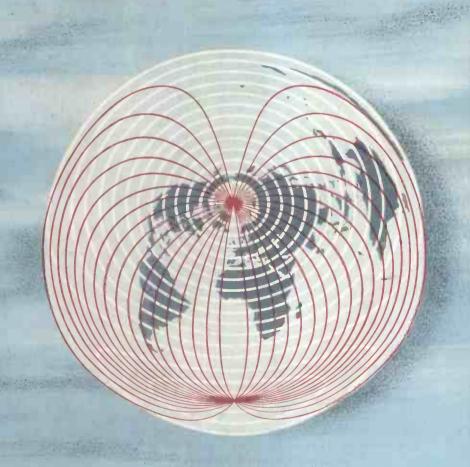
# Wireless World

Radio · Electronics · Television



FORTY-FOURTH YEAR OF PUBLICATION



# Photo-Electric Multipliers 27M1 and 27M2

for light operated relays, film scanning, facsimile transmission, and many Research and Laboratory investigations involving low light levels.

### Now available for prompt delivery

**27M1** The 27M1 is a nine stage high vacuum photo cell with high response in the visible region. When operated at 100 volts per stage it is capable of multiplying very small currents produced under weak illumination by an average value of one million times. Under normal operating conditions the resultant output current is a linear function of the exciting illumination. The frequency response is flat up to the frequencies at which transit time of electrons within the valve becomes a limiting factor.

Because of its great sensitivity, low noise level, low dark current and freedom from distortion the 27M1 may be used for light operated relays, film scanning, facsimile transmission and in scientific research involving low light levels. In many applications its small size is an advantage. List Price: £15.

**27M2** The 27M2 is a nine stage high-vacuum photo-cell similar to the 27M1 except that it has wider tolerances on the anode dark current necessitating a lower anode supply voltage with a resultant reduction in the current amplification to approximately one quarter of that obtainable from the 27M1. It is capable of multiplying very small currents produced under weak illumination by an average value of 250,000 times when operated at 80 volts per stage.

The 27M2 is suitable for the same applications as the 27M1 wherever the reduced magnification is acceptable. List Price: £6.



The secondary cathodes, or dynodes, of these multipliers are arranged in cylindrical formation so that they are exceptionally compact.

Incident

#### TYPICAL OPERATION

Voltage between anode and secondary cathode K10- - - - - 50 volts Voltage difference per stage - - - 100 volts Maximum anode dark current (with 100 volts between anode and cathode K10) - 0.25µA Luminous sensitivity (taken on the basis of a lamp colour temperature of 2700°K and a light area of 5 mm x 20 mm) - - 20A/lumen Current amplification (ratio of anode sensitivity/cathode sensitivity) - - - 10e

### TYPICAL OPERATION

Voltage between anode and secondary cathode K10- - - - - - - - 50 volts Voltage difference per stage - - - - 80 volts Maximum anode dark current (with 80 volts between anode and secondary cathode K10) - - - - - - - - - 0.25µA Luminous sensitivity (taken on the basis of a lamp colour temperature of 2700°K and a light area of 5 mm x 20 mm) - - 2.5A/lumen Current amplification (ratio of anode sensitivity/cathode sensitivity) - - 0.25 x 10°

Either the 27M1 or the 27M2 may be used as a plug-in replacement for the American type 931A. A special stabilised power unit providing a highly stable H.T. supply for photo-multipliers is available. Full details on request.

# EDISWAN

MAZDA RADIO DIVISION

THE EDISON SWAN ELECTRIC COMPANY LIMITED

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SVI

# Wireless World

RADIO, TELEVISION AND ELECTRONICS

#### 44th YEAR OF PUBLICATION

Managing Editor: HUGH S. POCOCK, M.I.E.E.

Editor: H. F. SMITH

SEPTEMBER 1954

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### VALVES, TUBES & CIRCUITS

#### 21. DETECTION IN F.M./A.M. RECEIVERS

For the detection of frequency modulated signals it is necessary to convert frequency changes into amplitude changes and to recover the intelligence contained in the original signals from the amplitude modulated carrier. The method most widely used for this purpose employs a form of phase discriminator known as the ratio detector. The particular advantage of the ratio detector is its excellent suppression of any amplitude modulation which may be present on the F.M. carrier as a result of noise or variations of gain in the earlier stages of the receiver. This type of circuit has good sensitivity and eliminates the expense of providing additional limiting stages.

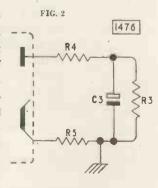
A typical form of ratio detector circuit is shown in Fig. 1, and it will be noted that two diodes with independent cathode connections are necessary. The Mullard EABC80 is recommended for use in this type of circuit. This valve is a combined triple diode and voltage amplifying triode, with a heater rating of 6.3V, 0.45A, and it is mounted on the B9A (noval) base. One diod (a"d) is provided with a separate cathode (pin 3), the other two diodes and the triode sharing a second cathode (pin 7). The ratio detector circuit employs two of the diodes (a"d and a"'d) which have low impedances (about 200 $\Omega$ ) whose ratio never exceeds 1.5. The other diode (a'd) is suitable for use in A.M. reception as a conventional detector and generator of A.G.C. voltage. The triode section is designed to be used as an audio amplifier following the detector during both F.M. and A.M. reception. Its electrical characteristics are similar to the triode section of the Mullard EBC41.

In the circuit illustrated, the primary winding L1 of the ratio filter is in the anode circuit of the final I.F. valve. The secondary coil, L2, is tuned to the intermediate frequency (10.7 Mc/s). The voltages in the two halves of L2 have a 180° phase difference, and their magnitudes depend upon the sweep frequency of the F.M. signal. The tertiary winding, L3, consisting of a few turns wound over the anode end of the primary, matches the anode circuit of the preceding I.F. stage into the diode circuit.

The ratio detector can take the form of a balanced circuit in which two equal capacitors are placed across the load resistor, R3, and their common connection taken to earth. In Fig. 1 the unbalanced type of circuit is given. Here only one capacitor, C1, has been retained, from which the audio output is taken. The  $5\mu F$  electrolytic capacitor, C3, is then necessary to stabilise the voltage across R3.

The value of load resistance ( $56k\Omega$ ) is a compromise between that required for optimum gain and the necessary A.M. suppression. Good A.M. suppression is also achieved by using a relatively high resistance,  $1.2k\Omega$ , in series with the tertiary coil. Further increase in the value of load resistance (say, to  $68k\Omega$ ), whilst resulting in larger ouput voltage, requires more satisfactory balancing in the preceding circuit in order to keep the rejection of A.M. to an acceptable value. Thus a trimmer capacitor could be connected from the centre-tap on the secondary to earth, and a small series resistance included in the lead from the centre-tap to the tertiary coil L3. These modifications will lead to a considerable improvement in suppression and some increase in sensitivity, but the preliminary adjustments to the trimmer are much more involved.

As a further refinement, some suppression can be sacrificed by connecting the stabilising capacitor across only a part of the total diode load (Fig. 2). With suitable values for R4 and R5 the suppression will depend to a much smaller extent on spreads in the forward resistance of the diodes and on variations in the amplitude.





Reprints of this advertisement together with additional notes may be obtained free of charge from the address below.

# Wireless World

SEPTEMBER 1954

VOL. 60 No. 9

### Authority and Independence

E have now had ample time to study the new Television Act, which became law just after our last issue appeared. The Government's plan for an "additional" television service, though somewhat involved, is not on the face of it, difficult to understand, though we must admit to doubts as to how some of the details will work out in practice.

To us, the most interesting section of the Act is that in which the Postmaster-General is given what appears to be very wide powers over the technical activities of the Independent Television Authority. In this matter, at least, there appears to be little independence and no authority! Of course, it is a fact that in Great Britain the P.M.G.'s power over every form of radio activity is sweeping; he may make regulations prescribing "the things that are to be done or are not to be done" by any one of his licensees. Of course, he may intend to keep these powers up his sleeve, and allow the I.T.A. as much technical autonomy as is enjoyed by the B.B.C. If he does not, one is tempted to ask, what is the purpose of the I.T.A.? It would surely have been less wasteful of national resources and effort to leave the technical means of television distribution in the hands of the B.B.C. The Government's quarrel with the B.B.C. monopoly was that it represented a monopoly in the dissemination of ideas; that objection would have been overcome much more economically by setting up a chain of transmitters operated by the B.B.C. but fed with programmes under the control of a truly independent body getting its revenue from advertisements.

The Post Office decision, announced before the new Authority came into being, that the I.T.A. transmissions were to be polarized like those of the B.B.C. in the same areas, may or may not lend colour to the idea that the P.M.G. intends to make himself responsible, not only for controlling technical policy, but for shaping it as well.

Further support for the same idea comes from the fact that one of the members of the Authority has any radio-technical qualifications or experience, and so must depend entirely on the engineering staff they may appoint or on outside advisers. And, of course,

there is still another body that comes into the picture: the P.M.G.'s decisions on technical policy for both the I.T.A. and B.B.C. will be affected by the recommendations of the Television Advisory Committee.

Fortunately, there is a good deal of flexibility in the Act, and plenty of room for second thoughts. The word "may" occurs much more often than "shall" and the P.M.G. can make new regulations at short notice. Throughout all the debates, the Government has wisely kept to the principle of leaving a loophole for subsequent changes.

It is wrong to shoot the pianist who is doing his best, and still worse to shoot him before he has played a single note. The I.T.A. needs the full support of everyone concerned with radio in implementing the complicated scheme laid down in the Act. Wireless World's only fear is that, with so many secondary problems to overcome, attention may be distracted from the primary task of planning the long-term technical development of television.

#### Radio Eavesdropping

A GOOD deal of publicity has been given in the daily Press to a recent case in a London magistrate's court, where two men were charged with contravening the section of the Wireless Telegraphy Act that forbids the interception and disclosure of messages. It was stated they had listened to police and fireservice v.h.f. transmissions and passed on information so gained to news agencies and fire assessors. The defendants, who pleaded guilty and said they had no idea they were acting unlawfully, were ordered to pay £8 8s and £2 2s costs, respectively.

Newspapers, in reporting the case, made play with the fact that this was the first prosecution of its kind. That may be true enough, but no new principle is involved. Lack of secrecy has always been a skeleton in the radio cupboard and for 50 years the Postmaster-General has rightly had the power (which he has used widely) to make regulations against unauthorized interception and disclosure of messages.

# The Television Act

#### Summary of the Main Provisions

WELL over two years ago, the Government first declared their intention of establishing a new television service, alternative to that conducted by the B.B.C. Two basic principles for the proposed scheme were affirmed by Government spokesmen; it was to be competitive and was to be financed by advertisments. Since then, many methods of attaining the desired end have been debated, only to be abandoned or modified later; even the basic principles have been watered down to some extent. Now, at last, a cut-and-dried plan has appeared in the final form of an Act of Parliament. In view of all the changes that have taken place and in spite of the vast number of words that have been written in the Press, readers may like to have a summary of those provisions of the Act most

likely to affect them.

The Television Act, 1954 (H.M.S.O., price 9d) makes "provision for television broacasting services additional to those provided by the British Broadcasting Corporation, and to set up a special authority for the purpose . . . to be called the Independent Television Authority." The I.T.A. is to provide, for the period of 10 years, television services "of high quality, both as to the transmission and as to the matter transmitted," and shall be composed of a chairman, deputy chairman and eight others. These under the chairmanship of Sir Kenneth Clark have now been appointed by the Postmaster-General. They comprise an assemblage of persons distinguished in the Arts, literature, industry and the world of affairs. It is stipulated that none of them shall have any interest in an advertising agency, in the selling of radio equipment or in programme contracts. The members are to be paid, and, in addition to membership, may perform other salaried work in the Authority.

The I.T.A. is to be a "body corporate" but not a body exercising functions on behalf of the Crown. It enjoys no special privileges under the Wireless Telegraphy Act, and will need the Postmaster General's licence for its stations. The aim is that the Authority shall be financially self-supporting as soon as possible, but it may be granted by the P.M.G. up to £750,000 a year. Initial capital expenditure is to be met by a

grant of up to £2M, spread over five years.

First and foremost, the function of the I.T.A. is to build and operate television broadcasting stations. It must also arrange for studios to be provided, or if need be, itself provide them. By arrangement with the P.M.G., the I.T.A. may also arrange for wired distribution of programmes through relay companies.

Provision of programmes is primarily a matter for "programme contractors," but the Authority itself may when necessary transmit its own material, in which paid advertisements may be inserted. programme contractors will, in effect, "buy time" from the I.T.A., recouping themselves by charging fees for advertisements which will be transmitted during the intervals between items or at natural breaks in the programmes. There is to be no "sponsoring"; advertisements must not be directly associated with the programmes.

The matter of the programme contracting companies is still somewhat obscure. From our point of view, virtually all we know from the Act is that it will be the duty of the I.T.A. to secure "adequate competition" between a number of them to supply programmes. It is not known how the time of the various I.T.A. stations is to be divided between the various contractors.

Wide powers of control over the contractors are conferred by the Act on the I.T.A., who may impose heavy penalties for breach of contract. They are bound by the Act to observe certain rules as to the

pay and conditions of their staff.

The Authority, in its turn, is subject to pretty drastic Government control of their day-to-day activities. The P.M.G. or any other Minister of the Crown may require them to broadcast any announcement, while the P.M.G. may at any time impose a ban on the broadcasting of "any matter or classes of matter." He also has the power to determine the hours of broadcasting, both as to maximum and minimum hours per day and as to the actual times of the transmissions.

On the technical side the Authority is subject to equally rigorous control under the powers conferred on the P.M.G. by the Act. They may be required to use "such technical measures or processes as may be specified" or to set up additional stations thought to

be necessary to extend coverage.

There are a number of secondary provisions, including permission for the I.T.A. to do various things arising out of its main function and to embark on ancillary business enterprises that may be found necessary. The I.T.A. must not, however, manufacture or sell radio equipment.

The rest of the Act-in fact, the greater part of itis concerned with detailed control of broadcast matter. An obligation is put on the Authority to see that programmes do not offend good taste or decency, do not incite to crime or lead to disorder or offend public feeling. They also have the responsibility of ensuring balanced programmes, of presenting news accurately and impartially and of showing no political bias.

#### Resistor and Capacitor Preferred Values

A British Standard for the preferred values and tolerances of resistors and capacitors used in telecommunications equipment is now obtainable from the British Standards Institution, 2, Park Street, London, W.1 (price 2s.)

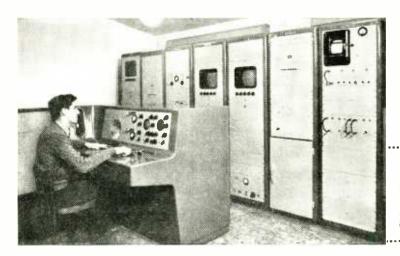
The standard specifies a series of rounded values based on the 12th root of 10 system and with tolerances of 5, 10 and 20%. The 10% series is compiled by omitting alternate terms in the 5% series; likewise the 20% omits alternate terms in the 10% series.

While the 20% series is well known the other two are possibly not common knowledge and we give below the series. Values are in ohms for resistors and in pico-

farads for capacitors.

Five per cent values: 1.0, 1.1, 1.2, 1.3, 1.5, 1.6, 1.8, 2.0, 2.2, 2.4, 2.7, 3.0, 3.3, 3.6, 3.9, 4.3, 4.7, 5.1, 5.6, 6.2, 6.8, 7.5, 8.2 and 9.1. The other two series start with 1.0 and are thus easily compiled from this list.

# WORLD OF WIRELESS



Fleming Valve Jubilee

fonosphere Meeting

tus. Television

TELEVISION RELAY.—The operator-controlled diversity receiving station in Jersey where, as described last month, a wired service is distributed over the island by Rediffusion. The monitor tubes show London and Wenvoe Pictures.

#### Jubilee of the Valve

IT WILL be fifty years on November 16th since Sir Ambrose Fleming took out the fundamental thermionic valve patent, No. 24850—"Improvements in Instruments for Detecting and Measuring Alternating Electric Currents." To mark the jubilee the I.E.E. has arranged an exhibition of historical apparatus and three lectures on the development of the valve will be given by Sir Edward Appleton, Professor G. W. O. Howe and Dr. J. Thomson.

The lectures will be given on the actual anniversary and the proceedings will be opened by the Lord President of the Council, the Marquess of Salisbury.

#### Ionospherists Meet

AS already announced a conference on "The Physics of the Ionosphere" is being organized by J. A. Ratcliffe, F.R.S., reader in physics at Cambridge University, in collaboration with the Physical Society. It will be held at the Cavendish Laboratory from September 6th to 9th, and will be devoted mainly to discussions of the following topics: (a) the lowest ionosphere; (b) irregularities and movements in the ionosphere; (c) the F2 layer; (d) the mathematics of wave propagation through the ionosphere.

As the conference follows the meeting of the International Scientific Radio Union at Amsterdam many foreign delegates will be among the 200 or more

participating.

Abstracts of the sixty papers presented and the surveys summarizing the present position in each of the subjects discussed will be published later by the Physical Society.

#### U.S. Colour Television

THE cost, and more especially, the size of the threecolour tube have been cited as the main reasons for the slow "get-away" of colour television in the United States. So far colour tubes have had only comparatively small screens and have, therefore, been unacceptable to viewers who have become accustomed to 21-in and even larger monochrome screens. Answers to both criticisms have been given by C.B.S.-Hytron who have produced a 19-in tri-colour tube at \$175. The principle employed for the production of these tubes, which, it is stated, will be at the rate of 400 a day by the end of September, was briefly described in our January issue.

#### Radio Research

A START was recently made on the new building to be erected for the Radio Research Station of the

D.S.I.R. at Ditton Park, Slough, Bucks.

Naturally everything is being done to reduce interference to a minimum. The building is over 200 yards from the nearest road, the adjoining 100 acres has been acquired to ensure isolation and as a further precaution to minimize disturbance with experimental work, the waste outlet from the building will be conveyed in a non-metallic pipe to the main district sewer.

The building has been designed specifically to meet the requirements of the Radio Research Station, of which Dr. R. L. Smith-Rose is the director with a staff of just over 100 who are at present in temporary

accommodation.

#### Increased Exports

THE radio industry's exports during the first six months of the year increased by £2.25M compared with the same period in 1953. Of this figure £1.7M was accounted for by increased exports of communication and navigational equipment which totalled £5,974,841—approximately 46 per cent of the whole industry's exports. Increased exports are also recorded for components (£893,000), p.a. equipment and loudspeakers (£58,000) and sound reproducing gear (£38,000).

The six-months' total was £12,996,603.

#### Industrial Television

INCREASING use is being made by leading U.S. industrialists of closed-circuit television for nation-wide sales conventions. Instead of salesmen and distributors from all over the country travelling at considerable expense to a central meeting they merely

go to the studios of local television stations, which are linked with a central station where the company's executives are gathered to present their wares.

According to a report in the *Financial Times* on the activities of Box Office Television, Inc., which specializes in such "telecast conventions," Westinghouse Electric recently saved \$375,000 by introducing its new receivers and appliances to 2,000 distributors through a television convention.

#### Valve Data

ELECTRICAL characteristics and base connections of over 2,000 British and American valves and British transistors and some 200 cathode-ray tubes are given in the latest edition of "Radio Valve Data."\* The valves are classified under main headings according to their type—frequency changers, screened tetrodes, pentodes, etc. In each of these sections, they are listed under makers' names and are further classified as current, replacement or obsolete types.

Seventeen British valve manufacturers co-operated with Wireless World in ensuring that the information is accurate and up to date

is accurate and up to date.

Additional features included in this edition are a list of equivalents, which is combined with an index, and special quality valves.

\* "Radio Valve Data." fourth edition, 100 pages (11in×81in), published for Wireless World by Iliffe & Sons Ltd., price 3s 6d.

#### PERSONALITIES

Sir Ben Lockspeiser, F.R.S., secretary of the Department of Scientific and Industrial Research since 1949, is to receive the honorary degree of Doctor of Science at Oxford University. The presentation will precede the opening of the 116th annual meeting of the British Association for the Advancement of Science on September 1st.

- E. P. B. Metcalfe, appointed engineer-in-charge of the Isle of Wight television station, which is coming into service in November, has been engineer-in-charge of the temporary Brighton station since May last year. He joined the B.B.C. in 1936 and was a maintenance engineer at various sound stations before becoming senior maintenance engineer at the Wenvoe television station in 1952.
- E. J. Power, head of Murphy Radio, has been invited to become a member of the Council of the Royal College of Art. This may be taken as a tribute to the part played by his firm in industrial art; it was in the early thirties that Murphy first produced a receiver cabinet that set a new standard in functional external design.
- J. P. Salter, the contributor of the article in this issue on the measurement of small voltage differences, is a senior engineer in the Armament Design Establishment of the Ministry of Supply. He served throughout the war in the Royal Artillery as an instructor in fire control (anti-aircraft radar). Before joining the Ministry of Supply for work on fuzes, on which he was engaged for six years, he was for a short time at R.R.D.E., Malvern.
- C. E. Knight Clarke, who had been publicity manager for Decca Radar for two years, is now running his own business producing technical literature. Before joining Decca's he was with the G.E.C. publicity organization, where he handled the production of radio and valve technical literature. His address is 36, Denbigh Street, London, S.W.1. (Tel.: Victoria 5394.)

#### IN BRIEF

The increase in licensed viewers in the U.K. during the first six months of the year was 454,200. The June increase was 31,680, bringing the total to 3,411,046. The total number of Broadcast Receiving Licences at the end of June (including the above and 236,057 for car sets) was 13,512,275.

November 12th has been given by the B.B.C. as the date for the opening of the Isle of Wight Television Station. When this permanent station at Rowridge comes into service the temporary booster transmitter on Truleigh Hill, near Brighton, which has been in operation since May, 1953, will be closed down. The new station will operate in Channel 3 (56.75 and 53.25 Mc/s) and use vertical polarization as the Brighton booster has done.

The ninth Electronics Course covering the design, use and maintenance of electronic instruments used in nuclear physics, radio chemistry and in work with radio isotopes, will be held at the Isotope School, at Harwell, from November 1st to 5th. Physicists and electronic engineers, holding a degree or equivalent qualification, can obtain application forms from the Electronics Division, A.E.R.E., Harwell, Didcot, Berks. Attendance is limited and the fee is 12 guineas, excluding accommodation.

The operating frequency of the Lugo, Spain, Consol Station has been changed from 303 kc/s to 285 kc/s. The Seville station recently changed from 311 to 315 kc/s.

I.E.E. Students.—The new chairman and vice-chairman of the London Students' Section of the I.E.E. are M. C. Cubitt (Pye, Ltd.) and M. H. F. Collins (B.T-H.), respectively.

I.P.R.E.—At the inaugural meeting of the Yorkshire section of Incorporated Practical Radio Engineers (previously the Institute of Practical Radio Engineers), over 150 servicemen and traders were present. The local secretary is P. A. Senior, 5, Calverley Moor Avenue, Thornbury, Bradford, 3.

A miniature TV camera, manufactured by Pye, Ltd., was used recently at the Hospital for Sick Children, Great Ormond Street, London, to enable 100 surgeons to watch a series of operations. The surgeons were attending the inaugural meeting of the British Association of Pedriatic Surgeons.

A new Third Programme Transmitter is to be built by the B.B.C. at Swansea, Glamorgan. Rated at 1 kW, it will operate on 1546 kc/s (194 metres).

Tape Letters.—A miniature spool of 120ft of tape, weighing less than 1½ oz and, therefore, particularly suitable for recording messages for posting, has been produced by Grundig. The "Mailspool," which permits six minutes recording on each track at 3¼ in/sec, costs 6s 9d (export price 4s).

Hungarian TV.—Preparatory to planning the country's television service experimental transmissions are being radiated in Budapest. Some 200 foreign-made television receivers are said to be in use in the city for this investigation.

Indian Manufacturers.—A new class of membership—associate members—has been introduced by the Radio Manufacturers' Association of India to provide for smaller manufacturers. The member-firms constituting the R.M.A.I. committee are:—General Electric Company of India; Gramophone Company; International General Electric Company (India); Murphy Radio of India; National Ekco Radio & Engineering Company; Philips Electrical Company (India) and Radio & Electrical Manufacturing Company.

Glass being one of the many raw materials used in radio and electronics, we make no apology for drawing readers' attention to the information centre provided by the Glass Manufacturers' Federation at its new head-quarters at 19, Portland Place, London, W.1.

Electronic Cooking.—The first electronic bakery in France is being set up by the French Ministry of Agriculture in Paris. It is planned to produce up to 30 tons of bread a day. Radio-frequency cooking has been used on a small scale in the United States for the commercial preparation of foodstuffs, but, according to our contemporary, Electronics, domestic r.f. cookers are being "home tested," and mass production at \$1,000 each is planned for 1955.

ECHO OF THE ECLIPSE. Radio astronomers as well as optical astronomers were in Norway to observe the eclipse of the sun this year. The equatorially-mounted aerials shown here were set up on a peninsular near Sandefjord by an expedition from the M.o.S. Radar Research Establishment led by C. R. Ditchfield (right). Measurements of solar noise were made on a wavelength of 8 mm, the reflectors being arranged to follow the course of the sun.

"W.E." Editorials—The index to Dr. Howe's editorials in Wireless Engineer during the past twenty-eight years, to which we referred last month, has been prepared personally by Dr. A. J. Small, of the Department of Electrical Engineering, The University, Glasgow, W.2. We omitted to state that the index, which is obtainable direct from Dr. Small, costs 5s.

No fewer than 2,500 British Standards, current at March 31st, are listed and briefly described in the 1954 edition of the "British Standards Yearbook." It also gives particulars of work in hand by the various Industry Standards Committees. The Yearbook is obtainable from the British Standards Institution, 2, Park Street, London, W.1, price 12s 6d.

Readers concerned with the Transport of Goods may like to know of the publication of the new "ABC Goods Transport Guide," published by Motor Transport. It includes a directory of operators of regular, long-distance road transport services and of specialist carriers. It costs 3s 6d (inc. postage).

Nottingham Central Library has issued a catalogue of some 200 books and periodicals on radio, television and radar which are available through its various branches. Journals are kept for three months, except in the case of Wireless Engineer, which is available from 1936, and Wireless World for the past six years.

#### EDUCATIONAL OPPORTUNITIES

The course of ten lectures on "Crystal Valves and Transistors" at the Borough Polytechnic, London, S.E.1, which proved so popular last year that it was run in triplicate with a total attendance of some 300, is being given in duplicate this year. The lectures, by members of the Mullard research and development staff, will be given on Tuesdays at 3.0 and 7.0 beginning on October 19th. The fee is 2 guineas. For the fourth successive year the Borough Polytechnic is also arranging a course of lectures on "The Fundamental Principles of Pulse Techniques."

A thirteen-week intensive Course in Electronics, designed to give those unable to take a long course an insight into the underlying principles and some of the applications of electronics, is provided by the Norwood Technical College, London, S.E.27. The college also provides a three-year full-time course in telecommunication engineering, one-year courses for the 1st and 2nd Class P.M.G. Certificates, and part-time day and evening courses in radar principles and techniques, radio and television servicing, television theory and for the Brit.I.R.E. Graduate examination.

The prospectus of Evening Courses arranged by the Electrical Engineering Department of The Polytechnic, Regent Street, London, W.1, includes approved telecommunications courses for the award of the Ordinary and Higher National Certificates and courses in radio and television servicing in preparation for the examination of the Radio Trades Examination Board.



Day and Evening Classes covering communication engineering (National Certificate courses), City and Guilds telecommunication engineering, and radio and television servicing, are listed in the prospectus of the Department of Electrical Engineering and Applied Physics of the South East London Technical College, Lewisham Way, S.E.4.

Amateur Classes.—We have been notified of a number of establishments providing classes during the coming session in preparation for the Radio Amateurs Examination. Among them are the Wembley Evening Institute, Copland School, Wembley Hill, Middx. (Mondays); Ilford Literary Institute, Cranbrook Road, Ilford, Essex (Wednesdays); South East London Technical College, Lewisham Way, S.E.4 (Tuesdays); and the Grafton School, Eburne Road, Holloway, London, N.7 (Mondays). Courses commence on or after September 20th.

The recently formed Electrical Section of the Wilmslow Guild (Adult Education Centre), 1, Bourne Street, Wilmslow, Cheshire, is planning a series of classes of instruction in electronics. They will be held at 8.0 on Tuesdays beginning September 28th.

#### RADIO EXPORTS

Among the eight members of the new Export Panel formed by the British Standards Institution to advise on standards in relation to exports and how best B.S.I can assist export trade are J. W. Ridgeway, of Edison Swan, and Leslie Gamage, of the G.E.C.

Navigational radar equipment, radio transmitters, receivers and associated test equipment are to be supplied by Marconi's for five warships of the Egyptian Navy.

Radio-telephone equipment, including a 15-W fixed station, three smaller fixed stations and five mobile transmitter-receivers, has been supplied by Pye, Ltd., to the Lisbon Tramway Company.

Radio equipment, including receivers, transmitters, teleprinters, terminal equipment and aerials, is listed among the products to be secured by the Burma Purchasing Mission to visit this country.

U.S. Enquiry.—Details of British-made industrial electronic equipment, inter-communication systems and p.a. gear are being sought by Warmington, Woodcock and Williams, Inc., 423, South 11th Street, Minneapolis, Minesota, U.S.A. Interested manufacturers should send literature and c.i.f. prices in U.S. dollars by airmail.

Colombian Agency.—Casa Dyrma Ltda, Edificio Banco de Bogota, Oficina 632, Bogota, Colombia, have informed the British Embassy at Bogota that they are interested in

acting as agents for U.K. manufacturers of electronic equipment. A long list of equipment, components and accessories is given in the announcement of this enquiry by the Export Services Branch of the Board of Trade (Ref. ESB/15127/54).

King's Dock, Singapore, has recently been equipped with a public address system by the G.E.C. It comprises six horn loudspeakers mounted on the lighting pylons, which are fed by two 30-W amplifiers and have a range of a quarter of a mile. Microphone points are provided at intervals around the dock.

Ekco Electronics, Ltd., have secured an order from the Carborundum Company, of Niagara Falls, New York, for a thickness gauge installation for measuring Carborundum coated abrasive products during various stages of manufacture.

Decca Radar is to be fitted in ships of the South African Navy, which, it is understood, is the twenty-sixth navy to use Decca equipment.

#### ANDUSTRIAL NEWS

Radio manufacturers participating in the British Trade Fair to be held in Baghdad from October 25th to November 8th include Pye (who are planning to demonstrate closed-circuit television), B.T-H., G.E.C. and S.T.C. The fair is being organized by British Overseas Fairs, Ltd., 21, Tothill Street, London, S.W.l, on behalf of the Federation of British Industries.

The new 20,000-ton Shaw Savill liner Southern Cross, the first passenger ship without any cargo space, is being equipped with Marconi Marine transmitters, receivers, sound reproducing equipment, radar, direction finders and echometer equipment.

Coaxial telephone cables and television camera cables and accessories will be shown by B.I. Callender's Cables at the International Trade Fair at Leipzig (September 5th to 15th).

Marconi Marine radio-communication equipment is to be fitted in the new 3,300-ton cable ship *Recorder* which is being built for Cable & Wireless.

What is believed to be the first installation of v.h.f. radio-telephone gear in British fishing craft has been completed by Rees Mace Marine in two vessels of the Claydeep Fishing Company, of Grimsby.

Standard Telephones & Cables, Ltd., have erected a new factory at Southampton New Docks for the production of submarine telephone cable and repeaters.

Leevers-Rich Equipment, Ltd., has moved from Wardour Street, London, W.1, to 78, Hampstead Road, London, N.W.1 (Tel.: Euston 1481). The studios of the associated company, Leevers Rich & Company, Ltd., professional recordists, are remaining at 80, Wardour Street, where Western Electric recording equipment has recently been installed to provide a sound-on-film transcription service.

Ferguson Service.—The Birmingham service depot of Thorn Electrical Industries, Ltd., has moved to 24, Sheepcote Street, Birmingham, 15 (Tel.: Birmingham, Midland 5291).

Pam (Radio & Television), Ltd., manufacturers of domestic sound and television receivers and sound reproducing equipment, have moved from North London to 295, Regent Street, London, W.1 (Tel.: Langham 7246).

Elesco Electronics, Ltd., has been formed to sell the electronic and electrical equipment handled by Land, Speight & Company, of 73, Robertson Street, Glasgow, C.2.

Anglo-Swiss Screw Company has opened a sales office at 12, St. Ann's Square, Manchester. 2 (Tel.: Deansgate 7552).

#### COMMERCIAL LITERATURE

Core Laminations made by Magnetic and Electrical Alloys are now available from H. W. Forrest, 349, Haslucks Green Road, Shirley, Birmingham, who are sole distributors in England. The latest catalogue of chokes and transformers from this firm includes isolating transformers for the heaters of c.r. tubes with heater-cathode shorts.

Transformers and Chokes as specified for the Osram 912 amplifier (see p. 430) are described in a leaflet from Partridge Transformers, Tolworth, Surrey.

"Proc. L.L.L.", described as a "journal of random frequency," gives frank opinions on electronic instruments and test gear of various makes for which Livingstone Laboratories are agents. Qualities of "handleability" are assessed. No. 1, Vol. 1, from Livingstone Laboratories, Retear Street, London, N.19.

Powder Cores and Magnets; their production and use described in a booklet "Gecalloy Low Loss Cores and Micropowder Magnets" which also gives technical specifications, performance graphs and suitable core designs for various applications. From Salford Electrical Instruments, Peel Works, Silk Street, Salford, 3, Lancs.

#### CLUB NEWS

Birmingham.—At the meeting of the Slade Radio Society on September 3rd, A. B. Cape, M.B.E., will speak on "The Balancing of Rotors." The subject for the meeting on September 17th is "The Possibilities of Inter-Planetary Travel," introduced by W. E. Merrill. Meetings are held on alternate Fridays at 7.45 at the Church House, High Street, Erdington. Sec.: C. N. Smart, 110, Woolmore Road, Erdington, Birmingham, 23.

QRP Exhibition.—Plans are being made by the QRP Society to hold an exhibition at Walton-on-Thames on October 30th. In addition to displays of amateur-constructed gear—including television—there will be exhibits of components and commercial sound and vision receivers. Provisions are being made for the demonstration of high-fidelity equipment and radio-controlled models. The exhibition will be held in St. Mary's Parish Church Hall, admission 1s. Sec.: J. Whitehead, 92, Rydens Avenue, Walton-on-Thames, Surrey.

South Shields.—The opening meeting of the winter programme of lectures and demonstrations for members of the South Shields and District Amateur Radio Club (G3DDI) will be held at 8 on September 10th in the Trinity House Social Centre, 134, Laygate Lane, South Shields. The club is installing transmitting equipment at the South Shields annual flower show (August 26th to 29th) which will be in operation in the 20-, 40- and 80-metre bands, using the specially allocated call-sign GB3SFS. Sec.: W. Dennell (G3ATA), 12, South Frederick Street, South Shields, Co. Durham.

#### MEETINGS

#### British Institution of Radio Engineers

London Section.—"Computing Circuits in Flight Simulators," by Dr. A. E. Cutler, B.Sc. (Redifon), at 6.30 on September 29th at the London School of Hygiene and Tropical Medicine, Keppel Street, Gower Street, London, W.C.1.

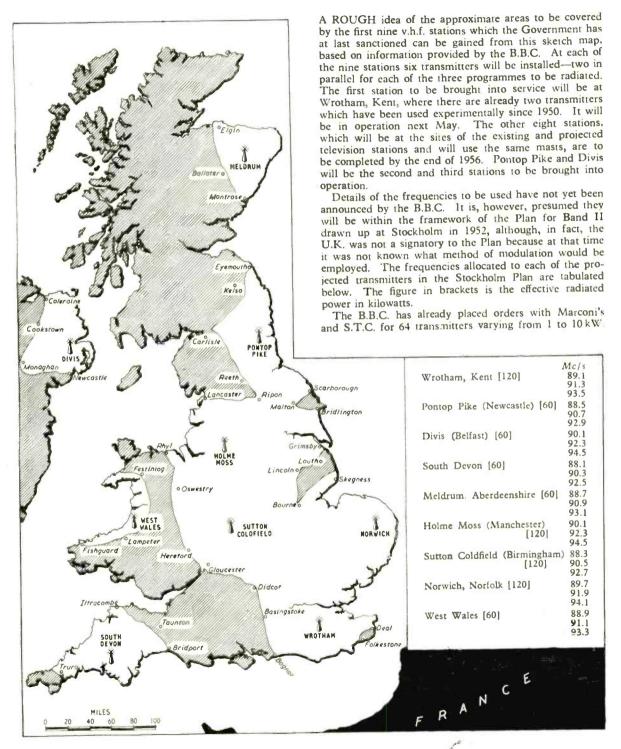
#### British Sound Recording Association

London.—Presidential address by N. Leevers, B.Sc., at 7.0 on September 24th at the Royal Society of Arts, John Adam Street, London, W.C.2.

Manchester Centre.—"New Reproducing Equipment," by J. S. Holiday, at 7.30 on September 13th at the Engineers' Club, Albert Square, Manchester.

# V.H.F. Broadcasting : B.B.C. Plans

#### COVERAGE OF FIRST NINE F.M. STATIONS



# 21st National Radio Show

#### STAND-TO-STAND PREVIEW OF TECHNICAL EXHIBITS

HE annual exhibition of British domestic radio equipment opens at Earls Court on August 25th. The preview of technical exhibits presented in the following pages differs from that given in the past few years in that it is a stand-to-stand report instead of a tabulated list of products. Prepared from information given to us by exhibitors, it will inevitably be incomplete in that there are bound to be a few manufacturers who will await the actual opening of the show to uncover their latest productions. Despite this, we feel that the following pages will provide a useful guide to visitors and a comprehensive survey for readers unable to attend the show.

The Radio Industry Council, which organizes the show, has again arranged for collective displays of electronic equipment. There are four such displays—two on the ground floor (marked E1 and E2 on the plan opposite) and two on the first floor (E3 and E4).

The exhibits will not, this year, be grouped together

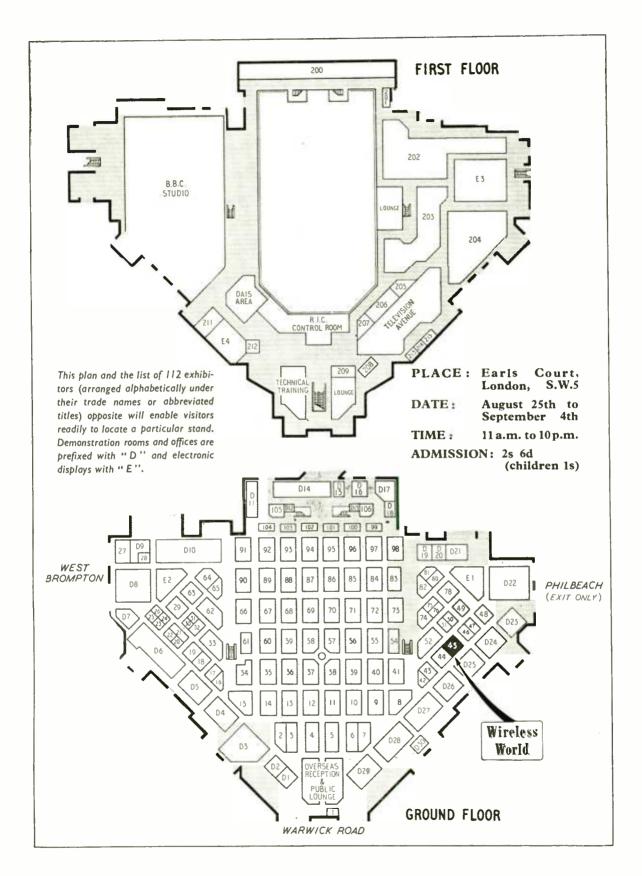
under "applications" except in the case of radio control gear. In all some twenty-five examples of applied electronics will be shown and demonstrated.

The industry, the Radio Trades Examination Board and some training establishments have co-operated in providing this year's Technical Training Display, located near the B.B.C. Studio, which, as usual, occupies a large part of the first floor. The focal point of the display is a 15-minute film on training in industry. To reach the cinema, which will hold about 50, one passes displays illustrating machine shop practice, glass manipulation, component manufacture, circuit testing, servicing and aerial techniques.

This year's television distribution system at the exhibition provides, in addition to a signal on Channel 4 (used to avoid interference from Alexandra Palace), a Band III signal superimposed on the same cable network. This signal will be a simple picture for demonstration purposes only.

#### ALPHABETICAL LIST OF EXHIBITORS AND GUIDE TO THE STANDS

Name				5	Stand	Name				S	tand	Name					Stand
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Alba					35	Gibbs		٠.		• •	20						93
Ambassado					41	Goodmans	• •	• •	• •	• •		R.S.G.B.					209
Antiference					34	Goodmans			• •		63	R.T.R.A.					206
Argosy					8							Reflectogra					
Army					202	H.M.V.				10 (	D22)	Regentone					38
Associated '	Techn	ical N	Aftrs.		25	Hobday					78	Roberts					102
Avo					61	Hunt					90	Rola Celesi	ion				3
								• •	• •	• •	,,						_
B.B.C.					200	Invicta					95						
Baird					88	MINICIA	• •	• •	• •	• •	90	S.T.C.					82
Belling-Lee					67	I D . O						Simon		٠.			104
Bernards					24	J.B. Cabine					18	Sky-Masts					30
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Brimar					6							Sobell					12
British Radi	o and	Telev	ision		215	K.B.					70	Star, The					211
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Cossor	• •		• •	57 (	(D11)	McMichael					72	Thompson,	Diam	ond &	& Butcl	her	15
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Decca					(D28)	Masteradio					62	Ггіх					65
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											(D9)	Wireless &				105 (	17
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#### 21st NATIONAL RADIO SHOW

### Guide to the Stands

ACOS (44)

Components employing piezoelectric crystals have always been one of the principal products of this firm. This year the "Hi-g" pickup movement, designed to track the highest record groove accelerations which are, or can be, engraved on a record, will be seen in a wide variety of types, including plug-in heads for most well-known proprietary gramophone units.

A recent addition to the range of crystal microphones is the Type MIC36 which is adaptable to a

variety of applications.
Cosmocord Ltd., 700 Great Cambridge Road, Enfield, Middlesex.

AERIALITE (64)

Aerials for sound and television broadcasting and cars, with a wide range of aerial accessories and cables of various kinds, will be found on this stand. There will be two new "Aerfringe" type television aerials, one a 3-element 7.5-db gain model and the other a 4-element 11-db model. Some specimens of Band III acrials will also be available, together with other v.h.f. types.

A new "Mastatic" aerial fitted with an 18-ft whip is of the anti-interference type. Another new item is a partially air-spaced 72-ohm.

item is a partially air-spaced 72-ohm coaxial cable of extra low-loss qualities to meet fringe area and Band III requirements.

Aerialite Ltd., Castle Works, Stalybridge.

ALBA (35)

Two completely new television receivers, T321 (14in) and T324 (17in) have been added to the Alba range. These are designed for Band I and Band III and employ special valves in a 19-valve circuit using turret tuning. The specification includes a.g.c. and interference sup-pression on both sound and vision, frame flyback suppression, built-in aerial attenuation and a forwardfacing loudspeaker.

In addition to the C114 miniature all-wave superhet and the 707 mains/battery portable radio-gramophone, the sound receiver range will include a new moderately priced 5-valve a.c./d.c. table model (3122) with built-in aerial.

A. J. Balcombe Ltd., 52-58 Tabernacle Street, London, E.C.2.

AMBASSADOR (41)

In all there will be five television models in the Ambassador programme, making use of completely redesigned chassis with turret tuners for Bands I and III stations. Sets will go out with Band I coils, and others will be supplied as additional programmes become available. The TV15CR is a combined television and sound receiver.

Four sound receivers will be shown, and two radio-gramophones, including the Viscount (Series III) with 8-waveband receiver, 3-speed record changer and storage for 200

records. R. N. Fitton Ltd., Princess Works, Brighouse, Yorks.

**ANTIFERENCE (34)** 

The range of television aerials made by this firm offers a wide variety of types for home and over-seas requirements. Considerable emphasis is placed on the "Snapacitor" feature which permits virtual assembly at the factory and also does away with actual metal-to-metal contacts in the electrical circuitry of the aerial.

Of particular interest to overseas visitors will be the wide range of television and v.h.f. aerials for the particular frequencies and polarizations used in other countries. The pre-assembly feature is also embodied in these models. Antiference Ltd., 67 Bryanston Street,

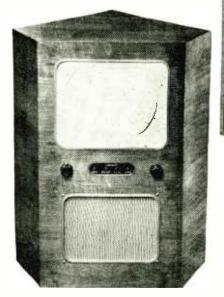
London, W.I.

ARGOSY (8)
Three-speed automatic changers are used in all the latest radio-gramophones to be shown by this firm, while the receiver sections

cover long, medium and short waves. In each model the 10in loudspeaker is fed from a pentode capable of giving 4 watts output at less than 5% distortion. Two superhet receivers will also be shown, the five-valve TR525 and the six-valve TR626/U.

Argosy Radiovision Ltd., Argosy Works, Hertford Road, Barking,

Essex.



Baird P2114 two-band receiver with 14-in tube.

Left: Ambassador corner console, TVI5CC.

Right: Argosy 5-valve super-



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ARMY (202)

The space devoted to the Regular Army's exhibit is shared by the Royal Corps of Signals—the operators of its telecommunications system —and the Royal Electrical and Mechanical Engineers, responsible for the maintenance of the equip-

An Air Support Signal Unit armoured vehicle, equipped with sets Nos. 52 and 62 and a v.h.f. transmitter-receiver, which provides direct communication between forward troops requiring air support and H.Q., will be on view. The supporting aircraft are "talked" on to the target through the v.h.f. set.

Some of the aids used in training telecommunication and radar mechanics and control equipment electricians will be displayed. War Office. Whitehall, London, S.W.I.

#### ASSOCIATED TECHNICAL MANUFACTURERS (25)

Manufacturers of cables, wires and sleevings for radio and industrial purposes. Special grades of heatresisting sleevings will be shown in addition to standard p.v.c. and polythene coverings.

Associated Technical Manufacturers Ltd., Vincent Works, New Islington, Manchester

AVO (61)

While basically the existing range of Avometers and test equipment will remain largely unchanged, usefulness is being extended by the introduction of some new multipliers to cover the higher voltages now encountered in television equipment. Expected to be shown will be one extending the range of the Model 8 Avometer and other 20-k\O/V instruments to read up to 25 kV.

In addition to test equipment coil winding machines of various kinds will be available for inspection. Automatic Coil Winder and Electrical Equipment Co. Ltd., Winder House, Douglas Street, London, S.W.I.

#### B.B.C. (200)

Working models illustrating operational processes and pieces of equipment in operation are again a feature of this stand. Among the "how it works" exhibits are a model television camera illustrating the operation of the "zoom" lens, equipment for measuring the characteristics of telephone lines, a representation of the reflection of radio waves by the ionosphere and sound recording equipment.

Developments in technical facilities for the production of studio and outside broadcast sound programmes will be illustrated by several new pieces of equipment and visitors will see some of the methods used in producing sound effects for programmes. British Broadcasting Corporation, Broadcasting House, London, W.I.



Avo 25-kV multiplier for extending the range of certain Avometers.



Alba Model 3122 a.c./d.c. receiver.



Acos Type GP20 "Hi-g" crysta! pickup.



Bulgin "Domina" 2-pole plug and socket.

#### BAIRD (88)

Some television receivers shown will have a turret tuner for Bands I and III. This tuner is normally fitted with coils for three Band-I channels and two Band-III channels, but up to seven further channels can be covered by extra coils. A 14-in table model and three 17-in models will be available. Single-channel sets will also be on view.

All sets can be supplied as fringearea models, with flywheel sync and a form of vision a.g.c. Hartley Baird Ltd., 37-39 Thurloe Street, South Kensington, London, S.W.7

BELLING-LEE (67)

Aerial equipment of all kinds, radio interference suppressors and a wide range of important items such as terminals, plugs and sockets and fuses, are the main exhibits to be found on this stand.



Belling-Lee double "Junior Multirod " for fringe areas.

Television aerials will include, on the one hand, simple designs for indoor use and on the other quite elaborate multi-element systems for extreme fringe-area conditions. An amplifier installed at the masthead and requiring no special cabling is another fringe-area aid to better reception. Distribution amplifiers will also be included.

There will be a new and almost television interference miniature suppressor for fitting in the mains leads of small domestic appliances; it will carry up to 2 A and is described as the "Telefilter." Belling & Lee Ltd., Great Cambridge

Road, Enfield, Middlesex.

#### BRIMAR (6)

Among cathode ray tubes on show will be a new 21-in tube, type C21HM, which has an improved tetrode gun assembly giving better focusing and minimum astigmatism. A 17-in self-focusing tube, type C17JM, will also be displayed. This incorporates an internal focusing electrode and so avoids the need for external focusing magnets and controis.

The range of valves will meet the requirements of both high-quality and economical a.m./f.m. receivers, and various circuits for these will be displayed. There will also be special quality valves at lower prices than hitherto and valves for Band III tunable television receivers.

Standard Telephones and Cables Ltd., Footscray, Sidcup, Kent.

#### BULGIN (99)

Connectors, signal lamps, knobs, switches and a host of other small, but quite vital, items in electronic and radio equipment comprise the main activities of this company. Among the newest items are a Lilliput lampholder no larger than a littlefinger nail; miniature micro-switches which operate by almost a featherweight touch and some new multipole connectors. One pattern is in the form of a strip with the plugs, or sockets, in line and self-centring;



Bush 14-in table model TV.43 with flyback suppression.



Champion "Midget" receiver, Model 825.



Collaro "54" 3-speed record changer.

Dubilier "Hi-K" ceramic feedthrough and midget moulded silvered mica Type SM22 capacitors.

another new design takes the form of a 2-pole unit (plug or socket) which can be mounted in line or stacked vertically to give almost any number of connections. They are mainly intended for inter-chassis or interunit connection, one part being on the chassis the other on the rack or cabinet, when the chassis is pushed home all the contacts, which are selfaligning, engage. A. F. Bulgin & Co. Ltd., Bye-pass Road

Barking, Essex.

BUSH (86, 89)

Television receivers shown by this firm all include tuners for Bands I and III, tuning on each band being continuous with a band selector switch. All models, too, have a.g.c. on sound and a form of a.g.c. on vision, the control voltage in this case being derived from the syncseparator grid current. One model, the TV33, has flywheel synchronizing. All the sets are of the a.c./d.c. type.

Table models with 12-in, 14-in and 17-in tubes will be shown, a console with a 17-in tube and the Mobile 17, which is a floor model

with a 17-in tube.

Sound-broadcast receivers will include the well-known DAC90A and a battery set introduced last year. A new set is the AC41 and an a.c./d.c. counterpart-the DAC41.

A radio-gramophone with a threespeed motor and auto-changer will be shown. An exhibit of particular interest at the present time will be a v.h.f. broadcast receiver. Bush Radio Ltd., Power Road, London, W.4.

**CHALD** (26)

Shown by this firm will be a new indoor television aerial in the form of a single-turn square "loop" known as the "Sqarial." It is said to give a 20-% gain over a dipole, has a back-to-front ratio of 7 db and may be expected to give satisfactory reception up to 30 to 35 miles. It is less than 3ft square. Chald Products Ltd., 184 Low Road, Leeds, 10.

CHANNEL (214)

Television pattern generators will be shown, one model, 'I'l, for Band I and another, T2, for Bands I and III. Also on view will be television pre-amplifiers, multi-outlet distribution amplifiers, and t.v.i. suppression

Channel Electronic Products, Ltd.. Burnham-on-Sea, Somerset.

CHAMPION (33)

This year Champion are concentrating on sound receivers, and in particular small portable and "midget" table models.

Model 825, a "midget" table receiver for a.c./d.c. mains, is new and will be available in a plastic cabinet with a choice of colour. Ferrite rod aerials are used in the Model 822 battery suitcase portable

and in the Model 820 "Radio Revler" transportable 3-speed radio-gramophone. The larger Model 781, which is a 7-valve superhet mains-battery portable of high sensitivity, is being continued. Record playing equipment includes the portable 'Revler" with crystal pickup, amplifier and 5-in loudspeaker. Champion Electric Corporation Ltd., Drove Road, Newhaven, Sussex.

COLLARO (II)

A new record changer, Model 54, which mixes 7, 10 and 12-in records and has a constant change time, irrespective of the turntable speed, will be shown; also a new inexpensive 3-speed motor unit with turnover pickup

cartridge (AC3/554).

"Transcription" units (Models 2,000 and 2010) fitted with the Collaro "Studio P" crystal pickup will be of special interest to high-quality enthusiasts. Collaro Ltd., Ripple Works, Bye-pass

Road, Barking, Essex.

COSSOR (57)

In sound broadcast receivers the most interesting exhibits on the stand will be two models capable of receiving v.h.f. as well as existing programmes. The model 523 covers three wavebands and uses

seven valves, while the model 522 is a radio-gramophone with an automatic record changer.

Most of the television receivers on show will either be tunable to Bands I and III or will have facilities for the addition of a tuner unit.

A. C. Cossor Ltd., Cossor House, Highbury Grove, London, N.5.

**DECCA (39)** 

Four television receivers with directviewing 14-in or 17-in tubes will be shown as well as a projection receiver (Model 1000). There will also be two television-radio-gramophones. The Model RG98 and 102 radio-gramophones have 3-waveband receivers and 3-stage audio amplifiers.

Record reproducers made by this firm include a new "Panatrope" which is an inexpensive console incorporating a Garrard RC/111 record changer with a 3-stage negative feedback amplifier giving 21 watts. Another interesting model is the "Deccamatic II" portable portable player which employs a single pentode amplifier with a Collaro 3-speed motor and crystal pickup. Decca Record Company, Ltd., 1-3 Brixton

Road, London, S.W.9.

DEFIANT (106)

The five television receiver models exhibited cover both bands, being pre-set for any station in Band I and adjustable by the user to all eight channels of Band III.

sets include a mains filter and the completely line time-base is screened. Co-operative Wholesale Society Ltd.,

I Balloon Street, Manchester, 4.

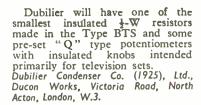
**DOMAIN (213)** 

Television receiver tables of metal tubular construction will be on show here. They have undershelves for carrying sound receivers or record players. Equipment for dealers' showrooms will also be displayed. Domain Products Ltd., Domain Works, Barnby Street, London, N.W.I.

DUBILIER (83)

Capacitors, resistors, fixed and variable, and radio interference suppressors comprise the main tadio parts in which this firm specializes. Miniaturization being an all-important requirement to-day, attention is being given to this aspect of design and some midget moulded silvered mica capacitors in a useful range of values are now available.

Among the ceramic dielectric capacitors interest will be focused on the "Hi-K" feed-through, stand-off and bushing styles in view of their particular suitability as r.f. by-pass capacitors in v.h.f. and Band III television receivers.



DYNATRON (103)

A range of large radio-gramophones will be on this stand and among them the Ether Marshal, a new model, is noteworthy for its elaborate specification. It is a 5-band set with an earthed-grid r.f. stage on short waves. There is variable selectivity and provision for the connection of an f.m. tuner. The a.f. amplifier, on a separate chassis, has a push-pull triode output stage.

The model TV27C television re-

ceiver, for a.c. only, has a 17-in tube and a.g.c. on both sound and vision channels. There is a black-level stabilizing circuit, a black spotter, and an anti-flutter circuit.

A television "mast-head" pre-

amplifier for fringe-area reception will be on view; also a range of nucleonic and electronic equipment. Dynatron Radio Ltd., The Firs, Castle Hill, Maidenhead, Berks.

E.A.R. (49)

Portable electric gramophones are a speciality of this firm, and models are available, with three-speed turntable motors or record changers, all of which play with the lid closed. The Model A750 high-quality instrument is fitted with a 10-in  $\times$  6-in elliptical loudspeaker and separate bass and treble tone controls.

Other products of this firm include a console record reproducer with 8-watt push-pull output, a 12-watt portable a.c./d.c. amplifier for p.a.

work, and a range of high-quality amplifiers for a.c. mains. Electric Audio Reproducers Ltd., 17 Little St. Leonards, Mortlake, London, S.W.14.

E.M.I. (9, 73)

One of the chief exhibits on these stands will be the BTR/2 tape recorder, which is available in console or transportable form and with tape speeds of either 15 and 30 or 71 and 15in/sec. Other tape recorders on show will be the transportable TR/50 with playing times of 64, 32 and 16 minutes (according to tape speed); the "Emicorda" domestic type and the portable battery-driven

model L/2 which weighs 14½ lb.

Amongst test gear displayed will be a bridge for measuring resistive and capacitive impedance in situ and signal generator covering the B.B.C. television channels. Electric & Musical Industries Ltd., Hayes, Middlesex.

EDISWAN (37)

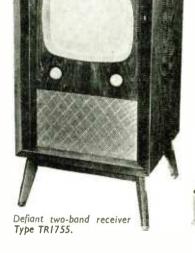
Aluminized cathode ray tubes will be the main feature of this stand and the range on show will include the latest 21-in rectangular type. A demonstration exhibit will show the 60 per cent increase in picture brightness obtained by aluminizing.

In valves, the 30L1 cascode double triode and the 30C1 triode pentode frequency-changer will be on view separately and as used in the Ediswan-Clix television turret tuner. This is a 12-position tuner, with pre-tuned r.f. and mixer stages, for multi-channel receivers operating in Bands I and III.

The Edison Swan Electric Co. Ltd., 155 Charing Cross Road, London, W.C.2.

EKCO (22, 92)

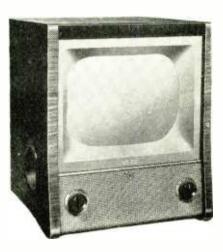
The television receivers exhibited will be types having either a built-in 13-channel turret tuner for Bands I and III or provision for adding such a tuner when required. The tubes range in size from 12-in to 17-in; one of the larger models is the a.c./d.c. type TC209 with flywheel sync, and a form of vision a.g.c.; spot wobble is



Chassis of Dynatron "Ether Marshal."

Left: Cossor Model 523 a.m./ f.m. receiver.

Right: Ekco 14-in table model, Type T221.



Wireless World, September 1954

included and the set is unusual in including an f.m. receiver for Band

Among the sound-broadcast receivers, the A239 is of especial interest because it provides for f.m. reception on Band II as well as the normal a.m. bands It has a builtin Band II aerial and provision is made for the use of a tape recorder.

The New Radiotime is an a.c. set, including an electric clock which can act as an alarm or be set to switch the set on or off at predetermined times.

E. K. Cole Ltd., Southend-on-Sea, Essex.

#### **ENGLISH ELECTRIC (85)**

The "40" series of television sets have a 17-in rectangular tube operating at 14 kV and they are of the a.c./d.c. type with a barretter for the control of the heater current. A 12channel turret tuner is included to cover Bands I and III, but, as the coils in it are changeable, it can also be used for Bands IV and V if required. There are three cabinet styles; the T40 and T41 are table models without and with doors and the C42 is a console with doors.

A tuner unit (the "Rotamatic")

enables Band-III reception to be obtained on existing Band I sets. It is a 12-position turret tuner like that in the "40" series sets and it 1eplaces the early valves in English Electric one-band sets. The output is at i.f. and connection is by plugs to the valveholders. The English Electric Co. Ltd., Marconi

House, 336-7 Strand, London, W.C.2.

**EVER READY (66)**Layer-type batteries for portable receivers will be shown with miniature and sub-miniature layer types for hearing aids. There will also be a range of all-dry battery receivers, including portables and table models, and two tropicalized export receivers. The Ever Ready Co. (Great Britain) Ltd., Hercules Place, Holloway, London, N.7.

