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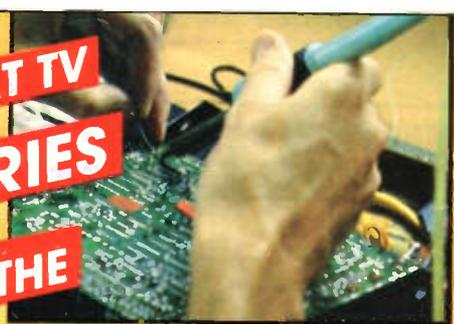
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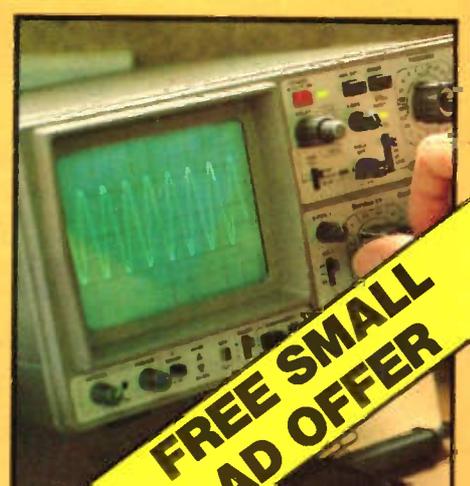


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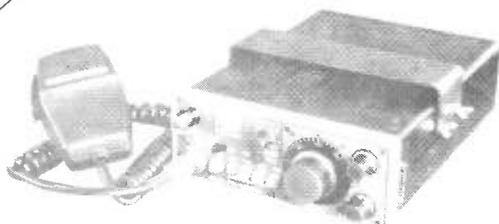
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Radio & Electronics World

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New Publishers

Welcome to the new improved **Radio & Electronics World**.

We are pleased to announce that we have bought **Radio & Electronics World** from its previous owners, Broadercasting Ltd.

Our policy is to produce the most innovative, absorbing and best selling magazine embracing the fields of communications, electronics and computers and the interaction of these areas.

Our aim is to continually improve the magazine and provide you the reader, with what you want. We will be pleased to receive your comments which will be invaluable in helping us to plan future issues.

Free supplement

The second and third parts of the Amateurs Handbook, forming a comprehensive compilation of data for everyone using the airwaves, will be included completely free of charge, with the January and February issues of **Radio & Electronics World**.

Publication date change

For production reasons we have altered the publication date of **Radio & Electronics World** to the 2nd Friday of the month — so the January issue will be on sale from 9th December.

Don't miss the next issue

Do not risk being disappointed by not being able to obtain your copy. Place a regular order at your newsagent or take advantage of our post-free subscription offer.

Whilst every care is taken when accepting advertisements we cannot accept responsibility for unsatisfactory transactions. We will, however, thoroughly investigate any complaints.

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Highways of The Future

British Telecom has notched up yet another world first in the field of optical fibre communications, this time with the first commercial single-mode optical fibre 140Mbit/sec link. The cable in question runs between Luton and Milton Keynes, a distance of some 17 miles, and the losses are so low that the data signal does not need to be boosted by any of the intermediate regenerators that have to be installed every 4—6 miles along multimode cables. This represents yet another step towards a system that should (in the long run, at least) bring significant savings in capital and operating costs. Each 140Mbit/sec system, by the way, could carry nearly 2000 simultaneous phone calls or two colour TV pictures.

These and other similarly influential developments were the subject of a recent IEEIE national lecture given by Mr C A May, Director of Research at British Telecom. Modern technology has not only provided us with optical fibres with all the advantages of size, weight and cost over coax for handling the same number of telephone calls — and communication via pulses of light: it has also given us the opportunity for 'digitalisation' of our communication services. 'Digitalisation' may be a bit of a horrible word but transmission of information in digital rather than analogue form has two very important advantages. The first is negligible distortion and so legibility is readily maintained: the second is compatibility with computerised systems. The latter opens up a whole new world for communications and already the telephone network is beginning to be used for the transmission of computer data, electronic mail, facsimile and visual images.

The drive behind all these developments is towards a totally integrated service network offering the customer maximum choice over transmitter, receiver and form for the information exchange. Much of the technology for this is incorporated in the hardware and software of modern telephone exchanges, with the principal problems being ones of finding methods of handling both analogue and digital signals and of finding appropriate switching algorithms. Mr May pointed out that there was some useful research on the latter to be done, probably in some university computer science department. The software is obviously the more flexible component here and so the new concepts of the future will probably be incorporated via this medium.

Another major area of recent progress is satellite-based communications. Their disadvantage is that the route via a satellite takes around 0.25sec, but this is easily outweighed by their power (in terms of the number of communications channels that can be supported and the fact that it takes a maximum of two satellite hops to get anywhere round the world) and the flexibility offered through satellites essentially being a broadcast medium. The latter has the advantage that a suitable receiver can be set up almost anywhere, the only problem being pointing it in the right direction to 'see' the geostationary satellite. Indeed the common 3m dishes can be used mounted on a trailer. However, its broadcast nature does cause problems of security though these can readily be overcome with the use of encryption techniques.

One aspect of all this development that is not yet clear is whether the *pattern* of the exchange network will change. (We are already seeing a reduction in the number of exchanges with the present 400 or so analogue exchanges due to give way to about 60 digital ones by 1988.) One possible leader in any such change is cellular radio, although how influential this will be could depend on its overall success. This particular network could well find itself in trouble through running out of available spectrum.

An event to remember

Members of the Farnborough and District Radio Society made intensive use of the airwaves from 14th October until the 22nd, working the bands both CW and SSB in the hope of making contact with radio amateurs all over the world. The reason for all this activity was a scheme to commemorate the 75th anniversary of Colonel SF Cody's first sustained powered flight in Britain on 16th October 1908 over Laffans Plain, an area now accustomed to the rather more sophisticated machines that feature biennially at Farnborough Air Shows. And the arrangements made included the use of a special callsign — GB2CDY — and a

special QSL card, pictured here.

The station operated from the local Railway Enthusiasts' Club, where the radio society meet and the site for an Open Day on the 15th attended by the local mayor and Colonel Cody's grandson. The event also featured displays set up by some of the sponsors of the commemoration, three amateur radio stations and an amateur TV station, as well as a number of individual displays.

The flight 75 years ago, by the way, came to a somewhat undignified end when the left wing struck the ground as Colonel Cody banked to avoid a clump of trees. The flying machine — though, fortunately, not Colonel Cody — was substantially damaged.



A story of a sponsorship

Back in 1982, which you may remember was Information Technology Year, BP Oil announced that it was issuing another in its sequence of Challenges to Youth. This time the problem was to design and construct a robot to perform a simple but realistic task — 'sniffing out' a small cube, picking it up and returning to base.

The Buildarobot Competition attracted more than 400 enquiries from schools, of which just 21 were chosen as finalists, after convincing the judges that they had the ideas and the enthusiasm to grasp and extend the science of robotics. And one of these was the Royal Latin School, Buckingham, whose team is pictured here. They unfortunately didn't win



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2. 500mW TV Transceiver	(As 1 above plus TVUP2) + PSI 433	50.00	
3. 10W TV Transmit	(As 1 above plus 70FM10 + BD335)	50.00	
4. 10W TV Transceiver	(As 2 above plus 70FM10 + BD335)	70.00	
5. 70cms 500mW FM Transceiver	(70T4 + 70R5 + SSR1)	70.00	
6. 70cms 10W FM Transceiver	(As 5 above plus 70FM10)	90.00	
7. Linear/Pre-amp 10W	(144PA4/S + 144LIN10B)	36.00	
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9. 70cms Synthesised 10W Transceiver	(R5+SY+AX+MOD+SSR+70FM10)	120.00	
10. 2M Synthesised 10W Transceiver	(R5+SY+SY2T+SSR+70FM10)	100.00	

70cms Equipment

	Code	Assembled	KR
Transceiver Kits and Accessories			
FM Transmitter (0.5W)	70FM05T4	38.10	24.95
FM Receiver	70FM05R5	68.15	48.25
Transmitter 6 Channel adaptor	70MCO6T	19.85	11.95
Receiver 8 Channel Adaptor	70MCO6R	27.15	19.95
Synthesiser (2PCB's)	70SY25B	84.95	60.25
Synthesiser Transmit Amp	A-X3U-06F	27.60	17.40
Synthesiser Modulator	MOD1	8.10	4.75
Bandpass Filter	BPF433	6.10	3.25
PIN RF Switch	PSI433	7.10	5.95
Converter (2M or 10M if)	70RX2/2	27.10	20.10

TV Products

	Code	Assembled	KR
Receiver Converter (Ch 36)	TVUP2	26.95	19.60
Pattern Generator	TVPG1	39.93	32.53
TV Modulator	TVM1	8.10	5.30
Ch 36 Modulator	TVMOD1	10.15	6.95
3W Transmitter (Boxed)	ATV-1	87.00	-
3W Transceiver (Boxed)	ATV-2	199.00	-

Power Amplifiers (FM/CW) Use

	Code	Assembled	KR
50mW to 500mW	70FM1	14.65	8.85
500mW to 3W	70FM3	19.65	13.25
500mW to 10W	70FM10	30.70	22.10
3W to 10W	70FM3/10	19.75	14.20
10W to 40W	70FM40	58.75	45.20
Combined Power Amp/Pre-Amp	70PA/FM10	48.70	34.65

Linears

	Code	Assembled	KR
500mW to 3W	70LIN3/LT	25.75	18.60
3W to 10W (Compatible ATV1/2)	70LIN3/10E	39.10	28.95

Pre-Amplifiers

	Code	Assembled	KR
Bipolar Miniature (13dB)	70PA2	7.90	5.95
MOSFET Miniature (14dB)	70PA3	8.25	6.80
RF Switched (30W)	70PA2/S	21.10	14.75
GaAs FET (16dB)	70PA5	19.40	12.65

2M Equipment

	Code	Assembled	KR
Transceiver Kits and Accessories			
FM Transmitter (1.5W)	144FM2T	36.40	22.25
FM Receiver	144FM2R	64.35	45.76
Synthesiser (2 PCB's)	144SY25B	78.25	59.95
Synthesiser Multi/Amp (1.5W O/P)	ST2T	26.85	19.40
Band pass Filter	BFP144	6.10	3.25
PIN RF Switch	PSI144	9.10	7.75

Power Amplifiers/Linears

	Code	Assembled	KR
1.5W to 10W (FM) (No changeover)	144FM10A	18.95	13.95
1.5W to 10W (FM) (Auto-changeover)	144FM10B	33.35	25.95
1.5W to 10W (SSB/FM) (Auto-changeover)	144LIN10B	35.60	26.95
2.5W to 25W (SSB/FM) (Auto-changeover)	144LIN25B	40.25	29.95
1.0W to 25W (SSB/FM) (Auto-changeover)	144LIN25C	44.25	32.95

Pre-Amplifiers

	Code	Assembled	KR
Low Noise, Miniature	144PA3	8.10	6.95
Low Noise, Improved Performance	144PA4	10.95	7.95
Low Noise, RF Switched	144PA4/S	18.95	14.40

General Accessories

	Code	Assembled	KR
Toneburst	TB2	6.20	3.85
Piptone	PT3	6.90	3.95
Kaytone	PTK3	8.20	5.95
Relayed Kaytone	PTK4R	9.95	7.75
Regulator	REG1	6.80	4.25
Solid State Supply Switch	SSR1	5.80	3.60
Microphone Pre-Amplifier	MPA2	5.95	3.45
Reflectometer	SWR1	6.35	5.35
CW Filter	CWF1	6.40	4.72
TVI Filter (Boxed)	HPF1	5.95	-

6M Equipment

	Code	Assembled	KR
Converter (2M i.f.)	6XR2	27.60	19.95

Prices include VAT at the current rate. Please add 75p for postage and handling to the total order. Kits are usually in stock but please allow 28 days maximum for delivery should there be any unforeseen delay. Kits when assembled will be gladly serviced at our Aldermaston works.

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School of Electronic Engineering, Arborfield, Berkshire—indeed, they were one of a number of teams whose robots did not fulfil the task on the day. What was special about them was that *R&EW*, together with Ambit International, had given them support following an initial request for help with components. The story of their design, which involved a robot controlled by a BBC Micro responding to signals from dual scanning light sensors made from bicycle lamps, will be told in the near future in *R&EW*.

The winner of the competition was Hinchingsbrook School, Huntingdon, who steered their robot by pulse width modulated (PWM) signals fed to the kind of servo you would find on a radio controlled model aircraft or car: it took just 4.7sec for this robot to complete the task. Their prize of £500 and the Buildarobot trophy was presented by Kenneth Baker, who emphasised in his address the value of new technology in creating the wealth of the future and expressed his delight at the interest and inventiveness shown by all the finalists.

In the eye of the beholder

According to Alex Durrant, quality control manager at Protronic 24, some purchasers of custom—designed PCBs place more emphasis on the appearance of the board than on its inherent quality. This opinion accompanied the announcement that Protronic 24, an independent designer and producer of PCBs, had been granted BSI approval, a step that called for the building of a suitable secure area to serve as a bonded materials store and in-depth documentation of procedure: good customer references, it seems, were not enough.

But it's not the BSI that Mr Durrant feels strongly about; his concern is based on instances when buyers have sought to reject jobs as defective because certain contacts had not been gold plated when there was, in fact, no need for them to be

so. At the same time, he has been made aware of other PCB manufacturers that have produced boards high on appearance but low on functionality with plating through the hole well below the required thickness, for example.

Protronic 24 has long used sophisticated process controls and test procedures, and so its products should always come up to standard and may often be better than those of its competitors. However, Mr Durrant may well have a valid point about the way a typical customer views the product he is intending to pay good money for.



The latest fashion accessory at Harvey Nichols—an Apricot microcomputer. Today's shoppers at certain stores within the Debenham's empire can—given suitable financial resources—buy one of these ACT machines from the shop-within-a-shop there known as Greens Business Systems. The sales campaign is designed with the executive in mind and is said to reflect the current state of affairs whereby 'Microcomputers are no longer the preserve of a commercial elite: they've hit the High Street.' Training sessions will be held in-store through which most users should pick up the basics of microcomputing in a couple of hours. The branches of Debenhams in question are, by the way, Oxford, Guildford, Harlow, Staines, Romford and Southampton.

Company News

The American Company of **Dielectric Communications**, a recognised leader in the field of RF technology, has picked out **Chapman Electronics (TCE)** of Epping, Essex, as a key element in its present drive to improve product availability and associated back-up services in Europe. TCE already handles a number of Dielectric's lines which extend from the proven to the novel, e.g. diplexers. It now incorporates in its range the coaxial switches and patch panels that facilitate fast RF switching with maximum isolation and low VSWR.

Axiom Electronics is attempting to give the lie to the opinion that 'ROMs have unacceptably long lead times'. In conjunction with **Motorola**, it has established a service whereby a 64K ROM could be taken to prototype level (150—200 pieces) in six weeks and to the 10,000-piece production level just eight weeks after approval. Axiom sees the products of this service as representing a competitive alternative to EPROMs.

Ferranti Computer Systems has signed an agreement with **Advance Technology (UK)** whereby it produces the new Advance 86 microcomputer—which, it is no surprise to learn, is designed around a Ferranti ULA. The agreement covers PCB assembly, board testing, general assembly, burn in and full functional testing. Ferranti's testing facilities are said to be among the most advanced in Europe.

Racal Electronics has recently come to an agreement with **Thorn Ericsson Telecommunications** whereby the latter develops the system that will form the basis of the cellular radio service Racal is hoping to get into operation in 1985. Equipment for telephone exchanges, signal processing, radio channel handling and base stations 'meet' the UK Total Access Communications System (TACS) specification is to be supplied by Thorn Ericsson in a deal involving as much as £100 million before the end of the decade.

RFI Shielding, believed to be Britain's only manufacturer of shielded windows, is to start offering custom designed (and manufactured) units in addition to its standard range. These will encompass the customer's requirements with regard to choice of materials as well as his electrical, environmental and other physical specifications. Applications for RF shielded windows include instrument panels, computers, communications equipment and sensitive measuring devices.

Oric Products—father of the Oric 1, a familiar sight in your local Lasky's or Dixon's—had an eventful month in October. On the 5th, it was acquired by **Edenspring Investments** in a move to have sufficient financial backing to accelerate its programme of R & D aimed at developing 'a number of new products to expand Oric's product base, not solely in the computer field'. Then its main assembly plant, Kenure Plastics at Feltham, suffered a major fire on the 13th—but production was able to start the following day in a new factory, making everyone confident that they would fulfil all the October orders by the end of that month. A few days later, Oric announced that Oric 1's were to be sold in all branches of the **Comet** and **Rumbelow** chains.

Dawne Instruments and Electronics has achieved its first major distributorship in becoming North-East Stockist/Distributor for **GEC Measurements**. The firm already handles a wide range of laboratory equipment (including Apple microcomputers) which it backs up with data, appropriate guarantees and the assembly of prototypes. It has now taken on GEC's range of multimeters and portable test equipment.

PRODUCT NEWS

Featured on these pages are details of the latest products in communications, electronics and computers. Manufacturers, distributors and dealers are invited to supply information on new products for inclusion in Product News
Readers, don't forget to mention **Radio & Electronics World** when making enquiries

ELECTRONICS RESINS

Ciba-Geigy has announced a new range of epoxy resins that have been specially formulated for the electronics industry.

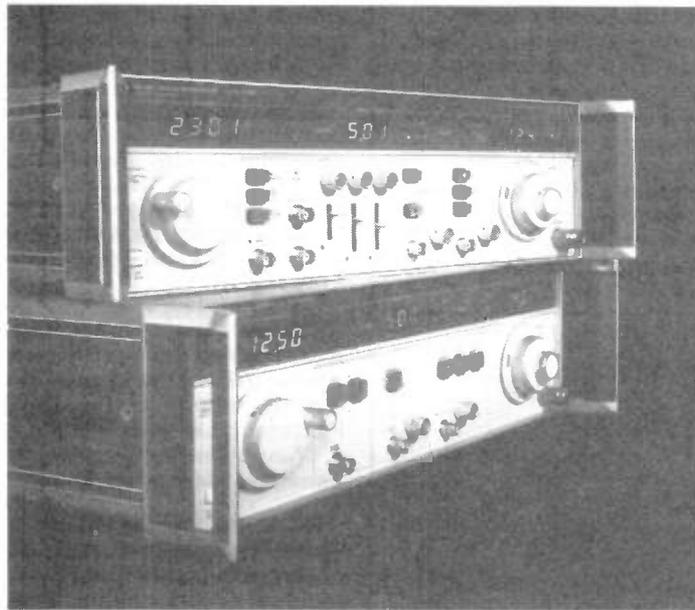
The Araldite 1300 range comprises 16 formulations, developed individually with the intention of providing a product to suit almost every application. As a result, the resins are either hot or cold setting and include filled and



unfilled systems, resins that offer a considerable degree of flame retardancy, flexible resins and low viscosity impregnation systems.

Many of the formulations within the range are supplied in preweighed quantities to ease mixing, while two systems are available in 0.5kg sachets designed for use in less extensive applications. A wallchart detailing the complete Araldite 1300 range in terms of processing information and physical properties is also available from Ciba-Geigy.

Plastics Division, Ciba-Geigy, Duxford, Cambridge. CBZ 4QA



EXTENDED FREQUENCY GENERATION

Hewlett-Packard has announced that its HP 8683D and 8684D cavity-tuned signal generators now include an internal doubler system that extends the available frequency bands and provides doubled FM deviation.

The internal pulse generator within these models (and their forerunners, the 8683B and 8684B) generates pulses at 10Hz–1MHz, with pulse widths of 100nsec–100msec and pulse delays of 50nsec–100msec. These signals can readily be amplitude modulated at depths of up to 70% and rates of up to 10kHz. The new models offer DC–10MHz modulation and +10MHz deviation, making them suitable for satellite-video applications. They also feature high performance pulse modulation in both the main and the doubled bands for use in radar and EW applications which require rise/fall times shorter than 10nsec and an on/off ratio of more than 80dB.

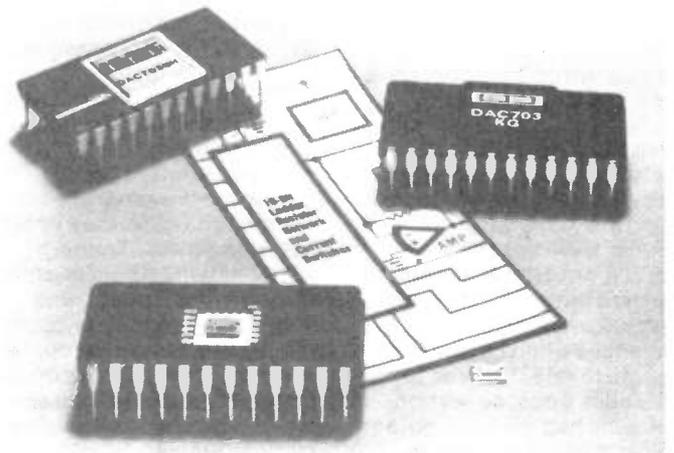
Cavity-tuned generators generally offer a number of advantages, including a spurious signal level of less than –80dB(C), a SSB phase noise below –72dB(C)/Hz at an offset of 10kHz in the X-band and a broadband noise floor of –135 to –150dB(C).

Hewlett-Packard Ltd, Eskdale Road, Winnersh, Wokingham, Berks. RG115DZ

16-BIT MONOLITHIC DAC

The DAC701 and DAC703 are both versions of what is believed to be the first 16-bit monolithic digital-to-analogue converter that also incorporates a precision Zener voltage reference and a low-noise fast-settling output op-amp. Both of these devices accept binary-coded TTL and LS TTL input signals and employ current switching in providing a monotonic (to 14 bits) output over the specified temperature range of either 0–70°C or –25 to +85°C: the difference is in their output voltage range which is 0–10V for the DAC701 and –10 to +10V for the DAC703.

Burr-Brown has designed the new converters to be pin compatible with the industry standard DAC70, 71 and 72 families, so that they can be used to upgrade existing systems. Applications are envisaged in a wide range of mini/microcomputer-based industrial control systems and other instrumentation, including that operated by the Military as the devices pass the leak requirements of the appropriate standard. Other advantages include a maximum linearity error of 0.003%, a settling time of



PRODUCT NEWS

8 μ sec following a fullscale input change and drifts of no more than 18ppm of FSR/ $^{\circ}$ C.

Burr-Brown International Ltd, Cassiobury House, 11-19 Station Road, Watford, Herts. WD1 1EA.

ULTRATHIN TRANSFORMER

The OB range of transformers supplied by Avel-Lindberg includes one said to be the thinnest transformer yet. The 0.8VA model shown here is less than 10.5mm thick and so can fit even the smallest card frames.

The facilities offered by these transformers include dual primaries for 240 or 120VAC 50/60Hz mains operation, together with twin centre-tapped secondaries that give 10V (80mA)–48V (17mA) in series and 5–24V in parallel. The windings are on separate bobbins to give maximum isolation and low inter-winding capacitance. The normal method of fixing them

to a PCB is to direct solder the connecting pins, but they can also be screwed to the board if extra mechanical strength is required. The advantage of having transformers of this level of power rating (the other members of the range have ratings of 2–14VA) is that they offer the option of extra power capacity actually on the board, for example, as a modification to an existing design.

The transformers are proof-tested at 5kVAC and 120 $^{\circ}$ C, and they conform to IEC 65, BS415 and VDE 0550 regulations.

Avel-Lindberg Ltd, South Ockendon, Essex. RM15 5TD

SOLID STATE 'TAPE RECORDER'

Johne & Reilhofer's Universal series of PCM data acquisition equipment has

gained a new member — a high capacity semiconductor storage memory system known as the 32KS13. In common with other members of the series, each module within this system receives up to eight analogue signals, samples them and uses this data to represent each sample by a 12-bit word, the individual data streams being multiplexed on a time division basis.

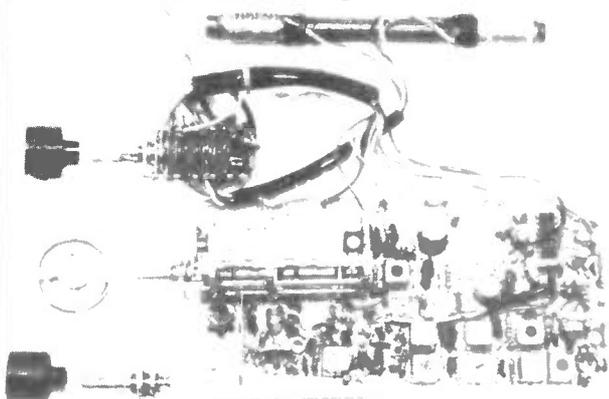
Normally the resulting PCM serial bit stream is then transmitted to a 4-track tape recorder where it is recorded on one track. The solid state system mimics this through having four modules, each handling eight channels and each storing up to 2¹⁸ (~256,000) measurement values. This data can subsequently be accessed via a RS232-driven memory controller and output either via a RS232 port or to a computer by using the DMA handshake.

The 32KS13 should not be seen as just part of the Universal series; it is also electrically compatible with

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Please write to **Kevin Bond, Radio & Electronics World, Sovereign House, Brentwood, Essex CM14 4SE**

PRODUCT NEWS

Johne & Reilhofer's other PCM data acquisition systems. Its main role will be where the moving parts of a tape recorder are at risk, for example where there is much vibration or high dust levels. Its other advantage is its zero start-up time, which is particularly beneficial where transients are of interest.

Johne & Reilhofer (UK) Ltd, Oddstones House, Thompsons Close, Harpenden, Herts. AL5 4ES

GRAPHICS TABLET

Terminal Display Systems (TDS) has announced the first series of graphics tablets to be both made and marketed by the firm. The top of the range tablet shown here — the HR48 — is intended for professional use by such people as cartographers, seismologists and engineering designers.

Of more interest to readers of *R&EW* should be the 'baby' of the series, the TDS12, which is said to be 'compact, easy to use, lightweight, portable and — most of all — low cost'. This device offers a highly accurate and linear method of inputting x,y coordinates from graphic data, the operating principle involved being that of phase-sensitive electromagnetic induction with both the cursor and the stylus containing an energised coil. The tablet's active area is square with a side of 12" enabling it to take A4 documents either landscape or portrait. Thus a grid representing a standard form can be used to facilitate data

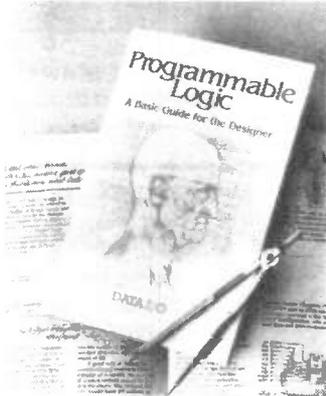
entry into your microcomputer.

TDS has put all the experience it has acquired in the past as a distributor for Applied Systems, Megatech, Ramtek and Gould among others (a role that it still performs) into the design of these tablets. The micro that drives the tablet is programmed to provide the interface to any popular microcomputer, making the system very easy to incorporate into an established system.

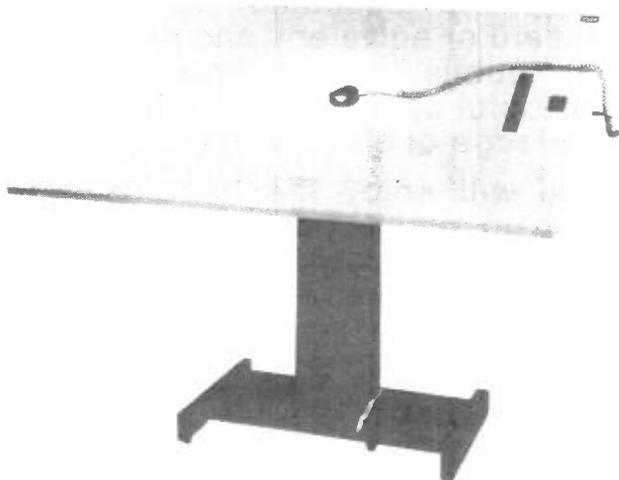
Terminal Display Systems Ltd, Philips Road, Whitebirk Estate, Blackburn, Lancs, BB1 5TH

LOGICAL CHOICE

DATA I/O has recently published a 32-page booklet covering all aspects of programmable logic including comparisons with fixed function LSI/MSI and



custom logic. *Programmable Logic — A Basic Guide for the Designer* also takes the reader through a specific



TRANSTEL DOT MATRIX PRINTER. Compact Serial Interface. 230 Volts. £88 each.
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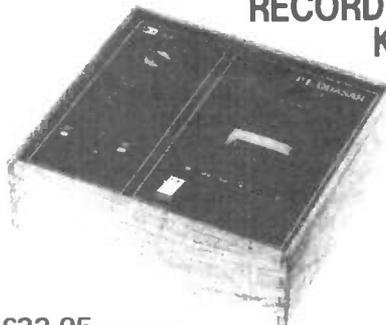
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£24.95 + £2.00 p&p.
E.T.I. kit version of above without chassis, case and hardware. £12.95 plus £1.50 p&p.

In the cut-throat world of consumer electronics, one of the questions designers apparently ponder over is "Will anyone notice if we save money by chopping this out?" In the domestic TV set, one of the first casualties seems to be the sound quality. Small speakers and no tone controls are common and all this is really quite sad, as the TV companies do their best to transmit the highest quality sound. Given this background a compact and independent TV tuner that connects direct to your Hi-Fi is a must for quality reproduction. The unit is mains operated. This TV SOUND TUNER offers full UHF coverage with 5 pre-selected tuning controls. It can also be used in conjunction with your video recorder. Dimensions: 11¼" x 8½" x 3¼".

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Featured in April issue P.E. Reprint 50p. Free with kit. Self assembly simulated wood sleeve £4.50 + £1.50 p&p

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FEATURES: VHF, MW, LW Bands, interstation muting and AFC on VHF. Tuning meter. Two back printed PCB's. Ready made chassis and scale. Aerial: AM - ferrite rod, FM - 75 or 300 ohms. Stabilised power supply with 'C' core mains transformer. All components supplied are to strict P.E. specification. Front scale size 10½" x 2½" approx. Complete with diagram and instructions.

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ACCESSORY: Stereo/mono mains power supply kit with transformer. £10.50 plus £2.00 p&p.



SPECIFICATIONS:

Max. output power (RMS): 125W.
Operating voltage (DC): 50 - 80 max.
Loads: 4 - 16 ohms.
Frequency response measured @ 100 watts: 25Hz - 20KHz
Sensitivity for 100 watts: 400mV @ 47K
Typical T.H.D. @ 50 watts, 4 ohms: 0.1%.
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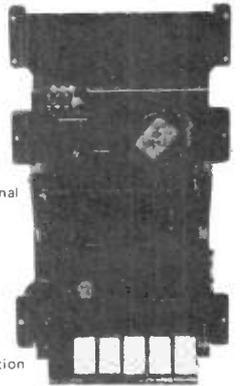
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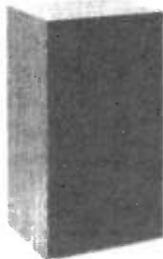
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UHF ALL-MODE TRANSCEIVER

TR 9500



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The transceiver is designed for FM, SSB, and CW modes, utilizing a microcomputer which permits frequency selection in 100Hz, 1kHz, and 5kHz, 25kHz steps by means of two digital VFOs. The microcomputer also permits memory, scanning, searching, and other features.



SP 120 TR-9500 BO-9 PS-20
£395 + carriage £5.00

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- 25 watts output on FM, SSB and CW.
- FM/USB/LSB/CW all mode operation.
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- Six memories. On FM, memories 1 through 5 for simplex or +600kHz offset, with the OFFSET switch. Memory 6 for non-standard offset. All six memories may be operated simplex, any mode.
- Memory scan. Scans memories in which data is stored. Stops on busy channels.
- Internal battery memory back-up. With Ni-Cad installed (not Trio supplied), memories will be retained approximately 24 hours, adequate for the typical move from base to mobile. A terminal is provided on the rear panel for connecting an external back-up supply.
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- CW semi break-in circuit with sidetone. Built-in, for convenience in CW operations.
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- Transmit offset switch for repeater shift
- High performance noise blanker.
- RIT (Receiver Incremental Tuning) circuit. Useful during SSB/CW operations.
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- CBM 2032 computer printer dot-matrix perfect condx. First offer over £250. Taken copy of print sent on receipt of S.A.S.E. complete with IEEE cable, full H/BK and box paper also for £400 o.n.o. Sharp PG1500 computer, case, printer 8KRAM P.S.U. case. Two H/BKS pristine condx. Will swap or W.H.Y. the perfect portable computer. Ron Broadbent, 94 Herongate Road, London, E12 5EQ. Tel: (day) 01-987-5864.
- Trio TR2200G NI-Cads charger Mic. Case all Xtals £70. Want Datong Woodpecker Blanker. Trowell, "Hamlyn", Saxon Avenue, Minster, Sheerness, Kent. ME12 2RP. Tel: (0795) 873100.
- Microwave modules MMA144V preamp with RF switching for two metres FM or SSB. Uses 3SK88 device. Good condition. Bargain £10 o.n.o. Contact Chris G8PKM (not QTHR). Tel: Chelmsford (0245) 323323 after 5.30 on weekends.
- Datong PC150KHZ to 30MHZ receive converter uses 2 mtr transceiver to listen to all HF bands £90 o.n.o. R.S.Blyth, 36 Mickleburgh Hill, Herne Bay, Kent, CT6 6DT. Tel: H/Bay 63799.
- Trio VF0120 for TS120 and TS130 transceivers only £50 o.n.o. Also Jaybeam 12XY with harness for 70cms at £38. DPCO 12v relays with 130R or 280R coils only 75p each. Limited number of 74LS series I.C.'s 20's at 10p, 27's at 10p, 47's at 30p, 373's at 45p, 161's at 30p, 193's at 30p, 92's at 24p, 374's at 65p, and 08's at 10p each. All carriage at cost or buyer collects. G. Caselton, 19 Cowden Road, Orpington, Kent, BR6 0TP. Tel: 0689 29230.
- TONO 9000E £520 GEC High band TX/RX £20. Brookes MBR6 RTTY TU £40. ORIC electron BBC programs Morse tutor £4.50. Locator £4.50 BBC RTTY £5. FT-290R with NICADS HELICAL £200. MML 144/30 LS £55. T. Tugwell, 11 The Dell, Stevenage, Herts. Tel: 0438 354689.
- C432 70 CMS hand-held case. Handbook. Ext. mic. RBO RB11 RB13 SU8 SU20 no mods £85 o.n.o. G4AWY not QTHR. R.A. Mekka, 57 St Johns Road, Caversham, Reading, RG4 0AL. Tel: (0734) 482559.
- YAESU FT 902 DM FM filter mint condition £625. Tel: 0272 873691, Clevedon, Avon.
- AR88D fine condition, some spare valves, £40 o.n.o. Tel: Reading 65013.
- FX-1 wave meter. As new, never used £30. Tel: 0903 753102.
- Marconi Marina Atlanta Receiver. Full 10 bands to 28 MEGS. Excellent condition. £75. Palm 4 40 channel 2mtr. hand-held with charger. £80. Leonard Davies GW4 HAW 46 Maes Glas, Rhos-on-Sea, Clwyd, North Wales, LL28 4AZ. Tel: 0492 40920.
- Yaesu FRG770M little used £200. Wanted manual or circuit for telequipment S51 scope. Can copy if required. Howden G6JUP QTHR. Tel: 0977 662706.
- Creed 7BRP teleprinter, immac. condition £15. Creed 656 tape reader as new £15, Pye base station transmitter £5, Homebrew 2M transceiver, valved, works off 12v £7, ICOM 1050 converted to 10M but deaf £25, 25W PA for ICOM 1050 £15. Tel: 061 773 8824.
- YAESU FL101 TX, 100% OK, with new spare pair PA valves. £100. Tel: Roy G3LBT 0268 2282 Ext. 3252 Business hours or 0268 412177 evenings.

- Plessey ICs Motorola RF power devices. RCA linear ICs etc. etc. S.A.E. list. All new guaranteed devices. G3VFP 17 Laleham Green, Bramhall, Stockport, SK7 3LJ. FT707 inc. narrow CW filter, immac. condition £400. No offers. Address as above.
- FRG 7 Radio receiver, brand new in box 150HZ to 30Mz with full guarantee. A. Slark, 43/45 Thicketford Road, Bolton, Lancs. Tel: Bolton 26684.
- Codar T28 RX cheap. Also power supply and accessories for base and mobile operation. Delivery by arrangement inclusive. Also wanted Codar AT5 TX cheap. For sale small portable tape recorder £5 plus carriage. Two small scope tubes AOR Z03 and CDU 3-FP7 £5 each plus carriage. Mr. D.F. Thompson, Four Winds, 131 St. Johns Road, Exmouth, Devon, EX8 4EW. Tel: 265059
- Optiscan SBE-12SM 12/240v AM/FM scanning receiver. Daiwa search 9 12U(CAR) FM manual tune. £10 Switched xtal Marine bands. I.M. Tasker, Colsterworth Road, Stainby, Nr. Grantham, Lincs. Tel: 078 081 315.
- Yaesu FT290R as new 8 months old boxed complete with case and Bremi 3 amp P/S. No mods £210. Buyer to collect. H.F. Barker G4BXY, 372 Gosbrook Road, Caversham, Reading, Berks, RG4 8EG.
- ZX81 plus 16K RAM pack, also seven games tapes including flight simulation, 3D Defender, Fantasy games and scramble £50 o.n.o. Tel: Wisbech (0945) 61946
- IC22A F.M. 2MTR Trans. 1 watt/10 watt Simplex S18, S19, S20, S21, S22, Repeater, R1, R3, R4, R5, R6, R7 fitted. Space for 12 more channels complete with mic and mobile fixing bracket, excellent working order £95. R Stevenson, 39 Croftway, Selby, North Yorkshire YO8 9DD. Selby 706057.
- Creed 7E Teleprinter and spares and 656 Tape reader. Will sell or swap for an unmodified ZX81 with its PSU and 16K ram. Given up RTTY. Space is required. Must be got rid of. Please contact for arrangement to collect, Ian Ruddock G8NCZ, 46 High Road, Stapleford, Hertford, Herts. SG14 3NW, Telephone Ware 871486 Saturdays only.
- Bearcat 220 AM/FM VHF/UHF Scanner. Faulty band — switching circuit. Full service and owners manuals, mobile bracket, original packing, £90. No offers. Please write to S. Langlois/GJ40DX, Merchant Navy College, Greenhithe, Kent, DA9 9NY. Can deliver within 40 miles of Dartford.
- Professionally aligned Wood and Douglas 70cm T.V. tx, 10w P.A. and Microwave Modules Up-Converter £90, RO390 Printer, 20mA, RS232 and Apple II interfaces £70, Feranti UDU 80 x 25 character green screen, manual, spares £50, multi rail computer PSU £15, 32K Nascon 22K of EPROM lots of software £250, all o.n.o. Phone Philip, Guildford 573871.
- Trio 7800 5 and 25 watt as new, boxed with manual and mobile mount. Dave G4NDJ QTHR, telephone Skelmersdale 21814 £200 ono.
- FT480 2M Multimode 9 months old, used only as base station £300. Phone Bradford-on-Avon (02216) 3600.
- Drae Morse Tutor, mains operated current model, little used as new £30, Whitstable 274947.
- Collins S Line 3253 Transmitter 75S3 receiver, good condition and working order with PSU. Revalved, well worth seeing £625, Worcester 421908.
- FDK multi Palm II for sale xtaled S20, S21, S22, 15, R4, R5, complete with wave aerial charger. Tone burst fitted, good condition, price £75 or ono. Contact Dave Drizen G8UUO, 40 Gilbert Way, Braintree, Essex.
- Binatone Video Game £25 ono, Merlin electronic game £10, power supply for both £3, all in good condition still guaranteed, will sell or swap for a Spectrum or ZX81 or a Rotator to turn a HQ1 eg HR40, 9502, 9523 or even a Morse Tutor. Please contact Mr. A. Buckton, 17 Drake Close, Marske/Sea, Redcar, Teeside, TS11 7JG, telephone (0642) 471331.
- Eddystone High Stability Professional Solid State general coverage Receiver model EC958 10kHz to 30mhz in mint condition, handbook and history £500. Datong FL3 Audio Filter £99. FT102 5 months old as new, handbook, £650. A P Davis G41ZG, 88 Goring Road, Goring-by-Sea, Worthing,

- Sussex, BN12 4AB, telephone Worthing 41109.
- Yaseu FRG7 receiver with handbook and battery power supply module, excellent condition, £135. Alec J. Mitchell (G4ICE), 11 Poplar Lane, Cannock, Staffs, WS11 1NQ. Tel: 05435 2836.
- R & EW Airband receiver. Assembled and wired all voltages correct, needs BPF 274 transistor and alignment, no case, £45. Sony 2001 as new with wave book £120, perfect condition. Radiotelephone Pye Vanguard Cat. AM25B/V/6 I2 volt, used as airfield fixed base VHF R/T £25. J T Grant, Bank House, Reepham, Norfolk NR10 4JJ, Tel: 0603 870852.
- Cushcraft TR1 band vertical with data sheet (unused) £30 ono. Tel: Larkhall 883982.20-15-10.
- N1500 Video Head and Electronics for spares or repair, all working o.k. Will exchange for audio cassette recorder, small oscilloscope, ultrasonic transducers, W.H.Y. or £15 ono each, Ring 0742 311191 after 4.30 pm.
- Racal 801R frequency conner including service manual, offers? phone Royston 71160.
- Nascom IMP Printer 80 chars. second RS232 input with full documentation in good order. 01 399 4177 after 7 pm. £100 ono.
- Marconi SIG GEN TF2006 10-500 megs £350 spare one £90, Marconi SIG GEN TF2604 £50, Marconi watt meter CT44 £6, Marconi SIG GEN TF1066 fixed output £75, advance SIG GEN SG62B £20 Scope Ex-min CT 436 £60, spare £20, KT88s GEC £5, T/former 1K,0,1KV 235ma £10, Scope advance OS15A £30. Scope, Service Scope, S51A £40, AR88D tuning gang and switch £6, Sanyo receiver RP 888OG, 9 bands crystal marker, double conversion £85, OSC tubes Hewlett Packard 61N 5083 — 0353 £15, GEC 1074H two gun £5, ACR 10 with screen and base £4, Mullard DG7/6 Screen and base £6, Marconi valve V/meter TF 2604 £75. Mr P Baylis, 42 King Edward Ave, Dartford, Kent DA1 2HY, Tel: Dartford 72913.
- ICF 2001 general coverage receiver, as new. Reason for sale — going back on air so need rig. Offers around £95. Ring Pip G8NOP on Great Cudley 506 evenings. Also Creed 7ERP Teleprinter £5 or free with above receiver.
- Nascom Two, 48K RAM, KIB, PSU, bare holmes colour PCB, all documentation. A few games, cassette player, £200 ono, Eastleigh 617214 Hants.
- Workshop clear out. Several B/W TVs, some work or could be used for spare parts or components including tubes and valves, reasonable offer would not be refused. Would suit young enthusiast. Van is advisable for collection. Phone after 7 pm 0702 78178 Southend-on-Sea area.
- RS232 interfaces for Epson and Seikusha Printers. Unused. £25 each. UK101 computer and software £60. 16K RAM boards £20 each. Honeywell qwerty keyboard, unused, £25. Dr P D Coker, 23 Darwin Close, Orpington, Kent, Tel: 0689 58510.
- Ex-BT Modem. Full Duplex or half Duplex up to 1200 B/S Assynchronous, full working order and reprint of data diagrams P.C.B. layouts etc. £50 ono. B. G. Oldford, 4 Field Close, Malinslee, Telford, Shropshire, TF4 2EH. Tel: Telford 507312.
- William Stuart Speech system new and unused, cost over £100, want £80. Includes all documentation and interface leads. Speech Synthesiser and speech recognition 'Big Ears'. John Taylor, 47 Spur Road, Orpington, Kent, BR6 0QT, tel: Orp. (0689) 35353.
- Mizuho MX-2 144mhz SSB hand held transceiver, NI-CAD battery £60. VHF VMOS power FET 20w £8. Colchester 572685.
- Trio 3R 500S £60 also old valves, D. Hardy, 12 Fyfield Road, Walthamstow, London, E14 3RG.
- Hams and SWL's are you interested in frame loop antennas, see for details, write F G Rylands, 39 Parkside Avenue, Millbrook, Southampton SO1 9AF
- Hatfield R.F. Bridge LE300A £20, Hustler mobile aerial 5 resonators Q.D. mount £40, 3WP1 tube £3, DG7-5 tube unused £10, Lumb, 14 Linton Gardens, Bury St. Edmunds, Suffolk. Tel: (0284) 4318.
- Clear-out sale. As new Scopex dual-beam 10mhz 'scope, £125, various S-100 boards: 12-slot motherboard, and 8v @ 15A PSU £35, ADS 6809 CPU (2 monitor eproms) £60, Z80A CPU (3 monitor Eproms inc CP/M B105) £80, 64 K dram with many options £50, 4 channel SI/O 1 CH populated £30,

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floppy disk controller for 8in Shugart £60, 2 x prototyping cards, 1 with RTC and Z8-pin prom SKT. I.T.T.2020 (Apple look-alike) £300 cased, 2 x Apple disk drives £125 each, green phosphor 20mhz monitor £60, 2 x ASCII keyboards £25 each, 80 column card £25, floppy disk card £25, language card £30, Z80/CPM card £35. Full original documentation supplied. 50+ disks of software available KIM-1 system £50, FT207R £80, also lots of PPSUs, meters, junk box components, odds and ends, books and mags. A Thring, 142 Kennel Lane, Great Burstead, Billericay, Essex, CM11 2SU, tel: 027-74-52325 (eve).

● DTXV Converter: receives VHF bands 1,2,3 on UHF TV. Plugs into aerial socket. £28.00. Phone 0702-8858

● 13ft6ins Ski boat inboard eng. exchange for any general coverage transceiver. Mr James Cushen, 42 Wallace Road, Bodmin Cornwall. PL31 2EX Tel: Bodmin 4681

● RA17 as new £150 AR88mint £100 HRO Restored 9 coils £90 Codar £25 6MEG 2 beam Scope £75 Heathkit Scope £25 old Cosser 2 beam Scope £40 Taylor valve voltmeter £25 Marconi valve voltmeter £35 Airmec same £35 dozens old domestic radios o'hauled. Ring anytime. Tons of spares, values etc. Ashley James, The Mount, High Street, Chalford, Stroud, Glos. GL6 8US. Tel: 0453 882164

● IBM 3982 'golfball printer with parallel port interface. Requires software to run off ASCII-Z80 program supplied. Complete with IBM manuals and a few spare and several typeheads. Has mechanical fault that requires attention. (runs, but letters not aligned properly.) £50 to knowledgeable enthusiast, carriage extra (probably £15. Porthlawn 890688. (Cornwall)

● Datong UC1 up converter £70. UK101 6502 based computer, 8k memory, wemon centronics printer interface, fan, cased, £80. Prefer buyer collects UK101. Tel: Witney (0993) 4890 evenings

● ICOM IC202S £115. FDK multi 700 EX £125. 10GHz FM transceiver with dish X-coupler wavemeter £70. All ono. Ring 0453 833411

● Eddystone receiver 840A very good condition with manual £60. Trio 2200G FM Nicads Charger carrying case £70. Buyer collects. Collectors item 1928 edition Practical Television by Larner forward by John Baid offers G2HKU Trowell 'Hamlyn' Saxon Ave, Minster, Sheerness, Kent. Phone (0795) 873100

● Radio and television servicing books 1974 to 1982 8 volumes mint condition unused cost £172.50 sell £112 inc postage to you Thandar SC110 Scope new in box with re-chargeables and switchables probe X1-X10 cost over £200 £140 inc post. Telephone monitor built & tested £8. Digital multimeter £30 Tel: Durham 719400 evenings/weekends

● Loads of new components for TV Radio etc clearing out due to retirement too much stuff to list send sae 9x6 for free catalogue of all my equipment & spares. 6 Rydal Close, Sacriston, Durham DH7 6DG

● TRS800 level one computer 4k with monitor and tape recorder. All itmes boxed £150 ono Dave Lucas, G6HLQ 62 St Austell Avenue, Macclesfield, Cheshire. SG10 3NN

● VDU keyboard interface unit, with professional quality keyboard, R5232, 64 Char/line, 16 lines, £25. Heathkit H14 line printer, RS232, excellent condition, with manuals, £130. Phone 01-751 2262 after 6pm

● Heathkit model 10-12U laboratory oscilloscope complete with data and construction details etc. Bargain at £35. Telephone Sheffield (0742) 664453

● Xerox Hy-type daisy wheel printer. Full connection details for this very professional unit. £95 Tel: 0272 717424

● Ferrograph series 5 reel to reel tape recorder faulty £25, collect. J-beam six element quad 2-mtr aerial £10, collect. 40 chnl 29 MHz txceiver 4W with mic as new £20, postage £2. Smith, No 1 Barton Drive, Paignton, Devon.

● Exchange Radio Shack for SX200-N and R1000. Shack list FT290R, Nicads, 144/432mm UHF transceiver 2m SmeP/A FM/SSB 25W lin SP400 Welz, Daiwa CN620N, Ae switches many cables HB9CU AE DA1WA search 9RX + UFO, 8A PSU all fits into cabinet, value £760+ bargain of the year.

