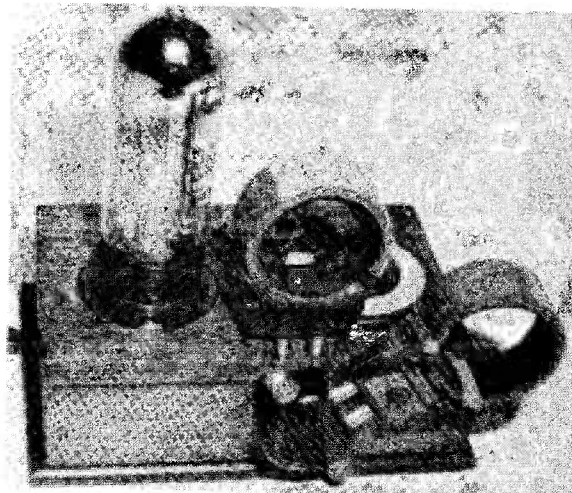
An overall view of Mr. Pozniak's collection of Burndept receivers. The small receiver shown at the top centre of the picture and the set in the centre of the picture together with frame aerials are shown enlarged below.



The James Super Six All Waver (c 1927).

1927 James Super Six All Waver (medium, long and short). The reader says that he purchased this set from an old radio shop which was a booming concern in the 1920's, together with a BTH horn speaker, and the person who sold it to him, told him, as he removed the set from the dusty shelf, that he was the first person to touch the set in 40 years.

The neat little receiver shown in the third photograph seems to Mr. Pozniak to be an unusual type, for he says that there appear to be two resistors and



Louwe receiver with encapsulated components.

two capacitors encapsulated in glass tubes which have then been assembled inside the glass envelope of the valve. The make on the case reads "Louwe Radio Berlin" and on the valve it states "Louwe Radio British Made". This set is in working order on headphones although it was originally made to drive some sort of speaker. The reader would like to know the date and origin of this set if anyone can help him and he would also be interested if anyone could supply him with original Burndept valves for any of their makes of receivers.

#### TITANIC DISASTER

We would like to thank the many readers who have written to us about the Titanic Disaster. We are gradually answering all the letters and we hope you will bear with us.



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A really first-class Hi-Fi Stereo Amplifier Kit. Uses 14 transistors including Silicon Transistors in the first five stages on each channel resulting in even lower noise level with improved sensitivity. Integrated pre-amp with Bass, Treble and two Volume Controls. Suitable for use with Ceramic or Crystal cartridges. Output stage for any speakers from 5 to 15 ohms. Compact design, all parts supplied including drilled metal work, high quality ready drilled printed circuit board, attractive front panel, knobs, wire, solder, nuts, bolts—no extras to buy. Simple step by step instructions enable any constructor to build an amplifier to be proud of. Brief specification; Power output: 14 watts r.m.s. per channel into 5 ohms. Frequency response  $\pm 3\text{dB}$  15-20,000 Hz. Sensitivity: better than 80mV into 1M $\Omega$ . Full power bandwidth:  $\pm 3\text{dB}$  12-15,000 Hz. Bass boost approx. to  $\pm 12\text{dB}$ . Treble cut approx. to -16dB. Negative feedback 18dB over main amp. Power requirements 35v. at 1.0 amp. Overall size 12" w. x 8" d. x 2 1/2" h.

Fully detailed 7 page construction manual and parts list free with kit or send 18p plus large S.A.E.

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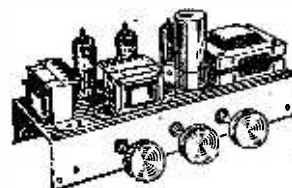
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# WAVE METER

# MONITOR

R. F. GRAHAM

**T**HIS unit has four switch-selected bands, covering from 1600kHz to 100MHz and it can be used as a wavemeter, field strength meter or phone transmission monitor. It is fully enclosed, self-contained, and requires no battery.

Figure 1 shows the circuit. One pole of the switch, S1, selects the inductors L1, L2, L3 or L4, which are tuned by VC1. Pole S2 switches the diode D1 to the appropriate small coupling winding. When the circuit is tuned to resonance by VC1, rectified current is indicated by the meter.

To monitor phone signals, high impedance headphones or earpiece can be plugged into the phone jack and the phones are then in series with the meter. C1 is for r.f. and a.f. by-pass purposes, while C2 is an r.f. by-pass capacitor.

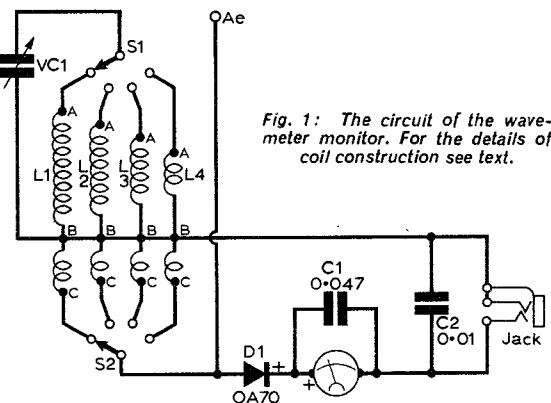
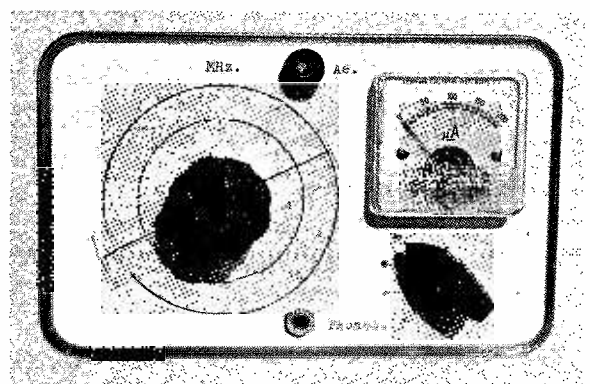


Fig. 1: The circuit of the wave-meter monitor. For the details of coil construction see text.

## INDUCTORS

L1, L2 and L3 are wound on  $\frac{1}{2}$ in. diameter paxolin formers. These can be prepared by cutting  $1\frac{1}{2}$ in. lengths of  $\frac{1}{2}$ in. diameter tube, and drilling small holes to secure the ends of the windings. The tubes can later be fixed with adhesive, with small brackets or by having them a push fit on small discs of insulating material screwed in place. Surplus or junk box formers could probably be utilised, but if these are of different diameter it may be necessary to modify the number of turns to suit.

L1 is wound with 34 s.w.g. enamelled copper wire. The tuned portion A to B is 65 turns, in a compact pile about  $\frac{3}{16}$ in. long. A space of about  $\frac{3}{16}$ in. is left and section B to C is wound on in the same direction, and has 8 turns side by side.

L2 also uses 34 s.w.g. enamelled copper wire. A to B is 50 turns wound side by side. A space is left as before, and a 4 turn coupling winding ends at C.

L3 uses 24 s.w.g. enamelled wire and has  $12\frac{1}{2}$  turns from A to B, and 2 turns from B to C. Figure 2 shows the general construction of L1, L2 and L3.

The windings are doped, smeared with clear *Bostik 1* or with some other suitable coil cement.

L4 is self-supporting, of 16 s.w.g. bare wire, and is shown in Fig. 3. It is wound and shaped to have 8 turns in all and is  $\frac{1}{2}$ in. outside diameter, and 1in. long. B is a tapping 2 turns from end C. This coil is soldered directly to tags A and C of the 4-way switch as shown in Fig. 3. A lead runs from tapping B

## ★ components list

- VC1 200pF Wavemaster variable capacitor.
- C1 0.047F or similar.
- C2 0.01F or similar.
- D1 OA70 or OA71 diode.
- S1 50 3-pole 4-way miniature rotary switch.
- Small closed circuit jack.
- 200uA miniature meter.
- Inductors as text.
- Paxolin or other box about 6 x 3½ x 2½in., aerial socket, knobs etc.

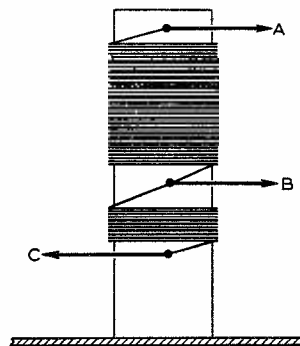


Fig. 2: The general construction of coils L1, L2 and L3 wound on  $\frac{1}{2}$ in. diameter paxolin formers. Details of L4 are given in the text and in Fig. 3.

directly to the moving plates tag of the variable capacitor.

## CONSTRUCTION

The wavemeter was built to occupy a rigid plastic 'snack box' approximately 6in.  $\times$  3 $\frac{1}{2}$ in.  $\times$  2 $\frac{1}{2}$ in. deep. A piece of paxolin sheet, a little under 6in.  $\times$  3 $\frac{1}{2}$ in., was cut to fit inside the box lid. The wavemeter is built wholly on this paxolin panel.

Screws holding L1, L2 and L3 are countersunk. A piece of stout paper to bear dial markings is cut the same size as the paxolin, and cemented to it. The wavemeter is then assembled and calibrated and the scales are marked. The meter and fixing nuts of the switch, jack, and VC1 are then removed and the paxolin panel is fitted inside the box lid. This places the scales under the transparent material of the lid. Paxolin and lid are held together by the meter and the nuts mentioned.

Holes for the jack, switch and VC1 are first drilled in the paxolin and the meter hole cut with an adjustable washer or tank cutter. The paxolin is then placed in the lid, and the positions of holes marked on the lid itself, so that they can be made to match up correctly with those in the paxolin.

The box should be of material which is reasonably strong. It should be drilled and cut with tools which are really sharp, and without forcing, to avoid cracking.

A suitable case could be assembled from  $\frac{1}{4}$ in. thick wood, glued and pinned at the joints. The paxolin panel would then be large enough to be fixed with small wood screws.

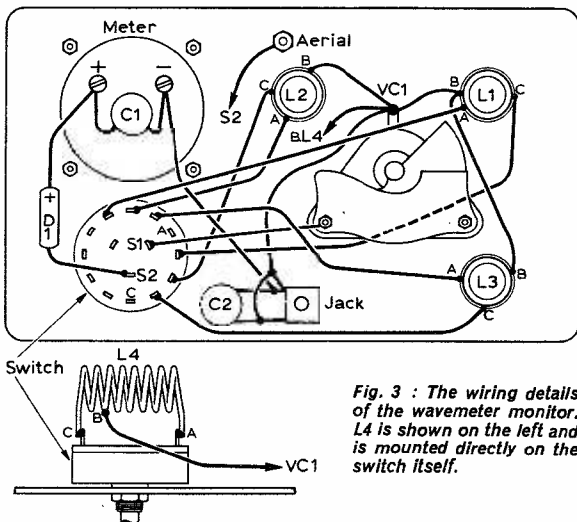
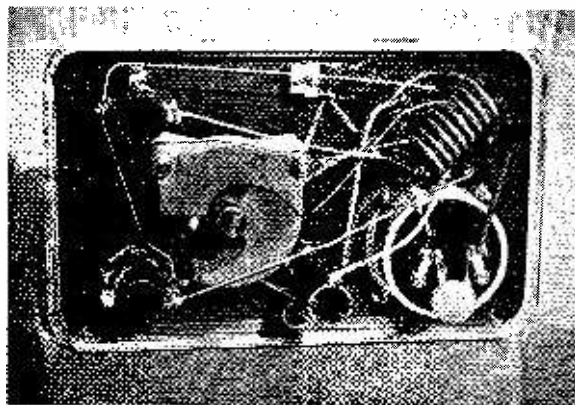


Fig. 3: The wiring details of the wavemeter monitor. L4 is shown on the left and is mounted directly on the switch itself.

All wiring is shown in Fig. 3. Connections should be of stout wire and run clear of each other, and should be reasonably short and direct, especially for L3 and L4.

VC1 is 200pF, but this exact value is not essential, provided that the ranges overlap a little. If an alternative diode is fitted, be sure it is suitable for frequencies up to 100MHz.