#### **FERGUSON (14)**

Television receivers with 12-in, 14-in and 17-in tubes will be shown. The 103T and 105T, using the larger tube sizes, have turret-switch tuners for Bands I and III; others are primarily Band I sets but have provision for the addition of a plug-in three-way tuner unit to cater for two Band III stations. Frame-flyback suppression is used on all sets and Halolight, an illuminated surround to the picture, is now fitted on four of the console models.

Among sound-broadcast receivers, there are three models which give f.m. reception on Band II as well as the normal long, medium and short wavebands. In addition to several radio-gramophones of console pattern, there is a new table model

a three-speed automatic having record changer. Thorn Electrical Industries Ltd., 105-109 Judd Street, London, W.C.I.

#### FERRANTI (58, 76)

An exhibit of considerable interest here will be a table projection television receiver giving a picture size of  $16-in \times 12-in$ . The receiver is permeability-tuned over the five channels of Band I. The front end of the receiver is detachable so that it can be replaced by a Band I/Band III tuner unit. Beam current a.g.c. is applied to the final vision i.f. amplifier and this ensures minimum peak white defocusing and enables the set to be operated at a high average brightness level.

Among the valves and cathode-ray tubes on view will be a new 21-in rectangular tube with a 90° deflection

Ferranti Ltd., Moston, Manchester.

G.E.C. (68)
A range of new sound and television receivers will be on view. New Osram valves notable for their very high slope of 15 mA/V are the Z759 and Z359, both B9A pentodes intended as video amplifiers. The first has a 6.2 V heater and the second a 0.3 A heater. For Band III television tuners there will be the B319 double triode and the LZ319 triode pentode, while a new addition to the audio range of valves will be the N709 output pentode with an anode dissipation of 12 watts.

Among the c.r. tubes will be a development 21-in rectangular tube. General Electric Co. Ltd., Magnet House, Kingsway, London, W.C.2.

#### GARRARD (71)

The record changers and gramophone turntable units shown by this firm will be seen in the new standard colour scheme of cream and brown. From a comprehensive range the retooled Model 301 "transcription" motor, the new compact RC110 and RC111 three-speed record changers and the Type GC2 and GCE3 piezoelectric pickups may be selected as worthy of closer inspection. The GC2 is a Rochelle salt crystal turnover unit with a frequency range comparable with that of separate crystal heads, and the GCE3 employs a ceramic element for use under extreme conditions of heat and humidity.

Garrard Engineering and Manufacturing Co. Ltd., Newcastle Street, Swindon,

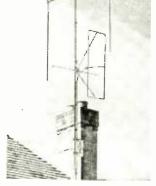
#### **GIBBS (20)**

This firm will be showing a record cabinet with a capacity of 170 records, and a range of tables suitable for television sets. Herbert E. Gibbs Ltd., First Avenue, Montague Road, Edmonton, London, N.18.

#### GOODMANS (63)

This stand will be virtually a soundproof theatre for the demonstration of high-quality reproduction, and

Tunable table projection receiver by Ferranti, Model 20T4.



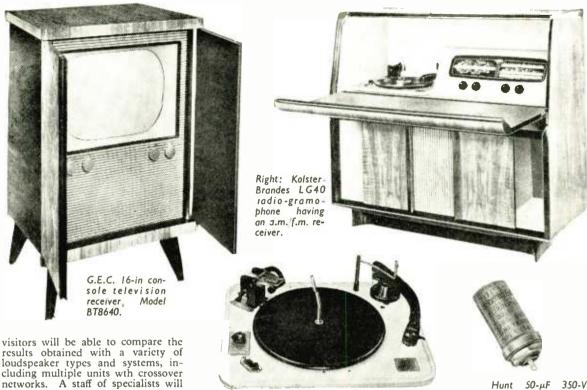
J-Beam 3-element Band I television aerial combined with a skeleton slot for Band III.



English Electric Rotamatic tuner for Band III television.



Ekco " New Radiotime" receiver.



networks. A staff of specialists will be in attendance to answer questions.

A new 12-in, 12-watt reproducer, the "Orlin III," will be shown in which the top response can be modified to give optimum performance on inputs of varying quality.

Goodmans Industries Ltd., Axiom Works, Wembley, Middlesex.

H.M.V. (10)

An important feature of this stand will be a new projection television receiver, Model 1823, with a projection tube of twice the screen area of more usual types. This gives a brighter picture than normally obtainable from such receivers. The current range of 14-in and 17-in direct-viewing sets on show will be available either as two-band versions or as Band I versions which can be modified for Band III reception when required. Three fringe-area sets incorporate a.g.c. on vision and sound, dark-scene contrast expansion, fly-back suppression and interference inversion.

Among the radiograms will be a portable and a transportable, both with a 3-speed record player on a pivoted counterbalanced desk which swings into the back of the cabinet when not in use.

Two new sound receivers will be shown. Model 1360 is a transportable in a plastic cabinet while model 1126 is a 5-valve table receiver. The Gramophone Co. Ltd., Hayes, Middlesex.

HUNT (90)
The Supermoldseal Type W96 is a miniature metallized-paper capacitor having a tough cast resin

case which is not easily damaged by accidental contact with a hot soldering iron. Working voltages are 200, 400 and 600 d.c. and capacitance values range from 50 pF to 100,000 pF.

changer.

Garrard RC80M 3-speed record

A new miniature single-hole fixing dry electrolytic known as the Type L136 will be shown, together with a range of low-voltage miniature electrolytics measuring 1 in long and & in in diameter, with working voltages of from 12 to 150 V d.c. and in capacitances of 1 to 50 µF.

A new development, described as the sprayed plate technique, is said to result in small bulk for a given capacitance.

A. H. Hunt (Capacitors) Ltd., Bendon Valley, Garratt Lane, Wandsworth, London, S.W.18.

INVICTA (95)

A 13-channel selector switch on the side of the cabinet will be a feature of three television sets to be displayed. These receivers, one 14-in and two 17-in, also incorporate automatic vision gain control (the blacklevel adjusting circuit), flywheel sync, a dark screen for daylight viewing and a built-in Band I aerial for areas of high signal strength.

A new console radiogram of small size is capable of playing L.P. records and has a receiver section covering the trawler waveband. Invicta Radio Ltd., 100 Great Portland Street, London, W.I. miniature lytic.

Type

L136

electro-

wkg

J.B. CABINETS (18) This firm manufacture radio and and radio-gramophone cabinets for the trade and their exhibit will comprise a selection of the latest and most interesting types which have been recently produced.

J.B. Manufacturing Co. (Cabinets) Ltd., 86 Palmerston Road, Walthamstow,

London, E.17.

J-BEAM AERIALS (31)

A special feature of this firm's television aerials is that the feeder is connected to one end of the main dipole via an impedance niatching stub. The stub can be incorporated in the supporting mast which then becomes virtually an extension of the dipole. They will be showing also a "skeleton slot" aerial for Band III. J-Beam Aerials Ltd., Cleveland Works, Weedon Road Industrial Northampton.

K.B. (70)

The television sets to be shown on this stand include a multi-channel turret tuner for Bands I and III. There is a table model with a 14-in tube and another with a 17-in, while the two console types have 17-in tubes. One of these has a tube with electrostatic focus, pre-set in the factory.

Adaptors to enable single-band K.B. receivers to be used on Band III are being produced.

A newcomer to the range of broad-

cast sound receivers is the KR20FM. This is a 6-valve set for a.c. operation which covers the usual medium and long wavebands and also the v.h.f. band. Some of the older models are still being retained, among them the FP151 a.c./d.c./battery portable.

Five radio-gramophones will be shown. Among the new types is the LG40AM/FM in which the receiver covers the f.m. band and has a pushpull output stage. Kolster-Brandes Ltd., Footscray, Kent.

M.o.S. (212)

The main exhibit on this stand is a telemetering system for guided missiles.

Ministry of Supply, Shell Mex House' Strand, London, W.C.2.

#### McMICHAEL (72)

The new television receivers will be available with 14-in or 17-in rectangular flat-faced tubes and in table and console models, with or without sound ragio receivers. One chassis is common to all the new sets.

Special attention has been given to reliability and service accessibility. The entire chassis can be taken out of its cabinet in 13min and the tube in 11min.

These new sets will be adequately supported by a comprehensive range of sound receivers including an a.c./ d.c. mains/battery portable set with

a self-contained ferrite rod aerial. McMichael Radio Ltd., 190 Strand, London, W.C.2.

Another addition to the "Companion" range of sound receivers will be model T37DA, a 5-valve a.c./d.c. transportable covering two wavebands. There will also be a new mains/battery portable, model T36AB, in attache-case form and a new table receiver, model T38A, covering three wavebands. radio-gramophones on show will be the model ARG40A, the ARG41A in a "contemporary" style cabinet and the TARG39A table model, all with 5-valve 3-waveband receivers.

Television receivers will also be displayed. The Marconiphone Co. Ltd., Blyth Road, Hayes, Middlesex.

#### MASTERADIO (62)

To be shown for the first time at the exhibition will be a new table radiogram in a distinctively designed walnut veneered cabinet. It incorporates a 3-speed automatic record changer and covers short, medium and long waves. Also entirely new will be a portable electric gramo-phone known as "The Harmony" which plays 12-in records.

Television receivers will include two 17-in models with built-in Band III converters; one is a multi-channel table model, the other a console type with full-length doors. Some car radio sets will conclude an interesting display.

Masteradio Ltd., Fitzroy Place London, N.W.I.

#### MULLARD (56)

For the amateur constructor this firm have produced a new design for a high-quality ten-watt amplifier, built around five Mullard audio valves—EF86 input, ECC83 phasesplitter, two EL84 output pentodes in push-pull and GZ30 rectifier. The response is almost flat from 10c/s to 20kc/s and harmonic distortion is below 0.4%. A booklet giving details will be available on the stand and the amplifier itself will be demonstrated in an associated room. Mullard Ltd., Century House, Shaftesbury Avenue, London, W.C.2.

#### MULTICORE (100)

Designed to increase soldering speed, a 5-cored wire solder will be shown publicly for the first time. This contains a new flux (362) which in some applications permits the use of cheaper solder alloys containing less



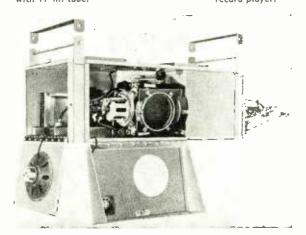
Murphy V250 two-band receiver with 17-in. tube.



Masteradio "Harmony" portable recard blaver.



Philco 14-in. tunable television set, Model A1467.





To demonstrate the large-scale use of Multicore solder in industry, the assembly and wiring of Ferguson television tuning units will be carried out.

Special soldering alloys to be shown include TLC, with a melting point of 145°C and "Consol" containing silver and having a melting point of 296°C.

Multicore Solders Ltd., Hemel Hempstead, Herts.

#### MURPHY (40)

This year's receivers are based on a chassis which is substantially the same for all models, the chassis differences between the 14-in V240 and the 17-in V250 being mainly the provision of higher voltages for the tube of the latter. Fringe-area models have flywheel sync, a gated a.g.c. circuit and a special noise limiter.

Provision is made in all models for Band-I and Band-III reception by means of a 12-channel turret tuner, the r.f. stage being of the cascode type. A direct-drive line-scan circuit is used.

Among sound-broadcast receivers, the new V198 and A212 will be shown. The V198 is an a.c./d.c. set with a built-in ferrite-cored aerial covering medium and long wave-bands. The A212 is a larger table model for a.c. mains only and including one s.w. band. It has an internal plate aerial and provision for an external aerial.

Murphy Radio Ltd., Welwyn Garden City. Herts.

NAVY (204)

Operational conditions for underwater television are simulated by the provision of a large glass-sided tank on the ground floor, in which the camera is suspended, while the remote control and monitoring gear is in the gallery. Training exhibits are being provided by the two Naval electrical schools-H.M.S. Collingwood and H.M.S. Ariel—and the R.N.V.(W)R. Examples of radio

communication equipment, tronic control and navigational gear and facsimile apparatus used in the Navy are being provided by Mar-coni's, Pye, Redifon, Muirhead, Decca, Murphy and G.E.C. for display and demonstration on this stand.

Admiralty, Whitehall, London, S.W.I.

#### **NERA** (208)

This firm will be showing projection television equipment for picture sizes ranging from 30in to 84in. A projector for ceiling mounting is designed to give a picture 4ft by 3ft.

A 12-channel converter for Nera receivers will also be shown.
Nera of England Ltd., Jeffries Passage,
High Street, Guildford, Surrey.

#### PAM (4, 84)

Five television models will be shown, all for a.c./d.c. operation and with 13-channel tuners. A form of a.g.c. is provided in all but the cheapest 12-in Model T954.

Two table model sound receivers (955a and 965) employ basically the same 4-waveband chassis, which is also used in the Model 966RG radio-gramophone.

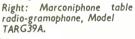
The Model 610 wide-range record player has a push-pull output driving an 8-in loudspeaker. The table cabinet is designed to reinforce the bass response when the lid is closed and the loudspeaker aperture is designed to give wide-angle diffusion of high frequencies.

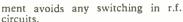
Pam (Radio and Television) Ltd., 295, Regent Street, London, W.I.

#### PETO SCOTT (60)

The television receivers shown by this firm are designed primarily as Band-I sets with a switch changeover to an alternative tuner, which is physically a separate unit, for Band III. The tuner has a cascode r.f. stage and tuning is continuous by the adjustment of ganged cores to the coils. The circuit arrange-

> Left: Pam Model 966/RG radio-gramophone.





Among the sound equipment to be shown is a table-model receiver including one s.w. band, the R54, an automatic 3-speed record changer radio-gramophone and a record reproducer with auto-changer. Peto Scott Electrical Instruments Ltd. Addlestone Road, Weybridge, Surrey,

#### PHILCO (36)

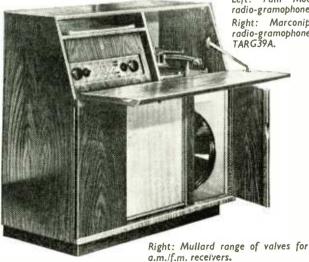
Among the new television sets to be shown is a 14-in table model incorporating a turret tuner for reception of Band-III programmes. It has a.g.c. and noise suppression on both vision and sound channels. Similar facilities are offered by a 17-in model, with the additional feature of a removable front to the cabinet which allows the tube and mask to be cleaned.

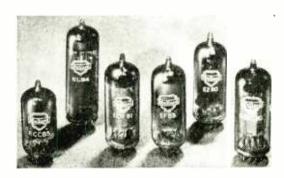
Three sound receivers on view are notable for having all metal parts and components fully tropicalized so that they can be operated in kitchens, etc., without fear of deterioration from steam and damp. Philco (Great Britain) Ltd., Romford Road, Chigwell, Essex.

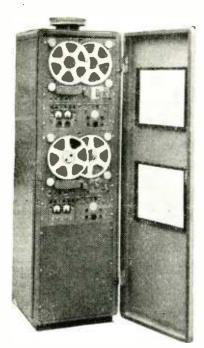
#### PHILIPS (96, 97)

Of most topical interest on these stands will be an a.m./f.m. table receiver, Model 543A. It uses 7 valves and is designed for a.c. mains only. Another new exhibit will be a 5-valve receiver which also acts as









Simon dual tape monitoring equip-

an alarm clock and will switch itself on and off at pre-set times. It is pre-set tuned for four stations, three medium-wave and one longwave.

Amongst radio-gramophones and record players will be a new portable record player, Model AG2121, incorporating a 3-valve amplifier and, in the lid, a 7-in loudspeaker.

Two new table television re-ceivers, one 14-in and the other 17-in, will incorporate a turret tuner for reception of B.B.C. and Band-III programmes.

Philips Electrical Ltd., Century House, Shaftesbury Avenue, London, W.C.2.

#### **PILOT (59)**

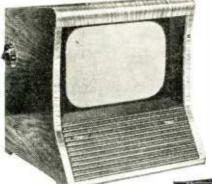
Five television sets to be shown by this firm will all have provision for plugging in a tuner for reception of alternative programmes. Two are 14-in models and three are 17-in models. The 12-position tuner is a turret type covering 13 channels and costs 6 guineas. It has a dual control knob, with a numbered inner section for selecting the channel and an outer rim for fine oscillator tuning.

Among the sound broadcast receivers will be a new battery/mains portable (a.c./d.c.) in attaché-case form. It has a Ferroxcube built-in rod aerial and a 6in × 4in elliptical

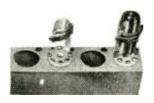
Pilot Radio Ltd., Park Royal Road, London, N.W.10.

#### PLESSEY (28)

This firm manufactures an extensive range of components, accessories and complete radio assemblies for the trade; their exhibit will consist of some of the newer and more inter-



Pye 13-channel receiver, Model



Plessey valveholder clip for mounting sub - miniature valves.



Germanium junction power rectifiers by S.T.C.

esting items now in production. A novel development is some special clips for sub-miniature valves, one is for chassis mounting like a valveholder, the other holds two valves and can be fixed in any position. A strip switch for a.m./f.m. sets will also be shown.

Plessey Co. Ltd., Vicarage Lane, Ilford, Essex.

#### PYE (94)

One of the latest television receivers to be shown by this firm will be the 13-channel Model VT4. This is a 14-in table receiver with a tilted-forward screen, and the 12position channel selection switch covers the five B.B.C. channels in Band I and channels 7 to 13 in Band III (channel 6 being brought in by oscillator trimmer tuning when required). The receiver also incorporates vision a.g.c., flywheel sync, vision interference inversion and frame fly-back suppression.

High-quality sound reproduction equipment will also be on view. Pye Ltd., Radio Works, Cambridge.



Pilot 13-channel Turret Tuner.



Philips 14-in. tunable television set, Model 1446U.

#### R.A.F. (203)

Inspection and repair of v.h.f. airborne equipment as undertaken in the workshops of the Maintenance Command of the R.A.F. is to be Radio's part in demonstrated. weather forecasting will be illustrated in a typical Meteorological Forecasting Office set-up on the stand. Visitors will also see the complex assembly of radio and electronic equipment now carried in modern jet aircraft.

Air Ministry, Whitehall Gardens, London, S.W.1.

R.G.D. (93)
Four table-model and two console receivers comprise the R.G.D. television programme together with a combined television and radio-gramophone (Model C55). An improved synchronizing circuit ("Synchrolock") is a feature of the 17valve circuit.

Twin 6½-in loudspeakers and a push-pull output stage are used in the "Two-Ten" table model radiogrambphone which takes its place with the R.G.D. console models. The "One-Ten" sound receiver is a 6-valve, 3-waveband model with push-pull output.

Radio Gramophone Development Company Ltd., Eastern Avenue West, Mawneys, Romford, Essex.

#### R.S.G.B. (209)

A wide variety of modern amateurconstructed sound and vision transmitting and receiving equipment will be seen on the R.S.G.B. stand. The emphasis is on equipment for use in the recently formed Radio Amateur

Emergency Network. V.H.F. and u.h.f. gear, some transistor transmitters and s.s.b. transmitting and receiving equipment will also be displayed. Historic amateur equipment and a clandestine receiver constructed in a prisoner-of-war camp will be seen.

Radio Society of Great Britain, New Ruskin House, Little Russell Street, London, W.C.I.

REFLECTOGRAPH (207)

An ingenious continuously variable drive mechanism forms the basis of the magnetic tape recorders made by this firm. In addition to standard portable domestic recorders, a number of scientific and industrial machines will be shown. For some of these (Series P) a frequency response of 80 c/s to 15 kc/s  $\pm$  3 db is claimed at 7½ in/sec.

Two systems of recording very low frequencies have been developed, one of which (Model PLF2), employing a differential pulse-code system, is capable of recording down to zero frequency and is independent of tape speed.
Rudman Darlington (Electronics) Ltd.,

Wednesfield, Staffs.

REGENTONE (38)
Sound receivers and radio-gramophones include the "Multi 99" table radio-gramophone incorporating a B.S.R. "Monarch" record changer. This model is also available in console form.

Three portable gramophones in tough-fibre cases are designed for hard use. They are the RP2 record player for feeding the pickup terminals of any broadcast receiver, the HG2 "Handy-Gram" with built-in amplifier and loudspeaker, and an automatic record changer version (AHG2).

Regentone television sets are being re-designed in detail and will be shown in new cabinets.

Regentone Radio and Television Ltd., Eastern Avenue West, Mawneys, Romford, Essex.

ROBERTS (102)

Portable sound broadcast receivers are associated with the name of this firm and in the current range Model RP4 (battery) and RMB (a.c. mains/ battery) are now available in "rexine" covered cabinets. Models CR (a.c. mains/battery), BR (battery) and MR (a.c. mains) can be obtained in a wide range of colours. Roberts Radio Company Ltd., Creek Road. East Molesey, Surrey.

**ROLA CELESTION (3)** 

A loudspeaker designed to be operated under conditions of extremely high or low atmospheric pressure, and capable of surviving complete immersion in water is indicative of the wide field of activities of this firm. All sizes from 2½ in to 18 in diameter are available, including elliptical types and other special designs for receiver manufacturers. A wide range of output transformers, including hermetically sealed types for tropical climates will be shown.

Public address loudspeakers and line-matching transformers, under the Truvox marque, for powers from 3 to 120 watts also form part of this exhibit.

Rola Cèlestion Ltd., Ferry Works, Thames Ditton, Surrey.

S.T.C. (82)

Asymmetric resistors (working on a rectifier principle) suitable for digital computors will be shown under construction and as used in an electronic accounting machine. Also on view will be metal rectifiers for h.t. and e.h.t. supplies; battery charging rectifiers; high voltage aluminium rectifiers for aircraft power supplies; germanium junction power rectifiers and a germanium junction photocell suitable for direct operation of relays. Standard Telephones

and Cables Ltd., Connaught House, Aldwych, London. W.C.2.

Some fine examples of engineering construction will be seen in the professional and domestic magnetic tape recorders made by this firm. The long-duration tape monitors for recording air traffic control messages and the Model SP/1 portable recorder with 10-watt output are of great technical interest.

SIMON (104)

Simon Equipment Ltd., 48-50 George Street, Portman Square, London, W.I.

SKY-MASTS (30)

The design and erection of aerial masts and complete aerial installations constitute the main activities of this company and their exhibit will show in model and in actual form some of the more interesting types they produce. Sky-Masts, Beadon Garage, Beadon Road,

London, W.6.

SOBELL (12)

Sound-broadcast, television receivers and radio-gramophones will be displayed on this stand. Most of the last include automatic record changers and all have three-speed motors and employ crystal pickups. The sound receivers have provision for a pickup and an external loudspeaker.

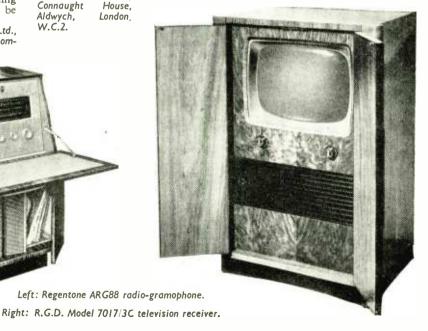
Most television sets include turret tuners for Bands I and III; the 12-in model, which does not, has provision for a Band-III adaptor. A form of a.g.c. is included in the sets and flyback suppression is fitted. models include 12-in, 14-in and 17-in types and all are for a.c./d.c. operation.

Sobell Industries Ltd., Langley Park, Slough, Bucks.

STELLA (SS)

Four new table television receivers will be shown with provision for re-



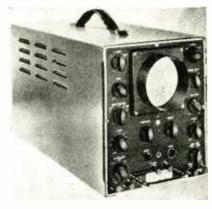




17-in. table model, type Ultra V.9-17.



Vidor "Lady Margaret" handbagsize portable, but with 5-in. loudspeaker.



Telequipment oscilloscope Type 520 with 4-in. flat-faced tube.



Whiteley concentric Duplex loudspeaker.



Taylor Model 67A signal generator.



ception of Band-III programmes. The ST8314U 14-in model and ST8317U 17-in model are designed to incorporate a tuner when the programmes become available, while the 14-in model 6414U and 17-in model 6417U already include the tuners and have fine tuning and pre-set sensitivity controls for each channel.

An important feature of the model 102A sound receiver is bass compensation for low positions on the volume control. Also on view will be a portable record player with a pickup needle pressure of less than one-

third of an ounce. Stella Radio & Television Co. Ltd., Oxford House, 9-15 Oxford Street London, W.I.

T.C.C. (101)

Among the many capacitors shown by T.C.C. this year will be six new ceramic types for incorporating in Band III television converters and in multi-channel dual-band tuners. Some are known as "Hi-K" and some "Low-K," the former being fairly large-capacitance bypass types for soldering into punched holes in the chassis. They take the form of lead-through, bushing and stand-off types. The "Low-K" are mostly pre-set variables with very small capacitance sweep; 0.5 to 3 pF and 1 to 5 pF are typical.

Electrolytic capacitors with very high insulation resistance are now

included in the T.C.C. range and these are suitable for inter-valve a.f. couplings. A feature this year of the T.C.C. exhibit will be a demonstration of power-factor correction.
Telegraph Condenser Co. Ltd., Wales Farm Road, North Acton, London, W.3.

TAYLOR (54)

Some entirely new models of test apparatus are being introduced on this occasion; one is a 100-kc/s to 240-Mc/s signal generator known as Model 67A. Internal modulation at 400 c/s is provided.

Another interesting test set is the Model 92A; this is a television sweep oscillator covering 0-250 Mc/s and with a frequency deviation, or sweep, variable from  $\pm 1.5$  to  $\pm 15$  Mc/s.

Other new items include a d.c. valve voltmeter covering 1 to 1,000 V with an input impedance of 25 M2 and a 10-c/s to 100-kc/s RC oscil-

Taylor Electrical Instruments Ltd., 419-424 Montrose Avenue, Slough, Bucks.

TELEMAX (81)

Two models of front-projection television receiver are being shown by this firm. The 2352 gives a 4-ft by 3-ft picture and is self-contained; the new CT1 is in two units, camouflaged as normal articles of furniture.

There will be a direct-view receiver, with a 17-in tube and a 12channel tuner, which is unusual in being combined with a record player.



Waveforms type 405 television signal generator.

The exhibit will include a Band-III converter and an insulation test set covering 150 V to 10 kV Telemechanics Ltd., 3 Newman Yard, Newman Street, London, W.I.

TELEQUIPMENT (80)

Television test apparatus is the speciality of this firm, who this year will show a 625-line Monoscope equipment which provides a complete video signal and synchronizing pulses to C.C.I.R. standards. Models for 405 and 525 lines have been available for some time.

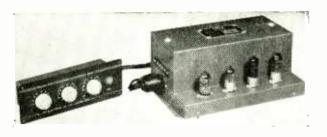
Specially designed for television work is the Type 520 oscilloscope embodying a 4-in flat-faced tube and a "Y" amplifier of exceptional performance. The "X" amplifier gives an expansion up to 5 screen diame-

Telequipment Ltd., 1319A High Road, Whetstone, London, N.20.

TELERECTION (5)

Considerable thought has been given by Telerection to the problems involved in the design of multi-band television aerials and while final designs cannot very well be produced before all the facts of Band-III television are known, they will be showing some examples of how the problems can be tackled for both the semi-local and fringe area viewers. Telerection Ltd., Antenna Works, St. Pau.s, Cheirenham, Glos.

Wireless World, September 1954







Left: Trix T41 domestic high-quality amplifier. Centre: Valradio tuner covering Bands I, II and III. Right: T.C.C. ceramic trimmer for use in TV tuners.

TELEVISION SOCIETY (205)

The equipment to be displayed has been chosen to illustrate the various aspects of television engineering covered by the papers read at the society's meetings. Reprints of some of the papers read during the past session will be available. Television Society, 164 Avenue, London, W.C.2. Shaftesbury

#### TRIX (65)

Amplifiers and auxiliary equipment for every class of sound reproduction from portable "crooner" outfits to rack-mounted large-scale p.a. installations are made by this firm. Designed for high-quality music reproduction in the home, the Model T41 amplifier, with a power output of 3-4 watts, is of special interest. A separate control unit is provided with independent bass and treble controls and there are two inputs for use with pickups of all types giving maximum output for 3 mV and 130 mV. Trix Electrical Company Ltd., I-5 Maple Place, Tottenham Court Road, London,

#### **ULTRA** (69)

W.L.

Receivers embodying tubes of from 12-in to 17-in will be exhibited. Because of the particular mask shape adopted, a somewhat bigger picture than is usual for the tube size is claimed. The tuning system has a switch channel selector giving a choice of one Band-I and two Band-III stations, the Band-III tuner being a separate unit

In addition to a range of soundbroadcast receivers, a radio-gramophone will be on view. This is the ARG891 which includes space for record storage. A model for f.m. record storage.
reception is available.
reception is discounted from the storage of the storage

Ultra Electric Ltd., Acton, London, W.3.

#### VALRADIO (29)

Reception of f.m. transmissions in Band II, as well as television transmissions in Bands I and III, is possible with the new multi-channel tuner to be shown by this firm. It uses a PCC84 cascode r.f. amplifier and a PCF80 frequency changer and covers 40-100 Mc/s in four steps and 170-225 Mc/s in two steps. Continuous tuning is provided over each step by ganged iron-dust cores and brass slugs in the coils.

Incorporating this tuner will be a new projection television set, giving a picture of  $27 \text{in} \times 20\frac{3}{4} \text{in}$  on a screen in the lid.

Valradio Ltd., New Chapel Road. High Street, Feltham, Middlesex.

#### **VIDOR (87)**

No fewer than five different portable sets will be shown this year; one, the "Lady Margaret," is entirely new and although no larger than a lady's handbag  $(8 \times 8 \times 4 \text{ in})$  it incorporates a 4-valve receiver, takes a 90-V battery and boasts a 5-in loudspeaker; the weight is 6½ lb only.

Provision is made in the latest 14in and 17-in television receivers for internally fitting a Band-III con-

A special feature will be made of export type receivers, the batteries being protected against humidity and extremes of temperature.

Dry batteries of some 370 different types, ranging from those for torches to special models for nucleonic equipment, will be shown. Vidor Ltd., West Street, Erith, Kent.

#### WAVEFORMS (75)

A new television signal generator will be on this stand. The Radar 405 provides an r.f. signal, tunable over Bands I and III, which is modulated by the correct sync pulses and a selection of test patterns. The sound and vision outputs are independently tunable and can be used together. The output is adjustable from 10 µV to 10 mV.

A more elaborate instrument, the type W90, will also be shown, to-gether with a range of other test Waveforms Ltd., Radar Works, Truro

Road, London, N.22.

#### WEARITE (74)

Principal interest on this stand centres on the Ferrograph magnetic tape recorder, which is available in many forms for scientific and industrial research as well as for domestic and professional sound recording.

A special version (2A/NH) of the Model 2A recorder will be 3hown, with tape speeds of  $7\frac{1}{2}$  and 15in/sec instead of 3\frac{3}{4} and 7\frac{1}{2} in/sec. Another interesting version is the YDC with simultaneous dual-track recording for comparative analysis or stereophonic recording. Wright and Weaire Ltd., 131 Sloane

Street, London, S.W.I.

WESTINGHOUSE (2)

Tubular e.h.t. rectifiers will be prominent on this stand and the normal range will cover d.c. outputs of up to 15kV in single units with current outputs of between 100  $\mu$ A and 8 mA. Copper-oxide instrument rectifiers, "Westectors" and germanium diodes will also be on view.
Westinghouse Brake & Signal Co. Ltd., 82 York Way, King's Cross, London, N.I.

#### WHITE-IRROTSON (98)

Large-screen projection television receivers will be shown on this The 4836 gives a picture stand. 4ft × 3ft and is available in front- or back-projection forms. The 2418 and 2015 are rear-projection types and give pictures of 24in by 18in and 20in by 15in respectively.

Vision and waveform monitors will also be shown.

White-Ibbotson Ltd., Mortimer House, 37-41 Mortimer Street, London, W.I.

#### WHITELEY ELECTRICAL (105)

The cambric cone, introduced last year, has now been applied to the 12-in concentric Duplex and other loudspeakers in the high-quality range. A new dismountable "bass reflex" cabinet, which can be easily assembled, has been introduced for use with the 10-in and 12-in highquality loudspeakers. Extension loudspeaker units with volume controls and optional push-button remote control will also be shown.

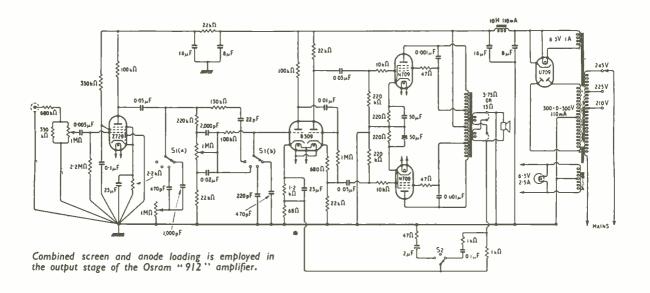
Sound reproduction is by no means the only activity of this firm, and the exhibit will also provide examples of a wide variety of components, including amplifiers, wavemeters, a.m.

and f.m. transmitters. Whiteley Electrical Radio Company Ltd., Mansfield, Notts.

#### WOLSEY (16)

To be shown this year will be a new "X" type television aerial with a "delta" matching section incor-porated in one of the Vs formed by the crossed dipoles. Appropriately named the "Deltex" aerial it is said to give better matching between aerial and feeder. As neither dipole need be split and insulated at the. centre it results in a far stronger construction. Like all other Wolsey aerials the "Deltex" is pre-assembled to simplify erection.

Wolsey Television Ltd., 43-45 Knight's Hill, West Norwood, London. S.E.27.



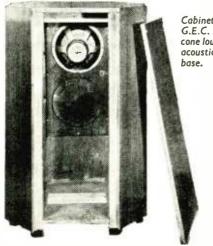
## HIGH-QUALITY SOUND REPRODUCER

Osram "912" Amplifier and G.E.C. Metal-Cone Loudspeaker

NOW that the G.E.C. "F.R." metal-cone loud-speaker is in quantity production, the makers have decided to issue a design for an amplifier which will ensure that its full capabilities are realized. This design will be published as a booklet (price 3s 6d), which will also give details of a recommended cabinet for the loudspeaker.

The circuit type number "912" indicates that the frequency range is 9 octaves (30 c/s-16 kc/s) and that the power output is 12 watts. The first stage is a Z729 low-noise pentode, followed by a B309 double triode in which one triode acts as the second a.f. stage and the other as a phase splitter.

Two N709 pentodes in push-pull have the output load distributed between anodes and cathodes, thus giving a compromise between pentode and triode



Cabinet designed by G.E.C. for the metalcone loudspeaker. The acoustic vent is in the operation as far as efficiency and harmonic distortion are concerned.

Feedback is applied over the last three stages and can be modified by a switched RC network in the feedback loop to give a flat response or one with an approximately 5 db level lift or drop from about 3,000 c/s upwards. This is described as a "presence" control and when "in" has the effect of transporting the listener to the front seats of the concert hall where the ratio of high to low frequencies is higher than, say, at the back of the hall, where the increased proportion of reverberation and high-frequency absorption tend to depress this ratio. The device is admittedly artificial but the effects are more realistic than those which would be obtained with normal sloping tone control characteristics. Normal tone control is, of course, provided (between the first and second stage) to cope with variations in recording and pickup characteristics.

The "F.R." metal-cone loudspeaker\* in addition to its low non-linearity distortion is capable of a very uniform and extended frequency response when housed in a suitable enclosure. A very rigid cabinet of octagonal section has been developed in which unwanted panel resonances are suppressed, only the single Helmhotz resonance being applied at or near the fundamental cone resonance to control the impedance rise and extend the low-frequency response. The vent is situated in the centre of the cabinet, which is raised from the floor by four supports, the height of which tunes the acoustic resonance, since the air mass between the floor and base is in radial vibration. It is conceivable that, with this arrangement the resistive damping is increased. However this may be, the result is a remarkably smooth and full bass response down to 30 c/s which adds no trace of coloration to the reproduction of speech.

<sup>\*</sup> See Wireless World Nov. and Dec. 1952.

# Combination F.M./A.M. Receivers

Design Factors of Sets for the New B.B.C. Service

By G. H. RUSSELL,

Assoc, Brit, L.R.E.

districts about

REQUENCY modulation broadcasting is to comcombination receivers will have to be provided for the reception of both the f.m. transmissions in the v.h.f. Band II, and the a.m. transmissions which will continue to be radiated in the medium and long broadcast

The standards of f.m. transmission will be similar to those prevailing in America and Germany; 100 per cent modulation will correspond to 75 kc/s deviation, maximum modulation frequency will be 15 kc/s, and pre-emphasis corresponding to a time constant of  $50 \,\mu$  secs will be used. The nominal channel separation

will be 200 kc/s, and judging from a preliminary list of stations it would appear that stations serving the same area will be separated by 2.2 Mc/s. Generally, the minimum field strength in towns may be expected to be in the region of 800 uV/metre, and in country

250 "V/metre.

Translating this information into receiver requirements, we arrive at the following design data. The receiver should be tuneable over the whole of Band II; that is, 87.5 to 100 Mc/s, although initially only 88-95 Mc/s will be available for the f.m. service. Regardless of the modulation frequencies involved, the bandwidth will have to be made considerably greater than that theoretically required, to allow for oscillator drift; 3 db at  $\pm 100$  kc/s should be regarded as a minimum. In this respect, it is safer to err on the liberal side as the distortion produced on a f.m. receiver by mistuning is at least as great as that obtained on selective a.m. receivers. Taking into account the "capture effect" and the distribution of stations, a selectivity characteristic of  $-3 \, db$  at  $\pm 150 \, kc/s$  would probably make a good compromise.

As the vast majority of these receivers will undoubtedly be used with the inevitable "piece of wire" acting as an aerial, a sensitivity of the order of 10 µV will almost certainly be required. Sensitivity in f.m. receivers means not only that the standard 50-mW output is obtained with a given r.f. input signal 30 per cent modulated, but also that the receiver limits satisfactorily with the same input. If satisfactory limiting requires a greater input than that required to produce standard output, it is this figure that expresses the true sensitivity of the receiver. Satisfactory limiting may be defined as that which produces an f.m. to a.m. ratio of not less than 30 db. For preference the figure should be in the region of 40 db. The f.m. to a.m. ratio expresses the difference in the output of a receiver produced by injecting consecutively (at the centre frequency) f.m. and a.m. signals both 30 per cent modulated. It is as well to point out here that the majority of f.m./a.m. signal generators available in this country to date show a distressing tendency to change frequency when the system of modulation is changed. As 100 per cent modulation corresponds

to 75 kc/s deviation, it should be clear that 30 per cent modulation corresponds to 22.5 kc/s deviation.

General Considerations.—From the foregoing, the outline of the combination f.m./a.m. receiver becomes apparent. First, two tuners are required; one to tune the long- and medium-wave broadcast bands, and the other to tune the v.h.f. band. For obvious reasons these should be controlled by a single knob. Secondly, two separate intermediate frequency amplifier chains are required; one for the broadcast bands which will embody the usual selective amplifier operating at a frequency of about 470 kc/s, and the other a relatively wide-band amplifier operating at a considerably higher

frequency. Thirdly, in all but a few cases, two detectors are required—one for a.m. and one for f.m. demodulation, the latter including, or being preceded by, some form of amplitude limiting.

Fourthly, a method of switching

both the wavebands and the systems must be devised. In all but the most expensive receivers, the short waveband, which has been a feature of the majority of our receivers since the mid-thirties, may now be expected to disappear. In western Germany, where over 90 f.m. stations give almost complete coverage, even the long waveband has disappeared from what may be termed the standard receiver. eventually be expected to happen here when complete f.m. coverage is attained, but until then a long waveband will have to be provided in our receivers for the reception of Droitwich.

Due to the use of a higher value of intermediate frequency and the need for a considerably wider bandwidth, more stages of amplification are needed for f.m. than for broadcast reception. The usual method of obtaining this is to use the heptode section of the broadcast frequency changer as an extra i.f. amplifier, together with a second i.f. stage using a valve with a higher slope than is usual in broadcast receivers. A special series of valves has been made available for combination receivers. The Mullard range includes the ECH81 triode-heptode, the EF85 variable-mu pentode with a mutual conductance of 6 mA/V, and the EABC80 triple-diode triode. With the latter, two diodes are used for the f.m. demodulator and the third for detection and a.g.c. on the broadcast bands.

Delayed a.g.c. cannot be provided with this arrangement, but as a great deal more gain can be obtained from the i.f. amplifier than is usual in broadcast receivers, this should be of little consequence. Alternatively, a separate germanium diode could be fitted. A.G.C. is not generally used with f.m. receivers as minor variations in amplitude do not affect the receiver output, and the lack of a.g.c. provides extra limiting with large inputs. Both the ECH81 and EF85 are operated with relatively large screen resistors  $(22 k\Omega)$  and  $56 k\Omega$  respectively) which make it almost impossible to exceed the maximum permissible dissipation. With standard 470-kc/s i.f. transformers, the

EF85 stage gain will be far too high and instability will result unless this is reduced to manageable proportions. This can be achieved either by using i.f. transformers with a suitably low dynamic resistance or, possibly more simply, by switching in a supplementary cathode resistance. The conversion conductance of the ECH81 is  $775 \,\mu\text{A/V}$ , and the mutual conductance of the heptode section is  $2.4 \,\text{mA/V}$  when it is used as a straightforward amplifier.

V.H.F. Tuning Unit.—As the heptode section of the ECH81 is used as an i.f. amplifier for v.h.f. reception, it clearly cannot be used as a frequency changer at these frequencies. It is, furthermore, undesirable that it should be so used, as at v.h.f. it would give very poor gain in comparison with other methods. It would also require switching at v.h.f. which is some-

thing to be avoided as far as possible.

The v.h.f. mixer is therefore almost invariably a separate valve; triodes and pentodes being equally popular. Both types are usually employed as selfoscillating mixers; a circuit which gives a high conversion gain. In Germany, a triode self-oscillating mixer (EC92) is much favoured, but as the Germans tend to use this without a stage of r.f. amplification, oscillator radiation is a problem. To minimize this, the valve is used in a form of bridge circuit the function of which is to cancel out the oscillator voltages at the aerial. Its efficacy, however, seems somewhat limited, as one German receiver employing this circuit which the author tested showed 300 mV to be present across the correctly terminated aerial sockets. It is understood that this is by no means uncommon. As German receivers use an i.f. of 10.7 Mc/s and make use of the whole of Band II, it can be seen that the oscillator frequency actually falls within the It can only be assumed that this fact was taken into account when frequencies were allocated.

There can be no doubt that in this country such a practice would be frowned upon, and an r.f. stage should be regarded as a necessity. For the same reason, the use of a super-regenerative type of receiver is almost out of the question. Its high efficiency and apparent simplicity make it appear an attractive

proposition, but as it makes use of a pulsed oscillator it could be placed under the heading of "small power transmitters." The power radiated by these oscillators is so high that it is doubtful whether an r.f. stage would provide adequate protection. To return to the r.f. stage, here again a choice between triodes and pentodes can be made; the triode being earthed-grid connected. As receiver noise is of little moment in f.m. receivers, the choice between triodes and pentodes for the mixer or r.f. amplifier is purely a matter of convenience. The choice is usually made by balancing amplification against cost.

Either permeability or capacitive tuning can be used; the latter being more convenient from a mechanical design standpoint. Tuning capacitors made specially for these receivers are now available. If permeability tuning is used, the r.f. stage can be pre-set tuned to the centre of the band to avoid alignment problems. Little is lost by so doing. One advantage of not having externally controlled signal frequency tuning is that the inter-valve circuit capacitance can be kept low, permitting a higher LC ratio to be obtained. A unit similar to that published in Wireless World recently, but designed for use on Band II, with an aerial step-up transformer and a 1:1 i.f. transformer, will give a gain from the aerial input to the secondary of the i.f. transformer considerably in excess of 100. One last word about the usefulness of the r.f. stage. Quite apart from the fact that it isolates the oscillator, it is well worth the extra cost because a well-designed stage will provide appreciable rejection of spurious responses as well as worthwhile gain.

I.F. Amplifier.—A typical i.f. amplifier for a combination a.m./f.m. receiver is shown in Fig. 1. As can be seen, system switching takes place at intermediate and audio frequency. Great care must be taken with the layout of the switch wiring, and particularly the relative positions of the grid and anode wires. German designers tend to use a slider switch which runs almost the whole length of the chassis in some cases. This enables the switching of each stage to be carried out as close to the valve as

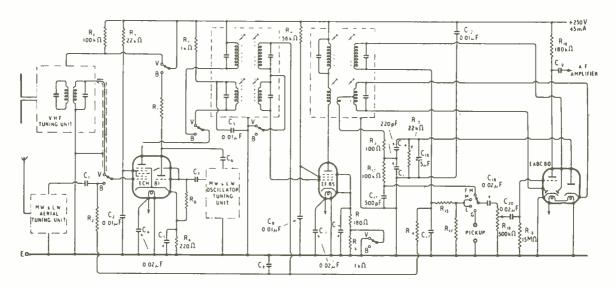


Fig. 1. Circut diagram of i.f. amplifier and detectors for combination a.m./f.m. receiver. "V" indicates switch position for f.m. reception and "B" that for medium- and long-wave reception.

possible. This type of switching is facilitated in German receivers by the fact that only a two-position switch is necessary. British receivers will be complicated by the necessity for incorporating a long waveband. Nevertheless, a similar arrangement will probably be necessary for switching the ECH81 anode and the EF85 grid and cathode. Care must also be taken with the output lead of the v.h.f. unit. It may not always be possible to place the output connections of the unit close to the switch, and if the connecting lead is more than an inch or two long it must be screened. Low-capacitance screened lead should be used and the i.f. transformer secondary tuning capacitance reduced accordingly.

The necessity for switching the ECH81 anode and the EF85 grid may not at first be clear. The reason for switching the ECH81 anode is that many frequencies are present at the anode of a mixer, and the presence of two circuits tuned to different frequencies in the output could cause undesirable effects. One obvious one is the possibility of unwanted signals passing through the wrong channel and reaching the audio section through leakage across the switch. The switch in the EF85 grid circuit is intended primarily to short-circuit the a.g.c. line when using the higher i.f. in order to prevent stray coupling between the i.f. stages. It incidentally performs the additional function of short-circuiting the secondary of the first 470-kc/s i.f. transformer which results in slightly improved v.h.f. sensitivity.

The reason for  $R_1$  may also appear obscure. It is included in order to comply with the valve manufacturer's requirements which do not tolerate operating high-slope valves with their heaters on but with no high tension. Nevertheless, it is desirable to stop the v.h.f. unit operating when the receiver is being used for broadcast reception, and  $R_1$  covers both requirements by reducing the h.t. to some 20 volts.

The f.m. discriminator is a ratio detector of the unbalanced variety; R<sub>13</sub> is the load and C<sub>16</sub> the stabilizing capacitor. R<sub>12</sub> and C<sub>13</sub> form the de-emphasis circuit. It will be noticed that grid current biasing is used with the EABC80 triode. This is preferable because it enables the cathode to be taken directly to chassis potential. As this cathode is common to one of the ratio detector diodes, this circuit reduces the possibility of unbalance in the detector. It incidentally shows a slight saving in cost over the cathode biasing arrangement. The distortion introduced by this stage is remarkably low and no fears need be felt on this score.

F.M. Detector.—There are many forms of f.m. detector, most of which are only of academic interest to domestic receiver designers as they are either very inefficient, or they require additional valves to act as limiters. Information on these can be obtained from the literature and it is proposed to confine this section to a discussion of two types only.

Until 1947, limiting in f.m. receivers was nearly always provided by two saturated amplifiers preceding the discriminator. That tended to make these receivers rather expensive. It would not be far from the truth to state that if a simpler solution to the limiting problem had not been found, f.m. broadcasting on a large scale would have been made impossible through the lack of listeners. Combination receivers are expensive enough without the additional cost of two extra stages! In fact, two solutions were found; the nonode valve and the ratio detector.

The nonode valve, designated EQ80 in this country,

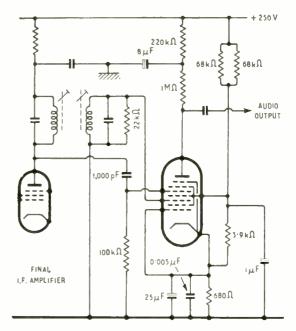


Fig. 2. Typical circuit of a nonode f.m. detector.

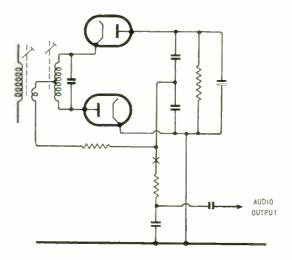


Fig. 3. Circuit diagram of ratio detector.

is a "gating" valve. Two voltages having a phase angle between them of 90 deg are applied to the third and fifth grids. The voltages at the first and second grids are held constant and anode current can only flow when both the third and fifth grids are positive. As in a pentode, if the first and second grid voltages are held constant, the electron current is likewise constant. Therefore, in the nonode valve any change in anode current will be solely a function of the phase difference of the voltages at the third and fifth grids. If this phase difference is made to vary in accordance with an f.m. signal, the valve will convert changes in frequency to changes in amplitude, and the valve will become an f.m. demodulator. As the electron current is constant, the valve will not respond to changes in amplitude of the input signal and limiting is therefore automatic. There is, however, one serious drawback. For efficient limiting, over 11 volts peak is required at grids 3 and 5, and as the phase difference is usually obtained by means of a transformer, something of the order of 23 volts peak must be provided across the primary. Needless to say, at the intermediate frequencies generally used in f.m. receivers this is difficult to obtain, and the saving on the conventional phase detector with two limiters is probably one valve. Nevertheless, once limiting does take place, the results are excellent. A typical circuit is shown in Fig. 2.

It is not proposed to go into any detailed description of the operation of the ratio detector, as this has been dealt with elsewhere<sup>2</sup>. The circuit is shown in Fig. 3. As can be seen, it bears a resemblance to the conventional phase detector but with two major differences. The diodes here are connected in series and the resultant voltage developed across the load resistance is stabilized by means of a large capacitor. This capacitor holds the amplitude constant and limiting is therefore automatic. Satisfactory limiting can be obtained with about 6 volts input. As the loading is heavy, a form of matching is used between the primary and secondary of the discriminator transformer. Possibly the most important factor in the design of the ratio detector is what the designers have termed the S/P ratio; that is, the ratio of secondary to primary voltage. On this depends whether the detector will limit satisfactorily, if at all. After all other parameters have been fixed, the S/P ratio becomes a function of the coupling between the primary and the secondary, and therefore between the primary and the tertiary.

An easy method of adjusting the coupling is during alignment. A d.c. meter (low loading) is placed across the stabilizing capacitor and an unmodulated signal is injected into the receiver. All i.f. circuits except the secondary of the discriminator transformer are adjusted for maximum d.c. output. The meter is then transferred to the audio take-off point (point X in Fig. 3) and the secondary of the discriminator transformer is adjusted to give a d.c. voltage half of that which was obtained across the stabilizing capacitor. The primary may then require a slight re-adjustment after which the secondary setting should be checked. This process should be repeated until no further adjustment is necessary. The signal is then amplitude modulated and the point of maximum limiting should occur within about 10 kc/s of the alignment frequency. If it does not, the position of the tertiary winding should be adjusted with relation to the primary. The alignment process must then be repeated. The whole process must be repeated as often as is necessary until the point of minimum a.m. response does fall within about 10 kc/s of the alignment frequency. If it does not occur anywhere within the permissible range of adjustment of the tertiary winding (that is, between the top and bottom of the primary winding) the transformer has been incorrectly designed. It will be noted that it is not absolutely necessary to use an f.m. signal generator to align this detector. The need for such a generator will only arise if some obscure fault

The ratio detector has enjoyed great popularity both in America and in Germany, and will no doubt become just as popular here. It is simple, reasonably sensitive, and f.m./a.m. ratios of 40 db and more can be obtained in practice with quite low inputs. It has another advantage in that the sideband responses are small and it tends to limit even on random noise. The result of this is extraordinarily low interstation

develops, or for more involved tests.

noise. This is a great advantage in domestic receivers as it is doubtful whether most people would appreciate the colossal din, common with receivers using other types of detector, that occurs when tuning from one station to another.

Intermediate Frequency.—The choice of an intermediate frequency is, as usual, a difficult one. The designers of the ratio detector chose 10.7 Mc/s as being the highest frequency that would give a reasonably high gain per stage. Unfortunately, this frequency has the drawback of causing the fundamental oscillator frequency to fall in Band II, and the second harmonic to fall in the middle of Band III. In spite of this, 10.7 Mc/s has virtually become standard in both America and Germany.

The same considerations hold good for this country. Although initially an i.f. of 10.7 Mc/s may not cause the oscillator to interfere with broadcast reception in Band II, it will almost certainly affect the public services operating in Band II and to the commercial television services in Band III. It is highly debatable whether radiation in mass-production receivers can be kept within the limits laid down by B.R.E.M.A. The radiation problem is further complicated in f.m. receivers by the fact that the majority will not be used with a matched aerial. The piece of wire that will probably stand proxy for an aerial will almost certainly increase the nuisance value of the receiver. For this reason it is suggested that the oscillator voltage at the aerial socket should be measured without the usual terminating resistance.

Any frequency above 12.5 Mc/s will keep the oscillator out of Band II, but to keep its second harmonic out of Band III requires an i.f. above 20 Mc/s. For the same stability margin this frequency will only give half the gain per stage that can be obtained with 10.7 Mc/s. Even so, the sensitivity of the receiver should be adequate, and the higher frequency has advantages to offer. It will give increased protection from spurious responses; an important point when it is remembered that television stations in Band III could cause interference due to the oscillator second Another advantage is that the farther harmonic. removed the signal frequency is from the oscillator, the greater will be the protection against radiation given by the signal-tuned circuits. A minor advantage is that it makes the design of a receiver with a pre-set tuned r.f. stage easier by keeping the oscillator frequency well away from the centre of the band.

The Pseudo F.M. Receiver.—It will have become quite clear by now that combination f.m./a.m. receivers are going to be somewhat more expensive than the standard 4+1 domestic receiver we have been used to. In the circumstances, it was only to be expected that attempts would be made to produce something considerably cheaper—if only for use in high signal strength areas. It is well known that f.m. signals can be received on an a.m. receiver by the simple expedient of tuning down the slope of the selectivity characteristic3. This is often referred to as slope-detection. This form of detection has many drawbacks. It is very inefficient, it provides no limiting, and it gives two tuning points for each station. The use of it is only justified by its simplicity and cheapness.

A receiver using a slope-detector for f.m. reception has been produced in Germany; the circuit is shown in Fig. 4. It can be seen that the receiver consists of three valves plus rectifier. The first valve is a v.h.f. triode (EC92) used as a self-oscillating mixer

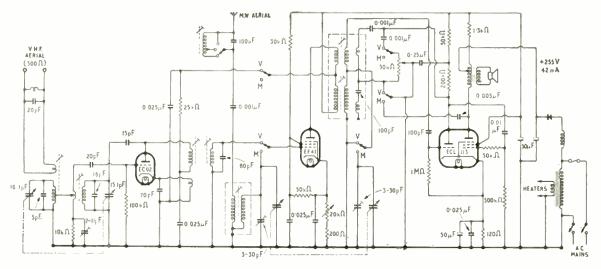


Fig. 4. Circuit diagram of German Grundig f.m. a.m. receiver, Model No. 810, showing use of slope-detector for f.m. demodulation. "V" indicates switch position for v.h.f. and "M" that for medium-wave reception.

on v.h.f. only. It incidentally illustrates the typical way in which this valve is used. The second valve (EF41) does service as an i.f. amplifier on v.h.f. and an r.f. amplifier on medium waves. The final valve (ECL113) is a triode-pentode, the triode section acting as a leaky-grid detector on both bands, the pentode being the audio output valve. Volume is controlled by a variable resistance in the cathode of the EF41, and a potentiometer in the anode circuit of the detector provides a reaction control on medium waves and a tone control on f.m. Whether for f.m. or a.m. reception, this receiver is only suitable for use in high field strength areas, and it is not known what success it has had.

This receiver has no r.f. stage, nor does it provide any form of limiting. As far as this country is concerned, such a circuit might conceivably fill a temporary need as a converter, but as a receiver it should surely be rejected. Quite apart from the ethics of the case, it is doubtful whether such a receiver would be capable of any better performance on f.m. than the standard broadcast receiver gives on medium and long waves.

Audio Amplifier.—The B.B.C. has stated that it is introducing v.h.f. broadcasting, "not as a complete substitute for long and medium wavelengths but as a powerful reinforcement of the sound services." We may therefore take it that fidelity will only be a secondary consideration. Taking into account the high-frequency attenuation of land-lines and the frequency response of studio equipment, it will only be on rare occasions that full advantage will be taken of the upper modulation frequency limit of 15 kc/s. This, however, need not make us downcast, as reception in many places will be considerably better than that which is obtainable on medium and long waves. It is suggested that in combination receivers the distortion level should not be higher than 2 per cent at the maximum rated output, and should preferably be of the order of 1 per cent. To attain these figures will require a substantial amount of negative feedback with a consequent reduction in amplification. The amount of feedback that has to be used may be so great as to reduce the sensitivity of the receiver to a level which is below that required. In this case, it may be thought

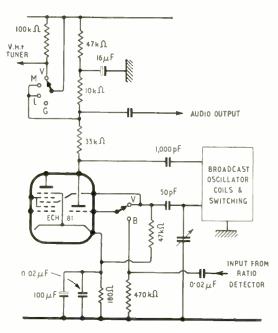


Fig. 5. Circuit diagram showing the method by which the triode section of the ECH81 can be used as an audio amplifier on v.h.f. without detriment to its function as an oscillator on medium and long waves.

worth while to use the otherwise idle triode in the ECH81 as an extra audio amplifier on v.h.f. The method by which this may be done is shown in Fig. 5. Hum is the greatest problem here, and extra smoothing must be used in the anode supply. Even then, full use of the valve cannot be made, and it will be noticed that only one-quarter of the anode load is used. This keeps the hum level low and enables the stage to give a useful power gain of over six times.

Results.—Three receivers comprising an EF80 preset tuned r.f. stage, EF80 self-oscillating mixer, ECH81 i.f. and a.f. amplifiers, EF85 i.f. amplifier, EABC80 ratio detector and a.f. amplifier, EL85 power

amplifier and EZ80 mains rectifier, used in a similar manner to that described in this article, had sensitivities of 3, 4 and 9  $\mu$ V respectively, and f.m./a.m. ratios of between 36 and 40 db at these signal levels. The intermediate frequency was 19.5 Mc/s. Bass boost at 80 c/s was between 4 and 5 db with reference to 400 c/s, and the frequency response with preemphasis was level up to 8 kc/s. Overall distortion at 1.5 watts output was in the region of 2 per cent.

Conclusions.—It was mentioned in the "Second Report of the Television Advisory Committee, 1952," that the additional cost of incorporating v.h.f. in new receivers will be of the order of 30 per cent. It was also stated that the additional cost would be greater unless the receivers were mass-produced. Whether these receivers can be produced on anything like the scale of the 4+1 receiver will depend on two factors. The first is the speed with which the B.B.C. are able to erect the stations, and the second is whether the ordinary man-in-the-street is going to think it worth while to spend that extra 30 per cent on his receiver. If demand is great enough, we may be well on the way to building up a thriving industry in a.m./f.m. receivers. In this case, it may be possible to reduce the 30 per cent substantially, and that will justify all the arguments that have been made in favour of f.m. broadcasting.

#### References

Russell, G. H., "Band III Convertor," Wireless World, Vol. 60, No. 5, May, 1954, p. 211.

Seeley, S. W., Avins, J., "The Ratio Detector," RCA Review, June, 1947.

Sturley, K. R., "Radio Receiver Design," Part II, Chapman and Hall, 1947, p. 335.

