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practical WIRELESS

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8 page supplement

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Offer**

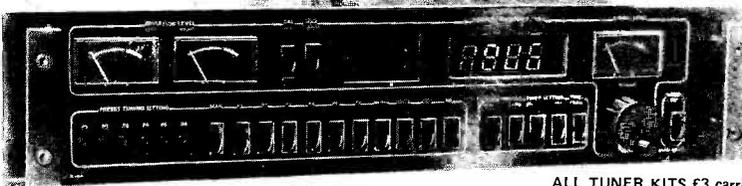


**Radio
Control**
series begins

Tecknowledgedgy for sale.

The Mark III FM Tuner

DIY Hi-Fi will never seem the same again. Ambit's Mark III tuner system is electrically & visually superior to all others. Some options available, but the illustrated version with reference series modules: £149.00 + £18.62 VAT
With Hyperfi Series modules £185.00 + £23.12



- ### Features of the system:
- * Precision construction & design of all parts
 - * Time/frequency display
 - * State of the art performance with facilities for updates, using modular plug in systems.
 - * Deviation level calibrator for recording
 - * All usual tuner features

Digital Dorchester All Band Broadcast Tuner: LW/MW/SW/SW/FM stereo

A multiband superhet tuner, constructed using a single IC for RF/IF processing - but with all features you would expect of designs of far greater complexity. The FM section uses a three section (air gang) tuned FET tunerhead, with ceramic IF filters and interstamper duty; AM employs a double balanced mixer input stage, with mechanical IF filters - plus a BFO and MOSFET product detector for CW/SSB reception. Styled in a matching unit to the Mark III FM only tuner, employing the same degree of care in mechanical design to enable easy construction. MW/LW reception via a ferrite rod antenna.

Electronics only (PCB and all components thereon) £33.00 + £4.95 VAT
Complete with digital frequency readout/clock-timer hardware £99.00 + £14.85 VAT
Complete with MA1023 clock/timer module with dial scale £66.00 + £9.90 VAT
Hardware packages are available separately if you wish to house your own designs in a professional case structure. Please deduct the cost of electronics from complete prices.

LW/MW FM LCD Digital Frequency Display - July PW feature

Update your old radio, or build this into a new design. Or use it as a servicing aid - this low power unit with LCD display reads direct frequency in kHz/MHz, or with usual AM/FM IF offsets for received frequency. Low power LCD means no RFI - 15-20mA at 9v even with the divide by 100 prescaler. FM resolution is 100kHz, AM 1kHz. Sensitivities better than 10mV. Complete kit £19.50 + £2.93 VAT, built and tested module £27.00 + £4.05VAT

Ambit stocks and distributes a wide range of frequency counter LSI for all types of DFM-part two of the catalogue contains details of the MS5523/4/5/6 range, and the versatile MSL2318 divide by ten or hundred prescaler IC. The DFM1 combined counter for AM, FM SW and direct/clock/stopwatch/timers - details available, but SAE please!

PW SANDBANKS PI METAL LOCATOR

Maintaining our professional approach to home constructor kits, we offer the pulse induction "Sandbanks". Now with injection molded casing for greatly improved environmental sealing. £37.00+£5.55vat

VHF MONITOR RX WITH PLESSEY IC 4/9 channel version of the PW design but using standard (funda)9 crystals, and TOYO 8 pole crystal filter with matching transformers. Coil sets from our standard range to cover bands from 40 to 200MHz. Complete module kit £31.25 +£3.90vat.

RADIO and AUDIO MODULES: Consistently the most advanced FOR FM

EF5801-3-4 series: 6 stage varicap tuning, all with oscillator output
5801 Dual gate MOSFET RF stages, bipolar mixer £17.45 + 2.61VAT
5803 Dual gate RF/mixer stages, amplified LO out £19.75 + 2.96VAT
5804 "Hyperfi" series, with internal PIN diode agc, and ultra wide range tuning system £24.95 + 3.74VAT

EF540 4 stage varicap tuner with TDA1062 and LO output. Uses FET/IC input. PIN agc £10.75 + 1.61VAT

FOR 30-200MHz

The EF series are available on special order to cover bands (usually approx 20% of the centre frequency) in the range described. Details in our price list.

FOR FM IFs at 10.7MHz

7030 single 6 pole linear phase filter IF with HA1137E10.95 + 1.64VAT
7130 two 8 pole linear phase filter IF with CA3189E £16.25 + 2.44VAT
7230 Hyperfi IF, switched bandwidth, AGC IF preamp, linear phase ceramic filters with diode switched narrow filter £24.95+3.74VAT

DECODERS FOR MPX (STEREO)

Various types, guaranteed the world's biggest and best ranges

LARSHOLT FM TUNERSETS

7252 MOSFET front end combined with CA3089 IF £26.50 + 3.97VAT
7252 JFET front end, combined with IF and decoder £26.50 + 3.97VAT
FM/AM tuning synthesiser, see details elsewhere in the advertisement

COMPONENTS FOR RADIO/COMMUNICATIONS/AUDIO/TV etc.

As usual, Ambit brings you the latest and best, a small selection of which is shown in this advertisement. The Ambit catalogues contain information on most of the devices mentioned here - and an order for the new part three will ensure you stay up with latest developments. Data photocopying service described in price list info.

RADIO ICs for FM vat	SL1600 series	Audio preamps vat
CA3089E 1.94 29	SL1610 1.60 24	LM381N 1.81 27
CA3189E 2.45 37	SL1611 1.60 24	LM382N 1.65 25
HA1137W 2.20 33	SL1612 1.60 24	KB4436 2.53 38
HA11235 2.20 33	SL1613 1.89 28	KB4438 2.22 33
SN76660N 0.75 11	SL1620 2.17 33	TDA1028 3.50 53
RADIO ICs for AM/FM	SL1621 2.17 33	TDA1029 3.50 53
TDA1090 3.35 50	SL1623 2.44 37	TDA1074 3.75 56
TDA1083 1.95 29	SL 624 3.28 49	
TDA1220 1.40 21	SL1625 2.17 33	Audio power
IF AMPLIFIERS	SL1626 2.44 37	TB820TM 0.75 11
KB4406 0.50 07	SL1630 1.62 24	TB810AS 1.09 16
MC1350 1.20 18	SL1640 1.89 28	LM380N 1.00 15
see comms ics also	SL1641 1.89 28	ULN28B3 1.00 15
COMMUNICATIONS	SL6640 2.75 41	ULN28B3 1.00 15
KB4412 2.55 38	SL6690 3.20 48	TDA2002 1.95 29
KB4413 2.75 41	MC3357 3.12 47	HA1370 2.99 45
SD6000 3.75 56	MC1496 1.25 19	TDA2020 2.99 45
	NE544 1.70 25	FETs, MOSFETs, bipolar, and various others: see PL

MICROMARKET OSTs overflow:

6800P	650p	8212	230p	2102	170p
6820P	600p	8216	195p	2112	340p
6850P	275p	8224	350p	2513	754p
6810	400	8228	475p	4021	575p
6852	365p	8251	625p	2114	1000p
8080	630p	8255	540p	+15% VAT	

OSTs: Remember all OSTs stocks are obtained from BS9000 approved sources - your assurance that all devices are very best first quality commercial types. Some LPSN TTL is presently in great demand, so please check by phone before ordering.

TTL-Standard AND LP Schottky

All prices listed in pence x

N	LSN	N	LSN	N	LSN	N	LSN
7400	13 20	7472	28	74142	265	74257	108
7401	13 20	7473	23 38	74143	812	74260	153
7402	14 20	7474	37 38	74144	812	74273	108
7403	14 20	7475	38 40	74145	65 87	74283	120
7404	14 24	7476	37 38	74147	175	74293	95
7405	18 26	7478	38	74148	109 191	74365	49
7406	38	7480	48	74150	99	74366	49
7409	17 24	7481	38	74151	64 84	74367	43
7410	15 24	7482	89	74153	64 84	74368	49
7411	20 24	7485	104 99	74154	96	74373	77
7412	17	7486	40	74155	54 110	74374	77
7413	30	7489	205	74156	80 110	74377	124
7414	51	7490	33 90	74157	67 85	74379	130
7415	24	7491	76 110	74158	60	74383	140
7416	30	7493	38 98	74159	210		
7417	30	7493	38 98	74160	82		
7420	16 24	7494	75	74161	82		
7421	29 24	7495a	65 99	74162	130		
7423	27	7496	58 120	74163	92 78		
7425	27	7497	185	74164	104 130		
7426	27	7497	185	74165	105		
7427	27	7497	185	74166	200		
7428	32	74107	32 38	74167	200		
7430	17 24	74109	63 38	74169	230 200		
7432	25 24	74110	54 54	74172	625		
7437	40 24	74112	68	74174	87 120		
7438	33 24	74113	38	74175	87 110		
7440	17 24	74114	38	74176	75		
7441	74	74116	198	74177	78		
7442	70 99	74118	83	74181	165 350		
7443	115	74118	83	74183	210		
7444	112	74120	115	74184	135		
7445	94	74121	25	74185	134		
7446	94	74122	46	74188	275		
7447	82 89	74124	46	74190	92		
7448	56 99	74125	38 44	74192	105 180		
7449	59	74126	57 44	74193	105 180		
7451	17 24	74128	46	74195	110		
7453	17	74128	46	74196	99 110		
7454	17 24	74132	73 78	74197	110		
7455	35 24	74136	40	74198	150		
7460	17	74138	60	74199	160		
7463	124	74139	60	74247	90		
7470	28	74141	56	74253	105		

CD4000 MORE FROM THE GENERAL AMBIT CATALOGUE RANGES:

Varicap tuning diodes for AM/FM/TV: 1-9 v AM tuning (Cr 15:1) from TOKO...
MPU controllable digital frequency synthesiser PCB, Preliminary. Serial data controlled, with the standard swallow count system for multi-rate operation. Multiple time constant filters, suitable for AM/FM and other communications/generator applications. Not for beginners. Full preliminary data package £1 + VAT. No phone enquiries answered on this system for the time being. Watch this space..... Protected cost of the controller PCB less than £30: comprises the two modulus counter, prog. div, phase detector, multiple TC loop filter/integrators.

LINEARS
4024 76 CA3130E 84
4025 17 CA3130T 90
4026 180 CA3140E
4027 55 CA3140T 72
4028 72 LM303AH 67
4029 90 710P1AN 30
4030 55 LM339N 66
4035 120 LM338AN 186
4040 83 LM3900N 60
4042 85 709HC 64
4043 85 709PC 36
4044 80 710HC 65
4045 130 710P1AN 30
4048 60 723CN 65
4049 55 741CH 66
4050 55 741CN 27
4051 65 747CN 70
4052 65 748CN 36
4053 65 NE531N 105
4055 135
4056 135
4060 115
4063 109
4066 53
4068 25
4069 20
4070 20
4071 20
4072 20
4073 20
4075 20
4076 90

TOP GRADE LEDS by AEG. PRICES ARE EXG. VAT (add 15%)
SIZE Red Green Yellow Orange
5mm 14p 16p 15p 20p 10 per type - less 10%
3mm 13p 15p 18p 19p 100 per type - less 30%
2x5x17p 20p 20p 24p 100 mix in 10s - less 25%

FUTABA FLUORESCENT VACUUM DISPLAYS for CLOCKS etc
5LT02 clock display (static drive) with AM/PM flags 9r + 1.35
5LT03 DFM display for MS5525 LSI counter £9.45 + 1.42 vat
5LT06 5 digit DFM display (G1 AY58100) mpxed £9.75 + 1.46 vat

TOKO COILS, FILTERS, CHOKES etc for AM/FM/TV comms -
TYPE Size: 5mm 7mm 10mm (I please add VAT @15%)
AM IF 5p 33p 30p Various for ICs, transistor etc.
FM IF 11 55p 33p Various for ICs, transistor etc.
SW coils 65 33p Two impedances series
OSC coils 55p 33p 35p For LW/MW/SW
TV vif/5f 35p

7-SEG DISPLAYS
HP5082 series...
Red 7650 233p
Yell 7653 233p
4069 20
4070 20
4071 20
4072 20
4073 20
4075 20
4076 90

MULTIPLEX/PILOT TONE ELEMENTS (FM IF FILTERS (see cat and))
CFSE10.7/5FE10.7 - stereo FM IF ceramic filters (5im FM4 etc) 50p
CFSE10.7/5FE10.7M - mono bandwidth ceramic FM IF filters 50p
SFE10.7M - ultra linear phase stereo ceramic IF filters 70p
CDA10.7 - 10.7MHz ceramic discriminator (AM CA3089 etc) 70p

IMPORTANT: ALL PRICES SHOWN EXCL. VAT - WHICH MUST BE ADDED AT 15% OVERHEAD. PLEASE NOTE THE REDUCED CMOS/LPSN TTL RANGES DUE TO CURRENT SUPPLY SHORTAGE.

Current news: A PCB for the Mullard DC tone and volume control system is now available £3 + 0.45 VAT. HMOS PA modules for 60-100W - kit £14 + £2.10VAT, heatsink £4.10+0.61. FM radio control system crystals £3.75 pair inc VAT (Sept on). MK50366N: static drive clock/timer IC £3.78 + 0.57 VAT. 12kHz channel spacing 8 pole 10.7MHz XTAL filter by TOYO type H4402 £15.50 + £2.32VAT. A further updated price list is now available, and we would like to remind you that enquiries can only be answered if accompanied either by an official business letterhead, or an SAE. STOP PRESS: TOKO's new split-arter triple AM tuning diodes are in stock £2.45 + 37p VAT, (KV1215). S BL1 diode DBM 1-500MHz - £4.25+0.64p.

Terms: CWO please. Account facilities for commercial customers OA. Postage 25p per order. Minimum credit invoice for account customers £10.00. Please follow instructions on VAT, which is usually shown as a separate amount. Overseas customers welcome - please allow for postage etc according to desired shipping method. Access facilities for credit purchases.

Catalogues: Ambit, Part 1 45p. Part 2 50p 90p pair. TOKO Euro shortform 20p. Micrometals toroid cores 40p. All inc PP etc. Full data service described in price list supplements.

Hours/phone: We are open from 9am - 7pm for phone calls. Callers from 10am to 7pm. Administrative enquiries 9am to 4.30pm please (not Saturdays). Saturday service 10am to 6pm.

ambit international (R) AMBIT catalogues are guaranteed to contain the most up-to-date and best informed comment on modern developments and advances in the field of radio and audio. There is no competitive publication that even approaches the broad range of parts/information on modern techniques.

2 Gresham Road, Brentwood, Essex.

practical WIRELESS

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BRITAIN'S LEADING JOURNAL FOR THE RADIO & ELECTRONIC CONSTRUCTOR

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QUERIES

While we will always try to assist readers in difficulties with a *Practical Wireless* project, we cannot offer advice on modifications to our designs, nor on commercial radio, TV or electronic equipment. Please address your letters to the Editor, *Practical Wireless*, at the above address, giving a clear description of the problem and enclosing a stamped self-addressed envelope. Only one project per letter please.

Components are usually available from advertisers. A source will be suggested for difficult items.

SUBSCRIPTIONS

Subscriptions are available to both home and overseas addresses at £10.60 per annum, from "Practical Wireless" Subscription Department, Oakfield House, Perrymount Road, Haywards Heath, West Sussex RH16 3DH.

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Our January 1980 issue will be published in early December

All these advantages...

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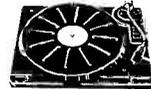
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(Partners: J. H. Birkett, J. L. Birkett)

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WIRE ENDED DIODES 50 PIV 2 1/2 Amp @ 6 for 25p.

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DUAL GATE MOS FETS like 40673 @ 33p, 4 for £1.10.

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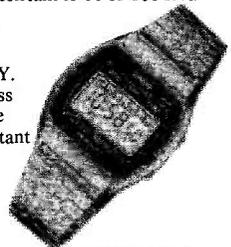
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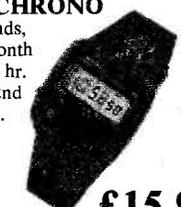
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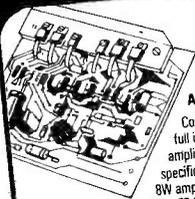
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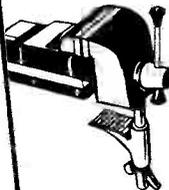
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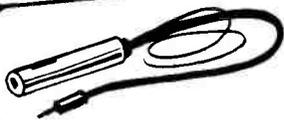
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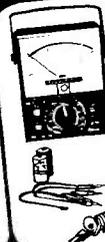
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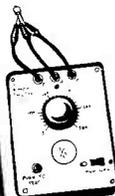
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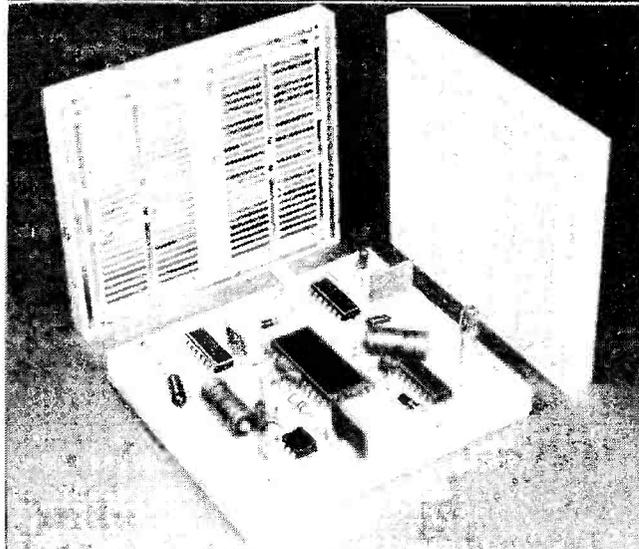
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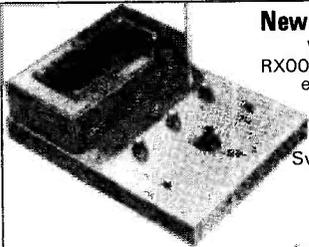
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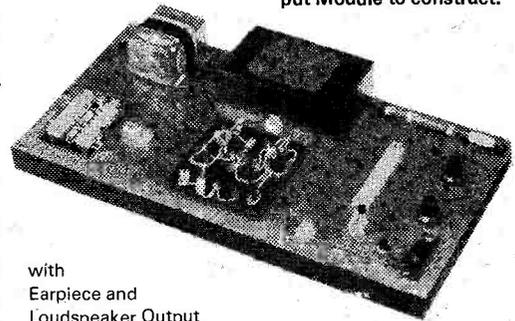
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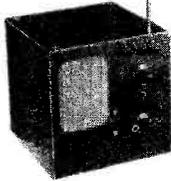


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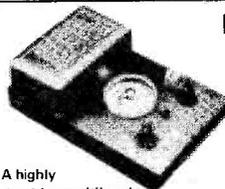
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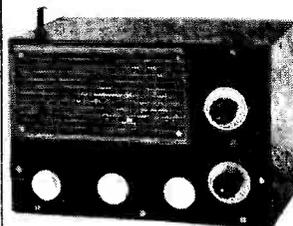
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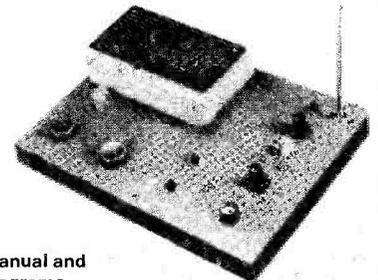
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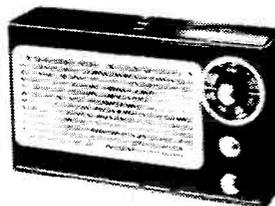


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PW1279

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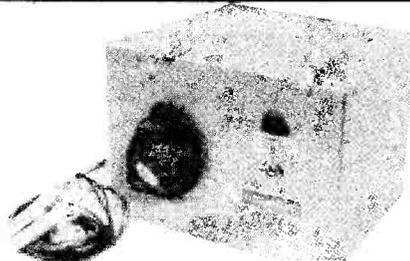
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CONTROL UNIT (mains powered)



Vol. (left) Vol. (Right)
 Tape input and volume
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 Carr. £1

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 With Headphone Socket and
 Vol. Control Carr. Free. **£7.95**

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 Mains powered Carr. £1.50 **£29.95**

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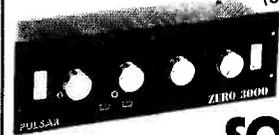
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 Imp 8-15 ohms



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SEIKO MEMORY BANK

Calendar watch M354
Hours, mins., secs.
Month, day, date in
12 or 24 hour format
all indicated continuously.
Monthly calendar display
month, year and all dates
for any selected month over
80 year period.
Memory bank function.
Any desired dates up to 11
can be stored in advanced.
2 year battery life.
Water resistant.
Metac Price



£79.50

M11

SEIKO Alarm Chronograph

With WEEKLY Alarm.
Hours, mins, secs, month,
date, day, am/pm.
Weekly alarm - can be set
for every day at designated
time e.g. 6.30 am on Mon,
Wed and Friday.
Alarm set time displayed
above time of day.
Full stopwatch functions,
laptime, split etc.



£89.95

M10

SEIKO Melody Alarm Chronograph

Chiming Alarm.
plus chrono.
Hours, mins, secs, date,
day, 24 hour alarm, 12
hour chronograph, 1/10th
secs, Laptime, Back light,
Stainless steel, mineral
glass.



METAC PRICE

£92.95

M19

SEIKO Calculator Watch

Full specification
calculator with
memory, plus multi
function watch.
Hours, mins, secs,
day, date, backlight.
Automatic calendar.
Long life battery.



£99.95

M27

CASIO CHRONO 95QS-3LB

Stainless steel case,
water resistant to 66 feet.
Hours, mins, secs, am/pm,
year, month, date, day.
Auto-calendar
pre-programmed
until the year 2029.
12/24 hour. Stopwatch
function.
Range 7 hours, 1/100 sec.
(Mode) Net time/lap-time/
1st-2nd place times.
Dual time function.
Accuracy 15 secs per month.
Battery life approx 4 years.



£22.95

M22

CASIO LADIES 86CL-23B-1

Elegant slim line.
Stainless steel bracelet,
fully adjustable.
Hour, mins, 10 sec symbol
second by flash, am/pm.
Month, date, day.
Auto-calendar preprogrammed
for 28th day in Feb.
Accuracy per month 15 secs.
Battery life approx 15 months.



£29.95

M23

CASIO F-200 Sports Chrono

Attractive Mans watch
in black resin with
mineral glass.
Hours, mins, secs, am/pm.
Month, date,
alpha-numeric day.
Auto-calendar set
28th Feb.
Stopwatch working
range 1 hour,
units 1/100 sec. Mode,
Net Time/lap/time/
1st-2nd place times.
Accuracy approx 15 secs
per month.
Battery 12 months.



£14.95

M24

CASIO ALARM CHRONO 81CS-36B

Hours, mins, secs, day,
and also day, month and year
perpetual automatic calendar.
100th sec chronograph to
7 hours.
Net time/lap/time/1st
and 2nd place times. User
optional 12/24 hr display. 24
Alarm. User optional,
hourly chime.
Backlight, mineral glass,
stainless steel.
Water resistant to
100ft.
Battery life approx 4 years.



£34.95

M25

BELTIME Chronograph

(9-Functions)
Hours, mins, secs,
day, date, month,
interchange feature,
automatic calendar,
backlight. Net
time/lap/time.
Stainless steel bracelet.
Battery life 1 year.



£14.95

M34

BELTIME Multi Alarm

29 Functions
Hours, mins, secs,
date, day.
Alarm, chronograph,
Light.
Watch 8 functions,
Alarm 4 functions,
chronograph 17
functions.
Stainless steel
bracelet.



£29.95

M35

CASIO F-8C 3 Year Battery life.

Hours, mins, secs,
am/pm, date, day.
Auto calendar set
28th Feb.
Stopwatch function.
Accuracy 15 secs per
month. Battery life
approx 3 years.



£9.95

M36

CASIO CALENDAR 200

47CS-23B-1 Black.
Stainless steel.
Hours, mins, 10 second
symbol, second (by flash),
am/pm. Month, day, date.
Auto-calendar set from
1901 to 2009.
Full month calendar display.
Dual time function.
Accuracy 10 secs per
month. Battery life
approx 15 months.



£59.95 M37

MELODY Multi Alarm Chronograph

Hours, mins, secs,
Day, Date, Count-
down alarm,
Dual time zone,
1/100th sec
stopwatch.
Lap/split time,
1st and 2nd place
times, Melody test
function.



£26.95

M30

DUAL TIME-ALARM CHRONOGRAPH

Incorporating module
of world famous
Japanese watch
manufacture.
Hours, mins, secs,
days of week, month,
day and date,
24 hour alarm,
12 hour chronograph,
1/10th secs,
lap time, Back light,
stainless steel case
and bracelet.
Mineral glass.
Battery hatch,
long life battery.

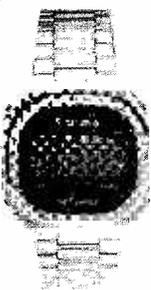


£35.00

M12

PICOQUARTZ Microprocessor Alarm Chronograph

Multilanguage-day of
the week can be set
to English, French,
German, Italian or
Spanish.
Chime - every full
hour combined with a
response signal,
beeping at every
pressing of the
functions.
Can be switched off.
12-24 hour format.
Backlight.
Chrono - 1, full scale
chrono with lap,
counting hours upto
24 hrs. Mins, secs,
1/100th secs.
Two Alarm systems.
Two time zones.



£37.95

M32

SEIKO CHRONOGRAPH

Hours, mins, secs
and day of the week.
Month date and
day of the week.
Stopwatch display -
Hours, mins, secs
up to 12 hours
(mins, secs, 1/100 secs
up to 20 minutes).
Lap timing.
Continuous time
measurement of two
competitors.
Stainless steel,
mineral glass.



£56.00

M33

Metac

ELECTRONICS
& TIME CENTRES

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Telephone: 03272 76545

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**QUARTZ LCD
5 Function**

Hours, mins, secs., month, date, auto calendar, back-light, quality metal bracelet.

£6.65

Guaranteed same day despatch. Very slim, only 6mm thick.



M1

**SOLAR QUARTZ
LCD 5 Function**

Genuine solar panel with battery back-up. Hours, mins., secs., day, date. Fully adjustable bracelet. Back-light. Only 7mm thick.

£8.65

Guaranteed same day despatch.



M2

**QUARTZ LCD
11 Function** SLIM CHRONO

6 digit, 11 functions. Hours, mins., secs., day, date, day of week. 1/100th, 1/10th, secs., 10X secs., mins., Split and lap modes. Back-light, auto calendar. Only 8mm thick. Stainless steel bracelet and back. Adjustable bracelet. Metac Price

£10.65 Thousands sold!
Guaranteed same day despatch.



M3

**QUARTZ LCD
ALARM 7 Function**

Hours, mins, secs., month, date, day. 6 digits, 3 flags plus continuous display of day and date or seconds. Back-light Only 9mm thick.

£12.65

Guaranteed same day despatch.



M4

**MULTI ALARM
6 Digits 10
Functions**

- Hours, mins., secs.
- Months, date, day.
- Basic alarm.
- Memory date alarm.
- Timer alarm with dual.
- Time and 10 country zone.
- Back-light.
- 8mm thick.

£18.65



M5

**FRONT-BUTTON
Alarm Chrono
Dual Time**

6 digits, 5 flags, 22 functions. Constant display of hours and mins., plus optional seconds or date display. AM/PM indication, month, date. Continuous display of day. Stop-watch to 12 hours 59.9 secs., in 1/10 second steps. Split and lap timing modes. Dual time zones. Only 5mm thick. Back-light. Fully adjustable open bracelet.

£22.65

Guaranteed same day despatch



M6

**SOLAR QUARTZ LCD
Chronograph with
Alarm
Dual Time Zone
Facility**

6 digits, 5 flags, 22 functions. Solar panel with battery back-up. 6 basic functions. Stop-watch to 12 hours 59.9 secs., in 1/10 sec., steps. Split and lap timing modes. Dual time zones. Alarm. 9mm thick. Back-light. Fully adjustable bracelet.

£27.95



M7

**ALARM CHRONO
with 9 world
time zones**

- 6 digits, 5 flags.
- 6 basic functions.
- 8 further time zones.
- Count-down alarm.
- Stop-watch to 12 hours 59.9 secs.
- in 1/10 sec. steps.
- Split and timing modes.
- Alarm.
- 9 mm thick.
- Back-light.
- Fully adjustable bracelet.

£29.65



M8

**SOLAR QUARTZ LCD
Chronograph**

Powered from solar panel with battery back-up. 6 digit, 11 functions. Hours, mins., secs., day, date, day of week. 1/100th, 1/10th, secs., 10X secs., mins. Split and lap modes. Back-light, auto calendar. Only 8mm thick. Stainless steel bracelet and back. Adjustable bracelet. Metac Price

£13.65

Guaranteed same day despatch.



M9

**QUARTZ LCD
Ladies Day Watch**

Only 25 x 20mm and 6mm thick. Hours, minutes, seconds, day, date, backlight and auto calendar. Elegant metal bracelet in silver or gold fully adjustable to suit very slim wrists. State colour preference.

£9.95

Guaranteed same day despatch.



M15

**QUARTZ LCD
Ladies Fashion Watch**

Elegant bracelet in bronze/gold finish or silver colour. Hours, mins, secs, day, date, backlight and auto calendar. Adjustable for the slimmest of wrists. State colour preference.

£14.95

Guaranteed same day despatch



M17

**QUARTZ LCD
Ladies Cocktail Watch**

Highly functional watch which also suits those special occasions. Beautifully designed with a very thin bracelet which retains strength as well as elegance. Hours, mins, secs, day, date, backlight and autocalendar. Bracelet fully adjustable to suit slim wrists. State gold or silver finish.

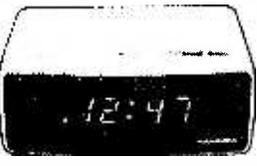
£19.95

Guaranteed same day despatch



M18

**HANIMEX
Electronic
LED Alarm Clock**



Features and Specification
Hour, minute display. Large LED display with p.m. and alarm on indicator. 24 Hours alarm with on/off control. Display flashing for power loss indication. Repeatable 9 minute snooze. Display bright/dim modes control. Size 5.15" x 3.93" x 2.36" (131mm x 11mm x 60mm) Weight 1.43 lbs (0.65 kg) AC power 220V.

£10.20 Thousands sold!
Mains operated.

Guaranteed same day despatch.

M13

**EXECUTIVE ALARM
WATCH**

6 Functions plus Alarm:
Conference signal.
5 minute snooze alarm.
Conference signal sounds 4 secs., before main alarm to give advance warning and an option to cancel.
Snooze sounds 5 mins., after main alarm and is always preceded by the conference signal.

£14.95



M60

**MACY QUARTZ
ANALOGUE**

Automatic Calendar Day and Date infinite bracelet. This mans watch has elegance as well as the robust appearance provided by a watch with traditional features. Accuracy is provided by a quartz crystal powered by a long life miniature battery.

£24.95



M21

Metac price breakthrough for an Alarm Chronograph with Dual Time only

£18.95

OUTSTANDING FEATURES

- **DUAL TIME.** Local time always visible and you can set and recall any other time zone (such as GMT). Also has a light for night viewing.
- **CALENDAR FUNCTIONS** include the date and day in each time zone.
- **CHRONOGRAPH/STOPWATCH** displays up to 12 hours, 59 minutes, and 59.9 seconds.
- On command, stopwatch display freezes to show **intermediate (split/lap) time** while stopwatch continues to run. Can also switch to and from timekeeping and stopwatch modes without affecting either's operation.
- **ALARM** can be set to anytime within a 24 hour period. At the designated time, a pleasant, but effective buzzer sounds to remind or awaken you!

Guaranteed same day despatch. **M16**

HOW TO ORDER
Payment can be made by sending cheque, postal order, Barclay, Access or American Express card numbers. Write your name, address and order details clearly, enclose 40 pence per single item for post and packing or the amount stated in the advert. All products carry 1 year written guarantee and full money-back 10 day reassurance. Battery fitting and electronic calibration service is available to customers at any Metac shop. All prices include VAT currently at 15%.

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SUPERSOUND 13 HI-FI MONO AMPLIFIER



A superb solid state audio amplifier. Brand new components throughout. 5 silicon transistors plus 2 power output transistors in push-pull. Full wave rectification. Output approx. 13 watts r.m.s. into 8 ohms. Frequency response 12Hz 30KHz ± 3db. Fully integrated pre-amplifier stage with variable volume controls. Suitable for 8-15 ohm speakers. Input for ceramic or crystal cartridge. Sensitivity approx. 40mV for full output. Supplied ready built and tested, with knobs, escutcheon panel, input and output plugs. Overall size 3" high x 6" wide x 7 1/2" deep. AC 200/250V. PRICE £18.40, P. & P. £1.20.

separate Volume. Bass boost and Treble cut controls. Suitable for 8-15 ohm speakers. Input for ceramic or crystal cartridge. Sensitivity approx. 40mV for full output. Supplied ready built and tested, with knobs, escutcheon panel, input and output plugs. Overall size 3" high x 6" wide x 7 1/2" deep. AC 200/250V. PRICE £18.40, P. & P. £1.20.

HARVERSONIC MODEL P.A. TWO ZERO



An advanced solid state general purpose mono amplifier suitable for Public Address system, Disco, Guitar, Gram, etc. Features 3 individually controlled inputs (each input has a separate 2 stage pre-amp). Input 1, 15mV into 47k. Input 2, 15mV into 47k (suitable for use with mic. or guitar etc). Input 3, 200mV into 1 meg. suitable for gram, tuner, or tape etc. Full mixing facilities with full range bass & treble controls. All inputs plug into standard jack sockets on front panel. Output socket on rear of chassis for an 8 ohm or 16 ohm speaker. Output in excess of 30 watts music power. Very attractively finished purpose built cabinet made from black vinyl covered steel, with a brushed anodised aluminium front escutcheon. For ac mains operation 200/240 volts. Size approx. 12 1/2" wide x 5 1/2" high x 7 1/2" deep. Special introductory price £29.00 + £2.50 carriage and packing.

"POLY PLANAR" WAFER-TYPE, WIDE RANGE ELECTRO-DYNAMIC SPEAKER

Size 1 1/2" x 1 1/2" x 1 1/2" deep. Weight 19oz. Power handling 20W r.m.s. (40W peak). Impedance 8 ohm only. Response 40Hz-20KHz. Can be mounted on ceilings, walls, doors, under tables, etc., and used with or without baffle. Send S.A.E. for full details. Only £8.80 each + p. & p. (one 90p, two £1.10). Now available in 8" round version. 10 watts RMS 60Hz 20KHz £6.30. P. & P. (one 65p, two 75p).

STEREO MAGNETIC PRE-AMP. Sens. 3mV in for 100mV out. 15 to 35V neg. earth. Equ. ± 1dB from 20Hz to 20KHz. Input impedance 47K. Size 1 1/2" x 2 1/2" x 5 1/2" H. £3.20 + 20p P. & P.

MAINS OPERATED SOLID STATE AM/FM STEREO TUNER



200/240V Mains operated Solid State FM AM Stereo Tuner. Covering M.W. A.M. 540-1605 KHz VHF/FM 88-108 MHz. Built-in Ferrite rod aerial for M.W. Full AFC and AGC on AM and FM. Stereo Beacon Lamp Indicator. Built in Pre-amps with variable output voltage adjustable by pre-set control. Max o/p Voltage 600mV RMS into 20K. Simulated Teak finish cabinet. Will match almost any amplifier. Size 8 1/2" x 4" h x 9 1/2" d approx. LIMITED NUMBER ONLY at £29.00 + £1.50 P. & P.

10/14 WATT HI-FI AMPLIFIER KIT A stylishly finished monaural amplifier with an output of 14 watts from 2 EL84s in push-pull. Super reproduction of both music and speech with negligible hum. Separate inputs for mike and gram allow records and announcements to follow each other. Fully shrouded section wound output transformer to match 3-15 Ω speaker and 2 independent volume controls, and separate bass and treble controls are provided giving good lift and cut. Valve line-up 2 EL84s, ECC83, EF86 and EZ80 rectifier. Simple instruction booklet 50p + SAE (Free with parts). All parts sold separately. ONLY £18.40, P. & P. £1.40. Also available ready built and tested £22.50, P. & P. £1.40.

STEREO DECODER MK.II SIZE 1 1/2" x 2 1/2" x 1 1/2" ready built. Pre-aligned and tested for 10-16V neg. earth operation. Can be fitted to almost any FM VHF radio or tuner. Stereo beacon light can be fitted if required. Full details and instructions supplied. £7.00 plus 20p P. & P. Stereo beacon light if required 40p extra.

SPECIAL OFFER

Slightly shop soiled radios by well-known manufacturer for AC Mains or battery use. MW and FM bands. Dynamic M/coil speakers. telescopic aerial and internal ferrite aerial. Earpiece socket for personal listening. Finished in attractive simulated leatherette. Size 7" H x 9 1/2" W x 4" D approx. Fully guaranteed. Bargain price of only £10.25 + £1.30 p. & p.

Mullard LPI159 RF-IF module 470KHz £2.50 + P. & P. 20p. Full specification and connection details supplied.

Pye VHF FM Tuner Head covering 88-108MHz 10.7 MHz I.F. output 7.8V + earth. Supplied pre-aligned, with full circuit diagram with precision-ganged F.M. ganks and 323PF + 323PF A.M. Tuning gang only £3.40 + P. & P. 35p.

VYNAIR & REXINE SPEAKERS & CABINET FABRICS app. 54 in wide. Our price £2.30 yd. length. P. & P. 50p per yd. (min. 1 yd.). S.A.E. for samples.

HARVERSONIC SUPERSOUND 10 + 10 STEREO AMPLIFIER KIT

A really first-class Hi-Fi Stereo Amplifier Kit. Uses 14 transistors including Silicon Transistors in the first five stages on each channel resulting in even lower noise level with improved sensitivity. Integral Pre-amp with Bass, Treble and two Volume Controls. Suitable for use with Ceramic or Crystal cartridges. Very simple to modify to suit magnetic cartridges—instructions included. Output stage for any speakers from 8 to 15 ohms. Compact design, all parts supplied including drilled metalwork, high quality ready drilled printed circuit board with component identification clearly marked, smart brushed anodised aluminium front panel with matching knobs, wire, solder, nuts, bolts—no extras to buy. Simple step by step instructions enable any constructor to build an amplifier to be proud of. Brief specification: Power output: 14 watts r.m.s. per channel into 5 ohms. Frequency response: ± 3dB 12-30,000 Hz Sensitivity: better than 80mV into 1M Ω; Full power bandwidth: ± 3dB 12-15,000 Hz. Bass boost approx. to ± 12dB; Treble cut approx. to ± 16dB. Negative feedback 18dB over main amp. Power requirements 35v at 1.0 amp. Overall Size 12" w. x 8" d. x 2 1/2" h. Fully detailed 7 page construction manual and parts list free with kit and send 25p plus large S.A.E. AMPLIFIER KIT £14.95 P. & P. 80p (Magnetic input components 33p extra) POWER PACK KIT £6.20 P. & P. 95p CABINET £6.20 P. & P. 95p SPECIAL OFFER—only £25.80 if all 3 items ordered at one time plus £1.25 p. & p. Full after sales service Also avail. ready built and tested £32.20, P. & P. £1.50.

HARVERSONIC STEREO 44

A solid state stereo amplifier chassis, with an output of 3-4 watts per channel into 8 ohm speakers. Using the latest high technology integrated circuit amplifiers with built in short term thermal overload protection. All components including rectifier, smoothing capacitor, fuse, tone control, volume controls, 2 pin din speaker sockets & 5 pin din tape rec./play socket are mounted on the printed circuit panel, size approx. 9 1/2" x 2 1/2" x 1" max. depth. Supplied brand new & tested, with knobs, brushed anodised aluminium 2 way escutcheon (to allow the amplifier to be mounted horizontally or vertically) at only £10.40 plus 50p P. & P. Mains transformer with an output of 17v a/c at 500m/a can be supplied at £2.15 + 40p P. & P. if required. Full connection details supplied.

All prices and specifications correct at time of press and subject to alteration without notice.

PLEASE NOTE: P. & P. CHARGES QUOTED APPLY TO U.K. ONLY. SEND SAE WITH ALL ENQUIRIES.