A 100 $\mu$ A meter would be a little more sensitive than the one specified, but would also cost a little more. Should a 500 $\mu$ A meter be to hand, it is suitable, though less sensitive. The sensitivity with a 1mA meter becomes rather low so an instrument in the neighbourhood of 200 $\mu$ A is probably most suitable.



An internal view of the completed prototype.

The dial cursor is a 2 $\frac{3}{4}$ in. piece of perspex about  $\frac{5}{8}$ in. wide, marked with a hair line. Readings will be confused if VC1 can rotate through 360°, so the extreme corner of the back moving plate was turned up with pliers to limit rotation to about 180°.

Values used for C1 and C2 are not particularly important. A medium or high impedance pair of headphones will give best general results.

## CALIBRATION

Actual band coverage with the inductors described is as follows

- Range 1 1.6-4MHz
- Range 2 2.8-10MHz
- Range 3 8-32MHz
- Range 4 21-100MHz

This gives 160 and 80m bands in Range 1, 80 and 40m bands in Range 2, all h.f. bands 20-10m in Range 3, and 15-10m bands and harmonics in Range 4, without having to use the extreme h.f. end of the ranges, where readings become close together.

The simplest means of calibration is to use a grid dip oscillator, placing its coil 2in. or so from the appropriate inductor in the wavemeter. This allows complete calibration of all ranges with a minimum of difficulty.

A transmitter can be used for calibration in the amateur bands, and these will probably be of most importance. Place the wavemeter some distance from the transmitter, its dummy load or the aerial lead or tuner, as required to obtain a deflection on the meter.

Some signal generators have an r.f. level meter. If the output of the generator is coupled to the wavemeter by a small loop, a dip may be observed on the level meter when the wavemeter is tuned to resonance. This offers another possible way to secure calibration.

If the wavemeter is coupled to a receiver having a sensitive S-meter, a slight dip in the S-meter reading can be observed when the wavemeter is tuned to the receiver frequency. Input to the receiver can be from a signal generator, or transmission.

All calibration is made with no external connection to the wavemeter and minimum coupling to avoid unnecessary inaccuracy.

## USES

A wavemeter is normally used to indicate frequency bands and harmonics, not exact frequencies within a narrow band. It is placed or held to pick up sufficient r.f. energy from the circuit being investiga-

—continued on page 534

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2G303	20p	2N3414	45p	40312	47p	BCY31	30p	BX261	62p	NKT402	80p
2G304	42p	2N3415	25p	40313	47p	BCY32	30p	BX262	82p	NKT403	75p
2G308	30p	2N3416	37p	40320	47p	BCY33	25p	BX277	25p	NKT405	75p
2G309	30p	2N3417	37p	40323	32p	BCY34	30p	BX278	27p	NKT406	75p
2G371	15p	2N3570	11-25	40324	47p	BCY38	40p	BX280	27p	NKT406	62p
2G374	20p	2N3572	87p	40326	37p	BCY39	60p	BX281	27p	NKT451	62p
2G381	22p	2N3605	27p	40329	37p	BCY40	50p	BX294	15p	NKT452	62p
2G401	20p	2N3622	27p	40342	47p	BCY42	15p	BX295	15p	NKT453	47p
2N696	20p	2N3607	22p	40437	57p	BCY43	15p	BX296	15p	NKT453	47p
2N697	17p	2N3702	11p	40348	52p	BCY64	32p	BX297	17p	NKT700P	32p
2N698	25p	2N3703	10p	40360	42p	BCY68	25p	BX298	17p	NKT767F	30p
2N706	12p	2N3704	11p	40361	47p	BCY69	22p	BX299	17p	NKT767F	30p
2N705A	12p	2N3705	10p	40362	47p	BCY60	97p	BX322	25p	NKT7713	25p
2N708	15p	2N3706	09p	40370	32p	BCY70	20p	BX326	25p	NKT781	30p
2N709	62p	2N3707	11p	40406	37p	BCY72	25p	BX327	25p	NKT10419	30p
2N718	25p	2N3708	07p	40407	40p	BCY79	17p	BX328	25p	NKT10433	37p
2N726	30p	2N3709	09p	40408	52p	BCZ10	27p	BX329	25p		
2N727	30p	2N3710	09p	40410	62p	BCZ11	42p	BX340	32p	NKT10519	
2N914	17p	2N3711	12p	40467A	57p	BD116	11-12p	BSY51	32p		
2N916	17p	2N3715	11-23	40468A	57p	BD121	65p	BSY52	32p	NKT20329	
2N918	30p	2N3716	11-30	40600	57p	BD123	32p	BSY53	37p		
2N921	22p	2N3717	20p	40601	67p	BD107	32p	BSY54	40p	NKT20333	37p
2N930	27p	2N3819	35p	AC126	20p	BD131	75p	BSY56	90p		
2N1090	22p	2N3823	97p	AC127	20p	BD132	85p	BSY78	47p	NKT80111	
2N1091	22p	2N3854	27p	AC128	20p	BDY10	11-37p	BSY79	45p		
2N1131	22p	2N3864A	27p	AC184	22p	BDY11	11-62p	BSY82	62p	NKT80112	
2N1132	22p	2N3856	27p	AC176	25p	BDY17	11-50	BSY90	57p		
2N1302	22p	2N3858A	30p	AC187	62p	BDY18	11-75	BSY95A	12p	NKT80113	
2N1303	17p	2N3856	30p	AC188	37p	BDY19	11-97p	BSY92	42p		
2N1304	22p	2N3856A	35p	ACY17	27p	BDY20	11-121	BW670	27p	NKT80211	
2N1305	22p	2N3858	25p	ACY18	25p	BDY38	97p	C111	75p		
2N1306	25p	2N3858A	30p	ACY19	25p	BDY90	11-25	C424	27p	NKT80212	
2N1307	25p	2N3859	27p	ACY20	25p	BDY61	11-25	C425	55p		
2N1308A	30p	2N3858A	32p	ACY21	25p	BFY82	11-00	C426	40p	NKT80213	
2N1309	30p	2N3860	30p	ACY22	20p	BF115	25p	C428	37p		
2N1507	17p	2N3866	11-50	ACY28	20p	BF117	47p	C744	42p	NKT80214	
2N1613	20p	2N3877	40p	ACY40	20p	BF163	37p	D16P1	37p		
2N1621	35p	2N3877A	40p	ACY41	25p	BF167	18p	D16P2	42p	NKT80215	
2N1632	30p	2N3900	37p	ACY44	40p	BF173	18p	D16P3	37p		
2N1638	27p	2N3901	47p	AD140	53p	BF177	30p	D16T1	47p	NKT80216	
2N1639	27p	2N3901	47p	AD140	53p	BF178	30p	GET102	62p		
2N1671B	11-00	2N3903	35p	AD150	62p	BF179	30p	GET113	20p	OC20	75p
2N1721	25p	2N3904	35p	AD161	37p	BF180	35p	GET114	20p	OC22	50p
2N1889	32p	2N3905	37p	AD162	37p	BF181	32p	GET118	20p	OC23	60p
2N1893	37p	2N3906	37p	AD166	42p	BF184	25p	GET119	20p	OC24	60p
2N1917	22p	2N3905	17p	AF114	45p	BF185	42p	GET120	62p	OC25	50p
2N2148	27p	2N4059	17p	AF115	25p	BF186	42p	GET121	12p	OC26	25p
2N2160	57p	2N4060	17p	AF116	25p	BF195	15p	GET880	30p	OC28	62p
2N2193	40p	2N4061	12p	AF117	25p	BF196	42p	GET887	20p	OC29	62p
2N2193A	42p	2N4062	12p	AF118	62p	BF197	42p	GET889	22p	OC35	50p
2N2194A	30p	2N4244	47p	AF119	20p	BF198	42p	GET890	22p	OC36	62p
2N2217	27p	2N4285	17p	AF124	22p	BF200	32p	GET896	22p	OC41	62p
2N2219	25p	2N4286	12p	AF126	25p	BF202	14p	GET892	22p	OC42	25p
2N2219	25p	2N4287	17p	AF126	20p	BF225	20p	GET898	22p	OC43	22p
2N2220	25p	2N4288	17p	AF127	17p	BF237	28p	MJ400	11-07p	OC45	12p
2N2221	25p	2N4289	17p	AF139	37p	BF238	28p	MJ420	11-12p	OC46	15p
2N2222	30p	2N4290	17p	AF178	42p	BF244	28p	MJ421	11-12p	OC70	15p
2N2270	47p	2N4291	17p	AF179	72p	BFW61	47p	MJ430	11-02p	OC71	12p
2N2297	27p	2N4302	17p	AF180	57p	BFX1	32p	MJ440	35p	OC72	12p
2N2368	17p	2N4303	47p	AF181	42p	BFX13	22p	MJ448	37p	OC73	12p
2N2369	17p	2N4307	52p	AF239	42p	BFX29	30p	MJ481	11-25	OC75	22p
2N2369A	17p	2N5028	57p	AF279	47p	BFX30	30p	MJ490	11-00	OC76	22p
2N2410	42p	2N5029	47p	AF280	62p	BFX42	37p	MJ491	11-37p	OC77	30p
2N2483	27p	2N5030	48p	AF291	32p	BFX44	47p	MJ1800	22-17p	OC81	30p
2N2484	32p	2N5172	12p	ASV26	65p	BFX68	67p	MJE340	62p	OC81D	22p
2N2589	22p	2N5174	52p	ASV27	37p	BFX84	27p	MJE521	27p	OC82	25p
2N2540	42p	2N5175	52p	ASV28	27p	BFX85	32p	MJE521	27p	OC84	25p
2N2613	35p	2N6176	45p	ASV29	27p	BFX86	25p	MPF102	42p	OC139	32p
2N2914	30p	2N6292A	30p	ASV38	25p	BFX87	27p	MPF103	37p	OC140	32p
2N2946	52p	2N6293	45p	ASV39	25p	BFX88	25p	MPF104	37p	OC170	30p
2N2956	32p	2N5246	42p	ASV41	32p	BFY89	62p	MPT105	37p	OC20	30p
2N2711	25p	2N5249	67p	ASV44	25p	MPS5638	32p	OC200	40p		
2N2712	25p	2N5265	11-25	ASV86	32p	BFY10	32p	NKT0013	47p	OC201	60p
2N2713	27p	2N5266	22-75	AU103	11-25	BFY11	42p	NKT1214	47p	OC202	75p
2N2714	30p	2N5267	22-82	ASV21	42p	BFY17	22p	NKT1225	27p	OC203	42p
2N2965	62p	2N5305	37p	BD107	10p	BFY18	22p	NKT1226	27p	OC204	42p
2N2990	30p	2N5306	40p	BC130	19p	BFY19	22p	NKT1227	27p	OC205	60p
2N2904A	32p	2N5307	37p	BC109	10p	BFY20	11-60	NKT135	27p	OC207	75p
2N2905	37p	2N5308	37p	BC113	15p	BFY21	42p	NKT137	32p	OC271	42p
2N2905A	40p	2N5309	62p	BC115	15p	BFY24	45p	NKT210	30p	ORP12	62p
2N2906	25p	2N5310	42p	BC116A	15p	BFY25	25p	NKT211	30p	ORP61	50p
2N2906A	27p	2N5354	27p	BC118	10p	BFY26	20p	NKT212	30p	P346A	22p
2N2907	30p	2N5355	27p	BC121	20p	BFY29	50p	NKT213	30p	TIS84	37p
2N2923	25p	2N5356	32p	BC122	20p	BFY30	50p	NKT214	22p	TIS843	27p
2N2924	25p	2N5365	47p	BC125	20p	BFY41	50p	NKT215	22p	TIS844	10p
2N2925	15p	2N5366	32p	BC126	20p	BFY43	62p	NKT216	37p	TIS845	10p
2N2926	15p	2N5367	37p	BC140	37p	BFV50	28p	NKT217	42p	TIS846	11p
Green	14p	2N5457	37p	BC147	10p	BFV51	30p	NKT219	30p	TIS847	11p
Yellow	12p	2S005	75p	BC148	10p	BFV52	25p	NKT220	27p	TIS848	13p
Orange	12p	2S020	11-00	BC149	12p	BFV53	12p	NKT224	27p	TIS849	13p
2N3011	30p	2S102	60p	BC152	17p	BFV56A	57p	NKT225	22p	TIS850	17p
2N3014	32p	2S103	35p	BC157	30p	BFV75	30p	NKT229	30p	TIS851	12p
2N3053	18p	2S104	25p	BC158	11p	BFV76	42p	NKT237	35p	TIS852	12p
2N3064	40p	2S501	32p	BC169	12p	BFV77	57p	NKT238	25p	TIS853	22p
2N3065	62p	2S502	35p	BC160	62p	BFV78	57p	NKT240	27p	TIS854	22p
2N3133	30p	2S503	37p	BC167	11p	BFW68	27p	NKT2			

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# TAKE 20

JULIAN ANDERSON

A series of simple transistor projects, each using less than twenty components and costing less than one pound to build.

