191.

Wireless World

Radio · Electronics · Television



FORTY-FOURTH YEAR OF PUBLICATION



Photo-Electric Multipliers 27M1 and 27M2

for light operated relays, film scanning, facsimile transmission, and many Research and Laboratory investigations involving low light levels.

Now available for prompt delivery

27M1 The 27M1 is a nine stage high vacuum photo cell with high response in the visible region. When operated at 100 volts per stage it is capable of multiplying very small currents produced under weak illumination by an average value of one million times. Under normal operating conditions the resultant output current is a linear function of the exciting illumination. The frequency response is flat up to the frequencies at which transit time of electrons within the valve becomes a limiting

Because of its great sensitivity, low noise level, low dark current and freedom from distortion the 27M1 may be used for light operated relays, film scanning, facsimile transmission and in scientific research involving low light levels. In many applications its small size is an advantage. List Price: £15.

MZ The 27M2 is a nine stage high-vacuum photo-cell similar to the 27M1 except that it has wider tolerances on the anode dark current necessitating a lower anode supply voltage with a resultant reduction in the current amplification to approximately one quarter of that obtainable from the 27M1. It is capable of multiplying very small currents produced under weak illumination by an average value of 250,000 times when operated at 80 volts per stage.

The 27M2 is suitable for the same applications as the 27M1 wherever the reduced magnification is acceptable. List Price: £6.



The secondary cathodes, or dynodes, of these multipliers are arranged in cylindrical formation so that they are exceptionally compact.

Voltage between anode and secondary - 50 volts cathode K10- - - - --100 volts Voltage difference per stage - -Maximum anode dark current (with 100 volts between anode and cathode K10) ·0.25µA Luminous sensitivity (taken on the basis of a lamp colour temperature of 2700°K and a light area of 5 mm x 20 mm) - - 20A/lumen Current amplification (ratio of anode sensitivity/cathode sensitivity)

Voltage between anode and secondary cathode K10- - - -- 50 volts Voltage difference per stage -80 volts Maximum anode dark current (with 80 volts between anode and secondary cathode K10) 0.25µA Luminous sensitivity (taken on the basis of a lamp colour temperature of 2700°K and a light area of 5 mm x 20 mm) - - 2.5A/lumen Current amplification (ratio of anode - - 0.25 x 10⁴ sensitivity/cathode sensitivity)

Either the 27M1 or the 27M2 may be used as a plug-in replacement for the American type 931A. A special stabilised power unit providing a highly stable H.T. supply for photo-multipliers is available. Full details on request.

RADIO DIVISION

THE EDISON SWAN ELECTRIC COMPANY LIMITED

Member of the A.E.I. Group of Companies

155 Charing Cross Road, London, W.C.2. Telephone: Gerrard 8660. Telegrams: Ediswan, Westcent, London

Wireless World

RADIO, ELECTRONICS, TELEVISION

44th YEAR OF PUBLICATION

Managing Editor: HUGH S. POCOCK, M.I.E.E.

Editor:

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NOVEMBER 1954

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VALVES, TUBES & CIRCUITS

23. MINIATURE VALVES WITH 25mA FILAMENTS

The Mullard range of low-consumption valves for all-dry battery receivers consists of four types, the DK96, DF96, DAF96, and DL96, mounted on the standard B7G base. The filaments are economically rated at 1.4V, 25mA. The DL96 output pentode has two such filaments which are normally operated in parallel.

The filaments in a receiver using these four types may be fed in three alternative ways: (i) in parallel; (ii) in pairs in a 50mA chain, with the odd filament (say the DAF96) shunted by a 5% tolerance resistor to maintain the correct filament current; (iii) in a 25mA chain. The third method is suitable for ABC receivers with separate h.t. and l.t. batteries; but the variation of cathode current in the output valve, which can occur when the batteries are at different

stages of exhaustion, must be limited. For this purpose a special filament chain has been devised, of which full particulars are given in the Additional Notes.

For mains operation, supply variations should be allowed for by presetting the filament current (by means of a variable portion of the dropping resistor) to $24\text{mA} \pm 2\%$ at nominal mains voltage.

The valves are designed for optimum performance with a 90V supply; but there is no serious loss of sensitivity in the amplifier stages at voltages down to 67.5V, as the recommended screen-grid voltages of the amplifier valves are about 65V. In the output stage, however, the loss of power caused by battery exhaustion is more marked with lower nominal battery voltages.

The Mullard DK96 is a heptode frequency changer in which the first two grids form the oscillator, and the third grid is the signal grid. The optimum conversion conductance is $300\mu A/V$, and the cathode current is 2.4mA at an oscillator voltage of 4.0V r.m.s. The variable-mu characteristic gives good cross-modulation and allows the use of AGC. The screen-grid voltage is about 65V, but in ABC receivers it should be adjusted to give 0.6mA anode current at zero bias.

A tuned-grid oscillator circuit is recommended, with the earthy end of the oscillator grid resistor taken to the positive side of the filament. Feedback should be derived from the oscillator anode, with the feedback winding of the oscillator coil preferably series-fed, especially at the higher frequencies.

The DK96 is not suitable for use above 20Mc/s. Pulling at frequencies above 10Mc/s should be reduced by capacitive neutralisation between the oscillator and signal grids.

The Mullard DF96 is an IF amplifier with a mutual conductance of $750\mu A/V$ at a cathode current of 2.2mA. It is suitable for AGC operation, as its grid base has been lined up with that of the DK96. The DF96 and the DK96 can be operated with a common screen-grid dropping resistor; but in ABC receivers this is allowable only if the two filaments are in parallel or if the control-grids are biased to their respective filaments. In all circuits, however, a common screen-grid resistor allows the relatively high screen-grid current of the DF96 to affect the gain of the DK96, and thus to increase the spread in the overall sensitivity of the receiver.

The Mullard DAF96 is a pentode AF amplifier with a detector diode. A voltage gain of 60 is obtainable when the detector presents a source impedance of $500 \mathrm{k}\Omega$, and a voltage output of $5.0 \mathrm{V}$ r.m.s. is obtained at 3% distortion. If the valve is used as a triode, the gain is about 11 and the voltage output is $5.0 \mathrm{V}$ r.m.s. at 2% to 3% distortion.

With a bias resistor of $10M\Omega$ the detector load resistor should be limited to $500k\Omega$ to give minimum attenuation in the control grid input circuit and an adequate a.c. to d.c. load ratio. With a detector load resistor of $1.0M\Omega$ the bias resistor should be $22M\Omega$.

Anti-microphonic precautions are necessary only when the control grid voltage is less than 20mV for 50mW output.

The Mullard DL96 output pentode is designed for 90V operation; but the grid base at 67.5V is sufficient to allow operation at this lower supply voltage. A single valve, under Class A conditions with a 90V supply, will give a 200mW output at 10% total harmonic distortion for an input signal of 3.4V r.m.s. At 67.5V the output is reduced to 100mW.

Two valves may be used in push-pull, with the grid signal provided by a driver transformer, a centre-tapped choke, or a phase-inverter valve. The total cathode current of the two valves must not exceed 12mA. Class B operation, with all four filaments in parallel, gives, at 2% to 3% distortion, 440mW output at 90V and 235mW at 67.5V. The comparable outputs for Class AB operation, at 3% to 4% distortion, are 420mW and 220mW.

The Mullard DM70 subminiature tuning indicator, which has been described in Valves, Tubes, and Circuits Nos. 5 and 6, is suitable for use with these valves.

Reprints of this a lvertisement, with additional notes on the design of filament supply chains, a circuit for a four-value battery receiver, and value data, may be obtained free of charge from the address below.



Wireless World

NOVEMBER 1954

VOL. 60 No. 11

B.B.C. Report

HE recently published Report* to the Postmaster-General for the year 1953-54 by the B.B.C. Board of Governors loses a little of its interest and value through being a trifle out of date. The document was prepared just before the final passing of the Act setting up the Independent Television Authority, and so, naturally enough, any attempt to consider the position of the Corporation vis-à-vis the new competitive body is specifically disclaimed.

Such incidental mention as there is of the possible effects of competition is confined to finance. It is a matter of some concern that, on present estimates, the B.B.C. will receive about £6M less than it expects to need for carrying through development plans during the next three years. Even if the financial stresses of that period can be weathered, the Corporation will, in the words of the Report, "inevitably have to ask for a larger share or even the whole of the proceeds of the £1 and £3 licences thereafter." We imagine that public opinion, and especially opinion in the radio world, will be strongly in favour of allowing the B.B.C. sufficient finance to carry through at least those parts of its development plan that have already been approved in principle by the Government. British broadcasting has been built up on a basis of successful long-term planning and even its harshest critics will not deny that the B.B.C. has in the past shown excellent engineering judgment, not to say foresight.

As might be expected, the bulk of the Report deals with the programme side and also gives detailed accounts of income and expenditure. There is, though, a 10-page section devoted to engineering in which the past year's work is surveyed and plans for the future are set out. In this section there is also a note on present policy in recruitment and training of technical staff. In addition to recruiting ready-trained men, the Corporation is taking in probationary technical assistants. No specific qualifications are expected of these, but they must pass a qualifying examination after an initial 12-week training course.

Colour television is accorded several mentions and

* Cmd. 9269 H.M.S.O., 4s. 6d.

it is interesting to read that the main effort of the research department was concentrated on this subject during the latter part of the year. Then there is the rather surprising statement that "the B.B.C. does not expect to introduce regular transmissions in colour within the next two years." This statement, with its inevitable implication that a regular colour service will start shortly after that period has expired, seems rather over-optimistic. In this matter, the Board of Governors appear to be slightly at variance with Sir Ian Jacob, the Director-General, who, in the current number of *The B.B.C. Quarterly*, was (rightly, we think) much more cautious and noncommital. "Nothing," he said, "could be more foolish than a precipitate start with coloured programmes."

V. II. F. Quality on

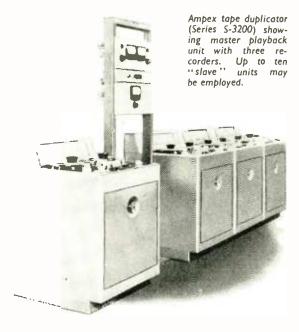
AS most of our readers know, the B.B.C.'s plan for reinforcing the present sound broadcasting service with v.h.f. three-programme stations is due to start with Wrotham next May. The remaining eight stations of the first stage of the scheme should be finished within less than two years.

This scheme is described in the Report discussed in the preceding paragraphs, and was also the subject of a talk given recently to the Radio Industries Club by Harold Bishop, B.B.C. Director of Engineering Services. Some disappointment was felt, even among the more realistic, at Mr. Bishop's summary dismissal as "nonsense" of the idea that f.m. broadcasting would automatically bring about a great improvement in quality of reproduction. No doubt, as he said, the idea of giving a bandwidth of 15 kc/s is impracticable for a nation-wide service depending on a long and complicated network of landlines for linking the stations. However, the quieter background and freedom from interference that many f.m. listeners will enjoy will inevitably focus attention on quality of reproduction. It will be a great pity if the B.B.C. does not do all it can, within the bounds of good engineering, to ensure the best possible quality from the new service.

WIRELESS WORLD, NOVEMBER 1954

Tape Duplication System

EQUIPMENT for the duplication of recorded magnetic tapes on a commercial basis is now being sold in America. A master playback unit feeding a master amplifier and bias oscillator supplies from one to 10 "slave" recorders. Both tracks of the twin-track



master tape are read and re-recorded simultaneously and the tape speed for duplication may be as high as 60 in/sec. This calls for pick-up and recording heads capable of handling frequencies up to 120 kc/s if the original tape carries 15 kc/s at 7½ in/sec. The heads used are designed for supersonic recording and are similar to those which have been developed by Ampex for recording data in flight testing.

No time is wasted in rewinding the master since the machine duplicates in both directions. It has been calculated that, with the full complement of 10 recorders, the output of 33-in/sec tape duplicates is increased by a factor of as much as 320 over a pair of standard recorders running at the original speed of the recording. (Speed \times 16, twin tracks \times 2, recorders

Total cost for a 10-unit installation is said to be less than \$20,000. The makers are Ampex Corporation, 934, Charter St., Redwood City, California.

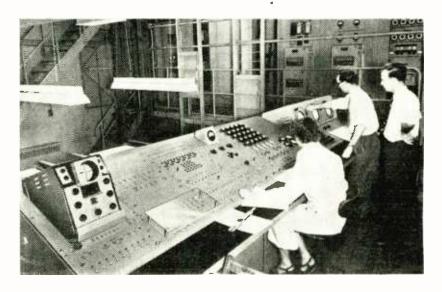
N.B.S. Laboratories

THE new research centre of the American National Bureau of Standards at Boulder, Colorado, was officially opened on September 11th. A series of scientific meetings was held coincident with the opening and included a symposium on propagation. standards and problems of the ionosphere. Among those present at the opening was H. J. Finden, chief engineer of the Electronic Instruments Laboratory of the Plessey Company, to whom we are indebted for the following report.

The Boulder Laboratories, which supplement the N.B.S. facilities in Washington, D.C., include the Bureau's Central Radio Propagation Laboratory transferred from Washington. The C.R.P.L. is the chief American research centre for the study of the troposphere and ionosphere as media for the propagation of radio waves. It also develops and maintains the national primary standards for the complete radiofrequency spectrum. As the nation's central agency for collecting radio propagation data, the C.R.P.L

GUIDED-MISSILE SIMULATOR

The control desk of "Tridac," a large-scale analogue computor built by Elliott Brothers and recently put into operation at the Royal Aircraft Establishment, Farnborough. It calculates the flight behaviour of new types of guided missiles in three dimensions and gives the distance by which they miss the target. Parts of actual missile control systems can be included in the computor, as it behaves as a model of the missile flight and operates in "real" time. The c.r.-tube displays on the right give a representation of the missile approaching its target in three separate dimensions. Computing elements in the machine include large numbers of d.c. amplifiers, and some idea of the techniques used can be gathered from " Electronic Analogue Computing" in our March, 1954, issue.



WIRELESS WORLD, NOVEMBER 1954

analyses and disseminates information which is of vital importance for the maintenance of radio services

in aviation, shipping and communications.

The Laboratory's studies of frequency allocation and interference affect the establishment and operation of all American broadcasting stations. Data on v.h.f. radio propagation and the development of micro-wave techniques are important to the weather bureau and military aerologists for use in the measurement of upper air temperature, humidity and wind.

Boulder is well situated in that the plains extending hundreds of miles eastwards from the mountains permit many phases in radio propagation research. Use is also made of the nearby mountains and several transmitters are located in the Cheyenne, near Colorado Springs. Frequency utilization research carried out by the N.B.S. is providing valuable data on the effects of noise due to the troposphere as well as the sun and terrain, particularly at frequencies above 50 Mc/s.

"A Guide to Amateur Radio"

THIS book was first published by the Radio Society of Great Britain in 1933; a new edition appeared each year on the opening of the National Radio Exhibition until 1937, when it was superseded by *The Amateur Radio Handbook*. The present publication, styled the sixth edition, follows the tradition of the earlier ones, but is far more comprehensive.

Its aim is to provide the newcomer to amateur radio with up-to-date information on present-day practices and to give expert advice on how to obtain an amateur transmitting licence. There are chapters on learning morse, making simple equipment, abbreviations commonly used in amateur transmission and sundry other subjects not easily found elsewhere.

The publisher's address is New Ruskin House, Little Russell Street, London, W.C.1, and the price is 2s 6d

(2s 9d by post).

Fleming's Pre-Valve Work

From Watts to Kilowatts

THE name of Sir Ambrose Fleming is inevitably bound up with the invention of the thermionic diode and this month celebrations are being held to mark the jubilee of the first valve patent (see October issue, p. 474). On such an occasion it is interesting to recall that Fleming had been engaged in radio work for some time before making his great invention, and can be considered as one of the pioneers of the spark transmission era.

Probably his most important pre-valve work was on the design of the famous Poldhu transmitting station, by means of which the Atlantic was first spanned by radio in December, 1901. Here he was acting as scientific adviser to the Marconi Company. Up to this time, radio people had been thinking in terms of the conventional induction-coil spark transmitter, but Fleming realized that a different approach would be needed for a station that would have to radiate kilowatts instead of watts.

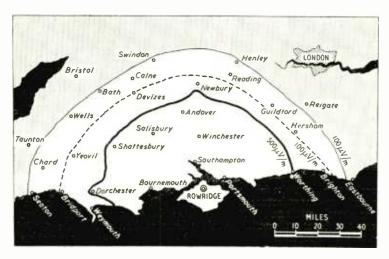
In place of an induction coil he specified an alternator driven by a 25-h.p. engine and working into high tension transformers to give an output voltage of 20kV. This arrangement fed an oscillatory circuit, having the usual spark gap and capacitor, which in turn was coupled by a step-up r.f. transformer to a second similar circuit. Finally came a radio-frequency transformer or "jigger" for coupling to the aerial. Keying the transmitter was achieved by short-circuiting air-core chokes inserted in the leads running from the alternator to the high-tension transformer.

Fleming's contribution to the famous transatlantic experiment is commemorated on the granite column which marks the site of the station on the cliff-top at Poldhu.

SOUTH COAST TV STATION

Coverage of Isle of Wight Transmitter

Provisional field-strength contours of the new Rowridge, Isle of Wight, television station which has been radiating test transmissions for the past fortnight and is scheduled to be brought into service on November 12th. The station, which operates in Channel 3 (56.75 and 53.25 Mc s), will use initially a temporary most and aerial system and the service area will, therefore, be restricted. The anticipated 100-µV m contour for the temporary aerial is shown dotted on this map. This and the other contours are based on a receiving aerial height of 30ft. The temporary station on Truleigh Hill, near Brighton, which has been serving part of this area of the south coast since May last year, will close down.



Wireless World, November 1954

WORLD OF WIRELESS

C.C.I.R. Interference Investigation * Receiver Exports * Personal and Industrial Notes and News

I.F. for TV

REALIZING that a nationally protected i.f. band for television does not offer protection against interference from other countries, Italy has asked the International Radio Consultative Committee (C.C.I.R.) to study a number of questions relating to interference with television reception and interference to other ser-

vices by television receivers.

Among the specific subjects to be studied are: the factors which govern the frequencies and amplitudes of undesired receiver responses and the characteristic values for different types of receiver (sound, television, etc.); the methods which can be adopted to reduce these responses without greatly increasing the cost of receivers (the choice of i.f. falls into this category); the best methods for measuring and evaluating local oscillator and i.f radiation; typical values of the amplitudes of these radiations and the variation of their power as a function of distance; the methods whereby a useful reduction in the amplitudes of these radiations could be achieved without appreciable increase in receiver costs and the extent of this reduction.

Information on these subjects is to be submitted by national representative organizations to the C.C.I.R. and, in the meantime, the European Broadcasting Union Document Tech. 3062 (see our July issue) has been submitted as a contribution to the inquiry.

Amateur Radio Show

AT noon on November 24th, the eighth annual Amateur Radio Exhibition, organized by the Radio Society of Great Britain, will be opened at the Royal Hotel, Woburn Place, London, W.C.1, by H. Faulkner, C.M.G., director of the Telecommunication Engineering and Manufacturing Association. The exhibition will continue until November 27th and be open daily from 11.0 a.m. to 9.0 p.m. Admission is 1s.

Members of the R.S.G.B. will be exhibiting a wide range of home-constructed equipment, and the following manufacturers and organizations are taking space: Air Ministry, Amos, Avo, Cosmocord, English Electric, Enthoven Solders, G.E.C., Grundig, Labgear, Magnetic Devices, Minimitter Co., Philpotts, Pye, S.T.C., Short Wave Magazine, Taylor Instruments,

War Office, Wireless World.

Television Exhibition

THE Television Society's annual exhibition will be held from January 6th to 8th in the gymnasium at University College, Gower Street, London, W.C.1. Admission on the opening evening (6.0-9.0) is limited to members, but tickets will be available to non-members for the following two days, when the show will be open from noon to 9.0 p.m. and 10.0 a.m. to 7.0 p.m. respectively. Tickets will be available from the secretary at 164, Shaftesbury Avenue, London, W.C.2.

About 40 exhibitors will be participating. The majority of exhibits will be laboratory equipment provided by manufacturers, but there will be some members' exhibits. The exhibition is concerned more with research and industrial television than with

domestic reception.

Middle East Market

TWELVE receiver manufacturers are sharing the B.R.E.M.A. pavilion at the British Trade Fair which is being held in Baghdad from October 25th to November 8th. The firms participating are: Bush, Cossor, Ekco, E.M.I., English Electric, G.E.C., Kolster-Brandes, Mullard, Murphy, Philco, Pilot and Regentone. Other radio and electronic manufacturers participating in the Fair are B.I. Callenders, Ediswan, Ever Ready, Pye, Redifon, Roberts Radio, S.T.C., and Thorn Electric.

Television programmes for the demonstration of receivers at the Fair are broadcast by a temporary transmitter (using a 60-foot mast) installed by Pye.

The Middle East is regarded as one of the most promising markets for British radio equipment. Figures provided by B.R.E.M.A. show that the value of receivers and radio-gramophones exported to this area in the first eight months of this year almost equalled those for the whole of 1953—£364,906, compared with £412,359.

"No Half-way House"

"NOW that colour has become the obvious next move in the development of television, let us learn from our past mistakes and not again hitch ourselves to a wrong system [as in 1946 when we re-adopted 405 lines]. . . . Let us make our own mistakes if we must, but not a mistake just because the Americans have already made it. . . . The system we start with is the system we shall end with, and in my opinion it rules out any public experiment of a compatible or semi-compatible system in Band III with the hope that later we will be able to move colour television to Bands IV and V." This extract is taken from a speech by C. O. Stanley printed in the annual report of Pye, Ltd., of which he is chairman. He concluded by saying that the radio industry, as a whole, could and should provide the answer to the colour TV question, and not wait for any committe, Government or otherwise, to produce a recommendation.

Servicing Exams

OF the 367 candidates who sat for the Radio Servicing Certificate Examination last May, 143 passed, 96 were put back in the practical test and 128 (35 per cent) failed. The percentage of failures in the television servicing exam was lower—28 per cent. Of the 104 entries 55 passed, 20 were put back in the practical test and 29 failed. The examinations, which are conducted jointly by the Radio Trade's Examination Board and the City and Guilds of London Institute, were held at 24 centres for radio servicing and 7 centres for television servicing.

As mentioned in our last issue the 1955 radio servicing exams will be held on May 3rd and 5th (written) and 14th (practical). Those for television servicing will be on May 9th and 11th (written) and June 18th (practical). Entries for the television servicing exam. (fee 3 gns), must be sent to the R.T.E.B., 9, Bedford Square, London, W.C.1, by January 15th, and those for the radio servicing exam. (fee £2 12s 6d),

by February 1st.

PERSONALITIES

Dr. W. H. Penley, B.Eng., Ph.D., A.M.I.E.E., who in 1940 joined the Telecommunications Research Establishment and for the past four years has been superintendent, air defence radar, has been appointed senior superintendent, guided weapons, at the Radar Research Establishment, Malvern, which now incorporates T.R.E.

Group Captain R. C. Richmond has been appointed to the London Office of Marconi's Wireless Telegraph Company (Marconi House, Strand, W.C.2) where he will be concerned with the Company's aeronautical radio business. He joined the R.A.F. in 1929, and took the specialist signals course. During the war he was Chief Signals Officer of various commands and was at one time Chief Signals Officer, Air Defence of Great Britain. Prior to retiring, Group Captain Richmond was Commanding Officer of No. 2 Radio School, Yatesbury.





Grp. Capt. R. C. RICHMOND

S. E. ALLCHURCH

S. E. Allchurch, O.B.E., secretary of the British Radio Equipment Manufacturers' Association since 1946, is at the British Trade Fair in Baghdad to take charge of the composite exhibit of domestic receiving equipment by 12 member-firms. During the war Mr. Allchurch joined a new department of the Ministry of Aircraft Production which dealt with the co-ordination of research, development, production and installation of communication and radar equipment for the R.A.F. He was assistant director when he left to join B.R.E.M.A.

William H. Date, B.Sc.(Eng.), M.I.E.E., has retired from the position of head of the Electrical Engineering Department of the Polytechnic, Regent Street, London, which he has held for seven years. He joined the full-time staff of the department in 1913. During the first world war he was a technical officer (wireless) in the Royal Flying Corps and during the last war was lent to the War Office and was attached to the department concerned with the organization of training schemes for Service men at technical colleges throughout the country.

The new head of the Electrical Engineering Department of the Polytechnic is **Dr. D. O. Bishop**, Ph.D., who received his academic training at the Portsmouth Municipal College and then went to B.T-H. at Rugby. After war service as an education officer in the R.A.F. he returned to the Portsmouth Municipal College and became senior lecturer in 1947. He joined the Regent Street Polytechnic as senior lecturer in the Electrical Engineering Department in 1948.

G. E. Middleton, M.A., the new chairman of the I.E.E. Cambridge Radio Group, went to B.T-H., Rugby, after graduating from Cambridge in 1927. During his 21 years with B.T-H., one of which was spent in the U.S.A. under the company's Fellowship scheme, Mr. Middleton was engaged on the design of small motors. In 1948 he went to Cambridge as university lecturer in engineering—his present position.

Major P. L. Barker, B.Sc., this year's chairman of the Northern Ireland Centre of the I.E.E., has been chief engineer of the N. Ireland Region of the Post Office since 1946. After graduating from Birmingham University in 1923 he entered the Post Office Engineering Department. From 1925 to 1935 he was at the Dollis Hill Research Station working on short-wave propagation and from 1936 until he was commissioned in R.E.M.E. in 1940 he was at the Wembley Laboratories.

Dr. J. H. Mitchell, Ph.D., B.Sc., the new chairman of the East Midland Centre of the I.E.E., has been head of research with Ericsson Telephones, Ltd., Nottingham, since 1947. He studied at Bristol University after which he joined B.T-H. at Rugby as a research engineer. During the war Dr. Mitchell was a member of the Government Scientific Research Pool and undertook research on radar and radio navigational aids and v.h.f. communication.

David H. Thomas, M.Sc.Tech., chairman of the North-Eastern Radio and Measurements Group of the I.E.E. for this session, was for eight years lecturer in tele-communications at the University of Nottingham and is now head of the Electrical Engineering Department of the Rutherford College of Technology, Newcastle-upon-Tyne. Before entering the scholastic field he was a research engineer with Metropolitan Vickers whom he joined as an apprentice.

M. I. Forsyth-Grant, A.M.I.E.E., has resigned from International Aeradio, Ltd., with whom he had been chief engineer since 1952, and has joined the board of Racal Engineering, Ltd. Before joining I.A.L. in 1947 he was with E.M.I. Engineering Development, Ltd. D. W. Morrell, B.Sc.(Eng.), A.M.I.E.E., who has been sales manager of Racal for the past 18 months, has also been appointed a director.

A. R. Lash, A.M.I.E.E., recently appointed managerengineer of the Ongar (Essex) radio station of the Post Office, was previously on the staff of Marconi's W.T. Co. and Cable & Wireless. His duties as a radio communications engineer have taken him as far north as Spitsbergen and as far south as the Falkland Islands.

OUR AUTHORS

W. R. Cass, who, with R. M. Hadfield, contributes the article on "Dip-soldered Chassis Production" in this issue, is in charge of the Methods Development Department of Pye, Ltd., Cambridge. Joining Pye from Telephone Rentals, Ltd., in 1951, he was initially connected with power control and television receiver circuitry development. Mr. Cass obtained the Higher National Diploma in Telecommunications at the Regent Street Polytechnic and was an electronics instructor in R.E.M.E. during the war R. M. Hadfield studied at Reading University after serving as a pilot in the R.A.F. In 1952 he joined the Methods Development Department of Pye, Ltd., and is now responsible for operational research and work study development.

Arieh F. Fischmann, author of the article on the design of a tape recording amplifier on page 564, is at present studying at the Polytechnic Institute of Brooklyn, U.S.A. After training at the Deutsche Technische Hochschule, Prague, he emigrated to Palestine in 1938 where he worked on the design of audio amplifiers. From 1948 until going to Brooklyn he was in the Scientific Department of the Israeli Ministry of Defence on development work in the field of pulse techniques.

H. H. Ogilvy, contributor of the article on the measurement of phase and amplitude in this issue, has been employed in the fire-control section at the Admiralty Engineering Laboratory, West Drayton, Middlesex, since 1951. He is concerned with the development of electronic equipment for fire-control systems and the design of equipment for analysing the performance of servo-mechanisms. After war service as h.f. direction-finding

officer in the Navy he took a full-time engineering course at Loughborough College from 1946 to 1950.

IN BRIEF

Broadcast Receiving Licences current in the United Kingdom at the end of September totalled 13,527,864, including 3,677,796 for television and 245,836 for sets fitted in cars. During the month television licences increased by the unprecedented figure of 144,098.

Electronics in Action is the theme of an exhibition of electronic aids to production, design and research being organized by the Scientific Instrument Manufacturers' Association for November 23rd to 25th at the Chamber of Commerce Hall, New

Street, Birmingham. Admission to the exhibition is by complimentary ticket. from obtainable S.I.M.A., 20, Queen Anne Street, London, W.1, or the Chamber of Com-merce. The exhibition, at which there will be some 20 will be some 20 exhibitors, opens at 2.0 on the first day and 10.0 on subsequent days and closes daily at 8.0.

This combination aerial for television and f.m. sound, exhibited by Belling-Lee at the Radio Exhibition, was by mischance overlooked when our review of the show was compiled for last month's issue

The proposed dates for the second post-war Northern Radio Show which the Radio Industry Council plans to hold in the City Hall, Manchester, have been amended; they are now May 4th to 14th, 1955

I.T.A.—The temporary headquarters of the Independent Television Authority, of which Sir Robert Fraser is director-general, are at 12-16, Wood's Mews, Park Lane, London, W.1. (Tel.: Mayfair 6272). The I.T.A. has, so far, been operating from the Post Office headquarters.

The P.M.G. has relaxed one of the regulations included in the recently introduced Amateur (Television) Licence. Holders may now transmit messages by telephony or morse without a separate licence provided they are concerned with the technical matter of the visual transmission.

Extending French TV.—The fourth French television station—at Marseilles—was brought into service in September. Operating on 186.55 Mc/s vision and 175.4 Mc/s sound, the 819-line transmitter has an e.r.p. of 50 kW. Initially the station is relying on filmed programmes flown from Paris. On October 15th the fifth television station was brought into service at Lyon-ville which is linked with Paris by radio relay stations. The Lyon-ville 200-watt transmitter operates on 164 Mc/s vision and 175.15 Mc/s sound.

Brit.I.R.E. Awards.—The Clerk Maxwell premium (20 guineas) has been awarded by the British Institution of Radio Engineers to Dr. W. Saraga, D. T. Hadley and F. Moss for their paper "An Aerial Analogue Computer"; the Heinrich Hertz premium (20 guineas) is given to B. E. Kingdor, for his paper "A Circular Waveguide Magic-Tee and Its Applecations to High-Power Microwave Transmission"; Dr. D. A. Bell receives the Louis

Sterling premium (15 guineas) for "Economy of Bandwidth in Television"; Dr. Paul Eisler the Marconi Premium (10 guineas) for "Printed Circuits—Some General Principles and Applications of the Foil Technique" and J. A. Youngmark the Dr. Norman Partridge Memorial award (5 guineas) for "Loudspeaker Baffles and Cabinets." The first award of the Sir J. C. Bose Premium (250 rupees—approx. 18 guineas) for the most outstanding paper by an Indian engineer has been made to S. K. Chatterjee for "Microwave Cavity Resonators—Some Perturbation Effects and Their Applications."

Cable and Wireless announce the opening of the first direct Radio-telephone Service between Aden and India on October 15th. A radio-telephone service between Aden and London and thence to Europe and north America is also provided by the company via its station at Nairobi.