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OH9 1.00	EF93 0.85	PC28B 0.85	1S4 0.45	1S5 0.45	6BW7 1.15	906 0.85
OL92 0.80	EF183 0.85	PC28C 0.85	1S5 0.45	1S6 0.45	6C4 0.70	10C2 0.70
OY86/87 0.85	EF184 1.85	PC28D 0.85	1S6 0.45	1S7 0.45	6C4 0.70	10F18 0.70
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E182CC 3.95	EL37 3.45	PCF802 0.75	300 0.50	300 0.50	6E8A 1.20	12A7T 0.65
EA76 2.25	EL38 4.80	U191 0.85	304 0.50	304 0.50	6F86B 0.85	12A0 0.60
EABC80 0.60	EL41 4.05	U25 1.15	304 0.50	304 0.50	6F86 0.85	12A6 0.60
EB91 0.65	EL81 1.20	U26 1.00	304 0.50	304 0.50	6F12 0.90	12AX7 0.85
ECB33 1.15	EL82 0.70	U27 1.15	304 0.50	304 0.50	6F15 1.30	12B6 0.60
EF80 0.60	EL84 0.90	U28 1.15	304 0.50	304 0.50	6F17 1.15	12BH7 1.10
EF83 0.60	EL86 1.05	U29 1.15	304 0.50	304 0.50	6F24 4.75	12C8 0.65
EF89 0.80	EL90 1.50	U30 1.05	304 0.50	304 0.50	6F33 4.75	12E1 4.95
EC52 0.50	EL91 3.25	U31 0.65	304 0.50	304 0.50	6H6 1.90	12J56GT 0.55
EC81 0.65	EL95 0.80	U32 0.65	304 0.50	304 0.50	6J4 1.60	12K76T 0.70
EC82 0.60	EL96 0.80	U33 0.65	304 0.50	304 0.50	6J4W 2.00	12K8GT 0.65
EC83 0.65	EL97 0.80	U34 0.65	304 0.50	304 0.50	6L4 1.60	1207GT 0.85
EC84 0.55	EL98 0.80	U35 0.65	304 0.50	304 0.50	6R4G 1.30	6J6 0.85
EC85 0.60	EL99 0.80	U36 0.65	304 0.50	304 0.50	6R4G 1.30	6J7 0.85
EC86 0.60	EL99 0.80	U37 0.65	304 0.50	304 0.50	6R4G 1.30	6J7 0.85
EC87 0.60	EL99 0.80	U38 0.65	304 0.50	304 0.50	6R4G 1.30	6J7 0.85
EC88 0.75	EM81 0.70	U39 0.65	304 0.50	304 0.50	6R4G 1.30	6J7 0.85
EC89 0.95	EM84 0.50	U40 0.65	304 0.50	304 0.50	6R4G 1.30	6J7 0.85
EC90 0.80	EM87 1.15	U41 0.65	304 0.50	304 0.50	6R4G 1.30	6J7 0.85
EC91 0.55	EY51 0.55	U42 0.65	304 0.50	304 0.50	6R4G 1.30	6J7 0.85
EC92 0.55	EY81 0.55	U43 0.65	304 0.50	304 0.50	6R4G 1.30	6J7 0.85
EC93 1.15	EY86/87 0.65	U44 0.65	304 0.50	304 0.50	6R4G 1.30	6J7 0.85
EC94 0.55	EY88 0.65	U45 0.65	304 0.50	304 0.50	6R4G 1.30	6J7 0.85
EC95 0.55	EY89 0.65	U46 0.65	304 0.50	304 0.50	6R4G 1.30	6J7 0.85
EC96 1.70	EY88 0.65	U47 0.65	304 0.50	304 0.50	6R4G 1.30	6J7 0.85
EC97 0.55	EY89 0.65	U48 0.65	304 0.50	304 0.50	6R4G 1.30	6J7 0.85
EC98 1.40	EY90 0.65	U49 0.65	304 0.50	304 0.50	6R4G 1.30	6J7 0.85
EC99 0.70	EY91 0.65	U50 0.65	304 0.50	304 0.50	6R4G 1.30	6J7 0.85
ECL82 0.65	G232 3.95	U51 0.65	304 0.50	304 0.50	6R4G 1.30	6J7 0.85
ECL83 1.40	G234 2.30	U52 0.65	304 0.50	304 0.50	6R4G 1.30	6J7 0.85

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POSTAGE: £1-£2 20p; £2-£3 30p; £3-£5 40p; £5-£10 60p; over £10 free, minimum order £1. A lot of these valves are imported and prices vary for each delivery, so we reserve the right to change prices for new stock when unavailable.

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PRACTICAL WIRELESS T.V. SOUND TUNER

(Nov. 75 article by A. C. Ainslie) Copy of original article supplied on request
IF Sub-Assembly (G8) £7.82. P&P 85p.
Mullard ELC1043 V'cap UHF Tuner £6.33. P&P 40p.
3-way Station Control Unit £1.38. P&P 30p.
6-way Station Control Unit (Special Offer) £1.15. P&P 35p.
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IT'S FREE

Our monthly Advance Advertising Bargains List gives details of bargains arriving or just arrived—often bargains which sell out before our advertisement can appear—it's an interesting list and it's free—just send S.A.E. Below are a few of the Bargains still available from previous issues.

12v SUBMERSIBLE PUMP

Just join it to your car battery, drop it into the liquid to be moved and up it comes, no mess, no priming, no pump. Suitable for water, paraffin and any non explosive, non corrosive liquid. One use if you are a camper, make yourself a shower. Price £6 + 9p. A free gift, first 100 purchasers will get tap with built in switch and length of plastic tubing.

PRECISION RESISTORS

A fortunate purchase enables us to offer almost a complete range of Mullard metal film precision resistors, 1% tolerance. Values start at 5r and go right through to 976k. Most values are available in 1/2 watt and 1 watt rating. Price 25p + 3p each in small quantities, or 20p + 3p each where supplied not less than 10 of a value, 15p + 3p each not less than 100 of a value.

THIS MONTH'S ELECTRICAL SNIP

Parcel of M.E.M White flush 13 amp sockets, switches etc. Total retail value over £56 + vat for only £28 + £4.20p. You get 10 double 13 amp sockets and 6 single 13 amp S. sockets with neons, 14 power (20 amp dpt switches and spurs some with neons), 20 single ganged one way, two way and intermediate switches, and super free gift worth £3. If not collecting please add £2.

M.E.M. WHITE FLUSH SOCKETS ETC.

We have picked out the popular items for the snip parcel described above but a list of the other parts available is as follows (makers list nos): 220, 240, 240, 242, 244, 711, 712, 813, 1000, 1005, 1010, 1011, 1020, 1021, 1022, 1024, 1025, 1033, 1400, 1400 WH, 1401 WH, 1402, 1402 WH, 1403, 1403 WH, 1404, 1404 WH, 1405, 1405 WH, 1407, 2025, 7092. Electricians and Contractors using these accessories should send for our M.E.M. Electrical List where prices and quantity discounts will be available.

VARI-CAPT.V. PUSH BUTTON TUNER

W. German make but fitted to several popular colour T.V.'s, makers ref no 2357 0076. This has 6 push buttons each of which is in effect a multi turn pot, total resistance is 15 k. The buttons are black with chrome metal tops. Price £1 + 15p, post 25p. Good quantity available at usual discount rates.

MULTI TURN POT WITH KNOB

100 k lin, 20 turn used in many T.V. receivers, makers ref. 7802 412-00051. Suitable for fine control of resistance in general circuitry. Price 40p + 6p.

T.V. DIPLEX

On plastic moulding size 2 1/2" x 1 1/2". We are able to offer these at such a low price that they can be used as T.V. aerial sockets only. Price 10 for £1 + 15p.

TRANSDUCCERS

As used remote control T.V. receivers. Price £1.50p + 22p.

BURGLAR ALARM

Mains operated new circuit available, this is simple to install and trouble free. Price list and diagram free on request.

ARMY 46 SETS

As made for and used in the Second World War, we have a few of these in mint condition, complete with carrying satchels, headphones, throat mikes and instruction cards. In unopened boxes. Price £30 + £4.50, post £2.

MUSIC CENTRE COVER

Size 20" x 13 1/2" x 4". Clear plastic £3.50p + 52p, carriage and special packing £2.

25 AMP D.C. METERS

Flush panel mounting, wide angle, extra long, 320° scale made for G.P.O. Really beautiful instrument, brand new in original cartons. Limited quantity only so no discounts. Price £8 + £1.20p. (Less than half maker's price).

BIG BLOWER

Driven by 1/2 H.P. mains motor but compact and quiet running. This is ideal for air conditioning, fume extraction, pressurizing and many other applications. Overall size 10 1/2" x 10 1/2" dia, outlet size 10 1/2" x 4 1/2". Price £15 + £2.25p, carriage £3. Note this is the largest of our 'Snail shaped blowers, we have smaller ones right down to 10 watt motors with outlets as small as 2" x 2" in fact we can cover almost any application and welcome your enquiries. Price are from £3 complete with motor.

DOLLS HOUSE SWITCH

Time is fast approaching when you may be thinking of making toys. Small surface mounting switches are often a problem and this why we are now offering this plastic bodied rotary switch suitable for low voltage applications. Price 10 for £1.50p + 22p, carriage £2.

CASSETTE STORAGE CASE

With dust cover, holds 5 cassettes and comes complete with clip for joining to another, so you can make up in lengths to suit yourself. Price 50p + 7 1/2p + 50p post or ten for £4 + 60p, post £1.50p.

TELEPHONE ANSWERING MACHINES

Grade 2 machines are in stock ready for immediate despatch or collection, (if coming specially to collect please telephone first). For the benefit of new readers we supply these machines on the understanding they will be broken up or at least used for their original purpose. The machines are secondhand but so far as we can see they are complete and quite possibly in good working order. We do not test them but guarantee to replace any part of the machine should it be missing or faulty, providing we are notified within 14 days of receipt. Prices for the machines are as follows: Grade 2 that is in very good condition £15.50p + £2.25p, and Grade 1 which are top grade machines and are our very best almost perfect £20 + £3.00 each, but there is likely to be one month's wait. To these prices must be added £2.50p to cover carriage.

MAINS POWER PACK IN PLASTIC CASE

For telephone answering machine. Price £4.50p + 63p. Post 50p.

POT CORES

We now have good stocks of Ferrite pot cores. These are un-used equipment and contain the bobbin and have been opened ready to use.

Diameter	Thickness	Price
FX 2243 4.5 cm	3.0 cm	75p + 12p per pair
FX 2242 3.5 cm	2.3 cm	60p + 9p per pair
FX 2240 2.5 cm	1.6 cm	50p + 7p per pair

COMPONENT BOARD

Again from unused equipment, major items on these are two power silicon transistors. Motor Rola ref. SJ 5433 mounted on a heat sink with mica insulators, also behind the panel are two power rectifiers ST NS 1008. Price 90p + 6p.

DELAY SWITCH

Mains operated—delay can be accurately set with pointers knob for periods of up to 2 1/2 hrs. 2 contacts suitable to switch 10 amps—second contact opens few minutes after 1st contact £1-50

SOUND TO LIGHT KIT. Based on the Everyday Electronics circuit this is a very efficient little unit when made up is in every way equal to professional models costing many times the price. This unit is not tuned to any particular frequency, it is simply dependent upon volume. This is no disadvantage, in fact the effect is very pleasing. It will control up to 750w of lighting and works well with amplifiers with outputs of 250 watts. The kit complete with leads and plastic case is £25 only.

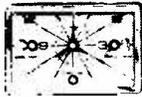
MULLARD UNILEX

A mains operated 4 + 4 stereo system. Rated one of the finest performers in the stereo field this would make a wonderful gift for almost anyone in easy-to-assemble modular form and complete with a pair of speakers this should sell at about £30—but due to a special bulk-buy and as an incentive for you to buy this month we offer the system complete at only £15 including VAT and postage.



25A ELECTRIC PROGRAMMER

Learn in your sleep. Have radio playing and kettle boiling as you wake—switch on lights to ward off intruders—have a warm house to come home to. All these and many other things you can do if you invest in an electrical programmer. Clock by famous maker with 15 amp on/off switch. Switch-on time can be set anywhere to stay on up to 6 hours independent 60 minute memory logger. A beautiful unit. £4.50



HUMIDITY SWITCH

American made by Honeywell. The action of this device depends upon the dampness causing a membrane to stretch and trigger a sensitive micro-switch, quite sensitive—breathing on it for instance will switch it on. Micro 3 amp. at 250v a.c.



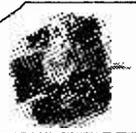
MAINS BLOWER

The Torrinq—quiet but powerful outlet size 2 1/2" x 1 1/2" for cooling equipment etc. Will extract of outlet is blowing outwards price £5-50. Other models from £2-00.



INDUCTION MOTORS

One illustrated is our reference MM11 made for ITT 1/2" slack 1/2" spindle £2-25, 1 stack model £1-75, 1 stack £2-75, 1 1/2 stack £3-25.



DRILL CONTROLLER

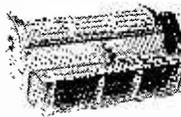
Electronically changes speed from approximately 10 revs to maximum. Full power at all speeds by finger-tip control. Kit includes all parts, case, everything and full instructions. £3-45 Made up model £1-00 extra

MOTORISED DISCO SWITCH

With 10 amp changeover switches. Multi adjustable switches are rated at 10 amps. This would provide a magnificent display. For mains operating. 8 switch model £5-25, 10 switch model £6-75, 12 switch model £8-75.



TANGENTIAL HEATER UNIT



3KW MODEL £5-95 + £1-50 P & P

2 k.w. model made in metal case with control switch £12-00

A most efficient and quiet running blower-heater by Solstron—same type as is fitted to many famous name heaters—Comprises mains induction motor—long turbo fan—split kw heating element and thermostatic safety trip—simply connect to the mains for immediate heat—mount in a simple wooden or metal case or mount direct onto base of say kitchen unit—price, 1000w post £1-50 cold switch to give 2kw, 1kw, cold blow or off available 60p extra.

MINI-MULTI TESTER



Amazing, deluxe pocket size precision moving coil instrument jewelled bearings—1000 opv—mirrored scale. 11 instant ranges measure:—DC volts 10, 50, 250, 1000 AC volts 10, 50, 250, 1000 DC amps 0-1mA and 0-100 mA Continuity and resistance 0-150K ohms. Complete with insulated probes, leads, battery, circuit diagram and instructions.

Unbelievable value only £6-50 + 50p post and insurance. FREE Amps directly kit enable you to read DC current from 0-10 amps, range on the 0-10 scale. It's free if you purchase quickly but if you already own a mini tester and would like one send £1-50.

TERMS: Cash with order—but orders under £6 must add 50p to offset packing, etc. BULK ENQUIRIES INVITED. PHONE: 01-688 1833. ACCESS & BARCLAYCARD ACCEPTED

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HEAVY DUTY 3 CORE APPLIANCES LEAD

15 amp wire 6 ft long, conventional yellow green, brown and blue cores, grey pvc outer, prepared ends, this flex normally sells at 30p per metre. 10 leads for £2.50p + 40p. Post £1.50p.

E.M.T. MAINS TRANSFORMER

1500 volt, 3.5 kv 3 mA. These transformers are unused P.S.U.'s. Price £2 + 30p, post 40p.

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We do not normally offer second hand equipment for breaking down but this particular item contains so many useful pieces that we have decided to break our rule. The unit is in fact a pocket "bleeper" in a most useful case, size about 2 1/2" wide by 4" thick by 5 1/2" deep, ideal size to fit into the top jacket pocket. Case comes apart by undoing two screws, inside is printed circuit board upon which are mounted a miniature loud speaker, three rechargeable nicad cells, 1500 - 4 ferrite potted coils, three of which are tunable, 4 ferrite rod. Mercury tilt switch on when case is upright, 4 electrolytic condensers, one micro switch, 8 resistors all with usable length leads, 4 polystyrene capacitors, 2 pin plug for charging batteries without uncasing and approximately 4 diodes and approximately 30 various capacitors and resistors, most of the resistors being 1/2 watt type, truly a very useful unit although secondhand, still in reasonable condition. Price £1-50p + 22p.

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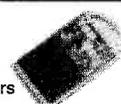
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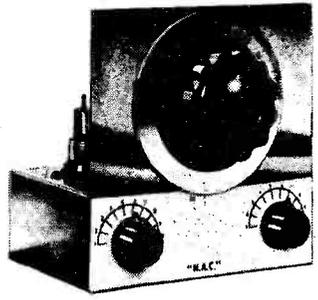
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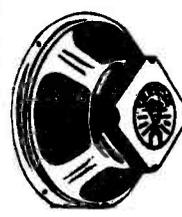
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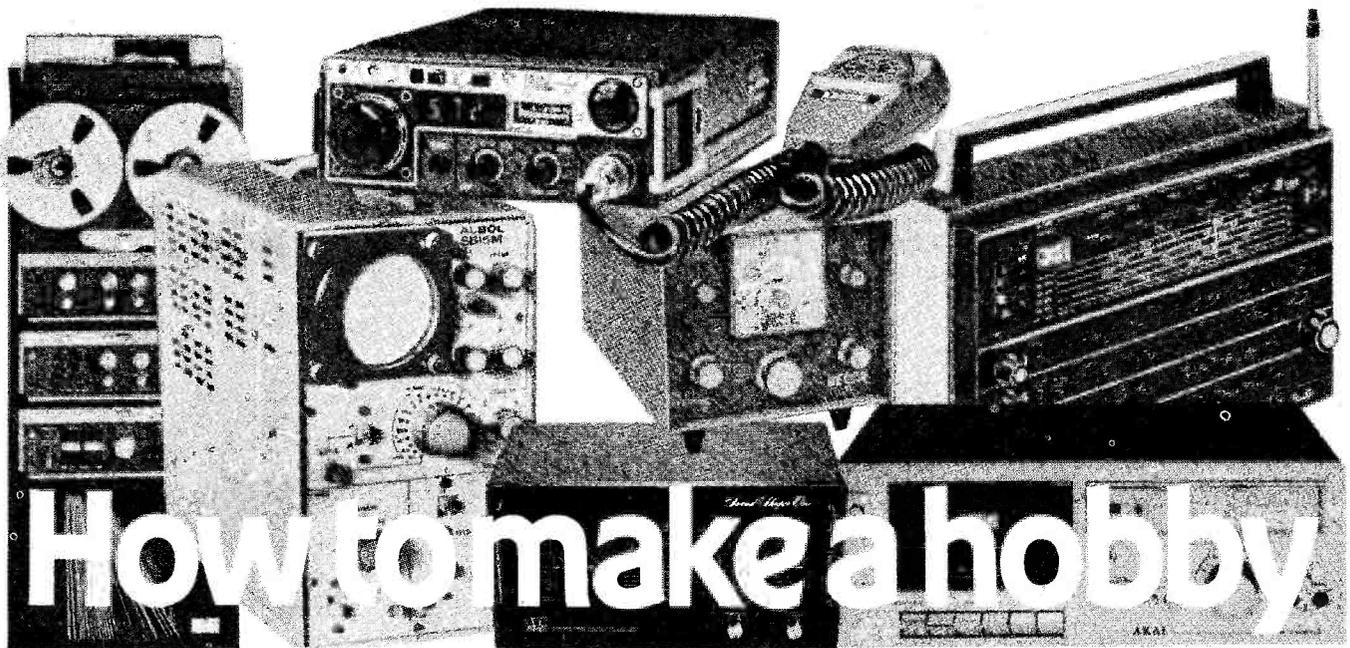
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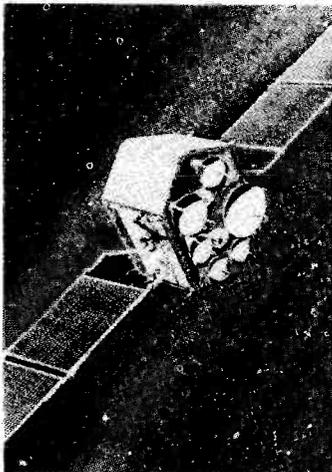
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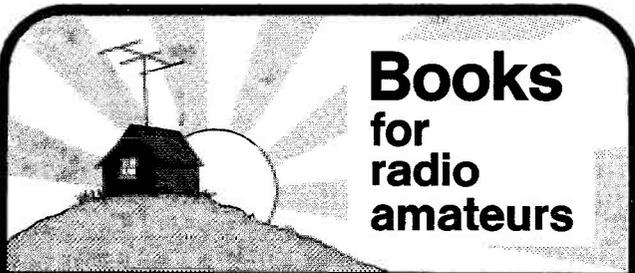
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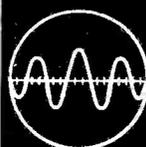
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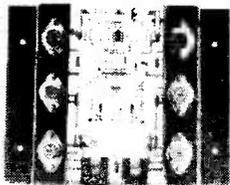


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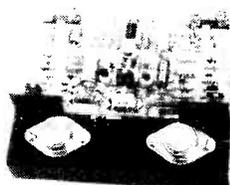
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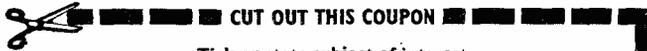


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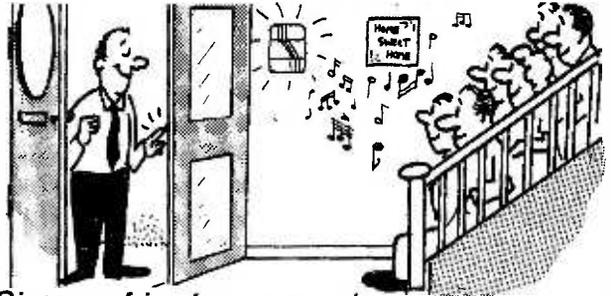
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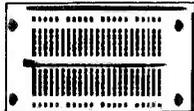
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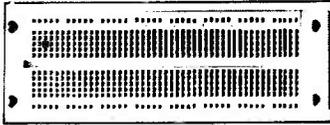
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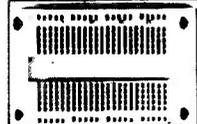
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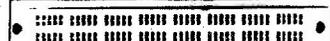
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AA130	£0.10	BY114	£0.25	BY216	£0.47	OA182	£0.15
AA213	£0.17	BY124	£0.25	BY217	£0.41	OA200	£0.09
BA100	£0.11	BY126	£0.17	BY218	£0.41	OA202	£0.09
BA102	£0.37	BY127	£0.18	BY219	£0.41	SD10	£0.07
BA148	£0.17	BY128	£0.18	OA5	£0.69	SD19	£0.07
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162	5 1/2in	4in	1 1/2in	£0.87
163	4in	2 1/2in	1 1/2in	£0.87
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volts		volts		
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Capacity for Confusion

THERE are some electronic components that seem to present few problems in identifying their type and value. The resistor, for instance, since it moved on from its original form of a hexagonal carbon rod with the value stamped on and a screw terminal at each end (in those days it was a *resistance*), has just one universally accepted code, based on colour. Admittedly, those of us who were around at the time had to make the mind-blowing transition from the **Body End Dot (BED)** system (remember the fun of identifying a 2.2k Ω ?) to the Rings system, but at least the basic code has remained the same. And there are mnemonics to help us remember the code: **Bye Bye Rosie, Off You Go, Birmingham Via Great Western** (we're really into the nostalgia bit this month) and others, mostly unprintable!

Capacitors, or condensers for the old hands, have always given difficulty. They originally had the values printed or stamped on, but then someone had the idea of using a colour code. Unfortunately, it didn't stop there, and by the early 1950s reference books were quoting no less than seven different systems of marking capacitors by means of coloured dots. Mullard added yet another system for their C280 "mint humbug" polyester capacitors. Meanwhile, silvered mica, polystyrene and some other varieties continued to have values printed on.

Then came a new problem—capacitors were getting too small to carry all the coloured dots or bands required, so it was back to printed values again, using microscopic lettering. Things had got a lot easier since the old days when, admittedly, "0.00005 MFD" could take up rather a lot of space. With the widespread familiarity with picofarads and nanofarads, a simple unified system could be devised. But did the manufacturers take the opportunity to adopt a common system? Not on your life!

Instead, each seems to have dreamed up his own pet scheme. We now have capacitors marked in pF, tens of pF, nF, decimals of nF, and even a weird system using a numerical version of the colour code so that, for example, a 1 nF is marked 102 (A "1", a "0" and two "0"s=1000pF). Add to this an assortment of other letters which presumably convey tolerance, temperature coefficient, working voltage and the like (maybe even the colour of the operator's socks), and is it any wonder that suppliers and users alike are confused, and equipment manufacturers are driven to devising their own crib sheets to translate the various codes for their own and their customers' benefit?

Incidentally, what does that Russian character which looks like a backward "N" signify on a capacitor? My dictionary tells me it's pronounced eeeeeeee . . .



Joe Bishop—Technical Sub-Editor

After spending the first sixteen years of his life on the same square mile of ground receiving a public school education, Joe reacted by joining first the Merchant Navy and then the Royal Corps of Signals in which he pursued a successful career for over ten years.

As the Irish say, Joe has "something of the travelling man" about him and there followed a period of some years working for a major telecommunications manufacturer as an Installation and Commissioning Engineer, special-

ising in tropospheric scatter, microwave and television broadcast equipment. From snorkel-diving in the Red Sea in July to antenna construction in the North Sea in midwinter, Joe did it all and enjoyed it all before coming finally to earth in his Dorset cottage.

Hobbies have generally been "those consistent with the available amenities" at a number of locations at home and overseas. Now that he has settled down, Joe intends to follow his first loves—good books, writing, concert-going, walking, sailing and "real ale".

R.A.I.B.C.

The Radio Amateur Invalid and Blind Club is currently celebrating its Silver Jubilee.

The Club is formed of invalid and blind members interested in amateur radio; their local representatives who undertake to help by visits, repairs and advice; and supporter members whose financial contributions enable help to be given. The sole condition of membership, in any of the above categories, is an annual subscription of £1 minimum for "Radial" the club newsletter which is issued every six weeks.

Would readers who are interested in joining this very worthy club, please contact: *Mrs F. E. Woolley, Hon Sec, R.A.I.B.C., 9 Rannoch Court, Adelaide Road, Surbiton, Surrey KT6 4TE.*

New Catalogues

Toolrange Limited, the Reading based company who specialise in selling tools and production aids to the electronics market, have just issued their latest 104 page colour catalogue. The new catalogue contains over 2000 lines from some 80 manufacturers.

To obtain your copy of the catalogue apply to: *Toolrange Ltd., Upton Road, Reading RG3 4JA. Tel: (0734) 29446 or 22245.*

Available from Technocentre, a free, convenient pocket-sized electronics construction guide. Comprising nearly 200 coloured photographs and illustrations, circuit symbols and practical tips on mounting and soldering, make this

handy-sized guide of particular interest to beginners, students, etc.

Send s.a.e. to: *Technocentre, 54 Adcort Road, Acklam, Middlesbrough TS5 7ES.*

Suhner have just produced a new edition of their Crimp Technique brochure. As well as giving comprehensive information about their connector crimping system for r.f. cables, the brochure has been updated to include Suhner's range of crimpable connectors. The brochure also gives details about tools, accessories, connectors and suitable cables as well as examining the physical and mathematical concepts behind the process of crimping.

Copies of the catalogue are available free of charge from: *Suhner Electronics Ltd., Telford Road, Bicester, Oxon OX6 0LA. Tel: (08692) 44676.*

Breadboard '79

A larger "Breadboard", with more to see and do, is promised by the organisers, Trident International Exhibitions Ltd., at the *Royal Horticultural Halls, Elverton, Street, Westminster SW1* from Tuesday, 4 December to Saturday, 8 December inclusive.

Breadboard '78 attracted over 10,000 visitors and, once again, U.K. and overseas manufacturers and suppliers of components, tools and test equipment have been quick to take advantage of participating in this particular show.

Over 90 exhibition stands will feature micro-computer systems, analysers, logic test accessories, hi-fi amplifier kits, modulators, etc., as well as a varied range of exciting construction kits and TV games.

Competitions and demonstrations will take place during the show when visitors can participate, among other things, in constructing their own lie detectors and working radios.

For further information contact: *Trident International Exhibitions Ltd., 21 Plymouth Road, Tavistock, Devon PL19 8AU. Tel: (0822) 4671.*

Business News

Drake Transformers has acquired all the transformer interests of Lascar Electronics. The change coincides with the recent move by Lascar into portable instrumentation. Both parties express themselves as well pleased with the move. Peter Rowling, Drake MD explains: "Although long established as a high-quality manufacturer of OEM transformers, this acquisition gives us the opportunity to introduce a standard range of 'off the shelf' transformers. All Lascar services will continue, and we intend to ensure that no customers are inconvenienced by the changeover."

Details of the Drake standard range and services can be obtained from: *Drake Transformers, Kennel Lane, Billericay, Essex. Tel: (02774) 51155.*

Latest from Trio

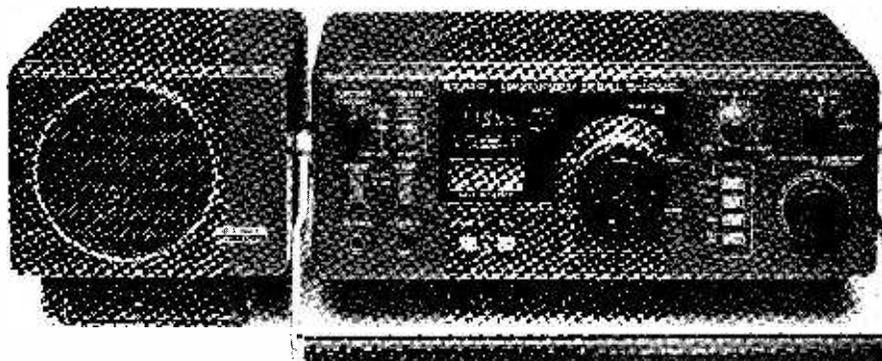
Lowe Electronics inform us that they now have the latest communications receiver from Trio in stock.

The R-1000 is a high class general coverage receiver covering 30 bands between 200kHz and 30MHz with a p.i.l. synthesiser that incorporates all of Trio's sophisticated electronic technology developed over recent years.

Both digital display readout (1kHz resolution) and analogue display (10kHz resolution) are provided for easy and accurate tuning.

The R-1000 also includes a quartz digital clock with timer, three i.f. filters, r.f. attenuation and tone control, etc., to ensure the best receiving conditions for each mode.

Due consideration has been given to innovative design and compactness,



making the R-1000 an excellent station receiver for amateur radio operators, professionals, broadcast and short wave listeners, etc.

The R-1000 costs approximately £300 retail and as soon as we are

able *Practical Wireless* will produce a "Radio Special Product Review" on the R-1000.

Further details from: *Lowe Electronics Ltd., 119 Cavendish Road, Matlock, Derbyshire DE4 3HE. Tel: (0629) 2817.*

AERIALS for 160 Metres

PART 2

J.R.GREEN G3WVR

Vertical aerials for low-frequency ground-wave propagation have been a topic of keen interest to the author for many years. In particular, due to their sheer impractical size, the question of optimum loading is paramount in their design.

Theory

To avoid making the theoretical argument unnecessarily complicated, the basis of this section rests on two simple formulae which provide a good approximation to more complex methods:

$$\text{Aerial Efficiency} = \frac{R_{\text{RAD}}}{R_{\text{RAD}} + R_{\text{DC}} + R_{\text{G}}} \dots \dots \dots (1)$$

where R_{RAD} = The radiation resistance of the aerial (dependent on useful length and height);

R_{DC} = The ohmic d.c. resistance in all wire, coils, and radials;

R_{G} = Ground losses, i.e., Earth resistance.

Near Field Strength E (mV/metre)

$$= \frac{377 \times I_a \times h_e}{\lambda \times D} \dots \dots \dots (2)$$

where I_a = Aerial current at the base of the aerial (amps);

h_e = Effective height of the aerial;

λ = Wavelength;

D = Distance from aerial (kilometres).

Equation (2) is taken from the ITT *Reference Data for Radio Engineers*. Note that h_e and λ must be in the same units.

Effective Height

The Effective Height (h_e) of a grounded vertical aerial is equal to the height of a vertical wire producing the same vertically polarised field as the actual aerial, provided that the vertical wire carries a current that is constant along its entire length and of the same value as the current at the base of the actual aerial. For the more mathematically minded, $I_a \times h_e$ is the value of the integrated sinusoidal current in the actual aerial of physical height h .

The diagram Fig. 6 shows clearly how this definition makes sense, the areas "A" and "B" being equal for the correct value of h_e . Typically, h_e would range from 0.5 h for a very short vertical aerial, such as a base-loaded whip, to 0.66 h for a quarter-wave vertical.

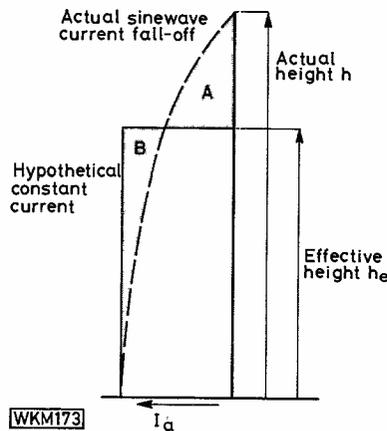


Fig. 6: Relationship of Actual Height and Effective Height of a $\lambda/4$ vertical aerial. Areas "A" and "B" are equal

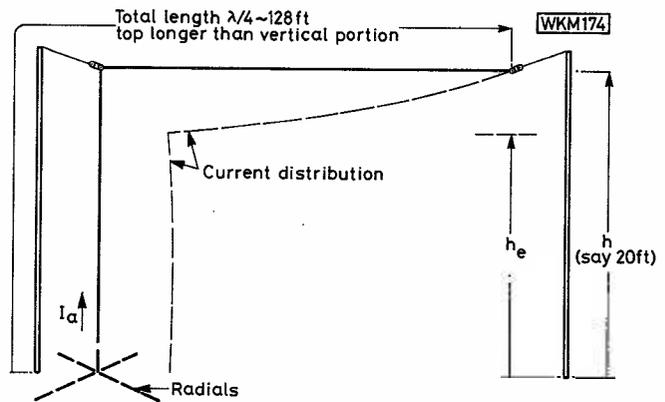


Fig. 7: Current distribution and Actual and Effective Height relationship for an Inverted "L" aerial

Practical Implications

On the basis of theory, we may assume that:

1. From Equation (1), we require a large R_{RAD} (which means a large aerial, and a small R_{DC} (which means thick, heavy wire) and a small R_{G} (which means a field full of radials).
2. From Equation (2), both I_a and h_e should be as large as possible.

These implications are not really very "practical" at all, but we can at least examine them to make the best use of

what facilities are available. Let us first consider a commonly used amateur aerial, the Inverted "L". The diagram Fig. 7 shows a typical inverted "L" whose top section is much longer than the vertical section, and hence the current distribution is almost constant along the vertical portion. This gives an effective height h_e which is nearly equal to the actual height, i.e., about 18ft, which is very poor compared with, say, a $\lambda/4$ vertical, whose effective height would be $128 \times 0.66 = 84$ ft, but better than a 20ft short vertical, whose h_e would be only 10ft.

As regards radiation resistance, the inverted "L" is fairly good (i.e., high) because of its $\lambda/4$ length, but poor in respect that most of its radiation is horizontally polarised and very high-angle due to its low height.

The vertically-polarised radiation could be reduced by top loading in a non-radiating way. This will reduce the radiation resistance, thereby increasing I_a in the vertical portion, and a greater vertically-polarised field strength will result, although the actual aerial efficiency is lower.

For the standard inverted "L", we might have

$$R_{\text{RAD}} = 30\Omega, \quad R_{\text{DC}} = 5\Omega, \quad R_G = 20\Omega$$

giving:

$$\text{Efficiency} = \frac{30\Omega}{30\Omega + 5\Omega + 20\Omega} = 55\%$$

and an effective height of 18ft.

The first step towards increasing I_a without worsening h_e is to use "T" top loading, as shown in Fig. 8. Note that the current distribution splits at the top of the vertical radiator and, to a first approximation, cancels out. This eliminates horizontally-polarised radiation and reduces the radiation resistance, increasing I_a and actually increasing the vertically-polarised field strength.

Note that the efficiency might now be, say:

$$\frac{20\Omega}{20\Omega + 20\Omega + 5\Omega} = 45\%$$

but the higher value of I_a still has the desired effect.

LC Top Loading

The aerial may now be made more compact by using a smaller top composed of multiple wires to increase the capacitance, plus a top-loading inductor to bring the system to resonance, as shown in Fig. 9.

A large capacitance C is preferable, since then less inductance L is required and hence there is less loss (R_{DC}) in the L , and a wider bandwidth in the resonant frequency due to the lower Q of the system.

The top section should be symmetrical if possible, in order to cancel horizontally-polarised radiation. Since the actual vertical portion will be small compared with a quarter wavelength, the LC resonant frequency on its own will be only slightly higher than the overall aerial resonance, which is reduced by the extra radiator inductance.

Hence, it has been shown that top loading, although nominally not improving overall antenna efficiency, can usefully channel "wasted" horizontally-polarised radiation into improved vertically-polarised radiation, although I daresay that many users of inverted "L" aerials do not consider the horizontal component to be wasted!

Improving Aerial Efficiency

By improving the efficiency we could, of course, improve the radiated field strength still further, since all we have done so far is to make the radiated energy all vertically-polarised. We must now consider the d.c. and ground losses.

The d.c. resistance losses are usually the least of our problems, since they are generally very low. However, the

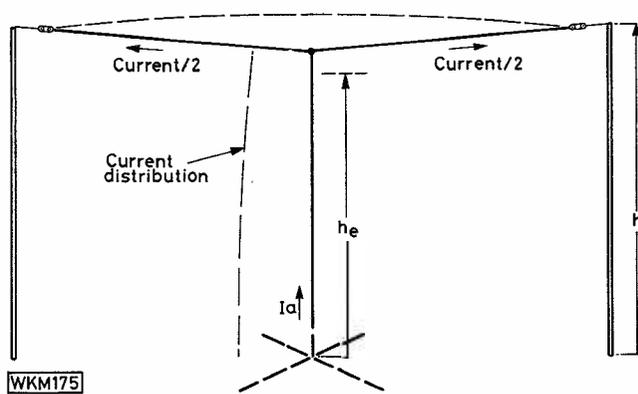


Fig. 8: Current and height relationship for a "T" aerial

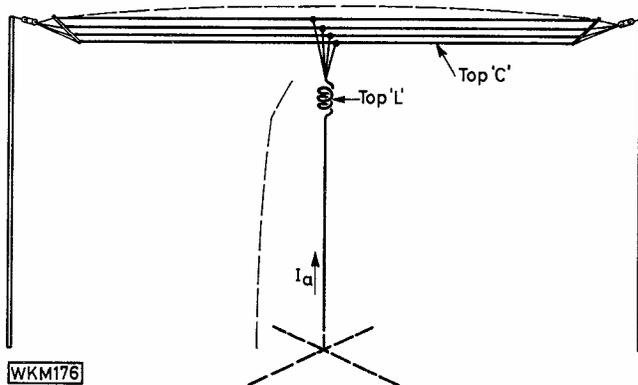


Fig. 9: A "T" aerial with multiple top span giving added capacitance loading, and top loading inductance

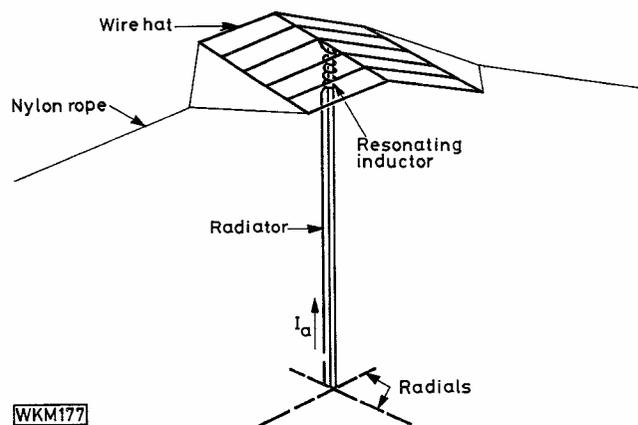


Fig. 10: Top-hat loading for a single guyed mast aerial. For maximum efficiency, the guy ropes should be led down at the shallowest possible angle, so that the top hat encloses the minimum amount of the vertical radiating element

use of a large capacity hat of reasonably thick wires plus an inductor wound from the thickest available wire (consistent with weight constraints) is advised, with the actual radiator constructed from coaxial cable braid, or aluminium tubing salvaged from Band I TV aerials or Band II f.m. aerial booms.