Ring Sick of Amateur Radio. John 047-385 526 anytime.

● 32k Dynamic ram card, nearly new cond. £25 ono. Industrial F8 system CPU CARD ROM card and V.DU card in frame £25 ono. Wanted Texas 'Speak and Spell', damaged unit considered. Chris S Warwick, 118 Site Field Road, Kings Norton, Birmingham. B38 9JA

● Intel 8086 development system offers WHY several S100 boards including microplis FD controllers wanted 49Hz satellite equipment and micropolis disk drive. Also wanted schematics for spring B+W 310 portable TV — Bridge, 175 Crofton Rd, Orpington, Kent. BR6 0JX

● Sony MX-610 mixer 6 in to 2, mic, line or phono. Turn UK meters, head phone output etc, £50 or exchange for compressor/limiter. MJ Gamley, 4 Walnut Grove, Trowbridge, Wilts. BA14 0HR

● Vernier slow motion drive type D ref 10A/8510 brand new neon power indicator complete set radio communication mags. 1982 variable condenser 1 toggle switch DX. Foreign listings callbook Guy wires brand new Japanese BM3 desk nic, £30 cot absolute bargain pack will sell mic, separate at £15 phone G3XWV 0564 822280 evenings

● 1KW out 432mKZ Linear amplifiers for SSB and CW and ATV contact Geoff Brown Lemnos, Longueville Rd, St Helier, Jersey C1

WANTED

● Manual for Tektronix 502A Dual Beam Oscilloscope. Mr Richard Coull, 113 Westmorland Ave, Luton, Beds, LU3 2PT. Tel: (0582) 581256

● Non Working Transmitters, Receivers or W.H.Y. D.H. de Souza Kirby, 17, Laleham Green, Bramhall, Stockport, SK7 3LJ. Tel: 061 439 2377.

● Eddystone 770U VHF/UHF or AR2001 Receivers. Microwave Modules ATV and 136 MHZ Receive Converters. Will collect reasonable distance. Phone Middlesborough (0642) 318451 after 6pm.

● Light to medium duty aerial rotator for VHF Beam. Tel: Wisbech (0945) 61946

● Radio gear offers in exchange for American Super 8 Cine and Projector. Both zoom. Richard Stacey, 3, Westpark, South Molton, Devon, EX36 4HJ Tel: 07695 3382

● Exchange Kleinshmidt Tele-Printer, Perforator-Transmitter for any TV gear, Test gear, W.H.Y. Phone Mac (G6 PPW) on Mansfield (0623) 640626.

● C B Rig wanted working or not. Please give complete details and price. After 6pm if phoning, can collect if local. R. Moores, 117 Horton Road, Brighton, BN1 7EG Tel: (0273) 503869

● Linear Amp 2 Meter 50-100W Microwave Modules or similar. Also heavy duty Rotator with control box. Phone Dave (Eve only) Cardross (Scotland) 841452

● Up to twenty pounds for a vertical high frequency Aerial. Mr G Nash, 530 Archer Road, Stevenage. Tel: Stevenage 62554

● Circuit Diagram for PSU for 19 set or pin out for DC input lead to 19 set supply unit No 2 (Dynamo Vibrator.) Circuit Diagrams for add ons to Texas T199/4A Computer I E R5232, RTTY, RAM, D.O.S. boards. Also exchange ideas etc with other radio amateur users of T199/4A. M. Austin G6UKP. 15, Bursley Way, Bradwell, Newcastle-U-Lyme, ST5 8JQ Tel: Stoke on Trent 639406

● Members wanted no experience req! Top band and VHF direction finding club. Write Hon. Sec. Dartford D.F. Club, 49 School Lane, Horton Kirby, Dartford, Kent, DA4 9DQ. Subs £3 yr.

● Wanted any information on Mods or Conversions to Murphy B40D receiver. M.F. Turvey, 106 Foxwell Street, Worcester, WR5 2ET.

● Stanford Le Hope and District Amateur Radio Club Welcome new members. Monday nights 2000 at Parish rooms, St Joseph's School, Stanford. Come along and join a friendly club. John Allan (GALTH) 13, Vincent Close, Corringham, Essex, SS17 7QL Tel: Stanford Le Hope 674301

● Wanted Clandestine 'Spy-Set' Radios, A.P.4. A Mk II, 3Mk III, B.P.3. etc Compact or unusual, military surplus Receivers Transmitters. Also, early Amateur Radio Equipment, Short-Wave Receivers up to late thirties. Anything early with values in it considered. W.H.Y. Please Tel: John 01-450 6449.

● Surplus Data Manuals especially Motorola RF Semiconductor Manual. D.Bieber (G4Air QTHR) Sandale Lodge, Rosslyn Lane, Cuddington, Northwich, Cheshire. CW8 2JZ. Tel: 0606 882949

● Wanted any info on servicing ZX81 any reas. expense paid. Wanted Service Sheet for Berry 510 CTV. 1973 Hire Loan? to R. Norean, 67, Wilson Road, Boscombe, Bournemouth, Dorset. 0202 303798.

● Wanted complete E.H.T Unit for Marconi Oscilloscope Model TF1331. Any reasonable price plus carriage. W. Mawson, 8, Elsdon Drive, Forest Hall, Newcastle upon Tyne, NE12 9RH Tel: Newcastle 662082

● Wanted Handbook, Circuit, Diagram, Mods for Belcom Liner Two SSB Transcur copies, loan, purchase, anything considered. Contact John G6UGU 12 Ingram Crescent, Dunscoft, Doncaster. Tel: 0302 841530

● Wanted by desperate enthusiast, a Valve Amplifier using Power Triodes like, PX25, V503, PA40 etc. Also any HIVAC miniature valves for my collection? To Mr N Covington, 25 Ridge Road, Letchworth, Herts SG6 1PW

● THE VALVE SET CLUB. I intend to start a club with a monthly news sheet, with information, for sale, wanted, swap etc. If you would like to contribute or just be a member, please write to me so as I can colate a list of interested people. This hobby (Valve) is growing very fast!. To: Mr N Covington, 25, Ridge Road, Letchworth, Herts, SG6 1PW

● Radio Valves wanted, must be unused. ECC40, EL41, X78, N78, NR44, NR47, CV1040, 6B4G, P27/50, PP5/400, AC/HL, AC2/HL, PX25, PX4, V503, ELL80, ACO44, 12AH8, EL34, UY41, MH4, or what have you? to Mr Covington, 25, Ridge Road, Letchworth, Herts, SG6 1PW. Tel: (04626) 79681

● Wanted FR50B or FRG 7 in good condition. Niall Reilly, 6 Windsor Avenue, Portadown. Phone Portsmouth 333412.

● Wanted: Heath RA1 RX. KW E-ZEE Match. Joystick antenna. Write Marris, 35 Kingswood House, Farnham Road, Slough, Berks.

● Datong Woodpecker Blanka. HF Vertical new condition only. G2HKU Trowell Hamlyn Saxon Ave, Minster Sheerness, Kent. Phone (0795) 873100.

● Eimac SK606 Chimney to complete project. Ediswan B8F base and chimney, UHF type screen bypass capacitor at about 1000PF to start next linear or WHY? QRO VHF UHF bits also 2C39's for 23cm. If you can help phone Alastair G4RUL on (0323) Eastbourne 53618 eves and Sundays only please or QTHR as G6EWL

● Good quality compressor limiter, stereo if possible also any other signal processing equipment. M J Gamley, 4 Walnut Grove, Trowbridge, Wilts. BA14 0HR

● Wanted either Trio TS120V, TS520 or Rascal RA17 with SSB adaptor, as applicable, mike PSU and hand book req'd to: LCPL Booker, 54 Lodge Hill Lane, Rochester, Kent. ME3 8NR

● 4CX250B sockets, type SK620A, SK600, SK610, etc must be new condition. Write CJ41CD, SMC, Belmont Rd, St Helier, Jersey, C1

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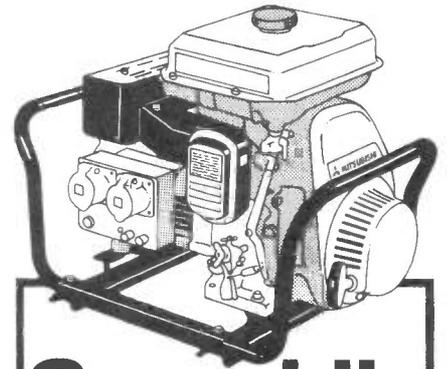
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667125	SOBELL word, and device with a bell	Radio receiving sets, television receiving sets and radio gramophones
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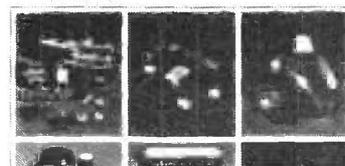
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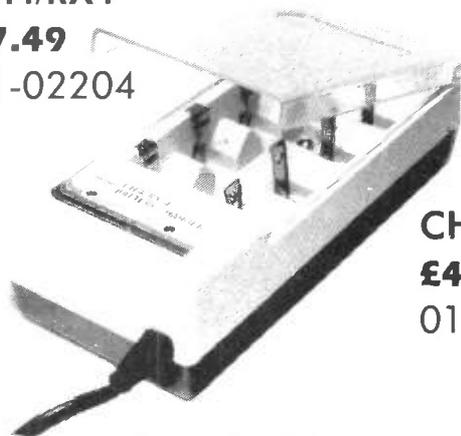
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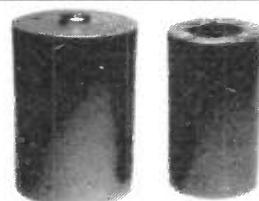
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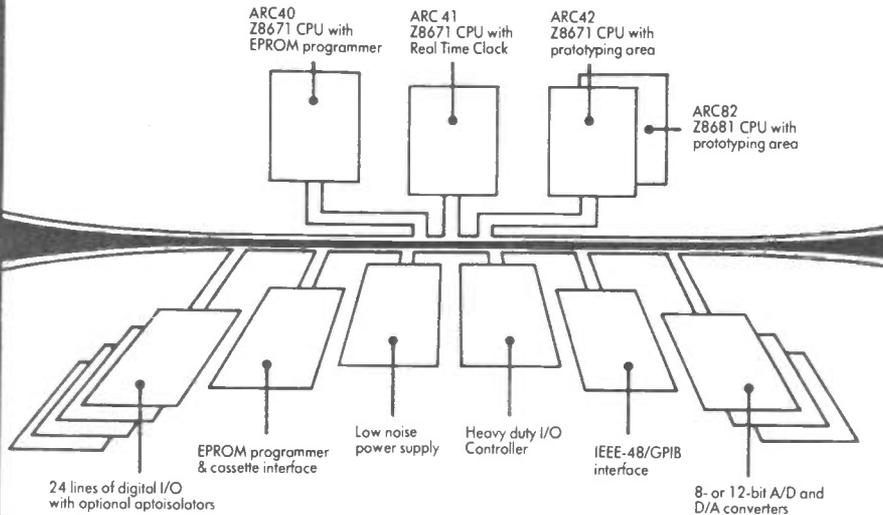
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Radio & Electronics World

The communications, electronics & computers magazine

ADVERTISING RATES & INFORMATION

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depth mm x width mm	ad space	series rates for consecutive insertions			
		1 issue	3 issues	6 issues	12 issues
61 x 90	1/8 page	£91.00	£86.00	£82.00	£73.00
128 x 90 or 61 x 186	1/4 page	£160.00	£150.00	£145.00	£125.00
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issue	colour & mono display ad	small ad	mono artwork	on sale
Jan 84	9 Nov 83*	15 Nov 83*	16 Nov 83*	9 Dec 84
Feb 84	8 Dec 83*	14 Dec 83*	16 Dec 83*	13 Jan 84
Mar 84	12 Jan 84	18 Jan 84	20 Jan 84	10 Feb 84
Apr 84	9 Feb 84	15 Feb 84	17 Feb 84	9 Mar 84

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Previous copy will automatically be repeated if no further copy is received.
A 'hold ad' is acceptable for maintaining your series rate contract. This will automatically be inserted if no further copy is received.
Display Ad and Small Ad series rate contracts are not interchangeable.

If series rate contract is cancelled, the advertiser will be liable to pay the unearned series discount already taken.

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For illustrations just send photograph or artwork.
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Printed – web-offset

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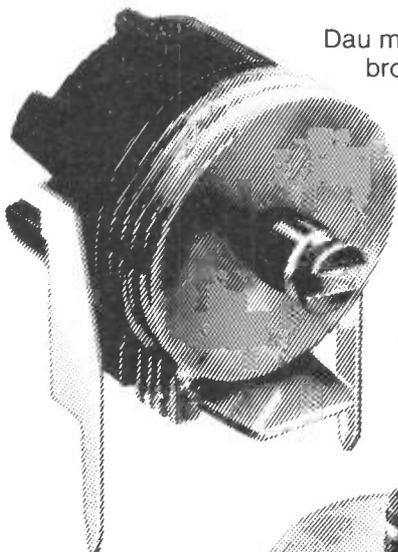
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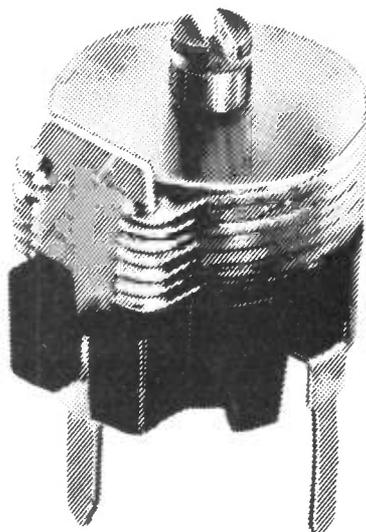
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AP3 AUTOMATIC SPEECH PROCESSOR This kit is a real winner, we have sold hundreds of these since the constructional article in Septembers 'Ham Radio Today'. Ian, G6002 used his AP3 to help him come top of the fixed stations in the Practical Wireless QRP Contest—a real winner indeed! The AP3 Automatic Speech Processor uses a combination of compression and clipping to give a really punchy signal that cuts through the QRM to give you contacts that may not be possible without it.

- * Automatically compensates for changes in speech level
- * Automatic on/off switching from your PTT switch
- * Four switch selectable clipping levels in approx 6db steps.
- * Will run from a 9 volt battery, or your rigs 12 volt supply

Prices: AP3 kit **£14.80**, Assembled PCB **£19.80**.

XM1 CRYSTAL CALIBRATOR—a really useful piece of test equipment, as well as helping to meet those licence requirements. O/Ps: 1MHz, 100KHz, 25KHz & 10KHz. Features include an on-board voltage regulator (i/p 8 to 24V DC) and a pulsed ident facility to identify markers on crowded bands. Usable from Top Band to 70cm. Kit **£15.80**, assembled PCB **£19.80**.

DcRx DIRECT CONVERSION COMMUNICATIONS RECEIVER, single band versions for 20, 30 & 80 meters, modes SSB and CW. We have sold many of these to both beginners and owners of expensive Japanese rigs. They really are amazing! All coils are ready wound. Kit **£13.95**, assembled PCB **£18.90**.

ST2 CW SIDE-TONE/PRACTICE OSCILLATOR. This unit gives a nice sounding sinewave note and will work from your key, or the output of your TX by RF sensing. Output power approx 1 watt at 800Hz. Kit **£6.20** Assembled PCB **£8.90**.

NEW! LINEAR AMPLIFIERS for 2 meters. 15W version for use with up to 1.5W rigs, 30W version for use with up to 4W rigs. Just the job for your FT290, IC202 etc. Kits **£18.90** and **£22.90**, assembled PCB **£22.80** and **£26.90**. A PTT or RF operated TX/RX change over module for use with these linears is available: **CO1 KR £8.90**, assembled PCB, **£11.90**—Yes, there is provision for adding a pre-amp.

All the above are PCB modules and include all board mounted components, a drilled, and tinned fibre-glass PCB with the component locations screen printed on it, and full, detailed instructions. Our instructions are more comprehensive than those used by most of our fellow kit manufacturers.

Please add 60p P&P to your total order value. SAE for more details on any item. Goods are normally in stock and delivery within 7 days, but we sometimes run out of one item or another no matter how hard we try!

73 de Dave G4KQH Technical Manager



ANTENNA

SUPERB 70CMS BAND AERIAL

- ‡ High Gain - 16db
- ‡ Low VSWR - better than 1.2 at 432MHz
- ‡ Wide Bandwidth - greater than 10MHz
- ‡ Low Weight - 1.1kg (wind loading 0.080 sq.metre)
- ‡ British Made throughout
- ‡ 2 years guarantee

ALSO

Superb range of two metre antenna. An essential asset for the serious DX man

High quality 'performance' antenna backed by a full two year's guarantee. Made in England so your valuable pounds don't go abroad into foreign pockets! Full spares availability.

Tiger LY6 £12.95

The economical and portable beam.
6 elements boom length 63.5" weight 0.7 kilo wind load area 0.5 sq.ft. gain 9dbd beamwidth 50° connector S0239 Also in portable form. Complete with clamps and plug shroud.

Tiger LY8 £19.50

For the operator who wants both high performance and compact size.
8 elements boom length 105" weight 0.9 kilo wind load area 0.65 sq.ft. gain 11dbd beam width 38° connector S0239 rigid bracing. Complete with clamps and plug shroud.

Tiger LY10 £32.95

For the discerning DX man who wants only maximum performance at the lowest price!

10 elements boom length 185" weight 1.5 kilo wind load area 1.3 sq.ft. gain 14dbd beamwidth 30° connector S0239 rigid bracing. Complete with clamps and plug shroud.

Delivery by securicor **£4.50 extra**



TIGER

ANTENNA

Ant Products

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and Commercial Aerials supplied

PRODUCT NEWS

design example. This illustrates how appropriate Boolean equations are generated, how the fuse tables are prepared, actual device programming and testing to ensure that the result meets the original design specification.

The booklet is available free of charge from Microsystem Services.

Microsystem Services, PO Box 37, Lincoln Road, Cressex Industrial Estate, High Wycombe, Bucks. HP12 3XJ

NOVEL HANDHELD MULTIMETER

Fluke recently launched a new range of low-cost handheld multimeters which is said to break new ground by having both an analogue and a digital display. The manufacturers believe that this 70 Series should therefore capture a large share of the analogue market, whilst maintaining their place in the digital part of the



market.

The range consists of three fully autoranging models incorporating proprietary CMOS ICs, the only control being an eight-position function switch. The analogue display is a fast-moving 32-segment LCD bargraph and its digital equivalent a 3½-digit LCD display but with 3200 counts and therefore 4½-digit resolution for readings up to 3200. Other advantages

include an estimated 2000-hours battery life and 0.7%/0.5%/0.3% accuracy (depending on the model). The deluxe model also features Touch-Hold which enables the user to concentrate on the test probes rather than continuously watching the display. The Model 77 beeps when it detects a stable reading and then holds that until a new stable reading is detected or the user changes test points.

All models measure DC voltages to 750V, AC voltages to 1kV, current to 10A and resistance to 32MΩ.

Fluke (GB) Ltd, Colonial Way, Watford, Herts. WD24TT

FELD STRENGTH METER

Sadelta's TC40, available from House of Instruments, is designed to measure the performance of aerials in their current location. Its readings will therefore suggest the best position in which to install the aerial.



The signals from the aerial are fed to the TC40's 75Ω coaxial-type input connector, whereupon the meter indicates the RMS voltage and dB's/microvolt on one of seven scales covering 100μV fullscale to 100mV fullscale (lowest reading 20μV). Coarse and fine tuning controls enable Band I TV (45–88MHz), Band II FM (87–108MHz), Band III TV (163–230 MHz) and Bands IV and V TV (470–862MHz) to be fully covered. In addition, there are facilities for audio monitoring of AM and FM, and for

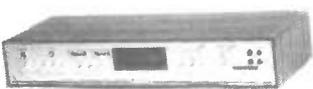
HART

LINSLEY-HOOD 300 SERIES AMPLIFIERS



30 Watt Complete Kit £55.00
35 Watt Complete Kit MosFet O/P £79.50
45 Watt Complete Kit MosFet O/P £93.90
Reprints of 30 Watt Article from 'Hi-Fi News' 50p
Reprints of MosFet Postscript to above 30p

'P.W. WINTON' TUNER AND AMPLIFIER



Tuner, Complete Kit £163.00
Amplifier, Complete Kit £98.00
Amplifier Reprint £1.25

SOLENOID CONTROLLED HI FI/DIGITAL CASSETTE MECHANISM



Front loading deck with full solenoid control of all functions including optional read in fast wind modes. 12 volt operation. Fitted 3-digit memory counter and Hall IC Motion Sensor. Standard erase and stereo R/P Heads. Cheapest price ever for all these features. Only £38.90 plus VAT. Full technical specification included.

LINSLEY-HOOD 100 WATT POWER AMPLIFIER

Our complete kit for this brilliant new design is the same size as our Linsley-Hood Cassette Recorded 2. Kit includes all parts for two power amplifiers with large heatsink area, huge power supply and speaker protection circuit. Total cost of all parts is £114.46 but our special introductory price for all parts bought together is only £105.50.

THIS MONTH'S SPECIAL OFFERS

DOLBY 'B' NOISE REDUCTION IC LM1011
Marvellous opportunity for home experimenters, build your own noise reduction system. Supplied complete with circuit showing typical application. **Absolute knockout price only £3.50 for two inc. VAT and post**

COMPLETE STEREO CASSETTE DECK
Brand new high quality top-loading Cassette Deck complete with Record/Play electronics. Supplied with connection data and circuit diagram. Automatic chrome/ferric switching. Only needs 9v DC supply. **Total price only £18.34 inc. VAT and post**

COMPLETE STEREO TUNER MODULE
Three band LW/MW/FM Stereo Tuner fully assembled on PCB 165 x 85mm. Supplied with Ferrite rod aerial and band switch fully wired. Facility provided to drive tuning meter and stereo LED. Only needs 12v DC supply. FM sensitivity, 2.5uV. **Price only £7.99 inc. VAT and post.**

ALPS FF317U FM FRONT END
Beautiful, precision made High Quality variable capacitor tuned FM Front End with Dual-gate MosFet. The tuning capacitor also has 2-AM Gangs and built-in 3:1 reduction gear. Covers full FM range of 87 to 109 MHz. Supply needed is 12v at only 30mA Max. Inputs are provided for AGC and AFC signals. These have recently been on special offer from another supplier at £4 plus VAT. **OUR PRICE IS ONLY £3.99 INCLUDING VAT AND POSTAGE!** Circuit if required 35p.

HIGH QUALITY REPLACEMENT CASSETTE HEADS



Do your tapes lack treble? A worn head could be the problem. Fitting one of our replacement heads could restore performance to better than new! Standard mountings make fitting easy and our TC1 Test Cassette helps you set the azimuth spot-on. We are the actual importers which means you get the benefit of lower prices for prime parts. Compare us with other suppliers and see! The following is a list of our most popular heads, all are suitable for use on Dolby machines and are ex-stock.

HC20 Permalloy Stereo Head. This is the standard head fitted as original equipment on most decks. £4.25
HM90 High Beta Permalloy Head. A hard-wearing, higher performance head with metal capability. £6.20
HS16 Sandust Alloy Super Head. The best head we can find. Longer life than Permalloy, higher output than Ferrite, fantastic frequency response. £8.20
HQ551 4-Track Head for auto-reverse or quadrophonic use. Full specification record and playback head. £7.40
Please consult our list for technical data on these and other Special Purpose Heads.

HART TRIPLE-PURPOSE TEST CASSETTE TC1

One inexpensive test cassette enables you to set up VU level, head azimuth and tape speed! Invaluable when fitting new heads. Only £3.80 plus VAT and 50p postage.

Tape Head De-magnetiser. Handy size mains operated unit prevents build up of residual head magnetisation causing noise on playback. £3.68
Full details of the entire range of HART products is contained in our illustrated lists.
Ask for your FREE copy NOW.
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In a hurry? A telephone order with credit card number placed before 3pm will be despatched THAT DAY!
Please add part cost of post, packing and insurance as follows:

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Orders up to £10 — 50p
Orders £10 to £49 — £1
Orders over £50 — £1.50

OVERSEAS
Postage at cost plus £2 documentation and handling

PLEASE ADD VAT TO ALL PRICES

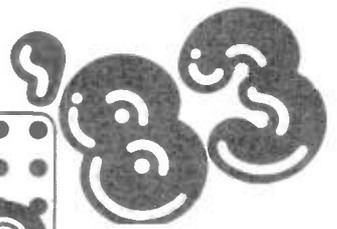
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Personal callers are always very welcome but please note that we are closed all day Saturday



HART

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PENYLLAN MILL
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**If you missed
out on Breadboard
'79, '80, '81 and '82
Now's the time to catch up with**



FRIDAY November 25th	10am – 6pm
SATURDAY November 26th	10am – 6pm
SUNDAY November 27th	10am – 4pm

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We have transferred BREADBOARD to the Cunard Hotel, offering improved facilities to the visitor, including car parking and ease of access by rail, tube and car, all in a modern attractive setting.

Planned Features include

- Lectures: covering aspects of electronics and computing.
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- Holography presentation.
- Practical demonstration: 'How to produce printed circuit boards'.
- Computer Corner – 'Try before you buy'.
- Amateur Radio Action Centre.
- Computer controlled model railway competition.
- Pick of the projects – Demonstration of the best from ELECTRONICS TODAY INTERNATIONAL, HOBBY ELECTRONICS and ELECTRONICS DIGEST.
- Giant TV screen video games.
- Robotic display.

The Breadboard Exhibition is sponsored by Electronics Today International, Hobby Electronics, Electronics Digest and Digital and Micro Electronics

Breadboard '83 ASP Exhibitions 145 Charing Cross Road London WC2H 0EE

PRODUCT NEWS

continuity and short-circuit testing.

The TC40 is both compact and lightweight which, together with its internal power supply of two 4.5V batteries and its carrying case, makes it fully portable.

House of Instruments, Clifton Chambers, 62 High Street, Saffron Walden, Essex. CB10 1EE

EMERGENCY-STOP BUTTON

Quiller Components has added a new push-button switch that could be used as an emergency-stop button to the range of Breter control switches it stocks. The new switch — the M206SR — has a 35mm diameter mushroom head, either a thermoplastic or a metal body and a 'turn to release' action. The use of snap-on contact blocks gives it flexibility in circuit arrangement, while the contact block can also be wired separately from the operator if so required. The contacts are of high



conductivity silver alloy to give resistance to wear.

The switch conforms to all major European and International standards and regulations, and is suitable for use in the control of industrial equipment.

Quiller Components Ltd, 85 Stanley Road, Bournemouth, Dorset. BH1 4SD.

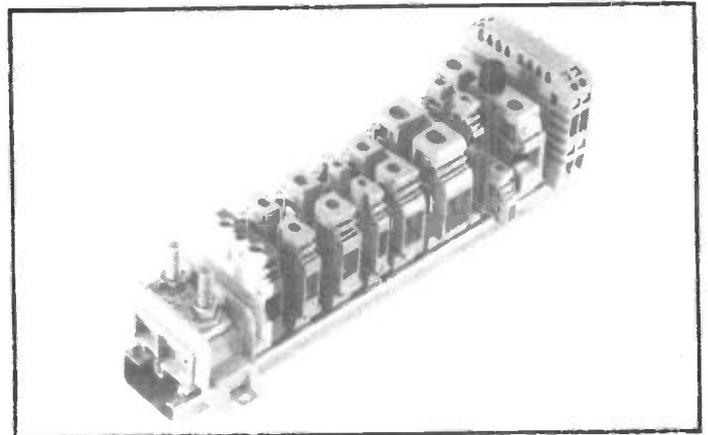
DIN RAIL-MOUNTED TERMINALS

The Entrelec Series 500 range of DIN rail-mounted terminals illustrated here is a recent addition to the Verospeed catalogue. There are five sizes of standard terminals within the range, with nominal current ratings between 35 and 138A, as well as 'fused', 'space-saver' and 'interruptable' types of terminal.

All the terminals fit DIN 1, 2,

3 and Cenelec rails and are manufactured from a material known as super polyimide that gives them a non-brittle and flexible construction over the temperature range -55°C to +130°C. The Series 5000 also features locked-in parts, individual terminal locking and a unique kind of preformed jumper bar.

Verospeed, Stansted Road, Boyatt Wood, Eastleigh, Hants. SO5 4ZY



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Now, **73: Amateur Radio's Technical Journal** is available to the readers of *Radio & Electronics World* at a special introductory rate of under £17.

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73: Amateur Radio's Technical Journal PO Box 931, Farmingdale, NY 11737, USA.

73DRRE

Offer expires on February 29, 1984.

SWITCHES
Toggle: 2 A, 250 V
SPST 35p
DPDT 48p

SUB-MINI TOGGLE
SPST on/off 54p
SPDT c/over 80p
SPDT c/over off 85p
SPDT biased both 105p
ways 105p
DPDT 6 tags 75p
DPDT centre off 88p
DPDT biased both 110p
DPDT 14 145p
DPDT 3 positions on/off 185p
3-pole 2-way 205p

SLIDE 250 V
DPDT 1 A 14p
DPDT 1 A c/off 15p
DPDT 1/2 A 13p

PUSHBUTTON 6 A
with 10 mm Button
SPDT latching 110p
DPDT latching 160p
SPDT moment 110p
DPDT moment 145p

Mini Non Locking
Push to Make 15p
Push to Break 25p

DIL SWITCHES
(SPST) 4 way 65p 6 way 80p
8 way 85p 10 way 100p
(SPDT) 4 way 190p.

ROTARY SWITCHES:
(Adjustable Stop type)
1 pole/2 to 12 way; 2 pole/2 to 6 way;
3 pole/2 to 4 way; 4 pole/2 to 3 way 48p

ROTARY: Mains DP 250V 4 Amp on/off 68p

ROTARY: (Make & switch)
Make a multi-way switch. Shifting assembly stop Accommodates up to 6 wafers (max 6 pole/12 way - OP switch) Mechanism only 90p

WAFERS: (make before break) to fit the above switch mechanism
1 pole/12 way; 2 pole/6 way; 3 pole/4 way; 4 pole/3 way; 6-12 way
Mains DP 4 A Switch to fit Spacers 4p. Screen 5p

ROCKER 5A/250V SPST 28p
ROCKER 10A/250V SPST 38p
ROCKER 10A/250V DPST c/off 98p
ROCKER 10A/250V DPST with neon 85p

THUMBWHEEL
Mini front mounting
Decade Switch Module 25p
8 C.D. Switch Module 275p
Mounting Clips (per pair) 75p

VEROBARD D 1in
clad plain
2 1/2 x 3 1/2 85p
2 1/2 x 5" 100p
3 1/2 x 3 1/2 100p
3 1/2 x 5" 115p
3 1/2 x 17" 198p
4 1/2 x 17" 495p 275p
Pkt. of 100 pins 55p
Spot face cutter 150p
Pin insertion tool 185p

PROTO DECS
Veroblock 405p
S-Dec 350p
Euroboard 520p
Bimboard 1 575p
Superstrip SS2 1350p

DALD ETCH
RESIST PEN 100p
Plus spare tip

ULTRASONIC TRANSDUCER
40 kHz 350p

VERO WIRING
PEN + spool 340p
Spare spool 75p
Combs 8p

FERRIC CHLORIDE
1 lb bag Anhydrous 195p
- 50p P&P

ICD CONNECTORS
PCB Plugs
Male Header
Female Header
Card Edge Connect

10 way 80p 85p 120p
16 way 130p 150p 110p
20 way 145p 160p 125p 195p
26 way 175p 200p 180p 240p
34 way 205p 230p 180p 320p
40 way 220p 250p 190p 340p
50 way 235p 270p 200p 395p
80 way 270p 320p 495p

PANEL METERS
F80
80 x 46 x 35mm
0-50
0-100A
0-500A
0-1mA
0-5mA
0-10mA
0-50mA
0-100mA
0-500mA
0-1A
0-2A
0-2.5V
0-50V AC
0-300V AC
"S"
"VU"
425p each

RELAYS
Miniature, enclosed, PCB mount.
SINGLE POLE Changeover
RL6-91 205 Ohm Coil; 12 V DC (10V5 to 19.5V); 10 A at 30V DC or 250 V AC 185p

DOUBLE POLE Changeover: 6 A
30 V DC or 250 V AC
RL6-100 53 Ohm Coil; 6 V DC (5V4 to 9V8) 190p
RL6-111 205 Ohm Coil; 12 V DC (10V7 to 19.5V) 195p
RL6-114 740 Ohm Coil; 24 V DC (22 V to 37 V) 200p

ELEKTOR PROJECTS
We stock most of the parts



JUMPER LEADS (Ribbon Cable Assembly)
Length 14 pin 16 pin 24 pin 40 pin
Single ended DIP (Header Plug) Jumper
24 inches 145p 165p 240p 380p
6 inches 185p 205p 300p 465p
12 inches 198p 215p 315p 490p
24 inches 210p 235p 345p 540p
36 inches 230p 250p 375p 595p

1DC Female Header Socket Jumper Leads 36"
Single ended 20p 20p 34p 40p
Double ended 180p 200p 280p 300p
480p 525p

COPPER CLAD BOARDS
Fibre Single Double S.R.B.P.
glass sided sided 9.5" x R 8"
6" x 6" 100p 125p 110p
8" x 12" 175p 225p

DIL SOCKETS
Low Wire Prof Wrap
8pin 8p 25p
14pin 10p 35p
16pin 10p 42p
18pin 16p 52p
20pin 20p 80p
22pin 22p 65p
24pin 25p 70p
28pin 28p 80p
40pin 30p 95p

EURO CONNECTORS
Female Socket Male Plug
Strt. Angle Strt. Angle
Pins Pins Pins Pins

DIN41617 31way 170p - - 175p
DIN41612 2x32 A+B 275p 320p 220p 285p
DIN41612 2x32 A+C 295p 340p 240p 300p
DIN41612 3x32 A+B+C 360p 385p 260p 395p

CRYSTALS
32.768KHz 100
100KHz 236
200KHz 260
455.5KHz 370
1MHz 275
1.008M 275
1.28MHz 362
2.048MHz 362
1.8MHz 335
1.8432M 226
2.0MHz 226
2.4576M 298
3.2768M 150
3.5794M 98
3.6864M 300
4.0MHz 150
4.032MHz 290
4.8032M 200
4.194304M 175
4.433619M 100
5.0MHz 160
5.185MHz 300
5.24288M 380
6.0MHz 140
6.144MHz 150
6.5536MHz 225
7.0MHz 160
7.168MHz 250
7.68MHz 200
8.0MHz 160
8.08333M 385
8.5M 230
9.0MHz 175
9.000MHz 150
10.0MHz 175
10.24MHz 200
10.278M 175
10.2MHz 175
12.528M 300
14.31814M 170
16.0MHz 200
18.0MHz 180
18.432MHz 200
20.0MHz 200
19.968MHz 150
24.0MHz 170
24.930MHz 325
28.5M 175
27.648M 170
27.145M 190
38.66667M 176
100.0MHz 170
116.0MHz 250

AMPHENOL PLUG
24way IEEE 10C Solder
36way Centronics 525p 485p

ASTEC UHF MODULATORS
6 MHz Standard 325p
8 MHz Wideband 450p

BUZZERS, miniature solid-state
6V 9V & 12V 70p

PIEZO TRANSDUCERS
PB270 55p

LOUDSPEAKERS
Miniature, 0.3W 8Ω
2in. 3in. 2 1/2in. 3in.
2 1/2in. 40Ω, 64Ω or 80Ω 80p

TRANSFORMERS
3.0-3V, 6.0-6V, 9.0-9V, 12.0-12V, 15.0-15V
@ 100 mA 98p

pcb mounting, Miniature, Split Bobbin
3VA: 2x6V 0.25A; 2x9V 0.15A; 2x12V 0.12A
2x15V 0.1A
6VA: 2x6V 0.5A; 2x9V 0.3A; 2x12V 0.25A;
2x15V 0.2A 270p

Standard Split Bobbin type
6VA: 2x6V 0.5A; 2x9V 0.4A; 2x12V 0.3A;
2x15V 0.25A 250p
12VA: 2x4.5V 1.3A; 2x6V 1A; 2x9V 0.6A;
2x12V 0.5A; 2x15V 0.4A; 2x20V 0.3A
325p (35p p&p)

24VA: 2x6V 1.5A; 2x9V 1.2A; 2x12V 1A;
2x15V 0.8A; 2x20V 0.6A 365p (60p p&p)

50VA: 2x6V 4A; 2x9V 2.5A; 2x12V 2A; 2x15V 1.5A; 2x20V 1.2A; 2x25V 1A; 2x30V 0.8A
465p (60p p&p)

Specialty wound for Multirail Copiers PSUs
50VA Outputs +5V/5A, +12V, -25V, -5V,
12V at 1A 575p (60p p&p)

100VA: 2x12V 4A; 2x15V 3A; 2x20V 2.5A;
2x25V 2A; 2x30V 1.5A; 2x50V 1A 920p (75p
p&p charge to be added over and above our normal postal charge)

VOLTAGE REGULATORS
1A TO220 Plastic Casing
+ve -ve
5V 7805 40p 7905 45p
12V 7812 40p 7908 40p
15V 7815 40p 7912 45p
18V 7818 40p 7915 45p
24V 7824 40p 7918 45p
7924 45p

100mA TO92 Plastic package
5V 78L05 30p 79L05 50p
6V 78L06 30p -
8V 78L08 30p -
12V 78L12 30p 79L12 50p
15V 78L15 30p 79L15 50p

ICL7660 248p TAA550 50p
LM309 135p TDA1412 120p
LM317K 250p 78H05 +5V/5A 550p
LM317KP 99p 78H12 +12V/5A 640p
LM323K 450p 6x4 x 3" 180p
LM337 175p 78HG +5V to +25V 10x4 x 3" 240p
LM723 Var 30p 5A 10x7 x 3" 260p
RC4194 375p 79HG +2.25V to 24V 12x5 x 3" 280p
RC4195 160p 8A 12x8 x 3" 235p

EDGE CONNECTORS
2 x 18 way 180p
2 x 22 way 195p
2 x 23 way 175p
2 x 25 way 225p
2 x 28 way 190p
2 x 30 way 245p
2 x 36 way 295p
2 x 40 way 315p
2 x 43 way 395p
2 x 43 way 350p
2 x 75 way 550p

SIL SOCKETS
495p
525p
525p
225p
175p

RIBBON CABLE
price per foot
Grey Color
10 way 15p 28p
15 way 25p 40p
20 way 30p 50p
24 way 40p 65p
34 way 60p 85p
40 way 70p 90p
60 way 85p 110p
64 way 100p 135p

'D' CONNECTORS miniature
9 15 25 37
MALE way way way way
Angle pins 80p 105p 160p 250p
Angle pins 150p 210p 250p 365p
PCB pins 120p 130p 195p 295p
FEMALE
Solder lugs 105p 160p 200p 335p
Angle pins 165p 215p 290p 440p
PCB pins 150p 180p 240p 420p
COVERS 85p 80p 80p 100p
100 pins 385p
1DC 25way 'D' Plug Socket 450p

MONITORS
●ZENITH - 12" Green, Hi-Resolution Popular: £ 75
●MICROVITEC 1431 14" Colour RGB input. Connecting cable incl. £ 250
●KAGA 12" Med-Res. RGB Colour. Has flicker-free character. Ideal for BBC, Apple, VIC, etc. £ 219 (car. 7)
●KAGA 12" As above but Hi-Res. Colour interface or can be used as a stand alone typewriter. As typewriter, it has a built in timing function to measure the operator's speed making it ideal for teaching or proofing jobs correctly. Friction feed, 11 CPS, 12" max width, 5 different colour ribbons. Portable. Supplied complete with hard cover carrying case. £ 259 (car. 7)
●Connecting Lead for KAGA £ 5

TRANSFORMERS
3.0-3V, 6.0-6V, 9.0-9V, 12.0-12V, 15.0-15V
@ 100 mA 98p

pcb mounting, Miniature, Split Bobbin
3VA: 2x6V 0.25A; 2x9V 0.15A; 2x12V 0.12A
2x15V 0.1A
6VA: 2x6V 0.5A; 2x9V 0.3A; 2x12V 0.25A;
2x15V 0.2A 270p

Standard Split Bobbin type
6VA: 2x6V 0.5A; 2x9V 0.4A; 2x12V 0.3A;
2x15V 0.25A 250p
12VA: 2x4.5V 1.3A; 2x6V 1A; 2x9V 0.6A;
2x12V 0.5A; 2x15V 0.4A; 2x20V 0.3A
325p (35p p&p)

24VA: 2x6V 1.5A; 2x9V 1.2A; 2x12V 1A;
2x15V 0.8A; 2x20V 0.6A 365p (60p p&p)

50VA: 2x6V 4A; 2x9V 2.5A; 2x12V 2A; 2x15V 1.5A; 2x20V 1.2A; 2x25V 1A; 2x30V 0.8A
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2x25V 2A; 2x30V 1.5A; 2x50V 1A 920p (75p
p&p charge to be added over and above our normal postal charge)

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+ve -ve
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12V 7812 40p 7908 40p
15V 7815 40p 7912 45p
18V 7818 40p 7915 45p
24V 7824 40p 7918 45p
7924 45p

100mA TO92 Plastic package
5V 78L05 30p 79L05 50p
6V 78L06 30p -
8V 78L08 30p -
12V 78L12 30p 79L12 50p
15V 78L15 30p 79L15 50p

ICL7660 248p TAA550 50p
LM309 135p TDA1412 120p
LM317K 250p 78H05 +5V/5A 550p
LM317KP 99p 78H12 +12V/5A 640p
LM323K 450p 6x4 x 3" 180p
LM337 175p 78HG +5V to +25V 10x4 x 3" 240p
LM723 Var 30p 5A 10x7 x 3" 260p
RC4194 375p 79HG +2.25V to 24V 12x5 x 3" 280p
RC4195 160p 8A 12x8 x 3" 235p

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5 x 4 x 2 1/2" 120p
5 1/2 x 1 1/2" 80p
5 1/2 x 2 1/2" 120p
6 x 4 x 2" 130p
6 x 4 x 3" 150p
6 x 4 x 3 1/2" 180p
8 x 6 x 3" 210p
10 x 4 x 3" 240p
10 x 7 x 3" 260p
12 x 5 x 3" 280p
12 x 8 x 3" 235p

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Angle pins 150p 210p 250p 365p
PCB pins 120p 130p 195p 295p
FEMALE
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Angle pins 165p 215p 290p 440p
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4007	15	4082	50	4553	246
4008	32	4083	50	4554	246
4009	24	4086	80	4556	36
4010	24	4089	125	4556	36
4011	15	4093	20	4557	320
4012	18	4094	70	4558	120
4013	20	4095	85	4559	396
4014	46	4096	70	4560	160
4015	40	4097	280	4561	104
4016	20	4098	75	4562	496
4017	32	4099	110	4566	165
4018	46	4100	85	4568	250
4019	25	4161	39	4569	175
4020	42	4162	39	4572	36
4021	40	4163	39	4580	480
4022	40	4164	39	4581	260
4023	15	4175	105	4582	99
4024	32	4194	105	4583	99
4025	16	4408	790	4584	40
4026	80	4409	790	4585	60
4027	20	4410	790	4586	320
4028	39	4411	675	4599	290
4029	45	4412	775	40085	90
4030	15	4415	480	40097	45
4031	125	4419	280	40098	62
4032	80	4422	770	40102	215
4033	125	4440	980	40101	130
4034	140	4435	860	40104	95
4035	46	4450	360	40103	175
4036	276	4451	360	40105	105
4037	116	4490	670	40106	35
4038	110	4500	350	40107	80
4039	250	4501	28	40108	198
4040	40	4502	80	40109	80
4041	40	4503	40	40110	225
4042	40	4504	75	40114	240
4043	40	4505	185	40181	194
4044	40	4506	35	40163	60
4045	105	4507	35	40174	45
4046	48	4508	130	40175	50
4047	40	4510	46	40181	220
4048	40	4511	46	40182	90
4049	25	4512	40	40192	75
4050	25	4513	198	40193	70
4051	45	4514	115	40194	70
4052	80	4515	115	40195	75
4053	80	4516	85	40196	196
4054	85	4517	275	40245	196
4055	85	4518	40	40257	196
4056	85	4519	30	40373	160
4057	1915	4520	60	40374	160
4059	435	4521	90	45106	590
4060	46	4522	125		
4061	1195	4526	70		
4062	80	4527	95		
4063	85	4528	95		
4066	24	4529	150		
4067	245	4530	90		
4068	18	4531	130		
4069	18	4532	70		
4070	18	4533	40		
4071	20	4536	275	25677	45
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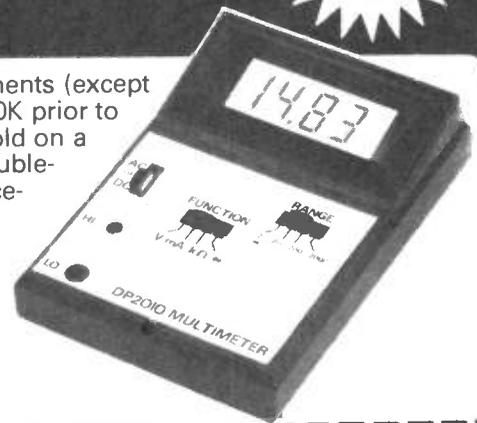
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	200V			200mA	4% ±5 digit
	500V			2000mA	12% ±5 digit
Current (d.c.)	2mA	1% ±1 digit	Resistance	2k	1% ±1 digit
	20mA			20k	1% ±1 digit
	200mA			200k	1% ±1 digit
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	200V				
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LETTERS to the EDITOR

Do you have an opinion to air? Do you know the answer to something which puzzles, or a tip that might help, fellow enthusiasts? Have you something to add to a feature or review?

Your letters are invaluable in helping us to develop the magazine for you
Write to Letters to the Editor, **Radio & Electronics World**, Sovereign House, Brentwood, Essex, CM14 4SE. £2 will be paid for each letter published

Improvements

Referring to the letter in *R&EW* (September '83) from Mr Dudley of Guildford and the Editor's reply, here are some improvements made to the Cybernet 134 board in my 'Oscar' rig.

Oscillator Buffer: Two versions of the following circuit (*Figure 1*) were made up on pieces of veroboard and inserted in the oscillator outputs to both the 1st and 2nd mixers, to provide a buffer against the effects of oscillator blocking.

It was found that as the input to the 1st mixer is a balanced type, the circuit used here gave best results at a quiescent current of about 4.5mA. Using this value for direct injection into the base of the second mixer proved too much, so the current was dropped to about 1.8mA: hence the two sets of resistor values. Positive voltage is taken from the ON/OFF switch, and R3 is used to drop the excess voltage, decoupled by C1.

Both circuits were soldered to convenient RF/IF coil cans using the earth tracks. This method not only provides an earth return but also mechanical stability.

Links J13 and J15 are removed and the holes used for the buffer's input/output connections.

Two Pole Crystal Filter: Matching the 10MO8AA 10.695MHz crystal filter turned out to be a matter of assumption. It was assumed that the input/output impe-

dance of the ceramic filter was 300R, and that the output of T9 and the input to Q10 were matched to this impedance. The following resistive potential divider circuit (*Figure 2*) was used to match the 1k8 impedance of the crystal filter.

The circuit can be made up on a small piece of veroboard and the same mounting method used as for the oscillator buffer. Connections can be made using the holes left by the removal of the ceramic filter, or using the holes left by removing link J14. A link between the first and third holes of the original filter position would then have to be made.

Not having the appropriate equipment to take quantitative measurements, all RF/IF coils were peaked for maximum S-meter reading, and a listening test carried out. There appeared to be no degradation in audio quality, and instead of losing the signal completely to

oscillator blocking effects, it now just drops by an 'S' point or two, even on very strong off-channel transmissions. Cross modulation effects (sorry — third order IMD) are also way down on what they were.

All in all a vast improvement for a moderate cost, and well worth the effort involved. In fact the rig now compares favourably with the Magpie Autoscan 5000, which I have had pleasure in listening to.

RF Millington, Cheltenham

Satellite prediction

Following on from the recent articles in *R&EW* about polar orbiting satellites, I thought readers who own a 16K ZX81 personal computer might be interested in the orbit-prediction program presented herewith.

The program, when fed with reference orbit data of a polar satellite, will give accurate predictions for about one month ahead with orbit number, date, time and longitude west at which the satellite crosses the Equator. The writer of this program ran it for more than a year and was well satisfied with its accuracy and troublefree performance.