# Colour Television Tests

FRANKLIN

IF any television experimenters in London happened to have their sets running after programme hours during July they may have been lucky enough to see some strange things on the screen. The things in question, which I saw quite by chance on my receiver, were orderly patterns of white dots on a synchronized, but otherwise blank, raster. Sometimes the patterns had a bar or several bars across them and at other times they were quite plain.

Having been following developments in colour television pretty closely, I realized immediately that the B.B.C. were transmitting a sub-carrier frequency on the main 45-Mc/s carrier wave from Alexandra Palace—a sub-carrier such as would be used for conveying colour information in a compatible colour television system of the N.T.S.C. type. As is generally known, this sub-carrier in the N.T.S.C. system enables the colour information to be transmitted within the same video band as the monochrome signal, and its frequency is chosen so that the colour sidebands are interleaved between the monochrome sidebands.

The great problem which British television people seem to be faced with at the moment is whether or not we can adapt the N.T.S.C. type of colour system to our existing 405-line standards. And this depends to some extent on whether the system is compatible enough. In short, is the presence of a sub-carrier and its resultant pattern on the screen going to cause too much deterioration of our pictures? I imagine that the B.B.C. were attempting to answer this question by arranging a series of test transmissions of a sub-carrier signal so that observations could be made on typical receivers. An interesting problem here is: what is the best frequency for the sub-carrier?

In the June issue of Wireless World a report was given of a British version of the N.T.S.C. colour television system developed by Marconi's, and in this the sub-carrier used was approximately 2.66 Mc/s. I therefore assumed that the B.B.C. were transmitting something comparable with this. Tests with an absorption wavemeter, however, showed the frequency to be more like 2.8 Mc/s, or perhaps slightly under. This higher frequency, of course, would give a finer and less visible dot pattern on the screen than in the Marconi system, and I personally found that I could not see the dots when I moved to a distance of about 4-5 feet from the screen.

On the other hand, the higher the sub-carrier frequency the more likely is the colour signal to interfere with the sound channel of the system. I presume that the bars I saw on the screen were a form of modulation on the sub-carrier to test for this effect (probably square-wave modulation). There was, in fact, a perceptible low-frequency noise in the loudspeaker when these bars appeared, but it did not strike me as being particularly obtrusive. No doubt the amount of this interference would vary with different receivers.

Presumably some organized observations were made on these test transmissions, apart from the clandestine ones such as my own, and it will be interesting to see the results when they are eventually published.



Colour television camera used with the Marconi system referred to in the article. It has only two pick-up tubes (one for high-definition monochrome information and the other for low-definition colour) and is notable for its small size.

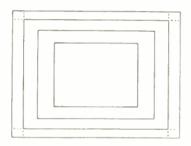
#### LETTERS TO THE EDITOR

The Editor does not necessarily endorse the opinions expressed by his correspondents

#### "Why Lines?"

THE "Lissajous" scanning system proposed by F. P. Hughes (your August issue), if it earns full marks for originality surely merits none for practicability.

If one inscribes three similar and symmetrical rectangles within the screen so that the smallest is one quarter of the whole screen area, and the area between each rectangle and the next larger is also one quarter of screen area, it is clear that with B.B.C. standards the spot will be in each of the four equal areas for approximately 22 per cent of total transmission time, the remainder being lost to synchronizing pulses, etc. With "Lissajous" scanning the spot will be 11 per cent of transmission time in the central area, 14 per cent in the next area as one moves outward, 19 per cent in the next and 56 per cent in the outmost fringe. Moreover the spot will take as long in total to scan the four small rectangles in the corners (comprising together 1.8 per cent of screen area) as it does to scan the important centre area. In fact the transmission time wasted on the edges and corners of the picture will be very much greater than that "wasted" in sync. pulses in conventional systems and definition in the important central area will be equivalent to a 30 per cent cut in line number and 50 per cent in bandwidth as compared with the conventional.



Even more serious would be the consequences of the timebase waveform departing in the slightest degree from purity. As the screen is being scanned equally from left to right and from right to left any phase drift will shift half the picture elements one way and the other half in the opposite direction. At screen centre a drift of 0.001 c/s will cause the picture elements to separate by approximately 0.006 of the total picture width, giving a "defocus" effect equivalent to complete loss of the onemegacycle bands on the test card. Similar loss of definition, but varying in complex fashion from place to place on the screen, would result from 0.6 per cent of total harmonic distortion. As these results would be additive on some parts of the screen, it would probably be necessary to specify tolerances of not more than 0.0002 c/s max. phase drift and 0.1 per cent total harmonic distortion for the timebase oscillators. Such a specification is probably not unattainable, but the cost and complication would obviously be prohibitive.

Teddington, Middx. S. HOSKING TAYLER.

#### Why A.G.C.?

I SEE from p. 40 of the August issue that "Diallist" proposes to build a modified version of my midget sensitive t.r.f. receiver (described in the April issue) without a.g.c. A.G.C., he maintains, is unnecessary because the receiver is intended only for reception of local stations which, in his locality, are free of fading. Surely "Diallist" isn't under the impression that a.g.c. is used only to combat fading? It has another merit, equally important; namely, that it ensures equal volume from all signals. This fully justifies its inclusion in a local-station receiver. "Diallist" is indeed fortunate if all his local transmissions are of equal strength and, if they are not, he will need to reset the volume control after each tuning adjustment. The inclusion of a.g.c. avoids this, making operation easier and prolonging the life of the volume control potentiometer.

Although it may not apply in this particular case, a.g.c. is sometimes used to avoid the application of large signals to the detector. Such protection may be necessary if the detector overloads easily (as anode bend detectors do) or if the detector may be damaged by large signals (as

some crystals are).

I. L. OSBOURNE.

#### Ionic or Iontic?

PEOPLE speaking languages of Anglo-Saxon or Latin origin employ, generally successfully, a great number of technical and scientific terms derived from the Greek. Occasionally, though, in the process of adaptation, there

is a regrettable loss of clarity and precision.

An example of successful use is the word ion, which is the neuter present participle of a Greek verb meaning go." But non-Greek technologists, in coining derivatives and compounds of this useful word, have introduced error and confusion. Ionic order (architectural), Ionic school (philosophic), etc., refer to the ancient Greek land Ionia. Ionic is a synonym of Ionian; therefore, ionic bombard-ment might (and should, by the rules of language) refer, say, to a naval action off the Ionian Islands! The mythological Greek priestess Io ('I\omega'), sweetheart of Zeus, who gave her name to these islands, bore no relation whatever to the electrically charged atoms, molecules or radicals in which the radio engineer is interested. She also had nothing to do with the new radio-active isotope ionium.

To avoid confusion, derivatives of ion should be formed from the genitive ionios (iorros which gives us the root ioni-, or sometimes, for the sake of euphony, ionio-.

The correct practice has already been adopted by the medical profession in the word iontophoresis (introduction of ions into human tissues). Radio technologists and physicists should, I suggest, follow suit by changing, for example, ionize into ionize, ionosphere into ioniosphere, ionium into iontium, etc.

DIONYSIUS J. BATAIMIS. Hellenic National Broadcasting Institute,

Athens.

#### Electronics and Automation

IN your report on a debate at the Brit, I.R.E. Convention ("Industrial Electronics," Wireless World, August, 1954, p. 358) you mention a discussion on the possibilities of flexible machines which could be programmed for different tasks as required: these would in fact be something like the original concept of a Robot; i.e., a mechanical substitute for a human being. One attempt to mechanize a production process in terms of "replacing human labour" has convinced me that this is a wrong approach. Human labour is very flexible and fairly cheap (especially if female) and a machine to carry out precisely an adjustment such as tuning a circuit to resonance, which at present is done by hand, is prohibitively complex. Not least of the difficulties is that of making the robot connect automatically with the appropriate part of different models of equipment.

The future of "automation" (factory production with the minimum of labour) lies mainly in the development of appropriate manufacturing techniques, such as printed circuitry in radio and electronics, and the pressed-steel body in place of the coach-built body in the automobile

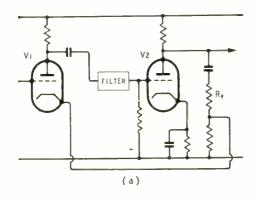
industry. The future of industrial electronics lies in doing things which the average human operator cannot do successfully. This applies particularly to fast-moving flow production; e.g., colour printing, textile manufacture, continuous steel strip mills, but it is also beginning to find application in precision machine tools. Whenever the quickness of the machine deceives the eye, or the potential accuracy of the machine is greater than that of human hand and eye, there may be an essential job for electronics.

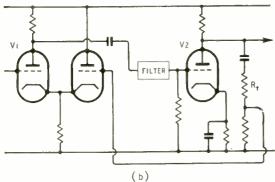
Birmingham.

D. A. BELL.

#### Feedback Circuits

THE well-known feedback circuit (diagram (a)) is fully discussed in "Radio Designer's Handbook," p. 334. However, one soon finds out when trying to apply the circuit that either the anode load of V<sub>2</sub> becomes inordinately low or that the cathode load of V<sub>1</sub> becomes inordinately high with anything more than a small feed-





back ratio. These snags disappear when the feedback is applied to the grid of a cathode follower which is direct coupled to V, (diagram (b)). It is possible to vary the feedback between wide limits without upsetting the work-

ing characteristics of either  $V_1$  or  $V_2$ .

I am using this circuit in a pre-amplifier with a parallel-T whistle filter between  $V_1$  and  $V_2$ . Coupled to a Baxandall tone control (Wireless World, Oct. 1952) the whole arrangement works very well, is silent, stable and, judged by ear, of high fidelity.

It is possible that this circuit may be discussed somewhere in the literature and if one of your readers could enlighten me I would be grateful.

Burgess Hill, Sussex.

A. V. SLATER.

#### Vector Diagram Conventions

IN his July article, "Cathode Ray" has advocated that certain conventions should be adopted to ensure that there should be only one correct voltage vector diagram

to correspond to any given circuit diagram. The suggested conventions involve the addition and placing of vectors in an order uniquely determined by the circuit configuration. The conventions thus imply a slight restriction on the commutative law of addition of vectors, and also on the usual understanding of a graphical vector as having length and direction but no defined position.

In my view, although it is desirable in every problem to establish a defined relationship between the sign convention for the circuit diagram and the sign convention for the vector diagram, it is undesirable to extend this

to "a perfect tie-up between circuit and vector diagrams" in the rigid one-to-one manner that has been advocated by "Cathode Ray."

"Cathode Ray" has invited his readers to point out any flaw in the system which might account for its lack of general acceptance since it was first proposed in 1951. It is possible that this may reside in the restriction to which the diagrams are subject when an attempt is made to develop them into vector loci. For example, with reference to Fig. 14 of the July article, and considering a constant current condition, diagram (a) would provide the most convenient basis for a locus to illustrate the variation of E and V with variation of oL, R, and R. being constant. On the other hand, diagram (b) would be more convenient if R<sub>2</sub> were to be varied with R<sub>1</sub> and wL held constant, while diagram (c) would be more convenient if R1 were to be varied with R2 and oL held constant. To justify these alternative forms of vector diagram, "Cathode Ray" would have to redraw his circuit diagram to match each case, thus attributing undue importance to the cyclic order of the components in a circuit in which the only really significant fact is that the components are connected in series.

Bangor, N. Wales. DAVID MORRIS.

### FURTHER EDUCATION

#### Radio Courses Available

IF the proposal put forward by the Parliamentary and Scientific Committee in a memorandum on higher technological education\* is adopted, some twenty of the existing technical colleges will be granted charters and become Royal Chartered Colleges of Technology, with the right to award degrees in technology. They would provide for advanced full-time "sandwich" and part-time day and evening courses, post-graduate courses and full-time and part-time research.

These are, of course, purely recommendations. Facilities for further technological education do already exist even if some of them are inadequate. We have secured from the Ministry of Education a list of further education establishments providing classes in radio and allied subjects. The term "further education," by the way, is used for establishments providing classes for those whose whole-

time formal education has ended.

On the opposite page is tabulated some 150 further education establishments in England† (grouped under counties) providing courses in telecommunications (col. A), radio theory, transmission and marine wireless (B), radio servicing (C), and television servicing (D). The letters used in these columns indicate full-time courses (F), parttime day courses (P) and evening courses (E).

<sup>\* &</sup>quot;Memorandum on Higher Technological Education," Parliamentary & Scientific Committee, 31, Palace Street, London, S.W.1, price 2s.

<sup>†</sup> It is hoped to give similar details for Scotland and Wales next

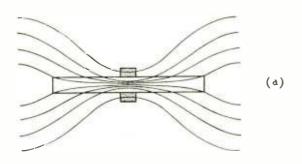
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Reading T.C.	PE				Hendon I.C PI	E		
Buckinghamshire Bletchley E.I.	Е			1	Holborn, Kingsway Day College P	.		
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Colchester, Ardleigh House C.F.E.					Oxford C.T E	P		
., N.E. Essex T.C Dagenham, S.E. Essex T.C		E	E		Shropshire			
Southend-on-Sea Mun. T.C		E P	PE	E	Bridgenorth E.I E Oswestry T.I P			
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Beckenham T.I			-		Mitcham E.I.			
Dartford T.C		E	E		Richmond T.I.		PE	
Dover T.C	. E		-		Weybridge, Brooklands T.C.		E	
Faversham E.I		E			Sussex		-	
Gillingham, Medway T.C	PE		PΕ		Brighton Mun. T.C PE	PE		
Gravesend T.C			E		Crowborough E.I E	PE		
Ramsgate, Thanet T.C Funbridge Wells, W. Kent T.C	. E					E		
incashire	PE				Warwickshire Birmingham, Bournville Day College P			
olackburn Mun. T.C		E	PE	E	Bournville & Northfield T.L			E
Blackpool T.C	. PE	-	E	-	,, C.T PE	E	PE	E
Bolton Mun. T.C			PE		Coventry T.C p	Ē	-	_
Lancaster & Morecambe C.F.E					Westmorland Kendal, Allen T.I E			
Liverpool C.T	. E	E			Wiltshire			
Old Swan T.I				_	Chippenham, N.W. Wilts. C.F.E E	E	E	
, Riversdale T.C	1 1		PE	E	Malmesbury F.E. Inst E Salisbury & S. Wilts. C.F.E		_	
Manchester, Openshaw T.C			PΕ	E	Worcestershire		E	
Oldham, Mun. T.C			PE		Bromsgrove Tech. School	E		
Preston, Harris Inst		E	E	Е	Worcester, Victoria Inst E			
Stretford, Metrovick School		Р	E	E	Yorkshire Barnsley Mining & T.C			
Wigan & Dist. Mining & T.C		E			Bradford, Hanson T.I P	E	E	
icestershire					, T.C PE	E	E	Е
Leicester C.T		E	PE	PE	Doncaster T.C E	E	P	
maiton mowbray I.C	-				Huddersfield T.C P Kingston-upon-Hull Mun. T.C P E	E	PE	E
Gran ham T.C	E				Kingston-upon-Hull Mun. T.C P E Leeds C.T E	FE	E	Е
Grimsby C.F.E			P_E		Middlesbrough, Constantine T.C P F	E		-
Lincoln T.C ndon			Е	E	Rotherham T.C		Р	
Acton T.C		PE	Е		Scarborough T.I E Sheffield C.T PE	E		
Battersea Polytechnic	E	_	-		University	E		
Dep. ford, S.E. London Day College	P			. 1	York T.C P E			

C.T. College of Technology; T.C. Technical College; T.I. Technical Institute; E.I. Evening Institute; C.F.E. College of Further Edutation

# Ferrite Rod Aerials

Underlying Principles and Basic Design Formulæ

By W. A. EVERDEN, \* G.I.Mech.E.



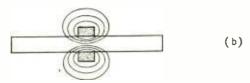


Fig. 1. The effective permeability  $\tilde{\mu}$  of the rod to an external field (a), must be distinguished from the permeability  $\mu_c$  relative to the coil (b).

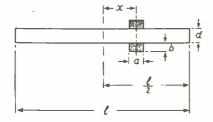


Fig. 2. Relevant physical dimensions of an aerial rod and coil.

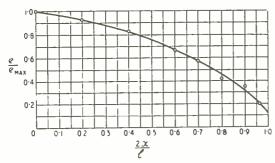


Fig. 3. Distribution of e.m.f. (e/ $e_{max}$ ) induced in a coil as a function of its distance 2x/l from the midpoint of an aerial rod.

W ITH the introduction of the nickel-zinc grades of Ferroxcube with their high material permeabilities and low losses many new fields of application have been opened up. Not the least important of these is the replacement of bulky frame aerials by relatively small rods and coils. All aerial rod designs in this article are based on Ferroxcube rods in grade B2, which has an initial permeability of approximately 200 and a resistivity of  $10^5$  ohm-cm. Its loss factor  $\tan \delta/\mu$  at 0.5 Mc/s being  $90 \times 10^{-6}$ .

It should not be assumed that rod aerials, as they have come to be known, can only replace frames or indoor systems; with a rod of larger proportions than those discussed in this article, a signal voltage comparable with that of an outdoor aerial in combination with a normal input circuit can be approached. Interference which is now so prevalent all over the long and medium wavebands can often be reduced by the directional effect inherent in these assemblies.

Although the advantages of such a system are immediately evident, the design of a suitable assembly is rather complex, due mainly to the lack of practical design data on open-ended coils. An attempt will be made in this article to combine all necessary data on this form of aerial into workable formulæ, and to present examples of the manner in which ferrites can be used in practical aerial systems.

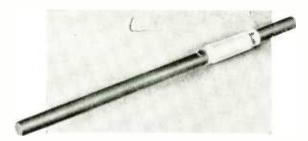
Before analysing the physical properties of rod aerials it may be worth while to discuss the relative merits of inductive and capacitive aerials, as the basis of comparison may not be immediately obvious.

#### Inductive and Capacitive Aerials

The efficiency of any type of aerial is usually judged from the voltage delivered to the grid of the first valve. With an average domestic aerial of dimensions under a half wavelength, used in conjunction with a matching transformer, the voltage is proportional to the product of the field intensity (vectorially) in volts per metre, the effective height (h) in metres and the transformer ratio (N).

With inductive aerials, including rod aerials, the voltage at the first grid is mainly determined by the product of the effective height (h) and the aerial circuit quality factor (Q). No direct comparison should be made between these two types of aerial. However, a comparison can be made between the products of effective height (h) and transformer ratio (N) of the capacitive aerial against the effective height and quality factor Q of the latter.

Mullard. Ltd. (Components Division).



Experimental ferrite rod aerial for frequencies of the order of 1 Mc/s.

#### Basic Design Data

**Frame Aerials.**—At the input to any aerial the field concentration and frequency of the transmitter signal are usually known. A loop of *n* turns enclosing a part of the radiated field will then have induced in it an e.m.f. of

$$e_1 - \phi \omega n.10^{-8}$$
 .. .. (1)  
= Ba  $\omega n.10^{-8}$  volts .. .. (2)

where the cross-sectional area of the loop is a sq. cm., the flux  $\phi = Ba$  and the flux density B is in gauss.

If Q is the input circuit quality factor, then the voltage becomes  $e_1Q$ , denoted  $e_0$ , and is applied to the grid of the first valve. Therefore

 $e_0 = \mathrm{QB} a \, \omega n.10^{-8} \, \mathrm{volts}$  . . . . . . (3) **Rod Aerials.**—The main purpose of a high-permeability ferromagnetic core is to increase the flux density B within the closed loop. For satisfactory operation this should take the form of a rod so that the flux may be concentrated within the turns of the coil (Fig. 1(a)).

By redesigning the aerial coil and inserting a ferromagnetic core, the effective permeability of the enclosed medium to an external field is increased. This effective permeability  $\mu'$  is much lower and should not be confused with the initial permeability  $\mu_0$  of the core material as measured in a closed magnetic circuit. The output voltage now becomes:

 $e_0 = \mu' \text{QBa} \, \omega n. 10^{-8} \, \text{volts}$  . . . . . . (4) The calculations of  $\mu'$  will not be dealt with here, as it is fully covered in the literature<sup>1</sup>; it is only necessary to say that  $\mu'$  can never exceed  $\mu_0$ , and depends mainly upon the physical dimensions of the core. This can be seen from Fig. (5).

It has often been argued that a flat plate of ferromagnetic material would be more suitable for this application than a small-diameter rod, but experiments leading to the computing of Fig. 5 have shown that the flux density inside a plate at right angles to the magnetizing field differs very little from that of the magnetizing field. This can be shown if we take a plate of Ferroxcube with an initial permeability of 200 and dimensions l=114 mm, d=6.3 nm. The  $l_ld$  ratio then becomes 0.055 and from Fig. 5 we obtain an effective permeability  $\mu'$ , which is for practical purposes unity.

With the introduction of a ferromagnetic core, the aerial system becomes considerably modified. So far we have been considering it primarily in relation to the external field, but it is also part of a tuned circuit and must have a specific value of inductance L. From this it should be evident that the increased permeability

necessarily involves a reduction in both a and n, and therefore equation (4) must be developed, to contain L as a parameter. It is thus obvious that the physical size of the coil may be reduced to one not very much larger than that of the core. With the introduction of any ferromagnetic core, the inductance L increases by a factor  $L_c/L_a$ , where  $L_c$  is the inductance with ferromagnetic core and  $L_a$  is the inductance with an air core. This is often termed the coil permeability  $\mu_c$  and differs considerably from  $\mu'$  (see Fig. 1).

At this stage all coils will be shown diagrammatically as being short pile-wound coils. The designing of the most efficient coil will be dealt with later. The inductance of an air-cored coil of the form shown in Fig. 2 is given by the following formulæ:

$$L = n^2 d\phi \cdot 10^{-8} \text{ henrys}$$
 .. (5)

where  $\phi$  is a constant which depends on the dimensional ratios a/d and b/d of the coil.

The ratio of the external and internal reluctance paths of an air-cored coil mainly determines this value of inductance. It can be assumed that this ratio of reluctance within the coil to that outside the coil is 10:1. Thus approximately 1/11th of the circuit reluctance is outside the coil. For a coil where a ferromagnetic core is introduced the reluctance of the magnetic path inside the coil can be neglected compared with the external path.

If we now continue the assumption given above it is evident that the inductance ratio of a coil with a

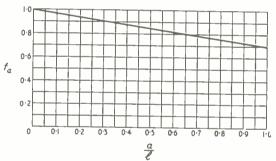


Fig. 4. Ratio of mean to maximum flux density  $(f_a)$  as a function of coil length relative to the length of the core.

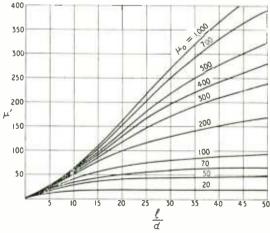


Fig. 5. Effective permeability of rod in an external field as a function of the ratio I d with initial permeability as a barameter.

<sup>&</sup>lt;sup>1</sup> See for example "Demagnetizing Factors of Rods" by R. M. Bozorth and D. M. Chapin, J. Appl. Phys., Vol. 13, p. 321, 1942.

ferromagnetic core to that of an air-cored coil will be

approximately 11:1.

It can be shown that for a short-section coil of the type shown in Fig. 2 the effective coil permeability  $\mu_c$ is usually between 5 and 15. With a ferromagnetic core the inductance will be:

$$L = n^2 d\phi \mu_c . 10^{-8} \text{ henrys} \dots (6)$$

By substituting in equations (4) and (6) we obtain:

$$e_0 = QBa \omega \mu' \sqrt{\left(\frac{\bar{L}}{d\phi \mu_c}\right)}.10^{-4} \text{ volts}$$
 .. (7)

Equation (7) thus shows that a high value of output volts e<sub>0</sub> can be obtained by the optimum choice of the effective values  $\mu'$  and  $\mu_c$ . These factors can be controlled during the design stage.

Control of Rod Permeability.—If a ferromagnetic rod is placed in a uniform magnetic field B, the field is distorted towards the centre of the rod. The maximum flux density is at the centre and decreases towards the two ends. The rod permeability  $\mu'$  is of the ratio of maximum flux density with the rod in position, to that of the original field flux density B. For rods with large l/d ratios having reasonably high material permeabilities the flux distribution along the rod is almost parabolic. curve of Fig. 3 shows this effect in terms of the ratio of induced e.m.f.'s for a grade B2 Ferroxcube rod 200 mm long and 8 mm diameter. From this curve it can be seen that equation (4) only holds when the coil is placed at the centre of the rod, where the flux density is maximum. The ratio of the mean to maximum flux density has been termed the averaging factor  $f_a$  and a curve, derived from Fig. 3 by integration, showing the dependence of  $f_a$  on the relative length of coil and rod for a symmetrical arrangement is given in Fig. 4. For a very short coil,  $f_a = 1$  and for a coil surrounding the entire length of the rod it

Fig. 5 shows  $\mu'$  plotted as a function of the initial permeability  $\mu_0$  and the ratio l/d. To obtain a high value of effective permeability  $\mu'$  the ratio l/d and the initial permeability  $\mu_0$  must be high. As a first approximation,  $\mu'$  may be assumed proportional to the ratio l'd, say

$$\mu' = \alpha \frac{l}{d}$$
 .. .. (8)

From equations (7) and (8), and substituting  $a = \frac{\pi d^2}{4}$ 

$$e_0 = \mathrm{QB} \, \omega \, \alpha \, \frac{\pi l}{4} \sqrt{\frac{d \, \mathrm{L}}{\phi \, \mu_s}} . 10^{-4} \, \mathrm{volts} \quad \dots \qquad (9)$$

Circuit Quality Factor (Q).—The circuit quality factor Q is, of course, one of the main considerations. The reason for this is that an optimum Q value not only determines the output voltage  $e_0$  but also the circuit selectivity. It would seem that as high a Q as possible would be an advantage, but tests have shown that if a Q value greatly in excess of 200 at 1 Mc s is used, severe sideband cutting is experienced.

Influence of Q on Signal/Noise Ratio.—When calculating the effective Q of the circuit the effect of valve input impedance must not be overlooked. To account for this, our quality factor will now be denoted as Q'. The circuit quality factor Q' also has an influence upon the signal/noise ratio  $e_0/V_n$ .

It can be proved that a given noise voltage  $(V_n)$ does not in any way depend on the value of Q' but is

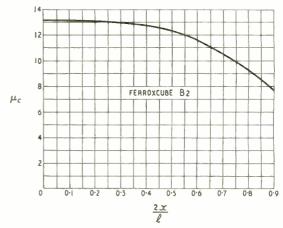


Fig. 6. Measured values of  $\mu_c$  plotted as a function of distance 2x/I from centre of rod.

directly proportional to the frequency. By looking at either equation (3) or (4) it can be seen that  $e_0$  is proportional to the frequency and quality factor, therefore  $e_0/V_n$  will not be subject to the frequency but will be proportional to the quality factor.

From this statement it can be seen that a high value of Q would be an advantage in respect of signal/noise

Temperature Coefficient.—The temperature coefficient of open-ended coils using Ferroxcube cores is a subject by itself and is extensively dealt with elsewhere.2 It should suffice to say that at normal ambient temperature the permeability of Ferroxcube has a small positive temperature coefficient which, in this type of application, produces a positive temperature coefficient of inductance of approximately  $0.4 \times 10^{-4}$  (°C.). This variation of inductance can in turn influence the shape of the tracking curve.

Mechanical Mounting.—Wherever possible the rod should be mounted above or to one side of the chassis so that the additional losses introduced due to the proximity of any metal-cased components are reduced to a minimum. In order to ensure optimum performance it is also advantageous to keep the length of the rod almost the same as that of the chassis, otherwise the latter will have a screening effect, thus lowering the obtainable grid voltage.

A general method of mounting is to extend small plastic brackets from the end of the chassis and insert the rod between rubber grommets so that any vibration or torsion that may be set up during transportation is absorbed. Tag boards and soldering lugs should be mounted away from the actual coil, otherwise a reduction of Q of as much as 20% at 1 Mc/s (299.8 metres) may result. This loss and any other which may be set up due to metal objects, is proportional to the square of the frequency.

Adjustment of Inductance.—Two methods of adjustment are now in general use, the more popular being to slide the coil along the rod until the required value of inductance is obtained. This will be found to be most critical as the centre line of rod is approached. The second method is that of removing or spacing of end turns, and is used where the coil is wound directly on the core.

Material Tolerances.-Mechanical tolerances on

<sup>&</sup>lt;sup>1</sup> Electronic Application Bulletin, Vol. 13, No. 6. Tolerances and temperature coefficient of coils with Ferroxcube slugs.

the dimensions of Ferroxcube B2 are  $\pm$  3% on diameter and  $\pm$  4% on length, and the value of initial permeability  $\mu_0$  is generally quoted on ring specimens as being > 200. The combined effect of these tolerances can cause a spread in  $\mu_c$  of  $\pm$  5% when measured with a given coil in a fixed position, e.g., in the middle of the rod. For most rods and an average coil the required inductance should be designed at a point where 2x/l = 0.45. Fig. 6 shows that for starting value 2x = 0.45 a displacement of the coil to a position where 2x'l = 0.2 or 0.6 will be sufficient to compensate for a spread in  $\mu_c$  of  $\pm$  5%. Effective Height.—The factor known as the

Effective Height.—The factor known as the effective height has already been discussed in so far as it affects the comparative merits of inductive and capacitive aerials. As already explained it is common to express the field intensity in volts metre and the performance of an aerial as the effective height.

The effective height of a loop aerial is usually expressed as:

$$h = \frac{2\pi An}{\lambda} \cdot 10^{-4} \text{ (metres)} \qquad . . \qquad (10)$$

where A is the mean area of the loop in cm<sup>2</sup> and  $\lambda$  is the wavelength in metres. If a ferromagnetic rod is now introduced having a permeability  $\mu'$  equation (10) becomes:

$$h = \frac{2\pi A \pi f_a \ \mu'}{\lambda} \cdot 10^{-4} \text{ (metres)} \qquad \dots \qquad \dots \qquad (11)$$

where  $f_a$  is derived from Fig. 4, A is the mean area of the coil in cm<sup>2</sup> and  $\lambda$  is the wavelength in metres.

**Coil Design.**—First let us decide what is going to be the main design parameter, i.e., maximum output voltage or a high value of Q. If a high value of  $e_0$  is aimed at, the Q value will more often than not be poor, and if a high Q value is the main requirement then the grid voltage may well be below avarage. Because most radio engineers are continually striving to achieve better selectivity we will consider first a design with a predetermined Q value.

Most of the information which has so far been published on this subject has treated the problem on the basis of a fixed frequency of 1 Mc/s. Experiments have shown us that the value of Q increases with the rod diameter, but from an economic standpoint the optimum value occurs at about 200-210 on a 5/16in diameter rod 8in long in Ferroxcube grade R2

If we take this value of Q as a general figure and design our coil around a rod 5/16in dia.  $\times$  8in long this will form a basis for all further designs. A coil whose length is relatively small has been chosen so

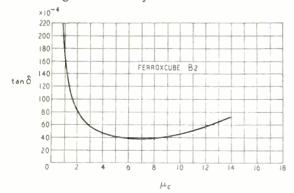


Fig. 7. Total losses plotted as a function of  $\mu_r$ .

that the value of temperature coefficient can be kept within reasonable limits. It will be found that due to the manufacturing tolerances essential with most ferrite materials, the coil will have to be moved toward one end of the rod to obtain the required value of Q. Assuming an inductance of 197  $\mu$ H for the medium-wave coil and a coil permeability of 13, the theoretical position of the coil from the centre line of the rod can be obtained from Fig. 6.

If we now take the reciprocal of our quality factor, i.e.,  $1/Q = \tan \delta = 50 \times 10^{-4}$  we see from Fig. 7 that this value of Q can be obtained with a coil permeability of 11. If this value of permeability is accepted the new position of the coil, with reference to the centre line of the rod can be found by referring to Fig. 6 to be 2x/l = 0.6.

The decrease in coil permeability must now be compensated for by an increase in the number of turns, in this particular case by multiplying by the ratio of 1:1.1 where it will be found that the required number of turns will increase from 27 to 30.

Due to the displacement of the coil, the flux distribution will decrease as shown in Fig. 3, for 2x/l = 0.6 the decrease of  $e/e_{max} = 0.68$ .

Converting physical dimensions into cm and taking  $n = 30, f_a = 1$  and  $\mu' = 117$ , the effective height is

$$h = \frac{2\pi \times 0.5 \times 30 \times 1 \times 117 \times 0.68}{299.8} \cdot 10^{-4}$$
= 0.0025 metre

The overall performance,  $hQ = 0.0025 \times 200 = 0.5$ . If this value is compared with that of the second design it will be found that the increase of Q was obtained at the expense of overall performance.

From laboratory tests it has been determined that short thick rods should be employed where exceptionally high values of Q are required, i.e. say 9/16in × 4in long. A typical design for a mediumand long-wave aerial coil utilizing the core stated above would be 50 turns of 9/40 litz wound approximately lin from one end, this forming the medium wave section with 120 turns of 9/40 litz wound on the opposite end and used in conjunction with the medium wave coil for the long wave reception. A multi-turn coupling coil is sometimes found to be necessary between the two windings, when coupling to an external aerial

With an assembly of these dimensions, and taking n = 50,  $t_a = 1$ ,  $\mu' = 40$  and  $e/e_{m.i.x} = 0.75$ , the effective height is

$$h = \frac{2\pi \times 1.54 \times 50 \times 1 \times 40 \times 0.75}{299.8} \cdot 10^{-4}$$
= 0.00484 metre

and the overall performance  $hQ = 0.00484 \times 250$  = 1.21 where a Q of 250 is applicable for this type of rod.

Let us now consider a design where the voltage applied to the grid of the first valve becomes a main consideration. This design is again based on the same Ferroxcube rod as the first example, i.e 5/16in dia. × 8in long.

The initial or toroidal permeability of Ferroxcube grade B2 is given as 200; knowing this and the l/d ratio we can find  $\mu'$  from Fig. 5, i.e. 117. The coil effective permeability factor  $\phi\mu_c$ , on the other hand, can be determined from Fig. 8, which is a curve of measured values of  $\phi\mu_c$  plotted as a function of a/l. The quality factor will be  $Q=10^4/62=161$ .

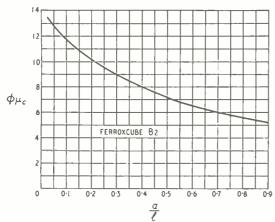


Fig. 8. Variation of  $\phi\mu_c$  with the ratio of coil length to rod length.

With this information it is now possible to calculate the effective height, inductance, etc., of the aerial. As already explained, the value of  $f_a$  for the short type of coil used is practically unity.

Therefore the effective height is

$$h = \frac{2\pi \times 0.5 \cdot 27 \times 117}{299.8} \cdot 10^{-4} = 0.0033 \text{ metre}$$

and the overall performance of the aerial system will be  $hQ = 0.0033 \times 161 = 0.532$ .

For proof that a higher overall performance can be obtained by increasing the value of the l/d ratio the above example has only to be re-calculated with an l d ratio of say 40. The objection here being that the rod would be difficult to manufacture by normal processing and hence not an economical proposition.

From Fig. 8 the effect of increasing the length of the coil can be seen, the slope between unity and a/l = 0.5 is reasonably flat and between 0.5 and zero extremely sharp. Therefore there is little benefit to be gained in increasing the ratio of a/l above 0.5 as the price of a decrease of  $\phi \mu_c$  would be considerable increase in both losses and temperature coefficient.

Variation in Coil Performance.—Recent tests on the size, shape and wire diameter of which medium wave coils are wound have proven rather interesting and will be summarized as follows. For reasons already explained, short-length single-layer coils have, up to now, been used, positioned towards one end of If we now spread-wind, or prothe ferrite rod. gressively wave-wind over approximately 2-3in of the rod length, keeping the ratio a/l less than 0.5, it will be found that the quality factor will drop by approximately 25%, i.e. from 200-210 to 150-160. pick-up voltage will, however, increase. Therefore, before finally deciding upon the type of coil necessary for a particular circuit, the main parameter of selectivity or sensitivity should be decided upon. If a long loosely wound coil is used then the value of  $\phi \mu_c$  will increase, which in turn will decrease the value of inductance, so that the number of turns must be increased to compensate for this loss.

The effects of temperature coefficient on the type of coil described influence the overall performance of the aerial by very little and can be more or less neglected.

Effect of Winding Wire.—For close wound coils the Q values vary greatly both with wire diameter and type. For instance, with solid wire 25 s.w.g. the

Q value is approximately 100, whereas with the same coil wound from 9.40 litz the quality factor increases to 270. It is worth noting that the input voltage increases with a decreasing wire gauge and is a maximum with litz. On the other hand, with long spread windings the quality factor remains almost constant with the type and wire gauge, the circuit voltage following the same trend.

Up to now we have only considered the effects of various types of coil on the quality factor, but it is of importance to take into account the effects of varia-

tions in the coil upon the inductance.

1. The maximum variation of inductance as a function of frequency is  $\pm 1^{\circ}_{\circ}$ , and does not depend upon the coil dimensions.

2. As already pointed out, by increasing the length of the coil we also increase the value of  $\mu_c$  and decrease the true value of inductance. Therefore for a constant inductance, the number of turns must be increased, but this in turn decreases the value of Q.

3. The type of wire used does not influence the value of inductance but can greatly effect the quality

actor.

All coils so far described have a diameter which only exceeds the diameter of the rod by the thickness of the coil former which is usually of brown paper or very thin presspahn. To find what influence this increase in diameter has upon the circuit quality factor a series of measurements were taken with an increasing diameter of coil former and keeping the length of the coil and number of turns the same.

Coil Diameter (mm)	Quality Factor (Q)
8	203
9.5	227
12	233
14	224
20	216
28	205

All measurements were taken at 1 Mc/s.

#### Miniature Radio-Gramophone

WEIGHING only 10 lb, the "Babyphon" portable radiogramophone is operated entirely from batteries—90-V h.t. and two 1.5-V cells being required for the valves and four 1.5-V cells for the special turntable motor. This is designed for 45 r.p.m. 7-in records and a speed control is provided to compensate for battery voltage variation. The miniature pickup is fitted with a sapphire stylus.

In the receiver, which covers medium waves only, four low-consumption (0.025-A) valves are used, in conjunction with a ferrite rod aerial. The circular tuning dial is concentric with the record turntable. Storage is provided for

five records in the lid.



The price of this instrument, which is of German manufacture, is £32 9s 11d (including tax, but without batteries) and the distributors in the United Kingdom are Distributors G-A (Whitchall), Ltd., 29, Whitehall, London, S.W.1. mains feeder unit is available costs £4 4s.

## Filters Without Fears

2.—Tchebycheff: a Name to Conjure With

#### By THOMAS RODDAM

LAST month I embarked on the task of persuading the reader that if he kept his nerve when confronted by a cumbersome algebraic expression there was no reason why he should not plunge into the exact theory of filter design without any fear of finding himself embroiled with the higher mathematics. As we shall see later, there are many problems where the classical theory is virtually useless. This is not because there is anything wrong with the classical theory itself, but is simply because the classical theory assumes that you have a lot of filter between the two ends, so that the end effects are relatively small correction terms. Where the filter is nearly all end, the direct approach is both easier and better. Moreover, the algebraic approach is balanced in regard to effort: a simple filter is easy to design, a complicated filter is extremely tedious.

The first stage of the process, which is always based on the low-pass filter, is to calculate the ratio of generator voltage to load assuming that we have a

resistive generator, a resistive load, and n reactances in between. The nreactances, consisting of alternate shunt capacitances and serial inductances, form a low-pass filter of the nth order, and the standard way of calculating the currents and voltages is by means of Maxwell's circulating currents. Although I worked in terms of voltage, the whole treatment can be carried out in terms of current: often, indeed, it is desirable to work with current at one end and voltage at the other. For example, a pentode working into a valve grid suggests that we consider the input current/output voltage ratio; a triode working into a transistor emitter would best be treated by considering the input voltage/output current ratio: all we need to consider really is the ratio of input quantity/output

quantity with and without the filter network. The ratio of those two ratios is the insertion loss.

The first article expressed this ratio of ratios in the form  $|N|^2$ , where the insertion loss in decibels is  $10 \log |N|^2$ . We found that for the class of network we are considering,  $|N|^2$  took the general form.

 $a_0 + a_1 \omega^2 + a_2 \omega^4 + \ldots a_n \omega^{2n}$  where n is the order of the network. The coefficients  $a_0, a_1 \ldots a_n$  depend on the resistances, capacitances and inductances and some of the results are displayed in Table I. Since a low-pass filter has no insertion loss at zero frequency, the term  $a_0$  is actually unity as you will see by looking at the table.

We then went on to the problem of choosing the element values. For a low-pass filter the insertion loss should be small if  $\omega$  is less than some particular value  $\omega_1$ , and large if  $\omega$  is greater than some other value  $\omega_2$  ( $\omega_2 > \omega_1$ , of course). If  $\omega$  is less than unity,  $\omega^4$  is smaller than  $\omega^2$ ,  $\omega^6$  smaller than  $\omega^4$ , and so on. Near  $\omega = 0$ , therefore, the general form of

TABLE I

	NETWORK	N
IST ORDER	$V_1$ $C = R_2$ $V_2$	$R = R_1 R_2 / (R_1 + R_2)$
2nd OROER	$R_1$ $V_1$ $C$ $R_2$ $V_2$ $V_1$ $C$ $R_2$ $V_2$	$I + /\omega (CR_p + \frac{L}{R_s}) - \omega^2 LCk$ $k = R_2 / (R_1 + R_2)$ $I + /\omega (CR_p + \frac{L}{R_s}) - \omega^2 LCk'$ $k' = R_1 / (R_1 + R_2)$ $R_s = R_1 + R_2 \qquad R_p = R_1 R_2 / (R_1 + R_2)$
309 ORDER	R <sub>1</sub> C <sub>2</sub> R <sub>2</sub> V <sub>2</sub>	$I + j\omega \left[ (C_1 + C_2) R_p + \frac{L}{R_s} \right] - \omega^2 \frac{L}{R_s} (C_1 R_1 + C_2 R_2) - j\omega^3 L C_1 C_2 R_p$ $R_s = R_1 + R_2 \qquad R_p = R_1 R_2 / (R_1 + R_2)$

Summary of insertion coefficients for basic low-loss filter structures

 $|N|^2$  is very close to  $a_0 + a_1 \omega^2$ , so that we can keep  $|N|^2$  small by taking  $a_1 = 0$ . Then we transfer our attention to  $a_0 + a_2 \omega^1$ , and by similar reasoning we can arrive at the Butterworth function  $(a_0 + a_0 \omega^{20})$ which keeps very close to  $a_0$  for small values of  $\omega$ and then tips up sharply and smoothly. This gives us a maximal flatness, critically coupled, transitionally coupled response: there may even be some more names for it. Even more attractive, it gives a form which is fairly easy to work with.

The only problem is whether the Butterworth response is the most efficient one. There are three regions in a filter characteristic: the pass band, the transition region and the stop band. The transition region is that range of frequencies where there is too much attenuation for the signal to be useful, and too little attenuation to prevent it being a nuisance. Fig. 1, which shows the Butterworth function of the second order  $(1 + x^{1})$ , indicates that if we regard the pass band as the region in which we can satisfy a  $\pm \frac{1}{2}$  db condition, and the stop band as the region in which we have more than 20 db attenuation, the ratio of  $\omega_2/\omega_1$  is about 4.7.

It is very tempting to see whether we cannot do something to improve this state of affairs. Tchebycheff, in St. Petersburg in 1875, published a paper discussing what are now known as the Tchebycheff polynomials, which are exactly what we need. There is, by the way, the usual difference of opinion about the correct way to spell this name, which in some post-war writing appears as Chebyshev, which conforms with the post-revolutionary alphabet. But the polynomials are always written as  $T_n(x)$  and I see no reason for allowing foreign politics to confuse us.

I do not propose to delve into the mathematics of the Tchebycheff polynomials because we shall have all the mathematics we can stand before we reach the end. All we need to know is that these polynomials oscillate up and down within prescribed limits for values of x between -1 and +1, and then increase steadily. Curves showing this pass-band behaviour are given in Fig. 2, which shows the first five Tchebycheff polynomials. You will perhaps recognize the shape in the region  $-1 \le x \le 1$  as that of the Lissajous figures of the same order and the appropriate phase conditions. It is not surprising, therefore, to find that the even polynomials, which are the only ones which concern us, are given by the equations:

$$\omega = \omega_0 \sin \Phi$$
$$T_n = \cos n \Phi$$

These two equations are given by Darlington, but other writers prefer:

$$\begin{array}{rcl}
\omega & = & \omega_c \cos \phi \\
T_n & = & \cos n \phi
\end{array}$$

For our purposes there is yet a third form, which is much more convenient. The even polynomials

$$\begin{array}{lll} T_2(x) &=& 2x^2 - 1 \\ T_4(x) &=& 8x^4 - 8x^2 + 1 \\ T_6(x) &=& 32x^6 - 48x^4 + 18x^2 - 1 \\ T_8(x) &=& 128x^8 - 256x^6 + 160x^4 - 32x^2 + 1 \end{array}$$

In the region we are considering as the pass band,  $0 \le x \le 1$ , these functions oscillate between a maximum value of +1 and a minimum value of -1. For  $x \gg 1$  the highest order term takes control, and off they go, getting larger as  $x^n$  so that the asymptote has a slope of 10n db decade or 33n db/ octave. A third order filter, for example, which we shall see is associated with  $T_6(x)$ , cuts off at the rate of 18 db/octave.

How can we make use of these polynomials? We have an insertion loss function  $|N| = a_0 + a_1 x^2 +$  $a_2x^4 + ... a_nx^{2n}$  where x, of course, is either  $\omega$  or  $\omega/\omega_0$ , whatever  $\omega_0$  might be. We want this function to be within the limits  $1 \le |N|^2 \le 1 + t$  or  $1-t \le |N|^2 \le 1$  over a range of frequencies, the pass band. To fix our ideas, let us work with the second order filter. We have to consider the Tchebycheff polynomial  $T_4(x) = 8x^4 - 8x^2 + 1$ . At x = 0  $T_4(0) = 1$ . At x = 1,  $T_4(1) = 1$ . At x = 0.71,  $T_4(0.71) = -1$ . For values of x > 1,  $T_4(x)$  increases rapidly. We therefore take a function

 $1-t+t T_1(x)$ which lies between 1 and 1-2t for all positive values of x less than unity. The response is then  $\pm \frac{1}{2}$  10 log (1-2t) decibels. Let us take as our permitted tolerance  $\pm$  0.625 db, for which we find t = 0.125. I have chosen this rather odd tolerance to make the arithmetic

easier. Now we have the function

 $1 - 0.125 + 0.125 (8x^4 - 8x^2 + 1) = 1 - x^2 + x^4$ The response of the second order filter is,

$$|N|^2 = 1 - \omega^2 \left[ \left( CR_p + \frac{L}{R_s} \right)^2 - 2LCk \right] + \omega^4 L^2 C^2 k^2$$

In this expression,
$$R_{\nu} = R_1 R_2 / (R_1 + R_2)$$

$$R_s = R_1 + R_2$$

$$k = R_2 / (R_1 + R_2)$$
Last month L worked out in detail the

Last month I worked out in detail the conditions for a

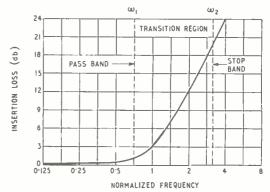


Fig. 1. Butterworth response of second order. The pass band is defined as the region in which the response is within  $\pm$  0.5 db, the stop band as the region in which the insertion loss exceeds 20 db.

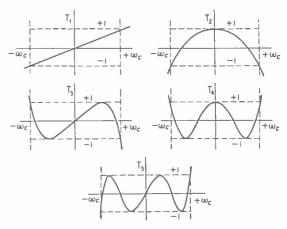


Fig. 2. Form of the first five Tchebycheff polynomials.

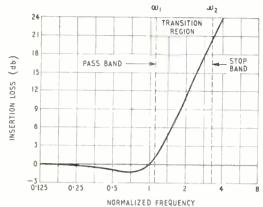


Fig. 3. Tchebycheff response of second order. The pass band is defined as the region in which the response is ± 0.625 db, and the stop band as the region in which the insertion loss exceeds 20 db.

Butterworth response with  $k=\frac{1}{2}$ , corresponding to R<sub>1</sub> - R<sub>2</sub>. If you try to get a Tchebycheff response under these conditions, you find that you need a negative resistance somewhere in the circuit. We can, however, take  $R_2=\alpha$ , so that k=1. Then  $|N|^2=1+\omega^2$   $[(CR_1)^2-2LC]+\omega^4L^2C^2$ 

We now compare this with the form

$$1-x^2+x^4$$

For identity we must have

$$\begin{array}{rcl} x^4 & = & \omega^4 L^2 C^2 \\ x^2 & = & (2LC - C^2 R_1^2) \ \omega^2 \end{array}$$

It is not very hard to reach the equation

$$\omega^2 LC = (2LC - C^2R_1^2) \omega^2$$

so that

$$C^2R_1^2 = LC$$

$$L = CR_1^2$$

which we must compare with the condition for a Butterworth response,

$$L = \frac{1}{2} CR_1^2$$

To see what we have gained by this change, let us look at Fig. 3 and compare it with Fig. 1. The small bump, less than 12 db, at a normalized frequency of 0.7, has reduced the ratio  $\omega_2/\omega_1$ , from about 4.7 to about 3.3. Another way of expressing this result is that for the same stop-band response the  $\pm$  0.6 db pass band is increased from 0.7 to 1.

Most important of all, we have made full use of one piece of information, the permitted tolerance in the pass band. There is nearly always some inefficiency in a circuit which can be designed without using one of the vital parameters.

We should, I suppose, complete our calculations for the example. At  $\omega^2 LC = x^2 = 1$ , the edge of the pass band is reached. This, of course, means that  $\omega_0^2 LC = 1$ . Then as  $L = CR_1^2$ 

$$\begin{array}{ll} L = R_1{}'\omega_0 \\ C = 1/\omega_0 R_1 \end{array}$$

The other case of k = 1, with  $R_1 = 0$ , leads us to  $L = CR_2^2$  instead of  $L_{(B)} = \frac{1}{2} CR_2^2$ , with

$$egin{array}{cccc} L &= R_2/\omega_0 \ C &= 1/\omega_0 R_2 \end{array}$$

This particular example is, I must confess, deceptively simple. The reason is that the choice of t =0.125 got rid of all the awkward numbers. If we had decided to adopt  $\pm$  0.5 db. as our design criterion we should have been working with the function

$$1 - 0.8x^2 + 0.8 x^4$$

which although theoretically no harder, leads us to

Of course there is no more mathematics, really, but the actual arithmetic is more tedious. interesting to notice here that the new value of  $\omega_0$  is 0.945 (LC)!, so that by tightening the tolerance from  $0.625\,\mathrm{db}$  to  $\pm$   $0.5\,\mathrm{db}$  we have cut the pass band down by just over 5%. We may, perhaps, come back to this matter later.

The third order filter is related to the Tchebycheff polynomial of the sixth order,  $T_6(x)$ . For x = 0,  $T_6(x) = -1$ , so that we consider

$$1+t+t$$
.  $T_6(x)$ 

which oscillates between 1 and 1 + 2t. The expression we arrive at is therefore

$$1 + 18t x^2 - 48t x^1 - 32t x^6$$

Any value of t is going to make this look pretty alarming, and it is this sort of arithmetic which gives network design a bad name. A little investigation shows, however, that if we take t = 1/16, so that the response is to be within \_ 0.25 db, and then take as our function  $1 + x^2 - 3x^4 + 2x^6$ , we shall not be too much in error. In the special case when  $R_2 = \infty$ , we can pick up the expression quoted in the previous article and simplify it to:

$$\begin{aligned} |\mathbf{N}|^2 &= 1 + \omega^2 [(\mathbf{C}_1 - \mathbf{C}_2)\mathbf{R}_1]^2 + \omega^4 [-2\mathbf{L}\mathbf{C}_1\mathbf{C}_2(\mathbf{C}_1 + \mathbf{C}_2)\mathbf{R}_1] \\ &+ \omega^6\mathbf{L}^2\mathbf{C}^2\mathbf{C}_2^2\mathbf{R}_1^2 \end{aligned}$$

and the conditions for this Tchebycheff response become

$$\begin{array}{lll} \omega^{6}L^{2}C_{1}^{2}C_{2}^{2}R_{1}^{2} &=& 2\,x^{6} \\ 2\,\omega^{4}LC_{1}C_{2}\,(C_{1} + C_{2})R_{1} \\ \omega^{2}\,(C_{1} + C_{2})^{2}\,R_{1}^{2} &=& x^{2} \end{array} = 3\,x^{4}$$

I am not going to solve these equations for L, C, and C2, though they do not present insuperable difficulties. You will realize, however, that if we had not cheated in our writing of the polynomial, if we had taken t as, say, 0.1, and if we had chosen  $R_2 = 3R_1$ , the equations might have been rather grim.

Fortunately, there is a much more advanced approach to this problem, and this leads, as is not unusual, to a rather simpler arithmetical process. If you want to know the amount of £100 at 500 after 17 years, you do not write down a long table:

You know that the answer is  $100 (1.05)^{16} = 100$ antilog (16 log 1.05). If you deal a lot with money you will not even do this: you will look the answer up in tables.

There are tables which give the values of the elements in second and third order Tchebycheff low-pass filter, for response tolerances up to  $\pm$  0.5 db. They are given in chapter 12 of "Filter Design Data," by J. H. Mole (E. & F.N. Spon, 1952). With the aid of these tables the use of the Tchebycheff response becomes a matter of no greater complexity than the use of the Butterworth response. The only trouble is that you must be satisfied, in the third order case, to work with either equal resistances at both ends, or with one end open-circuited.

Perhaps we should just look back. The ordinary processes of the application of Maxwell's circulating

currents have led us to an expression for the insertion loss of a network

$$20 \log \left[ \left( \frac{\text{V or I in}}{\text{V or I out}} \right) \underset{\text{network}}{\text{with}} / \left( \frac{\text{V or I in}}{\text{V or I ou}} \right) \underset{\text{work}}{\text{without}} \right]$$

$$= 10 \log |\mathbf{N}|^2$$

where

 $|N|^2=1+a_1\;\omega^2+a_2\;\omega^4\;\ldots\;a_n\;\omega^{2n}$  We have then sought a function of the same form which represents the frequency characteristic of a low-pass filter. Such a function, which we can call a filter function, is

 $F(x) = 1 + \alpha_1 \omega^2 + \alpha_2 \omega^4 + \dots + \alpha_n \omega^{2n}$ If our network is to have this characteristic, obviously

and so on.

Two basic kinds of filter function, the Butterworth and the Tchebycheff, have been discussed, and we have seen how we can solve this set of simultaneous equations to find the reactances required. We have also seen that in the simple form we have used, the Tchebycheff equations become very cumbersome. It's a good thing we can dodge the hard work by looking up the answers in tables. We have not yet

Correction: In the first part of this article it is regretted that the curves of Figs. 4 and 6 on pages 369 and 370 of the August issue became transposed.

decided whether the Tchebycheff response is always worth while, or what price we must pay for a flatter response. These are matters of very great interest, but they will occupy more space than I can demand

The phase characteristics of filters are often of interest, and it must be noted that we have all the information for plotting these characteristics. From the results in part I we can see that the insertion phase shift is:

 $\theta = arc tan \omega CR$ 1st order

2nd order

$$\theta = \arctan \frac{\omega(CR_p + L/R_s)}{1 - \omega^2 LCK}$$

3rd order

$$\theta = \arctan \frac{\omega \left\{ \left[ (C_1 + C_2) R_p + \frac{L}{R_s} \right] - \omega^2 L C_1 C_2 R_p \right\}}{1 - \omega^2 \frac{L}{R_s} \left( C_1 R_1 + C_2 R_2 \right)}$$

Into these expressions we can now substitute the values we have found for the responses we consider. This may become one of the factors which settles our final choice of response.

Acknowledgment. Fig. 2 is adapted from Fig. 2 of "Network Synthesis Using Tchebycheff Polynomial Series" by S. Darlington, B.S.T.7. Vol. 31, p. 613

## Ultrasonic Developments

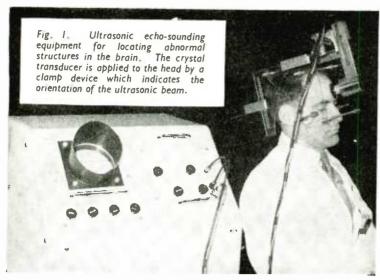
Techniques Revealed at Oxford and Manchester

ROBABLY the most familiar ultrasonic device to radio technical people is the ultrasonic flaw detector, which works on an echo-sounding principle and uses electronic circuitry somewhat akin to radar. While this idea has become well established it has not been allowed to stagnate, any more than has radar, and recently some interesting variants and developments of the original theme have come to light. One or two were described in papers read at the recent Brit. I.R.E. Convention on industrial electronics at Oxford, while others were on show as actual apparatus at the Ninth Annual Exhibition of Electronic Devices organized by the Institution of Electronics (North-West Branch) at the Manchester College of Technology.

A fairly straightforward application of the flawdetector principle was an equipment for obtaining echo patterns from the living human brain, the idea being to detect abnormal structures such as cerebral tumours. This was shown at Manchester by the Department of Physics of the Royal Cancer Hospital (see Fig. 1). The ultrasonic waves are generated by a quartz crystal which is pulsed by a thyratron discharge at a repetition rate of 50 c/s and produces a series of damped wave trains at a frequency of 1.25 Mc/s. When the crystal transducer is applied to the patient's cranium a beam of ultrasonic energy about ±4° wide passes through the brain until it encounters an internal surface differing in elasticity or density, and then some of the energy is reflected back. The crystal also acts as a pick-up device, in between the times it is being pulsed by the thyratron, and it receives the burst of reflected energy and converts it back into an electrical signal. This is then amplified and applied to the Y plates of a cathode-ray oscillograph, which has a timebase locked to the 50-c/s thyratron pulse generator. The original transmitted pulse appears at the left-hand edge of the time-base sweep (since it is fed back into the receiver amplifier) while the returned pulse appears farther along to the right, the actual distance between them indicating the distance of the internal reflecting surface from the cranium.

The time-base of the oscillograph will show echoes from surfaces up to 20cm away, and it has been possible to calibrate it in centimetres by using a water tank and immersed reflecting surface in place of the patient's head, for the velocity of the ultrasonic waves in water is very little different from their velocity in brain tissue (a depressing thought!). Since the transmitted pulse is applied straight back to the receiving amplifier, however, this amplifier is paralysed for a short while and as a result echoes from less than 3-4cm away do not appear on the oscillograph.

With an amplifier gain of something like 100 db the equipment is extremely sensitive, and an echo with a



high signal-to-noise ratio can be obtained in a tank of water from a glass fibre of less than 0.001in in diameter. Particles and bubbles in the water, too small to be seen, can also be shown up clearly. As for the accuracy of location, a resolution of 20 microns is claimed for the equipment.

When the Wireless World reporter was invited to try the apparatus on his own head he was somewhat reluctant, having heard of the emulsifying and cavitation effects produced by ultrasonic waves. It appears, however, that there is no danger of the brain becoming addled, as the average power used is only about 10 microwatts.

One problem in ultrasonic flaw detection which is providing a great deal of food for thought is that of launching the ultrasonic wave into the material at an oblique angle—or more particularly at a variable angle so that the material may be scanned for flaws. Normally, of course, the beam simply travels in at right angles to the surface from the point where the transducer is applied. One approach to the problem

has been the use of suitably shaped blocks of glass or Perspex between the transducer and the work. The lower surface of the block, in contact with the work, is made flat, while the upper surface is curved so that the transducer (also suitably curved to fit) may be slid round it in an arc. In this way a steerable beam is obtained, but the method is still rather slow and cumbersome.

A rather ingenious system of beam steering and scanning which the National Physical Laboratory has tried out was described by G. Bradfield at the Brit.I.R.E. Convention. This works on the principle of causing the ultrasonic wave to be

launched from one side of the transducer slightly before or after it starts from the other side. The result is an inclined wave front (the actual inclination depending on the time lag) and the beam travels obliquely from the crystal instead of at right angles to its surface. A comparable situation in Nature is that of sea waves coming in at an oblique angle to a beach, so that they break at one end of the beach somewhat later than at the other end—though here, of course, the waves are arriving instead of departing.