“WHAT’s an automatic light?” you may well ask. Well, lights are only needed when it’s dark, and a very simple electronic switch circuit can be made to turn a small light on as soon as the general light level drops below a certain level; this has its most obvious application in motor cars. Many parts of the country have local regulations requiring cars to display lights shortly after sunset, even when parked. In other areas car parking lights are needed only when the local street lighting is turned off, which in some areas is as late as 2 a.m. There cannot be many people who relish the thought of going out to their cars at that hour to turn on the side or parking lights.

Porch lights which automatically turn themselves on after dusk are another application and although the circuit as shown is not really meant for this, many readers will realise the potential and modify the circuit to operate a thyristor or relay to apply the mains supply to the porch light.

## THE CIRCUIT

Like last month we are making use of a light dependent resistor, that is a resistor whose value in ohms falls with an increase in light falling on it. Also like last month this component is coupled into the base bias potential divider circuit, thus controlling the bias on the transistor, Tr1. R1 may have to be altered in value in order to make the “switch” operate at the correct light level.

As darkness falls, the potential at the base of Tr1 falls as the value of the LDR rises and after a certain point Tr1 begins to turn off, less current is passed and the potential between the emitter and the collector rises. This in turn starts to turn Tr2 on. This transistor, when light was falling on the LDR, thus holding Tr1 on, was off since the potential between base and emitter was held at a very low level due to the small potential across Tr1. As soon as Tr2 begins to conduct this increases the current through R4, thus causing Tr1 to cut off even more and in turn switching Tr2 more on. This action takes place very quickly and Tr2 is switched fully on, applying the supply voltage across the bulb causing it to light up.

This switching circuit is known as the *Schmitt Trigger* and a very useful circuit, it is too, with applications in many fields of electronics. As can be seen, only a few components are required and the switching action, using modern transistors, is very rapid and very positive. As soon as the potential at the base of Tr1 either reaches or falls to a preset level, Tr2 will switch.

The supply necessary to operate the circuit is taken directly from the car battery, though it is good practice to take this via the car’s fuse as any

—continued overleaf

## No. 30 AUTOMATIC LIGHT

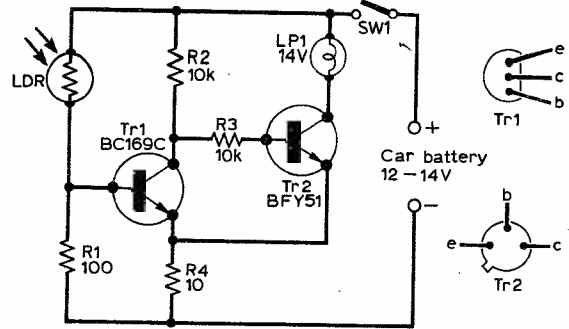


Fig. 1: The circuit of the automatic light with the lead connections of the transistors shown on the right.

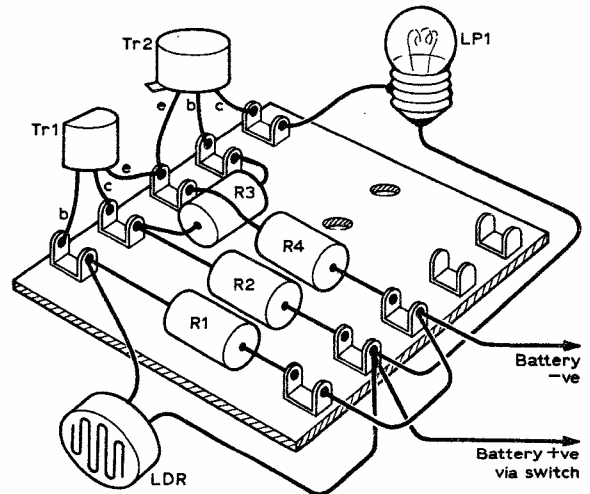


Fig. 2: A suggested component layout on a small piece of tag board.

## ★ components list

Tr1	BC169C	10p
Tr2	BFY51	20p
LDR	Light Dependent Resistor	40p
R1	100Ω 1/2W	10
R2	10kΩ 1/2W	10
R3	10kΩ 1/2W	10
R4	10Ω 1/2W	10
LP1	14V LED Lamp Radiolux type	10
SW1	DPDT toggle switch	10
		25p

† Electronic Ltd.  
 ‡ J. G. (Electronics) Ltd.  
 ††† Radio Shack

The above sources listed are available from most main  
 component stockists. Prices are those currently available  
 and may have changed. No alternative is made for  
 alternative order codes or part numbers and packing  
 charges should be checked before ordering.

mistakes or serious component failure could create a fire risk.

Car batteries are capable of giving very high currents and therefore the quiescent current is of no great importance but it is in fact low, in the order of 2mA. The recommended bulb draws 40mA and it can be seen that these currents can be supplied by a number of dry batteries, though operation in this manner will not be cheap.

The bulb should last a considerable time as it is being slightly under-run; there is of course a small volts drop across R4 and Tr2.

## CONSTRUCTION

A suggested layout is shown in Fig. 2 but this is not critical. One point must be watched however; if the light from the bulb is allowed to fall onto the LDR it will switch the circuit in the same way that sunlight will. This will cause the circuit to oscillate; this can easily be seen as the bulb will flicker or flash. To avoid this the LDR must be pointed away from the bulb. ■

## WAVEMETER MONITOR—by R. F. GRAHAM

continued from page 530

ted. Tuning resonance is shown by maximum meter reading. In driver and similar circuits with small power, the wavemeter needs to be reasonably close to the circuit inductor. For P.A. and high power circuits, it can be at some small distance.

To check the frequency of low level multipliers and similar circuits, or those which are inaccessible, a link line may be used. This is twin flex or co-axial cable about 2ft. long with a loop of two or three turns each end. One loop is held near the equipment inductor, and the other near the wavemeter inductor. Clipping a lead to jack and aerial socket also allows the coil primaries to be used for coupling. Resonance will be shown by a dip in grid current in a subsequent stage.

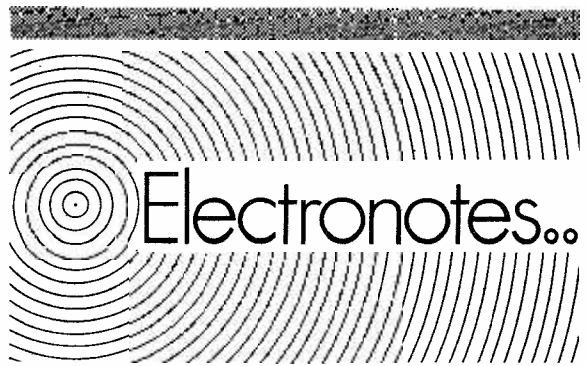
To monitor the audio of an outgoing transmission, plug in phones, tune to resonance and situate the unit where pick-up gives adequate volume.

To tune an aerial, transmitter, tuner or coupling device for maximum radiation from the aerial, a vertical rod or wire is plugged into the aerial socket of the unit, which should be at some distance. Adjustments are then for maximum meter reading, which corresponds to maximum field strength. It is also possible to link couple a dipole or aerial-earth system to the wavemeter for this purpose, or take a short aerial to VC1, ignoring calibration.

The wavemeter produces no signal. It can be used to find bands on a t.r.f. receiver by adjusting the latter until oscillation just arises, and holding the wavemeter coil in line with the receiver coil. Resonance when tuning the wavemeter is then shown by the receiver going out of oscillation. ■

### BLUEPRINT SERVICE

We would like to draw readers' attention to the fact that the BLUEPRINT SERVICE has been discontinued and therefore no further BLUEPRINTS are available.



## S. GINSBERG

**I**N the beginning there were photocells enclosed in glass envelopes. Variations of these were more sensitive and multi-electrode secondary emission cells appeared like the 931A photomultiplier tube.

In more recent years, many experimenters, and indeed, most of the electronics industry too, has opted for solid state when thinking in terms of a light sensing device. An example here is the ORP12 light-dependent resistor, not to mention the earlier plastic-encapsulated transistors with some of their paint removed!

In America, work is currently proceeding on a technique known as charge coupling for imaging devices. One oxidised surface of a tiny silicon chip is covered with some 288 minute electrodes. These are arranged into groups of three, the last electrode in each group being a common conductor for the whole array.

The area immediately beneath each group of three elements forms a tiny light sensitive device in its own right. Minority carriers are generated in the silicon beneath the electrodes whenever light is focussed onto them. The greater the intensity of the light, the greater the charge, thus forming a direct relationship between light intensity and electrical charge.

The centre electrode of each group is purposely made more positive than the other two elements and thus the charges on minority carriers are attracted to, and congregate at, these centre electrodes.

Individual charges are next moved along the array from one electrode group to the next by putting a successively greater positive voltage on the electrode next to the one which is holding the charge. Eventually all the charges will have been passed along to the end of the device where they are collected by an output electrode.

Because the size of the charge will be dependent upon the amount of original light applied, the final electrode has, in effect, an analogue electrical signal which has a linear relationship to original light patterns of intensity.

How big is a 100,000 $\mu$ F capacitor—think of the size of some electrolytics. Now imagine how big a one Farad capacitor would be. Just to stretch the imagination even further, think of a 50 Farad capacitor. Fantastic—but they exist and are for sale. Twist in the tale is that the 50F is contained within one-third of a cubic inch. The devices will also retain their storage (if charged with a voltage) and leakage is so low that even after 16 months they will have retained over 97 per cent of the original charge. Think; they could be charged up and used as a form of battery. When discharged, they could simply be recharged again ad infinitum.



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#### Type MR.55P. 4 1/2 in. x 4 1/2 in. fronts.



50mA ..... \$2.60	100mA ..... \$2.60	500mA ..... \$2.60	1 amp. .... \$2.60	5 amp. .... \$2.60	15 amp. .... \$2.60	30 amp. .... \$2.60	20V. D.C. .... \$2.60	50V. D.C. .... \$2.60	150V. D.C. .... \$2.60	300V. D.C. .... \$2.60	15V. A.C. .... \$2.60	300V. A.C. .... \$2.60	8 Meter 1mA ..... \$2.60	5 Meter 1mA ..... \$2.60	1 amp. A.C. .... \$2.60	5 amp. A.C. .... \$2.60	10 amp. A.C. .... \$2.60	20 amp. A.C. .... \$2.60	30 amp. A.C. .... \$2.60
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#### Type MR.55P. 1 21/32 in. square fronts.