The Radar Association, which, although originally formed as a social link between ex-R.A.F. "radar types," is now open to radar engineers and technicians in the other Services and industry and holds regular lecture meetings. The second meeting of the 1954/55 session will be held at 7.30 on November 10th in Theatre No. 1 of the Lime Grove Television Studios, Shepherds Bush, London, W.12, when Group Capt. Philip Dorté and John Elliot (B.B.C.) will deal with the production of the television film "War in the Air." Tickets are necessary.

E.I.B.A. Ball.—The annual ball in aid of the funds of the Electrical Industries' Benevolent Association will be held at Grosvenor House, Park Lane, London, W.1, on November 12th. Tickets, price 2½ guineas, are obtainable from the association at 32, Old Burlington Street, London, W.1.

Two lectures on the design, construction and erection of Television Aerials are to be given by P. Jones, of Aerialite, Ltd., at the Gloucester Hotel, Aberdeen, on November 3rd and 4th at 3.0. Admission tickets are obtainable from Aerialite, Ltd., Castle Works, Stalybridge, Cheshire.

The Electrical Engineering Department of the Oldham Municipal Technical College, which is now occupying a new building, offers part-time day or evening courses in radio servicing (3 years), television servicing (2 years), telecommunication engineering and for the Higher National Certificate.

A series of eight lectures intended to present an up-todate account of Information Theory and its implications in the field of communication engineering is to be given at the College of Technology, Manchester, on Friday evenings, beginning January 21st. The fee is 30s. Twelvelecture courses on "Automatic Control in Industry," which began on October 26th, and "Transient Electrical Phenomena" beginning on January 13th (fees 35s) are also provided by the College.

Among the new courses provided at the recently opened engineering block of the N.E. Essex Technical College at Colchester is a year's evening course in electronics and measurements for the H.N.C. Part-time day and evening courses in preparation for the radio service work certificate of the City and Guilds of London Institute are also provided by the college which has a well-equipped radio servicing laboratory.

Information additional to that given in our September issue (p. 439) regarding courses provided by the N.W. Kent College of Technology (previously the Dartford Technical College) has been received from the head of the Electrical Engineering Department. An evening course in television servicing is provided and as an alternative to the evening course in radio servicing a part-time day course has now been introduced.

Properties of Glass Reinforced Plastics and their applications in various industries are dealt with in the 256-page book "Glass Reinforced Plastics," edited by Phillip Morgan and published for British Plastics by our Publishers, price 35s. One of the chapters deals with glass fibre laminates in the electrical field.

The second edition of Kenneth W. Gatland's book "Development of the Guided Missile," which has been completely revised and enlarged, includes an appendix giving details of the telemetering equipment used in British missiles. Published for Flight by Iliffe and Sons Ltd., this 292-page book costs 15s.

Philips have arranged for the future distribution in this country of their three journals Philips Technical Review, Philips Research Reports and Communication News to be undertaken by Cleaver-Hume Press, Ltd., 31, Wright's Lane, Kensington, London, W.8.

BUSINESS NOTES

Transmitters for the first three stations of the Independent Television Authority have been ordered from Marconi's. The vision transmitters will have a power of 10 kW and the associated sound equipment 2.5 kW. They will, of course, operate in Band III. To expedite the start of transmissions from the London station at Crystal Palace prototypes of the transmitters are being lent to the LT.A.

International Aeradio, Ltd., of this country, and Adalia, Ltd., of Montreal, Canada, have entered into an agreement to pool their knowledge, experience and staff in order to offer consultancy services to governments and industry throughout the world. Their first joint contract is for the planning of a telecommunications system for the Creole Petroleum Company, of Venezuela.

Claude Lyons, Ltd., the well-known manufacturers of Variac transformers and importers of American laboratory instruments, have acquired a new factory at Valley Works, 4-10, Ware Road, Hoddesdon, Herts. (Tel.: Hoddesdon 3007.) The London office has closed, but the head office and works will remain at 76, Oldhall Street, Liverpool. The new factory houses the research and development staff and provides a repair and recalibration service.

The Service Department of Baird Television has been transferred to 308, Battersea Park Road, London, S.W.11 (Tel.: Battersea 7838). All correspondence relating to servicing and replacement parts for television receivers and Baird tape recorders should be sent to this address.

The West Bromwich firm of spring manufacturers, George Salter & Co., Ltd., have built a "Dry Room" to Ministry of Supply regulations for the packing of electronic equipment under conditions which ensure that it is not only impervious to outside climatic changes but also that each piece of equipment is thoroughly moisture-free before being packed.

The recently opened factory of 20th Century Electronics at New Addington, Surrey, has now been extended.

at New Addington, Surrey, has no doubling the floor space. The manufacturing and research sections of the cathode-ray tube department, formerly at Dunbar Street, London, S.E.27, are now at New Addington, where new plant has been installed for the production of multi-gun tubes. All correspondence should now be addressed to King Henry's Drive, New Addington, Surrey. (Tel.: Springpark 1026.)

WIRELESS ROOM in the 3,300-ton cable ship Recorder, the latest and fastest vessel in the Cable & Wireless fleet of eight. Marconi's installed the radio-communication equipment and Kelvin & Hughes the radar and echo sounders. An aerial-iplitter system permits the use of 35 broadcast receivers in the ship without interference from the transmitters.

Electric Audio Reproducers, Ltd., manufacturers of sound reproducing equipment, of 17, Little St. Leonards, Mortlake, London, S.W.14, have opened a new factory at Worton Road, Isleworth, Middlesex. The development section will occupy part of the factory, but the offices and service department will remain at Mortlake.

A new branch office and depot at 2, St. Nicholas Buildings, Newcastle-upon-Tyne, 1, has been opened by the Telegraph Construction and Maintenance Company. The company has also opened a London sales office at Norfolk House, St. James's Square, S.W.1.

Hudson Electronic Devices, Ltd., of Appach Road, London, S.W.2, have appointed Pendry & Kennedy (Electronics) of 6, Coed Celyn Road, Derwen Fawr, Swansea, to handle the land sales and services of their v.h.f. radio-telephone equipment in the south Wales area.

Transvision, Ltd., has been formed by B. J. Martindill, until recently general manager of Wolsey Television, and F. Gould, for the production of television and v.h.f. aerials and accessories. The address is 118, Denmark Hill, London, S.E.5. (Tel.: Brixton 6551.)

FOREIGN TRADE

Redifon, Ltd., has received a substantial order for marine radio equipment on behalf of the Soviet Fishing Authority. The equipment, comprising transmitters, all-wave receivers, combined medium- and short-wave direction finders and ancillary units, will be installed in twenty deep-sea fishing vessels now under construction for the Soviet Union at Lowestoft, Suffolk.

Haiti.—The British Embassy at Port-au-Prince has received an enquiry from a Government source in Haiti for the supply of robust, cheap battery receivers for use in rural areas. The proposal is to supply about 500 sets for domestic use or for use by small groups, or, alternatively, to equip a smaller number of centres with larger receivers designed for communal use. Manufacturers are invited to send details of their offers direct to H.M. Consul-General, British Embassy, Port-au-Prince, Haiti, W. Indies.

Salvador Agency.—Almacen Liverpool, Calle Ruben Dario-32, San Salvador, are interested in securing an agency for British-made domestic receivers. Transmitters in the western hemisphere operate on medium waves and the mains voltage in Salvador is 110 (50 c/s).

Colombian Agencies for British-made components and accessories are sought by Almacen Radion, Guillermo Ibanez, Calle 36, No. 41-78, Barranquilla, and J. Angers, Apartado Aereo 913, Barranquilla.



Dip-Soldered Chassis Production

Simplifying the Assembly of Sound and Television Receivers

By W. R. CASS, *H.N.D., Grad.I.E.E., and R. M. HADFIELD, *B.A.

N the endeavour to reduce the cost of massproduced electronic assemblies it became apparent that a simpler way of making electrical connections was needed. Conventionally, pliers are used to anchor connecting wires to tags and then solder is applied with an iron to make these mechanical connections into sound electrical joints. In a television receiver there are between 500 and 800 such connections to be made.

After costing several systems it was decided that the most suitable basic technique was one in which all connections are made simultaneously with a single dip in hot solder. For this method it is convenient to bring all points of interconnection into one plane. This is done by laying all the components on an insulated board and inserting their pre-formed wire ends into holes so that all points to be soldered are on the underside. Once such a layout has been adopted it is a short next step to use a printed wiring pattern on the underside of the chassis to replace the wire links which connect one part of the circuit with another.

Superficially it might appear that the addition of printed wiring is of little value, since it obviously costs more than the wires it replaces and only saves a small amount of assembly time. However, this is not so, because the most important function of printed wiring is not, as its name suggests, to eliminate wire links, but to provide a base for dip-soldering. At each component junction a piece of copper foil surrounds the wires, even if there is no circuit line joining this point to another point. This piece of copper picks up solder, which links the adjacent component wires. Besides assisting the soldering of electrical connections small areas of copper foil left on the board provide

points to which the heavier components can be secured in the dip-soldering operation. This saves much mechanical fixing with screws, brackets, etc. A dip-soldering system that does not use a printed wiring base must make use of eyelets at all points where a soldered connection is required. The insertion of these eyelets costs more in material and labour than does a printed wiring board.

Four times as many sound or television receiver chassis can be made by an assembly line using the dip technique as can be made by one using hand assembly methods. This means not only lower labour costs but reduced overhead costs per unit as well. Savings of the last-mentioned include supervision, factory space, heating, lighting, power and soldering-iron maintenance. It must be

Underside view of a 4-valve battery receiver made by the "dip-circuit" technique with (belcw) the same chassis mide by conventional methods. The top of the dip-soldered chessis is shown in the picture at the top right of page 538.

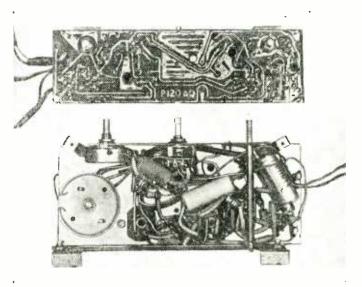
emphasized, however, that the assembly cost in massproduced television and sound receivers is only a small fraction of their total cost. Thus, even the 300 per cent improvement in chassis assembly productivity achieved will only result in overall cost savings of the order of 2-3 per cent.

Material savings result from the elimination of nearly all brackets, tag strips, sleeving, wire, screws, eyelets and rivets. These savings more than offset the extra cost of the copper-faced Bakelite chassis. Some of the savings are possible because the mechanical attachment of many components becomes unnecessary: all forms of screening can be dip-soldered, and trimmers, valveholders, transformers and large capacitors need no additional fixing. Other savings result from the fact that much insulation can be dispensed with when a non-conducting chassis is used. At present this means that neither sleeving nor insulated resistors are necessary in the receivers, and ultimately it will result in cheaper valveholders and transformers as well

The elimination of the above items plus the use of a laminated Bakelite chassis results in considerable weight saving; this reduces the problem of adequately securing the assembly in a cabinet. The weight saved on the chassis varies from 1lb on a small sound receiver to 4lb on a television set.

Generally, electronic units made by this technique and using conventional components show little reduction in size. It is hoped, though, that with the efforts of the component designers taking advantage of this

* Pyc. I td.



new approach to manufacture, drastic reduction in equipment sizes will be achieved.

A description will now be given of the manufacturing methods used to produce a complete "dip-circuit" chassis. First of all the production of the chassis circuit board.

Bakelite faced with copper foil is supplied in 9-in wide strip. This is fed through a piercing and shearing tool which makes some of the larger holes and cuts the material into pieces the size of the chassis blank. Two of the holes made at this stage are for location during printing and during the subsequent major piercing operation.

An acid-resistant ink is next printed on to the copper face of the boards in the pattern of the circuit. The boards are placed, ready for etching, in special acid-proof racks as they leave the printing stage. The printing is done by the silk-screen method. This equipment is cheap and is suitable for work on Bakelite. Output at the rate of 150 circuit boards per hour is maintained with standard equipment, modified to enable the operator to raise the screen frame by a foot pedal. This has reduced fatigue and permits a less complex pattern of hand motions. The operator's hands are not required for lifting the screen frame and so are left free to handle the squeegee and the circuit boards.

Etching the Circuit

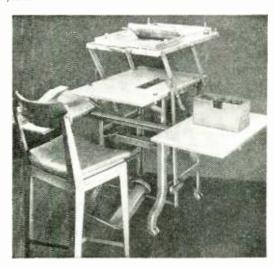
Etching is carried out in tanks containing a solution of nitric acid and copper nitrate. A constant balance is maintained between the acid solution and the weight of copper dissolved in it by calculating the quantity of acid required to etch one chassis and then adding a quantity of acid appropriate to the number of chassis being etched, plus a fixed percentage. The size of this fixed percentage determines the rate at which etching takes place. A 10 per cent excess of acid (which means, in effect, a 10 per cent wastage) gives an etching time of six minutes, using a solution 50 per cent by weight nitric acid in water. This acid wastage varies inversely with the etching time but prolonging the etching time beyond six minutes saves very little acid. Fresh acid is added at the top of the tank and the outflow is taken from the bottom. Turbulence created during etching ensures that the acid is well mixed.

Ferric chloride is sometimes used for etching purposes but we are using nitric acid because it has the following advantages. (a) Four hundred chassis can be etched in six minutes using very simple equipment; no mechanical agitation is needed. To achieve this rate with ferric chloride very expensive equipment is required. (b) Ferric chloride is awkward material to handle and requires heating, stirring and the addition of hydrochloric acid to bring it into solution, whereas nitric acid is readily diluted with the necessary water. Against this must be set the problem of fumes when using acid; this, however, has been solved by using standard extraction equipment. (c) Nitric acid is 30 per cent cheaper to use than ferric chloride.

After etching, the boards are rinsed in water, neutralized in a 2 per cent solution of ammonia and then rinsed again. It was decided to use ammonia in preference to sodium bicarbonate because ammonium salts are volatile, and if traces remain on the board they are dispersed during dip-soldering. Next, the circuits are pierced to take the component wires and the valveholder contacts. Finally, the circuits are



Preparation of the silk-screen master from the photographic plate.

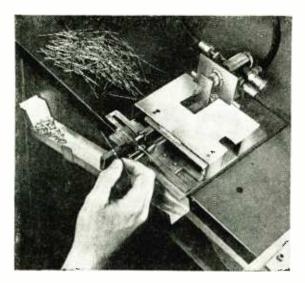


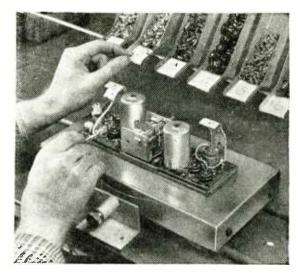
Silk-screen printing machine with foot-operated frame.

placed in a trichlorethylene degreaser to remove the resistant ink.

To make the maximum use of the labour-saving possibilities of "print-dip" technique, the wire ends of the resistors and capacitors are pre-formed suitably for direct insertion into the holes in the chassis. A machine to do this has been made which cuts and bends both wires of the component and which can be hand led at rates of 1,200 to 1,500 components per hour.

The machine is driven by a compressed air cylinder linked to an air valve in such a way that it operates automatically once the air is turned cn. It can be set to any speed to suit the operator and the position of the cutting and forming blades is continuously adjustable to leave any wire length that is desired. When they have been formed the components drop into a container. This container is one of the interchange-





Left: Wire cutting and forming machine for resistors. Right: Part of the assembly line for the 4-valve dip-soldered battery set whose underside is shown in the picture on page 536.

able component storage bins used on the assembly line.

Both the rigid layout imposed by the system and the mechanical pre-forming of the components have tended to standardize assembly operations. This improves assembly efficiency and leaves less to chance in positioning the components—it is virtually impossible to build a short circuit into a printed assembly.

Assembly Trolleys

The fact that only one side of the chassis has components on it has simplified assembly cradles and work on the chassis. Material layout has also been helped because the pre-formed components are more compact and require less bench space. The assembly cradle is a rubber wheeled trolley free to run in a channel on an ordinary wood-topped bench. A shallow rectangular frame is used to locate the chassis on top of the trolley. At each work station there is a spring loaded catch for retaining the trolley while it is being worked on. Trolleys from the end of the line are returned to the beginning on a sloping shelf at the back of the assembly bench.

Component storage bins are of the gravity-delivery type with a protruding lip at the bottom to facilitate the selection of material. The lip of the bin is clear of the bench so that, with the thumb under the lip and the forefinger on top, the resistor or capacitor can be drawn to the edge and held between the thumb and finger as it comes clear of the bin.

For dip-soldering a machine has been devised to do the job because, while it can be done quite simply by hand, the quality of the soldered joints is so important and the factors which can vary are so numerous that to obtain consistent results a mechanical method is necessary.

To use the machine the operator simply hooks the chassis on to a bracket and presses a button. The machine then moves the chassis to a flux spray position, then gives it two dips in the solder. During these dips, and for a short period after each one, the chassis is vibrated. This vibration helps to break down any oxide film on the circuit or on the components and also removes any excess of solder.

Finally, the machine ejects the completed chassis and returns it to the operator for inspection.

There are some benefits accruing from the introduction of "dip-circuits" whose value it is difficult to assess, but which may turn out to be important in the long run:—

1. Storage and material handling will be less for the smaller, non-insulated pre-formed components.

2. Training time will be cut down, as workers will no longer require skill in the use of pliers and soldering irons.

3. Testing, inspection and repair time will all be cut because of the reduction in wiring errors and the ease with which such errors that remain can be detected on the accessible layout that "dip-circuits" provide.

4. The quality of the finished product will be improved and more easily controlled. The rigid layout of the printed wiring assembly will impose a uniformity not obtainable with conventional assembly methods. This uniformity will, of course, mean better quality as closer adherence to the designed performance will be achieved. It must also be emphasized that the mechanization of the soldering operations will greatly improve the reliability of the units.

5. The servicing of a "dip-circuit" chassis will differ only slightly from that of a normal one. Faulty components can be cut away from the top side of the chassis, or, alternatively, the components can be removed by heating the soldered joints on the reverse side with a small-wattage iron and pulling out the components. As there is no mechanical wrapping of the component wires and no wiring mistakes are possible, servicing time will be reduced. In cases where, due to misuse, the printed wiring pattern has been broken, a wire replacement can easily be inserted or the gap can be closed by the use of a soldering iron.

There will be other changes that will be less welcome. For example, in the immediate future purchasing policy will be less flexible because the rigid circuit layout will not permit any change in the middle of a production run to components of a very different shape or size. Later on this may bring benefits by stimulating standardization among the products of different manufacturers.

Another consequence of adopting the printed layout will be an increase in the cost of circuit modifications after tooling. Alterations to the circuit pattern are quite a simple matter, but modifications to the chassis piercing tools are expensive. This does not mean that there need be serious delay in the introduction of modifications, because temporary expedients, such as the use of a drill jig, are available. However, it does mean that adequate pre-production planning will be at an even greater premium than it is at present.

Until a new process has been widely adopted there is usually a period when many firms are developing their own methods more or less in secret. This has certainly been the case with printed circuits. As a result, there has been no agreement yet in this country on standards of quality for the materials used, or on the dimensions and style of components for "dip-circuit" application. Unless the electronics industry, through its consultative bodies, soon agrees on the general direction that component development is to follow, the cost and quality of components is likely to suffer.

Automatic Component Insertion

With the advent of dip-soldering and printed wiring three-quarters of the possible saving on existing assembly times will have been achieved. If machinery were developed for the automatic insertion of components these times could be reduced by about a further one-tenth. This machinery would be highly specialized and would cost more to develop and install than would the equipment necessary for producing "dip-circuits." In view of this it is not likely that such equipment will repay development in this country, except in cases where production runs are very large or where part of an automatic component manufacturing process can be combined with the automatic insertion process.

A further argument against developing specialized machinery solely for component insertion is that the biggest scope for reducing the cost of electronic equipment lies with the component manufacturers. This may result in the development of components very different in shape and size from those commonly used at present. One such development, called "modular assembly" has already been tried in the U.S.A.* In this system small capacitors and resistors are printed on ceramic wafers and the wafers are assembled in

tiers supported by wires; the wires also provide electrical interconnection. This tiered assembly or "module" is surmounted by a valveholder. Several such assemblies go to make a complete circuit and they can be assembled in one unit on a printed wiring base. In the opinion of the authors it has not yet been proved whether such an arrangement is really economical or has a very wide application, but it

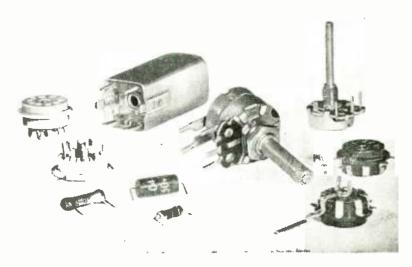
Components with electrical terminations made suitable for dip-soldering use.

* See Wireless World, April, 1954, p. 185

indicates the possibilities for a radically new approach to the problem of manufacturing electronic components.

Finally, there is the possibility of reducing the costs of component manufacture. In their essentials electronic units consist of four types of elements: capacitors, resistors, inductors and valves. With the possibility of transistors replacing valves there are left for consideration the first three types of elements. Reducing these in turn to their essentials, their costs are made up of: manufacturing labour, conductive and resistive material, some form of casing and terminals for assembly. Of these, the first offers scope for economy but the last two, performing no essential electronic function, are the main targets for material cost reduction. The largest labour savings will result from cheaper methods of producing inductors. In this field printed circuits will have an important part to play. The smaller inductors can be incorporated in the circuit pattern or printed on a separate circuit board which plugs into the base board. This method has been used commercially in the U.S.A. for the coils of a television i.f. strip. This strip was marketed as a separate unit, comprising three valves, five coils and the associated resistors and capacitors assembled on a printed wiring base. Larger inductors such as chokes, transformers and deflection coils need to be printed on a thinner, flexible base material and folded to make them into working units.

The elimination of non-essential material on resistors and capacitors can be achieved by the use of basic components without wires and with simpler insulation. To this end it is sometimes possible to include several electronic elements in one package. The printed circuit "couplet," which consists of a thin, flat, ceramic plate with multiple resistor and capacitor patterns silk-screen printed on one side, has done this and so also has "modular assembly." Multiple capacitor packs and transformers with several voltage tappings use this principle to a lesser extent. However, this trend towards multiple components conflicts with the standardization essential to economic mass production; it also increases the cost of rejects during manufacture. A more flexible system, making use of the physical configuration of either the "couplet" or the "module" but having standard or new-type hasic components inserted during the final production process, will perhaps prove to be the best answer.



Colour Camera Convertor

Adapting Frame-Sequential Pictures to Simultaneous Transmission System

HE frame-sequential system of colour television has been out of favour lately as a possible means of establishing a public colour service because of its non-compatibility—not to mention the difficulty of the rotating discs at the receivers. Despite this it is known to give very good colour pictures. Moreover, although the system as a whole may be unsuitable, there is a particular part of its equipment—the colour camera—which can offer some very definite advantages if incorporated in a simultaneous compatible system such as the one now operating in America.* This camera is much smaller and lighter than the three-tube type normally used and is simpler and less costly to produce. Having only one pick-up tube, it avoids the necessity for matching and registering the three separate tubes and also the need for three separate amplifiers. Moreover, it avoids the complex optical system which makes turret changes difficult and causes loss of light in the three-tube camera.

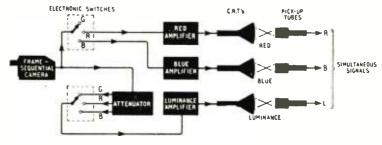
To permit the frame-sequential camera to be used in a simultaneous system a device called the "Chromacoder" has been produced. This operates on the

three colour-component signals from the camera—red, blue and green—in such a way that they appear not in sequence but simultaneously. The original Chromacoder" was designed in America by the Columbia Broadcasting System and the General Electric Company, but recently a new version of the device has been demonstrated in this country by Emitron Television, a subsidiary of Electric and Musical Industries.

The principle of the Emitron convertor (see block diagram) is to take the sequential red, blue and green signals from the camera and pass them to an electronic switching system which distributes the red signals to one c.r. tube, the blue signals to another and certain proportions of all three signals to a third tube. These three c.r. tubes are then viewed by three pick-up tubes whose outputs give the simultaneous signals. Although the effect on the screens of the c.r. tubes is still sequential, the pick-up tubes store the images on their mosaics until they are scanned off and consequently the outputs become truly simultaneous.

The convertor is arranged in this particular way to make it suitable for the N.T.S.C. type of transmission system, which sends out a luminance signal to provide a monochrome picture for existing black-and-white receivers and two colour-difference signals to provide colour information. In the convertor the luminance information (a mixture of all three colour components) is received in sequential form by the appropriate c.r. tube and the associated pick-up tube

One advantage of this scheme over the three-tube type of "simultaneous" camera is that the three colour components which are added to form the luminance signal all come from the same pick-up tube-the camera tube. They are therefore registered perfectly with each other and no loss of definition occurs through mis-registration. In the threetube carnera, however, the three components come from separate tubes and this difficulty of registration has to be overcome. It is, of course, particularly important for the luminance signal to have good definition because the human eye has great acuity for fine detail in the form of brightness changes, and it is the luminance information which really controls the sharpness of the final picture. On the other hand, the eye is not very sensitive to detail in colour, so that as the red and blue signals from the first two



pick-up tubes only provide colour information, not luminance, there is no need for these two tubes to be so accurately registered and give such good definition.

At the demonstration the frame-sequential camera was operating on 405 lines, interlaced 2:1, with 150 frames per second, and the bandwidth was 9 Mc/s. The three pick-up tubes, however, which were C.P.S. Emitrons, were scanned with 625 lines, interlaced 2:1, at 50 frames per second. No doubt the difference of standards helped to avoid the line-beating patterns which might have been caused by the interaction of two similar rasters, but E.M.I. say that there is no reason why two identical standards should not be used.

One inherent drawback of the convertor is that the storage in the pick-up tubes is liable to cause blurring of quickly-moving objects in the picture. This was particularly noticeable at the demonstration when the camera was panning from one subject to another. The colour rendering, however, was very pleasing on all the display systems used, which included an R.C.A. tri-colour tube and a three-tube projection unit.

integrates it into a complete luminance signal simultaneous with the colour signals. (The green component is recovered later at the receiver by subtracting the red and blue signals from the luminance signal.)

^{*} See Wireless World, November, 1953, p. 524.

Cathode-Follower Probo

For Test and Measurement

By SYDNEY H. FINN

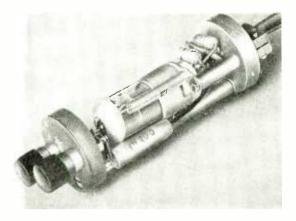
IT is usually required of an electronic measuring device that its input impedance be high, but the value to which an amplifying-valve grid resistor may be raised is limited, particularly so if potentiometer attenuation is used. Some improvement on a continuously variable input potentiometer is possible by fitting a switch and equalizing each position independently. If a high value of resistance is used then a screening cover will probably be required to reduce hum pick-up. For some purposes the clicking of a switch would be a disadvantage.

In quite a number of instances it is possible, by fitting a probe housing a cathode-follower valve, to more or less completely solve the problem. attenuator in the main instrument may then be of some conveniently low value, whilst the input impedance to the probe will be very high. By using a probe extremely short leads to the measuring point are possible, although the cable-form to the main

instrument can be relatively long.

One such practical arrangement is shown in the circuit diagram and picture. As for some purposes it may be required to use a valve with a high cathode current the load resistor R_L is fitted to the socket on the main instrument, thereby avoiding undue heating of the probe. It also allows some flexibility, in that the same value of load resistance may not be desired for every instrument to which the probe is attached. The six-way socket is so wired that this resistor does not shunt the input circuit after removal of the probe. The cathode follower anode, being at earth potential (to a.c.), acts as a screen around the grid and there is normally no need to use a screened probe. In any case, the outside of the probe should be insulated, otherwise it may be a nuisance when working inside apparatus (particularly if using very short connecting leads) and one wishes to lay the probe down inside the chassis.

The mechanical arrangement is not necessarily the best that could be devised, but is very simple if a lathe is available. The base is made of an aluminium alloy, the outer sleeve of Paxolin tube, and the terminal plate of loaded ebonite (Caramot RM70). A cable clamp is an essential if the probe is to be much used



Construction of the probe with the Paxolin-tube cover removed.

and would ideally be formed as part of the base. Actually it was modified from an already-existing device. A very simple type of clamp can be made using a short piece of angle with one end flanged. This is screwed to the base (by means of the flanges) so that the cable lies inside the included angle. Twine is then bound tightly round the whole, preferably within grooves filed on the edges of the angle. These grooves prevent any subsequent movement of the binding.

Choice of Valve

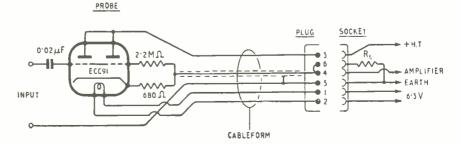
The particular valve fitted was used only because it was to hand and was adequate for the job. A triodeconnected pentode of the Z77-EF91 type would do just as well. If for some reason a valve with a higher cathode current is required, the Osram N78 has a B7G base and a maximum anode dissipation (triode connected) of 12 watts. As screening will, in general, be unnecessary, ventilation can be provided without compromising the design electrically. The valve retainer is a Carr Fastener type 77/264.

Instruments designed to have an input impedance high in relation to, say, 600-12 lines, are commonly found in the laboratory. This input impedance, which may be around 100kQ, will often be the limiting factor in an otherwise first-class instrument. fitting of a probe may greatly increase its scope, and perhaps even save the cost of a new instrument, if for any reason higher impedance networks must be dealt with. The author has found this probe a very useful instrument to use in conjunction with a c.r. oscillo-

If absolute measurements are required an initial calibration will have to be carried out, as the voltage

output is somewhat less than the input.

Circuit of the probe with plug and socket connections. load resistor $R_{\rm L}$ is $22k\Omega$ nominal. For the plug and socket, Painton types 500693 and 500680 were used.



Miniature Bedside

Two-Valve A.C. Mains Circuit With Pre-set Tuning

HIS article describes a receiver recently built by the author for bedside use by a child. It is a very simple a.c. mains-operated receiver employing two valves and giving approximately 1 watt output from a 5-inch diameter loudspeaker. Tuning is pre-set, the local Home Service or Light Programme being selected by a 2-way switch. The receiver is relatively inexpensive to build and all the components, including the tuning coil, are standard commercial products which are readily obtainable. Where local-station reception is all that is required and great volume is unnecessary, the receiver is suitable for general domestic use.

As the receiver was intended for a child, consideration was first given to the use of batteries, but battery-replacement cost can be serious when a receiver is used in this way and mains operation was decided in spite of the additional bulk and first cost of mains transformer, rectifier and smoothing components. An earthed chassis was considered essential and a mains h.t. transformer is used although receivers with a filament transformer or an l.t. dropping resistor are smaller and cheaper. As the receiver is mains-operated it does not greatly matter if it is accidentally left on, but if this occurs the indicator lamp at the front serves as a reminder.

Great volume is not required from such a receiver and 1 watt output is quite adequate. This can be obtained from a miniature valve of the 6AM6 type for approximately 1 volt input, and two valves of this type give all the gain necessary for local-station reception. A second 6AM6 is therefore used as a leaky-grid detector, the two valves being coupled by a "starvation" circuit as shown in Fig. 1. This particular form of coupling has been described elsewhere 1.2 and is adopted because it is economical of

¹ W. K. Volkers, "Direct-coupled Amplifier Starvation Circuits," Electromics, March, 1951.

¹ H. E. Styles, "Sensitive Two-valve Receiver," Wireless World. May, 1953.