To achieve this effect a barium titanate transducer is used and is divided into a number of sections by grooves (Fig. 2). Each section is then fed from a corresponding section of an LC delay line into which a short  $2\frac{1}{2}$ -Mc/s electrical wave-train is injected. (Actually the barium titanate sections themselves form part of the capacitive

elements of the line.) As a result the ultrasonic wave is launched from the "injection" end straight away and from the other end a fraction of a microsecond later. Using a 0.235- $\mu$ sec delay line the wave-front is given an inclination of 4° from normal and with a 0.47- $\mu$ sec line it has an inclination of 8°. This gives two beam angles in, say, an "easterly" direction, and by injecting the  $2\frac{1}{2}$ -Mc/s signal into the other end of the line the same angles of inclination can be obtained in a "westerly" direction. Thus, with the normal propagation of the beam straight into the material, there are five beam angles available altogether.

A rotating switch enables any one of these five beam angles to be selected, but in practice it is arranged to sweep through them in rapid succession so that the returning echoes along the beams can be displayed almost simultaneously on a cathode-ray tube. In this way the material is scanned in a similar fashion to radar and the range and bearing of the echoes can be presented either in B-scope form (Cartesian co-ordinates) or as a p.p.i. display.

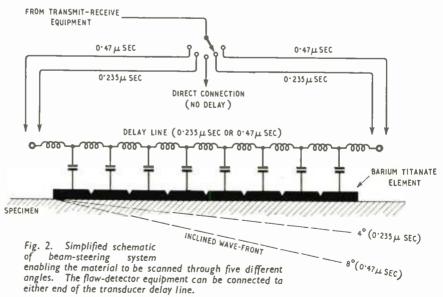




Fig. 3. Portable thickness gauge working on a mechanical resonance principle, with quartz crystal transducer in front.

Another ultrasonic examining device with cathoderay tube presentation was mentioned by F. Gutman at Oxford. This is an ultrasonic microscope developed by the Russian scientist Sokolov for detecting and studying objects in opaque media. Here, a beam of ultrasonic waves is reflected from the object under examination and is focused and collected on a plate of piezoelectric material which is mounted in a cathode-ray tube. Secondary electrons are produced from the plate by the action of the electron beam and their path is modified by the piezoelectric charges caused by the ultrasonic waves. An image is then obtained by the usual television method. A magnification of several thousand is claimed for this instrument.

#### Thickness Measurement

Ultrasonic techniques are also being used a great deal nowadays for gauging the thickness of materials, and, as they generally utilize reflection of the waves, they are particularly valuable when only one surface of the material is accessible. The reflection, however, is not used in the same direct way as in the flaw detector. An ultrasonic generator is applied to one surface of the material and the reflected waves returning from the far side intersect with the outgoing beam to produce standing waves. At a certain frequency (determined by the thickness of the material and the velocity of the waves in it) a resonance condition occurs, and from this frequency the thickness can be calculated. The mechanical resonance also occurs at harmonics of this fundamental frequency.

To put the principle into practice it is therefore necessary to be able to vary the frequency of the ultrasonic generator and to obtain an indication of the mechanical resonance. The first is easily done with a variable frequency oscillator, while the resonance indication is obtained from the fact that the internal damping of the material at resonance puts a load on the oscillator; this can be detected by an increase of anode current in the oscillator valve.

Unfortunately, this increase of anode current is not

always enough to give a good indication. One way of overcoming the trouble was described by F. M. Savage at Oxford, and the improved technique has been used in a commercial instrument which was exhibited at Manchester (see Fig. 3). The oscillator is frequency-modulated over a small deviation range by a motor-driven capacitor. Then, when the oscillator is tuned (by a permeability control) to the mechanical resonance frequency of the material, pulses of anode current are produced as the oscillator frequency is swung back and forth through this point. These pulses are at an audio frequency rate (determined by the motor-driven capacitor) and they are amplified, rectified and applied to a meter and to a pair of headphones. Resonance is then indicated by an increase in the meter reading or by an audible note

Padding capacitors are placed in series with the motor-driven capacitor so that modulated bands of various widths can be chosen. Narrow bands provide maximum selectivity and accuracy while the wider bands are used when the material has a rough surface or is of variable thickness. The oscillator covers a range of 0.75 Mc/s to 2 Mc/s and this enables the same crystal transducer to be used for all frequencies with very little loss of sensitivity. If only the fundamental resonance indications were used the thickness measurement range would be of the same order as the frequency range (just over 2 to 1), but by using harmonic resonance indications as well this range can be extended to about 1,000 to 1.

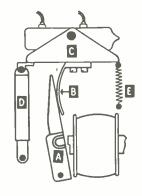
#### MERCURY SWITCHES

THE Tiltray mercury switch is operated by a built-in relay, but the design is a little unusual in that the mercury elements are carried by a tilting tray pivoted in such a way that it ensures a smooth surgeless flow of mercury from one contact to the other. In certain operating sequences this could be important.

How this is achieved is shown in the schematic diagram reproduced here. The armature A moves the tilting tray C carrying the mercury capsules by what is called a variable ratio one-tooth gearing, consisting of an extension of the armature A and a curved finger B. This slows down the movement of the tray as the armature accelerates towards the coil. Acceleration of the tray is further retarded by the action of the pneumatic damper

D and the return spring E. Mercury switches find many applications in circuits where heavy currents flow, and they are especially useful where inductive loads are involved as quite high inductive surges can be handled safely since the energy is released in a mercury-vapour arc and there is no high-voltage build up.

Tiltray mercury switches are made by Besson and Robinson, Ltd., 6, Government Buildings, Kidbrook Park Road, London, S.E.3, and can be arranged for switching three circuits of up to 60 A each in a single compact unit; the operating power is ½ to 2 W d.c. or 5-15 VA a.c.



Schematic diagram of the Besson and Robinson Tiltray mercury switch.

## Measuring Small Voltage Changes

Simplified Method Using Polystyrene Film Capacitors and Electrometer Valves

By J. P. SALTER, A.M.I.E.E.\*

A problem that arises quite frequently in development work is the accurate measurement of small changes in the d.c. level of relatively high voltages. The change of level may be produced deliberately by an adjustment made elsewhere in the circuit, or it may develop over a matter of minutes as a result of slow changes in circuit constants.

A change of, say, 0.1 V at a 300-V level would be imperceptible on a voltmeter; the rate of change would be too slow for normal a.c. techniques to be employed; and the application of manually adjusted backing-off voltages is fraught with danger to the meter on which

the change is to be read.

The development of the polystyrene film capacitor and the low grid conductance of modern electrometer valves enables this problem to be solved very simply. Fig 1 shows the basic circuit where C<sub>1</sub> and V<sub>1</sub> are the capacitor and the electrometer valve respectively, and S<sub>1</sub> is a polystyrene-insulated switch. So long as the switch is closed the valve and the difference meter are protected from any changes of d.c. level at the input. When a measurement is required the switch is opened and, as the capacitor is already charged to the correct backing-off voltage, only difference voltages are transferred to the metering system. The potential across the capacitor can change only as a result of internal leakage, of leakage across the switch, of leakage or grid current in the valve, or of electrification effects in the dielectric.

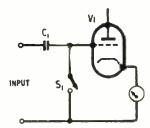


Fig. 1. Basic circuit used for measuring very small voltage changes.

The insulation resistance of good types of polystyrene film capacitor is so high that their time constants are measurable in terms of years, and in this application both internal leakage and electrification effects can be ignored entirely. On most types of relay the supporting insulant of one of the contacts can be replaced by polystyrene without difficulty. The grid conductance of the valve can be kept acceptably small by choice of valve and operating potentials.

The system has many advantages. Backing off is automatic, is independent of polarity, and is independent of input level within the operating range of the capacitor. Since leakage in the capacitor can be ignored, a direct calibration check against any voltage

standard of suitable range can be carried out at zerovoltage level, and drift in the instrument itself over any desired period can be checked simply by shorting the input and opening the switch.

Polystyrene film capacitors are now generally available in values up to 0.2 µF with quite a modest ratio of volume to capitance. A single 0.2-µF capacitor is sufficient for most applications, but there are occasions when, in order to be able to use a more familiar type of valve such as the EF37A or the ME1400, it may be worth while using a number in parallel to provide, say, 1 µF. Various voltage ratings are available, and capacitors rated at 350 V working at 65°C (1,000-V d.c. test) have operated very satisfactorily at a 500- to 600-V level when mounted in such a position that they remain substantially at room temperature.

#### Practical Circuit

In considering the layout of the instrument, there is only one lead whose insulation is vital; that connecting the grid, the capacitor, and one contact of the switch. The use of a length of polythene-insulated coaxial cable for this lead and the adoption of a simple "guard" system(1) will reduce leakage to negligible proportions. For the guard system, the mounting clip for the capacitor, the outer conductor of the cable, the framework of the switch (preferably relayoperated), and the metalizing of the electrometer valve, should all be connected to the earthy input lead.

The characteristics of electrometer valves and of general purpose valves which can be pressed into use in this role have been the subject of a number of articles of recent years<sup>(2)</sup>, and little need be added here. The electrode potentials are so chosen that normal grid current is almost completely suppressed, and the "reverse" grid current which flows is predominantly the result of ionisation of free gas molecules by the electrons flowing to the other electrodes. The gas pressure varies somewhat from one type of valve to another, and from valve to valve within any one type, but there is little the user can do about it other than to avoid any careless maltreatment which might result in the release of further gas from the electrodes.

The choice of a valve for this application depends mainly on the range of difference voltages to be measured, on the time interval over which the measurement is to extend, and on the accuracy demanded. By reducing the anode voltage to some 5-10 V, and by adjusting one's methods to deal with

<sup>\*</sup> Ministry of Supply.

1 Scroggie, M. G. "Measuring High Resistance," Wireless World,
June 1952

2 Scroggie, M. G. "A Valve Megohmmeter," Wireless World,
November 1953.

values of  $g_m$  and  $\mu$  as low as  $15~\mu\text{A/V}$  and unity respectively, grid currents of  $10^{-13}\text{A}$  and below can be achieved without much difficulty, but the range of input and output voltage tends to become somewhat limited. It is advisable, therefore, to be content to achieve a grid current no lower than is really necessary for the particular application in mind. The arithmetic is quite simple; one assumes a constant charging rate for the capacitor and employs VC=Q=it (volts, farads, amps and seconds) to calculate the grid current that would result in the development of an acceptably

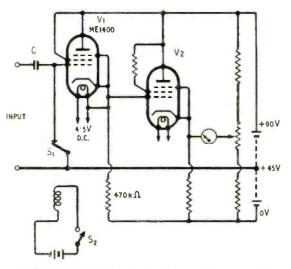


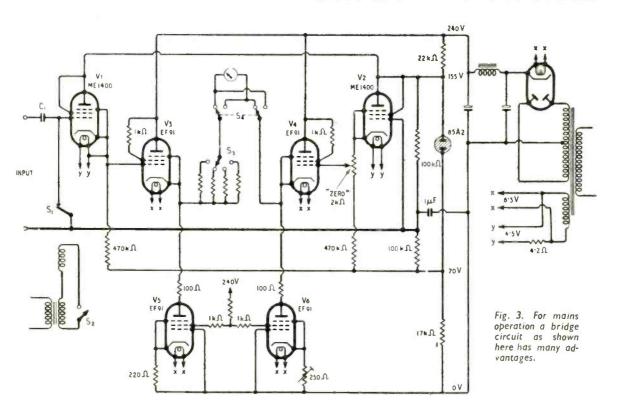
Fig. 2. Simple form of measuring set using battery operation.

small error voltage across the chosen capacitor during the time needed to complete the measurement.

As an example of what can be achieved using quite conventional circuitry, we can take the case of the ME1400. Strapped as a triode, the electrode potentials recommended by the makers are 4.5 V on the heater, 45 V on the anode, and -2 V bias on the grid. Under these conditions the valve has a  $\mu$  of 20 and a  $g_m$  of  $300 \,\mu\text{A/V}$ , whilst the anode current is about  $100 \,\mu\text{A}$ and the grid current is around 6 µµA. The grid can be swung about half a volt each side of the recommended operating point without approaching too close to anode current cut-off on the one hand or the commencement of normal grid current on the other. The grid current is reduced by a factor of three, or thereabouts, at the peak of the negative swing, and is increased by a similar factor at the peak of the positive swing.

With such a limited grid base there are obvious advantages in adopting the cathode follower technique. The required conditions will be met by the use of 90 V h.t. and a 470-k $\Omega$  cathode load. Using such a value of cathode load, the gain of the system will approximate to  $\mu/(\mu+1)$  and only  $1/\mu$  of the input voltage will appear between grid and cathode. A change of level at the input not exceeding 10 V, of either polarity, could therefore be handled satisfactorily.

If we use a 1- $\mu$ F capacitor and take 6  $\mu\mu$ A as being a representative value of grid current for small excursions, we obtain a leakage rate (V/t=i/C) of 6  $\mu$ V per second or 22 mV per hour. If the error due to this leakage is not to exceed say 1 per cent, we should have about three minutes in which to complete a difference measurement of 0.1 V, or about half an hour for one of 1 V. For a 10-volt measurement



(taking the positive-going input as being the worst case) the leakage rate would increase to about 70 mV per hour, giving us an hour and a half for the same

percentage error.

Periods such as these are quite long enough for the completion of most tests in which the change to be measured is the result of a change in the effective value of a component (e.g., a thermal change), and it is only in the more specialized applications that it is worth employing one of the more esoteric types of electrometer valve. In fact, for applications where the change of voltage level develops more or less concurrently with the making of some adjustment elsewhere in the circuit, as, for example, when one is examining the response of a stabilized power pack to changes of load or of input voltage, we could safely use a single 0.2-µF capacitor and still have a large margin in hand for stray leakages. In the same way, there are occasions when it would be in the nature of an extravagance to employ an electrometer valve at all and when the average EF37A would do the job quite satisfactorily if used in the circuit described.

The design of the metering portion of the instrument is largely a matter of personal choice. Although the valve is operating as a cathode follower in the arrangement described, the output impedance is not particularly low and it is not really satisfactory to feed even a 25- $\mu$ A meter movement direct from the cathode. The simplest form of practical circuit is probably that shown in Fig. 2, in which  $V_2$  is any convenient valve of reasonable slope. An unbalanced circuit such as this is very vulnerable to both l.t. and h.t. variations, and is best suited to battery operation, particularly as the current requirements are small.

#### Mains Operation

For mains operation, the use of a Bridge circuit such as that shown in Fig. 3 makes the provision of stabilized h.t. and l.t. unnecessary for most applications. Pentode loading of the cathode followers  $V_a$  and  $V_a$  provides them with high impedance cathode loads through which they can be fed with 8 or 9 mA apiece at the expense of a very modest voltage drop. This keeps up their  $g_m$  and permits the use of a robust meter. With correct adjustment of the preset variable resistor which provides the bias for  $V_a$  the bridge will remain balanced over quite a wide variation of mains voltage.

Since the change to be measured may be of either polarity, a centre-zero meter or a change-over switch for the meter should be provided, and voltage ranges of 0.25, 1.0, 2.5, and 10 volts f.s.d. can be provided by the use of a range switch and series resistors suitable to the meter employed. The use of a relay-operated switch for S<sub>1</sub> simplifies the control of surface leakages and permits the linking of other events to the opening of the switch. Where the power supplies are unstabilized and the relay is a.c.-operated, it is advisable to feed the relay coil from a separate transformer. For general use it is desirable to include in the instrument a suitable resistor in series with the input terminal; this will limit the charging current when the instrument is first attached to a high voltage point.

#### Infra-red Analysis



Mervyn-NPL infra-red spectrometer for chemical analysis and process control.

THE selective absorption of electromagnetic waves by organic and other liquids and gases is becoming increasingly important as a rapid method of analysis in the petroleum, chemical and many other industries. Wavelengths of the order of  $3\mu$  ( $3\times10^{-3}$ mm) in the infra-red region of the spectrum are generally used, and a curve is plotted showing how the absorption varies with wavelength. From this and a knowledge of the absorption characteristics of pure substances, an analysis of mixtures can be made.

The first essential is the production of a "monochromatic" source of radiation of variable frequency, and in the past this was provided by a refracting prism and an expensive auxiliary optical system. Recently the National Physical Laboratory have developed an efficient method of making diffraction gratings, based on a method originated by Sir Thomas Merton, which produces comparable resolu-

tion at a fraction of the cost.

Mervyn Instruments, Copse Road, St. John's, Woking, Surrey, have undertaken the commercial production of an infra-red spectrometer using the Merton-NPL grating. The source of radiation is a Nernst filament lamp and the beam is interrupted 800 times per second. After absorption in the specimen under test, the beam passes to a lead selenide photocell, the output of which is amplified and recorded on a chart.

To achieve accuracy comparable with a balanced double-beam null method of measurement, a high degree of overall stability is required. In the Mervyn instrument this is achieved by continuously monitoring the source of radiation and the sensitivity of the detector and applying any variations to the amplifier in the form of gain control. Compensation for the wavelength-dependent characteristics of the source, the grating filter and the detector is effected continuously, as the spectrum is transversed, by an adjustable shaped cam.

#### Magnetic Tape Spools

DIMENSIONS of spools for nominal tape lengths of 300, 600, 1,200 and 1.750ft are given (with tolerances) in a new specification (B.S.2478:1954) obtainable from the British Standards Institution, 2, Park Street, London, W.1, price 2s. These spools are for domestic and commercial recording, as distinct from those used in broadcasting studios.

Other matters touched on by this specification include the width of safety lane and the direction of recording in dual track tapes. It is recommended that if the tape moves from left to right with the active side away from the observer, the upper track should be in use.

Hay G. A. "Receiving Valves Suitable for Electrometer Use." Electronic Engineering, July 1951

Yarwood, J. and Le Croisette, D. H. "D.C Amplifiers," Electronic Engineering, January 1954.

### TRANSFORMERS for

### Low and High Frequencies

By "CATHODE RAY"

Demonstrating Their Differences by "General" Vector Diagrams

OW that we have spent two issues studying vector diagrams—and I hope the time has not been wasted—we should be better equipped to tackle problems like the one an Australian reader put to me some while ago. He asked for an explanation of the fact that in critically-coupled r.f. transformers, such as those often used in i.f. amplifiers and f.m. discriminators, the voltage across the secondary is 90° out of phase with the voltage across the primary. He says that the textbooks (and "Cathode Ray"!) gloss over this part of the story.

Well, I can't easily forget that when dealing with the discriminator stage in f.m. receivers a few years ago I tripped up over this very thing, so it is some comfort to be told that it is a difficult point. One catch, perhaps, is that in ordinary low frequency transformers the secondary voltage is in phase with the primary voltage, or very nearly so, and it is easy to assume the same thing holds for transformers

A clue can be given quickly by saying that the r.f. transformer is very loose-coupled and normally works in the condition of resonance, whereas the ordinary power transformer is very close-coupled and non-resonant. To get a complete picture, however, there is nothing for it but to pull out our small but trusty kit of basic principles and get to work.

Probably the best approach is to start with a theoretically perfect 100% coupled transformer and see what happens as the coupling is loosened. If you like we can start with something simpler still—a

single winding on an iron core, as in Fig. 1. When this is connected to an a.c. generator, as in Fig. 2(a), the alternating current that flows through the coil produces an alternating magnetic flux in the core. Because the current is the direct cause of the flux, the flux is in phase with the current.

The alternations of flux generate an e.m.f. ("the e.m.f. of self-induction") in the coil, proportional to the rate of flux variation, and always tending to oppose its cause—the variation of current. According to the current notation explained last month, IJK means the current whose positive direction in Fig. 2(a) is clockwise around the circuit. At the start of the current cycle, as shown in Fig. 2(b), the current is increasing at its greatest rate, so this induces the maximum e.m.f. tending to oppose the increase of current, and therefore anticlockwise at this moment. To keep the current increasing, notwithstanding this opposition, it is necessary for the generator to be exerting an equal e.m.f. clockwise (we are neglecting the resistance of the coil). Whether one looks at it from the point of view of the coil or the generator, b must be maximum positive with respect to a. So  $V_{ab}$ (which, using the "potential-rise" convention, means the voltage change on moving from a to b) is peak positive, as shown. In the familiar words of the textbooks, the current lags the applied e.m.f. by 90°. The information given in Fig. 2(b) is much more conveniently portrayed in Fig. 2(c), which is the general vector diagram for Fig. 2(a). (The whole point of going over this very elementary stuff is really to remind ourselves of the conventions explained in detail in the last two issues.)

It would make no difference in principle if the wire we used for this coil happened to be composed of two strands. Nor would it make any appreciable difference whether the strands were insulated

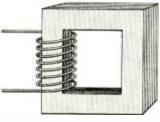
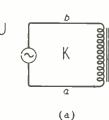
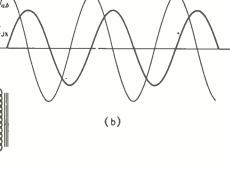
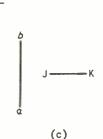


Fig. 1. The starting point—a single iron-cored coil.

Fig. 2. (a) s the lettered circuit diagram for the coil connected to an a.c. generator; (b) is the waveform diagram; and (c) the general vector diagram—ab for voltage and JK for current.







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The flux causing the or not. e.m.f. would link both strands practically equally, and if one strand happened to become disconnected from the generator, the same voltage, in the same phase, would exist between the ends of disconnected strand between the ends of the connected strand. Fig. 3 shows an enlarged view of the separated strands, with the disconnected one dotted to distinguish it. What we have now is a virtually 100%-coupled transformer, and there can be no doubt that the secondary e.m.f.  $V_{ed}$  (Fig. 4) is in phase with the primary e.m.f.  $V_{ab}$ .

Now consider what happens when a load is connected across resistance Being a resistance, it passes the secondary. current  $(I_{JL})$  in phase with  $V_{cd}$ . This current of course has to flow through the secondary winding, and in doing so it creates an alternating magnetic flux -a quite unchangeable result, like the law of the Medes and Persians, only more so. Yet it can't be allowed! The generator is still applying the same e.m.f. as before (we assume) and this must be exactly balanced by the e.m.f. generated in the primary by the alternating magnetic flux. That flux was just right before I<sub>JI</sub>. started to flow, so it can't still be right when another lot of flux is being caused. There is only one way out of this deadlock; the way of the Persian monarch Ahasuerus when his wife convinced him that a law he had made under the influence of a sinister courtier was wrong. He couldn't rescind it, but he could issue another that would neutralize it. Nothing can be done to prevent I<sub>JL</sub> exerting its magnetizing influence, but this influence can be exactly neutralized and the status quo restored if the generator supplies a primary current that creates an equal and opposite flux. This current is of course in addition to the original magnetizing current needed to induce the back e.m.f.

#### 100% Coupling

It is time we brought our vector diagram up to date. Because it is induced by the same flux as the primary e.m.f., the secondary e.m.f. is represented in Fig. 5 by cd, an exact duplicate of ab. The current diagram at (a) applies before the secondary was loaded; the fact that  $I_{JL}$  was then zero is shown by the distance J to L being zero. After connecting the resistance load the current  $I_{JL}$  is represented at (b) by JL in phase with cd. The current effective for causing magnetic flux is the total current crossed on moving from L to K ( $I_{LK} = I_{LJ} - I_{JK}$ ), and this can only be kept the same as in (a) by raising K to the new position shown at (b); that is to say, by adding the vertical dotted portion (equal to JL) to the original horizontal portion.

The fact that there is no actual connection between meshes K and L is appropriately represented by leaving K and L without a direct connecting line in Fig. 5(b), but the distance from K to L does nevertheless correctly represent the total current in the two windings lying between meshes K and L. This logical interpretation of vector diagrams constructed on this plan is particularly helpful in transformers, for it shows the net magnetizing current, irrespective of the individual currents flowing through the windings.

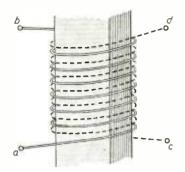
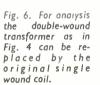


Fig. 3. The result of separating the two strands of the wire with which the coil in Fig. 1 is wound.





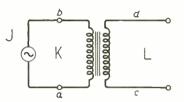
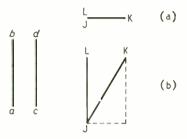
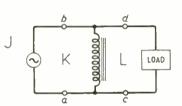


Fig. 4. Circuit diagram of the closecoupled 1:1 transformer formed by separation of strands as in Fig. 3.





The sign of the currents is automatically taken care of, provided that the circuit diagram is drawn so that the coils are wound in the same direction—see Fig. 4—and have equal numbers of turns. (This is covered by the normal practice with transformer vector diagrams, of working in volts per turn and ampereturns, rather than total volts and amps, so as to avoid vectors of absurdly different lengths.) It is easy enough to take separate account of unequal turns, by multiplying or dividing by the turns ratio as required.

In Fig. 5(b) the primary current  $I_{JK}$  lags the applied e.m.f.  $V_{ab}$  much less than the original 90. Power transformers are usually designed so as to make the magnetizing current ( $I_{LK}$  here) small compared with the other part of the primary current needed on account of full load. That other part has the same phase relative to the e.m.f. applied to the primary as the secondary current has to the e.m.f. given by the secondary. For instance, if the secondary is loaded by a capacitor, a leading current is added to the magnetizing current in the primary.

On the equal-turns-ratio assumption, if a in Fig. 4 is joined to c, d is at the same potential as b and can be joined to it without making any difference. We have, in effect, reverted to our single-winding two-strand coil, and the load current can be regarded as going straight from generator to load, only the magnetizing current flowing via the coil, which is no more than an inductive shunt (Fig. 6). This "distinction without a difference" would be represented in Fig. 5 by making cd coincide with ab, and joining L directly to K.

The next step is to take account of the resistances of the windings. These can be shown separately from

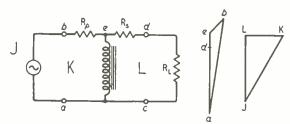


Fig. 7. Circuit of 1:1 transformer with resistive load, and corresponding vector diagram; account being taken of the primary and secondary coil resistances.

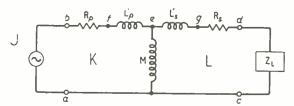


Fig. 8. Elaboration of the transformer equivalent circuit to take account of incomplete magnetic coupling.

the coils, as if they were resistors in series with the primary and secondary coils. In the Fig. 6 representation they are also in series with one another, so if the magnetizing current were small enough to neglect they could be lumped together as one resistance; but as we don't know whether we shall always be justified in neglecting the magnetizing current we shall keep them separate. Fig. 7 shows the modified diagrams. Since  $R_{s}$  and  $R_{L}$  form a simple potential divider, the potential of d is part of the way down from e to a, and on the assumption that R<sub>s</sub> is small compared with R<sub>L</sub> it is shown only a little way below e in the voltage diagram. The voltage  $V_{eb}$  across  $R_p$  must be in phase with the current flowing through it, however, so eb must be drawn parallel to JK. The result is that the phase angle between primary current and generator voltage is slightly reduced. But the more important practical effect of these resistances is to make the secondary terminal voltage Vad less than the primary terminal voltage V<sub>ab</sub>.

#### Leakage Inductance

And now we come to the point of this enquiry: to see what happens when the coupling between the two windings is not 100%. It never quite is, of course, in any actual transformer. If the windings are separate they cannot coincide, so at least a small amount of the flux caused by the primary current fails to link with the secondary winding. One of the objects of using a closed iron core is to make the magnetic path around both coils so easy that very little flux will take short cuts. With care, the leakage flux (as it is called) can be reduced to less than 1% of the whole, so a very good approximation can be made to the theoretical fully-coupled transformer—at least at low frequencies. At high frequencies it is much more difficult, for several reasons: the iron core loses much of its permeability, and very close coupling of the windings tends to cause excessive stray capacitance and loss. Fortunately, very close coupling is seldom wanted in r.f. transformers.

The effect of the magnetic leakage in a transformer

is the same as if the inductance of each winding were divided into two parts: one part common to both windings as in Fig. 7, to represent the flux that links both; and the other completely uncoupled, to represent the leakage flux. Putting two and two together we get—three, as in Fig. 8 (since one inductance in each winding is common to both).

Let us remember that inductance is the name given to the flux-making ability of any part of the circuit. This ability is reckoned as the number of volts the flux would generate if the current in that part of the circuit were made to change at the rate of 1 amp. per sec. When an alternating current of 1 amp. (r.m.s. value) is made to flow, the r.m.s. value of its rate of change is  $2\pi f$  amps per sec, so the back voltage generated by an inductance L is  $2\pi f$ L. To drive the 1 amp against the back voltage, an equal e.m.f. must be applied. The number of volts needed to drive 1 amp. through a resistance equals the resistance in ohms; by analogy,  $2\pi f$ L is the reactance in ohms of the inductance L.

So the effect of leakage thux  $L_p'$  in the primary winding is similar to that of the resistance  $R_p$ , except for the usual 90° difference in phase. And the same for  $L_s'$ . The inductance common to both windings is the mutual inductance, M. And the coefficient of coupling, usually denoted by k, is equal to  $M \lor (L_p L_s)$ , where  $L_p$  and  $L_s$  are the total primary and secondary inductances. This formula applies whatever the ratio of the transformer, but if the ratio is 1:1, so that  $L_p = L_s$ , then  $k = M L_p = M/L_s$ , and  $L_p = L_p' + M$  and  $L_s = L_s' + M$ . When  $L_p = M$ , then  $L_p' = 0$  and k = 1, which means that the coupling is 1000%.

Before we go on to loose-coupled transformers, shall we just draw the general vector diagram for a loaded power transformer with appreciable leakage, on the basis of Fig. 8. Although this case is a "must" in every book and course on electrical engineering, so that one would have thought that by now a standard technique would have been arrived at, there is still the utmost chaos. Some teachers draw an upward arrow alongside the generator and another upward arrow alongside the primary (to represent the back e.m.f. opposing it); some show the primary arrow pointing downward, in the same circuital direction: some show both arrows pointing both ways; some draw two primary voltage vectors pointing in opposite directions; some in the same direction; and so on. No wonder that when a certain teacher tested a class by asking what, in Fig. 3, would be the polarity of the voltage from c to d relative to that from a to b, 11 said the same and 12 said the opposite!\*

It is usually easiest to work backward from the load to the generator. So the first vector to draw in Fig. 9 is ad, representing the output terminal voltage  $V_{ud}$ . The nature of the load  $Z_L$  is unspecified, but a mixed power load is generally somewhat inductive, so we draw the load current vector JL slightly lagging on ad. (If we take the e.m.f. applied to  $Z_L$  in the direction ad, that is to say clockwise, the corresponding direction of current is downwards, that is to say in the direction JL.) Now that we have the phase of  $I_{JL}$  we can draw dg in phase with it to represent the drop in the secondary resistance, and ge leading 90°, for the drop in the secondary leakage inductance. That gives us ae, representing the e.m.f. induced in the

<sup>\*</sup> J. E. Parton, Bulletin of Electrical Engineering Education, No. 7 (Nov. 1951), page 22,

transformer. The current needed to create the flux to induce it is  $I_{LK}$ , which (since it passes wholly through inductance, M) lags  $V_{ae}$  by 90°, and LK is therefore drawn accordingly. (To be quite correct it should be slightly less than 90°, to allow for core losses.) If we like we may mark this vector " $\boldsymbol{\Phi}$ ," to show that it also represents  $\boldsymbol{\Phi}_{LK}$ .  $I_{JK}$ , the primary current, is of course  $I_{JL} + I_{LK}$ , so we join J straight to K to represent it. This shows its phase, enabling us to draw *ef* and *fb*, and so finally to arrive at  $V_{ab}$ , the generator voltage needed to maintain the assumed load conditions.

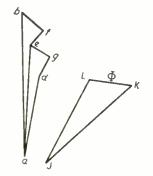
If you have a book on electrical engineering handy, look up its vector diagram for the equivalent transformer circuit, Fig. 8, and compare it with Fig. 9 for clarity and ease of construction.

Just to exercise this new simplicity you might care to redraw Fig. 9 for a highly capacitive load, making JL turn well to anticlockwise of ad. Then you will demonstrate the untruth of the axiom that the part cannot be greater than the whole. But, of course, being radio men, familiar with the workings of tuned circuits, we see nothing new or surprising in this. It is quite normal for the current in one branch of a parallel tuned circuit to be very much greater than the whole current fed in.

#### **Tuned Transformers**

This thought makes a convenient bridge to the loose-coupled tuned r.f. transformer. Its equivalent circuit, Fig. 10, is almost the same as Fig. 8, except for the capacitance in series with the primary, and the explicitly capacitive load. But the proportions of L and M are vastly different. In the power transformer, nearly all the inductance is mutual,  $\mathbf{L'}_p$  and L'<sub>s</sub> being just minor leakage. In the r.f. transformer, nearly all the inductance is L', M being relatively tiny. The condition for "critical" coupling—the coupling between two resonant circuits giving the greatest secondary voltage—is that the reactance of  $M = 2\pi f M = R$ . (So that we don't become involved in complications right at the start, we are assuming that the two tuned circuits are identical.) Now since the reactance of the whole primary or secondary,  $2\pi f(L' + M)$ , is Q times R, M is 1 Q of the whole inductance of either coil-and a typical value for Q is 100. It may seem queer that the biggest output voltage is obtained with something like 1% coupling; it might be expected that it would be with 100%. But close coupling throws the two circuits out of tune and largely destroys their magnification. Any closer than critical coupling makes the single resonant peak divide into two, and it is the deepening hollow between them that makes the output at the original resonant frequency drop.

Fig. 9. Vector diagram corresponding to Fig. 8, for a transformer having comparatively little magnetic leakage.



Just before drawing the complete vector diagram for Fig. 10 it may be a good thing to take note of the characteristic shape of the diagram for a single tuned circuit, as shown in Fig. 11(a). The current in a series tuned circuit is a maximum at resonance, so we make JL fairly long. But R in a good tuned circuit is relatively small, so notwithstanding the maximum current we draw a short line dg in phase with JL. The voltages across C and L are Q times as great however;  $V_{ge}$  leading and  $V_{ad}$  lagging the current by 90°. (Even if we had made dg quite small, a Q of 100 or more would put a and c well off the paper—and probably off the desk as well !--so a somewhat lower Q will have to do.) The result is a long thin rectangle, with a and e so placed as to show that  $V_{ae}$ , the injected e.m.f., is equal to and in phase with  $V_{dq}$ . This picture fits all that one knows about series resonant circuits—I needn't go into all the details. The only point to note is that if R and L in the circuit changed places the voltage diagram would be as in Fig. 11(c). Seeing that in reality R and L are mixed up together, it is purely a matter of choice which order we show them in the equivalent circuit; personally I think (b) is a clearer and more recognizable picture than (c).

We already have a good start towards the vector diagram for the coupled circuits, of which Fig. 10 is the equivalent circuit. As you see, I cunningly lettered Fig. 11 so that it corresponds with the secondary, the "generator" being M, which induces the necessary e.m.f. There is one other important difference however: the reactance of L' is not exactly equal and opposite to that of C, for L' is L less M. Now we have made the reactance of M equal to R, so the amount by which eg must be shortened is equal to dg, representing the drop across R (Fig. 12). The vector ae is now the diagonal of a square instead of one of its sides, so is  $\sqrt{2}$  times as long as before;

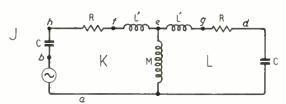


Fig. 10. Modification of Fig. 8 equivalent to a loose-coupled tuned r.f. transformer with identical primary and secondary coils.

Fig. 11. (a) is a single tuned circuit; (b) the corresponding vector diagram; and (c) the modified form of the voltage diagram if L and R in (a) changed places.

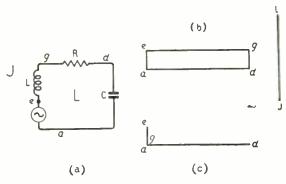


Fig. 12. Vector diagram for secondary circuit only of Fig. 10 at resonance.



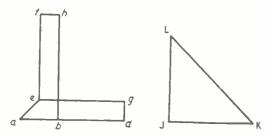


Fig. 13. Complete vector diagram for Fig. 10, at the resonant frequency.

and its phase is 45° behind. The current through M is therefore  $\sqrt{2}$  times  $I_{JL}$  (it includes  $I_{JK}$  as well), and of course 90° behind  $V_{ea}$ . So we know the length and direction of KL, which we draw accordingly, Fig. 13. This gives us  $I_{JK}$ , the primary current, and we can now proceed to complete the diagram by drawing first ef, 90° ahead of JK, and equal to eg (for JK = JL); then fh in phase; then finally hb 90° behind JK, and equal to ad.

This complete picture has been arrived at without any deep thought, just by following exactly the same rules as for previous examples—the three fundamental phase relationships (for R, L and C) and the two prescribed rotations for voltage and current. Apart from following these rules correctly, there has been no need to worry about which way arrows should point, or whether we have the vectors in the right directions. And the diagram is simplicity itself to interpret. We see at once the two slim rectangles representing the two tuned circuits, and that they are at right angles to one another, showing that the voltages across them are 90° out of phase-which was what we set out to do. We see that the primary current is in phase with the injected e.m.f., which therefore sees a resistance load (as of course it should, at resonance). Since fh and dg are only half as long as ab, we see that the primary and secondary currents and the voltages across the circuits are half what the same input e.m.f. would produce across a single tuned circuit with the same characteristics. (If you are not quite sure about this, take away the secondary L, R and C from Fig. 10 and draw the voltage diagram for what is left. It should be a rectangle standing on ab, twice as tall as bh).

If you have become intrigued by all this you probably won't be kept from going on with it, drawing diagrams for less and more coupling than critical, and in doing so will learn (or confirm) quite a lot about coupled circuits. So far, I haven't come across a conventional vector diagram for critically-coupled tuned circuits. Perhaps it is such an unintelligible mess that no one dared publish it!

#### **BOOKS RECEIVED**

Microwave Theory and Techniques, by H. J. Reich, P. F. Ordnung, H. L. Krauss and J. G. Skalnik. Textbook for advanced students covering basic field and electron motion theory and its application in the design and operation of practical microwave generators, amplifiers, waveguides and radiators Pp. 901+XIII; Figs. 602. Price 75s. Macmillan and Company, St. Martin's Street, London, W.C.2.

Grundlage der Verstärkertechnik, by Hans Bartels. Revised and enlarged fourth edition of a monograph on the design of feedback amplifiers and their auxiliary stages, with an extensive bibliography. Pp. 279+XII; Figs. 181. Price DM20. S. Hirzel Verlag, Stuttgart, Germany.

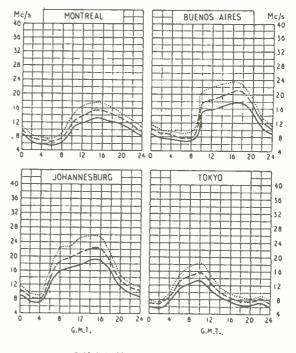
Electrical Measuring Instrument Practice by E. H. W. Banner, M.S.E., M.I.E.E., F.Inst.P. Survey of the types and designs of pointer instruments and recorders and their uses, including applications to the measurement of non-electrical quantities. Pp. 130; Figs. 50. Price 15s. United Trade Press, 9 Gough Square, London, E.C.4.

#### **Short-wave Conditions**

Predictions for September

THE full-line curves given here indicate the highest frequencies likely to be usable at any time of the day or night for reliable communications over four long-distance paths from this country during September.

Broken-line curves give the highest frequencies that will sustain a partial service throughout the same period.



FREQUENCY BELOW WHICH COMMUNICATION SHOULD BE POSSIBLE ON ALL UNDISTURBED DAYS

---- PREDICTED AVERAGE MAXIMUM USABLE FREQUENCY
FREQUENCY BELOW WHICH COMMUNICATION SHOULD BE POSSIBLE FOR 25% OF THE TOTAL TIME

## Neon Timers

#### Simple Circuits Based on CR Time Constants

By B. T. GHLING

N radio work neon tubes are used mainly as voltage stabilizers and occasionally as saw-tooth generators, but they also have a very useful field of application as interval timers. Two different types of timers have recently been built by the writer and they are described below as examples of what can be done and also as exercises in simple relay switching. A very good article on relays by T. Dawson appeared in the January, 1953, issue of Wireless World and this should be consulted.

The basic neon timer circuit is shown in Fig. 1(a). A large capacitor is charged slowly from a high voltage through a high-value resistor. The voltage across the capacitor will rise until it reaches the striking voltage of the neon, which will fire and discharge the capacitor until the extinguishing voltage of the neon is reached. The relay in series with the neon will operate and close its contacts and this will complete the discharge of the capacitor. The relay will then drop off, opening its contacts, and the whole operation will recommence. This cycle of events will continue as long as the high voltage is applied. A small resistor of a hundred ohms or so is connected in series with the contacts to prevent a too rapid discharge of the capacitor with consequent sparking.

A disadvantage of this circuit is that only the small portion of the charge of the capacitor between the striking and extinguishing voltages of the neon flows through the relay coil, the rest being dissipated in the series resistor. The circuit can be rearranged as Fig.

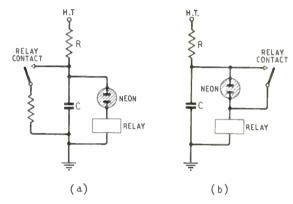


Fig. 1 Above. Basic neon timer circuit (a), with improved arrangement (b) giving a more positive action.

1(b) to overcome this. When the neon strikes the relay operates and its contacts short-circuit the neon; the capacitor then discharges through the relay and a more positive action is achieved. This latter method in a slightly modified form is used in both of the instruments to be described.

The first one is an interval indicator, shown in Fig. 2. The object of this instrument is to give an audible indication at the end of any half minute from one to two-and-a-half minutes. It was developed to time the

operations of a cleaning machine used by watch repairers in which the parts to be cleaned are immersed in different fluids for set times. It is push-button operated for simplicity of working and uses one relay. This relay has windings of 50 and 1,500 ohms and three sets of contacts, two being change-overs and the third a single make which is arranged to close at low spring pressure before the others start to move. The operation is as follows. Assume push-button 1 is pressed. C will charge through R<sub>4</sub>. When the neon strikes

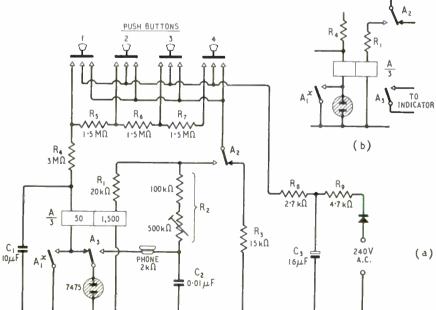


Fig. 2 (Left). Circuit of interval indicator giving an audible note at the end of any half minute from one to two-and-a-half. x indicates early operation.

the current through the 50-ohm coil will cause the relay to start to operate and A<sub>1</sub> will close, short-circuiting the neon. The entire remaining charge in the capacitor will then flow through the coil, causing the relay to operate completely. A<sub>2</sub> will change over, locking up the relay through its 1,500-ohm coil and R<sub>1</sub>. A<sub>3</sub> will change over, transferring the neon to the oscillator circuit R<sub>2</sub>C<sub>2</sub> and a note will be heard in the telephone earpiece. This note is adjusted by the variable portion of R<sub>2</sub> and will continue until any one of the projecting buttons is pressed, releasing the operated button. The supply voltage is thus removed, the relay drops off and the instrument is ready to be operated again.

The values of the resistors in the high voltage circuit,  $R_3$ ,  $R_8$ ,  $R_9$ , are chosen to give an operating value of 150 volts at the push buttons,  $R_3$  being chosen to pass the same current as the holding and tone generating circuits combined. In this instrument, close accuracy of timing was not essential and so no attempt was made to stabilize the high voltage. The values of the capacitor and resistors in the charging circuit give times of 1,  $1\frac{1}{2}$ , 2 and  $2\frac{1}{2}$  minutes. This depends on the value of the high voltage and it may be necessary to alter the value of  $R_8$  to obtain exact timing on an individual instrument.

A Post Office type 3000 relay is used and the values of the windings are not critical. The first coil will work at any value up to 1,000 ohms, and provided appropriate alterations are made to R<sub>1</sub> any high resistance value will suit the second coil. A point to bear in mind is that the second coil has only to hold the armature after it has been operated, therefore a very much lower value of current is called for than would be needed had the relay to be operated by this winding.

The method of generating the indicating signal is a simple one calling for the minimum of additional components but the circuit can be rearranged as shown in Fig. 2(b) to switch in an external indicator, either sound or light.

The second instrument (Fig. 3) was designed to switch on the lamp of a photographic enlarger for any predetermined time with close accuracy. It is operated by a telephone key-switch having a central off, one locking and one non-locking position. Two relays are used, one having a 50-ohm coil and change-over contact. The other has a 2,000-ohm coil and three contact sets, two make contacts and a change-over. It is a twostep relay, the first step being controlled by B<sub>1</sub> which closes at light spring pressure before the other two sets move.

The operation is as follows. The key-switch is pressed in its non-locking position, closing its contacts K<sub>1</sub> K<sub>2</sub>, the contacts K<sub>2</sub> being adjusted to close a fraction before K<sub>1</sub>. Relay B will operate, but as K<sub>2</sub>

#### TABLE I

The resistance values are selected to give an increase of approximately one half per step in a ratio series familiar to photographers as f numbers.

			-,			-			:		
Seconds	1	1.4 2	2.8	4	5.6	8	11	16	22	32	45
Kilohms	62.5	25 37	.5 50	75	100	150	190	310	400	600	800
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has put  $R_4$  in shunt with its coil there is only sufficient power to close  $B_1$ . This state of affairs will continue until the key-switch is released. The shunt is then removed and full current passed through the relay over  $B_1$ , operating the relay fully.  $B_3$  closes, connecting the enlarger lamp across the mains.  $B_2$  changes over, connecting the resistor  $R_1$  to the capacitor, which starts to charge. When the neon strikes relay A operates.  $A_1$  changes over, disconnecting relay B which drops off and the enlarger lamp is extinguished.  $B_2$  changes over, disconnecting the charging circuit and completely discharging the capacitor through  $R_2$ , and the apparatus is ready to be used again.

The locking position of the key-switch is to enable the enlarger lamp to be switched on permanently for setting-up and focusing operations. The high voltage supply is stabilized by a tube, type VR150/30, and an accuracy better than 5 per cent is obtained from one exposure to another.  $R_1$ , which is the time control, can be a variable resistor of  $2\,M_2$  calibrated in seconds, but a preferable method is to use a Yaxley type switch with fixed resistors so chosen that each step increases the time by one half of the previous one. Resistor values for this are given in Table I.

A Post Office type 3000 relay is used for B and since differences in spring pressure and armature clearance will alter its characteristics the values of  $R_a$  and  $R_a$  may need modification. The method of setting up is as follows. With  $R_a$  disconnected a value for  $R_a$  is found which will give a good positive action to the relay when the key-switch is depressed. This

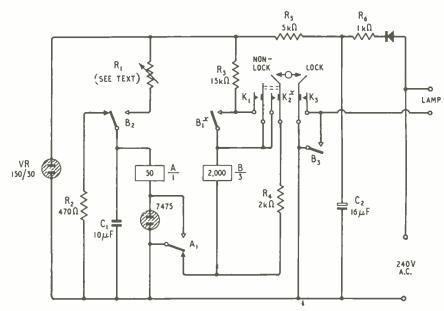


Fig. 3. Timer for switching on a mains circuit for any predetermined time with close accuracy.

value is wired in circuit and a variable resistor connected in place of R4. A value for this is found which will allow the relay to operate only to close B, when the key-switch is operated. Finding the value of these resistors in this way also permits the use of relay coils having a resistance other than 2,000 ohms. Relay A is a Post Office type 600 and its resistance is not critical; values of up to 1,000 ohms can be made to

In the examples shown the high voltage supply is obtained directly from the mains. This is a simple and efficient method but it must be very strongly emphasized that either the instrument must be in a case made entirely of insulating materials with no metallic controls exposed, or, if a metal case is used, no wiring must be allowed to come into contact with it and it must be securely earthed. Rectification is by a small 24-section selenium unit and smoothing is of the simplest, consisting of resistor and a single 16-µF capacitor in each case. The maximum current drawn in either is less than 20mA.

A point of importance to be observed in all timers is that the charging capacitor must be of high-grade paper construction with very low leakage and, in fact, all parts associated with the charging part of the cir-

cuit must be of the highest insulation.

## Training in Television Servicing

By G. N. PATCHETT,\* Ph.D., B.Sc., A.M.I.E.E., M.Brit, I.R.E.

Special Apparatus for Practical Demonstrations

N the training of television service technicians there are a number of problems which do not occur in most other subjects. The course is essentially a craft type and the people normally attending such courses have a limited academic background, so that the subject must be dealt with in as simple and as practical a manner as possible. Unfortunately, a modern television set is a complicated piece of equipment and is tending to become more so with the introduction of efficiency diodes, Band III, etc. It is extremely difficult to explain the operation of many television circuits without going into mathematics and complicated circuit theory. Although a television servicing technician is only required to repair sets and not design them, the author finds it difficult to understand how a satisfactory repair can be made without at least an elementary knowledge of how the circuit operates and, what is equally important, what will happen under various fault conditions. It is, of course, possible to cure many faults by a trial and error method, but this may be very time-con-suming and expensive. Experience of typical faults on particular models is, of course, most valuable but is something which cannot be easily taught.

In view of the difficulties of explaining many circuits the author considers that practical demonstrations are the ideal way and essential to the teaching of this subject. This idea is used to a great extent

Fig. 1. Experiment board of frame blocking oscillator.

at Bradford Technical College, where the course consists of two nights per week for a period of two years. One night is devoted to lectures and demonstrations and the other night to practical work by the students themselves. Turning to the practical work, this is divided into two types, (a) experiments on simple circuits, (b) actual fault finding on commercial television receivers. The work done during the first year of the course consists of type (a). For this purpose a number of experiment boards have been constructed, each board consisting of a simple circuit of a section of a television receiver, e.g., a time base or a synchronizing separator. These boards are designed so that they may be used for three purposes:-

- 1. Experiments on the general operation of the circuit. Voltages, waveforms, etc.
- 2. The effect of faults on the general operation of the circuit and on the voltage readings and waveforms.
- 3. The actual location of faults on these circuits.

A typical board is shown in Fig. 1. The "board" consists of hardboard covered with drawing paper on one side. The circuit is drawn on this paper which is then covered with celluloid or, rather better but more expensive, Perspex. More recently a transparent plastic covering has been used which can be secured to the paper by heat. The components of the circuit are fastened to the back of the board and are con-

AME OLCURING DECL - TIME BASE

<sup>\*</sup> Bradford Technical College.

nected to small terminals which are located in the correct positions on the circuit diagram. In series with most components are connected two terminals which are normally joined together by a link. By removing the link the component is effectively open circuited. The board is most useful to show the operation of the circuit, and voltage readings and oscillograph waveforms may be taken at various points. Since these are taken at points on an actual circuit diagram it is easy to see just what voltage is being measured. By removing the links, one at a time, the effect of open-circuited components can be seen on both voltage readings and oscillograph waveforms. The effect of short circuits may be seen by connecting appropriate terminals together.

#### Fault Finding Scheme

In order that the same board may be used for actual fault finding the links are of special construction. They are made of a sandwich of Leatheroid and copper foil (cemented with Bostik) and are used with the Leatheroid upwards. For fault finding, a number of dummy links are available which are constructed in a similar manner but a slot is cut in the copper foil so that, although the circuit is not completed, the link appears the same as normal. Short circuits may be placed on the circuit by shorting links fitted with crocodile clips on the underside of the board, the students being instructed not to turn the board over. From the point of view of fault finding these boards have the advantage that they can be used repeatedly, whereas when soldered connections are broken and remade to place faults on circuits the apparatus soon becomes useless, owing to damage to components, soldering tags, etc.

In order to operate these boards a coaxial cable is fed to each position in the room. Each position may be supplied with any of the following:—

- 1. B.B.C. signal from aerial.
- 2. R.F., modulated with test pattern.
- 3. Video signal of test pattern.
- 4. Composite synchronizing pulses.
- 5. Line pulses.
- 6. Frame pulses.

The last four are fed through an amplifier and cathode follower unit on each position so that the output may be varied in amplitude and either polarity may be obtained by means of a switch. These supplies and boards have been found invaluable for demonstrations and save much time in connecting up circuits when wishing to give demonstrations. If much connecting up is required in order to give a demonstration the general result is that the demonstration does not get shown.

At present 33 such boards are available and it is hoped to make more in the near future. For the second part of the practical work a number of commercial television receivers are available and also two sets constructed at the college. One is a normal circuit

(largely Wireless World design) arranged with separate chassis for the various sections while the other is a projection set. Faults of various types are placed on these sets and the students get experience in locating them.

Apart from the normal equipment of cathode-ray oscillographs, valve voltmeters, signal generators, etc., a number of special pieces of equipment are available which are most useful. The first is a commercial oscillograph with d.c. amplifiers and an X trace which can be expanded to approximately five times the screen diameter. This is invaluable for showing the operation of d.c. restorers and of circuits where the d.c. component is important.

The second is a television waveform display apparatus which was constructed at the College and is described in more detail elsewhere. The apparatus is essentially a special cathode ray oscillograph arranged so that the waveform of 2 to 250 lines of a television picture may be shown. The lines can be varied so that any selected ones may be shown and a pulse is available for brightening the corresponding lines on a picture on a normal receiver. This is particularly useful for showing the operation of synchronizing separators, which are almost impossible to demonstrate on a normal cathode-ray oscillograph. Fig. 2(a) shows the frame synchronizing period on even frames taken on the signal from the pattern generator, while (b) shows the effect of integration of the frame pulses. In this the build-up of voltage can easily be seen but it is quite impossible to show anything of this nature on an ordinary oscillograph since the frame synchronizing pulses occupy only a small fraction of the total frame time. The apparatus can, of course, be used with advantage for fault finding.

#### Camera Equipment

Recently a complete television camera has been constructed to help in clarifying some of the mysteries of the camera side of television, which cannot normally be seen by students outside the London area. The camera itself consists of a Pye Staticon miniature pickup tube with a two-valve pre-amplifier, a cathode follower and a pulse amplifier. It also contains an electronic view-finder with corresponding time bases and video amplifier. The camera is fed from a control unit which is mounted on two racks. These contain the power supplies, video amplifiers, time bases, pulse generator and monitor tube. The signal from the preamplifier is fed by coaxial cable to the video amplifier on this control unit. After amplification and frequencyresponse correction, the signal is fed to a clamp circuit to set the black level, and then to a blanking amplifier which suppresses the signal for the required periods. The synchronizing signal is then added to give a complete video waveform. The control unit also contains a small r.f. oscillator and amplifier which is modulated

Patchett, G. N. "A Television Waveform Display Apparatus," Electronic Engineering, May and June, 1953.



Fig. 2. (a) Video signal of pattern generator during even frame synchronizing period. Negative picture signal. (b) The effect of integrating the synchronizing pulses during the frame synchronizing period. Positive pulses.

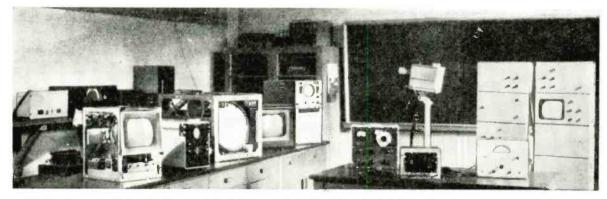


Fig. 3. A corner of the television servicing laboratory at Bradford Technical College, showing camera and control unit.

with this video signal so that the camera may be used to operate a normal commercial set.

The camera is most useful for showing effects of d.c. component, definition, etc., which are difficult to show on a normal pattern-generator signal. It is designed to give a correct B.B.C. synchronizing signal and will resolve at least the 2-Mc/s bars on Test Card C. Built into the same control unit is a monoscope which enables a Test Card C pattern to be produced when required. Some further work is required on this section to give complete satisfaction but it will be a most useful addition as this signal is not available (apart from a few minutes) during normal class time.

Fig. 3 is a general view of part of the laboratory with the television camera control unit and other apparatus.

Although much time and effort have been devoted to this work it is felt that it is well worth while if it enables students to obtain a better understanding of the working of a television receiver. With the introduction of more channels and, at some later date, colour, the complexity of the television receiver will increase and it will be even more difficult to give satisfactory training. The servicing trade is already short of technicians and it will become more important to have highly skilled people available as more sets are installed and as their complexity increases.

#### MODERN AIRFIELD RADIO

A NEW civil airport near Dungeness, known as Ferryfield, opened recently by Silver City Airways, is said to be the first airfield in the world planned especially to deal with the transport of vehicles, as distinct from passengers or freight. It will eventually replace the cross-channel car ferry now operating from Lympne.

Its interest from our standpoint is that, being a new airport, it has no legacy of existing radio facilities that must be integrated with new services and the whole radio and radar installation has been planned from the ground up, so to speak.

First and foremost is the air-toground communication; this is carried out primarily on two v.h.f. channels in the 118- to 132-Mc/s aircraft band by means of modified T1131 crystal-controlled transmitters of 50 watts telephony rating and four Mar-

The flying controller's desk at Ferryfield is typical of the type now installed at civil airports. Facing the controller is a panel of instruments giving wind velocity, time and barometric pressure information. On the left is a recessed loudspeaker to which all receivers are connected, and on the extreme left is the runway's lighting control. Convenient to the controller's left hand is a panel carrying switches and indicator lights for remote control of all radio services. A hand telephone set is in a recess below.

coni HR82 receivers. Two transmitters and receivers are in service and two on stand-by. There are also two h.f. transmitters (one operational and one stand-by) for single spot-frequency operation in the 2- to 25-Mc/s band. They are rated at 250 watts telephony and 350 watts c.w. telegraphy and have been installed to handle long-distance communications in connection with charter work. There are two h.f. receivers of Racal design.

Two aids to navigation are provided; one is a v.h.f. direction finder operating on the null-signal aural



principle and employing a pair of rotatable dipoles with switched reflectors to give "sense." Bearings are taken on the normal R/T transmissions from the aircraft. The other navaid is a Decca 424 radar with the scanner and radio-frequency head located about 400 to 500 yds from the control tower. The i.f. signal is "piped" to the tower where, in a room fitted with tinted glass windows, are two c.r. tube display units, with separate i.f. receivers to allow for independent operation. Thus one can cover the distant approaches out to 25 miles or so, while the other can give an expanded picture of aircraft movement within a mile or two of the airfield.

Radio-telephone facilities are provided in this room to enable aircraft to be "talked down" to within visual distance of the runways under conditions of poor visibility. Here is located also the v.h.f. direction finder so that all the radio navigational aids are conveniently

Not yet installed, but planned, is a v.h.f. radiotelephone system for keeping in touch with all airport vehicles. It, and all the other radio services, will be operated from the controller's console as is now customary practice at all airfields, large and small.

The radio and other airport equipment at Ferryfield was planned and installed by Racal, Ltd., and, of course, is approved by the Ministry of Transport and Civil Aviation.

#### International Technical **Questions**

PROFESSOR BALTH. VAN DER POL, director of the International Radio Consultative Committee (C.C.I.R.), has sent us a copy of Volume I of the Proceedings of the VIIth Plenary Assembly of the Commit-tee which was held in London last September. Engineers and technicians interested in the international aspects of technical radio questions will find the book (which is available in English and French) of considerable interest.

Volume I contains the full text of 90 recommendations, reports and resolutions adopted by the assembly. It also gives full details of the study programmes and questions which will be investigated during the three years before the next assembly, to be held in Warsaw in 1956. These investigations are carried out by the study groups of each of the member countries of the International Telecom-munication Union of which the C.C.I.R. is a permanent organ. It is as a result of the papers submitted by these national study groups that the recommendations and further study programmes are arranged.