Some explanations about the logic employed should prove helpful to those readers wishing to try the program, particularly if they envisage making changes to it later to fit specific needs. These follow:

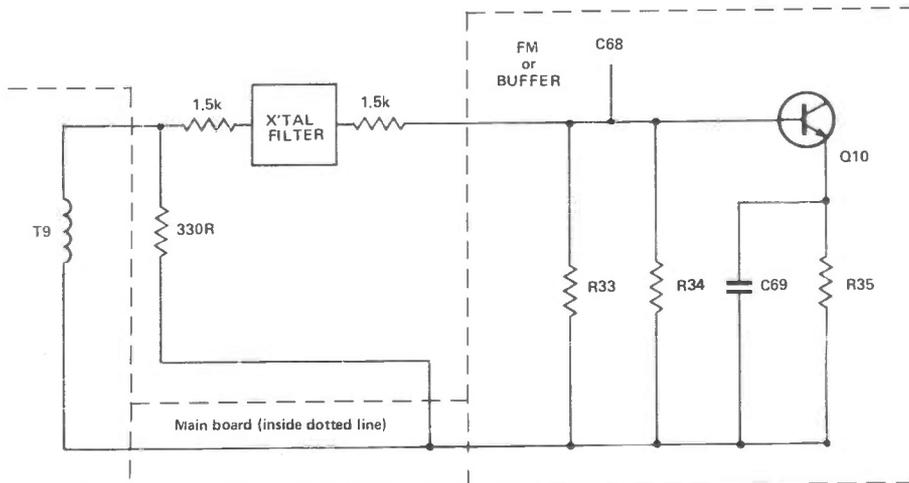
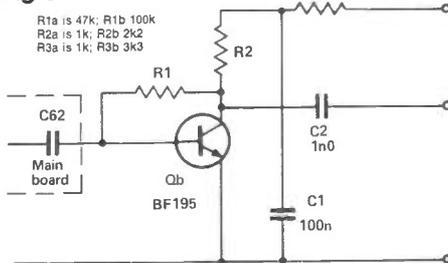
Lines 40-230 feed the computer with reference orbit parameters. These parameters usually can be found in Radio Amateur magazines such as QST (for the OSCAR satellites in particular) or can be requested from the National Oceanic and Atmospheric Administration in the US in the case of the NOAA 7 and 8 weather fax satellites.

Lines 290-320 arrange the way the expected data will be displayed and printed.

Lines 340-570 instruct the computer how to calculate the exact orbit number, date, time and longitude west at which the satellite crosses the Equator.

Depending on the particular location of the user, he should add the time the satellite will need to reach his location after crossing the Equator (the satellite speed is approximately 3.5° per minute).

Fig 1



```

10 REM WRITTEN BY
11 REM ARGYRIS ADAMIDIS
20 REM SATELLITE ORBIT PREDICT
30 REM PROGRAM
40 REM SATELLITE DATA
50 PRINT "1. INPUT NAME OF SATE
LLITE (EG, NOAA 7)"
60 INPUT N$
70 PRINT "2. INPUT REF. ORBIT NU
MBER (EG, 3075)"
80 INPUT O
90 PRINT "3. INPUT DAY OF REF. O
RBIT (EG, 1)"
100 INPUT D
110 PRINT "4. INPUT MONTH OF REF
. ORBIT (EG, 4)"
120 INPUT M
130 PRINT "5. INPUT YEAR (EG, 1982)"
140 INPUT Y
150 PRINT "6. INPUT HRS TIME OF
REF. ORBIT (EG, 1)"
160 INPUT H
170 PRINT "7. INPUT MINUTES TIME
OF REF. ORBIT (EG, 12.50)"
180 INPUT I
190 PRINT "8. INPUT U. LONGITUDE
OF REF. ORBIT (EG, 155.11)"
200 INPUT J
210 PRINT "9. INPUT LONGIT. INCRE
MENT PER ORBIT IN DEGREES (EG, 35.
5100)"
220 INPUT K
230 PRINT "10. INPUT ORBIT PERIO
D IN MINUTES (EG, 102.0810)"
240 INPUT P
250 CLS
260 PRINT TAB 12; N$
270 PRINT
280 PRINT
290 PRINT TAB 0; "DATE"; TAB 5; "O
RBIT"; TAB 12; "EQX TIME"; TAB 24; "
U. LONGIT."
300 PRINT
310 PRINT TAB 0; "D/M"; TAB 5; "N
O"; TAB 12; "H"; TAB 24; "
DEGREES"
320 PRINT
330 PRINT
340 LET A=A+P
350 GOSUB 4100
360 IF A>=60 THEN LET H=H+1
370 IF A>=60 THEN LET M=M+60
380 IF A>=60 THEN GOTO 360
390 IF M>=60 THEN LET D=D+1
400 IF M>=60 THEN LET H=H+24
410 GOSUB 3000
420 REM EQX LONGITUDE CALC
430 LET L=L+I
440 GOSUB 5100
450 IF L>=360 THEN LET L=L-360
460 IF L<=0 THEN GOTO 450
470 LET O=O+1
480 IF O>=30 THEN PRINT TAB 8; D; TR
A 2; " "; TAB 3; H; TAB 5; O; TAB 12; M
490 GOTO 340
500 REM DAYS OF MONTH CALC
510 IF M=1 OR M=3 OR M=5 OR M=7
OR M=8 OR M=10 OR M=12 AND D>=31
THEN GOTO 300
520 IF M=4 OR M=6 OR M=9 OR M=1
1 AND D>=30 THEN GOTO 300
530 IF M=2 THEN GOTO 3100
540 IF D>=31 THEN LET M=M+1
550 IF D>=31 THEN LET D=D-31
560 RETURN
570 IF D>=30 THEN LET M=M+1
580 IF D>=30 THEN LET D=D-30
590 RETURN
600 REM DAYS OF FEBR. CALC. FOR
FEBRUARY YEAR
610 LET Z=Y/4
620 IF Z-INT(Z)=0 THEN LET X=2
630 IF Z-INT(Z)>0 THEN LET X=
25
640 IF D>X THEN LET M=M+1
650 IF D>X THEN LET D=D-X
660 RETURN
670 REM TIME AND LONGITUDE ROUN
D OFF
680 LET A=(INT(10000*(A+.00005
))) / 10000
690 RETURN
700 LET L=(INT(10000*(L+.00005
))) / 10000
710 RETURN
7200 RETURN

```

NOAA 7					
DATE D/M	ORBIT NO	EQX TIME H MIN (GMT)	U. LONGIT DEGREES		
1	-6	4837	2	34.1547	177.76
1	-6	4842	11	4.1762	305.26
1	-6	4843	12	45.1209	330.76
1	-6	4844	14	28.1176	355.26
1	-6	4850	05	43.3558	149.76
1	-6	4851	05	43.0805	174.06
1	-6	4855	10	52.054	307.76
1	-6	4857	10	34.0467	327.26
1	-6	4858	14	15.0434	353.26
1	-6	4864	09	48.0116	148.76
1	-6	4865	09	48.0853	171.76
1	-6	4871	10	31.9745	324.76
1	-6	4872	14	3.9892	358.26
1	-6	4875	09	15.0374	143.26
1	-6	4879	1	57.3221	163.76
1	-6	4885	13	51.895	347.26

Sample of the printed data

The way forward

In the Editorial in the October '83 issue of R&EW, we challenged our readers to come up with suggestions as to how they would create wealth and employment, using new technology as a catalyst. **John de Rivaz of Truro took up our challenge, and we present his ideas here.**

The problems of today are due to insufficient creation of wealth, a situation accentuated through the way the profits of manufacturing, construction and other such wealth-creating industries are consistently reduced through vast sums of money being paid to people who create no wealth at all, for example, chartered accountants. Members of these professions are on a kind of chain-letter rip-off: they write laws that other members of this elite get paid £100 per hour or so to interpret to lesser mortals. For instance, the solicitors' and estate agents' bills associated with moving house are comparable with the cost of a colour TV with a VCR to go with it. And it is impossible for manufacturing industry — or the general public — to avoid paying out for these services, directly or indirectly, which pushes up the price of manufactured goods; and so it continues.

Inflating the currency is no solution as this only pushes the debt into the future. Moreover, these problems cannot be solved through more governmental control: as Hitler demonstrated, extreme forms of control only bring disaster. Indeed, various Acts of Parliament have themselves added considerably to the overheads to be borne by industry.

A possible way that new technology could ease matters is through being

more substantially incorporated into the production of essential consumer goods, instead of just those designed for entertainment such as televisions, video cassette recorders, hi-fi and computers. As the prices of the latter group have been steadily falling over the past few years, surely the technology employed here can be incorporated in the manufacturing procedures of such equipment as washing machines, the quality of which has not increased in line with their cost!

Unfortunately, this would probably just put pressure on those self-same manufacturing industries that are already suffering from the bureaucracy problems mentioned above.

Perhaps a better solution is to ask that the new technology be used to make machines that self-employed people could use to make these essential consumer goods. In that case, not only would the production costs themselves be so much cheaper but so would the overheads. There would be nothing to pay either in time or money, in travelling to work nor would there be great cost in distribution or advertising as each person's market would be close to home.

Moreover, such an arrangement would do a lot for the self-esteem and general satisfaction of each worker, their time would be their own and there would be no bosses or trade unions to order them about. In addition, the automatic nature of the processes used would give these people plenty of spare time. How much better their lot than that of the present factory worker! To cap it all, this scheme should provide increased employment at reduced costs.

A present example of this basic idea is given by the home computer with its owner earning money by writing and selling programs. Unfortunately, these generally — at least, so far — have had purely an entertainment value.

In essence, what is suggested is that, instead of designing another entertainment product to replace the VCR once that market has been saturated, the same technology be used to design a wealth-creating product. Considering that VCRs find their way into homes other than those of the very rich, surely the latter product could similarly find its way into such homes and start creating wealth for us all.

At the writer's location, for instance, (Thessaloniki, Northern Greece), it will take five minutes for the satellite to travel the distance between the Equator and the southern edge of the Mediterranean Sea, which is when the satellite signal can first be heard. This is valid for the ascending node in the evening, when the satellite moves from south to north.

The program provides information on a selected group of orbits every day. This limitation is essential if one wants to save time and printer paper. With the parameters given to this program (line 530), the predicted orbits cover the area from the Caspian Sea to Gibraltar and from the Mediterranean coasts of Africa to the North Sea. Of course, these parameters can be changed to fit requirements of other areas of the world.

The subroutines in lines 3000-3800 arrange for the changing number of days in each month (including February), while lines 4000-5100 round off the long decimals of times and longitudes.

Argyris Adamidis, Thessaloniki

MICRO MANIA

Your editorial in R&EW in October has prompted me to produce the following verse on the subject of Technology.

As I travel life's great computer buss,
I ask myself what's all this fuss?
My watch plays tunes and entertains,
The fridge and cooker rack their brains,
The washing machine beats me at chess,
While washing out my new string vest.

My car tells me the tyres are thin,
It phones the garage to book me in,
I cannot go to work this way,
It thinks that it will snow today.

My summer holiday in Corfu
Is booked and cancelled by VDU,
The Great God IT is in control:
That's what we are told when on the dole.
The bills arrive and don't get paid,
The bank's computer is badly made.

At work my terminal greets me with a grin,
'You're late again, please log in'.
The day's work is neatly planned,
I must learn to type with either hand.
The jobs around us disappear,
The people cry out in doubt and fear:
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HPF1 HIGH PASS FILTER & BRAID BREAKER General Purpose	Rejection – Inner>60dB @30MHz & below Outer>15dB @30MHz & below Insertion loss<2dB Useable to 200MHz Limited use to 400MHz	£6.32	BB1 BRAID BREAKER	Braid rejection – >25dB @ 30MHz & below Insertion loss <2dB	£6.32
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INSIDE THE SINCLAIR FLAT TV

Rod Greenaway presents an inside view of the flat screen pocket TV project

In a hotbed of innovation and dynamic new technology such as exists at Sinclair Research, the rule about information is 'Need to Know'. In other words, the various participants in the project tend only to know what is pertinent to their specific participation in the design. At least, that was the excuse given when the questioning got too intense at the press launch.

There obviously must be some managers who possess a general overview, or the radiated output from the line hold circuit could serve to obliterate the RF input to the tuner among other such minor disasters. The net result of the development (estimates range between 5 and 6 years and between 4 and 5 million pounds) is the most magnificent piece of all-British consumer technology since Sinclair's last effort with the Spectrum. The man is a veritable one-man national face-saver, working against some pretty daunting odds in terms of our national attitude towards people who want to spend money developing high technology products.

The innovative technology of the set itself breaks down (forgive me) into two major features: the tube and the chip. There is, as you can see from *Photo 1*, little else to it other than a couple of TOKO 10P coils (these people really know what they are doing), and a disturbingly large number of presets which I am advised are actually 'not a problem' in production. The interior view presented in the photograph is dominated by the flat tube, so we'll start our technical appreciation there.

Down the tubes

The problem when designing a tube with a side entry electron beam is really quite simple and does not involve rewriting the laws of physics. You just

need to bend the beam a bit harder, that's all. The tubes in use in the prototypes on show are remarkably similar to those first leaked to the press and appearing in features as long ago as summer 1981.

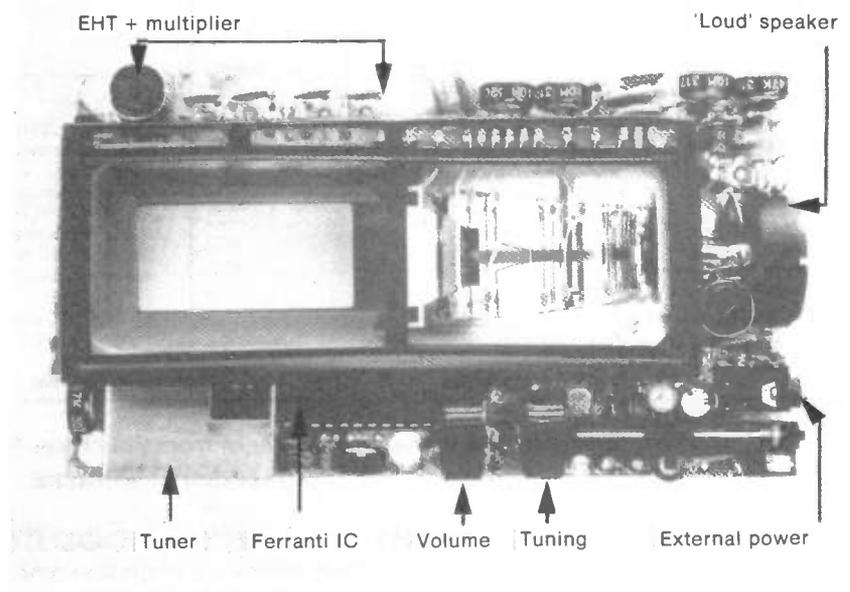
The actual receiver itself isn't much like that proposed on the cover of *Radio-Electronics* back in 1981 (*Photo 2*). This 'kite' was quite widely flown with a projected price of \$100 (check), but including VHF FM radio (definite pass) and VHF TV (pass so far). The tube is one of the most 'sensitive' areas of the design, being subject to many patents and much secrecy. Nevertheless, it's fairly obvious how the basic principle works with two sets of electrostatic deflection plates in the gun assembly to provide the horizontal and vertical

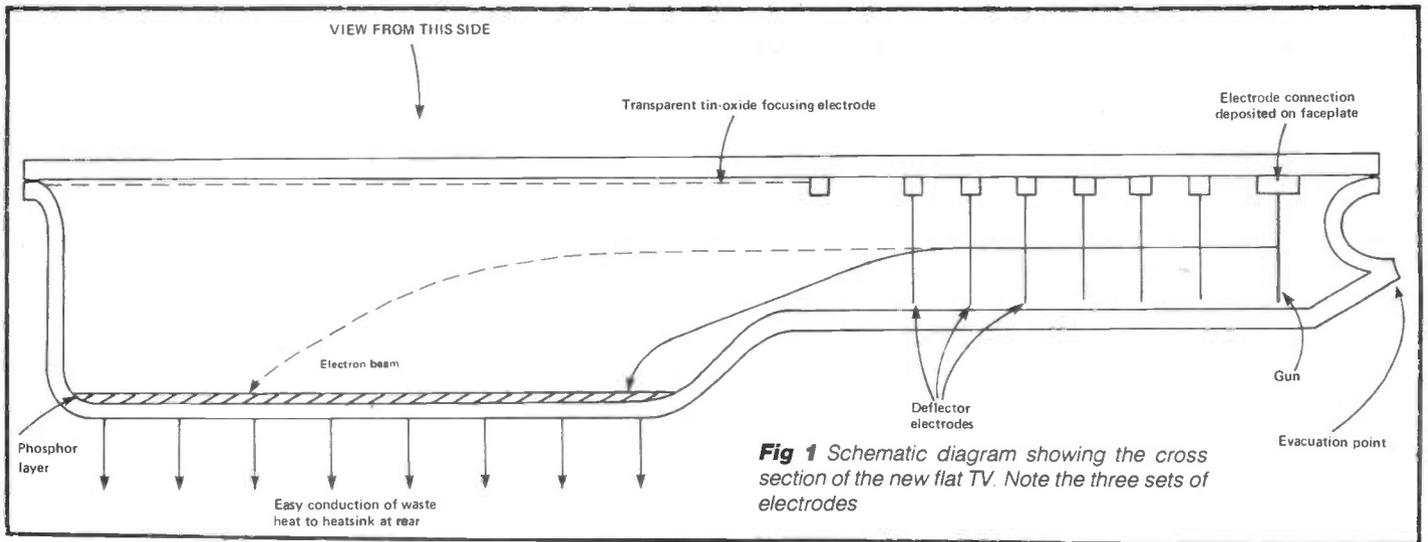
scanning, and a third set between the phosphor screen and the front face (a transparent tin oxide coating on the latter acts as the focusing electrode) — see *Figure 1*. This third set provides focusing by preventing the angle of incidence of the electron beam spreading into an ellipse at the edges of the tube.

The information supplied by Sinclair states that 'If uncorrected, folding the electron optics would distort the raster scan to produce a keystone-shaped frame, in which the vertical edges are curved and the horizontal edges form the side of a trapezium. Both electronic and optical techniques are used to correct for this distortion'.

When is a 2" TV screen not a 2" TV

Photo 1





screen? It would seem that the answer is slightly vexed in that the Sinclair set uses an optical magnification/correction process prior to that dimension being measured. This aspect is potentially as tricky as the 'when is RAM not RAM' argument that has caught up with many of the personal computer makers.

The aspect ratio of the tube phosphor area shown in the internal photograph (*Photo 1*) is nothing like that of a conventional TV tube. In fact, it's only about two thirds the height, and the correction is applied using a Fresnel screen built into the faceplate. The reason for using this approach is to simplify the problems of distortion and power consumption arising from scanning an electron beam too far off the gun axis. No specific side effects (pardon the pun) are apparent to the viewer, and most viewers will never actually notice the effect.

The trapezium distortion is corrected electronically via the waveform used to scan the vertical plates — more of which anon when we come to look into the IC.

Constructing the tube is one of the

project's major technical problems/achievements since it involves a vacuum-formed backplate with a flat front plate on which the electrode connections are screen printed (much as in an LCD). The art of spreading the phosphor evenly across the display area, coupled with trimming the glass and frit sealing the electron gun and deflection assemblies, is one that has taken a lot of time and money to perfect — and it must be said that it is yet to be proven to the satisfaction of us cynics that the yield rate is acceptable.

Is it idle to speculate that a good many of these specific problems are likely to have been encountered by fluorescent display makers such as Futaba and Itron? If so, just how long will it take them to perform a passable emulation of the present technology? Let's hope Sir Clive has employed a sound patent agent.

The NRDC has stumped up around £1 million of the stake money for the tube project, which has been used to install a manufacturing facility at Timex's Dundee factory. This would appear to mean business, and it is to be hoped that other applications of the tube and its technology will emerge: not the least of which is likely to be instrument displays. Who said 'oscilloscope'?

Chips from Chadderton

They make chips in Oldham that are nothing to do with mushypeas. Whilst the Ferranti custom device process is not the most sophisticated in terms of the capability of CAD for interactive design and emulation, the flat TV project was not deflected from pursuing this line of development. The suitability of the CDI (collector diffusion integration) process to an application that mixed high frequency linear and TV logic with scanning functions seems unequalled — especially in view of the low power involved. And, by thunder, it's British.

Peering out from the gloom beneath the tube in the photo, you may be able to make out the presence of the Ferranti IC. Reference to the block diagram (*Figure 2*) supplied with the launch information reveals what goes on therein. This receiver is one of the first examples of genuinely single-device TV sets. A Motorola development we mentioned in *R&EW* some months ago does nearly as much (at the expense of greater power consumption) but it certainly doesn't provide automatic sound IF selection, nor the field correction DAC that provides the necessary tweak to the scanning waveforms to accommodate the tube requirements.

Listed amongst the IC's special features are 'integrated sound selectivity, video innovations to eliminate image problems in the UHF channel, and an advanced synthesised scan generator to control the complex waveforms needed



Photo 2 The Microvision 2700, Sinclair's earlier kite in the world of flat TV

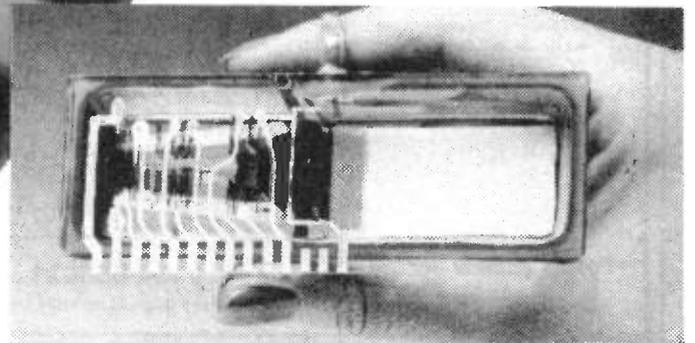


Photo 3 Internal view of the Microvision 2700

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R4	4 0305	8 0611	12 0916	15 0000	18 1375	45 0000
R5	4 0319	8 0638	12 0958	15 0055	18 1437	45 0156
R7	4 0326	8 0652	12 0979	15 0083	18 1468	45 0250
S8	—	—	12 1000	14 9444	18 1500	44 8333*
S9	—	—	12 1020	14 9472	18 1531	44 8416*
S10	—	—	12 1041	14 9500	18 1562	44 8500*
S11	4 0354	8 0708	12 1062	14 9572	18 1593	44 8583
S12	—	—	12 1083	14 9555	18 1625	44 8666*
S13	—	—	12 1104	14 9583	18 1656	44 8750*
S14	—	—	12 1145	14 9638	18 1718	44 8916*
S15	—	—	12 1145	14 9638	18 1718	44 8916*
S16	—	—	12 1167	14 9667	18 1750	44 9000*
S17	—	—	12 1187	14 9694	18 1781	44 9083*
S18	—	—	12 1208	14 9722	18 1812	44 9166*
S19	—	—	12 1229	14 9750	18 1843	44 9250*
S20	4 0416	8 0833	12 1250	14 9777	18 1875	44 9333
S21	4 0423	8 0847	12 1270	14 9805	18 1906	44 9416
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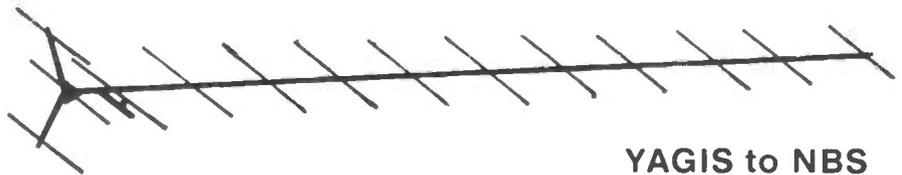
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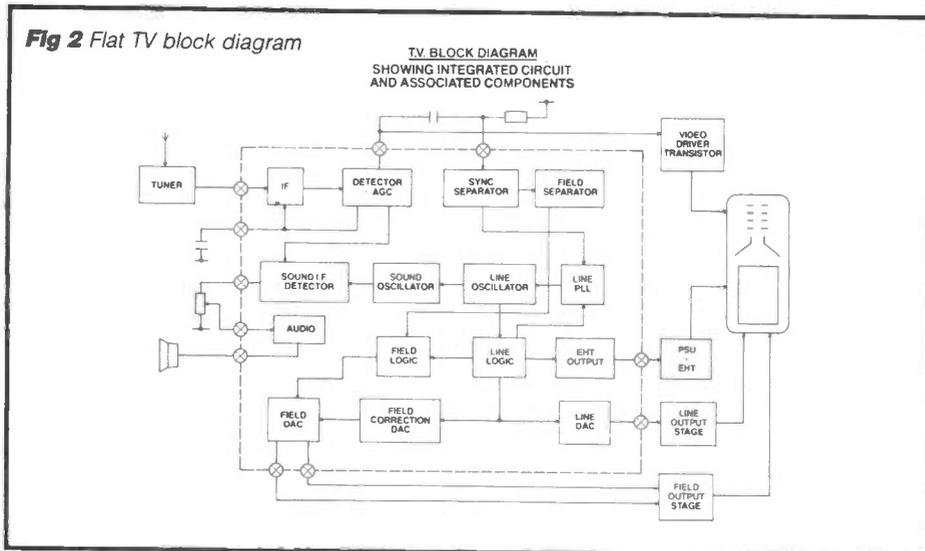
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Fig 2 Flat TV block diagram



to scan the flat CRT. It runs a check 50 times per second to ensure picture hold'. All coupling, decoupling and phase shift networks are integrated on the chip.

The really nifty aspect of the IC is its ability to select the local sound IF standard by looking at the line rate. This piece of innovation was being explored long ago in the days when the Sinclair HQ was still the Mill in St Ives and it's nice to see a practical application emerge that works so effectively. The technique is deceptively simple, since with 625-line transmissions the sound IF is either 5.5MHz or 6MHz, so mixing the intercarrier FM signal with 5.75MHz (derived from the line oscillator — see Figure 2) always gives a difference frequency of 250kHz. Neat stuff.

When the set discovers 525 lines are being received then the sound VCO is switched to 4.75MHz as $4.75 - 4.5 = 250\text{kHz}$ again. No clue was given by the literature (or personnel) supplied as to the technique used on the 250kHz IF, but this is likely to be reminiscent of the pulse counting techniques exploited in the erstwhile Sinclair Micro FM receiver.

The Ferranti wonderchip, then, may have gone over the top and spoilt itself through attempting to provide a viable sound output stage on top of everything else. If you thought the sound output from the original Microvision was rather mean, then have a listen to this one. The 'loud' speaker (pictured towards the right edge of the PCB on axis with the

tube centre) is not adequate. Old cynics like me who have had experience of multifarious ICs that do everything, including class AB output and putting the cat out, wonder if the current fluctuations on volume peaks have caused the same impossible on-chip power supply decoupling problems that have sunk many a lesser project. Watch these pages for a Sinclair TV combined NiCad battery pack, charger and sound booster project!

The Noise Abatement Society should endorse this product as it is unlikely to upset the tranquillity of the average Sunday afternoon on Brighton's promenade.

Synthesised scanning

The major technical problem in trying to present an orthogonal picture on the flat tube was in generating scan waveforms that compensated for the differing path lengths travelled by the electron beam. It could be done by analogue techniques, but only in a way that required vast setting-up complexities and additional circuitry and power.

The Ferranti ZN401E device uses a high frequency VCO that is locked to a multiple of the received line sync pulses to provide both standard 'recognition' and a single master clock source for the entire set. The VCO centre frequency is set by a single external resistor and is counted down to the field rate. On-chip logic determines reception of a 625- or

525-line picture, setting the count number and VCO accordingly. Noise immunity of the field and line lock is aided by additional on-chip processing.

DACs (digital to analogue converters) derive line scan, field sweeps and correction signals from the countdown system. It must be assumed (hoped?) that the tubes are sufficiently repeatable that these waveforms do not require tweaking on test.

Tuning

The tuner lives in the small screened box to the left of the Ferranti IC. It uses printed line techniques, varicap control and surface mounted components for compactness. It is not generously dimensioned in the UHF-only version, so heaven knows how tight the VHF/UHF model will be. The UHF model uses the relatively high IF frequency of 230MHz (it's a good job CB never went so high as far as this project is concerned).

Quite why the IF is 'up there' is not obvious from the words supplied by Sinclair, but perhaps we can speculate that the rule of 'the higher the frequency, the easier it is to produce compact LC filters, came into play and, in this case, the trade off between Q and signal image still leaves a performance worthy of comparison with the usual alternative of 39MHz. It may also have something to do with the possibility of up-converting the lower VHF bands. Sinclair wouldn't let on.

To tune 45MHz to 900MHz in the combined VHF/UHF version is good fun indeed. Sir Clive's own words were that it would be using a single range tuner, in which case up-conversion to 1GHz and a SAW device would appear to be on the cards. Maybe there's some very innovative thinking going on in Cambridge at this moment.

The set uses a four-stage AGC controlled amplifier at 230MHz, and implies from the literature supplied that this is actually in the Ferranti IC. Video detection uses a 'novel low level envelope detector' with no sign of any tuned circuit in sight. Hmmm. Shades of the coil-less radio devices described in October's R&EW.

It will be interesting to see if Ferranti is persuaded to put any of this experience to work in other radio and communications circuitry. It's about time it followed up the ZN414.

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POOR MAN'S SPECTRUM ANALYSER - Part 2

The second part of this feature, based on an article written by Frank Perkins in Wayne Green's '73' magazine, describes the testing and alignment of this spectrum analyser and illustrates its performance

TESTING AND ALIGNMENT

The minimum test equipment needed to align and test the HF spectrum analyser includes a high-impedance volt ohmmeter, a 350MHz frequency counter, and a 5MHz bandwidth, single-channel, DC-coupled oscilloscope with a triggered sweep. A grid-dip oscillator is also useful. You should make up several two-foot RG-58 cables with BNC connectors. These will be used during testing. For best results, testing and alignment should be done in the order listed below.

Power supply testing

Check the resistance between primary and secondary of the wallplug transformer before use. It should show an open circuit. Check the secondary AC voltage. It should be 12VAC to 15VAC with no load. Hook the 12VAC to the power supply and check the 12VDC, 24VDC, and -6VDC outputs. They should be within 0.5V.

Sweep generator testing

Connect the power supply to the sweep generator and turn the power supply on. Check pin 2 of the 555 IC with your oscilloscope. You should find a 10-12Hz ramp waveform. The bottom of the waveform should be at 4V and the top of the waveform at 8V. The front of the ramp (log slope) should appear straight. You should find a similar ramp at the X-axis output connector. This ramp will be between -0.6V and 3.4V.

Check pin 8 of the TLO84C op-amp. You should find a pulse train with a 10-12Hz repetition rate. The pulse train should be high (20V) about 20% of the time and low (-3V) about 80% of the time.

Turn the frequency-span pot fully clockwise (no ramp) and set the centre-frequency pot mid-range. You should find 6-12VDC on pin 7 of the TLO84C op-amp (VCO-tuning voltage). Vary the setting of the centre-frequency pot. The VCO-tuning voltage should vary from -3V to 21V. Set the centre-frequency pot for a 10V output. Turn the frequency-span pot counter-clockwise until you have a ramp waveform from 2V to 20V (re-adjust the centre-frequency pot as needed). This completes preliminary sweep generator testing.

If your sweep generator fails to act as above, re-check component values and circuit hook-up for problems. Refer to the section on the theory of operation (*November issue of R&EW*) for additional hints.

VCO testing

Connect the VCO-tuning voltage from the sweep generator to the VCO. Ground the RG-58 shield at the VCO enclosure. Connect 12VDC from the power supply to the VCO power input. Disconnect one side of the oscillator coil for a moment. Power up and check the MRF901 (KV1210) collector voltage. It should be about 6-8VDC. If it is too high, reduce the value of the 100k bias resistor; if it is too low, increase the value of the bias resistor. You can't use a pot here! Once the collector voltage is verified, power down and reconnect the coil.

Power up and connect your counter to the VCO RF test jack. Turn the frequency-span pot fully clockwise (no ramp) and adjust the centre-frequency pot for a 3V output. Your counter should

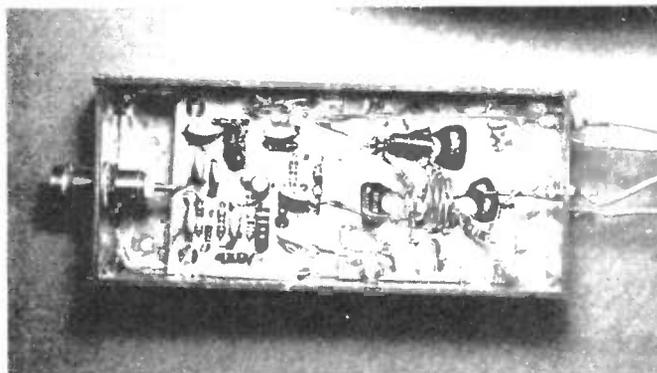
read about 90MHz. Adjust the VCO coil spacing to get the VCO in the 89.5-90.5MHz range. Check the DC output from the RF detector of the VCO amplifier output for a 0.8-1.3VDC level. Adjust the spacing between the VCO coil and the amplifier pick-up loop, if necessary, to obtain the proper detector output.

Set the centre-frequency pot for a 150MHz oscillator output. You should have a tuning voltage of about 18VDC. Check the RF detector output voltage again to be sure it's still between 0.8 and 1.3VDC. Monitoring the DC voltage from the RF detector with your scope, tune the centre-frequency pot back and forth between 3V and 18V. The detector output voltage may vary a little but smoothly; it certainly should not 'jump'. An abrupt voltage change indicates a parasitic oscillation. If this should occur, work on your oscillator layout (aiming for very short leads in particular) to get rid of it.

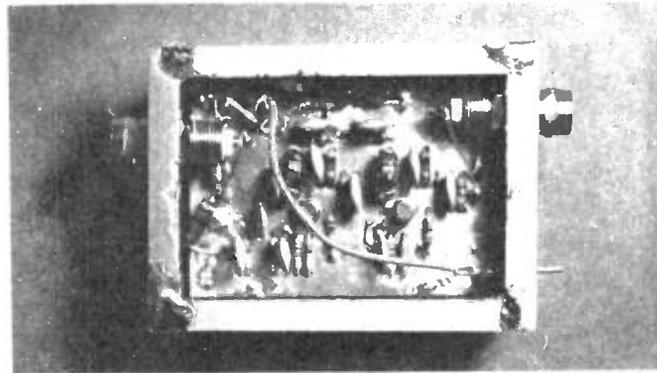
A tuning voltage of less than 1V may cause the oscillator output to be erratic in frequency and amplitude. This is not a problem. Once the VCO oscillator and amplifier are operating properly, install the VCO enclosure top.

Pre-amplifier and Log Amplifier Testing

Connect 12VDC to the pre-amplifier and log amplifier circuits and power up. Turn the frequency-span pot fully clockwise (ramp off) and adjust the centre-frequency pot for 90MHz at the VCO RF test jack. Disconnect the frequency counter. Hook the attenuator box to the VCO RF test jack with a two-foot RG-58 cable. Hook the output of the attenuator



VCO layout



Pre-amplifier layout

to the input of the pre-amplifier with another two-foot cable.

Set the bias pot on the log amplifier about mid-range. Monitor the DC output of the RF detector on the log amplifier buffer. Tune the buffer transformer slug for peak output. Use the attenuator to set the detector output to 0.2Vdc. Now adjust the bias pot of the log amplifier for peak output. Adjust the attenuator for a just-detectable output at the log amplifier buffer. If all seems well with the pre-amplifier, install the top on its enclosure. Prepare the top for the log amplifier section. Drill 1/8-inch-diameter holes in the top over each IF transformer location and over the bias pot. (Use drafting vellum as a template.)

Hook the oscilloscope to the video output of the log amplifier. Adjust the slugs in each log amplifier stage for peak video output. The tuning of each stage should be smooth, and the tuning of the bias pot should also be smooth. If the video output from the log amplifier jumps suddenly whilst tuning, you may have self-oscillation in the log amplifier. If this happens, work on your layout. Ferrite beads, extra bypass capacitors, and small copper shim stock shields can be used to eliminate the problem.

If you live near a commercial FM station, it may interfere with your tuning efforts. Tape the shield top on the log amplifier during initial tuning to help reduce this problem. As soon as it appears that the log amplifier is working, solder on the top. Once the top is soldered on, it will totally eliminate the interference.

BANDPASS FILTER TUNING

Set the VCO to 90MHz. Hook the attenuator between the VCO RF test jack and the bandpass filter input. Hook the bandpass filter output to the pre-amplifier and log amplifier. Monitor the video output of the log amplifier on your oscilloscope. With the tops off the bandpass sections, you should get some signal. If not, temporarily bridge the input and output sections with a 1pF capacitor tack-soldered at the input and output tap points. Tune the input and output stages for peak response; then remove the 1pF capacitor. Now peak the two middle stages. You probably will get an overcoupled response (double-hump). Just centre the tuning between the humps.

Now install the shield tops, one at a time. Tune all bandpass stages after

Specifications for HF Spectrum Analyzer

Frequency range	0 to 60 MHz
3-dB bandwidth	220 kHz
30-dB bandwidth	1,100 kHz
3:30-dB shape factor	1:5
Dynamic range	60 dB
Spurious responses	60 dB below full-scale
Noise floor	65 dB below full-scale
Full-scale input	- 8 dBm \pm 2 dBm
Y-axis output	0 to 2.5 volts
X-axis output	- 0.5 to + 3.5 volts
Y-axis calibration	10 dB/division
X-axis calibration	6 MHz/division (approximate)
	4 MHz \pm 0.75 MHz/division
	8 MHz \pm 1 MHz/division
	6 MHz \pm 1 MHz/division

each top is installed. Tuning will become very sharp, especially if you are using air-variable tuning capacitors instead of piston trimmers. When the last top is installed, carefully peak all stages.

Set up your oscilloscope for X-Y operation, using the X-axis output of the sweep generator for the oscilloscope horizontal input and the log amplifier video output for the vertical input. Gradually turn the frequency-span control counter-clockwise until you get a sweep display of the filter bandpass. Make fine adjustments for a smooth bandpass shape. Stagger-tune the two middle bandpass filter sections just a bit to sharpen the nose of the filter. Be sure to put in enough attenuation to keep the video output from the log amplifier under 2V during the bandpass filter tuning procedure.

If it seems that you have an overcoupled response in your filter, narrow the aperture between the two middle bandpass filter sections. If the filter tunes sharply but exhibits high loss, then widen the aperture between the two middle sections.

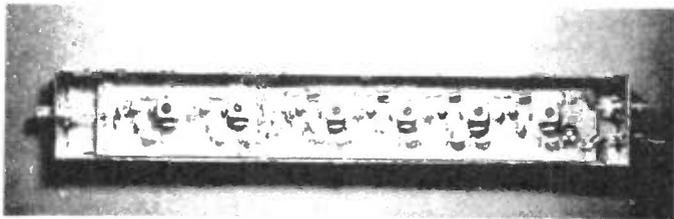
FINAL SET-UP

Install all circuitry on your chassis and complete all wiring and coaxial cable hook-up. Set the analyser upside down in

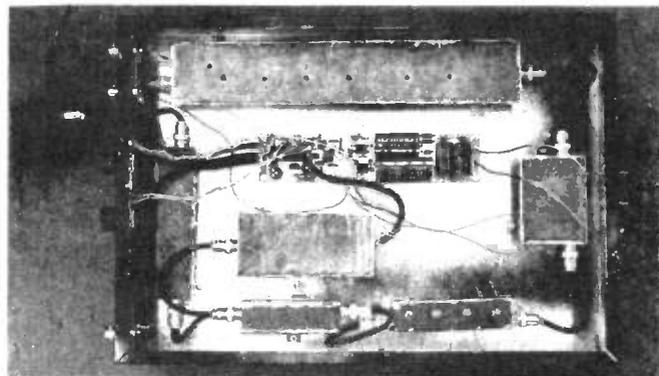
front of your scope. Connect your oscilloscope to the analyser X- and Y-axis outputs. Set up the oscilloscope again for X-Y operation. Turn the analyser on (no signal). Turn the frequency-span pot fully clockwise (no ramp). Using your frequency counter, adjust the VCO for 90MHz operation with the centre-frequency pot. You should see two horizontal lines about 2V apart. Rotate the frequency-span pot counter-clockwise a little. You should see the bandpass-filter response again. This is due to mixer leak-through and is normal.

Set the retrace line (lower straight line) under the bandpass response curve at the bottom of the CRT screen. Widen the trace with the oscilloscope controls to reach across the screen. Turn the frequency-span pot fully clockwise again. Set the VCO frequency to 120MHz. Now turn the span pot counter-clockwise until the zero-frequency half-spike appears on the left side of the screen. There should also be some grass above the retrace line along the bottom on the screen. The analyser should now be scanning 0-60MHz.

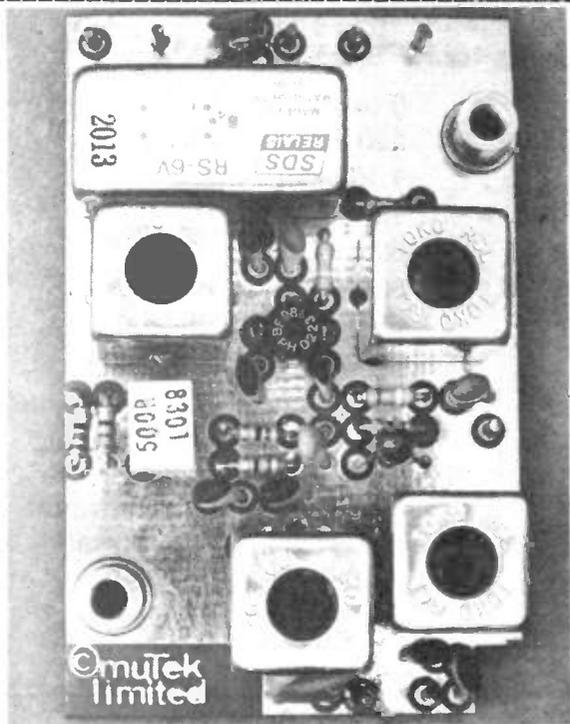
Feed a small 30MHz signal from a grid-dip oscillator (use a pick-up loop as shown in *Photo 1*) or a low-power-signal generator through the attenuator to the analyser. You should now see the 30MHz



Above: Log amplifier layout



Right: Bottom view of spectrum analyser chassis



Bigger Ears Than Dumbo!

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There are usually two reasons for the less than adequate sensitivity of current 144MHz transceivers. Firstly, the receiver designer's brief includes a dynamic range specification which leads him to balance large signal handling with sensitivity. With devices currently available at prices the transceiver manufacturer is prepared to pay, the balance comes-out to around 4dB noise figure and 70dB intermodulation-free dynamic range in ssb bandwidths.

The second point is that, also to save money, designers shy away from the use of electromechanical relays for antenna change-over switching and tend to use various forms of diode switch. These inevitably introduce greater insertion losses than suitable relays, approaching 4dB in some circumstances. Thus it's not unusual for the overall noise figure of a transceiver to reach 8dB.

At 144MHz sky-noise limits the maximum usable sensitivity of a receiver used for terrestrial communications to about 2dB noise-figure. (This about the same as 0.05 μ V for 10dB s+n/n in ssb bandwidths). Lower noise figures are easily obtainable with modern devices, but they won't let you hear any more! However there is a distinct advantage in using a very low-noise preamp to improve the sensitivity of a transceiver — if it has been designed properly.

Overall (or system) noise-figure depends not only upon the noise figure of the preamplifier, but also on its gain and the noise figure of the subsequent stage (the transceiver, in this case). By adjusting the gain of the preamplifier it is possible to set the system noise-figure to any wanted value greater than that of the intrinsic noise figure of the preamplifier.

Why bother to adjust the gain? Because any preamplifier will degrade the strong-signal performance of the receiving system. The name of the game is to use as little gain as possible ahead of the receiver; just enough low-noise gain to set the overall sensitivity to a level where external noise is the limiting factor is all that is required. Use any more and the dynamic performance of the receiver will suffer unduly. A very low noise preamplifier will minimise the gain needed ahead of the transceiver and hence the degradation of the dynamics.

The SLNA 145sb is a preamplifier which has been designed using the principles summarised above specifically for incorporation in the FT290. It will also complement other 144MHz transceivers for which no complete front-end modification is available. Ask us about FDK 700's and 750's for example.

A low-loss nitrogen-filled relay provides a same alternative to diode switching. This is followed by a BF981 in an input noise-matched, output conjugately matched configuration for a very low noise-figure and optimum dynamic performance. Following the output matching a variable attenuator provides gain control without compromising the dynamic performance, which would be the case if the normal amateur practice of providing gain control by varying the bias on G_2 of the BF 981 was followed.

After the attenuator, a properly designed Butterworth bandpass filter provides substantial rejection of out-of-band signals.

The preamplifier is constructed and tested to very high standards. A plated-through-hole epoxy fibreglass pcb is employed and bushed mountings are provided for mounting in the FT 290R. A cable kit utilising high quality ptfе dielectric cables is also provided.

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signal spike about mid-screen. You may also see the 2nd harmonic of the 30MHz signal on the right edge of the screen. Adjust the attenuator so that the 30MHz signal is about the same height as the zero-frequency half-spike. If things have gone well so far, you are getting a signal through the low-pass filter and mixer, so you can now install their enclosure tops.

Set the frequency-span control so that the 30MHz signal spike is about two scope divisions wide. Now fine-tune the bandpass filter again and re-peak the log amplifier. Switch the 10dB attenuator section in and out whilst adjusting the vertical gain of the oscilloscope so that the signal height changes one CRT division. Now switch a 20dB section in and out. The signal height should change by two CRT divisions. Re-adjust the frequency span control for a 0–60MHz analyser tuning range.

Increase the signal strength until the first small spike pops out of the grass between the 0 and 30MHz signals. This is slightly above the overload point of the analyser. The 30MHz signal spike should be near the top of the CRT screen (8th vertical division). Full-scale inputs should be the next (7th) CRT division down. Touch up the oscilloscope controls if necessary. The zero-frequency half-spike will be about six divisions tall. Switch all attenuation out and reduce the signal generator output so that the 30MHz test signal is seven divisions tall. Check the vertical calibration of the analyser over the attenuator's 59dB range.

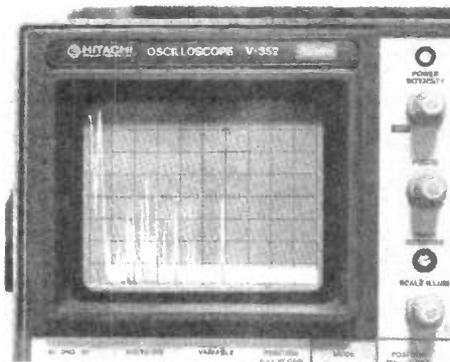
Using your signal generator and frequency counter, make notes on the horizontal calibration of your analyser. This is done by centring a signal from your signal generator on each CRT horizontal division (vertical line) and recording its frequency. Your analyser is now ready for use. But first, test the L-pad carefully!

Hook up your L-pad to your transmitting equipment. Be sure everything is grounded properly. The author suggests mounting the L-pad and attenuator on an aluminium plate which is in turn wall-mounted. Ground the plate! Do not connect the attenuator to the L-pad yet. Connect your transmitter to an SWR meter, the SWR meter to the L-pad and the L-pad to your dummy load. The L-pad should introduce little, if any, SWR. Starting with low power (100W or less), apply power for 30sec. Power down your transmitter completely and quickly inspect the inside of your L-pad. The 'fuse' should be OK and nothing should be hot. Continue testing to full station power.

If everything has gone well, then power down your transmitter completely and connect the attenuator to the L-pad. Switch in all attenuation and connect the attenuator to the spectrum analyser. Remember that the analyser and the oscilloscope cases should be solidly grounded. Starting again with low power, apply power and adjust the attenuator for a full-scale spectrum analyser display. How does your spectrum look? Always switch in full attenuation before increasing power. Remember, do not go over

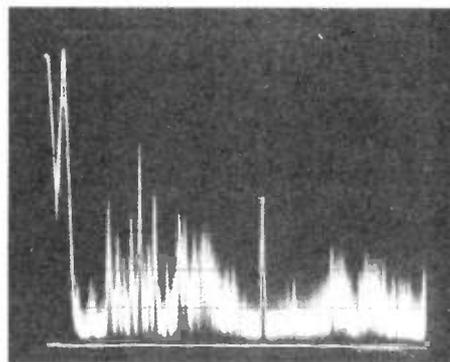


Left: The finished spectrum analyser



Below left: 0–60 MHz spectrum taken from a long wire antenna

Below right: The same but with an adjacent computer turned on



1kW continuous output (2kW p–p). Do not attempt to use the spectrum analyser system where your SWR is greater than 2:1. Be sure you are using an L-sampler with a high enough power rating!

COMPONENT SOURCES AND SUBSTITUTIONS

It often is lamented that home-brewing projects is difficult these days because of poor component availability. The author started seriously experimenting with electronics 20 years ago in the good old days of component availability. The difference between now and then is that we have about a thousand times more components to experiment with!

It's simply a matter of motivation and tenacity. You can get any component that you need. True, the local TV component place doesn't carry everything, but they may be able to order it for you.

Best of all, look at the ads in this magazine. There are many mail-order distributors which market primarily to the experimenter.

The high frequency spectrum analyser should be fairly tolerant of component substitutions except in the VCO circuit and the L-pad. For example, the 'hotter' 3SK88 could substitute for the 40673 if you crank its gain down a bit with the log amplifier bias pot. You could use MRF901s in place of the 2N5179s (don't try to go the other way!). Any decent electrolytics of the proper capacitance and voltage rating could be used in the power supply and sweep generator circuits. Electrolytics could also be used in place of the tantalum capacitors at a pinch. Try to get close-tolerance parts in this case.