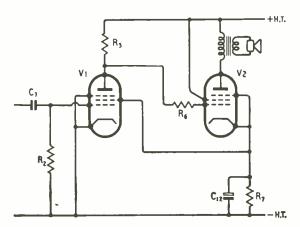


Fig. 1. Basic circuit of the receiver illustrating the starvation technique adopted.

components and gives high gain. It is not desirable, however, to carry the process of starvation too far, otherwise the receiver does not function very well on strong signals. V1 is a leaky-grid detector and, on receipt of signals, generates a negative bias on the control grid approximately equal to the carrier amplitude. If the valve has a very low screen-grid potential, the bias produced by a strong signal may cause the valve to operate on a markedly non-linear part of the I_a-V_a characteristic producing unpleasant harmonic distortion. To minimize this effect the screen-grid potential must be kept high to give V1 an adequate grid base; this sets an upper limit on the value of anode load which can be used and prevents full exploitation of the starvation circuit. In the compromise solution adopted by the author, the screen grid is operated at 40 volts and results are satisfactory provided that the input signals are reasonably small. If a long outdoor aerial is used, or in regions of particularly high field strength, it may be desirable to reduce the input to the detector. A convenient way of doing this is described later.

The required screen-grid potential of 40 volts is obtained in the following way. This potential is also that of the cathode of V2 and, for optimum results, V2 should consume approximately 12 mA. This gives the value of R_3 as $40/(12 \times 10^{-3}) = 3.3 \, k\Omega$. The value of R_3 is now chosen to give a screen-grid potential of 40 volts. The value used by the author was 820 k Ω but others may find a slightly different value is required, dependent on the characteristics of the particular valve used as detector.

Gain Control

One of the difficulties of a circuit such as that shown in Fig. 1 is that of controlling gain. It is not possible to use a potentiometer in the coupling between the valves without upsetting operation of the starvation

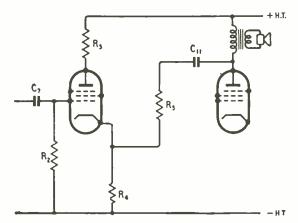


Fig. 2. Method of applying negative feedback without risk of instability.

Receiver

By S. W. AMOS,* B.Sc. (Hons.) A.M.I.E.E.

circuit. Practically the only form of gain control which can be used is one employing variable negative feedback. Such a method of gain control has the advantage that any gain in excess of that required at any moment is not "thrown away" in an attenuator, but is usefully employed in reducing distortion and improving loudspeaker damping.

Feedback gain controls usually have a number of disadvantages; for example their range is often inadequate, because the maximum degree of feedback is limited to a value which does not cause instability, and output volume cannot be reduced to zero. The circuit used in this receiver is free from these limitations; it was developed from the circuit shown in Fig. 2 in which a feedback potentiometer R₄R₅ is connected between the anode of V2 and the cathode of V1. This arrangement permits a very large degree of negative feedback without instability; in fact R₅ can be reduced to zero without provoking oscillation.

To give control of gain either R₅ or R₅ can be made variable. If R, is variable, it must have an inverse logarithmic law to give smooth control of volume; on the other hand if R₅ is variable this must have a logarithmic law to give smooth gain control. Accordingly R₅ is made variable and the circuit takes the form shown in Fig. 3. A further advantage of making R₅ variable is that, at the position of minimum gain, it effectively short-circuits the primary winding of the output transformer to give zero output from the receiver. However, the shunting effect of R₅ on the primary winding is undesirable at settings of R_s other than near the minimum. This can be minimized by choosing the values of R₄ and R₅ in the following way. For reception of a reasonably strong signal the a.f. gain of the receiver averages approximately 1000. For such values of gain, the gain is determined by the constants of the feedback loop and is given approximately by R₅ R₄. To keep the a.f. loss in R₅ reasonably

^{*} B.B.C. Engineering Training Department.

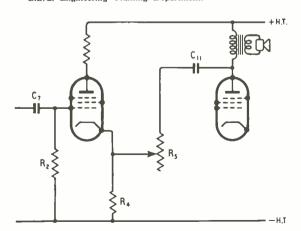
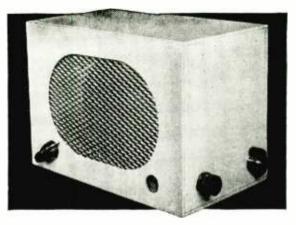


Fig. 3. First stage in the development of the feedback gain control.



Translucent Perspex sheet was used for making the cabinet.

low, R_s should preferably not be less than $100~k\Omega$ (5 times the effective loudspeaker impedance at the primary winding). This gives the minimum value of R_s as $100~\Omega$ and a value of $140~\Omega$ is used.

Maximum Gain

There now arises another difficulty. To obtain maximum gain from the receiver there should be no feedback when R_5 is set to its maximum value. This requires that the ratio of R_5 to R_4 should be large compared with the internal gain of the circuit (i.e., the gain in the absence of feedback). The internal gain is approximately 60,000 (150 from V2 and 400 from V1) and thus R_5/R_4 should preferably not be less than say, 300,000. Since R_4 is 140 Ω , R_5 must be 42 M Ω ! There is, however, no need for such a large value if the "free" end of R_5 is returned to h.t. negative as shown in Fig. 4. When R_5 is advanced to its maximum setting it now short-circuits R_4 thus removing feedback and giving maximum gain. R_5 can be a standard logarithmic volume control of 1 M Ω .

Finally the value of C_{11} must be determined. This must be fairly large because R_5 may be $10 \text{ k}\Omega$ or less at low volume settings and, if the reactance of C_{11} is comparable with this at low audio frequencies, an

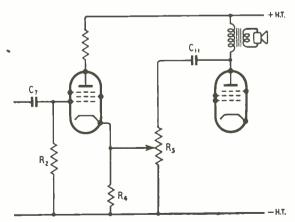


Fig. 4. Final circuit diagram of the feedback gain control giving maximum volume range.

accentuation of the lower audio frequencies results. To restrict any bass lift to less than 1 db at 50 c/s when R_5 is 10 k Ω , C_{11} must be greater than 0.6 μF and a miniature 4- μF electrolytic capacitor is used.

To keep the receiver simple it was decided to use only a single LC circuit for tuning. Such a simple tuning arrangement is, of course, incapable of giving good reception of weak signals when there are strong ones on the same waveband but, with the aid of reaction, it has proved capable of separating the two medium-wave signals in the London area without pressing reaction to the point of oscillation. For ease of operation it was decided to employ pre-set tuning, the Home or Light programmes being selected by a 2-way switch. This decision simplified the problem of coupling the aerial to the tuning circuit, for it is possible to connect the aerial to the "hot" end of the LC circuit via a fixed capacitor as shown in Fig. 5. Such simple coupling can be very effective in a circuit operating at fixed frequency but is unsatisfactory in

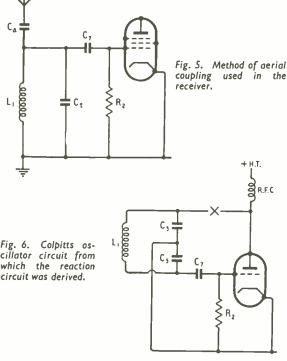


Fig. 7. Form of reaction circuit developed from the Colpitts oscillator circuit of Fig. 6.

receivers with variable tuning because gain and selectivity are greatly dependent on frequency and vary considerably over the band.

As shown in the appendix, the gain of an aerial coupling circuit of this type is given approximately by C_aQ/C_t where C_a is the coupling capacitance, by $C_a \cup C_t$ where C_a is the tophing capacitance, C_t is the tuning capacitance and Q is the reactance/resistance ratio of the inductor L_1 . Thus if C_a is an appreciable fraction of C_t , the gain is an appreciable fraction of C_t . For example if $C_a = 50$ pF and $C_t = 200$ pF a gain equal to Q/4 is available. This is hardly a practical condition, however, for if C_a is 50 pF, the effective purpose repositions is greatly effected by the effective tuning capacitance is greatly affected by variations in aerial capacitance. Thus the calibration of the receiver tuning control is dependent upon the aerial constants and varies from aerial to aerial. It is particularly desirable that the tuning of the receiver should be substantially unaffected by changes in aerial constants, because adjustment of tuning is not so convenient as in a receiver without pre-set This condition can be achieved by making C_a small compared with the capacitance of the aerial itself; a value such as 10 pF is suitable. To achieve high gain with $C_a = 10 \text{ pF}$, C_t must also be small, say 30 or 40 pF. To tune the Home Service (1088 kc/s in the Midland area, for which this receiver was destined) with such a small capacitance necessitates an inductor of approximately 700 µH. Such a value was accordingly used. It enables the whole of the medium waveband to be covered with a capacitor of 120 pF maximum capacitance, and also has the advantage that the long-wave Light Programme (200 kc/s) can be tuned with a capacitor of 1000 pF.

Thus the medium-wave Home Service and the long-wave Light Programme are both tuned using the same inductor by simple selection of capacitors. The coil used (Osmor QIFI) is a standard component used in a 465 kc/s i.f. wavetrap and gives an inductance range of 500 to 800 μ H by adjustment of the iron core. This inductance adjustment is used for tuning long waves (the 1000-pF capacitor being fixed) and the Home Service is tuned with an adjustable trimmer of 70 pF maximum capacitance. Since C_t is 1000 pF on long waves C_a should be approximately 200 pF to maintain the same gain as on medium waves. This is of the order of the capacitance of an aerial and thus no physical capacitance is necessary for longwave coupling, the aerial being connected directly to the top of the coil. Variations in aerial capacitance are unlikely to affect the long-wave calibration because they will in general be small compared with the

1000-pF tuning capacitance.

Reaction Circuit

Reaction is usually obtained by use of an additional inductor closely coupled to the tuning inductor, but such a circuit is not suitable for use in this receiver because it requires a coil assembly which would need to be specially wound. It was decided therefore to use a reaction circuit which can be applied to a single untapped inductor such as that chosen for tuning purposes. The circuit adopted is derived from that of the Colpitts oscillator shown in its usual form in Fig. 6. A significant feature of this circuit is that oscillation is most vigorous when C_3 is equal to C_5 , the effective tuning capacitance being then $C_3/2$. The amplitude of oscillation can be controlled by a variable capacitor C_8 introduced at the point X and if this capacitance is reduced below a certain value, oscillation ceases,

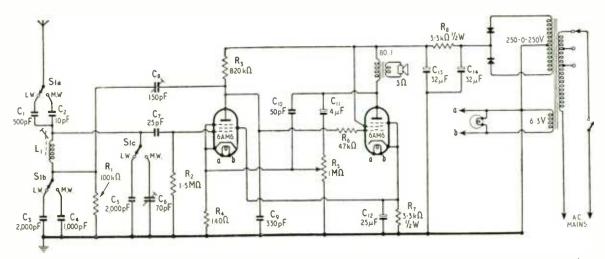


Fig. 8. Complete circuit diagram of the receiver for reception of one medium-wave and one long-wave signal. All resistors can be $\frac{1}{4}$ W unless otherwise specified.

the circuit then resembling that of a detector in which C_8 acts as a reaction control. This is precisely the circuit used for long-wave reception although in the complete circuit diagram it is drawn in the form shown in Fig. 7. C_3 and C_5 are both 2000 pF, giving the required effective tuning capacitance of 1000 pF. A maximum value of 150 pF is adequate for C_8 and adjustment of its value has no significant effect on runing. The fact that C_3 and C_5 are both equal implies that only one half the signal developed across L_1 is applied to the detector.

As shown in the complete circuit diagram (Fig. 8), for medium-wave reception C₅ (2000 pF) is replaced by C₆ (70 pF maximum) and C₃ (2000 pF) by C₄ (1000 pF). If C4 and C6 were made equal C8 would need to be very much smaller to control reaction on medium waves than on long waves. In a pre-tuned receiver it is desirable that the reaction control should not require readjustment after each operation of the station-selector switch. The value of C, is chosen to satisfy this condition as far as possible but the capacitance of C₈ required to give oscillation on medium waves increases as C6 is decreased; this differs from the behaviour of the more usual reaction circuits. The large ratio of C4 to C6 ensures that nearly all the signal developed across L₁ is applied to the detector and it also enables the whole of the medium waveband to be covered by variation of C₆ alone. To cover the whole of the band C6 should be 120 pF maximum; a value of 70 pF was used by the author to tune in the Midland Home Service. Medium-wave

TABLE

Maximum wavelength in metres	Minimum frequency in kc/s	Maximum capaci tance of trimmer required in pF
250	1200	25
300	1000	35
350	857	50
400	750	65
450	667	80
500	600	100
550	545	120

These va'ues are based on an inductance of 700 µH

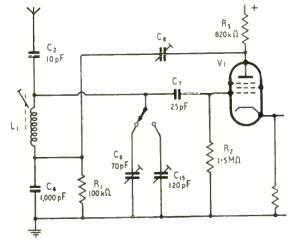


Fig. 9. Input circuit suitable for reception of two mediumwave stations.

tuning is substantially unaffected by operation of the reaction control.

A third section of the station-selector switch connects a 10-pF capacitor (C2) in the aerial lead for medium-wave reception. If long-wave reception is not required there is no need for the 2000-pF capacitors or to change the series aerial capacitance and C4 can be retained for both stations as shown in Fig. 9. As suggested in this circuit C₆ could be, say, 70 pF for a station near the high-frequency end of the band and C₁₅ could be 120 pF maximum for a station at the other end. If the receiver is pre-tuned to two medium-wave signals of widely different frequencies, say one near 600 kc/s and the other near 1.5 Mc,s it may be desirable to have different values of C4 for the two signals to give approximately the same degree of regeneration on both. A value of C, of 2000 pF is suitable for 600 kc/s and 500 pF for 1.5 Mc/s, a value of 1000 pF being suitable for 1 Mc/s as shown in Fig. 8. Approximate values of C6 necessary for various frequencies are given in the table.

R₁ and C₁ are included in the circuit to provide some attenuation to 50-c/s signals from the aerial.

Without R_1 the tuning inductor has a high impedance to earth at 50 c s and on long waves, when the aerial is in direct contact with L_1 , 50 c/s signals can be of sufficient amplitude to modulate a received signal. This trouble is not present to any extent on medium waves because of the very high reactance at 50 c/s of the series capacitor C_2 .

As mentioned earlier, in certain circumstances, results from a particular transmission may be unsatisfactory due to overloading of the detector. If this occurs the input can be reduced by decreasing the appropriate series input capacitor $(C_1 \text{ or } C_2)$.

In receivers with pre-set tuning it is advantageous to have equal volume from all stations; the stationselector switch can then be operated without necessity

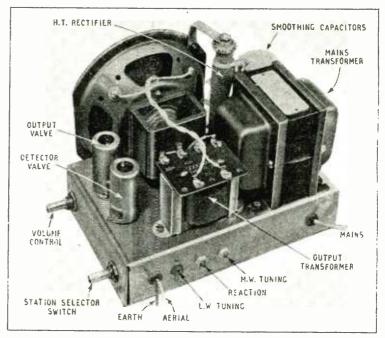
for subsequent volume readjustment. This can be achieved in this circuit by correct choice of values for C₁ and C₂. If both transmissions give good signals, one being stronger than the other, the capacitor corresponding to the stronger of the two signals can be decreased until the volume obtained is equal to that from the other signal.

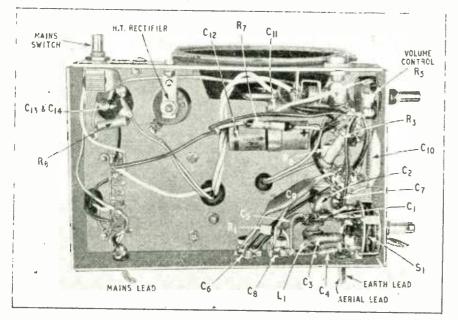
The only other points of note in the circuit are the capacitors C_9 and C_{10} which are for r.f. decoupling and the resistor R_6 which also provides some r.f. attenuation with the input capacitance of V2 but which is primarily intended as a grid stopper

A full-wave selenium rectifier is used to supply h.t. and the smoothing circuit $R_{\star}C_{13}C_{11}$ supplies 280 volts at 12 mA. Approximately 40 volts are lost across R_{τ} and the effective h.t. supply for V2 is thus 240 volts.

The construction of the receiver is illustrated in the accompanying photographs. The four-sided chassis measures 7 inches by 4½ inches by 1½ inches and much of it is occupied

by the mains transformer which is rated at 250-0-250 volts 60 mA and has a single 6.3-volt l.t. winding. This is an unnecessarily generous rating for such a small receiver but this type of transformer (Electro-Voice Type 104E) is used because it is fairly small and readily obtainable. The selenium rectifier is a 250-volt 60-mA bridge type, a government surplus component type 280 LU997AW used here as a push-pull rectifier after removing the link joining the outermost tags. The current rating is again unnecessarily high and any push-pull rectifier rated for 250 volts and capable of supplying 12 mA will be satisfactory. The output transformer is a Goodmans Type 74/243. The station-selector switch and volume control are mounted on one end wall of the chassis, the on-off switch and





Plan view of chassis is shown above. The mains transformer is somewhat larger than it need be. On the left is the underside of chassis showing positions of most resistors and capacitors.

indicator lamp on the front, runing and reaction controls being on the rear flange.

In setting up the receiver it is necessary to tune in the long-wave programme first, by adjustment of L₁, and the medium-wave programme afterwards by adjustment of C_6 . If possible the 6AM6 used for detection should be specially selected because some valves of this type tend to be microphonic and can set up continuous oscillation by acoustic feedback from the loudspeaker.

The cabinet illustrated was home-made of Perspex, and the internal dimensions are $8\frac{1}{2}$ in \times 6 in \times 5 in. The length of the chassis is thus $1\frac{1}{2}$ inches less than the corresponding dimension of the cabinet, this margin being necessary when the chassis is inserted in the cabinet to enable the controls on the end wall of the chassis to be fitted into the corresponding holes in the cabinet.

APPENDIX

The essential features of the aerial-coupling circuit are shown in Fig. 10 in which r and c represent the resistance and capacitance respectively of the aerialearth system. Values of r and c commonly used in medium-wave dummy aerials are 40 ohms and 200 pF. C_a is the coupling capacitor and r_L is the r.f. resistance of the inductor L₁.

Maximum voltage is developed across C, at the frequency at which the net inductance of L1, Ct and $r_{\rm L}$ resonates with the net capacitance C of c and

 C_a in series.

The impedance Z of the network L_1 , C_t and r_L

is given by

$$\begin{split} \mathbf{Z} &= \frac{(j\omega\mathbf{L}_1 + r_{\mathrm{L}})/j\omega\mathbf{C}_t}{j\omega\mathbf{L}_1 + r_{\mathrm{L}} + 1/j\omega\mathbf{C}_t} \\ &= & \frac{j\omega\mathbf{L}_1 + r_{\mathrm{L}}}{1 + j\omega\mathbf{C}_t r_{\mathrm{L}} - \omega^2\mathbf{L}_1\mathbf{C}_t} \end{split}$$

By rationalizing this expression we can show that the network is equivalent to a series circuit of inductance given by

$$R = \frac{r_L}{(1 - \omega^2 L_1 C_t)^2} \dots \dots (2)$$

Since the inductance (1) resonates with the capacitance C we have

$$\frac{1}{\omega C} = \frac{\omega L_1}{1 - \omega^2 L_1 C_t}$$

from which

$$1 - \omega^2 L_1 C_t = \omega^2 C L_1$$

Substituting for $(1 - \omega^2 L_1 C_t)$ in (2)

$$R = \frac{r_L}{\omega^4 C^2 L_1^2}$$

Thus the circuit is equivalent to the simple series network shown in Fig. 11. The voltage gain of this circuit is equal to the quotient of the reactance (of the inductance or the capacitance) and the resistance,

$$Gain = \frac{1/\omega C}{r + r_L/\omega^4 C^2 L_1^2}$$

If practical values are substituted for the symbols in this expression it is found that r is normally small Fig. 10. Aerial-coupling circuit with aerial re- | placed by equivalent | ⊨ C. generator.

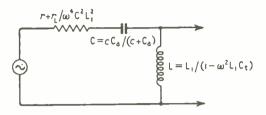


Fig. 11. Simple series circuit equivalent to the network of the previous figure.

in comparison with the other term in the denominator. If r is neglected the gain is given approximately by

$$Gain = \frac{\omega^3 C L_1^2}{r_L}$$

Now r_L is given by $\omega L_1/Q$ and substituting for r_L we have

$$Gain = \omega^2 CL_1 Q$$

which shows that the gain is proportional to the square of the frequency. It thus varies in the ratio 9:1 over the medium waveband.

 C_a is made small compared with c in order to make the calibration of the receiver substantially independent of variations in c. For such values of C_a the frequency of maximum gain is approximately the resonance frequency of L_1 and C_t . Thus $\omega^2 L_1$ may be replaced by $1/C_t$ and we have

$$Gain = \frac{CQ}{C_t}$$

If Ca is small C is approximately equal to Ca. Hence

$$Gain = \frac{C_a Q}{C_t}$$

which is the result used in the text.

"DECADE COUNTER"

Correction

An error unfortunately appeared in this article in the May issue. In Fig. 2 the second feedback path should go from the anode of V2 in the fourth stage to the grid of V1 in the third stage. Then, in the right-hand column of page 235 the section beginning 20 lines from the top, "This time, a negative pulse..." should be deleted to the end of the paragraph and be replaced by the following: "The third stage remains in this condition (the original state) for only a fraction of a microsecond because this transition causes a reversal of itself. The negative transient produced when the third stage is triggered by the second stage switches stage four through a half-cycle of its operational cycle. A positive pulse is thereby returned to point "C" of the third stage, re-triggering it extremely quickly. So brief was the excursion of the third stage to its original state that insufficient pulse energy is delivered to the second stage via the feedback path to cause any disturbance."

Recording Low Frequencies on Magnetic Tape By D. W. THOMASSON, A.M.Beit., L.R.E.,

The Application of Pulse Code Techniques

OT many years ago it used to be said that the upper frequency limit of a tape recording system was approximately one kilocycle per inch of tape speed. Today, with responses sensibly flat to 15 kc/s at a speed of 7½ inches per second, this is no longer true. There has been no comparable development at the other end of the frequency range, however, the "hum barrier" at 50 c/s still setting a limit to low frequency response in most cases.

The difficulty arises from the small output given by the playback head at low frequencies, typical figures being 200 µV at 50 c/s and 100 µV at 25 c/s. Since 1.5 µV effective input hum represents good performance in an amplifier with an a.c. heater supply, the signal/hum ratio cannot exceed 40 db, and even when a d.c. heater supply is used hum pick-up imposes a serious limitation. At lower frequencies the problem of obtaining high gain without instability sets the ultimate limit.

For recording the very low frequencies involved in some types of scientific and industrial measurement, a pulse code method can be used. Two systems are employed in apparatus introduced by Messrs. Rudman, Darlington (Electronics), Ltd., Clyde Works, Lichfield Road, Wednesfield, Wolverhampton, Staffs., one covering the 0-150 c/s range with manual setting of the d.c. level (tape speed 34 inches per second) and

the other covering the 0-250 c/s range with fully automatic d.c. maintenance (tape speed $7\frac{1}{2}$ inches per second).

The first method uses pulse interval modulation, Fig. 1 (a). The pulses are of uniform length and amplitude, varying only in their separation, and they are converted by a charging circuit into triangular pulses having a mean level that follows the modulation. The coding frequency component is filtered out, leaving the original input signal.

It will be appreciated that, while the system is unaffected by a reasonable degree of hum and noise superimposed on the code signal, any variation in tape speed alters the d.c. level at the output, and provision is therefore made to balance out any spurious d.c. component by manual adjustment. A very good performance in respect of wow and flutter is essential and the tape drive used has a maximum variation of only 0.2 per cent at 3½ inches per second, giving a negligible disturbance of the output signal. A second recording channel on the same tape deals with higher frequencies up to 6 kc/s using orthodox techniques.

While this method of coding allows maximum tape economy, it was recognized that there is a need for a system in which the d.c. component is maintained without manual adjustment, and the second method meets this need. In this case all low-

frequency stages are of balanced d.c.coupled form, allowing a higher input sensitivity, and the coded signal conveys two information channels, each represented by a set of time intervals, Fig. 1 (b). With zero input voltage all the time intervals are equal and the twin decoders pass equal voltages to the balanced output. With any other input voltage level one interval is increased, the next decreased, and so on, the decoder signals becoming unequal by a corresponding amount. The output is proportional to the difference in the two time intervals divided by their sum, and since all the intervals change in (Continued on page 549)



Twin-cnannel pulse coded strain gauge magnetic recorder, for use in aircraft.

Right: Fig. 1. (a) Simple pulse time system (b) push-pull system giving modulation amplitude independent of tape speed.

(a)

the same proportion when the tape speed is altered the recording can be played back at any speed without

altering the output voltage levels.

The more complex waveform of the coded signal makes heavier demands on the actual recording process and it is interesting to note that the success of the system largely depends on the improvement in high frequency response which has already been mentioned.

Both methods are of especial interest in strain gauge and vibration testing, but can be applied in many fields where pen recorders are usually employed. Recordings can now be inspected and selected before transfer to paper and the time scale can be changed

by alteration of the tape speed if it is necessary to ease the demands made on pen recorder performance.

Another interesting application arises in connection with the flight testing of aircraft. The equipment illustrated is used for flight testing jet engines, and is designed to minimize the effect of the aircraft's movements. If the recorder cannot be mounted in the aircraft the second coding system can be used to provide a telemetering system that is unaffected by the signal fading which is inevitable over air-toground paths. The technique is likely to be of even greater interest soon, as current development work is aimed at recorders giving four or eight independent channels on a single tape.

LEIPZIG FAIR

Impressions of Eastern European Radio Products

By V. A. SHERIDAN, A.M.I.E.E.*

OMMENCING with the ordinary domestic radio receivers, these were being exhibited in profusion by most East European countries. In appearance and performance they are not unlike ours. Radio-gramophones, however, were few and far between and certainly had no automatic record changers. Generally, all receivers are of the table type, housed always in wooden cabinets.

Of television receivers, I only saw the East German product being demonstrated. The sets are of the table type and arc fitted with an approximately 8-inch tube The brightness is very poor and the picture can only be viewed in complete darkness. Also there is a distinct flicker present obviously due to insufficient persistence of the screen material. The definition is good, as would be expected from the 625-line system. The only other exhibitors of television receivers were the U.S.S.R. who are showing 9-inch table models. These sets were not being demonstrated.

The German radio receivers are priced between 300 and 400 marks. It is difficult to translate this into our currency as the official rate of exchange is 6.20 marks to the pound. I think the West German rate of 12 marks to the pound does give a fair comparison in relation to the people's income. Television sets are priced at 1,300 marks. Needless to say, the popular demand for these sets is negligible.

The valves are much of the same design as ours; that is the all-glass construction with bases similar to our B7G and B9A. The main difference is that the contact wires are fitted with shaped sleeves soldered on to the wires. This results in a rather more positive grip in the valve holder itself and dispenses with valve retainers. Specialized valves such as magnetrons and klystrons, etc., were also exhibited. Crystal diodes and transistors were conspicuous by their absence.

Cathode-ray tubes displayed were of the all-glass design as well as the metal-glass construction. A wide range of oscilloscope tubes of the single and doublebeam variety were exhibited.

In the component field a very wide range was shown. The makes known before the war are being produced under new names, as practically all firms * British Physical Laboratories.

have been nationalized, and are called People's Owned Works.

The general range and design is much the same as ours. However, nearly all paper capacitors employ the metallized paper process. resulting in very neat and small units. Carbon resistors are all of Grade I type and are made from 1/20th watt to 2 watts. I have brought back some samples and find they are equal to the best British ones whilst their price is about 1/5th of what we pay here. Furthermore, they supply a precision-type high stability resistor with 0.5 per cent limits. For high resistance values they have a so-called "colloidal" type. I was assured by the chief research engineer of one of the firms concerned that they do not employ a colloidal graphite coating. The standard values are up to 1010 ohms, whilst small quantities can be supplied up to 1012 ohms. They claim that a maximum voltage of 1,000 volts d.c. can be applied. The resistors are contained in evacuated glass envelopes.

A wide range of rotary switches are available. The makers of one type claim a maximum contact resistance of 20 milliohms. I confirmed this value on a sample. However, by applying a contact oil the value dropped to 5 milliohms. This value was maintained after 3,000 operations.

Components which employ much metal are not

of the standard which we are accustomed to. This is due to the acute shortage of all raw materials in Eastern Germany. For instance, brass will be used instead of copper wherever possible, in order to save the copper. It must be borne in mind that the whole economy is working under typical wartime conditions

throughout.

Regarding instrumentation, not only did the East Germans show a wide range, but also the Russians, the Czechs and the Hungarians. The equipments cover the entire range from indicating instruments up to equipment for the measurement of centimetre waves.

The general appearance and finish of the East German instruments is very good. In particular they have developed excellent designs of dials, resulting in a very clear indication. The dial rotates according to the multiplier setting, permitting up to eight ranges, thus completely eliminating reading errors.

Some Electrical Theorems

Their Practical Utility

By W. TUSTING

EXTBOOKS of the more mathematical kind abound in theorems having more or less high-sounding names. The ordinary man is apt to pass over such matters as being difficult and of little practical value. In this, however, he is quite wrong, for some of them are not at all hard to understand or to remember and they are of considerable utility. Apart altogether from their mathematical applications they sometimes help considerably to an understanding of circuits.

Thévenin's Theorem

One of the best-known of such theorems is the one commonly known as Thévenin's theorem. This states that any linear network, no matter how complex, containing any number of sources of e.m.f. is, when regarded from any pair of terminals, equivalent to an impedance in series with an e.m.f.; the impedance is that measured between those terminals with all internal sources of e.m.f. short-circuited and the e.m f. is the open-circuit voltage at those terminals.

This sounds very difficult, but a few simple examples will make it clear. Suppose the network comprises a potential divider R_1 and R_2 connected to a battery E as shown in Fig. 1. The impedance measured between the terminals with E short-circuited (if one were making a real measurement instead of an imaginary one, one would naturally remove the battery and short-circuit the terminals to which it had been connected, just to avoid destroying the battery!) is clearly R_1 and R_2 in parallel. Call it

$$R = \frac{R_1 R_2}{R_1 + R_2}$$

The voltage measured across the terminals on opencircuit (that is, with no current-consuming device connected to them) is plainly

$$V = E \frac{R_2}{R_1 + R_2}$$

The equivalent circuit is thus Fig. 2(b) and it is in every respect identical in performance with the more complex original (a).

A numerical example may help here. Suppose E is 250 V, the h.t. line of a receiver, and R_1 and R_2 form a potential divider to provide a lower voltage supply; suppose R_1 is $100 \, k\, \Omega$ and R_2 is $25 \, k\, \Omega$. Then $V = 250 \times 25/125 = 50 \, V$, and $R = 100 \times 25/125 = 20 \, k\, \Omega$. The supply obtained in this way is exactly the same as one obtained from a 50-V source through a $20-k\, \Omega$ resistor.

The theorem holds for a.c. as well as d.c., but the voltage may then become frequency dependent. Consider Fig. 2(a) in which a resistor R and a capacitor C are connected to an a.c. generator e. Applying

Thévenin's theorem gives (b) the internal impedance being R and C in parallel. The generator voltage is

$$v = e \frac{1/j\omega C}{R + 1/j\omega C}$$

and this varies in magnitude and phase with the

frequency.

The theorem is quite valid under this condition but is less useful. In this particular example there is really no point in using the theorem at all, for it tends to complicate matters rather than to simplify them. However, with a circuit like Fig. 3(a) its use is very helpful if it is applied discriminatingly.