As the book also contains the texts of those reports, etc., adopted at the previous two plenary assemblies which are still valid, it forms a complete collection of the

current C.C.I.R. documents.

Some idea of the diversity of subjects covered in this 406-page book may be gained from the following summary of some of the entries in the 20-page index:-

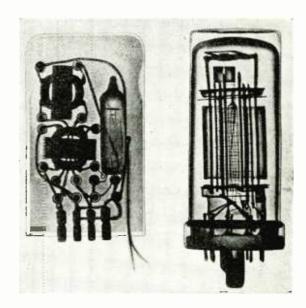
Propagation: Ionospheric, tropospheric and ground-wave. Receivers: Noise and sensitivity; selectivity; frequency stability;

Recording: Standards for sound on discs, film and tape. Television: Recording, polarization, standards conversion, picture and sound modulation, combining monochrome and colour.

Two further volumes covering the reports of the study group chairmen and the director (Vol. II), and the minutes of the plenary assembly (Vol. III) will be published later.

Volume I is obtainable from the Publications Department, International Telecommunication Union, Palais Wilson, Geneva, Switzerland, price 23.10 Swiss francs.

#### ELECTROSTATIC RADIOGRAPHY



THIS picture shows an x-ray image of a valve and a potted circuit obtained by a new process called xeroradiography which dispenses with ordinary photographic techniques. The method is cheap because the plates can be used over and over again and is very quick—the radiograph being ready in less than a minute from the time of exposure.

In place of the ordinary photographic plate a thin film of selenium on a conductive backing plate is used, and this is charged electrostatically. On exposure to the x-rays the charge is modified according to the pattern of the object being radiographed, so that an electrostatic image is obtained. This image is then made visible by spraying on to the plate a very thin film of charged powder, which adheres in accordance with the charge distribution. For re-use it is only necessary to wipe the plate clean and recharge.

The method has been developed by Ferranti, who say that it is possible to obtain pictures with an even finer grain than in conventional x-ray photographs.



#### Problem Picture

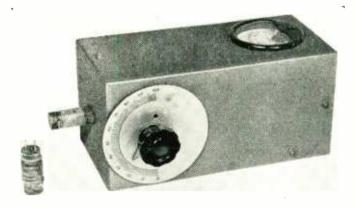
What is it? Clue: the external form is strictly functional. No, it is not a r.f.-heated pressure cooker, but the latest transmitter-receiver for ships' lifeboats, made by Marconi Marine.

The "Salvita" set, as it is called, is waterbroofindeed, submersible—and is powered by a handdriven generator. It complies with the 'atest Government specification, and operates on 500 kc/s and 8.364 Mc's.

# COMPACT GRID-DIP OSCILLATOR

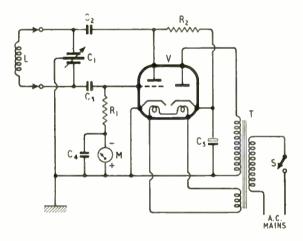
By G. P. ANDERSON

(Amateur Radio Station G2QY)



#### A Useful Method of Finding the Resonance Frequency of Coils and Circuits

URING recent years the increasing appreciation of the value of the grid-dip oscillator as an item of test gear has been reflected in the number of articles published describing different varieties of the species. The only excuse the present writer has for offering yet another contribution on the



Circuit diagram of the grid-dip oscillator described in the text.

subject lies in the use of a triode-diode v.h.f. mixer valve as an oscillator and mains h.t. rectifier.

Basically the GDO comprises an oscillating valve tunable over the desired frequency range, and including a meter to show the rectified current flowing in the grid circuit. The oscillator coil is usually placed on the outside of the unit in order to permit it to be brought near to the circuit under test. When the test circuit and the GDO are tuned to the same frequency, power is absorbed from the oscillator causing the grid current to fall; hence its name.

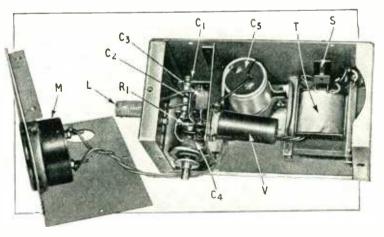
An examination of the makers' characteristics for the diode part of the Mullard EAC91 shows that it is designed with limiting values of 50 volts between heater and cathode, and a cathode current of 5 mA. Using the triode section as an oscillator with approximately 50 volts h.t., the current taken is well within this limit, and the valve may be made to oscillate easily up to frequencies of the order of 220 Mc s, using components suitable for operation at lower frequencies as well. The particular model shown in the photographs is designed to cover the range from 5 to 160 Mc s with seven coils, which are arranged to plug in to the end of the unit.

The mains transformer may be quite small as it supplies about 2 watts only, and the smoothing shown in the circuit diagram, comprising  $C_5$  (32 $\mu$ F) and  $R_s$  (10 k $\Omega$ ), is adequate for the purpose. The

#### LIST OF COMPONENTS

$C_1$	20 + 20 pF variable
$C_2, 3, 4$	100 pF silvered mica
C 5	$32 \mu F 50 V$ wkg.
$R_1$	22 kΩ ¼ W
$R_2$	10 kΩ ½ W
V	EAC91 (Mullard)
A	250 μA meter
L	See table
T	Mains transformer;
	secondaries 50 V at
	5 mA, 6.3 V at 0.3 A.

On the right the layout of the parts inside the box is shown with the top and one side removed.



signal produced, if listened to in a receiver, is modulated very deeply with 50 c/s, but this is no disadvantage in using the instrument; it is in fact very useful for identifying the signal when accurate frequency checking is desired.

The model shown is built into a box measuring  $7 \times 3\frac{1}{4} \times 3\frac{1}{4}$  in, which is a convenient size for holding in the hand. It could be made smaller, but was originally built as a companion to a self-contained battery model, which used one triode of a 3A5 in a similar oscillator circuit, driven by hearing aid batteries. The only external difference was in the replacement of the mains toggle switch by a springloaded push button, conveniently placed for thumb operation. This switch was fitted in the heater

COIL TABLE

Coil	Approx. Freq. Range	Turns	Winding Length	Wire
A B C D E F	5-9 Mc s 9-15 ,, 14-24 ,, 23-40 ,, 37-63 ,, 60-110 ,, 100-160 ,,	681 391 241 151 821 51	ain  ,, ,, ,in lin	36 s.w.g. enamel 28

The coils are each wound on 1-in lengths of ½-in diameter Paxolin rod, and are terminated on two 20 s.w.g. tinned copper wires inserted in the ends, spaced to suit the socket on the grid-dip oscillator. In the original model, the socket is a diode valveholder (Base Type B3G).

circuit in order to prevent the batteries being run down unnecessarily.

Details of the coils, and the approximate ranges covered, are shown in the table. If use at the upper end of the range only is contemplated a smaller capacitor at  $C_1$  permitting a different layout to secure shorter leads in the oscillator circuit would probably enable the GDO to be used at even higher frequencies. In passing it may be mentioned that tests have been carried out with 120 volts applied to the rectifier without any signs of distress; with the heater left unearthed, this voltage does not appear across the heater and cathode, but only between the two cathodes, and, of course, the cathode and anode of the diode.

For completeness, a few notes on the use of the GDO may be added. Each range should be calibrated, conveniently by comparison with a suitable receiver, but it should be kept in mind that such calibration is only approximate, since coupling to a tuned circuit tends to "pull" the oscillator. In use the coil of the GDO should be brought near to the circuit under test, and the tuning condenser varied until a decrease in grid current i. indicated. The coupling should then be reduced, by moving the GDO away, until the smallest observable "dip" is obtained; in this way, the "pulling" of the oscillator frequency is reduced to a minimum. If more accurate knowledge of the frequency than is given by the GDO calibration is required, the oscillator frequency may be checked on a receiver, maintaining meanwhile the coupling to the circuit under test.

Apart from the obvious uses in adjusting tuned circuits in receivers, transmitters and such like, the GDO may also be used to find the resonant frequencies of aerials, guy-wires, etc.

#### FITTING CAR RADIO

IN order to encourage radio dealers not having facilities for handling motor cars to take a more lively interest in car radio, Pye Telecommunications are organizing fitting depôts throughout the country to which dealers can send their customers for skilled and prompt fitting of the latest Pye car radio receiver. At the time of writing depôts are functioning in Birmingham, Cambridge and Manchester.

To facilitate speedy installation in the widest possible range of cars the new set is made in three separate parts; radio tuner, combined output and power unit and loud-speaker respectively. The first and last only need be in the body of the car and space can generally be found somewhere under the bonnet for the power unit, where, incidentally, it will be within easy reach of the battery in most cases.

The tuner is a complete three-valve, two-waveband superhet less output stage, and is designed to have a reasonably small frontal area so that it can be accommodated conveniently in the space provided on the dash board, or immediately below without obstructing either the driver or passenger.

Tuning and the combined volume/on-off controls are fitted with normal type knobs and disposed on either side of a rectangular dial, while the tone control and wave-

change switch have disc-shaped "dollies" for finger or thumb operation and are let into the lower part of the dial. There are separate scales for medium and long waves with illumination for night-time operation. The price of the new set, including aerial, purchase tax and fitting fee is £28.



Wireless World, September 1954

Right: To facilitate installation the new Pye car radio receiver is broken down into the three units shown here.

## Manufacturers' Products

NEW EQUIPMENT AND ACCESSORIES FOR RADIO AND ELECTRONICS

#### Strip Connectors

THE plug and socket connector illustrated is one of a new range introduced by Bulgin for the electrical interconnection of individual items of a larger equipment. A typical application would be where several chassis are mounted in a rack or a cabinet and slide in and out on guide rails for maintenance and servicing. The socket part can be fixed to the back of the chassis and the plug part (or vice versa) on the back of the rack or cabinet. When the chassis are pushed fully home the two parts mate together and the electrical interconnections are automatically made. To ensure correct alignment of the pins and sockets, individual sockets



Bulgin 3-way plug and socket strip

allowed a free lateral movement of  $\pm 5$  deg.

Plugs and sockets are mounted on strips of good-quality bakelized material, the pin spacing being 1% in. Pins are hollow and the leads are secured by tip soldering as in the older-type valve pins. Sockets are fabricated from resilient metal strips, bent to shape, and have integral soldering tags.

These new connectors are available in 3- to 6-, 8-, 10- and 12-way types and prices range from 1s 1½d for a 3-way plug and socket to 3s 6d for a 12-way.

The makers are A. F. Bulgin and Co., Ltd., Bye Pass Road, Barking, Essex.

#### Auto-alarm Receiver

THE "Seaguard" auto-alarm receiver is intended to take the place of the ship's radio officer when he goes off duty. It maintains a constant watch on the marine distress frequency of 500 kc/s, and, in the event of a distress signal conforming to the international standard of 12 four-second dashes at one-second intervals being received, operates an alarm. In order to allow for slight mis-tuning of the caller's transmitter the Seaguard receiver is pre-tuned



Marconi Marine Seaguard auto-alarm equipment with chassis withdrawn for inspection.

for reception over the band 490 to 510 kc/s.

A receiver of high sensitivity is employed and elaborate precautions are taken to ensure that only a genuine distress signal of the agreed form will actuate the alarm mechanism, which comes into operation after the fourth dash of correct duration and spacing.

The Seaguard consists of two main units, receiver and power supply, both housed in a single cabinet with draw-out chassis for servicing. A built-in meter provides means for checking all valve feed currents and failure of either unit is indicated by one of two lamps lighting up; also the alarm bells ring.

The equipment is supplied by the Marconi International Marine Communication Co., Ltd., Marconi House, Chelmsford, Essex.

#### NON-FERROUS METALS

ELECTRICAL, physical and mechanical properties of non-ferrous metals and alloys are given in the 472-page "Metal Industry Handbook and Directory, 1954," which also includes summaries of relevant British Standard specifications, compositions and melting points of solders and a classified directory of products. The volume, which is in its 43rd year of publication, is published by the Louis Cassier Company, Ltd., Dorset House, Stamford Street, London. S.E.1, price 21s.





This latest, most striking addition to the TRIX range combines fidelity of reproduction with adequate power for Independent bass and treble tone controls, together with the mains switch and illuminated lamp, are fitted to the attractive control panel which is connected to the power amplifier by a single multiway cable. High and low gain inputs, for use on all types of pick-up, and speaker output tappings for 15 and 3 ohms are incorporated. For the critical enthusiast this is an ideal amplifier of remarkable value.



TRIXADIO, WESDO, LONDON.

## RANDOM RADIATIONS

By "DIALLIST"

#### Sporadic E

YOU'VE probably had your whack of television interference by sporadic E reflections at one time or another in the course of the present summer (sic). "Clouds" of intense ionization, forming sporadically in the E-layer and capable of propagating long-distance interference with our TV services were forecast as most likely to occur in the daytime between May and August by T. W. Bennington,\* whose work is well known to Wireless World readers. His forecast has been amply borne out by what happened this year. At one time or another from early May onwards severe modulated r.f. interference during daylight has been reported from many parts of the country. Unless there's some interesting event, sporting or otherwise, on tap, I don't often use my receiver during the afternoon. Hence it wasn't until early in July that I saw sporadic E interference in full swing. It began more or less mildly with the appearance of a number of faint whitish lines on the screen. They were not stationary, but jittered about, sloping now from left to right and now from right to left between the top and bottom of the screen. The lines grew rapidly more obvious and "greys" appeared between the "whites." Meantime, they became steadier and less inclined this way or that. Watching them was very trying to the eyes, but I was too fascinated to switch off. So far as I remember, the next development was sudden: the lines became alternate black and white vertical bars of equal width, covering the entire screen. They were at one time so steady that I could count them: 24 black bars, with jagged edges indicating modulation.

#### Long-Range TV

TELEVISION is full of surprises. If you were asked what were the chances of obtaining consistently good pictures at a seaside town, 70 odd miles from the nearest transmitter and with huge hilly areas inland, you'd probably reply without hesitation that they were not very bright. That's certainly what I should have said about Torquay—if I hadn't just

returned from a visit to friends who live there and seen for myself the quite excellent pictures that they regularly have on their screen. Good reception is rare in the more lowlying parts of the town; but, given an efficient receiver and a high 3- or 4element Yagi array, pictures in the higher parts are very nearly up to the standard of those obtainable in a normal service area. When you think of Torquay you are apt to picture it as lying under the shadow of Dartmoor. You might even feel that the direct path from Wenvoe must pass over Exmoor as well. Take a look at the map and you'll see that a straight line between the two places doesn't cross either: there are, in fact, few natural obstacles in the way of a metre-wave transmission.

#### .1.G.C.

Almost the only fly in the ointment in this part of South Devon is slow, and sometimes not so slow, fading. My host had done a good deal towards minimizing the effects of this by rigging up a remote-control arrangement for the contrast. With this he could keep the picture-level more or less steady; but I couldn't

help feeling that this job of work should have been done in the receiver itself by means of effective a.g.c. It is not only in places far from a transmitter that receivers have to cope with signal variations big enough to be a nuisance to the viewer. I am glad to see that an increasing number of manufacturers are including a form of a.g.c. in their sets. What a boon it will be if it is really effective against aeroplane flutter; for this form of interference is becoming more and more frequent with the increasing number of planes in the air.

#### The F.M. Scheme

THOUGH the first stage of the B.B.C.'s plan for v.h.f. broadcasting provides for only nine stations, it will cover a good 75 per cent of the homes of this country. The idea is to turn every TV station eventually into a combined television and sound broadcaster This means that the provision of interference-free sound broadcasting will go forward hand in hand with steadily improving television coverage. Since it should be possible to share much of the building, maintenance and running costs

"WIRELESS WORLD" PUBLIC	ATIC	NS
TECHNICAL BOOKS	Net Price	By Post
SHORT-WAVE RADIO AND THE IONOSPHERE. T. W. Bennington, Engineering Division, B.B.C. Second Edition.	10/6	10/10
SUPERHETERODYNE TELEVISION UNIT. Second Edition.	2/6	2/8
INTRODUCTION TO VALVES. R. W. Hallows, M.A. (Cantab.), M.I.E.E., and H. K. Milward, B.Sc. (Lond.), A.M.I.E.E	8,6	8/10
TELEVISION ENGINEERING: Principles and Practice. VOLUME ONE: Fundamentals, Camera Tubes, Television Optics, Electron Optics. A B.B.C. Engineering Training Manual. S. W. Amos, B.Sc.(Hons.), A.M.I.E.E., and D. C. Birkinshaw, M.B.E., M.A., M.I.E.E., in collaboration with J. L. Bilss, A.M.I.E.E.	30/-	30/8
WIRELESS WORLD TELEVISION RECEIVER MODEL II: Complete constructional details with notes on modernizing the original design	3/6	3/9
RADIO INTERFERENCE SUPPRESSION as Applied to Radio and Television Reception. G. L. Stephens, A.M.I.E.E	10/6	10/11
SOUND RECORDING AND REPRODUCTION. A B.B.C. Engineering Training Manual. J. W. Godfrey and S. W. Amos, B.Sc. (Hons.), A.M.I.E.E	30/-	30/8
ADVANCED THEORY OF WAVEGUIDES. L. Lewin	30/-	30/7
FOUNDATIONS OF WIRELESS. M. G. Scroggie, B.Sc., M.I.E.E. 5th Edition	12/6	13/-
TELEVISION RECEIVING EQUIPMENT. W. T. Cocking, M.I.E.E. 3rd Edition	18/-	18/8
Obtainable from all leading booksellers or from		
ILIPPE & SONS LTD., Dorset House, Stamford Street. Le	ondon,	S.E.1.

<sup>\*</sup> B.B.C. Quarterly, Autumn 1953.

between the two services this should make for a considerable saving in expense. A saving in manpower, too; for the number of engineers and technicians needed to run a "combined" transmitting station should be quite a bit smaller than that called for by two completely separate outfits. Although we may not be the first country to have a nation-wide high-fidelity sound service we shall, I believe, be the first to demonstrate the economies of combined sound broadcasting and television stations.

#### AWARDS AUTHORS

AUTHORS of a dozen or more papers on radio and allied subjects read before the Institution of Electrical Engineers last session, or accepted for publication during the session, are to be awarded premiums

by the Institution.

The Duddell Premium (£20) goes to G. W. Barnes (R.A.E., Farnborough), for his paper "A Single-Sideband Controlled-Carrier System for Aircraft Communication," the Blumlein-Browne-Willans Premium (£20) to G. Dawson, K. G. Hodgson and R. A. Meers (all of S.T.C.), and L. L. Hall and J. H. H. Merriman (P.O.), for "The Manchester-Kirk o'Shotts Television Radio Relay System," the Ambrose Fleming Premium (£10) to Dr. M. M. Z. Kharadly (Imperial College), and Dr. Willis Jackson, F.R.S. (Metrovick), for "The Properties of Artificial Dielectrics Comprising Arrays of cial Dielectrics Comprising Arrays of Conducting Elements," the Fahie Premium (£10) to T. Hayton, C. J. Hughes and R. L. Saunders (all of C. & W.), for "Telegraph Codes and Code Convertors" and the Heaviside Premium (£10) to J. F. Coales (Cambridge University), for "The Application of Information Theory to Data-Transmission Systems and to Data-Transmission Systems and the Possible Use of Binary Coding to Increase Channel Capacity." A £10 Premium will also be awarded to Dr. A. L. Cullen (University College, London), for "The Excitation of Plane Surface Waves."

Plane Surface Waves."

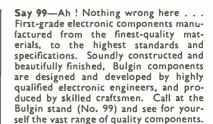
Premiums valued at £5 will be given to the following authors for the papers quoted:

E. D. Daniel and Dr. P. E. Axon (B.B.C.). for "The Influence of Some Head and Tape Constants on the Signal Recorded on a Magnetic Tape" and "The Reproduction of Signals Recorded on Magnetic Tape"; Dr. E. A. O'Donnell Roberts (Mullard), for "A Study of Some of the Properties of Materials Affecting Valve Reliability"; Dr. J. A. Saxton and B. N. Harden (Radio Research Station. Slough). for "Basic Ground-Wave Propagation Characteristics in the 50-800 Mc/s Band" and "Ground-Wave Field Strength Surveys at 100 and 600 Mc/s"; J. Brown (Imperial College), for "A rifficial Dielectrics Having Refractive Indices less than Unity"; Dr. A. Talbot (Imperial College), for "A New Method of Synthesis of Reactance Networks"; and E. Green (Marconi's), for "Synthesis of Ladder Networks to give Butterworth or Chebyshev Response in the Pass Band."

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## UNBIASED |

#### **Teleoptics**

I HAVE been reading with very great interest an article in the June issue of the French journal Télévision in which the author, Gaston Muller, puts forward some very original ideas. He is, like myself, afflicted with a divine discontent, as, indeed, is F. P. Hughes, who wrote "Why Lines?" in last month's Wireless World.

Muller criticizes the use of scanning in television; the picture is transmitted piecemeal and not in one complete whole as in the long-range TV system employed by the moon and other heavenly bodies.

Although the viewer thinks he sees a complete picture it is in reality a. mere illusion-like marriage, where one gets to know the real personality of ones partner bit by bit instead of all at once. As things are at present the marriage between electronics and optics, which produces as its offspring the television picture on our screens, is rather an unsatisfactory one from Muller's point of view. The offspring, by means of the scanning process, grows up gradually into a fully fledged adult over a period of time in the same way as an infant in the biological world. M. Muller wants the offspring to arrive in the world like Venus as a readymade adult with none of this timewasting growing business.

He describes his proposed remedy for this unsatisfactory state of affairs at considerable length, but admits that practical details are likely to prove very formidable. It is these tiresome practical details that are holding up a teleoptical scheme of my own as I want to provide every room in my house with television,

using one set only.

As you cannot just couple up an extension c.r.t. as you can a loudspeaker I propose to mount my set on the roof next to my masthead pre-amplifier and to distribute the picture optically. I intend to use a small projector-type c.r.t. in the set

#### By FREE GRID

and by an elaboration of the optical arrangement used in a binocular microscope, coupled with the necessary number of periscopes, I shall be able to beam the picture down each chimney of my house. It doesn't look as if we are going to get any coal next winter and I don't like to think of the chimneys as being entirely useless.

In the empty grate of each room, there will be a prism or inclined mirror to throw the image forward on to the back of a translucent screen standing in the position occupied by the normal fire screen. In this way television will be available in each room and the occupants will be able to gather in a half-circle round the fireplace as has been the habit of families for generations

The Etch and the Itch

ONE sometimes comes against the problem of replacing a defunct valve, on which the etched type number is indecipherable, in a receiver about which no technical information is available.

In a recent issue of the American journal Radio-Electronics a gallant attempt is made to solve this problem by suggesting various things which may be done to enable the faint and elusive type number to be read. All depend on the fact that the etching process causes a slight roughening of the glass over the actual etched area. Among other things suggested is that the valve be rubbed on your hair; the rough etched area of the glass collects more of the natural scalp oil than the rest and so shows up. But those of us who have dry scalps need not despair. All we need do is to stick the valve in the refrigerator and when it is really cool take it out and breathe on it; and we shall find that the resultant condensation has collected more readily on the rough etch

than elsewhere. These suggested remedies are all very well in their way, but I am surprised at a technical journal like Radio-Electronics having any truck with such nonelectronic methods. I must confess, however, that I only discovered the correct method myself by chance.

One day I had on my laboratory table the chassis of a set which I had picked up cheaply in the Petticoat Lane of radio. I was having trouble in deciphering the valve numbers and had left the room for a few moments in search of a valve data book and when I returned I noticed the cat rubbing itself against the valves and other components of the up-ended chassis.

There was nothing abnormal about all this, of course, but when I reached the chassis I noticed that the etching stood out boldly amid the dust which had gathered on the rest of each valve. The explanation is simple. When glass is rubbed with a piece of catskin it becomes electrified and readily attracts particles of dust. But there had been a much greater degree of friction between the itching skin of the cat and the rough area of the etching, and, therefore, a greater electrical charge

with the result that the dust had

been attracted there to a much



greater extent than elsewhere on the glass envelope of each valve.

#### Mobile Phone Boxes

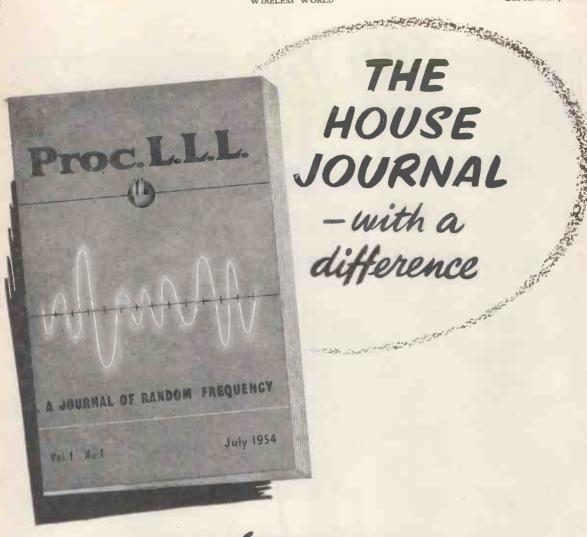
EACH YEAR there is an outcry from punters at the shortage of phone boxes at Newmarket, Epsom and other racing centres, to give people a chance of getting on to their London bookmakers for the later events in the programme after they have lost all their hard cash to the ready-money course bookmakers in the earlier races.

The usual excuse of the G.P.O. is that the capital outlay in building dozens of telephone kiosks which would be used for only a few days in the year would not be justified. Have they never heard of such things as radio waves, or are the officials in charge of the telephone department totally lacking in imagination?

I see no reason at all why tem-porary 'phone boxes made of wood and canvas should not be dumped down where needed, each containing a battery-powered radio unic for linking with a similar installation on the roof of the local telephone exchange. Such temporary boxes, with their complete freedom from connecting cables, could be readily moved by a suitably equipped pan-technicon from course to course as required.







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Valve requirements of extremely diverse equipments, from servo amplifiers to video modulators, are ideally met by the new Mullard beam tetrode, QV06-20.

This compact and rugged valve with an anode dissipation of 20 watts will function equally well as driver, frequency multiplier, power oscillator or output valve at all frequencies up to 60 Mc/s. With ratings reduced the frequency of operation may be increased to 175 Mc/s.

One QV06-20 as a class "C" amplifier will deliver 52 watts at 60 Mc/s, and two in a class "AB1" push-pull amplifier will provide 82 watts of audio power. The mutual conductance is 7 mA/V, and even with relatively low anode voltages a large output can be obtained with small driving power.

The anode connection of the QV06-20 is brought out to a top cap, and this feature, together with a short metal base screen which is connected to a base pin, ensures excellent separation between input and output.

The QV06-20 is directly equivalent to the popular American 6146. Further details of the QV06-20 and other valves in the comprehensive Mullard range are readily obtainable from the address below.

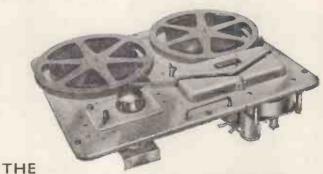
QV06-20

TETRODE

Heater:		-	Typical Applications	Va (V)	Pout (W)	f (Mc/s)
V <sub>h</sub>	6.3 V 1.25 A		R.F. Power Amplifier			
Limiting Va	lues:		Class "C" Telegraphy and F.M. Telephony	600 320	52 25	60 175
V <sub>a</sub> max. p <sub>a</sub> max. V <sub>g2</sub> max.	600 20 250	v w v	Class "C" Anode and Screen-grid Modulated  A.F. Power Amplifier or Modulator (Two valves.)	400	32	60
V <sub>gl</sub> max. f max.	150 175	V Mc/s	Class "AB1"	600	82	A.F.
Base	Octal		Class "AB2"	600	90	A.F.



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The reputation of the 'Tapedeck' is so well-known and so firmly established as to call for no extravagance in describing its many virtues. Indeed, it forms the basis of the recorder instruments in common use in the Defence Services of the United Kingdom and many other countries, as well as being the choice of broadcasting Authorities throughout the World.

FERROGRAPH 2A A reasonably inexpensive instrument approaching professional standards with a specification commending it to those engaged in educational and cultural pursuits.

FERROGRAPH MODEL YD A triple-speed instrument designed mainly for use in the scientific and industrial fields. Principally intended for operation from and into 600 ohm lines, a high gain stage has been provided, however, to allow for recording direct from normal microphones.

EQUIPMENT YDC A simultaneous dual-channel Recorder-Reproducer offering special facilities for analytical research into medical, aeronautical and scientific problems. Any two activities capable of translation into electrical phenomena within the frequency and phase shift limitations can be recorded and relayed simultaneously.

Demonstrations of Ferrograph Recorders will be given in Demonstration Room D.20.



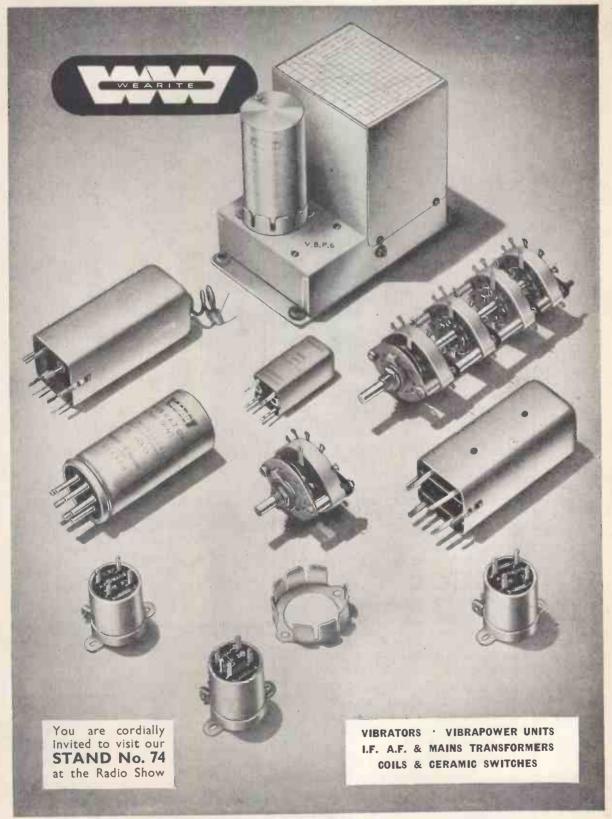
Originators of Tapedecks

WRIGHT & WEAIRE LTD

WEARITE

131 SLOANE ST., LONDON, S.W.1

Phone: SLOane 2214/5 & 1510



#### WRIGHT & WEAIRE LTD



## RCA is first choice for television equipments

RCA TELEVISION in the Philippines and Thailand has quickly followed the first TV installation in Asia in 1953. The first transmitter in Japan has now expanded to three . . . all completely RCA-equipped.

So the tremendous educational and cultural capacities of television are being introduced 'round the world... the most powerful means ever conceived for public enlightenment and international understanding.

Abroad, as in the U.S.A., RCA provides everything for television . . . from camera to antenna, from mobile remote units such as pictured here to complete studio and transmitter equipments. RCA also makes available the services of distributors and companies long versed in the electronic needs of their countries.

You can look with confidence to RCA for this complete co-ordinated service . . . manufacturing, installation facilities, instruction, servicing . . . everything that goes to make RCA TV such a dependable instrument of education and enjoyment throughout the world.

Your RCA distributor or company will gladly tell you about RCA TV; or write to RCA International Division.



RCA produces complete TV studio equipments, from microphones to monitoring consoles. This scene shows a broadcast from the RCA-equipped station DZAQ-TV, Manila.

"Marca Registrada"

World Leader in Radio First in Recorded Music First in Television



RCA INTERNATIONAL DIVISION

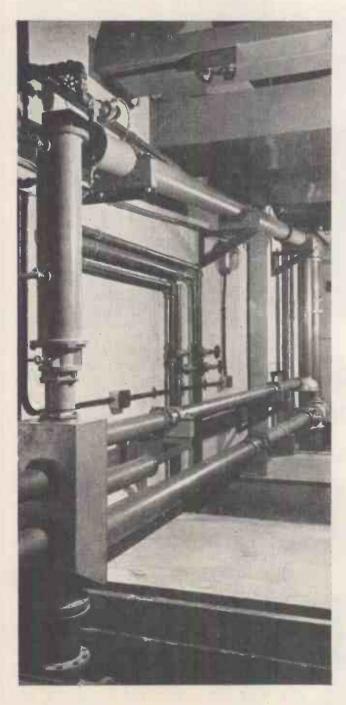
RADIO CORPORATION OF AMERICA

RCA BUILDING

30 ROCKEFELLER PLAZA, NEW YORK, N.Y., U.S.A.

# **B.B.C. TELEVISION AERIALS**

are matched to better than 1.1: 1 vswr using Wayne Kerr V.H.F. Bridges





MODELS B. 701 AND B. 801

Balanced and unbalanced measurement from 1-100 Mc/s.

MODEL B. 901

For unbalanced measurement from 50-250 Mc/s.

These instruments are also ideal for the measurement of receiver input admittances.

(Illustrated)

The asymmetric sideband filter behind the high-power vision transmitter at Holme-Moss.

(By courtesy of the B.B.C.)



The Wayne Kerr Laboratories Ltd.
New Malden, Surrey, England

# The performance of only as good as



Multiway Plugs and Sockets for quick action and positive contact

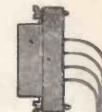
These reliable Plugs and Sockets, proved in service, provide a quick positive connection for up to 28 terminations. They need lower insertion pressure per contact than any comparable product, and when fully mated a dust and damp proof seal is provided between Plug and Socket. Considerable latitude in matching can be allowed when they are used in rack mounting applications.

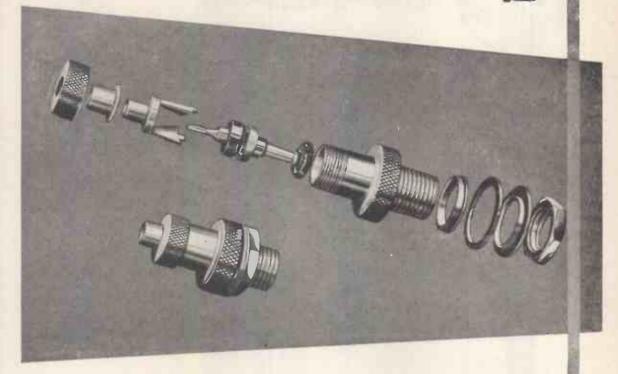
These components are in regular use by :— The English Electric Co. Ltd., Messrs. Marconi's Wireless Telegraph Co.Ltd. and Messrs. Standard Telephones & Cables Ltd.

4 WAY 8 WAY 12 WAY

20 WAY

28 WAY any equipment is its terminals





These versatile Miniature connectors provide perfect coupling between co-axial cables and instruments, and are extensively used in Television, Radar, and Communications equipment. They are 100% pressure and flash tested before despatch. The full range consists of a variety of Cable and Panel Mounting units of either plug or socket type, and a recent addition is an elbow connector for applications where it is desired to keep the face of the panel clear. Suitable for use with co-axial cable Uniradio 32 and 43.

Miniature hermetically sealed Co-axial Plugs and Sockets to RCS.322

A.I.D & A.R.B - APPROVED

**POWER CONTROLS** 

LIMITED

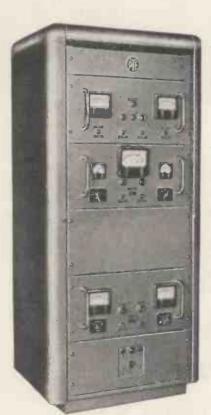




POINT-TO-POINT F M

# VHF RADIO-TELEPHONE LINK





This Equipment will provide first-class single channel point-to-point facilities and, at the same time, possesses the necessary capacity for extension to six channels if required.

## ABBREVIATED SPECIFICATION

Frequency range: 60-216 mc/s

Transmitter output Power: 10 watts or with Amplifier Unit
—50 watts

Maximum Deviation: 50 kc's

Receiver Bandwidth: 6 db down  $\pm$  120 kc/s Overall Transmitter-Receiver Performance

Frequency Response: 300 c/s — 6 kc/s ± 3 db; 6 kc/s —

36 kc/s ± 1 db

Intermodulation Level: At least — 55 dbm—for 2 tones applied each at 0 dbm



Pye (New Zealand), Ltd., Auckland C.I., New Zealand.

Pye Radio & Television (Pty.) Ltd., Johannesburg, South Africa. Pye Canada, Ltd., Ajax, Canada.

Pye Limited, Plaza de Necaxa 7, Mexico 5. Pye-Electronic Pty., Ltd., Melbourne, Australia.

> Pye Limited, Tucuman 829, Buenos Aires.

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# Before you can say

"SNAPACITOR"



THIS BECOMES THIS

in four
easy movements

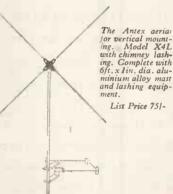
Yes, it's as easy as that. The unique

Snapacitor principle permits

factory pre-assembly and alignment of all Antiference Aerials. This saves erection time and guarantees peak performance.

# CORROSION-PROOF, TOO!

There's another vital point about Antiference capacitor couplings; there are no metal-to-metal connections. This eliminates intermetal corrosion and guarantees life-long 100% electrical efficiency. There are no servicing headaches with Antiference.



The Antiference range of T.V. aerials extends from single dipole to multi-element arrays. Details of the complete range on request.

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Aug 25-Sept 4

STAND No. 34

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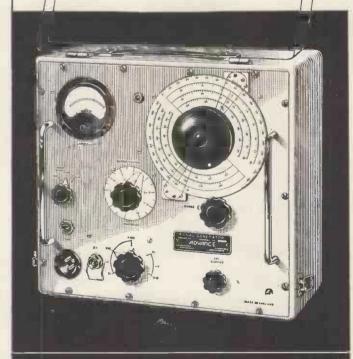
ADVANCE COMPONENTS LTD., MARLOWE ROAD, WALTHAMSTOW, LONDON, E.17. Telephone: LARkswood 4366/7/8

# 10 to 300 Mc/s DIRECTLY CALIBRATED

been recognised as supreme in its sphere for accuracy, ease of operation and reliability. Now comes the D1/D—an up-to-the-minute successor—possessing all those proven qualities, but plus the advantage of being DIRECTLY CALIBRATED. Whilst the range of the D1/D (10 to 300 Mc/s) is only slightly less than the original D1, its characteristics, given below, prove the "D" series to be the finest V.H.F. instruments available in their price class.

Frequency range 10 to 300 Mc/s
 Directly calibrated with an accuracy of plus/minus 1% Sine wave modulation 30% at 1,000 c/s
 Square wave modulation approx. 50/50 at 1,000 c/s
 Max. attenuation error at 300 Mc/s
 plus/minus 4 db Negligible stray field
 Light weight, only 34 lbs.

Advance
V.H.F. SIGNAL GENERATOR



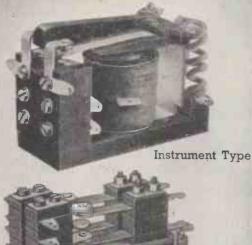
MODEL DI/D

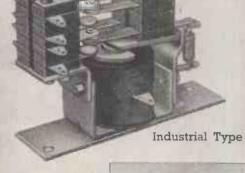
Full technical details available in Leaflet W26

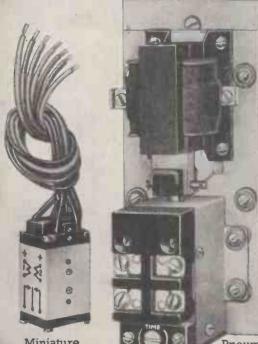
Net Price in U.K.

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£97







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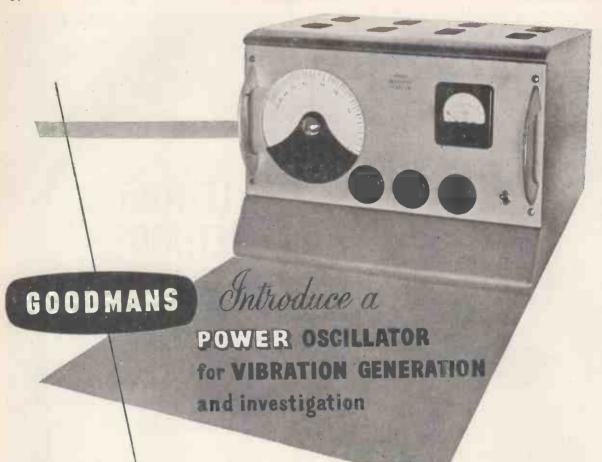
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RELAYS

Comprehensive technical data of our extensive range of standard relays will be forwarded on request

Most types now available for PROMPT DELIVERY

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PHONE: STEVENAGE 780



# -provides a stabilised 10-10,000 c/s supply

A vibration generator depends for its accuracy largely upon the suitability of its driving equipment. Goodmans—who pioneered vibration generators in this country—have now produced a self-contained drive unit consisting of oscillator, amplifier and power pack. Although primarily intended for use with Goodmans Model V.47 Generator, it will also find wide application in the laboratory and in industrial processes where a high quality source of audio frequency is required. A brief specification of this latest Goodmans product is given below, and full circuitry details are available on request to "Vibration Dept. W".

FOR USE WITH
THE GOODMANS
VIBRATION
GENERATOR
MODEL V.47

or where small scale vibration testing is involved



## **Brief Specification**

Frequency range—10-10,000 c/s. in 3 ranges. Power output—5 watts into 3 ohms. Output Level Stability—±0.05 db 10-10,000 c/s. Distortion—less than 0.2%. Hum level—72 db down on 5 watts. Power supply—100/115 v, 200/225 v, 225/250 v; 50-60 c/s. 75 watts. Weight—45 lb. Dimension—16½in. × 13in. × 11in.

# THE and special supplements

THE TIMES has gained a special reputation for its supplements, for the great thing about a supplement is that it should be thorough.

That is why the supplement for the radio industry published separately by THE TIMES on August 23rd will be so well worth reading. The articles, on varied subjects ranging from the radio show and current trends in set design to detailed news of the latest developments in components, will be informative and authoritative to a high degree. Reports on the B.B.C.'s plans for sound and television, a special article on the use of navigational aids in the air and on the sea, communications equipment, electronics as an aid to production, and many other articles of general interest are included.

This supplement of 32 pages published by THE TIMES reviews the radio industry fully and lucidly. Those who serve that industry, and the public in general, will find it stimulating and valuable reading.

THE MANAGE TIMES

# Radio and Television Supplement

**Published August 23rd** 

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Stock volt ranges 6/7, 12/13, 22/24, 50/55, 100/110, 200/220, 230/250.



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FREQUENCY
MONITOR (20 Mc/s)

Designed for the measurement of any frequency in the range 10 c/s to 20 Mc/s with a basic accuracy of ± 1 part in 10<sup>6</sup> ± 0.1, 1.0, or 10 c/s. Higher accuracies available if required. The unknown frequency is determined by counting the number of cycles that pass through a 'gate' open for a selectable time interval of 0.1, 1.0, or 10 seconds. The result is presented on eight panel mounted meters each scaled 0 to 9 and is in decimal notation. Full information available on request.

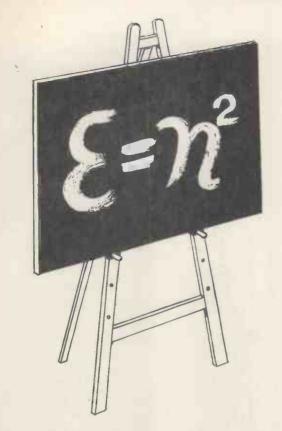
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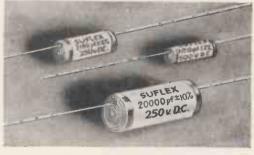


IN 1881 J. C. MAXWELL
derived this relationship
between dielectric constant
and refractive index.
That this holds true for
Polystyrene implies that
polarization is almost
entirely due to elastic
displacement of electrons only.
This means LOW DIELECTRIC
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and voltage.

#### SUFLEX POLYSTYRENE CAPACITORS

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\* The capacitors shown here are actual size.

CAPACITIES: 5 pf. to 0.5 mfd.

TOLERANCE: 20% to 1%.

VOLTAGES: 250v. to 750v. D.C.

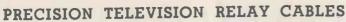
HS Type: for general use.

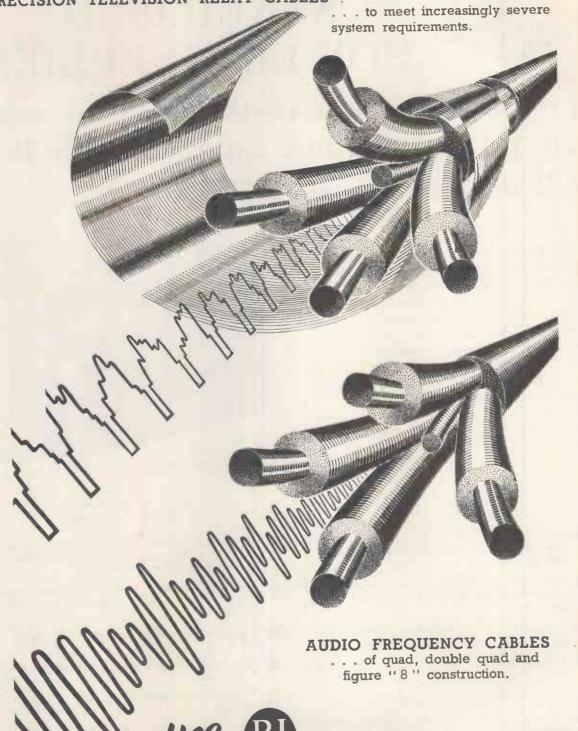
HSA Type: with additional sealing

for use in exceptional humidity conditions.

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POLYTHENE INSULATED & SHEATHED CABLES for the highest standards of television

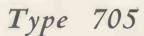
and radio relay engineering.



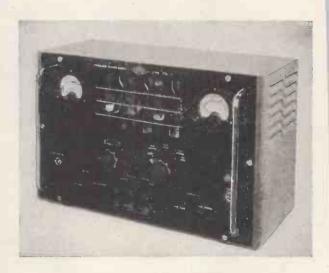
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provide all the necessary power supplies for electronic equipment in the LABORATORY and WORKSHOP.

THE Airmec Stabilised Power Supplies which operate from 100-130 and 200-250 volts 50 c/s mains are designed for either bench use or for forward mounting on a standard 19in. rack. Both current and voltage meters are incorporated, and in the Type 776, a meter switch enables any of the four separate direct outputs to be monitored. Separate switches and fuses controlling all D.C. outputs are fitted to each unit for convenience of operation,



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- Output change is less than  $\pm$  0.5 per cent. for  $\pm$  10 per cent. input change.
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- Source Impedance 5 ohms.
- A.C. output 6.3 volts at 5 amps, centre tapped, unstabilised.
- Price £55—Immediate delivery.



# Type 776

- Stabilised positive output continuously variable from 200-350 volts at maximum currents of 200-100 mA.
- $lackbox{lack}$  Positive output change is less than  $\pm$  0.5 per cent. for  $\pm$  10 per cent. input change.
- Stabilised negative output of 85 volts at 5 mA.
- Unstabilised positive output of 500 volts at 200 mA.
- Unstabilised negative output of 500 volts at 3 mA.
- A.C. output 6.3 volts at 5 amps. unstabilised.
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Full details of these or any other Airmec instruments will be forwarded gladly upon request.

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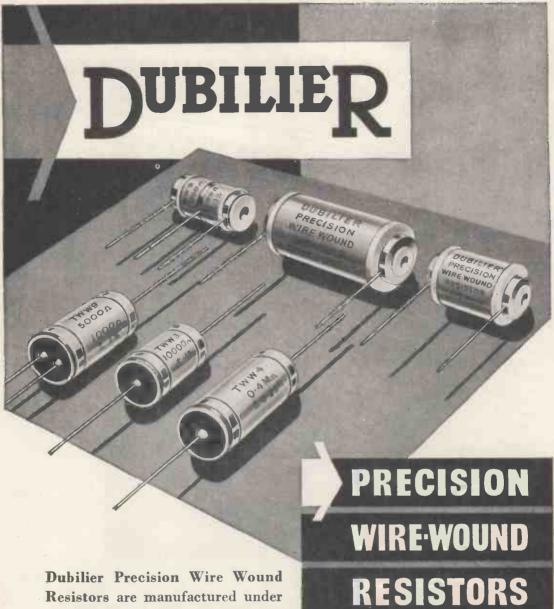
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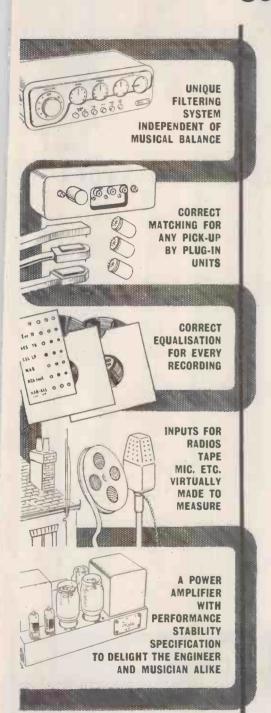
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The QUAD II for convenience of installation, is constructed in two units—the main amplifier and the control unit. Each is complementary to the other, offering in complete form the best which present techniques can devise.



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1A3	3C24	6B6G	6P7G	7N7	17 <b>Z</b> 3	78	809	40214	CM V6	DL63	EY51
1A5GT	3C45	6B7	6Q7G	7Q7	18	80	810	4033A	CMV28	DL66	EZ40
1A7G	3CP1	6B8	6Q7GT	7R7	19AQ5	80/S	811	4045A	CV3	DL82	FG17
1A7GT	3D6/129+	6B8G	6R7	787	19E2	81	813	4046A	CV6	DL92	FG27A
1B26	3DP1	6B8GT	6R7G 6R7GT	7W7 7¥4	19X3	82 83	814 815	4060A	CV24 CV43	DL93	FG67
1B27 1C5G	3FP7 3LF4	6BA6 6BE6		7Z4	19Y3 21A6	83 <b>V</b>	816	4205E 4212E	CV52	DL94	FX215 G650
1C5GT	3Q4	6BG6G	687 6SA7	8D2	23D	84	826	4260A	CV57	DRM1B DRM2B	CDMAG
1D5	3 <b>Q</b> 5G	6B <b>H</b> 6	6SA7GT	8D5	24G	88J	828	4313C	CV58	DRM3B	GDT48 GEX00
1D6	3Q5GT	6BJ6	6SC5	9D2	25A8/G	89 (Y)	829A	4328D	· CV64	E444S	GEX34
1D8/GT	354	6BR7	6SC7GT	9D6	25A6GT	100TH	829B	4378	CV67	E1148	GEX35
1E7G	3V4	6BS7	6SD7GT	9HP7	25L6 .	117L7GT	830B	4690	CV72	E1155	GEX44/1
1E7GT	4C27	6BW6	6SF5	10	25L6GT	117N7GT	832	5763	CV75	E1190	GEX45/I
1F5G	4C29	6BW7	6SF7	10¥	25SN7GT	117Z6GT	832A	7193	CV83	E1191 E1192	GEX54
1G4GT	4D1	6BX6	6SG7	10D1	25Y5	210HL	833/833A	7475	CV85	E1192	GEX54/3
1G5G	4J53	6C4	68 H7	11D3	25Z4G	210SPG	836	8011	CA88	E1931	GEX54/4 GEX54/5
106/GT	4THA	6C5	6SH7GT	11D5	25Z5	210SPT	837	8012A	CV92	E1248 E1254	GEX54/5
1H5G	4TPB	6C5G	6SJ7	12A6	25 <b>Z6G</b>	210VPT	838	8013A	CV100	E1254	GEX55/1
1H5GT 1H6G	5AP1 5A/102D	6C5GT 6C6	6SJ7 <b>GT</b> 6SJ7 <b>Y</b>	12A6GT 12A8GT	25 <b>Z6GT</b> 27	212E 215P	841 843	8016	CV101/3	E1265 E1266	GEX64
1L4	5B4G	6C21	6SK7	12AH7GT	28D7	215SG	850	8019 8020	CV118 CV119	E1271	GEX66
1LA6	5B/502A	6CD6G	6SK7GT	12AH8	30	217C	860	9001	CV 195	E1271	GEX69 GL466A
1LC6	5BP1	6CH6	6SL7GT	12AT6	32	220B	861	9002	CV 125 CV172	E1273 E1320	GL451
1LD5	5CP1	6D6	6SN7GT	12AT7	33	220P	863	9003	CV174	E1323	GTIC
1LH4	5CP7	6D7	6SQ7	12 A IT 6	33A/100A	220RC	864	9004	CV179	E1359	GT1C GU20
1LN5	5C/450A	6E5	6SQ7GT	12AU7	35A5	220TH	865	9006	CV192	E1368	GTI21
1N5G	5D21	6E6	6887	12AX7	35L6GT	231 <b>D</b>	866A	AC4/PEN	CV415	E1379 E1436	GU50 H30
INSGT	5FP7	6F5	6ST7 6T7G	12BA6	35 <b>T</b>	250 <b>TH</b>	866JR	ACP4	CV967	E1436	H30
1P5GT	5GP1	6F5G	6 <b>T</b> 7 <b>G</b>	12BE6	35 <b>T</b> G	262A/B 279A	869B	ACT6	CV980	E1468	H63 HD14
1Q5GT 1R4	5JP4 5L35	6F5GT 6F6	6USG	12BH7	35 W 4	279A 282A	872A	ACT17	CV988	E1474 E1481	HD14
1R5	5LP1	6F6G	6U5/6G5 6U7G	12C8 12C8GT	35Z3 35Z4GT	304TH, TL	874 875A	APP4B APP4C	CV1481 CV1583	E1481 E1494	HF30
184	5R4GY	6F6GT	6V6	12DP7	35Z5GT	307A	876	APP4G	CA 1989	E1494	HL2
185	5T4	6F7	6V6G	12H6	36	310A	878A	AR12	CV1588 CV1596 CV6008	E1496 EA50	HL2K HL4
185 1 <b>T4</b>	5U4G	6F7E	6V6GT	12J5GT 12J7GT	36 37	310B	884	AR13	CÝ6008	EB34	HL23
105	5 <b>∀</b> 4G	6F8G	6 <b>W</b> 2	12 <b>J7GT</b>	38	311A	905A	AR300A	CY31	FR01	RL41
17	5X4G	6F8GT	6W7G	12K7GT	39/44	313C	923	AR4101	CY32	EBC3 EBC33 EBC41	HP210 HR210 KMV6
2A3	5¥3G	6G5G	6X4	12K8	40	323A	931A	ARP3	D1	EBC33	HR210
2A4G 2A5	5 Y 3 GT 5 Y 4 G	6G6G 6H6	6X5	12K8GT 12Q7GT	41	327A 328A/4328A	954	ARP4	D15	EBC41	KMV6
2A6	5Z3	6H6G	6X5G 6X5GT	12SA7	41MP 41MPT	337A	955 956	ARP13 ARP38	D41 D42	EC54 ECC81 ECC82	KR3 KR6/3
2A7	5Z4	6H8GT	6 <b>Y6G</b>	12SA7GT	41MTL	354V	957	ARS6	D43	ECCOL	KRN2
2B7	5Z4G	6J5	6Y7G	12SC7	41MXP	357A 368A	958A	AT4	D63	ECCSS	WTO
2C26	5Z4GT	6J5G	6 <b>Z</b> 5	12SG7	41STH	368A	959	AT15	D77	ECC91	KT2 KT8
2C26A	.6A3	6J5GT	7A2	12SH7	42	380A	991	AT40	D77 DA30	ECC91 ECH22	KT24
2C34	6A6	6 <b>J6</b>	7A4	12SJ7	42SPT	388A	1299A	ATP4	DA60	ECH35	KT30
2C40	6A7	637	7A5	12SJ7GT	43	394A	1616	ATS70	DA90	ECH42	KT30 KT31
2C43 2D21	6 <b>A8G</b> 6 <b>A8GT</b>	637G 637GT	7A6 7A7	12SA7 12SK7GT	45 45SPEC	450TL 703A	1619	AU5	DA100	ECL80	KT32
2E22	SART	638G	7B6	12SL7GT	455 PEC 46	705A	1622 1624	AU7	DAF91	EF22	KT33C KT44
2J21A	6AB7 6AB8	6K6G	7B7	12SN7GT	50C5	707A/B	1625	AZ1 AZ31	DDR25 DET5	EF36 EF37	KT44
2J34	6AC7	6K6GT	7B7E	12SQ7	50 CD6G	708A	1626	AZ41	DET9	EF37A	KT61 KT66
2136	6AF6G	6K7	7BP7	125Q7GT	50L8GT	709A	1629	B21	DET12	EF39	KT71
2J39	6AG5	6K7G	7C4	12SR7	50 Y 6G T	713A	1635	B30		EF41	KTWA1
2J48	6AG2	6K7GT	7C5	12U5G	53A 53KU	714AY	1642	BL63	DET16	EF50	KTW61 KTW62
2J54	6AJ7	6K8	706	12 <b>X</b> 3	53 <b>K</b> U	717A	1648	BT45	DET19	EF54	KTW63
2J54B	6AK5	6K8G	707 7D5	1274	54 57	723A/B	1815	C5B	DET25	EF80	KTZ41
2X2/879	6AK6	6K8GT	7D5	14B6	57	724A	1851	ClC	DF91	EF91	KTZ63
2X2A	6AL5	6L5G	7D7	14E7	58	725A	1960	C9A	DF92	EF92	KTZ73
3A4 3AP1	6AM5 6AM6	6L6 6L6G	7D8 7D9	14H7	59 61P	728A	2050	CAG25	DH63	EF93	L2
3B7/1291	8AQ5	6L6GA	7E5	14K7 14R7	71A	800 801	2051	CAV25	DH76	EF94	L30
3B24	6AT6	6L7	7E6	1487	.72 .72	801A	2151 3951	CK1005	DH77	EF95	L63 L77
3B26	6AU6	6L7G	7E7	15D2	73	803	4003A	CL33 CMG8	DH81 DH101	EL22 EL32	177
3B/151A	6AV6	6N7	7F7	15E	75	805	4019A	CMG22	DH107	EL33	L610 LD219
3BP1	6B4G	6N7G	7G7	15R	76	807	4019B	CMG25	DK91	EL41	LD410
									2711111	ALMAY	BUTAV



# HALL ELECTRIC LTD

HALTRON HOUSE, 49-55 LISSON GROVE,

LONDON N.W.1.

Tel.: Ambassador 1041 (5 lines)

Cables: Hallectric, London



# Ask your dealer \_ to show you



The TAPE RECORDER for every Home

Here at last is a Tape Recorder all can afford. The 'PLAYTIME' offers a new world of entertainment and interests at a price until now unimaginable.

A scientifically developed, precision engineered instrument, it weighs only 16lb. and is built in a beautifully appointed, compact case, finished in attractive two-tone leathercloth.

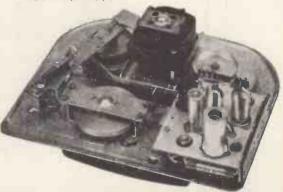
The 'PLAYTIME' is the lowest priced Tape Recorder giving a full hour's playing time. Completely self-contained for recording. Plays back through normal adio or amplifier.

#### ACCESSORIES

The 'PLAYTIME' is supplied complete and ready for use, optional extras being a matched High Fidelity Crystal Microphone at \$2/- and ONE HOUR Spool of special matched tape at \$26/6.

# Automatic erasure of unwanted recordings.

- Powered by specially designed motor.
- High fidelity twin track recording heads completely enclosed in handsome dress cover, affording complete protec-tion against stray magnetic and electro-static fields.
- Self contained for recording. For play-back plug into any radio or amplifier.
- Miniature self contained equipment VERY portable and compact, finished in attractive 2-tone leather-cloh suit-case of ultra modern design thished with handsome gilt fittings; detachable lid for case of handling.
- Overail size 12 in. × 10in. × 4 in. Weight 16 ib.
- Storage space for spare spools of tape.
- \* Size of tape table only 11in. x 9 % in.
- For use on AC mains 230/250 v



This is the lightweight precision engineered chassis of the Playtime—scientifically developed and superbly presented

\* Write for coloured leaflet.