USEFUL ACCESSORIES

You could duplicate the two-stage wideband pre-amplifier circuit for use as an accessory ahead of the attenuator. This will allow you to view the 0–60MHz radio spectrum on a long-wire antenna and quickly judge the band conditions up to 6m. VCO frequency tuning is somewhat non-linear, which is typical of simple wideband oscillators.

A 6MHz crystal oscillator driving a TTL Schmitt trigger makes a useful calibrator. The output of the TTL gate contains every harmonic up to 60MHz. Lightly couple the TTL gate to the spectrum analyser input with an insulated wire antenna placed near the analyser input connector. A momentary-on pushbutton can be used to activate the calibrator.

ANALYSER APPLICATIONS

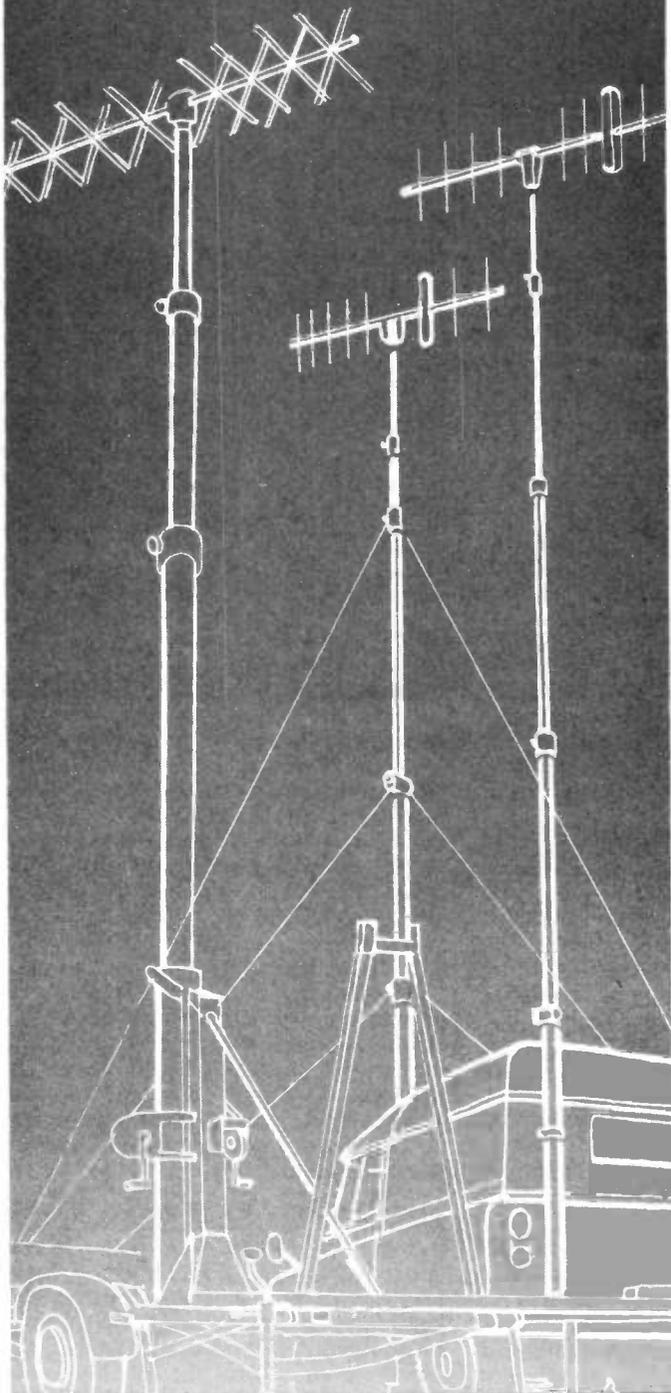
We have talked about using the HF spectrum analyser to monitor transmitting equipment. This was the primary application the author had in mind when he designed the analyser. It is especially useful to hams who are home-brewing their own HF transmitters or linears. It is also useful for checking low-pass filter performance and band conditions. Doubtless you will find other applications.

The analyser has a 50Ω input impedance and is DC-coupled. Be sure to add a blocking capacitor ahead of the attenuator if you are going to look at a RF signal that is riding on a DC level. Stay away from high-voltage DC circuits.

The bandpass of this analyser is too wide for looking at SSB modulation linearity. However, this can be judged

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adequately from a two-tone pattern on a normal oscilloscope.

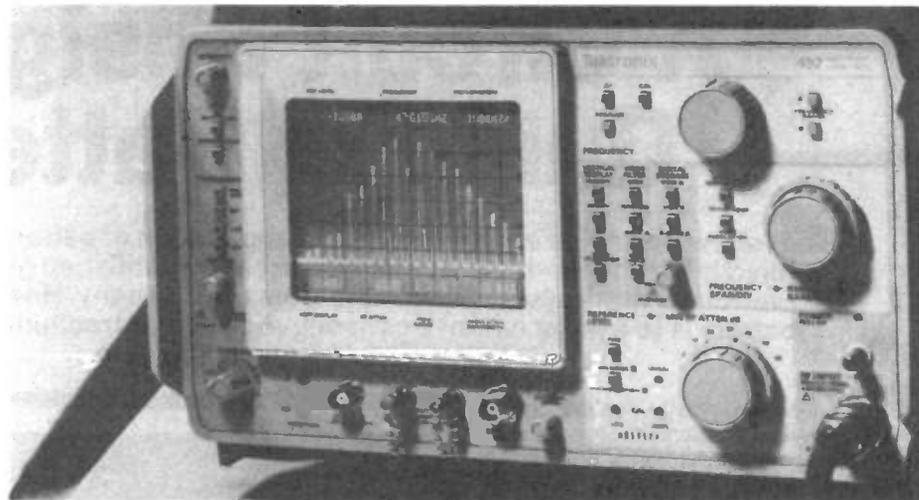
FROM HERE

This project demonstrates that a useful spectrum analyser can easily be built from relatively common and inexpensive components. Avid experimenters should treat this design as a starting-off point and be ready with the matching tracking generator — or possibly a version engineered onto PCBs using commercial helical filters so that this admittedly advanced project can be made more accessible to the less experienced constructor. Meanwhile, let's get those transmitter spectra cleaned up!

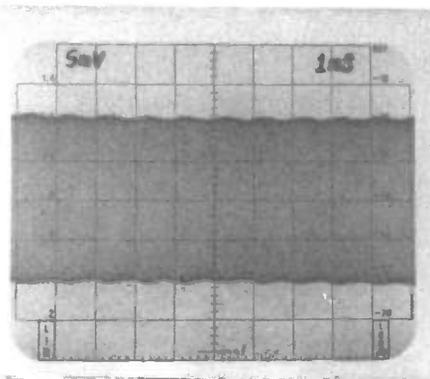
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References

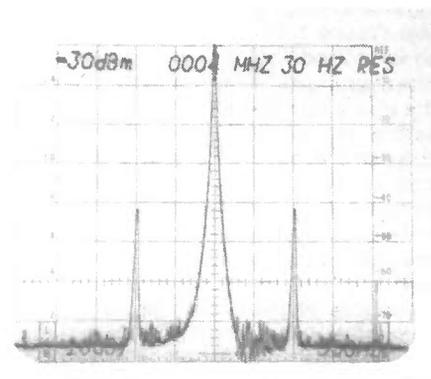
1. Wes Hayward and Doug DeMaw *Solid state design for the Radio Amateur* (ARRL Publications)
2. *Hewlett-Packard Electronic Instruments and Systems* (Hewlett-Packard, Palo Alto, California) 1981
3. Wayne Ryder 'High Performance Spectrum Analyser' *Ham Radio* June 1977
4. Clyde F Coombs *Printed Circuits Handbook* 2nd Edition (McGraw-Hill)



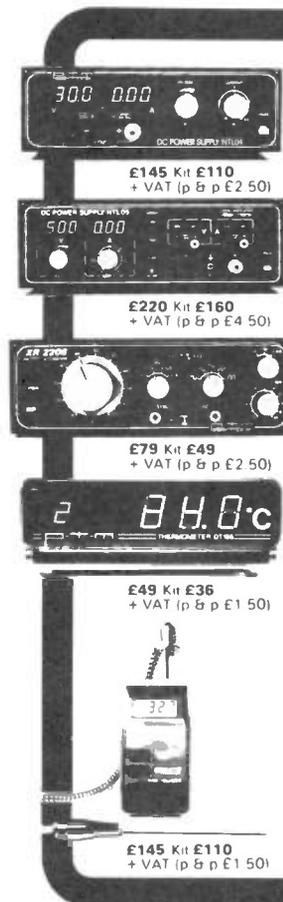
The Tekronix 492 spectrum analyser



Received signal



Its spectrum on the 492



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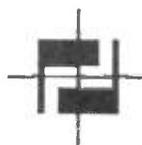
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A Circuit Designer's Guide to Batteries

The following advice on the choice and application of batteries is based on information supplied by Duracell – in particular on a recently published guide that gives full details of the various battery systems available from the company. However, the performance of a battery is to a great extent a consequence of electrochemistry, making this advice generally applicable

The first commercially available battery employed the zinc/carbon system in which the zinc container is the anode and the electrolyte is an acidic solution of ammonium chloride and zinc chloride, infused into a core of manganese dioxide and carbon black (the cathode) – see *Figure 1*. However, this system was soon found to have a number of disadvantages. For instance, because the container takes part in the reaction as the anode, the highly acidic electrolyte can corrode its way out of the casing and so can readily damage electrical circuits. Moreover, World War II demonstrated that these batteries were unable to cope with either tropical conditions or extreme cold, in the latter case proving incapable of producing any significant current. It was this set of circumstances that in fact led Duracell to develop the battery system that has since evolved into its well-known range of alkaline batteries with the familiar copper-coloured tops.



Modern battery types

The alkaline system mentioned above (and shown in *Figure 2*) takes its name from the electrolyte, which is a highly conductive aqueous solution of potassium hydroxide. The electrodes are of highly pure manganese dioxide and granulated zinc. This combination gives a 'superior, yet economic, battery capable of operating efficiently at high as well as low rates and over a wide range of duty cycles'. For a start, the discharge curve is considerably flatter than that for the zinc/carbon system – in other words, an alkaline battery produces a more stable output voltage-wise. Moreover the case does not take part in the electrochemical reaction and so there is little or no risk of leakage, an important consideration in these days of delicate ICs. This also permits the energy density that can be stored to be higher than would otherwise be the case: hence the Duracell claim that its batteries last up to six times as long as conventional

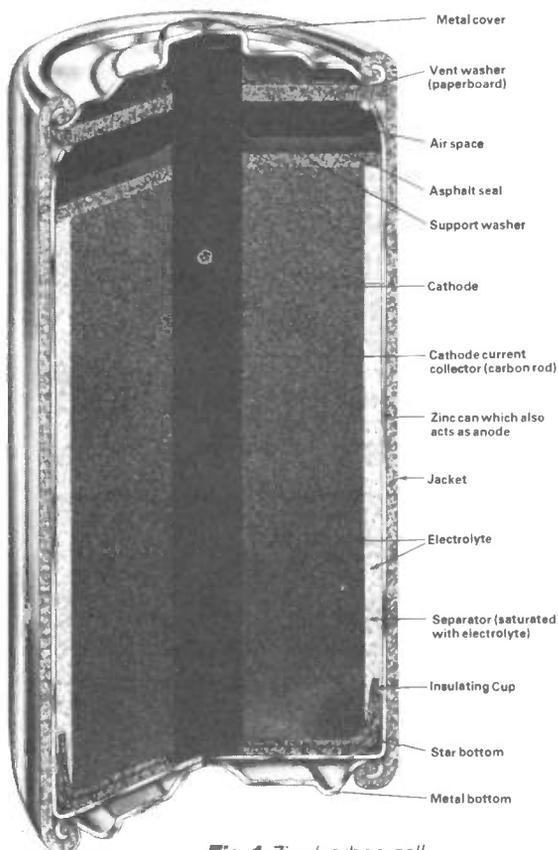


Fig 1 Zinc/carbon cell

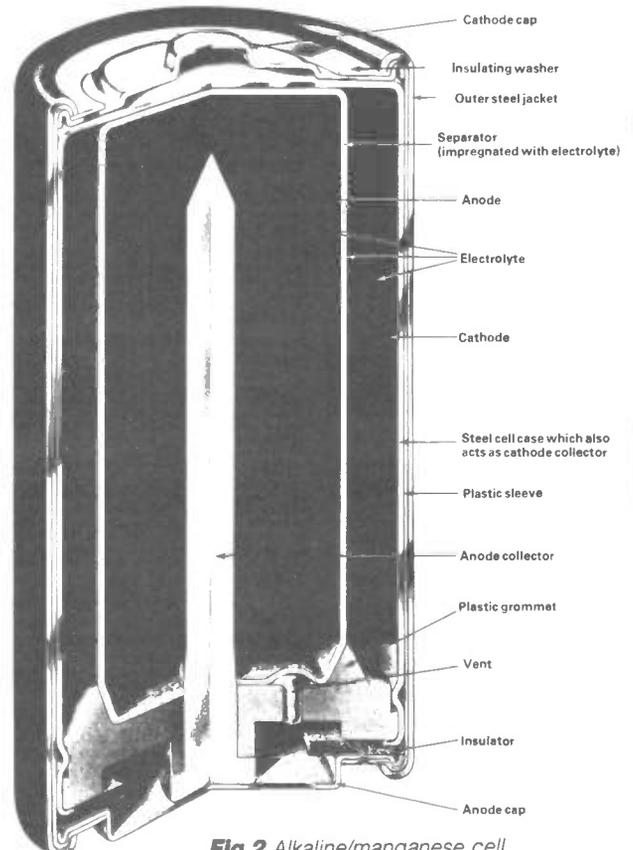


Fig 2 Alkaline/manganese cell

zinc/carbon cells – which, being electrically and mechanically similar, they increasingly replace.

Lithium, being a highly reactive metal, makes one half of a number of potential electrochemical couples, two of which have become quite well developed within the Duracell range (see *Figure 3*). These are lithium/sulphur dioxide (Li/SO₂) and lithium/manganese dioxide (Li/MnO₂) cells, both of which have a nominal voltage of 3.0V permitting one lithium cell to replace two conventional 1.5V cells. The former is based on a lithium anode in close contact with liquid sulphur dioxide as the cathode, the electrolyte being acetonitrile to which lithium bromide has been added to increase the conductivity. This combination makes for a very powerful battery, capable of efficient operation down to very low temperatures (-50°C), a property that leads to their wide usage in military applications. The Li/MnO₂ system combines a lithium anode with a manganese dioxide cathode in lithium perchlorate as the electrolyte. The latter is dissolved in an organic solvent, making the cell totally non-aqueous to preclude the potentially catastrophic evolution of hydrogen gas. Li/MnO₂ cells are particularly suited to applications that require low quiescent currents and short pulses of up to a few hundred milliamps on demand. Other advantages of this system include a long shelf-life (in excess of six years) and an ability to function at temperatures as low as -20°C.

A third lithium system that has been considered incorporates a lithium anode, a lead/lead iodide/lead sulphide cathode and an electrolyte that is a dry mixture of lithium iodide, activated alumina and lithium hydroxide. It relies for its operation on ionic conduction in the solid state, making it a very unusual electrochemical system indeed. The current supplied would be only a few microamps at room temperature but it would increase with temperature, making this type of battery highly suitable for memory protection applications. However, its future is uncertain at present.

Further systems

Another system supported by Duracell is based on a zinc/mercuric oxide couple in an alkaline electrolyte (*Figure 4*). The principal properties of this 'mercury' system are stable voltage, high energy density and a reasonably long storage life, making it 'the first choice' in applications where voltage stability and/or space is at a premium. At present these cells are most commonly found in hearing aids.

While the monovalent silver oxide batteries to be found in digital watches and certain photographic applications are another Duracell product, a recent development is that of the zinc/air system (*Figure 5*) which uses atmospheric oxygen at one of the electrodes. The concept is simple, drawing on the basic electrochemical reaction of the cathode liberating oxygen and the anode becoming oxidised as the means of

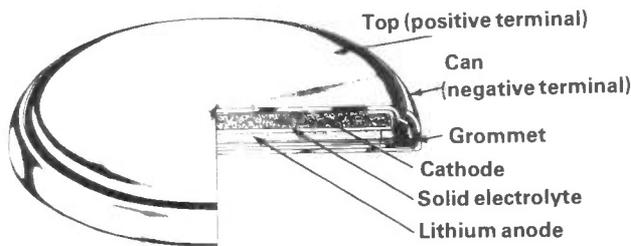


Fig 3 Construction of a lithium cell

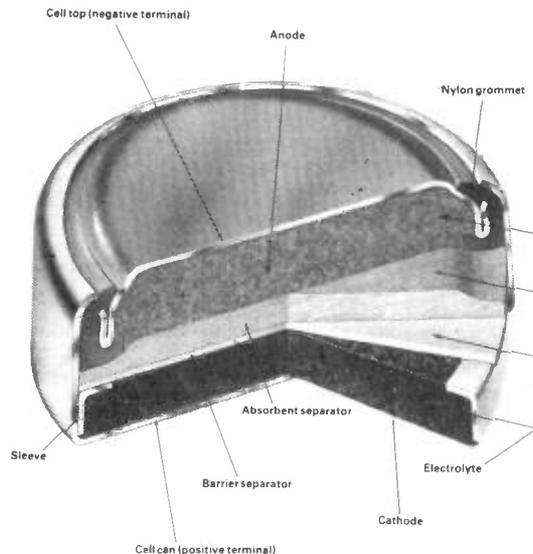


Fig 4 Mercury button cell

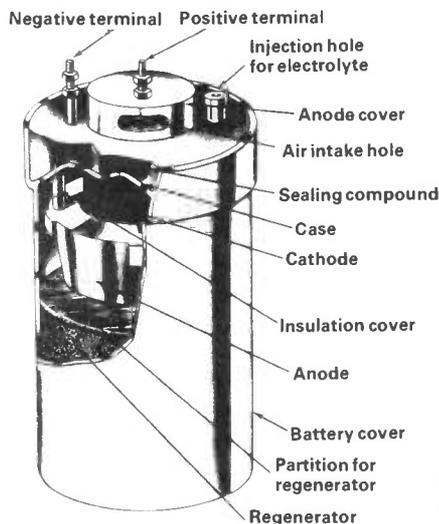


Fig 5 Zinc/air cell

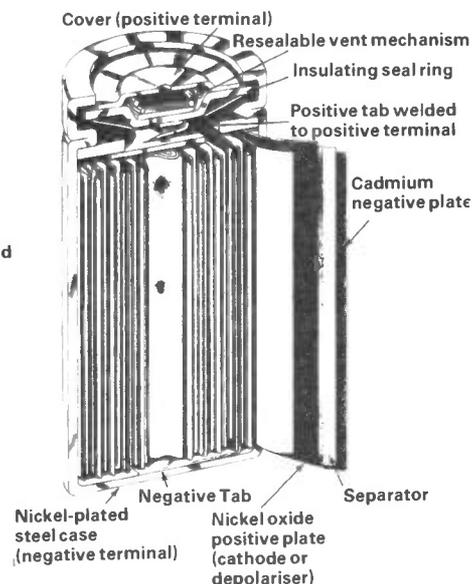


Fig 6 Construction of a NiCad cell

transferring charge between electrodes. Thus to use atmospheric oxygen just as though it has been liberated by the cathode should give the cathode almost infinite life. The voltage characteristic of the zinc/air system remains stable between 1.2 and 1.3V during most of the discharge and this system too is

being used for hearing aids (where it is directly interchangeable with mercury cells) and other such specialised applications. However, it is still subject to development as there are several factors that can interfere with its functioning – for example, impurities in the air.

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TRANSISTORS				THYRISTORS				CMOS				CPU IC's				VOLTAGE REGULATORS			
BC 107B	12p	BC 546	10p	BF 195	12p	MPSA 55	20p	C106D	28p	4000	14p	40162	52p	6800	395p	Positive			
BC 108C	12p	BC 546B	10p	BF 196	12p	MPSA 56	20p	C116D	70p	4001	14p	40163	52p	6802	550p	100mA			
BC 109C	10p	BC 547B	9p	BF 197	12p	MPSA 63	22p	C126D	90p	4002	14p	4501	16p	6808	520p	78L05 30p			
BC 113/4	16p	BC 548B	9p	BF 198	10p	MPSA 64	22p	C126M	90p	4006	50p	4502	55p	6810	250p	78L12 30p			
BC 119/6	17p	BC 548C	9p	BF 199	12p	MPSA 92	24p	MCR 101	30p	4007	16p	4503	34p	6820	250p	78L15 30p			
BC 139	32p	BC 549C	9p	BF 200	40p	MPSA 93	24p	MCR 102	34p	4008	50p	4504	98p	6821	190p	78L18 45p			
BC 140	28p	BC 550	10p	BF 224	15p	TIP 29A	30p	2N3400	58p	4011	14p	4506	70p	6840	595p	78L24 45p			
BC 141	29p	BC 550B	10p	BF 244C	22p	TIP 29B	33p	2N3441	120p	4012	15p	4508	145p	6850	180p	1 A TO220			
BC 142	27p	BC 557B	9p	BF 245	25p	TIP 29C	33p	2N3442	120p	4013	24p	4510	50p	6852	360p	7805 36p			
BC 143	27p	BC 557C	9p	BF 256C	32p	TIP 30A	33p	2N3702	10p	4014	54p	4511	52p	6880	140p	7808 55p			
BC 160	30p	BC 558B	9p	BF 257	32p	TIP 30B	33p	2N3703	10p	4015	46p	4512	48p	6885	130p	7812 36p			
BC 161	32p	BC 558C	9p	BF 258	32p	TIP 30C	33p	2N3704	10p	4016	24p	4513	98p	6889	140p	7815 30p			
BC 169C	8p	BC 559C	9p	BF 259	35p	TIP 31A	33p	2N3705	10p	4017	42p	4514	110p	68000 POA		7815 36p			
BC 171B	9p	BC 560C	10p	BF 336	36p	TIP 31C	37p	2N3707	10p	4018	47p	4516	55p	8T26A	140p	7818 36p			
BC 172C	9p	BC 637	20p	BF 337	39p	TIP 32A	37p	2N3708	10p	4019	30p	4517	180p	8T28	120p	7824 40p			
BC 173C	9p	BC 638	20p	BF 338	40p	TIP 32B	35p	2N3711	170p	4020	46p	4518	52p	8T95	140p	5 A TO3			
BC 177B	15p	BC 639	23p	BF 457	32p	TIP 32C	35p	2N3712	170p	4021	42p	4520	55p	8T97	140p	78H05 540p			
BC 178C	15p	BC 640	24p	BF 458	32p	TIP 33A	55p	2N3717	190p	4022	46p	4522	65p	8T98	140p	Negative			
BC 179	15p	BCY 70	18p	BF 459	37p	TIP 34A	60p	2N3819	20p	4023	14p	4526	64p	8030A	400p	100 mA			
BC 182	9p	BCY 71	18p	BF 494	12p	TIP 41A	46p	2N3823	50p	4024	39p	4528	56p	8085A	500p	79L05 50p			
BC 182B	9p	BCY 72	17p	BF 595	16p	TIP 41C	60p	2N3866	95p	4025	14p	4529	72p	8156C	600p	79L12 50p			
BC 183B	9p	BD 115	50p	BF 596	20p	TIP 42A	65p	2N3903	10p	4026	84p	4530	92p	8212C	198p	79L15 50p			
BC 183C	9p	BD 131	45p	BFX 29	28p	TIP 42C	65p	2N3904	10p	4027	29p	4531	70p	8224C	140p	1 A TO220			
BC 184B	9p	BD 132	48p	BFX 30	28p	TIP 110	45p	2N3905	10p	4028	42p	4532	88p	8228C	450p	7905 45p			
BC 184C	9p	BD 133	70p	BFX 84	28p	TIP 115	45p	2N3906	10p	4029	48p	4541	70p	8251AC	495p	7906 65p			
BC 212	9p	BD 135	30p	BFX 85	28p	TIP 120	70p	2N4030	30p	4030	18p	4542	70p	8253AC	800p	7908 65p			
BC 212B	9p	BD 136	30p	BFX 87	27p	TIP 121	70p	2N4033	30p	4031	48p	4553	180p	8257C	750p	7912 55p			
BC 213B	9p	BD 137	30p	BFY 88	23p	TIP 122	70p	2N4037	40p	4032	48p	4554	148p	8259C	900p	7915 55p			
BC 213C	9p	BD 138	35p	BFY 50	23p	TIP 126	70p	2N4058	7p	4033	42p	4555	48p	8288	£16	Variable			
BC 214B	9p	BD 139	35p	BFY 51	22p	TIP 127	70p	2N4059	10p	4034	44p	4556	48p	TMS9980A22		LM 309K 120p			
BC 214C	9p	BD 140	35p	BFY 52	22p	TIP 2955	70p	2N4060	10p	4035	56p	4557	160p	TMS9981N25		LM 317K 250p			
BC 237	7p	BD 203	70p	BSY 95A	22p	TIP 3055	70p	2N4061	10p	4036	56p	4558	110p	TMS9991E500		LM 317T 98p			
BC 238	9p	BD 204	70p	BU 205	140p	TIS 44	20p	2N4062	10p	4037	40p	4559	390p	TMS9992N5500		LM 350T 395p			
BC 239	9p	BD 205	70p	BU 206	150p	TIS 90	24p	2N4400	15p	4038	44p	4560	170p	Z80A 4M 580p		LM 723CN 35p			
BC 251	9p	BD 206	70p	BU 208	140p	TIS 92	20p	2N4401	15p	4039	52p	4562	270p	Z80A PM10500p		78H05 540p			
BC 300	40p	BD 239A	40p	MJ 2500	230p	2N1613	30p	2N4402	15p	4040	52p	4565	140p	2101 4A 350p					
BC 301	35p	BD 239C	50p	MJ 2501	245p	2N1711	30p	2N4403	15p	4041	52p	4572	42p	2114 4A 120p					
BC 302	35p	BD 240A	42p	MJ 2955	90p	2N1893	30p	2N5400	18p	4042	28p	4573	198p	2147 70S 600p		TIL 32 55p			
BC 303	35p	BD 240C	50p	MJ 3001	225p	2N2218	24p	2N5401	20p	4043	15p	4574	198p	2147 45S 700p		TIL 38 40p			
BC 304	35p	BD 241A	42p	MJ 3002	225p	2N2218A	25p	2N5402	20p	4044	15p	4575	198p	2166	£10	TIL 78 50p			
BC 307	10p	BD 241C	54p	MJE 340	48p	2N2219	24p	2N5403	20p	4045	15p	4580	280p	4716 150S 400p		TIL 100 100p			
BC 308	10p	BD 242A	42p	MJE 350	70p	2N2219A	25p	2N5404	20p	4046	15p	4584	38p	5016 200S £7		TIL 111 85p			
BC 309	10p	BD 242C	54p	MJE 370	80p	2N2221A	20p	2N5405	20p	4047	15p	4585	74p	5101 LCL 340p		2N5777 50p			
BC 327	12p	BD 243A	55p	MJE 371	84p	2N2222	18p	2N5406	38p	4048	15p	4599	178p	5101 LCL 1395p		4N25 80p			
BC 328	12p	BD 243C	68p	MJE 520	60p	2N2222A	20p	2N5550	18p	4049	15p					4N28 70p			
BC 337	12p	BD 244A	64p	MJE 521	68p	2N2368	23p	2N6027	23p	4050	15p					4N33 128p			
BC 338	12p	BD 244C	78p	MJE 2955	80p	2N2369A	15p	2N6028	23p	4051	15p					4N35 150p			
BC 413C	10p	BF 180	30p	MPSA 05	20p	2N2484	24p			4052	15p					4N37 100p			
BC 414C	10p	BF 181	30p	MPSA 06	20p	2N2646	48p			4053	15p					BPX 38 390p			
BC 415C	10p	BF 182	30p	MPSA 07	20p	2N2904	22p			4054	15p					BPX 43 340p			
BC 416C	10p	BF 183	30p	MPSA 10	22p	2N2904A	23p			4055	15p					TIL 221 20p			
BC 477	25p	BF 184	30p	MPSA 13	22p	2N2905	23p			4056	15p					(high output clear red)			
BC 478	23p	BF 185	30p	MPSA 42	23p	2N2906A	22p			4057	15p								
BC 479	24p	BF 194	12p	MPSA 43	23p	2N2907	23p			4058	15p								

LINEAR IC's				CAPACITORS				DIODES				RESISTORS				HARDWARE			
CA 3046	72p	LM 565	100p	SAA5041	£25	Electrolytic radial/axial.		AA 119	9p	1/2 Watt Carbon film 5% E24		4xTO3 mounting kits 20p		64mm Loudspeakers 8R 70p		each			
CA 3065	190p	LM 567	150p	SAA5050	£10	Tantalum bead.		BAX 13	5p	200µF 100V		4xTO66 mounting kits 20p		64R 78p each		300mW rating			
CA 3080	72p	LM 709	35p	SAA5052	£10			BAX 16	6p	series 4 7 R		5 x TO126 bushes/washers 14p		PP3 battery snaps 6p		each			
CA 3086	56p	LM 710	70p	SL490	300p			OA 47	9p	2M2 1p each		10xTO220 bushes/washers 22p		4xHP7 battery holder 22p		each			
CA 3089	170p	LM 711	60p	SN76115	98p			OA 90	7p	1/2 Watt Carbon film 5% E12		5 x TO3P bushes/washers 14p		6xHP7 battery holder 32p		each			
CA 3090AQ	300p	LM 733	75p	SN76690	90p			OA 91	7p	film 5% E12		20mm panel fuseholder 32p		20mm chassis fuseholder 7p		each			
CA 3130E	95p	LM 741	14p	TBA 120S	70p			OA 95	8p	series 1R 10M 2p each		4mm plugs 12 4mm sockets 20p		4mm insulated terminals 30p		3.5mm jack socket 15p			
CA 3140E	40p	LM 748	35p	TBA520Q200p				OA 200	8p	1/4 Watt Metal film 1% E24		Phono sockets 15p		Switches: miniature toggle, SPST 60p		DPDT 78p each			
CA 3160E	100p	LM 1458	36p	TBA550	240p			IS44	6p	series 10R 1M 4p each		250p per 100, one value only		280p per 100		mixed values.			
CA 3161E	140p	LM 3900	47p	TBA625	100p			IS921	9p	2.5 Watt wire-wound OR22		CP100 20 BC183/BC213 transistors, 10 of each		130p		CP102 20 BC183/BC213 transistors, 10 of each			
CA 3240AE	165p	MC 1455	16p	TBA800	70p			IN914	3p	10 ohms E12 series 25p each.		CP103 20 BC184/BC214 transistors, 10 of each		130p		CP104 20 BC549C/BC559C transistors, 10 of each			
CA 3240E	110p	MC 1458	34p	TBA810A	595p			IN916	4p	Presets: miniature horizontal & vertical		CP105 20 BC560C/BC560C transistors, 10 of each		160p		CP106 100 IN914 switching diodes, 75-100V/75mA 240p			
CA 3260E	100p	MC 1748	35p	TBA810S	95p			IN4148	3p	Potentiometers: Single gang with DPST switch		CP107 100 IN916 switching diodes, 75-100V/75mA 280p		240p		CP108 100 IN4148 switching diodes, 75-100V/75mA 160p			
CA 810QM	250p	MC 3302	72p	TBA820M	78p			IN4149	4p	1K to 1M 32p each.		CP109 500 IN4148 switching diodes, 75-100V/75mA 680p		100p		CP110 30 IN4002 1A/400V rectifiers			
LF 347	160p	MC 3401	68p	TBA920	195p			IN5400	11p	Dual gang.		CP111 10 MC145B Dual op amps (741 type)		320p		CP112 100 400mW zeners, 4 of each 2V7 to 33V			
LF 351	45p	MC 3403	65p	TBA950	210p			IN5401	11p	80p each.		CP113 100 1.3W zeners, 4 of each 4V7 to 51V		850p		CP114 4 LF351 JFET op amps, Low noise			
LF 353	80p	NE 529	220p	TCA270	120p			IN5402	12p	1K to 1M 32p each.		CP115 4 LF3							

The movement of oxygen discussed above has been essentially the crucial factor in ruling out recharging for all the above-mentioned battery systems. Unfortunately the anode cannot be simply restored to its metallic state because it swells up in becoming oxidised. Moreover, anode particles may break up or shift about, with the result that the original structure is largely destroyed. The only system to date to circumvent this difficulty whilst at the same time being compact enough to be competitive with small primary cells is the nickel/cadmium rechargeable. Here both the anode material (cadmium) and the cathode material (nickel oxide) are contained in porous plates that prevent the anode structure from being seriously distorted as the cadmium is oxidised (Figure 6). The cathode structure is similarly maintained and so it is safe to recharge the cell. However, their cost, along with that of the recharging unit, and the frequency with which they need to be recharged have so far limited NiCads to a relatively small share of the consumer market.

Putting batteries into circuits

A number of 'golden rules' are stressed by Duracell, their aim being to aid any circuit designer in establishing a design that operates with a satisfactory power source, in terms of both performance and cost. These are:

1) Always select the battery or cell type before finalising either the circuit parameters or the mechanical design. In an extreme case, it might not be possible to find any battery – however expensive – that meets your requirements.

2) Select the circuit parameters so that the equipment operates within the desired specification over as much as possible of the available voltage range of the chosen battery as indicated by diagrams such as those shown in Figures 7 and 8. In other words, reconcile the requirements of the equipment with the battery's ability to deliver current: any mismatch can cost a lot in lost energy particularly in the case of those battery systems that deliver their energy over a considerable voltage range.

3) Design the equipment to be able to accept the battery's open-circuit voltage which may exceed the nominal voltage by as much as 15%.

4) Always aim to use standard rather than special batteries; not only are the former less expensive but they are also much more widely distributed, offering the promise of cost-efficient service for many years.

5) Aim for the lowest system voltage compatible with the power requirement at the lowest specified temperature, particularly where cells are connected in series; this is generally regarded as good practice.

6) Where cells are connected in parallel, ensure that the current passed by any

cell stays within the range stipulated on its data sheet.

7) Never mix cells of different brands, types or ages as this will almost certainly lead to the weakest cell being at some stage driven in reverse with consequent gassing, leakage or even rupture.

Practicalities

Of course, not all of these aims are particularly easy to implement. For example, while data sheets can generally indicate well enough the acceptability of a proposed load at 20°C, the detailed rate capability is a complex function of temperature, duty cycle and previous storage history and so it is rarely, if ever, fully documented. However, special tests that give a good indication of performance at low temperatures, say, can be performed and data

relating to performance at specific temperatures either side of normal ambient conditions can generally be provided by the manufacturer. There is further guidance on this in the Duracell guide.

Even taking all that into consideration is not enough, for one must also remember that the reliability of any battery decreases as the number of cells increases (as there is a greater risk of the weakest cell being driven in reverse) and that, when connecting Li/SO₂ cells in parallel, series diodes must be added to each parallel path. (In fact the latter action generally increases the reliability of cells under parallel connection.) Another point to consider is the use of lithium cells with their nominal output of 3V in place of conventional 1.5V cells where space and/or weight is at a premium.

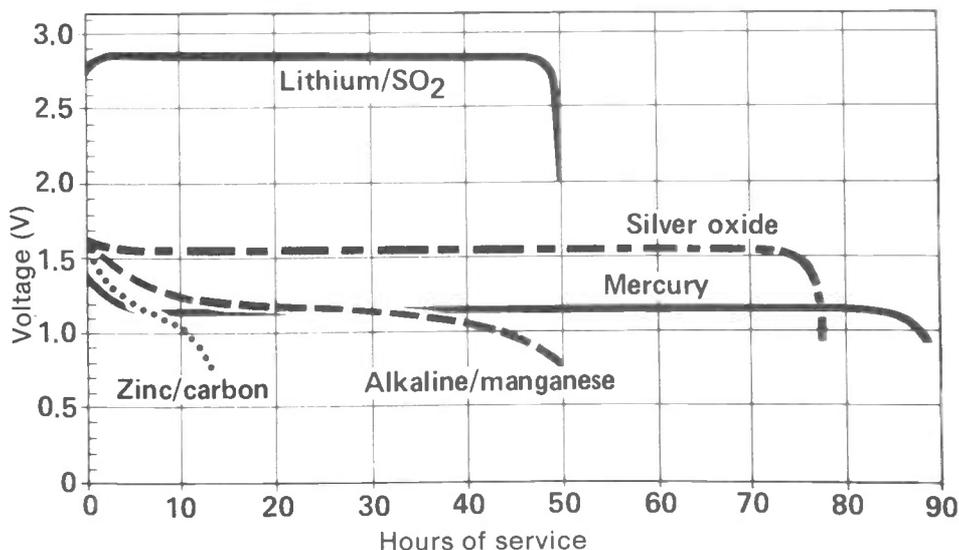


Fig 7 Typical voltage characteristics on medium load of some Duracell batteries

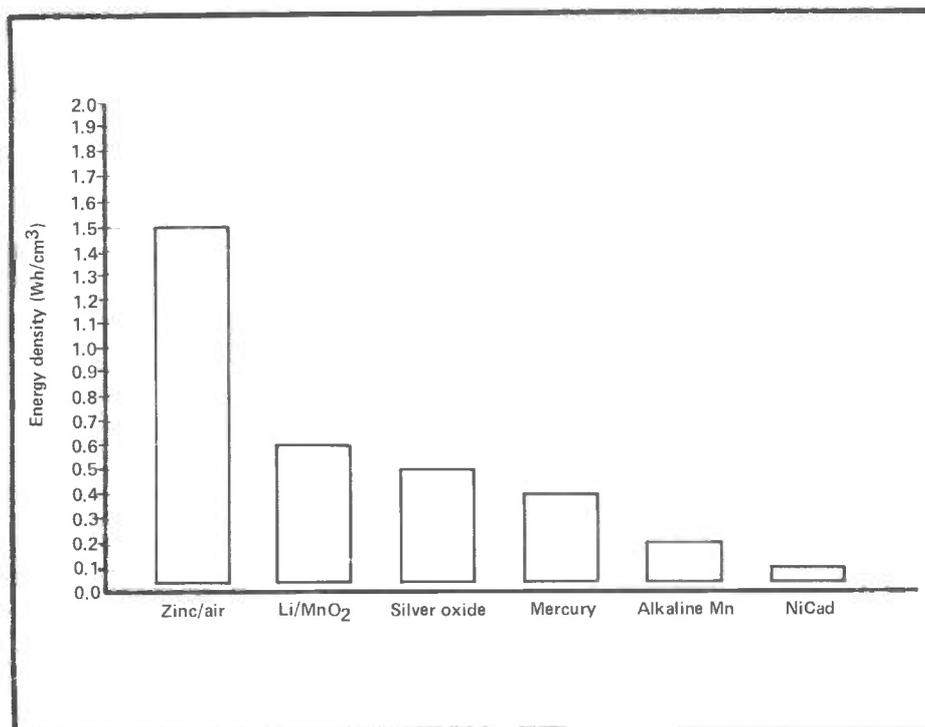


Fig 8 Typical energy densities for a number of battery systems

Ultimately, the best source of advice is a specialist battery manufacturer and indeed Duracell offers a free battery consultancy service. The company might even be able to oblige with a custom-designed battery, exactly right for the purpose.

The battery housing

The other major area of advice is concerned with the battery compartment. Not only should this keep the cells clear of any metallic battery jacket but it should also be able to accommodate cells individually, allowing for all sizes

up to the maximum size each cell could be, appropriate contact springs taking up the difference between this and the actual dimensions.

The springs themselves should in turn conform to certain standards. For example, the pressure they apply should be just enough to mark the cell and, still more importantly, they should be made of a compatible material i.e. one that won't encourage galvanic corrosion following a cycle of temperature and humidity that leads to condensation. The materials recommended include austenitic 18/8 stainless steel, steel with an 8µm thick layer of nickel-plating, and inconel; copper alloys are definitely not recommended. By the way, the white deposit that can develop on the contacts does not affect the performance of the cell itself but it will, of course, increase the circuit resistance: however, it can readily be removed with a dry cloth.

Other points to note regarding these contacts are: that the contact should be single-point for low currents but multiple-point for larger ones; that screw terminals are unacceptably restrictive and so should not be used; and that there should be no conductive path between the battery jacket and the equipment. Duracell also recommends the use of polarised battery contacts and that the compartment be designed to make it impossible to insert the batteries the wrong way round. This is particularly important where more than one Li/MnO₂ cell is being used either in series or parallel as one of these driven in reverse could explode!

Apparently, an increasing number of applications are side-stepping the insertion problem by making use of Duracell's new Flat-Pak. This is essentially a number of high performance alkaline cells welded together and sealed into a flat cassette only 9mm thick. This cassette is so designed that it cannot be inserted incorrectly: moreover it reduces the size, complexity and cost of the battery compartment as only two contacts are needed instead of multiple springs, etc. In addition, users should note that it is Duracell policy only to supply Li/SO₂ cells in packaged form complete with fuses and protective diodes.

And finally.....

Questions of storage, recharging and disposal come up as a matter of course when handling batteries. Duracell recommends storage at 10–25°C and where the relative humidity is less than 65%; other conditions are certain to encourage a quicker deterioration in battery performance. With regard to recharging, most of the cells considered here are not designed for this: any attempt to recharge them will induce an imbalance in the cell which could lead to gassing and ultimately to an explosion. Duracell, naturally, does not accept responsibility for injury or damage resulting from this or other abuse—and it is highly unlikely that any other manufacturer would.

Last, but not least, don't dispose of them in the fire!

Characteristics of Duracell Batteries

Type	Open-circuit voltage	Voltage on load	End voltage	Operating temp	Shelf life indication
Alkaline manganese	1.56V	1.5V	0.8V ¹	-30 to +70°C	>85% retention after 2½ years at 20°C
Mercury (two forms)	1.35–1.36V 1.36–1.55V	1.3–1.4V	0.9V	-30 to +70°C	≤95% retention after 1½ years at 20°C
Monovalent silver oxide	—	1.5V	1.2V	—	~90% after 1 year at room temperature
Lithium/sulphur dioxide	3V	2.8–2.9V ²	2V ³	-50 to +70°C	10 years
Lithium/manganese dioxide	3.3V	3V	~1.4V	-20 to +50°C	6 years at room temperature
Zinc/air	1.4V	1.2–1.3V	0.9V	—	2½ years sealed 3 months unsealed

¹ 1V per cell when 6 or more cells used in series

² 2.55–2.8V at -30°C

³ 1.5V in high rate applications: must not be allowed to go below 0V

Alkaline Manganese

- No defined upper limit but it is suggested that no more than 2A is drawn on intermittent load at room temperature.
- These batteries are unaffected by high pressure, high vacuum or high relative humidity but they shouldn't be used for more than short periods above 45°C.
- Available in all common (ie international) sizes.
- Storage at temperatures above 20°C will lead to progressive deterioration in both capacity and high rate capability

Mercury

- The difference between the two forms of cell is only important a) during the first 5–0% of the discharge and b) when maximum voltage stability is required.
- Energy can be taken from these batteries at up to the 20hr rate at 20°C without significant loss of efficiency.
- These batteries are unaffected by high pressure, high vacuum or high relative humidity.

Li/SO₂

- Open circuit voltage modified in time through formation of a passivation layer of lithium dithionite on the anode but this is rapidly stripped on discharge.
- Operation above 70°C risks accidental venting.
- Tolerant of high vacuum but high pressure can inhibit the safety vent.
- Can supply up to 30A intermittently but the energy should not be dissipated at more than the 8hr rate over longer periods.

NB: The transportation of those batteries containing more than 0.5g of lithium are subject to international regulations.

Li/MnO₂

- Maximum load that can be taken is a function of the particular cell type.
- The voltage characteristic is substantially flat.
- These cells all contain less than 0.5g of lithium and so are not subject to restrictions over their transportation.

Duracell's 86-page guide for designers of electrical circuits and equipment is available free of charge from Duracell UK (Technical Division), Duracell House, Gatwick Road, Crawley, West Sussex RH10 2PA (Tel: Crawley [0293] 517527), which is also the address to write to for further information.

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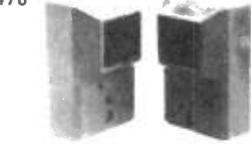
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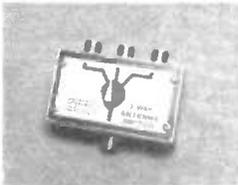
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COMMUNICATIONS

BUILDING

BLOCKS

Front ends for all -Part 2

Before making an attempt within this series at quantifying mixer and front-end performance, we offer some practical insight — and a choice of different active mixer configurations for experimenters and building block users.

As already discussed in this series, the section of the receiver most likely to make or break the design when judged in terms of conventional standards of performance is the first mixer. Dynamic range is the thing — and whereas valves provided a comparatively easy route to wide dynamic range, semiconductor systems do not.

The requirement is simple. If a receiver has a 'free range' sensitivity of one microvolt for 12dB SINAD, then it should be able to handle a strong signal in the passband of the RF stage that is 90dB 'up' on one microvolt — approximately 30mV — without cross modulation, intermodulation or other manifestations of non-linearity in the RF amplifiers or the mixer.

Now there's nothing mystical or magical about dynamic range. Despite the problems it creates, it is a simple concept to grasp: *Figure 1* illustrates the basic reasoning. But the solutions are not so simple in semiconductor technologies where the maximum rail voltages are between ten and thirty times less than those used with valves. And there are other considerations, the major one being the old chestnut about the influence of impedance levels on power levels with respect to available voltage swing. Read on.

Low Z

In terms of power, one microvolt into 50 ohms translates into $4.47\mu\text{V}$ into 1000 ohms. (Power = [volts.volts]/resistance.) A bipolar transistor junction rejoices in a voltage difference between base and collector of some 300mV. A 100mV input signal presented to the base of a transistor RF amplifier will cause it to overload quite hopelessly. However, the input impedance is very low, and a signal of 100mV at 1000 ohms will drop significantly as a result of the impedance presented by the transistor base.

A transformer is used in tuned RF amplifier stages to match both the input from the antenna, and the output to the ensuing active circuitry. *Figure 2* illustrates this. One side effect of this method

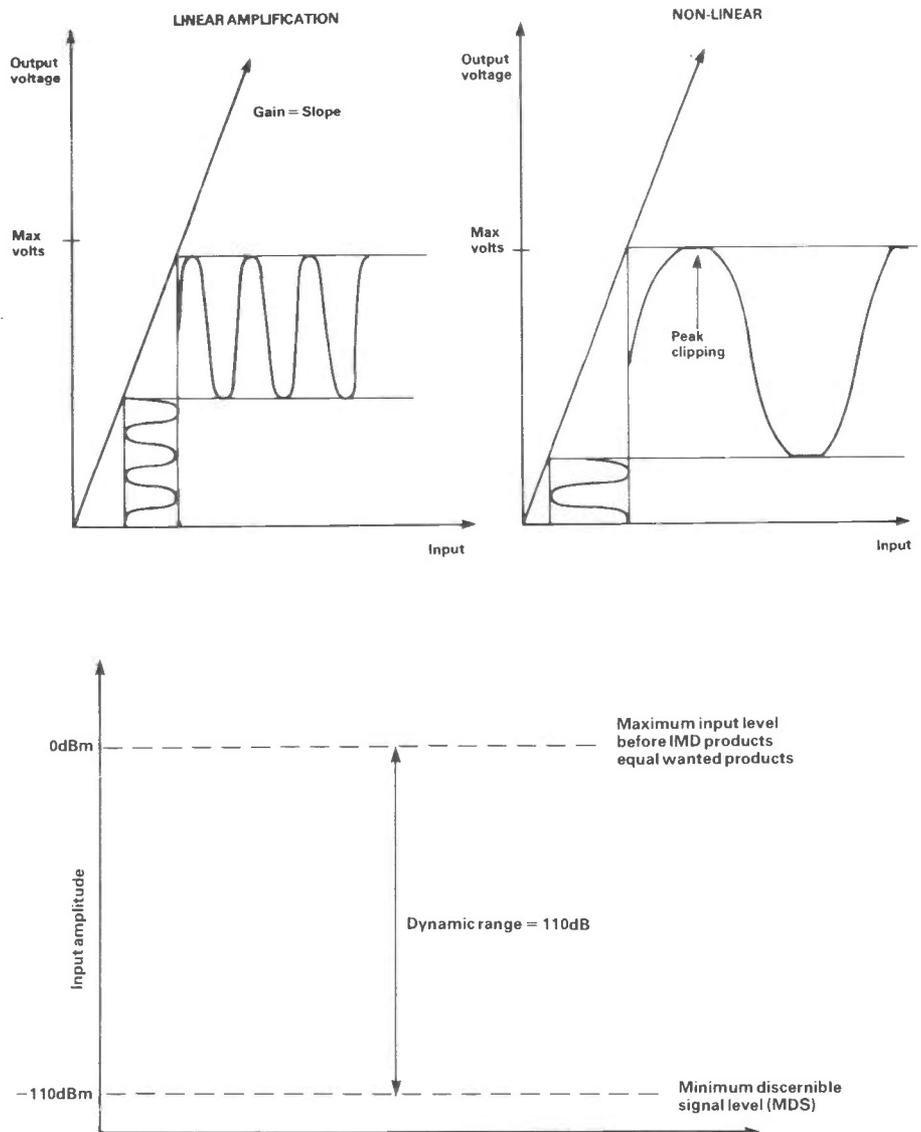


Fig 1 a) Demonstration of why the dynamic range of an amplifying stage is limited by the available voltage swing at the output. b) Receiver dynamic range. NB for **in band** signals, the maximum input level can be considerably greater due to AGC effects.