In view of the weight involved, the system may be adapted to a single guyed mast as shown in Fig. 10. The ground

Comparison of an "Ideal" and a Practical Aerial

Ideal $\lambda/4$ Vertical

Actual height (h) 128ft
 Effective height (h_e) 84ft

$$\begin{aligned} R_{\text{RAD}} &= 37\Omega \\ R_{\text{DC}} &= 0\Omega \\ R_{\text{G}} &= 0\Omega \end{aligned}$$

Efficiency = 100%

Practical Vertical

Actual height (h) 38-40ft
 Effective height (h_e) 35ft

$$\begin{aligned} R_{\text{RAD}} &= 10\Omega \\ R_{\text{DC}} &= 2\Omega \\ R_{\text{G}} &= 10\Omega \end{aligned} \left. \vphantom{\begin{aligned} R_{\text{RAD}} \\ R_{\text{DC}} \\ R_{\text{G}} \end{aligned}} \right\} \text{ approx.}$$

Efficiency = say 45%

Aerial current for 7W r.f. input to aerial system (i.e., 10W d.c. input to transmitter p.a.)

$$\begin{aligned} W &= I_a^2 R_{\text{total}} \\ I_a &= \sqrt{\frac{W}{R_{\text{total}}}} \\ &= \sqrt{\frac{7}{37}} \\ &= 0.435\text{A} \end{aligned}$$

$$\begin{aligned} W &= I_a^2 R_{\text{total}} \\ I_a &= \sqrt{\frac{W}{R_{\text{total}}}} \\ &= \sqrt{\frac{7}{22}} \\ &= 0.565\text{A} \end{aligned}$$

Note that I_a is higher for the top-loaded vertical since R_{total} is lower. This helps to compensate for its reduced efficiency

Field strength at a distance D of 1km

$$\begin{aligned} E &= \frac{377 \times I_a \times h_e}{\lambda D} \\ I_a &= 0.435\text{A} \\ h_e &= \frac{2}{3} \times \frac{\lambda}{4} \\ E &= \frac{377 \times 0.435 \times 0.67 \times \lambda}{\lambda \times 1 \times 4} \\ &= \frac{377 \times 0.435 \times 0.67}{4} \\ &= 27\text{mV/metre at 1km} \end{aligned}$$

This is the "ideal" best possible figure

$$\begin{aligned} E &= \frac{377 \times I_a \times h_e}{\lambda D} \\ I_a &= 0.565\text{A} \\ h_e &= \frac{35}{128} \times \frac{\lambda}{4} \\ E &= \frac{377 \times 0.565 \times 35 \times \lambda}{\lambda \times 1 \times 128 \times 4} \\ &= \frac{377 \times 0.565 \times 35}{512} \\ &= 14.6\text{mV/metre at 1km} \end{aligned}$$

This is a "practical" realisable figure

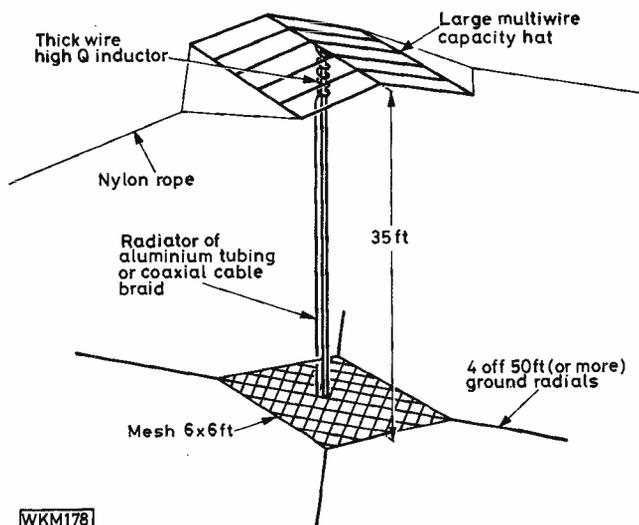


Fig. 11: More practical details of the author's top-loaded vertical aerial and the associated ground-plane

losses, however, usually present the major headache in terms of aerial efficiency, because not many amateurs have a convenient field in which to bury the recommended 200 or so $\lambda/2$ radials which a medium wave broadcast station, for example, would use with its aerial.

A very ancient radio data book studied by the author some years ago suggested that 4 radials, instead of 200, would reduce the field strength to around half of the theoretical maximum, and a commonsense deduction suggested also that the radials need be no longer than the actual physical height of the radiator.

Experiment has shown that four 50ft radials offer quite a good ground, certainly much better than an earth stake, and if these cannot radiate in all directions from the aerial

continued on page 56 ▶▶▶

Wing Commander John Scott-Taggart OBE MC

Born 27 May 1897

One of the best-known pioneers of radio, John Scott-Taggart died at the end of July 1979. He was recognised as one of the founding fathers of the wireless valve era and a powerful force in initiating broadcasting and establishing a large audience for it in its early days. As author of many textbooks and articles, as well as papers read before learned societies, he both popularised radio and made serious contributions to its development. His first article appeared in *Wireless World* in December 1914.

He joined the army at 17 and served in France from the first battle of the Somme, later becoming Instructor in Wireless to the 1st Army. In 1917 he began his thirteen articles in *Wireless World* which educated the public and technicians in the revolutionary effect on radio of the valve.

In 1918, as wireless officer of the 55th Division, he was Mentioned in Despatches and later won the Military Cross. Also in 1918, he obtained the first of some thirty patents; some of these were of the greatest importance and were sold to leading companies in the radio and cable industries.

After the first world war he joined Ediswan and subsequently Radio Communication Co. As Head of the Patent Dept of that company and of Mullard he was chiefly responsible for the successful defence of a patent action brought by Marconi's and thus prevented a valve monopoly.

In 1921 John Scott-Taggart published a standard textbook entitled *Thermionic Tubes in Radio Telegraphy and Telephony*. In 1922 he founded Radio Press Ltd and successively launched five radio periodicals which contributed very greatly to establishing an audience for the BBC. His set design ST100 alone was built to the extent of 100 000 by amateurs.

In the winter of 1926/27 he sold his publishing interests to Amalgamated Press Ltd, and became chief wireless patent consultant to several world-famous companies. He was called to the Bar in 1928. At this period of his life he qualified as an amateur pilot.

From 1932, Amalgamated Press employed him for five years as chief designer and contributor on a free-lance basis. His annual set designs ST300 to ST900 were built in hundreds of thousands. In 1935 he was elected Fellow of the Institute of Radio Engineers, and he was also a fellow of the Institute of Electrical Engineers, the Institution of Mechanical Engineers and of the Institute of Physics.

In May 1939, foreseeing events, he obtained a commission in the RAFVR, going to France on the second day of the war. Returning later to England, he was chosen to take a course in radar. In late 1939 he went to France to command a radar station. He left just before Dunkirk, having been Mentioned in Despatches for gallant and distinguished service.

On return to England he commanded a Battle of Britain radar station and subsequently became responsible for all radar training (ground and air) in the RAF, and then for the installation and maintenance of all the CH (Chain Home) radar stations in the UK—the chief radar defence system in this country—and several coastal stations serving the Royal Navy. He obtained his third Mention in Despatches.

After the war, John Scott-Taggart joined the Admiralty Signal and Radar Establishment (later named Admiralty Surface Weapons Establishment) as a technical civil servant, retiring in 1959. He wrote many technical manuals for the Royal Navy.

After retirement, John Scott-Taggart actively pursued his interest in art matters, both as collector and author of books. In 1962 the President of Italy appointed him a Knight Officer of the Italian Order of Merit for services to art. In the New Year Honours List in 1975 he was appointed OBE for services to radio engineering.

Stanley Robert Mullard MBE (MIL)

Born 1 November 1883

Stanley Robert Mullard, one of the pioneers of the UK radio industry, died in a Sussex nursing home on September 1, at the age of 95.

He was born on 1 November 1883 and, after attending a local school and the Borough Polytechnic, joined a firm of electric lamp manufacturers. He continued his studies at the Northampton Institute (now the City University) and became a student member of the Institution of Electrical Engineers in 1903. His employers appointed him a director of the company when he was only 24.

Later he joined the Ediswan Company. In 1915, while working in the lamp research laboratory, he developed the "Pointolite" arc lamp which was used in projection apparatus for over 40 years.

At the start of the first world war Mullard enlisted in the Engineers' Battalion of the Royal Naval Reserve, but continued his work with Ediswan at the Admiralty's request. His interests now extended to radio valves. His wide knowledge of glass technology and vacuum techniques enabled him to make valuable contributions to the fast-growing use of valves in military radio equipment.

In 1916 he was commissioned as a lieutenant in the Royal Naval Volunteer Reserve, posted to the Royal Naval Air Service and put in charge of a special valve laboratory at Imperial College, London. He also attended meetings at the HM Signal School, Portsmouth, to assist with the design and production of high-power transmitting valves. It was largely due to his participation that the manufacture of silica types became practicable and by the end of 1919 there was a pressing demand for them for Naval purposes.

It was on the strength of an order for 250 valves that he was able to raise capital required to form the Mullard Radio Valve Company in September 1920. Although this company was started primarily to make high-power transmitting valves, it quickly became involved with the production of smaller types. Public interest in "wireless" was quickening. Many ex-army signallers obtained licences to operate low-power transmitters and were also building their own receivers. Public broadcasting had not yet commenced, but it was possible to pick up private and commercial transmissions from Hilversum, Paris and Berlin.

The start of a public service brought a great demand for reliable valves and, appreciating the enormous potential, Mullard turned over part of his limited manufacturing facilities to the production of small receiving types. They were sold under the trade name ORA, signifying the valve's three main functions: to Oscillate, Rectify and Amplify. Output quickly rose to thousands a week. Demand soon out-stripped manufacturing capacity and larger premises were acquired. These, too, became inadequate when the BBC opened its London transmitter, 2LO, and in 1923 Mullard moved again, this time to Nightingale Lane, Balham. By the end of 1924 production had reached 2½-million a year and by demonstrating that reliable valves could be made cheaply Mullard helped materially to lay the foundations of the British radio industry.

By this time the commercial side of Mullard's activities had become important and he established a second company, the Mullard Wireless Service Co., to handle marketing and distribution. From its London headquarters it published a magazine, *Radio for the Million*, which made an immediate impact. It appeared quarterly for the next two years and sold in millions of copies.

In 1927, with the continuing increase in valve demand, production was moved to a still larger factory at Mitcham, Surrey. This remains one of the company's manufacturing plants, turning out more sophisticated components, but still handling the production and repair of high-power silica valves.

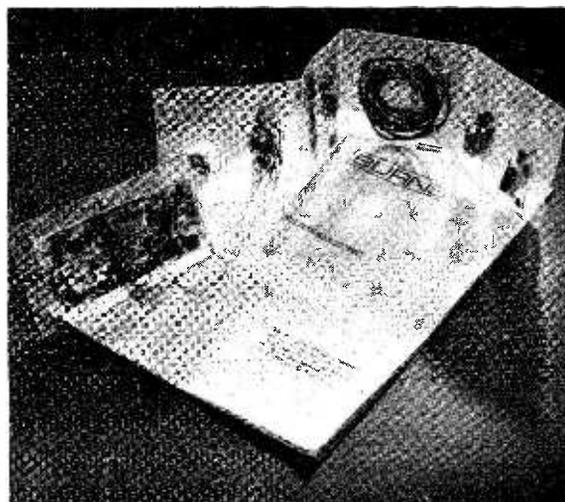
Impending developments in valve technology began to call for research facilities beyond the scope of a company so young as Mullard's. This demand led to the establishment in 1924 of close links with N.V. Philips of Holland and over the next few years Philips acquired all the shares of the company.

In 1929 Mullard resigned as managing director, but continued as a director, actively interesting himself in the company's affairs until its golden jubilee celebrations in 1970.

Stanley Mullard lived to see the small venture he founded grow to an organisation employing more than 11 000 people and occupying a leading place in the world's electronics industry.



FMD-7 FM DETECTOR MODULE



The FMD-7 is an f.m. detector designed originally for the FRG-7/FRG-7000 series of receivers, but it may be used with any receiver that has an intermediate frequency of 455kHz. The module contains a buffer stage to isolate any s.s.b./a.m./c.w. filters in the receiver from those in the FMD-7, two ceramic filters to give adjacent channel selectivity, a multi-function integrated circuit type MC3357P providing high gain, signal limiting, quadrature f.m. detection and squelch, plus output audio filtering and a low power d.c. regulator. Facilities are provided for an external tuning meter and a squelch disable switch.

★ specification

Sensitivity: 20dB S/N ratio for an input of 10 μ V at 455kHz deviated \pm 3kHz at 1kHz
Limiting Threshold: 10 μ V
Limiting Characteristic: \pm 1dB change in output level for 20 μ V - 100mV input
Maximum Deviation: \pm 5.5kHz for 10% distortion
Selectivity: -6dB at \pm 10kHz from 455kHz
 -56dB at \pm 25kHz from 455kHz
Audio Frequency Response: -3dB at 300 and 3000Hz relative to 1kHz
Squelch: S/N ratio operated. May be preset to fully open at 15dB S/N
Audio Frequency Output Level: 800mV peak to peak for \pm 5kHz deviation
Power Supplies:
 8 - 16V d.c. at 6-12mA at pin N (main)
 8 - 16V d.c. at 1-3mA at pin C (buffer)
Temperature Range: 0° to +70°C
Dimensions: Printed circuit board 51 x 112mm (2 x 4.4in)

Assembly

All parts for the module come packed in stout polythene envelopes. The kit is complete, right down to mounting hardware and wire—all you need is solder and the necessary tools. The printed circuit board is single-sided, epoxy-glass and has all the component locations and references silk-screen printed in white. The only drawback found is that most of the references are covered up once the components have been inserted, making it difficult to locate an item if subsequent fault-finding should be required. It would be a good idea to print the layout in the handbook as well.

Assembly of the module took just on two hours, and no major snags were encountered. Those that were, resulting from a few errors in p.c.b. drilling, were easily overcome. I think that it would have been easier to insert the terminal pins before fitting the remainder of the components, rather than afterwards.

Installation

The review module was installed in an FRG-7, and this proved to be far more time-consuming than assembly, taking some three-and-a-half hours altogether. Fitting details are given in the handbook for the FRG-7, FRG-7000, Lowe SRX-30 and Drake SSR-1, plus general guidance on other receivers, including valved types, for which a special power supply module is available, if necessary.

Most of the installation time was spent in positively identifying the components and links which have to be removed from the host receiver before the module can be connected. Even after years of experience in carrying out mods on professional equipment, I still approach the first one of a new type somewhat heart-in-mouth, and cross-check about three times before cutting or removing anything!

continued on page 36 ▶▶▶



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U.K. MAIN DISTRIBUTOR

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Deluxe Communications Receiver.
See review in the November issue

FRG7000 £375

In addition to offering an enormous range of major communications equipment, masts and antennas SMC are proud to be your single stop source for all those necessary but often hard to get accessories, some of which we list below.

COAX PLUGS UHF (Post and Packing £0.20) + VAT 15%	
PL259 Standard UHF plug	£0.48
UG175/U Reducer UR43	£0.12
UG175/U Reducer UR70	£0.12
PL259R "Reduced" plug to UR43	£0.58
PL259SL "Solderless" UR67	£0.55
PL259SS "Solderless" UR43	£0.55
PL259P Push-on plug	£0.89
PL259E Elbow plug UR43	£0.83
Panel mount PL259	£0.93
S0239F 4 hole socket	£0.42
S0239T 2 hole socket	£0.42
S0239NI Socket "nut" inside	£0.51
S0239NO Socket "nut" out	£0.51

COAX PLUGS BNC (Post £0.20) + VAT 15%	
UG68 Plug, Std UR43	£0.54
UG659 Plug, Large UR67	£2.66
UG291 Socket, 4 hole std	£0.56
UG1094 Socket, Nut fixing	£0.56
UG68 Socket, Free, UR43	£0.72
UG614 Double female	£0.93

LIGHTNING ARRESTORS COAXIAL (Post £0.30) + VAT 15%	
SM566 Spark, S0239/PL259	£2.55
SM567 Spark, S0239/S0239	£2.55

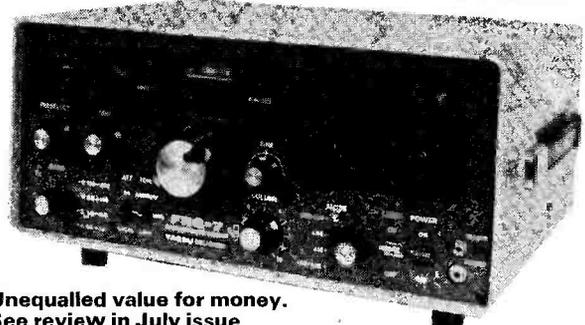
WIRE & BRAIDS (Post and Packing extra) + VAT 15%	
7/029H Cu Hard Drawn	yd £0.15
7/036H Cu Hard Drawn	yd £0.18
7/044H Cu Hard Drawn	yd £0.24

CABLES RF FEEDERS (Carriage extra) + VAT 15%	
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UR43 50Ω 0-2" Solid	yd £0.19
UR76 50Ω 0-2" Stranded	yd £0.19
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R6213 50Ω 0-405" Heavy	yd £0.47
306 300Ω Ribbon	yd £0.13

AERIAL INSULATORS (Post Extra) + VAT 15%	
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Unequalled value for money.
See review in July issue

FRG7 £215

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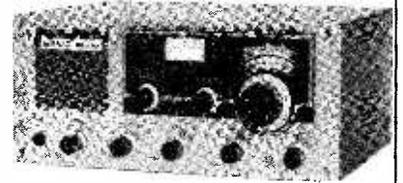
STOP! . . . THIS IS WHERE SHORT WAVE LISTENING BEGINS



£214 inc. VAT

THE SHOP THAT
SPECIALISES IN HAM RADIO

RECEIVERS – TRANSMITTERS
TRANSCEIVERS – HF – VHF – UHF



£178 inc. VAT

This month we present to you two excellent short wave receivers that give you top value for money. In July we mentioned how the FRG7 was the perfect receiver for both the beginner and experienced listener or radio amateur alike. And, of course, our many hundreds of satisfied customers know that we have a special test schedule that every receiver has to pass before it is despatched to its proud new owner.

We can now tell you that we are stocking the latest version of the Lowe SRX30 receiver. Now this receiver is very similar in many respects to the FRG7. In fact, electrically, there's not a great deal of difference between the two receivers. In other words, the ability of the SRX30 to pull the stations in is every bit as good as the FRG7. But there is a difference. It's not quite so pretty as the FRG7 but electrically it's every bit as good – both models are in stock for immediate free Securicor despatch.



**AND NOW
VHF!**

Yes, the TM56B receiver is ideal for home and car, having both 12v DC and 240V AC mains supplies built-in. We've already sold hundreds. It covers all the popular amateur VHF channels and repeaters. It also features automatic scanning of up to 4 channels of your choice. The amateur band version is £106. We can also supply a marine version with 10 channels fitted at £115 – as used by coast guards and river pilots, etc.

STOP PRESS

NEW R-1000 receiver is the latest receiver from Trio. 200KHz-30MHz and digital readout at a very realistic price. Send 10p stamp for full details.

Opening hours **MON-SAT 9.00 a.m.-5.30 p.m. E.C. Wed 1.00 p.m.**

WATERS & STANTON ELECTRONICS

18-20 MAIN ROAD, HOCKLEY, ESSEX. TEL: HOCKLEY (03704) 6835

TRIO R-1000 Stand by to receive the world

It's goodbye Wadley loops and hello to the new, true up-conversion, PLL system HF general coverage receiver from Trio.

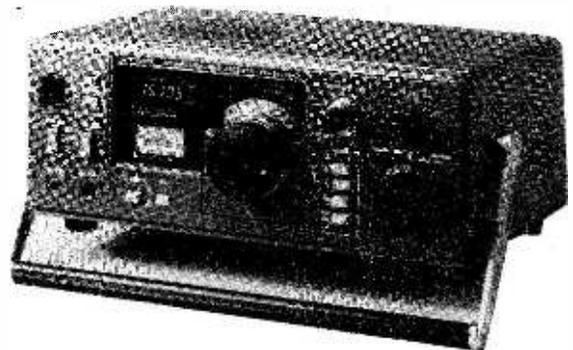
The new R-1000 is going to turn the general coverage receiver world upside down since it combines professional performance with a really attractive price, thanks to Trio's commitment to using advanced technology to simplify operation rather than make complex gimmickry.

The R-1000 uses an advanced PLL system in an up-conversion scheme to a high (48MHz) first IF to remove any possibility of image responses. The receiver covers the entire frequency range from below 200kHz right up to 30MHz in 30 bands, each 1MHz wide. The bands are selected, not by ambiguous knob twiddling as in receivers using the Wadley loop but by a 30 position band switch which controls the PLL system.

The band switch also electronically selects the appropriate band pass filter network in the RF stages of the receiver so there are no "preselector" or "antenna trim" controls to twiddle – simply set the band switch to the range required – that's it!

A highly stable VFO tunes each 1MHz range and its linear, back lit scale makes readout easy. However, in addition to this dial, Trio have also provided 5 digit true frequency digital readout so as to guarantee spot on accuracy on any frequency. As a further feature, the digital display can also be switched to read time, this being derived from a quartz standard. Marvellous for accurate log keeping. The display uses high intensity readout units which can be dimmed for use in low light conditions.

As for what else is inside this superb instrument – selectivity is catered for by three custom made IF filters; a 12kHz wide AM filter; 6kHz narrow AM filter; and a new 2.7kHz SSB filter with a shape factor of better than 1:2 6:60dB. Selectable sidebands are available at the touch of a switch.



For the first time in a mid price receiver, a true noise blanker is provided to remove pulse type ignition noise.

To minimise front end overload, a step RF attenuator is included which gives 0–60dB attenuation in four steps.

All the rear panel connectors are recessed on a sloping panel so that you can stand the receiver either on its back, or pushed hard against a wall when used in conventional shelf mounting. The antenna inputs allow the use of either a high impedance wire aerial or a 50ohm balanced input so that the proverbial long lump of wire will work really well with the R-1000.

Almost forgot – the R-1000 will work from either 12V dc or any mains supply from 100-240V 50/60Hz so you can really take it anywhere with you.

The basic features of the R-1000 do not tell the full story, because you cannot explain the superb "feel" of the receiver until you can handle it in the flesh. So, the advice is to see it soon at Lowe Electronics in Matlock.

For all that's good in Amateur Radio, contact:

LOWE ELECTRONICS LTD., 119 Cavendish Road, Matlock, Derbyshire. Tel: 0629 2430 or 2817.

For full catalogue, simply send 50p in stamps and request catalogue CPW.

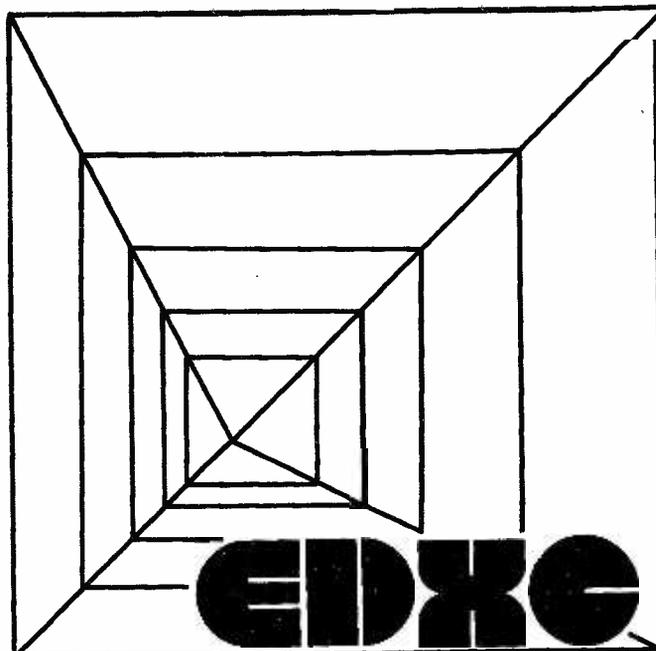
The European DX Council was formed 13 years ago in Copenhagen by a group of DXers and Short-wave Listeners who felt that co-operation between DX Clubs in various countries in Europe could be of mutual advantage. Since then it has succeeded in linking together over 20 clubs within Europe, and organising an annual conference where DXers can have an opportunity to meet fellow listeners and also broadcasters.

Since April 1979, the headquarters of the council has moved from Bochum in West Germany, to St Ives, Huntingdon, in England, from where all projects are now centrally organised. Clubs outside Europe are eligible for observer status with the EDXC, and the organisation also co-operates closely with its North American counterpart, the Association of North American Radio Clubs (ANARC). EDXC is currently undertaking a number of research projects.

Receiver Information Bank

The Receiver Information Bank is probably the most ambitious project ever undertaken by the EDXC and aims to serve the individual DXer or short-wave listener. In August 1979 a questionnaire was sent out to all registered DX clubs in the world, with the request that it be reprinted in their club bulletins. By this means EDXC has managed to reach a potential of around 40 000 DX magazine readers. In addition, an extensive publicity campaign in a variety of languages was launched to run concurrently in the DX programmes of various s.w. radio stations. These short "spots" warned listeners to look out for the questionnaires and to fill them in. Non-DX Club members were invited to write in to the central address in Huntingdon for a copy of the questionnaire. Response from these requests for help has been very encouraging.

The questionnaire is designed to appeal both to the technical and non-technical SWL. It is interesting to note that non-technical listeners often are not using their receiver properly due to poor instruction booklets, while the more technically minded report persistent or common faults with particular models.



A close dialogue has been established between the EDXC and 15 radio manufacturers, and it is planned to pass on the results of the survey to the designers of the various sets for their attention. In addition, using outlets in DX programmes on Austrian Radio, Radio Nederland, AWR Sines, and BBC (Finnish Section), the EDXC plans to report on new models and compare the various sets on the s.w. market.

EDXC is primarily concerned with broadcast band listening. It does not cover amateur band or utility DXing.

Results will be sorted by a computer into various files. Each file will deal with a particular set and contain (1) A manufacturer's brochure; (2) A circuit diagram; (3) Details of any modifications that are possible; (4) Extracts from reviews; (5) User comments on reliability, servicing, and "usability". It is expected that such files will be available in early 1980 and will cost the price of return postage. Comparative tests on sets in the same price category will be undertaken later.

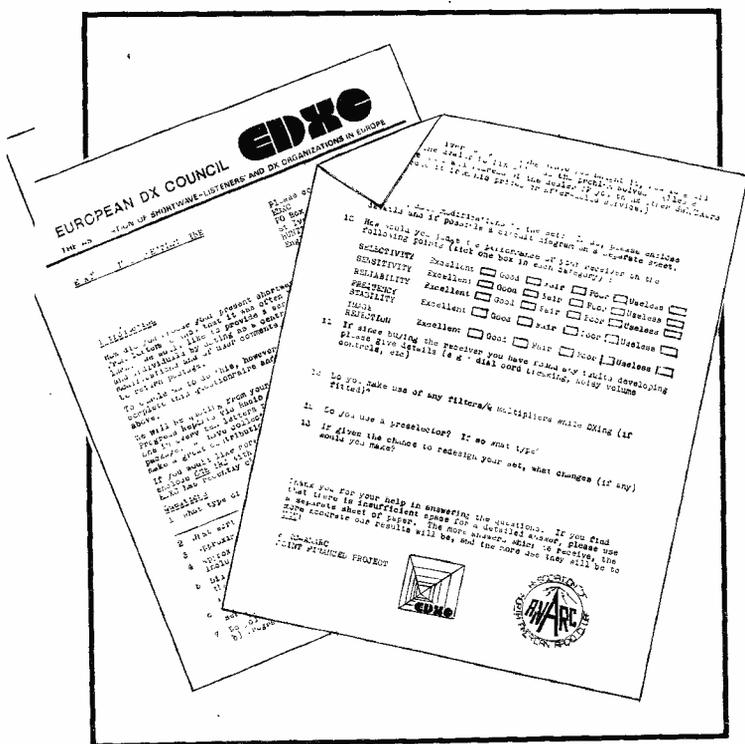
For a copy of the questionnaire, drop a line to: EDXC, P.O. Box 4, St Ives, Huntingdon, England PE17 4FE, enclosing a stamp if possible. EDXC is a volunteer organisation.

QSL Survey

In August a multiple choice questionnaire was sent out to 57 s.w. radio stations, all of whom have a foreign service. Its purpose was to establish whether or not reception reports are still of use to them, now that many stations rely on technical monitors who are paid for their work. The results of this survey will be made known as soon as possible.

EDXC-HAP Co-operation

In future, EDXC will act as the central mailing address for the Handicapped Aid Programme—UK organisation in order to simplify the address. In addition, all the stamps on mail to EDXC are being saved for HAP-UK to raise money and the EDXC publicises any projects that HAP-UK organise. John Rose remains as HAP-UK chairman.●



Throw-away Computers

Comedians commonly use throw-away lines, but now electronics has turned to throw-away computers. The new concept is the brain child of a computer manufacturer who is intent on marketing a computer that is designed to have faulty parts thrown away.

The machine (a 16-bit model) is made up of plug-in boards each carrying a separate function. Each board measures roughly 210 x 160mm and has light-emitting diodes on its outer edge, wired in as go no-go indicators. Every time the machine is switched on, a self-diagnostic routine is initiated which tests all circuitry on each of the boards. Any fault that's located causes the no-go diode on the appropriate board to light. The board is then unplugged and thrown away. A new board is plugged in and the system is again fully operational. New boards are reckoned to cost around \$200.

If this trend catches on, I can see piles of boards stacked up 100's deep in Lisle Street—just like T1154 and T1155's used to be in the old days.

Printers Again

Electronic printers are becoming big business, and the latest one could prove extremely useful in both amateur and professional field. Called the VP-850 it uses c.r.t. signals (in a scope etc) directly to drive the print head matrix. Thus whatever is displayed on the screen would be printed out on a roll of electrosensitive paper in the printer.

In operation, the printer takes the analogue signals direct from the c.r.t. gun and samples each raster line 1350 times until it has stored 24 complete raster lines in its RAM. The data, which has now been converted to digital data, is fed to activate the printing head. Costs around \$1200 were rumoured in the US.

Cheapies

Just when I thought that electronic calculators couldn't get any cheaper, I find I'm deluding myself. In absolute cheapness the local store selling a four function machine for less than £4.00 is approaching the limit. But for sheer value the battle appears to be far from over.

Newest and "bestest" to arrive is the Slimline T1-35. In addition to doing so many things (I just couldn't list them all; it's a 54 function calculator!) it also offers keys for finding mean and/or standard deviation for samples and population data. And there's a factorial key. The price of this 54 function machine is to be around \$25. Eventually, the batteries will cost more than the calculator!

Speaking chips

There's chips and there's chips, but the latest one to hail from Japan is going to take a lot of beating. So new it hasn't got a reference number, this one is a speech synthesiser—all on one chip. This miniature marvel codes and decodes human speech by analysing it into sound source parameters (this corresponds to the human vocal chords) and into filtering parameters (corresponding to the roof of the mouth). Onto a piece of silicon measuring less than 3.7mm square, the manufacturers have managed to get 3500 gates, a 2240-bit ROM, and a 350-bit RAM. Wonder how many you could get in the boot of a Mini?

Scribble

If you dislike licking gum on envelopes every time you post a letter, then your aversion may be in for some assistance. It could come under the intriguing title of "Scrib". This comprises a very novel typewriter that also has a few other tricks it can perform—like word processing, storage of letters and articles (or whatever) on magnetic tape and the ability to transmit your treasured words over the telephone at around 30 characters a second. The self-contained Scrib has its own video screen so that you can see just what you are typing, letter at a time. You can erase or alter as you go along.

Another useful little dodge provided by electronics is that Scrib will display the "old" text you are working on plus the new, updated version with your amendments too. It does this by splitting the screen image into two parts—a sort of schizophrenic c.r.t.! A mini-printer gives you hard copy and Scrib will also keep an accurate record of the number of characters you type in. A

cassette magnetic tape is used for storage. No price is mentioned, and although Scrib may weigh heavily on the cheque book, it's only a mere 8.5kg to carry around.

Der Zug am Gleis . . .

With computer-generated voices being featured in the news these days, it's nice to look around and pick an application or three. A useful one that comes to mind is the German railway station that uses a computer to give out train information to callers. The idea is that the person needing the information rings a special number. They are then asked the identification of the destination station and the desired times of departure. In response, the computer will speak giving the best train around that time.

Perhaps British Rail could use the idea, the computer being used to pick an excuse for late arrival from a long list. Perhaps a suitable program might be:

```
10 LET BR =  
    EXCUSE(INTL + 100*RND(0))  
20 PRINT "BR"  
30 NEXT BR  
40 GOTO 10
```

Solar cells

News has just filtered through that researchers are busy developing a photoelectrochemical solar cell (try saying it quickly!). This rare creature not only obligingly changes sunshine into electric power, it also stores energy while it's doing it. Most solar cells employ comparatively expensive photocrystalline materials, or single crystal ones. This new cell uses the less expensive cadmium selenide and it has three photo anodes. One of these anodes is used to store electrical energy while the sun is shining. Connecting it with a common anode enables it to be persuaded to give an energy after darkness. The efficiencies so far are very low, typically a few per cent. However, the researchers are hopeful, and so am I.



SEMICONDUCTOR TESTER

For OSCILLOSCOPE DISPLAY

J. SCOTT PATERSON

This simple add-on unit uses two a.c. voltages in quadrature (90° out of phase) which are fed to the semiconductor under test. The condition of the device is displayed on an oscilloscope used in X-Y mode. With no device connected, the Lissajous figure produced is a circle. With a transistor connected, both voltages are half-wave rectified, the transistors being treated as back-to-back

diodes, and this results in one quarter of a circle being displayed (Fig. 3). If there is any leakage, the shape will be shrunk in one direction so that either the X or Y voltage is reduced. Horizontal shrinking is due to base-emitter leakage, vertical shrinking due to base-collector leakage, so that the "corners" of the quarter-circle represent the base, emitter and collector connections.

If only a vertical line results (a radius of the original circle) there is a base-collector short; a horizontal line indicates a base-emitter short. Should the line be at 45° then there is a collector-emitter short, and when both junctions are shorted only a dot is shown.

In Fig. 1, we show the patterns produced by good devices; the figures for the various faults can be worked out by connecting resistors between terminals to simulate leakage, by connecting terminals together for shorts and by not connecting terminals together for shorts and by not connecting terminals for open circuits.

Circuit Diagram

Operational amplifier IC1 is a low-pass filter, and together with IC2, an integrator, forms a sinusoidal oscillator with quadrature outputs, the amplitude of which are controlled by the two back-to-back Zener diodes. If good temperature stability is required, the two Zeners can be replaced by two diode-connected npn transistors (collector to base) with reverse breakdown voltages similar to the original Zener voltages.

Table 1: Connection chart for different devices

Terminal	1	2	3
Transistor	Emitter	Base	Collector
Diode	Anode	—	Cathode
SCR	Cathode	Gate	Anode

WAD454

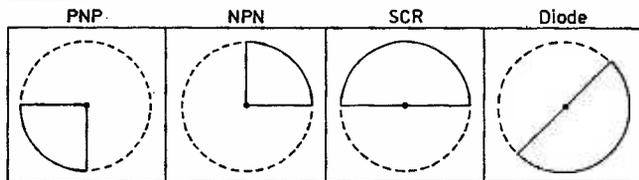


Fig. 1: The various displays produced on the c.r.t. for good devices

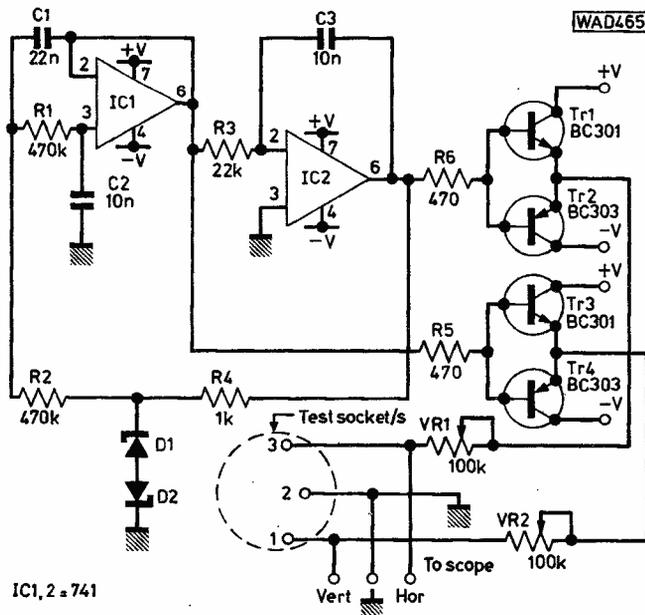
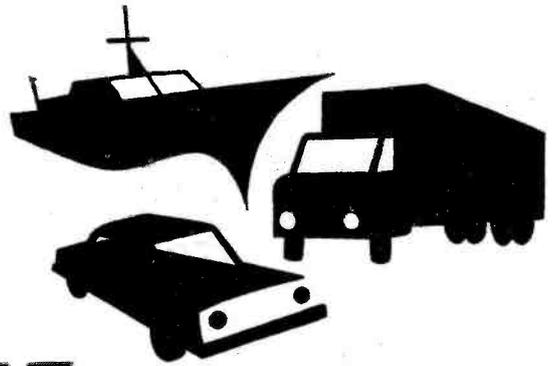


Fig. 2: Circuit diagram of the semiconductor tester. The leads marked Vert and Hor are connected to the scope Y and X amplifier inputs respectively

★ components

Resistors		
1W 5%		
470Ω	2	R5, 6
1kΩ	1	R4
22kΩ	1	R3
470kΩ	2	R1, 2
Potentiometers		
100kΩ	2	VR1, 2
Capacitors		
<i>Polyester</i>		
10nF	2	C2, 3
22nF	1	C1
Semiconductors		
<i>Diodes</i>		
Zener 8-2V	2	D1, D2
<i>Transistors</i>		
BC301	2	Tr1, 3
BC303	2	Tr2, 4
<i>Integrated circuits</i>		
741	2	IC1, 2
Miscellaneous		
Test socket, Veroboard, Plastics case		

continued on page 56▶▶▶



CITIZENS BAND UK

THE FACTS & THE FUTURE

By the time this issue of *PW* appears on the bookstalls, it is quite likely that a government announcement will have been made regarding a Citizens' Band Radio Service in the UK. If so, then what is said here may, in some ways, be less relevant than it was when written. It seems right, however, to give one of our vehemently pro-CB

readers the right to reply on behalf of all those who thought the article *CB — an Unbiased Review* in our September issue was in fact strongly biased against CB. I should add, however, that some readers thought it fair, and some even thought it pro-CB! Opinion is a very varied thing.

Sir: Would you kindly allow me space in *PW* as you did J. D. Pearson G3KOC in order that I may answer that most Biased-of-Unbiased reviews on CB that I have ever read.

It is my opinion G3KOC that if you honestly consider that your article was unbiased then you are suffering from "Key Clicks" in the tuned circuits of the brain. What frequency are these "clicks"? 27MHz.

"Do we need CB?" If so "Why?" Let me put a filter on your spurious emissions.

1. If one doctor in 1000 arrived at a person's side in time to save his life as a result of CB — WE NEED IT.
2. If one Ambulance man, Nurse, Police Officer, Pedestrian or Motorist did the same. That's five more reasons why WE NEED IT!
3. If any of the people mentioned heard a Small Boat in distress — WE NEED IT.
4. If Muggers were caught as a result of CB, if Bombers and Terrorists were caught — WE NEED IT.
5. If old people in distress received help. If a disabled driver is able to get help, when broken down and incapable of walking to a telephone. If every lonely, elderly, crippled, blind, bedridden person will be able to call up a "good buddy" who can bring some cheer and purpose in their life — WE NEED IT.
6. If Bank robbers, or any other criminal escaping by vehicle were very soon caught as a result of a CB trace, if a multiple motorway pile-up was avoided — WE NEED IT.
7. If a few CB'ers choose to move to greater heights and join the RSGB and the Hams — WE NEED IT.

What we don't need are the very few Hams, who think because they have passed the RAE, the air-waves should only be for them. There are quite a few Hams who only know just enough to pass the examination. They then go out, pay a few hundred pounds for a set and a matching aerial and never take the cover off the set. When it goes wrong, they return it to the manufacturers. In other words, they are no better than a CB'er. Most of all, we can do without people like you. Professionals, calling themselves Hams, who consider themselves "God's Keepers" to the TX Channels. The conversations on the Ham Bands, drive me mad. Everyone does not wish to talk or listen to dB's, p.a. output or how many elements the latest Yagi has.

You and your fellow "knockers" of CB should be giving it the go-ahead and encouraging MPs to do so. Why? Because you should be overjoyed at the thought of how many more people will be brought into the fold, to enjoy radio as you and I do. After all, does it matter what form their enjoyment takes?

Think very hard, some Hams don't like v.h.f., some dislike h.f., others don't like either and go on slow scan TV, Telex or Moon-bounce. People like me collect ex-WD sets and monitor all the marine frequencies and by the way more than once have been responsible for people receiving help at sea, once in Sardinia and another time off the NE coast of Canada.

There is also another type like me — 30 years into radio at sea, Coast-guard and Ham, who knows quite a lot but not all by any means, but who simply falls apart at the thought of an examination. Have you the right to deny me the means of speech? The answer G3KOC is NO, you do not have that right. 73s.

A Dorsett BRS39730
Alton, Hants

CB UK

In the past few months, CB has received a great deal of exposure in the press. A lot of the points, both for and against, have been repeated over and over again; and — if the newspaper reports are to be believed — a lot of drivel and half-truths have been spouted by many people, including licensed radio amateurs, CB fans, Members of Parliament, even the Home Office! There seem to be misconceptions about just what a CB service is for, what regulations it operates under in other countries, what the causes and effects of radio interference are and how it can be overcome, and many other aspects. Even some of our rival electronics publications have been unable to get all the technical facts right. We will try to clear up some of these points.

(a) CB radio is intended as a means of communication between mobiles, or between mobile and fixed stations, for messages about the licensee's private or business affairs. Since messages on business matters are expressly prohibited in the amateur service, an amateur licence is **NOT** a viable alternative. In any case, many potential CB users are not interested in radio technology. The argument that people from all walks of life can and do pass the RAE is irrelevant.

(b) CB radio is **NOT** intended as a hobby in itself. The regulations of the various countries differ in the way in which they express this. Among the most forthright are the Canadian General Radio Service Regulations, which prohibit: "Communication used in itself as a diversionary or recreational activity". If you want to experiment with radio communication then licensed amateur radio is a means available to you. Maybe there should be a Novice class to introduce beginners to the hobby, but that is a separate argument.

(c) CB radio in other countries is not as free and unfettered as some people seem to think. In the USA, for instance, only type-approved CB transmitters may be used; transmitters must not be modified in any way; linear amplifiers are prohibited (possession of a linear is considered to be sufficient evidence that it has been used); all internal repairs and adjustments to CB transmitters must be carried out by, or under the direct supervision of, a person holding a first- or second-class commercial radiotelephone operator licence. Violations of provisions of the FCC Rules or the Communications Act are punishable by fines up to \$10 000 and/or up to one year's imprisonment.

The argument advanced that many of the US CB Rules are not enforced really reflects no credit on the CB fraternity there, but only goes to support the arguments put forward by opponents of the service.