Frequency response 60/6,000 c.s.

Patents applied for

TECHNICAL DATA "PLAYTIME" gives you ONE HOUR'S PLAYING TIME.

THE ONLY RECORDER WITH SINGLE KNOB CONTROL FOR RECORD, PLAYBACK, REWIND AND FAST FORWARD WITHOUT UNLACING TAPE.

"PLAYTIME" records and plays back with equal ease in any position even upside-down or on its side.

Because it is scientifically developed and precision engineered, there is absolute minimum wow and flutter.

Separate variable control ensures correct volume for all types of recording and playing back.

Built-in 3-stage specially matched pre-amplifier with miniature MULLARD valves.

Instantaneous and positive braking.

Manufactured by :

(ELECTRONICS)

3 FITZROY STREET . LONDON Tel.: MUSeum 5563

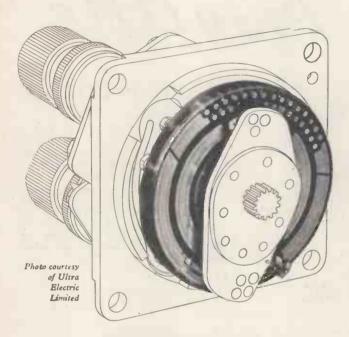
The (Wantage) Tape Deck by:

Walter Instruments Ltd. · Garth Road · Lower Morden · Surrey

# **Track Assembly**

# Moulded with

# 'Araldite'



This selector unit (part of the Ultra Jet Pipe Temperature Control System) controls the temperature of the exhaust gases of a turbo-jet aero-engine.

The resistance elements and track segments are moulded in 'Araldite' Casting Resin B, simplifying assembly and sealing the elements against climatic changes and ensuring mechanical stability.

This is another example of the versatility of 'Araldite' epoxy casting resins which combine exceptionally low shrinkage on setting with resistance to high temperatures, humidity and corrosive agents. 'Araldite' epoxies are facilitating production in many industries—most notably in the potting and sealing of components for radio, electronics and electrical engineering generally.

#### THESE ARE THE NEW EPOXIES!

'Araldite' (regd.) epoxy resins are obtainable in the following forms:—

- Hot and cold setting adhesives for metals and most other materials in common use
- Casting resins for the electrical, mechanical and chemical engineering industries
- Surface coating resins for the paint industry and for the protection of metal surfaces

Full details will be sent gladly on request.

'Araldite'

epoxy casting resins

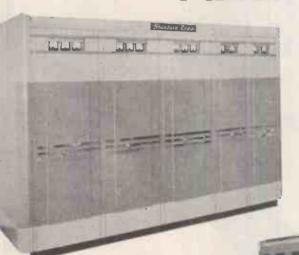
**Aero Research Limited** 

# Standard

in Continents

RADIO POINT-TO-POINT

TRANSMITTER



owerful 40 kilowatt D.S.13's were used to transmit Her Majesty the Queen's Speech direct from Auckland, New Zealand, to the United Kingdom on Christmas Day, 1953.

More than 180 of these transmitters are in use throughout the World

Available for early delivery

		ters ******
*D.S.10	3/5 kW	Double Sideband
*D.S.12	4 kW	Independent or Single Sideband *
*D 5 13	40 kW	Independent or Single Sideband

\*\*\*\*\*\*\*

Write for Radio leaflets:

Type D.S.10 No. 179/25 Type D.S.12 No. 129/25 Type D.S.13 No. 130/25

# Standard Radio



Standard Telephones and Cables Limited

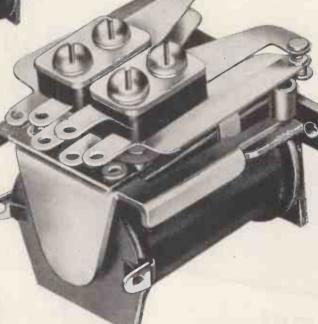
Registered Office; Connaught House, 63 Aldwych, London, W.C.2.

RADIO DIVISION . OAKLEIGH ROAD . NEW SOUTHGATE . LONDON, N.I.

SEPTEMBER, 1954

# RHTAYS

A compact design for close stacking



SERIES 595 D. C. OPERATED

> This extremely compact relay has its connections to both contacts and coil brought conveniently to one end, and is designed without projections to facilitate close stacking where banks of Relays are in use. The contact current handling capacity is exceptionally high in relation to the overall dimensions of the Relay. Good armature design has reduced the effects of shock, vibration and acceleration, and the spring type hinge eliminates backlash friction and risks of displacement.

For further details of our range please write.

TELEPHONE: NEWMARKET 3181-2-3

TELEGRAMS: MAGNETIC NEWMARKET



MAGNETIC DEVICES LTD

ADVANCE COMPONENTS LTD., MARLOWE ROAD, WALTHAMSTOW, LONDON, E.17.

Telephone: LARkswood 4366/7/8

# 7.5 to 250 Mc/s ON FUNDAMENTALS IN FIVE RANGES SINE AND SQUARE WAVE MODULATION R.F. OUTPUT 1 MV to 100 mV

Advance
MODEL Q1
V.H.F. SIGNAL GENERATOR

£45
(List price in U.K.)

Again Advance lead the way—this time with a V.H.F. Signal Generator covering 7.5 to 250 Mc/s, a range that embraces Bands 1 and 2 and also the impending Very High Frequency Television Transmissions on Band 3. Moreover, this instrument is available at a price well within the reach of every service man. In the traditional Advance manner, this instrument is designed for simple operation and with a versatility that not only fulfils present needs, but anticipates the even more exacting requirements to deal with the television test problems of tomorrow.



Below are some outstanding features:

- WIDE RANGE—7.5 to 250 Mc/s
- SINE AND SQUARE WAVE MODULATION
- RELIABLE ATTENUATION
- LOW LEAKAGE—less than 3 microvolts
- TRULY PORTABLE—weighs only 171bs
- COMPETITIVE PRICE



The Q1 provides the ideal complement to the Model E2. These together give complete coverage from 100 kc/s to 250 Mc/s.

Full technical details available in Folder W23 on request.

# IT'S A QUESTION OF



# SOME SUGGESTED EQUIPMENT COMBINATIONS

Lowther Amplifier A.10F. Lowther Master control unit Lowther F.M. unit Lowther DT.4 radio unit Connoisseur motor Lowther pick-ups with diamond styli Pick-up transformer Extra power pack	37 23 43 1	0 6 8 19 17 10	0 0 3 11 8 6
	£189	2	4
• •			
Rogers Baby-de-Luxe amplifier and	£	S.	d.
Rogers Radio Feeder unit 3 wave-	23	0	0
band	24	16	0
Garrard T/B unit with 2 Decca pick- ups		0	_
Goodsell amplifier and pre-amp. type be substituted for the above if desired.		.5 C	an

	75	13.	CA+
Goodsell Williamson amplifier	33	10	0
Goodsell pre-amplifier	18	18	0
Goodsell F.M. unit	15	0	0
Connoisseur 3-speed motor		8	11
2 Leak pick-ups with diamond styli	-3	0	* 1
and transformer	21	19	9
	£112	т6	8
	4-1-		
		)	
	1	62	d.
Leak T.L.10 and Leak Point One	7.5	٠.	44.
	- 0		
pre-amp	28	7	0
Leak pick-up with 2 diamond styli			
and transformer	21	19	9
Collaro transcription motor		9	
Goodsell F.M. unit.			
Goodsen I .m. ante	13	0	0
	1.78	15	9
	-0.7		_

Loudspeakers and Cabinets to choice. Standard Radio Feeder units available, and special Export units with extra short wavebands it required.

GLASSIC

THE

# STANDARDS . . .

It seems paradoxical to refer to variable standards. Yet even amongst Hi-Fi enthusiasts—whose critical perceptions none could question—there is no yardstick of performance. A "Standard" is that which wholly satisfies an individual requirement. And requirements are as diversified as the means to their attainment. To misquote—"Perfection lies in the ears of the listener."

We are well aware of this at Classic, and we devote our service to matching individual requirements, backing it with specialised advice.

When you come\* to Classic you can be sure of getting the precise combination of equipment you need. Any combination of equipment can be supplied to specification and will be specially packed for export orders. All equipment and cabinets are available on hire purchase or credit sale terms in Great Britain and Northern Ireland.

\* and you get the same specialised attention if you write—wherever you may be. We can ship any equipment anywhere in the world.

#### LOUDSPEAKERS HI-FI

					Credit Sale				Hire Purchase					
	Cash			h	9									
		Price			P'mts of			De	Deposit			P'mts of		
		1		d.	1	0	d.	£		d.	11	6	d.	
Witness Wilmschaus		- た				S.		~			~		8	
Vitavox Klipschorn		145			17			40	0			II		
Lowther Type PM3		-	0				7	40				2	8	
Acoustical Corner Ribbon		95	0	0	II	12	3	32	0	0	6	0	0	
Wharfedale "Triune"		96	0	0	II	14	7	32	0	0	6	2	-8	
Wharfedale Corner 3 Unit		72	0	0	8	16	0	24	0	0	4	12	0	
Tannoy 15in. dual concent	ric	33	IO	0	4	2	0	H	IO	0	2	19	0	
Tannoy 12in. dual concent	ric	27	10	0	3	6	0	9	10	0	I	14	6	
Lowther PWI (walnut)		78	10	0	9	12	0	26	10	0	5	0	0	
Goodmans Axiom 22 (in	re-													
commended reflex cabin		37	14	0	4	12	3	12	14	0	.2	7	0	
Goodmans 150 in Corr			,		· ·									
Baffle		22	17	0	2	16	0	7	17	0	I	8	9	
Wharfedale Super 12/CS/			,					- 1	,					
in Classic Reflex cabinet		38	10	0	4	14	3	12	IO	0	2	10	0	
Wharfedale W/10 CSB Corn		5				- 4	3							
Baff. Assembly		24	16	0	3	4	0	8	16	0	т	TO	8	
COMPLETE WHARFED		. An	D	GU	יינעטי	VLA i	N 5	ANL	) \\	.B.	N.	AN	J E	
NORMALLY STOCKED.														

Bass reflex cabinet of contemporary design and heavy construction finished in straight grained or burr walnut veneer, or oak veneer, lined with Cellotex and fitted with a Wharfedale W12/CS/AL Loudspeaker. Dimensions 20in. × 21in. × 42in. high. . . £37 10 0 Radiogram Cabinet to match. Dimensions 20in. × 21in.

Equipment Cabinet to match for Tape Recorder or Record storage. Dimensions 20in. × 21in. × 36in. high. £27 0 0



# ELECTRICAL GO LTD

'HI-FI' SPECIALISTS

352-364 LOWER ADDISCOMBE ROAD CROYDON SURREY TEL. ADDISCOMBE 6061-2

Mullard

**Ferroxcube** 

being extruded into

rods for H.F. cores.





# TRANSISTORS



# for hearing aids

The smallest glass-encapsulated transistor in the world; a result of the specialised valve manufacturing techniques pioneered by HIVAC.

Hermetically sealed against moisture.

All British manufacture throughout.

Contains a germanium junction element manufactured and supplied by (B)

The new HIVAC junction transistor type XFTI, because of its extremely small size and high performance, is the perfect element for all stages of the most modern Hearing Aids.



Dimensions are only 5.3 x 3.8 x 15 mm.
DELIVERIES WILL COMMENCE IN SEPTEMBER

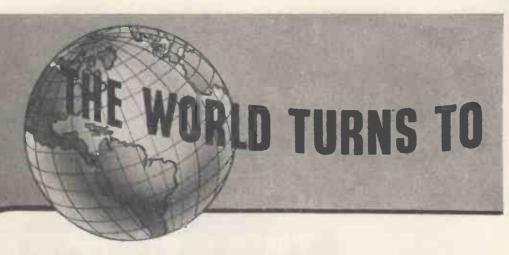
Samples are available now to Hearing Aid Manufacturers

# Hixag Limited

STONEFIELD WAY, VICTORIA ROAD, SOUTH RUISLIP, MIDDX.

Telephone: Ruislip 3366

Cables: HIVAC RUISLIP.



# 3-SPEED TRANSCRIPTION UNITS

## **MODEL 2000**

Comprises Transcription Motor and Turntable complete with 3-speed gear and switch mounted on banjo-type unit plate

## MOP EL 2010

Same specification as Model 2000, but mounted on rectangular unit plate and equipped with a studio "P" High Fidelity pickup head



Absolutely uniform speed; reproduction free from rumble and 'requency modulation. Available for A.C. voltages 100/125 and 200/250. Finished in cream scratchproof enamel. Also available for A.C./D.C. supply

# GRAMOPHONE UNITS Single- and 3-speed

New in design and supplied in two types:—A.C.554 for 78 r.p.m. records; A.C.3/554, a new unit for 3-speed operation.

Turntable is heavy duty steel, rubber covered; fitted with striker for operating automatic stop.

Spring Suspension and check springs eliminate acquistic leed-back.

Pickup Rest fitted with safety clip.

Motor-4 pole, dynamically balanced

The above units are also available for A.C./D.C. supplies.



See them at the Radio Exhibition, Earls Court, London, Aug. 25th—Sept. 4th, Stand No II and Demonstration Room No D 26.

COLLARO LTD., Ripple Works, By-Pass Road, Barking, Essex.

# Collaro PRODUCTS

# RECORD CHANGERS

"54" High Fidelity Changer. COLLARO'S latest complete mixing unit for 7in., 10in. and 12in. records. Suitable for A.C. voltages 100/125 and 200/250 and available for A.C./D.C. supplies.

RC531. Non-Mixing Changer for single-speed operation at 78 r.p.m. with 10in. and 12in. records. Also 3RC531, 3-speed version for operation at 33\frac{1}{2}, 45 and 78 r.p.m. with 7in., 10in. and 12in. records.

RC532. MixIng Version o Model RC531 for single-speed operation at 78 r.p.m. with 10in. and 12in. records intermixed in any order. Also

3RC532, 3-speed version, for operation at 33½, 45 or 78 r.p.m. with 7in. records, or 10in. and 12in. records intermixed in any order



# PICKUP HEADS

\*Studio " High Fidelity crystal pickup Head. No specia filters required. Non-hygroscopic; full tropical guarantee.

Orthodynamic head for 78 r.p.m. and long-play records. Change over effected by switch. Permanent twin point stylus of special durable alloy.

Magnetic Head for 78 r.p.m. records only. Standard type semi-permanent needles. Unsuitable for sapphire stylus.



Magnetic Low or High Impedance Heads for 78 r.p.m. records only. Interchangeable miniature steel needles or permanent sapphire stylus.

See them at the Radio Exhibition, Earls Court, London, Aug. 25th—Sept. 4th, Stand No II and Demonstration Room No D 26.

COLLARO LTD., Ripple Works, By-Pass Road Barking, Essex.

# We can deliver these from stock.



THE

Pape recorder with SINGLE KNOB CONTROL

Scientifically developed and precision engineered, this new Tape Recorder is the most portable, compact and lightweight unit giving a FULL HOUR'S PLAYING TIME. At 26 gns. it represents unbeatable value. Completely self-contained for recording and only connecting to pick up terminals of any radio or input of any amplifier for play back.

Supplied ready for use with the following optional extras. Matched High Fidelity Crystal Microphone 52/-. Laboratory Matched special ONE HOUR spool of Tape 26/6.



#### TECHNICAL DATA

- THE ONLY TAPE RECORDER WITH SINGLE KNOB CONTROL FOR RECORD, PLAY-BACK, REWIND AND FAST PORWARD WITHOUT UNLACING TAPE.
- "PLAYTIME" gives you ONE HOUR'S FULL PLAYING
- HOUR'S FULL TIME.
  "PLAYTIME" records and plays back with equal case in any position, even upside down or on its side.
- or on its side.

  Because it is scientifically developed and precision engineered there is absolutely minimum wow and fintter.
- Separate variable control ensures correct volume for all types of recording and playing back.
- Built-in 3 stage specially matched pre-amplifier with miniature Mullard valves.
- Frequency response 60/3,000 c/s.
   Instantaneous and positive brak-
- Automatic erasure of unwanted recordings.

   Powered by specially designed
- motor.

  High fidelity twin track recording heads completely enclosed in handsome dress cover affording complete protection against stray magnetic and electrostatic fields.
- For use on A.C. mains 200/250 v
- Self-contained for recording and to play back just use any radio or ampiltier.
- or amplifier.

  "PLAYTIME" is very portable and compact, finished in attractive 2 tone leathercloth sultcase of ultra modern design finished with handsome glif fittings, detachable tid for ease of handling.
- Overall size I2}in. × 10ln. 4}ln.
- Weight 16 lbs. only.
- Storage space for spare spools of tape.
- Size of tape table only 11in. × 9 % in.

M.O.S. PERSONAL CREDIT PLAN

SEND ONLY 10% DEPOSIT with balance spread over any period up to 24 months.

THE

SUITCASE TAPE RECORDER

TWO SPEED TAPE RECORDER

The Tape Recorder for the Connoisseur who wants the best in Tape Recording. At 45 Gns. there is no better value. The "EDITOR" is now available with two speeds giving 2 HOURS' PLAYING TIME

With operating height of just over 5in, this wonderfully compact unit is amazingly simple to use for a hundred and one different recording purposes. Superb true balanced recording and listening can be obtained. The "EDITOR" is the smallest mains operated Tape Recorder giving 2 HOURS' FULL PLAYING TIME.



Fully Guaranteed

#### M.O.S. PERSONAL CREDIT PLAN

GNS.

Complete with Ronette

Crystal Desk Micro-phone, 1,200ft. spool high coercivity tape

high coercivity and take up spool.

SEND ONLY 10% DEPOSIT with balance spread over any period up to 24 months.

#### TECHNICAL DATA

- INDEPENDENT BASS AND TREBLE CONTROLS FOR RECORDING AND PLAY-BACK.
- Two speeds 3 lin. and 7 lin. per sec.
- High quality Amplifier can be used quite independently for PA or gramophone record re-production.
- · Overall negative feed-back.
- · High flux speaker together with amplifier giving superb and bril-
- liant reproduction.

  Instantaneous and positive brak-
- ing.

  High fidelity recording heads (twin tracks), automatic erasure.

  Powered by three high grade recording motors.

  Past forward and rewind without unlacing tape.

  Precision englacering giving negligible wow and ilutter.

- Magic eye recording | evel contro
- Speaker muting switch and provision for external speaker.
   Radio/Gram and microphone inputs.
- Size only 16lin. × 12in. × 5in (without lid).
  MULLARD Miniature Valves.
- Attractive 2 tone leathercloth case with detachable lid with handsome gilt fittings.
- · For use on AC mains 200/250 v

# See and hear them at the RADIO



The relaxation of Hire Purchase Restrictions makes it possible to supply any equipment you regulre on Easy Terms up to 24 months repayment period with a YERY LOW initial deposit.

E. & G.

Telephone: MUSeum 6667.

THE RADIO CENTRE.

**ACCESSORIES** 



rgoyne

# TWO SPEED TAPE DECK

33in./sec. and 71in./sec.

# Carr. & Packing 7/6.

## TECHNICAL DATA

- . 2 HOURS' PLAYING TIME
- 2 SPEEDS: 3%in. and 7%in./sec.
- Fully automatic mechanical speed change (no tinkering with pulleys and balts).
- o Instantaneous and positive braking.
- · Precision engineered giving minimum wow and
- Frequency range 50/10,000 c/s. at 7½ln./sec. with suitable amplifier.
- @ Overall size 115in. x 14fin.

Here is the heart of your Tape Recorder! If you are building or modernising your own equipment—you MUST have the latest BUR-GOYNE Tape Deck giving 2 speeds, designed for building into complete recorders. Greatest value ever offered.

- For use on A.C. Mains 200/250 v.
- · Powered by 3 high grade motors.
- . Fast forward run and high speed rewind without unlacing tape.
- · Automatic high frequency erasure.
- Twin track high impedance heads totally enclosed in cover affording complete protection from stray magnetic and electrostatic fiesdl.
   No matching transformers required.
- Deck will take all standard plastic and paper tapes up to 1,200lt, capacity.
- · Washable top pauel of very durable finish. unobtainable elsewhere

1200 ft. Spool Burgoyne Tape (high coercivity) 35/-600 ft. Spool Burgoyne Tape (high coercivity) 21/-Take-up Spool ... ... 4/3

M.O.S. PERSONAL CREDIT PLAN

SEND ONLY LI TO SECURE ANY EQUIPMENT

SEND ONLY 10% DEPOSIT balance spread over any period up to with balance spread over as 24 months.

ORDER SUPPLY and exclusively for MAIL

This is the EASY way to BUY!

The M.O.S. PERSONAL CREDIT PLAN gives you a variety of methods of purchase. Here is a further selection of equipment:-

. . . . . . . . . . . . . . . . .

CASH CREDIT PRICE SALE £1 dep. 8 inst. HIRE PURCHASE ITEM Deposit 12 18 inst. (Instalments are monthly) AMPLIFIERS AND TUNERS Goodsell oodsell GW18 Williamson GW12 Williamson £11 1 £9 3 £4 10 £3 10 £4 18 £6 6 42/5 28/6 35/- 24/-18/4 12/6 15/- 10/4 20/- 13/8 24/6 16/8 840000 000000 F/TC Tone Control .
F/U/TC Tone Control PFA Tone Control . Lowther AM/FM Tuner ..... £22 0 58/6 £7 6 8 28/-18/11 0 TL10 Amp. & Pre-amp.
Tuner Unit £9 9 £11 13 £29 7 0 £35 0 0 76/-..... £42 0 0 114/- £14 0 0 53/4 36/-Quad Mk. II Amplifier Rogers logers
Senior Main Amplifier
Senior Control Unit
Mark II Baby de Luxe Amp.
Mark II Junior Pre-Amp.
Mark II Junior Pre-Amp.
Mark II Minor Amplifier
RD Minor Baffle
RD Junior Corner Horn
Junior Tuner Unit £28 0 £15 0 £14 0 £9 0 £12 17 £8 15 £18 17 £25 6 75/-39/6 37/6 25/-34/6 24/6 50/-66/6 8 0 4 0 10 00006061 £9 6 £5 0 £4 13 £3 0 £4 5 £2 18 £6 6 £8 9 13/6 12/10 9/-16/8 21/6 Burgovne £23 2 0 63/9 £3 12 6 11/3 LOUDSPEAKERS Goodmans 6210 Tannoy £33 10 £27 10 0 Wharfedale £3 5 0 £4 2 6 £2 4 5 £2 11 1 £1 10 11 £9 15 £12 6 £6 13 £7 13 £4 12 W12C8
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ITEM		CASH PRICE			CREDIT		HIRE PURCHASE				
					£1 dep. 8 inst.	De	posi	it	12 inst.	18 inst.	
						(Ins	taln	nent	s are mo		
	PICK-UPS	£	S.	d.	s. d.	£	S.	d.	s. d.	s. d.	
	Connoisseur, with 2 Heads Decca XMS, with 2 Heads Cosmocord HOP39/0P20 Arm Leak Ruby 78 r.p.m. or LP Romette Miniweight, with 2 Heads Ronette Superweight, with 2 Heads	£9 £6 £3 £11 £3	9 8 11	634	31/-	£3 £1 £3 £1 £1	1 3 2 17 3 5	10 1 9 0 2 5	13/4 10/- 7/- 15/10 7/- 7/4	9/3 7/- 4/11 0 11/- 4/11 5/3	
	PLAYERS										
	Regentone RP2 3-speed	£9	19 15	6		£3 £5	6	6	14/6 20/10	10/- 14/3	
	Amp. Place Agram Junior Place As Agram Junior Place As Agram Junior E. A.R. Auto 3-speed Amplifier E. A.R. Non-Auto 3-speed Amp. Volmar L425 3-speed Auto Amp.	£21 £9 £37 £24 £19 £24	17	000606	68/- 52/-	£7 £3 £12 £8 £6 £8	0 3 12 5 11 4	0 0 0 10 8 6	26/8 14/- 48/4 31/6 25/4 31/6	18/2 9/6 32/8 21/6 17/4 21/5	
	TEST EQUIPMENT										
	Advance P1 Generator J1 Generator E2 Generator H1 Generator	£19 £35 £28 £25		0000	52/6 95/- 75/3 66/3	£6 £11 £9 £8	13 17 6 6	0488	25/6 45/6 36/6 32/-	17/9 31/6 24/3 23/-	
	Avo Model S Meter. Model 7 Meter. Universal Avominor Electronic Test Meter Signal Generator D.C. Avominor Universal Bridge	£23 £19 £10 £40 £30 £5 £34		0000000	80/6 5 15/-	£6	16 10 10 6 0 15	8008008	30/4 26/- 14/6 51/- 39/- 9/2 43/-	21/3 18/4 10/8 35/- 27/- 6/6 29/6	
	Amplion Test Meter	£5	19	6	17/-	£2	0	0	9/3	6/8	
	Oscilloscope 1039 Oscilloscope 1052 Voltage Calibrator 1433	£29 £104 £18	10 0 5	000	79/6 283/- 1	£9 234 £6	16 13 1	848	37/3 132/10 24/-	25/9 90/- 16/4	
	Dengo Modulated Test Oscillator	£3	15	0	_	£1	5	10	7/6	5/3	
	Pullin Series 100 Test Meter	£11	11	0	31/-	£2	0	0	19/6	13/6	
	Taylor  44A Meter  77A Universal Meter 88A Universal Meter 110C Bridge 150A Output Meter	£14	10 0 0 10 10	00000	39/6 57/9 38/- 90/- · £	£5 £7 £4	16 0 6 16 3	80884	5/- 20/- 28/- 19/5 42/4	3/9 13/9 19/3 13/4 29/-	

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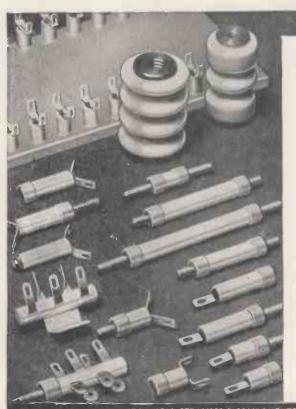
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# that to see at the

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## MULLARD DEMONSTRATION ROOM D3

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#### MULLARD DEALER RENDEZVOUS D29

The Mullard Dealer Rendezvous displays the more recent additions to the growing range of Mullard Dealer Aids. Of particular interest is a demonstration of the unique Mullard Expandabox System and Expandapak, the ideal valve carrier for service engineers.

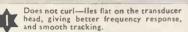
The popular Mullard High Speed Valve Tester will also be demonstrated.

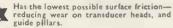


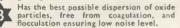
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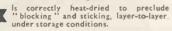
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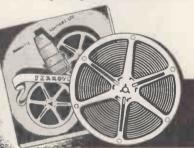
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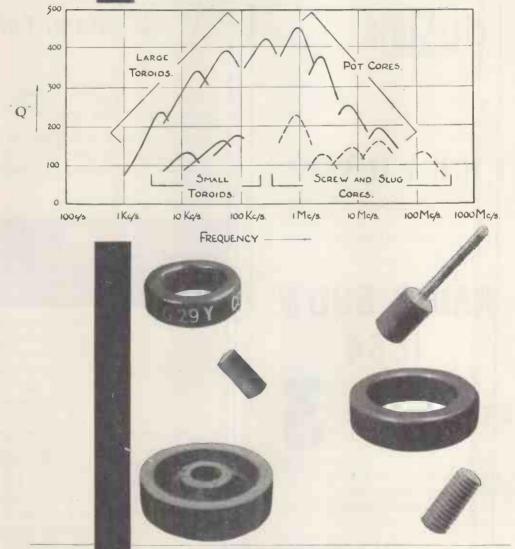


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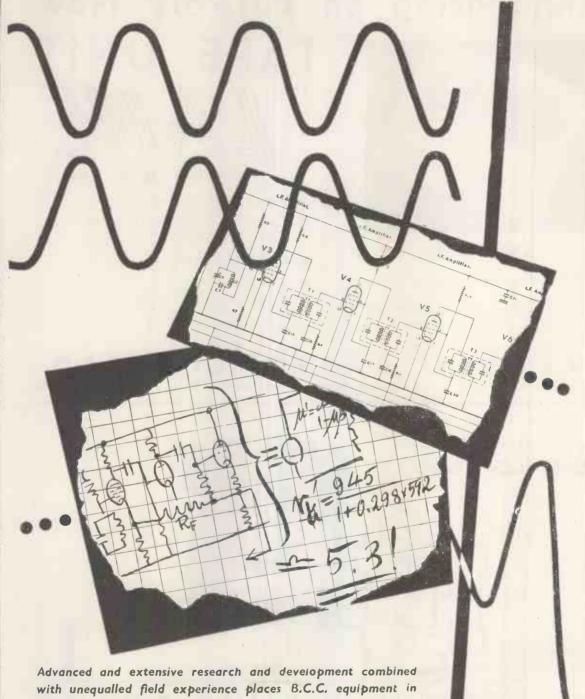
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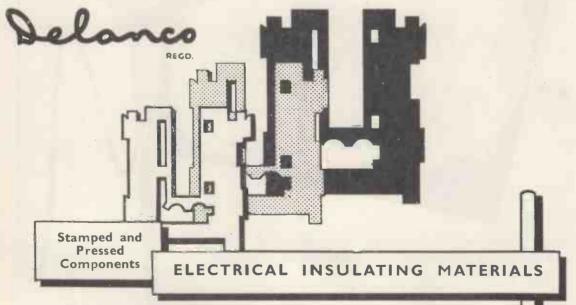
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HS3	1 watt	i watt	750	to 500 megohms	1.1" x 0.1"
	T	olerance ava	ilable ±5%	, 2%, 1%	
		WIREWOU	ND RESIS	TORS	
	5 (	ohms to 100K	ohms	5 - 10 watts	
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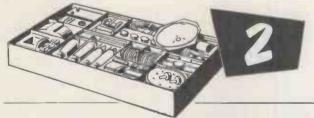
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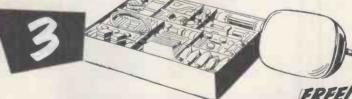
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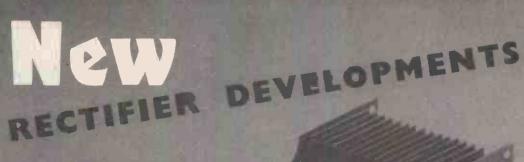
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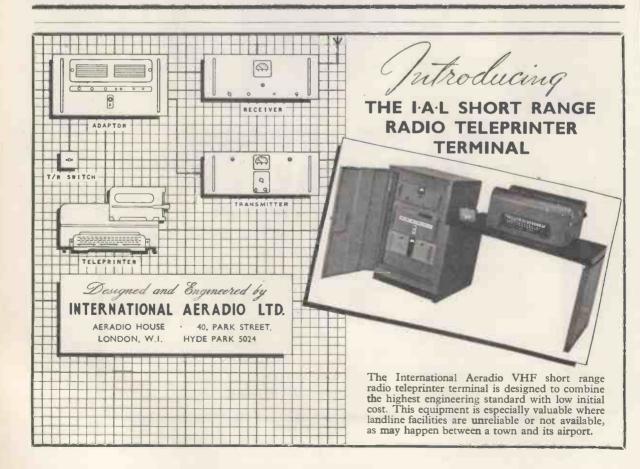
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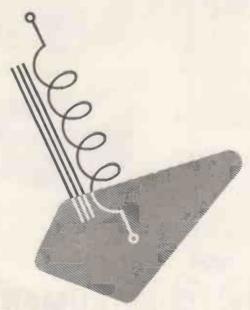
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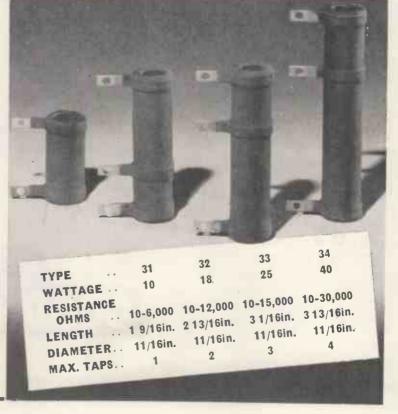
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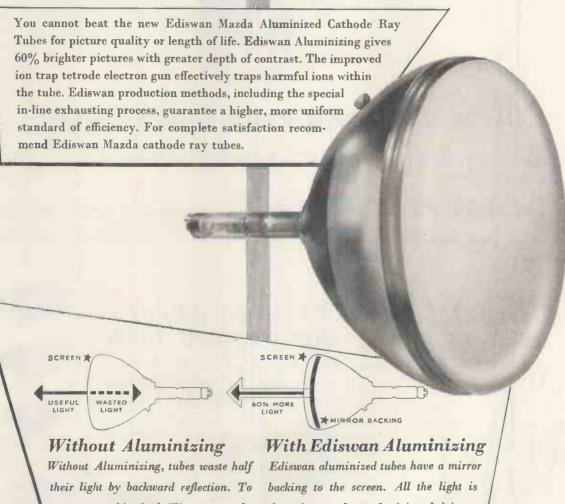
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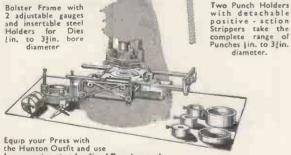
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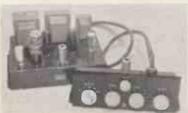
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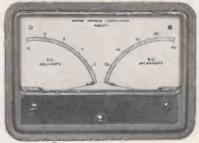
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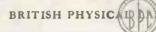
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Standard input for 20 db:-

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Less than 2 db down at 50 c/s Less than 6 db down at 5,500 c/s

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Output constant within 3 db for 100 db change in signal input.

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Stabilisation Ratio	100 : 1	60 ; 1	70 : 1+ ve 300 : 1-ve
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Maximum Control Grid Voltage	Vg2(max) Vg1 (max)	100
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gl and g2 (volts)	Vg1-g2	400
Mutual Conductance (mA/V)	gm	14
Inner µ	µg1,g2 Pa	5.3
Maximum Anode Dissipation (watts)	Pa	
Maximum Screen Dissipation (watta)	Pg2 Ik(max)	5.0
Maximum Cathode Current (mA)	1k(max)	300
Maximum Potential Heater/Cathode	Vi	300
(volts DC)	$V_{h-k(max)t}$	300

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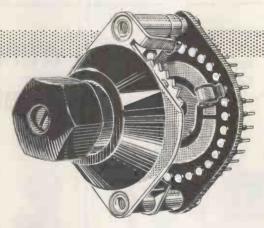
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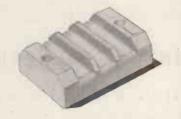
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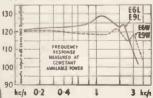
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HIS new Independent Sideband Receiver type THIS new independent obtained no long-distance, point-to-point, short-wave radio links forming part of the international trunk network. On independent sideband working, the GFR 552 provides facilities for the reception of two single sideband signals, each 6 kc/s wide, one above and one below the frequency of a reduced-level pilot carrier. Each sideband will accommodate either two 3 kc/s wide telephony channels, or several voice frequency telegraph channels. The GFR 552 may also be used for reception of single sideband or double sideband transmission. In the case of the second application this receiver offers two advantages: firstly, the absence of non-linear distortion which occurs in normal d.s.b. receivers when signals are subjected to selective fading conditions; and, secondly, the ability to select upper or lower sideband for demodulation, dependent upon which is freer from adjacent channel interference. The circuit and chassis layout of the GFR 552 closely

follows that of the Mullard Receiver GFR 551, which was based on a British Post Office design (Receiver, Radio No. 22).

Special features of the GFR 552 include a high order of oscillator stability and freedom from cross-modulation through which cross-talk between channels or intermodulation between wanted and unwanted signals might occur. A brief technical summary is given below. More detailed information supplied on request.

FREQUENCY RANGE—4-30 Mc/s.
NOISE FACTOR—better than 7 dB over the band.
SIGNAL TO NOISE RATIO—25 dB for 4 microvolts peak sideband

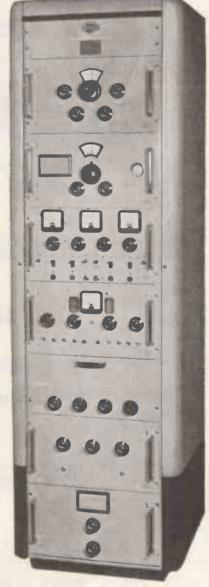
input over the band.

SELECTIVITY—The response is flat within 2 dB for sideband frequencies between 100 c/s and 6000 c/s. At 10 kc/s from the carrier frequency the response is -60 dB relative to the pass band. A.F.C.—The a.f.c. system operates effectively with a pilot carrier level of –26 dB relative to 1 microvolt (which corresponds to a peak sideband level of 1 microvolt and a signal to noise ratio of 15 dB)

NON-LINEAR DISTORTION—Third order intermodulation products which might result in cross talk between sidebands do not exceed

-50 dB relative to the sideband levels.

OUTPUT-Variable up to +14 dB relative to 1 mW into 600 ohms.







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FREQUENCY RANGE 19 Mc/s. to 165 Mc/s. CONTINUOUS COVERAGE



- A.C. operation. 110-250 volts. 40-60 cycles.
- Dimensions 163 in. x 15in. x 83 in.
- Weight 60lb.

- Highly efficient signal frequency circuits.
- Substantial diecast rotary coll turret.
- Excellent frequency stability and selectivity.
- Accurate re-setting and ease of handling.
- High sensitivity and excellent signal-tonoise ratio.
- High quality push-pull output.
- For AM, FM, NFM and CW Signals.
- Robust construction and outstanding reliability.
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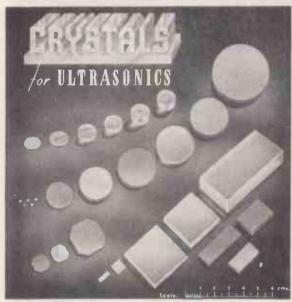
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## "LISTEN THROUGH" FACILITY

A high speed relay circuit applies a pre-set blocking bias to certain valves of the receiver to "mute" it during actual transmission. This facilitates listening through during spacing periods.

### FREQUENCY RANGE

Range 1. 60 —125 kc/s ,, 2. 100 —260 kc/s I.F. 460 kc/s

3. 260 —660 kc/s I.F. 1.4 Mc/s and 460 Kc/s.

4. 0.66—1.5 Mc/s 5. 1.5 —3.4 Mc I.F. 460 kc/s.

7. 7 —15 Mc/s I.Fs. 1.4 Mc/s and 460 kc/s.

8. 15 —32 Mc/s

### SIZE

103" H x 133" W x 143" Deep. Weight: 67 lbs.

### POWER SUPPLIES

The set operates from single phase AC 50-60 c/o 100-125 and 200-250 volts. For DC operation specially approved rotary convertors with control units are avilable for 24, 110 and 220 volts. It can also be used on dry batteries.

### OUTPUT

Two simultaneous outputs are provided; 2 watts into 500 ohms for loudspeaker and 60 millwatts into 100 ohm loads for headphones. Negative feed back is used in the final stages to ensure a constant voltage output under varying load conditions.

### GAIN CONTROLS

Separate RF and AF gain controls are provided. The RF control is imperative when the AGC is in use.

The automatic gain control can be switched on and off as required. With an increase in output of 60 db the output will not increase by more than 8.0 db.

#### CRYSTAL CONTROL

Facilities are provided to Crystal control the receiver in the range 1.5-30 Mc/s when required.

### TUNING SCALE

The calibrated tuning scale is  $6\frac{1}{2}$  long, and coarse and fine scales for logging purposes are provided.

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Exceptional Chassis
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# Announcing the NEW Armstrong F.C. 48

### OUTSTANDING FEATURES INCLUDE :-

\*8 Valves including 2 double Triodes. \*8 watts output from push-pull tetrodes. Heavy negative feed back is used resulting in negligible distortion and high damping factor. \*Provision for using F.M. adaptor to receive the present high quality transmissions from Wrotham and the new B.B.C. V.H.F. stations. \*An accessible socket at rear provides the power supply for this unit THE F.M. UNIT WILL BE

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PRICE £23/18/- (including P.T.).

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R.F. 41. Ten valves, four wavebands, ten watts of audio, R.F. stage and 2 I.F. stages. PRICE £31/19/8 (inc. P. Tax). EXP. 125/C. 14 valves, 5 wavebands, 15 watts of high quality audio output. Provision for F.M. adaptor as provided on the F.C.48.

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#### EXPORT MODELS :-

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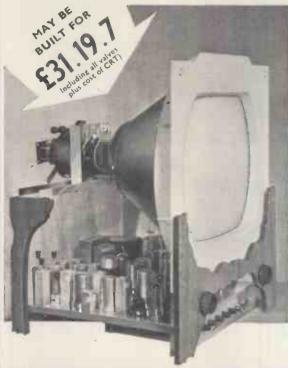
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THE COMPLETE TELEVISOR IS SAFE TO HANDLE, BEING COMPLETELY ISOLATED FROM THE MAINS BY A DOUBLE WOUND MAINS TRANSFORMER. ALL PRESET CONTROLS CAN BE ADJUSTED FROM THE FRONT, MAKING SETTING UP VERY SIMPLE.



Brief Technical Details are as follows:

20 valves (plus tube) Superhet Receiver, tunable from 40-68 Mc/s without coil or core changing. Wide Angle scanning Flyback EHT giving 14 kV, Duomag Focaliser, permanent magnet focussing with simple picture centring adjustments, suitable for any wide angle Tube, may also be used with a 12in. Tube with very minor modifications.

VISION CIRCUIT. Common RF Amplifier, single valve frequency changer, two IF stages, Video Detector and Noise Limiter followed by special type of Video Output Valve. ALL COILS PRE-TUNED ASSURING ACCURATE ALIGNMENT AND EXCELLENT BAND-WIDTH

SOUND CIRCUIT. Coupling from anode of frequency changer, two IF stages, Double Diode Triode detector and first LF Amplifier, Diode Noise Limiter and Beam type Output Valve, feeding a 10in. Speaker. ALL COILS PRE-TUNED.

TIME BASES. 2 valve sync. Separator, giving very firm lock and excellent interlace.

LINE TIME BASE. Blocking Oscillator using a pentode driving a high efficiency output stage comprising Ferroxcube Cored Output Transformer with Booster Diode.

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POWER PACK. Double wound Mains Transformer supplying all L.T. and H.T. using two full-wave Rectifiers.

The Televisor may be constructed in 5 easy stages: (1) Vision, (2) Time Base, (3) Sound, (4) Power Pack, (5) Final Assembly. Each stage is fully covered in the Instruction Book, which includes layout, circuit diagrams and point-to-point wiring instructions.

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This Transformer has an additional 6.3v. 3A and is cap able of supplying an extra 50mA for Pre-amp o £2.12.6 Feeder Unit

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12H	150mA	Fully	shrouded			19/6
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ln.	in.		
25A 14	2½ round	R.F. Thermo	7/6
3.5A 14	21×21	R.F. Thermo	7/6
4A 15	21×21	R.F. Thermo	7/6
20A 11	21 round	M/C	8/6
40A 11	2½ round	M/C	8/6
1.5m.A 14	21 round		12/6
5 m.A2	31 round		7/6
6mA 2	31 round		16/9
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The circuit is the latest type TRF using 3 valves and Meral Recrifiers for operation on 200/250 A.C. Metal Rectifiers for operation on 200/250 A.C. mains. Wave band coverage is 180/550 metres on medium wave and 800/2,000 metres on long wave. The dial is illuminated and the Valve line-up is The dial is illuminated and the Valve line-up Is 6K7 H.F. Pentode 6J7 Detector and 6V6—Output. The attractive Cabinets to house the Receiver size long, 6\frac{1}{2}in. high, 5\frac{1}{2}in. deep, can be supplied ther WALNUT or IVORY BAKELITE or WOOD

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£10.10.0 Plus packing and carriage 5/-BRAND NEW, guaranteed and in manufacturer's orig. carton. LIST PRICE MINIATURE TUNING CONDENSERS 2-gang .0005 mfd. with trimmers ..... 6/9

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These are brand new in Maker's Cartons
Plus 2/6 Pkg. and Cart.

For onl 47/6

#### **ACCUMULATORS**

volt 10 amp. (by famous maker) ....

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A super quality Moving Coli Meter basic movement 2 mA. and 4 mA. Scale dimension 2½m., Overall dimensions 2½m. dia 1½m. deep. Bakelite Case projecting type. At present scaled 1 amp. R.F. By removing thermo couple, reversing scale and recalibrating the meter, a high grade test instrument with any range above the basic F.S.D. may be built up. Frice 2 mA., 5/9, 4 m A., 4/9.

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ACOS. High impedance Crystal Microphone, type 35-1, 25/-.

25/-. ACOS. High Impedance Crystal Microphone, type 33-1. 22/10/-.
ACOS. MIC 30 Impedance Crystal Microphone £2/10/-.
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CRYSTAL MICROPHONE An entirely insulated crystal microphone which can be saiely used on A.C./D.C. amplifiers. High impedance. No background noise, really natural tone. The ideal Mike for tape, wire and sound projectors, price 22/C.

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Two specially designed chokes with three smoothing condensers with circuit diagrams. Cuts out all mains noise. Can be assembled inside existing receiver, 4/11. plus 6d. pkg. and carr.

Germanium Crystal Diodes. G.E.C. wire ended, 2/60 24/0 doz.

VCR517C

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Plus 1/6 Pkg. and Carr.

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Model PC/I	
Brown Rexine covered	22/6
Overall dimensions 15in. x 13hin. x 5 in.	
Clearance under lid when closed 24in.	
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Overall dimensions 15in. × 13in. × 6ln.	
Clearance under lid when closed 21in.	
Model PC/3	
Rexine type covering in various cols	69/6
Overall dimensions 16 lin. x 14 lin. x 10 lin.	-510

Clearance under lid when closed 6 in.
All the above Cabinets are supplied with Panel, Carrying All the above Capital
Handle and Clips.
Packing and Postage 2/8.

PREMIER MAINS TRANSFORMERS All primaries are tapped for 200-230-250 v. mains 40-100 cycles. All primaries are screened. SP175B, 175-0-175, 50 mA., 4 v. @ 1 a., 4 v. @ SP350A, 250-0-250, 100 mA., 5 v. @ 2-3 a., 6.3 v. 21/-@ 2-3 a. SP352, 350-0-350, 150 mA., 5 v. 2-3 a., 6.3 v. 2-3 a.,  $\begin{array}{c} 6.3 \times 9.3 \, a. \\ \text{BF501, 500-0-500, 150 mA, 4 v. @ 2-3 a, 4 v. @ } \\ 2-3 \, a., 4 v. @ 2-2 \, a., 4 v. @ 3-5 \, a. \\ \text{SF501A, 500-0-500, 150 mA, 5 v. @ 2-3 a, 6.3 v. @ 3-5 a, 5 v. @ 2-5 a. \\ \text{2425A, 425-0-425, 200 mA, 6.3 v. @ 2-3 a, 6.3 v. } \\ \text{250-0-250, 80 mA, 6.3 v. @ 4 a, 5 v. @ 2 a. } \\ \text{250-0-250, 80 mA, 6.3 v. @ 4 a, 5 v. @ 2 a. } \\ \text{200-230-250 output 3 v. 30 v. @ 2 a.} \end{array}$ 

- I	RECTIFIERS	
	E.H.T. Pencil Type S.T.C.	
Type K3/25	650 v. 1 m.A	4/7
K3/40	3.2 kV. 1mA	6/-
" K3/45	3.6 kV. 1 mA	8/2
K3/50	4 kV. 1 mA	8/8
" N3/160		21/6
	H.T. Type S.T.C.	
Type RM1	125 v. 60 mA	4/-
, RM2	125 v. 100 mA	
, RM3	125 v. 125 mA	5/6
" RM4	250 v. 250 mA	18/-
	L.T. Type Full Wave	
6 v. 1 amp.		4/-
12 v. 1 amp.		8/-
12 v. 2 amp.		1,0/9
12 v. 4 amp.		15/-
	BATTERY CHARGERS	_
200,250 1	AC Will charge 2 v 6 v and 12 v	Car

Battery at 1 amp. Hor Finished in Green han Housed in strong metal casing. long, 33in. wide, 33in. high. Guaranteed 12 mths. The above unit is manufactured by PREMIER and does not contain Ex-Govt. components. Plus 2/6 post and pkg. 39/6

BATTERY CHARGER KITS All incorporate metal rectifiers. for 200/250 v. A.C. cycle mains. Transformers are suitable

2002 Charges 6 volt accumulator at 1 amp. Resistance, supplied to charge 2 v. accumulator

2004 Charges 2, 6 and 12 v. accumulators at 1 amp. 22/6 ALUMINIUM CHASSIS 18 s.w.g.
ubstantially made from Bright Aluminium, with four

7×51×2in	4/-	10 × 9 × 31n.		7/-
7 × 3½ × 2in	3/9	12 x 10 x 3in.		7/9
91×41×2in	4/3	14 × 10 × 3ln.		7/11
10 × 8 × 2½ in	5/6	16 x 10 x 3in.		8/3
12 × 9 × 2 in	71-			
14×9×21n	7/6	16 × 8 × 2 lin.		8/-
ALUMINIL	JM PA	NELS 18 s.	w.g.	
7 × 6 in	1/3			1/-
91 × 6in	1/8	9½ × 4in		1/5
10 x 9in	2/2	10×7in		1/11
12 x 9in	2/8			2/5
14×9in	3/2			2/11
16 x 9in	3/8			3/5
20 × 9in	4/8	20 × 7 in		4/5
22 x 9in	5/2	22 × 71n		4/11

## LIMITED SUPPLIES OF 5-VALVE SUPERHET RADIO RECEIVER



CHASSIS Built to high standards ensuring quality recep-tion. Specifications: tion. Specifications:— VALVE LINE-UP: 787, 787, 7C6, 7C5, 7Y4, 3 WAVEBANDS,

774, 3 WAVEBANDS,
Long, medium and,
Long, medium and,
CONTROLE: Tuning,
wave change, volume tone control
on/off Gram Position on Switch. Pick-up and Extension Speaker Sockets incorporated. For use on 200,
250 v. A.C. mains. DIMENSIONS: Length 14in.,
height 11in, width 6in. Distance between controls,
let't to right from edge of chassis: lin. 27.19.6
3in., 6in., 3in. Plus 5i. pkg., carr., ins.

The above Chassis with 61in. Speaker, Output Transformer and Wainut Cabinet, Plus pack. £10.19.6 ing and carriage 7/6.

Famous Manufacturer's Surplus of

### ANTI - INTERFERENCE AERIALS offered at a fraction of original cost

offered at a fraction of original cost

The aerial is designed for reception of long, medium
and short waves, with any ordinary or communications
receiver, having an input impedance greater than 1,000
ohms long/medium waves and 150 ohms short waves.
The installation discriminates against locally generated
electrical interference, especially on the short wave
bands. The equipment enables the installation of an
8.3 Mo/s fiatly-tuned dipole which operates as a "T"
aerial on medium and long waves. The aerial and receiver transformers are intended to be interconnected
with a 70 ohms co-axial cable.

COMPONENT PARTS

Aluminium Aerial Transformer Assembly. Comprising

COMPONENT PARTS

Aluminium Aerial Transformer Assembly. Comprising one each: Aluminium transformer, Transformer clip, Rubber sucker, §im. x įim. brass serew, 4AB x įin. brass bolt, 4BA nat.

Receiver Transformer. Complete with Insulators, clips, etc.; Porcelain Insulators, 2 each, 60ft. Insulated Aerial Wire, 60ft. Sereened Co-Axial Down lead, Installation instruction leaflet included.

LESS CO-AXIAL CABLE & AEBIAL WIRE, 15/-, plus 146 pkg. and carr.

1/6 pkg. and carr. COMPLETE 35/-, plus 1/6 pkg. and carr.

## The New

"PREMIER PORTABLE"

USING THE NEW LANE 2 SPEED TAPE UNIT MARK 6

COMPLETE

Packing & Carriage 1 gn.

(Including Reel of Scotch Boy Tape and Microphone)

or Complete Kit including All Parts, Valves, Speaker Cabinet, Tape Unit, Reel of Scotch Boy Tape, Rewind Spool and £37.4.0 plus pkg. & carr. 15/-. Microphone at

### SPECIFICATION

★ TWO SPEEDS 7½ in. AND 3½ in. ★ 7 VAPER SECOND AMPI
--

★ THREE SPECIALLY DESIGN-★ INDEPENDENT TREBLE AND ED RECORDING MOTORS BASS CONTROLS

★ 1,200ft. TAPE REELS PRO-VIDING PLAYING TIMES OF 1 HR. AND 2HRS. ★

\* DROP IN TAPE LOADING

EASY FORWARD OR RE- COMPARTMENT WIND WITHOUT REMOVING ING MICROPHON TAPE

\* ONE KNOB DECK OPERA-

HIGH QUALITY VE FIER

MAGIC EYE RECORD LEVEL INDICATOR

AMPLIFIER MAY BE USED FOR RECORD REPRODUCTION OF HIGH QUALITY FOR HOUS-

ING MICROPHONE SPECIALLY DESIGNED MIC-ROPHONE BY A LEADING MANUFACTURER



#### SEPARATE UNITS CAN BE SUPPLIED AS LISTED BELOW:-

Amplifier (built, wired and tested with Speaker), £14/15/-, plus postage and carriage 7/6. Hire purchase terms, Deposit £4/18/4 and 12 monthly payments of £1/4/7.

Kit (including speaker,) £11/-/-, plus packing and Amplifier Amplifier Ait (Including speaker), 222 [7], plus packing and New Lane 2 speed Tape Unit Mark 6, £18/10/-, plus packing and

New Lane 2 speed Tape Unit Mark 6, £18/10/-, plus packing and carriage 7/6.

Hire purchase terms, Deposit £6/3/4 and 12 monthly payments of £1/10/10.

Portable Cabinet (Rexine covered), £4/19/6, plus postage and carriage 5/-.

Microphone, £2/19/6, plus postage and carriage 1/-.

Reel Scoth Boy Tape MC2-111 (1,200ft.), £1/15/-, plus packing and carriage 1/-.

Instruction Booklet, 2/6. Post free.

# THE MONABOLI lasts a lifetime!



## 500,000 CHANGES WITHOUT A FAULT

A radiogram manufacturer reports that the Monarch mechanism, using a special test disc, performed 500,000 changes without developing a fault.

This amounts to something like a lifetime of normal use.

Because the Monarch automatic record changer is a scientifically designed precision built instrument, leading radiogram and record player manufacturers install it as standard equipment. The excellent high fidelity performance makes this compact and streamlined unit famous for every modern gramophone use throughout the world.



The world's finest and most wanted auto-changer.

Write for complete details.

## TEN RECORD FEATURES

- 1 Plays 10 mixed diameter records at 331, 45 or 78
- records at 331, 45 or 78
  r.p.m.

  2 The unique "Magidisk"
  automatically selects 7in,
  10in, and 12in, discs,
  3 Pick-up returned and
  motor switched off after
  last record.
  4 Extended frequency range
  dual sapphire styli pick-

- dual sapphire styli pickdual sapphire styli picksapphire styli pickdual sapphire styli pickdual sapphire styli picksapphire stylin picksapphire stylin

BIRMINGHAM SOUND REPRODUCERS LIMITED. OLD HILL, STAFFS.

# Wireless World

RADIO, TELEVISION AND ELECTRONICS

## 44th YEAR OF PUBLICATION

Managing Editor: HUGH S. POCOCK, M.I.E.E.

Editor: H. F. SMITH

SEPTEMBER 1954

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## VALVES, TUBES & CIRCUITS

## 21. DETECTION IN F.M./A.M. RECEIVERS

For the detection of frequency modulated signals it is necessary to convert frequency changes into amplitude changes and to recover the intelligence contained in the original signals from the amplitude modulated carrier. The method most widely used for this purpose employs a form of phase discriminator known as the ratio detector. The particular advantage of the ratio detector is its excellent suppression of any amplitude modulation which may be present on the F.M. carrier as a result of noise or variations of gain in the earlier stages of the receiver. This type of circuit has good sensitivity and eliminates the expense of providing additional limiting stages.

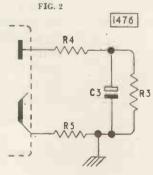
A typical form of ratio detector circuit is shown in Fig. 1, and it will be noted that two diodes with independent cathode connections are necessary. The Mullard EABC80 is recommended for use in this type of circuit. This valve is a combined triple diode and voltage amplifying triode, with a heater rating of 6.3V, 0.45A, and it is mounted on the B9A (noval) base. One diod (a"d) is provided with a separate cathode (pin 3), the other two diodes and the triode sharing a second cathode (pin 7). The ratio detector circuit employs two of the diodes (a"d and a"'d) which have low impedances (about 200 $\Omega$ ) whose ratio never exceeds 1.5. The other diode (a'd) is suitable for use in A.M. reception as a conventional detector and generator of A.G.C. voltage. The triode section is designed to be used as an audio amplifier following the detector during both F.M. and A.M. reception. Its electrical characteristics are similar to the triode section of the Mullard EBC41.

In the circuit illustrated, the primary winding L1 of the ratio filter is in the anode circuit of the final I.F. valve. The secondary coil, L2, is tuned to the intermediate frequency (10.7 Mc/s). The voltages in the two halves of L2 have a 180° phase difference, and their magnitudes depend upon the sweep frequency of the F.M. signal. The tertiary winding, L3, consisting of a few turns wound over the anode end of the primary, matches the anode circuit of the preceding I.F. stage into the diode circuit.

The ratio detector can take the form of a balanced circuit in which two equal capacitors are placed across the load resistor, R3, and their common connection taken to earth. In Fig. 1 the unbalanced type of circuit is given. Here only one capacitor, C1, has been retained, from which the audio output is taken. The  $5\mu F$  electrolytic capacitor, C3, is then necessary to stabilise the voltage across R3.

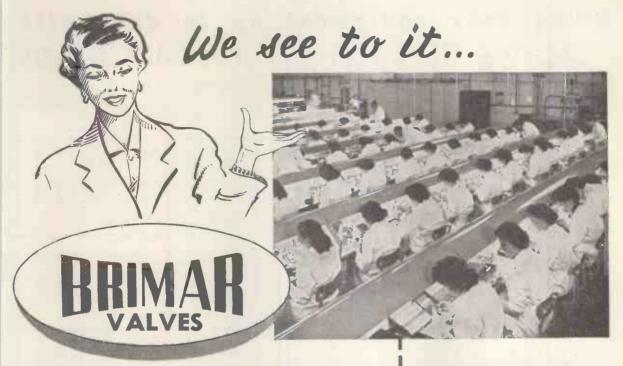
The value of load resistance ( $56k\Omega$ ) is a compromise between that required for optimum gain and the necessary A.M. suppression. Good A.M. suppression is also achieved by using a relatively high resistance,  $1.2k\Omega$ , in series with the tertiary coil. Further increase in the value of load resistance (say, to  $68k\Omega$ ), whilst resulting in larger ouput voltage, requires more satisfactory balancing in the preceding circuit in order to keep the rejection of A.M. to an acceptable value. Thus a trimmer capacitor could be connected from the centre-tap on the secondary to earth, and a small series resistance included in the lead from the centre-tap to the tertiary coil L3. These modifications will lead to a considerable improvement in suppression and some increase in sensitivity, but the preliminary adjustments to the trimmer are much more involved.

As a further refinement, some suppression can be sacrificed by connecting the stabilising capacitor across only a part of the total diode load (Fig. 2). With suitable values for R4 and R5 the suppression will depend to a much smaller extent on spreads in the forward resistance of the diodes and on variations in the amplitude.





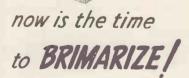
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# are more reliable than EVER!

Rigid control of production processes, a ready acceptance of improved manufacturing techniques, and continual vigilance in the analysis and selection of raw materials ensure that every BRIMAR valve will do its job more efficiently . . . more reliably.