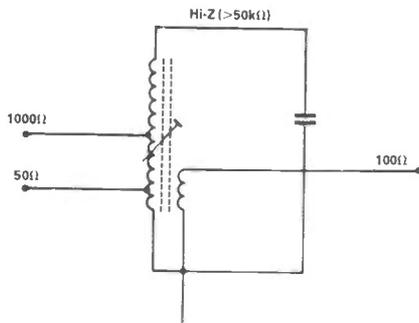


Fig 2: Typical input stage transformation

Fig 3: Cybernet balanced mixer stage

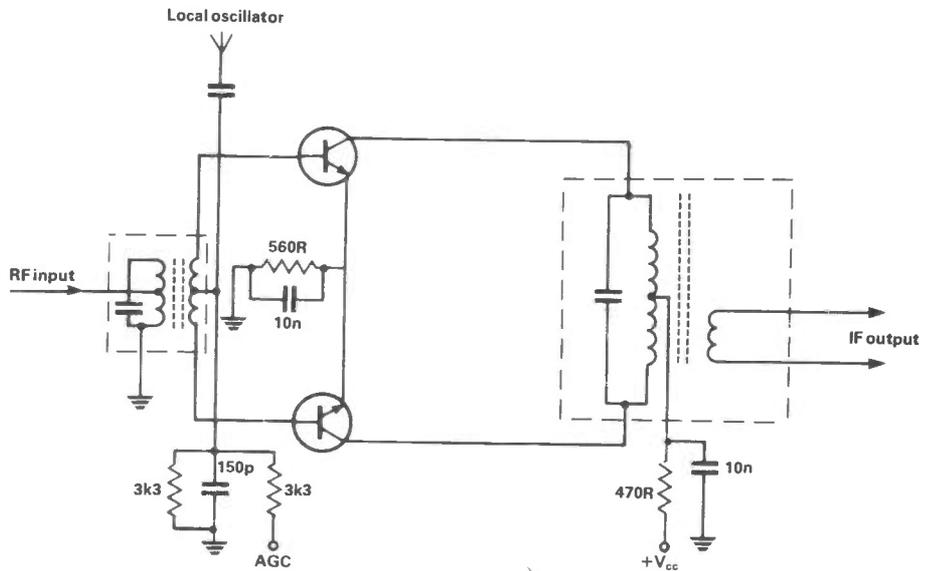
of matching is the way in which the impedances of an amplifier alter across its tuning range: it's not possible to design a variable capacitance tuned circuit to have constant input/output impedance over a broad tuning range.

Virtually regardless of the rail voltages available, a given configuration of bipolar transistor amplifier (or mixer) will tend to produce similar dynamic ranges (assuming the bias currents are adjusted to remain the same). The situation is not helped by operating the stage at low collector currents, since the relatively high collector impedance will increase the collector voltage swing for a given power level. Thus a higher collector current is generally synonymous with improved dynamic range.

One popular method of extracting more performance from bipolar mixer stages is to use the 'balanced' configuration. This approach relies on a similar principle to that used in class B audio power amplification: each transistor can devote its entire 'dynamic range' to only half of the waveform. The (singly) balanced mixer used in a number of CB sets within the Cybernet range (*Figure 3*) seems particularly commendable, judging by the result of various equipment reviews, yet it's relatively simple and exotic.

Mixing it with FETs

Ever since the FET and MOSFET were introduced into radio design, they have tended to displace bipolar alternatives in areas where high level signal performance is required. There was a large element of fashion involved in the early days of FETs, and quite a few designs sporting FETs simply plugged them in where the bipolar devices once lived. A FET is basically a high impedance device like a valve — but unlike a valve it doesn't enjoy a lot of headroom in the anode voltage. It nevertheless provides an excellent transformation between high input impedances and the relatively lower impedance of the drain, and is more forgiving of biasing. By the same token, a single ended FET amplifier with a tuned input is prone to instability as a result of the input and the output 'seeing' each other 'in phase'.



The Sony ICF2001

The FET does not provide inherently much better dynamic range than a correctly biased and matched bipolar RF stage — but it does provide better performance in service as a mixer, and it is a great deal more forgiving of inaccurate design and matching. An FET mixer with the signal applied to the gate and the oscillator supplied via the source is a popular solution, although the oscillator feed to the source must be well buffered, since strong RF input signals are not at all isolated from the source. One or two designs have been known to collapse completely when the oscillator has been effectively turned off in this way.

The singly balanced FET mixer has been thoroughly explored in a number of Japanese designs. All yield an IMD performance in the region 85—95dB with respect to the minimum discernible signal (MDS), with anything from 5 to 20dB of gain. One of the more interesting manifestations occurs in the Sony ICF2001 where the HF input stage (*Figure 4*) also embodies an 'active' antenna pre-amplifier in the shape of Q52 and Q50. The legendary propensity to overload exhibited by the ICF2001 is not prompted by this aspect of the circuit

but the very wide first IF and the less than razor sharp selectivity afforded by the input tuned stages formed across L6 through L10.

The signal in the ICF2001 is fed to gates of the balanced mixer stage via a source follower buffer stage. Local oscillator injection is onto the source via Q21 and T3, whose properties are regrettably not defined in the parts list. It seems reasonable to make an initial guess of a centre tapped 1:1 broadband transformer wound on a small dual aperture ferrite core.

The tuned drain circuit is conventional enough (centre tapped, don't forget), and you can forget Q18, Q23 and their associated components, since these are used in the FM/AM switching. One slightly curious aspect of the design is the size of the source resistors: at 4k7 and a voltage drop of 300mV, the current flowing is $(0.3/4k7)=65\mu A$ — which is barely using the FET at all. In applications where the cautious use of supply current isn't a problem, it seems likely that dropping their value to 470 ohms

would improve the performance. The basic consideration in these matters is that the power levels biasing and operating the active circuitry should not be swamped by the power derived from the signal.

A similar style of stage occurs at the front end of the highly regarded NRD515 (Figure 5). Here the source resistors are effectively 1k Ω , and the local oscillator is fed from a local buffer stage (TR7), whose output level is controlled by the AGC loop fed from C180 round to TR6.

The ubiquitous Ulrich Rhode has been known to favour the passive FET mixer of Figure 6, which can provide an intercept of +40dBm when correctly matched. If you choose this approach, you'll be in the excellent company of the Racal RA6790. The catch is the requirement for a 23dBm drive signal, along with two of the most obscure FET types yet seen in these pages. No, a 2N3819 won't do!

The input to the ICF2001 is resistively terminated: another look at a similar configuration (from Yaesu) with a tuned stage (in this case a second conversion stage) is provided by Figure 7a. The R1000 does a similar thing with dual gate MOSFETs (Figure 7b), taking advantage of the control gate to inject the local oscillator and add to the effectiveness of the AGC control. Purists, however, don't hold with that sort of thing, since AGC on the mixer will cause the dynamic characteristics to be modified, thus altering the matching between the mixer and the filter stage. It's a pedantic point that shouldn't really concern any enthusiast prepared to try out some of the designs suggested herein.

Mixing it with Plessey

The Plessey SL6440 is widely used as a 'convenience' product because it provides good dynamic range with relatively low oscillator drive levels. The device is based on the classic among double balanced mixers — the MC1496 (Figure 8). A similar transistor tree configuration occurs in a large number of radio ICs, doing service as mixers and product detectors (SL1640, ULN2242, TDA1083, KB4412/3 etc).

The Plessey implementation uses this same basic transistor tree arrangement,

Fig 6 Passive FET mixer

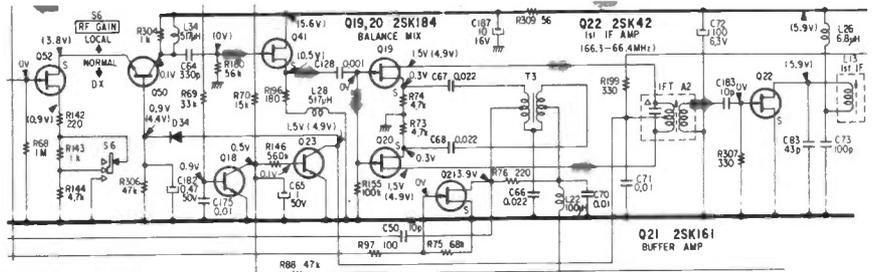
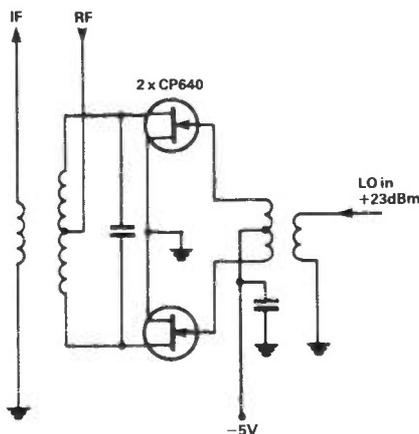


Fig 4 HF input stage of the Sony ICF2001 — an interesting manifestation of the singly balanced FET mixer

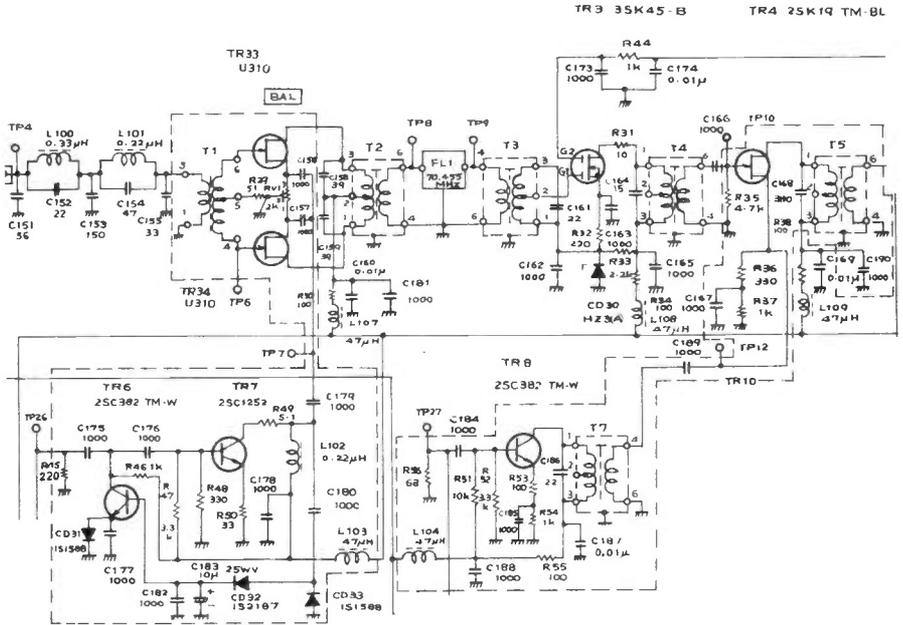
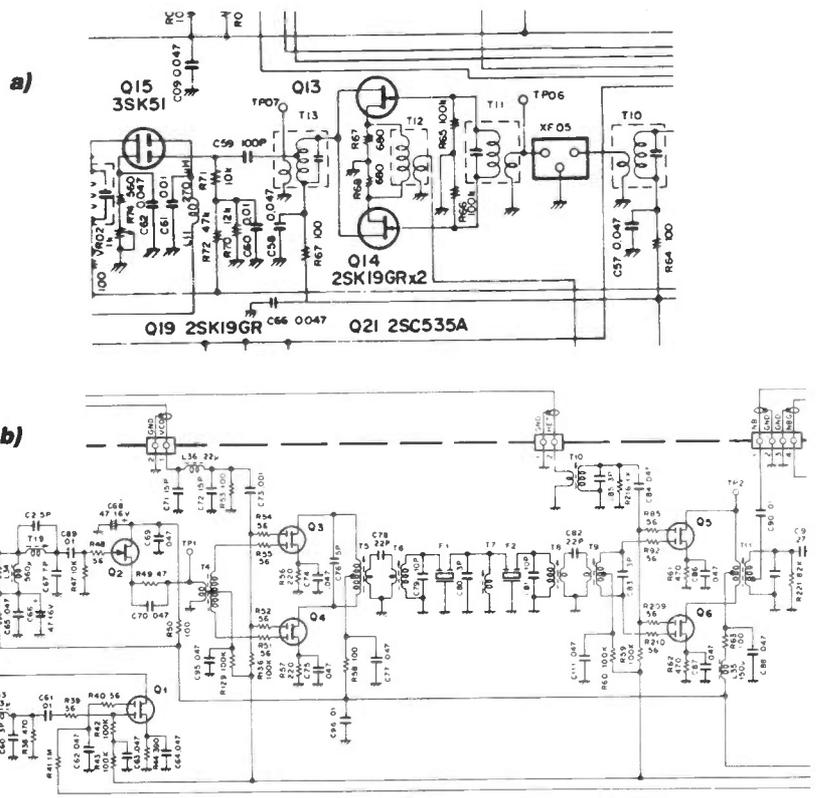


Fig 5 Front end of the NRD515

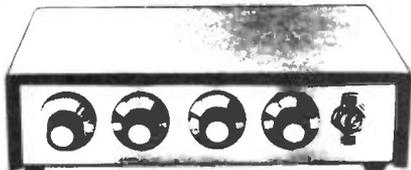
Fig 7 a) Yaesu mixer configuration, and b) Equivalent circuit from the R1000, this time using dual gate MOSFETs



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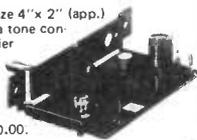
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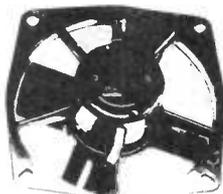
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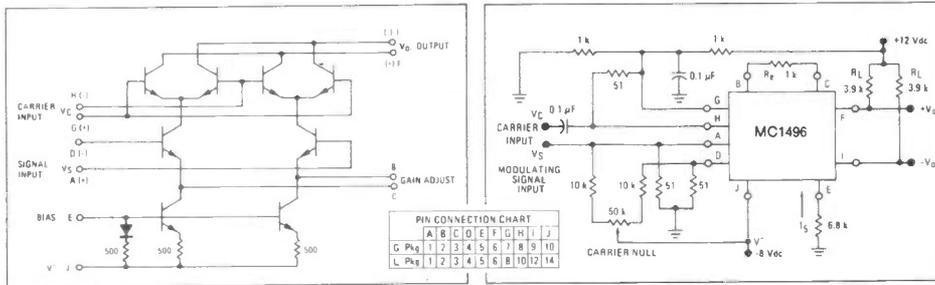


Fig 8 a) Schematic representation and b) Typical modulator circuit for the MC14196

optimised through the use of large multiple-emitter transistors and careful selection of emitter resistance values. In the application circuit shown in Figure 9, the SL6440 returns a performance that represents probably the best available to the home experimenter without an array of sophisticated test equipment to tweak and optimise discrete alternatives.

Sensitivity is -113dBm for 15dB S+N/N in a 3kHz bandwidth; the third order IMD ratio with two signals of -4dBm is a high 70dB ; only $30\mu\text{W}$ of LO required; and a gain of 10dB is available — countered by the only drawback of this approach, a noise factor of 11dB . However, Plessey and Peter Chadwick argue with considerable justification that, within the HF spectrum, such a noise figure is not the factor limiting the overall performance.

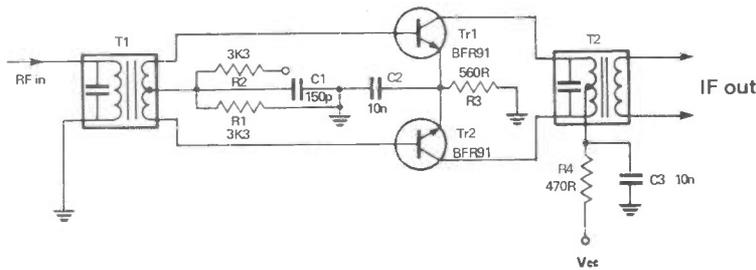


Fig 9 High performance SL6440-based mixer circuit

In Conclusion

Mixer designs provides a lot of scope for experimentation. A number of communications buildings blocks may be derived from the types described herein, and next month we'll be catching up with some PCB designs and performance results for the active antenna system discussed last month, along with those for a couple of the mixers described in this instalment.

Fig 10a: PCB for the SL6440-based mixer circuit shown in Figure 9. Bottom plane foil pattern

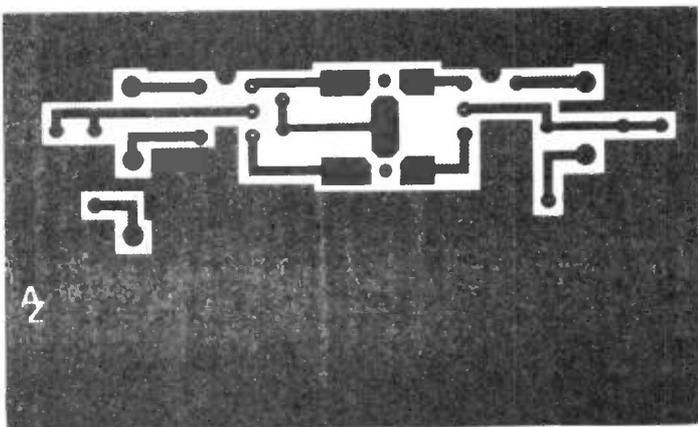


Fig 10b: PCB top plane

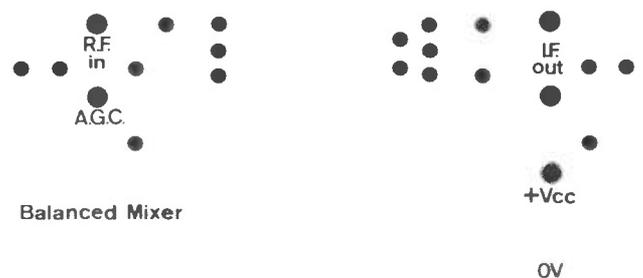
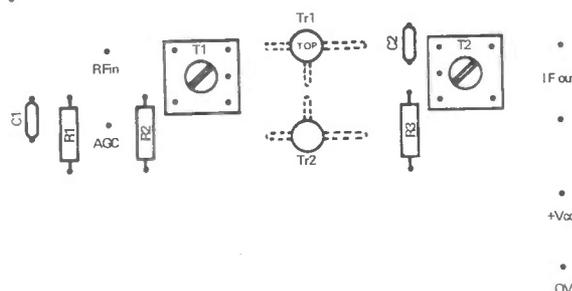


Fig 11: Component overlay



DATA FILE

Ray Marston presents the first of a four-part in-depth survey of op-amp principles and applications. This month he concentrates on basic principles and configurations

A conventional operational amplifier (op-amp) can be simply described as a high-gain direct-coupled voltage amplifier 'block' that has a single output terminal but has both inverting and non-inverting input terminals, enabling the device to function as either an inverting, non-inverting or differential amplifier. Op-amps are very versatile devices: when coupled to suitable feedback networks they can be used to make precision AC and DC amplifiers and filters, oscillators, level switches and comparators, to name but a few.

Three basic types of operational amplifier are currently available. The most important of these is the conventional 'voltage-in voltage-out' op-amp (typified by the 741 and the 3140), and in this and the next three editions of 'Data File' we'll take an in-depth look at the operating principles and practical applications of this type of device. The other two are the current-differencing or Norton op-amp, and the operational transconductance amplifier or OTA; we've already taken in-depth looks at both of these types of device in earlier editions of 'Data File' (April—June 1983).

Op-amp basics

In its simplest form, a conventional op-amp consists of a differential amplifier (bipolar or FET) followed by offset compensation and output stages, as shown in Figure 1; all of these elements are integrated on a single chip and

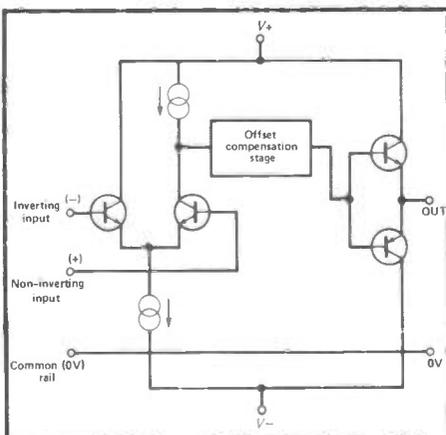


Fig 1 Simplified op-amp equivalent circuit

housed in an IC package. The differential amplifier has inverting and non-inverting input terminals and has a high-impedance (constant-current) tail to give a high input impedance and a high degree

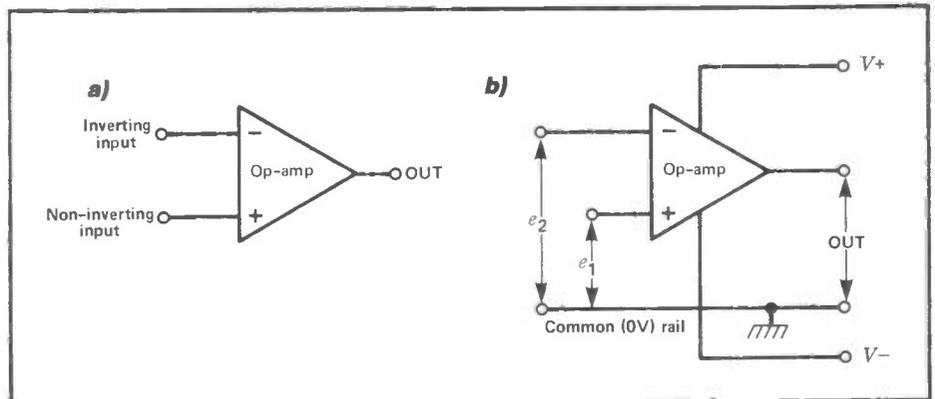


Fig 2 a) Basic symbol and b) Supply connections for an op-amp

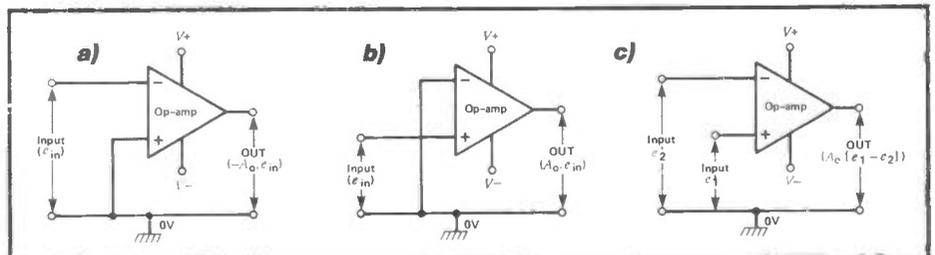


Fig 3 Methods of using an op-amp as a high gain, open-loop, linear amplifier. a) Inverting DC amplifier, b) Non-inverting DC amplifier, and c) Differential DC amplifier

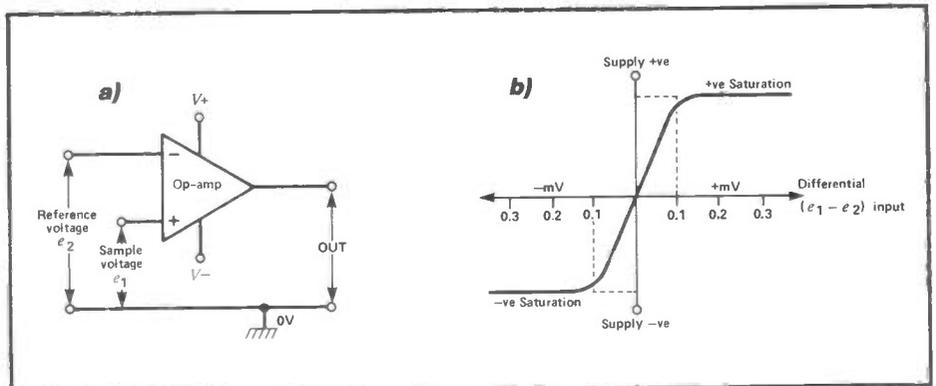


Fig 4 a) Circuit and b) Transfer characteristics of a simple differential voltage comparator

of common-mode signal rejection. It also has a high-impedance collector (or drain) load, to give a large signal-voltage gain (typically about 100dB).

The output of the differential amplifier is fed to the circuit's output stage via an offset compensation network, which causes the op-amp output to centre on 0V when both input terminals are tied to 0V. The output stage takes the form of a complementary emitter follower and gives a low-impedance output.

Op-amps are represented by the

standard symbol shown in Figure 2a, and they are normally powered from split supplies, as shown in Figure 2b. This arrangement provides +ve, -ve and common (0V) supply rails, enabling the op-amp's outputs to swing either side of zero and to be set at 0V when the differential input voltage is zero.

Basic configurations

We have seen that the op-amp is a high-gain direct-coupled voltage amplifier with a high input impedance and a low

OP-AMP PARAMETERS

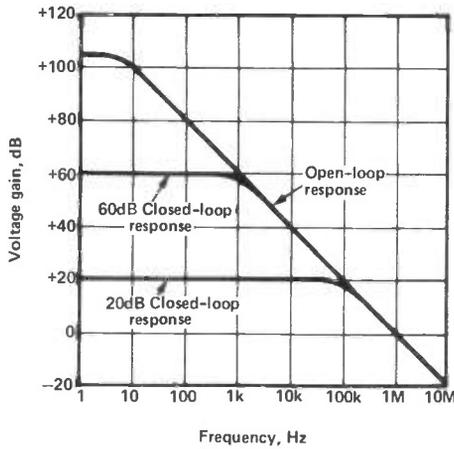


Fig A Typical frequency response curve for the 741 op-amp

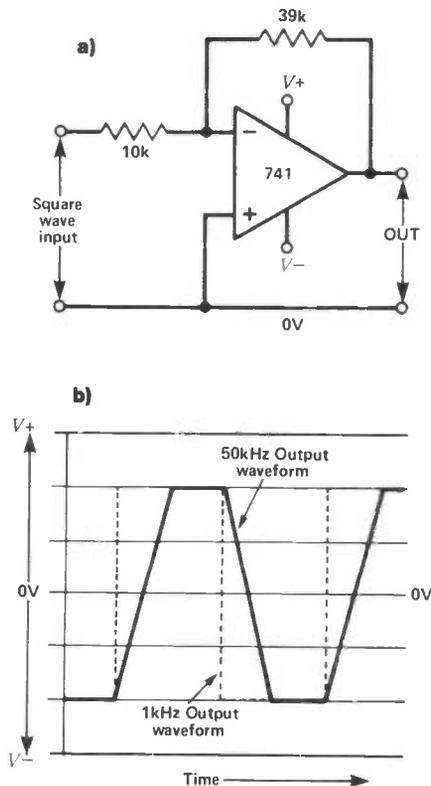


Fig B Effect of slew-rate limiting on the output of an op-amp fed with a square-wave input

An ideal op-amp would have infinite values of input impedance, gain and bandwidth, as well as zero output impedance and the ability to execute perfect tracking between input and output. Practical op-amps fall short of all these ideals. Consequently, various performance parameters are detailed in op-amp data sheets that indicate the 'goodness' of a particular device. The most important of these parameters are detailed below.

A_o (Open-loop voltage gain):

This is the low-frequency voltage gain that appears between the input and output terminals of the op-amp, and may be expressed in direct terms or in terms of dB. Typical figures are 100 000 or 100dB.

Z_{in} (Input impedance):

This is the resistive impedance looking directly into the input terminals of the op-amp when used open-loop. Typical values are 1Mohm for op-amps with bipolar input stages and a million megohms for FET-input op-amps.

Z_o (Output impedance):

This is the resistive output impedance of the basic op-amp when used open-loop. Values of a few hundred ohms are typical of most op-amps.

I_b (Input bias current):

The input terminals of all op-amps sink or source finite currents when biased for linear operation. The magnitude of this current is denoted by I_b, and it is typically a fraction of a microamp in bipolar op-amps or a few picoamps in FET types.

V_s (Supply voltage range):

Op-amps are usually operated with split (+ve and -ve) supply rails, and these have both maximum and minimum limits. If voltages are too high the op-amp may be damaged, but if they are too low the op-amp will not function correctly. Typical limits are ±3V to ±15V.

V_{i(max)} (Input voltage range): Most op-amps will only operate correctly if their input terminal voltages are below the supply line values. V_{i(max)} is typically one or two volts less than V_s.

V_{io} (Differential input offset voltage):

In an ideal op-amp, perfect tracking would exist between the input and output terminals and the output would register zero with both inputs grounded. In practice, slight imbalances within the op-amp cause the device to act under these conditions as though a small offset or bias voltage exists on its inputs. Typically, this 'differential input offset voltage' has a value of only a few mV, but when this voltage is amplified by the gain of the circuit in which the op-amp is used, it may be sufficient to drive the op-amp output well away from the 'zero' value. Because of this, most op-amps have some facility for externally nulling out the effects of this offset voltage.

CMRR (Common mode rejection ratio):

An op-amp produces an output proportional to the difference between the signals on its two input terminals. Ideally, it should give zero output if identical signals are applied to both inputs simultaneously, i.e. in common mode. In practice, such signals do not entirely cancel out within the op-amp and so there is a small output signal. The ability of an op-amp to reject common mode signals is usually expressed in terms of its 'common mode rejection ratio', i.e. the ratio of the op-amp's gain with differential signals to the gain with common mode signals. CMRR values of 90dB are typical of most op-amps.

f_t (Transition frequency):

An op-amp typically gives a low-frequency voltage gain of about 100dB and, in the interest of stability, its open-loop frequency response is internally tailored so that the gain falls off as the frequency rises. That frequency at which it falls to unity is known as its transition frequency and is denoted by f_t. The response usually falls off at a rate of 6dB per octave or 20dB per decade. Figure A shows a typical response curve for a type 741 op-amp, which has an f_t of 1MHz and a low frequency gain of 106dB.

It should be noted that when the op-amp is used in a closed-loop amplifier circuit, the bandwidth of the circuit depends on the closed-loop gain. Thus, in Figure A, if the amplifier is used to give a gain of 60dB its bandwidth is only 1kHz, but if it is used to give a gain of 20dB its bandwidth is 100kHz. The f_t value can thus be used to represent a gain-bandwidth product.

Slew Rate:

As well as being subject to normal bandwidth limitations, op-amps are also subject to a phenomenon known as slew rate limiting which has the effect of limiting the maximum rate of change of voltage at the output of the device. Figure B shows the effect that slew rate limiting can have on the output of an op-amp that is fed with a square-wave input. Slew rate is normally specified in terms of volts per microsecond, and values in the range 1-10V/μs are usual with most popular types of op-amp. One effect of slew rate limiting is to make a greater bandwidth available to small output signals than is available to large output signals.

output impedance. In practice, the output signal voltage of an op-amp is proportional to the differential signal voltage between its two input terminals, and is given by

$$e_{out} = A_o (e_1 - e_2)$$

where A_o is the open-loop voltage gain of the op-amp (typically 100 000), e₁ is the signal voltage at the non-inverting input terminal, and e₂ is the signal voltage at the inverting input terminal.

Thus an op-amp can be used as a high-gain inverting amplifier by grounding the non-inverting terminal and feeding the input signal to the inverting terminal (see Figure 3a). Alternatively it can be used as a non-inverting amplifier by

continued on page 46

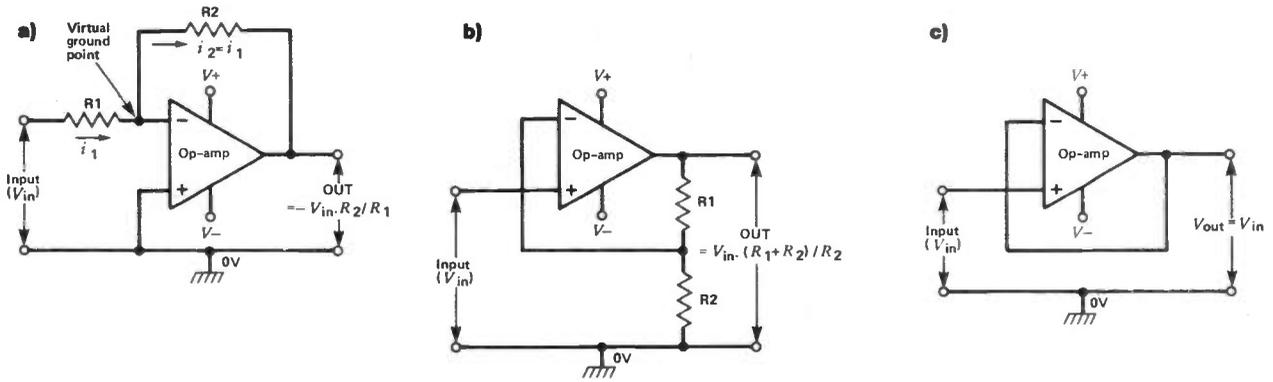


Fig 5 Closed-loop linear amplifier circuits. a) Inverting DC amplifier; b) Non-inverting DC amplifier; and c) Voltage follower

reversing the two input connections (Figure 3b), or as a differential amplifier by feeding the two input signals to the op-amp (Figure 3c). In the latter case, note that if identical signals are fed to both input terminals the op-amp should, ideally, give zero signal output.

The voltage gains of the above circuits depend on the open-loop voltage gains of the individual op-amps that are used, and are thus subject to wide variations. Consequently, op-amps are rarely used in open-loop mode as linear amplifiers.

One special application of the 'open-loop' op-amp is as a differential voltage comparator, one version of which is shown in Figure 4a. Here, a fixed reference voltage is applied to the inverting terminal and a variable test or sample voltage is fed to the non-inverting terminal. Because of the very high open-loop voltage gain of the op-amp, the output is driven to positive saturation (close to the +ve rail value) when the sample voltage is more than a few hundred microvolts above the reference voltage, and to negative saturation (close to the -ve supply rail value) when the sample is more than a few hundred microvolts below the reference value.

Figure 4b shows the voltage transfer characteristics of the above circuit. Note that it is the magnitude of the input differential voltage that determines the magnitude of the output voltage, and that the absolute values of input voltage are of little importance. Thus, if a 2V reference is used and a differential voltage of only 200µV is needed to swing the output from a negative to a positive saturation level, this change can be caused by a shift of only 0.01% on the 2V signal applied to the sample input. The

circuit thus functions as a precision voltage comparator or balance detector.

Closed-loop amplifiers

The most useful way of using an op-amp as a linear amplifier is to connect it in the closed-loop mode, with negative feedback applied from the output to the input, as portrayed in the circuits of Figure 5. This technique enables the overall gain of each circuit to be precisely controlled by the values of the external feedback components, almost irrespective of the op-amp characteristics (provided that the open-loop gain A_o is large relative to the closed-loop gain A).

Figure 5a shows how to wire the op-amp as a fixed-gain inverting DC amplifier. Here, the gain (A) of the circuit is dictated by the values of R_1 and R_2 and equals R_2/R_1 , while the input impedance of the circuit equals R_1 . Thus the circuit can readily be designed to give any desired values of gain and input impedance.

It should be noted, however, that although R_1 and R_2 control the gain of the complete circuit, they have no effect on the parameters of the actual op-amp. Thus the inverting terminal still has a very high input impedance and negligible signal current flows into the terminal. Consequently, virtually all of the R_1 signal current also flows in R_2 , and signal currents i_1 and i_2 can be regarded as being equal, as indicated in the diagram. Also note that R_2 has an apparent value of R_2/A when looked at from the inverting terminal, making the R_1 - R_2 junction a low-impedance 'virtual ground' point.

Figure 5b shows how to connect the op-amp as a fixed-gain non-inverting

amplifier. In this case the voltage gain equals $(R_1 + R_2)/R_2$ and the input impedance is approximately $(A_o/A)Z_{in}$, where Z_{in} is the open-loop input impedance of the op-amp. The above circuit can be made to function as a precision voltage follower by connecting it as a unity-gain non-inverting amplifier. This is shown in Figure 5c, where the op-amp operates with 100% negative feedback. In this case the input and output signal voltages are identical but the input impedance of the circuit is very high, being approximately $A_o Z_{in}$.

The basic op-amp circuits of Figure 5 are those for DC amplifiers, but they can readily be adapted for AC use.

Practical op-amps

Op-amps also have many applications other than as simple linear amplifiers. They can be made to function as precision phase splitters, as adders or subtractors, as active filters or selective amplifiers, as precision half-wave or full-wave rectifiers, or as oscillators or multivibrators, for example.

Practical op-amps are available in a variety of IC technologies (bipolar, MOSFET, JFET, etc), and in a variety of types of packaging (plastic DIL, metal-can TO5, etc). Some of these packages house two or four op-amps, all sharing common supply line connections. Table 1 lists the parameters, while Figure 6 gives the corresponding outline details of eight popular 'single' op-amp types, all of which use 8-pin DIL (DIP) packaging.

Among the bipolar types, the 741 is a general purpose op-amp featuring internal frequency compensation and overload protection on inputs and output, while the NE531 is a high-performance

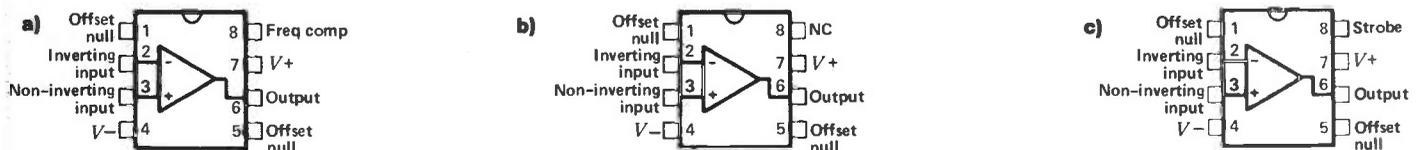


Fig 6 Parameter and outline details of eight popular 'single' op-amp types

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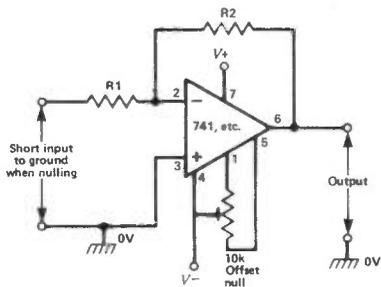


Fig 7 Typical offset nulling system

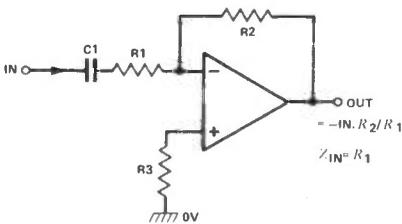


Fig 8 Inverting AC amplifier

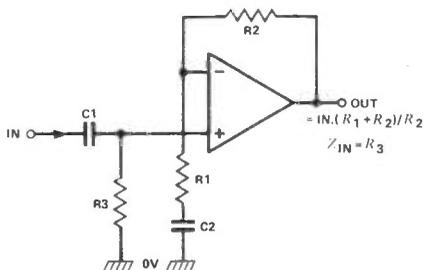


Fig 9 Non-inverting AC amplifier

type which can handle a very high slew rate. In the latter case, an external compensation capacitor (of, say, 100pF), wired between pins 6 and 8, is needed for stability, but this could be reduced to a very low value (say 1.8pF) if a very wide bandwidth at high gain is desired.

The CA3130 and CA3140 MOSFET-input type op-amps can operate from either single or dual power supplies, can sense inputs down to the negative supply rail value, have very high input impedances (1.5Tohms, i.e. 1.5×10^6 Mohms) and have outputs that can be strobed. The CA3130 has a CMOS output stage, and an external compensation capacitor (typically 47pF) between pins 1 and 8 permits adjustment of bandwidth characteristics. The CA3140 has a bipolar output stage and is internally compensated.

The LF351, 411, 441 and 13741 are JFET type op-amps with very high input impedances. The LF351 and 411 are high performance types, while the LF441 and 13741 are general purpose devices that can be used as direct replacements for the very popular 741. Note that the LF441 quiescent current consumption is less than one tenth of that of the 741.

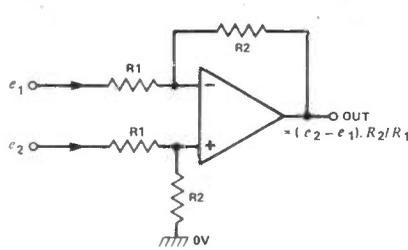


Fig 10 Differential amplifier or analogue subtractor

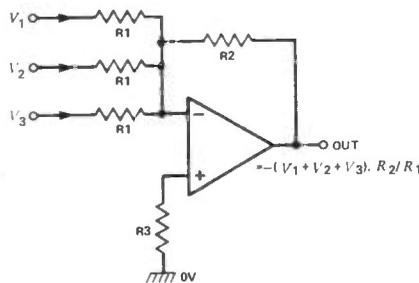


Fig 11 Inverting analogue adder or audio mixer

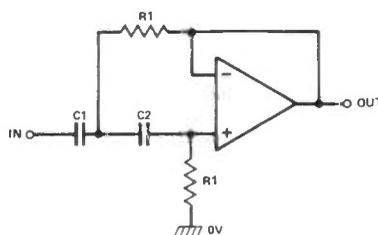


Fig 12 High-pass second-order active filter

Offset nulling

All of the above op-amps are provided with an offset nulling facility to enable the output to be set precisely to zero when the input is zero. In most cases, offset nulling is achieved by wiring a 10k pot between pins 1 and 5 and connecting the pot slider to the negative supply rail (pin 4) either directly (as shown in *Figure 7*) or via a 4k7 'range limiting' resistor. In the case of the CA3130, a 100k offset nulling pot must be used.

Applications roundup

Operational amplifiers are very versatile devices, and can be used for a wide variety of linear and switching roles. *Figures 8—22* show a small selection of the basic 'applications' circuits that can be used. In most of these diagrams, the supply line connections have been omitted for the sake of clarity. We shall be looking at these circuits in greater detail in the next three editions of the 'Data File', but for now just a flavour of how they operate.

Figures 8 and 9 show how op-amps can be used to make fixed-gain inverting and non-inverting AC amplifiers, respectively. In both cases, the gain and the

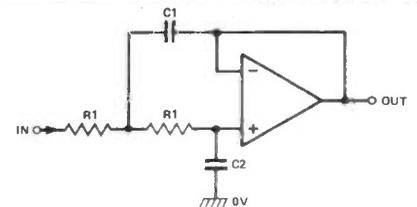


Fig 13 Low-pass second-order active filter

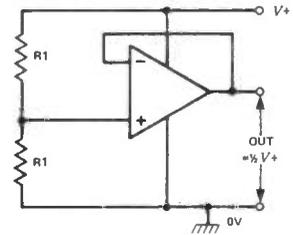


Fig 14 Supply-line splitter

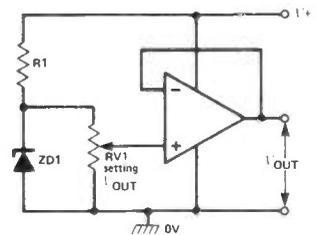


Fig 15 Adjustable voltage reference

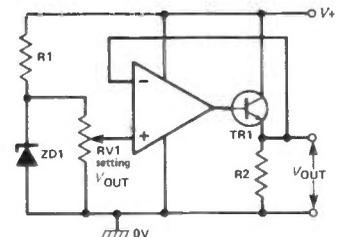


Fig 16 Adjustable voltage power supply

input impedance of the circuit can be precisely controlled by suitable component value selection.

Figure 10 shows how to make a differential or difference amplifier with a gain equal to R_2/R_1 ; if R_1 and R_2 have equal values, the circuit acts as an analogue subtractor.

Figure 11 shows the circuit of an inverting 'adder' or audio mixer; if R_1 and R_2 have equal values, the inverted output is equal to the sum of the input voltages.

Op-amps can be made to act as precision active filters by wiring suitable filters into their feedback networks. *Figures 12 and 13* show the basic connections for making second-order high-pass and low-pass filters, respectively; these circuits give roll-offs of 12dB/octave. We'll look at more sophisticated versions of these circuits next month.

Figures 14—16 show some useful applications of the basic voltage

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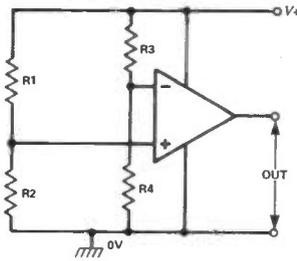


Fig 17 Bridge-balance detector/switch

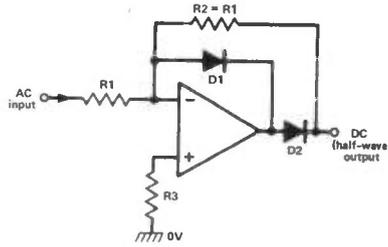


Fig 18 Precision half-wave rectifier

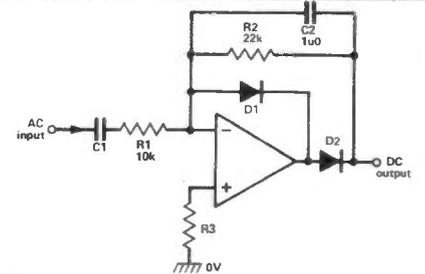


Fig 19 Precision half-wave AC/DC converter

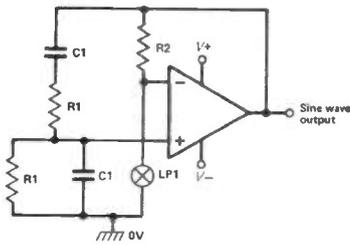


Fig 20 Wien Bridge sine-wave generator

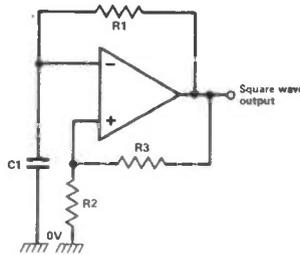


Fig 21 Free-running multivibrator

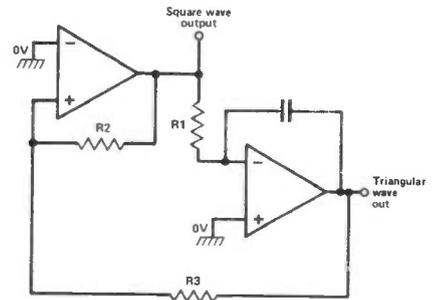


Fig 22 Sine/square-wave function generator

follower or unity-gain non-inverting DC amplifier. The first of these circuits acts as a supply-line splitter and is useful for generating split supplies from single-ended ones, while the second acts as a semi-precision variable voltage reference. The last member of this group shows how the output current drive can be boosted so that the circuit acts as a variable voltage power supply.

Figure 17 shows the basic circuit of a bridge-balance detector, in which the output swings high when the inverting

pin voltage is above that of the non-inverting pin, and vice versa. This circuit can be made to function as a precision opto- or thermo-switch by replacing one of the bridge resistors with an LDR or thermistor.

Figures 18 and 19 show how to make precision half-wave rectifiers and AC/DC converters. These are very useful instrumentation circuits.

Finally in this edition of the 'Data File', Figures 20—22 show some useful waveform generator circuits. The first of these

designs uses a Wien Bridge network to generate a good sine wave, amplitude stabilisation being obtained via a low-current lamp, while Figure 21 is a very useful square-wave generator circuit in which the frequency can be controlled via any one of the passive component values. The frequency of the last function generator circuit (Figure 22) can also be controlled via any one of its passive component values, but this particular design generates both square and triangular waveforms.

Parameter	Bipolar op-amps		MOSFET op-amps		JFET op-amps			
	741	NE531	CA3130E	CA3140E	LF351	LF411	LF441	LF13741
Supply voltage range	±3V to ±18V	±5V to ±22V	±2.5V to ±8V or 5V to 16V	±2V to ±18V or 4V to 36V	±5V to ±18V			
Supply current	1.7mA	5.5mA	1.8mA	3.6mA	800µA	1.8mA	150µA	2mA
Input offset voltage	1mV	2mV	8mV	5mV	5mV	0.8mV	1mV	5mV
Input bias current	200nA	400nA	5pA	10pA	50pA	50pA	10pA	50pA
Input resistance	1MΩ	20MΩ	1.5TΩ	1.5TΩ	1TΩ	1TΩ	1TΩ	0.5TΩ
Voltage gain, A _o	106dB	96dB	110dB	100dB	88dB	106dB	100dB	100dB
CMRR	90dB	100dB	90dB	90dB	100dB	100dB	95dB	90dB
f _T	1MHz	1MHz	15MHz	4.5MHz	4MHz	4MHz	1MHz	1MHz
Slew rate	0.5V/µs	35V/µs	10V/µs	9V/µs	13V/µs	15V/µs	1V/µs	0.5V/µs
8-pin DIL outline (referred to Figure 6)	b	a	c	c	b	b	b	b



Photo 1: The 156 PMD mine detector in use. The aerials (two transmitting, one receiving) and the transmission lines are mounted on a laminated glass cloth plate in a search head 22cm square.