(d) The interference problem will not be magically solved overnight by putting CB on a different channel, since *all* radio transmitters are capable of causing interference, particularly at close range. The reduction of interference depends upon good design, correct adjustment and adequate maintenance of transmitters, and good design of receivers (and audio equipment), and upon the sensible allocation of frequencies to various services.

(e) The argument advanced for the adoption of 27MHz CB on the ground that it would allow travellers within the

EEC countries to maintain communication throughout their journey is not valid. Although there is a CEPT Specification for 27MHz CB, few of the European countries adhere to it. In fact, if an Italian takes his CB into Germany, it is quite likely to be confiscated and destroyed, because it does not comply with the German regulations.

(f) The commandeering of sections of the r.f. spectrum, in the way that some UK CB fans are trying to do on 27MHz, is not really a blow for freedom: quite the reverse. After all, if you steal something from someone, you cannot really complain if someone else then steals it from you. That way lies chaos, and I'm sure CBers will be quick to complain if they get an allocation and someone else interferes with that!

(g) The problems of interference to radio-controlled models are dismissed by many CBers, but the fact remains that the potential for loss to the modeller, and injury to bystanders, is considerable in the case of aircraft models. In the UK, 26.96–27.28MHz is allocated to radio control, and this band includes 28 of the 40 channels allotted to CB in the US, in other words 70 per cent of the total allocation.

There are reputed to be around 72 000 model control licences currently in force in the UK, and very few models indeed are using the alternative u.h.f. band, as yet.

It has been argued that a CB user finding a radio-controlled model operating on the channel that he has selected will quickly change to another channel. Since most CBers are supposedly non-technical, how will he recognise the strange sounds he might hear as being caused by a radio-control transmitter? In any event, by the time he has recognised that the channel is occupied by a r.c. user it will be too late — the model will most likely have gone out of control with possibly fatal consequences.

The Future

The recent announcement of the reorganisation of the Post Office, and the opening up of some aspects of the telecommunications services to outside competition, gives an opportunity for a re-think on the licensing and control of radio and the like, and also of the form that CB might take.

The present system of notifying sales of TV sets to the TVLRO could be extended to such things as radio control systems, metal detectors, and CB transceivers (if legalised!). Licence application forms could be included with each equipment sold, and licences made available over Post Office counters. This could even be extended to amateur licences. After all, the Post Office already issue vehicle licences on presentation of the relevant documents and fee. If buying or renewing a licence were made easier, it might even persuade some of the present unlicensed metal detector and radio control fans to do the decent thing.

Licences for any portable or mobile equipment could, with advantage, be produced in a form like a credit card or driving licence. Maybe even made to be attached to the

CB UK

set. And while they're about it, they could make the metal detector licence valid for any type-approved design, and save the aggravation of getting a new licence when buying a new detector.

On the subject of CB, there is much to be said for adopting a system flexible enough to allow it to be used at the level of technology and expense desired by the individual. With modern microprocessor circuitry, it would be comparatively simple to extend the service to offer the options of data handling, selective calling, or linking in to the public telephone system. This would allow the current exorbitantly-expensive GPO Mobile Radiophone system to be done away with.

This scale of service would involve a countrywide network of repeaters, but these could easily be sited along motorways and main roads. The repeater system would, even for the lowest level of service — the simple handheld — offer the advantages of more reliable communication, plus lower transmitter power, and therefore lower battery drain.

Perhaps it's a little 1984'ish, but it would be easy to arrange for an auto-identification signal to be built into each transmitter, to allow a computer to check if you had paid your licence and, if not, refuse to provide you with service, except possibly for emergencies! Remember, 1984 is not all that far off now.

★ ★ ★ ★

We are indebted to readers who have contributed information and ideas to this article. Perhaps, finally, we should try to sum up *PW's* viewpoint on the subject of CB in the UK:

1. We believe that there is a need for a portable/mobile radio communication service for the general public, at a reasonable cost. This should be entirely separate from the amateur service and should not involve the user in passing any sort of exam.

2. This service should be on a frequency band other than 27MHz, which is unsuitable for reliable short-range communications by reason of propagation characteristics, and is already allocated to other services. The band and modulation system chosen should be the best available from the point of view of reduction of interference and should allow for the optional use of special facilities.

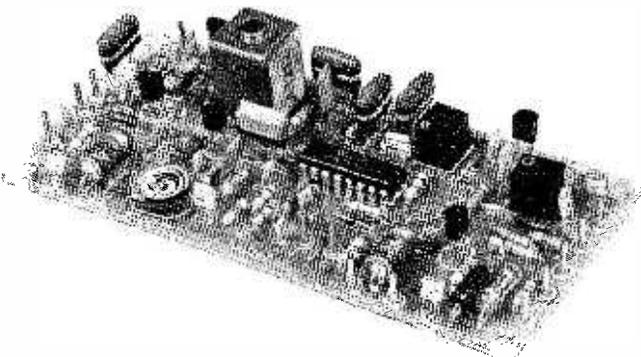
3. Transmitters used should be type-approved, and the use of linear amplifiers prohibited.

4. The service should be capable of being effectively licensed and controlled with a minimum of bureaucracy.

FMD-7 FM DETECTOR

▶▶▶ continued from page 28

There was one mistake in the installation instructions for the FRG-7, but this was pretty obvious and should not cause any problems.



Switching the module into use ideally requires another position on the MODE switch. This is possible on the FRG-7/7000 if you are prepared to sacrifice the AM/ANL facility, and use this for NBFM. Otherwise, you will need to fit an additional switch somewhere on the receiver. Instructions are given for both methods.

Results

Once one problem, caused by overlooking a correction slip in the handbook, had been overcome, the module worked perfectly. Tuning, which involves adjustment of the quadrature coil for maximum audio output, takes but a moment, and the only other adjustments required are one preset potentiometer for squelch threshold, and one to make the audio output level roughly equal to that on other modes. Audio quality is good and sensitivity entirely adequate.

Apart from those points about the handbook mentioned already, it includes a full technical description, detailed assembly instructions, test procedures, and fault-finding procedures including comprehensive d.c. and a.c. checks. A full component list and the circuit diagram complete the information.

Price

The FMD-7 was supplied by Burns Electronics, 43a Chipstead Valley Road, Coulsdon, Surrey CR3 2RB. Telephone 01-668 7766. The price in kit form is £21.42, or the module is available ready-built for £26.68. Both prices include UK carriage and insurance and VAT. ●

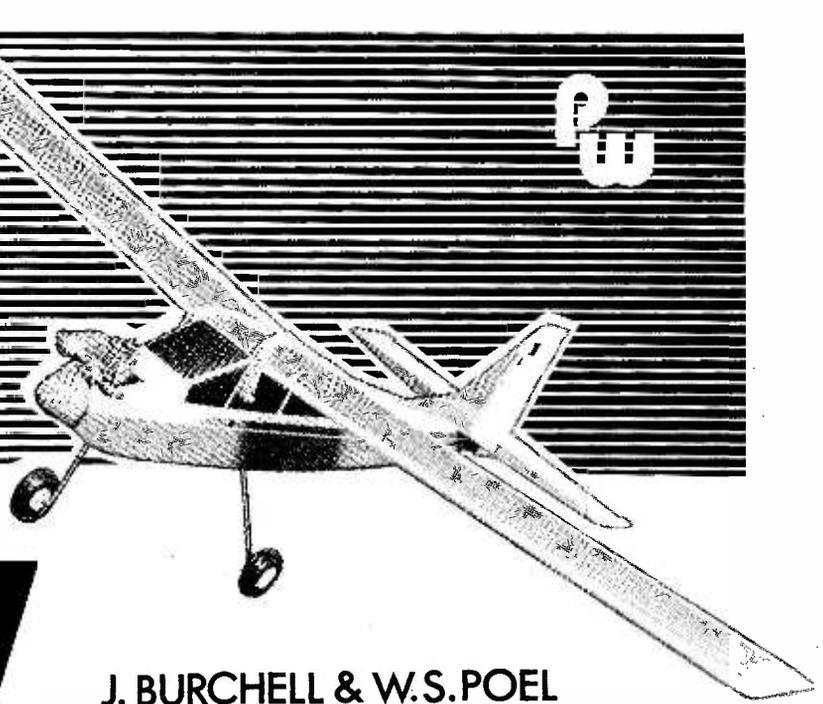
KINDLY NOTE!

VHF DF Loop Aerial October 1979
The length of each limb of the loop should be 443mm,
not 380mm as shown in Fig. 2.

Model Radio Control

Part 1

THE
PW FM-80
SYSTEM



J. BURCHELL & W.S. POEL

Historically, radio control has evolved through all manner of what now seems to be the most appalling anachronisms, the first types using valves. But after a long and reasonably happy association with the transistor circuitry, the recent emergence of suitable i.c.s, first in the encoder/decoder circuit, and now in the actual radio sections too, has led to considerable advances in the sophistication and reliability of these systems.

Reliability

The most sophisticated system in the world is of little use if the whole system fails at a crucial moment. The plane flies never to be seen again, or the boat ends up marooned in the middle of the pond, frantically harassed by a bemused duck.

Predictability

Early systems were based on straight switching, where the control device slammed from one extreme to another. Or, if motor driven, operated either too slowly or erratically to be of much use in delicate control operations. The use of servo units gives a positional feedback to the control medium, so that a movement of the control stick is directly related to the actual movement observed in the model. In the toy market at present, there are several cheap imported radio controlled cars — and these are nearly all non-proportional control, relying on crude switching functions for forwards/backwards and left/right/centre control. The radio links themselves are extremely dubious, since the cheap receiver techniques employ a super-regenerative technique that itself emits a rather grubby spectrum of noise and hash both on and around the control frequency, and on many harmonically related frequencies. Several examples seen have been excellent at jamming u.h.f. as far as TV frequencies.

Interference

The question of interference on the 27MHz band allocated to radio control is one of the burning issues for present day modellers, since estimates of some 400 000 radio control devices (including unlicensed users), point to a severe congestion of the few frequencies available.

Freedom from interference and from adjacent channel operators is, primarily, a function of the type of receiver circuit in the equipment. The avoidance of unnecessary power levels in the transmitter is good practice too—but since the aeromodeller is more prone to interference, by virtue of the height of the receiving antenna when airborne, it is understandable that they will wish to use the maximum permitted 1.5W of r.f. to ensure best range. Certainly, on the ground, and on the water, a power of 25–100mW will control any reasonable system just about as far as the eye can follow the manoeuvres of the model. Operation out of eyeshot is not necessarily of much use, since the feedback between the eye and the model under control is the crux of r.c.

The avoidance of interference is one of the prime preoccupations of the serious 27MHz user, and with so much illegal CB equipment in the UK, let alone the 'legal interference' from Europe, and even the USA, this preoccupation is readily understood. However, CB is either a.m. or s.s.b. and since this can scramble an a.m. radio control system on the fringe areas of operation, the use of narrow deviation f.m. is rapidly beginning to gain popularity, due to the a.m. rejection facilities afforded by this mode. The f.m. carrier is also transmitted continuously, and not switched on and off like so many of the a.m. approaches, which means there are no pauses in the data stream to allow the receiver to accept any other signals on the channel (see Figure 1).

The limiting action of f.m. means that the problems associated with good a.g.c. need not apply, since the r.f. and i.f. amplification can be class C, limiting the signal and rejecting a.m. Good limiting with a low input signal means that the recovered carrier information remains constant over a wide range of input signals, which, in the a.m. system requires carefully designed a.g.c. action to achieve.

Thus f.m. can significantly improve the rejection of co-channel signals (those on the same frequency but from some distance away), but for good adjacent channel rejection—such as from other modellers using the same area but on different frequencies—the problem becomes one of i.f. selectivity in the receiver.

The classic a.m. channel spacing for r.c. has been 50kHz, resulting in six channels. However, since the capture effect of f.m. combined with modern ceramic filters can dramatically improve receiver selectivity, 10kHz spacing is possible, greatly increasing the number of possible channels. However, unless you are very certain of your own equipment *and* that of the other users in the vicinity, always put as many kHz between yourself and the other operators as possible, since whilst your receiver may be fine, their transmitters may be slightly off-channel, or, if a.m. the splatter caused may spread well outside their basic channel.

Technically, 27MHz is not ideal, since under the correct conditions, usually associated with sunspot activity, the band has ranges of 6000 miles plus, with hardly any power at the transmitter. This makes life both unpredictable and precarious for 27MHz users. The actual wavelength is 11 metres, so aerials fall into the category of, 'electrically short' (less than $\frac{1}{4}$ wave), which introduces complicated variables into their design. In fact, receiver aerials usually end up as being strictly high impedance capacitive types, tacked on the end of the first tuned circuit—which is in itself not really too bad a compromise, but apart from electrostatic susceptibility (even to the extent of being bothered by rubbing control surfaces), such aerials mean that the conscientious designer really needs to trim each aerial coil to suit the aerial conditions to ensure optimum performance at all times. These types of aerials are not to be confused with good old transmission line impedance of

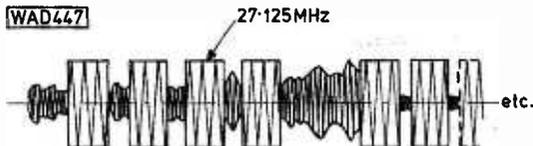


Fig. 1(a): The waveform above shows a typical a.m. transmission while below is the same information transmitted as an f.m. signal.

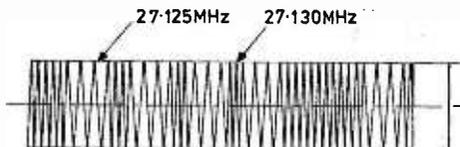


Fig. 1(b): The level changes with model movement for an a.m. system (above) while for the equivalent f.m. system the level is constant

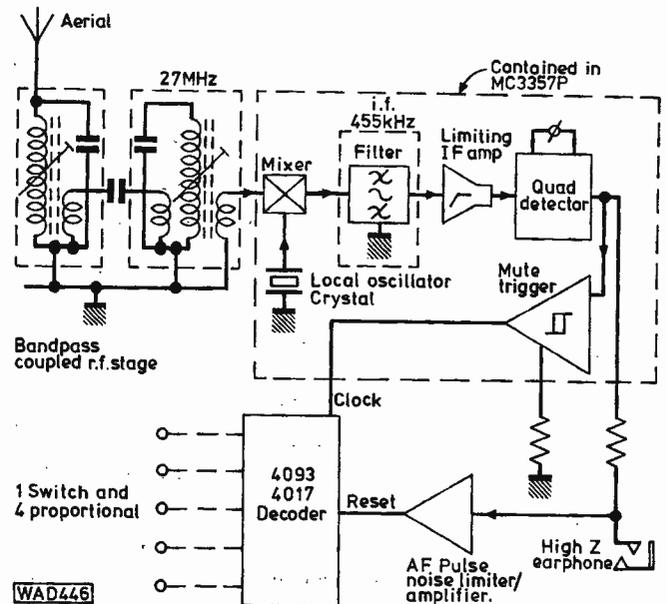
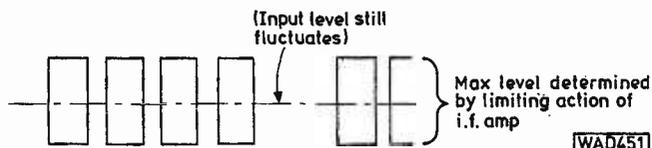


Fig. 2: The design approach chosen for the PW FM-80 f.m. receiver

50Ω, and they must not be fed down coaxial cable, since that merely 'looks' like a big capacitor across the tuned circuit, with little hope of getting the circuit to peak.

At the transmitter, power transfer cannot be achieved the same way, and even if you tried, the r.f. voltages developed across such high impedances can lead to r.f. burns. The aerial is thus loaded with a coil at the base, or in the middle. Loading reduces the impedance to the desired level.

An ideal frequency for radio control would be the 144–146MHz amateur radio band (assuming co-channel interference were to be avoided), but it is unlikely to be permitted in this country. The 19in-long, 2 metre band quarter wave antenna is ideal, and the technology available today could permit the construction of suitable miniature receivers to the same dimensions as present 27MHz types. 459MHz u.h.f. is outside the scope of most constructors, since everything from signal generators to strip line technology are just that little bit outside the grasp of the keen amateur. The stability demanded of the crystals used means that they cost about 5 times as much too!

Armed with the aims and objects of a comprehensive r.c. system, we can consider how best to apply currently available technologies to solve the problems. A summary of the features sought, and alternative approaches available are listed in Table 1.

Receiver Design

The approach to the receiver design is shown in Figure 2. A couple of added features are apparent, since it is a very useful thing to have some means of actually listening to the receiver in operation. This is particularly so with f.m. where the Tx crystal is a fundamental cut, and the range of frequency pulling is quite substantial when compared to the usual 3rd overtone types used for a.m. Basically, this makes life a bit difficult for the home constructor, since it is almost impossible for a setup with 3rd O/T crystals to be more than the i.f. bandwidth off tune. This is not so with f.m. and being able to listen-in means that you can pull in the crystal trim by ear, if you do not

Table 1

Receiver Feature	Approaches commonly used	Conclusions
Small size	Universally semi-conductor, though surprisingly few using i.c.s. at the moment. Recent i.c.s. from Motorola and Plessey seem to offer real advantages for f.m. applications	use MC3357P
Low Power, flexible supply voltages	This factor tends to rule out the use of j.f.e.t. and m.o.s.f.e.t. techniques, since r.c. has grown up with 4-8V being the recognized supply. But at low currents, bipolar stages can suffer from cross modulation very easily. Again, the technique used in the MC3357 scores, since the input configuration is a fully balanced mixer stage, possessing superior performance to a simple transistor r.f. stage of mixer. It also happens to work down to 3V and less, with some 2mA current drain!	use MC3357
Good selectivity	The r.f. tuned circuits should be at least a double tuned pair—but space prevents anything very much more sophisticated. Keeping r.f. gain down will assist here. The main i.f. filter should be a good class ceramic unit, bearing in mind the criteria mentioned earlier. The cost to performance ratio will reflect the final application of the equipment. Since the receiver is basically going to be cheap, it is not really too much to expect that the enthusiast will be prepared to make separate receivers for separate applications.	use miniature ceramic or mechanical filters

have access to a digital frequency meter. All that is needed is a high impedance crystal earpiece—which is tapped in via a crystal earpiece jackplug socket. This also provides a safety check to hear what's going on, on the channel you propose to use. The mute function may be considered pointless by some, since most commercial systems do not appear to offer this feature yet, possibly because a reliable circuit takes up too much space if not fully integrated as in the MC3357P. The final circuit for the receiver is shown in Figure 3 and whilst this may not be the smallest receiver in the world, it is certainly a manageable size for the home constructor—and particularly those who are being tempted into radio control for the first time.

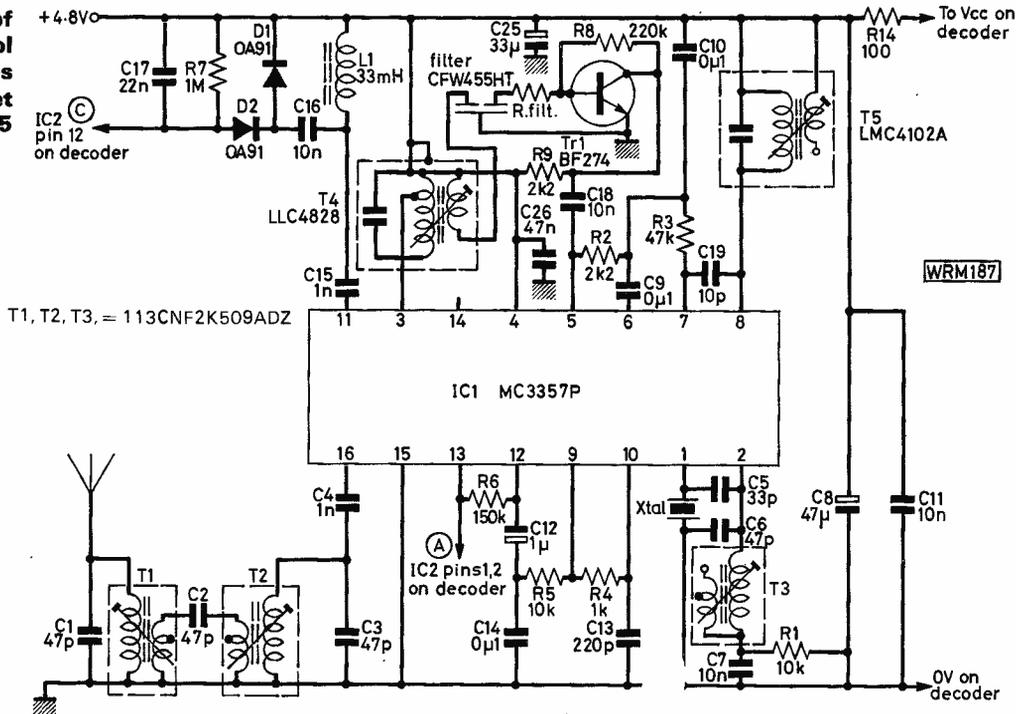
The Receiver Circuit

Starting at the front end, the wire aerial is fed into the top of the input half of a bandpass coupled pair. Top coupling, and proximity (mutual inductive) coupling is frequently used in r.c. but both these tend to suffer from problems which deserve a brief word of explanation. Both methods nearly always tend to overcouple the circuits, providing too wide a response, and the classic 'double hump'. Top capacity coupling can also be a reasonably good way of allowing v.h.f. and static type interference through, since L1 and L2 look like fairly amiable chokes at 175MHz, permitting passage of some of the very strong v.h.f. carriers likely to be 'seen' by a model aircraft at 100 feet or so. This can lead to blocking of the mixer, despite the fact it has excellent overload capability anyway, with the subsequent demise of the whole system.

So the technique adopted, after some experimentation, was the lower impedance coupling, using the coil secondary to provide a much lower impedance point, and thence requiring use of a higher value coupling capacitor. The overall r.f. response is thus greatly enhanced, and quite excellent close to the desired frequency. Despite this, the use of 455kHz means that the i.f. image rejection is still only 18dB or so down, but that is only improved by going to a higher i.f., and using crystal filters which may not stand up to the rigours of model vibrations.

The actual responses of the r.f. input stage are shown in Figure 4. The h.f. response of this input arrangement is ideal, and the v.h.f. feedthrough is only beginning to get obtrusive as the frequency reaches levels that are outside the receiver frequency response, which tails off at about 60MHz. The plot was taken with a spectrum analyser and high impedance (10MΩ) r.f. probe with a 900MHz response, and so is a reasonable approximation. One very important point for the r.c. enthusiast to bear in mind is the fact that the usual airborne aerial of 15-16 inches (or less) is getting to look suspiciously like a quarterwave antenna for either the commercial 175MHz band, or worse—the Band III TV transmitters. Further work on these types of electrically short aerials is being carried out to investigate methods of making them less attractive to unwanted r.f. of this type. This aspect also means that the use of a really wideband f.e.t. at the input stage is not a good idea, since the response of such a stage will not be bandwidth-limited, and, if the input is wideband then the aerial is certainly going to tend towards its natural resonance, unless suitably loaded. The circuit used can be shown to provide reliable control with an input p.d. of 4μV by rearranging the input circuit to match the 50Ω generator source. This is quite enough for most applications, and too much for some—so further gain in front of the major selectivity of the set is not considered necessary. Remember that the aerial may be thought of as an extension of C1, and so T1 must be trimmed to suit each aerial—and also the aerial when in situ, since the high

Fig. 3: The circuit diagram of the FM-80 f.m. radio control receiver. This circuit gives excellent performance yet remains simple to build. C25 should be 47 μ



impedance of such an aerial is liable to be influenced by the proximity of metal parts of the installations.

From the input stage, which is a fully balanced mixer, fed from the oscillator and the input signal, the signal passes to the i.f. after mixing. The crystal oscillator used here is worthy of note, since the original function of the MC3357 required a fundamental mode Colpitts circuit to be used here—performing the function of the second conversion in f.m. receivers, from 10.7MHz to 455kHz. However, the circuit needs to run on the 27MHz third harmonic, and since the fundamental of a third overtone crystal is not exactly one third of the 3rd overtone frequency, even the unsatisfactory expedient of running the crystal at its fundamental, and trusting to there being sufficient third harmonic content is not viable. Approaches such as trying to force the crystal onto its third overtone in all manner of 27MHz tuned circuitry around the oscillator

pins at 1 and 2 were tried, and found wanting. Unreliable starting was the main problem—and since the Colpitts circuit works well enough when the crystal is replaced by an LC tuned circuit, trying to force the crystal with LC arrangements only provided a free running oscillator that was loosely locked to the crystal. The answer is to prevent operation at 9MHz, and this is the function of the parallel tuned trap formed by C6 and T3. Since pin 2 of the i.c. represents the emitter of the Colpitts configuration, this approach presents an impossibly high impedance at 9MHz, and so the next most likely mode—the 3rd overtone is automatically selected. The 10k Ω resistor R1 is used to further encourage the circuit into life, shunting the internal 100k Ω emitter resistor to provide more urge. To perform the same trick, but at the fifth overtone, the tuned circuit at pin 2 needs to be a more complex double trap, but it still works!

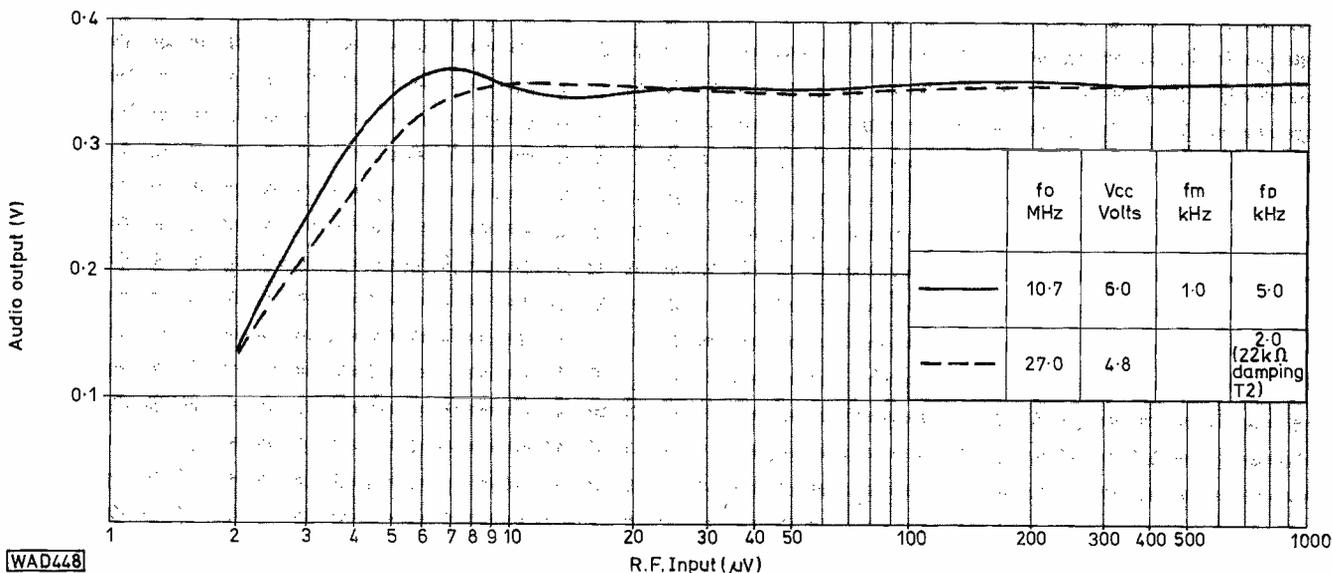


Fig. 4: The response curves for the r.f. input stage of the receiver

T4 provides i.f. output matching to the subsequent filter stage. Various possibilities exist here ranging from the very low cost CFM2 filter, which still provides better overall selectivity than the comparable four i.f.t. circuit, to the more expensive ladder filter ceramics, such as the Murata and NTK series CFX and SLF-D series, where the adjacent channel disappears to some 80 or 90dB down. The CFM2 described is not a ceramic filter, but a miniature mechanical filter, and as such, the inter-electrode capacitance causing some of the problems associated with ceramic ladder filters, is far less. Overall stopband is thus better, and combinations of the CFM2 and ceramic ladder filters may be used to good effect, although a higher insertion loss results.

Pin 5 of the i.c. is the entry point for the i.f. and limiter, and although the basic circuit is capable of $4\mu\text{V}$ operation with the decoder described, there may be certain applications where a bit more is considered desirable. As mentioned earlier, the temptation to place gain at the front end of the circuit should be resisted at all costs, as this tends to amplify not only the 27MHz, but much else besides. The place to put the gain is in the i.f. after the filter stage has limited the bandwidth. The circuit used is very simple, and is in fact the same as many audio amplifier circuits, contributing some extra 12-15dB of noticeable gain.

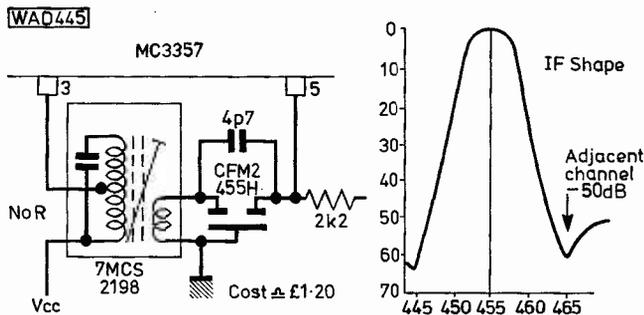
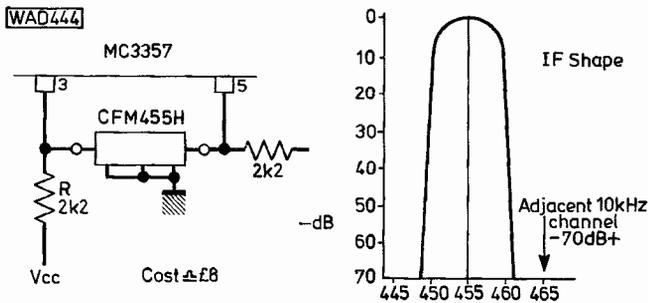


Fig. 5: Two different filter design approaches for the receiver. The filter chosen for the FM-80 system is the Murata CFW455HT



The MC3357 amplifier, limiter and detector stage are all biased externally via R2 and R3, and since these resistors basically represent different ends of a very high gain amplifier chain, the junction must be very effectively decoupled to ground with a capacitor that possesses ideal r.f. performance. The types used also need to be about $0.1\mu\text{F}$ to be effective at all the frequencies involved, and so C9 and C10 are monolithic ceramic plate types, which also happen to be the smallest variety of $0.1\mu\text{F}$ capacitor anyway. The detector is the usual quadrature phase-shifted system fed from pin 7 via only 10pF, resulting in very little detector loading, and a very steep slope to the detector characteristic at this point.

It is from here that the advocates of the f.m. system tend to mumble quietly to themselves about noise perfor-

mance. With all that gain before the detector, a no-signal condition results in white noise within the bandwidth of the i.f. system that crashes from rail to rail, i.e. a fully limited output, presenting very nice edges for edge triggered decoders to 'see' and clock from.

When the signal disappears, the residual noise can send the servos into fits of apoplexy, although pure white noise is usually too 'fast' for the decoder, which sits in a condition of reset. The really embarrassing point is the transition from full control to no control, since the partial control area can allow just enough of the desired control information to pass through the decoder, but can also let through noise at the same time. In a.m. systems, the transition from control to partial control is a far more orderly affair, since the noise in no-signal conditions is rarely enough to create spurious operation of the decoder.

The ideal decoder will only permit the passage of correct width control information and immediately reset when it sees the noise. Most present circuits wait until the decoder has buzzed through all channels to the end before holding the reset condition, leaving a trail of jarred servos in its wake.

Original thoughts were that the built-in mute should be used. Indeed a means of signal mute was tried and found to work using the communications noise mute function. However, this took up a lot of space, as well as the rather handy trigger amplifier in the i.c. itself. Handy, because this amplifier provides the ideal means by which the data train may be reconstituted. The amplifier can produce a perfect squarewave from a moderately dishevelled array of data pulses, and so makes a big contribution to noise immunity. However, this still does not entirely get around the problem above—since noise can still foul the decoder, and so a noise mute of another variety is used, with a coil and capacitor combination and a diode 'pump' detector. This mute is almost a linear function of the noise input, relying on the finite reset level of the decoder i.c. for its trigger action. This also means that the mute may be applied in such a way that the reset can occur at any point in the data train, providing instant shutdown, rather than waiting for the decoder logic to rush about randomly until it resets itself.

Thus the transition occurs without major servo jerking and jittering, and may be likened in many respects to the behaviour of an a.m. system at threshold levels.

The Decoder

The data system used in radio control is a stream of pulses whose width is varied from 1 to 2 milliseconds by the control medium at the transmitter.

In order that the first pulse of a series, or frame, may be recognised by the decoder, a reference or reset pulse is transmitted at the end of each stream of data. This reset pulse is made to be 2 or 3 times the length of the data channel pulse (see Figure 7) and so may be detected by a process which is basically integration with an RC time constant. Thus perhaps the generic term 'digital' is a slight

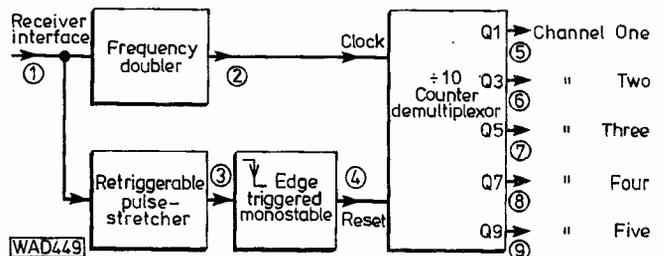
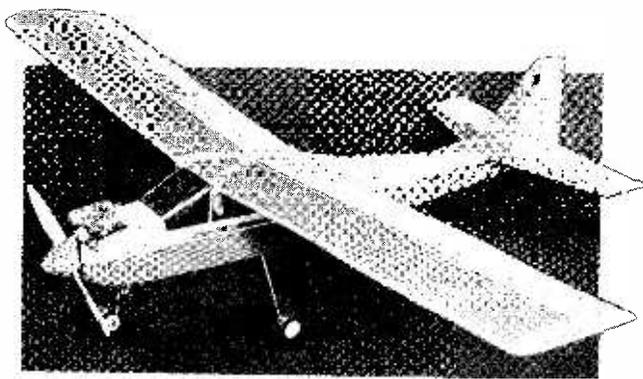


Fig. 6: Block diagram of the decoder



The prototype FM-80 system was installed in a Mini-Escort trainer model aircraft built from a kit made by Galaxy Models and powered by a Flash 15 glow-plug motor supplied by Neway Models. A later part of this series will deal in greater detail with the models and installation

misnomer, as the system is more accurately a linear function of the channel pulse width, which provides the necessary control information to operate the standard servo mechanism decoders and other control media. To be truly digital, a data stream of fixed pulse width would have to be transmitted in the form of a digital word (binary), and then decoded into positional information directly. The process would require a large number of 'bits' to be accurate, since the present technique offers potentially infinite resolution of control over the range of the servo output. However, pure digital control would not need positional feedback in the classic servo fashion, since a word could be directly translated to a positional function. Thus such a system would only need an update when a control position had changed, as opposed to the usual system of p.w.m. where an absent pulse can cause problems, and so is being continually refreshed. Fully digital control of several channels would require a much longer serial frame length to accommodate all the bits, and the loss of a single bit would cause a system "glitch" that

may not be refreshed for almost a second. Thus the present system of control is the ideal compromise, since channel information is updated at a rate of 50-60Hz, within the scope of the relatively narrow r.f. bandwidth available.

The decoder employed is slightly unusual in many respects, since the incoming pulse train is first doubled in the 4093, where leading edges of the data output correspond to the leading and trailing edges of the input signal.

This doubled pulse train then clocks a 4017 Johnson counter, whose alternate outputs correspond to the originally encoded data train. The reset pulse is fed to the retriggerable pulse stretcher, and then used to reset the 4017 to accept the start of a new frame. As long as there is an input to the pulse stretcher, the output remains high, since the input voltage does not reach the threshold. However, after a period determined by the time constant of the stretcher, usually 2 to 3 ms after the trailing edge of an input signal, the output goes low and resets the 4017.

The pulse doubler is built around the first two gates of the 4093, taking advantage of the Schmitt action to provide noise immunity and a perfect clock for the 4017.

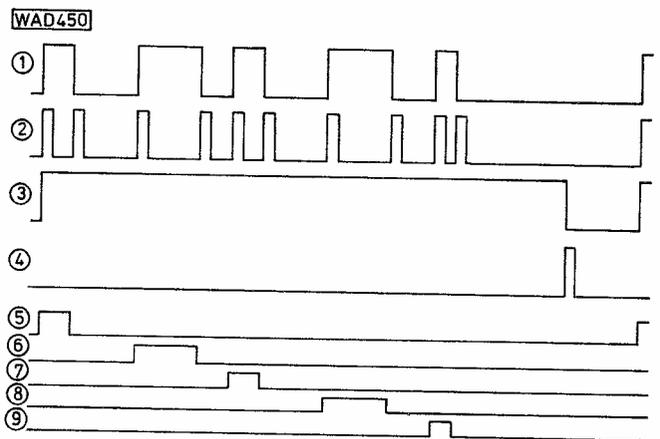


Fig. 7: Waveforms at various points in the decoder

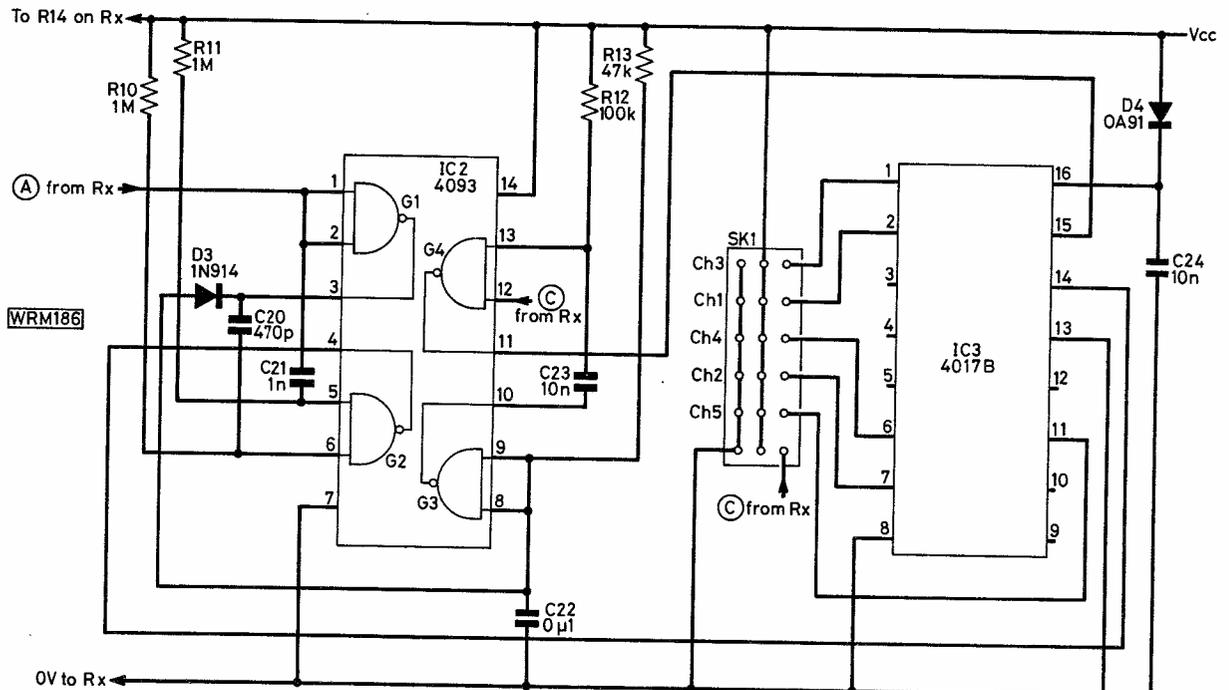


Fig. 8: Circuit diagram of the FM-80 decoder. The output socket is shown wired in a suitable manner for the majority of servos available but if servos of a different design to those to be described later are used then the socket connections must be checked

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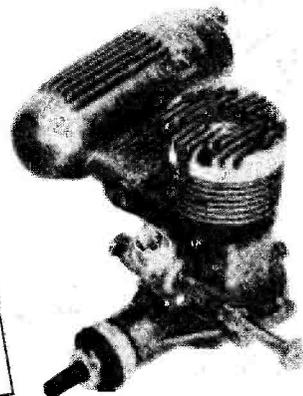
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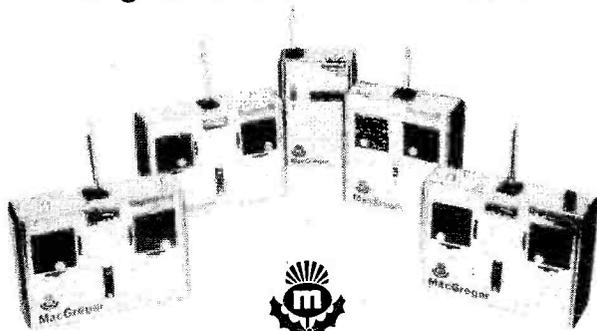
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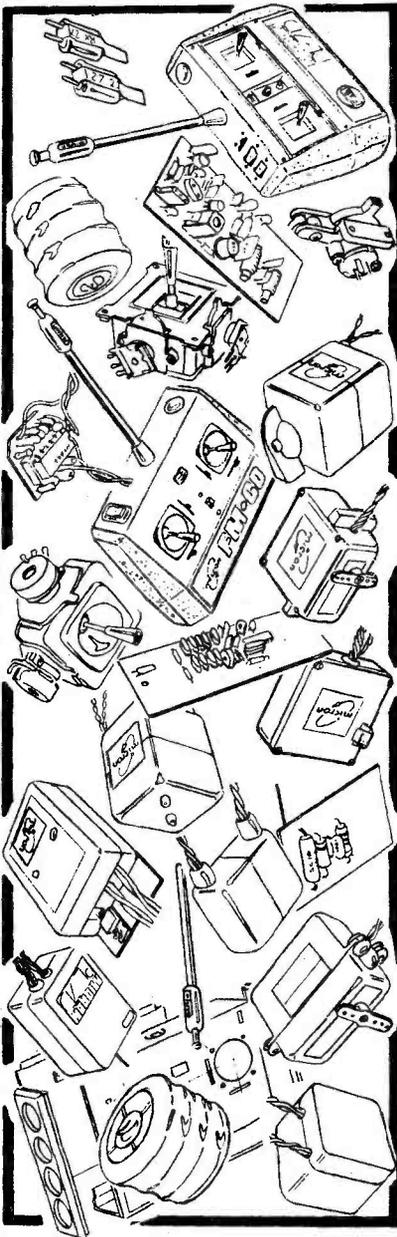
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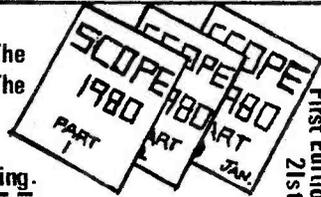
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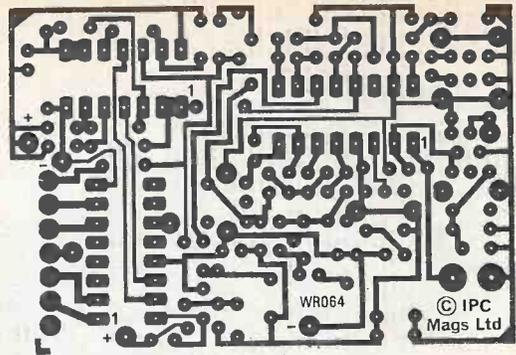
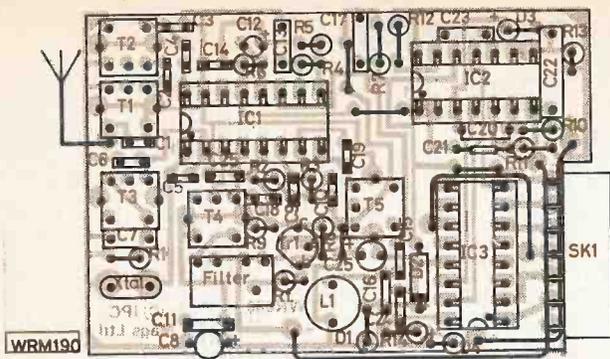


Fig. 9: The copper track pattern for the printed circuit board used for the complete receiver and decoder is shown full size on the right. The laminate should be $\frac{1}{32}$ inch thick and the p.c.b. is carefully trimmed to fit snugly in the plastics case. The component placement for the p.c.b. is shown above. It should be noted that all components must be as small as possible and fitted flush with the board surface with the exception of the two jacks for the crystal

Operation

Gates G1 and G2 form a frequency doubler, where G1 inverts the incoming signal, whilst R10/C20 and R11/C21 differentiate the signal present on their inputs. The output of G2 remains high until the voltage on C10 or C11 has passed the threshold of G2, according to the CR time constant. The retriggerable pulse stretcher is formed from G1, G3, D3 and R13, C22. Whenever the input to G1 is high, the output is low—thereby discharging C22 and keeping the input to G3 low—resulting in a high on the output. When G1 goes low at the end of the last pulse in the data, D3 ceases to conduct, and C22 starts to recharge via R13. After a period related to R13, C22, the output of G3 goes low, unless the capacitor C22 is again discharging by a further data pulse entering G1, when the whole cycle repeats until the reset period is reached. When G3 goes low, the output of G4 goes high—but at the same time, C23 will charge via R12, and after a further period related to R12/C23 product, the output of G4 goes low once again. Desired channel information appears at alternate outputs of the 4017 (frequency doubling makes the intermediate outputs meaningless), Q1, 3, 5, 7 and 9 and the servo control outputs, with Q9 representing the switching channel, which is switched from 1-2ms for functions such as undercarriage retract. The outputs of the CMOS decoder are sufficient to drive all modern servos directly. G4 of the 4093 also includes an input from the linear squelch/noise detector of the receiver output, such that the presence of noise tends to drive the output of the noise detector low, thus creating a reset at any point in the preceding cycle of operations to prevent spurious triggering of the decoder circuit.