50μA ..... \$2.60	100-500μA ..... \$1.87	500μA ..... \$1.87	100-100μA ..... \$1.75	200μA ..... \$1.75	500μA ..... \$1.60	500-500μA ..... \$1.87	1mA ..... \$1.87	1-0-1mA ..... \$1.87	2mA ..... \$1.87	5mA ..... \$1.87	10mA ..... \$1.87	20mA ..... \$1.87	50mA ..... \$1.87	100mA ..... \$1.87	150mA ..... \$1.87	5 amp. .... \$1.50	10V. D.C. .... \$1.50	50V. D.C. .... \$1.50	100-100μA ..... \$1.87	200μA ..... \$1.60	500μA ..... \$1.60	500-500μA ..... \$1.87	1mA ..... \$1.50	10mA ..... \$1.50	100mA ..... \$1.50	500mA ..... \$1.50	1 amp. .... \$1.50
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### "SEW" BAKELITE PANEL METERS

#### Type MR.55P. 3 1/2 in. x 3 1/2 in. fronts.



50μA ..... \$3.37	50-50μA ..... \$2.75	100μA ..... \$2.60	100-100μA ..... \$2.37	200μA ..... \$2.60	500μA ..... \$2.97	500-500μA ..... \$2.10	1mA ..... \$2.10	5mA ..... \$2.10	10mA ..... \$2.10	50mA ..... \$2.10	100mA ..... \$2.10	500mA ..... \$2.10	1 amp. .... \$2.10	10V. D.C. .... \$2.10	20V. D.C. .... \$2.10	50V. D.C. .... \$2.10	150V. D.C. .... \$2.10	300V. D.C. .... \$2.10	15V. A.C. .... \$2.10	300V. A.C. .... \$2.10	8 Meter 1mA ..... \$2.10	5 Meter 1mA ..... \$2.10	1 amp. A.C. .... \$2.10	5 amp. A.C. .... \$2.10	10 amp. A.C. .... \$2.10	20 amp. A.C. .... \$2.10	30 amp. A.C. .... \$2.10	5V. D.C. .... \$2.10
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#### Type MR.55P. 2 1/2 in. square fronts.



50μA ..... \$2.25	50-50μA ..... \$2.10	100μA ..... \$2.10	100-100μA ..... \$1.87	200μA ..... \$1.60	500μA ..... \$1.60	500-500μA ..... \$1.50	1mA ..... \$1.50	10mA ..... \$1.50	50mA ..... \$1.50	100mA ..... \$1.50	500mA ..... \$1.50	1 amp. .... \$1.50	5 amp. .... \$1.50	10V. D.C. .... \$1.50	50V. D.C. .... \$1.50	100-100μA ..... \$1.87	200μA ..... \$1.60	500μA ..... \$1.60	500-500μA ..... \$1.50	1mA ..... \$1.50	10mA ..... \$1.50	50mA ..... \$1.50	100mA ..... \$1.50	500mA ..... \$1.50	1 amp. .... \$1.50
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50-0-50μA ..... \$4.25	
1-0-1mA ..... \$3.97	
1A d.c. .... \$3.97	500mA/5A d.c. \$4.25
5A d.c. .... \$3.97	5V/50V d.c. .... \$4.25
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2N3415	2N3417	2N3418	2N3419	2N3420	2N3421	2N3422	2N3423	2N3424	2N3425	2N3426	2N3427	2N3428	2N3429	2N3430	2N3431	2N3432	2N3433	2N3434	2N3435	2N3436	2N3437	2N3438	2N3439	2N3440	2N3441	2N3442	2N3443	2N3444	2N3445	2N3446	2N3447	2N3448	2N3449	2N3450	2N3451	2N3452	2N3453	2N3454	2N3455	2N3456	2N3457	2N3458	2N3459	2N3460	2N3461	2N3462	2N3463	2N3464	2N3465	2N3466	2N3467	2N3468	2N3469	2N3470	2N3471	2N3472	2N3473	2N3474	2N3475	2N3476	2N3477	2N3478	2N3479	2N3480	2N3481	2N3482	2N3483	2N3484	2N3485	2N3486	2N3487	2N3488	2N3489	2N3490	2N3491	2N3492	2N3493	2N3494	2N3495	2N3496	2N3497	2N3498	2N3499	2N3500	2N3501	2N3502	2N3503	2N3504	2N3505	2N3506	2N3507	2N3508	2N3509	2N3510	2N3511	2N3512	2N3513	2N3514	2N3515	2N3516	2N3517	2N3518	2N3519	2N3520	2N3521	2N3522	2N3523	2N3524	2N3525	2N3526	2N3527	2N3528	2N3529	2N3530	2N3531	2N3532	2N3533	2N3534	2N3535	2N3536	2N3537	2N3538	2N3539	2N3540	2N3541	2N3542	2N3543	2N3544	2N3545	2N3546	2N3547	2N3548	2N3549	2N3550	

Integrated Circuits	FJH101	FJH111	FJH121	FJH131	FJH141	FJH151	FJH161	FJH171	FJH181	FJH191	FJH201	FJH211	FJH221	FJH231	FJH241	FJH251	FJH261	FJH271	FJH281	FJH291	FJH301	FJH311	FJH321	FJH331	FJH341	FJH351	FJH361	FJH371	FJH381	FJH391	FJH401	FJH411	FJH421	FJH431	FJH441	FJH451	FJH461	FJH471	FJH481	FJH491	FJH501	FJH511	FJH521	FJH531	FJH541	FJH551	FJH561	FJH571	FJH581	FJH591	FJH601	FJH611	FJH621	FJH631	FJH641	FJH651	FJH661	FJH671	FJH681	FJH691	FJH701	FJH711	FJH721	FJH731	FJH741	FJH751	FJH761	FJH771	FJH781	FJH791	FJH801	FJH811	FJH821	FJH831	FJH841	FJH851	FJH861	FJH871	FJH881	FJH891	FJH901	FJH911	FJH921	FJH931	FJH941	FJH951	FJH961	FJH971	FJH981	FJH991	FJH1001
FJH101	FJH111	FJH121	FJH131	FJH141	FJH151	FJH161	FJH171	FJH181	FJH191	FJH201	FJH211	FJH221	FJH231	FJH241	FJH251	FJH261	FJH271	FJH281	FJH291	FJH301	FJH311	FJH321	FJH331	FJH341	FJH351	FJH361	FJH371	FJH381	FJH391	FJH401	FJH411	FJH421	FJH431	FJH441	FJH451	FJH461	FJH471	FJH481	FJH491	FJH501	FJH511	FJH521	FJH531	FJH541	FJH551	FJH561	FJH571	FJH581	FJH591	FJH601	FJH611	FJH621	FJH631	FJH641	FJH651	FJH661	FJH671	FJH681	FJH691	FJH701	FJH711	FJH721	FJH731	FJH741	FJH751	FJH761	FJH771	FJH781	FJH791	FJH801	FJH811	FJH821	FJH831	FJH841	FJH851	FJH861	FJH871	FJH881	FJH891	FJH901	FJH911	FJH921	FJH931	FJH941	FJH951	FJH961	FJH971	FJH981	FJH991	FJH1001	

### VALVES

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6X4	6X5	6X6	6X7	6X8	6X9	6X10	6X11	6X12	6X13	6X14	6X15	6X16	6X17	6X18	6X19	6X20	6X21	6X22	6X23	6X24	6X25	6X26	6X27	6X28	6X29	6X30	6X31	6X32	6X33	6X34	6X35	6X36	6X37	6X38	6X39	6X40	6X41	6X42	6X43	6X44	6X45	6X46	6X47	6X48	6X49	6X50	6X51	6X52	6X53	6X54	6X55	6X56	6X57	6X58	6X59	6X60	6X61	6X62	6X63	6X64	6X65	6X66	6X67	6X68	6X69	6X70	6X71	6X72	6X73	6X74	6X75	6X76	6X77	6X78	6X79	6X80	6X81	6X82	6X83	6X84	6X85	6X86	6X87	6X88	6X89	6X90	6X91	6X92	6X93	6X94	6X95	6X96	6X97	6X98	6X99	6X100	

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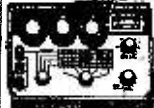
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IA7GT	.33	6CW4	.63	7B7	.38	20P4	.89	ATP4	.12	ECC83	.22	EM83	.75	PC86	.48	PL508	.90	UP80	.35	AC128	.20	BF163	.20	OA85	.08
IB3GT	.37	6DE7	.50	7BT	.35	20P6	1.00	AZ1	.40	ECC84	.28	EM84	.81	PC88	.48	PL509	1.30	UP85	.34	AC156	.20	BF173	.38	OA90	.13
IF5GT	.36	6DT6	.60	7C6	.60	25A6G	.29	AZ21	.40	ECC85	.25	EM87	.35	PC89	.45	PL512	.75	UP86	.63	AC157	.25	BF180	.30	OA91	.09
II4	.15	6EW6	.65	7HT	.23	25L8G	.22	AZ41	.58	ECC86	.40	EY61	.38	PCF20	.28	PL515	1.16	UP87	.54	AC166	.25	BF181	.40	OA95	.09
IN3GT	.37	6F1	.59	7RT	.45	25Y5	.35	CL33	.90	ECC88	.45	EY81	.35	PCF22	.30	PL518	.50	UM80	.33	AC177	.28	BFY50	.38	OC22	.38
IR5	.27	6F6	.63	7Z4	.50	25Y5G	.43	CY1C	.63	ECC189	.48	EY83	.55	PCF24	.40	PL520	.75	UY21	.55	ACY18	.20	BFY52	.20	OC24	.88
184	.22	6F6G	.65	9D7	.78	25Z4G	.30	CY31	.81	ECC804	.55	EY84	.50	PCF28	.44	PL522	.75	UY41	.38	ACY19	.19	BY100	.18	OC25	.38
1U4	.29	6F13	.33	10C1	1.25	25Z5	.40	DAF91	.20	ECC807L	.70	EY87/6	.30	PCF30	.28	PL523	.75	UY51	.25	ACY20	.18	BY105	.18	OC26	.24
1U5	.48	6F14	.43	10C2	.50	25Z6G	.43	DAF96	.33	ECC808	.27	EY88	.43	PCF32	.30	PL524	.75	UY61	.45	ACY21	.19	BY114	.18	OC28	.60
2D21	.35	6F18	.45	10D17	.50	30C1	.28	DF91	.14	ECC828	.27	EY91	.53	PCF34	.40	PL525	.75	UY71	.45	ACY22	.19	BY126	.15	OC29	.63
3D6	.19	6F22	.68	10F9	.45	30C15	.60	DF95	.33	ECC866	.65	EZ40	.40	PCF36	.44	PL526	.75	UY81	.45	ACY23	.19	BY137	.18	OC35	.32
3Q4	.38	6F24	.68	10F18	.35	30C17	.77	DF97	.63	ECC8042	.10	EZ41	.43	PCF38	.68	PL527	.75	UY91	.68	ACY24	.20	CG12E	.20	OC36	.43
3Q5GT	.35	6F25	.68	10LD11	.53	30C18	.60	DI76	.68	EZ20	.21	EZ21	.22	PCF40	.67	PL528	.75	UY92	.68	ACY25	.20	CG12E	.20	OC37	.27
384	.27	6F28	.70	10P13	.54	30F5	.70	DK40	.55	ECH42	.61	EZ21	.22	PCF42	.44	PL529	.75	UY93	.68	ACY26	.20	CG12E	.20	OC38	.43
3V4	.32	6F28	.70	10P13	.54	30F5	.70	DK40	.55	ECH42	.61	EZ21	.22	PCF42	.44	PL529	.75	UY93	.68	ACY26	.20	CG12E	.20	OC38	.43
5V4G	.35	6GH8A	.15	10P14	1.10	30F1L	.60	DK92	.38	ECH81	.27	EZ20	.20	PCF44	.33	PL530	1.98	UY94	.68	ACY27	.20	CG12E	.20	OC39	.63
5V4G	.35	6GH8A	.15	10P14	1.10	30F1L	.60	DK92	.38	ECH81	.27	EZ20	.20	PCF44	.33	PL530	1.98	UY94	.68	ACY27	.20	CG12E	.20	OC39	.63
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# new

## Super IC-12



### High fidelity Monolithic Integrated Circuit Amplifier

Two years ago Sinclair Radionics announced the World's first monolithic integrated circuit Hi-Fi amplifier, the IC.10. Now we are delighted to be able to introduce its successor, the Super IC.12. This 22 transistor unit has all the virtues of the original IC.10 plus the following advantages:

1. Higher power.
2. Fewer external components.
3. Lower quiescent consumption.
4. Compatible with Project 60 modules.
5. Specially designed built-in heat sink. No other heat sink needed.
6. Full output into 3, 4, 5 or 8 ohms.
7. Works on any voltage from 6 to 28 volts without adjustment.
8. NEW 22 transistor circuit.