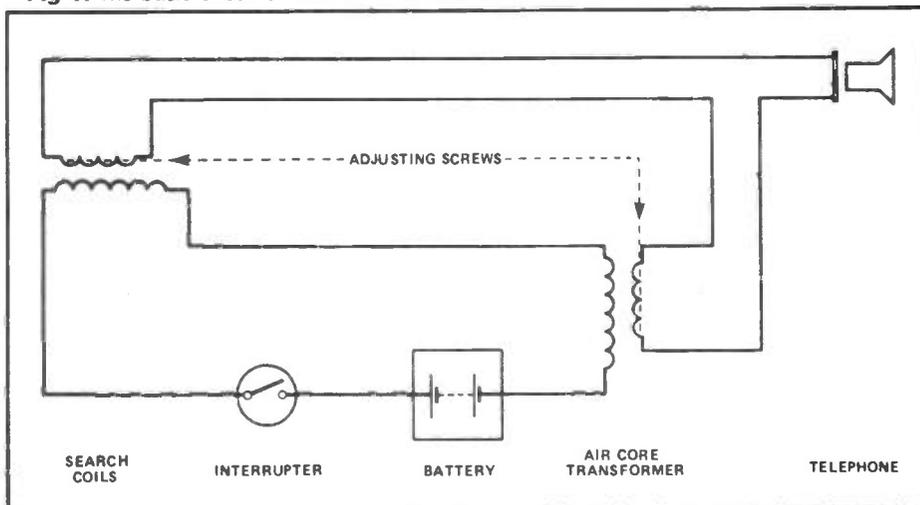
METAL DETECTORS IN WARFARE

Richard Turner describes the various military applications to which metal detectors have been put over the last 100 years

On 15th May 1879, Professor David Edward Hughes demonstrated his latest discovery to the Royal Society in London, and in closing his address he invited inventors to exploit his 'Induction Balance' to the full in physics, medicine and metal detection. As was described earlier in *R&EW* (April '82), the attempted assassination of America's 20th President, James Garfield, in July 1881 led Alexander Graham Bell to build an instrument for locating bullets and other metal objects within the human body, based on the induction balance principle (see *Figure 1*) — though he called on a different phenomenon in developing his second medical metal-detecting device, the Telephonic Probe.

The use of the induction balance for military purposes was apparent just as quickly, with a British Patent being

Fig 1: The basic circuit of Alexander Graham Bell's 1881 induction balance metal detector.



granted in December 1881 for a 'Submarine and shipwreck finder. This was soon followed by a 'Metal shell and land mine locator' and an 'Automatic sea mine using the Hughes induction balance as sentinel'. In 1885 the Royal Army Medical Corps developed their own metal detector — quite distinct from those of Alexander Graham Bell — specifically for locating bullets and shrapnel in wounded servicemen.

These very much set the pattern for the way metal detection has contributed to military strategy. However it is interesting to look more closely at the applications themselves and at the way metal detection is achieved in each case.

Finding bombs

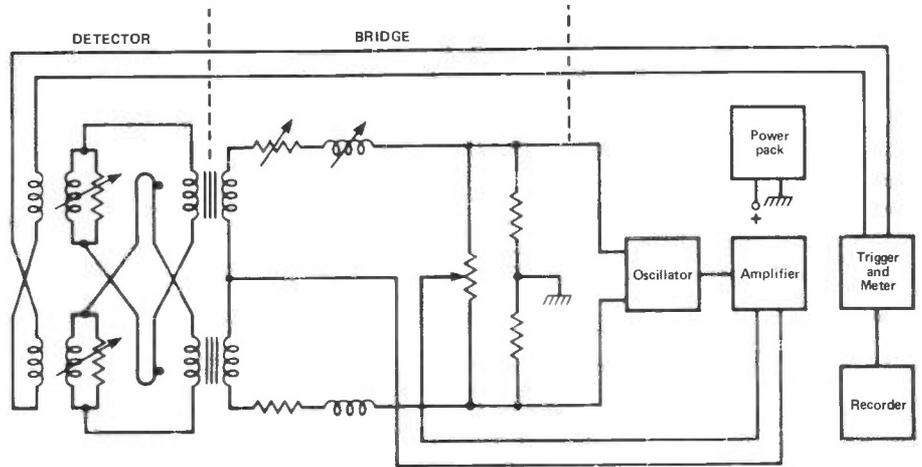
One of the prime movers (as far as the UK was concerned) in the development of ways of locating bombs was the intensive bombing of our cities in the spring of 1940. There was an urgent need for devices that could seek out the many bombs that failed to explode — some having faulty mechanisms, others incorporating delay fuses. The alternative was perpetual fear of imminent explosions.

Locating bombs beneath city streets is complicated by the nature of the subsurface: pipes and sewers can readily deflect any bomb off its course. A good example is the bomb which fell on 11th September 1940 in St Pauls Churchyard in London. It penetrated to a depth of eight feet from the point of impact before changing its course, only to be found later at a depth of 27½ feet lodged in the foundations of the Cathedral!

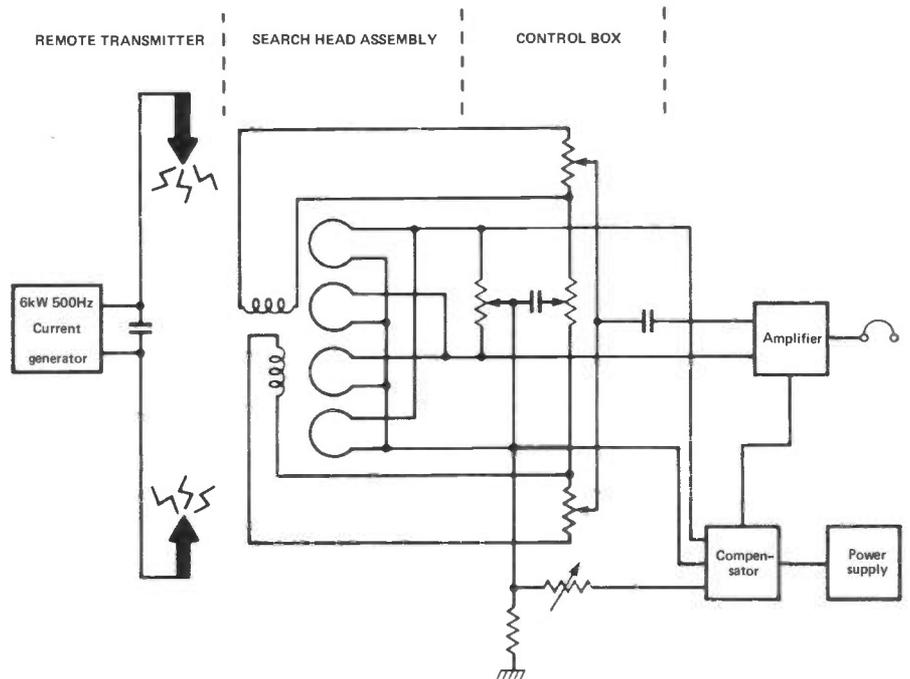
Naturally Winston Churchill gave high priority to the development of bomb and mine locators, and by August 1940 no fewer than nine laboratories had assigned their top scientists and engineers to the task. The locator adopted for the task was that designed by Mr A Butterworth and developed at ERA Laboratories by a team led by Mr L H Daniel.

The ERA bomb locator was basically a differential magnetometer, an appropriate choice since bombs contain very large amounts of ferromagnetic material. Briefly it consisted of a Maxwell impedance-measuring bridge with two adjacent arms both in the detector unit but separated in the vertical plane by about three feet. These arms incorporated mu-metal wires as the sensors because their inductance and resistance varies with the magnetic field along the axis of the wire.

The equipment consisted of a search unit, mounted on a pole and connected by a cable to the case containing the electronics, and two borehole probes. The former was only used to confirm the presence and the general location of the bomb, its precise position being established by the borehole probes. The latter procedure involved at least three holes being dug and measurements being plotted on a chart that gave the location, depth and size of the bomb to the nearest inch. This enabled a shaft to be dug directly over the bomb, facilitating defusing and subsequent disposal.

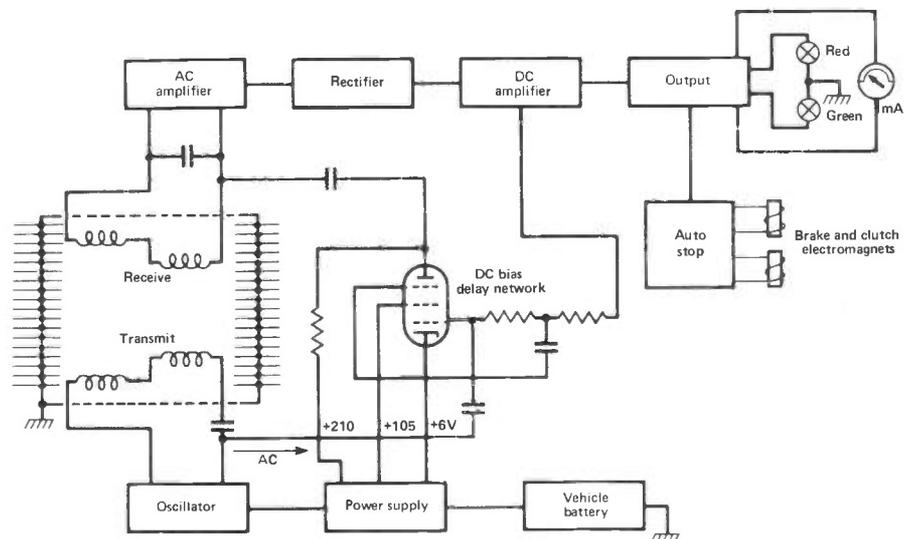


Above ERA Bomb Locator. The mu-metal elements are shown as variable R-L elements



Above No 7 deep seeking mine locator

Below Vehicle-mounted transmit/receive mine detector, dating back to World War II



The prototype was capable of detecting a 1000kg bomb at a depth of 20 feet and it was brought into service in March 1941, its manufacture being assigned to British-Thomson-Houston.

Finding mines

Deep seeking land mine detectors were also developed by ERA, in particular the No 7 locator designed by ERA's then Director, Dr Stanley Whitehead, and Mr Benjamin Rosenblum. (The No 1 locator had been developed in 1938 by the Signals Experimental Establishment, while those most widely used at the time — numbers 3 and 4 — were designed by Mr Stanley Spencer West of Cinema-Television Ltd).

The operating principle of this device was as follows:

A heavy duty current was established by a petrol-driven generator, tuned to 500Hz (audio) by a capacitor and injected into the ground by means of a two-turn 150x300-yard induction loop. Several operators would then use balanced coil search units to seek out deeply-buried land mines.

This method produced very rapid and positive results, and it was mainly used in clearing mines from beaches and marshy areas where the mines often sank out of the range of conventional detectors.

If anti-personnel or AC-sensitive mines were suspected, a 'probe injection' method would be used first, whereby probes would be inserted into the ground and the search team would take cover before the main current was switched on. Any AC-sensitive devices in sufficiently close proximity to the probes would explode, and the search coils could then be used in the normal way to pick out the remaining mines because they do not themselves transmit any AC fields.

Tank- and other vehicle-mounted mine detectors are typically based on the transmit/receive (T/R) technology that came with the advent of 'Wireless'. Here the search coils are mounted on a boom and electrostatically screened to prevent the generation of false signals by vegetation or minerals within the ground. The presence of a mine is either indicated on a meter or turned into an audio signal heard through headphones. An automatic braking system is often an adjunct to these detectors.

The current 'mainstay' of the British and NATO forces is the No 4C mine detector manufactured in England by United Scientific Instruments. This operates on the principles established by Professor Hughes and has two modes of operation — normal mode and 'pave' mode for use where there is significant contamination by ferrous metals. This device is capable of operating over a very wide temperature range and has proved itself on active service throughout the world.

Over the years, many electronic innovations have made their appearance on mine detectors, some of the more important ones being temperature and frequency compensation, non-inductive search coils and phase angle discrimination.



Photo 2: The No 4C mine detector. This operates on the induction balance principle and has a 28.5cm search head and solid state electronics.

Airborne and marine applications

Detecting enemy submarines through their metal content has always been well exploited by the Royal Navy, the induction balance being the first method to be used here. However, the advent of the transmit/receive technique gave a much greater range. The transmitters were mounted on one ship or aircraft while the receivers were on other ships or aircraft. As a result, several miles of sea could be scanned at any one time.

The induction coil principle has also been used for detecting submarines, a good example of this being the construction of the world's largest ever metal detector — an induction coil laid across the Straits of Gibraltar. Its purpose was to spot German U-boats which would otherwise avoid detection through turning off their engines and floating out of the Mediterranean Sea into the Atlantic Ocean with the aid of the tide. Similar devices — but on a smaller scale — made a significant contribution to the defence of Singapore.

Nowadays both ships and aircraft are

equipped with magnetometers for the purpose of spotting submarines as this system's high level of sensitivity enables, for example, just one aircraft to cover several cubic miles of sea.

An interesting application of metal detection technology is for the ignition of anti-aircraft shells, the philosophy being that an explosion near to an aircraft is better than a complete miss. A near explosion will often result in a piece of shrapnel lodging in a vital part such as a fuel tank or some control, thus doing as much damage as a direct hit. The 'Aerial mine' (or 'Proximity fuse', as it is now known) was developed in the early days of World War II. This is based on the transmit/receive technique and the power for the electronics is supplied by a wind generator. This means that the shell has to be fully airborne before it has sufficient velocity to generate the necessary current and so premature explosion triggered off by objects on the ground can be avoided.

But perhaps the least known application of a metal detector is its use as a sensor to explode a sea mine. The general idea is to lay the mine in enemy territory with the sensitivity preset to a level at which small unimportant ships do not trigger it, giving the enemy a false sense of security, while a cruiser or a battleship certainly would.

Conclusion

As it can be seen from this brief survey, metal detection has contributed a great deal to warfare technology both in the past — and the present. The recent events in the South Atlantic have proved once again that mine warfare is a very lethal weapon. The indiscriminate mining of huge areas of the Falklands by the Argentinians has once again focussed attention on mine detecting devices. Due to the nature of the terrain and the type of mines used, their clearance is a very dangerous and slow process.

But technology has met the challenge in the form of the British made 156 PMD mine detector from the USI Group of companies. Using T/R technology, this detector emits an RF field in the 300—500MHz band; it is thus able to detect plastic and metal mines in any terrain at any temperature between -32 and $+52^{\circ}$. Lithium batteries provide the power for the 16-bit microprocessor-controlled electronics that generate and receive signals via aerials contained in the search head. In the null condition, one click is emitted per 2.5 seconds, indicating correct operational setting, while on detection the pulse rate varies from 3 to 150 clicks per second depending on the proximity and size of mine.

Photo 1 shows this detector being used in the crawler mode employed by commandos sussing out enemy defences. It can be equally used in the conventional walk and sweep mode by extending the handle to 1.2m and clipping the electronics box to the operator's belt. The latest reports from Falkland Islands indicate that the 156 PMD is making a great contribution towards the return of life to normal in those islands.

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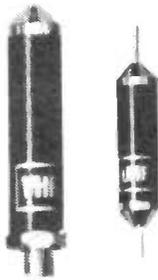
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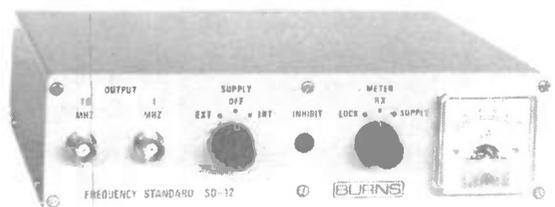
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BLOCK CAPS PLEASE

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LM1821S Video IF PLL synchronous detector

Despite recent rationalisation of its linear IC range (which has resulted in the loss of, amongst others, the LM373/374 families), National Semiconductor still has a storehouse full of interesting linear devices. The magnitude of the National Linear Data Book bears witness to this fact: it's easily the biggest book on the R&EW databook shelf.

The LM1821S featured here is one of National's cornucopia of TV circuits. It wasn't easy to actually lay hands on the device from a National distributor, but since they sent us a press release implying they would welcome promotion, we trust that readers wishing to explore some of the promise of this circuit will not have too much trouble persuading their National distributor to cough up the goods.

The device is a combination video IF, with a PLL synchronous detector, an automatic fine tune circuit, a video output for sound extraction and a main video output with white spot noise inversion. The most interesting point on the data sheet is the fact that operation to 70MHz is cited as a feature. Satellite TV IFs are thus within its grasp — as well as applications in up-conversion communications receivers.

You can see from the simplicity of the external circuitry built around the block diagram (Figure 1) that National has paid

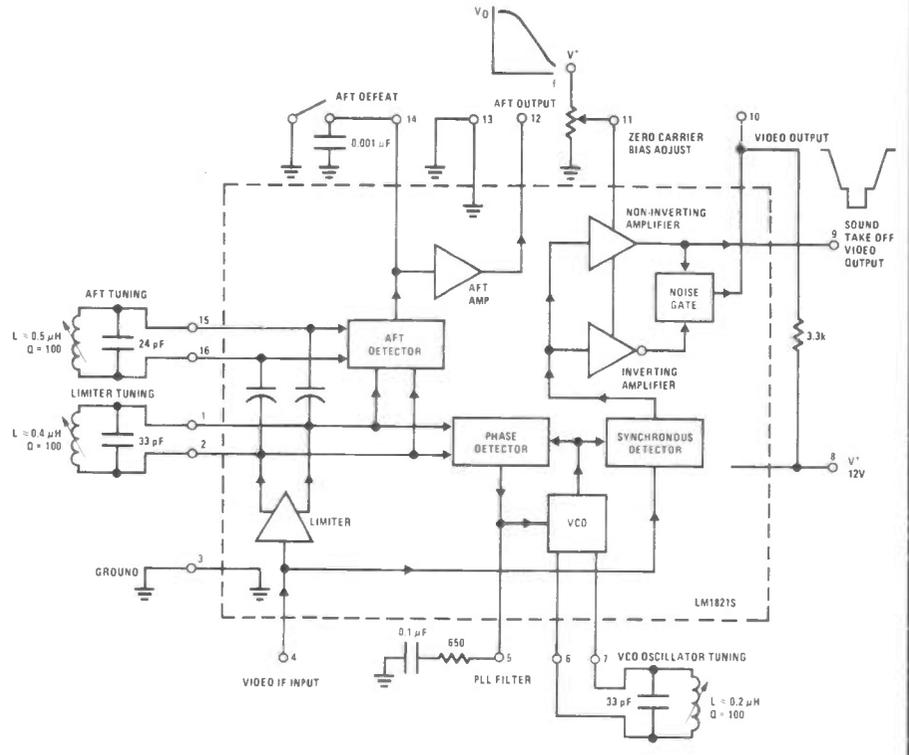


Figure 1: Block diagram

DC Electrical Characteristics (Reference Test Circuit, all SW position 1 unless noted)

Parameter	Conditions	Min	Typ	Max	Units
Supply Current, I _B + I ₁₀		35	55	75	mA
0 Carrier Adjust Voltage, V ₁₁	SW 1 Position 2	7.9	8.5	9.0	V
0 Carrier Output Voltage, V ₉	SW 1 Position 2	6.8	8.5	10.2	V
0 Carrier Bias Difference, V ₁₁ -V ₉	SW 1 Position 2		0	± 1.3	V
0 Carrier Output Voltage, V ₁₀	Adjust V ₁₁ for V ₉ = 7.0V	6.0	6.3	6.5	V
AFT Output Reference, V ₁₂		2.5	3.0	3.5	V

AC Electrical Characteristics (SW 2 position 2, V_{IN} = 100 mVrms, see Set-Up Procedure)

Parameter	Conditions	Min	Typ	Max	Units
Detector Gain, V ₁₀		2.3	3.6	4.4	V
Output Capability, V ₁₀	V _{IN} = 500 mVrms		1	2	V
AFT Maximum Output, V ₁₂	SW 4 Position 2, f _{IN} = 44.5 MHz	9	10		V
AFT Minimum Output, V ₁₂	SW 4 Position 2, f _{IN} = 45.5 MHz		0.4	1	V
APT Pull-In Range	Difference Between Upper and Lower Lock Frequencies	1	3		MHz
Noise Inversion Defeat Voltage	SW 3 Position 2, Adjust V ₅ for Beat Frequency at Pin 10, Measure Difference in (-) Peaks		0.3	± 0.6	V

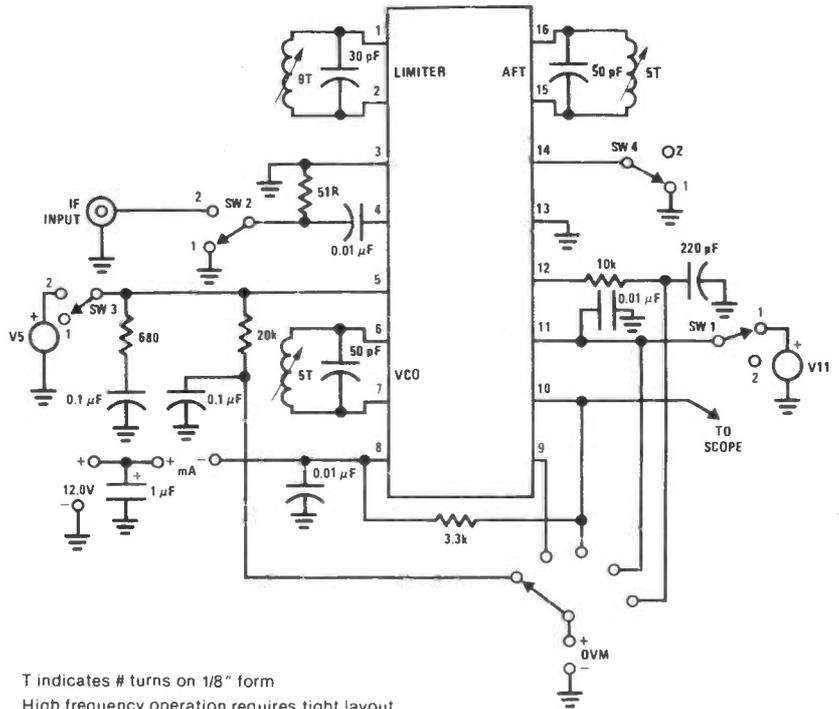


heed to the TV manufacturers' desire to minimise component count. The adjustments required are also a bare minimum, and it seems reasonable to expect that the PLL system will help in ensuring long-term stability and easy detector alignment.

The power supply requirement at 12V is fairly high at 55mA — a consequence of the high frequency of operation — so this device is not for battery-powered portable applications.

The AC parameter specification of this device is distinctly vague by National Semiconductor's usual standards, but a brief dabble with samples reveals that this device has potential at frequencies in the 10.7MHz range as well as at TV IF frequencies. Used in shortwave applications, the effects of synchronous demodulation on signals suffering from selective fading are usually worthwhile. The output at pin 5 is a representation of the FM on the signal. A little more time might reveal the effects of the noise inversion process on received noise.

The first two readers to send letters promising faithfully to have a good dabble with these useful devices, and to report their findings for other R&EW readers, get the spare samples we have in the office. First come, first served and no other correspondence can be entered into without an SAE.



T indicates # turns on 1/8" form
High frequency operation requires tight layout

Fig 2: Test circuit

Absolute Maximum Ratings

Power Supply Voltage	15V
Power Supply Current	100 mA
Input Signal Voltage	1 Vrms
Device Dissipation	1.5W
Thermal Resistance, θ_{JA}	55°C/W
Operating Temperature Range	0°C to +70°C
Storage Temperature Range	-65°C to +150°C
Lead Temperature (Soldering, 10 seconds)	265°C

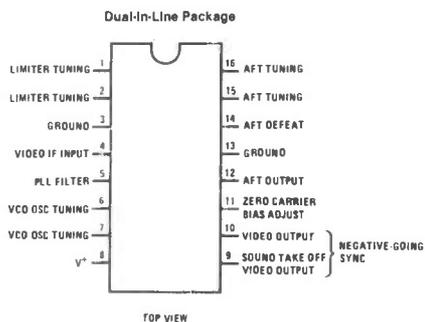
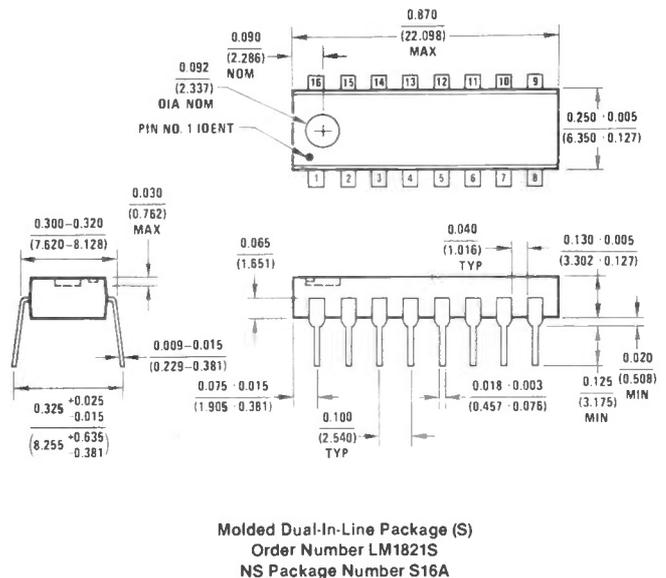


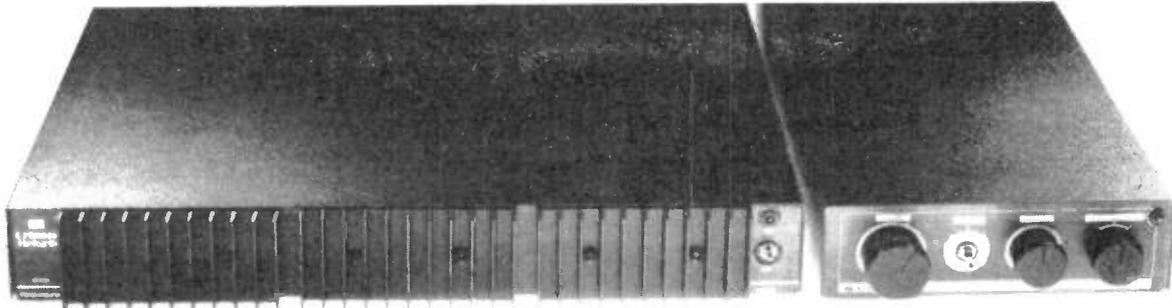
Fig 3: Connection diagram



Molded Dual-In-Line Package (S)
Order Number LM1821S
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Fig 4: Physical dimensions

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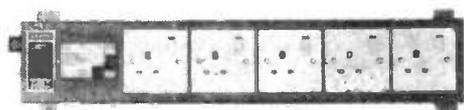
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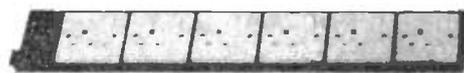
N13A/6



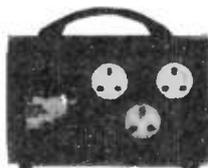
13A/5/R



13A/4SW



13A/6SW Sloping



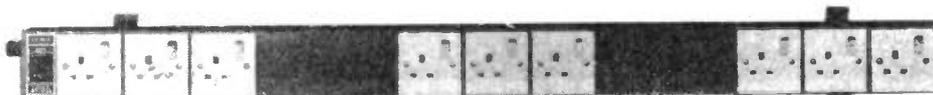
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This tester is based on a warbling alarm circuit.

Two gates are connected together as a square wave oscillator, while the output

gates another square wave oscillator whose output is in the audio spectrum... i.e. we can hear it. As all four gates are used, it should be obvious if one gate is 'duff'; it either won't work at all or it produces a non-warbling note when SW2 is pressed. (NB: It may produce a note when the supply is turned on. This should be ignored as it is the note produced when SW2 is closed that is important.)

Because the 4001 and the 4011 are opposite in their logic outputs, if a 4001 is inserted, SW2 when pressed will stop the warble, but if a 4011 is inserted, SW2 will start the warble. Thus the two devices can be easily differentiated. SW1 is included so that the supply can (as it

should) be disconnected when a device is being plugged in.

Construction

Either veroboard or a PCB can be used, and a PCB design is given in *Figures 2 and 3*. First mount the resistors, capacitors, and PCB socket. It might be wise to use a wire-wrap socket which stands proud of the PCB so that the unit can be housed in a shallow handheld case with the socket protruding through the front panel. Connect the switch(es), transducers and a battery, and then insert a good sample of both a 4011 and 4001 to check that the unit is functioning. So little current is taken in normal use that a PP3 battery should last several months.

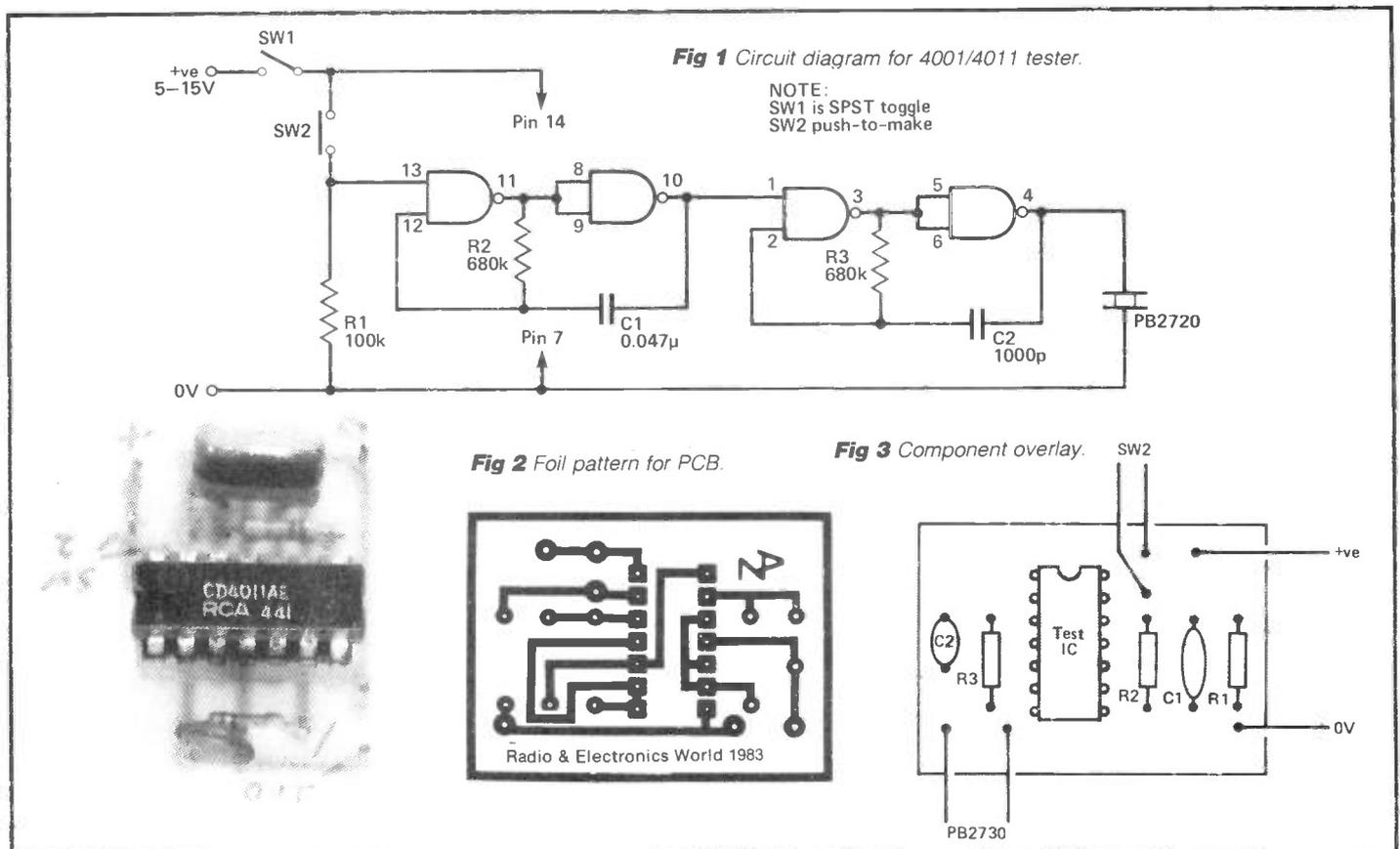


Fig 2 Foil pattern for PCB.

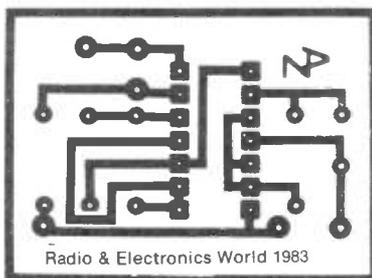
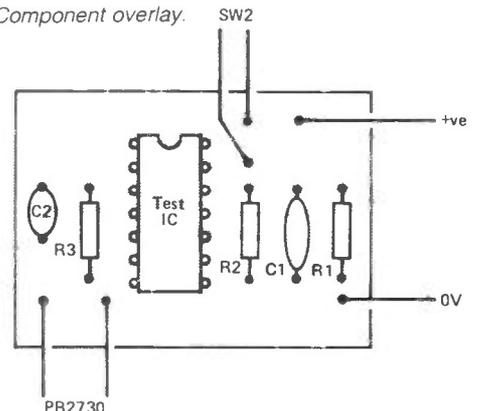


Fig 3 Component overlay.



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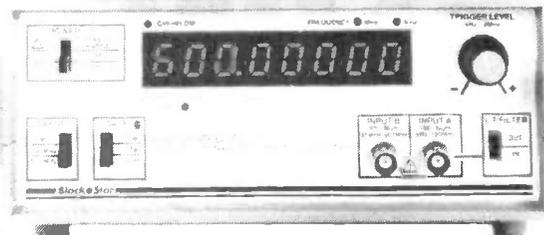
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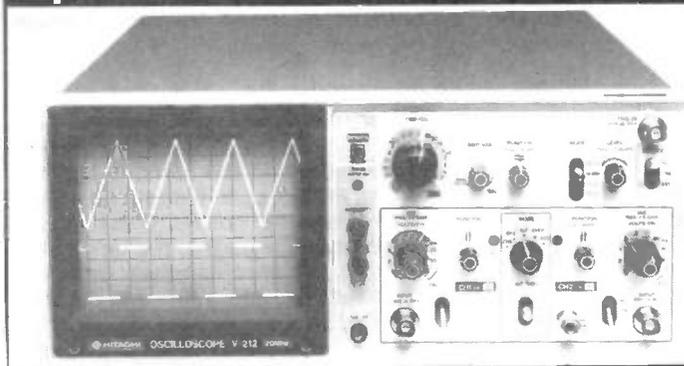
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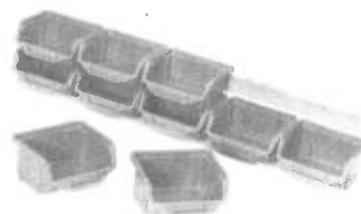
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TANTALUM CAPACITORS

David Francis takes an in-depth look at these compact — yet powerful — devices

Although it had been known for many years that tantalum was a highly suitable material for the manufacture of capacitors, it wasn't until the end of the 1950's that processing techniques and production methods were sufficiently refined to allow the large scale manufacture of reliable units.

The first production tantalum capacitor was based on knowledge gleaned from the manufacture of aluminium capacitors and so, naturally, resembled that type of component. Since then the tantalum foil capacitor has evolved and developed its own constructional techniques, as is evidenced by the gelled and solid tantalum slug units available today. Equally obvious is the fact that each style of capacitor has its own relevant attributes and drawbacks, and it is the intention of this article to enumerate some of the major differences between the models.

Gelled tantalum capacitors

The construction of a typical component of this type is shown in *Figure 1*. The anode is formed by mixing tantalum powder with an organic binder and pressing the mixture into a pellet. It is then sintered in a vacuum oven, which boils off all the organic products and leaves a pellet of high porosity and mechanical strength. After electrochemical treatment, anode leads are attached to the pellets, which are then sealed into cases filled with electrolyte. At this stage it should be noted that the most common form of electrolyte is a gelled form of sulphuric acid. Should one of these capacitors be ruptured, it is important that care be taken in handling the remains.

The gelled tantalum capacitor gives the highest concentration of capacitance per unit volume of all the available varieties and also gives the lowest leakage ratings. Both of these properties are demonstrated in *Table 1* which compares the three basic types of construction.

Regrettably it is not possible to make a non-polar version of a tantalum capacitor since, if reverse potential is applied, it causes destructive breakdown that ruins the component beyond redemption. It will, however, withstand very short intermittent reverse polarities, but

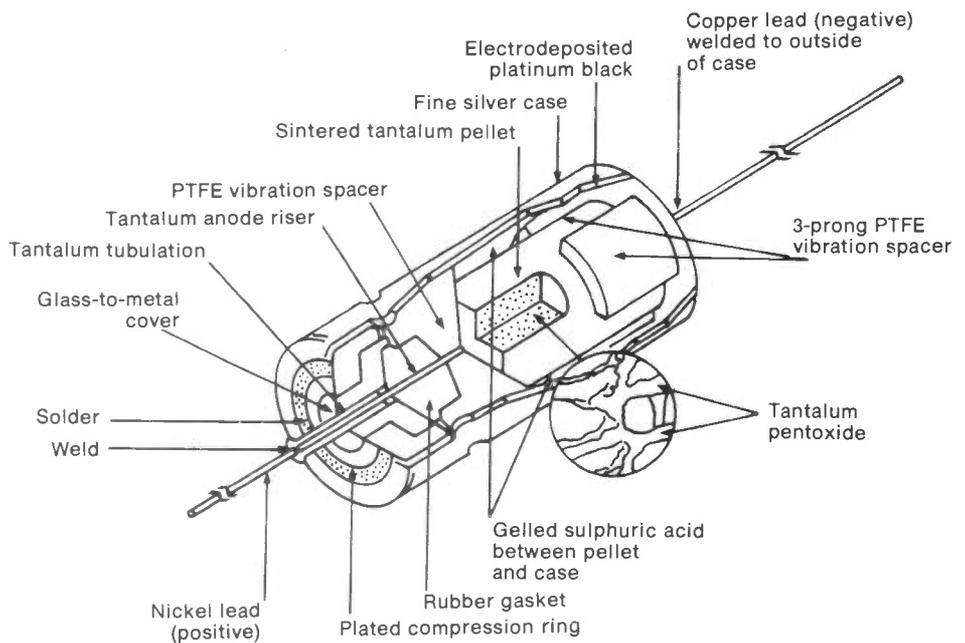


Fig 1 Structure of the gelled type of tantalum capacitor

it is not recommended that this factor should be relied on for obvious reasons.

On the advantageous side, these capacitors have extremely low self inductance and are capable of handling high ripple voltages — two factors which make them the ideal choice for use in the output filter of switch-mode power supplies. To verify this aptitude, tests were conducted whereby a number of capacitors were subjected to a 37Vdc

potential with a 15.5V_{RMS} ripple content. This was run for 2000 hours at a temperature of 85°C. As can be seen from *Table 2*, this only resulted in a small decrease in both the capacitance and the dissipation factor of each of the units under test.

Although these gelled capacitors are renowned for their longevity, they do eventually fail. However the mode of doing so is not immediately obvious

Table 1: Basic properties of tantalum capacitors

	Foil	Gelled	Solid
Maximum voltage	300	125	125
CV product	Flexible	Inflexible	Inflexible
Max temperature	125°C	175°C	125°C
Volume efficiency	Least	Highest	Next
DC leakage current	Next	Lowest	Highest
Reverse V _{dc} permissible	3V max	0	5% of rated V _{dc}
Parametric change	Highest	Next	Least
Mode of failure	Degradation	Degradation	Hi Z degradation Low Z catastrophic
Reliability	Least	Next	Highest

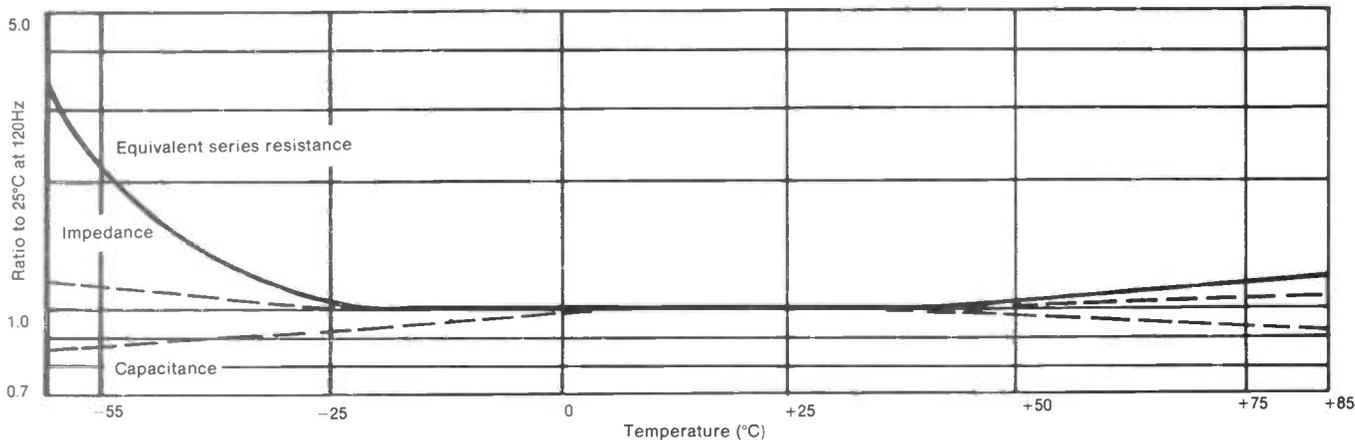


Fig 2 Typical temperature dependence of the characteristics of a 6V plain-foil capacitor

since it involved a gradual degradation in performance brought about by evaporation of the electrolyte through the end seal of the capacitor. Early models (and to some extent many of the cheaper models available today) suffered from a secondary mode of failure brought about by the migration of silver from the cathode; the result was a short circuit

between cathode and anode. Fortunately most manufacturers use newer processing methods which have, to a very large extent, removed this problem. Despite this, many governments (including our own) have banned the use of silver-cased gelled tantalum capacitors in critical applications. The direct alternative is to use tantalum cased

models which are very much more expensive.

Foil tantalums

This type of capacitor consists of two thin tantalum foil electrodes with tantalum wire leads spot welded to them. Since the capacitance is proportional to the surface area, the foils are usually etched to increase that area. The anode foil is then oxidised by voltage polarisation and both foils are assembled, along with a porous spacer material, and rolled into a cylindrical form with an axial wire on each end. The rolled section is now impregnated with an electrolyte and then sealed into a suitable container.

One of the major advantages of this type of capacitor is that the capacitance value and the impedance are relatively unaffected by temperature variations (see Figure 2). On the other hand the equivalent series resistance increases 3—8 times as the temperature drops below zero. However this factor is not critical in most applications. Environmentally, the type of construction is well able to withstand extreme shock and vibration, as well as being able to operate at altitudes up to 100,000 feet.

The foil construction is also ideal when it comes to manufacturing non-polar capacitors. The normal polar type is capable of taking 3V in the reverse direction but, after adding an oxide coating to the cathode foil, the capacitor may certainly be treated as a non-polar type.

Despite these advantages, the foil type is not the most popular type of tantalum capacitor since it tends to be relatively expensive.

Solid tantalums

The solid tantalum is the lowest cost and the most popular of the three types. It is also the most flexible in terms of variations in form available, with (for example) the bead style (Figure 3), the chip style and, of course, the metal cased type (Figure 4). Since the construction of all types is basically the same and since the bead style constitutes 80% (by quantity) of all sales, we shall consider here just how this style is made.

The first stage in the process of manufacture is the formation of a pellet of compressed tantalum powder around

Table 2: Results of long term testing of gelled tantalum capacitors

Rating	Unit number	Initial			2000 hours		
		Capacitance (μF)	Dissipation factor (%)	Leakage current ¹	Capacitance (μF)	Dissipation factor (%)	Leakage current ¹
20 μF , 60V	1	21.3	1.90	0.1 μA	21.0	1.60	0.1 μA
	2	20.8	1.45	0.1 μA	20.4	1.20	0.1 μA
	3	21.0	1.42	0.1 μA	20.5	1.28	0.1 μA
	4	21.5	1.60	0.1 μA	21.2	1.50	0.1 μA
	5	21.2	1.36	0.8 μA	20.9	1.12	0.1 μA
	6	21.3	1.36	0.1 μA	21.0	1.12	0.1 μA

All measurements at 120Hz.

¹Leakage current was measured after five minutes at rated direct voltage at room temperature.

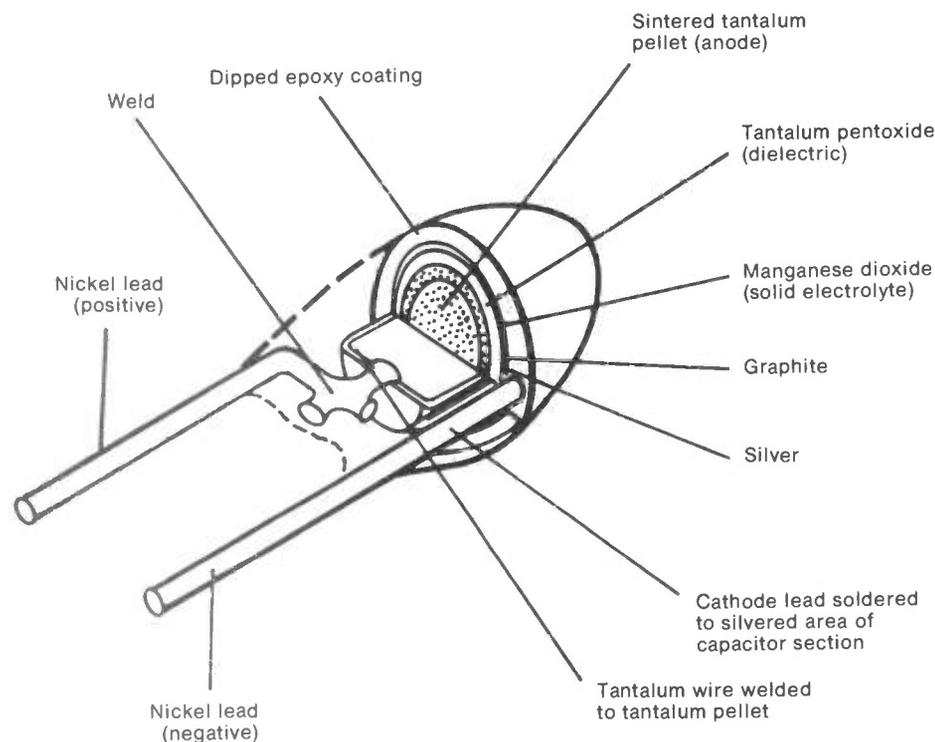


Fig 3 Bead style of tantalum capacitor

Table 3: Back-to-back operation of solid tantalum capacitors under various test conditions

Test	Rating	Before test				After test			
		Capacitance (μF)	Dissipation factor (%)	Leakage current (μA)		Capacitance (μF)	Dissipation factor (%)	Leakage current (μA)	
				A	B ¹			A	B
Rated DC voltage applied continuously in one direction for 1000 hours at +85°C	7.5 μF — 20VNP	High 7.53	3.1	3.0	2.5	7.60	3.4	5.0	4.5
		Low 6.89	2.2	0.5	0.1	6.84	2.6	0.5	0.1
		Av. 7.18	2.7	1.0	0.8	7.20	3.0	1.5	1.0
Rated DC voltage, polarity reversed every 168 hours. Test duration 1000 hours at +85°C	7.5 μF — 20VNP	High 7.56	3.0	5.0	2.5	7.75	3.5	4.0	4.0
		Low 6.88	2.3	0.5	0.5	6.82	2.9	0.5	0.1
		Av. 7.25	2.8	1.5	1.0	7.30	3.2	1.3	1.3
AC voltage of 6V _{RMS} . 60Hz applied continuously for 1000 hours at +85°C	30.0 μF — 6NNP	High 35.2	7.5	2.0	3.0	33.4	8.4	1.8	2.0
		Low 30.9	5.0	0.5	0.5	29.8	6.4	0.5	0.5
		Av. 33.3	6.3	1.5	1.6	31.7	7.3	1.2	1.0
AC voltage of 10V _{RMS} . 400Hz applied continuously for 1000 hours at +85°C	7.5 μF — 20VNP	High 7.68	4.4	2.0	3.0	7.65	5.5	2.6	3.0
		Low 7.03	3.7	0.1	0.5	7.05	3.1	0.1	0.1
		Av. 7.30	4.1	0.9	0.9	7.33	4.3	0.7	0.9

Capacitance and dissipation factor measured at 120Hz
¹Leakage current in microamperes on both polarities.