Construction

The p.c.b. layout is shown in Figure 9, and by some r.c. standards this may seem large. However, many constructors may be tempted into this as a first exploit in r.c. and so the design is left as manageable, rather than miniaturised. As with any r.f. circuit, all leads should be left cut short as possible—but sockets for the i.c.s are permissible providing you choose ones that will not permit the i.c.s to vibrate out of place.

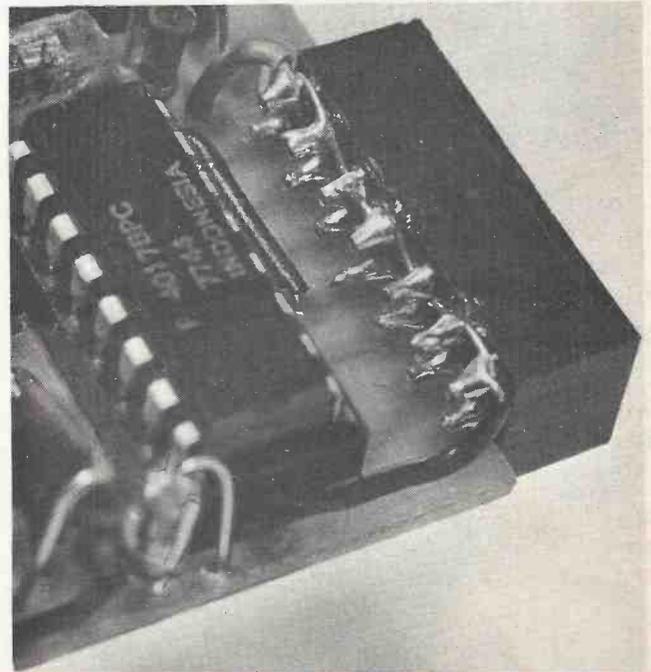
As many standard parts as possible have been used, since although some purists may like to wind their own coils, and grind their own crystals, most constructors prefer the expedient of using tried and tested components in areas where adjustments and tolerances are not trivial. The outputs are taken via a proprietary SLM servo connector block, which also provides access for the supply.

The aerial is connected at the other end of the works—which all fit into a standard SLM receiver box type PT309.

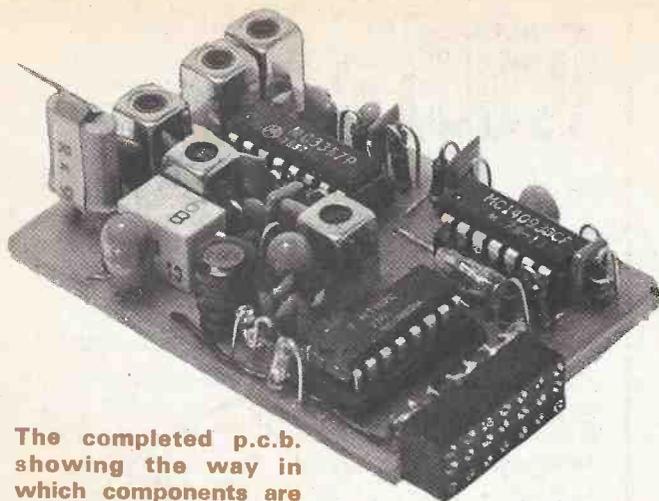
When constructing the receiver p.c.b. use a clean, tinned, hot iron of the miniature 15W variety. Insert the smallest components first finishing up with the i.f. transformers last. The SLM socket is wired up before soldering to the pads on the board. Note that the socket block is mounted vertically on the board edge with the row of output pins soldered to the pads and the other two rows used as supply rails for the servos.

The SLM case will need to be carefully cut as shown in the photo to fit the socket block. A small cut-out can also be made in the lid immediately above the crystal to allow it to be changed without having to undo the box.

All components must be mounted as close to the board as possible without straining the leads and the wires on the copper track side must be cropped as close as possible to the pads. The two Cambion cage jacks used for the crystal holder are fitted to be almost flush with the copper pads.



Close-up view of the SLM socket block showing the method of mounting and wiring to the p.c.b. The two rows of pins above the board are wired using 22s.w.g. tinned copper wire which also serves to complete the power rails on the p.c.b.



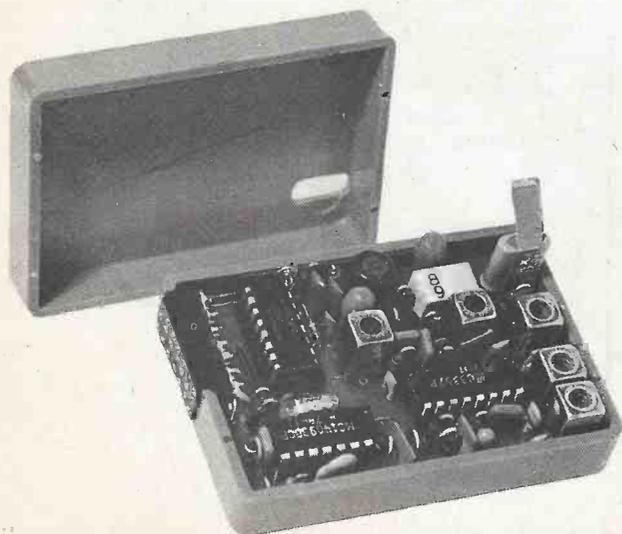
The completed p.c.b. showing the way in which components are mounted on the board

Testing and alignment

Much of this aspect of the receiver will have to wait until you have completed the encoder/transmitter described next month—but you can perform a preparatory test by applying 4.8V from a current-limited supply, and checking that the current is around 4-6mA. If it is, then you have a good chance of success. If not, check the soldering, the chances of a faulty component are so marginal compared with the incidence of faulty construction as to be discounted.

Assuming the 4.8V supply is providing 4-5mA, then listen to the audio output at the junction of R5 and C14. There should be a characteristic hiss, which changes tone as you dab a finger on the underside by the r.f. and i.f. inputs. Pulling the crystal out should have a marked effect, but if not, adjust the core of T3 until an increase in the noise is noted, indicating this section has started up.

T4 should then be trimmed by NOT MORE THAN A TURN EITHER WAY, to peak the noise apparent in the output. With the i.f. section thus optimised, the detector T5 may be adjusted, again by not more than a single turn, and you should notice a distinct change in the character of the noise. Measuring the d.c. voltage at the junction of R5 and C14 will reveal that it changes its quiescent state be-



The finished p.c.b. mounted into the SLM case. This picture also shows the two cut-outs to be made in the case halves

Resistors

$\frac{1}{4}$ W 5% carbon film

100 Ω	1	R14
1k Ω	2	R4, R filter
2.2k Ω	2	R2,9
10k Ω	2	R1,5
47k Ω	2	R3,13
100k Ω	1	R12
150k Ω	1	R6
220k Ω	1	R8
1M Ω	3	R7,10,11

Capacitors

Ceramic

10pF	1	C19
33pF	1	C5
47pF	4	C1,2,3,6
220pF	1	C13
1nF	3	C4,15,21
10nF	6	C7,11,16,18,23,24
22nF	1	C17
47nF	1	C26
0.1 μ F (see text)	4	C9,10,14,22

Tantalum

1 μ F 35V	1	C12
47 μ F 16V	2	C8,25

Polystyrene

470pF	1	C20
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1N914	1	D3

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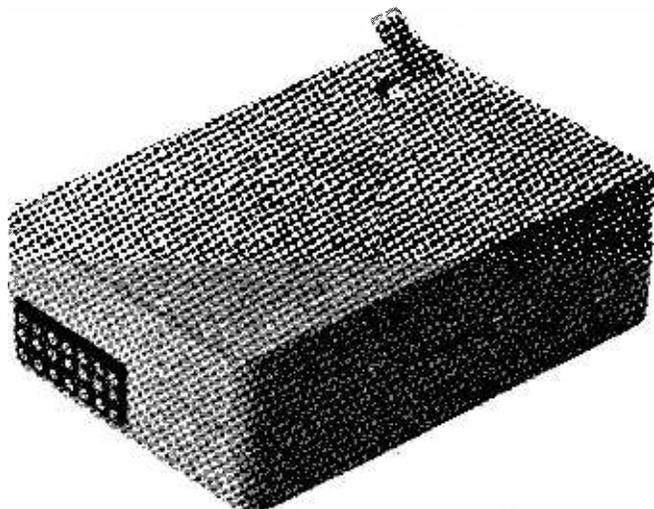
Inductors

113CNF2K509ADZ	3	T1,2,3
LLC4828	1	T4
LMC4102A	1	T5
33mH	1	L1
All by Toko		

Miscellaneous

Filter CFW455HT (Murata); Crystal (see text), Cambion cage jacks (2); p.c.b. (1); 14 pin d.i.l. socket (1); 16 pin d.i.l. socket (2); 7 channel socket block (SLM); Case PT309 (SLM).

tween extremes of 1 and 3 volts as the detector coil T5 is rotated. This is because the d.c. level follows the characteristic 'S' curve of the f.m. discriminator, with the noise shaped in the i.f. filter providing sufficient 'substance' for the detector to operate. The detector will usually be set at the halfway point between the voltage extremes, corresponding to the crossing point of the detector curve, for symmetrical modulation systems such as speech. But in p.w.m. systems, the information relies on only the two logic levels 0 and 1, and the quiescent point should not be set using an unmodulated carrier from the transmitter/encoder, as this represents one extreme of the detector curve. Accordingly, although an approximation may be made by 'centering on noise', the detector should be adjusted for most consistent results when using a correctly modulated carrier. Thus a sinewave-modulated generator set for about 1-1.5kHz deviation will not give the best results in practice.



The value of R4 may need some adjustment, since this is providing bias for the noise squelch amplifier. Listening to the output of this amplifier at pin 11, using a crystal ear-piece may reveal a rather broken sound under no-signal conditions, rather than the usual white noise hiss—and the value of R4 should then be changed for 10kΩ, up to a maximum of about 47kΩ until the output at pin 11 is a constant hiss. The detector setting will have a considerable bearing on the choice of R4, and so you must satisfy yourself that the setting of T5 is accurate before changing R4, as retuning T5 may necessitate a further change in R4. Now check the d.c. voltage at the output of the noise—the signal should be approaching 0V, rising to Vcc as the noise is slowly reduced. During reception of an r.c. transmission, part of the waveform will be detected, and so point C may not be at Vcc, although it should not approach the reset level of the decoder.

In the development of this circuit, two basic prototype stages were evolved, and over 10 actual receivers of the final design have been made, proving the results achieved. This should give confidence to first-time builders that the design is repeatable so long as the correct components are used.

Part 2 deals with the transmitter and its construction.

A licence is required to operate radio control equipment. This costs £2.80 for five years. Application forms are available from: The Home Office, Radio Regulatory Dept., Waterloo Bridge House, Waterloo Road, London SE1 8UA

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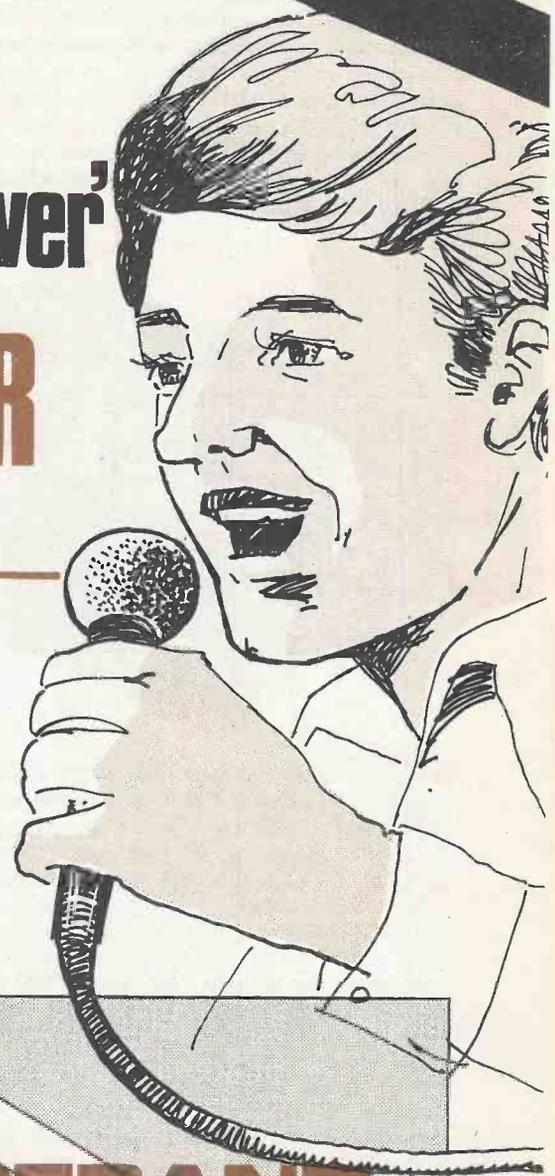
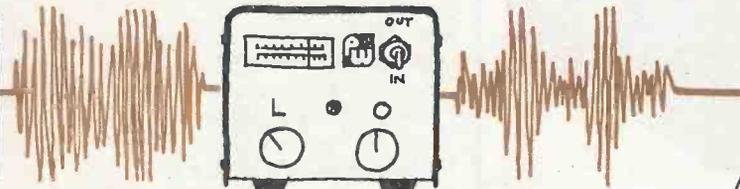
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The 1-off price is £18.37 plus VAT and 75p P&P from: *OMB Electronics, 30 Riverside, Eynsford, Kent. Tel: (0322) 863567.*



Nice Pair

Lascar Electronics have recently introduced two new digital multimeters. Both have l.c.d. readouts for clarity and long battery life, and are claimed to be considerably lower cost than imported products of similar specification.

The LMM-100 is suitable for field or bench use, has 25 different ranges, a basic accuracy of 0.1% and is priced at £69.95 plus VAT.



The LMM-200 is a compact hand-held instrument, with 15 different ranges, a basic accuracy of 0.5% and a 200 hour battery life. It is priced at £34.95 plus VAT.

Another ten instruments are to be introduced over the next year and eventually, the range will include frequency counters, counter-timers, thermometers and other general purpose instruments. All with feature l.c.d. readouts.

Lascar Electronics, Unit 1, Thomasin Road, Burnt Mills Industrial Estate, Basildon, Essex. Tel: (0268) 727383.

New Cassette

Agfa-Gevaert have recently introduced a new tape cassette—Agfa Superchrom—and added 6 more minutes of playing time (3 mins each side) to their entire range of C60s and C90s. They are also re-launching the cassette range in new packing designs and colours.

Agfa Superchrom is a new, highly sophisticated dual-layer chrome tape which records at very high levels without distortion. In the company's own laboratory tests, Superchrom registered a t.h.d. of only 1.5%—significantly lower than the 2.2% of a Japanese competitor. At 62dB, the new cassette also has a wider dynamic range than any other cassette—by 2dB, Agfa claim.

Agfa Superchrom is also said to overcome the traditional weakness of chrome tapes in the middle to lower frequencies, having perfect linear response from 333Hz to 10kHz. It has been produced for machines with CrO₂ switching, and Agfa assert it has no rival in terms of sophistication and technical performance.

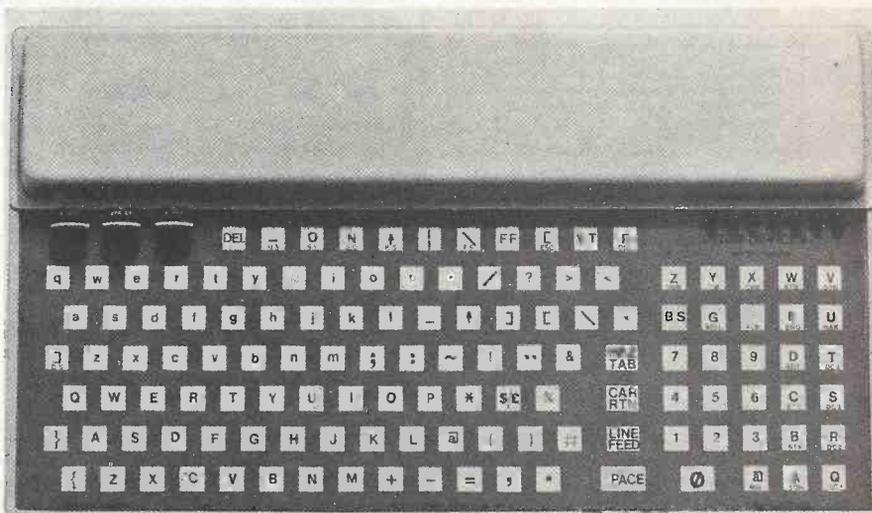
Further details from: *Magnetic Tape Products, Agfa-Gevaert Ltd., 27 Great West Road, Brentford, Middx. Tel: 01-560 2321.*

ASCII Keyboard

The latest from Star Devices is an ASCII encoded touch keyboard which measures 365 x 203 x 31mm, weighs 454 grams and operates within a temperature range of 0° to 35°C.

The complete "stand-alone" data terminal features 7-bit parallel ASCII encoded output; positive and negative strobe edges; full ASCII set—128 characters—upper and lower case in dual QWERTY layout, individual pads for all control codes; all code outputs will drive 4 t.t.l. loads; i.e.d.s to show ASCII code of selected character; audio feedback with volume/tone control; character output rate continuously adjustable from 0.1 to 1 second; auto repeat and modified 2 key rollover; automatic scan facility—will automatically scan through and output each character in the ASCII set, useful for testing and setting-up systems; operational life in excess of 250 million operations.

Requiring a power supply of 5V d.c. ±0.25V at only 200mA, the keyboard



is presented in a low profile case with non-slip feet and wipe-clean polyester touch pad area with back printed characters, which eliminates wear-off.

The assembled, "burnt in" and tested keyboard, manufactured in the

UK carries a six month guarantee and costs £37.50 plus VAT.

Further details of optional extras and availability from: *Star Devices Ltd., PO Box 21, Newbury, Berkshire. Tel: (0635) 40405.*

Outside Detector

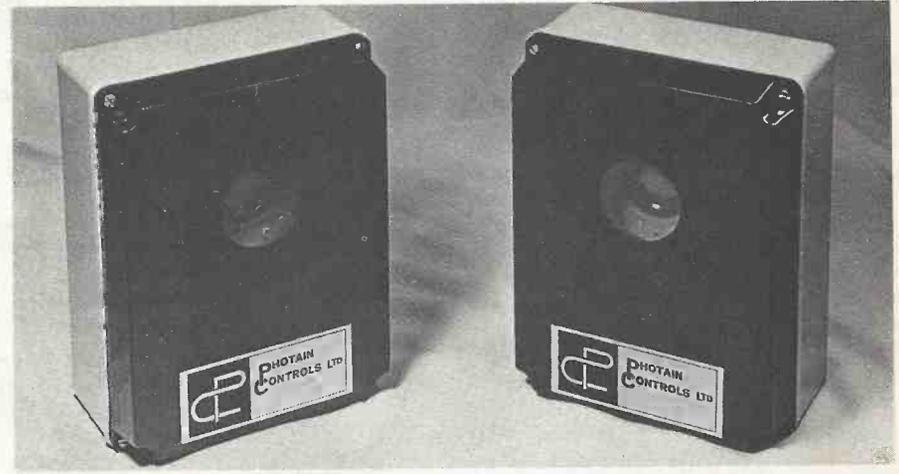
It is now generally accepted that the protection of property is primarily the responsibility of the owner and that he should take appropriate action within the law to minimise his risk.

Most alarm systems are based on detecting intruders entering buildings, but now the emphasis will have to change with the object of detecting intruders before entry is attempted thereby enabling the occupier to take appropriate action in good time. Exterior detection of potential intruders presents a number of problems not associated with internal protection and, depending upon the layout of any particular site, it is not always possible to provide complete protection at an economical price. However, any form of prior warning is worthy of consideration and to meet this need Photain Controls Ltd., have designed a new Pulse Modulated Gallium Arsenide Infra-Red Beam Unit, which is contained in a waterproof housing and will provide coverage up to a distance of 50 metres.

The unit comprises two housings, one containing the solid state infra-red emitting device complete with optical system and associated circuitry and the other containing the photocell, optical system, de-modulator circuit and with an output relay. The relay is normally

energised and when the beam is interrupted the relay is de-energised changing over the output contacts to perform a switching function. The switching function can be designed to provide a variety of warnings for example:

1. To operate an alarm bell for a period of time (say 5-50 seconds) and then to automatically re-set.
2. To operate an alarm bell continuously until manually re-set by a push button inside the building.
3. To switch on exterior floodlights either for a timed period or until manually re-set.



4. To operate silent alarms inside the premises or remotely to the police.

Various units are available, starting with a beam range of 5 metres up to a beam range of 50 metres. Prices start at £40 plus VAT to £80 plus VAT. The units operate from the mains supply and the output contacts are rated at 5 amps, alternative models are also available operating from a 12V d.c. supply.

Further details from: *Photain Controls Ltd., Unit 18, Hangar No. 3, The Aerodrome, Ford, Nr. Arundel, West Sussex BN18 OBE. Tel: (09064) 21531.*

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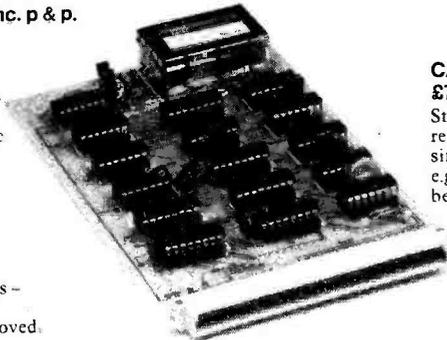
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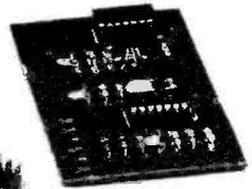
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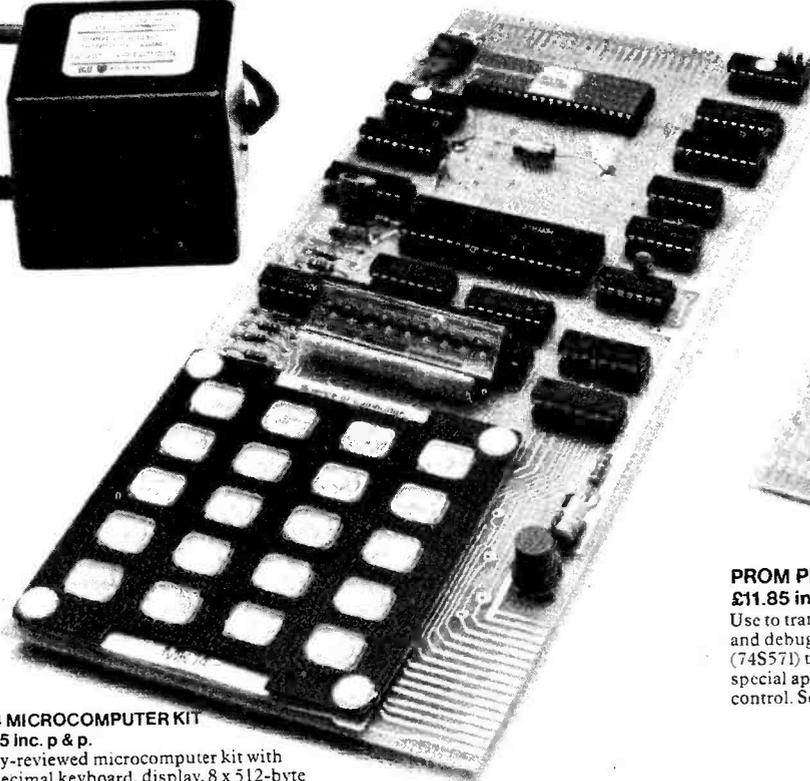
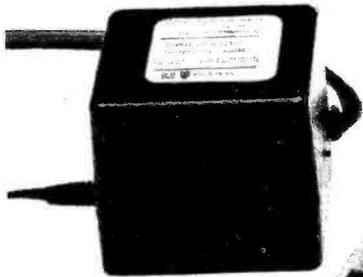
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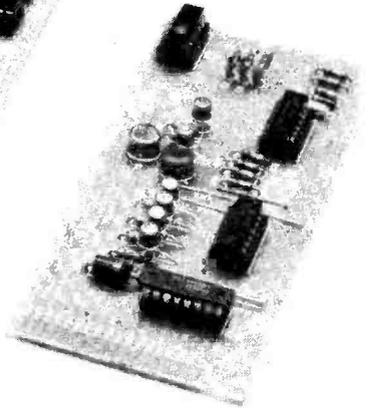
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HI-FI GLOSSARY

3

Gordon J. KING

D

DECODER

This is a passive or active circuit which restores the "integrity" of programme material subsequent to *encoding* (see under Encoder). The *multiplex decoder* used in f.m. stereo receivers exemplifies one such application. It is the job of this decoder to reclaim the separate left and right stereo signals from the encoded stereo multiplex information which is modulated on the v.h.f. (very high-frequency) carrier wave (Fig. 10).

In certain types of *noise reduction* circuits, such as Dolby B which is used in domestic cassette decks, the

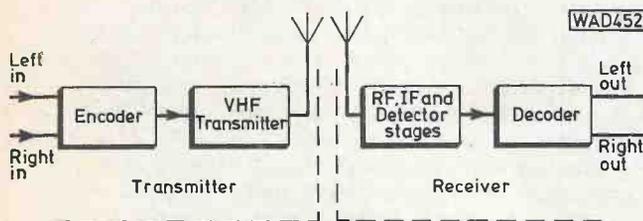


Fig. 10: Basic principle of f.m. stereo encoding and decoding

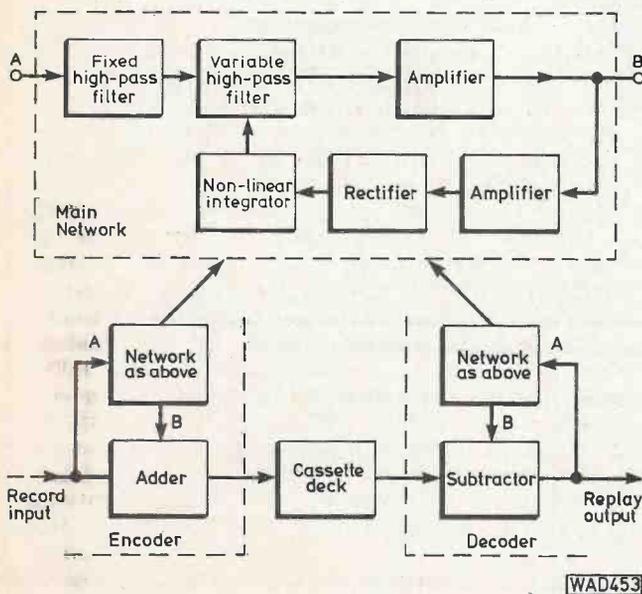


Fig. 11: Block diagram of Dolby B noise reduction encoding and decoding

signal is first encoded during recording and then decoded during replay to restore the frequency response integrity while at the same time reducing the noise content. What happens here is that the upper-frequency part of the recording signal is boosted by an amount determined by the signal level. On high-level signals corresponding to a recording level of 200nWb/m (this is called the *Dolby level*) or more, no boost is applied, but as the level reduces so more upper-frequency boost is progressively applied, reaching a maximum of 10dB.

When the encoded signal is replayed, the Dolby decoder comes into operation and introduces upper-frequency attenuation to correspond to the boost applied during recording. The attenuation is thus also determined by the signal level. The net result is not only restored frequency integrity but also a significant improvement in *signal/noise (S/N) ratio* owing to the integrated upper-frequency noise being reduced by an amount corresponding to the decoding attenuation.

The scheme ensures that maximum noise reduction occurs only on low-level signals thereby avoiding impairment to the effective *dynamic range*. The higher level signals automatically mask the noise, anyway. A block diagram of the encode and decode parts of the Dolby B noise reduction system is given in Fig. 11.

It will be appreciated that the encode and decode sections need to track with changing signal level very accurately to avoid frequency response errors when replaying a tape, and for this reason the gains of the two sections need to be normalised with respect to a tape of given sensitivity. Some cassette decks are equipped with a 400Hz oscillator for recording a suitable level tone on the tape used, so that on replay the decoder gain can be adjusted to yield a corresponding output.

DE-EMPHASIS

For some applications, notably f.m. radio, a fixed amount of upper-frequency boost is introduced at the input. This calls for a fixed amount of treble attenuation at the output for correct frequency integrity, which is generally called *de-emphasis* (also see under *Pre-emphasis*). Because of this the noise is also reduced. However, because of the fixed pre-emphasis, the average level of input signal needs to be restricted to avoid overloading at the high frequencies. The frequency at which the input treble boost and the output treble attenuation start to take effect is commonly referred to a simple time-constant. The European (including the UK) time-constant for f.m. radio (and TV) is 50µs, which corresponds to a -3dB frequency of $1/2\pi T$ (where T is the time-constant in seconds), or 3184Hz. The time-constant in the USA is 75µs, corresponding to a -3dB (turnover) frequency of 2123Hz.

When Dolby B noise reduction is used on f.m. (in the USA—in the UK this has so far only been experimented with) the time-constant is reduced to 25µs (6369Hz turnover frequency).

If the receiver set for the American standard is used in the UK the treble frequencies are rolled-off prematurely. Conversely, if a receiver set for the European standard is used in America the treble frequencies are boosted.

HI-FI GLOSSARY

DIN

These are the initials of the German Industrial Standards organisation, or *Deutscher Industrie Normen*—and not to be confused with the noises produced by dubious so-called hi-fi systems! It commonly refers to the standards for plugs, sockets, equalisation, measurement references and so forth, but also includes the basic requirements for hi-fi under DIN 45-500. Like our own British Standards Institution (BSI), it also defines the standards for numerous items outside the field of hi-fi and electronics.

As DIN 45-500 refers essentially to the basic requirements for hi-fi (though it is being updated) it is not regarded by UK hi-fi devotees as a very strict standard, and many items of hi-fi carrying the DIN 45-500 label often exceed the minimum requirements.

DROP-OUT

When there is a momentary vanishing of signal from a recording tape this is commonly referred to as a drop-out. It is caused either by a flaw in the magnetic-oxide or metal-particle coating of the tape or a mechanical aberration resulting in the tape momentarily losing contact with the tape head. Some tapes are more prone to drop-out problems than others, which is one reason why cheap, non-proprietary tapes cannot be recommended for use with hi-fi decks. Another reason is that the loose oxide particles of cheap tapes can clog the minute gaps of the heads and impair the upper-frequency response, the output, S/N ratio and the erase ratio.

DYNAMIC RANGE

One aspect of this is the dB distance between the highest *distortion-limited output* and the noise floor of the reproducing equipment, including the noise of the programme source itself. For example, if the distortion-limited output of a cassette deck with a particular brand of tape is referred to 0dB and 3 per cent distortion and the noise floor is 50dB below this output, then the effective dynamic range would be 50dB.

With acoustic programme material such as “live” music from a concert hall the dynamic range is the difference in *phons* between the strongest and the weakest sounds.

With hi-fi equipment some sort of *noise weighting* is commonly adopted so that the annoyance value of the noise correlates to the measurement. With *CCIR weighting*, for example, a cassette deck with Dolby B noise reduction might return a dynamic range of 65dB at low and middle frequencies with chrome or pseudo chrome tape, a hi-fi f.m. tuner 72dB stereo, and a hi-fi amplifier 75dB at pickup input, the latter referred to an output of 1W, which is thus more accurately the S/N ratio.

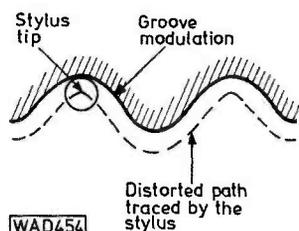


Fig. 12: Illustration of tracing distortion

E

EIGENTONE

This term refers to sound resonance in a room owing to parallel boundaries. The effect is basically the “bouncing” of the waves to and fro between the parallel surfaces before they decay to a non-disturbing value. When the inter-boundary spacing is a multiple of half the wavelength of the sound the reflections become phase coincident and a *standing wave* resonance is then evoked, so that a listener moving in the sound field will experience successive *nodes* and *antinodes* as he traverses the line of wave incidence.

A primary eigentone corresponds to a sound whose wavelength corresponds to twice the distance between the boundaries. For example, if two parallel surfaces (walls) are spaced by 6m then the room will produce a strong eigentone around 30Hz and possibly “colour” the reproduction. The frequency of a sound can be found from c/λ where c is the propagation velocity (close to 344 metres per second at sea level and 20°C) and the wavelength in metres (frequency in Hz). By remembering that an eigentone results from half a wavelength it is possible to calculate the frequency of an eigentone which will develop between any two parallel surfaces.

Coloration resulting from eigentones can be reduced by damping the boundary interfaces with acoustic tiles, drapes, etc., but the effect of such damping tends to diminish with decreasing frequency. It has been calculated that, based on unity height, the best dimensions for hi-fi are 1.25 width and 1.6 length for a small room, and 1.6 width and 2.5 length for a large room.

ELLIPTICAL STYLUS

One aberration of disc replay is the distortion resulting from the tip of the stylus tracing high-frequency, short wavelength groove modulation, as shown in Fig. 12. This is called *tracing distortion* which can only be reduced by decreasing the radius of the stylus tip so that the short wavelength modulation can be better defined.

When this is done with a spherical tip, the tip tends to “bottom” in the groove and decrease the S/N ratio. This is combated by the so-called elliptical stylus which has a small radius for defining the modulation and a larger radius across the groove to avoid bottoming.

EQUALISATION

For recording or transmission it is often necessary to tailor the programme signal to suit the medium concerned. For example, disc recording calls for a progressively decreasing recording level with reducing frequency to prevent inter-groove collapse on loud bass signals. This

HI-FI GLOSSARY

is equalised during replay by passing the pickup signal through an amplifier whose gain rises with decreasing frequency.

At the other end of the spectrum it is desirable to give the recording signal a boost (*pre-emphasis*) so that the corresponding degree of attenuation on replay not only restores the frequency integrity but also reduces the noise. As with f.m. radio, time-constants are used to define the turnover frequencies, and with disc records these are 318 and 75 μ s. In addition, there is a low-frequency turnover of 3180 μ s (more recently also a subsonic turnover according to IEC 65) to avoid disc ripple effects on replay. These time constants collectively yield *RIAA record equalisation*.

Equalisation is also required for tape recording and replay. When a magnetic tape recorded at a constant input from low to high frequencies is replayed, the output from low to high frequencies rises at the rate of 6dB per octave up to a certain high-frequency where head and tape losses cause the output to start falling. In the replay amplifier, therefore, the gain needs to rise at 6dB per octave with decreasing frequency, while at that frequency where the head and tape losses come into play a suitable upper-frequency boost is also required. The upper-frequency losses are also countered to some degree by the application of treble boost (pre-emphasis) during recording.

The turnover frequencies involved depend on the tape speed and the magnetic properties of the tape. With cassette machines the time-constant is 120 μ s for basic ferric tape and 70 μ s for chrome, pseudo chrome, ferrochrome and metal particle tapes. As with disc replay, there is a further low-frequency time-constant of 3180 μ s to reduce the effects of mains ripple during replay.

ENCODER

This is a device which restores the integrity of the programme material during replay when the material has been subjected to encoding during recording or transmission (see under Decoder).

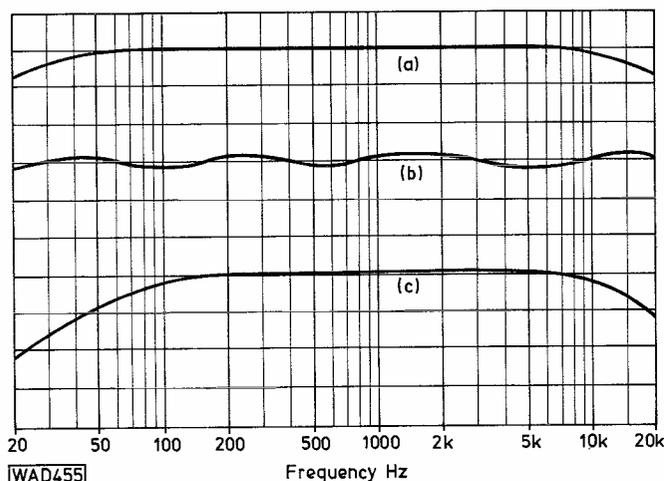


Fig. 13: Three types of frequency response defined in the text

F

FLUTTER

This term is commonly associated with tape machines and record players and refers to a waver of pitch resulting from spurious fluctuations of speed at periods in excess of about 10Hz. Lower rate fluctuations are referred to as *wow*. Flutter can cause an undesirable "roughness" to the reproduction as the result of intermodulation products. *Wow and flutter* are usually measured together by a suitable instrument, often via a *weighting network* to provide a more valid subjective indication, one standard being DIN peak weighted, often seen in the hi-fi literature.