#### SINCLAIR GENERAL GUARANTEE

Should you not be completely satisfied with your purchase when you receive it from us, return the goods without delay and your money will be refunded in full, including cost of return postage, at once and without question. Full service facilities are available to all Sinclair customers.

**Output power** 6 watts RMS continuous (12 watts peak).

**Frequency Response** 5 Hz to 100KHz  $\pm$  1 dB.

**Total Harmonic Distortion** Less than 1%. (Typical 0.1%) at all output powers and all frequencies in the audio band.

**Load Impedance** 3 to 15 ohms.

**Power Gain** 90dB (1,000,000,000 times) after feedback.

**Supply Voltage** 6 to 28 volts (Sinclair PZ-5 or PZ-6 power supplies ideal).

**Size** 22 x 45 x 28 mm including pins and heat sink.

**Input Impedance** 250 Kohms nominal.

**Quiescent current** 8mA at 28 volts.

With the addition of only a very few external resistors and capacitors the Super IC.12 makes a complete high fidelity audio amplifier suitable for use with pick-up, F.M. tuner etc. Alternatively, for more elaborate systems, modules in the Project-60 range such as the Stereo 60 and A.F.U. may be added. The comprehensive manual supplied with each unit gives full circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include car radios, oscillators etc. The very low quiescent consumption makes the Super IC.12 ideal for battery operation.



Price, inc. FREE printed circuit board for mounting.

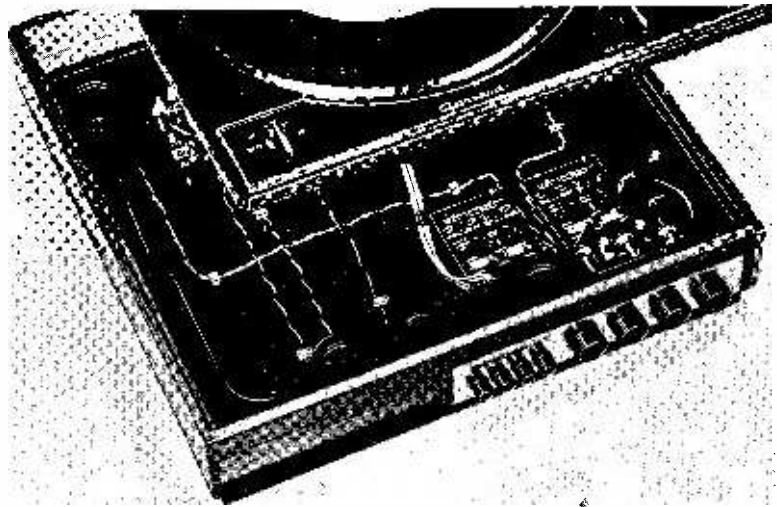
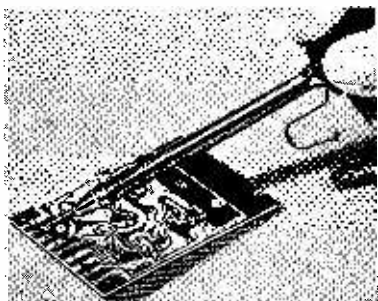
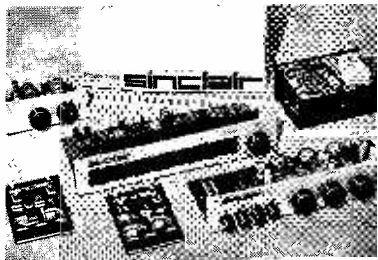
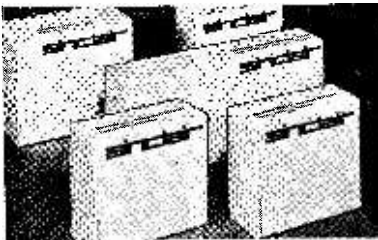
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## sinclair

# Sinclair Project 60

The World's leading range of high fidelity modules



Project 60 offers more advantage to the constructor and user of high fidelity equipment than any other system in the world.

Performance characteristics are so good they hold their own with any other available system irrespective of price or size.

Project 60 modules are more versatile – using them you can have anything from a simple record player or car radio amplifier to a sophisticated and powerful stereo tuner-amplifier. Either power amplifier can be used in a wide variety of applications as well as high fidelity. The Stereo 60 pre-amplifier control unit may also be used with any other power amplifier system, as can the AFU filter unit. The stereo FM tuner operates on the unique phase lock loop principle to provide the best ever standards of sensitivity and audio quality. Project 60 modules are very easily connected together by following the 48 page manual supplied free with all Project 60 equipment. The modules are great space savers too and are sold individually boxed in distinctive white and black cartons. With all these wonderful advantages, there remains the most attractive of all – price. When you choose Project 60 you know you are going to get the best high fidelity in the world, yet thanks to Sinclair's vast manufacturing resources (the largest in Europe) prices are fantastically low and everything you buy is covered by the famous Sinclair guarantee of reliability and satisfaction.

#### Typical Project 60 applications

System	The Units to use	together with	Cost of Units
Simple battery record player	<b>Z.30</b>	Crystal P.U., 12V battery volume control	<b>£4.48</b>
Mains powered record player	<b>Z.30, PZ.5</b>	Crystal or ceramic P.U. volume control etc.	<b>£9.45</b>
20 + 20 W. stereo amplifier for most needs	<b>2 x Z.30s, Stereo 60, PZ.5</b>	Crystal, ceramic or mag. P.U., F.M. Tuner, etc.	<b>£23.90</b>
20 + 20 W. stereo amplifier with high performance spkrs.	<b>2 x Z.30s, Stereo 60, PZ.6</b>	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc.	<b>£26.90</b>
40 + 40 W. R.M.S. de-luxe stereo amplifier	<b>2 x Z.50s, Stereo 60 PZ.8, mains trsfmr</b>	As above	<b>£34.88</b>
Indoor P.A.	<b>Z.50, PZ.8, mains transformer</b>	Mic., guitar, speakers, etc., controls	<b>£19.43</b>

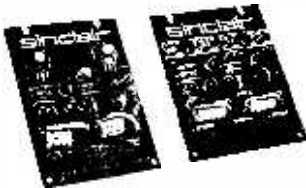
F.M. Stereo Tuner (**£25**) & A.F.U. Filter Unit (**£5.98**) may be added as required.

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**sinclair**

# from a simple amplifier to a complete stereo tuner amplifier with Project 60 modules

## Z.30 & Z.50 power amplifiers



The Z.30 and Z.50 are of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at full output and all lower outputs. Whether you use Z.30 or Z.50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and may be used with other units in the Project 60 range equally well.

**SPECIFICATIONS (Z.50 units are interchangeable with Z.30s in all applications).**

### Power Outputs

**Z.30** 15 watts R.M.S. into 8 ohms using 35 volts; 20 watts R.M.S. into 3 ohms using 30 volts.

**Z.50** 40 watts R.M.S. into 3 ohms using 40 volts; 30 watts R.M.S. into 8 ohms using 50 volts.

**Frequency response:** 30 to 300,000Hz  $\pm 1$  dB.

**Distortion:** 0.02% into 8 ohms.

**Signal to noise ratio:** better than 70dB unweighted.

**Input sensitivity:** 250mV into 100 Kohms.

For speakers from 3 to 15 ohms impedance.

**Size:** 14 x 80 x 57 mm.

### Z.30

Built, tested and guaranteed with circuits and instructions manual. **£4.48**

### Z.50

Built, tested and guaranteed with circuits and instructions manual. **£5.48**

## Power Supply Units

Designed special for use with the Project 60 system of your choice. Use PZ.5 for normal Z.30 assemblies and PZ.6 where a stabilised supply is essential.

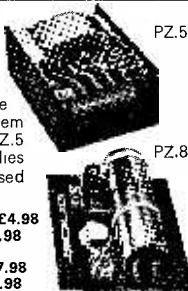
**PZ.5** 30 volts un stabilised **£4.98**

**PZ.6** 35 volts stabilised **£7.98**

**PZ.8** 45 volts stabilised

(less mains transformer) **£7.98**

**PZ.8** mains transformer **£5.98**



## Project 60 Stereo F.M. Tuner



*First in the world to use the phase lock loop principle*

The phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio. Now, Sinclair have applied the principle to an F.M. tuner with fantastically good results. Other original features include varicap diode tuning, printed circuit coils, an I.C. in the specially designed stereo decoder and squelch circuit for silent tuning between stations. Good reception is possible in difficult areas, and often a few inches of wire are enough for an aerial. In terms of a high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically as the tuning control is rotated, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with any other high fidelity system.

**SPECIFICATIONS—Number of transistors:** 16 plus 20 in I.C. **Tuning range:** 87.5 to 108 MHz. **Capture ratio:** 1.5dB. **Sensitivity:** 2 $\mu$ V for 30dB quieting; 7 $\mu$ V for full limiting. **Squelch level:** 20 $\mu$ V. **A.F.C. range:**  $\pm 200$  KHz. **Signal to noise ratio:** > 65dB. **Audio frequency response:** 10 Hz – 15 KHz ( $\pm 1$ dB). **Total harmonic distortion:** 0.15% for 30% modulation. **Stereo decoder operating level:** 2 $\mu$ V. **Cross talk:** 40dB. **Output voltage:** 2 x 150mV R.M.S. **Operating voltage:** 25-30 VDC. **Indicators:** Mains on; Stereo on; tuning. **Size:** 93 x 40 x 207 mm.

Built and tested. Post free.

**£25**

## Stereo 60 Pre-amp/control unit



Designed for Project 60 range but suitable for use with any high quality power amplifier. Again silicon epitaxial planar transistors are used throughout, achieving a really high signal-to-noise ratio and excellent tracking between channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs.

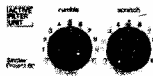
**SPECIFICATIONS—Input sensitivities:** Radio—up to 3mV. Mag. p.u. 3mV; correct to R.I.A.A. curve  $\pm 1$ dB; 20 to 25,000 Hz. Ceramic p.u.—up to 3mV; A.U.—up to 3mV. **Output:** 250mV. **Signal to noise ratio:** better than 70dB. **Channel matching:** within 1dB. **Tone controls:** TREBLE +15 to -15dB at 10 KHz; BASS +15 to -15dB at 100Hz.

**Front panel:** brushed aluminium with black knobs and controls. **Size:** 66 x 40 x 207mm.

Built, tested and guaranteed.

**£9.98**

## A.F.U. High & Low Pass Filter Unit



For use between Stereo 60 unit and two Z.30s or Z.50s, and is easily mounted. It is unique in that the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid (12dB/octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is suitable for use with any other amplifier system. Two filter stages—rumble (high pass) and scratch (low pass). Supply voltage—15 to 35V. Current—3mA. H.F. cut-off (-3dB) variable from 28KHz to 5KHz. L.F. cut-off (-3dB) variable from 25Hz to 100Hz. Distortion at 1KHz (35V. supply) (0.02% at rated output. **Size:** 66 x 40 x 90 mm.

Built tested and guaranteed.

**£5.98**

## The Sinclair Guarantee

If within 3 months of purchasing Project 60 modules directly from us, you are dissatisfied with them, we will refund your money at once. Each module is guaranteed to work perfectly and should any defect arise in normal use we will service it at once and without any cost to you whatsoever provided that it is returned to us within 2 years of the purchase date. There will be a small charge for service thereafter. No charge for postage by surface mail. Air-mail charged at cost.