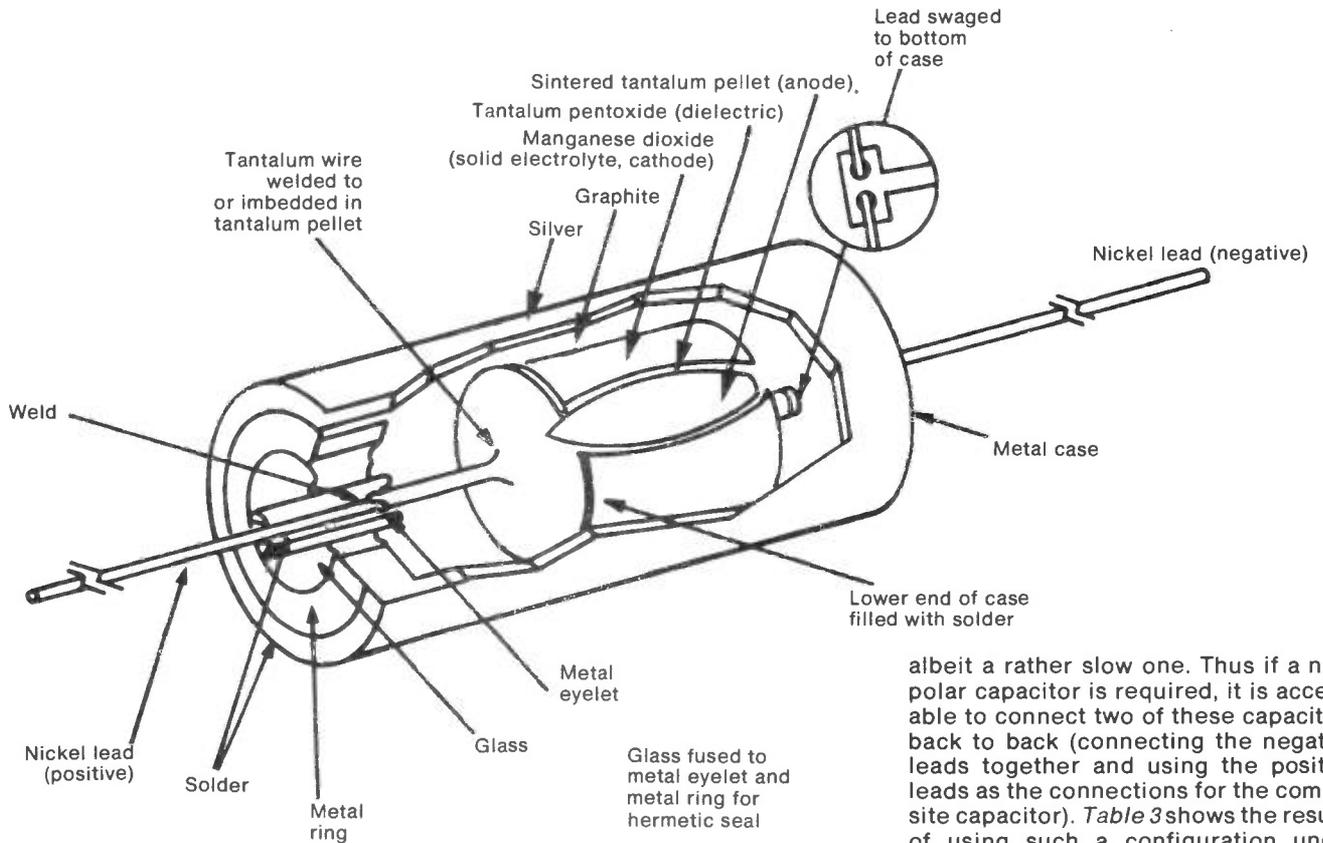


Fig 4 Structure of the metal-cased type of capacitor

a solid tantalum tab. The pellet is sintered in a furnace and electrochemically treated so that a dielectric oxide (tantalum pentoxide Ta_2O_5) is formed on the surface.

Next we impregnate the pellets with manganese nitrate and then heat treat the assembly so that the nitrate pyrolyses and generates a surface layer of manganese dioxide. The cathode is now applied in the form of a thin film of a carbon paste followed by a film of silver paste, to which is attached the cathode lead.

The anode connection is the tantalum tab previously referred to, onto which a lead is welded. The complete assembly is coated with a resin based material and, before leaving the factory, subjected to

an ageing process. Finally it is inspected for mechanical and electrical defects.

Solid tantalum capacitors have evolved into highly reliable units that will give excellent performance when properly used. It is highly stable (of the order of 1500ppm/C) in comparison with other types of electrolytic. At low temperatures it has no peer since all other electrolytics rely on liquids which, when approaching freezing, become sluggish; this sluggishness has a very drastic effect on their characteristics.

The solid tantalum will not accept reverse voltages exceeding 5% of the working voltage; however if it does occur, the breakdown will not be catastrophic. In fact the capacitor exhibits many of the characteristics of a diode,

albeit a rather slow one. Thus if a non-polar capacitor is required, it is acceptable to connect two of these capacitors back to back (connecting the negative leads together and using the positive leads as the connections for the composite capacitor). Table 3 shows the results of using such a configuration under various user conditions. As can be seen little or no effect is apparent.

Postscript

The past few years has seen significant increases in the prices of materials, which have forced component manufacturers to find ways of cutting costs. In the field of tantalum capacitors, powders with high CV values have been developed which have helped to make the capacitors smaller, electronic products lighter and tantalum as popular in this role as it was before the first price rises. The new devices not only lead to high component packing densities and lower costs, but they are also compatible with LSI technology and automatic insertion. Thus there has been a great upturn in demand for tantalum capacitors in line with recent growth in video cassette recorders, portable stereo, optical cameras and the like.

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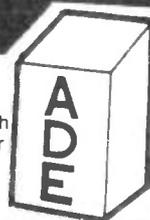
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SL6270 Gain controlled audio amplifier

Amongst the various RF IC's available from Plessey are hidden some useful IC's that function at audio frequencies. One such IC is the SL6270, available in an 8-pin DIL package (CDP) or in an 8-pin metal can (CCM).

The SL6270 is a gain controlled audio amplifier that incorporates a voice operated gain adjusting device (VOGAD). It is designed to accept low-level audio input and to provide an essentially constant output over a 60dB range of input signal. Numerous uses include transmitter audio, tape recorders, receiver audio etc.

Device details

Figure 1 illustrates the internal circuit of the SL6270. The input will accept either single-ended or differential signals via pins 4 and 5. When used single-ended, the other input should be decoupled to ground: moreover, the signal should ideally be AC-coupled.

Up to approximately 1mV, input signals are amplified with little or no AGC action. Above 1mV the output will remain essentially constant at 90mVRMS over a 50dB increase in input. If required, the dynamic range and sensitivity of the input may be reduced by connecting a resistor between pins 7 and 8. A 1k resistor will reduce both parameters by approximately 20dB. However the choice of a value below 680Ω is not recommended.

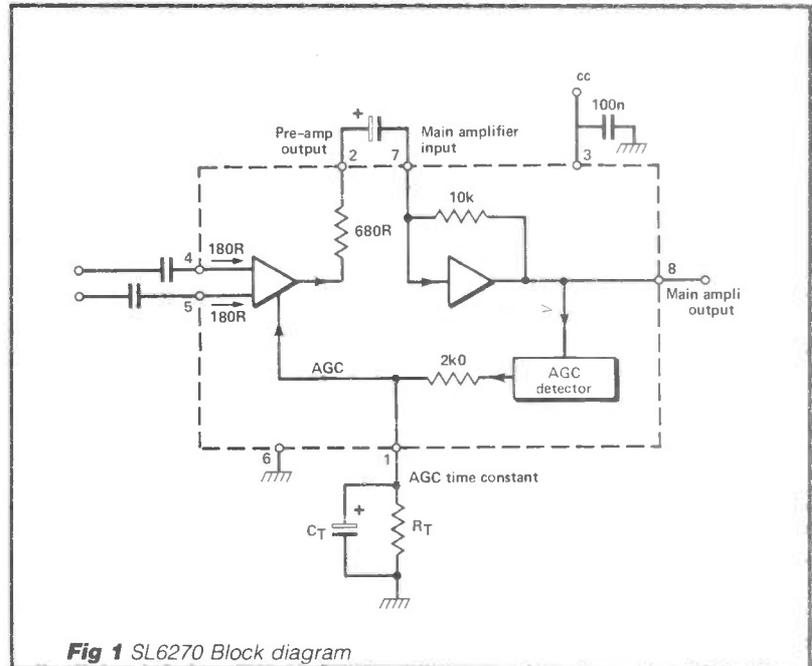
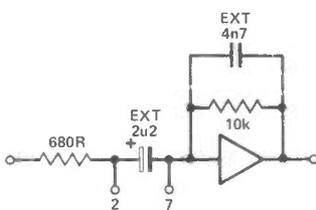


Fig 1 SL6270 Block diagram

Fig 3 Explanation of frequency response



Voltage gain = $10k\Omega/680R$

Upper frequency response = $10k/4n7 = 3kHz$

Lower frequency response = $680R/2\mu2 = 300Hz$

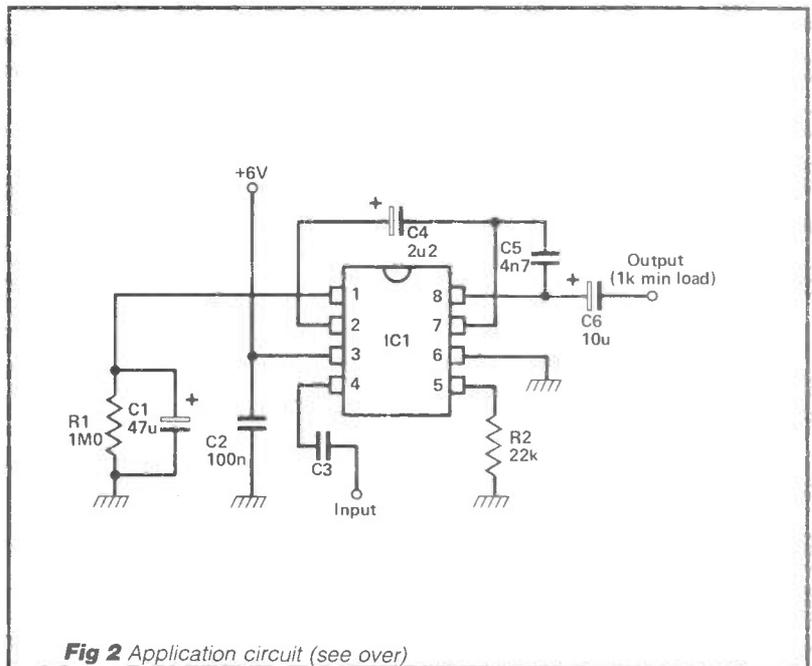


Fig 2 Application circuit (see over)

Characteristic	Value			Units	Conditions
	Min	Typ	Max		
Supply voltage	4.5	6	10	V	
Supply current		5	10	mA	
Voltage gain	40	52		dB	72 μ V _{RMS} pin 4
Output level	55	90	140	mV _{RMS}	4mV _{RMS} pin 4
THD		2	5	%	90mV _{RMS} pin 4
Ambient temp	-30	+20	+85	°C	

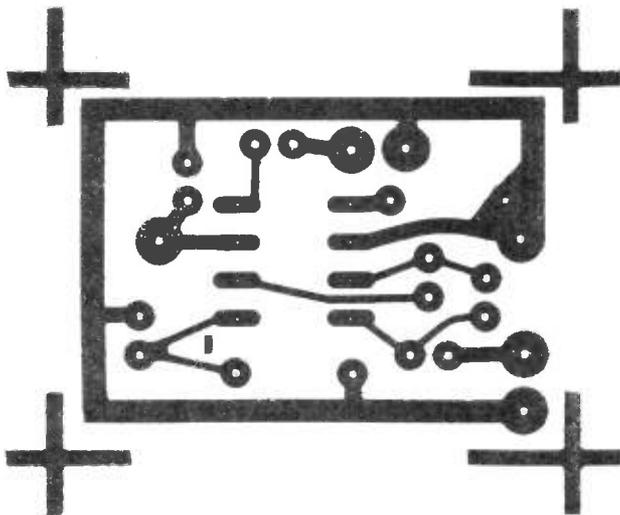
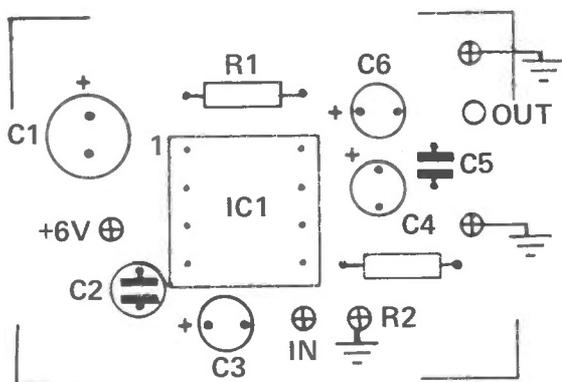


Fig 4 PCB foil pattern for a general purpose audio applications circuit using the SL6270

Fig 5 Component overlay



C1 is 47 μ 16V
 C2 is 100n mono
 C3, C6 are 10 μ 16V
 C4 is 2 μ 2 16V
 C5 is 4n7 ceramic
 R1 is 1M Ω
 R2 is 22k Ω
 IC1 is SL6270 CDP

The design of the SL6270 is such that both the low and the high frequency response is decided by two capacitors. The LF -3dB point is, in fact, determined by all three of the input, output and coupling capacitors. But for most communications purposes, the coupling capacitor between pins 2 and 7 is treated separately and it is usually chosen to be 2.2 μ F as this gives the -3dB point at 300Hz: the input and output are chosen to ensure a response to frequencies of 100Hz or less. Typically, the open-loop upper frequency response extends to several MHz, and the capacitor between pins 7 and 8 gives the required response. A 4n7 will give a typical HF point of 3kHz.

The attack and decay times are tailored to individual requirements through a suitable selection of the capacitor and resistor connected to pin 1. The 'attack time' — i.e. the time taken for the output to return to within 10% of original level following a 20dB increase in input — will be approximately 20ms when the values recommended are used (47 μ F and 1M Ω). It is principally determined by the value of C used and can be treated as 0.4ms/ μ F. The decay time is determined by the discharge rate of the capacitor via the parallel resistor. 1M Ω gives a rate of approximately 20dB/second.

Application for the SL6270

To give the reader some idea of the ways in which the SL6270 can be used, we present here the PCB foil pattern (Figure 4) and the associated component overlay (Figure 5) for a general purpose audio applications circuit, which would be incorporated where constant output levels are required from widely fluctuating input levels.

This circuit has been designed with communications particularly in mind. It has a tailored frequency response of (nominally) 300Hz—3kHz, and it should prove easy to insert between the volume control of the receiver and the existing audio amplifier/output stage.

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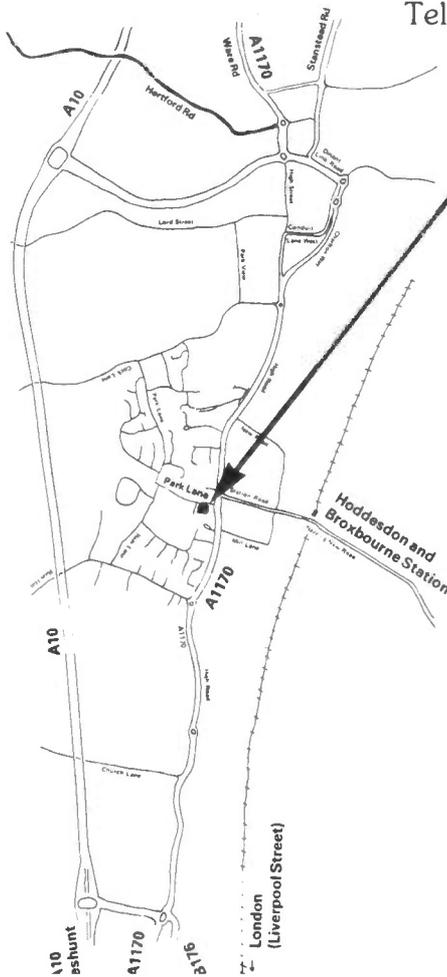
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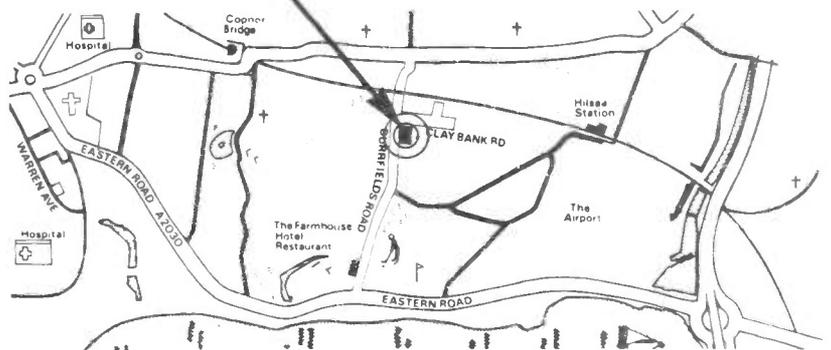
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'NOTES FROM THE PAST'

Twenty-seven years ago, people were starting to probe some novel ways of communicating round the world. While some were trying to receive the BBC in the States, others were speculating about the facilities offered by satellites

A number of British TV receivers have been shipped over to America where it is hoped to receive something of our BBC transmissions. The attempt is being made by the National Broadcasting Company, who are installing the receivers at their Riverhead Station, Long Island, hoping to relay any images received (duly filmed) in the 'Wide, Wide World' programme. By the time this appears in print the hoped for 'peak period' will have passed and perhaps something of the results will have appeared in the daily press. In any case we shall know something of the conditions, if they prove to be abnormal, by the interference affecting our own domestic receivers!

Attempts to pick up BBC signals in America were unsuccessfully made in 1953, at the time of the Coronation, but some years earlier, during a period of high sun-spot activity, successful reception of BBC signals was reported. At that time, of course, no attempt was made to re-broadcast them. What a spot for ITA to achieve this in reverse. A huge audience sitting agog waiting to see one of America's star programmes — and a couple of adverts slipped in!

Listener watch

Several readers, especially Mr Alex P Buchanan of Carrick Park, Ayr, have written about next year's launching of artificial satellites — particularly of the electronic equipment and of organised amateur reception of the radio signals they will send back to earth. While suggestions have from time to time been put forward that the services of amateur observers may be of value, as far as I can make out no practical steps have yet been taken to enrol their help. As the work is under the direction of the US Naval Research Laboratory it is doubtful that the initiative in seeking such help

will come from the official side. Nor are the Russians likely to ask for co-operation. Indeed, they are revealing no details of their project at all.

However, for visual observation, the Smithsonian Institution in Washington have arranged for (and are still organising) a world-wide chain of knowledgeable amateur observers to man posts to track the sphere, so as to make sure (if it gets lost) that we shall know something of what happened to it. As I mentioned when the project was first announced, it should be visible in the reflected light of the sun to watchers armed with quite ordinary binoculars, and under favourable conditions even with the naked eye.

As I see it, it is rather doubtful whether amateur radio observation would be of much value with our present unreliable maps. Errors of several miles occur in the charted positions of many of the smaller islands and even in the distances of continents from each other. Accurate measurement, for radio purposes is far beyond the scope of amateur equipment. Even the loss of signals, should the satellite wander off into outer space, could hardly be accurately plotted or timed without elaborate equipment. There is, however, one aspect scheduled for official investigation, in which a corps of widely spaced amateur listeners might be able to help. That is the problem of propagation for VHF working and the effects of the ionosphere in reflecting and refracting radio signals, with the view of making wide-coverage TV an early possibility.

First shot

I am not normally a pessimist but I have wondered just how many satellites will have to be launched before one can be made to circle in the planned orbit. The lay mind seems to take it for granted that it is already as good as done, quite

overlooking the amount of experimental work history teaches us is required for such ventures. And this is a stupendous step involving many unknown factors. Remember the early German V2 rockets? — only one in the first twenty or so worked and even *after* the war, development was brought only to a 60% successful launching stage. It is doubtful whether we can yet claim to be through the growing-pains stage, and we glibly talk of a three-stage tandem rocket reaching the right altitude and finally kicking the satellite off to an 18 000mph start. If its velocity is too slow it will sink back into an increasingly heavier atmosphere and burn up, perhaps even before completing one circuit. If it travels too fast it will fly off into space. The world's leading rocket engineers are confident that one day we shall get a satellite in the right orbit, but they won't quote how many firings they think may be needed before it is achieved.

Nor is there any agreement among scientists on how long it will stay up. Some think a few hours (it will circle the Earth from west to east every 90 minutes). Some venture to suggest perhaps for months. Either guess might be right. The satellite will approach within 200 miles of the Earth and wing out to 1400 miles at each revolution, moving about 1500 miles west at each circuit, and our present knowledge of atmospheric density at these heights is so slender that either conjecture might well prove right.

Remember, that even as a first effort, the engineers are building twelve satellites (not just one) and hope to get *one* into the planned orbit, if only for a short spell. When that has been achieved perhaps we shall be in a better position to evaluate just how a corps of skilled amateur radio enthusiasts might usefully be of service.



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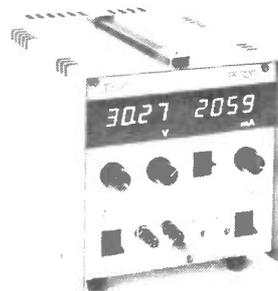
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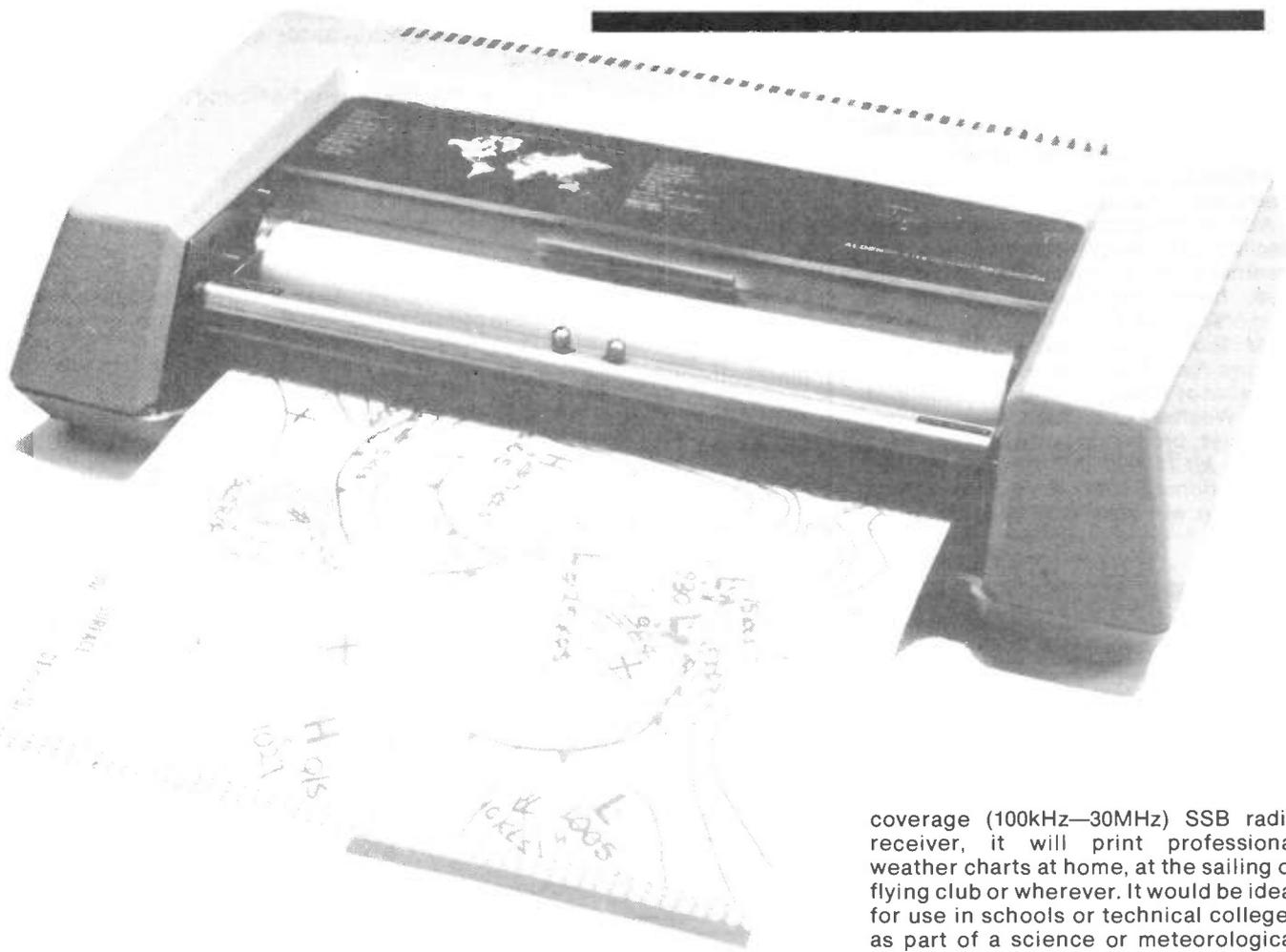
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The Alden Weather Chart Recorder

A kit for the home constructor — given an introductory review here by Arthur C Gee



One of the difficulties facing those interested in receiving weather maps (whether from HF radio stations or satellites), FAX and similar radio transmitted graphics, is the non-availability of suitable mechanical recording equipment. Some real enthusiasts have succeeded in building their own FAX machines, and some useful descriptions of such efforts have appeared in electronics journals in the past. But these are few and far between; moreover, one really needs workshop facilities to make a good job of such a project. For the most part enthusiasts have had to make do with obsolete or surplus professional machines, which are usually expensive and require a lot of work done on them before they can handle the characteristics of weather maps and FAX pictures

for which they were not originally designed.

At last a low cost facsimile recorder has become available, which is specifically intended for the radio amateur, SWL and weather buff. ALDEN Electronics of Westborough, Massachusetts, USA, has recently brought out an excellent Weather Chart Recorder in kit form, thus permitting the price to be kept at an affordable level for the type of customer they have in mind. It is a single speed, single IOC recorder, running on 115VAC. The firm specialises in equipment for professional marine use, for example its Marinefax Recorders, but this Kit Recorder is specifically for the radio amateur/home constructor/etc market.

Coupled into a stable HF general

coverage (100kHz—30MHz) SSB radio receiver, it will print professional weather charts at home, at the sailing or flying club or wherever. It would be ideal for use in schools or technical colleges as part of a science or meteorological project. Indeed, it is proving very popular in the States for just such applications.

Facsimile Weather Chart transmissions are broadcast worldwide and are available free of charge to anyone having the equipment to receive them. Moreover, all weather charts use international symbols, so one can easily interpret charts whether they are transmitted from sites in the USA, Canada, Japan, Russia or from other countries throughout the world.

Constructional comments

The ALDEN Weather Chart Recorder Kit is easily assembled, the time for doing so being about five hours, I reckon. An excellent Assembly Manual is provided. Complete illustrated step-by-step instructions are given for assembling, checkout and operation, while pre-assembled and tested circuit boards and mechanical assemblies are provided for

the more difficult sub-assemblies. An attractive moulded case gives a professional appearance to the completed unit. The solid-state circuitry and a simple electro-mechanical design should ensure long, trouble-free operation.

Electrically sensitive paper in disposable cassettes, 11" wide, is used, so no tricky threading procedures or processing will be required. Another welcome feature is that the printing process is quiet and free from smoke, fumes or smell. The overall size of the unit is approximately 17" x 10" x 4" and the weight is 10lbs.

A very nice feature of the recorder is its auto start and stop facility. The unit can be left in an operational state until a transmission starts, whereupon the machine automatically starts up because the transmission itself provides all the necessary start and stop signals as well as framing pulses that automatically frame the picture.

ALDEN produces a number of books dealing with weather forecasting and weather chart interpretation, one of the best being 'A Mariner's Guide to Radiofacsimile Weather Charts' by Dr J M Bishop. Another — 'Worldwide Marine Radiofacsimile' — gives a complete list of stations along with details of their Weather Chart transmissions, frequencies, broadcast times, etc.

The kit is available through ALDEN International SA, 117 North Main Street, Brockton, MA 02403-0860 at \$1100.

Weather Chart Recorder Kit Model 9321

SPECIFICATIONS

Recording rate:	120spm (scans per minute)
Index of Cooperation:	10C576 CCIR; 169 lines per inch
Control signals:	Auto start, stop, frame; manual start and frame
Start:	Signal shifting between 1500Hz and 2300Hz at a rate of 300Hz for five seconds
Frame:	A 1500Hz signal interrupted by a short burst of 2300Hz each scan line. Duration — 20-30s immediately following start signal
Stop:	Signal shifting between 1500Hz and 2300Hz at a rate of 450Hz for five seconds
Circuitry:	Solid state
Input impedance:	600Ω balanced
Input frequencies:	FSK 1500Hz black; 2300Hz white
Scanning electrode:	Stylus belt
Recording paper:	Alfax electrosensitive paper in throw-away cassettes with built-in printing electrode. Each cassette contains 35feet of 11-inch wide paper
Input voltage:	115VAc 10%, 50/60Hz
Maximum power:	Standby mode — 10W; operating mode — 30W
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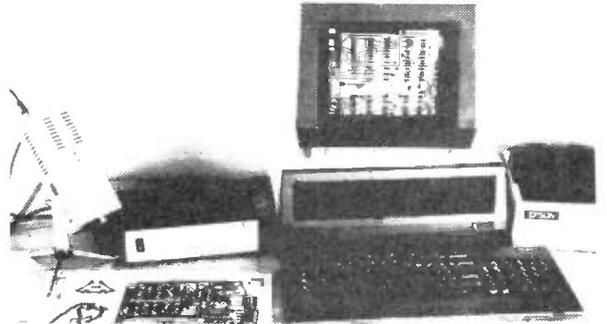
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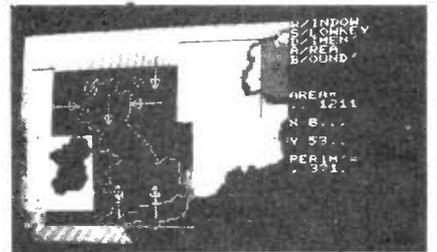
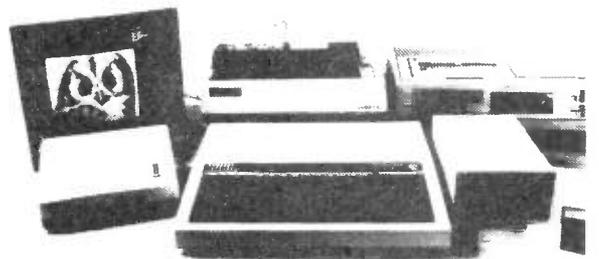


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EXPANSION BUS

In the second of our continuing series about personal computer add-ons, Roland Perry examines the Digithurst range of image analysis equipment



Most personal computers available these days have a bash at so-called 'pixel' graphics. These pixels are dots on the screen smaller than a whole character cell. Indeed their size will normally be that of the dots used to make up alphanumeric characters displayed on the screen, and this dimension thus corresponds to the maximum resolution provided. Depending on the sophistication of the particular machine it may be possible to display grey levels (that is, to control the brightness of each dot more specifically than just on and off) or colours.

Drawing pictures in graphics mode is normally limited to constructing them by putting together lines, blocks, parts of circles and any other available building blocks. However, the equipment that Digithurst offer allows the user to enter pictures directly from a TV camera and once in the computer the image can be processed in a number of ways. For example, measurements of particular areas may be made with the aid of an optional software package.

The review model provided fitted straight into the back of our favourite personal computer (BBC model B: what else?) and within seconds we were seeing pictures of the Editor's pen-tidy on the screen. The grey levels for such pictures are treated on the BBC compu-

ter by sacrificing resolution and turning on between one and four pixels arranged in a square. The more that are turned on, the brighter the 'dot' appears. We found this scheme worked very well even when viewed on a high resolution monitor, the individual pixels apparently merging to produce grey levels. The same principle is used when printing black-and-white photographs (half-tones).

The standard black-and-white version — the MicroSight 1 — may optionally be upgraded to colour (for another £100) via a colour vision system known as MicroSight Colour. This combination showed us a very convincing picture of an apple (the fruit rather than the computer!) and a section from one of *R&EW's* front covers.

The system

The system is basically in three parts. The first is a small black-and-white camera producing CCTV signals. Digithurst are reluctant to supply the system without a camera, even if you have one already. Understandably they are wary of the inevitable support problems. The camera plugs into a box of electronics called a MicroEye. Inside the MicroEye lies the scanning logic and the analogue-to-digital converter. It does not have any memory, and is certainly not a cheap frame-store. The philosophy of

the whole MicroSight system is that the memory to store the picture is inside the micro. The MicroEye is accessed via a parallel port on the host microcomputer.

The MicroEye interface runs essentially continuously, digitising all the incoming video signals. On receipt of a master reset signal, the unit begins to digitise the set of video image signals within this first frame that corresponds to the far left-hand side of the chosen image area, producing a column of pixels. When the interface starts to receive the second frame from the camera the timing circuitry steps one pixel horizontally along each line and digitises a column of pixels from that position. This process (illustrated more fully in *Figure 1*) continues until the whole image has been digitised. To capture the whole image takes 256 frames, or a little over five seconds.

The third and key part of the set-up is the software which runs in the micro-computer. The standard MicroSight 1 software handles all the data transfer from the MicroEye and converts the images into dots on the screen. Disk storage and retrieval of images is taken care of by BASIC programs, whereas the processing is performed by six machine code routines. The number of pixels and grey levels available will vary depending on the actual machine used. The options

for the currently supported machines are shown in the accompanying table.

An optional extra package called MicroScale, available with certain systems, permits further, more sophisticated, image analysis. This allows the display to be created from a 'window' in the captured TV image, and edge-enhancement to be performed within that area. Other facilities include measurement of boundaries, areas and distances on the image. These measurements are aided by an on-screen cursor which is manipulated via keystrokes at the user's micro. In addition, there is an MSDOS version of MicroSight which enables images to be filtered and to be merged within memory.

Overall

The MicroSight system is compatible with any microcomputer with an 8-bit parallel port and appropriate graphics, and it comes with two comprehensive manuals which give all the details of both the hardware and the software. Digithurst are very helpful and appear willing to support users attempting to apply the equipment to new applications and even to other micros.

Digithurst outline a number of applications for MicroSight from text recognition to robot vision systems. Its use for computer demonstrations, advertising and graphic design is obvious, but there are many additional applications as a piece of laboratory equipment, particularly where measurements are to be made on irregular areas. Medical studies, microscopy and satellite image processing come to mind.

After 0.5sec: 25 columns of pixels have now been created from the image and have been transferred to RAM as 25 columns of data. If a pulse was now sent from the computer along the master reset line the unit would start to digitise a new image from the top left hand corner again. This technique can be useful when a rapid frame grab rate is required; in this case, a 256x25 pixel image would have been captured.

After 5sec: If a full 256x256 pixel frame is required, then the master reset is not activated until the full frame has been read.

After 20msec: The first column of pixels have been created from the incoming video, and the unit is now waiting for the next line pulse before digitising the next column of pixels. The computer will also be waiting for the EOL pulse before reading in more data.

After 64µ: The first pixel has been digitised and has been transferred to the microcomputer's RAM and placed at the top of the first data column.

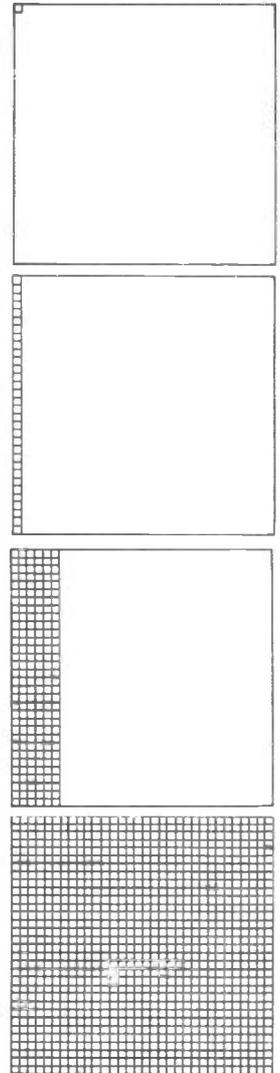


Table 1: MicroSight 1 systems

	Grey scales held in memory	Grey scales displayed	Mode Used	MicroScale available	Other software
BBC MODEL B					
High res. (256x256)	3	3	0	—	MicroSight system with printer dump, disk dump, etc. Options include animation image editing
Medium res. (128x100)	16	5	4	✓	
Colour high res. (256x200)	8 colours	8 colours	2	—	
Colour medium res. (128x100)	8 colours	8 colours	2	—	
ACT Sirius 1					
High res. (256x256)	255	7	768x400	✓	Vectoring package for turning images into CAD drawings. Contrast enhancement for X-ray analysis
Research Machines					
High res.	128x90	5	256x192	—	—
Medium res.	128x90	16	128x90	✓	—
Colour	128x90	8 colours	128x90	—	—
CBM 4032,8032					
Medium res.	128x100	5	256x300 (Supersoft Board)	✓	Histograms for image analysis
Apple II 48K					
Medium res.	128x100	5	256x192	—	Windows, area and boundary calculations included in MicroSight 1 system software

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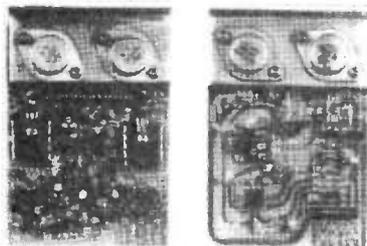
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ONE NIGHTS WORK

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This is the first thing I ever built, way back in 1979, and its usefulness has been proved time and time again. It checks fuses, lightbulbs, broken leads, as well as possible PCB track breaks etc. The original was mounted in an old transistor radio case, and a couple of nails with leads attached were — and are still — used as the probes. Eyebrows may rise when the circuit (*Figure 1*) is examined, but transistors and an audio transformer were used because they are so cheap and most readers should be able to get hold of an old transistor radio. The latter is often a valuable source of components; indeed all of the items for this tester, except the preset and transistors, were 'rescued' from one. The miniature transformer in such a radio is almost invariably red and to be found right next to the radio's speaker leads.

How it works

The transistors are used as switches, and the easiest analogy for the way they operate is that of three interconnected cog wheels, whereby if A goes anticlockwise, B goes clockwise, and C goes anticlockwise (*Figure 2*). Similarly, if transistor TR1 is turned on, as a result of the emitter being connected to ground through the probes, the base of TR2 will go to 0V, turning it off. This makes its collector (and the base of TR3) go virtually to the potential of the positive rail, thus turning on the oscillator constructed around TR3 and the transformer. RV1 adjusts the point at which TR1 turns on, the technique being to choose that setting at which the alarm just sounds when the probes are shorted. With the probes not connected, TR1

turns off and so TR2 turns on, turning off TR3 and the oscillator.

Construction

This tester may be built either on veroboard or a PCB, a design for the latter being given in *Figures 3 and 4*. None of the components are critical, so you could experiment with nearby values if the ones suggested are not available. Any npn general purpose transistor will work, but check the 'pin out'. I in fact used unmarked BC109 types in the original, having bought 150 untested ones for 30p... Ah! those were the days.

Check for solder joints or dry joints, and if all is well, switch on, adjust RV1 as mentioned above, and mount the unit in a suitable enclosure... verobox, cigarette packet, tobacco tin...

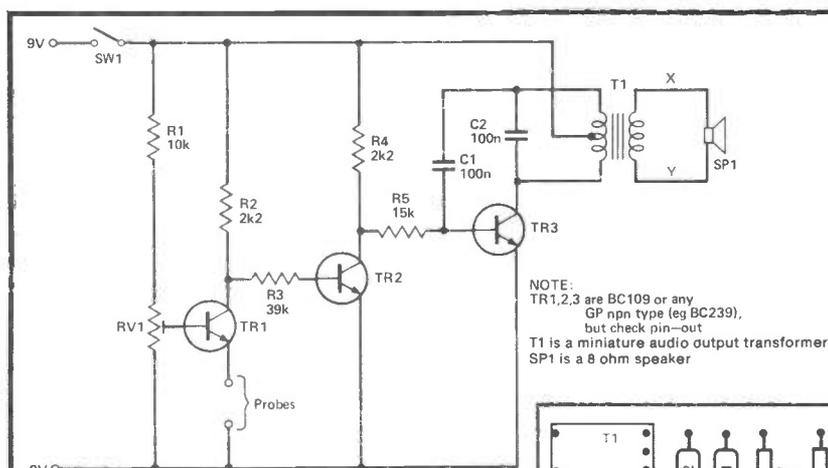


Fig 1: Circuit diagram

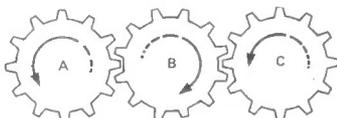


Fig 2: The principle of operation

NOTE:
TR1,2,3 are BC109 or any GP npn type (eg BC239), but check pin-out
T1 is a miniature audio output transformer
SP1 is a 8 ohm speaker

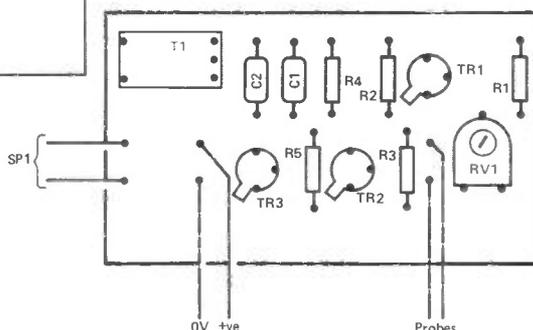
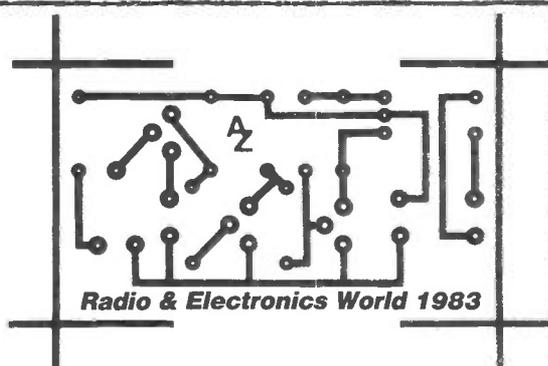


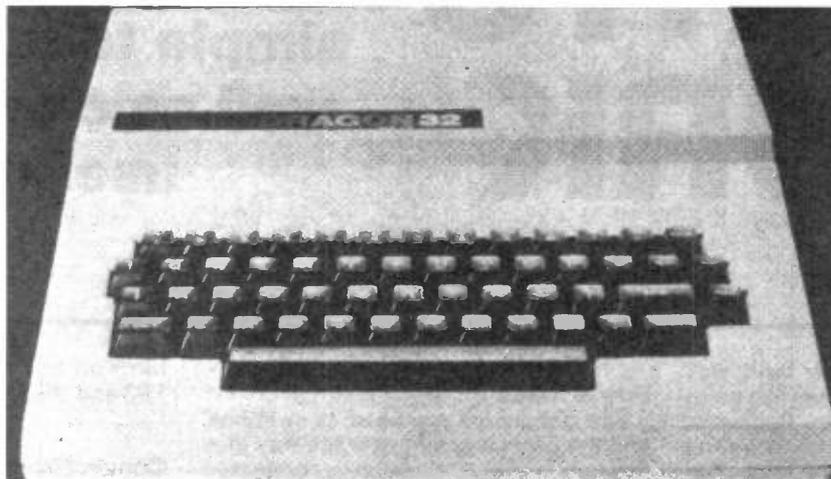
Fig 3: PCB foil pattern

Fig 4: Component overlay



AN RS232C INTERFACE FOR YOUR DRAGON 32

David Thomlinson of Cotswold Computers gives details of the interface that has been developed jointly by his firm and CP Engineering



The Dragon 32 has been described as 'The Affordable Sensible Computer'. Indeed, for its price, it is a remarkably complete micro: it does not require additional expansion boxes for the use or control of such devices as printers, joysticks or disk drives. Why then go to the trouble of designing and marketing an RS232C interface for the Dragon? To what uses can such an interface be put?

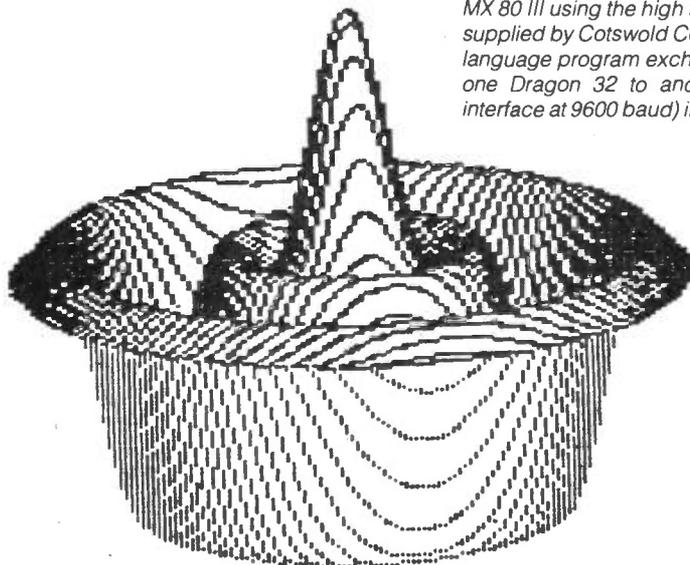
At Cotswold Computers, we believe that one of the next major developments for the home personal computer user will be in the area of communication. This will mainly be over telephone networks and will probably have as its object either accessing public databases such as REWTEL, placing orders for equipment or simply calling up other friendly

micros. Such communication needs a modem and modems need RS232C interfaces. And in that lies the reason for our joint venture with CP Engineering on an RS232C interface and a following modem.

To date we have supplied RS232C interfaces to both multinational and national companies, universities, private individuals and even the Police Force. The variety of uses to which their Dragons can now be put includes:

- 1) As a direct terminal to a large computer system
- 2) As a word processor, transmitting through a data modem to a larger computer system.
- 3) As a serial printer

A mode 4 high resolution graphics screen picture from a Dragon 32 printed by an EPSON MX 80 III using the high resolution dump routine supplied by Cotswold Computers. An assembly language program exchanged this screen from one Dragon 32 to another (via the RS232C interface at 9600 baud) in less than six seconds.



- 4) As a terminal connected to a speech synthesis unit
- 5) As a terminal connected to a liquid scintillation spectrometer
- 6) To control a teletype
- 7) To control a graph plotter

In addition the interface is being used to connect one Dragon with another.

So just what is an RS232C interface and how does it process data? To understand this we must first examine the way data is conventionally encoded.

A few basics

As you probably know, bits – or binary digits, each a 1 or a 0 – are combined into groups of eight called bytes when they are used to represent characters. The alphabet, all the Arabic numerals plus the various punctuation marks require a total of 72 characters. The bit code commonly used for this is that known as ASCII or the American Code for Information Exchange. When transmitting text via an RS232C link, it is usual to represent the letters and symbols by the ASCII code. And since the Dragon 32 has the required ASC\$ instruction, it is a simple matter to communicate text between the Dragon 32 and any other ASCII compatible computer or peripheral.

To display the ASCII code on your Dragon, load and run the following program:

```
10 FOR I = 1 TO 255
20 TIMER = 0
30 POKE 1500, I
40 IF TIMER < 25 THEN GO TO 40
50 NEXT I
```

In addition to this character set, ASCII also includes a number of control codes; for example, CHR\$(10) sent to most printers will produce a line feed. A

complete listing of the ASCII codes is shown in Table 1.

Having thus briefly discussed the codes for representing letters and numbers, we now turn to how they are transmitted.

The RS232C standard

RS232C is a common bit serial data transmission standard. Data is communicated as a sequence of bits on a single transmission line, preceded by a start bit and followed by a stop bit (or bits). The bit rate (and so similarly the baud rate) must be the same for both the transmitter and the receiver to allow the receiver to synchronise.

To understand how the interface operates, it is best to look at this in conjunction with a specific example. The waveform shown in Figure 1 is that resulting from the transmission of a single 8-bit data word (in fact, decimal 74 in 8-bit format). The line is in a 'marking' state corresponding to logical zero (below -3V) until the data word is transmitted. A start bit of logic one (greater than +3V) signals the presence of a data word and is used by the receiver to synchronise its testing of the following eight time periods which together represent the 8-bit data word being transmitted.

A number of transmission formats are in use which include the addition of an extra stop bit and/or the addition of (or alternatively, the use of d_7 as) a parity bit. The parity bit attempts to detect the occurrence of data corruption by ensuring that all data words sent contain an even number of logic ones (EVEN parity) or, alternatively, an odd number of logic ones (ODD parity). If a data word is received with incorrect parity, it may be assumed to have been corrupted in the transmission process. Obviously, 8-bit data (which can be thought of as taking any value from 0 to 255) may be transmitted except when the most significant bit is used as a parity bit when only 7-bit words (0-127) are allowed.

A further two lines are provided in addition to the data transmission line. These lines provide a means of exchanging information on the condition of the devices that are communicating, such as 'printer busy' or 'ready'. The accepted nomenclature for these control lines comprises 'Request to send' (RTS) for the line set by the transmitter and 'Clear to send' (CTS) for the line set by the receiver.

The time taken to transfer a single data word is set by the baud rate but the rate of data transfer can be significantly slower if the peripheral controls the transfer rate via the CTS line.