The thing to do here is to disregard C for the time being. Then apply the theorem to e and the resistors only. This bit of the circuit is the same as Fig. 1(a) and has the equivalent of Fig. 1(b). We now put back

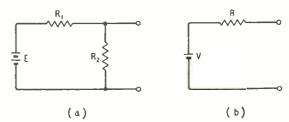


Fig. 1. Simble potential divider and battery (a) and its Thévenin equivalent (b).

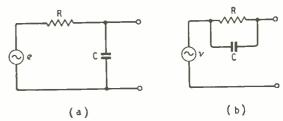


Fig. 2. An a.c. generator with an RC circuit (a) can be transformed to (b) but in this case there is rarely much advantage in doing sa.

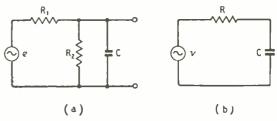


Fig. 3. An RC circuit of form (a) can be advantageously transformed to (b).

the capacitor and get Fig. 2(a) and draw it again as Fig. 3(b) where

$$v = e \; rac{R_{2}}{R_{1} + R_{2}} \; ext{and} \; R = \; rac{R_{1}R_{2}}{R_{1} + R_{2}}$$

The theorem can be applied in reverse. In Fig. 4(a) is shown a resistance-coupled stage, which might be the sync separator of a television receiver. The required value of R_a might be $10~\mathrm{k}\Omega$ and we might wish to operate the stage from a 20-V supply whereas the h.t. line might be $200~\mathrm{V}$. The natural thing to do is to make $R_a = 10~\mathrm{k}\Omega$ and to obtain the 20-V supply by a potential divider R_1R_2 as in Fig. 4(b) and this is necessary if decoupling as provided by C is needed. If it is not, we can leave off C. We can then apply Thévenin's theorem to R_1R_2 and get Fig. 4(c) and we can see that to keep the load on the valve at $10~\mathrm{k}\Omega$ we shall have to reduce R_a by the value of R.

It now becomes obvious that there is a redundant resistor, for if R is made $10 \text{ k}\Omega$ and V is made 20 V, R_a can be dispensed with and the potential divider itself becomes the load. This is shown at (d). For our figures we have

$$20 = 200 \frac{R_2}{R_1 + R_2} \text{ and } 10 = \frac{R_1 R_2}{R_1 + R_2}$$
 so
$$\frac{R_2}{R_1 + R_2} = \frac{1}{1 + R_1/R_2} = \frac{1}{10} = \frac{10}{R_1}$$
 and
$$R_1 = 100 \text{ k}\Omega,$$

$$R_1/R_2 = 9, \quad R_2 = 11.1 \text{ k}\Omega$$

This form of circuit, in which the load and voltage-droppers are combined in potential-divider form is sometimes used in television receivers. It is a bit puzzling when first met but is easily unravelled with the aid of Thévenin's theorem.

Norton's Theorem

One could go on quoting examples of the application of Thévenin's theorem indefinitely but enough has been said to show its utility and the time has come to turn to another—Norton's theorem. This is a very similar one and states that any network, containing any number of sources of e.m.f. is, when regarded from any pair of terminals, equivalent to an impedance in shunt with a current generator of infinite internal impedance; the impedance is that measured between those terminals with all internal sources of e.m.f. short-circuited and the current is the current which will flow between the terminals when they are short-circuited.

Let us apply this to the circuit of Fig. 5(a). which is the same as Fig. 1(a). The impedance measured at the terminals is

$$R=\frac{R_{\scriptscriptstyle 1}R_{\scriptscriptstyle 2}}{R_{\scriptscriptstyle 1}+R_{\scriptscriptstyle 2}}$$

as before, and the equivalent circuit is Fig. 5(b) where I is the current generator. The short-circuit current in (a) is E/R_1 and this is the value of I in (b).

Norton's theorem is much less used than Thévenin's in this general sense, but it is very widely used in connection with pentode valves. The ordinary equivalent circuit of a valve is of the form of Figs. 1(b) or 3(b) and is expressed like Fig. 6(a). By the use of Norton's theorem it can be put in the form of Fig. 6(b) which is equally known. The resistance is the same in both. In (a) the short-circuit current is

 $\mu v_a/r_a = g_m r_a$, which is the current generator of (b). It is only because we commonly write μ/r_a as g_m , the mutual conductance, that we do not always recognize (b) as a transformation by Norton's theorem of (a).

Star-Delta Theorem

Another very useful theorem is that commonly known as the star-delta theorem, but also called the T-delta, $T-\Delta$, or $T-\pi$ theorem. Any three impedances in the

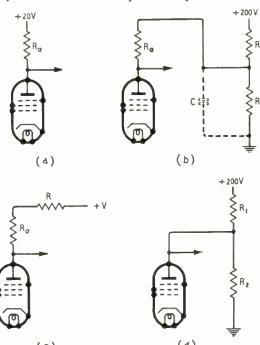


Fig. 4. A valve with a load R_a which requires a low h.t. voltage as in (a) might be used with a potential divider R_1R_2 when the supply is of high voltage. The Thévenin transformation is (c) and shows there is an unnecessary resistance and so the final circuit can be reduced to (d).

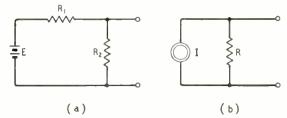


Fig. 5. By Norton's theorem these two circuits are equivalent.

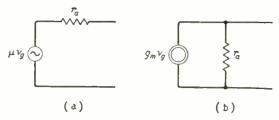
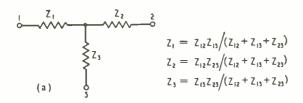


Fig. 6. Norton's theorem in the case of a valve: (a) is the circuit commonly used to represent a triode and (b) that used for a pentode.



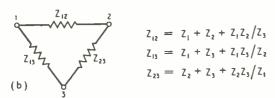


Fig. 7. The star and delta networks shown here are identical if the impedances have the relations shown.

star or T form of Fig. 7 (a) can be transformed into three different impedances in delta or π form as shown at (b) or, of course, vice versa. The relations between the impedances are given in the figure. If the network is symmetrical (i.e., $Z_1 = Z_2$ or $Z_{13} = Z_{23}$) the relations simplify considerably.

There are many uses for this equivalence. One simple one is in attenuators, perhaps for a television aerial feeder. In such a case, the values for a star might be $Z_1 = Z_2 = 59~\Omega$ and $Z_3 = 14.6~\Omega$, values which would give 20-db attenuation for a feeder impedance of 72 Ω . It might well happen that one had no suitable resistors available and the delta equivalent might be more convenient. From Fig. 7,

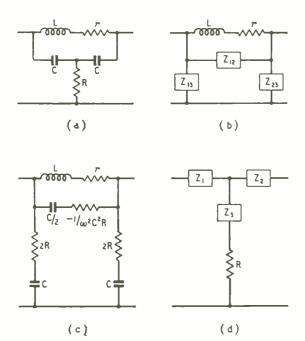


Fig. 8. Application of star-delta theorem to a bridged-T network (a). The star of C and R is transformed to a delta (b) and gives the result (c). Alternatively, the delta of L,r,C can be transformed to a star as in (d).

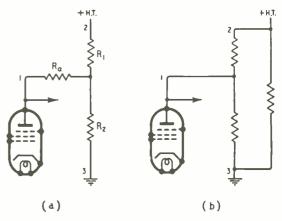


Fig. 9. The application of the star-delta theorem to the problem of Fig. 4. The star of (a) transforms to the delta of (b) and at once shows up the redundant resistance.



Fig. 10. Basic 4-terminal network.

this would call for $Z_{12}=59+59+59^2/14.6=358~\Omega$ and $Z_{13}=Z_{23}=59+14.6+(59+14.6)/59=88.2~\Omega$.

The star-delta theorem is often of great use theoretically in simplifying things. This is especially the case in bridged-T networks. The circuit of Fig. 8(a) without the resistance R is a simple parallel resonant circuit which might be used as a rejector. The inductance L has losses which are represented by the series resistance r and it is tuned by the two capacitors C in series having the total value C/2. At resonance the circuit behaves as a high resistance of value 2L/Cr, the dynamic resistance.

When R is added, it is possible to make it behave as though the dynamic resistance were infinite. Physically, some current passes through L and r and some through the T network C, R, C. By the adjustment of the components, the currents at the output can be made equal and opposite. The conditions are most easily determined by using the stardelta transformation, which can be applied in two different ways. The first is to transform the star of two capacitances and one resistance to a delta (b). We get

$$Z_{12} = 2/j\omega C - 1/\omega^2 C^2 R$$

 $Z_{13} = Z_{23} = 1/j\omega C + 2R$

and can re-draw the circuit as Fig. 2(c). This is an exact equivalent of (a) but is not physically realizable in this form because it includes a negative resistance $-1/\omega^2 C^2 R$. From this, one can write down at once the conditions for resonance and infinite attenuation

$$\omega^{2}LC/2 = 1$$
and $r = 1/\omega^{2}C^{2}R$
or $R = L/2Cr$

The alternative way of applying the transformation is to turn the delta of L, r and the capacitors into a star as in Fig. 8(d). In this particular case, this is not such a good transformation as the first, because

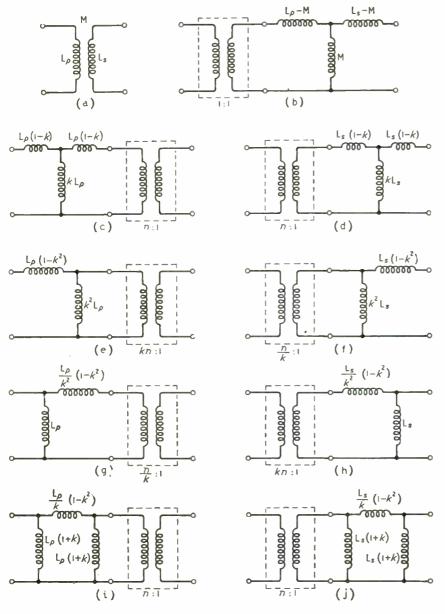
the expressions for the star impedances turn out to be more complex than those for the delta impedances of (b).

Wherever such alternatives for transforming a circuit exist, it is quite usual for one to be simpler than another and one naturally chooses this one.

The star-delta theorem can be applied to the valve problem of Fig. 4 and, although it is not so useful as Thévenin's in this instance, it does show up more clearly the redundancy of one of the resistors in Fig. 4(b). The circuit is repeated in Fig. 9(a) and the three resistors form a star which can be replaced

by a delta formation as in (b). It is at once obvious that one resistance R_{23} comes straight across the h.t. supply and performs no useful function. We can remove it, therefore, which is the same as making it infinite and the equations of Fig. 7 show that when Z_{23} is infinite Z_1 is zero. In Fig. 9(a), R_a is the Z_1 component and becomes zero. We end up then with the simple potential divider.

In this instance, the star-delta theorem is less useful than Thévenin's because it does not include the supply voltage and so does not permit us to calculate component values for particular conditions.



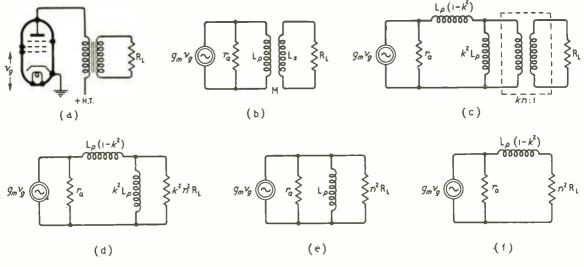
Equivalent Circuit Theorem

There is a theorem which states that any two circuits are equivalent if their open- and short-circuit impedances are the same. It applies to four-terminal networks, shown diagrammatically in Fig. 10. The open-circuit redances are the impedances between 1 and 2 when 3 and 4 are open and between 3 and 4 when 1 and 2 are open. The short-circuit impedances are the impedances between 1 and when 3 and 4 are shorted and between 3 and 4 when 1 and 2 are shorted. By the application of this theorem it is possible to prove a whole series of equivalent circuits for the transformer, some of of great which are utility. No less than ten such equivalents are shown in Fig. 11.

These circuits are all exact equivalents and the basic arrangement is shown in Fig. 11(a), a primary coil L_{ν} and a secondary coil L_{ν} and a secondary coil L_{ν} having mutual inductance M between them. In the equivalents, the transformer shown in a dotted box is an ideal one which serves to preserve the d.c. isolation and to provide a voltage transformation ratio. It has no other

where n= ratio $\frac{\text{PRIMARY}}{\text{SECONDARY}}$ turns $=\sqrt{\frac{L_{\rho}}{L_{s}}}$ and k= coupling coefficient $=\frac{M}{\sqrt{L_{\rho}L_{s}}}$.

Fig. 11. Ten equivalent circuits for a transformer are shown here. The ideal transformer, surrounded by a dotted box, provides the turns ratio and d.c. isolation but has no other characteristics. The coupling coefficient is $k=M/\sqrt{(L_pL_o)}$ and the ratio of the primary secondary turns is nominally n; actually $n=\sqrt{(L_p/L_o)}$.



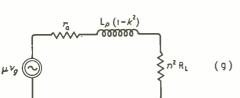


Fig. 12. Application of transformer equivalent circuit. At (a) a valve is transformer-coupled to a load R_I, and the equivalent of this is shown at (b). The transformer part of this can then be changed to give the form shown at (c) and, in turn, this reduces to (d). For low and high frequencies respectively this can be further simplified to (e) and (f). When r,, is small, as with a triode, (g) is a more useful form than (f).

characteristics. The other inductances represent the other characteristics of the real transformer. In these equivalents k is the coupling efficient of the real transformer and equals $M/\sqrt{L_pL_s}$ while n is $\sqrt{L_p/L_s}$ and is usually the turns ratio of the real transformer. The true definition is $\sqrt{L_p/L_s}$, however, and there are cases where the two are not quite the same.

Some writers make great use of the symmetrical forms of circuit (c) and (d) but the others are often simpler and, in particular, (f) is a very convenient one.

These circuits are of considerable help when one wishes to determine transformer characteristics by measurement. From Fig. 5(f), for instance, it is obvious that if one measures inductance at the secondary terminals one measures L, with the primary open and L_s $(1 - k^2)$ with the primary shorted, and from the two k can be determined. From Fig. 5(e) similar measurements on the primary give L_p and L_p $(1 - k^2)$, from which k can again be determined. Then, knowing L_p and L_s , n can be found.

One great use of these equivalent circuits is the way in which they make important factors almost obvious instead of being determinable only after a lengthy calculation. For example, suppose a valve is coupled to a load resistor R_L as in Fig. 12(a). We replace the valve by its Norton equivalent circuit, and the We now use the equivalent circuit becomes (b). transformer equivalent of Fig. 11(e) and get (c) and then transfer the load R_L from the secondary to the primary of the ideal transformer where it takes the value $k^2n^2R_L$, as in (d).

It is at once obvious that k^2L_p will rob $k^2n^2R_L$ of current, for it comes in shunt with it, while $L_n(1-k^2)$ will cause a voltage drop, since it comes in series. In practice, in a.f. applications k^2 is very nearly unity and $L_p(1-k^2)$ is consequently very small compared with k^2L_p . Because of this, the former has a negligible effect at low frequencies and the latter is negligible at high frequencies.

The circuit can thus be further simplified to the

equivalents (e) and (f) of Fig. 12, which are valid respectively for low and high frequencies only. If r_a is large compared with n^2R_L it can usually be neglected. If it is not large, the Thévenin equivalent is better than the Norton at high frequencies and (f) can be changed to (g).

It is plain from (e) that the frequency response at low frequencies depends only on the relation of L_p to the value of r_a and n^2R_L in parallel and that at the lowest frequency $f = \omega/2\pi$ we must have ωL_p large enough compared with this resistance for it to shunt it negligibly. It is equally clear from (g) that the leakage reactance at the highest frequency must be small compared with $r_a + n^2 R_L$; if it is not, it will reduce the current.

If the lowest and highest frequencies are fixed, L_v must be fixed by low-frequency requirements and $L_p(1-k^2)$ by high frequency, which means that k is fixed by the high-frequency needs. strictly, k is fixed by the bandwidth required.

The use of the transformations brings out the important factors very simply and clearly without the use of appreciable mathematics. From (e) and (g) it is easily possible to write simple equations expressing the performance from which numerical values can be obtained.

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LETTERS TO THE EDITOR

The Editor does not necessarily endorse the opinions expressed by his correspondents

Output Stage Performance

IN a description of the Osram 912 amplifier given in the September issue (page 430), it is stated that the output circuit is a compromise between pentode and triode operation as far as efficiency and harmonic distortion are concerned.

The object of employing the "ultra-linear" circuit in the Osram 912 is to provide virtually the same efficiency and power as pentode-connected valves, but a distortion lower than that of either pentodes or triodes at their respective full outputs.

Some data relevant to the Osram N709 valves specified for this circuit are as follows:

	" Ultra-							
	itode linear"	Triode						
Anode input, per pair 3	33.4 31.5	25.2 watts						
Output power	15 14	6.5 watts						
Distortion, full output :	3 1.5	2 per cent						
Distortion 6.5 watts approx.		2 per cent						
Output impedance		4,000 ohms						
Grid-to-grid input voltage	14 18	18 (r.m.s.)						

The accompanying curves enable a comparison to be made at other power levels. These results are for the output stage alone, without external feedback.

					ANODE SUPPLY VOLTAGE			BIAS				
					,	UPFL	A AOF	TAGE		RESIST	ORS	
	1.	PξN	TODe.				290 .			550	U	
	2.	TRIC	DE				315			. 330	U	
	3	"טנדו	11-AF	MEAR			315 .			270	U	
DISTORTION (PER CENT)				2				0			3/	15
					WATT	'S 0U	TPUT					

Other valves, such as the KT66, also work well in the circuit.

The output transformer is connected to the anodes and screens and not to the cathodes as stated.

GRAHAM WOODVILLE.

The M.O. Valve Co., Ltd.

"Inexpensive 10-Watt Amplifier"

WITH reference to the second part of E. F. Good's letter in your October issue concerning "the obstinate refusal to adopt the tertiary feedback-winding system" as used in P. J. Baxendall's amplifier, I would suggest the reason why this ampifier did not become as famous as others such as the Williamson is not connected in any way with the method of obtaining feedback, but because of the use of beam-tetrodes in the output stage.

With the tetrode output and about 40 db negative feedback the Baxendall amplifier has roughly the same distortion as triode output types, such as the Williamson,

on a resistive load.

With a variable impedance device such as a loudspeaker, the load presented to the output valves rises to a high value at the high audio frequencies, and also at the bass resonant frequency. With a triode-output stage and to a lesser extent with the triodetetrode connected type, any increase in load above the nominal causes a reduction in distortion; but with the tetrode or pentode a violent increase in third harmonic results. Negative feedback only reduces distortion by a given factor (x 100 for 40 db) and does not eliminate the cause.

Mr. Baxendall states that when his amplifier was tested on a loudspeaker load, "a several times increase in dison a loudspeaker load, a several times increase in distortion of the output voltage occurred due to the non-linearity distortion in the current drawn by the loudspeaker" (W.W., Jan., '48). I am not so sure that all the blame for this can be attributed to the speaker. I will admit that the RC network across the primary

of the output transformer in the Baxendall amplifier keeps the load reasonably constant with increase of frequency, but this does not alter the situation at the l.f. end. I am also surprised that the new Mullard amplifier

circuit contains no such load correctors.

From the above reasoning it seems that to get equivalent performance to a triode from a tetrode or pentode output stage on loudspeaker load, considerably more feedback is required than is apparently necessary from comparative tests on resistive loads. This, of course, is not practicable with a single-loop feedback circuit. A multiple-loop feedback arrangement, including one loop in the output stage, by triode-tetrode connection, seems to be the best answer to the problems of size, weight, and heat developed.

A further advantage of the multiple feedback loop system is that those unpleasant peaks outside the audio band can be avoided. The rise in response below 10 c/s with the Williamson circuit is the main reason why the complication of an additional mains transformer and smoothing system is necessary for the h.t. supply to auxiliary apparatus.

Aldeburgh, Suffolk.

IOHN BRIGHTON.

"Why Lines?"

AS one who has long been interested in Lissajous scanning and who recently has spent considerable time observing television pictures produced in this way, you may imagine my surprise at seeing this article in your August issue. Why lines, indeed?

As I read further through the author's list of supposed advantages, and the Editor's list of probable difficulties, I noted that he, too (as I) had failed to anticipate a major objection to the scheme. Here is a short account

of the work which brought this to light.

The possibility of producing television signals with essentially no geometrical distortion is very attractive for various industrial applications. The simplicity of the equipment (which appealed so much to Mr. Hughes) had made the idea appear very promising. Hence we constructed four sine-wave amplifiers to drive the horizontal and vertical deflection coils of a flying-spot scanner and monitor kinescope and used separate audio oscillators, set at approximately 11,350 c/s and 15,250 c/s. It at once became evident that the phasing was very critical, in order to avoid a double image due to mis-register between the forward and reverse scans. It also turned out that the frequencies must be held very nearly correct to prevent the pattern from degenerating into a lower-order coarse pattern or, worse still, a very badly flickering one, if reasonable brightness were used. We then built a synchronizing generator to produce locked signals, and while this never did work perfectly, we were nevertheless convinced that no insuperable obstacles stood in the way of a satisfactory solution of the scanning problem.

All observers remarked favourably on the geometry of the picture and noted with genuine surprise the fact that there was no need to make any brightness correction due to non-linear scanning. Even on a blank raster (no video signal) the pattern appeared uniformly bright except at the very edge, and when a picture was present even this

effect was practically invisible.
You might reasonably ask, in view of the above favourable results, what is wrong with the system? It is this: Each point in the picture is scanned twice. At the centre, for example, the first scansion occurs as the beam is moving down to the right and the second as the beam moves up to the right. Nearby points may be scanned to the left. Now if the picture detail at this point happens to be a straight narrow line, those segments reproduced by the first scansion are shifted slightly down to the right, and alternate segments reproduced by the second scansion are shifted up to the right, due to the finite bandwidth of the system. The line is reproduced as a zig-zag, and the entire scheme is shifted into uselessness. This effect is most noticeable on a test chart, such as the RMA Resolution Chart, 1946. On low-detail subjects such as close-up portraits, the effect is not serious and merely gives a "soft" rendering.

In passing, it is worth noting that sinusoidal scanning, rather than being entirely novel, was analyzed in the report of the first N.T.S.C., "Television Standards and Practice," McGraw Hill, 1943, p. 33, and was rejected at that time for reasons similar to the Editor's list of prob-

able difficulties.

W. F. SCHREIBER.

Technicolor Motion Picture Corp., Hollywood, U.S.A.

"Filters Without Fears"

I HAVE read with great interest the article by Thomas Roddam in your September issue, in which the application of Chebyshev polynomials to filter theory is clearly and explicitly given. The purpose of my letter is to point out explicitly given. The purpose of my letter is to point out that the above spelling of this distinguished mathematician's name has nothing to do either with the "post-revolutionary alphabet" or with "foreign politics." A slight acquaintance with the Cyrillic alphabet will show that only minor changes were made at the time of the revolution, none affecting the name in question, and all made with the laudable object of removing redundant letters. Transliteration from non-Roman alphabets is always a matter of some difficulty and should aim at rendering, letter by letter, words printed in one alphabet into another. It is desirable in this process to obtain a result which will also enable the reader of the transliterated material to pronounce it as nearly as possible in the original way. It is unfortunate that many of the Russian proper names with which we are familiar came into Western literature via German transliteration, Tchebycheff being a case in point. Librarians and linguists in Englishspeaking countries have devised consistent systems of transliteration based upon English phonetics and conforming to the above criteria. These are widely used—as reference to Science Abstracts will confirm-and the spelling Chebyshev is the recognized English translitera-tion, which should be universally used in place of the German monstrosity given by Mr. Roddam.

The further point that the polynomials are denoted by T_n (a) is irrelevant. After all, the Bessel functions are J(x) and Y(x), in no way suggesting their discoverer; and the elliptic functions have a notation far removed from

the names of Jacobi or Weierstrass.

Glasgow University.

B. HAGUE.

Television Interference

G. O. THACKER'S letter in the October issue of the Wireless World concerning the radiation of interference from television receivers raises a further point.

If it were possible to comply with Condition 4 of the broadcast television licence, which states that apparatus shall be so maintained and used that it does

not cause interference . . ." the television pirate detector vans described and depicted on p. 476 of the same issue would need to be rather more complicated and probably less effective.

I wonder if this is why the G.P.O. has limited powers

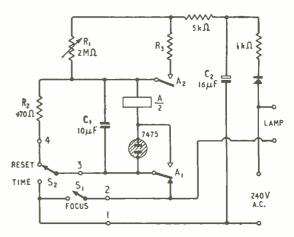
in preventing television generated interference?

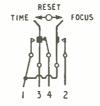
Further, it would seem ironical that, as the law stands at the moment, following the detection of a pirate television receiver by the existing means, a summons could be issued on two counts (a) the use of a television receiver without a licence, and (b) failing to comply with Condition No. 4 governing the use of a television receiver.

Stoke-on-Trent, Staffs. G. E. KING.

" Neon Timers"

WITH reference to the circuit in Fig. 3 of the article by B. T. Gilling (your September issue, p. 460), this could be made much simpler and still perform the same





Circuit of the simplified photographic timer. The key on the left could be used in place of S₁ and So and would be connected to the numbered points on the circuit.

functions by using the arrangement shown in the accompanying diagram.

Resistor R, would depend on the resistance of relay A, and is adjusted to allow a current greater than its holding current to flow to hold the relay after C, has discharged. The resistance of the relay is not critical. The voltage regulator has been dispensed with as any inaccuracies in the time lag would be due to the firing potential of the 7475 tube and the c.r. time constant of C₁R₁. Also, I do not think the mains supply voltage varies sufficiently to justify its use for the order of accuracy needed for photographic purposes.

The operation is as follows. When S₁ is thrown to the TIME position, C₁ charges via R₁ until the 7475 tube fires, when the relay operates and locks via S2, A1. the relay coil, A2 and R3. On throwing S2 to the RESET position, the relay releases and C. discharges via R. S. is used leaving S₂ in the RESET position for focusing without timing. S₂ could be a change-over toggle switch and S₁ a make-break switch, or a single-lever key could be used.

Norwich. J. R. BARNARD.

Flywheel Synchronizing

2.—Principles of Automatic Frequency Control

By W. T. COCKING, M.I.E.E.

N practice, flywheel synchronizing is normally obtained through the use of an automatic frequency control (a.f.c.) system. In this, the sync pulses are compared in a phase discriminator with a locallygenerated voltage which is usually obtained from the line timebase. As a result of the comparison, an error signal is developed which depends upon any difference of frequency or phase between the sync and the local waveforms. This error signal is passed through a filter, which provides the flywheel effect, and is then applied to the timebase as a control voltage which operates to bring any frequency error to zero.

The system is not, however, the same as the one which is used to control the frequency of the local oscillator of some superheterodyne receivers, in spite of the fact that that is also called an automatic frequency control system. In that, a control voltage is developed which depends upon the difference of the frequency generated from its proper value and the circuit cannot reduce an error to zero, for some error must exist for there to be a control voltage at all. This kind of circuit acts only to reduce the magnitude of an

error but it cannot bring it to zero.

In the case of a timebase, it is essential that the frequency be exactly that of the sync pulse recurrence. The frequency error must be zero. Frequency and phase change together and it is not possible for one to change without the other changing also. It is, however, possible to have two frequencies which are exactly the same but which have any desired constant-phase relation. It is the relative phase of the local waveform and the sync pulses which is used, therefore, in order to develop a control voltage. Because of this, the system is sometimes known as one of automatic phase control, although it is not phase which is controlled, it is phase which is the controlling quantity.

In general form, all a.f.c. systems can be represented by the block diagram of Fig. 1, but sometimes an amplifier is included between the low-pass filter and the timebase. It can be seen from this that the circuit includes a closed loop, for the output of the phase detector depends on both its inputs and one of them is derived from the timebase which is under the control of the output via the low-pass filter. It is, therefore, a feedback system and, as in all such systems, the problem of obtaining stability is important.

There are many forms of a.f.c. circuit and it is not practicable to discuss all of them here. So far as possible the discussion will be in general terms and we shall endeavour to find the most suitable type before coming to the particular.

For correct synchronism, the start of flyback in the timebase must occur nearly in coincidence with the leading edge of the sync pulse. It need not coincide exactly but, in general, it must not occur more than $1\,\mu$ sec earlier nor more than $4\,\mu$ sec later. Any difference greater than this is likely to result in a noticeable displacement of the picture on the raster and, possibly, to fold over or cut off. The total difference of timing

can thus vary over a range of about 5 µsec at most. When the two frequencies are the same, the phase detector produces an output which is dependent on the relative timing (that is, the relative phase) of two particular parts of the waveforms. This is illustrated in Fig. 2, in which the sync pulse waveform is shown at (a) and the saw-tooth wave of the timebase in (b), (c) and (d). In (b) the relative timing, or phase, is such that the start of flyback coincides with the leading edge of the sync pulse, which is the normal condition with direct locking. In (c) the flyback is shown starting about 1 µsec earlier and in (d) about 4 µsec later

Let us now consider a timebase which has no synchronizing system at all, but a manual hold control which is capable of very fine adjustment. As this control is turned, slowly, the frequency of the timebase comes nearer and nearer to the correct value and at length equals it. The timebase is then in synchronism with the signal and the frequency error is zero.

The saw-tooth and the sync signals are not necessarily in their right relative phase, however, and the sync pulses may well appear somewhere remote from the flybacks. The picture will then appear divided into two parts separated by a vertical black bar which corresponds to the blacker than black of the sync pulses and the black of the back and front porches. What should be the left-hand part of the picture will appear to the right of the bar and what should be the right-hand part will be on the left. The picture will be quite coherent, however.

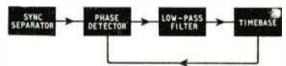


Fig. 1. Basic form of an a.f.c. system for flywheel sync.

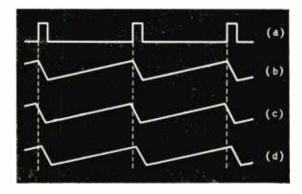


Fig. 2 Sync pulses are shown at (a) with a saw-tooth in correct phase relation at (b). The limits of permissible phase error are indicated in (c) and (d).

To obtain the correct picture it is necessary to bring the sync pulses and flybacks into approximate phase coincidence, as in Fig. 2. In order to do this, the timebase frequency must be slightly altered by the hold control and then brought back again to its correct value by returning the control to its previous setting. Synchronism is then established again but with a different phase condition.

The attainment of the correct frequency demands the provision, by the hold control, of a certain steady voltage, the precise value of which depends on many factors. such as supply voltage, temperature, stability of components, etc. If any of these change the "steady" voltage must change in a compensating manner.

Correct phasing can be secured only by a momentary change of frequency. If the black bar occurs in the centre of the picture, for instance, it is theoretically possible to bring it to its proper place at the edge by making one individual scanning line of one-half its normal duration. The change of "frequency" can occur and be over all in less than one line, which implies a momentary change to double the normal value. Alternatively, the change can be minute and persist for many lines, so that the black bar gradually creeps to the edge.

In practice it is not easy to observe these effects, but they can be seen if the timebase is a very stable one and the hold control permits sufficiently fine adjustment to be made.

An a.f.c. system performs the equivalent action to adjusting a manual control by providing automatically the voltage which would otherwise be provided by the manual control. When there is no freouency error, a voltage is developed by the discriminator which has a constant value depending only on the phase difference between the sync pulses and the saw-tooth waveforms. The system then settles down in synchronism, but with a phase error which depends upon the voltage needed by the timebase for it to run at the correct frequency. If anything changes to make the timebase need a different voltage, the relative phase must change so that this new voltage can be provided. While the change is actually occurring there is, of course, a change of frequency also.