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IR5	35	6BW6	85	6K8M	60	10C2	35	25A6	35	80	DH3-91	£6-00	ECH21	63	EM84	38	PC884	40	Y82	30		
IS4	27	6BW7	70	6K8G	35	10F1	90	25L6GT	45	85A2	40	DH77	30	ECH35	60	EY51	40	PC899	53	Y83	38	
IS5	25	6C4	33	6K8GT	50	10F3	90	25Y5	60	160B2	60	DK32	40	ECH42	70	EY86	40	PC189	55	Y800	£1-00	
IT4	25	6C5G	30	6K25	75	10F9	50	25Z4	45	10C4	60	DK91	50	DF1	25	EC834	30	PC89	38	Y800	£1-00	
IA4	35	6C5	50	6L6C	45	10F18	50	25Z6GT	55	801	50	DK92	50	ECC83	43	EZ40	45	PCF82	35	Y801	50	
3Q4	40	6CD6G	£1-20	6L18	45	10LD11	60	25Z6	65	807	50	DK96	42	ECL80	40	EZ41	48	PCF84	50	R2	60	
8Q5	45	6CH6	55	6Q7G	30	10P13	68	30C1	33	813USA	£3-75	DL66	£1-25	ECL82	65	EZ80	28	PCF86	60	R19	40	
3S4	35	6CW4	63	6Q7GT	43	11E3	£4-00	30C15	80	866A	75	DL92	35	ECL83	65	EZ81	28	PCF81	50	S130	£1-75	
3V4	45	6D6	25	68A7M	40	12A7E	30	30C17	35	954	60	DL93	35	ECL86	45	GY501	80	PCF802	50	SP4	50	
5R4GY	60	6E2	38	68CTM	70	12A77	30	30C18	78	1025	40	DL94	45	ECL800	40	EZ82	£1-50	PCF806	70	SP41	45	
5V4G	42	6F5G	50	68HTM	35	12A7U	30	30F1L	75	5763	70	DL96	48	EF9	£1-00	GZ34	60	PCF808	78	STV280/50	UM80	
5Y3GT	38	6F6G	30	68J7GT	30	12A7X	30	30F1L2	95	7193	20	DM70	40	EF37A	60	HN309	£1-50	PCF82	38	U10	£10-00	
5Z4G	40	6F8G	35	68K7GT	30	12BA6	35	30F1L4	75	7475	40	DY86	33	EF39	40	K736	£1-00	PCF83	58	SU25	£1-00	
6/30L2	75	6F11	38	68L7GT	35	12BE6	35	30L15	85	A61	48	DY87	35	EF41	65	K761	£1-25	PCF84	48	UT2160	75	
6A7	75	6F13	38	68N7GT	35	12C9GT	35	30L17	85	ATP4	35	EB8CC	65	EF50	25	K766	£1-70	PCF85	40	T41	£1-00	
6A8G	63	6F14	65	68Q7GT	40	12E1	£1-35	30P4	£1-12	ATP5	60	EAS0	28	EF80	25	K781	£1-75	PCF86	45	TD4	50	
6AK5	30	6F23	80	6T4GT	60	12J5GT	30	ATP7	80	EABCS0	50	EAF85	35	EF88	35	K781(7C5)	PD500	£1-50	TH41	£1-75	UY41	45
6AM5	32	6F25	75	6V6M	60	12J7GT	35	30P19	80	AU2	£4-00	BAF42	55	EF86	33	£1-13	PEN4A	£1-00	U10	60	UY85	33
6AM6	33	6F28	70	6V6G	30	12K8GT	50	30P1L3	93	AZ1	48	EBB33	50	EF91	33	KTW61	£1-00	PEN45	40	U19	£2-50	
6AQ5	35	6F32	25	6V6GT	30	12Q7GT	35	30P1L4	90	AZ31	55	EBB41	55	EF92	40	KTZ41	45	PEN46	40	U26	78	
6AS7G	80	6G6	25	6X4	30	12SA7GT	40	38A5	75	CB13L	90	EBB90	30	EF98	75	M14	88	PL36	55	U36	78	
6AT6	30	6H6	23	6X5G	35	12S7G	35	35L5	50	CB13S	75	EBF80	40	EF183	35	ML6	40	PL81	60	U76	80	
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6B4G	£1-00	6J5G	30	7B6	70	12S77	30	35Z4GT	50	CY31	43	E8L1	70	EL33	63	MU14	60	PL84	40	U92	68	
6B8G	20	6J5GT	30	7B7	45	12S7K7	45	35Z5	40	DAC32	42	E8L21	60	EL34	53	MX40	63	PL500	80	U403	50	

**Transistors**

1N914	08	2N697	18	2N2218	30	2N4989	18	AD149	60	BC169C	13	GE782	25	NKT228	33	OA2200	55	OC81D	20	ZS170	10		
18115	25	2N706	10	2N2219	33	AAZ12	30	AD161	38	BF898	28	GJ7M	38	NKT211	24	OA2201	50	OC82	25	Z8271	18		
18092	28	2N1192	30	2N269A	20	AC126	25	AF115	30	BF750	28	KS100A	20	NKT765	25	OA2207	48	OC82D	15	U93	15		
2G302	23	2N1305	25	2N3026	13	AC137	25	AF117	25	BF751	20	MJ520	10	OA2210	48	OC84	25	OC84	25	Z1108	15		
2G371	23	2N2147	15	2N3702	18	ACY20	23	BC107	13	BY100	18	MJ2955	10	OA2222	40	OC58	60	OC170	30	Z1X300	13		
2N404	23	2N2160	63	2N3819	35	5C108	13	CR81-40	18	BY88	18	£1-75	OA81	10	OA2224	38	OC59	65	OC171	30	Z1X304	28	
						5C109	13	DD003	15	CR81-40	18	MJ3065	93	OA85	13	OA2241	23	OC71	15	OC200	40	Z1X500	20
						5C113	18	DD005	16	NKT212	27	OA91	08	OA2242	23	OC72	25	OC72	25	OC72	25	Z1X503	20
						5C119	13	GET102	30	NKT214	15	OA211	38	OA2246	23	OC81	25	ORF12	50	Z1X531	30		30

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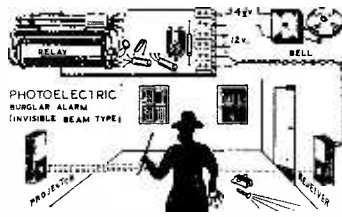
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10	600V	4 x 3 x 2	T/E	0-60	0-10	6,600	50V	4 1/2 x 2 1/2	S/T	0-65	0-12
32	450V	1 1/2 x 1	T/E	0-20	0-05	7,000	50V	4 1/2 x 2 1/2	S/T	0-75	0-12
32	500V	2 x 1 1/2	C	0-20	0-05	8,000	50V	4 1/2 x 2 1/2	S/T	0-75	0-12
50	450V	3 x 1	W/E	0-20	0-05	9,200	35V	4 1/2 x 2 1/2	S/T	0-50	0-12
60	300V	3 x 1	C	0-30	0-05	10,000	70V	4 1/2 x 2 1/2	C	0-80	0-12
80	300V	2 1/2 x 1	W/E	0-30	0-05	13,000	38V	4 1/2 x 2 1/2	S/T	0-60	0-12
100	450V	3 x 1 1/2	C	0-35	0-05	14,000	35V	4 1/2 x 3	S/T	0-60	0-15
1,000	70V	3 x 1 1/2	C	0-35	0-05	20,000	50V	6 x 3	S/T	1-25	0-18
1,200	350V	4 1/2 x 2 1/2	C	0-20	0-15	33,000	25V	4 1/2 x 2 1/2	C	0-70	0-12
1,500	50V	4 1/2 x 1 1/2	C	0-35	0-08	34,800	40V	6 x 3	S/T	2-00	0-18
2,000	35V	4 x 1	C	0-40	0-07	100-4-200	300V	4 1/2 x 1 1/2	C	0-50	0-08
2,500	60V	4 1/2 x 1	C	0-40	0-07	100-4-200	275V	4 1/2 x 1 1/2	P.C.	0-50	0-08
3,000	100V	4 1/2 x 2 1/2	C	0-60	0-15	200-4-200	350V	4 1/2 x 1 1/2	C	0-50	0-12
3,600	20V	4 1/2 x 1 1/2	S/T	0-50	0-12						

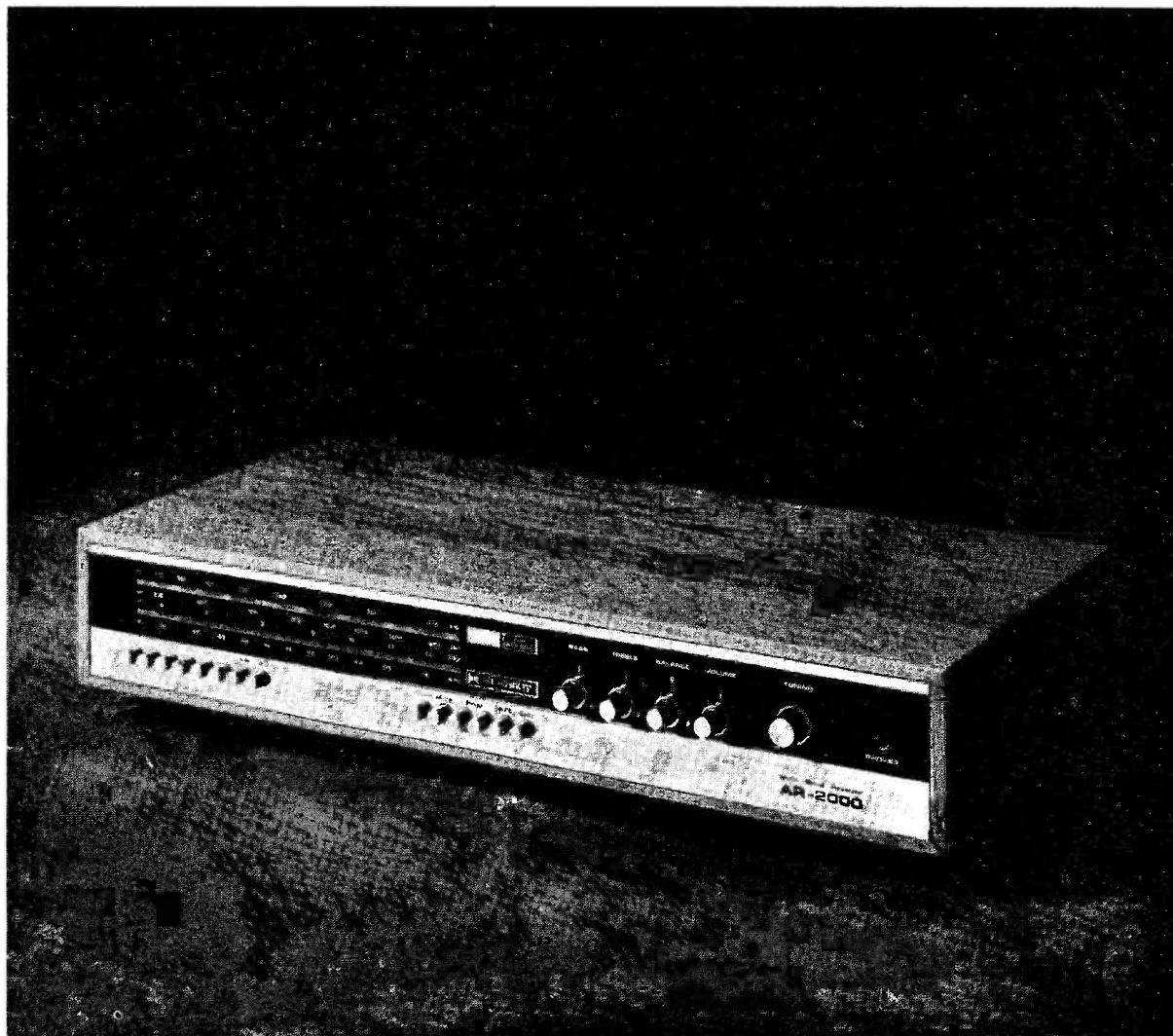
T/E=Tag ends. C=Can. W/E=Wire end. S/T=Screw terminals. P.C.=Printed Circuit. The above references only a mere fraction of our huge stocks.  
**OSCILLOSCOPE TUBES CV2184** 4 volt heaters, £1.50, p.p. 25p.  
**MULLARD POWER DIODES** 0.2Z 224 6.3V 10 watts, 25p post free.  
**PLESSEY MOLDED TRACK POTENTIOMETERS** less Switch Linear. 470 ohms, 4.7K, 6.8K, 22K, 15p post free. 250+250 ohms ganged lin. pre-set, 25p post free.  
**OVER LOAD CUT-OUTS** BY SUNVIC CONTROLS. All types encased. Type F102-5M control volts 220/230, load watts 2,000, 50p, p.p. 15p. Type F103/3M control volts 220/230, load rating 15 amp, 75p, p.p. 25p. Type F106/3M control volts 220/230, Load watt 5,000, £1.25, p.p. 30p.  
**UNMASKED N.P.N. P.N.P. SILICON TRANSISTORS.** 75% guaranteed OK. 100 for only 50p. p.p. 10p.  
**PYE PUSH-BUTTON COIL PACK** for MW, LW, SW & FM wave-bands, 60p, p.p. 10p.  
**MULLARD BY127 DIODES,** 15p post free. Discount on quantities.  
**CASSETTE TAPES IN LIBRARY BOXES.** C90 62p or 3 for £1-80. C120, 75p or 3 for £2-15. All post free.  
**DOUBLE-SIDED COPPER LAMINATED BOARD** 12 x 12 x 1/8 ins. 25p, p.p. 8p.  
**G.P.O. TYPE 3000 RELAYS** from 1 ohm up to 40,000 ohms. Various contacts or made up to your requirements.  
 If you have difficulty in obtaining any electronic parts try our service next time. Our location nr. Goodge St. Station, opposite Heals of Tottenham Court Road.