Modern manufacturing methods backed by an intensive research and development organisation enable BRIMAR to anticipate and meet the changing demands of the radio and electronic Industries. There is bound to be a BRIMAR valve to exactly meet YOUR specification.



BIMAR

The 12AT7 is a very reliable frequency changer and is widely used in modern TV receivers, VHF and UHF communications equipment. It is also frequently employed in industrial equipment, computors, navigational aids and test equipment.



BRIMAR MULLARD		MARCONI OSRAM	COSSOR EM!TRON	
I2AT7	ECC81	B152 & B309	I2AT7	

Standard Telephones and Cables Limited FOOTSCRAY, KENT. FOOtscray 3333

# Use the BRIMAR 12AT7

with improved performance at

NO EXTRA COST

# Bring your equipment up to date with COCOS REPLACEMENT PICK-UP HEADS

If you already own a fine radiogram or record-player you now have the opportunity of rejuvenating it—of bringing it right up to date for a quite modest sum. Acos Hi-g crystal pick-ups are now available in a range of specially designed "plug-in" models to suit most famous

makes of record reproducing equipment. These Acos "Hi-g" pick-ups, you will find, represent a truly phenomenal advance in pick-up design—with regard to both reproduction and tracking characteristics (so important with many of the new microgroove recordings). Ask your Dealer!

MODEL **HGP 33-1** R HGP 37-1 Collaro **HGP 33-1** HGP 37-1 Garrard HGP 39-1 **HGP 35-1 HGP 41-1** HGP 45

HGP 33-1 Collaro. A Hi-g pick-up head incorporating the HGP 33-1 turnover cartridge for both standard and microgroove records. Will fit Collaro units RC 532; AC 534; AC3/534; 3/RC 532; and the Studio

pick-up.

HGP 37-I Collaro. A Hi-g pick-up head incorporating the HGP 37-I turnover cartridge with cantilever sapphire styli. Designed for both standard and microgroove records. Will fit the above mentioned Collaro units.

Both models available in cream or walnut.

Ask for Data Sheets No. 4700 and 4800.

HGP 33-1 Garrard. Hi-g pick-up head incorporating the HGP 33-1 turnover cartridge for both standard and microgroove records. Will fit Garrard units RC 75M; RC 80M; RC 90; RC 111; Model TA.

HGP 37-1 Garrard. A Hi-g pick-up head incorporating the HGP 37-1 turnover cartridge with cantilever sapphire styli. Designed for both standard and microgroove records. Will fit the above mentioned Garrard units.

Ask for Data Sheets No. 4700 and 4800.

Hi-g pick-up heads incorporating cantilever sapphire styll. Separate heads for standard and microgroove records. Will fit the Acos GP 20 pick-up arm and the Garrard C type adaptor. Used on the following Garrard units: RC 72A; RC 75A; RC 80; and the model M unit. Can be used on any units which at present use the GP 19 heads.

Ask for Data Sheet No. 4400.

Separate plug-in type Hi-g heads for standard and microgroove records; fitted with cantilever sapphire styli. The crystal unit is identical to that of the HGP 39-I above. Can be used on Garrard units RC 75M; RC 80M; RC 90; RC 111; and the TA player.

Ask for Data Sheet No. 4000.

Separate Hi-g plug-in type heads for standard and microgroove records incorporating the crystal unit as used in the HGP 39 pick-up head. Will fit Collaro units RC 532; AC 534; AC3/534; 3RC 532. Available in cream or walnut

Ask for Data Sheet No. 4500.

Separate Hi-g pick-up heads for either standard or microgroove records. The crystal unit is identical to that used in the HGP 39-1 head. Will fit Garrard units RC 80; RC 72A; RC 75A; and the Model M player. Can be used on any unit which at present uses the Garrard C adaptor with GP 19 heads.

Ask for Data Sheet No. 4600.



PRICE 32/6 (plus 10/5 P.T.) for all types except HGP 39 models which are 32/- (plus 10/3 P.T.)

. . always well ahead

STAND No. 44
RADIO SHOW
EARLS COURT

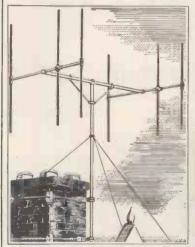
ACOS devices are protected by patents, patent applications and registered designs in Great Britain and abroad.

## "BELLING-LEE" NOTES

## A New Multi-Element Array

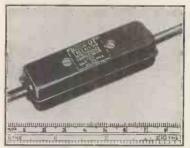
On the "Belling-Lee" stand at Earls Court there will be seen for the first time, the broadside array illustrated below.

Recently we were asked to provide a good picture in a location surrounded by the hills of South Wales. There was a poor signal and several ghosts. We arranged for the erection of a double 3element array, comprised of two "Junior Multirods" spaced a halfwave length apart. With this arrangement you can expect a theoretical gain of 3 dB over a



single "Junior Multirod" or in micro-volts, about half as many again. As the erection was something of a problem the aerial was tried out on the ground, and right away the ghosts had gone. When properly installed, the customer wrote to say that they now enjoyed a marvellous picture, black and white instead of grey. It is well worth pointing out that we could have obtained the same gain with quarter-wave spacing and consequently a smaller and more manageable array, but the half-wave spacing gives a truly remarkable front-to-back ratio, which in turn greatly reduces unwanted signals.

The installation of this rather difficult aerial was in the capable hands of Mr. G. R. Silverthorne, Radio House, Abergavenny, who is fine job.



## "Telefilter"

This is the name given to a miniature flex lead suppressor designed to be fitted in the lead of a small domestic appliance for the abatement of interference to television. As it contains chokes, its application is limited to appliances taking not more than 2 amps. It does not suppress at broadcast frequencies unless used with a plug suppressor such as L.1308.

The "Telefilter" is also available moulded into a lead with which an appliance could be wired.

#### Aircraft Fuselink

This new fuselink L.1330 has been specially developed for use on 30 V circuits and is being manufactured in ratings from 35 amp. to 275 amp. It is very light



in weight and is intended for direct bus-bar mounting, thus obviating the use of a holder with its cost and weight. It is expected to be explosion proof, and tests in this respect are still being carried out.

This type of fuse-link is already in service on considerable numbers of American aircraft and is expected to go into service very shortly on the Vicker's Viscount and other British-made aircraft. A.R.B. and Ministry of Supply approval is being sought. It is interchangeable with the American types and is, as far as we know, the only one of its kind manufactured on this side of the Atlantic, and therefore should be a dollar saver.

Advertisement of BELLING & LEE LTD. to be congratulated on a really Great Cambridge Rd., Enfield, Middx. Written 20th July, 1954.

# ACHIEVEMENT



The unique internal soldering technique, employed in the manufacture of "Belling-Lee" standard fuse-links, bonds caps, element and glass into one unit. The risk of caps becoming loose is minimised, and a 100% fuse-link can only be rendered useless by breaking the glass, or by blowing in

Improvement in electrical performance is achieved by setting the wire element on the diagonal, which enables it to be more accurately tensioned, thus ensuring that the fusing currents will be kept within "close . This new method of construction limits applies only to ratings from 500 mA up to 25 A. Lower ratings, down to 60 mA, are however, available.

Designed to blow within 10 sec. on a steady a.c. or d.c. 100% overload. List No. L1055/Rating. Size I½" x ½"

- More consistent electrical and mechanical performance
- Caps, element and glass held as one-no cement to deteriorate, no solder blobs
- Caps permanently fixed
- Rating coded on caps

All "Belling-Lee" fuse-links undergo full inspection, and blowing tests are constantly carried out on sample batches.

Please write for catalogue P.347/W.W.

GREAT CAMBRIDGE RD., ENFIELD, MIDDA., ENGLAND



Typical of the Ekcovision range is this 14" aluminisedtube table model incorporating Ekcovision Turret Tuning, Full Automatic Picture and Sound Control and Optical Filter. Handsome cabinet in walnut veneers. AC/DC mains.

MODEL T221

66 GNS.

Tax Paid.

GOOD LOOKING See for yourself the clear brilliant pictures on Ekcovision. And notice the many picture-improving refinements of this fine range of 14", 15" and 17" receivers. Choose for the future, too! Ekcovision 13-channel Turret Tuning is already incorporated in some models, and can be fitted at any time in others for easy, efficient reception of the Alternative Programmes as and when they become available in your locality.

GOOD LISTENING Hear and enjoy the wonderful fidelity and

depth of sound of Ekco radio. You will find there are models of every size and price for your listening pleasure.

GOOD VALUE Every receiver, Vision and Radio, is backed by outstanding Ekco quality-engineering and utmost reliability. Distinctive in design and performance, these receivers offer you exceptional value-for-money! Your Registered Ekco Dealer can offer you expert Ekco 'Sales and Service' and will see that you get full and lasting satisfaction from the receiver you choose.

**EKCO** 

vision and radio

NATIONAL RADIO SHOW STAND 92

choose

# EKGO

for

good ...



#### **MODEL ARG233**

5-valve all-wave, floor standing auto-radiogram. Plays up to eight 12" or ten 10" or 7" records at three speeds. 5-position tonecontrol. Mahogany veneered cabinet, For A.C. mains. 66 gns. Tax Pald,



#### MODEL A160

All-wave superhet in handsome walnut veneer cabinet. 8" speaker. Floodlit tuning scale. Sockets for gramophone pick-up and for tape recording. For A.C., mains.

£26., Tax Paid.

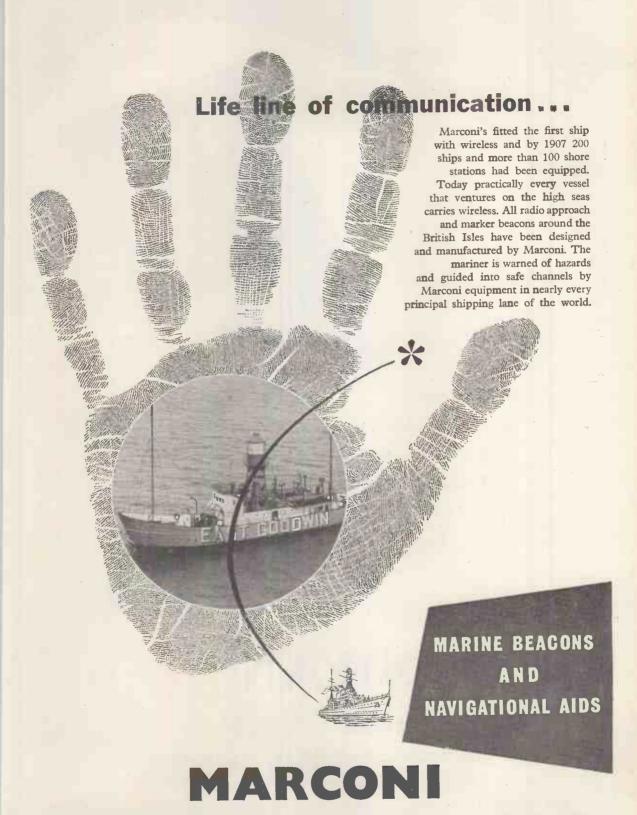


#### MODEL A222

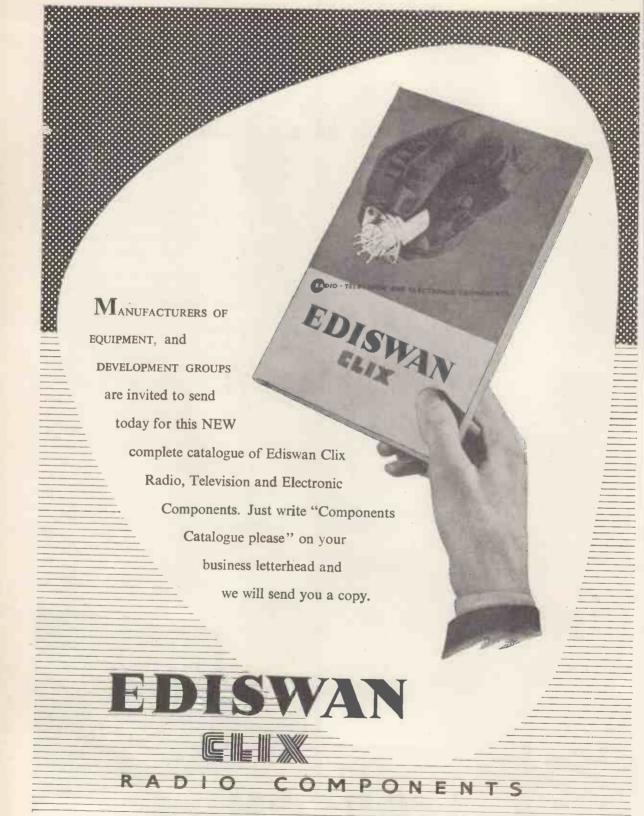
The Ekco 'New Radiotime' combines a 4station switch-tuned radio and a Smiths mains-operated clock, It tells the time, acts as an alarm and switches itself 'on' and 'off'. Inbuilt aerials and sockets for extension speakers. For A.C. malns.

20 gns. Tax Paid.

K. GOLE LID., SOUTHEND-ON-SEA, ESSEX

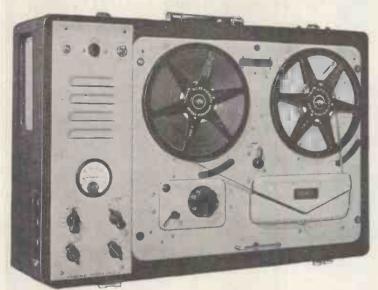


MARCONI'S WIRELESS TELEGRAPH COMPANY LIMITED . CHELMSFORD . ESSEX



THE EDISON SWAN ELECTRIC COMPANY LIMITED, Member of the A.E.I. Group of Companies
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C.R.1a Radio Components Sales Office: 21 Bruton Street, London, W.1 Telephone: Mayfair 5543

# VORTEXION TAPE RECORDER



The amplifier, speaker and case, with detachable lid, measures  $8\frac{1}{4}$  in.  $\times$   $22\frac{1}{2}$  in.  $\times$   $15\frac{3}{4}$  in. and weighs 30 lb.

 ★ The noise level is extremely low and audibly the hum level and Johnson noise of the amplifier and deck are approximately equal. Only 25% of this small amount of hum is given by the amplifier alone.

Extremely low distortion and background noise, with a frequency response of 50 c/s.—10 Kc/s., plus or minus 1.5 db. A meter is fitted for the measurement of signal level and bias level.

★ Sufficient power is available for recording on disc, either direct or from the tape, without additional amplifiers.

★ A heavy mu-metal shielded microphone transformer is built in for 15-30 ohms balanced and screened line, and requires only 7 micro-volts approximately to fully load.

The .5 megohm input is fully loaded by 18 millivolts and is suitable for crystal P.U.s, microphone or radio inputs.

A power plug is provided for a radio feeder unit, etc. Variable bass and treble controls are fitted for control of the play back signal.

★ The power output is 3.5 watts heavily damped by negative feedback and an oval internal speaker is built in for monitoring purposes.

★ Facilities are provided for using the amplifier alone and using power output or headphones while recording or to drive additional amplifiers.

★ The unit may be left running on record or play back even with 1,750 ft. reels with the lld closed.

POWER SUPPLY UNIT to work from 12 volt Battery with an output of 230 v., 120 watts, 50 cycles within 1%. Suppressed for use with Tape Recorder. PRICE £18 0 0.

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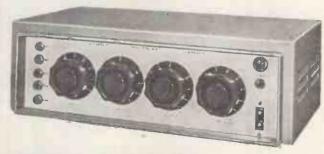
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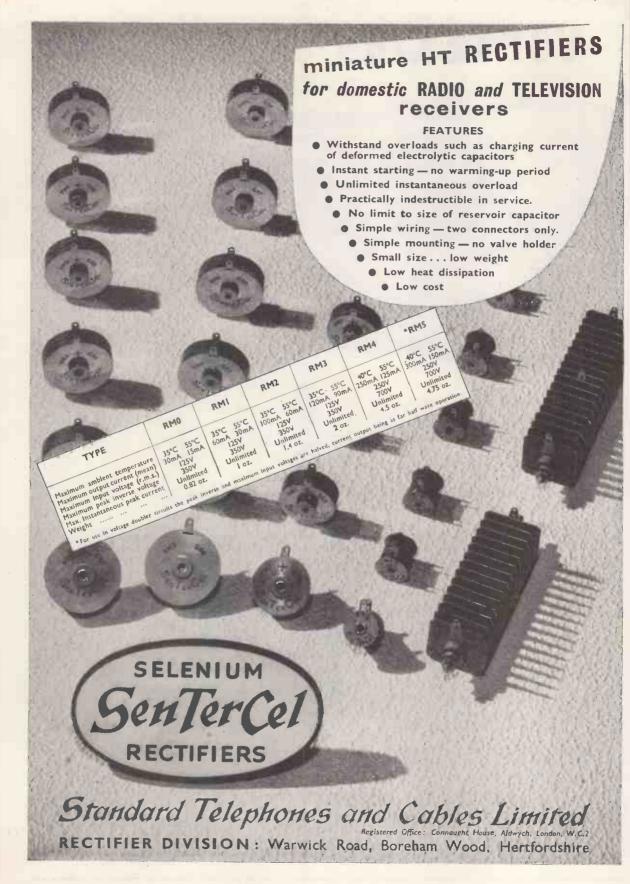


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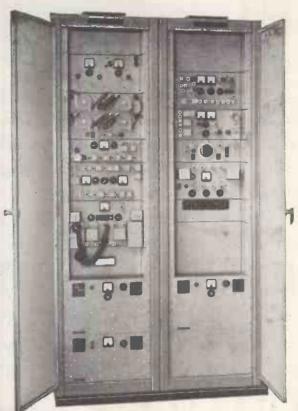
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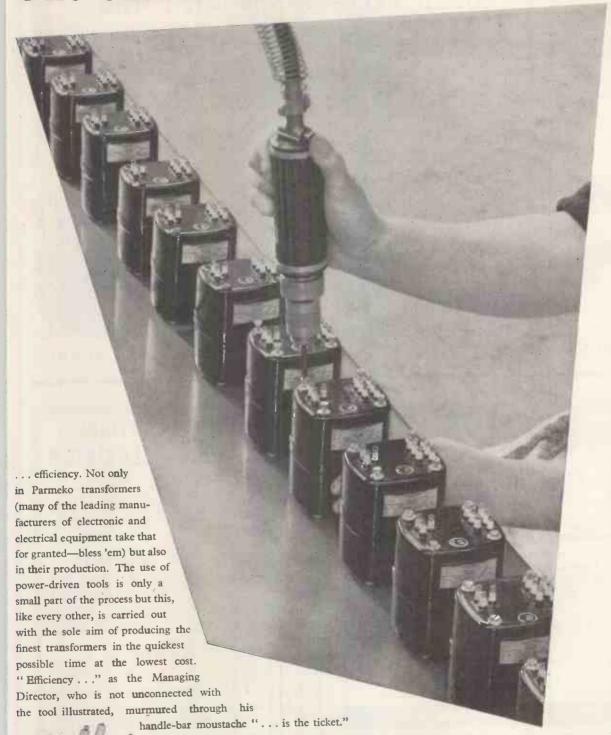
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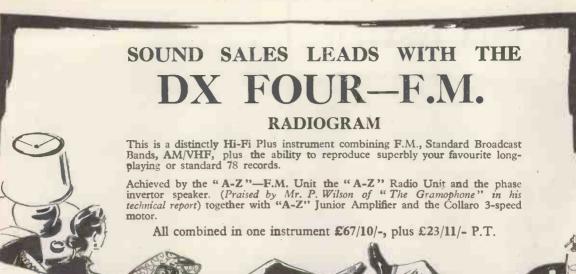


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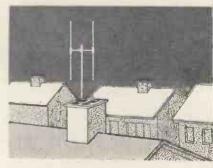
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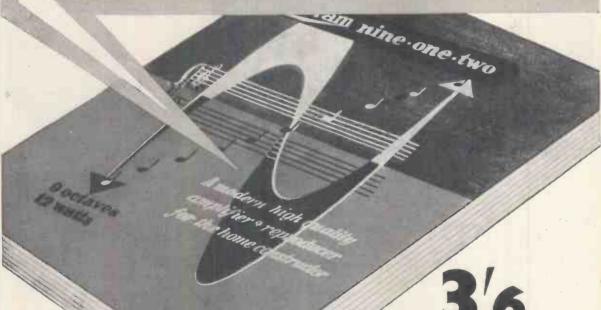
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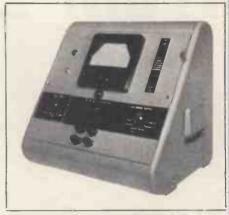
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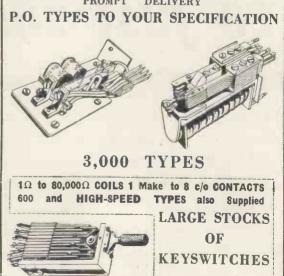
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2 amps	16/6	
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100 m/a.  All the above have 6.3 4-0 v, at 4 amps., 5-4-0 v. at 2 amps.	23/	
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The above have inputs of 200/250 v.	31/6	
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FU6. 0-2-4-5-6.3 v. @ 2 amps., 10/ F12. 12.6 v. tapped 6.3 v.		
@ 3 amps	16/6 23/6	
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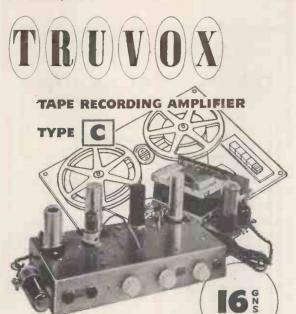
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#### TECHNICAL SPECIFICATION

(a) Inputs: At Jack No. I (i) during recording 1-2 mV (crystal microphone) at I megohm impedance. (ii) for use as microphone amplifier 1-2 mV at I megohm. At Jack No 2 (i) during recording 0.5 v. at impedance of  $\frac{1}{2}$  megohm suitable for pick-ups and radio connection. (ii) for replay 0.5 v. at  $\frac{1}{2}$  megohm. At Jack No 3 for replay 0.5 v. suitable for pick-up connection at  $\frac{1}{2}$  megohm. (b) Output: 4 watts output at impedance of 3 ohms suitable

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(c) Oscillator: Brought into circuit on record. Flxed frequency at approximately 45 Kcs. at high impedance to suit Truvox Tape Deck. Erase voltage at least 150 v. Bias 80 v. approx.

(d) Level indication by Magic Eye Indicator: Taken out

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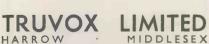
(e) Hum level: 50 db down at 4 watts.

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not in excess of 300 v.

The amplifier is designed to operate from AC supply mains 110-250 v. List price 16 gns.





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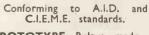
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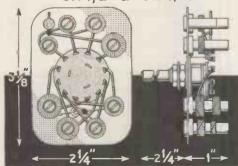
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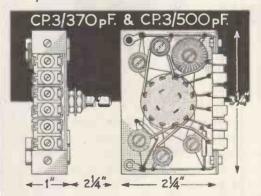
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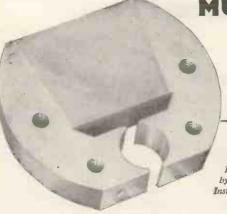


These 3 waveband Coil Packs are available for use with either 370 pF or 500 pF tuning condensers. The coverages are: Long wave 800-2,000 metres, Med. wave 200-550 metres, Short wave 16-50 metres. Designed for use with Jackson Bros. Full Vision Drive or SL8 Spin Wheel Drive. Retail Price of each unit:

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8 dB
Front/back Ratio
21.6 dB
Acceptance

Angle 55°



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Max/min Ratio
25 dB
Acceptance
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25 dB
Acceptance
Angle 176



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3.75 dB
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40 dB
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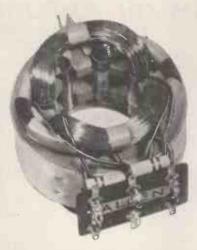


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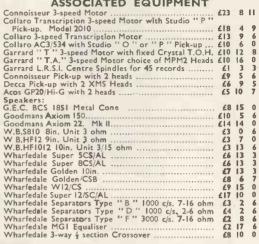
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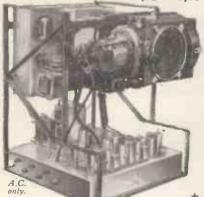


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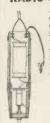
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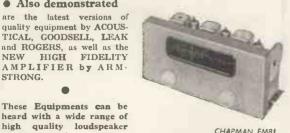
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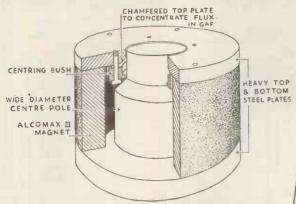
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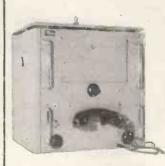
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than 80 db down. overall loop being 28 db obtained by means of a tertiary winding on the output transformer. Input required: 250 millivolts for 10 watts overall loop being 28 db obtained by means of a tertiary winding on the output transformer. Input required: 250 millivolts for 10 watts output. Valves used: Mullard low noise pentode EF86, ECC82, double triode, 2 EL37, triode-tetrode connected, GZ32 indirectly heated rectifier. ALL COMPONENTS FULLY TROPICALISED. Mains transformer by WODEN, PARTRIDGE output transformer, TCC condensers, Morganite controls and resistors. Mains input: Model Al0, 200-250 v. A.C. 50 cycles, Model Al0E, 100-110 v. A.C. 40-60 cycles. Finished: Hammered bronze.

When comparing prices of High Fidelity Equipment THE A.10 INCORPORATES ALL NECESSARY FILTERS, and no additional filter units are required. ARY FIL-

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Controls: 1. Input (a) Radio 50-150 Millivolts. (b) Gram. (low impedance) 15-100 m.v. (c) Gram. (high impedance) 70-150 m.v. (d) Microphone or Tape Recorder 10-100 m.v. 2. Equaliser (a) 78<sup>1</sup> (b) 78<sup>2</sup> (c) L.P. (d) American NARTB 3. Filter (a) Roll-off 5 kcs. (grad.) (b) 7kcs. (c) 9 kcs. (d) 9 kcs. (steep). (e) Level response. 4. Treble lift or cut of 15 db. 5. Bass lift or cut of 15 db. 6. Volume control combined with on/off switch. Valve: Mullard BCC83 double triode. Power supply for radio unit 300 v. 20 ma., 6.3 v. 1.5 a. Finished: Hammered bronze with engraved Florentine bronze panel.

SEE PAGES 82-129 for our NEW Radiogram Chassis, Radiograms, and Television Models.

EARLS COURT VISITORS see Page 161 for details of how to get to our DEMONSTRATION ROOM at HOLLOWAY. We shall be open daily from 9 a.m. to 6 p.m. (Saturdays until 5 p.m.). Special High Fidelity Demonstrations on Thursday evenings 8 p.m. DEM-ONSTRATIONS also available at your local High Fidelity Specialists.

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Captain			27	£860	£997
Major			34	£1,188	£1,325
Lt. Colonel			42	£1,453	£1,581
Colonel			45	£1,791	£1,919
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(Note:—This is the U.K. scale; there are various additions in certain overseas stations. In this table the figures of a single officer's pay include an element for food and accommodation which are normally provided in kind. This has been done to provide a direct means of comparison with civilian scales of

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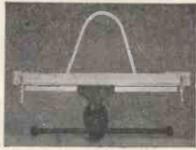
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a. Excellent band width of I.F. circuits.

a. Excellent band width of I.F. circuits.
b. A really efficient video amplifier.
c. C.R.T. Grid modulated from low impedance source.
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The picture brilliance is also much above the average and enables comfortable viewing with normal room lighting or daylight.
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Negative feedback is used in the audio frequency circuits which provide 2/3 watts of High Quality Sound.

Entire receiver built on two chassis units each measuring 14in. x 6in.

C.R.T. mounting enables entire receiver to be safely handled with tube in position.

All pre-set controls are mounte d on side of chassis, enabling all adjustments to be carried out whilst facing the C.R. Tube.

This complete TELE-VISOR, including all Valves, can be built for only £28/16/4

As no hire purchase terms are available the receiver can be bought As no hire purchase terms are available the receiver can be bought in five separate stages (practical diagrams and circuits are provided for each stage) thus enabling hire purchase interest rates to be avoided. The complete set of ASSEMBLY INSTRUCTIONS is available, price 5/-. The instructions include really detailed PRACTICAL LAYOUTS, WIRING DATA AND COMPONENT PRICE LIST. ALL COMPONENTS ARE AVAILABLE FOR INDIVIDUAL PURCHASE.

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A design that retains all the distinctive features of the 121n. Telvisor but with increased Time Base efficiency, producing 15 to 16 kV. E.H.T., with ample scanning power for C.R. Tubes up to 17in.

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This amplifier will give 3 watts output for the small input voltage of only 75 millivolts, and is therefore suitable for use with any type of pick-up from the crystal type to the miniature H/F Magnetic type.

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short trailer aerial.

The simple design of this Receiver is so arranged that either a 3-valve set or a 2-valve (afterwards easily converted to the 3-valve) can be

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Valve line up 174—

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A design of a simple 1-valve 2-stage Battery Receiver, giving excellent results on medium and long wavebands and having exceptionally low battery consumption. Drilled chassis and practical diagrams make it the ideal set for the beginner to build.

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Valve line up 6K8—6J7—KT61, plus Metal Rectifier.

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Or to cover both Long and Medium Waves for If the Receiver is first built to cover the Medium Waveshor, Long Waves can be added at any time, separate diagrams are provided for this purpose. The attractive Polished Wood Cabinet 114 inches wide, 81 inches high and 6 inches deep illustrated above is The CONSTRUUTOR'S MANUAL is available for 1/1-, this shows the component prices, which are all available for separate purchase.

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This comprehensive PRE-AMPLI-PIER and TONE CONTROL UNIT provides a full con-trol of base and treble in conjunction with a main Volume/Mixer Control.

Volume/Mixer Control.

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VALVE T.R.F. CHASSIS FOR ONLY

Including a 5in, P.M. SPEAKER and VALVES

This receiver is of the very latest design and is for use on A.C. or D.C. Mains. It covers both Long and Medium Wavebands, and includes the modern BVA miniature valves. The line up being 12 BA6-12AT6-12A6-35W4.

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Price of COMPLETE KIT including Valves and Drilled Chassis, etc. £7/10/0

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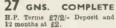
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Designed for high quality reproduction up to an output level of 10 watts, having 8V8s in Push-Pull and incorporating negative feedback. It is suitable for use with all types of Pick-ups and most types of microphones and the output transformer provides for use of 3 and 15 ohm speakers.

#### RRIEF FEATURES

- Valve line up 6J5, 68N7, 5Z4, with 6V6s in push-puil.
- The undistorted output level of up to 10 watte is produced from an input of 25 First class reproduction of Radio (where a Tuning Unit is used) and Record Playing.
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- Power supplies (HT and GT) are available for a Tuning Unit.
- For operation on A.C. Mains 200-250 volts 50 cycles.
   THE ASSEMBLY MANUAL is available for 1/- and includes detailed layouts and com-

The NEW "LEAK" TL/10 AMPLIFIER and "POINT ONE" PRE-AMPLIFIER



This Amplifier has a maximum output of 10 watts and maintain in overy sepect maintain in overy sepect maintain in overy sepect maintain in overy sepect maintain of the overy sepect maintain over the over th

A BULK PURCHASE ENABLES THIS SPECIAL PRICE REDUCTION OF THE FAMOUS

#### SHAFTESBURY PORTABLE AMPLIFIER



Suitable for home use and small Halls. Has matched inputs for both Record Players and Microphone. Also provides for the "mixing" and "fading" of both Gram, and speech as requested.



(a) A 4 Vaive High Gain Amplifier for use on A.C. or D.C. mains 200-230 volts with 5 watta output. Incorporating independent Volume Controls for Mike and Gram, either of which can be taded at will, a variable Tone Control and independent input sockets for Mike and Gram.

(b) A Transverse Carbon miorophone which obtains its polarizing current from the amplifier—no batteries are necessary.

(c) An Sin. Goodman P.M. Speaker with the "Ticonal" magnet for first-

THE COMPLETE EQUIPMENT is all contained in the £18' PORTABLE CARRYING CASE U

Having been reduced from £30/9/-. HIRE PURCHASE TERMS DEPOSIT £4/10/0 and 13 monthly payments of £1/5/4.

• Light in weight • Easy to CARRY • GENUINELY PORTABLE An illustrated leadet containing free data is available on receipt of S.A.E.

#### A 12 Watt "HIGH FIDELITY" Push-Pull AMPLIFIER

Push-Pull AMPLIFIER
Comprising a Main Amplifier Chassis and a Remote Control Pre-Amplifier-Tone Control Unit. The remote control unit measures only 7in. × 4in. × 2in. and contains four controls, being: Bass-Treble-Volume and a Radio, Gram, Microphone Switch control. It incorporates its own feedback circuit on the Bass Channel. Loop negative feedback is employed on the Main Amplifier which has a valve line up of 615-6N7-5U4 with two PX25's in push-pull and 635 and 68N7 are used in the remote control unit. THE COMPLETE KIT IS AVAILABLE FOR £14/0/0

(Carr. & Ins. 3/. extra). THE COMPLETE UNIT ASSEMBLED

THE COMPLETE UNIT ASSEMBLED
AND READY FOR USE 217 / 0 / 0 (Carr. & Ins. 5/- extra).
H.P. Terms 24/5/- Deposit, 12 Months at 21/3/11.
The measured frequency rags or the amplifier with this unit shows an excellent response from 160 to 10 gain at so the amplifier with this unit shows an excellent response from 160 to 10 gain at both ends of the frequency range from zero to a gain of 50.
The short of the short of the short of the frequency range from zero to a gain of 50.
The short of the short of



### A 4-VALVE QUALITY "PUSH-PULL" 6-8 watt AMPLIFIER

for use on A.C. mains. Incorporat-ing Negative Feedback. FilterInput Circuit and employing 6V6s in Push-Pull. A 6V6s in Push-Pull. A simple arrangement is provided to enable either a magnetio, crystal or lightweight plck-up to be used, and is suitable for use with Standard or pushing records.

### WE HAVE IN STOCK THE NEW COLLARO "TRANSCRIPTION" RECORD PLAYERS

Model 2000 comprises the Transcription Motor and Turntable complete with 3-speed Gear and Switch mounted on a banjo type unit plate. Price 213/9/8. H.P. terms—Deposit 23/7/- and 12 monthly payments of 19/. Model 2010 has the same specification as the Model 2000 except that it is mounted on a rectangular unit plate and is equipped with the STUDIO "P" HIGH FIDELITY PIOK-UP HEAD. Comprising a special low resonance arm and special bearings.

Price £18/4/9.

H.P. Terms—Deposit £4/14/9 and 12 monthly payments £1/5/4. An illustrated leaftet is available on receipt of 8.A.E.



RODGERS-RD BABY de Luxe Mk IJ AMPLIFIER with RD JUNIOR MK II

£23/0/0 (Plus 7/6 Carr. & Ins.)

H.F. Terms: £5/15/- Deposit and 12 months at £1/12/4.

In months at £1/12/4.

A medium-priced 8-10-watt push-pull de Luxe Amplifier of very attractive appearance and embodying a high standard of workmanship. Complete performance data is available. Please send S.A.E.

THE COLLARO MODEL 3/514 3-Speed Non-Auto Change Unit £7/19/6 (Plus 6/- Carr. and Insur.) Normal Price £12/17/6

- Complete with High Fidelity Crystal "TURNOVER" Head which incorporates a separate stylus for L. P. and Standard Records.
   Will play 7 Inch, 10 inch and 12 inch Records.
   Brand New and Complete with mounting instructions.

When submitting orders, please include postage and packing.



RECEIVER CHASSIS

# Modernise your old Radiogram

### RECORD PLAYERS

COMPLETE RADIOGRAM EQUIPMENT-QUALITY AT LOW COST

STERN'S DESIGN FOR HOME CONSTRUCTORS This AUTOCHANGE UNIT by a famous Manufacturer The "SUPER-SIX"

compact and highly efficient superhet Radio-Radiogram chassis of outstanding quality.

YOU CAN BUILD IT FOR £10/7/6 Including the OCTAL VALVE LINE.UP. (£12/7/6 with the miniature valves)

We will supply it assembled and READY FOR USE for

£13/13/0 (Plus 7/6 Carr. & Ins.)

H.P. Terms £3.10.6, deposit and 12 months t 19/-.

at 19.Incorporating the new B.V.A. Miniature Valve Line-up.
This receiver is designed to the very latest specification
and provision is made to incorporate either the standard Octal
Valve Line-up or the new B.V.A. range of miniature valves. Great
attention has been paid to the quality of the reproduction of both Radio reception and Record
playings, and excellent clarity of speech and music is obtained.

A few brief details:

A few brief details:

Covers 3 wavebands 18-50 metres, 190-550, and 800-2,000 metres.

Employs 6 valves having PUBH-PULL for 5-6 watts output.

Incorporates delayed A.V.C. on all wavebands and pre-selective feedback.

A 4 position Tone Control operates on both Radio and Gram.

Has independent mains supply socket for a Record Player.

Size of Assembled Chassis Izlin. × 8 lin. × 8 lin. Dial aperture 8 lin. × 4 lin.

For operation on A.C. mains 200-250 volts 50 cycles.

THE INSTRUCTION and ASBEMBLY MANUAL is available for 2/-, it contains very detailed practical drawings and circuit diagrams and a complete Component Price List.

#### THREE COMPLETELY ASSEMBLED ALL-WAVE SUPERHET CHASSIS

Model B.3. A 5-valve 3-waveband Receiver.

Model B.3.P.P. A 6-valve 3-waveband Receiver with PUSH-PULL OUT-

Model B.3.P.P. A 6-valve 3-waveband Receiver incorporating an R.F. stage with PUSH-PULL OUTPUT.

The three Receivers are for operation on A.C. mains 100/110 voits and 200/250 voits, and majov the very latest miniature valves. They are designed to the most modern specification, reat attention having been given to the quality of reproduction which gives excellent clarity of speech and munic on both gram, and radio, making them the ideal replacement chassis or that "old Radiogram," etc.

Brief specifications: Model B.3.—Valve line-up, 6BB6, 6BA6, 6A76, 6BW6, 6X4—waveband coverage short 16-50, medium 187-550, long 900-2,000 metres. Controls: (1) volume with on/08; (2) tuning (flywheel type); (3) wavechange and gram; (4) tone (3-position switch operative on gram, and radio), Regative feedback is employed over the entire audio stages. Chassis size: 11 x 78 x 8 yiln, high, Duls size 63 x 4 its. Price complete and READY FOR UBE, excluding speaker 212/12/- (carr. and ins. 7/6 extra).

H.P. Terms: £3/4/- deposit, 12 months at 17/6.

H.P. Terms: £3/4/- deposit, 12 months at 17/6.

months at 17/6.

Model B.3.P.P. This model is to be a few first and many and the surface of the surface and th

#### !!AN OUTSTANDING OFFER!!

A BULK PURCHASE ENABLES US TO OFFER THIS "PUSH-PULL" 7 VALVE SUPERHET RECEIVER

For only £12/19/6 (Carr. and Ins. 7/6 extra). H.P. Terms £3/4/6 Dep. 12 months at 18/4.

(Carr. and ins. 7/9 extra). 12 months at 18/4.

These receivers Model AW3-7 are made by a well-known set manufacturer and incorporate the latest Osram Valve Line-up of X79—W77—DH77—H77—U79 and two X78's in Push-Pull for approx. 7 watts output.

They cover 3 wavebands 18-50 metres, 190-550 and 800-2,000 metres, and are for operation on A.O. mains 200-250 volts.

They make an excellent replacement Radlogram Chassis having a P.U. connection on the chassis. Extension speaker connection is also provided.

Overall size of chassis: 12lin. long x 7½ in. x 8½ in. high, dial aperture

8½ in. x 4½ in. (Dial Escutcheon available for 4/9).

THESE RECEIVERS ARE BRAND NEW AND FULLY GUARAN-TEED.

109 and 115 FLEET ST.

London, E.C.4. 'Phone: CENtral 5812/3/4

is offered for £11'10'0 (Plus 7/6 Carr. and Ins.)

Hire Purchase Terms £2/17/6 Dep. and 12 Months at 16/4. (Normal price is £16/10/-).

• These units will autochange on all three speeds, 7in., 10in. and 12in.

• They play MIXED 7in., 10in. and 12in. records.

They have separate sapphires for L.P. and 78 r.p.m., which are moved into position by a simple switch.

Minimum baseboard size required 14in. x 12½in., with height below baseboard 2½in. and height below baseboard 2½in. A bulk purchase enables us to offer these BRAND NEW UNITS at this exceptional varies.



The COLLARO 3RC/521 3-SPEED AUTO CHANGE UNIT H.P. Terms £2/10/0 Deposit and 11 months at 15/9. £9/19/6 (Plus 7/6 Carr. and Ins.)

Normal price £18/10/-.

Complete which High Fidelity Crystal "Turnover" Head which incorporates separate stylus for L.P. and 78 r.p.m. Records.

Will autochange on 7in., 10in. and 12in. records not inter-mixed.

Minimum Baseplate size
 15in. x 12½in., with height above
 4½in. and below baseplate 3in.

Brand new in Maker's Cartons, complete with Mounting instruc-tions.



#### A Replacement RADIO-RADIOGRAM

CHASSIS



e MODEL AW3-5. A 5-Valve Superhet Receiver covering the standard 3 wavebands, 16-50, 190-559, 900-2,000 metres. PRICE COMPLETELY ASSEMBLED E10/10/0 (plus 7/6 carr. and ins.)

R.P. Terms 22/12/6 Deposit and 12 Months at 15/-. This receiver is for operation on A.C. Mains 200-250 voits. It contains the latest MULLARD VALVE LINE-UP. being ECH42 (Freq. Ch.), Fr41 (LF.), EEC41 (Det. 1st Audio), EL41 (Output) and EZ41 (Rect.). It incorporates Negative Feedback and delayed A.V.C., the four controls being (1) Tuning. (2) Wavechange and Gram. Switch. (3) TONE. (4) VOLUME-OFF. It provides really good reproduction on both Gram. and Radio and gives an exceptionally good range of ration selection. Overall size 134 in. × 7in. high x 6in. deep. Diai aperture 10in. x 44in.

### SPECIAL REDUCTIONS FOR COMPLETE EQUIPMENT

SUMMARY

Select a RECORD PLAYER and CHASSIS and we will supply it TOGETHER WITH AN 8-inch or 10-inch P.M. SPEAKER as follows :-

THE £11.10.0 AUTOCHANGER WITH A SPEAKER AND Cash Price Deposit Monthly

B3 chassle 224 176 Deposit Dep (a) With Model B3 chassis (b) Rapp 12 of £1 12 10 12 of £1 17 4 12 of £2 1 6 12 of £2 1 6 12 of £1 17 4 12 of £1 9 10 12 of £1 13 2 000000

# Prices slashed at Clydesdale

PLEASE NOTE. Carriage and Postal charges refer to the U.K. only. Overseas freight, etc., extra

INDICATOR UNIT "A.S.B." SERIES (U.S.A.)

Contains: 5 BPI C.R.T. with mu-metal screen, 3/6H6s, 2/6SH7s, 6AG7, 6AC7, plus H.V conds, etc. Metal case 18½ in. x 8½ in. x 8½ in. All controls brought to front panel beside viewing screen. ASK FOR X/E771

ASK FOR X/E771

29/6 each 1/6 EXTRA RECEIVER UNIT R3601. Ref.: 10DB/6037 £3.19.6 each

INDICATOR UNIT TYPE 62 With VCR-97 tube, and valves, 16-VR65-CVII8 (SP61), 2-VR54 (EB34), 2-VR92 (EA50), etc. Dim.: 18in. x 18\frac{1}{2}in. Wgt. 42 lb. In original wood case. ASK FOR CARRIAGE £3.19.6 each

INDICATOR UNIT TYPE 62

as above, but in used, good condition, loose stored. ASK FOR X/E774 CARRIAGE £2.9.6 each

INDICATOR UNIT TYPE 305
Ref. 10 QB/6504. Brand New.

With tubes, VCR/524A, VCR525, and valves
7/VR91 (EF50), 2/VR54 (EB34), 6/VR92 (EA50).

Dim.: 12ln. x 7in. x 18in.
ASK FOR Dim.: 12In ASK FOR X/H493.

£3.19.6 each CARRIAGE **POWER UNIT TYPE 285** 

Ready made for T.V.
A.C. mains, input 230 v. 50 cps. Outputs E.H.T.
2kV. 5 mA. H.T. 250 v. 150 mA. L.T. 6.3 v. 10 a. and 6.3 v. 5 a. Fully smoothed and rectified with valves VUI20, 5U4G, VR91 (EF50), plus cond.

resistors, etc. ASK FOR X/H947 £4.19.6 each CARRIAGE

INDICATOR UNIT TYPE 6 With VCR97 Tube and valves 4/VR91 (EF50). VR54 (EB34), 3/VR92 (EA50), VR78, (D1), etc. Dim.: 18In. x 8½in. x 7½in. Wgt. 21 lb. In original wood case.

£2.19.6 each CARRIAGE 5/- extra ASK FOR X/H524

BEGINNER'S T.V. Mains Transformer each £1 12
Output Transformer each Crystal Diodes each 5

THE BEGINNER'S TIMEBASE Mains Transformer ......each £1 0 0 E.H.T. Transformer each £2/10/- and £2 5 0

INDICATOR UNIT TYPE 6H With VCR97 Tube and valves 4/VR91 (EF50). 3/VR54 (EB34). Dim.: 18in. x 8½in. x 7½in. Wgt. 22 lb. In original wood case. ASK FOR £4.9.6 each CARRIAGE X/F777

ION TRAP MAGNET ASSEMBLY

Type IT/6 by Elac for 35 mm, tube neck.
X/H919 2/6 each 3d. EXTRA

IF/AF AMPLIFIER UNIT R1355
With Valves 8/VR65 (5P61), 5U4G, VUI20A
(5U150A), I.F 7 mc/s., etc. Dim.: 18in. x 8jin. x
7jin. Wgt. 31 lb. Used, good condition. In transit case,

ASK FOR X/E770A £1.12.6 each R.F. UNIT TYPE 24. In original carton. With valves 3/VR65 (SP61), etc. Range 20-30 mc/s. switched tuning, Dim.: 9½in. x 7½in. x 4½in.

Wgt. 7 lb. ASK FOR X/H850 15/- each I/6 EXTRA

R.F. UNIT TYPE 25. In original carton.
Range 40-50 mc/s., otherwise as R.F.24. ASK FOR X/H847 POST 19/6 each I/6 EXTRA

RECEIVER UNIT R3601. Ref.: 10DB/6037 With valves 2/VR136 (EF54), VR137 (EC52), 5/VR65 (SP61), 4/VR92 (EA50), VR91 (EF50), 6V6G, VU39A (R3), etc. 1.F. 13 mc/s. Dim.: 18in. x 9in. x 8in. Wgt. 38 lb. ASK FOR £1 10 6 CARRIAGE

£1.19.6 each **XEH493** 

EX U.S.N. TEST OSCILLATORS TS-24/ARR2

Low/high frequency, battery powered for TBX alignment, H.F. signal 245 mc/s. I.F. signal tunable 540 to 830 kc/s. with valves 2/955 acorn triodes and clockwork time switch with calibrated dial 0/30 minutes. Unit Dim.: 9\frac{1}{2}\text{in. x 7\frac{1}{2}\text{in. x 7\fr

27/6 each

Aluminium, telescopes from 14in. to 7ift. Seven sections, base dia. in. Wgt. 4 oz. ASK FOR X/H489

4/6 each

CARRIAGE

AERIAL ROD

AEKIAL ROD

15in, lengths, copper plated steel tube, ferruled to interlock an aerial of desired length. 12in. dia. Ask for X/H709. 13in. dia. Ask for X/H710. EITHER

166 doz. POST 4/6 doz. POST lengths. 6d. EXTRA UNIT

RADAR REFLECTOR AERIAL MX/137/A Spider web mesh aerial in original molsture-proof carton, with assembly instructions. ASK FOR 1/14 POST

4/11 each 9d. EXTRA X/E175

AERIAL SYSTEM TYPE 62 U.H.F. Antenna on streamlined moulding with VR92 (EA50), untuned detector stage. Overall dim. 13in. x 4\frac{3}{2}in. Antenna 22.5 cm. ASK FOR 2/8

3/6 each 9d. EXTRA X/H496 Circuit 1/3 each.

CERAMIC AERIAL SPREADER
Individually boxed. Length overall IIin., between centres 9 iin.
ASK FOR 4/ per POST 1/- per pair X/H718 3d. EXTRA

GLASS DOMED INSULATORS With threaded terminal top and metal lead-through rod. Dome dim.: 2½ n. x 1½ n. high, lead-through projects 6½ n. Overall length 9½ n. ASK FOR POST 2/- each 3d. EXTRA

MICROPHONE, Ref. 10A/14381 (Flying Helmet type) Electro Magnetic 500 ohms. with switch, lead and

2 way sockets. ASK FOR X/E16 3/11 each 6d. EXTRA

WALNUT-FINISH WOOD RADIO

CABINET

Dim.: Internal H. 8½ in. x L. 15½ in. x D. 7½ in. approx. External, H. 9½ in., x L. 17in., x D. 8in. approx. ASK FOR POST X/H394

12/6 each PAID

**VOLUME CONTROLS** Potentiometers, Carbon Track. ‡ meg. (500,000 ohms), long spindle, fitted DP/ST switch and mtg. plate.

ASK FOR 2/44 POST

3/11 each X/E189 3d. EXTRA

2 watt by Clarostat, U.S.A. 10,000 ohms. Ref.: CMC-63532 Preset. ASK FOR X/H957 2/6 asch 2 POST 2/6 each 3d. EXTRA MORSE PRACTICE BOARD ONLY

Comprises key, buzzer and 'phone terminals on board 64in. x 64in. x .4in with battery clamps. ASK FOR X/EIX

5/6 each 9d. EXTRA

HALF MILE REELS (880 YARDS)
23 s.w.g. P.V.C. covered signal corps wire.
ASK FOR
X/H855
25/- reel
ASK FOR
ASK F

METAL (MINE) DETECTOR NO. 5A Amplifier Unit with Search Coil Assembly 7 A 22158

ZA.22158.

An A.F. Amplifier, employing 3/ARPI2s (VP23) valve mounted, with battery space in metal case 11 in. x 11 in. x 4 in., plus small metal box fitted with controls, which can be fitted to search coil, with slight modification (details supplied), and used for finding buried metal. Power requirements are 6 "5" type 1½ volt cells, and a 60/90 volts H.T. battery (not supplied).

ASK FOR CARRIAGE X/EF68 39/6 each

SUITABLE AS UNIVERSAL ELECTRIC MOTORS
For 200/250 v. A.C. or D.C. mains. By simple external wiring, full data supplied. New method gives better than 1/6th H.P. with MG.29, or approx. ½ H.P. with MG.30.

MOTOR GENERATOR TYPE 29 as Generator, Input 24 v. 16 a. Out 200 mA. Dim.: 11in. x 5½in. x 5½in. x 5½in. X/E880 17/6 each Output 1,200 v. CARRIAGE

MOTOR GENERATOR TYPE 30

Ref. 10K/21. Input 9.3 v. 23 a. Output 7.2 v. 13 a. 255 v. 110 mA. Size: 12in. x 5½in. x 5in. ASK FOR X/H488

15/= each CARRIAGE PAID

COOLANT PUMP, by Packard, U.S.A. A turbine type pump, directly driven from semi-ball joint splined socket (by motor NOT 5UP-PLIED) clockwise rotation. Dim.: overall II lin. x 7½in. x 13in. ASK FOR X/H407 39/6 each

HAND OPERATED WOBBLE PUMP, R98, BC-1444
Reclprocating action provides a suction and exhaust action to each stroke. Designed to pump hydraulic oil to a maximum reservoir pressure of 750 lb. per square inch. This pump is capable of drawing water from approximately 5 feet below its own level, and exhausting same to a height of 4 feet above its own level, at a rate of 60 strokes per quart. Inlet and outlet threaded nozzles fitted at one end of the unit. Suspension arms and rams fitted at the other end. fitted at one end of the unit.

Tams fitted at the other end.

Length of Pumping Handle 27½in. Length of pump overall 4in.

POST

POST

overall 4in. POST PAID pump overall 8in. ASK FOR 12/6 each X/H568

X/H568 IZ/V each PAID
FUEL PUMP (STANDARD) TYPE 36R/82450
Part No. FB66881.
A Rotary unit with two pump chambers each having 4 blades, complete (less motor) with inlet and outlet valves, gear wheel, drive with \$\frac{1}{2}\text{In.}\$ spindle. Diecast aluminium body, 6 hole mtg. at gear end. Overall dim.: 6\frac{2}{2}\text{in.} x 4\frac{1}{2}\text{in.} x 4\frac{1}{2}\te Wgt. 41 lb lb. 16/6 each X/H922 PAID

ROTARY PUMP, 24 v D.C. 2.5 AMPS.

ROTARY PUMP,
Ref. 5U/2492.

§in. bore inlet, §in. bore outlet. 4\frac{1}{2}\text{in.} flange for connecting to tank. Ideal for pumping oil, petrol, water, etc. Diecast constructions with brass rotor blades. Dim.: 4\frac{1}{2}\text{in.} x 7\frac{1}{2}\text{in.} Wgt. 5 lb.

POST

PAID

PAID blades. Di ASK FOR X/H944 £1.15.0 each

Output 14/32 v. 9 amps. 2,500 r.p.m. §in. dia. splined spindle lin. projection. Size I lin. x 7in.x 6in., Wgt. 31 lb. Can be used as a battery charger or low voltage lighting generator, when driven by a motor or petrol engine.

ASK FOR X/H937 £2,19 6

ENGINE DRIVEN GENERATOR TYPE KX.

Ref. 5U/190. In Manufacturer's Carton. 24 volts, 1,500 watts (rotation clockwise). splined spindle: Dia. ‡in., projects ‡in., overall size 14in. x 8½in. Wgt. 27 lb. 4 hole fixing. Speeds, 3,500-5,000 r.p.m.

ASK FOR X/H880 £3.15.0 each CARRIAGE PAID

Order direct from:-

Phone: South 2706/9.

CLYDESDALE

SUPPLY 2, BRIDGE STREET, CO. LTD. GLASGOW . C.5

### R.1155 RECEIVERS

BRAND NEW BEFORE DESPATCH

These well-known ex-Air Ministry Receivers need no further introduc-tion. Supplied complete with 10 valves and full circuit data.

LASKY'S PRICE. £11/19/6 Secondhand. Grade 1 £9/19/6

Secondhand. Grade 2 £7/19/6 Carriage 17/6 per receiver extra. including 10/- returnable on case.

SUPERHET COIL PACKS
With Circuit.

No. 1. L.M.S.G. Size: 4\(\frac{1}{2}\) \times 5 \times 2\(\frac{1}{2}\) in. With \(\frac{1}{4}\) in. spindle. 19/6.

No. 2. M.S.S. Size:  $4 \times 4 \times 3$  in. With  $\frac{1}{2}$  in. spindle.  $\frac{16}{2}$ . Both for use with 465 Kc/s. I.F.

#### TABLE TELEVISION CABINETS

For 12 and 14 inch C.R. tubes. Beautifully fin-ished in polished medium walnut veneer. Comwith mask. glass, speaker - fret. Internal dimen-

slons:— 15in. wide. 16in. deep, 14in. high. wide. 16in. LASKY'S PRICE Carriage 39/11 7/6 extra. Also available in unpolished veneer. LASKY'S 10/11 Carriage 19/11 7/6 extra. PRICE

GANGED TUNING CONDENSERS .0005 MFD.

Standard 2-gang. Size: 21 × 11 × 2½in. 1 in. Spindle. 5/-. Standard 3-gang. Size: 2½ × 1½ × 3½in. ½in. spindle. 7/6.

Midget 2-gang with trimmers. Size:  $1\frac{1}{2} \times 1\frac{1}{2} \times 2\frac{1}{2}$ in. In. Spindle. 7/6. Midget 3-gang with trimmers and perspex cover. Size:  $1\frac{1}{2} \times 1\frac{3}{2} \times 2\frac{3}{2}$ in. Spindle. 12/6.



ASSEMBLED POWER PACK/OUTPUT STAGE FOR R.1155 RECEIVER
For use on 200-250 v. A.C. mains. Complete with 2 valves. In metal case size: 12 × 7 × 5½ins. LASKY'S PRICE, 79/6. Carr. 5/- extra.
Power Pack as above. Fitted with 6½in. p.m. speaker, LASKY'S PRICE, £5/5/-. Carriage 5/- extra.

SOLON SOLDERING IRONS 220-250 volts

Latest model instrument iron.. 

HEARING AIDS

By well-known Manuracturer. In metal case, size: 2½in. ×4½in. X lin. Complete with batteries and 3 subministure valves. Only two controls: volume and on/off. Fitted with internal crystal micro-

used condition.
LASKY'S PRICE
39/6. Postage 2/6 extra.
Earplece and cord for use with hearing
aid. LASKY'S PRICE 17/6.

MAGNETIC RECORDING TAPE, SPECIAL OFFER Plastic. 600 feet reels. 6/11. Paper Base. 1,200 feet reels, 17/3. Postage 1/6. per reel extra.

TANNOY PRESSURE UNITS 10 watts. 7.5 ohms impedance.

Last few only. 59/6

AERIAL ROD SECTIONS Steel, heavily copper plated. 12in. long, in. diameter. Any number may be fitted together. PRICE 2/6 per doz. POST FREE.

300 PF. FEED THROUGH CONDENSERS Ceramic. 6d. each. 4/6 per

20 PF. AIR SPACED TRIMMERS 9d. each. 7/6 per dozen.

RADIO CABINETS RADIO CABINETS
Size: 12in. wide, 6 slin deep,
8in. high. Finished in
medium walnut veneer, with
high polish. Complete with
back, chassis, and dial, calibrated L. M. and S.
LASKY'S PRICE 16/11.
Carriage 2/6 extra.

L. AND M. DUAL WAVE SUPERHET COILS Aerial and Oscillator. 5/11 pair. L. AND M. WAVE T.R.F. COILS With circuit 4/6 pair.

INTERCOM. UNITS 4-station operation. For use on A.C./D.C. mains 200-250 volts. Complete, with 3 valves. Fitted in

attractive plastic cabinet. MASTER UNIT £5/19/6. Carr. 5/- extra. Extension Units. Price 21/- each complete. Carriage 2/- each extra.

A 30-page booklet giving full instructions for building a large 17 inch screen T.V. receiver, and a 3-speed auto-change gram. as an

extra. \* A.C./D.C. Mains. \* Table T.V. \* P.M. Focusing

THE UNIVERSAL

A.C./D.C. TELEVISOR AND RADIOGRAM

A 30-page booklet giving

TRIMMERS

Paxolin. 6d. each,

Ceramic. 9d. each. Up to 100pf. 5/- per doz. Up to 100pf. 7/6 per doz.

\* Mullard valves and C.R.T.

\* 5 Channel Superhet

\* Gram and T.V. entirely separate.

PRICE 3d. POST FREE.

Special Clearance Lines. Callers Only. TAPE RECORD AMPLI-FIERS. Fully wired but un-tested. With 6 valves: 2-6]7, Section Chrome. Heavy 2-6V6, 1 each 5Z4 and 6]5. PRICE £4/19/6.

DINGHY AERIALS. WIRE MESH. 3/11.

MICROPHONE FLOOR STANDS. 2 Section Chrome. Heavy Base. 35/-.

36/6

As previously advertised, complete with all valves, but less output transformer. LASKY'S PRICE £7/10/-.

J/RA/3 AMPLIFIERS.

P.M. LOUDSPEAKERS

All with 3 ohm speech coil 2 ½in., 15/-. 5in., 14/6. 8in., 19/11. 3in., 14/6. 6 ½in., 15/-. 10in., 19/6. 4in., 12/6.