Noise Reduction

It is necessary that synchronism should be obtainable only when the flyback is in approximate coincidence with a sync pulse and that the range of possible phase errors should be small. This is easily arranged by using the sync pulses on the one hand and a waveform derived from the flyback on the other as the signals on the phase discriminator, for a steady output can then be obtained only when at least some parts of them occur together.

If the manual hold control is adjusted while the a.f.c. system is in operation it is found that the visible picture moves as a whole sideways on the raster by a small amount. This is a characteristic of all a.f.c. systems and results from the change of phase needed to maintain the frequency at its correct value.

At this stage it will probably not be at all evident how an a.f.c. system reduces the effects of noise and interference. It does so in reality in substantially the same way as with the tuned-circuit system of Part 1. The sync pulses, together with the noise and interference, are mixed in some way with the local waveform in the phase discriminator and the output is usually some form of pulse having some characteristic de-

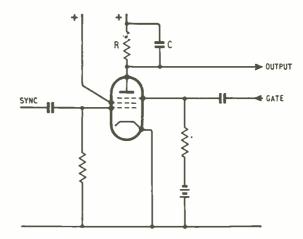


Fig. 3. Simple form of phase detector. Sync and gating pulses are applied to the control and screen grids of a pentode.

pendent on the relative phase of the signals, but it is also accompanied by noise and interference. The control voltage for the timebase is the mean value of the discriminator output and it is virtually d.c. It is the filter which changes the pulse output to d.c. and it does this by smoothing the wave. On a frequency basis it attenuates all the varying components to leave the d.c. and, in doing so, it naturally removes the noise and interference.

An analogy is helpful here. In a sound broadcast receiver a heterodyne whistle results if two stations are too near together in frequency. This whistle can be eliminated by making the r.f. circuits so selective that one r.f. carrier is sufficiently attenuated relative to the other, or it can be removed by using an a.f. filter after the detector. The first is analogous to the tuned-circuit flywheel system described in Part 1 and the second to the a.f.c. type of flywheel circuit. Both operate by frequency selectivity, but in different places. It is much easier to obtain the necessary selectivity in an a.f.c. system, however, and a simple RC network suffices.

There are a great many different a.f.c. circuits and the differences are chiefly in the form of the phase discriminator. The two most important divisions are between balanced and unbalanced discriminators; within these, most of the different kinds fall into the unbalanced category but the balanced type is probably the more widely used.

It will appear later that the balanced discriminator has important advantages over the unbalanced and we shall deal mainly with this kind. It is not however, the simplest to understand and it is helpful first to consider a particular form of unbalanced circuit.

The basic circuit of this is shown in Fig. 3. The sync pulses are applied to the control grid of a pentode; they are not differentiated and so the pulses are substantially rectangular. The pulses are negativegoing and the cathode current is cut off whenever a pulse is present, but at all other times the grid is at about cathode potential.

The timebase waveform comprises positive-going pulses which are preferably, but not essentially, of rectangular form. This gating-pulse waveform is applied to the suppressor grid of the pentode which is so biased that anode current is cut off except when a pulse exists on the suppressor.

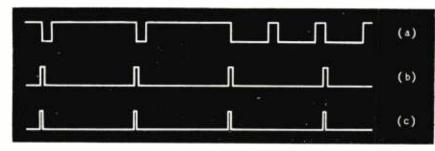


Fig. 4. Waveforms for the circuit of Fig. 3. are shown here. The sync pulses are at (a) and the gating pulses at (b). The anode-current waveform of the phase detector is shown at (c); the pulse width depends on the overlap of (a) and (b).

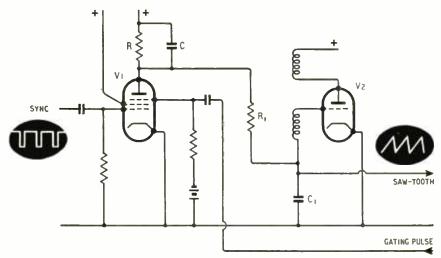


Fig. 5. The phase detector of Fig. 3. is shown here connected to a blocking oscillator to control it.

If sync pulses are absent, the valve passes anode current for the duration of every gating pulse and a mean voltage drop appears across R corresponding to the mean current through it. When sync pulses are present and overlap the gating pulses anode current is cut off during the sync pulses and so current flows only during that part of a gating pulse which is not overlapped by a sync pulse. Since the pulses are all of constant amplitude the magnitude of the anode current is always the same whenever it flows. The time for which it flows, however, depends on the overlap of the pulses and therefore, also, the quantity of electricity passed by the valve and carried into C. The resulting mean voltage developed across RC, which forms the output voltage, therefore, depends upon the degree of overlap of the pulses; that is, upon the relative phase of the sync and time-base waveforms.

Phase Discriminator Operation

One condition of operation is shown in Fig. 4. The sync pulses are shown in (a) with some of the frame pulses as well as the line. The gate-pulse waveform is shown at (b); it is generated by the timebase and is here rectangular and the pulses are assumed to have a duration of $4 \mu \, \text{sec}$, compared with the $10 \mu \, \text{sec}$ of the line sync pulses. The phase relation shown is with the gate pulses centred on the leading edges of the line sync pulses.

The anode current waveform is shown at (c) and comprises pulses of 2-µsec duration. Current flows for the first 2 µsec of the gate pulse because the sync pulse has not then started; the control grid is at about cathode potential and the current starts when the gate pulse brings the suppressor grid to cathode potential. No current flows for the last 2 μ sec of the gating pulse for, after the first 2 µsec, the sync pulse comes along and cuts off the current.

No change of current waveform occurs during the frame-pulse period, for the gating is accomplished on the leading edges of the pulses and these recur regularly during the framepulse period. The halfline pulses have no effect because there is no gate pulse when they occur. Generally, noise or interference can have no effect at all except when it occurs during the time for which the gate pulse exists. This alone can result in a considerable reduction in the frequency with which noise and interference can affect the synchronizing. although it does not alter

the magnitude of its effect when it actually does occur. If a phase change occurs between the sync pulses and the gating waveform, the effect is of a relative displacement of (a) and (b) in Fig. 3. If (b) is moved to the left, for instance, the pulse overlap is reduced and the current pulses are longer. If it is moved to the right, the overlap is greater and the current pulses are shorter. The maximum permissible movement is the width of the gating pulse— $4\,\mu$ sec in this instance. It can move to $2\,\mu$ sec later than the position shown, when anode current is just cut off completely, or to $2\,\mu$ sec earlier when the anode current flows for twice the time shown in (c) and so has twice the mean value.

The resistor R in Fig. 3 might have a value of $100 \, \mathrm{k}\Omega$ and the peak anode of this valve might be 5 mA. The mean voltage across R for $100\text{-}\mu\mathrm{sec}$ line period would be $500 \times 2/100 = 10 \, \mathrm{V}$ for the mean condition and would vary from 0 to 20 V as the phase varied from $2\,\mu\mathrm{sec}$ late to $2\,\mu\mathrm{sec}$ early.

If the timebase is normally running so that condition (c) is obtained and some change occurs, so that the gate pulses start arriving later, it means that the interval between them is increasing and the timebase is tending to run at a lower frequency. The resulting decrease of voltage across R, which is a rise of anode potential with respect to the positive h.t line, must be applied to the timebase so as to increase its frequency.

One way of doing this is to return the charging resistor of the timebase to the anode of the valve in

Fig. 3. The increase of voltage then increases the charging current and the capacitor of this circuit charges more rapidly. This means, of course, that the frequency of the timebase tends to rise.

If the initial charge is the other way round, every-

thing happens inversely.

The interconnection of the circuit of Fig. 3 with a blocking oscillator saw-tooth generator is shown in Fig. 5, in which R is the charging resistor and would normally be in part variable as a manual hold control. The circuit is not a very practical one for it is diffi-

cult to generate a suitable gating pulse.

Normally with direct locking the flyback is initiated by the leading edge of the sync pulse and may start almost immediately or after a small delay. The picture ceases 0.5-1 µsec before the leading edge. It is usually impracticable to make the leading edge of the gate pulse occur prior to the start of flyback and it is not easy to make it even coincide with it. The easy thing is usually for it to occur several microseconds after the start of the flyback.

When the leading edge of the sync pulse is gated and the start of the gating pulse coincides with the start of the flyback, then the flyback must start earlier than the sync pulse by up to the duration of the gating pulse. In the example quoted, flyback must start from 0 to 4 μ sec before the sync pulse. As a result, from 3-3.5 μ sec of the right-hand side of the visible part of the picture may be cut off or folded over. This can be avoided only by narrowing the gating pulse and it should not exceed 1 μ sec in duration and, preferably, be still less. The output of the phase detector is proportionally reduced and will quite likely not be enough for adequate control.

It would, of course, be possible to obtain the same result by delaying the sync pulses and this would be preferable if it could be done easily enough. At present, however, it seems to be economically

impracticable.

Another difficulty arises over the generation of a 1-µsec undelayed pulse by the timebase. The gating waveform is usually taken from the output stage of the timebase, for a large voltage exists there and it is buffered from the saw-tooth generator by the output stage. The pulse has considerable delay over the start of the flyback, however. If a voltage from the saw-tooth oscillator itself is used, there is a grave risk of the oscillator being triggered by the pulses in the phase detector, for the smoothing by RC of Fig. 2 is often far from perfect and appreciable amplitude of pulse does exist here. The circuit would then merely degenerate to an expensive and unsatisfactory way of obtaining direct locking. Because of these practical difficulties the circuit is not much used.

Effect of Noise

It will be remembered from Part 1 that the effect of noise and interference is partially or completely to fill a sync pulse or, by cancelling the signal just prior to a sync pulse, to make the pulse in effect start earlier than it should do. In the gating circuit the effect is, therefore, to make the anode current pulses somewhat variable in width. Noise and interference do affect the mean output voltage and hence the operation of the time base, but not to the same degree. Because of the integrating effect of CR, Fig. 2, any effect is very slow and spread over many scanning lines. The effect can be, in fact, no more than a slow and small sideways movement of the picture as a whole. If the time constant is smaller, so that the

integration is over a period corresponding to a dozen lines or so only, then there may be a displacement of these lines relative to the others, but it is not an abrupt and erratic displacement like that which occurs with direct locking. It is a gradual displacement and the visible effect may be more than the appearance of a slight bend in vertical lines.

If, on the average, the effect of interference is to cause sync pulses to be as much early as they are late, then because CR gives an averaging effect, the effect of the interference is zero. In practice this is not likely to occur, but some reduction in its effects may well occur because of the two different ways in which noise and interference can affect the pulses.

(To be concluded)

Headquarters for Scottish Electronics

ON October 11 the Duke of Edinburgh opened a new laboratory building adjacent to the Ferranti works at Crewe Toll, Edinburgh. It has been built by the Government, and as well as housing Ferranti's own research staff it will provide a centre for the Scottish Council scheme of developing the electronics industry in Scotland. As reported in our February, 1952, issue, this scheme is based on the fact that the Scottish Council have induced the Government to place a fair share of research contracts in Scotland, from which firms will be able to build up their technical knowledge and facilities. Once the firms have established themselves with this kind of work they will be in a position to go into the commercial applications of electronics.

Ferranti's are acting as a "parent" organization for the scheme and their main function is to accept large design contracts from the Government and sub-divide them amongst the firms participating. They also provide technical liaison in the progress of these contracts and assist the participating firms with administrative matters.

the participating firms with administrative matters.

The importance of the new laboratory block to the scheme is that it will provide a place where engineers from these firms can work alongside Ferranti engineers and so gain experience of electronic techniques which they would not otherwise obtain. The scheme is, in fact, mainly intended for existing firms who wish to establish their own electronics departments. One engineering firm, for example, which started by appointing one man to work in the Ferranti laboratories, now has a team of about 30, including six graduates, at work in its own factory.

Sunspot Minimum

SUNSPOT activity has, on the average, been decreasing since the maximum in May, 1947, and by the beginning

of this year had reached a very low level.

Although it is not possible to predict future sunspot activity with any certainty it had been generally expected that it would reach a minimum value sometime during 1954. According to information received from the Zurich Observatory the activity is now increasing again, and it is thought probable that the minimum occurred in June. It is too early yet to be certain about this, and it is also improbable that sunspot activity will increase sufficiently to have any very significant effect upon the usable radio frequencies for several months to come.

The significance of sunspot activity to radio men is, of course, that it is one of the observable phenomena indicative of the general solar activity, upon which depends the degree of ionization of the reflecting layers of the ionosphere. When the solar activity is high the ionization of the layers is greatest, and the higher frequencies become usable for long-distance communication, when solar activity is low the m.u.fs. are lower.

T. W. B.

Filters Without Fears

3.—Some Practical Design Calculations

By THOMAS RODDAM

N the two previous parts of this article which appeared in the August and September issues, some attempt has been made to show how low-pass filter networks can be designed from first principles. The first article, which contained two stupid slips at the beginning, was intended to lay a foundation for its successors and in this article the idea of the Butterworth, maximal flatness, response was introduced. The second article dealt with the more complicated Tchebycheff response, the closest approximation type of characteristic. The Wireless World "standard reader," who serves much the same purpose as the canary in the coal mine or the leech in the jam jar, has been heard muttering that all this mathematics would never have done for The Signal. Can I introduce a new non-symbolic algebra, to serve as a counterpart to that study now so popular among electronic engineers, symbolic logic? Dare I press on with the mathematics and tell those of you who find it too heavy going that I can do "nothing but sympathize?"

Let us at least see where we have reached. The basic circuit which we are considering is made up of a generator of impedance R₁ and a load, R₂. Across the load there appears a voltage V2, produced by the generator voltage V_1 . Quite obviously, $(V_1/V_2)' = (R_1 + R_2)/R_2$ (So obviously indeed that I wrote it incorrectly in

Part I).

This is the scene before we put in the filter, which consists of a chain of shunt capacitances and series inductances making a total of n reactive elements. which we call an nth order filter. For this filter we find a new expression (V_1/V_2) = some expression containing the frequency. The insertion loss of the filter is defined as

20 log (V_1/V_2) - 20 log $(V_1/V_2)'$ decibels.

If we were not being too strict about the exact meaning of the decibel, we could say that this meant simply the loss from generator to load with filter minus the corresponding loss without filter. Just at this time, however, the definition of the decibel is under scrutiny, so we must be careful with our words. For algebraic convenience, we can rewrite the expression above as

20 $\log [(V_1/V_2)/(V_1/V_2)']$ (In Part I, I'm afraid,

the prime was in the wrong place). Now the expression $(V_1/V_2)/(V_1/V_2)'$, which we call N for short, is a complex quantity which contains terms in j, j^2 , and so on. Of course $j^2 = -1$ and $j^3 = j$. $j^2 = -j$ but after getting rid of the j^2 's we finish up with N = A + jB, where A and B are expressions containing ω . The physical meaning of this is that N contains information about both the insertion loss and the insertion phase shift, and it is all mixed up together. We want to know the insertion loss, so we take $|N| \angle \theta = \sqrt{A^2 + B^2}$ arc tan B/A and the insertion loss is $20 \log |N| = 10 \log |N|^2 = 10 \log$ $(A^2 + B^2)$. If for any reason we want to work with the insertion phase shift, we have $\tan \theta = B'A$.

For the second-order filter we derived the two equations

$$V_1 V_2 = (R_1 + R_2)/R_2 + j\omega(CR_1 + L/R_2) - \omega^2 LC$$

 $(V_1 V_2)' = (R_1 + R_2)/R_2$
and dividing one by the other,
 $N_1 = 1 + i\omega[CR_1R_1/(R_1 + R_2) + L/(R_1 + R_2)]$

 $N = 1 + j\omega[CR_1R_2/(R_1 + R_2) + L/(R_1 + R_2)] - \omega^2LCR_2/(R_1 + R_2)$ Therefore $|N|^2 = 1 + \alpha\omega^2 + \beta\omega^4$, where the actual expressions for α and β were given in Part I. By putting $\alpha=0$, the expression for $|N|^2$ is simplified to $1 + \beta \omega^4$, which is what we call a Butterworth response. The equation $\alpha = 0$ fixes a relationship between the inductance L and the capacitance C, and this relationship was given at the beginning of page 369 (August issue). It depends on the ratio of the two

resistances R₁ and R₂, and some special cases were considered.

It is fairly certain that $\alpha = 0$ leads to the simplest solution, but is it the best? Bitter experience suggests that because it is the simplest it will not be the best. A more complicated solution is obtained by using the Tchebycheff polynomials, which are expressions giving a response oscillating between limits in the pass band, and offering us a choice of those limits. In Part II I used the limits of ± 0.625 db mainly in order to make the mathematics simple. This gave us two equations, $\alpha = -1$ and $\beta = +1$ and these in turn led to a new relationship between the inductance and the capacitance, a relationship which depends on the ratio of the two resistances.

Butterworth or Tchebycheff?

Have we wasted our time with the extra complication, and was the whole exercise worth while, anyway? The results which were derived in Part II showed us that the Tchebycheff filter has a much narrower transition region than the Butterworth filter. We can perform a different sort of calculation to compare the two types of filter and to give an idea of the sort of problem we may want to tackle. Suppose that we are dealing with the input to a video amplifier and we have a source with an impedance of 1,000 ohms. which is to be connected to the input grid, with a capacitance of 10 pF. In this particular example matching will be regarded as unimportant: what we shall look for is bandwidth. Common sense tells us that we should not put any resistance into the circuit, because that will reduce the available signal, so that in all the results derived in the previous articles we can take $R_2 = \infty$.

Let us consider what we will get. The simplest solution is just to connect the source directly to the input grid, giving us a first-order filter. It will be 3 db down when $2\pi f CR_1 = 1$ or f = 1.6 Mc/s. What is more, and more disturbing, it gives us a very gentle cut-off, and the response will be 1.25 db down when $10 \log \left[1 + (2\pi f CR_1)^2\right] = 1.25$ or f = 0.92 Mc/s.

We can do better than this by adding a series inductance to convert the network into a second-order filter. With a Butterworth filter we find that the response is 3 db down at $2\pi f CR_1 = \sqrt{2}$ or f = 2.26 Mc/s. It is a rather sharper cut-off, too, and at the 1.25 db. point we have f = 1.72 Mc/s. Another capacitance, across the input end of the network, would give us a third-order filter, with $f_{3db} = 2.4$ Mc/s and $f_{1.25db} = 1.95$ Mc/s.

For the Tchebycheff response, we have a tolerance of ± 0.625 db, and this gives us a response of the form $1-x^2+x^4$ with a 1.25-db bump at x=0.7. The edge of the pass band is at $2\pi f CR_1=1$ or 1.6 Mc/s.

For this tolerance, therefore, Butterworth seems to give a higher limiting frequency than Tchebycheff. Against this we must set the fact that the Tchebycheff response is always above the zero frequency level, while the Butterworth response is below it: the reduction in bandwidth is paid for by a small increase in gain.

When we consider very much closer tolerances on frequency response, in which there is no gain difference worth worrying about, we find that the Tchebycheff responses do offer some advantage in terms of bandwidth for a given capacitance-resistance situation. The arithmetic is complicated, and I don't propose to do more than assure you that it is so, and that facts and figures are given in "Amplitude-Frequency Characteristics of Ladder Networks" by E. Green, published by Marconi's Wireless Telegraph Company.

Tolerance Calculations

We can use all this algebra for interstage coupling networks, too, if we stick to third-order filters. One reader wrote to me and complained that R₁ was never really infinite, even with a pentode, and of course R₂ cannot really be infinite, what with grid leaks, transittime damping, dirty valve bases and anything else you choose to mention. The point which the reader made was that you need to get the volts on to the anode, so you must put in a physical resistor. Partly, of course, it all turns on tolerances: the tolerance on valve capacitance may be $\frac{1}{2}$ 15%, and in such a problem the effect of an anode supply resistance of 10 times the value of R₂ would not be too serious compared with the inherent inaccuracy of the analysis. In the example we have just considered we could make R, something like 100,000 ohms and never notice the slightest difference: after all, the components have some losses which are not included in the calculation. Anyway, in a second-order network which we meet very often, L is the leakage inductance of a transformer and we get a path for bias through the secondary, although we can neglect the actual shunt inductances for purposes of calculation.

There is, I think, sometimes a lack of understanding of the reasons why network theorists consider rather artificial networks. It is not that they want to analyse problems which are outside the experience of the practical man, but rather that they are rehearsing situations which illustrate fairly clearly some particular feature. Then when the practical man turns up with his problem, the theorist can say that, stripped of irrelevancies, the system is a network of such-and-such type, and you design it so and so. In these articles we have done a moderate amount of algebra, and we

now have this material as background. Let us take a rather different sort of problem, and use our old algebra again.

We shall take a second order filter, and for simplicity we shall take $R_2 = \infty$. That makes k = 1, and the response will be given by

$$|N|^2 = 1 + \omega^2(C^2R_1^2 - 2LC) + \omega^4L^2C^2$$

We know that if $C^2R_1^2 = 2LC$ we have a Butterworth response. But suppose we make a practical filter, with some small errors in the component values: what will happen to the response?

Let us take $C' = C + \delta C$ and $L' = L + \delta L$

In this pair of equations, δC and δL are perhaps about 1/10th of the values of C and L respectively.

First, let us assume that the method we use for adjusting the filter is one which makes $\omega^2_0 L'C' = \omega_0^2 LC$ where ω_0 is the design cut-off frequency. We shall have $LC + C\delta L + L\delta C = LC$ (neglecting $\delta L.\delta C$ which is very small) so that $\delta L/L = -\delta C/C$. The two tolerances are equal but in opposite directions. The response is now expressed by

 $\begin{aligned} |\mathbf{N}|^2 &= 1 + \omega^2 [(\mathbf{C} + \delta \mathbf{C})^2 \mathbf{R}_1^2 - 2\mathbf{L}\mathbf{C}] + \omega^4 \mathbf{L}^2 \mathbf{C}^2 \\ &= 1 + \omega^2 [2\mathbf{C}\delta \mathbf{C}\mathbf{R}_1^2 + \mathbf{C}^2 \mathbf{R}_1^2 - 2\mathbf{L}\mathbf{C}] + \omega^4 \mathbf{L}^2 \mathbf{C}^2 \\ &= (\text{dropping terms in } \delta \mathbf{C}^2) \end{aligned}$

The response was to be a Butterworth one, so $CR_1^2 - 2LC = 0$ and we have

 $|N|^2 = 1 + \omega^2 2C\delta CR_1^2 + \omega^4 L^2 C^2$

Now we know that $C^2R_1^2 = 2LC$ so that we can write $|N|^2 = 1 + 2\sqrt{2}.\omega^2\sqrt{LC}.\delta CR_1 + \omega^4L^2C^2$ If the cut-off frequency is ω_0 , with $\omega_0^2LC = 1$, we have

$$|N|^2 = 1 + 2\sqrt{2} \int_{\omega_0}^{\omega^2} .\delta CR_1 + \omega^4 L^2 C^2$$

From this, since $CR_1 = \sqrt{2/\omega_0}$ (see Part 1), we reach $|\mathbf{N}|^2 = 1 + 4\delta C/C \cdot \omega^2/\omega_0^2 + \omega^4/\omega_0^4$

We could now calculate the shape of the insertion loss characteristics for any particular value of $\delta C/C$. It is quite useful, however, just to look at this expression and to examine what happens if we have w = w. Then $|N|^2 = 1 + 4\delta C/C + 1 = 2 + 4\delta C/C$

 $\omega = \omega_0$. Then $|N|^2 = 1 + 4\delta C/C + 1 = 2 + 4\delta C/C$. Suppose we take $\delta C/C = \pm 0.25$. For $\delta C/C = \pm 0.25$ we have $|N|^2 = 3$ and the response is 4.77db down where it should be 3db down. If $\delta C/C = -0.25$ the response is not down at all at the ideal 3db point, and looking back we see that it has the form

 $|N|^2 = 1 - \omega^2/\omega_0^2 + \omega^4/\omega_0^4$ This is just the expression we found for the ±0.625db Tchebycheff case. As we know that Tchebycheff responses are in general more profitable than Butterworth ones, we can aim our design so that it falls between the two by making C' rather below than above the design value, and L' on the high side. The simple calculation above has given us a guide as to the way in which we must make provision for the errors of the practical solution.

Suppose, however, that you insist on a Butterworth response at all cost. We have $CR_1^2 = 2L$ so that in the practical case $C'R_1^2 = 2L'$ and therefore $\delta CR_1^2 = 2\delta L$

giving $\delta C/C = \delta L/L$

This time both reactances are in error in the same direction, and again the percentage error is equal. Now the insertion loss characteristic is given by

$$|N|^{2} = 1 + \omega^{4}(L'C')^{2}$$

$$= 1 + \omega^{4}(L + \delta L)^{2} (C + \delta C)^{2}$$

$$= 1 + \omega^{4}(L^{2}C^{2} + 2L^{2}C\delta C + 2LC^{2}\delta L +$$

terms in the products of the errors, which we can neglect).

From this
$$|N|^2 = 1 + \omega^4 L^2 C^2 \left(1 + 2 \frac{\delta C}{C} + 2 \frac{\delta L}{L} \right)$$

= $1 + \omega^4 L^2 C^2 (1 + 4 \delta C/C)$.

It is not very hard to get from this to the result that if $\omega_0^2 LC = 1$, the response will be 3db down at $\omega_0(1 - \delta C/C)$. While we quite cheerfully accepted a value of $\delta C/C = -0.25$ before, giving us a response change from ± 1.5 db to ± 1.25 db, this capacitance tolerance allied with the insistence on a Butterworth characteristic has cost us a 25% change in bandwidth. If we took $\delta C/C = +0.25$ the response would be narrowed by 25%, and would be 6.2db down at the design cut-off, instead of 4.77 db.

We really have collected quite a lot of information from the second-order equation, and now, you notice, it is really practical stuff, which gives us guidance when we are designing a network to be made. We want to lean our design towards the region between a Tchebycheff response and a Butterworth response, and we must adjust the components to give the correct resonant frequencies, rather than just try to get the individual values right.

Let us now look at yet another way in which we can make use of some of our results. The simple filter networks are often used for connecting one valve to another: the circuit used may not look exactly like one of those shown in Table I (page 445, September issue), but it reduces to the filter form if you twist it round suitably. When we have two filter circuits separated by a valve, the overall response characteristic is given by the equation $|\mathbf{N}|^2 = |\mathbf{N}_1|^2 . |\mathbf{N}_2|^2$ where \mathbf{N}_1 and \mathbf{N}_2 relate to the two filter networks. To save labour I shall confine myself to first- and second-order filters, for which

$$|N_1|^2 = 1 + x^2$$
 (first order)
 $|N_2|^2 = 1 + ax^2 + x^4$ (second order)

If then we have two first-order filters connected through a valve:

$$|N|^2 = (1 + x^2)(1 + x^2)$$

This is a very dull solution, 6 db down at x = 1. If we have a first-order filter and a second-order filter in tandem the most general form we can find for this is:

$$|\mathbf{N}|^2 = (1+x^2)(1+ax^2+bx^4) = 1+(1+a)x^2+(a+b)x^4+bx^6$$

I'm not sure if this can be made into a Tchebycheff response: I rather think it cannot. But if we put b=1 and a=-1 it reduces to $|N|^2=1+x^6$, a Butterworth response. We have, in fact, obtained a Butterworth response of the third order by combining a first-order characteristic with a second-order Tchebycheff response.

Two second-order filters in tandem will give us, in the most general case:

$$|N|^2 = (1 + ax^2 + x^4)(1 + bx^2 + cx^4)$$

There is an extensive field for study here, but let us put c=1, so that

$$|N|^2 = 1 + (a+b)x^2 + (ab+2)x^4 + (a+b)x^6 + x^8$$

Here we can take $a = -b = \sqrt{2}$, and we are left

$$|N|^2 = 1 + x^8$$

This particular result is one which happens to crop up in the design of feedback pairs, and we might also find it in the design of a system consisting only of an input circuit, a valve and an output circuit. One valve or four, low-pass or band-pass, its all part of the same family, and one lot of plodding suffices. In this case we should have to go back from

$$|N|^2 = 1 \pm \sqrt{2} x^2 + x^4$$

$$|\mathbf{N}|^2 = 1 + [(\mathbf{CR}_p + \mathbf{L} \mathbf{R}_s)^2 - 2\mathbf{LC}k]\omega^2 + \omega^4 \mathbf{L}^2 \mathbf{C}^2 k^2$$
 (September issue)

and the corresponding equation with k'. We would, perhaps, take k and k'=1, which you can find to be what happens if a pentode is used with an unloaded grid. Then $|N|^2=1+(CR^2-2LC)\omega^2+\omega^4L^2C^2$ and therefore $CR^2-2LC=\pm\sqrt{2}$ LC

$$\frac{CR^2}{L} = 2 \, \pm \, \sqrt{2}$$

In this composite equation R is the source impedance for the input filter, and the load impedance for the output filter. C is the valve capacitance, input or output. It doesn't really matter to us which filter we use at the input and which at the output, even though one is a characteristic with a hump in it, while the other is a rounded one. We should check both forms against the valve characteristic in practice, because one presents a much higher load resistance to the valve than the other.

We could, of course, go on to consider what happens if third-order filters are included, but the algebra becomes involved, and is, indeed, sufficiently involved to justify a slightly different approach, based on the distribution of the characteristic frequencies of the networks. I do not propose to discuss this matter at all, because the algebra really does get rather beyond the permitted limit.

Nothing in this article, of course, will enable you to design a filter wihtout thought. None of the equations should be taken on trust, because they are only introduced as examples of how to set about the job, and I usually work them out from first principles every time I need them. But if you can work out what happens in a simple RC circuit, you can calculate a second-order filter, too. If you can do that, you can try the third-order filter: better still, you can try the problems of variations, like the effects of component tolerances we have been considering above, or problems connected with the phase characteristic, which I haven't discussed at all. Then there's quite a different set of response characteristics, of the general form $N = (1 + j\omega/\omega_0)^n$. These are thoroughly well damped, and give no overshoot at all when a step wave is applied to them. Some of this work, perhaps, is just shadow boxing, just a light paddle between the locks, a chess problem by the fireside; but it is all part of the process of building up a solid foundation on which further development can take place.

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IMPROVED strength and toughness is claimed for a new epoxide resin ("Epophen" M-777) made by Leicester Lovell and Company, North Baddesley, Southampton. It is used as a contact adhesive for bonding metals, glass and plastics, as well as wood and other materials which are normally glued. In addition it can be used as a casting resin, and one application is in the production of press tools for sheet metal working Castings up to ½-ton in weight are possible, one reason being that there is no appreciable evolution of heat during the setting process.

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High-Quality Tape Recording

Circuit Design for a Recorder Using High-impedance Heads

By A. F. FISCHMANN*, A.M.Brit.I.R.E.

HE design described in this article is simple and may be adopted easily to different tapes and high impedance recording heads. Frequency-selective feedback is used throughout the system in order to modify the frequency response.

The author's equipment consists of the Model 5 Tape Desk built by Bradmatic Ltd., Station Road, Aston, Birmingham 6. It is equipped with erasing, recording and reproducing heads, all of the highimpedance type. Its performance using MC1-111 tape of the Minnesota Mining and Manufacturing Company Ltd. at a speed of 7.5in/sec. was found to be as fellows:

Response within ± 3 db between 40-10,000 c/s. Signal-to-noise ratio 45 db.

The distortion was not measured but the reproduction of high-quality discs through the recorder proved to be incistinguishable from the original. An extension of the frequency range could have been readily obtained, using additional equalization.

The system consists of a recording amplifier, playback amplifier and supersonic bias oscillator and may be used in connection with any high-quality pre-amplifier as a front-end control unit for a power amplifier. Obviously all the equalization necessary for the truthful reproduction of records or any other programme must be provided within the pre-amplifier, and the system itself is designed for flat response within the above-stated limits between its input and The main amplifier should provide the conventional tone control circuits (treble and bass lift and cut). A block diagram of the complete system is shown in Fig. 1 together with the selector switch. Switch S_1 is provided in order to compare the performance of the unit with direct transmission and is especially useful for the adjustment of its frequency response in the absence of accurate measuring gear.