FREQUENCY RANGE

This is the range of frequencies over which an item of equipment is operative. Because no defined output limits are included it is not a very meaningful *parameter* and one which should be treated with suspicion when reading the specification of an item of hi-fi equipment.

FREQUENCY RESPONSE

The frequency *response* is the range of frequencies provided by the equipment within prescribed output (usually dB) limits. The frequency response differs from the *power response* in as much as the former is measured at a low level (well below the full output yield of the equipment), while the latter is measured at or close to the rated output. The frequency response is commonly quoted as that frequency range between low and high terminal frequencies where the output is 3dB below that at 1kHz, as shown in Fig. 13 at (a).

A greater accuracy is provided by referring to the ± 1 dB undulations within a stated frequency range. Curve (b) in Fig. 13, for example, could be written as ± 1 dB 20Hz–20kHz. Curve (c) in Fig. 13 could be defined as 60Hz–15kHz -3 dB $+0.5$ dB, or as 150Hz–8.5kHz ± 0.5 dB. The greatest accuracy of all, of course, is provided by the frequency response curve proper being a part of the specification.

FRINGE AREA

This is the area in advance of the normal *service area* range of a transmitting station, usually an f.m. or TV station. The reliable reception range of a v.h.f. transmitter is a trifle in advance of the line-of-sight distance between the top of the transmitting and receiving aerials, assuming there are no large obstructions in between. This gives the *service area distance*, which corresponds in miles to $1.5\sqrt{h_t}$ plus $1.5\sqrt{h_r}$, where h_t and h_r are the heights of the transmitting and receiving aerials in feet. For example, if

HI-FI GLOSSARY

the height of h_1 is 1000 feet and the height of h_2 100 feet, then we get $47 \cdot 43 + 15$, or 62.43 miles.

This distance, however, can only be regarded as approximate because it depends on the power of the transmitter and on the prevailing *tropospheric conditions*. The factor 1.5 can increase during a spell of high pressure conditions (e.g., anticyclonic weather) and thus propagate v.h.f. signals more deeply into the fringe area.

H

HAAS EFFECT

A sound source is located by a listener by the differences in intensity and time of arrival of the sound waves at his two ears. Imagine two stereo speakers each emitting corresponding sound, of equal intensity but that the sound from one speaker is slightly delayed with respect to that from the other. A listener placed at an equal distance from the two speakers will hear the sound as though emanating from that speaker which is not subjected to the delay. This is called the *precedence effect* or Haas effect. If there is no delay, then the sound will appear to emanate from a point midway between the two speakers when the intensities are equal. If the sound from one speaker is louder than that from the other the sound will appear to come from the speaker of loudest sound.

These two properties of human hearing make it possible for us to enjoy stereo reproduction from a two-channel system; but it is the Haas effect which is the dominating factor, for with a 50ms delay the sound intensity from that speaker needs to be stepped up by some 10dB or more to reverse the apparent balance of sound.

HALF-POWER BANDWIDTH

If the rated power of an amplifier is, say, 50W, the half-power is 25W, which is 3dB down from 50W. Now, one way of expressing the bandwidth of a power amplifier is to locate the lower and upper frequencies at half power where the distortion is, say, 1% (or, perhaps, a lower value). This is shown diagrammatically in Fig. 14.

HANGOVER

Not quite the same as the morning after the night before, but just as disconcerting! The effect results from the speaker cone or diaphragm continuing in motion after the passing of a sharp transient. What happens is that the cone or diaphragm overshoots, undershoots, overshoots and so on at diminishing amplitude until all the stored energy has been exhausted. It can result from a very low damping factor (see Part 2) or from "ringing" (e.g., *damped oscillations*) in a filter circuit or part of the amplifier or receiver. The result is that the "edge" is taken from the music definition and the absolute attack of the reproduction is weakened.

HARMONIC DISTORTION

This results from amplitude non-linearity such that a ratio of increase or decrease of input signal does not result in precisely the same ratio of increase or decrease of output signal. A perfectly linear amplifier would have a straight line transfer (input/output) characteristic as shown by the broken line in Fig. 15. In reality no such amplifier exists. All have a very slightly curved characteristic as shown by the full line in the diagram, which is very much exaggerated, for the curvature of hi-fi amplifiers would not be detectable diagrammatically at this scale.

The mathematical nature of the characteristic determines the order of the distortion produced. A characteristic of even powers produces even-order distortion, such as second-, fourth-, sixth-, etc., harmonic, while a characteristic of odd powers produces odd-order distortion, such as third-, fifth-, seventh-, etc., harmonic. It is generally considered, and agreed by myself, that even-order distortion is more palatable than odd-order distortion, and this applies also to the odd-order (e.g., third-order) *intermodulation distortion* that odd-order non-linearity also evokes.

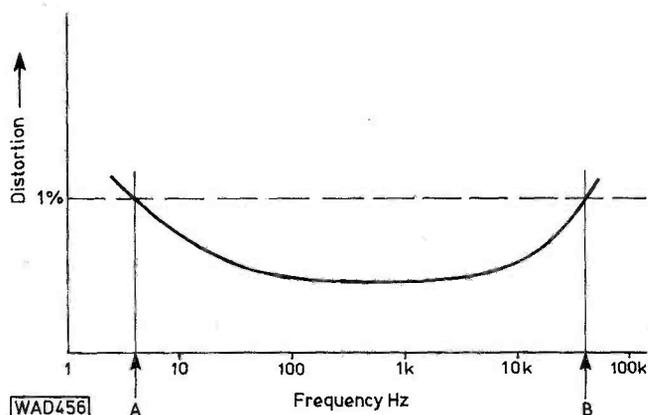


Fig. 14: Definition of half-power bandwidth

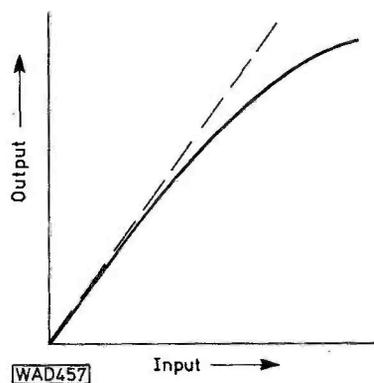


Fig. 15: Transfer characteristic of amplifier. Ideal state shown by the broken-line (perfectly linear), and realistic state (exaggerated) shown by the full-line curve

HI-FI GLOSSARY

HOLE-IN-THE-MIDDLE EFFECT

When the spacing of the two stereo speakers is correctly established in relation to the listening distance from the stereo pair, the sound appears to emanate evenly across the *sound stage* between the two speakers. However, if the two speakers are too far apart or if the phasing between the two is wrong, then there may appear to be an absence of sound coming from the centre of the sound stage. This is sometimes referred to as the hole-in-the-middle effect. If a large room or hall necessitates the use of wide speaker spacing, the hole-in-the-middle can be filled by the use of a third, centre speaker being fed with a correct mix of left and right signals.

HUM-LOOP

When a hi-fi system is earthed in more than one place, it is possible for minute mains ripple currents to flow round the closed earth loop and appear in series with low-level programme source signals, especially the small signals delivered by the gramophone pickup. When this happens a disconcerting background hum mars the reproduction.

The only solution to this problem lies in disconnecting the earths from all but one item of equipment, which is usually the amplifier. However, extreme care is essential when running certain items of hi-fi without an earth,

because under a fault condition this could render the system lethal! Some of the more recent equipment is designed with so-called Class II insulation, which avoids the need for earthing and hence makes it virtually impossible to create a hum-loop condition. However, if in any doubt at all about hi-fi earthing please always consult a reputable hi-fi dealer. It is better to be safe than sorry, particularly since all members of the family are likely to use the hi-fi system.

Index of Partly Defined Jargon

| | |
|----------------------------------|--------------------------|
| Antinode | Phons |
| CCIR weighting (also see Part 2) | Power response |
| Coloration | Precedence effect |
| Damped oscillations | Pre-emphasis |
| Deutscher Industrie Normen | Service area |
| Distortion limited output | Signal/noise (S/N) ratio |
| Dolby level | Sound stage |
| Dynamic range | Standing wave |
| Encoding | Tracing distortion |
| Intermodulation distortion | Tropospheric conditions |
| Multiplex decoder | Weighting network |
| Noise reduction | Wow and flutter |

TO BE CONTINUED

AERIALS for 160 Metres

▶▶▶ continued from page 26

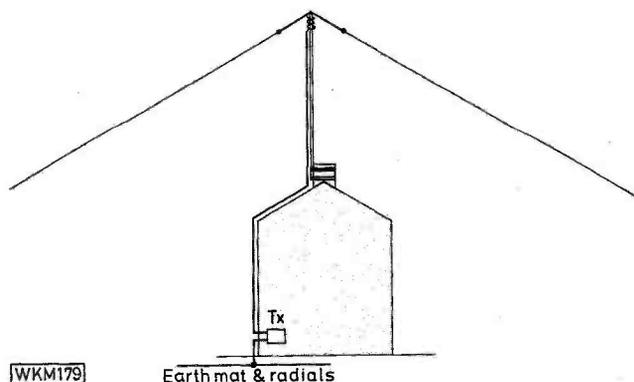


Fig. 12: If space does not permit a mast in the garden, the aerial of Fig. 11 may be mounted on the house-top

base, then commonsense suggests that they should run under the aerial's top section, although this may well affect the directivity. In the immediate vicinity of the aerial base, the ground current is highly concentrated and an earth mat of many interconnected wires, or chicken-wire mesh should be used.

To summarise the various recommendations, the author's "practical" 160m top-loaded vertical is shown in Fig. 11. If garden space does not allow the erection of a mast, the aerial may be mounted atop the house, on a chimney stack for instance, as shown in Fig. 12.

Semiconductor Tester ▶▶▶ continued from page 33

The two out-of-phase voltages are then passed to two complementary emitter followers which act as current output buffers. Fed through 100kΩ variable resistors, they are connected to the test sockets and also applied to the oscilloscope X and Y amplifiers. Before testing components, VR1 and VR2 are adjusted to give a good circular pattern on the screen.

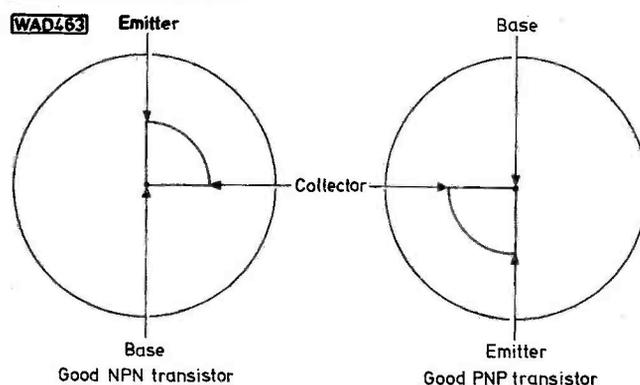


Fig. 3: The displays for good transistors showing the portions of the display representing the base, emitter and collector connections

Construction

Veroboard can be used for the main components, the actual layout not being critical. Power can be derived from two 6V batteries and the completed unit housed in a suitably sized plastics box. Screw terminals can be used to connect the device under test but a specially made socket would be preferable.

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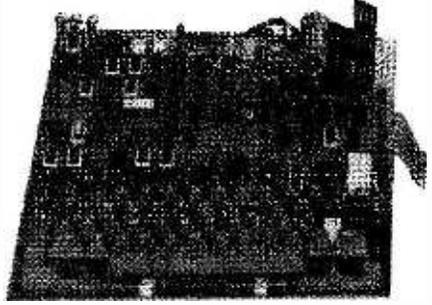
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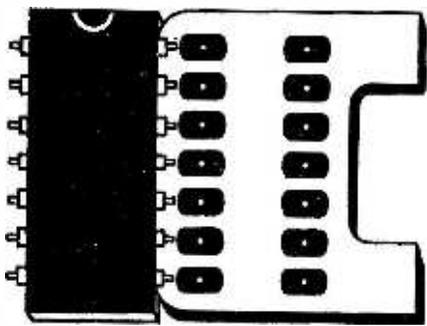
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| 7400 | 11n | 7497 | 150p | 74221 | 160p | 74LS192 | 140p | 74C157 | 250p | AY1-0212 | 680p | MC1496 | 120p | AC127/8 | 20p | BFY51/2 | 22p | TIP41C | 78p | 2N3866 | 90p | BY127 | 12p | | | |
| 7401 | 12n | 74100 | 130p | 74259 | 250p | 74LS193 | 140p | 74C160 | 155p | AY1-1313 | 680p | MC3340 | 120p | AD149 | 70p | BFY56 | 33p | TIP42C | 140p | 2N3903/4 | 18p | OA47 | 82p | | | |
| 7402 | 12n | 74104 | 65p | 74265 | 90p | 74LS195 | 140p | 74C161 | 155p | AY1-5050 | 212p | MC3580 | 120p | AD161/2 | 45p | BFY56 | 90p | TIP2955 | 78p | 2N4036 | 65p | OA81 | 15p | | | |
| 7403 | 14n | 74105 | 85p | 74273 | 280p | 74LS221 | 100p | 74C163 | 155p | AY5-1224A | 225p | MK50598 | 750p | BRX39 | 11p | BRX39 | 15p | TIP3055 | 70p | 2N4058/9 | 12p | OA85 | 15p | | | |
| 7404 | 14n | 74107 | 34p | 74279 | 140p | 74LS240 | 175p | 74C164 | 120p | AY5-1315 | 600p | NE543K | 225p | BU105 | 190p | BU105 | 190p | TIS43 | 34p | 2N4050 | 12p | OA90 | 9p | | | |
| 7405 | 18p | 74109 | 55p | 74283 | 190p | 74LS241 | 175p | 74C173 | 120p | AY5-1317 | 320p | NE555 | 25p | BU108 | 250p | BU205 | 220p | TIS43 | 34p | 2N4051/2 | 18p | OA91 | 9p | | | |
| 7406 | 32p | 74110 | 55p | 74284 | 400p | 74LS242 | 175p | 74C174 | 100p | CA3046 | 70p | NE561B | 425p | BU157/8 | 10p | BU208 | 240p | ZT X108 | 12p | 2N4123/4 | 22p | OA95 | 9p | | | |
| 7407 | 32p | 74111 | 70p | 74285 | 400p | 74LS243 | 175p | 74C175 | 210p | CA3048 | 225p | NE568B | 425p | BC147/8 | 9p | BU208 | 240p | ZT X500 | 16p | 2N4289 | 20p | OA200 | 9p | | | |
| 7408 | 32p | 74116 | 200p | 74290 | 150p | 74LS244 | 180p | 74C182 | 190p | CA3048 | 70p | NE566 | 155p | BC159 | 11p | BU208 | 240p | ZT X502 | 16p | 2N4401/3 | 27p | 1N914 | 4p | | | |
| 7409 | 19p | 74118 | 130p | 74294 | 200p | 74LS245 | 200p | 74C194 | 220p | CA3080E | 12p | NE565 | 130p | BC169C | 12p | BU208 | 240p | ZT X504 | 30p | 2N4427 | 90p | 1N916 | 7p | | | |
| 7410 | 15p | 74119 | 210p | 74298 | 200p | 74LS257 | 120p | 74C195 | 110p | CA3080E | 225p | NE566 | 155p | BC171/2 | 12p | BU208 | 240p | ZT X504 | 30p | 2N4427 | 90p | 1N916 | 7p | | | |
| 7411 | 24p | 74120 | 110p | 74300 | 200p | 74LS259 | 175p | 74C221 | 175p | CA3090A | Q375p | NE567 | 175p | BC177/8 | 17p | BU208 | 240p | ZT X504 | 30p | 2N4427 | 90p | 1N916 | 7p | | | |
| 7412 | 24p | 74121 | 90p | 74305 | 150p | 74LS298 | 240p | 74C221 | 175p | CA3130E | 100p | RC4151 | 400p | BC179 | 15p | MJ2501 | 225p | 2N457A | 250p | 2N4871 | 60p | 1N4148 | 4p | | | |
| 7413 | 30p | 74122 | 48p | 74306 | 150p | 74LS298 | 240p | 74C221 | 175p | CA3140E | 70p | SN76003N | 175p | BC182/3 | 10p | MJ2501 | 225p | 2N457A | 250p | 2N4871 | 60p | 1N4148 | 4p | | | |
| 7414 | 60p | 74123 | 48p | 74307 | 150p | 74LS373 | 200p | 4000 | 15p | CA3160E | 75p | SN76013N | 140p | BC184 | 11p | MJ2501 | 225p | 2N457A | 250p | 2N4871 | 60p | 1N4148 | 4p | | | |
| 7416 | 27p | 74125 | 55p | 74308 | 200p | 74LS374 | 195p | 4001 | 17p | ICL7106 | 925p | SN76013N | 140p | BC187 | 30p | MJ2501 | 225p | 2N457A | 250p | 2N4871 | 60p | 1N4148 | 4p | | | |
| 7417 | 27p | 74126 | 60p | 74309 | 200p | 81LS96 | 140p | 4002 | 17p | ICL8038 | 325p | SN76013N | 140p | BC212/3 | 11p | MJ2501 | 225p | 2N457A | 250p | 2N4871 | 60p | 1N4148 | 4p | | | |
| 7421 | 40p | 74132 | 75p | 74490 | 225p | 81LS96 | 140p | 4006 | 85p | ICL8038 | 325p | SN76013N | 140p | BC214 | 12p | MJ2501 | 225p | 2N457A | 250p | 2N4871 | 60p | 1N4148 | 4p | | | |
| 7422 | 22p | 74136 | 60p | 74 LS | | 81LS98 | 140p | 4007 | 18p | LM301A | 36p | SN76033N | 125p | BC477/8 | 30p | MJ2501 | 225p | 2N457A | 250p | 2N4871 | 60p | 1N4148 | 4p | | | |
| 7423 | 34p | 74141 | 70p | 74 LS | | 81LS98 | 140p | 4008 | 80p | LM311 | 190p | SN76033N | 125p | BC516/7 | 50p | MJ2501 | 225p | 2N457A | 250p | 2N4871 | 60p | 1N4148 | 4p | | | |
| 7425 | 30p | 74142 | 200p | 74LS00 | 13p | 8301 | 160p | 4009 | 40p | LM318 | 200p | SP6515 | 750p | BC547/8 | 16p | MJ2501 | 225p | 2N457A | 250p | 2N4871 | 60p | 1N4148 | 4p | | | |
| 7426 | 40p | 74145 | 90p | 74LS02 | 18p | 8302 | 175p | 4010 | 50p | LM324 | 70p | TBA441B11 | | BC549C | 18p | MJ2501 | 225p | 2N457A | 250p | 2N4871 | 60p | 1N4148 | 4p | | | |
| 7427 | 34p | 74147 | 190p | 74LS04 | 14p | 8308 | 315p | 4011 | 18p | LM339 | 90p | TBA441B11 | | MPSA12 | 50p | MPSA12 | 50p | 2N1210 | 60p | 2N5459 | 40p | SPECIAL OFFERS | | | | |
| 7428 | 36p | 74148 | 150p | 74LS08 | 22p | 8310 | 275p | 4013 | 34p | LM348 | 85p | TBA800 | 90p | MPSA15 | 32p | MPSA15 | 32p | 2N2102 | 60p | 2N5459 | 40p | 100-741 | | | | |
| 7430 | 17p | 74150 | 100p | 74LS10 | 20p | 8311 | 275p | 4014 | 50p | LM377 | 175p | TBA820 | 90p | MPSU08 | 62p | MPSU08 | 62p | 2N2160 | 120p | 2N5460 | 40p | 100-741 | | | | |
| 7432 | 30p | 74151A | 70p | 74LS13 | 33p | 8314 | 165p | 4015 | 84p | LM380 | 75p | TCA940 | 175p | BC559C | 18p | MPSU58 | 78p | 2N2219A | 30p | 2N5465 | 40p | 100-741 | | | | |
| 7433 | 40p | 74153 | 70p | 74LS14 | 75p | 8316 | 225p | 4016 | 45p | LM387AN | 150p | TDA4500 | 250p | OC28 | 130p | OC28 | 130p | 2N2222A | 18p | 2N6247 | 190p | 100-741 | | | | |
| 7437 | 35p | 74154 | 100p | 74LS20 | 22p | 8322 | 150p | 4018 | 89p | LM709 | 36p | TDA1004 | 325p | OC35 | 130p | OC35 | 130p | 2N2222A | 18p | 2N6247 | 190p | 100-741 | | | | |
| 7438 | 35p | 74155 | 90p | 74LS22 | 26p | 8328 | 200p | 4019 | 45p | LM710 | 50p | TDA1008 | 300p | BF257/8 | 32p | BF257/8 | 32p | 2N2369A | 16p | 2N6247 | 190p | 100-741 | | | | |
| 7440 | 17p | 74156 | 90p | 74LS27 | 38p | 8388 | 200p | 4020 | 100p | LM733 | 100p | TDA1022 | 600p | BF258B | 70p | BF258B | 70p | 2N2369A | 16p | 2N6247 | 190p | 100-741 | | | | |
| 7441 | 70p | 74157 | 70p | 74LS30 | 22p | 8370 | 200p | 4021 | 100p | LM741 | 20p | XR2206 | 400p | BF259 | 37p | BF259 | 37p | 2N2369A | 16p | 2N6247 | 190p | 100-741 | | | | |
| 7442A | 89p | 74159 | 190p | 74LS47 | 90p | 8374 | 200p | 4022 | 100p | LM747 | 75p | XR2216 | 875p | BF259 | 37p | BF259 | 37p | 2N2369A | 16p | 2N6247 | 190p | 100-741 | | | | |
| 7443 | 112p | 74160 | 100p | 74LS55 | 30p | 8374 | 200p | 4023 | 22p | LM747 | 75p | XR2216 | 875p | BF259 | 37p | BF259 | 37p | 2N2369A | 16p | 2N6247 | 190p | 100-741 | | | | |
| 7444 | 112p | 74161 | 100p | 74LS73 | 50p | 8374 | 200p | 4023 | 22p | LM748 | 38p | XR2216 | 875p | BF259 | 37p | BF259 | 37p | 2N2369A | 16p | 2N6247 | 190p | 100-741 | | | | |
| 7445 | 100p | 74162 | 100p | 74LS74 | 40p | 8374 | 200p | 4023 | 22p | LM748 | 38p | XR2216 | 875p | BF259 | 37p | BF259 | 37p | 2N2369A | 16p | 2N6247 | 190p | 100-741 | | | | |
| 7446A | 93p | 74163 | 100p | 74LS75 | 50p | 8374 | 200p | 4023 | 22p | LM748 | 38p | XR2216 | 875p | BF259 | 37p | BF259 | 37p | 2N2369A | 16p | 2N6247 | 190p | 100-741 | | | | |
| 7447A | 70p | 74164 | 100p | 74LS83 | 110p | 8374 | 200p | 4023 | 22p | LM748 | 38p | XR2216 | 875p | BF259 | 37p | BF259 | 37p | 2N2369A | 16p | 2N6247 | 190p | 100-741 | | | | |
| 7448 | 80p | 74166 | 130p | 74LS85 | 100p | 8374 | 200p | 4023 | 22p | LM748 | 38p | XR2216 | 875p | BF259 | 37p | BF259 | 37p | 2N2369A | 16p | 2N6247 | 190p | 100-741 | | | | |
| 7450 | 17p | 74168 | 100p | 74LS86 | 40p | 8374 | 200p | 4023 | 22p | LM748 | 38p | XR2216 | 875p | BF259 | 37p | BF259 | 37p | 2N2369A | 16p | 2N6247 | 190p | 100-741 | | | | |
| 7451 | 17p | 74167 | 200p | 74LS90 | 60p | 8374 | 200p | 4023 | 22p | LM748 | 38p | XR2216 | 875p | BF259 | 37p | BF259 | 37p | 2N2369A | 16p | 2N6247 | 190p | 100-741 | | | | |
| 7453 | 17p | 74170 | 240p | 74LS93 | 60p | 8374 | 200p | 4023 | 22p | LM748 | 38p | XR2216 | 875p | BF259 | 37p | BF259 | 37p | 2N2369A | 16p | 2N6247 | 190p | 100-741 | | | | |
| 7454 | 17p | 74172 | 720p | 74LS107 | 45p | 75450 | 120p | 4030 | 50p | LM748 | 38p | XR2216 | 875p | BF259 | 37p | BF259 | 37p | 2N2369A | 16p | 2N6247 | 190p | 100-741 | | | | |
| 7480 | 17p | 74173 | 120p | 74LS112 | 100p | 75491/2 | 96p | 4033 | 180p | LM748 | 38p | XR2216 | 875p | BF259 | 37p | BF259 | 37p | 2N2369A | 16p | 2N6247 | 190p | 100-741 | | | | |
| 7470 | 36p | 74174 | 93p | C-MOS I.C.s | | 75491/2 | 96p | 4033 | 180p | LM748 | 38p | XR2216 | 875p | BF259 | 37p | BF259 | 37p | 2N2369A | 16p | 2N6247 | 190p | 100-741 | | | | |
| 7472 | 30p | 74175 | 85p | 74LS123 | 75p | 75491/2 | 96p | 4033 | 180p | LM748 | 38p | XR2216 | 875p | BF259 | 37p | BF259 | 37p | 2N2369A | 16p | 2N6247 | 190p | 100-741 | | | | |
| 7473 | 34p | 74176 | 90p | 74LS132 | 90p | 75491/2 | 96p | 4033 | 180p | LM748 | 38p | XR2216 | 875p | BF259 | 37p | BF259 | 37p | 2N2369A | 16p | 2N6247 | 190p | 100-741 | | | | |
| 7474 | 30p | 74177 | 80p | 74LS157 | 80p | 75491/2 | 96p | 4033 | 180p | LM748 | 38p | XR2216 | 875p | BF259 | 37p | BF259 | 37p | 2N2369A | 16p | 2N6247 | 190p | 100-741 | | | | |
| 7475 | 30p | 74178 | 160p | 74LS158 | 80p | 75491/2 | 96p | 4033 | 180p | LM748 | 38p | XR2216 | 87 | | | | | | | | | | | | | |



TEXAS INSTRUMENTS TL497 REGULATOR

The integrated circuit regulator device is now widely used whenever a well regulated, smoothed supply is required which can be made with the absolute minimum of trouble. The most commonly used form of regulator device employs a series pass transistor which controls the continuous current flowing into a load. One of the disadvantages of this type of regulator is that a considerable proportion of the input power can be wasted, especially when the input voltage is much higher than the output voltage.

During the past couple of years or so, another type of regulator has come onto the market which has many advantages, but also some disadvantages. This new device, known as a switching regulator, can operate with very high efficiency so that little power is wasted in the regulator circuit. Therefore, one does not need a large heatsink to keep the regulator device cool (in contrast to the heatsink required with high-current regulators employing series pass transistors). Additional advantages of switching regulator circuits include the fact that one can obtain output voltages which are lower than the input voltage, higher than the input voltage or of the opposite polarity to the input voltage. Also, if the output voltage is lower than the input voltage, the output current can exceed the input current.

In spite of the versatility of the switching regulator circuits which enable such a wide range of outputs to be obtained at high efficiency, one must remember that these devices require more complex circuitry than series pass regulator devices, which often have just input, output and ground connections. Switching regulator circuits require an inductor. This type of regulator operates by switching current to a reservoir capacitor at a high frequency and is therefore liable to generate radio frequency interference.

Basic circuits

Before we consider the TL497 device in detail, let us first discuss three basic switching regulator circuit configurations which enable (a) an output voltage lower than the input voltage to be obtained with low input current (b) an output voltage greater than the input voltage to be achieved and (c) an output of inverted polarity to be obtained.

(a) The step-down circuit. The basic circuit of the step-down switching regulator (also known as the "buck regulator") is shown in Fig. 1(a). The output voltage is always less than the input voltage.

The transistor acts purely as a fast switch. When the transistor is biased to conduction, the voltage across the diode D rises almost to the input voltage. Thus a voltage approximately equal to the difference between the input and output voltages appears across the inductor L and

causes a steadily increasing current to flow through this inductor. This increasing current ceases to flow only when the transistor ceases to conduct.

The voltage across the inductor is now reversed and the diode is biased to conduction so that the magnetic energy stored in the inductor can be passed to the reservoir capacitor C. The internal control circuit used to operate the transistor switch is controlled by an oscillator circuit which automatically increases the "on" time of the transistor if the output voltage decreases and increases the "off" time if the output voltage increases.

The output voltage is therefore maintained almost constant. As the energy stored in the inductor is recovered during the "off" time of the transistor, when no current is being taken from the input, the circuit can operate at high efficiency with the output current larger than the input current. This type of circuit can generate a relatively large amount of noise in the input line due to the rapid switching.

(b) The boost circuit. The boost regulator circuit of Fig. 1(b) can be used when one requires an output voltage greater than the input voltage. At the instant the transistor is switched to conduction, most of the input voltage appears across the inductor and the diode is reverse biased, since the collector of the transistor is only a little above earth potential.

When the transistor is switched off, the energy stored in the inductor will send a current through the diode to the reservoir capacitor. The internal circuit automatically times the switching operations so that the mean diode current is equal to the load current and therefore the output voltage remains constant.

This type of circuit has the advantage that little noise is generated in the power supply input line, since current can flow into the circuit during both of the transistor switching states. Unfortunately it is not especially easy to filter the

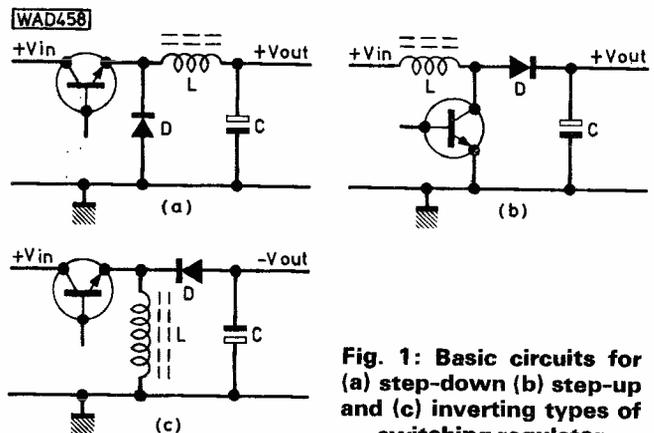


Fig. 1: Basic circuits for (a) step-down (b) step-up and (c) inverting types of switching regulator

output voltage so as to render it really smooth without any fluctuations at the switching frequency.

It should be clear that in this type of circuit the input current must exceed the output current, since otherwise there would be an inadequate flow of energy to allow the output voltage to exceed the input voltage.

(c) **The inverter or flyback circuit.** The inverter circuit of Fig. 1(c) provides a negative output voltage from a positive input voltage, the magnitude of the output voltage being either smaller or larger than the input, depending on the circuit design.

Almost the whole of the input voltage appears across the inductor L when the transistor conducts, so energy is stored in L as a magnetic field. When the transistor is switched off, the reverse voltage appearing across the inductor causes the diode to conduct so that the capacitor C becomes charged.

Both the input and output circuits tend to be quite noisy at the switching frequency in this circuit. The output should therefore be well smoothed, not merely by the use of an electrolytic capacitor (which has a high series inductance), but also by a smaller capacitor in parallel with the electrolytic.

The Texas Instruments TL497 device contains the semiconductor devices which are required to make any of the three types of circuits discussed. Output currents of up to 500mA can be obtained from the device itself, but the TL497 can also be used with an external transistor to provide much higher regulated output currents.

The basic internal circuit of the 14-pin TL497 is shown in Fig. 2. The most recent type is the TL 497A which has a Schottky type diode between pins 6 and 7, but either type can be used in the circuits to be discussed. The TL497AC is the economical commercial type.

It is important to note that the absolute maximum permissible input voltage to the TL497 device is 15V, but it is wise to limit the maximum input voltage to a somewhat smaller value, perhaps 12V, but certainly no more than 14V, so as to provide some margin of safety. The absolute maximum output voltage is 35V, but again it is wise to allow some margin of safety.

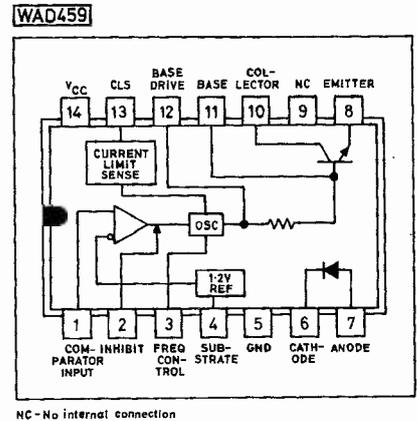
The TL497 contains an internal 1.22V precision reference voltage source. In practical circuits a fraction of the output voltage is tapped off by means of a potential divider circuit and is compared with this reference voltage by the use of the internal comparator. The output of the comparator determines whether the transistor switch is put in the "on" or in the "off" state.

Step-down circuit

A typical circuit for providing an output of +5V from an input of about +7V to +14V is shown in Fig. 3. The oscillator frequency is determined by the value of the capacitor connected between pin 3 and ground. The value of this capacitor, C_T in Fig. 3, is 150pF and this results in a maximum oscillator frequency of about 60kHz which is suitable for most TL497 circuits.

The output voltage is stabilised at a value which results in the pin 1 potential (one of the inputs to the internal comparator) being equal to the internal 1.22V reference voltage. The output voltage is divided in potential by R1 and R2, so with the values shown in Fig. 3, the pin 1 voltage is near to +1.2V. Obviously there are tolerances in the values of R1, R2 and in the value of the internal reference voltage, but if necessary R1 can be trimmed so that the circuit provides the exact output voltage needed. As the internal reference voltage is about 1.2V (actually 1.08V to 1.32V), it is convenient to choose the value of 1.2 k Ω for R2, since the output voltage is then the sum

Fig. 2: Internal components in block form of the TL497



of the values of R1 and R2 in kilohms—to a first approximation.

The use of the current sensing resistor R_{sc} between pins 13 and 14 is optional. If this resistor is omitted, these two pins should be joined directly together. If the resistor is included in the circuit, when the voltage at pin 13 is about 0.07V below that at pin 14, the internal switching transistor is turned off so that no output is obtained. Thus when the value of 1 ohm is employed for this resistor, the output current is limited to approximately 700mA and this will prevent damage to the device if the output is accidentally shorted to ground.

The circuit of Fig. 3 is based on that of Fig. 1(a). It should be clear that the inductance L and the capacitance C are in similar positions to those in Fig. 1(a), whilst the diode D of Fig. 1 is connected internally between pins 6 and 7 of the TL497 in Fig. 3.

In a typical case, the input to the circuit of Fig. 3 could be 12V at 130mA representing a power of 1.56W. The output could be 5V at 200mA which is 1W; thus the overall efficiency would be about 64%. Output ripple in this circuit is typically around 15mV.

Naturally other output voltages may be obtained by suitable choice of R1 and R2. The output voltage is equal to $(1 + R1/R2)$ times the value of the internal reference voltage.

A circuit for stepping up an input voltage of perhaps +5 or +10V to an output of +16.2V is shown in Fig. 4. This is based on the circuit of Fig. 1(b), but the input passes through the resistor R_{sc} before reaching the inductor L, this resistor performing the same function as the similar resistor in Fig. 3. As indicated in Fig. 1(b), the right-hand side of the inductor is connected to the switching transistor

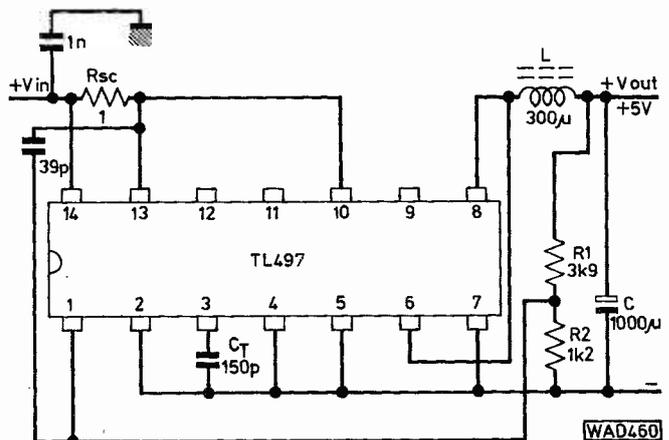
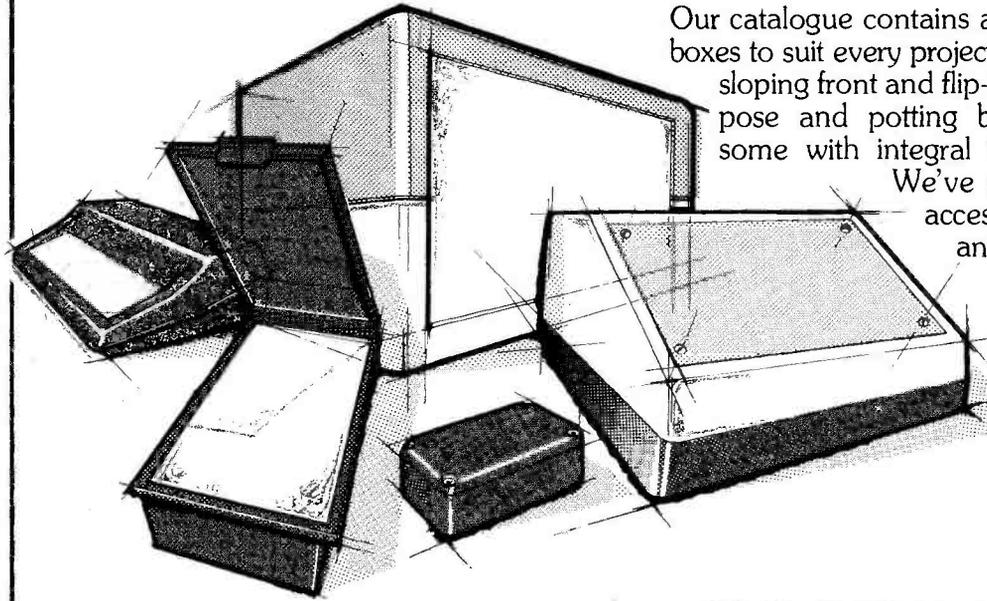


Fig. 3: A typical step-down TL497 circuit providing a +5V output

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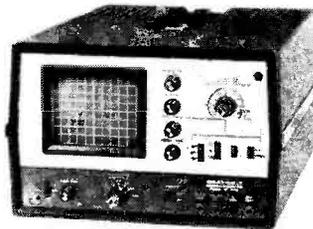


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(pin 10 in Fig. 4) and hence through a diode (pin 7 to pin 6) to feed the capacitor C.

As in the case of Fig. 3, the output voltage is equal to $(1 + R1/R2)$ times the value of the internal reference voltage. By selecting a value of 1.2 kΩ for R2, the output voltage is made equal to the sum of the values of R1 and R2 in kilohms.

Inverter circuit

An inverting regulator circuit for supplying an output of about -5V is shown in Fig. 5. This is based on the circuit of Fig. 1(c) with the addition of the short-circuit limiting resistor R_{sc} , as in the previously discussed circuits. In Figs. 3 and 4 the one side of the 1.2V internal voltage reference is grounded at pin 4 so that this reference voltage can be compared with the potential across a resistor, one side of which is grounded. In Fig. 5, however, pin 4 is connected to the output potential and pin 1 to the junction of the two potential dividing resistors so that the positive side of R2 can be connected to the comparator input at pin 1 in order to render the polarities at the comparator inputs correct.

The output voltage from the Fig. 5 circuits is equal to $-(1 + R1/R2)$ times the internal reference voltage.

General comments

The use of the TL497 device enables switching regulator circuits to be constructed much more simply than if discrete components are used. The basic circuits shown in Figs. 3 to 5 are simple to construct, but circuits using an external power transistor for controlling larger currents must be carefully designed.

The minimum input voltage for the operation of the TL497 is 4.5V. The step-down circuit of Fig. 3 is suitable for providing any output voltage from the +1.2V of the internal reference up to a value of 1V less than the input. The step-up circuit of Fig. 4 can be used to provide an output of not less than 2V above the input voltage up to the maximum of 30V. In the inverting circuit of Fig. 5, the output voltage can range from the negative value of the internal reference source up to -25V.

Texas Instruments have made available specially-designed inductors for use with the TL497 device, these being known as the RI 497. Four types are available, details being shown in Table 1. The 0.5V types are suitable for use in the circuits of Figs. 3 to 5 inclusive, the 5A types being required only when an external transistor is employed to obtain large output currents. These inductors are encapsulated in cases 25.4mm square by 9.53mm in height and incorporate a toroidal ferrite inductor.

Although the use of the specially-designed inductors is strongly to be recommended, any ferrite-cored inductor could be employed provided that the ferrite material does not become magnetically saturated at the maximum current at which it is likely to be used. As an experiment, the writer wound about 70 turns of 28 s.w.g. wire around a standard ferrite rod aerial and found that the TL497 device would operate satisfactorily in two of the three

Table 1. Data on the coils produced for use with the TL497 device

| Inductor type | Inductance ($\mu\text{H} \pm 10\%$) | Resistance (ohm, max.) | Max. Current (A) |
|---------------|---------------------------------------|------------------------|------------------|
| RI 497-01 | 75 | 4 | 0.5 |
| RI 497-02 | 150 | 6 | 0.5 |
| RI 497-03 | 75 | 0.1 | 5 |
| RI 497-04 | 150 | 0.15 | 5 |

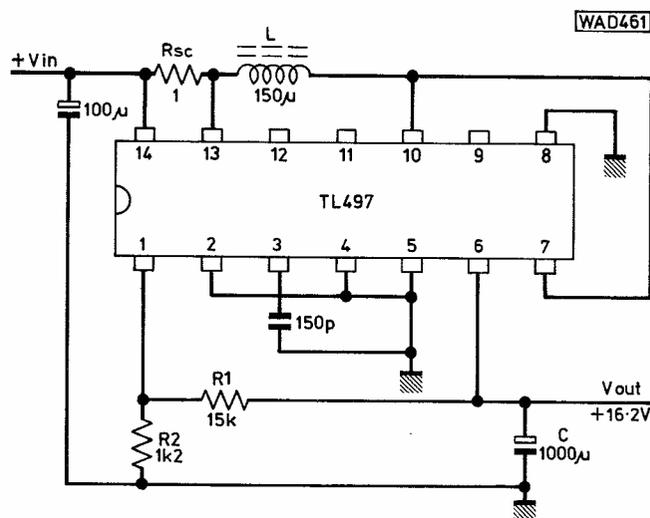


Fig. 4: A step-up circuit providing an output of +16.2V with the component values shown

circuits shown. However, the design of switching regulator circuits is not especially easy and it is well worth while using the recommended inductor.