I.F. TRA 520 Kc/s. TRANSFORMERS 445-

Miniature 1 x 1 x 21in. 9/6 pair Midget, 1 x 1 x 21in. 8/6 pair Wearite 500 and 550 8/6 pair

**ENERGISED SPEAKERS** 

8in. with O/T 600 ohm field 15/6 8in. less O/T 600 ohm field 12/6 8in. less O/T 1,200 ohm field 12/6 6½in. with O/T 600 ohm field 14/-

SPECIAL OFFER.
MANUFACTURER.

CAR RADIO

**AERIALS** 2 section, chrm.

75 inches. Side fitting. 15/-.

fitting. Post 3/6.

6 VOLT D.C. RADIO RECEIVER Uses 4 valves and metal rectifier. Valve line up: ECH35, EF39, EBC33, EL32. 8 i n . P . M . 8 in . P . M . Speaker fitted.

BY FAMOUS FRUSTRATED

In attractive polished alunut vener cabinet. Size 19 × 8 × 15in. Full vision dial, battery economy switch, p-u. sockets, tone control. Superhet. Wavebands: 200-500 metres; 50-120 metres; 20-50 metres; BRAND NEW AND UNUSED. COMPLETE WITH VALVES.

LASKY'S PRICE £9/19/6. Carriage and packing 10/6 extra.

EXPORT ORDER

TELESCOPIC PORTABLE **AERIAL** MASTS

Lightweight but extremely strong alloy. Extends to 15 feet. Guyed at at top and centre complete with all guys.

LASKY'S PRICE 32/6. Carriage 2/6 extra.



BAKER'S SELHURST SPEAKERS

BAKER'S SELHUR
"Stalwart." 12in. 15
ohms impedance. Frequency response 30.
13,500 c.p.s. Power handling capacity 15
watts, peak A/C. PRICE £5/10/-.
"Standard." 12in., 15
ohms impedance. Frequency response 3014,500 c.p.s. Power handling capacity 20



#### CAR RADIO SPECIAL-PARTLY. ASSEMBLED CAR RADIOS



Small size case, 12 × 4 × 6in. Will fit most cars. For either 6 or 12 volts, depending on vibrator. Chassis supplied with 5 octal valve holders, medium wave aerial and oscillator coils output transformers, volume

A LASKY'S RADIO ADVERTISEMENT. SEE OVER.





R.F. OSC. COIL KITS. Consisting of R.F. oscillator E.H.T. coil with EV51 heater winding, EY51 rectifier, 6V6 valve and base. All necessary condensers and resistances. Full circuit

and data supplied. 6-9 Kv. LASKY'S PRICE 45/-. 6-18 Kv. LASK Y'S PRICE 50/-.

E.H.T. OSC. COILS.	
6-9 Kv. PRICE	
6-18 Kv. PRICE	21/6

BRIMISTORS. CZ1, 1/6. CZ3, 9d. each.

METROSILS. 10 Kv., 5/- each.

#### LASKY'S T.V. CONSTRUCTORS' PARCELS.

3-WATT AC/DC MIDGET

**AMPLIFIERS** 

and glass, width and linearity controls. Also the following valves:-6U4gt, 6CD6, 6AL5, 2-6AM5 (N78), 3-12AU7. Full circuit.

LASKY'S PRICE COMPLETE £8/15/11.

Carriage 3/6 extra.

No. 2. The WIDE ANGLE PARCEL AS ABOVE, but less valves.

LASKY'S PRICE 94/11. Carriage 2/6 extra.

Push pull, very high gain

4 valves: 2 UL41 in push pull, 1 UCH42 and 1 UAF42. Input

voltage 100/110
AC/DC. Very easily converted to 230 volts.

Supplied with circuit diagram and full details. Size:-9 x 4 x 4 inches. Uses 2 metal rectifiers, 1 each RM2 and RM3. Ideal for ships'

and wired, with 4 valves.

No. 1 WIDE ANGLE PARCEL. Containing ferroxcube line E.H.T. transformer, ferroxcube scanning coils, frame output transformer, p.m. focus unit, frame blocking osc. transformer, 14, 16 or 17 inch mask E.H.T. rectifier, 12in. mask and older the components by Igranic. Comprises E.H.T. flyback line transformer, 7-10 Kv. with ferroxcube core and rectifier heater winding; scanning coils; frame output transformer; Elac focus unit with vernier adjuster, U37 or K3/100 plass. glass.

LASKY'S PRICE FOR THE COMPLETE PARCEL, 79/6. Carriage and packing 3/6 extra.

No. 4. Complete set of metal-work. Unassembled. Comprising main chassis, tube supports and valve-holders. (Less sound-vision chassis.) PRICE 25/-. Carriage 3/6 extra.

SPECIAL PARCEL. No. 5. No. 5. SPECIAL PARCEL.
Comprising line output transformer (Non E.H.T.) EL.38, frame output transformer, scanning coils, line and frame blocking oscillator transformers, large 250 m/a. smoothing choke.
LASKY'S PRICE 59/6
POST FREE.

R.1132.A RECEIVERS. Tested. SOILED CONDITION. Grade 1, 79/6, specially selected. Grade 2, 59/6. Carriage 10/- per receiver Carriage 10/- per receiver

EX-GOVERNMENT MAINS POWER UNITS, for R.1132.A Receivers. 200-250 v. A.C. working order. 59/6. Carriage 7/6 extra.

OUTPUT TRANSFORME	
Aidget Pentode	
Ainiature Personal, 3S4, etc.	
	3/11
	9/6
	12/6
leavy Duty. P.P 1	14/11

PORTABLE RECORD PLAYERS PORTABLE RECORD PLAYERS Containing a new Plessey single speed automatic record changer (78 r.p.m.). Magnetic pick-up and 2-valve amplifier, with metal rectifier. For use on 200-250 v. A.C. mains. Amplifier uses EF.36 and EL.32 giving 3-watts output, tone and volume controls, 5in. speaker. In rexine-covered cabinet, size: 17 × 17 × 8in. With carrying handle. Though store soiled, these players are new and every one is fully tested before despatch. LIMITED QUANTITY. LASKY'S PRICE £10.19.6

STAFF HOLIDAYS All departments will be closed on Tuesday and Wednesday, September 28th and 29th. Re-open on Thursday, September 30th.

Carriage 10/6 extra.

#### 12 VOLT-4 WATT MOBILE AMPLIFIERS

BRAND NEW AND UNUSED. KT.61 output. Complete with power unit and synchronous vibrator (Wearite type QFA/12), and all valves. Fitted with rubber covered heavy duty battery lead.

By famous manufacturer, in handsome metal cabinet, grey crackle finish. Size: 10in, x 6½in, x 8in. Output impedance 3 ohms. With the addition of a suitable loudspeaker, this is ready for operation. Finest quality components throughout. Robustly constructed for rough handling.

Complete with carbon hand-microphone with screened lead. LASKY'S PRICE, £7.19.6

.19.6 OR LESS MICROPHONE £6.19.6 Carriage 5/- per unit extra.

### DE LUXE T.V. CABINETS

Our new model. Mark II

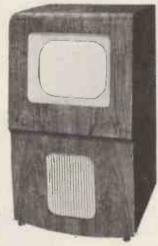
This cabinet is now supplied complete with mask, glass, castors, shelf, bearers, c.r.t. neck end protector, back, speaker fret and baffle board. Finished in beautiful figured medium, light or dark walnut veneer, with high polish. Suitable for most home constructor T.V. receivers, including the "Viewmaster," "Practical Television," "Tele-King," "Magniview," "Wireless World," etc. Can be supplied with cut-out for 14in., 16in. and 17in. c.r. tubes at no extra cost.

An allowance of 4s, 6d, will be made if the mask is not required. Inside Dimensions: Depth 16½in.; width 17½in.; height 28in. Overall height 32in. and width 18½in.

WHY NOT CONVERT YOUR TABLE RECEIVER TO A CONSOLE MODEL.

Adaptor frames for fitting 9in. or 10in, c.r. tubes can be supplied if required.

LASKY'S PRICE £8.10.0



BY FAMOUS MANUFAC-TURER. 3-SPEED AUTO-MATIC RECORD CHANG-ER. Mixer type. With turn over crystal pick-up. Incor-porates the latest "Magidisk" record selector mechanism.

record players, tape recorders, home record players, baby alarms, etc., etc. Supplied complete, fully assembled

LASKY'S PRICE £10/10/-Carriage Free.

PLESSEY AUTO RECORD CHANGER. 3-speed mixer type, with turn over crystal pick-up. LASKY'S PRICE pick-up. LASKY'S P £9/19/6. Carriage Free.

COLLARO 3-SPEED AUTO CHANGERS. Model 3RC/521. New and unused in maker's

CARRIAGE FREE

carton. Cream or fawn finish. Complete with hi-fi-delity "stu-dio" turn over crystal pick-up.

LASKY'S £9.19.6 Carriage PRICE

CRYSTAL DIODES. Glass type, wire ends. 1/6 each. Higher Grades Available. 12 Assorted for 30/-: Post Free.

#### FIECTROLYTIC CONDENSERS ALL RRAND NEW

FEEGINGE	1110.	OHDEHOL	HO, ALL	שווחווש	14 10 44 4
8 mfd. 450 v.w. 16 mfd. 350 v.w. 16 mfd. 500 v.w. 20 mfd. 500 v.w. 30 mfd. 450 v.w. 60 mfd. 350 v.w. 64 mfd. 450 v.w.		1/9 2/6 3/6 3/6 3/3 3/11	400 mfd. 150 v. 8 + 8 mfd. 450 8 + 16 mfd. 45 12 + 12 mfd. 3 16 + 16 mfd. 3 16 + 16 mfd. 4 20 + 20 mfd. 2	w	2/6 3/6 4/3 2/6 3/6
150 mfd. 350 v.w.		3/6	6000 mfd. 6 v.w 8000 mfd. 3 v.w	7	2/6
2 4 4 2 444 00044					

MANY OTHER SINGLE AND MULTIPLE CONDENSERS IN STOCK.

# THE TELE KING

SUPERHET RECE

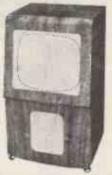
WIDE ANGLE — LARGE SCREEN

This famous and well tried home constructor set can now be built for £29/10/- including valves. Only tube and cabinet extra.

EVERY COMPONENT CAN BE SUPPLIED SEPARATELY.

Full constructional data, wiring Price 6/- POST FREE. diagrams and circuits.

WRITE NOW FOR OUR NEW TELE KING PRICE LIST. WE CAN SAVE YOU MONEY.





MULTI CHANNEL TUNER FOR THE TELE KING WILL BE AVAILABLE SHORTLY.

Co-axial Cable.	
impedance. Sing	
per yard. Twin	
yard. Twin Balance	ed Feeder, 6d.
per yard.	

40 m/a. . . 3/3 120 m/a. 7/3 60 m/a. . 3/11 200 m/a. 12/6 80 m/a. .. 4/11 250 m/a.

SPECIAL TRANSFORMER Secondary tapped as follows: 3, 4, 5, 6, 8, 9, 10, 12, 15, 18, 20, 24 and 30 volts at 2 amps. PRICE 17/6.

HIGH VOLTAGE E.H.	Т.
CONDENSERS	
.1 + .1 mfd. 3.5 Kv	
.1 mfd. 7 Kv	15/-
	7/6
.001 mfd. 15 Kv	10/-
.0005 mfd. 10 Kv.	3/6
.0005 mfd. 15 Kv	6/6
.04 mfd. 12.5 Kv	5/-

# SPECIAL T.V. CONDENSERS 64 mfd. 450 v.w. 3/11 100 mfd. 450 v.w. 4/11 32 + 100 mfd. 450 v.w. 7/16 100 + 200 mfd. 350 v.w. 5/11



CYLDON CHANNEL

T.V. TUNERS

Uses two valves, EF80 (6BW7) as R.F. amp. and ECC81 (12AT7) as frequency changer. Instant and positive selection of any channel by switching incremental inductances. Power gain 24dB, I.F. frequency output 9.5-14 Mc/s or 15.5-22 Mc/s. With full details and circuit diagram. Supplied less valves. Size:—4½ × 2½ × 2½in. The Tuner with Valves.

LASKY'S PRICE 37/6. Post 2/6 extra.

#### SURPLUS T.V. MANUFACTURERS COMPONENT BARGAINS

#### WIDE ANGLE 38 mm.

Line E.H.T. trans., ferroxcube core. 9-16 Kv. ...........25/-Scanning Coils, low imp. line Frame Output Transformer 10/6 Scanning Coils low imp. line Frame blocking osc. transformer ..... 7/6 Line blocking osc. trans-former, caslam cored .... 6/6 Focus Magnets Ferroxdure . . 25/-P.M. Focus Magnets. Iron Cored ...... 19/6 Duomag Focalisers ......29/6 300 m/a. Smoothing chokes 15/-Electro magnetic focus coil, with combined scan coils ... 25/-

#### STANDARD 35mm.

Scanning coils. Low imp, line Line blocking oscillator transformer ..... 4/6 Frame blocking oscillator transformer ..... 4/6 Frame output transformer . . 7/6 Focus Magnets.
Without Vernier ..... 12/6 With Vernier ..... 17/6 Focus Colls. Electromagnetic 12/6 200 m/a. Smoothing chokes 10/6

LESS VALVES POST FREE

## PERSPEX IMPLOSION GUARDS, incorporating escutcheon and filter plate.

12in. 12/6 12in. de Luxe 15/-16in. de Luxe 17/6

MAINS TRANSFORMERS All 200-250 v. 50 c.p.s. primary Finest quality, fully guaranteed. MBA/3. 350-0-350 v. 80 mA. 6.3 v. 4 a., 5 v. 2 a. Both fila-ments tapped at 4 volts. An ideal replacement trans. Price 18/-

18]-, MBA/6. 325-0-325 v. 100 mA. 6.3 v. 3 a., 5 v. 2 a. With mains tapping board. Price, 22/6. MBA/7. 250-0-250 v. 80 mA. 6.3 v. 3 a., 5 v. 2 a. Both filaments tapped at 4 volts Price,

18/-. MBA/8. SPECIAL OFFER Drop through type. 235-0-235 v. 60 mA. 6.3 v. 3 a. 12/6. MBA/9. 400-0-400 v. 60 mA. 6.3 v. 1 a., 4 v. 2.5 a. Price, 12/6. AT/3. Auto transformer. 0-10-120, 200-230-240 volts 100 watts. Price 17/6.

FILAMENT TRANSFORMERS 200-250 v. primary 50 c.p.s. 6.3 v. 1.75 a., 6/6. 6.3 v. 3 a., 9/6.

FOR CALLERS ONLY Secondhand cathode ray tubes. With heater-cathode short and/or ion burns. 9in. 35/-. 12in. 55/-.

C.R.T. MASKS. Brand New LATEST ASPECT RATIO

9in. 7/10in. 7/6
12in. 15/12in. Flat Face 15/12in. Old Ratio 9/6 12in. Old Ratio 9/6
12in. Escutcheon mask, with
Perspex filter 12/6
14in. Rectangular 12/6
15in. Cream rubber 17/6
16in. Plastic, white 12/6
17in. Rectangular 15/-

#### ARMOUR PLATE GLASS 16in. Actual size 17\(\frac{1}{2} \times 15\(\frac{1}{2} \times 15\(\fra ‡in. 15in. Actual size 16‡in. × 13in. ׇin. 12in. actual size 13in. × 6/11

3/-

### TRIPLEX DARK SCREEN FILTERS

FILTERS

14 × 12 ½ × ½ in. 7/6

15½ × 13 ½ × ½ in. 9/6

Postage and packing 5/- per piece
extra. (This charge is necessary
owing to extra packing required).

C.R.T. Neck Protectors 2/6.

### FAMOUS MANUFACTURERS TAPE RECORDER AMPLIFIERS

Complete with 5 valves. For 200-250 volts A.C. mains. Finest quality components throughout. Twin Inputs. Volume control, and record level control. Speaker on/off switch. On steel chassis, black crackle finish. Size 11½ × 2½ × 9in. Valve line-up: 2 6V6, 2 6SN7, 1 5Z4. Full circuit supplied. Complete with 8in. speaker and all valves.

LASKY'S PRICE COMPLETE £9/19/6. Less Cover, £8/15/-. Less cover and head lift transformer £7/15/-. Carriage 5/- per unit extra.

SPECIAL OFFER. 12 INCH CATHODE RAY TUBES. Standard types, suitable for T.V. LIMITED QUANTITY. LASKY'S PRICE £12/19/6. Carriage and insurance 15/- extra.

ION TRAPS. All types 3/-.

### S.T.C. SENTERCEL RECTIFIERS

R.M.1 3/10; R.M.2. 4/3; R.M.3., 5/-; R.M.4 16/-. K3/40, 3.2 kV., 6/-; K3/45, 3.6 kV. 8/2; K3/50, 4.0 kV. 8/8; K3/100, 8.0 kV. 14/8; K3/160 12.8 kV. 21/6. K3/200

LASKY'S (Harrow Road) Ltd.,

370 HARROW RD., PADDINGTON, LONDON, W.9

(Opposite Paddington Hospital)

Telephone, all departments: CUNningham 1979/7214. Please Add a Reasonable Amount For Postage.

#### SELENIUM DECTIFIEDS

	H.T. Types H.W.	
1/9	90 v. 20 mA	3/6
		3/11
2/9	250 v. 50 mA.	5/9
	250 v. 80 mA.	7/9
	RM2 125 v. 100	
0/9	mA	3/11
9/9	RM3 125 v. 120	
14/9	mA	4/11
,	RM4 250 v. 250	
19/9	mA	11/9
29/9	300 v. 275 mA.	12/11
	14/9 19/9	1/9 00 v. 20 mA 120 v. 40 mA. 250 v. 80 mA. 250 v. 80 mA. 5/9 RM2 125 v. 100 mA 9/9 RM3 125 v. 120 mA 19/9 mA

CO-AXIAL CABLE. 75 ohms in, 7d. yard. Or in 20yd. lengths, 6d. yd. Twin screened feeder,

RHEOSTATS (VARIABLE RESISTORS) ms 5 amps, 6/9; 7.5 ohms 5 amps, 8/9; 0.4 ohm, 8/9; 10 ohm 3 amps, 8/9; 150 ohms 1.5 amps, 2 ohms 5 amps 14/9. All complete with control knob.

SILVER MICA CONDENSERS. 5, 10, 15, 20, 25, 30, 35, 50, 100, 120, 150, 180, 200, 230, 300, 330, 400, 470, 500, 1,000 pfd. (.001µF), .002 mfd. (2,000 pfd.). All at 5d. each, 3/9 dozen one type.

DIAL BULBS, M.E.S., 8 v. 0.15 a., 8/9 doz.; 6.5 v. 0.15 a., 6/9 doz.

#### **ELECTROLYTICS** (Current production)

	MOI 6	X-GOVI.	
Tubular Type	es	Can Types	
8μF 450 v	1/11	16μF 450 v	2/9
16μF 350 v	2/3	24μF 350 v	2/11
<b>1</b> 6μF 450 v	2/9	32μF 350 v	2/11
16μF 500 v	3/9	32 mfd. 450 v.	4/9
24μF 350 v	3/3	64 mfd. 450 v.	4/9
<b>32</b> μF 350 v	3/9	8-8μF 350 v	3/9
32 mfd. 500 v.	5/9	8-8µF 450 v	3/11
8-16μF 500 v.	4/11	8-8 mfd. 500 v.	4/9
25μF 25 v	1/3	8-16μF 450 v.	2/11
50μF 12 v	1/3	16-16μF 450 v.	4/11
50μF 50 v	2/3	16·32μF 350 v.	4/9
Can Types		16-32 mfd. 450 v.	4/9
8mfd. 350 v.	1/3	32-32μF 350 v.	4/9
8mfd. 450 v.	2/3	32- <b>3</b> 2μ <b>F</b> 450 v.	5/11
8mfd. 500 v.	2/9	60-100 mfd. 450 v.	7/9
16mfd. 350 v.	1/11		

AMPLIFIER OR CHARGER CASES. Size 143 x 5\(\frac{1}{2}\) \text{7\(\frac{1}{2}\) ins. high. Strongly made in perforated steel. Grey enamel finish. Only 9/6.

VOLUME CONTROLS with long spindles, all values less switch, 2/9; with S.P. all values switch, 3/9.

WIRE WOUND POTS: 20 ohms, 500 ohms, 1,000 ohms, 5K, 20K, 50K (medium length spindles), 2/9. 220 ohms, 2K, 10K, 20K, 50K Preset type, 1/9 ea.

AMMETERS. Moving 0—5 amps, 2in. scale, 11/9.

EX-GOVT. E.H.T. SMOOTHING CONDEN	SERS
.02 mfd. 8,000 v. Cans	
.25 mfd. 4,000 v. Blocks	4/9 3/9 3/3
.5 mfd. 2,500 v. Blocks	3/9
.5 mfd. 3,500 v. Cans	3/3
.1 mfd. plus. 1 mfd. 8,000 v., large blocks	
(common negative isolated)	9/6
1.5 mfd. 4,000 v. blocks	5/9

EX-GOVT. ACCUMULATORS with non-spill vents. Unused and guaranteed. 2, v. 16 A.H., 5/9 each, or 3 in wood carrying case  $9 \times 7 \times 5$ in., 14/9, plus

EX-GOVT. BLOCK	PAPI	ER CONDENSERS	
2 mfd. 800 v	1/9	4 mfd. 2000 v	6/5
4 mfd. 500 v	2/9	6-6 mfd, 500 v.	5/9
4 mfd. 750 v	3/9	8 mfd. 500 v	5/9
4 mfd. 1500 v	4/9	11-7 mfd. 500 v.	8/9
		15 mfd. 500 v	7/5
4 mfd. 400 v. plus 2	mfd.	250 v. 1/11	

4 mid. 400 v. pids 2 mid. 200 v. 1/11	
EX-GOVT. AUTO TRANSFORMERS 50 c/s Double Wound 10-0-220-200-240 v. to	
10-0-270-290-310 v. 200 watts	25/9 25/9
0-110-190-230 v. 400 watts	49/6
55 v. to 230 v. 21 amps in steps of 11 v Double Wound 10-0-200-220-240 v. to	£6/15
10-0-275-295-315 v. 500 watts	69/6

M.E. SPEAKERS. All 2-3 ohms, 6 in Rola-field 700 ohms, 11/9. 10in. R.A. field 600 ohms, 23/9. 10in. R.A. field, 1,500 ohms 23/9. 10in. R.A. field 1,000 ohms, 23/9.

### R.S.C. TRANSFORMERS

#### FULLY GUARANTEED, INTERLEAVED AND IMPREGNATE

MAINS TRANSFORMERS Primarles 200-230-250 v. 50 c/s.

FULLY SHROUDED UPRIGHT MOUNTING 250-0-250 v. 60 mA., 6.3 v. 2 a., 5 v. 2 a., Midget type, 2\(\pi -3\)-3in.
350-0-350 v. 70 mA., 6.3 v. 2 a., 5 v. 2 a...
350-0-300 v. 60 mA., 12 v. 1.6 a., c.t....
250-0-250 v. 100 mA., 6.3 v. 4 v. 4 a., c.t., 22/9 22/9 0-4-5 v. 3 a. 0-4-5 v. 3 a. 350-0-350 v. 100 mA., 6.3 v.-4 v. 4 a. c.t., 350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a. 31/6 350-0-350 v. 150 mA., 6.3 v. 2 a., 6.3 v. 2. a, 350-0-350 v. 250 mA., 6.3 v. 6 a., 4 v. 8 a., 0-2-6 v. 2 a., 4 v. 3 a., for Electronic Eng. Televisor 425-0425 v. 200 mA., 6.3 v. 4 a., c.t., 6.3 v 4 a., c.t., 5 v. 3 a., suitable Williamson Amplifier, etc. 425-0-425 v. 250 mA., 6.3 v. 6 a., 6.3 v. 6 a, 15/9

14/11 21/9 350-0-350 v. 100 mA., 6.3 v. 4 a., c.t., 5 v. 21/9 350-0-350 v. 150 mA., 6.3 v. 2 a., 6.3 v. 2 a., 350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a. 26/9

E.H.T. TRANSFORMERS. 2,500 v. 5 mA. 2-0-2 v. 1.1 a., 2-0-2 v. 1.1 a., for VCR07, VCR517 or ACR2X 36/6 VCR517 or ACR2X 5,000 v. 5 mA., 2 v. 2 a.... 39/6 FILAMENT TRANSFORMERS Primaries 200-250 v. 50 c/s.

6.3 v. 2 a..... 0-4-6.3 v. 2 a.... 6.3 v. 1.5 a. ... 5/9 6.3 v. 3 a. ..... 6.3 v. 6 a. ...... 12 v. 3 à. or 24 v. 0-2-4-5-6.3 v. 4 a. 16/9 1.5 a. .....

CHARGER TRANSFORMERS

All with 200-230-250 v. 50 c/s Primaries: 0-9-15 1.5 a., 12/9; 0-9-15 v. 3 a., 16/9; 0-9-15 v. 6 1.5 a., 12/9; 0-9-15 v. 3 a., 16/9; 0-9-15 v. 6 22/9; 0-4-9-15-24 v. 3 a., 22/9; 0-9-15-30 v. 3

**ELIMINATOR TRANSFORMERS** Primaries 200-250 v. 50 c/s. 120 v. 40 mA. 120 v. 40 mA. 5-0-5 v. 1 a.

**OUTPUT TRANSFORMERS** Standard Pentode 5,000 $\Omega$  to 3 $\Omega$  . Standard Pentode, 8,000 $\Omega$  to 3 $\Omega$  . Standard Pentode, 10,000 ohms to 3 ohms Multi-ratio 40 mA. 301, 45:1, 60:1, 00:1, Class B Push-Pull 8 Watts 6V6 to 3 ohms Push-Pull 8 Watts 6V6 to 3 ohms Push-Pull 10-12 Watts 6V6 to 3 $\Omega$  or 15 $\Omega$ . Push-Pull 10-12 Watts to match 6V6 to 3-5-8 or 15 $\Omega$  . Push-Pull 15 Watt 6L6s, KT66s, etc. to 3 or 15 ohms 4 5/ 15 16/ 3 or 15 ohms.
Push-Pull 20 Watts high-quality sectionally 19 wound 6L6, KT66, etc., to 3 or 15Ω...... Williamson type, exact to author's spec.

8MOOTHING CHOKES
250 mA., 3 H. 50 ohms
150 mA. 7-10 H. 250 ohms
100 mA., 10 H. 250 ohms
80 mA., 10 H. 350 ohms
60 mA., 10 H. 350 ohms.
50 mA., 40 H. 1,000 ohms
20 mA., 30 H. 1,000 ohms 5/4 4/1

MICROPHONE TRANSFORMERS

#### THE SKY CHIEF T.R.F. RECEIVER





A design of a 4-stage, 3 valve 200-250 v. A.C. Mains receiver with selenium rectifier. Foinclusion in any of cabinets illustrated above. It inclusion in any of cabinets illustrated above. It consists of a variable Mu high gain H.F. stage followed by a low distortion grid detector triode. The next stage is a further triode amplifier with tone correction by negative feedback. Finally comes the output stage consisting of a parallel connected double triode giving ample output at an extraordinary low level of distortion. Point to point wiring diagrams, instructions, and parts list, 2/6. This receiver can be built for a maximum of £4/16/- including cabinet.

P.M. SPEAKERS. All 2-3 ohms. 2½in. Celestion, 14/9. 3½in. Goodmans (Ex New Units), 10/3. 4ln. Goodmans, 14/11. 5in. Goodmans, 15/9. 6½in. Goodmans, 16/9, 8in. Plessey, 15/9, 10in. Rola, 27/9. 10in. Plessey, 18/6. 10in. Rola with Trans 29/8.

R.S.C. BATTERY CHARGER KITS. For mains input 200-250 v. 50 c/s. To charge 6 v. accumu-



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5/8

22/9

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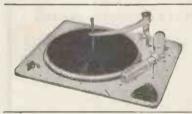
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Auto Trans. Input 200/250. H.T. 350 v. 350 mA. Separate L.T. 6.3 v. 7 a., 6.3 v. 1 amp., 5 v. 3 amp., 25/-P. & P. 3/-.

Heater Transformer, Pri. 230/250 v., 6 v. 1; amp., 6/-; 2 v. 2; amp., 5/-. Pri. 200/250. Secondary 9 v. 3.5 amp., v., 3.5 amp., 12/6.

Pri. 200/250. Secondary 9 v. 3.5 amp.,

Pri. 200/250. Secondary 9 v. 3.5 amp., 6.3 v. 3 amp., 12/6.

Mains Transformer, fully impregnated, luput 210, 220, 230 and 240. Sec. 600-6-600, 275 m.A., and 200 v. at 30 m.A., complete with separate heater transformer. Input 210, 220, 230, 240. Sec. 6.3 v. 2 amp. three times, 0. 4, 6.3 v. at 3 amp. and 5 v. 3 amp., 45/-P. & P. 5/-

Mains Transformer, fully impregnated Input 210, 220, 230, 240, Sec. 350-0-350

100 mA. with separate heater transformer. Pri. 210, 220, 230, 240. Sec. 6.3 v. 2 amp., 6.3 v. 3 amp., 4 v. 6 amp. and 5 v. 2 amp., 30/-. P. & P. 5/-.

MAINS TRANSFORMERS, chassis, mounting, feet and voltage panel. Primaries 200/250:

350-0-350 75 mA. 6.3 v. 3 a. tap 4 v. 6.3 v. 1 a., 13/6. 350-0-350 70 mA. 4 v. 4 a., 4 v. 2.5 a.

500-0-500 125 mA. 4 v. C.T. 4 a., 4 v. C.T. 4 a., 4 v. C.T. 4 a., 4 v. C.T. 2.5 a., 27/6. 500-0-500 250 mA. 4 v. C.T. 5 a. 4 v. C.T. 5 a., 4 v. C.T. 4 a., 39/6.

9in. T.V. Cabinet, front in contrasting walnut veneers, size 16in. long, 11in. high, by 12in. wide. Complete with two pieces expanded aluminium in gold, 12 x 9in. and 6in. speaker baffle, 15/-post paid.

P.M.	SPEAKERS										with trans.	less trans.			
24ln.														_	15/6
3jin.														-	13/6
5in.														16/6	12/6
6jin.														16/6	12/6
8in.														18/6	15/-
10in.					,									-	19/6

6½in. M.E. Speaker. 1,000 ohm field, 15/-.

R. & A. T.V. Energised 61in. Speaker, field coil 175 ohms. Requires a minimum 150 mA. to energise, maximum current 250 mA., 9/6. P. & P. 2/6.

Extension Speaker Cabinet, in contrasting walnut veneer, size 15×10; Will take 6; or 8in. speaker, 17/6.

Completely built All-dry Mains Unit by famous manufacturer, 200/250 v. Metal case size 8 × 5 × 31m., incorporating Westinghouse metal rectifiers, 3 500 mid., 16 × 24 mid., mains trans., 3 smoothing chocked, output 90 · 10 mA., 14 v., 0.26 amp., 3946. F. & F. 2/6. Volume Controls. Long spindle less switch, 50K, 500K, 1 meg., 2/6 each. P. & P. 3d, each.

Volume Controls. Long spindle and switch, ‡, ‡, 1 and 2 meg., 4/- each; 10K and 50K, 3/6 each. ‡ and 1 meg., long spindle double pole switch, miniature, 5/-. P. & P. 3d. each.

Trimmers, 5-40 pf., 5d. 10-110, 10-250, 10-450 pf., 10d.

Twin-gang .0005 Tuning Condenser 5/-. With trimmers, 7/8.

Line Cord, 2-way 0.3 amp., 60 ohms per foot, 1/3 per yard. Twin-Gang .0005, with feet, size 31 3×11in., 6/6.

3-gang .0005, with feet, size  $4\frac{1}{4} \times 3 \times 1\frac{1}{2}$  in., 7/6.

T.V. Coils, moulded former, iron-cored, wound for rewinding purposes only. Ali-can 1½ × 1½ in., 1/- each, 2 iron-cores ali-can 2½ × ½ in., 1/8 each. Used Metal Rectifier, 250 v. 150 mA.,

Metal Rectifier. 250 v. 250 mA., 12/6. Metal Rectifier. 230 v, 45 mA., 6/-. Metal Rectifier. RM2, 125 v., 100 mA., 3/6.

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T.V. CONVERTER for the new commercial stations complete with 2 valves. Prequency:—can be set to any channel within the 186-196 Mc/s band. I.F.:—will work into any existing T.V. receiver designed to work between 42-88 Mc/s. Sensitivity:—10 Mu/v with any normal T.V. set. Input:—arranged for 300 ohm feeder. 80 ohm feeder and ne used with sight reducion in R.F. gain. Circuit EF80 as local oscillator, ECC81 as R.F. amplifier and mixer. The gain of the first stage, grounded grid R.F. AMPLIFIER 10 db. Required power supply of 200 v. D.C. at 25 m.A. 6.3 v. A.C. at 0.6 amp. Input filter ensuring complete freedom from unwanted signals, 2 simple adjustments only. 22/10/v. P. A. P. 2/6.

HIGH-IMPEDANCE PLASTIC RECORDING TAPE, by famous manufacturer. 600tt. on aluminium spool, 8/v. 1,200ft. on aluminium spool, 17/6 post paid.

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PLASTIC CABINET, as illustrated, 11½×6½×5½im., in Walnut, Cream and Green.

I.B.F. chassis, 2 wave-band scale, station names, new wave-band, back-plate, drum, polinter, spring, drive spindle, 3 knobs and back, 22/6. P. & P. 3/6.

A ABOVE, with superhet chassis, 23/6. P. & P. 3/6.

A ABOVE, with superhet chassis, 23/6. P. & P. 3/6.

AS ABOVE, with superhet chassis, 23/6. P. & P. 3/6.
AS ABOVE, complete with new 5in, speaker to fit, and 0. P. trans, 35/-. P. & P. 3/6.
AS ABOVE, complete with new 5in, speaker to fit, and 0. P. trans, 35/-. P. & P. 3/6.
With superhet chassis, 36/-. P. & P. 3/6.
Used metal rectifier, 230 v. 50 mA. 3/8, gang with trimmers, 6/6; M. & L. T.R.P. colles, 5/-; 3 obsolete ex-Govt. valves, 3 v/h and circuit, 4/6; heater trans, 6/-; volume control with switch, 3/6; were volume control with switch, 3/6; volume control with switch

Clydon 5 channel T.V. Tuner, uses EF80 and 12AT7, less valves, 12/6, post paid.

Radiogram Chassis, 5 valve A.C./D.C. 3 wave-band superhet 195-255 v., 19-49, 200-550 and 1,000-2,000 metres, i.F. 470 Kc. size of chassis  $13 \times 6_1^4 \times 2_1^4$ lm., size of scale 7 $_1^4 \times 3_2^4$ lm. valve line-up 10C1, 10F9, 10LD11, U-64 and 10P14. Twin mains filter input, 2 dial lights and 8in. P.M.  $\pm 8/17/8$ . P. & P. 5/-.

CONSTRUCTOR'S PARCEL No. 1, comprising chassis 124 × 8 × 24 in., cad. plated 18 gauge, v/b., I.F. and trans., out-outs, backplate, 2 supporting brackets, 3 waveband scales, new wavelength station names. Size of scale 11½ × 4½ in., drive spindle drum, 2 pulleys, pointer, 2 builb holders, 5 paxolin international octal valve holders, 4 knobs and pair of 465 I.F.s., 16/6. P. & P. 3/-

AS ABOVE, but complete with 16×16 mfd. 350 wkg. and semi-shrouded drop thro' 250-0-250 60 mA., 6 v. 3 amp. Prl. 200-250, and twin-gang, 31/6. P. & P. 3/-.

CONSTRUCTOR'S PARCEL. As No. 1 plus 16×16 mfd. 350 wkg., semi-shrouded drop thro' 250-0-250 60 mA., 6.3 v. 3 a., 5 v. 2 a., twin gang, and 6 L. M., 8. superhet coils complete with trimmers and tracking condensers with circuit. 22/5/-. P. & P. 3/6.

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Coverage; 120 Kc/s.-320 Kc/s., 300 Kc/s.-900 Kc/s., 900 Kc/s.-2.75 Mc/s., 2.75 Mc/s.-8.5 Mc/s., 8.5 Mc/s.-25 Mc/s., 71 Mc/s.-50 Mc/s., 25.5 Mc/s.-75 Mc/s. Metal case  $10 \times 6\frac{3}{4} \times 4\frac{1}{4}$ in. Size of scale  $6\frac{1}{2}$ in.  $\times 3\frac{1}{4}$ in., 2 valves and rectifier. A.C. mains 230/250 v. Internal modulation

400 c.p.s. to a depth of 30 per cent., modulated or unmodulated. R.F. output continuously variable 100 millivolts. C.W. and mod. switch, variable A.F. output and moving coil output meter. Black crackle finished case and white panel, £4/19/6. Or 34/- deposit and 3 monthly payments of 25/-. P. & P. 4/- extra.

PATTERN GENERATOR, 40-70 Mc/s direct calibration, checks frame PATIERN GENERATOR, 40-10 mass direct calibration, checks trame and line time base frequency and linearity, vision channel alignment, sound channel and sound rejection circuits, and vision channel band wldth. Silver plated coils, black crackle finished case,  $10 \times 61 \times 41$  and white front panel. A.C. mains 200/250 volts. This instrument will align any T.V. receiver. Cash price £3/19/6 or 29/- deposit and 3 monthly payments of £1. P. & P. 4/- extra.

Similar in appearance to the above Sig. Generator.

OUTPUT TRANSFORMERS. Standard type 5,000 ohms tmp., 4/9; 42-1 with extra feed-back windings, 4/3. Miniature 42-1, 3/3. Multi-ratio 3,500, 7,000 and 14,000, 5/6. 10-watt push-puli, 6/96 matching, 7/-. 90-1 3 ohm speech coll, 6/6.

PUSH-BACK CONNECTING WIRE. Doz. yds., 1/6, post paid.

STANDARD WAVE-CHANGE SWITCHES 4-pole 3-way, 1/9; 5-pole 3-way, 1/9; 3-pole 3-way, 1/9; 9-pole 3-way, 3/6; Miniature type, long spindle 3-pole 4-way, 4-pole 3-way and 4-pole 2-way, 2/6 ach. P. & P. &d.

PERSONAL SHOPPERS ONLY. 9in Enlarger, 17/6; 12in., 27/6. Germanium Crystal Diode, 1/6, post

Used 9in. Tube, with ion burn. 17/6. post paid.

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Crystal Set, medium and long wave in plastic cabinet, 15/2.

In pusses cannet, 15)-.
Head-phones, per pair, 8(-.
Speaker Matching Unit on aluminium chassis, 3-15 ohms, reversible, 12/8.
Line and E.H.T. Transformer, 14 Kv. using ferrocart core, complete with line and width control, and corona shields, U37 rectifier winding, 35/-.

Line and E.H.T. Transformer, 9 Kv using ferrocart core complete with built in line and width control. Mounted on small ali-chassis. Overall size 4? ×1?in. EY51 rec. winding, 27/8. 4½ x ½ n. E v61 rec. winding, 27/6. Line and E.H.T. Transformer, 9 Kv., Line are tore, E v61 heater winding complete with sean coils and frame output transformer, and line and winded the control. £2/5/-. P. & P. 3/-. Sean Coils, low line, low impedance frame, complete with frame transformer, to match above, 27/6. P. & P. 3/-.

P. X. Y. 27.

Valve Holders, moulded octal Mazda and loctal, 7d. each. Paxolin, octal Mazda and loctal, 4d. each. Moulded B7G, B8A and B9A, 7d. each. B7G moulded with screening can, 1/6 each. 32 mfd., 350 wkg. 21-

32 mid., 330 wkg	21-
16 × 24, 350 wkg	4/-
4 mfd., 200 wkg	1/3
40 mfd., 450 wkg	3/6
16×8 mfd., 500 wkg	4/6
16 x 16 mfd., 500 wkg	5/9
16 x 16 mfd., 450 wkg	3/9
32 x 32 mfd., 350 wkg	4/-
32 x 32 mid., 350 wkg., and	-
25 mfd., 25 wkg	6/6
25 mfd., 25 wkg	11d.
250 mfd., 12 v. wkg	1/-
16 mfd., 500 wkg., wire ends	3/3
8 mfd., 500 v. wkg., wire ends	2/6
8 mfd., 350 v. wkg., tag ends	1/6
50 mfd., 25 v. wkg., wire ends.	1/9
100 mfd., 350 wkg	4/-
100 + 200 mfd., 350 wkg	9/6
16+16 mfd., 350 wkg	3/3
50 med 100 mbg	1/9
50 mfd., 180 wkg	1/6
65 mfd., 220 wkg	1/6
8 mfd., 150 wkg	7/6
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32+32 mfd. min. 275 wkg	
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Miniature wire ends moulded,	P9.3
100 pf., 500 pf., and .001, ea.	øa.
T.V. Filter in lightly tinted Pers	spex.
size 131 × 11 × 3/16ln., 4/6.	
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Combined 12in. mask and escutcheon in lightly tinted Perspex. New aspect, edged in brown. Fits on front of cabinet, 12/8. As above for 15in. tube, 17/6.

Frame Oscillator Blocking Trans. Line Osc. Blocking Traps., 4/6. Tube Mounting Bracket, size 91 × 42 in. 12in. tube clamps, 2/-.

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P.M. Pocus Unit for Mazda, 12in., with vernier adjustment, 17/6.

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Energised Focus Coil, low resistance mounting bracket, 17/6.

mounting bracket, 17/6.

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485 Ke. I.F.s. size 24 × 13 in. Q.110 removed from American equipment, 5/- per pair. Standard 465 Ke. Irop-fore ord I.F.s. 4×1½×1½in. per pr. 7/6. Wearite standard iron-cord 453 Ke. I.F.s. 3½×1½×1½in. per pr. 9/6.

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18in, x 4\frac{1}{6}in, x \frac{1}{16}in, \frac{1}{1} = each	1. × † in	
CONDENSERS	ь х үүнн	Per doz.
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2 Mfd. 150 v. Tubular Paper (aluminium tubes), 1/		
8 Mfd. 450 v. Electrolytic, 1/9 each		18/-
		21/-
8 x 16 Mfd., 350 v., 1/6 each		
20 x 20 Mfd., 275 v., Electrolytic, 2/9 each		30/-
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16 x 8 Mfd. Metal Cans Electrolytic, 350 v., 1/6 each		
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Condenser clips for above		
.1 Mfd. 400 v. Metal Cans, I/- each		
50 Mfd. 12 v., 1/- each		10/6
12 Mfd. 50 v. Tubular Paper (aluminium tubes), I		
100 Mfd. 6 v. Tubular Paper (aluminium tubes), 1		
.00005 Tubular, 4/- doz02, 500 v., 4/- per doz.,		., 4/- per doz.
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MIDGET MICA CONDENSERS: .0001, .0002		
200 Assorted Moulded Micas. Popular Values		
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CARBON RESISTORS: 1 watt 2/6; 1 w. 3/-; 1	w. 4/-; 2 v	w. 6/- per doz.
EX-GOVT. 60 mA. 10 HENRY CHOKE, no	ew	4/6 each
HIGH STABILITY RESISTORS:		

HIGH STABILITY RESISTORS:		_
Tolerance: 1% 2% 5%  # watt 1/- 9d. 6d. each COMPONENTS IN ST  # watt 1/3 1/- 9d. each	00	K
I watt 1/9 1/6 1/3 each PYE PLUGS AND	1/6	pai
WW AND VITREOUS RESISTORS. 5 watt, 1/6; 10 watt, 2/6; 15 watt, 3/-; 20/30 watt, 3/6. each.		
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500 ohms, IK, 20K, 25K, 50K, with spindle V/CONTROLS WITH SWITCH: most values, B-NSF	3/- 2/6	9.9
V/CONTROLS: Less Switch, Preset and Spindle. MOST	2/0	9.0
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lamp holders, I/9 each I/- each 9/- doz.

15/-

lamp holders, 1/9 each
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BC610 TRANSMITTERS with speech amplifier, aerial tuning unit, etc. Brand new.

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VENNER TIME DELAY SWITCHES, 24-v. operation, consists of a high grade clockwork movement, with external press button wind, 2 electro magnets with 5-pole cam operated contacts, in smart metal case size 3½m.×2½m.×2½m. Sitted 4-way terminal block, new boxed, fraction of original cost. 7/8, post 1/3.
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APPLIFIERS TYPE A.1271, consists of a VR-56 valve, type P-3000 relay, 400-ohm 6-post 1/3; 24/- dox., carriage 5/-.

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Disconnected distances, brand new boxed, tool shop price 15/-, our price 5/-, post 6d., por 10/-, post distances, post discon 10/-, post discon 10/-, post discon 10/-, post disconnected d

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- 5 Latest Type MULLARD Valves.
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- Chassis I IIn.  $\times$  7 in.  $\times$   $2\frac{1}{2}$  in. Scale 8 in. Square. Or Chassis  $13\frac{1}{2}$  in.  $\times$   $6\frac{1}{2}$  in.  $\times$   $2\frac{1}{2}$  in. Dial 10 in.  $\times$   $5\frac{1}{2}$  in. PRICE £10/5/-.
- BRAND NEW AND GUARANTEED, CARR., PACKING AND INS. 10/-.

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PYE 45 MC/S. STRIP. TYPE 3583 UNITS

TYPE 3583 UNITS
Size 15in. x Sin. x 2in. Complete with 45 Mc/s. Pye
Strip, 12 valves 10 EF50, EB34 and EA50, volume
controls and hoste of Resistors and Condensers.
Sound and vision can be incorporated on this chassis
with minimum space. New condition, Modification
data supplied. Price £5, Carriage paid.

VOLTMETERS							
6 v. 15 v. (50 c.) 20 v. 150 v. 300 v. 300 v.	M.C. M.C. M.C. M.C. A.C.	2 in. 2 in. 2 in. 2 in. 2 in. Projection	Projection Flush Square Flush Square on 5in. Dial	10/- 10/- 7/6 10/- 12/6 50/-			
		AMP-MET	ERS				
1 A. 3 A. 6 A. 15 A. 20 A. 30 A.	M.C. T/C T/C. M.I. M.I. M.C.	2½ ln. 2½ ln. 2½ ln. 4in. 2¼ ln. 2½ ln.	Projection Square Flush Projection Flush Mtg. Square	10/- 6/- 7/6 21/- 12/6 7/6			
	MI	LLIAMME	TERS				
600 uA. 1 mA. 1 mA. 1 mA. 1 mA. 5 mA. 10 mA. 30 mA. 30 mA. 50 mA. 50 mA. 50 mA. 60	M.C. M.C. M.C. M.C. M.C. M.C. M.C. M.C.	2in. 2in. 2in. 2in. 2in. 2in. 2in. 2in.	Round Square Flush Desk Type Square Flush Round Flush Square Square Flush Round Flush Round Flush Round Flush Round Flush Round Flush Round Flush Rot. doving Iron.	15/- 17/6 22/6 25/- 7/6 10/- 7/6 7/6 10/- 10/- 10/-			
T.C. = Thermo-Coupled.  All Meters are Brand New and in original cartons.							
All meters are Brand New and in original cartons.							

No. 38 "WALKIE-TALKIE" TRANS-NO. 38 "WALKIET ALTHOUGH AND A STATE OF THE ACTION OF A STATE OF A

"426" CONTROL UNIT Containing 4-EF50, 2-SP61, 2-EA50, 1-EB34, 2-single-gang .0005 tuning condensers. W/W volume/controls, switches, condensers and resistors. Size I2in. x 9in. x 5in. New condition, 35/-, carr. 3/-.

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Complete Kit obtainable at £6-7-6 or built and aligned at £8-10-0

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Will work into P/U sockets or amplifier

2

#### TRII96 RECEIVER

Receiver 25/73. This is a six-valve superhet receiver with 465 kc/s I.F.'s. Complete with all valves—2 EF39, I EK32, 2 EF36, I EB33. In brand new condition with full conversion data. 27/6, plus 2/6 post and pkg.

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Manufactured by Parmeko and Sound Sales
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AC/BL, MU14. Output Matching and 30
and 150, 100/250 v. A.C. COMPLETE IN
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RCA 931A PHOTO-ELECTRIC CELL AND MULTIPLIER. For facsimile transmission, flying spot telectne transmission and research involving low light-levels, 9-stage multiplier. Brand new and guaranteed, only £2/10/-. Special 11-pln base 2/-. Data sheets supplied.

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T.C.C. .1 mid. 5/7,000 v. wkg., type CP58QO, bakelite case, 7/8 each.

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Unit contains VOR517 Cathods Ray 6in. tube, complete with Mu-metal screen, 3 EF50, 4 8F61 and 1 5U46 valves, 9 wire-wound volume controls and quantity of resistors and condensers. Suitable either for basis of television (full picture guaranteed) or Oscilloscope. offered BRAND NEW (less relay) in original packing cases at 6716. Plus 7/6 carr. "Radio-Constructor" "scope circuit included. Complete kit of parts for this scopie. £8/18/6.

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600ft.	Reels		10/-
1,200f	t. Reels	**************************	17/6
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Complete with buzzer, morse tapper and battery compartment on baseboard, 6/-, post paid.

				CRYST	AL	S				
200	kc/s,	2	pin,	U.S.A.			 	 	10	/-
65	kels,	2	pin,	U.S.A.			 	 	10	-
00	kc/s,	2	pin,	British	٠,		 	 	15,	-

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The selected EF50, Red Sylvanian, original boxes 10/- each, 90/- for ten.

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METERS								
F.S.D.	SIZE	AND TYPE	PRICE					
1 milliamp	D.C.	2½in. Flush square	15/					
- I ,,	D.C.	2½in. Flush circular						
1 ,,	D.C.	21/2 in. Desk type	25/-					
5	D.C.	2in, Flush square	7/6					
100 ,,	D.C.	2½in. Flush circular						
150 ,,	D.C.	2in. Flush square						
500 .,	D.C.	2½in. Flush circular	12/6					
500	thermo	2in. Flush square						
	thermo	2in. Proj. circular	., 5/-					
20 amps	D.C.	2in. Proj. circular	7/6					
40 amps	D.C.	2in. Proj. circular						
30-0-30 amps	D.C.	Car type moving iron						
	A.C.	21in. Flush, circ., mov. iron	8/6					
All meters B	rand Ne	ew in Maker's Cartons.						

100 MICROAMPS METER, 21 in, circular flush mounting. Widely calibrated scale of 15 divisions marked "yards" which can be rewritten to suit requirements. These movements are almost unobtainable to-day and being BRAND NEW IN MAKER'S CARTONS are a snip at ONLY 42/6.

CARTONS are a snip at ONLY 42/6.

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ONLY 35/- each.

AMERICAN ROTARY TRANSFORMERS. 12 v. D.C. input.
Output 25 v. at 60 m/a. Ideal for car radio or running electric
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H.R.O. VIBRATOR PACK. 6 v. D.C. input. Output 165 v. at 85 m/a. fully smoothed. Complete with vibrator and 6 x 5 rectifier in black crackle cabinet, size 7½ x 7½ x 6in. Battery lead with croc clips supplied. ONLY 29/6.

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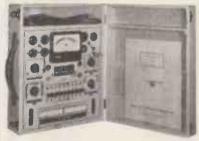
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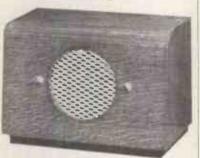
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tubes, 6/6, P.P. 9d.

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32 × 32 mfd. 4	150 7			6/11
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64 mfd. 350 v				
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A MPLIFIER, sound sales A-Z junior and pre-amplifier; £10, plus carriage.— Christie, Crondall, nr. Farnham, Surrey. [3205]

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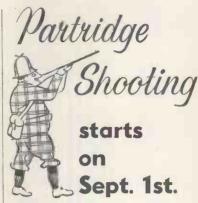
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£5; '55 unbound, 15/-—Box 6641. [3212]

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Rd., Peterborough.

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[3218]

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WEARTTE tape decks and component parts. DISC recording machines and blank discs.
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[3169

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prices as above; also supplied without smoothing, £25 del. immediate despatch; trade supplied.

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TELEVISION converter was tested on Ekcotelevision 12in tube, stated consumption 135 watts d.c. current from battery only 9½amps, pleture and sound were perfect and completely free of interference or flutter.

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TURN TO **PAGE NO. 147** 

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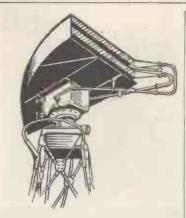
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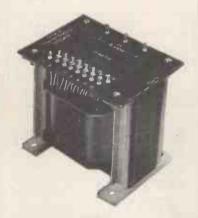
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3 Wave Bands, 16m-2,000m, R.F. pre-Amplifier, variable selectivity I.F. Delayed amplifier A.V.C. £21/6/8. Tax paid.

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200/250 voits in steeps of 10 voits, output 350/0/350
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6.3 voits 4 amps., 45/- each, post 1,6; another
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500/0/500 voits 150 amps., 4 voits 4 amps. C.T.,
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input, output 400/0/400 voits, 280 m/amps., 6.3
a., 2 v. 3 a., 5 v. 3 a., 4 v. 2 a., 4 v. 2 a., the last
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amps., £7/5/- each.

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1,000 WATT AUTO WOUND VOLTAGE
CHANGER TRANSFORMER tapped 0/110/
200/230/250 volts. £5/15/- each, carriage 4/6.
1,500 watt ditto, £7/15/-, carriage 7/6.
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NIGERIA for one tour of 15-24 months with
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The 12inch, 15 ohm Duode, with Dual Drive, built-in crossover and feedback, 14,000 gauss magnet, costs only 12 gns. New easy H.P. brings its enjoyment to you for 50/- down.

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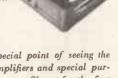
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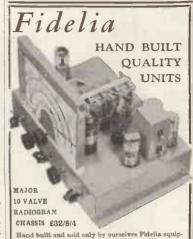
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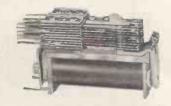
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Due to expansion in this department, applications are invited from Electronic Engineers and Physicists for posts concerned with the following fields of specialised

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Applicants for any of the above posts should possess a university degree or equivalent qualification and previous experience in similar work, although not essential, is considered an advantage.

In addition to the above posts, there are a number of less senior posts available for applicants who possess advanced level G.C.E. in science subjects or equivalent qualifications or who are at present pursuing courses leading to H.N.C. or external degrees. Such applicants should quote Ref. W.17. In addition to the above posts, there are a

Ref. W.17.

The vacancies outlined are at or near the Company's Mitcham factory. Salaries will be according to individual age, experience and qualifications and can be considered as progressive. Company policy regarding the employment of scientific staff provides adequate prospects for advancement and breadth of outlook is assured by opportunities of transfer to other fields of work within the Company's activities. There are facilities for further training and a Company Pension scheme. Pension scheme.

Applications in writing, which will be treated with the strictest confidence, should be addressed to the Personnel Officer, The Mullard Radio Valve Co. Ltd., New Road, Mitcham Junction, Surrey, quoting the appropriate reference number.

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ELECTRICAL engineer, qualified, required by cable manufacturers to work on the design of cable fittings; the work involves the development of fittings for polythene insulated high voltage cables; practical experience of cable accessories desirable; this post is pensionable and carriers a salary of £550-£600 upwards according to qualifications and experience.—Write details, quoting reference RG/2, to Staff Officer, The Telegraph Construction & Maintenance Co., Ltd., Telcon Works, Greenwich. S.E.10.

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N.I.

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moor Lane, Hall Green Birmingham. [3170 MITCHAM WORKS. Ltd., have vacandes for technical assistants able to carry out without close supervision, measurements on radio and/or television receivers and associated components; these posts offer excellent opportunities for young men to enter the factory laboratory of a leading receiver manufacturer COMMENICING salaries in accordance with age, experience and qualifications.—Candidates, who should have academic qualifications in radio to the standard of H.N.C., should apply in writing to the Personnel Officer, Mitcham Works, Ltd. New Rd., Mitcham Junction, Surrey, quotting reference G.1.

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- REF: The supervision of a small W.8 section carrying out quality control testing and special measurements of receiving valves, Liaison work with other departments will be required.
- REF: The testing of klystrons and simi-W.9 lar U.H.F. devices and the de-velopment of testing techniques for this purpose.
- REF: Testing and experimental work W.10 on semi-conducting devices of the crystal diode and transistor type,

Applicants for the above posts, which are permanent, should be Physicists or Electrical Engineers and should possess a university degree or equivalent qualification.

In addition to the above posts there are a number of less senior posts available for work in similar fields, for applicants who possess Advanced Level G.C.B. in science subjects or equivalent qualifications or who are pursuing courses leading to H.N.C. or external degrees. Such applicants should quote reference W.17.

For both grades previous experience is desirable but not essential.

The vacancies outlined above are at or The vacancies outlined above are at or near the Company's Mitcham factory and are due to the expansion of its activities in these fields. Salaries will be according to individual age, experience and qualifications and can be considered as progressive. Company policy regarding the employment of scientific staff provides adequate prospects for advancement and breadth of outlook is assured by opportunities of transfer to other fields of work within the Company's activities. There are facilities for further training and a Company Pension Scheme.

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Receiving Valve Development De-

Receiving valves
partment
REF. (a) The general engineering deW.1. velopment of receiving valves.
(b) Glass techniques, including
the control of existing and experimental work on new methods.
(c) The investigation of manufacturing processes with a view to attaining closer control and further development.

Filled Valve Development

Department. REF: (a) The

(a) The technological develop-ment of hot cathode gas filled rectifiers and thyratrons of all sizes and classes.

(b) The general development of cold cathode gas filled valves including stabilisers and reference tubes and also multi-electrode

Investigational work on gas discharge phenomena in relation to the tube classes mentioned under (a) and (b) above.

U.H.F. and Transmitting Valve

U.H.F. and Transmitting Valve
Development Department
REF: (a) The technological developW.3. ment of magnetrons, klystrons,
travelling wave tubes and kindred
devices. This work includes
metal-glass sealing, ceramic and
metal brazing techniques.
(b) General development work
on the more convertional class.

on the more conventional glass, metal-glass and disc seal valves usually for the V.H.F. range.

(c) Investigational work on the effects of variation of mechanical structure and of changes in materials used for (a) and (b)

Cathode Ray Tube Department REF: (a) The glass, mechanical and W.4. chemical technology of all types of cathode ray and kindred tubes including colour television tubes.

(b) Process development of methods used for the manufacture of new types of cathode ray tubes.
(c) Improvements in gun design

including electron optical work Semi-conductor Development

Department
REF: (a) The technological developW.5. ment of all types of semiconducting devices including
transistors and rectifiers.
(b) The investigation of semiconducting materials to establish
their possible application to
practical devices.
(c) The development of pro-(c) The development of pro-cesses and production methods

for semi-conducting devices. Applicants for the senior posts should be physicists, electrical engineers or, where appropriate, physical chemists and should possess a university degree or equivalent

possess a university degree or equivalent qualifications.

For the more junior posts candidates should possess Advanced Level G.C.E. in science subjects or equivalent qualifications, or should be pursuing courses leading to H.N.C. or external degrees.

should be pursuing courses leading to H.N.C. or external degrees.
For both grades past experience in similar work is desirable but not essential.
The vacancies outlined above are caused by the expansion of the Company's activities in these fields. Salaries will be according to individual age and experience and qualifications and can be considered as progressive. Company policy regarding the employment of scientific staff provides adequate prospects for advancement and breadth of outlook is assured by opportunities of transfer to other fields of work within the Company's activities. There are facilities for further study and a Company Pension Scheme. Applications in writing, which will be treated with the strictest confidence, should be addressed to the Personnel Officer, The Mullard Radio Valve Co. Ltd., New Road, Mitcham Junction, Surrey, quoting the appropriate reference number.

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Wembley. [3279]

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an interview.—Box 6485. [3178

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D.258/54.A. [3237]

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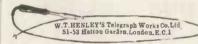
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