The CP RS232C interface

Our interface is designed for operation under program control and is arranged to appear to the user as two locations in memory. Since the only BASIC instructions which allow memory operations are PEEK and POKE, these are the instructions used to communicate with the interface. When programming in assembly language, however, all instructions which involve memory can be used. One

Table 1: The meaning of the ASCII code words

0 Null	1 Start of heading
2 Start of text	3 End of text
4 End of transmission	5 Enquiry
6 Acknowledge	7 Alarm/Bell
8 Backspace	9 Horizontal tabulation
10 Line feed	11 Vertical tabulation
12 Form feed	13 Carriage return
14 Shift out	15 Shift in
16 Data link escape	17 Device control 1
18 Device control 2	19 Device control 3
20 Device control 4	21 Negative acknowledge
22 Synchronous idle	23 End of transmission block
24 Cancel	25 End of medium
26 Substitute	27 Escape
28 File separator	29 Group separator
30 Record separator	31 Unit separator
32 Space	127 Delete

33 !	34 "	35 £	36 \$	37 %
38 &	39 '	40 (41)	42 *
43 +	44 ,	45 -	46 .	47 /
48 0	49 1	50 2	51 3	52 4
53 5	54 6	55 7	56 8	57 9
58 :	59 ;	60 <	61 =	62 >
63 ?	64 @	65 A	66 B	67 C
68 D	69 E	70 F	71 G	72 H
73 I	74 J	75 K	76 L	77 M
78 N	79 O	80 P	81 Q	82 R
83 S	84 T	85 U	86 V	87 W
88 X	89 Y	90 Z	91 [92 \
93]	94 ^	95 _	96 `	97 a
98 b	99 c	100 d	101 e	102 f
103 g	104 h	105 i	106 j	107 k
108 l	109 m	110 n	111 o	112 p
113 q	114 r	115 s	116 t	117 u
118 v	119 w	120 x	121 y	122 z
123 {	124	125 }	126 ~	

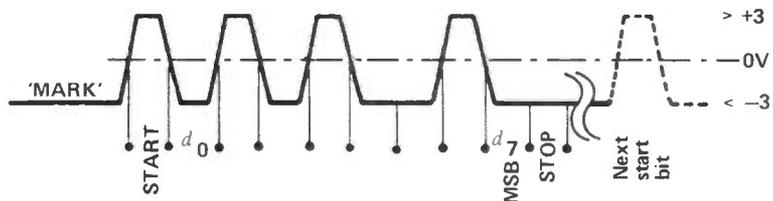


Fig 1 RS232C transmission waveform

of the memory locations (DATA : ADDRESS — 65370) is used to transmit and receive data while the other (CONTROL/STATUS : ADDRESS—65354) is used to send control words to and receive status words from the interface.

The exact form of the communication made using the interface will depend to some extent on the device involved but will in general consist of a sequence of steps as described below:

TRANSMISSION

- 1) The required format is ascertained and the corresponding control word POKED to 65354. The code will set the RTS line as required.
- 2) The status word may optionally be PEEKED from 65354 to ensure that the receiver is ready.
- 3) Data transmission is begun by POK-

ING the first word to 65370. The status word is then PEEKED from 65354 until it indicates that the interface is ready for the next data word. The next data word is then POKED to 65370 and the status word again checked. This process is then repeated until the data transmission is complete.

RECEPTION

- 1) The control word for the required format is POKED to 65354.
- 2) The status word may optionally be PEEKED until the transmitter indicates that it is ready.
- 3) The control word may optionally be POKED to instruct the transmitter to begin data transfer.
- 4) The status word is PEEKED from 65354 until the interface indicates that it has received a data word.

CONTROL AND STATUS WORDS

Baud rate: Bits 0, 1 of the control word

Normal mode provides the baud rate indicated by the switch table

Bit pattern		Decimal contribution	Resulting baud modes
Bit 1	Bit 0		
0	0	0	16 times Normal
0	1	1	Normal
1	0	2	¼ times Normal
1	1	3	Master Reset

Format: Bits 2-4 of the control word

Bit pattern			Decimal contribution	Bits	Format Parity	Stop
Bit 4	Bit 3	Bit 2				
0	0	0	0	7	even	2
0	0	1	4	7	odd	2
0	1	0	8	7	even	1
0	1	1	12	7	odd	1
1	0	0	16	8	no	2
1	0	1	20	8	no	1
1	1	0	24	8	even	1
1	1	1	28	8	odd	1

Line control: Bits 5, 6 of the control word

These bits give control over the logic level of the 'Request to send' output line from the interface. The bit patterns which result in RTS=high cause the peripheral to sense a 'Request to send' from the interface.

Bit pattern		Decimal contribution	Function
Bit 6	Bit 5		
0	0	0	RTS = high
0	1	32	RTS = high
1	0	64	RTS = low
1	1	96	RTS = high plus TRANSMIT DATA = high

For example:

Suppose the following communication format is required — 8 bits/No parity/2 stop bits/RTS low at a transmission rate of 1200 baud: what is the control word? Using the normal mode (decimal contribution = 1), the 8 bit/No parity/2 stop bits format (decimal contribution = 16) and RTS low (decimal contribution = 64) makes the control word $1+16+64 = 81$ giving the program line:

1 POKE 65354,81

A table of baud rate switch positions gives the switch pattern 'off', 'on', 'off', 'off' for 1200 baud. With that switch pattern set and 81 POKED to 65354, the interface will operate with the required format until a new value of the control word is POKED.

Make-up of status word

Bit number	Decimal equivalent	Function of bit
0	1	Data word received
1	2	Data word transmitted
2	4	Data-Carrier-Detect
3	8	Clear to send
4	16	Framing error
5	32	Receiver overrun
6	64	Parity error

5) A control word may optionally be POKED to 65354 to inhibit the transmitter while the data word is stored.

6) The first data word is PEEKED from 65370 and stored or processed as required. The process is repeated from '4' until all the data has been received.

There are a couple of additional points to note about communication via this interface. Firstly, it should be noted that, although the address of both control and status words is 65354, they are separate registers. Secondly, the required baud rate should be set via the switches on the interface before the Dragon is switched on. The make-up of the control and status words is described in the box on this page.

The more technically minded reader may be interested to know that the interface uses a memory mapped 6850 ACIA with the baud rate generated by a crystal-controlled 4702, whilst half of a 1488 together with half of a 1489 provide the 232C driver/receiver. The -ve supply for the 1488 is generated from the Dragon 32 +12V line. All the relevant lines from the 6850 are brought out to the interface edge connector to facilitate their connection to the modem.

The interface may (by making appropriate modifications to the board) provide RS232C on one interface cable and TTL levels on another. Moreover, the interface status word can provide a means of sensing the $\overline{\text{CTS}}$ and $\overline{\text{DCD}}$ TTL compatible inputs to the interface and the control word may be used to set RTS which is also TTL compatible. Thus the interface may be used to perform limited sense and control functions.

Interface output connections

A standard 'D' type subminiature connector is used to connect signal lines to and from the interface. Pins 1 to 7 are used for RS232C connections and are arranged conventionally. The other pins

Table 2: Pin-out for the interface connector

Pin	Description
2	Transmit data
3	Receive data
4	Request to send
5	Clear to send
7	Ground
8	RxDATA
9	$\overline{\text{DCD}}$
10	$\overline{\text{CTS}}$
11	TxDATA
12	RTS
13	+5V
17	$\overline{\text{CTS}}$
18	RxDATA
19	Baud clock output -- TTL
24	+12V
25	-9V -- Low current

All pins not mentioned are *not connected*

however are used for connection to the CP modem. *Under no circumstances should connections be made to the interface connector pins other than Nos1-7.* This requirement restricts the use of 25-way ribbon or other connectors. The user is advised to refer to the range of standard cables available from the manufacturer. The full pin-out is shown in Table 2.

Input, by the way, is via the cartridge slot on the Dragon.

In conclusion

The CP RS232C interface has been designed to allow your Dragon 32 to transmit to, and receive data from, any RS232C compatible device. The interface features all the common formats and bit rates under program and switched control respectively. In addition the bit rate may be multiplied by 16 or divided by 4 under program control.

It is supplied by Cotswold Computers in a sturdy case complete with a recess to allow access to the baud selector switches from the outside. The company can also supply software support in the form of a tape of the programs documented in the interface manual and a range of specialist software (and interface cabling). Parts are guaranteed for twelve months and the retail price for the interface is £49.50. Trade distribution enquiries are welcomed.

A program to communicate the graphics screen

The following program listings allow the transfer of graphics from one Dragon to another: The transmitting Dragon generates a random graphics pattern which is then transferred to the receiving Dragon. Both interfaces must be set to the same baud rate, a high rate reducing the transmission time.

Program to be entered into transmitting Dragon

```
10 TIMER=0
20 PMODE4:SCREEN1,1::PCLS1
30 X=RND(255): Y=RND(192)
40 LINE-(X,Y),PRESET,B
50 IF TIMER<300 GOTO30
60 POKE65354,3
70 POKE65354,17
80 A=B AND PEEK(63354)
90 IFA= 0 GOTO 80
100 FORI=1536TO7679
110 A=2ANDPEEK(65354)
120 IFA=0 GOTO 110
140 POKE65370,PEEK(I)
150 NEXTI
```

Program to be entered into receiving Dragon

```
10 POKE65495,0
20 PMODE4:SCREEN1,1:PCLS1
30 POKE65354,3
40 POKE65354,81
50 A=PEEK(65354) AND 8
60 IF A=0 GOTO 50
70 POKE65354,17
80 FORI=1536TO7679
90 A=1ANDPEEK(65354)
100 IF A=0 GOTO90
110 POKEI,PEEK(65370)
120 NEXTI
130 POKE65494,0
```

Stop Press: The CP RS232C Interface has just seen a couple of further enlargements. These have given it the capability for data handling at 19200 baud and full compatibility with the Tandy Colour Computer.

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SP901	External Speaker	31.00	(1.50)
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FC700	A.T.U.	99.00	(1.00)
FT757GX	H.F. Amateur Bnd Tx Gen. Cov. Rx	POA	
FC757AT	Automatic A.T.U.	POA	
FP757GX	Power Supply	POA	
FT726R(2)	Multimode multiband base station C/W 2M	675.00	(-)
FT230R	Transceiver 2M 25W F.M. mobile	239.00	(-)
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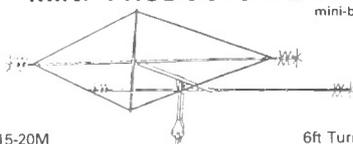
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AMATEUR RADIO WORLD

Compiled by Arthur C Gee, G2UK

Those readers of this magazine, who, whilst not being radio amateurs, find this page of sufficient interest to read in its entirety, may like to know more about Amateur Radio. They may have had their interest sufficiently stimulated to make them feel they would like to extend their knowledge of electronics into becoming radio amateurs.

If so, they will be interested in a brochure recently produced by the Radio Society of Great Britain. It is entitled *Amateur Radio — An Introduction*. It gives a very good synopsis of amateur radio as a hobby and will enlighten the reader on much about this activity which it is not possible to convey in a short feature like this article.

If you would like further information about amateur radio and the Radio Society of Great Britain contact:

David Evans, G3OUF, General Manager and Secretary, Radio Society of Great Britain, Alma House, Cranborne Road, Potters Bar, Hertfordshire, EN6 3JW.

10m FM Activity

Mention has been made in this feature on several occasions recently of the desirability of keeping as much activity going on the 10m amateur band as possible during the next few years, when the solar cycle will be such as to make any but local contacts unlikely. If this is not done and the band appears empty, others will soon move into it! No prizes for guessing who! FM activity on the band by radio amateurs is on the increase however, and it is to be hoped this mode will gain favour for local QSO's. There is some nice ex-CB gear around which can be bought for very reasonable prices and is easily modified for 10m FM amateur band use. So how about getting a 10m FM net going in your area? The preferred frequency for FM

seems to be from 29.440 to 29.700MHz, with 29.600MHz being the calling frequency.

Worldwide 14MHz Beacon Network

A worldwide beacon network has been set up as a contribution to this World Communications Year, using eight beacons on 14100kHz transmitting in sequence. They each transmit for one minute every ten minutes, commencing on the hour, and there is a two-minute break at the 8-minute point in each 10-minute period. The location and sequence of the beacons is as follows:

- 1) 4U1UN/B at United Nations, New York.
- 2) W6WX/B at Stanford University, California.
- 3) KH60/B at Honolulu Community College, Hawaii.
- 4) JA1IGY, Tokyo.
- 5) 4X6TU/B, Israel.
- 6) OH2B at Espoo, Finland.
- 7) CT3B, Madeira.
- 8) ZS6DN/B, Transvaal.

Each beacon transmits in morse code throughout its minute of the sequence, sending 'QST' followed by its callsign and four long dashes of nine seconds each, concluding with a repeat of its callsign. The power levels of the dashes decrease from 100 to 0.1W

For further information regarding operation and listener reports write to: *Al Lotze, W6RQ, 46 Cragmont, San Francisco, CA 94116, USA.*

This beacon net is working well and is an excellent indicator of propagation conditions on 14MHz. It is quite fascinating to follow the sequence throughout the day and observe how conditions change.

The Satellites

OSCAR 10 appears to be getting into its stride quite nicely. Lots of folk are having lots of fun with it. However the

same problem is arising as has happened with previous OSCARs; those with big aerials and high power are spoiling things for everyone else. The sort of power some people are using simply blocks the satellite, so that the majority of would-be users, operating at more reasonable power levels, cannot get in at all following the attenuation which comes into action when the satellite is subjected to too much power. To counter this, as much publicity as possible is being given to the problem and Mondays have been designated as 'QRP' days, as was done for earlier satellites.

Mode 'L' — 23cm up, 70cm down — was turned on on Wednesday 21st September. The responder response was considerably below what was expected, signals being well below those from the 70cm beacon. At the time of writing, the problem seems to be with a sticking relay. Mode L will also be on at various unspecified times, in addition to Wednesdays.

The next Space Shuttle trip should have a radio amateur aboard, as has already been publicised pretty widely. He is Dr Owen Garriott, W5LFL, who is an electrical engineer as well as an Advanced Class radio amateur. If all had gone to plan, the Space Shuttle 'Columbia' would have carried the European Spacelab into orbit at the end of October. Its scheduled flight path would have taken it over most of the more heavily populated areas of the world. The intention was (and still is) that the Shuttle would orbit at an altitude of 155 miles and at a speed of 17,000 miles per hour. This would give line-of-sight communication for up to eight minutes over most of the flight path. Normal QSO's cannot be engaged in under these conditions; instead — to enable as many folk as possible to 'get a look in' — W5LFL is to transmit on a number of pre-arranged frequencies and listen for

replies on a number of other frequencies. Earth amateur stations participating in this exercise would simply give their callsigns, which would be acknowledged by W5LFL.

The list of frequencies to be used is fairly complex, varying with the particular area of the world under consideration. Those interested in participating once the Shuttle is in orbit are advised to consult the specialist literature, or listen into the AMSAT-UK nets on 3780kHz on Sunday mornings at 1015hrs local time, for details of these 2m transmissions.

UOSAT is now working to a definite daily schedule, with different activities being arranged for each day; for instance the CCD camera is on on Wednesdays. Details and orbit times can be obtained by phoning the Satellite Control Centre at the University of Surrey's recorded message facility on *Guildford 61202*.

There is a possibility that another amateur radio satellite may be launched next year. A launch opportunity has become available through an existing satellite having 'gone sick'. A replacement for it is to be launched prematurely and there will be spare space — and weight — on the launch vehicle being used for this. So if anyone can get another amateur radio/experimental satellite built by then, we may get a replacement for OSCAR 8 in the not too distant future.



Dr Owen Garriott, W5LFL, at the console of Skylab in a photograph taken in 1973. He is shown controlling a battery of telescopes pointed at the Sun. Notice that, while he appears to be sitting, zero-gravity means that he doesn't need a chair.

When the Space Shuttle next goes up, taking the European Spacelab with it, Dr Garriott will again be aboard — and able to communicate with radio amateurs around the world on a number of pre-arranged frequencies.

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ATV on the Air

Presented by Andy Emmerson, G8PTH

We're back to activity reports again this month, justifying the 'on the air' title. So if you want to find out what's been going on in the 70cm band, higher up, or possibly in the world of slow-scan, sit back and enjoy.

70 centimetres

Seventy centimetres is where we start and it seems like we had some pretty good tropes (tropospheric conditions) this summer. John G8UWS in Folkestone, Kent, had a field day with some Belgians on 14th July, working Harry ON1AHT, Gerd ON1AGC, Jean-Paul ON6PD and Jean-Marie ON7ZR. RX only were ON7CI in central Brussels and Georges F6GOZ.

The name of Roger Bunney is well known in DX-TV circles, but Roger is into ATV as well. He uses a domestic UHF TV aerial at 58ft AGL, with plenty of low-noise pre-amplification and a modified Teleng bandpass filter (to cut out Group A broadcast QRM) to a Fortop converter. Good DX has been F6AGY (Blois, 325 miles) with P3 pix on 16th January and F1EDM (Bordeaux St Clair, 25km from Le Havre) P5 on the same day. Roger hopes to be transmitting from his Romsey location with a Fortop unit later this year. Activity in the Southampton area is high, thanks to a transmitter the Southampton club loans out. Roger also mentioned a scout demo station some time ago which operated for half the contest day of 18th June with no call sign and no 144.750 talkback. Demos are no excuse for inconsiderate operation; as it was, it largely wiped out Roger's chances.

Norrie Macdonald GM4BVU and three friends enjoyed the Leicester BATC exhibition, taking back a record of it on video to transmit later to less fortunates in central Scotland who could not make the trip. 1900hrs GMT on Monday is the local activity period up there; stations to find include GM6AOR (George, Longridge), GM6JUV (Bill, Motherwell), GM6UFJ (Andy, East Kilbride) and of course Norrie in Hamilton. Norrie

recently went portable 2000ft above Peebles and succeeded in working 40 miles to George GM3RVK in Kennaway, Fife with P5 pix. Norrie adds a final note: an appeal for tape swaps got a better response from USATV Society members than from UK ATVerS!

Jack G8ZWM in Crawley has become G4TVC! TV Crawley, I suppose — I wonder how much he had to bribe someone for that! (Ted G6CTV is another ATVer who managed to get a 'TV' call.) Anyway, Jack writes that activity in his neck of the Sussex woods is almost nightly with Andy G6LMU, Bob G6LVN, John G4SFP, Mick G6IPP and Mick G6COQ. Also Doug and Dave G3HYV and G4PFX in Horley, and an operator known as 'Pirate Pete' (BATC member and twice failed RAE!).

The Home Counties ATV Group (G6HCT) went /P for its July meeting to a spot known as Old Redding near Harrow Weald. Pix were exchanged with several locals, also with Mike G8LES/P in Petersfield, Hants, which sounds like a good haul to me.

24 centimetres

Moving up the spectrum to 24cm, or the growth band as we call it, we have more news from Jack G4TVC. He has built an experimental 24cm TX and has had some duplex QSOs. It is due for a rebuild now as soon as time can be found. Still in Sussex, the Worthing repeater mob put on a 24cm demo for the Brighton rally this year. John G6MPE provided a signal for reception at the Racecourse site from his home not far away. John has also had success working France: F1EDM was worked as a two-way with just 2W on 1255MHz. On 17th August John worked Georges F3LP in Le Havre, while Martin G8KOE had a two-way and Roy G6AIW saw them all P5. G6MPE and G8KOE are on the air almost every night with sound and colour vision over a 6km path on 1255. Pix are better than on 70!

John uses a 24cm Tonna, while Martin has a similar homebrew device with one

extra element. John's transmitter is to a KOE design, using a RadCom microwave drive source (FM modulated) which passes the signal to a varactor and an interdigital filter built to the VHF Handbook design (in CQ-TV 120). The filters were made by Roy, who also made some for the GB3WX repeater: these are silver plated and perform well. Martin's TX is the Wood and Douglas FM oscillator (latest design): this too performs well. Output is to a MHW-710 'blue brick' and varactor tripler, producing 2 or 3W on 1255. Both stations employ the CQ-TV122 design RX. Roy speaks for all the Worthing area stations when he says 'I am really chuffed with 1255. I think more people ought to have a go. RX can be critical but you get good results with just a few watts'.

Gary G4CRJ called in at the Woburn rally to tell us about 24cm activity in the London area. Apart from the stations mentioned last time, there are Mike G8LES in Thames Ditton (TX/RX) and Gary with 550ft ASL in High Wycombe (currently RX only). He sees Mike P2 with no pre-amp, the path being 15km. Gary is planning a transmitter, possibly a power oscillator and a phase-locked loop at 24cm. Although it is not an exceptional problem, radar interference from Heathrow is quite strong at two spots in the band, white spots appearing on the screen even with no aerial!

By the way, if you want a copy of the latest printout of 24cm stations on the air, just drop me a line — and an SAE — care of the editor.

Three centimetres

We haven't covered 10GHz before but Gary G4CRJ has been out trying portable operation on this band. On 13th August he took his gear to Blunston near Swindon in Wiltshire. Grade 3 pictures were received over a 14km path from G4CRG/P who was also out portable — at Barbury Castle 268m above sea level on the top of the Marlborough Downs.

The link was established for an hour (with some fading occasioned by passing cars), while Gary tried to find a way of making a video recorder work from a flat battery. Poking 12V from the car battery into the VCR camera socket had no effect, so in desperation Gary put jumper leads from the car battery across the VCR's NiCad! It worked and Gary came away with visual proof of the contact as well as being able to show G4CRG how the pictures had come across.

Gary's transmitter was G4CRG's design of varactor-tuned 15mW Gunn oscillator feeding a 10-inch dish aerial. The receiver was a G4CRJ design using a hybrid-tee mixer down to 500MHz, then a TV tuner down to 38MHz IF and a quadrature detector. An 18-inch dish aerial was used at the G4CRJ/P end. This equipment was built five years ago and apart from displays at exhibitions has never made a 'real' contact. Success, at last

Slow-scan

Not much SSTV news this time — just Jack G4TVC (he gets three mentions this time!). He explains that all the morse

Norrie Macdonald GM4BVU in his shack in Hamilton





How GM3ULP comes into Norrie's shack

bashing was to get his SSTV gear on HF. Hectic activity has resulted in contacts with VK3DUJ and VK6ES in Australia; he cannot find any SSTVers in New Zealand. He adds that suitable filters for SSTV are Kodak Wratten Nos 25, 47B and 58. These

are £3.43 each from *Allphotos Ltd, Tarring Road, Worthing, Sussex.*

Finally a note on our photos. If you're curious about how the other guy sets out his shack, the picture of Norrie Macdonald's place will be of interest; looks

like a loft conversion to me. Norrie is in Hamilton (see the namecheck in the 70cm section above) and the other pic displays how GM3ULP comes in there.

Oscar and ATV

To close, I must mention I have heard the first report of QRM between ATV and Oscar operators on 70cm. (No names but the Oscar SSB 'killed' the TV; not what you might have expected...) Despite what some space operators say about ATV's band occupancy on 70cm, just consider the following:

- With the 70cm band being whittled down by PMR, MOLD and SYLEDIS (and in Belgium, by direct confiscation), we amateurs need justification for ten whole MHz at 70cm. Wideband modes like ATV are just such a justification.

- ATV is still an experimental mode and on those grounds cannot be swept under the carpet.

- All amateur radio modes have an equal right to the bands, and ATV has been established on 70cm since the 1950s. No single mode has the right to take precedence.

Let's all work together to achieve peaceful coexistence between all modes and sort things out ourselves. The last thing we need is intervention by the official authorities, which is what has happened in Germany.

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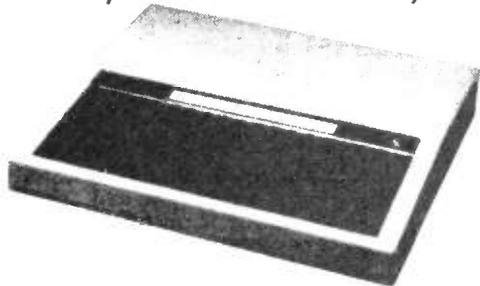
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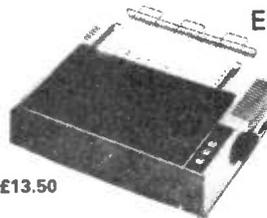
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	No. of ways			
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31-way	170p	170p
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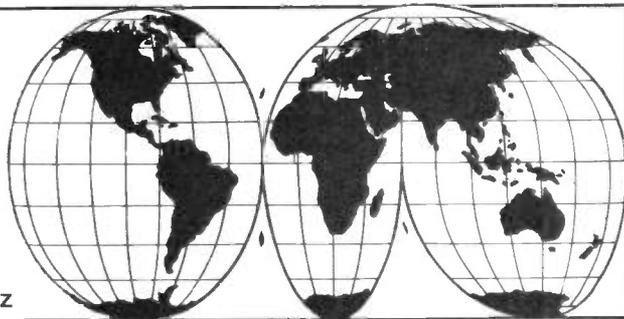
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SHORT WAVE NEWS FOR DX LISTENERS

by Frank A Baldwin

All times in GMT, **bold** figures indicate the frequency in kHz



Keeping to the promise made in the last issue of this journal, we deal now with some of the Latin American stations that may be logged on one of the difficult bands — the 90m Tropical Band (**3200 — 3400**) which is difficult in that commercial QRM (man-made interference) abounds and one therefore needs to be equipped with a highly selective receiver and, preferably, an outdoor long-wire aerial system. On this occasion I offer a selection of the more easy-to-receive transmitters.

Belize: Belmopan operates on **3285** and identifies as 'Radio Belize'. It opens at 1100 (Sundays from 1200) and closes at 0510, the power is 1kW, and the programme languages are English and Spanish. Probably the best times for UK listeners to log this one would be during the English language sessions which are scheduled from 0030 to 0510. Newscasts in this period are at 0100, 0200 and 0300, the latter being a relay of the BBC World Service. The full announcement in English is 'This is Radio Belize, Voice of the new Central American Nation of Belize in the Heart of the Caribbean Basin'. If you do manage to log this one and wish to QSL, the address for reports is Radio Belize, PO Box 89, Belize City, Belize, Central America.

Brazil: Two stations located in Brazil are most often reported as operating on this band, one being Lins Radio Clube which operates on **3225** from 0730 to 0400 with a power of 1kW. The callsign is ZYG859 and the address is CP 310, 16400 Lins, Sao Paulo, Brazil. The second easy-to-receive Brazilian is Radio Ribeirao Preto operating on **3205** from 0800 to 0400 with a power of 1kW. The address is listed under ZYG861 as CP 814, 14100 Ribeirao Preto, Sao Paulo, Brazil.

The best time for UK listeners to log either of these Brazilians would be from around 0100 to their closing times. Have I logged them? Yes, many times over the past few years.

Ecuador: HCYD4 Radio Iris in Esmeraldas Province can often be heard on **3380** at which point on the dial it is scheduled from 1000 (Sundays from 1100) to 0400 with a power of 10kW. The port of Esmeraldas, on the river of the same name, is noted for exports of bananas, tobacco, rubber and cacao (cocoa to you and me). Having set the scene, the address for reports is Casilla 8, Esmeraldas, Ecuador or Casilla 1018 Quito.

Another one to log is the 12.5kW transmitter of Radio Zaracay, Santo Domingo de los Colorados on **3395** from where it produces programmes for local consumption from 1000 to 1400 and from 2000 to 0500. The address is Casilla 31, Santo Domingo de los Colorados, Ecuador. Have I heard them? Yes, indeed most DXers have.

Guatemala: Probably the easiest of the Guatemalans for UK-based listeners is undoubtedly Radio Chortis Jocotan on **3380** with its schedule from 2100 to 0300 with a power of 1kW. Quite often logged when conditions on the band are good, the address for reports is Centro Social Jocotan, Chiquimula, Guatemala and this is one of the few in this country that does reply with a QSL — if you are lucky!

Another Guatemalan is Radio Cultural on **3300** with a 5kW signal which is on the air from 1100 to 1500 and from 2245 to 0430. The address is Apartado 601, Guatemala but the station is owned by Central American Mission, Box 28005, Dallas, Texas 75228, USA.

For Guatemala listen from 0130 onwards. Have I? Yes.

In the next issue, a change of scene as we will be dealing with some of the relatively easy-to-receive stations site in Indonesia and operating on the 60m band (**4750 — 5060**) simply for the reason that it is now the 'season' for European DXers to log these transmitters. We shall return to 90m band Latin Americans at a later date.

AROUND THE DIAL

In which are listed some of the transmissions recently logged and thought to be of interest both to the short wave listener and the DXer — a mix for the attention of both types of reader and sorted this month by computer!

AFRICA

This continent, is not so 'dark' as it once was; there are many stations in Africa that can be heard by UK listeners roving over the 60m band.

Benin

Radio Parakou on **5025** at 0429, orchestral music African style, YL's with a song in vernacular, OM with station identification at 0431. Schedule 0400 to 0900 and from 1700 to 2300. The power is 20kW.

Cameroon

R Bertoua on **4750** at 1948, YL with a local pop song complete with African musical backing. Operating with a 20kW transmitter, this one is on the air from 0430 to 0800 and from 1600 to 2208. There is an English programme from Monday to Friday from 1800 to 1840 and on Sunday from 0615 to 0645.

Central African Republic

Bangui on **5037** (listed **5035**) at 2022, OM and YL with a discussion in vernacular. Bangui operates from 0430 to

0700 and from 1630 to 2300 in French and the local language Sango. Not an easy one to log owing to the surrounding QRM. The power is 100kW.

Guinea

Conakry on **4910** at 0413, OM with a news review in French. No sign of Lusaka on the same channel. The schedule is from 1230 through to 0730 and the power is 18kW.

Kenya

Nairobi on **4934** at 1900, African drums, YL with a song in Swahili. This is the North Eastern and Coastal Service which is timed on this channel from 0250 to 0630 and from 1420 to 2010 with a power of 20kW.

Nigeria

Kaduna on **4770** at 1947, OM announcer with a programme of local pops on records. Kaduna is on the air from 0400 to 2400 according to the listing but I have recently heard them closing at 0100. The power is 50kW.

South Africa

Johannesburg on **4880** at 2016, when radiating a programme of classical orchestral music with announcements in Afrikaans. This is the Home Service in Afrikaans and is scheduled here from 0348 (Saturday from 0427, Sunday from 0457) to 0550 and from 1520 to 2120 (Saturday until 2200) with a power of 100kW.

Senegal

Dakar on **4890** at 2019, OM with a news review in French. This is the National Service (Chaine Nationale) which operates from 0600 to 0900, from 1155 to 1600 and from 1715 to 0100.

(LATIN) AMERICA

Plenty of stations to choose from in this part of the world.

Brazil

Radio Dragao do Mar, Fortaleza on **4925** at 2349, OM with an exciting sports commentary — in Portuguese of course. Listen for this one anytime between the opening of the evening session at 2130 and the closing time of 0300. The power is 5kW but wait for the identification — R Difusora Taubate — as another Brazilian is also on channel but with a 1kW signal.

Radio Globo on **11805** at 0038, OM with announcements in Portuguese, OM with a sorrowful ballad. With a 10kW transmitter in Rio de Janeiro, this one is timed from 0800 to 0330, the latter time being variable.

Radio Bandeirantes, Sao Paulo on **11925** at 0042, OM with a *futebol* (football) commentary — a review of past matches. R Bandeirantes is on the air from 0800 to 0400 and has a power of 10kW.

Colombia

Emisora Nuevo Mundo, Bogota on **4755** at 0447, YL with a ballad in Spanish, OM with station identification at 0450. Often heard around this time, it has a 24-hour schedule and a power of 1kW.

Radio Super, Medellin on **4875** at 0456, OM with station identification which was followed by a trumpet fanfare. This one also has a 24-hour schedule and has a power of 2kW. A regular 'visitor' to my shack!

Cuba

Havana on **4765** at 0224, OM with a talk in Russian which was a relay of the Moscow 'Mayak' (Lighthouse) domestic programme, presumably for the benefit of the Russian merchant marine etc, based in the general area. Bad news for DXers as this powerful transmitter effectively blocks other more interesting LA stations.

Dominican Republic

Radio Clarin, Santo Domingo on **11700**, OM with station identification and announcements in Spanish, then into a programme of local pops. Radio Clarin is on the air from 1100 to 0500 with a power of 50kW.

Ecuador

Radio Luzy Vida, Loja on **4851** at 0435, OM with a love song in Spanish and a guitar backing. The schedule is from 1045 to 0430 with a 2kW signal. Obviously running late or extended schedule on this occasion.

Honduras

La Voz Evangelica, Tegucigalpa on **4820** at 0449, YL's with a religious pop-type song with guitar backing, OM with announcements in Spanish. LV Evangelica has an English programme from 0300 to 0500 according to the list but deviated on this occasion for some reason or included a Spanish announcement on the tape.

Peru

Radio Andina, Huancayo on **4996** at 0442, guitar music in local style, OM with *noticias*. This one operates from 1000 to a variable closing time of 0500 with a 1kW signal. Take care, however, as this channel is now also occupied by a new station on the air based in Ecuador and logged here at 0212, identifying as 'Radio Bahai' at 0215.

Radio Eco, Iquitos on **5112** at 0356, OM with a long talk (or so it seemed) in Spanish. Rather difficult to log, this one operates from 1000 to 0500 and has a power of 1kW.

Venezuela

Radio Tachira, San Cristobal on **4830** at 0231, OM with a programme of local pops. Scheduled from 1000 to 0500 at 10kW. An easy one to log.

ASIA

The world's largest continent with a correspondingly large number of stations.

Afghanistan

Kabul on **4740** at 1843, OM announcer and music in the local style. This is the Home Service 1 which is timed from 0125 to 0330 and from 1230 to 1930.

China

Xizang PBS on **4735** at 2334, OM with the programme in Uigher. The best time to hear this one is during the scheduled 2230 to 0200 transmission. Also on **4750** at

2330, OM with a talk in Chinese during the 2230 to 0200 part of the schedule. Xizang was formerly Lhasa in Tibet.

India

AIR (All India Radio) Delhi on **9665** at 2001, OM with a newscast in English during the English transmission for the UK and West Europe, timed from 1845 to 2230 on this channel. Also on **11755** at 2015, OM with a newscast in the English programme for North and West Africa, scheduled from 1945 to 2230.

AIR Delhi also on **17387** at 0958, interval signal and YL with station identification in English at the start of the English transmission directed to North East Asia and Australasia, scheduled from 1000 to 1100.

Japan

Tokyo on **21610** at 0800, OM with station identification and frequencies at the start of the English programme for Europe, followed by a newscast of both world and Japanese events. The English transmission is timed for Europe from 0800 to 0830. Also logged in parallel on **17870**.

Kuwait

Radio Kuwait on **11675** at 2049, a programme of UK-made pop records during the English transmission to the Arabian Gulf, North Africa, South Africa, Europe and North America and timed from 1800 to 2100. Also on **11990** at 0802, local style music and songs in the Domestic/External Service which is on this frequency from 0600 to 2105.

Pakistan

Karachi on **17660** at 0813, YL with announcements in Urdu during a World Service transmission to the UK scheduled from 0715 to 1100 (news in English from 1005 to 1010).

Saudi Arabia

Riyad on **9870** at 1904, OM with songs in Arabic in a Domestic Service programme, this service being timed on this channel from 1700 to 2130.

South Korea

Seoul on **15575** at 1857, YL

with a talk about internal affairs in the English programme for Europe, scheduled from 1845 to 1945.

EUROPE

The easiest of all to receive and mostly of interest to those just starting in the hobby.

Bulgaria

Sofia on **17825** at 1843, YL with station identification and a talk about trade, all during the English transmission for Africa, timed from 1830 to 1930.

Finland

Helsinki on **15430** at 1850, OM with a talk about local theatres during an English programme for Europe, scheduled from 1830 to 1855.

Hungary

Budapest on **6110** at 2004, OM with a newscast in the English programme for Europe, on this channel from 2000 to 2030.

CLANDESTINE

Just for a change, try the following:

'La Voz del CID' on **5106** at 0446, OM with a ballad in Spanish, OM with station identification at 0447. CID stands for Cuba Independiente Democratica, and the programmes are anti-Castro.

'La Voz de Sandino' on **6220** at 0405, OM with station identification and then OM with a tirade in Spanish, all about El Salvador and Nicaragua.

'Radio 15th September' ('Radio Quince de Septiembre'), OM harangue about Nicaragua in Spanish. This one is anti-Nicaraguan, and thought to be located in Honduras.

NOW HEAR THESE

'Radio Los Andes', Tarija, Bolivia on **4775** at 0203, OM with ballad in Spanish, OM with announcements; 'Radio Tezulutlan', Coban, Guatemala on **4835** at 0152, OM with talk in Spanish about Guatemala; 'Radio Pampas', Tayacaja, Peru on **4854** at 0224, OM with pop song in Spanish, promos; 'Radio Madre de Dios', Puerto Maldonado, Peru on **4951** at 0123, YL with songs in Spanish, OM with announcements and local promos.

DX-TV RECEPTION REPORTS

Compiled by Keith Hamer and Garry Smith

Sporadic-E activity dropped dramatically and unexpectedly during early August; however this wasn't the end of DX reception. Anticyclonic conditions produced excellent tropospheric DX in Band III and on UHF from the 8th onwards and at the end of the month several rare transmitters were received in parts of the UK.

Band III MS (Meteor Shower) activity due to the Perseids around the 10th proved to be disappointing, but on the 30th the 100kW outlet at Pardubice on the Czechoslovakian channel R6 was noted here in Derby, showing the familiar EZO electronic test card.

Reception reports

Mike Allmark (Leeds) managed to log almost every transmitter in Europe, judging by his reception report. The highlights are as follows:

1/8/83: Several Eastern-bloc countries on channels R1 and R2; NRK (Norway) on E2 with the 'STEIGEN' PM5534 pattern; ORF (Austria) with the test card on E2a. All reception via Sporadic-E (SpE).

2/8/83: SR-1 (Sweden), NRK and DR (Denmark) all on channel E4 via SpE.

3/8/83: TVP (Poland) on R1 and R2 relays; DDR: F (East Germany) E4; Spain (RTVE); RAI (Italy) via SpE on channel IB.

8/8/83: Excellent strength UHF tropes from Northern Germany (mainly ZDF, i.e. Zweites Deutsches Fernsehen) on channels E23, 30, 31, 32, 33, 34, 35 and 39; NDR (Norddeutscher Rundfunk) 3rd network on E40 42 and 43; NDR 1st Network on E50 53 and 56. The DR channel E10 Vestjyl-land transmitter was also received.

10/8/83: DR on E5, 7 and 10; NRK from Halden on E11; NDR on E7 and 10 plus many NDR and WDR West German UHF outlets.

19/8/83: DR on E7, 10; WDR on E11; ZDF on E21, 22, 24, 30, 34, 37 and 39 plus NDR-1 on E40.

25/8/83 and 26/8/83: Similar to the 19th but with BRT (Belgium) on E10, NOS (Netherlands) on UHF and several TDF (France) UHF stations.

28/8/83: NOS on E6; NDR on E5, 7, 9, and 10; DR on E5, 7, 10; BRT on E10; SR on E9; NRK on E6 from Bjerkreim; SR-2 on E30; several ZDF and NDR outlets on UHF.

29/8/83: Band III stations similar to the 28th but also SFB (Sender Freies Berlin) on E7 and DDR:F on E5; SR-2 on E30; ZDF on E34, 35 and 39; NDR-1 on E53 and 56; NDR-3 on E43. NOS-1 and NDR-1 were also noted on channel E4.

30/8/83: DDR:F on E6; DR on E6, 7; SR on E5 and 10; HR-1 (Hessischer Rundfunk in West Germany) on E7; NDR-1 on E10; RTL

(Radio-Tele-Luxembourg) on E7; SR-1 on E43.

31/8/83: Tropospheric conditions declined but ducting brought in SR on channel E31, DR on E10, NOS in Band III and UHF plus a few ZDF and NDR signals on UHF. RTE-1 (Radio Telefis Eireann) on channel H was noted with very strong video.

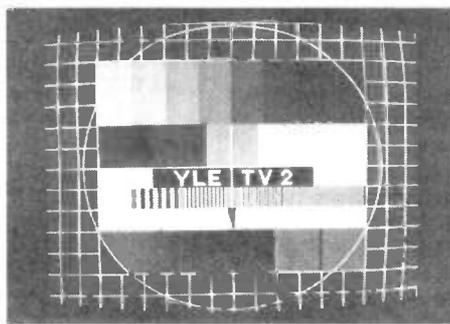


Fig 1 Finnish second network FuBK test card. (Photograph courtesy of Petri Poepoenen, Finland)

Mike comments that the 1983 DX season has been a 'short, sharp affair' with several exotics being in evidence although Band III SpE activity has been lacking. Towards the end of July (21st), Mike noted a prolonged opening to Jordan (JTV) on channel E3. JTV initially radiated frequency gratings from 0800 BST going on to the PM5544 test card which he resolved in colour. Tropospheric ducting was also present and he saw TSI-Switzerland (Italian-language network) on E34 from the La Dôle transmitter, SWF (Südwestfunk, West Germany) on E10 from Donnersberg, BR (Bayerischer Rundfunk based in Munich) on E10 from Wendelstein, BR-1 on E10 (Würzburg), SDR (Süddeutscher Rundfunk) from Heidelberg on E7 and Stuttgart on E11 plus ZDF on E40 (Raichberg) and E35 (Rottweil).

Kevin Jackson (Leeds) similarly did well with reception. His August SpE successes included ORF (Austria) on E3 from the 100kW transmitter at Birkfeld and several instances of strong and prolonged reception of the TVR-Rumania channel R2 outlet at Bucuresti. Tropospheric ducting on the 29th at 1102 GMT produced the Norwegian PM5534 pattern on E9 displaying the 'VEGA' transmitter identification. This is situated on an island just off the Norwegian coast some 80 to 100km south of the Arctic Circle. The transmitter power is 30kW and the reception path is about 1500km.

Equipped with a Wolsey Colour King

UHF array and a Labgear CM7060 amplifier, Derek Fenton (Mickleover, Derbyshire) has received several continental television signals recently. These include Belgium on E28 from Wavre and the E52 Riviere outlet radiating the 'Profondeville' PM5544, West Germany with the 'WDR 1' FuBK test card plus several IBA regions. His clear take-off to the west enables daily reception of HTV Wales on Channel E49 in colour from Moel-y-Parc.

Simon Hamer (New Radnor, Powys) has sent a very descriptive reception report detailing signals from TVE-Spain, RTP-Portugal, JRT-Yugoslavia, RAI, ORF, ARD (West Germany) with the news programme 'Tagesschau', TSS-USSR, DR-Denmark, Czechoslovakia and MTV-1 Hungary. One of his unidentified signals was one featuring Arabic writing on 4th August at 1900 BST from an E3 transmitter. This could well have been JTV-Jordan although one must not jump to conclusions every time Arabic script is received — it could well have originated from a West European country.

Armed with a Russian-made 'Vega' CCIR portable, Roger Bunney (Romsey) noted excellent SpE reception at his cliff-top holiday location on the Isle of Wight. Belgian E8 and E10 plus French UHF signals were present all the time — 'a good DX-TV location' comments Roger. Once back on the mainland he noted a strange Russian clock caption with the time exactly the same as in the UK!



Fig 2 Identification caption radiated by the first network of Yleisradio, Finland

Service Information

United Kingdom: The BBC and IBA have advised officially that the ultimate close-down of the VHF 405-line service will be on 6th January 1985 despite rumours that January 1984 would be the date.

West Germany: A new 500kW outlet on channel E56 has been opened at Hamburg.

Yugoslavia: The authorities have installed relay stations in the north of the country at Lakos and Lendava for the redistribution of programmes from the state-owned Hungarian service Magyar Televizio (MTV).

Sweden: A new regional television service was inaugurated last Spring, covering the Smaland area of southern Sweden. The studios are located at Växjö and the regional news programme is called 'Smalandnytt'. It is broadcast each weekday between 1815 and 1830 BST via the following TV-2 transmitters: Nässjö (1000kW, E22), Västernik (1000kW, E26),

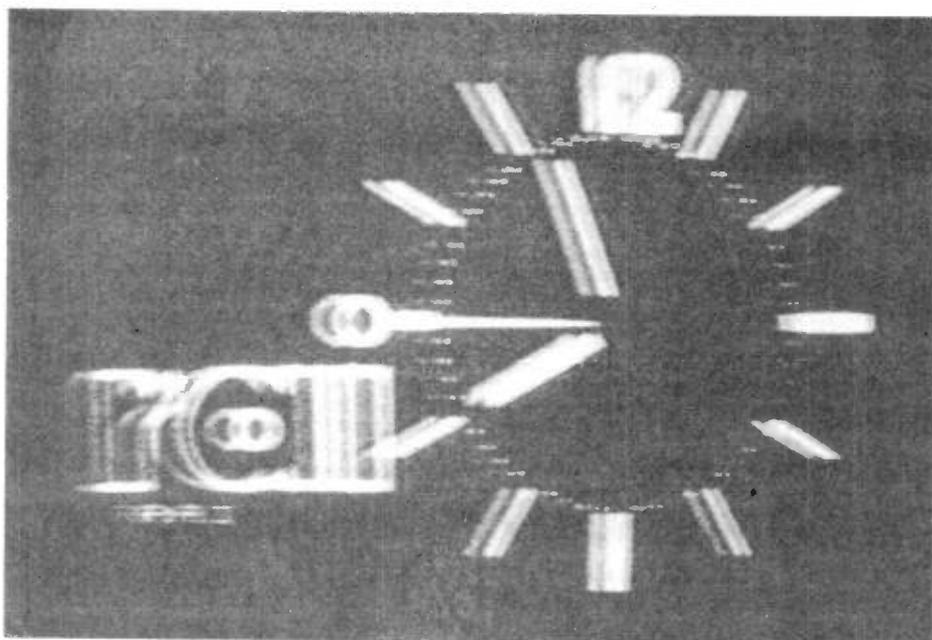


Fig 3 Clock caption received via Sporadic-E propagation from RAI-Italy. Note the typical SpE ghosting effect.

Jönköping (15kW, E28), Emmaboda (1000kW, E31), Vislanda (1000kW, E32) and Finnveden (1MW, E48).

Spain: A new regional test card has been seen on E4 during the month. We hope to have further details shortly.

Information this month courtesy of Roger Bunney (Romsey), Goesta van der Linden (The Netherlands), Alexander

Wiese (West Germany) and Clive Athowe (Norwich).

Euro-TV List

Roger Philips (Cobham, Surrey) has pointed out a few omissions from the 'Euro Broadcast TV Services' list which we included in the August edition of *R & EW*. The UK Channel 4 was missing

as was TV Koper Capodistria under the Yugoslavian section. The latter service beams a programme in the Italian language to Northern Italy, which is ultimately relayed via private stations. However, an earlier test card used by JRT carried the identification 'RTV LJUBLJANA' at the top and 'STUDIO KOPER CAPODISTRIA' at the bottom implying that it is part of the RTV-Ljubljana network. We would be pleased to hear from other readers with any comments on this subject.

In his letter, Roger suggests that Bands I and III should be reserved for a re-engineered UK service (for example, local TV) rather than being simply handed over for PMR etc. He points out that the interference problems created within Europe will be devastating for Continental television services during periods of enhanced propagation, if current whims and ambitions go ahead. Home Office take note!

German DX Club

This club's magazine, called 'Tele-audiovision', should prove of great interest to DX-TV enthusiasts with a good technical knowledge of German. All subjects associated with TV and VHF radio are covered in the magazine which is published bi-monthly. Full details can be obtained from the editor, Alexander Wiese, by sending an IRC to TAV, Postfach 801965, D-8000 München 80, West Germany. A brief summary in English is sent with each edition.

EVENTS: MOBILE RALLIES

15th November	The Workings of BBC Radio News	Biggin Hill	Ian Mitchell G4NSD
29th November	Advanced Manufacturing Technology	Carlton House Terrace, London	Royal Society, 01-839 5561
30th November	CAD Modelling	Southampton	Computational Mechanics Centre, 042129 3223
1st December	Holography and Holographic Measurements	SEEBOARD HQ, Hove	IEEIE, 01-836 3357
6th December	Electronic Aids for the Disabled	Granville College, Sheffield	IEEIE, 01-836 3357
6th December	IEE Wiring Regulations (15th edn)	SEB Offices, Reading	IEEIE, 01-836 3357
7th December	World Communications — Tomorrow's Trade Routes	Royal Lancaster Hotel, London	British Computer Society, 01-637 0471
7—8th December	Technology in the 1990s	Carlton House Terrace, London	Royal Society, 01-839 5561
10th December	RSGB AGM	IEE, Savoy Place, London	RSGB, Potters Bar 59015
11th December	Leeds & DARS 3rd Annual Christmas Rally	Civic Centre, Pudsey	G6CJI
12th December	Electrical aspects of the APT	IEE, Savoy Place, London	IEEIE, 01-836 3357
13th December	Sale of surplus equipment	Biggin Hill	Ian Mitchell G4NSD
14th January	RSGB Residential Installation	Cardiff Castle, Cardiff	RSGB, Potters Bar 59015
5th February	Bury Radio Society Ham Feast	The Mosses Centre, Cecil Street, Bury	MHS Bridge G3VC
18th March	4th Annual Components Fair	Carleton Community Centre, Pontefract	A Mason G4TGU
1st April	White Rose ARS Rally	University of Leeds	N Whittingham G4ISC
28—29th April	RSGB National Amateur Radio Exhibition	National Exhibition Centre, Birmingham	AN Bramley G4NDU
			RSGB, Potters Bar 59015