Switching regulator circuits can generate much high frequency noise if a reasonable layout is not adopted. In order to obtain low output voltage ripple, the output filter capacitor (marked C in the circuits of Figs. 3 to 5 inclusive) should be close to the integrated circuit and have

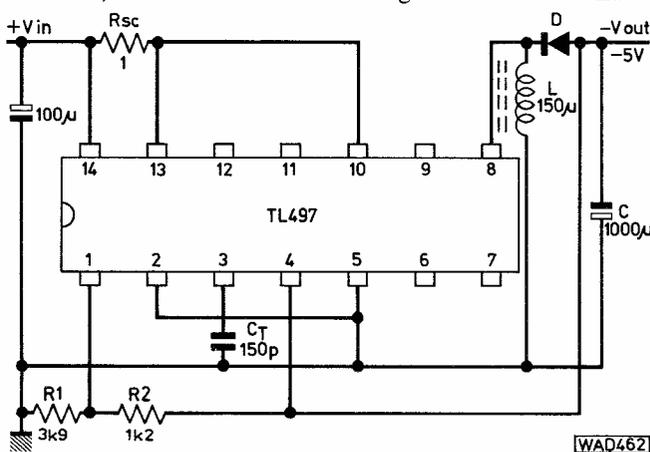


Fig. 5: An inverting switching regulator circuit providing an output of about -5V

a short lead to a point on the negative line close to pin 5 of the TL497. A good quality capacitor should be employed. If long power supply leads are used to bring current to the TL497, a larger value of input filter capacitor may possibly be required, but this capacitor should always be close to the integrated circuit. Inadequate filtering of the input and output leads can cause considerable problems with switching regulator circuits.

No capacitor behaves as if it were a pure capacitor without resistance. In switching regulator applications it is very important that the "equivalent series resistance" of the input and output filter capacitors should be reasonably small; this small resistance can be obtained by suitable constructional techniques when making the capacitors, namely by joining the input leads onto the metal foil of the capacitor in many places rather than just at one place. Such capacitors tend to be slightly more expensive than inferior types having a much higher series resistance.

The TL497 i.c. and the RI 497-02 coil are available from Arrow Electronics Ltd., Leader House, Coptfold Road, Brentwood, Essex, CM14 4BN.



The authors spend a large amount of their working year on site, commissioning complex electrical equipment. This often involves checking electrical panels several hundred yards from control panels and the work is usually hindered by poor or non-existent communications.

The simple telephone handset system described here was developed to provide versatile instant communications. To meet our requirements, the system must:

1. Be cheap. Despite million-pound budgets for projects, firms usually balk at a £10 order to RS Components.
2. Be battery-operated with a very long life on a PP3 battery.
3. Comprise, at each end, a telephone handset (or headset with a boom microphone) and an amplifier. The amplifier must be small and light enough to be carried in a pocket.
4. Unlike the usual "baby alarm" circuit, have two-way speech with no press-to-talk buttons.
5. Be a two-wire system, floating to allow use with spare cores in multicore cables shared with high-voltage, heavy-current signals without suffering from interference.
6. Have a call facility which will work with the receiving amplifier turned off.
7. Have a range of approximately 1 km.

These design criteria were met by a simple circuit built around standard Post Office-style handsets and the ubiquitous 741 amplifier.

Circuit Description

The basic design is shown on Fig. 1. We have two handsets and amplifiers, denoted A and B, connected by a signal pair. Each amplifier is connected to the signal line by a series resistor RSA and RSB. The two earpieces are connected direct onto the lines.

Suppose amplifier A is transmitting, and we have a voltage V_{OA} at the amplifier output. Since the output of amplifier B looks like a low impedance, the voltage on the line will be

$$V_{LA} = V_{OA} \times \frac{(\text{RSB in parallel with two earpieces})}{(\text{RSB in parallel with two earpieces}) + \text{RSA}}$$

Similarly the voltage on the line from amplifier B will be:

$$V_{LB} = V_{OB} \times \frac{(\text{RSA in parallel with two earpieces})}{(\text{RSA in parallel with two earpieces}) + \text{RSB}}$$

Since $V_{OB} = V_{OA}$ by design and $\text{RSA} = \text{RSB}$ by design then $V_{LA} = V_{LB}$ and speech of equal volume will be obtained in both earpieces, and two-way speech is possible. Note that when you speak into your handset, you will hear yourself in your own earpiece. This effect, known as sidetone, is deliberate, as it is disconcerting NOT to hear yourself, and in addition it reduces the natural tendency to shout in noisy locations.

The actual circuit of one handset and amplifier is shown in Fig. 2. The circuit of the other amplifier and handset is, of course, identical. The microphone in a standard PO handset is a carbon transmitter, and needs a bias current. This is provided by R1. In the absence of any data, the value of R1 was determined empirically. IC1 is a conventional 741 op. amp. connected as an inverting amplifier. The amplifier is biased by R2 and R3 to a point mid-way between the supply rails. The signal from the microphone is a.c. coupled to the amplifier and the gain of the amplifier is fixed by R4 and R5. This was deliberately made non-adjustable to ensure that V_{OA} and V_{OB} are equal. If moving-coil microphones are used, R4 and R5 may need to be changed, and R1 may be omitted. At the amplifier output, a signal of approximately 1 volt is produced. The amplifier output is a.c. coupled onto the line via C2. Resistor R6 is the source resistance RS of the amplifier mentioned above.

The earpiece is connected to the line via the volume control VR1. Note that this only affects the received volume, not the transmitted volume. In theory it will affect the volume on both earpieces as the load on the line is changed, but this effect is negligible.

The call facility is provided by S2. This simply applies positive feedback via C3, causing IC1 to oscillate. As a practical observation it is advisable to remove the handset from your ear before pressing the call tone button. If the circuit is used with earphones and a boom microphone, the call facility is best omitted in the interest of preventing induced deafness!

The ON/OFF switch is a two-pole switch. One contact switches the supply, the other causes the earpiece to bypass the volume control so that the call facility can be used when the receiving amplifier is turned off and the volume control is turned right down. When in use, battery consumption is a miserly 1-2 mA.

Construction and Use

The amplifiers were built on a piece of 0.1 in pitch Veroboard measuring 42 x 42 mm, with the layout shown on Fig. 3. The circuit board, volume control, ON/OFF switch, line connector and battery were mounted into a standard diecast box which is small and light enough to fit into a pocket.

The circuit is so simple it should be straightforward to fault-find on if problems are encountered. An obvious area to start is the voltages on pins 2, 3 and 6 of IC1. These should all be at half battery volts. To aid fault finding and repairs, IC1 should be mounted in a d.i.l. socket.

The connection to the line is made via a jack plug and socket or crocodile clips, as convenient. It is important that neither of the signal lines is connected to the case. There are two reasons for this; the first being safety. In impromptu use it is quite possible that a live wire could be used in error: with a signal wire connected to the case the

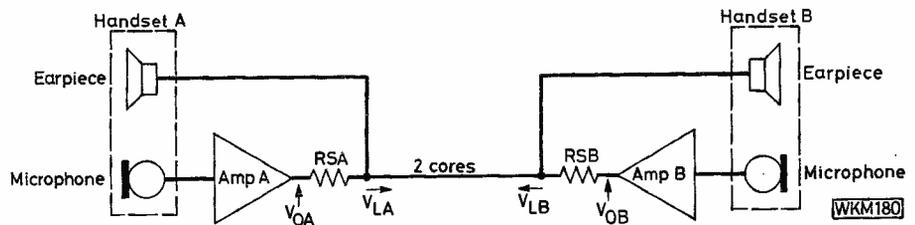


Fig. 1: Basic principles of two-way operation

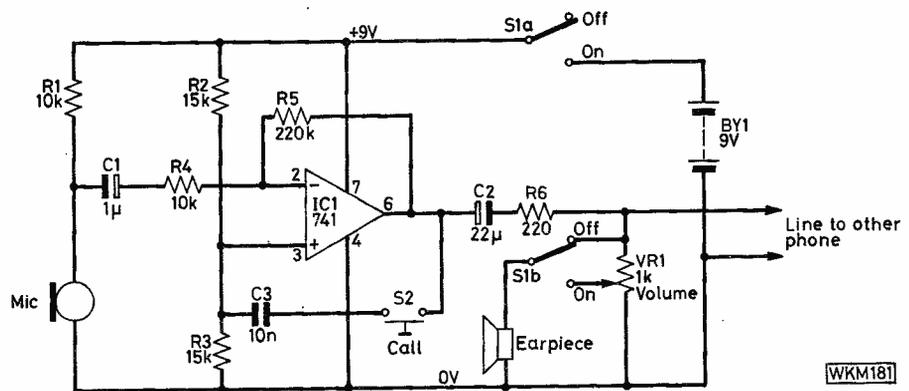


Fig. 2: Circuit diagram of one telephone

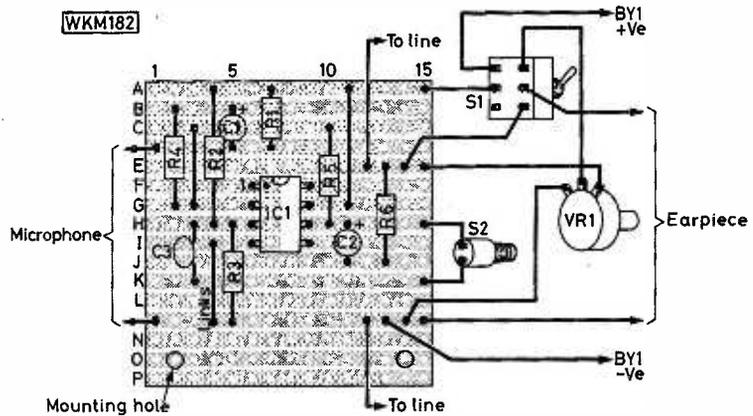


Fig. 3: Veroboard layout and external connections. The only track cuts required are those beneath IC1

★ components

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Resistors

$\frac{1}{4}$ W 5%

| | | |
|-------|---|-------|
| 220Ω | 1 | R6 |
| 10kΩ | 2 | R1, 4 |
| 15kΩ | 2 | R2, 3 |
| 220kΩ | 1 | R5 |

Potentiometers

| | | |
|-----|---|-----|
| 1kΩ | 1 | VR1 |
|-----|---|-----|

Integrated Circuits

| | | |
|-----|---|----------------------------|
| 741 | 1 | IC1 (8-pin d.i.l. version) |
|-----|---|----------------------------|

Capacitors

Disc ceramic

| | | |
|------|---|----|
| 10nF | 1 | C3 |
|------|---|----|

Tantalum bead, 16/35V

| | | |
|------|---|----|
| 1μF | 1 | C1 |
| 22μF | 1 | C2 |

Miscellaneous

S1 Min. toggle d.p.d.t.

S2 Min. push-to-make

Veroboard 0.1 in pitch, 42 x 42mm

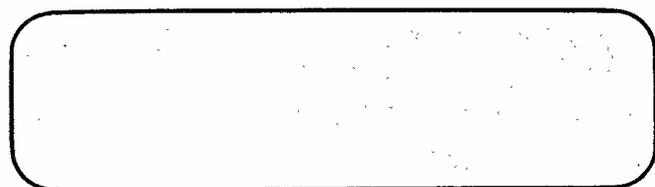
8-pin d.i.l. socket (optional but recommended)

Diecast box 114 x 64 x 30mm. PP3 battery and connector. Post Office-style handset and cable (available from surplus shops, etc.). Jack plug and socket, or crocodile clips (see text)

results could be fatal. The second reason is that if the signal wires were crossed, and both cases were on an earthed surface, the signal would be shorted and the phones would not work.

Several pairs of phones have been constructed, and they have proved to be a valuable aid to site work. They have been operated in adverse conditions with high background

noise and in the presence of electrical interference and have proved very durable. Apart from the obvious industrial use they were designed for, they are also useful for applications such as sports meetings, amateur dramatics, aerial adjustment, house to shed links etc. The simplicity and low cost makes them an excellent project for an inexperienced constructor.



by Eric Dowdeswell G4AR

It was a pleasure to read that the European CW Association (*PW* September, Letters) is supporting the idea that I and others have been putting forward from time to time of a Novice-style licence as an introduction to the full amateur licence. This will allow the newcomer a chance to get a good grounding in the construction and operation of equipment to combat the sad lack of experience so prevalent today among newly-licensed amateurs.

It seems to me that everyone nowadays wants to start at the top, with the best of equipment, regardless of the cost. Fine, but where does one go from there? Since the answer is obviously not "on and up" it must be "down and out". Out of one hobby into another, seeking some kind of satisfaction although, of course, the person concerned will never admit this.

Real, lasting satisfaction in a hobby is obtained by working one's way up from the bottom, learning and seeking new information on all aspects of the hobby, making and doing with one's own hands, saving up hard-earned cash to buy another bit of gear, meeting with others to share experiences, generally getting results from one's own efforts.

The acquisition of expensive equipment that is operated without a backing of knowledge and experience will bring only short-lived satisfaction in many cases. How much nicer to know what really goes on inside those black unimaginative boxes. If something goes wrong the best one can do is to change one anonymous-looking module or p.c.b. for another, which is not likely to prove very instructive, only expensive.

With the advent of some form of CB radio service in this country amateurs will need to be doubly sure that they are not wrongly blamed for TV QRM, and a more than skin-deep knowledge of TVI and its cure will be a necessity. The "appliance operator" in this situation will be ill-equipped to deal with TVI.

The introduction of some form of novice licence could mean that *PW* and similar magazines could once again publish constructional articles on low-power transmitters and all the associated equipment and test gear which were so popular in years gone by. There would be a whole new market for kits and components to meet the demands of

novice licensees. Readers would find a new interest in studying electronics at its roots with practical applications, instead of having to take so much for granted as they do today.

Merely soldering blank-looking i.c.s. to a p.c.b. is not a very inspiring or instructive pastime and is unlikely to hold the attention for very long. How many readers of this column have assembled such a p.c.b. only to find that it doesn't work and then have not had the slightest idea as to how they should go about finding the trouble? They then pass on to another project having learned precisely nothing in the process.

Whatever the hobby or interest may be, there is only one place to start if the genuine understanding of the subject is the target. At the bottom. The projected novice licence could easily provide the necessary inspiration and incentive, leading on to a new generation of amateurs who would be technicians as well as operators, which, after all, is what our amateur radio service is supposed to be all about. It might even lead to a rewarding career in electronics.

Clubs Ahoy

Just for a change, let's start with news of the clubs that have sent in info on their activities, like the newly formed **St. Helens and District ARC** which welcomes new members to its Wednesday meetings at the YMCA HQ, 107 Corporation Street, St Helens at 1945, with a preceding Morse code practice session. Paul Gaskell G8PQD, 131 Greenfield Road, St Helens, Lancs, will be pleased to hear from any interested reader or tel 25472 if it's easier.

Maidenhead and District ARC wants to get in on the act, and why not, seeing that the ad is free; meetings are on the first Thursday and third Tuesday of each month at 1945 at the Red Cross Centre, The Crescent, Maidenhead, and John Patrick G3TWG, Bedford Lodge, Camden Place, Bourne End, Bucks will be pleased to take your queries by letter or on Bourne End 27275.

Reading the **RAIBC** newsletter *Radial* recently I noted an excellent practice which deserves wider mention, namely the idea of clubs donating sums of money, from small to large, to the RAIBC, obtained by a general collection or from a particular function. Just 10 per cent from a junk sale could be several pounds with no trouble at all. And it all goes to helping handicapped and blind members get a receiver or transmitting gear installed and, believe me, every penny is put to good purpose, there are no "overheads". Contact Frances Woolley G3LWY at 9 Rannoch Court, Adelaide Road, Surbiton, Surrey for more info. Or listen to the RAIBC net with G4IBC on 3750 at 1000 on Tuesdays or 1400 Wednesdays.

West Kent ARS has meetings at Adult Education Centre, Monson Road, Tunbridge Wells, Kent at 8pm on



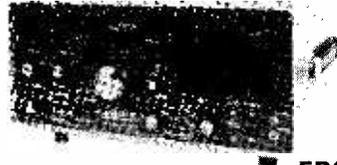
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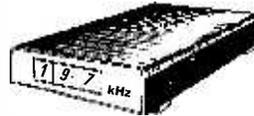


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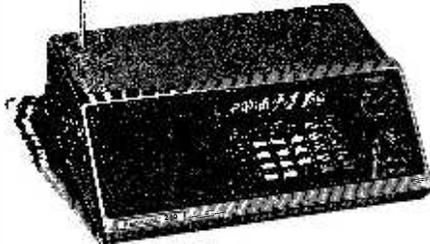


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ACCESS VISA DINERS CLUB H.P.

9 Nov. with Tom Douglas G3BA speaking on "Radio in PoW Camps", on 23 Nov. there is junk sale and 7 Dec. sees Laurie Crawford expounding on modernising old receivers. Contact is Brian Castle G4DYF, 6 Pinewood Avenue, Sevenoaks, Kent.

Bury ARS G3BRS every Tuesday night at Mosses Centre, Cecil Street, with 13 Nov. devoted to a junk sale, and 11 Dec. sees the AGM linked to a wine and cheese party with, I imagine, the ladies getting a word in for a change! A warm welcome awaits visitors to the **Edgware & District RS** at Watling Community Centre, 145 Orange Hill Road, Burnt Oak, on the second and fourth Thursdays at around 8pm. Latest gen on meetings from Howard Drury G4HMD QTHR. The *Edgware Ham News* is a good read combining technical and personal chit-chat with member G3SHY designing a CMOS logic keyer and organising a kit for less than £3.

Northern Heights ARS has a similar style newsletter plus an excellent fixtures card for the wallet, running right through to next August! That's what I call organisation and other clubs might do worse than think about this idea. At least it shows that the committee is doing its job! Meetings 8pm promptly at the Bradshaw Tavern, Bradshaw, near Halifax, on Wednesdays with 7 Nov seeing the RSGB's RR in attendance, a junk sale on 14 Nov. and the 28th welcomes Dr Bailey a Bradford University.

Here and There

Normally from West Wickham, Kent, **John Dainty** has been merrily caravanning around East Anglia and able to "listen without the infernal crackles etc at my QTH" his DXing being aided on this occasion by the vertical multiband aerial described in the RSGB Handbook. **Jim Rowland** in Tetbury, Glos., bought an a.t.u. which did nothing for his DX160, which seemed strange, as I told him. He persevered and eventually found a solder bridge in the wiring which, when demolished, let the a.t.u. do the job it was intended to. Then Jim bought a crystal calibrator by mail order which was supposed to provide signals from 1MHz to 1kHz, but didn't! Supplier took a month to reply but said nothing useful. Jim found a dry solder joint on a Veroboard "standing out like a desert island in a silver sea". Clearing this and all was OK. Needless to say, Jim is very apprehensive now about mail order, and rightly so, since in both cases the equipment could not have been tested properly at any stage which is just not good enough, but Jim has given me the names of the suppliers and these will be borne in mind.

Jim mentions his 130ft Windom "leaping over telephone wires and ducking under electricity cables". I am sure he is exaggerating a bit, or I hope so, because an aerial should never, ever, be allowed to come close to such installations. Over the years a number of amateurs have been killed when an aerial has fallen across power wires, so be warned, don't do it!

Eric Flack, 58 Victoria Road West, Hebburn, Tyne & Wear, would like to hear from readers who have been able to improve their DX160s in respect of selectivity, sensitivity and general stability. Ex-RAF wireless op **W. Thompson** is returning to the fold after some 40 years and would like to beg, borrow, or steal a manual for the CR300/1 receiver. Already he is back to 20 w.p.m. so if you can help write to him at 21 Polwarth Drive, Brunton Park, Gosforth, Newcastle-on-Tyne.

Rod Williams has got his B40 Owners' Club going, the main problem being lack of spares for these sets. If you know of a source or perhaps of any sets that could be cannibalised please write to Rod at 54 Woodlands Avenue, Talgarth, Brecon, Powys.

Far and Wide

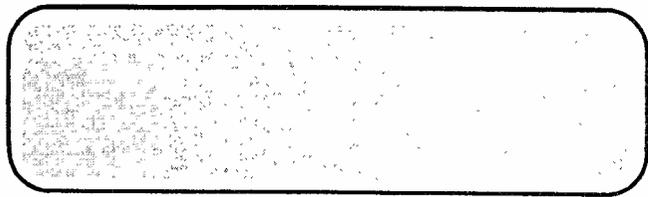
Strings of VP8s make **Bill Rendell** in Truro wonder what is "going on" down in them there parts! Like VP8SB on Adelaide Is (QSL G3ZMF "we only have one ship a year"), VP8SO on Signy Is., and VP8QI on Argentine Island, the site of the British "Faraday" Antarctic base (QSLs to G4CHD), all on 20m s.s.b. However, warmer climes produced SV1DC DXpedition to Greece's Mount Athos, (QSL Box 161, Athens) on 15m together with VP2ARS (QSLs to DF1EQ), VP2MM on Montserrat and 5T5AY.

Like most readers **Allan Stevens** of Crowthorne, Berks, found 28MHz becoming quite lively and improving all the time, producing YB0WR in Jakarta and P29GC on New Britain Is. in Papua New Guinea, with ZF1J on 21 MHz for good measure. **Peter Hawkes** from Stourbridge, West Mids, moved his DX160 into the end of his garage and so virtually cleared up his TVI problem, except on the Top Band, so that is one answer to the radiation from TV set time-bases. Peter mentions the Hurricane Net on 14325kHz, run by YLs K4HKL and WA1KKP, which presumably has had plenty to do of late! Peter logged stuff on 10m like SU1CR, AP2KS, YB0WR with 5T5AY, HS1ABD, 3D6BP and 3V8ONU on 15m. 20m provided VP8SO of Signy, with 8P6AH on 40m and VO1BB, ZS6DW (!), K6SVL/VP9 and 8P6KY on 80m, all s.s.b.

Mike Stollov G4HWP in Blackley, Manchester also has trouble trying to get his 60ft wire clear of telephone wires but his FRG-7 still found 10m wide open with a marked burst of solar noise on August 26 at 1135. He logged CP5JA/P2, JY5ZM, XT2AW, 5H3KS and 9G1JX. **Arthur White**, near Grantham, Lincs, had trouble with his Trio QR666 and borrowed an Eddystone 888 which he is now loath to return and hopes to buy! Using a 60ft wire and a.t.u. he found VK6NY on 10m, stacks of VKs on 20m, and ZS2MI of Marion Is. who QSLs via ZS6APO or WA2ZN. Our RTTY hero **Dennis Sheppard** (Sheerness, Kent) has not been too active, preferring to concentrate on a stereo amp he is building, but nevertheless logged, or rather got them to log themselves, DJ6UZ and JA1DSI on 10m, JA1BPQ and ZS6AKO on 15m and AH6D (Hawaii), G4BHT/4X4, VE3JCU, VK2EG, YV1EQ, ZS1LM, 3V8ONU and 5N0SID on 20m. Dennis now has 34C confirmed on this mode.

With a trapped dipole in the loft feeding his FRG-7, **Bob Anderson** of Canvey Island (no, it's not a new country!), Essex, logged ZE8JB and 9K2DR on 10m with A2CBT, HP1ACJ, VP2VBK and 7X2HM on 14MHz. **Pete Lucas**, near Newport, Salop, decided not to take his AR88 with him on holiday since he didn't want to have to hire a crane, so was out of touch with the bands for a while. He comments on the American prefixing system which seems to have gone quite mad making our prefix lists look rather sick. Space permitting I will try to sort this out by giving the new prefixes, but in the meantime take nothing for granted but check by listening for the actual QTH. This applies to almost any US and possessions station.

Great to hear that **Dave Coggins** is able to get something up other than a long wire. He has his 66ft as an inverted-V aimed at VK/ZL, feeding an a.t.u. into his DX160 which he is able to compare with a 2-element quad on the 10m band. On 10m it was ST2SA in Khartoum, VP8PU (another one!), YB0ADW, with FO8DT, P29GC and VU2LQA on 15m, 5W1BP (W. Samoa) and 9Y4TFL for 20m and CO2DC and 6W8DY representing 40m, while 80m produced FM7WS and ZS6DW, the latter confirming the reception by Peter Hawkes of this ZS6 mentioned earlier. So 80m is already showing an improvement and hopefully is a forecast of things to come this winter.



MEDIUM WAVE DX

by Charles Molloy G8BUS

The appearance of signals from the Droitwich transmitters on 693kHz, 1053kHz and 1215kHz "at a wide variety of places on the band" are making DXing difficult for reader **Stewart Kinsley** of Coventry. The receiver is a Drake SSR-1 used with a 20ft end-fed aerial.

Overloading

Overloading is the problem, which is giving rise to spurious responses within the receiver. Stronger signals than the receiver is capable of handling are being fed into the aerial socket, and the cure is to reduce these offending signals by means of an attenuator fitted between the aerial and the receiver.

A simple attenuator can be made using a 1kΩ potentiometer. There are three tags on the "pot". Connect the aerial to the centre tag. Connect either of the outer tags to the receiver aerial socket. Connect the remaining outer tag to the receiver earth socket along with the earth wire if one is used.

When the pot is set to one end of its travel there will be maximum signal. At the other end there will be little or no signal. Start with the pot at maximum signal and slowly rotate the control until the spurious signals disappear but, and this is the snag, you will also have reduced the strength of your DX signals as well. Only use the minimum attenuation necessary to cure the overloading.

It might also be worthwhile to check that the receiver r.f. stage is working properly, as a fault in this part of the receiver or in the mixer stage might give similar results.

In spite of his difficulties, Stewart managed to pull in Malta on 1557kHz, Tenerife on 621, Conakry, Guinea on 1404, Rhodes on 1260 and Batra in Egypt on 819.

FRG-7 Survey

As promised in the July issue here is a synopsis of a survey made from letters from forty FRG-7 owners. It was compiled by **George Tyler** of Bristol and it starts by saying that the FRG-7 is a fine receiver, well laid out externally and internally with each component marked on the printed board for ease of identification.

Reports on the various bands are welcome and should be sent direct, by the 15th of the month, to:

AMATEUR BANDS Eric Dowdeswell G4AR, Silver Firs, Leatherhead Road, Ashted, Surrey KT21 2TW. Logs by bands, each in alphabetical order.

MEDIUM and SW BANDS Charles Molloy G8BUS, 132 Segars Lane, Southport PR8 3JG. Reports for both bands **must** be kept separate.

VHF BANDS Ron Ham BRS15744, Faraday, Greyfriars, Storrington, Sussex RH20 4HE.

No component failure was reported and the manual is considered excellent. The stability is also excellent and the only spurious signal observed was on 21350kHz. The calibrated dial mechanism gives frequency readout to 10kHz and can easily be read to 5kHz. Selectivity is adequate for a.m. reception but is not for s.s.b. (A selectivity modification kit is available).

Power consumption on internal batteries is high. The receiver is poor for m.w. DXing. The attenuator is of little value unless a very strong signal overloads the receiver. The tone control is useful on both a.m. and s.s.b. The fine tuning knob is too small and the noise limiter has little effect.

High impedance phones give better results for DXing than the low Z types. The Dial Set is useful but the S meter is rather small.

Comment on the Survey

There are a couple of points I feel compelled to comment on. The first has to do with selectivity.

A receiver with fixed selectivity will have to compromise between a bandwidth wide enough to give good intelligibility, and narrow enough to pick out a wanted station from interference. Wide bandwidth means good quality audio along with poor selectivity. Narrow bandwidth means poor quality audio but good separating ability. Hi-fi and DXing do not go together! It would appear that the FRG-7's bandwidth is too wide hence the modification kit. What will the audio be like after modification? There really ought to be a selectivity switch, with two positions at least, on any communications receiver.

It is a pity that "poor for m.w. DXing" was not expanded. Readers of this column have reported some excellent DX on the FRG-7 and this is the first time I have heard this complaint. I wonder how many of the reporters are experienced m.w. DXers?

Finally, many thanks to George for making this survey available to readers of *PW* and my apologies to him for chopping it down from the original four pages.

Bats

"I thought you might like to hear of some unusual long wave DX—Bats", writes **Martin Mann** from Cambridge. He fixed a 40kHz transducer at a window and fed it to the aerial input of a receiver. At dusk he heard and recorded several bursts of bat sonar signals which sounded rather fluttery(!) with rapidly sweeping pulse frequency. The range was about 20ft which must make this the shortest distance DX reported to date.

A bat's radar system is based on ultrasonic sound waves, not radio, hence the need for the transducer. Martin has demonstrated how, with a little ingenuity, one can extend DXing into a new and interesting field, however it is *not* long wave DX! Wavelength equals velocity of transmission divided by frequency. The velocity of radio waves is 300 000km per second which gives a wavelength of 7500 metres for a frequency of 40kHz. The velocity of sound waves through air is roughly 330 metres per second which gives a wavelength of 8mm. So bats really use microwave radar and the report from Martin should have gone to Ron Ham!

Realistic DX160 Receiver

A rather disturbing report comes from reader **David Hyams** of Finchley who discovered that his newly-acquired DX160 has an internal aerial for use on the medium and long waves. This aerial replaces the aerial tuning coils

which are shown as T1 and T2 on the circuit diagram. If this aerial is disconnected then the receiver will not work. As it stands this latest version of the DX160 cannot be used with a m.w. loop. David is trying to get the supplier to restore the receiver to its original unmodified state and unless this can be done then it will be of limited value for m.w. DXing. Obviously the manufacturer has not heard of DXing on the medium waves.

It is easy to test if a receiver has an internal aerial. Unplug any external aerial and tune round the m.w. band. Any signals heard must be picked up by an internal aerial and they will still be heard when a loop is nulling out a station. The overall result therefore is no null. The directional properties of the loop are masked by the pick-up of the internal aerial.

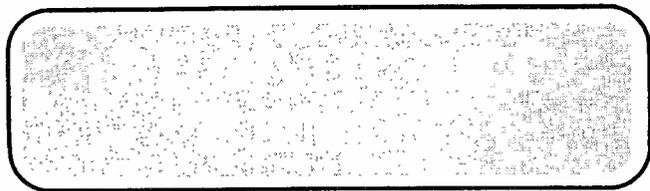
DX

A "40 inch" loop together with a home-brew receiver were used during the first week in September by **Alan Morton** (Edinburgh) to log the following North Americans: CJYQ St John's Newfoundland on 930kHz at 0330, WBZ Boston on 1030 at 0400, WINS New York City on 1010 at 0415 and CHNS in Halifax, Nova Scotia on 960kHz at 0430.

The maximum of the current sunspot cycle was expected during the autumn and with it a lower than average reception on the North American path. Once the maximum has passed then reception should pick up quickly, so listen around midnight for the stations listed above. Others to look for are CBN St John's on 640, CKVO Clarendville in Newfoundland on 710, CHER in Sydney on 950, WNEW New York City on 1130 and CKEC New Glasgow in Nova Scotia on 1320kHz.

DX signals on the medium waves are subject to slow cyclic fading which lasts over several minutes. A channel may have a reasonable signal on it at one moment, but two or three minutes later nothing can be heard. So tune slowly and come back later to any dead channels.

A short extract from my own log to round off this month. The receiver is a BRT400 used with a "40 inch" loop on 15 September to pull in: Conakry, Guinea on 1404kHz at 2220 SIO 333, Ouagadougou, Upper Volta on 747 at 2225 SIO 232 and CJYQ St John's on 930 at 2230 SIO 333. At first sight the reception of CJYQ at this time appears surprising, but local sunset here was some four hours earlier at 1829 and Newfoundland is 3½ hours behind GMT. In mid-winter, CJYQ has been heard as early as 1930 and it is only European QRM that prevents it being a conspicuous signal during the evening when conditions are good.



SHORT-WAVE BROADCASTS

by Charles Molloy G8BUS

Occasionally a frustrated DXer with a faulty receiver sends me details of his troubles in the hope that, like some modern Sherlock Holmes, I will instantly diagnose the

trouble and point to an easy and immediate remedy. That sort of servicing belongs, along with the famous detective, to the world of fiction. A modern receiver is really quite a complex piece of equipment and the chances that a novice would be able to repair it are negligible. He is more likely to be the phantom twiddler who knocks everything out of alignment and in the case of a mains operated receiver he may even receive a nasty shock. It is only on the test bench in the hands of a competent person that the trouble will be sorted out properly.

Home Made Receivers

The "competent person" need not necessarily be a service engineer. Radio Amateurs have the technical knowledge to deal with receiver problems and there are still a few about who even construct their own gear. Why not do the same? It is great fun and you do not need a technical background to construct a simple receiver. Designs and constructional details are easy to come by, in *Practical Wireless* for example. Not only will you have the satisfaction of using something you have made yourself but you will be able to peak it up, modify it and improve it to meet your own individual requirements. All the time you will become more proficient and knowledgeable and the day will come when you feel bold enough to try your skill on a commercial receiver.

TRF Receivers

"I cannot afford a communications receiver", writes student **Nick Quin** of Lansing, who built a 3-transistor t.r.f. receiver from a design in *Radio and Electronics Constructor* (oh!). The receiver nominally tunes over the range 1.2 to 24MHz but by altering the position of the tuning coil cores slightly he was able to get up to the 11m band which is from 25 600 to 26 100kHz. The aerial was a 30ft long wire, now increased to 90ft, and the receiver drives a pair of headphones. DX heard included Radio RSA on 25 790kHz at 1410, Radio Australia on 11 800 at 1824, All India Radio on 11 620 at 1805 and the Voice of the Revolution in Iran on the 31m band at 1920. Nick would be very interested to learn of DX heard by anyone else who has built a t.r.f. No need to worry if you are not sure of the exact frequency. Just mention the metre band, but DX only please.

The term t.r.f. means tuned radio frequency and refers to a complete receiver working on this principle. The expression has been used by at least one manufacturer in the United States to refer to a superhet with a tuned r.f. stage, which is rather confusing. In the UK t.r.f. means a simple receiver usually with a reaction control.

Broadcasting on 10 Metres

My suggestion in the September issue that the IBA Jerusalem broadcasts beyond the upper edge of the 10m amateur band might be a harmonic, has brought some interesting replies. **Paul Hardy**, who lives at Caversham, says that 29 705 is quoted in the IBA schedule, while **Andy Sennitt** of the *World Radio and TV Handbook* confirms that the transmission was really on the fundamental and he suggests that it was intended for reception by Russian radio amateurs. Paul says the frequency was withdrawn in June but **Harold Brodrigg** (St Leonards-on-Sea) picked it up again in September SIO 555 at 1415. The Programme, which was in Yiddish (sounds like German), was the same as on 25 605 and 25 640kHz in the 11m band, both of which were being jammed.

Beyond 10 Metres

The frequency mentioned is rather interesting as it lies in a sort of no man's land where h.f. ends and v.h.f. begins. The boundary is 30MHz, which was the lower of the two frequencies of the Knickebein beam navigation system used by German bombers during the last war. The other was 31.5MHz and both beams were discovered using a Hallicrafters S27 bought in Webbs Radio in Soho. At that time it was the only v.h.f. communications receiver available. I have an S27, which covers 28 to 143MHz in three bands and far from being an antique, it is still a very useful receiver.

Hallicrafters

Another Hallicrafters admirer is **Ashley Griffiths** who has acquired an S38E. It is in working order but he would like to know more about it. Replies to 73 Llanmiloe Est, Pendine, Dyfed, S Wales please. From memory I think it is a general coverage receiver without an r.f. stage. There was a commercial version of it called the Echophone which had a rather unusual bandspread control. By means of cord, pulley wheels and a spring, a piece of ferrite material was moved in and out of the air-cored oscillator coil.

Hallicrafters gave names to some of their receivers such as Sky Buddy, Sky Champion, Sky Rider; names that will bring a twinge of nostalgia to older DXers. What a pity modern manufacturers do not do the same. I have heard one currently available receiver referred to as the Frog!

Radio Japan

Transmissions of Radio Japan broadcasts over Radio Trans Europe in Portugal will take place again this winter. The frequencies are 17 815 from 0700 to 0730 for the Middle East and on 15 305 from 2200 to 2230 for Europe. Reception reports are welcome and should go to Overseas Dept, Nippon Hoso Kyokai, Tokyo, Japan.

Last winter the European transmission was on the 25m band where tests were conducted for the month of October only. It was possible to pick up the same programme on the 31m band direct from Japan, with a much inferior signal of course. At the time of writing the winter schedule of R Japan is not yet available.

Direct reception of Japan is usually at breakfast time on the 13 and 16m bands. When R Japan first appeared on the short waves before the war it gave a good signal in the evening. Overcrowding and high-power transmitters have made other than single-hop broadcasting unpopular and this has led to the modern practice of using relay stations.

Readers' Letters

Jakarta in Indonesia has been picked up by **A D Scholefield** (South Shields) on 11 790kHz between 1400 and 1500. **Paul Martin** (Edinburgh) used his Panasonic RF2200 to pull in Radio RSA on 25 790 at 1425 SIO 333 and Radio Japan on 21 610 at 0900 SIO 222. He asks if he can use an aerial tuning unit (a.t.u.) between this receiver and his 70ft long wire. An a.t.u. can be used with any receiver that has an aerial and earth socket.

The problems of getting a QSL from South American stations are highlighted by **Jeremy Boot** (BRS 41156), who speaks both French and Portuguese. He has been quite successful with Brazil, though many stations have not replied despite reports in their own language and IRCs. International Reply Coupons are not valid in some countries and are unwelcome in others. It is better if you



QSL Cards
from Radio
Japan



can send unused postage stamps of the relevant country if you anticipate problems. They are available from stamp dealers.

News Items

There are no longer any s.w. transmissions from Syria (*World Radio and TV Handbook Newsletter*, August 1979). Someone asked about Syria a few months ago.

Radio New Zealand frequencies for the period 28 October to 1 March (Spring and Summer!) are as follows, all times being in GMT:

Pacific Service

| | |
|-------------|---------------------|
| 1700 — 2005 | 11 835 or 17 860kHz |
| 2015 — 0715 | 17 860 |
| 1700 — 0525 | 15 345 |
| 1540 — 0930 | 6105 |

Australian and NW Pacific Service

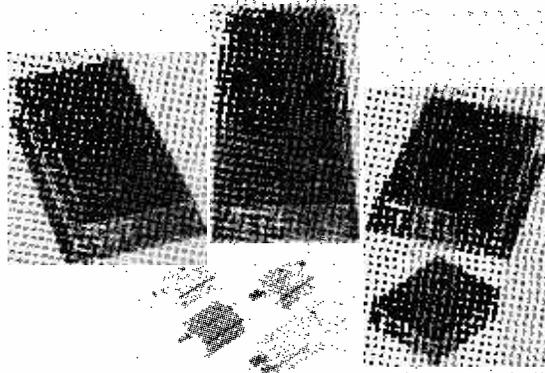
| | |
|-------------|--------|
| 0730 — 0115 | 11 945 |
| 0945 — 1115 | 6105 |

If a QSL card is required then RNZ are now asking for 3 IRCs, according to their latest schedule.

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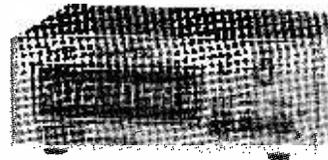
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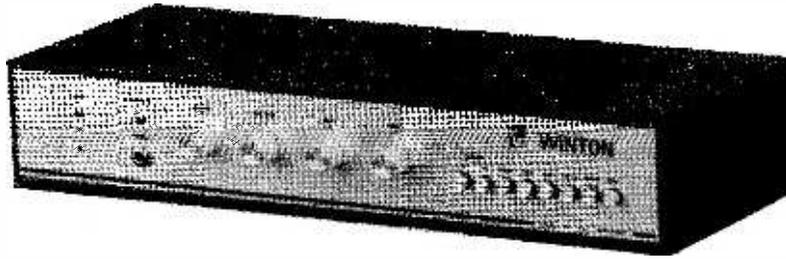
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There are so many repeats on the Telly that you are considering sending the Beeb some Alka-Seltzer, and to round off your happiness you are in the Doghouse with the Wife for thumping young Willie because he was trying to shave the cat with the Electric Razor Santa brought you.

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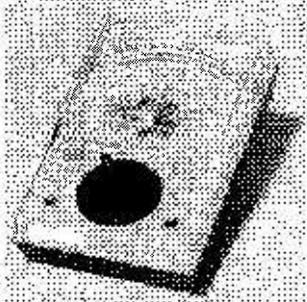
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by Ron Ham BRS15744

Generally speaking, DX, as far as v.h.f. is concerned is relative to where we live and the surrounding terrain. For instance, if the home QTH is situated on high ground then, under normal conditions, our signal catchment area is far greater than that of a station in a valley or behind a hill. All reader's reports are therefore welcome because, whether their particular DX is great or small, or whatever mode is used, it is worth writing about.