The diagram of the record amplifier is shown

* Israeli Ministry of Defence, Scientific Department.

Symbols

= Internal resistance of valve n.

Cathode resistance. = Anode resistance of valve n.

Amplification factor.

Mutual conductance of valve n.

 G_a

 Z_{out} = Output impedance of recording amplifier.

Recording current, C₉₂ connected.
 Recording current, C₉₂ disconnected.

= Inductance of recording head.

Equivalent series resistance of recording

in Fig. 2. To suit the special requirements of a tape recorder, it should provide a constant current through the recording head at all transmitted frequencies, thus ensuring equal magnetization of the tape over the whole transmission band. In addition, treble lift may be necessary to compensate for losses due to the tape and the airgap of the recording head, whose width sets a definite limit to the highest transmitted frequency. The constant-current characteristic is frequently achieved by providing a frequency response rising by 6db per octave. The signal is then applied to the recording head which represents a mainly inductive load and a substantially constantcurrent characteristic is thus obtained. arrangements use a resistance of about $50k\Omega$ through which the recording head is connected to a conventional amplifier. The latter has to provide a considerable output voltage at all frequencies due to the losses in that resistance and may give rise to distortion if not properly designed.

In this amplifier a different way was chosen. output stage, Fig. 3(a), will be considered separately and its equivalent circuit diagram is shown in Fig. 3(b),

$$R'_i = R_i + R_k(\mu + 1) \dots \dots \dots \dots (1)$$

 $(R_i = \text{internal resistance of V2}).$

The voltage across the load

$$E_{L} = -\frac{\mu E_{in} Z_{n}}{R_{i}' + Z_{n}} \qquad . \qquad . \qquad . \qquad (2)$$

where
$$Z_a = \frac{R_a Z_L}{R_a + Z_L}$$

$$g'_{m2} = \frac{\mu}{R_i' + Z_i} \qquad \dots \qquad \dots \qquad \dots \qquad \dots \qquad \dots \qquad \dots$$

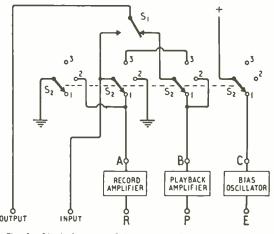
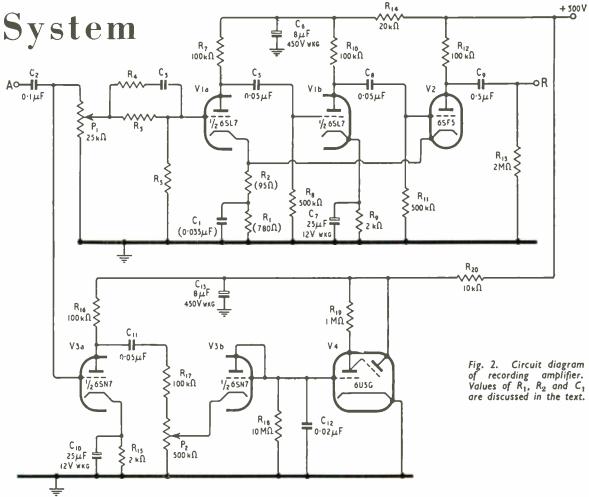


Fig. 1. Block diagram of the system Switch positions are: 1, recording: 2, reproducing: 3, direct.



may be considered as the effective transconductance of the valve V2 due to the current feedback from the cathode. As $R_i \gg Z_a$ within the transmitted fre-

quency spectrum, $g'_{m^2} \approx \frac{\mu}{\bar{R}_i'}$ and V2 is working as

a constant current generator.

R_k may be designed as to make R_i' sufficiently high in order to drive a recording head with a constant

current over a reasonable frequency band. However, in that case V2 would need a driving voltage of approximately 20 volts, which can hardly be provided by any of the pre-amplifiers generally in use. Therefore a double triode is added and the feedback is extended over two additional stages. Using the simplified diagram shown in Fig. 4 and putting $G_{a1} = G_{a2} = G_{a3} = 0$, the output admittance of that circuit is

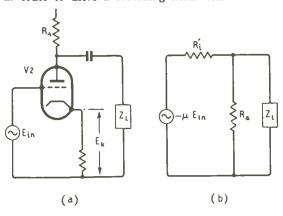


Fig. 3. (a) Output stage of recording amplifier and (b) its equivalent circuit.

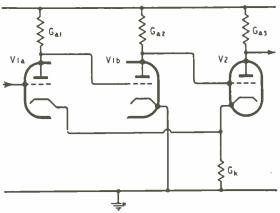


Fig. 4. Simplified diagram of feedback in the recording amplifier.

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$$Y_{out} = g_{p2} \left(1 - \frac{1}{1 + \beta G_k} \right) \dots \dots (4)$$
where $\beta = \frac{1}{g_{m2} + g_{p2} + \frac{(g_{m1} + g_{p1})g_{m2}g_{p2}}{(g_{p1})^2}}$

and g_{m1} , g_{m2} , g_{p1} , g_{p2} are the respective mutual conductances and plate conductances of V1 and V2.

As
$$\beta G_k \ll 1$$
, therefore $1 - \frac{1}{1 + \beta G_k} \approx \beta G_k$ and $\frac{1}{Y_{out}} = Z_{out} \approx \frac{1}{g_{p2}\beta G_k} = \frac{14.4 \times 10^6}{g_{p2}G_k} M\Omega$ for practical values of g_m and g_n .

Z_{out} may therefore be neglected in comparison with Ra and the latter determines solely the output impedance of the complete amplifier. Its current amplification will be inversely proportional to R_k and may be made to rise over a certain frequency range by introducing an R-C network (R₃, R₄, R₅, C₃, in Fig. 2). It should be designed to compensate for the loss of high frequencies as already mentioned, and may extend the flat frequency range by one octave. It should be noted that the high-frequency response of the amplifier may be controlled by extremely low impedances, avoiding the conventional high-impedance type networks which are most liable to capacitive pick-up if not properly screened. The recording amplifier response may also be easily adapted to different kinds of tape speed by changing C1, which will move both the low and the high frequency turnover point by an equal amount. The value of these components should be determined experimentally according to the characteristic of the individual tape and recording head. Their design procedure will be outlined later in this article.

A magic eye V4 is connected to the input of the recording amplifier through V3. It should close for full modulation of the tape and its sensitivity may

be adjusted by P₂ (Fig. 2).

The playback amplifier (Fig. 5) is designed along conventional lines. A signal recorded with a constant current characteristic will provide an output rising by 6db per octave at the terminal of the playback

head. In this particular case the response measured as shown in Fig. 6, using MC1-111 tape at a speed of 7½ in/sec. It rises by 6db per octave up to a frequency of 1,600c/s, then flattens out gradually and drops considerably above 6,000c/s. This is caused by losses due to selfdemagnetization, penetration and the gap effect1.

The response of the playback amplifier should be inverse to the curve shown in Fig. 6 and should therefore fall by 6db per octave from 40c/s per second (the lowest transmitted frequency) up to 2,500c/s. This is controlled by the frequency-selective feedback network between the anodes of V5 and V6 consisting of $R_{53}+R_{54}$, R_{56} ,

 C_{52} , R_{55} . The value of $R_{53}+R_{54}$ will determine the high-frequency turnover point, but leave the low-frequency turnover point unchanged as long as the other values of the network are retained. The playback amplifier characteristic may therefore be easily adapted to different tape speeds by changing the value of $R_{53}+R_{54}$.

C₅₁ belongs to the de-emphasis network and will be mentioned later. The respective values of these components are not specified and the reader is referred to the alignment procedure as outlined at the end of

this article.

As the output voltage at the playback head is extremely low, especially at low frequencies, the amplifier should be designed for minimum noise level. A triode-connected 12SJ7, with the heater d.c. fed, preferably from the main amplifier anode current, is used in the first stage, with an equivalent noise resistance due to shot effect of approximately

 $\frac{2.5}{2.5}$ ohms at the input³. To this is added the

flicker effect which increases with the square of the emission current, but decreases with the inverse square of the frequency4. Because of this frequency dependence, the flicker effect becomes appreciable at low frequencies where the amplification of the playback amplifier is just at its maximum value. The noise due to the flicker effect may however be held sufficiently low reducing the anode current of V5 by making R₅₇ $0.3M\Omega$.

Finally we come to the erase and bias oscillator Greatest possible freedom of harmonics is desired to ensure low noise level and low distortion of the recorded signal. It consists of a cathode follower type oscillator, the principle of which was described elsewhere². The variable feedback resistor P₃ provides a method of controlling the negative resistance injected into the tuned circuit with great accuracy. It may be adjusted to provide an amplitude of 8 volts at the cathode of V7. Under those conditions the grid-cathode voltage of that valve is small enough to ensure its linear operation, and such an oscillator will therefore provide an output containing less har-

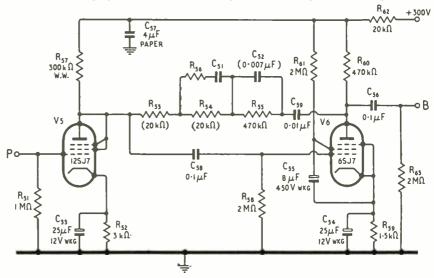


Fig. 5. Circuit diagram of playback amplifier. Values of R_{53} , R_{54} and C_{52} are discussed in the text. The heater of the first valve should be fed with d.c., preferably from main amplifier anode current.

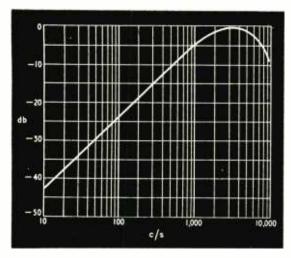


Fig. 6. Measured response at playback head, with constantcurrent recording.

monic distortion than a conventional one. However, its amplitude is not absolutely constant over a considerable time and therefore P_1 and M (Fig. 8) provide a means of adjusting the bias amplitude accurately during recording. The erasing head in the author's equipment was found to have an inductance of 29mH and an equivalent series resistance of 4,700 ohms at 60kc/s. It is brought to series resonance with C_{n0} (Fig. 8) thus providing the necessary load of 5,000 ohms for V8. In addition, the output voltage is stepped up, the Q of the circuit being about 2. This selectivity will also provide some attenuation of harmonics generated in the output valve.

It is important that C_{90} should be connected directly to the erasing head thus leaving the capacitance of the connecting cable in parallel with the tuned anode load of V8, which should resonate at the oscillator frequency of 60 kc/s.

+ 250 V Fig. 7. Circuit of erase and bias oscilla-R₈₄ \$ 35mH & tor. The stray capacitật Cas tance C₈₈ should re-S3 sonate with L₄ at 60 kc s. V7 ۷ø C 86 0-1 juF Cas 11 65.17 6V6 0.01µF C84 Rei 0.01µF 170kΩ $C_{/}^{82}$ R₈₃ 2·5 kΩ 0.01 µF ≷ R₈₅ 100 kΩ Res 50 kΩ C_{80} R₈₂ 60 kΩ 400 pF 35mH APPROX.20 R₈₆ C_{05} Cei 0-1 µF 250Ω 400 pF

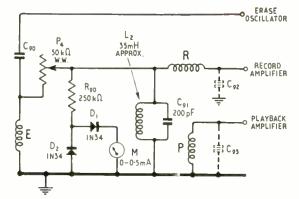


Fig. 8. Connections of magnetic heads and bias level meter. R, recording head: P, playback head: E, erase head. C_{92} and C_{93} are the capacitances of the connecting leads. C_{90} is adjusted to resonate with E at 60 kc/s.

The anode of the oscillator valve V7 is bypassed to earth with $8\mu F$ and consequently its anode voltage will decrease only gradually after interruption of the supply voltage by S_2 , which ensures slow damping out of the oscillations. This is important in order not to leave any magnetism in the erase and recording head after the oscillator is switched off. The relay L_3 , S_3 serves to short the erasing head to earth when the oscillator is inoperative. It should close only after the oscillations are completely damped out. This is accomplished by removing the copper rivet generally used in conventional relays. This rivet serves to prevent sticking of the relay due to remanent magnetism, after the current is interrupted. With this small alteration the relay will open with a certain delay and thus provide the necessary characteristic.

The recording bias is taken from the erasing head and is adjustable by P_1 (Fig. 8). The parallel tuned circuit L_2C_{91} resonates at 60 kc/s, thus forcing the bias current mainly through R and C_{92} (the capacitance

of the connecting cable), the voltage drop across the latter being negligible. The filter formed by P₄ L₂ C₉₁ will also provide additional attenuation of harmonics of the bias frequency.

The situation is different at recorded frequencies: L2 provides then a short circuit and C₉₂ will resonate with the recording head R somewhere above the highest transmitted fre-This method of quency. coupling was chosen in order to prevent the bias from entering the record amplifier and at the same time to maintain the high input impedance of R as seen by the record amplifier. Any capacitive load of the latter would considerably impair response at the highest audio frequencies due to its high output impedance.

A value of 200pF was chosen for C_{92} to resonate with the recording head used in the writer's equipment at 14,000 c/s. The voltage drop across that capacitance due to the bias will be fed into the record amplifier and, although small, it may give rise to beats with the recorded frequencies. It will, due to the feedback action of the amplifier, appear in antiphase at the grid of V2 with an amplitude determined by the voltage divider consisting of the cathode resistor and the internal resistance of V2. In order to keep this amplitude low a valve with a high internal impedance should be chosen for V2 and a 6SF5 having an internal resistance of about $60 \text{ k} \Omega$ was found to be adequate. However a pentode with an internal resistance of the order of a megohm may be chosen in extreme cases.

Circuit Adjustments

The values of the various components determining the frequency response should be found by trial and A signal generator providing frequencies between 40-15,000 c/s and a valve voltmeter calibrated in db are highly desirable. First the amplifier will be operated with C_1 , C_3 , C_{61} and C_{62} disconnected. The optimum bias may now be adjusted by means of P₄ using a signal of about 3,000 c/s. When increasing the h.f. bias from zero, the volume will rise and distortion will decrease considerably, until a maximum of volume is reached. A further increase of the bias will cause additional reduction of distortion but also of the volume. The optimum setting of P4 for minimum distortion will therefore slightly increase the signal-to-noise ratio, but minimizing the distortion is considered to be of primary importance. In the writer's equipment a bias of 135 volts across the recording head was found to correspond to minimum distortion.

After adjusting the bias, the amplification of the record amplifier may be adjusted by means of the feedback resistor R_1+R_2 (see Fig. 2) to deliver at the recording head a signal as specified by the makers of the tape desk. The response of the playback amplifier should now be plotted, yielding a curve similar to the one shown in Fig. 6. Then, taking the flat response between 2,500-4,000 c/s as the reference level, the value of C_{52} , $R_{53}+R_{54}$ may be found for flat response down to 40 c/s. $R_{56}C_{52}$ determines the low-frequency turnover and $R_{53}+R_{54}$, C_{52} the high frequency turnover. Now the treble boost provided by C_1 , R_1 , R_2 in the record amplifier may be adjusted to extend the frequency response at the high-frequency end. The time constant R_1C_1 determines the low-frequency turnover point and R_2C_1 the high-frequency turnover point.

In addition the response of the record amplifier at the high frequencies depends on the value of C_{92} , which works out as follows:

$$i_r \propto \frac{1}{R_{a2}(1 - \omega^2 L_R.C_{92}) + r_R + j\omega L_R \left(1 + R_{a2} \frac{C_{92}.r_R}{L_R}\right)}$$
 (5)

and the ratio of the response with C_{92} connected to the response without C_{92}

$$\frac{i_{r}}{i_{r}'} = \frac{R_{a2} + r_{R} + j_{\omega}L_{R}}{R_{a2}(1 - \omega^{2}L_{R}.C_{92}) + r_{R} + j_{\omega}L_{R}\left(1 + R_{a2}\frac{C_{92}.r_{R}}{L_{\omega}}\right)} (5a)$$

Consequently the response of the playback amplifier may be lifted at the high frequencies by a ratio indicated in equation 5a.

Additional treble equalization may be obtained by tuning the playback head to resonance at the high end of the transmitted frequency band. The capacities C_{92} , C_{93} may be fully or partly realized by the capacity of the connecting cables. An effective means of improving the signal-to-noise ratio is to use pre-emphasis for frequencies above 1000 c/s similar to the characteristic used for records. This may be introduced by the conventional network R_3 , R_4 , R_5 , C_3 connected to the input of the recording amplifier†. The loss of amplification due to this network may be compensated by decreasing the feedback from R_1 , R_2 .

As R_1 , R_2 , C_1 have been determined previously, the time constant R_1C_1 and R_2C_1 should remain unchanged in order not to affect this adjustment, The de-emphasis is incorporated in the feedback network of the playback amplifier and consists of

R₅₃, R₅₄, R₅₆, C₅₁.

If records are played with a magnetic pickup (giving constant output from constant velocity recording), they may be recorded on the tape without any correction of the frequency band above 1000 c/s, which will provide directly the wanted pre-emphasis characteristic.

The only correction applied in that case will then be the de-emphasis, incorporated in the playback amplifier.

† See, for example, "Radio Designers Handbook," by E. Langford Smith, p. 653.

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More Rectification

By "CATHODE RAY"

Far-reaching Effects of a Reservoir Capacitor

AST month we considered Fig. 1, the simplest possible rectifier circuit, reduced to its simplest possible terms, namely a resistanceless generator of pure sine waves feeding a pure resistance load through a perfect rectifier, i.e., one having no resistance at all to current in one direction and infinite resistance to current in the opposite direction. We considered the readings of perfect voltmeters of various types connected to read the three possible voltages in the circuit-across generator, load, and rectifier-and perfect ammeters to read the one possible current. And in spite of taking a long time over this apparently simple and straightforward job, we didn't even finish it. We drew up a table of readings given by three types of voltmeter: (1) the ordinary moving-coil type used for d.c., which responds to mean values; (2) the same with a full-wave rectifier to adapt it for a.c., which responds to mean values of rectified voltages, but is scaled to read r.m.s. values, which are 11% higher; and (3) the electrostatic or moving iron or any other type that actually responds to r.m.s. values as well as being scaled in them. Most valve voltmeters are outside all these categories because, although usually scaled to read r.m.s. values, they respond to peak values. Our first job now is to complete the table by filling in the entries for this type of meter.

Again let us assume that the instrument is perfect, so that the rather complicated matter of its errors doesn't arise. Now we know that the r.m.s. value of a sine wave is equal to its peak value divided by $\sqrt{2}$; in the usual symbols, $E = E_{max}/\sqrt{2} = 0.707E_{max}$. So to make the peak voltmeter read r.m.s. values directly, it is arranged so that it indicates 0.707 times the peak value. Consequently when connected across the generator in Fig. 1, where it sees waveform 2(a), it reads E, the r.m.s. value—like the other types of a.c. voltmeter.

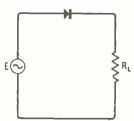
Next, connect it across the rectifier or the load. In either of these positions it sees waveform 2(b).

If the voltmeter has no blocking capacitor or transformer coupling it responds to the peak voltage from the zero line. Connected one way round, this peak voltage is E_{max} , and as the instrument is scaled to read 0.707 times this it reads E as before. If connected the other way round it receives only the half-cycle that has been removed by rectification, so the reading is nil.

But most valve voltmeters have a series capacitor,

Right: Fig. 1. The simplest possible rectifier circuit again.

Below: Fig. 2. Waveforms associated with Fig. 1: (a) across the generator; (b) across rectifier or load resistance; (c) after using a blocking capacitor on (b) to exculde the d.c. part.



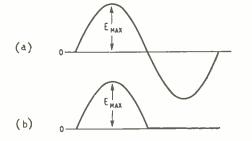




TABLE I

Type of voltmeter	Across generator (with or without blocking capacitor)	Across R _L or recti- fier (without block- ing capacitor)	Across R _L or recti- fier (with blocking capacitor)	
Mean (moving-coil)	0	0.450E or —0.450E	0	
Rectifier	E	0.500E	0.551E	
Square-law values of sine wave	Е	0.707E	0.545E	
Peak	E	or E	0.682E or 0.318E	

which blocks the d.c. component, and after the surge caused by the charging of this capacitor at the moment of connection has died away the voltmeter sees waveform 2(c). We have already found that the d.c. component is equal to the peak value divided by π , and the voltages are in the same proportion. So if connected one way the peak value is $(1-0.318) E_{max}$, and the other way $0.318E_{max}$; and the readings, being 0.707 times these, are 0.682E and 0.318E respectively.

So except across the generator, where the waveform is symmetrical, the reading of the peak voltmeter depends on which way it is connected; hence the two pairs of entries in Table I for this type. The only other reading that is affected by direction is the mean value, and that is not with regard to the actual value of the reading but only its polarity.

We must remember once more that if the generator provided some other waveform than sinusoidal, most of the figures in the table would be different. We noted before that if a rectifier meter were connected across a source of square waves (whose mean, r.m.s. and peak values are all equal) it would read 11% high—because it is designed to do this in order to allow for the inequality of the mean and r.m.s. value of sine waves. The inequality between peak and r.m.s. values is the other way around and greater; our compensated peak voltmeter would read square waves nearly 30% low.

Now for Current

No type of ammeter that I know reads in proportion to peak values. The only way would be to put a very low resistance in circuit, amplify the voltage across it, and measure that with a peak voltmeter. A cathoderary oscillograph would do as the amplifier and voltmeter. Any such arrangement would hardly be calibrated in either r.m.s. or mean values, so would not be comparable with other types of current meter. But while we are at it we might as well tabulate last month's findings for these other types (Table II).

Fig. 1 being a purely series circuit, there is only one current throughout, the waveform of which is as Fig. 2(b). But in the current table there are two columns of readings, because some meters receive the current directly, while others are coupled by a transformer, which eliminates the d.c. component. The moving-coil d.c. meter is always directly connected, for obvious reasons. But the rectifier meter can be connected either way, as in Fig. 3, and when it is used in a rectifier circuit the reading depends on which. In practice it is almost always transformer-coupled (b), because this allows the range to be varied by varying the number of primary turns in circuit. Fig. 3(a) only provides one range, up to the maximum rating of rectifiers and meter, because owing to the varying resistance of the rectifiers the range cannot be varied in the usual way by shunts. Lastly the squarelaw type, which is usually a heat operated instrument, because that can be accurately calibrated on d.c. The point to remember is that the true r.m.s. reading which it indicates (regardless of waveform) is, with a sinusoidal input to this simple circuit, 1.57 times the mean current, as read on a d.c. meter, so its heating power is $1.57^2 = 2.46$ times as much.

Having claimed so much of your valuable time on this absurdly simple(?) circuit, I may be running a grave risk of assault if I now calmly announce that it is of theoretical interest only, being rarely used in practice. But I hope that the effort may be seen to have been worth while, as a convincing warning against tackling even the simplest rectifier circuits and calculations without due care and attention. They are thoroughly deceptive things. That being understood, however, perhaps I can deal with the practical types more sketchily.

The reason why Fig. 1 is rarely used in that simple form is that d.c. in the Fig. 2(b) form is rarely desired. But the smoothing circuits needed to reduce it to pure d.c. have the incidental effect of radically altering the rectifier circuit. So let us now look into rectifier circuits modified by smoothing.

The simplest is Fig. I with a capacitor connected across R₁, as in Fig. 4(a). A closely related variety is Fig. 4(b). These come in for a great deal of attention, because they are so much used; nearly all detectors, nearly all valve voltmeters, and nearly all the rectifier circuits in a.c./d.c. sets are essentially one or other of these types. Quite recently they were discussed at some length from the valve voltmeter point of view.* Pages and pages of data appear on them in the Radio Designer's Handbook and indeed in most books on radio. So all I am going to do now is to outline how C in Fig. 4(a) affects the currents and voltages.

If we were to continue on our hitherto ideal lines, we would assume that C was infinitely large, so as to provide perfect smoothing. But these assumptions would lead to the generator being required to supply an infinitely great current for an infinitesimally small time during each cycle; and to avoid such arrant

* M. G. Scroggie, Wireless World, June, p. 294, and July, p. 339, 1954.

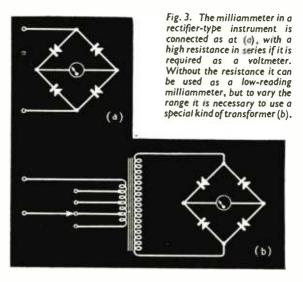


TABLE II

Type of ammeter	Directly in circuit	Trans- former coupled	
Mean (moving-coil)	Iar	0	
Rectifier Calibrated to read r.m.s.	1.11 I _{av}	1.22 I _{av}	
Square-law values of sine wave	1.57 I _a	1.21 I _{av}	

Peak value = πI_{av}

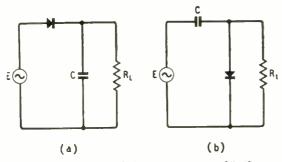


Fig. 4. Two varieties of the reservoir type of half-wave rectifier. (a) is used for power supply, and either (but usually (b)) for valve voltmeters.

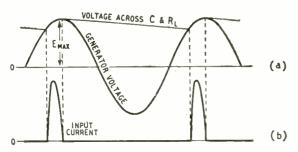


Fig. 5. Voltage and current waveforms for the Fig. 4 type of rectifier circuit.

nonsense we have to acknowledge the existence of resistance in the generator and rectifier (conducting phase). And this leads to all the complicated data and calculations referred to. However, the general picture is that when the rectifier conducts C charges up to nearly Emax; and, provided its capacitance is large enough to keep current flowing steadily through R_L during the rest of the cycle, its voltage remains not far short of E_{max} (Fig. 5(a)). Consequently it is only close to the peak that the generator voltage is great enough to overcome the capacitor voltage and make current flow through the rectifier. During this small fraction of the cycle, the generator has to supply enough current to C (Fig. 5(b)) to keep current going through R_L all the time. The larger C is the less its voltage drops below E_{max} , the shorter the time during which current enters it from the rectifier, and the heavier that current must be. It is quite usual for it to be five or even ten or more times the load current. In fact, in power circuits, having to supply a lot of load current, it is necessary to limit C, or to insert extra series resistance, or both, if the rectifier is to be preserved from an early death.

What about the meter readings and the actual currents and voltages? In valve voltmeters and detectors, where it is output voltage rather than current that counts, the resistance R_L can be made very high, and the load current consequently very low; so the output voltage is nearly steady at only a very little below E_{max} . (This is very different from Fig. 1, where the output voltage (Fig. 2(b)) is very unsteady and only momentarily reaches E_{max} , its average value being less than one third as much.) In these circumstances the output current is of course also steady at nearly E_{max}/R_L . But the generator current through the rectifier, although it is bound to have the same average value (as would be shown by a moving-

coil milliammeter), consists of a series of brief pulses. If these pulses were square-cut, then if they lasted one nth of each cycle they would be n times the load current. But being peaky their peak value is even greater than this. Almost the only practical way to measure it is by means of the c.r. oscilloscope across a low series resistance.

As you may have guessed from our experience with the Fig. 2(b) waveform, the true r.m.s. value of this current is much greater than its mean value. Suppose we take as an example a circuit in which the mean output voltage is 95% of E_{max} . Fig. 30.5 in Radio Designer's Handbook shows that if the series resistance (generator, rectifier, and any added) is 0.0005 R_L, the value of ωCR_L (time constant of the load multiplied by 2π times the frequency) is about 37. Fig. 30.8 in the same book then shows that (assuming constant rectifier forward resistance) the peak input current is nearly 20 times the mean output current, and the r.m.s. input current is about 3½ times the output. So although a d.c. milliammeter in series with the rectifier would indicate the same current as in R_L, its heating effect in a given resistance would be about $3\frac{1}{2}$ or 12 times as great! If one chose the gauge of wire for the transformer secondary (acting as the generator) on the basis of the d.c. meter reading, one would probably be able to burn one's fingers on the transformer after it had been running some time. That is if the rectifier, chosen on the same basis, was still rectifying, which would be unlikely. For power units it is uneconomic to attempt a 95% voltage yield; it is more usual practice for the output voltage, after allowing for the drop in further smoothing if any, to be equal to about E, say 70% of E_{max} . The peak current is then of the order of five times the output, and the r.m.s. value a little over twice. Even so, its heating value is some five times that of the same current after smoothing.

Readings to Take

The measurement procedure with this type of rectifier circuit, then, is to use an ordinary d.c. milliammeter for the output current. Multiplying this by R_L gives the mean output voltage. Comparing this with the peak input voltage (which is $\sqrt{2}$ times its measured r.m.s. value if sinusoidal waveform can be assumed) and knowing the component values, we can look up data sheets to find the r.m.s. and peak input currents, which are needed to design the transformer and choose the rectifier. If the data sheets are lacking, or we want to check them, it is necessary to have a true r.m.s. current meter (preferably a thermojunction type; but keep it shorted except when taking a reading, or it will almost certainly burn out when switching on!) and the low resistance and oscilloscope or sensitive peak voltmeter. A rectifier type of a.c. milliammeter is really more than useless almost anywhere in a rectifier circuit, because the readings it gives are quite different from what they purport to be. A rectifier voltmeter can be used to measure the generator voltage, provided pure waveform can be guaranteed; but even quite small generator impedance is enough to upset this guarantee, because of the very peaky current waveform.

Usually there are some additional smoothing components between C and R_L, and these affect the situation in rather a complicated way. But provided that C is relatively large, the basic action of the circuit as already described is not altered out of all

recognition. Apart from the actual smoothing effect, which I discussed in the October and November 1949 issues, the main practical point to reckon with is the voltage drop in the series smoothing components, and that is easy enough.

Although Fig. 4(a) is very widely used for power supplies, that is because it is almost the only choice in a.c./d.c. sets, and not because it is a good circuit for power supplies. Because the rectifier passes current only once per cycle, the current it does pass has to be so large that a high-rated rectifier must be used. And for the same reason the voltage drop between current pulses is apt to be large, and the output needs a lot of smoothing. When the source is definitely a.c., so that a transformer can be used, it nearly always is used, in order to take advantage of certain benefits obtainable therewith. One of the benefits is the ability to use both half-cycles of the source, replenishing the reservoir C twice per cycle. Another is the ability to step up the voltage, not only in the transformer itself but also by the arrangement of rectifiers. There is the centre-tapped transformer full-wave circuit, the rectifier-bridge full-wave circuit, two sorts of voltage doubler, and a voltage quadrupler, besides some rarer varieties. The first of these is the commonest, and the only one I am going to take for the present.

Fig. 6 is the basic circuit. I have drawn it that way, because it is how it usually appears in circuit diagrams; but obviously it would look simpler and clearer if C and R_L were drawn straight across between the transformer centre tap and the junction between the rectifiers. That would help to bring out the fact that it is really the same as Fig. 4(a) supplemented by a second rectifier fed by a source in opposite phase, to double the number of current input pulses per But except for the reduction in output voltage fall during the cycle, there is no increase in voltage obtained by the doubling of the end-to-end secondary voltage. For this reason it is not the circuit one would choose for high-voltage low-current output. Even an ordinary receiver requiring, say, 350 V., necessitates a considerably higher transformer voltage. Using our rough rule that in power units the output voltage is about equal to the r.m.s. input voltage, we see that the peak voltage of each half of the secondary is $\sqrt{2} \times 350 = 495$ V., so the total peak secondary voltage is practically 1,000-much too high for one's health if one gets it between the hands!