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 12A TOTTENHAM STREET, LONDON W1P 9PQ Telephone 01-680-7891



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PW 10

# COMET

## HI-FI DISCOUNT WAREHOUSES

	Rec. Retail Price	Comet Price
<b>STEREO AMPLIFIERS</b>		
ALBA UA 700	34-50	26-00
ANSTRAD 8000	25-95	16-95
ARMSTRONG 521	56-00	42-50
DULCI 207M	62-00	21-95
FERROGRAPH F307	62-00	21-95
GOODMANS Maxamp	54-00	36-00
LEAK Stereo 30 Plus	56-50	43-00
LEAK Stereo 30 Plus, in teak case	62-50	47-95
LEAK Stereo 70 Chassis	69-00	52-00
LEAK Stereo 70 Casod	75-00	58-95
METROSOUND ST20E	35-50	21-50
PHILIPS RH 591	79-00	61-50
PHILIPS RH 590	52-00	39-50
PHILIPS RH 580	29-00	23-00
PIONEER SA500	62-10	41-95
PIONEER SA700	98-00	69-95
PIONEER SA900	134-10	99-95
PIONEER Reverberation	45-00	32-95
RANK Rotel 310	69-00	49-95
RANK Rotel 610	69-00	49-95
ROGERS Ravensbourne	59-50	45-95
ROGERS Ravensbourne (cased)	64-00	49-50
ROGERS Ravensbrook Mk. II	47-50	36-50
ROGERS Ravensbrook (cased)		
Mr. I	52-50	41-50
SINCLAIR 2000	35-00	23-95
SINCLAIR Project 60/2 x Z30/PZ5	23-90	16-50
SINCLAIR PROJECT 60/2 x Z50/PZ3/trans.	34-96	23-25
SINCLAIR AFU	9-95	4-95
SINCLAIR Neoteric	61-95	46-00
SINCLAIR 3000	45-00	32-50
TELETON SAQ 206	29-00	18-50
TELETON GA101	37-50	28-50
VOLTEX 100w. Stereo Diacothèque, 8 electronically mixed inputs	185-00	139-00

All the above take both ceramic and magnetic cartridges.

	Rec. Retail Price	Comet Price
<b>TUNERS</b>		
*ARMSTRONG 523 AM/FM	53-76	42-00
*ARMSTRONG 524 FM	41-99	33-00
ARMSTRONG M8 Decoder	9-50	8-00
*DULCI FMT. 7 FM	26-00	22-00
DULCI FMT. 7S Stereo	35-00	28-25
GOODMANS Stereomax	82-52	49-95
LEAK Stereofetic Chassis	66-50	52-00
LEAK Stereofetic in teak case	72-50	58-90
PHILIPS RH 690	47-00	36-00
PHILIPS RH 680	89-00	75-50
PIONEER TX500-AM/FM	77-94	63-50
PIONEER TX900 AM/FM	153-69	123-00
RANK Rotel 320	54-57	42-95
ROGERS Ravensbourne chassis	61-99	47-95
ROGERS Ravensbrook	45-01	31-95
ROGERS Ravensbrook (cased)	51-26	41-00
TELETON GT 101	45-50	31-95

All above Tuners are complete with MPX Stereo Decoder except where starred.

	Rec. Retail Price	Comet Price
<b>TUNER/AMPLIFIERS</b>		
AKAI AA 8500	229-00	181-00
AKAI 8600	142-53	112-00
AKAI 8300	128-85	99-95
ARENA R500	82-00	67-00
ARENA 2400	90-30	72-00
ARENA 2700	105-00	85-00
ARENA T9000	303-45	258-00
ARMSTRONG M8 Decoder	9-50	8-00
ARMSTRONG 525	91-89	74-50
ARMSTRONG 526	104-71	84-50
GOODMANS Mod. 90, 35w. R.M.S.	95-00	72-00
MIDLAND 19542	49-56	37-50
PHILIPS RH 790	139-00	112-00
PIONEER SX770 AM/FM	180-43	126-00
PIONEER SX980 AM/FM	194-74	150-00
PIONEER 440	111-10	89-00
TANDBERG 1171 comp. with decoder	110-00	94-00
*TELETON F2000	51-50	39-50
TELETON 7AT20	105-00	77-95
TELETON 10AT1 150w. RMS	160-00	103-00
TELETON TFS50	82-50	59-00
TELETON TFS 80LA MW/LW/VHF	87-50	63-50
TELETON R 3000 with Speakers	63-25	37-50
TELETON CR55	120-00	87-00
WHARFEALE 100-1	149-00	119-00

Starred items above take ceramic cartridges only. All others take both ceramic and magnetic cartridges. All the above Tuners and Tuner/Amplifiers include MPX Stereo Decoder with the exception of Armstrong where decoder is extra as listed.



**COMET for after-sales service**  
THROUGHOUT THE U.K.  
Pictured, Service Dept. at Clough Rd., Hull also at Leeds, Stockton, Goole, Wakefield, Doncaster, Bridlington and Birmingham

	Rec. Retail Price	Comet Price
GOLDRING G850	6-50	5-25
EMPIRE 1000ZE/X	63-00	52-50
EMPIRE 999VE/X	44-50	36-00
EMPIRE 999TE/X	27-80	22-50
EMPIRE 999SE/X	21-00	17-50
EMPIRE 999E/X	16-50	13-00
EMPIRE 999/X	11-50	9-25
EMPIRE 909E/X	12-85	10-25
EMPIRE 909/X	9-00	7-50
EMPIRE 90EE/X	9-75	8-00
ORBIT Magnetic NM 22	Special Price 2-80	
PICKERING V18 AC2	8-40	7-00
ORTOFON SL15E	29-65	23-75
ORTOFON 2X15K Transformer	7-00	5-25
SHURE M3DM	7-41	5-50
SHURE M31E	12-05	8-95
SHURE M32E	11-10	8-25
SHURE M32-3	10-20	8-90
SHURE M44-7	11-10	7-95
SHURE M44-5	10-20	8-00
SHURE M44C	10-20	8-00
SHURE M44E	12-05	8-25
SHURE M55E	12-95	9-50
SHURE M75G	17-00	14-00
SHURE M75EJ	16-70	13-00
SHURE M75-6	19-45	18-00
SHURE M75E-85G	23-15	18-00
SHURE M75E	21-30	14-50
SHURE V15-11	40-78	28-85
SHURE V15-11-7	38-90	29-00

Starred cartridges above are ceramic. All others are magnetic.

	Rec. Retail Price	Comet Price
<b>PICKUP ARMS</b>		
GOLDRING Lenco L75	12-33	10-50
GOLDRING Lenco L69	9-29	7-00
SME 3009 with S2 Shell	34-47	27-00
SME 3012 with S2 Shell	36-71	30-50

	Rec. Retail Price	Comet Price
<b>TURNTABLES</b>		
The following Turntables are complete with base, plinth, perspex cover and cartridge. Fully wired and ready for use. All at special prices.		
GARRARD SP25 Mk 111 with Goldring G.800	Special Price £21-98	
GARRARD SP25 Mk 111 with Shure M.44-7	Special Price £22-95	
GARRARD SP25 Mk 111 with Shure M.155E	Special Price £23-95	
GARRARD AP76 with Goldring 6800	Special Price £30-95	
GARRARD AP76 with Shure M55E	Special Price £32-85	
GARRARD AP76 with Shure M75E	Special Price £36-95	
GARRARD 2025 with Sonotone STAHK	Special Price £15-50	
GOLDRING 705/P with G850	Special Price £15-95	
GOODMANS 3025 with G300	Special Price £28-90	

DUAL 1219 transcription	60-40	50-00
OVAL 1209 transcription	42-62	35-00
GARRARD SP25 Mk III	16-45	11-90
GARRARD SL65 B	21-25	15-50
GARRARD SL75 B	39-20	28-50
GARRARD SL95 B	50-01	35-50
GARRARD 401	39-67	32-50
GARRARD SL72 B	33-11	25-90
GARRARD 3500, with GKS Carf. Base and Cover to fit GARRARD SP25, SL55, SL65B and 3500	Special Price 4-00	
GARRARD 4078	13-84	10-97
GARRARD AP76	28-88	21-50
GOLDRING GL69 Mk. II	25-63	21-25
GOLDRING GL89P Mk. II	35-14	28-50
GOLDRING GL75	36-41	31-50

	Rec. Retail Price	Comet Price
GOLDRING GL75P	46-94	38-50
GOLDRING Covers for 69P and 75P	4-21	3-50
GOLDRING C99—plinth and cover for G99	11-45	9-90
GOLDRING G99	26-00	22-90
GOODMANS 3025	37-74	28-90
MCDONALD MP 50	15-75	11-75
MCDONALD 610	20-00	15-75
Base and Cover for MCDONALD MP 60 and 810	Special Price 4-50	
PHILIPS 220	31-50	25-00
PHILIPS GA146	69-00	54-00
PHILIPS 202 Electronic	39-00	32-95
PHILIPS 306 transcription unit complete with base and cover	49-93	37-95
PIONEER PL12A with base & cover	8-85	7-00
THORENS TX25 cover	70-04	61-95
THORENS TD125	180-20	88-00
THORENS TD125AB	46-16	35-95
THORENS TD150A Mk. II	49-96	42-95
THORENS TX11 Cover	4-43	3-95

	Rec. Retail Price	Comet Price
<b>SPEAKERS</b>		
B & W Model 70	159-50	121-95
B & W DM3	63-00	49-95
B & W DM1	32-00	23-50
CELESTION Ditton 16	34-00	18-90
CELESTION Ditton 25	32-00	23-50
CELESTION Ditton 25	65-00	50-95
GOODMANS Minister	25-00	20-50
GOODMANS Magister	62-80	47-95
GOODMANS Maxim	20-49	16-50
GOODMANS M320 3	34-00	27-90
GOODMANS Magnum KG	44-00	33-00
J & S Model SXMT (pair)	26-95	14-95
KEF Cresta	22-17	18-00
KELETRON Speakers		
KN500 4 speaker system (pair)	23-00	15-50
KN700 4 speaker system	27-50	18-25
KN1000 4 speaker system	19-25	13-95
KN1500 4 speaker system	24-75	18-95
KN2000 4 speaker system	28-75	20-95
LEAK 200	24-95	18-90
LEAK 300	32-50	23-95
LEAK 600	49-50	36-95
LOWTHER Acousta (with PM6)	45-50	38-50
LOWTHER Acousta (with PM7)	53-00	46-00
LWTHER Ideal Baffle	35-50	30-00
METROSOUND HFS103 (pair)	25-00	17-95
METROSOUND 202	21-50	15-95
METROSOUND HFS20 (pair)	39-00	27-95
METROSOUND HFS10 (pair)	27-44	22-95
PHILIPS RH481	11-00	8-95
PHILIPS RH482	18-00	14-95
SINCLAIR O16	8-98	6-95
STE-MA 278 3 speaker system	23-10	15-95
TANDBERG TAN 7	22-30	18-50
TANDBERG TAN 11	19-30	16-50
TANDBERG TAN 15	45-00	35-95
<b>WHARFEALE Speakers</b>		
Airedale.....Speakers	69-50	54-95
Denton	19-95	16-75
Super Linton	24-90	20-50
Melton	32-50	24-95
Rosedale	42-50	31-95
Trifon (pair)	65-00	50-95
Unit 3 Speaker Kit	59-90	45-95
Unit 4 Speaker Kit	13-00	10-95
Unit 5 Speaker Kit	18-00	13-95
Unit 6 Speaker Kit	26-00	19-95
<b>CHASSIS SPEAKERS</b>		
GOODMANS Axlette 8	8-10	6-50
GOODMANS Twinaxlette 8	9-17	7-95
GOODMANS Axium 10	9-16	7-75
GOODMANS Axium 80	28-31	23-75
GOODMANS Axium 201	14-45	10-95
GOODMANS Axium 401	17-86	14-95
GOODMANS Axium 8P	5-55	4-25
GOODMANS Axium 10P	6-05	3-95

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### COMPLETE HI-FI SYSTEMS

Completely wired, mounted and ready for use.