Solar

Cmdr Henry Hatfield, Sevenoaks, and I recorded solar noise at 136 and 146MHz respectively on August 22 and September 5, 9 and 14 and individual bursts on August 23, 24 and 31 and September 6 and 7, Fig. 1. Sam Faulkner, Burton-on-Trent, heard solar noise between 50 and 60MHz around 1715 on August 29 and Mike Allmark, Leeds, heard solar noise in the 2m band at 1518 on the 28th, all no doubt due to the 65 sunspots counted by Ted Waring, Bristol, on the 26th.

On September 9, Henry, using his spectrohelioscope, saw the remains of a flare and five sunspot groups, "two quite large", and at 0935 on the 14th he saw a bright loop prominence, about 100 000 miles high on the eastern solar limb. This could well have been the remnants of the event which caused the sudden ionospheric disturbance, at 0735, reported by Louis Prechner in the BBC's *World Radio Club* programme on the 16th.

Lucky Henry

At 1025 on September 15, Henry watched a bright patch, on the eastern limb of the sun, develop into an arched prominence rising about 50 000 miles above the sun and take 20 minutes to return to the solar surface approximately 100 000 miles away. "It was a beautiful sight", said Henry, who also recorded some radio noise at 136MHz from the event.

The 10 Metre Band

During the 28 days from August 21 to September 17, I heard signals from the International Beacon Project stations at Bahrain A9XC, on 12 days, Bermuda VP9BA, 2 days, Cyprus 5B4CY, 22 days, and Germany, DL0IGI, 8 days. Periodically, on some days, the signals from 5B4CY were peaking 599 and although Ted Waring's I.B.P. report was similar to mine he did hear the Canadian beacon VE3TEN, on August 24 and 31 and September 8 and 12. During the early morning of August 24 I heard many strong signals from Russian stations and by midday it was obvious that the band was wide open. In fact, some American stations who were coming in like locals, were saying that they were "surprised and delighted" about the good conditions. For example, I received 9-plus signals from both sides of a QSO between W4MB and 4Z4SG.

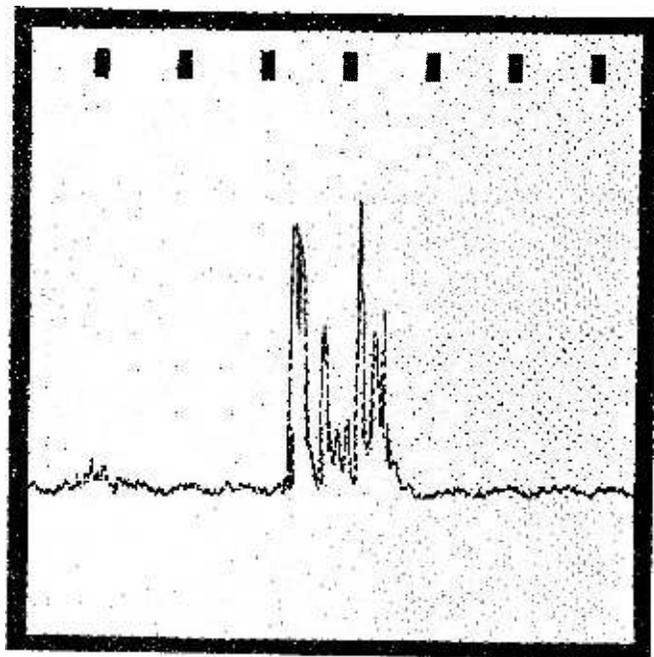


Fig. 1: A 1-5 minute duration solar burst recorded by the author at 146MHz at midday on 6 September

Russian signals were again very strong during the early mornings of August 27 and 28 and September 16 and 17 and at midday on the 15th and 17th. Around 1225 on the 17th I heard strong signals from VK3XF, Melbourne and VK5ZK, Adelaide, who both worked GD3EIG on the Isle of Man.

Satellites

"OSCAR-7B is going strong on sun power only" writes John Branegan GM4IHJ, Saline, Fife, on September 2. "Some recent QSOs include VE6KY and VE6TD in Edmonton, Alberta, K3BWD, Haverford, Pennsylvania, VE3TW, St Catherines, Ontario, W0CA, Backus, Minnesota and W8DX, Detroit, Michigan." John has now received QSL cards from stations in DB, DC, G, OH, OK, and W for QSOs through the Russian satellites and on September 2 he worked GD5UG giving him another country through OSCAR-8J.

Aurora

During the auroral event on August 29, John Branegan heard Tone-A c.w. signals from the 2m beacons in Cornwall GB3CTC and Northern Ireland GB3GI and amateur stations in Belgium, Denmark, France, Holland, Germany, Norway, Sweden and Wales between 1300 and 1900. In addition he had c.w. contacts with stations in EI, G, GM, GW and PA0. "Having c.w. even with 10 watts, makes a tremendous difference", said John who makes full use of his GM4 call. Roy Bannister G4GPX, Lancing, heard auroral signals from stations in GI and GM between 1800 and 1900 but could not raise them.

"We had a very good aurora on August 29 from 1519 to 1910", writes Mike Allmark. "Many countries were heard here on 2m and the TV bands went berserk. All G was heard from Cumbria to Cornwall." Kevin Jackson, Leeds, said: "The aurora was very intense at Band I frequencies, the strongest noted here in five years." During the event, Kevin saw a clutter of BBC-1 signals from all parts of the UK, some unidentified programmes on

Channels E2 and E4 and a signal in Band III from France-Lille on Channel F8a.

DX TV

In my August column I used the words: "I feel sure an F2 opening to Scandinavia occurred" when referring to a particular event. Well, my assumption was wrong, and three West Yorkshire readers, Mike Allmark, Kevin Jackson and **Clive Morton** G4CMV, were quick to tell me that it was due to sporadic-E and proved their claim with some most interesting letters. Welcome to the column Gentlemen, and I hope that my error has gained three new contributors.

Mike's interests range from Band I to u.h.f. and he is very experienced in these fields. On Band I he has seen all of Europe via sporadic-E, meteor scatter and some aurora, and USSR and possibly China and Malaysia via F2. Although on Band III he has seen lots of stations via tropo, best DX is Spain. He has received signals from stations in many countries by the meteor scatter mode, and while on u.h.f. his best DX is Poland, TVP on Channel R25, he has also seen pictures from Belgium, Netherlands, Luxembourg and Sweden.

Kevin has been a TV DXer for 5 years and, like Mike, has an impressive record. He is interested in all modes of propagation in addition to monitoring for the odd occurrences of Night-Es, which, as Kevin explains, is "like sporadic-E but at night only and all transmitters are from the auroral zone and only when a geomagnetic storm is in progress". Observations are reported to the IARU coordinator. Kevin's receiver, a Bush TV161, is connected to crossed dipoles for Band I, a dipole and 5-element Yagi for Band III, and an MBM 70, Group A and a 10-element, Group B for u.h.f. These aerials are all fixed, beaming south-east, because Kevin lives in a sheltered valley with a clear take-off in that direction. "Even so", writes Kevin, "I see Sweden at u.h.f., off the side of the beam over a 150ft rise in the ground which surrounds me except for the south-east." When Kevin installed the 70-element on u.h.f. he found that he could receive the Dutch TV from Goes on Channel 32 and what's more, he can see it daily, as he can the Belgian station on Channel 43 with his 10-element Yagi directed toward Egem. His best DX on Band I via F2 is Vladivostok, 8353km, Band III, sporadic-E, Italy, 2026km, and u.h.f., tropo, Feldis, Switzerland, 1101km.

It is letters like these from Mike and Kevin that stir the enthusiasm into others who wonder whether or not TV DX is worthwhile. On August 18, Mike Allmar, John Branegan and Sam Faulkner, all received RTVE, Spain, via sporadic-E. Sam also has very strong pictures from Budapest carrying adverts for HUNGEXPO followed by news and cartoons. On the subject of RTVE, I have just received a coloured QSL card, Fig. 2, in response to a photograph and report which I sent to them about their signals.

Sam watched a music programme, with a YL announcer on Channel R1, during the evening of the 19th and a fashion show around 1830 on the 21st. **Ian Rennison**, Horsham, also saw the YL announcer on R1 on the 21st at 1958. Ian has now added a JVC 3070 UKC to his DX TV equipment and is pleased with its performance.

Russian signals were also reported by John Branegan around this time, and Mike reported very strong sporadic-E signals from Austria, Czechoslovakia, Italy, Russia, Spain and Switzerland, during the morning and early evening, on Band I. On August 27, Sam received the 0249 test card at 0900 from TSS, USSR, Fig. 3; at 1400, Ian Rennison, received a strong PM5544 test card from

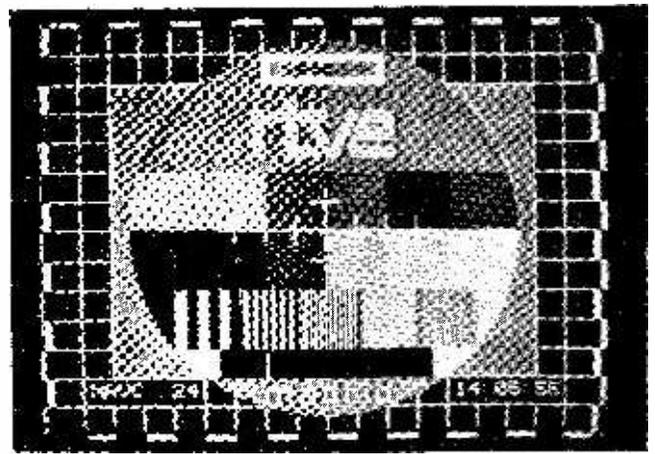


Fig. 2: The QSL card received by the author from RTVE Spain

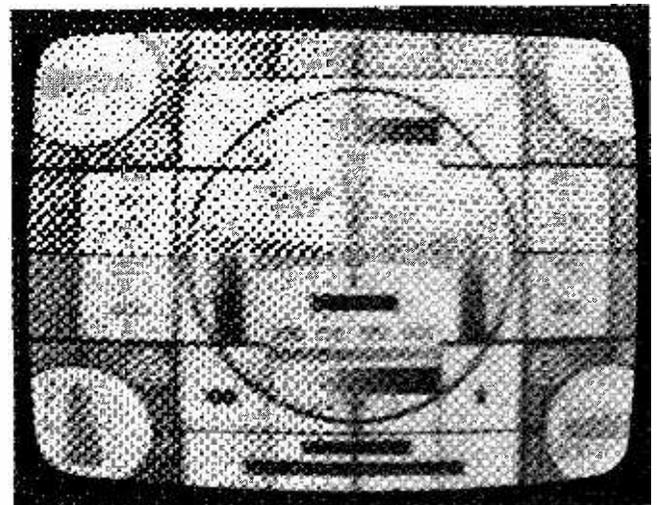


Fig. 3: The 0249 Test card from TSS, USSR, received by Sam Faulkner on 27 August

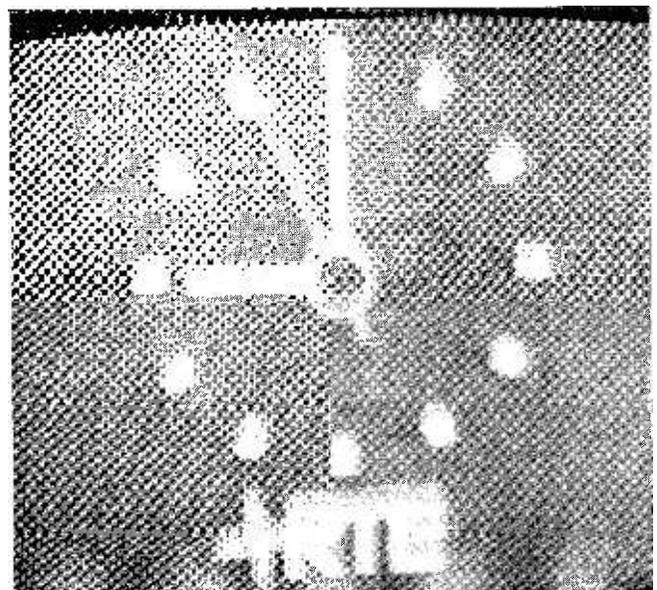


Fig. 4: The signal from RTE, received by Sam Faulkner on 4 September

Sweden, and later in the afternoon and early evening John Branegan watched television signals from both Russia and Spain. Both Sam and John received pictures from RTVE, Spain, on September 2 and on the 4th, Sam received pictures from RTE, Eire, Fig. 4, during a tropospheric opening.

During the good tropo conditions on August 29, 30, 31 and September 1 and 5, Mike Allmark received u.h.f. television pictures from stations in Belgium, France, Holland and West Germany. Ian Rennison received pictures from the Netherlands at 0700 on the 5th, and from Russia and Wales on the 7th.

Tropospheric

George Grzebieniek RS 41733, London, who entered the receiving section of the RSGB's 144MHz contest on September 1 and 2, heard F1CB/P, F1KBF/P, ON5FF/P, PE0AY and PE0MAR/P and a couple of GWs. Before the contest he heard signals through the Brighton GB3SR, Cambridge GB3PI and Malvern Hills GB3MH, repeaters. George has been carrying out receiver tests on 23cm with G3FZL and G3IDG, yet another example of co-operation between radio amateurs.

On August 30, Alan Baker G4GNX, Newhaven, told me that he heard signals on all repeater channels from R0 through to R9. Conditions on v.h.f. were generally good on September 1, 4, 5, 8, 11, 12 and 16, shown up on each occasion by the strength of the repeater signals. During the opening on the 1st, I heard a 3-way QSO between G3JEP, Exmouth, G4EJV, Worthing and GW3XJA, via the Bristol Channel repeater GB3BC. The GW was using 1 watt to a home-brew Slim Jim aerial.

At 2200 on the 16th, Alan heard signals through the French repeater FZ1THF, R0, and as it faded he worked a station in Kent via the Leicester repeater GB3CF, R0. Later he worked HB9ARI on s.s.b. and heard HB7MMM. Congratulations to Ken Jeal, Horsham, who has passed the RAE and now sports the call sign G8SVY.

Old Receiver

Can anyone help Mr E. G. Thomas of 11 Burrell Ave, Lancing, Sussex, with a manual or service info for a Hallicrafters, S20R, Sky Champion.

24 TUNE DOOR CHIMES

DOOR TUNES £16.44 + VAT.

Waddington's Videomaster announce a doorbell that doesn't go Brrringgg, Ding Dong or Bzzzzz. Instead it plays 24 different classical and popular tunes. It will play the tune you select for your mood, the season or the visitor you are expecting to call. Door tunes is not only great fun and a wonderful ice breaker, but is also very functionally and beautifully designed to enhance your home. There is something for Christmas, something for your continental visitors or your relations from the states, and even something for the Queen. Door tunes is easy to install and has separate controls for volume, tone and tempo.

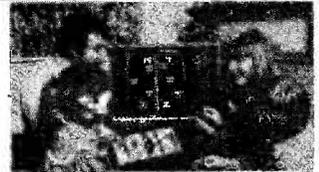


T.V. GAMES

PROGRAMMABLE £29.50 + VAT.

COLOUR CARTRIDGE T.V. GAME.

The TV game can be compared to an audio cassette deck and is programmed to play a multitude of different games in COLOUR, using various plug-in cartridges. At long last a TV game is available which will keep pace with improving technology by allowing you to extend your library of games with the purchase of additional cartridges as new games are developed. Each cartridge contains up to ten different action games and the first cartridge containing ten sports games is included free with the console. Other cartridges are currently available to enable you to play such games as Grand Prix Motor Racing, Super Wipeout and Stunt Rider. Further cartridges are to be released later this year, including Tank Battle, Hunt the Sub and Target. The console comes complete with two removable joystick player controls to enable you to move in all four directions (up/down/left/right) and built into these joystick controls are ball serve and target fire buttons. Other features include several difficulty option switches, automatic on screen digital scoring and colour coding on scores and bells. Lifelike sounds are transmitted through the TV's speaker, simulating the actual game being played. Manufactured by Waddington's Videomaster and guaranteed for one year.



EXTRA CARTRIDGE:

ROAD RACE - £8.87 + VAT.

Grand Prix motor racing with gear changes, crash noises

SUPER WIPEOUT - £9.17 + VAT.

10 different games of blasting obstacles off the screen.

STUNT RIDER - £12.16 + VAT.

Motorcycle speed trials, jumping obstacles, leaping various rows of up to 24 buses etc.

NON-PROGRAMMABLE TV GAMES

6 Game - COLOURSCORE II - £13.50 + VAT.

10 Game COLOUR SPORTSWORLD £22.50 + VAT.

CHESS COMPUTERS

STAR CHESS - £56.09 + VAT.

PLAY CHESS AGAINST YOUR PARTNER.

Using your own TV to display the board and pieces. Star Chess is a new absorbing game for two players, which will interest and excite all ages. The unit plugs into the aerial socket of your TV set and displays the board and pieces in full colour for black and white on your TV screen. Based on the moves of chess it adds even more excitement and interest to the game. For those who have never played, Star Chess is a novel introduction to the classic game of chess. For the experienced chess player, there are whole new dimensions of unpredictability and chance added to the strategy of the game. Not only can pieces be taken in conventional chess type moves, but each piece can also exchange rocket fire with its opponents. The unit comes complete with a free 18V mains adaptor, full instructions and twelve months guarantee.



CHESS CHALLENGER 7 - £86.65 + VAT.

PLAY CHESS AGAINST THE COMPUTER.

The stylish, compact, portable console can be set to play at seven different levels of ability from beginner to expert including "Mate in two" and "Chess by mail". The computer will only make responses which obey international chess rules. Casting, on passant, and promoting a pawn are all included as part of the computer's programme. It is possible to enter any given problem from magazines or newspapers or alternatively establish your own board position and watch the computer react. The positions of all pieces can be verified by using the computer memory recall button.



ELECTRONIC CHESS BOARD TUTOR £19.75 inc. VAT.

Price includes unit with wood grained housing, and Staunton design chess pieces. Computer plays black or white and against itself and comes complete with a mains adaptor and 12 months guarantee.

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CHESS CHAMPION - 6 LEVELS £82.87 + VAT.

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+ VAT.

BORIS - MULTI-LEVEL TALKING DISPLAY £165.28

+ VAT.

A special bulk purchase of these amazing chess teaching machines enables us to offer them at only £19.75 less than half recommended retail price. The electronic chess tutor is a simple battery operated machine that can actually teach anyone to play chess and improve their game right up to championship level. This machine is not only for total beginners but also for established players wanting to play better chess. Unit contains the electronic chessboard with 32 chess pieces, a 64 page explanatory booklet and a set of 32 progressive programme cards including 6 beginners cards, 16 check mate positions, 9 miniature games, 5 openings, 3 end games, 26 chess problems and 2 master games.

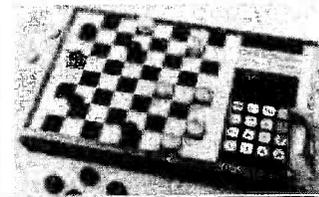
DRAUGHTS COMPUTERS

CHECKER CHALLENGER 2 LEVELS £43.98 + VAT.

4 LEVELS £80.00 + VAT.

The draughts computer enables you to sharpen your skills, improve your game, and play whenever you want. The computer incorporates a sophisticated, reliable, decision-making microprocessor as its brain. Its high level of thinking ability enables it to respond with its best counter moves like a skilled human opponent. You can select offence or defence and change playing difficulty levels at any time. Positions can be verified by computer memory recall. Machine does not permit illegal moves and can solve set problems. Computer comes complete with instructions, mains adaptor and twelve months guarantee.

PLAY DRAUGHTS/CHECKERS AGAINST THE COMPUTER



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 Learnabout—Making a Transistor Radio
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 Learnabout—Simple Electronics
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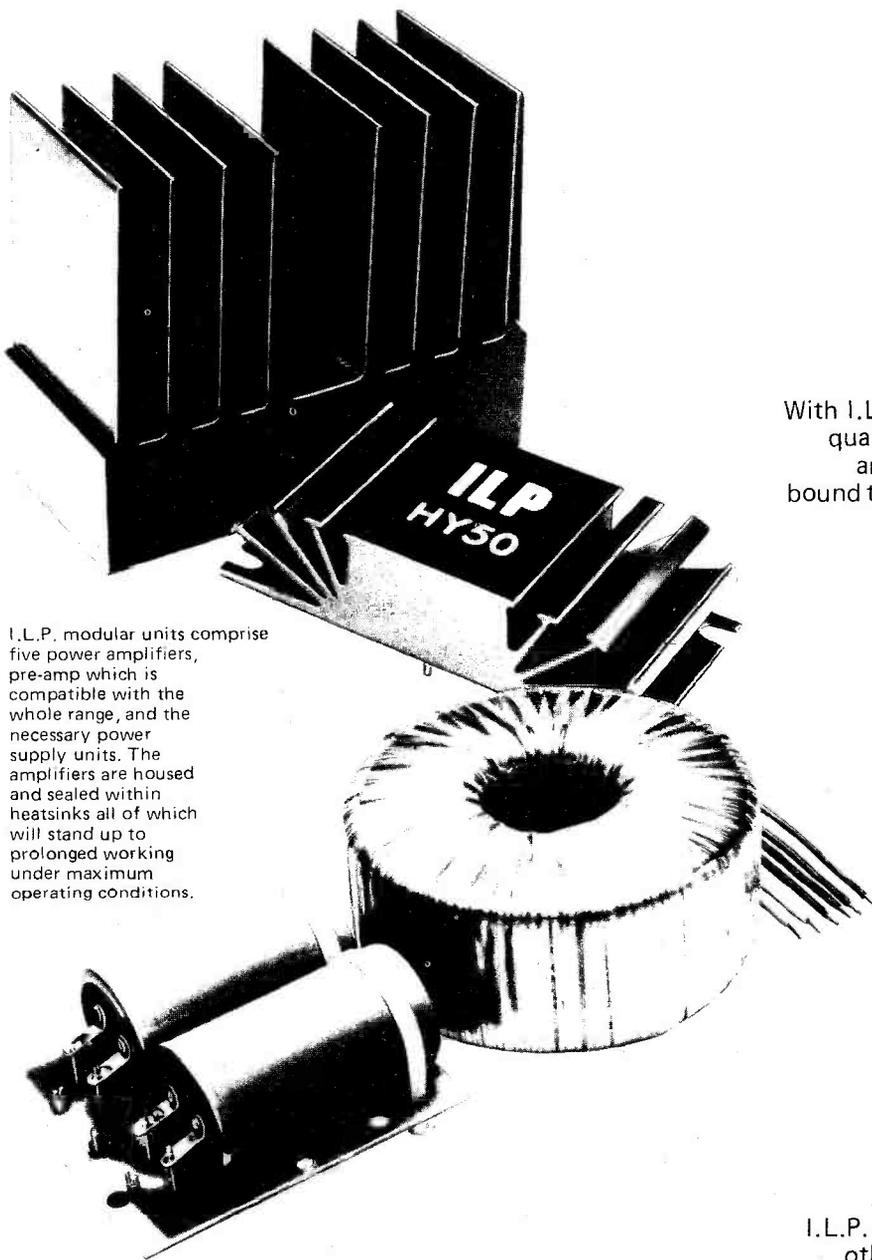
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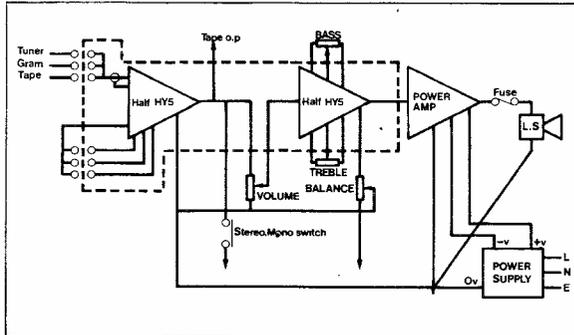
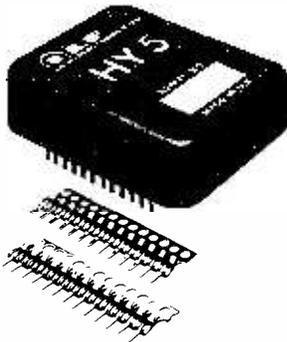
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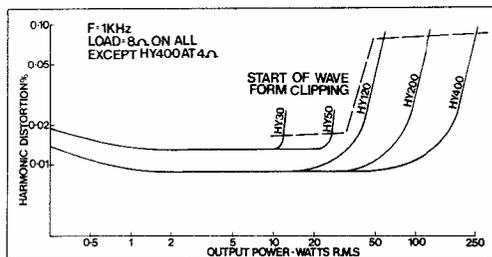
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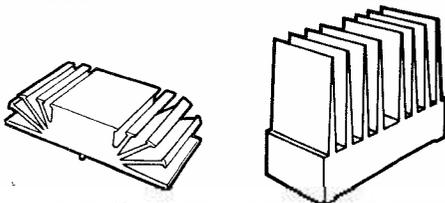
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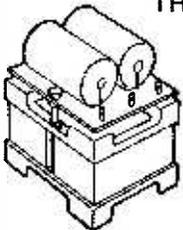


| Model | Output Power R.M.S. | Distortion Typical at 1KHz | Minimum Signal/Noise Ratio | Power Supply Voltage | Size in mm | Weight in gms | Price + V.A.T. |
|-------|---------------------|----------------------------|----------------------------|----------------------|------------|---------------|----------------|
| HY30 | 15 W into 8 Ω | 0.02% | 80dB | -20 -0- +20 | 105x50x25 | 155 | £6.34 + 95p |
| HY50 | 30 W into 8 Ω | 0.02% | 90dB | -25 -0- +25 | 105x50x25 | 155 | £7.24 + £1.09 |
| HY120 | 60 W into 8 Ω | 0.01% | 100dB | -35 -0- +35 | 114x50x85 | 575 | £15.20 + £2.28 |
| HY200 | 120 W into 8 Ω | 0.01% | 100dB | -45 -0- +45 | 114x50x85 | 575 | £18.44 + £2.77 |
| HY400 | 240 W into 4 Ω | 0.01% | 100dB | -45 -0- +45 | 114x100x85 | 1.15Kg | £27.68 + £4.15 |

Load impedance — all models 4 - 16 Ω
 Input sensitivity — all models 500 mV
 Input impedance — all models 100 KΩ
 Frequency response — all models 10Hz - 45KHz - 3dB



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|--------|--|--------------------|
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| PSU 50 | for 1 or 2 HY50's | £8.10 + £1.22 VAT |
| PSU 70 | with toroidal transformer for 1 or 2 HY120's | £13.61 + £2.04 VAT |
| PSU 90 | with toroidal transformer for 1 HY200 | £13.61 + £2.04 VAT |
| PSU180 | with toroidal transformer for 1 HY400 or 2 x HY200 | £23.02 + £3.45 VAT |
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7/8/9 | Price £12.84 & 30 pence p & p. |
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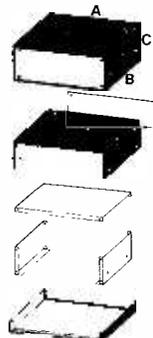
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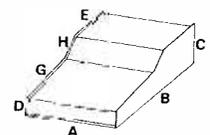
| | NOMINAL OUTSIDE DIMENSIONS | | | | | |
|------|----------------------------|------|------|-----|-----|-----|
| | inch | | | mm | | |
| | A | B | C | A | B | C |
| 19R2 | 19.25 | 9.75 | 3.75 | 489 | 247 | 98 |
| 19R3 | 19.25 | 9.75 | 5.50 | 489 | 247 | 140 |
| 19R4 | 19.25 | 9.75 | 7.25 | 489 | 247 | 184 |
| 19R5 | 19.25 | 9.75 | 9.00 | 489 | 247 | 227 |
| 17U2 | 17.50 | 9.75 | 3.38 | 444 | 247 | 88 |
| 17U3 | 17.50 | 9.75 | 5.13 | 444 | 247 | 130 |
| 17U4 | 17.50 | 9.75 | 6.88 | 444 | 247 | 175 |
| 17U5 | 17.50 | 9.75 | 8.63 | 444 | 247 | 219 |

17UXP=17U Box with 19R Front Panel for rack mounting.

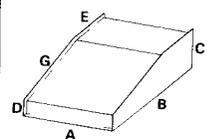


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|----------------------------|-------------------------------|-----|------|------|------|------|---|
| | A | B | C | D | E | G | H |
| inch | 6 | 13 | 15.5 | 8 | 12 | 15.5 | |
| mm | 152 | 330 | 394 | 203 | 305 | 394 | |
| inch | 8 | 13 | 17 | 8 | 13 | 17 | |
| mm | 203 | 330 | 432 | 203 | 330 | 432 | |
| inch | 3 | 4 | 4.25 | 3 | 4 | 4.25 | |
| mm | 76 | 102 | 108 | 76 | 102 | 108 | |
| inch | 25 | 26 | 44 | 51 | 63 | 63 | |
| mm | 635 | 660 | 1118 | 1300 | 1600 | 1600 | |
| inch | 1.5 | 2 | 2 | 2 | 2 | 2 | |
| mm | 38 | 51 | 51 | 51 | 51 | 51 | |

| TYPE | DS 6 | DS12 | DS15 | SS 8 | SS13 | SS17 | 19R2 | 19R3 | 19R4 | 19R5 | 17U2 | 17U3 | 17U4 | 17U5 | 17UXP2 | 17UXP3 | 17UXP4 | 17UXP5 |
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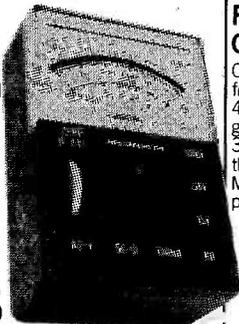
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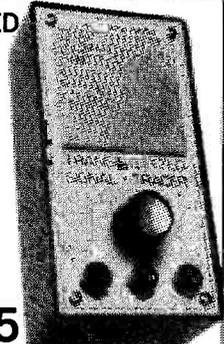
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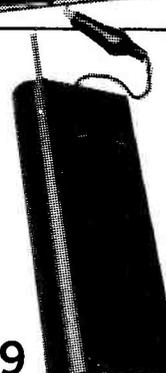
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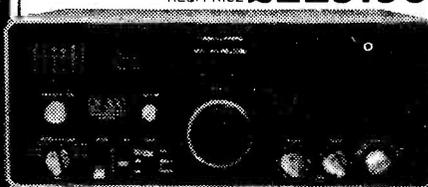
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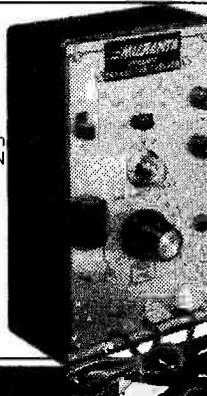
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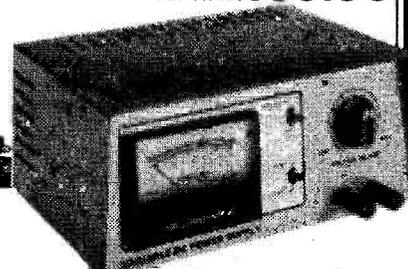
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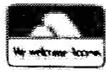
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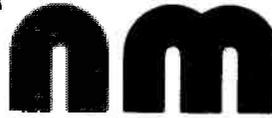
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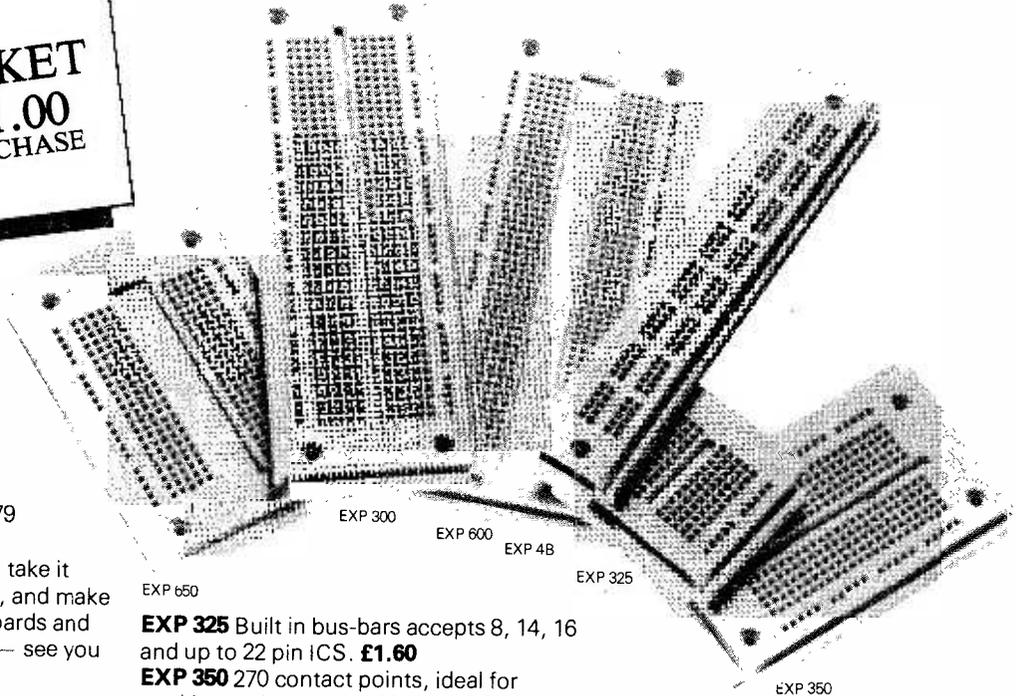
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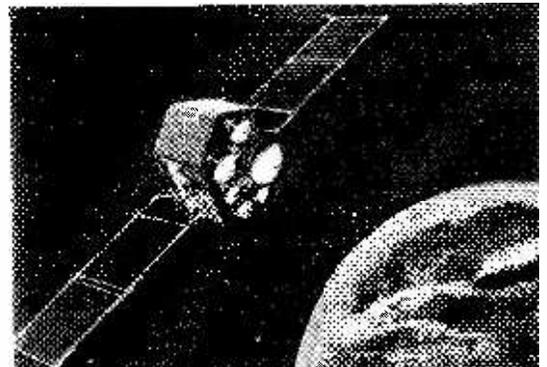
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| Ref | Amps | Price | P & P |
|-----|------|-------|-------|
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| 105 | 3.0 | 9.42 | 1.52 |
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| Ref | VA | Price | P & P |
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| 150 | 100 | 8.38 | 1.31 |
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| 152 | 250 | 14.61 | 1.73 |
| 153 | 350 | 18.07 | 2.12 |
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| 75 | 8.50 | 1.31 | 64W |
| 150 | 11.00 | 1.31 | 44V |
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| Ref | 12V | 24V | Price | P&P |
|-----|-----|------|-------|------|
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| 117 | 16 | 8 | 11.79 | 1.52 |
| 115 | 20 | 10 | 15.38 | 2.39 |
| 187 | 30 | 15 | 19.72 | 2.39 |
| 226 | 60 | 30 | 40.41 | O.A. |

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| Ref | mA | Volts | £ | P&P |
|-----|----------|-----------------|------|------|
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| 212 | 1A, 1A | 0-6-0-6 | 3.14 | 0.90 |
| 13 | 100 | 9-0-9 | 2.35 | 0.44 |
| 235 | 330, 330 | 0-9-0-9 | 2.19 | 0.44 |
| 207 | 500, 500 | 0-8-9-0-8-9 | 3.08 | 0.90 |
| 208 | 1A, 1A | 0-8-9-0-8-9 | 3.88 | 0.90 |
| 236 | 200, 200 | 0-15-0-15 | 2.19 | 0.44 |
| 214 | 300, 300 | 0-20-0-20 | 3.08 | 0.90 |
| 221 | 700 (DC) | 20-12-0-12-20 | 3.75 | 0.90 |
| 206 | 1A, 1A | 0-15-20-0-15-20 | 5.09 | 1.10 |
| 203 | 500, 500 | 0-15-27-0-15-27 | 4.39 | 1.10 |
| 204 | 1A, 1A | 0-15-27-0-15-27 | 6.64 | 1.10 |
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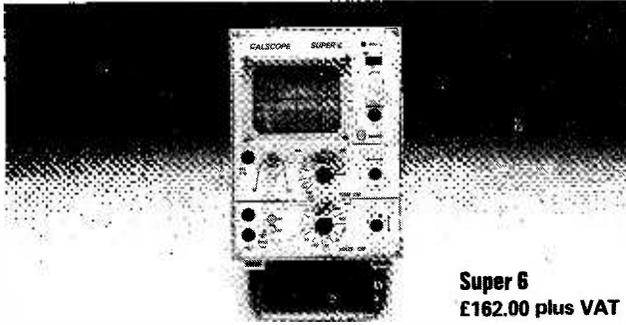
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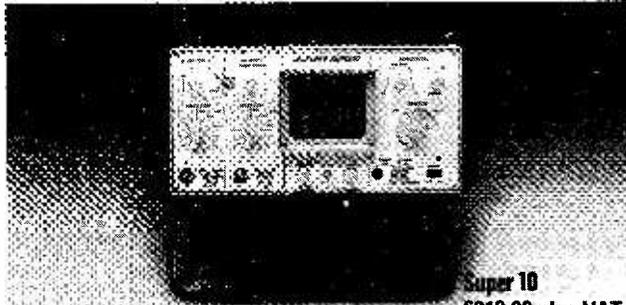
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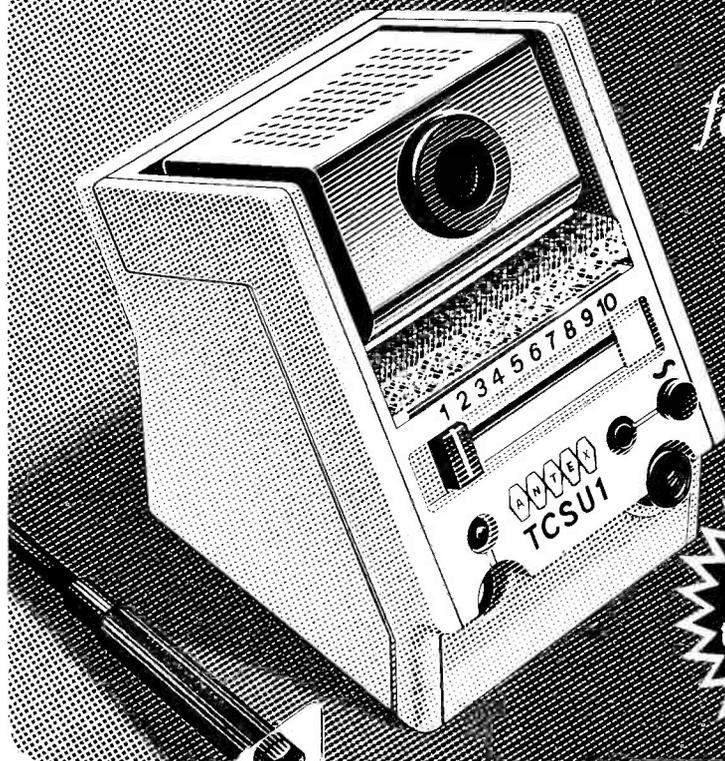
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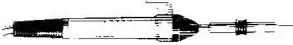


Accurate pin point temperature control between 65° and 400°C. Heating element and sensor built in tip of the iron for fast response. Interchangeable slide-on bits from 4.7mm (3/16") down to 0.5mm. Zero voltage switching, no spikes. No magnetic field, no leakage. Supplied with miniature CTC (35-40watt) iron or XTC (50watt) TCSU1 soldering station with XTC or CTC iron **£36** (6.44) Nett to Industry

Model TCSU2— Specification as TCSU1 except temperature range 200° - 400°C. Visual temperature indicators by square LED at 270, 300, 330 and 360°C. Priced at **£42.50** (7.50) Nett to Industry.



Model CX 17watts - 230 volts



A miniature iron with the element enclosed first in a ceramic shaft, then in stainless steel. Virtually leak-free. Only 7 1/4" long. Fitted with a 3/32" bit. **£4.20** (.98) Range of 5 other bits available from 1/4" down to 3/64". Also available for 24 volts.



Spare element Model CX230E

Model X25 25 watts - 230 volts



A general purpose iron also with a ceramic and steel shaft to give you toughness combined with near-perfect insulation. Fitted with 1/8" bit and priced at **£4.20** (.98) Range of 4 other bits available. Also available in 24 volts



Spare element Model X25 24GE

Model SK3 Kit



Contains both the model CX230 soldering iron and the stand ST3. Priced at **£5.70** (1.49) It makes an excellent present for the radio amateur or hobbyist.

Model SK4 Kit



With the model X25/240 general purpose iron and the ST3 stand, this kit is a must for every toolkit in the home. Priced at **£5.70** (1.49)

Model SK1



This kit contains a 15 watt miniature soldering iron, complete with 2 spare bits, a coil of solder, a heat sink and a booklet. How to Solder. Priced at **£5.95** (1.53)

Model MLX 12volts



The soldering iron in this kit can be operated from any ordinary car battery. It is fitted with 15 feet flexible cable and battery clips. Packed in a strong plastic envelope it can be left in a car, a boat or a caravan ready for soldering in the field. Price **£4.55** (1.14)

ST3 Stand.



A strong chromium plated, steel spring screwed into a plastic base of high grade insulating material provides a safe and handy receptacle for all ANTEX models soldering irons. Priced at **£1.50** (.57)

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