Assuming that the circuit is balanced—rectifiers and secondary half-windings identical—it is obvious that if we connect our moving-coil milliammeter in series with either rectifier it should read half the load current. In practice there is usually an appreciable unbalance, but it ought not to be more than 10 or 15 %. As with the half-wave circuit, the number of times the r.m.s. and peak values are greater than the mean depends on the component values and frequency. Approximately the same ratios-and output-voltage ripple—as in the half-wave circuit will be obtained in a full-wave circuit having everything the same, except for rectifier, etc., resistance being doubled on each side (because each carries only half the current) and C halved (because the ripple frequency is doubled).

Note that, although the voltage of the whole secondary coil in the full-wave circuit is in the same direction from end to end, so that the a.c. is likewise, the d.c. flows in opposite directions in the two halves.

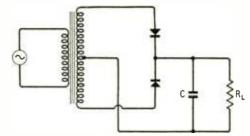


Fig. 6. Modification of Fig. 4(a) for full-wave rectification. This is the commonest type for supplying h.t. in a.c. receivers.

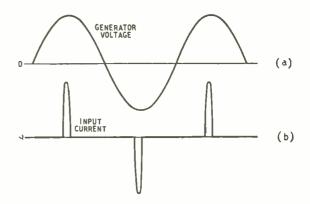


Fig. 7. Voltage and current waveforms in Fig. 6.

Consequently the core of the transformer is not magnetically polarized by d.c., as it is in the half-wave system, and this is a point in favour of the full-wave system. If it were not for the reservoir C, which distorts the current waveform into sharp peaks, the current would be sinusoidal, and the transformer would be working under the most comfortable conditions possible. As it is, however, the current is distorted, as in Fig. 7. Now here is a question. The r.m.s. value (E) of the transformer voltage is known, and for a given set of rectifier conditions and hence waveform the r.m.s. value (I) of the transformer current can be calculated. The question is, what is the power supplied by the transformer? Is it EI? In ordinary a.c. theory it would be, provided that E and I were in phase. Well, here they do seem to be, as near as makes no matter. But if you start calculating the power used up in the load, and add in the power lost in the rectifiers and transformer wire, you soon find that the power delivered by the transformer can't be accounted for on this basis. So, as there is no possibility of deceiving Nature's auditor with regard to the power balance sheet, the basis must be

Watch the Waveform

Well, it is just another example of how theory limited to sine waveform lets one down if applied to other waveforms regardless. As I mentioned some years ago while discussing phase,† it is not really allowable to compare the phases of dissimilar waveforms. It is true that the fundamental component of the Fig. 7(b) current is practically in phase with the

[†] Wireless World, May and June, 1948.

voltage, but the current is certainly not all fundamental. The peakier its waveform, the greater is the proportion in the form of harmonics. And while some half-cycles of these harmonics are admittedly flowing in the same direction as the generator voltage, others flow against it so represent negative power (i.e., power flowing back into the generator), and tend to cancel out the positive power. Just what the net result is necessitates a not-so-easy integration; but without knowing any integral calculus at all we can make sure that when the current is very peaky the power is not equal to EI. Suppose that the current is I_{max} for one-tenth of each half-cycle, from 81° to 99, and zero elsewhere. During this time the voltage varies from 0.988 E_{max} to E_{max} and back again. Its average is clearly above 99% of E_{max} , so we shall be near enough if we say it is E_{max} . The power during this period is therefore practically $E_{max}I_{max}$, and for the rest of the half-cycle is zero. The average power is therefore one-tenth of this—0.1 $E_{max}I_{max}$. Now compare this with EI. E is $E_{max}I_{max}$. While it is flowing, the current is I_{max} ; the current-squared is I_{max}^2 . I_{max}^2 ; the mean current-squared is $I_{max}^2/10$; the root mean current-squared or r.m.s. value is $I_{max}/\sqrt{10}$. So EI is $E_{max}I_{max}/\sqrt{20} = 0.223 E_{max}I_{max}$. In other words, the actual power is not EI but

$$\frac{0.1 \text{ EI}}{0.223} = 0.447 \text{EI}$$
 —

less than half what it would have been with a sine current waveform having the same r.m.s. value.

But although the r.m.s. value of the current, such as would be indicated by an accurate thermojunction milliammeter, doesn't necessarily count in reckoning power delivered, it counts only too well in reckoning heating of any resistance it passes through, so again it is the value that must be used for choosing the gauge of wire for the transformer secondary.

Summary

Let us sum up the voltage and current lore concerning the full-wave reservoir rectifier circuit. Voltages present little difficulty in practice: the "generator" (i.e. transformer secondary) usually supplies something reasonably sinusoidal, which can therefore be measured with any reasonably accurate voltmeter having an appropriate a.c. range. The significant voltage at the output is the mean value, measured with a moving-coil voltmeter. So far, the ordinary multi-range test meter is sufficient. The actual peak inverse voltage across either rectifier is important, but one doesn't usually bother to measure it, because the most it can be is a trifle less than twice the peak half-secondary voltage (or, if you prefer, a trifle less than the peak voltage across the whole secondary). The reason is pretty obvious: the greatest instantaneous voltage the generator can apply in the "wrong" direction is E_{max} , and at that moment C is also applying a voltage in the same direction, which at no-load would be very nearly E_{max} . So to be on the safe side the peak inverse voltage with this circuit is always taken as $2E_{max}$, or $2\sqrt{2E} = 2.8E$.

If one is interested in ripple voltage, then certainly complications do arise, because it has a decidedly non-sinusoidal waveform. But usually there is no need to distinguish very clearly between the several possible values—a rough idea will do. The peak value can be read by means of a peak valve voltmeter with blocking capacitor, or alternatively an oscilloscope.

Currents are trickier. There are:

(1) The mean value of the output current, measured by a moving-coil meter in series with R_L. This should equal the sum of the readings on the same meter connected to measure each rectifier current in turn.

(2) The peak value of the current through each rectifier. This is important for voltage rating. Use about 502 of resistance and a sensitive peak voltmeter or oscilloscope.

(3) The r.m.s. value of current through each rectifier. This is measurable with a thermal meter and is the one that must be used for calculating watts loss.

(4) The equivalent r.m.s. value of sinusoidal current in phase with the voltage. Presumably this could be measured by means of a suitable wattmeter, by dividing the watts supplied from the whole secondary by the r.m.s. voltage of the same. Lacking the suitable wattmeter (as most people do), one would have to reckon up the wattage bit by bit: chiefly the load power (load current × load voltage), plus twice the square of the r.m.s. current through either rectifier multiplied by the effective resistance of either rectifier and any limiting resistance in series with it.

(5) The ripple current through C. This is necessary for checking that the rating for the capacitor is not being exceeded. If a r.m.s. current meter is available, it can be read directly by connecting the meter in series with C. Because the ripple voltage waveform is far from sinusoidal—and the current waveform still farther from it, because the reduced reactance of C at higher frequencies favours the harmonics—the reading on a rectifier-type meter is likely to be somewhat out, but perhaps good enough for the purpose.

A disadvantage of the reservoir type of rectifier circuit, half-wave or full-wave, is that if the load is absent—as happens if the rectifiers come into action before the valves in the set have warmed up-the output voltage rises to nearly E_{max} . So if the smoothing capacitors have been chosen on a $E_{max}/\sqrt{2}$ basis they are not likely to be very happy during these periods. For this and other reasons (such as avoiding high rectifier peak current) use is sometimes made of the "choke input" circuit, in which a so-called swinging choke is connected between the rectifiers and C. This type of circuit works quite differently from any we have discussed, and would demand several pages to itself, moreover it is practically never used in domestic equipment, so I am only just mentioning it to show that when you have explored all the voltagedoubling etc. types there are still more worlds to conquer!

Receiving Valve Manual

VALVES for colour television are included in the latest edition (RC-17) of the well-known RCA "Receiving Tube Manual" which is now available in this country. The book has been revised, expanded and brought up to date, and contains technical data on more than 500 valves and c.r. tubes. There are also sections on basic theory, interpretation of data, applications, installation and testing which contain a good deal of new matter. The section on circuits now includes several new circuits for use in high-quality audio amplifiers. Among these are a low-distortion input amplifier stage, a two-stage input amplifier using cathode-follower output, a bass and treble tone-control amplifier stage and a complete 10-watt high-quality amplifier.

Priced at sixty cents in the U.S.A., the manual is available in this country from RCA Photophone, Ltd., 36, Woodstock Grove, Shepherds Bush, London, W.12, at 8s.

Pocket Wire Recorder

PLAYING times of up to 2½ hours are provided in the German-designed "Minifon 54" recorder which is to be distributed in this country by the "Emidicta" Division of E.M.I. Sales and Service, Ltd., 363, Oxford Street, London.

Measuring $6\frac{6}{8} \times 4\frac{8}{8} \times 1\frac{3}{8}$ in and weighing only $2\frac{1}{2}$ lb with batteries, the "Minifon" is a remarkable example of



"Minifon 54" wire recorder with lapel microphone and stethophone earpiece.

miniaturization, particularly in the mechanical drive mechanism and controls, which are of watch-like precision. A 12-V layer-built battery costing 5s 6d gives a running time of 10 to 15 hours. The motor, which is governed, drives a large diameter take-up spool which ensures a virtually constant winding speed of 11.8 in (30 cm)/sec: re-winding is at 2½ times this speed. The wire diameter is 0.002 in.

A three-stage amplifier using hearing-aid type valves is used for recording and playback, and runs from separate 1.5-V and 30-V batteries. The recorded frequency range claimed is 200-4,000 c/s and the quality of reproduction with saturation bias (a permaner magnet is used for erasure) is more than adequate for speech

erasure) is more than adequate for speech.

The basic price of the "Minifon 54" is £85 with batteries, 1-hour duration spool, lapel microphone, stethophone earpiece, and leather case. Numerous accessories are available including a wrist microphone, typists' footcontrol unit, mains power supply unit for the motor, and a pick-up coil for recording two-way telephone con-

News from the Clubs

Birkenhead.—The Wirral Amateur Radio Society continues to meet at 7.30 on the first and third Wednesdays of each month at the Y.M.C.A., Whetstone Lane, Birkenhead. Sec.: A. C. Wattleworth, 17, Iris Avenue, Claughton, Birkenhead, Cheshire.

Birmingham.—" Television Acrials" is the subject of the talk to be given by A. P. Hale, of Belling & Lee, to members of the Slade Rad'o Society at their meeting on November 12th at 7.45 at the Church House, High Street, Erdington. The annual general meeting will be held on November 26th. Sec.: C. N. Smart, 110, Woolmore Road, Erdington, Birmingham, 23.

Portsmouth.—The Portsmouth & District Radio Society now has its own club room, open every evening, at the British Legion Club, Queen's Crescent, Southsea. Meetings are held each Tuesday at 7.30. The November programme includes films (2nd), a lecture on television (9th) and a discussion on television interference (23rd). The club operates a QRP

transmitter, G3DIT. Sec.: L. B. Rooms (G8BU), 51, Locksway Road, Milton, Portsmouth, Hants.

Cleckheaton.—At the November 3rd meeting of the Spen Valley & District Radio & Television Society D. Skirrow (G3GFD) will speak on "Radio Valves and their Uses." The subject for the meeting on November 17th is "Oscilloscopes" by G. F. Craven, of Craven Electronic Instruments. Meetings are held at 7.30 at the Temperance Hall, Cleckheaton. Sec.: N. Pride, 100, Raikes Lane, Birstall, Leeds, Yorks.

Newark.—Technical films will be shown at the meeting of the Newark & District Amateur Radio Society at 7.0 on November 7th at the Northern Hotel, Newark. At the midmonthly meeting at Northgate House at 7.0 on November 18th a commercial trans-receiver will be demonstrated. Sec.: J. R. Clayton, 160, Wolsey Road, Newark, Notts.

Romford.—Meetings of the Romford & District Amateur Radio Society are held each Tuesday at 8.15 at R.A.F.A. House, 18, Carlton Road, Romford. Details of the winter programme, which includes lectures, discussions and films, are available from the secretary, N. Miller, 18, Mascalls Gardens, Brentwood, Essex.

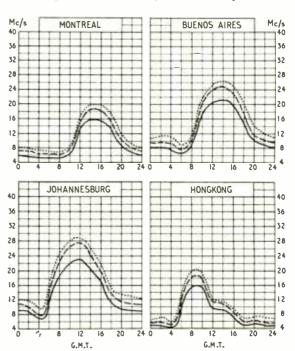
Southend.—Meetings of the Southend & District Radio Society are temporarily being held at the Ekco Works, Southend-on-Sea, on alternate Fridays at 7.45, the November meetings being on the 12th and 26th. Sec.: J. H. Barrance, M.B.E. (G3BUJ), 49, Swanage Road, Southend-on-Sea, Essex.

Short-wave Conditions

Predictions for November

THE full-line curves given here indicate the highest frequencies likely to be usable at any time of the day or night for reliable communications over four long-distance paths from this country during November.

Broken-line curves give the highest frequencies that will sustain a partial service throughout the same period.



FREQUENCY BELOW WHICH COMMUNICATION SHOULD
BE POSSIBLE ON ALL UNDISTURBED DAYS
PREDICTED AVERAGE MAXIMUM USABLE FREQUENCY
FREQUENCY BELOW WHICH COMMUNICATION SHOULD
BE POSSIBLE FOR 25% OF THE TOTAL TIME

WIRELESS WORLD, NOVEMBER 1954

versations.

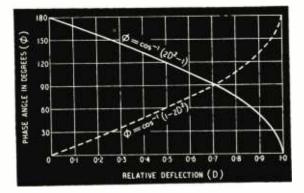
Measurement of Phase and Amplitude

Simple Method for Use with Feedback Amplifiers

By H. H. OGILVY, D.L.C.(Eng.), A.M.I.E.E.

T is well known that high-gain negative feedback amplifiers tend to become, in fact, positive feedback amplifiers at extreme frequencies and may, unless special phase shifting and attenuating circuits are introduced, actually oscillate and become useless for the purpose intended. Feedback amplifiers, such as those used for computing are especially likely to be troublesome, since the feedback is usually about 100%. It is very desirable to be able to measure the characteristics of a prototype amplifier so that the tendency to oscillate, or rather, the stability margin, may be determined and, if insufficient, the necessary steps taken to improve this margin. The data required to assess the performance is usually presented in the form of a Nyquist diagram, and the preparation of this diagram requires the measurement of relative phase and amplitude of output with respect to input under open loop conditions over a wide range of frequencies. In particular, the measurement of phase presents some difficulty.

The conventional method is to use a cathode-ray oscilloscope and estimate phase from a Lissajous



sine waves of equal amplitude and frequency, but with different phases.

Fig. 2. Schematic diagram of

phase measuring apparatus.

Fig. 1. Relative amplitudes resulting from the addition of two

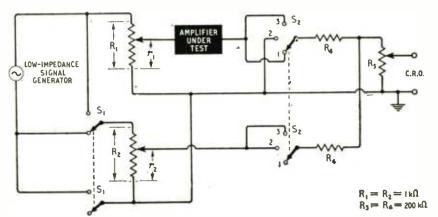


figure. This is rather clumsy and uncertain since the characteristics of the C.R.O. amplifier cause phase shift, particularly at the lower and upper frequencies. Commercial equipment is available for the measurement of phase, but is usually rather costly and complex. The method to be described is simple and economical.

If two sine waves of the same amplitude and frequency but differing in phase by an angle ϕ are added together, the resultant is also a sine wave, i.e., the resultant,

$$v = V \sin \omega t + V \sin(\omega t + \phi)$$

$$= V \sin \omega t + V \sin \omega t \cdot \cos \phi + V \cos \omega t \sin \phi$$

$$= V(1 + \cos \phi) \sin \omega t + V \sin \phi \cos \omega t$$

$$= V \sqrt{(1 + \cos \phi)^2 + \sin^2 \phi} \sin (\omega t + \alpha)$$

where
$$\alpha = \tan^{-1} \frac{\sin \phi}{1 + \cos \phi}$$

$$= V\sqrt{\cos^2\phi + \sin^2\phi + 1 + 2\cos\phi}\sin(\omega t + \alpha)$$

= $\sqrt{2}V\sqrt{1 + \cos\phi}\sin(\omega t + \alpha)$

Hence the amplitude of the resultant is proportional to $\sqrt{1+\cos\phi}$ where ϕ is the phase angle. The deflection of a C.R.O. or a moving coil rectifier instrument would therefore be dependent on this function. The maximum value of $\sqrt{1+\cos\phi}$ occurs when $\phi=0$ and if full-scale deflection (D=1) on the indicating instrument occurs when $\phi=0$ then $D=K\sqrt{1+\cos\phi}$, where K is a constant. Hence $1=K\sqrt{1+1}$ and

$$K=1/\sqrt{2}$$
 and therefore $D=\frac{1}{\sqrt{2}}\sqrt{1+\cos\phi}$ or $\cos\phi=2D^2-1$ and $\phi=\cos^{-1}(2D^2-1)$.

Fig. 1 shows the curve relating phase angle to relative deflection (full line). Phase angles between 80° and 180° are easily determined from the deflection, but below 80° the rate of change of phase with deflection becomes too great for reasonable accuracy of

observation. However, if the reference signal, Vsin ωt is reversed in phase the resultant wave is now

 $v = - V \sin \omega t + V \sin (\omega t + \phi)$

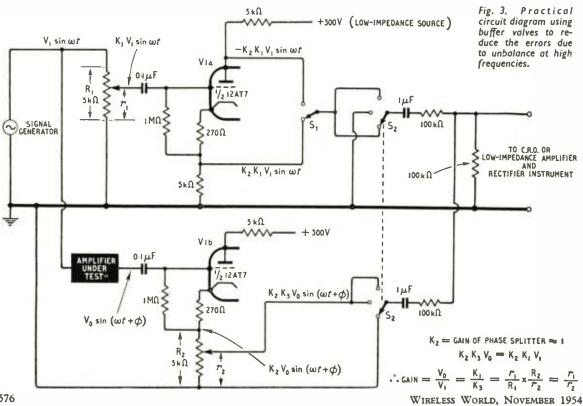
and this gives a resultant amplitude of $\sqrt{2V}\sqrt{1-\cos\phi}$. The relative deflection (D) is now 0 when $\phi = 0$ and 1 when $\phi = 180^{\circ}$, if the constant of proportionality is obtained as before. Hence the expression $\phi = \cos^{-1}(1 - 2D^2)$ is obtained and this is also plotted in Fig. 1 (broken line) showing that phase angles between 0° and 100° may be accurately determined. It should be understood, of course, that this method does not differentiate between leading and lagging angles, but where there is a doubt the sense can be easily determined. In general, the condition required, i.e., that both signals to be compared must be of equal a nplitude, will not apply but the method to be described shows how this may be achieved quite simply.

The basic scheme for measurement of phase and amplitude is shown in Fig. 2. It is assumed that a low-impedance signal generator is fed into two potentiometers of equal and relatively low resistance (about 1,000 ohms). With the switch, S1, in the position shown, equal antiphase voltages are available at the wipers of R₁ and R₂ with respect to earth. This condition is therefore suitable for the measurement of phase angles between 0° and 100°. The amplifier under examination is fed from the wiper of R₁ which is set to some convenient value $(=r_1)$ sufficiently small to avoid saturation of the amplifier. With S_2 in position 1 the deflection of the C.R.O. is adjusted, using R₅, to 50% of a predetermined arbitrary magnitude. S₂ is then placed in position 2 and R₂ adjusted for the same deflection $(=r_2)$. The condition of equality of amplitudes has thus been achieved and the ratio $r_2 r_1$ is obviously the gain of the amplifier at the particular frequency.

If S_2 is now placed in position 3, the output of the amplifier = V sin $(\omega t + \phi)$ is now added to the reference = $-V \sin \omega t$ in the network R_3 , R_4 and R_5 . The arbitrary full scale deflection will occur when $\phi = 180^{\circ}$. The relative deflection obtained will be according to the law $\phi = \cos^{-1}(1 - 2D^2)$ and ϕ may be determined from the curve in Fig. 1.

For phase angles greater than 100°, S, should be placed in the upper position and then $\phi = \cos^{-1}$ $(2D^2 - 1)$. In the majority of cases, the sense of the phase angle will not be in doubt. Where there is uncertainty, however, the sense may be determined by making the output of the amplifier lag, using a simple RC circuit and repeating the above procedure. If the angle obtained has increased, then the original angle must have been negative or lagging. The facilitate measurements, the C.R.O. time base should be switched off, except when checking the amplifier output for saturation.

Although the scheme shown in Fig. 2 will be satisfactory for many purposes, there may be errors in measurement at the higher frequencies due to unequal impedances to earth at the terminals of the signal generator. Also, in some applications, it may be undesirable to load the device under test, even though the load (R₃) is several hundred thousand To overcome these difficulties, the circuit shown in Fig. 3 is suggested. This presents a very high impedance to the amolifier. Phase splitting is obtained electronically by V1a which is one-half of a double triode (12AT7). The measurement procedure is the same as before. The potentiometer R₅, may be fed into an amplifier of low output impedance and used to drive a moving coil rectifier meter. convenience this meter may be scaled according to the law relating phase angle (ϕ) to relative deflection (D) (Fig. 1) and phase read off directly.



NOVEMBER

Institution of Electrical Engineers

London.-November 8th. Discussion

on "Methods of Teaching Technical Writing" opened by G. Parr at 6.0.
November 10th. "Standard Frequency Transmissions" by L. Essen, D.Sc., Ph.D., at 5.30, followed by "The Standard Frequency Monitor at the National Physical Laboratory" by J. McA. Steele, B.Sc.(Eng.), and "Standard Frequency Transmission Equipment at Rugby Radio Station" by

H. B. Law, B.Sc.Tech.
November 16th. Celebration of the Jubilee of the Thermionic Valve com-mencing at 2.30 with the address of the Lord President of the Council, the the Lord President of the Council, the Marquess of Salisbury, followed by "The Genesis of the Thermonic Valve" by Professor G. W. O. Howe, D.Sc., LL.D. At 3.30 "Thermionic Devices from the Development of the Triode up to 1939" by Sir Edward Appleton, D.Sc., LL.D., F.R.S., and at 5.30 "Developments in Thermonic Devices since 1939" by J. Thomson, M.A., Ph.D., D.Sc.

November 22nd. "Plastics for the Radio Engineer" by Maldwyn Jones at 5.30.

5.30.

November 23rd. "The Application of the Hall Effect in a Semi-Conductor to the Measurement of Power in an Electromagnetic Field" by Professor H. E. M. Barlow, Ph.D., B.Sc.(Eng.), at 5.30 followed by "Audio-Frequency Power Measurements by Dynamometer Wattmeters" by A. H. M. Arnold, Ph.D. D. Fing.

Ph.D., D.Eng. November 30th. Discussion on "The Servicing of Electronic Measuring Instruments and its Effect on their Design" opened by Denis Taylor,

M.Sc., Ph.D., at 5.30.
All the above meetings will be held at Savoy Place, London, W.C.2.

East Midland Centre.—November 9th.

East Midland Centre.—November 9th.
"Properties and Application of High
Permeability Magnetic Alloys" by
G. A. V. Sowter, Ph.D., B.Sc., at 6.3)
at Loughborough College.
November 23rd. "Telemetering for
System Operation" by R. H. Dunn.
B.Sc., and C. H. Chambers, at 6.30 at
the Gas Dept., Demonstration Theatre,
Nottingham.

Nottingham.

November 26th. "A Radio Position Fixing System for Ships and Aircraft" by C. Powell at 6.30 at the College of

Technology, Leicester.

North Midland Centre.—November 9th. Discussion on "The New I.E.E. Examination Regulations" opened by E. C. Walton, B.Eng., Ph.D., at 6.30 at 1, Whitehall Road, Leeds.

1, Whitehall Road, Leeds.

North - Western Radio Group.—
November 24th. "The ManchesterKirk o'Shotts Television Radio-Relay
System" by G. Dawson, B.Sc., L. L.
Hall, K. G. Hodgson, B.A., R. A. Meers,
and J. H. H Merriman, M.Sc., at 6.45
at the Telephone House, Chapel Street,

South Midland Centre.—November 22nd. "Loudspeaker Systems—Recent Trends in Design" by Major A. E. Falkus, B.Sc.(Eng.), at 6.0 at the James Watt Memorial Institute, Great Charles Street, Birmingham.

November 25th. "Colour Television" by C. J. Hirsch at 7.15 at the Winter Gardens Restaurant, Gt. Malvern.

Reading District.—November 29th.
"Television Interference" by K. R. Seamans at 7.15 at the George Hotel,

MEETINGS

British Institution of Radio Engineers

London Section.-November 24th. London Section.—November 2+th.

"The Development and Design of Direct-Coupled Oscilloscopes for Industry and Research" by M. J. Goddard at 6.30 at the London School of Hygiene and Tropical Medicine, Keppel Street, W'.C.1.

Scottish Section.-November Scottish Section.—November 4th.
"The Latest Developments in TV
Cameras" by H. McGhee at 7.0 at the
Institution of Engineers and Shipbuilders, Elmbank Crescent, Glasgow.

Merseyside Section.—November 4th.
"Radio Receiving Valve Manufacture"
by G. P. Thwaites, B.Sc., at 7.15 at the
College of Technology, Byrom Street, Liverpool, 3.

North-Western Section. - November "Electronic Servo Mechanisms

by J. L. Russell at 7.0.

November 30th. "Electronics and the Wind Tunnel" by G. J. Scoles, B.Sc., at 7.0.

at 7.0.

Both meetings will take place at the Reynolds Hall, College of Technology, Sackville Street, Manchester.

North-Eastern Section.— November 10th. "Stereophonic Sound" by R. A. Bull, B.Sc.(Eng.), at 6.0 at Neville Hall, Westgate Road, Newcastle-upon-Tyne. South Wales Section.—November 17th. "The Techniques of Power Measurements from D.C. to 5 Mc/s" by G. F. Lawrence at 6.30 at the College of Technology, Cathays Park, Cardiff.

British Sound Recording Association

London.—November 19th. "Balance and Control" by G. Elliott at 7.0 at the Royal Society of Arts, John Adam Street, W.C.2.

Manchester Centre.—November 22nd.
"Transformers and Chokes" by J. S.
Holiday at 7.30 at the Engineers' Club,
Albert Square, Manchester.

South-Western Centre.—November 24th. "Hi-Fi Can Be Music" by N. C. Mordaunt (Tannoy) at 7.30 at Callard's Café, Torquay, Devon. (Joint meeting with Incorporated Practical Radio Engineers).

Physical Society

November 5th. Duddell Lecture, "The Development and use of Large Radio Telescopes," by Professor A. C. B. Lovell at 5.0 at Burlington House, London, W.1.

Television Society

London.—November 12th. "Faulty Interlacing" by G. N. Patchett, Ph D., B.Sc., at 7.0 at the Cinematograph Exhibitors' Association, 164, Shaftesbury Avenue, W.C.2.

ı8th. Conversazione Novembe November 18th. Conversazione to mark the Jubilee of the Invention of the Thermionic Valve at 7.0 at University College, Gower Street, W.C.2.

November 25th. "European Television Programme Exchanges" by MALL REGION OF EMARCH P. C.

M. J. L. Pulling, O.B.E., M.A., (B.B.C.) at 7.0 at the C.E.A., 164, Shaitesbury Avenue, W.C.2.

Affecting Quality in Colour Television" by I. J. P. James, B.Sc., at 7.15 at the Gaumont-British Theatre, Film House, Wardour Street, W.1.

Radio Society of Great Britain

November 19th. Technical films at 6.30 at the I.E.E., Savoy Place, London, W.C.2.



gressive design and high-grade workmanship. There are standard units for every requirement. each a masterly expression of sound-reproduction technique. For large or small installations, our catalogue and expert advice are freely at your disposal.

MODEL G 7822 This new Ribbon microphone superlative perform-ance and attractive streamlined appearance, is of exceptionally small size and weight, measuring only 1 gin. in diameter.

With high sensitivity and minimum of feedback effects, it can be supplied in satin chrome or bronze finish, and with ad-ditional switch-box attachment if desired.





MODEL RE48. A heavy duty, reflex type, weatherproof horn speaker with

exceptional range and performance. Very suitable for all public address

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WIRELESS WORLD, NOVEMBER 1954

RANDOM RADIATIONS

By "DIALLIST"

TV Interference with Radio

THERE IS perhaps far more interference radiated by television receivers, to which I. Platts and G. O. Thacker refer in last month's Wireless World, than is generally realized. Many owners of broadcast receivers have come to regard any unwanted noise from the loudspeaker as just one of those things and don't know that, if they will only report it, the P.O. engineers will do their best to help. No one should be allowed to operate a television receiver which spreads alarm and despondency among his listening and viewing neighbours. But the P.O. anti-interference people either don't realize the existence of clause No. 4 of the television licence schedule or have been instructed not to enforce it-or to prohibit the use of the offending set (under clause 7) until it has been rendered innocuous.

A Bit Much?

The people really to blame, of course, when television interference is broadcast, are not the users but the manufacturers. It never occurs to the ordinary completely non-technical buyer of a TV receiver that the set of his choice may possibly cause various unpleasant things to happen to his neighbours' receivers whenever he switches it on. The advertisements assure him that it is the best of the lot; his wife likes the cabinet; the 17-inch tube will take the wind out of the sails of the Robinson's 15-inch next door. He puts down his money, or signs a "never-never" agreement, and feels that a good job has been well done. Can't you imagine his indignation and his "Pygmalion" retort when the P.O. engineers diffidently suggest that he should have something done to his beautiful set and pay for it? A warning to manufacturers by the P.M.G. that after a certain not-too-far ahead date a ban on the use of interfering receivers would be enforced might work wonders. The new B.R.E.M.A. standards for manufacturers should bring about a great improvement; but not all makers of television receivers are members of the association.

Anti-Flutter

WITH the rapid expansion of both civil and military aviation each year

sees more and more planes in the air. Unless we live in remote places they now pass over or near our homes at all hours of the day and night. Aeroplane flutter is already one of the commonest kinds of interference with television, particularly in places near aerodromes, or on regular flying routes. No form of a.g.c. seems able to cope adequately with flutter. for the time constants of the circuits are too long. Here's an opportunity for someone to develop an effective system of "automatic flutter suppression." It's sure to be done some day. As a dweller within a couple of miles of a big and busy aerodrome. I hope fervently that it may come soon.

All-Dry Sets

THE "ALL-DRY" receiver has many attractive points; and there is still more to be said for the kind that can be worked from the mains or from its own batteries. The "pros" for both sorts are that they are light, genuinely portable and of small size. But there is one serious "con" and that is the comparatively short life of the rather expensive combined h.t. and l.t. battery. Actually, it's the filament part of this battery which passes out, as a rule, and leads to distortion and, eventually, to a signal

too weak to be of any use. When the filament section has packed up the h.t. cells would usually be good for many more hours of useful service. Would it not be a great improvement if the h.t. and l.t. dry batteries were separate units? I haven't a doubt that it would; nor should there be any difficulty about it for set makers or battery manufacturers.

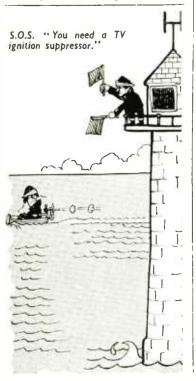
Time by the Forelock

DURING a recent visit to East Anglia I noticed over one house the familiar vertical H television aerial and a very much smaller horizontal array. The orientation appeared to be about right for Wrotham; but could this moderately powered f.m. transmitter possibly be receivable at so great a distance? The answer came a day or two later when I happened to meet the owner of the house. "Do you find Wrotham any good here?" I asked. "Wrotham," he said; "What's that?" "Why, the B.B.C. experimental f.m. station. Isn't that what your horizontal array's for? "He laughed: "Oh no," he said, "that's for Norwich, when it gets going." Nothing like being in good time! The temporary Norwich TV station, using, I believe, the present channel 3 Brighton "booster" as its transmitter, isn't due to make a start for 5 or 6 months yet.