	Rec. Price	Retail Price	Comet Price
GOODMANS Audiom 51	13-05	18-95	9-75
GOODMANS Audiom 61	18-95	24-00	14-00
GOODMANS 2P	12-37	20-00	10-00
GOODMANS 15P	34-00	26-97	26-97
GOODMANS Audiom 18P	20-00	16-97	16-97
GOODMANS Twin Axlom 10	10-23	8-25	8-25
GOODMANS ARU172	4-50	3-50	3-50
GOODMANS Trebax 100	8-60	6-00	6-00
GOODMANS Trebax 5K/20XL	9-70	7-50	7-50
GOODMANS Midax	12-95	9-00	9-00
GOODMANS Attenuator	3-55	2-50	2-50
GOODMANS Crossover Networks			
XO/850/5000	9-75	7-25	7-25
GOODMANS Crossover Networks			
XO/850	7-40	5-75	5-75
GOODMANS Crossover Networks			
XO/5000	2-85	2-00	2-00
WHARFEDALE 8In. Bronze/RS/DD	5-00	4-00	4-00
WHARFEDALE Super 8/RS/DD	8-50	7-00	7-00
WHARFEDALE Super 10/RS/DD	14-00	11-50	11-50
WHARFEDALE WMT1 Matching Transformer	0-84	0-75	0-75

#### HI-FI STEREO SYSTEMS COMPLETE

ARENA MR15	145-00	109-95	109-95
ALBA UA552	45-88	35-50	35-50
ALBA UA682	60-32	46-95	46-95
DECCA Sound 6013	69-89	57-95	57-95
DECCA Sound 6014	70-86	68-95	68-95
DECCA Sound 1204	95-30	75-95	75-95
DECCA Compact 3	100-14	109-95	109-95
DECCALIA 5 complete with stand	65-50	51-95	51-95
EKCO SRG 609	85-44	66-95	66-95
EKCO ZUS	159-29	129-00	129-00
FERGUSON 3422	84-80	67-95	67-95
FERGUSON 3423	114-15	89-95	89-95
FERGUSON 3424	119-00	94-95	94-95
FERGUSON 3425	120-10	109-95	109-95
FERGUSON 3450 with radio	74-40	59-95	59-95
FIDELITY UA2 Music Master	44-41	31-95	31-95
FIDELITY UA1 Music Master	103-30	82-95	82-95
HMV 2416	129-70	99-95	99-95
HMV 2045/6	199-00	159-95	159-95
HMV 2482	65-65	53-95	53-95
HMV 2450 with stereo radio	134-20	109-00	109-00
KB KA1250 complete with two 653 speakers	71-55	58-50	58-50
KB KA1250 complete with two 651 speakers	80-25	64-95	64-95
KB 2010 with radio	73-40	60-95	60-95
LEAK 30/Goldring/Wharfedale	182-65	142-95	142-95
LEAK 70/Thorens/Wharfedale	226-87	175-00	175-00
MARCONI Unit 4	74-77	63-95	63-95
MARCONI Unit 3	84-79	67-95	67-95
METROSOUND Stereo 1010	92-30	69-95	69-95
PHILIPS 580/481/105	71-00	55-95	55-95
PHILIPS GF 823	47-79	38-95	38-95
PHILIPS GF 824	67-09	54-95	54-95
PHILIPS GF 833	65-16	54-95	54-95
PHILIPS GF 834	84-85	69-95	69-95
PHILIPS GF 417	96-06	73-95	73-95
PHILIPS 882	96-50	76-95	76-95
TELETON 2S80F with radio	72-40	53-95	53-95
TELETON 8TK Stereo System	54-75	48-00	48-00
TOSHIBA SP8507	248-00	175-00	175-00
ULTRA 6405	77-00	64-95	64-95

#### TAPE RECORDERS AND TAPE DECKS

AKAI 1720L	93-67	65-95	65-95
AKAI 4000 D 8-track stereo deck	86-68	67-50	67-50
AKAI CR 80D 8-track stereo tape deck	91-56	78-95	78-95
AKAI CR80 8-track stereo recorder	110-83	96-95	96-95
AKAI X200D	183-07	129-95	129-95
AKAI 1800SD	192-16	129-00	129-00
AKAI 2000SD	300-00	239-00	239-00
BUSH Diacand Stereo 2000	21-19	16-50	16-50
BUSH TP60 Cassette tape recorder	28-38	23-95	23-95

	Rec. Price	Retail Price	Comet Price
BUSH TP70 Cassette battery/mains tape recorder	28-91	23-50	23-50
FERGUSON 3245 Twin track	38-70	28-95	28-95
FERGUSON 3246 4-track	42-55	33-95	33-95
FERGUSON 3247 4-track	47-93	38-95	38-95
FERGUSON 3248 4-track	52-76	42-95	42-95
FERGUSON 3252 4-track	100-70	81-95	81-95
FERROGRAPH 702 2-track tape deck	220-22	189-00	189-00
FERROGRAPH 704/W 4-track tape deck			
FERROGRAPH 722	220-22	189-00	189-00
FERROGRAPH 724	257-52	215-00	215-00
GRUNDIG C200 De Luxe Cassette	38-46	28-95	28-95
GRUNDIG TK 121 twin track	55-30	42-95	42-95
GRUNDIG TK 149 4-track	57-63	47-95	47-95
GRUNDIG TK 141 4-track	61-82	49-50	49-50
GRUNDIG TK 146 4-track Auto	67-30	52-95	52-95
GRUNDIG 222 stereo cassette	57-70	47-95	47-95
GRUNDIG TK 147 4-track Auto	93-96	77-95	77-95
MIDLAND TC 144 cassettes	18-00	11-95	11-95
PHILIPS 2202 cassette	26-89	19-95	19-95
PHILIPS 2204 cassette battery/mains	32-30	25-50	25-50
PHILIPS 2205 cassette tape recorder	41-59	33-95	33-95
PHILIPS 3302 cassette tape recorder	23-04	17-95	17-95
PHILIPS 4303 new release	40-55	33-95	33-95
PHILIPS 4307 4-track	47-78	37-95	37-95
PHILIPS 4308 De luxe 4-track	58-40	43-95	43-95
PHILIPS 4402 4-track stereo recorder	91-71	71-95	71-95
PHILIPS 4407 4-track stereo recorder	106-19	87-95	87-95
PHILIPS 4500 4-track stereo tape deck			
PHILIPS 4408 4-track stereo	121-64	96-95	96-95
PHILIPS Cassette Stereo N2503 tape deck	134-18	106-00	106-00
PYC Cassette Recorder/Radio 9000 battery/mains	52-05	44-95	44-95
PHILIPS 2400 stereo cassette less L/S	43-86	35-95	35-95
TANDBERG 1841 4-track stereo tape deck	65-55	57-95	57-95
TANDBERG 3021 4-track stereo	69-75	50-95	50-95
TANDBERG 3041X 4-track stereo	109-90	83-00	83-00
TANDBERG 4021X twin track stereo	109-90	83-00	83-00
TANDBERG 4041X 4-track stereo	180-00	150-00	150-00
TANDBERG 6041X 4-track stereo	188-00	158-00	158-00
TANDBERG 6021X twin track stereo	188-00	158-00	158-00
TELETON 610 cassette	22-00	14-95	14-95
TELETON TC110 cassette battery/mains	26-79	19-50	19-50
TELETON TRC130 cassette with VHF/AM Radio Batt./Mains twin motors	40-31	31-50	31-50
TELETON 611 battery/mains cassette			
TELETON FXB 510 D 4-track stereo	29-50	17-50	17-50
TOSHIBA GT 601V twin track	65-16	47-50	47-50
TOSHIBA 850 SA 4-track stereo tape deck	43-95	25-95	25-95
TOSHIBA GT 840S 4-track stereo tape deck	91-50	49-95	49-95
WHARFEDALE Dolby DC9 cassette stereo tape deck	105-20	55-95	55-95

#### BASES AND COVERS

GARRARD WBI Base	3-86	3-25	3-25
GARRARD WB4 Base	5-69	4-75	4-75
GARRARD SPC 1 Cover	3-74	3-00	3-00
GARRARD SPC 4 Cover	4-44	3-75	3-75
Special offer of Base and Cover to fit GARRARD SP25, SL55, SL65B and 3500			
GOLDRING Plinth 69	Special Price	4-00	4-00
GOLDRING Covers for 69P and 75P	8-52	7-00	7-00
GOLDRING Covers for 69P and 75P (for TD125AB)	4-21	3-50	3-50
THORENS TX25 (for TD125AB)	8-22	6-50	6-50
THORENS TX11 Cover	4-11	3-75	3-75
Base and Cover for TD125	15-18	12-90	12-90
PHILIPS Stereo 2000	39-20	31-25	31-25
MOTORBOARDS only	4-95	3-00	3-00

	Rec. Price	Retail Price	Comet Price
GOODMANS AUDIO SUITE, Goodmans Maxamp stereo amplifier, Goodmans stereomax AM/FM Tuner with decoder, Pair of Goodmans Magnum K2 speakers, Garrard AP78 turntable in base, complete with cover and Goldring G800 Cartridge. Beautifully finished in walnut	257-13	169-95	169-95
GOLDRING 705P turntable complete with G800 Cartridge, Midland Tuner/Amp., pair of Melrosound 103 Speakers	99-56	69-95	69-95
GOODMANS Module 80 Tuner/Amplifier, Garrard AP78 Turntable with Goldring G800 Cartridge and 2 Goodmans Minister Speakers	199-00	139-00	139-00
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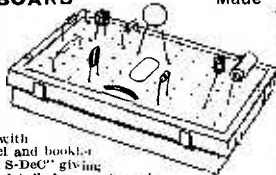


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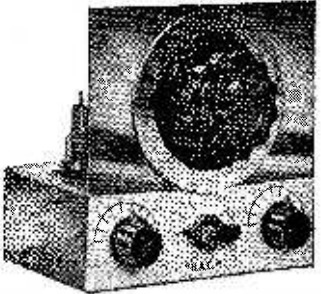
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EY88	0.43	PCL87	0.45	PCF823	0.70	UY49	0.40
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EZ54	0.50	PCL99	0.45	PCF835	0.70	UY61	0.40
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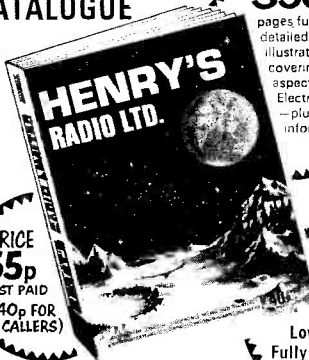
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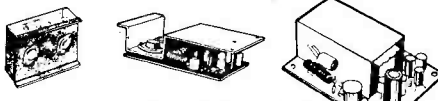
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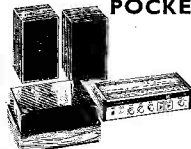
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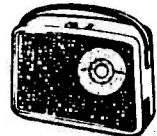
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