Modern Mains Receivers THE thing that I like least about our mains receivers of to-day is that the

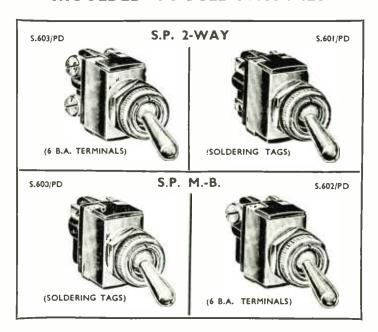
"WIRELESS WORLD" PUBLICATIONS ILIFFE By Post RADIO LABORATORY HANDBOOK. M. G. Scroggie, B.Sc., M.I.E.E. 6th Edition 25/- 26/3 RADIO VALVE DATA. 4th Edition Compiled by the Staff of "Wireless World" 3/10 SHORT-WAVE RADIO AND THE IONOSPHERE. T. W. Bennington, Engineering Division, B.B.C. Second Edition. 10/6 10/10 SUPERHETERODYNE TELEVISION UNIT. Second Edition. 2/6 2/8 INTRODUCTION TO VALVES. R. W. Hailows, M.A. (Cantab.), M.I.E.E., and H. K. Milward, B.Sc. (Lond.), A.M.I.E.E. ... 8/10 WIRELESS WORLD TELEVISION RECEIVER MODEL II: Complete constructional details with notes on modernizing the original design 3/9 RADIO INTERFERENCE SUPPRESSION as Applied to Radio and Television Reception. G. L. Stephens, A.M.I.E.E. ... 10/6 10/11 SOUND RECORDING AND REPRODUCTION. A B.B.C. Engineering Training Manual. J. W. Godfrey and S. W. Amos, B.Sc. (Hons.), A.M.I.E.E. 30/- 30/8 ADVANCED THEORY OF WAVEGUIDES. L. Lewin 30/- 30/7 FOUNDATIONS OF WIRELESS. M. G. Scroggie, B.Sc., M.I.E.E. 5th Edition ... 12/6 13/-TELEVISION RECEIVING EQUIPMENT. W. T. Cocking, A complete list of books is available on application. Obtainable from all leading booksellers or from ILIFFE & SONS LTD., Dorset House, Stamford Street, London, S.E.I.

great majority are built on a.c./d.c. lines with no transformer between them and the supply mains. On d.c. there's nothing much amiss, for neither sound nor television receivers will work unless the mains plug is put the right way round into its socket. But on a.c. both will function whichever way it's inserted. According to the law of averages this means that at any time half the mains sets operated on a.c.—say 5,000,000 "sound" and 1,500,000 television -are working with their chassis directly connected to the phase wire and with nothing earthed. thought of all those acres of chassis swinging through 500-700 volts peakto-peak 50 times each second must be a rather solemn one to any electrical engineer brought up on the old sound principles. Ours is, I believe, the only civilized country in which this sort of thing is permitted and I can't help feeling sorry that the I.E.E. regulation about the use of an isolating transformer between a.c. mains and apparatus was ever relaxed. But there it is, and we've got to make the best of it. As a safeguard, my suggestion is that all mains leads should be fitted with sockets which can be connected in one way only to the plugs in the receiver and that at the other end there should be a 3-pin plug. Those who install receivers should be required to see that the a.c. power supply is from a correctly connected 3-pin socket.



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ALL-MOULDED-INSULATION SINGLE-POLE Q.M.B. SNAP-ACTION TOGGLE-SWITCHES

THESE entirely new BULGIN Miniature Toggle Switches have been introduced to meet a need which will grow, for switches with all-moulded insulation and high test-voltage, with maintained high-insulation- $M\Omega$ even under adverse climatic conditions, or for switching to high- Ω "loads." They continue the firmly-established BULGIN reputation for reliable snap-toggle-Q.M.B. switches, meeting new needs. Alternatives with ball-dolly can be supplied.

BRIEF SPECIFICATION

Moulded Body and internal insulation of Thermo-setting Bakelite to Grade II/M, R.C.S.1000. Brass moving- and H.C.-copper fixed-Contacts with heavy SILVER-plating (to R.C.S.1000/7/2/2/2 if requested, and if ordered in quantity). External Metal parts heavily Nickel-plated, B.S.1224 (case=steel; Bush, dolly, nuts-Brass).

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By FREE GRID

Stars or Sunspots?

FORECASTING the future by means of the calculated positions of the heavenly bodies at certain given times is known as astrology when carried out by Madame Estelle or by those journals which cater for the unlettered masses, and astronomy when employed by the Astronomer Royal to give us the dates and times

of tides and eclipses.

Now, astrologers usually confine their prophecies to things like love, marriage and other disasters which depend on the whimsy of women and it is not very surprising therefore, that their percentage of success is so low. The Astronomer Royal on the other hand, eschewing women and their ways, bases his forecasts on the solid rock of science and so obtains 100% success.

I draw attention to these facts because something quite new in the realm of these stellar forecasts has made its appearance and this something concerns we radio men very much indeed. A super-modern stargazer hailing from the U.S.A. claims to be able to forecast ionospheric conditions for radio transmissions at certain times by studying the stars

instead of sunspots.

This celestial observer has secured the backing of one of the largest radio organizations in America, which has published figures showing that his successful forecasts represent 92% of the whole. However, in the opinion of some British ionospherists, this rather startling figure is obtained by a method of relating forecasts to ionospheric disturbances which, technically speaking, is open to

question.

I am inclined to agree with this opinion, although I think we ought to give this planetary pundit more rope with which to hang either himself or us. Any good racecourse tip-ster can produce first-class results over a limited period but he cannot keep it up. Indeed, we had a re-markable instance of this sort of thing in the middle of the war when the editor published a letter under the heading of "What the Sunspots Foretell."* The writer of this letter pointed out a striking correlation between the sunspot cycle and the career of Hitler and then proceeded to use this correlation to prophesy the end of the war with some degree of accuracy.

" History is Bunk"

WHY is it that the Radio Industry Council took such pains to stress that this year's radio show was the 21st

* The letter mentioned by Free Grid was published in our March 1942 issue.—ED.

when actually it was the 25th? believe that the official explanation is that the shows of the 1922-25 period were not "National" shows, and yet in a potted "Radio Show History" which the R.I.C. issued to the Press at the time of the show we are told that one of them was promoted by the National Association of Radio Manufacturers and Traders (NAR-MAT). What the R.I.C. means, I suppose, is that the pre-1926 shows were not organized by its progenitor -the Radio Manufacturers' Association-because it was not until that year that this new name-and a new constitution too-was adopted. It is as though the B.B.C. issued a history of British broadcasting and ignored the pre-1927 years because the service was then conducted by the British Broadcasting Company and not the British Broadcasting Corpora-

The "historian" picks out homeconstruction as the one thing worthy of mention at the 1924 show and completely ignores the fact that a valve with the then unheard-of amplification factor of 20 was shown. This was also the first show at which the superhet was seen; two very

prominent firms exhibiting it.
This official "history" describes
the superhet as one of the novelties of the 1927 show, whereas in actual fact it was rather in eclipse then. It did not start to stage a real comeback until over three years later, as I myself mentioned in W.W. for September 17th, 1930. The real novelty about which everyone was talking in 1927 was the screen-grid valve. And so I could go on.

Sackcloth and Ashes

I CERTAINLY put my foot in it when I said in the October issue that the smallest tape recorder available weighed 12 lb and was far from pocketable. I have had several letters pointing out to me that there is one on the market weighing only 2½ lb which is really pocket-size. As it is described elsewhere in this issue, I will say no more about it except to plead in my defence that at the time I wrote I don't think this instrument was available in this country; I won't split hairs by claiming that I said tape recorder, whereas this instrument uses wire.

Electronic Pulse Taking

LAST JUNE I suggested that the present method of pulse-taking in hospitals was out of date, likely to be very misleading and a gross waste of the nurses' time. I pointed out that this could be done electronically



The Palpatron

and automatically. By means of a miniaturized v.h.f. transmitter strapped to each patient's wrist and a receiver with a battery of c.r. tubes in the ward-sister's room, heartbeats could be read at any moment and, if desired, recordings could be made on film or magnetic tape.

Now I learn from the leading journal of the nursing profession (Nursing Mirror, August 27th) that an electronic device called the Palpatron is in use for this purpose at the Boston City Hospital, Massa-chusetts, U.S.A., and that its great sensitivity enables a pulse reading to be detected when nothing can be discerned by the normal manual method.

Τηλεόρασις

THROUGH the courtesy of a reader I learn that the terrible word τηλεβισιου is not used in modern Athens for television. No doubt some of you noticed that there was an unfortunate typographical error in my note last month, the omicron being omitted. The modern Greek word is τηλεόρασις but I don't think we should have taken kindly to teleorasis instead of television. same reader tells me of an excellent and up-to-date telecommunications dictionary of English and Modern Greek, published by the Sivitanideos Institution in Athens, with funds provided by the American Mission (European Co-operation Administration) in Greece.

WIRELESS WORLD, NOVEMBER 1954



An inexpensive yet precision instrument designed especially to meet the exacting needs of the modern service engineer and laboratory technician. frequency ranges covering 50 Kc/s. to 80 Mc/s., its accuracy is better than \pm 1% of the scale reading.

50Kc/s.-150Kc/s. 1.5Mc/s.-5.5Mc/s. 500Kc|s.-1.5Mc|s. 20Mc|s.-80Mc|s. 150Kc/s.-500Kc/s. Scale sub-divisions provide more than adequate discrimination for use in tele-Note the starred features below, which combine to vision circuits. maintain a minimum signal of less than 1µV up to 20 Mc/s, and less than 3µV between 20 Mc/s. and 80 Mc/s.

Co-axial socket for attenuated output. Force socket located totally within H.F. compartment. *OUTPUT_

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H.F. COMPARTMENT and CHASSIS *CAST ALUMINIUM Large number of fixing holes for H.F. compartment cover ensures excellent electrical bonding and good

Easily accessible when replacement is necessary. screening. 5 FUSE

Standard types run at a rating to ensure long life. VALVES TURRET COIL SWITCHING

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carbon resistors, low reactance rotary potentio-meter modified for H.F. operation with carefully designed screening.

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This is screened from main electrical assembly. *MAINS FILTER SYSTEM

provide additional rigidity for rotary controls.

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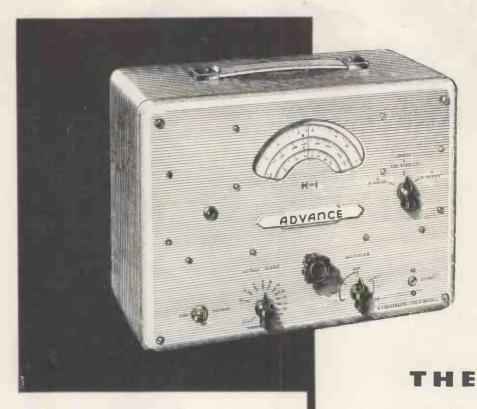
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Full technical details available in Folder W/16.

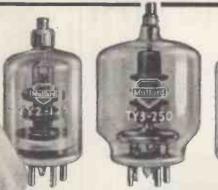
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	Small size
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Ten features to bear in mind—plus the assurance that these valves are already being widely employed with marked success in both communications and industry. The triodes TY2-125 (CV1924) and TY3-250 are recommended for grounded-grid R.F. amplifiers in communications equipment and as oscillators in compact R.F. heaters.

The tetrodes QY3-125 (CV2130) and QY4-250 (CV2131)—included in the Services Preferred Types List—are characterized by high power gain and high efficiencies at V.H.F.

Detailed information on the above range and other V.H.F. valves made by Mullard may be readily obtained from the address below.

MAXIMUM OPERATING CONDITIONS (CLASS C TELEGRAPHY) at 50 Mc/s							Max.		
Valve	Type of Service	∨a (∨)	VgI (V)	la (mA)	lgl (mA)	vin(pk) (V)	P load (W)	(%)	frequency (Mc/s)
TY2—125 (CV1924)	ampl.	2500	-200	205	40	390	310	76	200
TY3—250	ampl.	3000	-250	365	69	430	670	77	150
QY3—125 (CV2130)	ampl.	3000	-150	167	6.5	300	300	75	200
QY4-250 (CV2131)	ampl.	4000	-225	312	9	374	800	80	120



An outstanding general purpose communication receiver



Justly acclaimed as Britain's finest post-war communication receiver the BRT 400 D is in widespread use by Military, Post and Telegraph and Broadcasting authorities throughout the world.

Combining first-class performance with a wide range of facilities, the BRT 400 D is equally suitable for both narrow-band telegraphy and wide-band telephony reception—with a very high standard of reliability.

It is available in either cabinet or rack mounting form, with a 500 kc/s crystal calibration unit as an optional extra. Normal operation is from an A.C. mains supply: an auxiliary power unit is available for 12 volt battery operation.

9.6.C.

BRT 400D

SHORT SPECIFICATION

BAND COVERAGE

0.150—0.385 Mc/s o.510—30.0 Mc/s in 6 bands

SENSITIVITY

Better than 1.0 μV for 1.5 watts output, over the whole band.

SIGNAL/NOISE RATIO

Standard input for 20 db:-

1.3—30.0 Mc/s < 7.0 μ V 0.150—1.3 Mc/s ... < 10.0 μ V

SELECTIVITY

Six switched bandwidths:-

OVERALL FIDELITY

Less than 2 db down at 50 c/s Less than 6 db down at 5,500 c/s

A.G.C. CHARACTERISTICS

Output constant within 3 db for 100 db change in signal input.

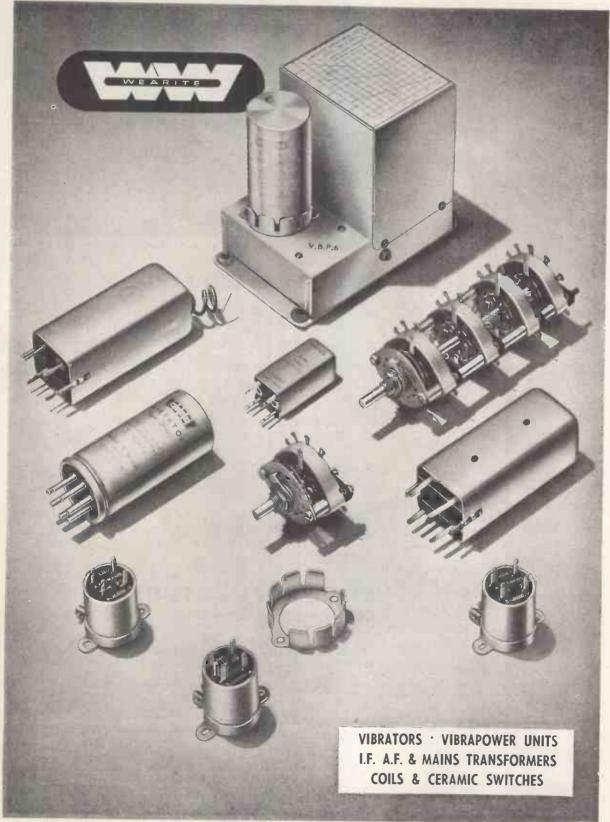
OUTPUT CIRCUITS

At 2.5 or 15 ohms 2.5 watts
At 120 ohms 0.05 watts
At 600 ohms 0.2 watts

POWER SUPPLY

95—130 and 195—250 volts, 40/80 c/s. Also from 12 volt battery, using BRT 401 auxiliary power unit.

For the full specification please send for a copy of publication BC2084.



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with the brilliant NEW Superson Soldering Iron

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- ★ Heats up from cold in 6 seconds—by a light thumb pressure on the switch ring.
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- ★ Simple to operate, ideal for precision work. Requires minimum maintenance at negligible cost. Shows lowest operating cost over a period.
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- ★ It is by far the most efficient and economical soldering iron ever designed for test bench and maintenance work.

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Designed on an entirely new principle, this light-weight, versatile iron is eminently suitable for soldering operations in the RADIO, TELEVISION, ELECTRONIC and TELECOMMUNICATION industries, particularly for all SERVICE work. For general purpose work the Superspeed Iron is the ideal stand-by soldering tool.

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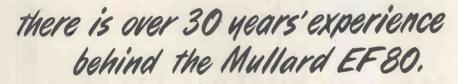
PROFIT ...

BYEXPERIENCE

The Mullard EF80, high slope R.F. Pentode is the most widely used valve of its type. This is as much due to its remarkable dependability as to its extremely efficient performance. Designed primarily as an R.F. or I.F. amplifier in television receivers, it is also suitable for use as a video amplifier, mixer or synchronising pulse separator.

The dependability of all Mullard valves is the logical outcome of Mullard advanced quantity production techniques, many of which are unique.

When ordering this type, BE SURE TO SPECIFY MULLARD.







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Mr. P. W. Pengelly, Service Engineer of Radio and Electrical Equipment Renters Ltd., Finchley, N.12. says:

"We pride ourselves on the quality of our service work. That is why we never risk our reputation by using substitutes for Mullard valves, which we have always found to be consistently efficient and dependable.

Mullard

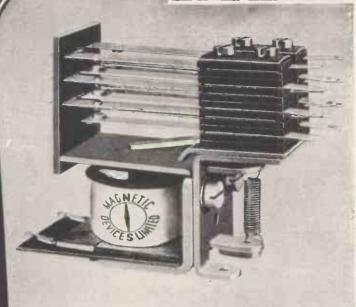
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A.C. OPERATED

SERIES 105

D.C. OPERATED

An extremely sturdy general purpose relay, which is available in a range of contact combinations from 1 pole normally open to 4 pole changeover, and 6 pole normally open, with a maximum contact rating of 10 amps 250v A.C. Normal power consumption is 3 watts, which can be reduced for the smaller contact assemblies if required. Vacuum impregnated coils can be supplied for tropical or humid conditions.

TWO GENERAL PURPOSE TYPES

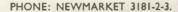
SERIES 600

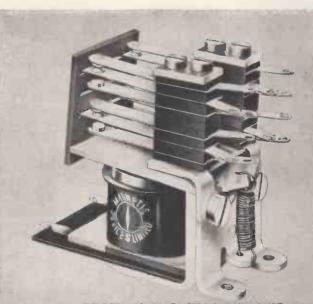
A.C. OPERATED

SERIES 605

D.C. OPERATED

This relay is similar to the Series 100/105 and has been specifically designed for light duty applications. Featuring sturdy and extremely compact blade assemblies from 1 pole normally open to 4 pole change-over, and 6 pole normally open. The contacts will carry 5 amps at 250v A.C. Following the usual practice all contact connections are conveniently grouped at one end, and coils can be wound for either current or voltage operation to requirement. Vacuum impregnated coils if specified.





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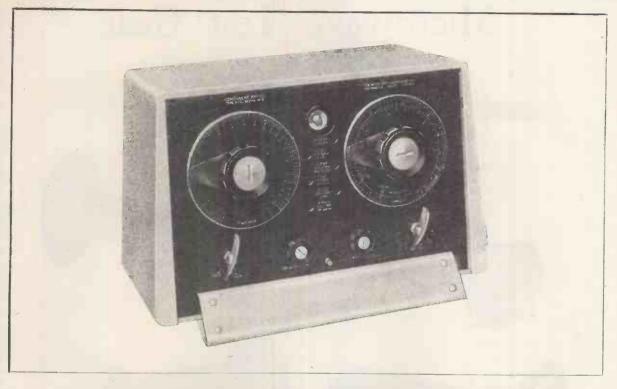
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Component Bridge

THE WAYNE KERR MODEL B.121

A MODERATELY PRICED self-contained instrument, capable of a wide range of accurate measurements.

In addition to giving direct readings of resistance, capacitance, and inductance, it will measure the impedance between any pair of terminals in a three-terminal network, and it can also be used for in situ measurements of component values.

Two individually calibrated dials give simultaneous readings of parallel combinations of resistive and reactive components, with independent scale multiplying of R and C values. The mains supply constitutes the source, and a selective amplifier with sensitive "magic eye" is used for null indication.

Specification

RESISTANCE RANGE: 3 ohms to 1,000 megohms, using six ranges and 3 multipliers of 0.1, 1 and 10.

CAPACITANCE RANGE: 1.0 pF to $1,000 \mu F$, using six ranges and 3 multipliers of 0.1, 1 and 10.

INDUCTANCE RANGE: 100 mH to 10,000 H in five ranges.

ACCURACY: 2% on all ranges over the major part of the scale. If higher accuracy is required, the instrument can be supplied hand-calibrated.

POWER SUPPLY: 110/115 V. or 200/250 V. at 50 c/s -10 W. approx.

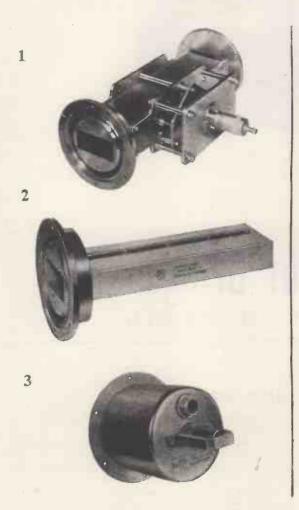
DIMENSIONS: 171 × 101 × 10 high.

WEIGHT: 15 lb. approximately.



Microwave Test Gear

Metropolitan-Vickers Electrical Company announce a complete range of precision microwave test gear for use in 3 in. x 1½ in. waveguide over a band of wavelengths from 10 cm. to 11 cm.





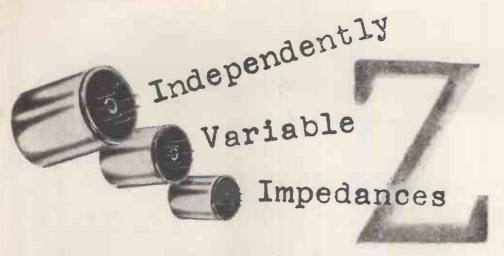




Other Metrovick microwave equipment includes variable attenuator type 502, standing wave detector type 512, wave meter type 517, high power load type 515, S & X band spectrometer type 518.

Full technical details will be sent on request.

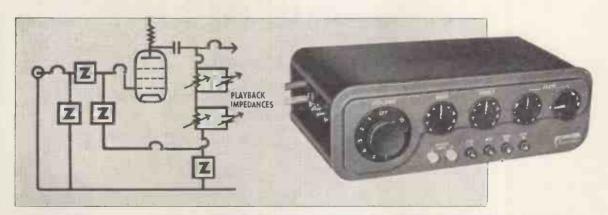
- 1 PRECISION ATTENUATOR Type 501
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When a designer contemplates the input stage from a gramophone pickup he can (a) amplify and then compensate, (b) compensate before amplification, (c) compensate over the first stage by feedback.

No single method is acceptable over a wide range of impedances if the requirement is low distortion and low noise. His choice and the circuit impedances used will depend upon the output level of the pickup, its source impedance, its load impedance and its characteristic.

In the QUAD 11, the first stage circuit connections and their impedances are contained within a detachable plug unit. A range of units covers optimum design requirements for all types of pickups.



ONLY THE QUAD 11 GIVES PERFECT MATCHING AND OPTIMUM INPUT CIRCUIT ARRANGEMENTS. ONE OF THE REASONS WHY THE QUAD 11 GIVES THE CLOSEST APPROACH TO THE ORIGINAL SOUND.



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MONITOR (20 Mc/s)

Designed for the measurement of any frequency in the range 10 c/s to 20 Mc/s with a basic accuracy of ± 1 part in 10⁶ ± 0.1, 1.0, or 10 c/s. Higher accuracies available if required. The unknown frequency is determined by counting the number of cycles that pass through a 'gate' open for a selectable time interval of 0.1, 1.0, or 10 seconds. The result is presented on eight panel mounted meters each scaled 0 to 9 and is in decimal notation. Full information available on request.

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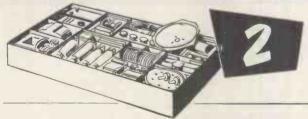
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With these outfits, which you receive upon enrolment, you are instructed how to build basic. Electronic Circuits (Amplifiers, Oscillators, Power Units, etc.) leading to complete Radio and Television Receiver Testing and Servicing.



RADIO Elementary—For carrying out basic practical work in Radio and Electronics, from first principles and leading to the design and building of simple Receivers.

ALL EQUIPMENT SUPPLIED IMMEDIATELY AND REMAINS YOUR PROPERTY



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To: E.M.I. INSTITUTES, Dept. 127x, 43, Grove Park Road, Chiswick, London, W.4.

NAME

ADDRESS

11/54

E.M.I. INSTITUTES The only Postal College which is part of a world-wide Industrial Organisation

PROSPECTUS



(photograph by courtesy of E.S.A. Itd., Stevenage)

I his is a typical application of R.F. Heating as used in the Woodworking Industry, showing how shapes are manufactured with veneers. The jig is of laminated wood, in the form of the final shape, and is lined with aluminium sheets which are connected to the terminals of the R.F. Heater.

The pressure, which should be about 50 lbs. per square inch, is applied on the centre ram by means of a hydraulic pump. With this method the R.F. is fed to the two plates which cause the wood mass to become hot and the resin to cure in a few minutes.

Thus only one jig is required to give a large daily output and the cost of the job is thereby reduced. Less floor space is required than for any other method.

The main advantage of R.F. Heating over other methods, however, is that heating can be localised and heat will only be applied where it is needed.

Agent for London & Southern England Messrs. H. F. Industrial Services Ltd., Fairfax Road, London, N.8. Telephone: Fitzroy 0045

Agent for Scotland

Messrs. Pye Scottish Telecommunications Ltd., 74 York Street, Glasgow. Telephone: Glasgow Central 7637.

Agents are required for other areas of the United Kingdom and countries abroad

ALL COMMUNICATIONS TO BE ADDRESSED TO:-



This low frequency oscillator

costs only

£75

(Bench stands 1 gn. extra)



oscillator is extensively used in the aircraft industry and elsewhere as a convenient source of signals down to 1.15 c.p.s. for the testing and calibration of vibration recorders, servo systems etc. It is also widely used in medical research and clinical work for the calibration of biological amplifiers and recorders, and low frequency wave analysers.

Brief Specification:							
TYPE	FREQUÊNCY RANGE	OUTPUT	INPUT	CONSTRUCTION			
Resistance capacity, with automatic am- plitude control effec- tive over the whole frequency range.	1.15 c.p.s. to 5,500 c.p.s.	Sine wave 50 volts peak to peak, push- pull, with built-in attenuator.	200-250 volts, 40-60 c.p.s.	Standard 19" rack mounting, but also suitable for bench use. Bench stands available.			

NOTES. An incremental switch is fitted. Provision is made for mixing other signals with the output.

Immediate delivery from EDISWAN

RADIO DIVISION . THE EDISON SWAN ELECTRIC COMPANY LIMITED

Member of the A.E.I. Group of Companies

155 Charing Cross Road, London, W.C.2. Telephone: Gerrard 8660. Telegrams: Ediswan, Wescent, London 8P 130

_the



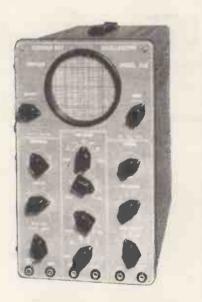
new series-

TAYLOR NEW OSCILLOSCOPE MODEL 31A

Versatile Oscilloscope primarily intended for T.V. and Radio Service work, also invaluable for general purpose use. 4" C.R. Tube. Electrostatic deflection.

Hard valve linear time base covers wide range of sweep frequencies, from below 10 c/s up to 500 Kc/s, and can be used as a free running or triggered time base. Push pull horizontal amplifier for internal use with the time base. Amplifier high gain band width 10 c/s to 6 Mc/s. Flyback suppression circuit fitted with tube modulator.

List price £60. Prompt delivery.



NO INTEREST HIRE PURCHASE

We can now offer all Taylor instruments on the easiest of H.P. terms including the new 3 months' scheme where all interest is refunded on completion of final payment on due date. Alternatively you can choose to spread the payment over 10 months or 15 months.

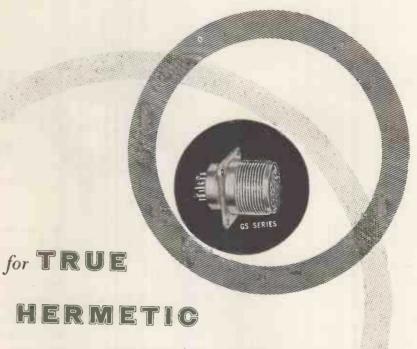
Some typical examples are:

	3 months	10 months	15 months
3IA Oscilloscope 4" Tube. Time base	•	Deposit £6 0 10 And 10 monthly	Deposit £6 0 10 And 15 monthly
10 c/s-500 Kc/s.		payments of £6 0 8	payments of £4 5 5
171A Valve Voltmeter	Deposit £3 19 6	Deposit £2 12 11	Deposit £2 12 11
20 c/s-200 Mc/s	And 3 monthly	And 10 monthly	And 15 monthly
1 v—25 KV D.C.	payments of £8 8 11	payments of £2 13 4	payments of £1 17 9
88A Multirange Meter	Deposit £3 6 0 [Deposit £2 4 3	Deposit £2 4 3
20,000 o.p.v. D.C.	And 3 monthly	And 10 monthly	And 15 monthly
2,000 A.C.	payments of £7 0 3	payments of £2 4 3	payments of £1 11 4
77A Multirange Meter	Deposit £2 5 0 [Deposit £1 10 1	Deposit £1 10 1
20,000 o.p.v. D.C.		And 10 monthly	And 15 monthly
5,000 A.C.	payments of £4 15 7	payments of £1 10 2	payments of £1 1 4
45B Valve Tester	Deposit £3 16 6-, [Deposit £2 12 2	Deposit £2 12 2
Measures 3,000	And 3 monthly	And 10 monthly	And 15 monthly
up-to-date valves.	payments of £8 6 4	payments of £2 12 4	payments of £1 16 3

TAYLOR ELECTRICAL INSTRUMENTS LTD. MONTROSE AVENUE, SLOUGH, ENGLAND

Telephone: SLOUGH 21381/3 Cables: Taylins Slough

Write for catalogue Illustracing full range of Taylor Test Gear



SEALING

mossell by cannon

Hermetically-sealed multi-contact Canseal connectors made by Cannon are really rugged! And . . . they are the only connectors that give you true hermetic sealing under adverse pressure and atmospheric changes. Here's why . . .

Cannon pioneered the first successful hermetically-sealed connector more than six years ago... since then has continuously refined and increased the line. All have special steel contacts. Glass insulation... fused to both contacts and shell for a perfect permanent seal... is stronger than steel, withstands temperatures to 1,000°F, and permits the use of the highest conductive steel contacts compatible with any glass fusing operation.

Available in a wide variety of insert layouts for control, relay, power, and instrument applications, also, special mounting flanges and brazing service to help you obtain a strong and leakproof overall assembly.



(Great Britain) Ltd.

Factories: London · Paris · Los Angeles · East Haven · Toronto · Melbourne



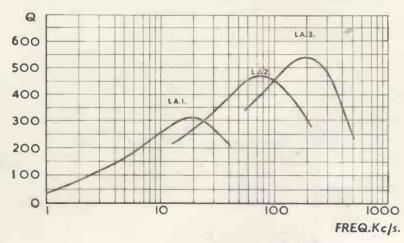
wound on Ferroxcube cores

ESIGNERS of compact and efficient tuned circuits and wave filters are making ever-increasing use of Mullard high Q inductance coils.

Based on Ferroxcube, the world's most advanced magnetic core material, these coils combine small size with an inductance of up to 30 henries over a wide frequency range. Furthermore, their convenient shape and self screening properties facilitate either individual mounting or stacking.

Full details of these and other high grade components now available from Mullard will be gladly supplied on request.

VALUES TYPICAL



Special Features

Small size

Low hysteresis loss factor

High value of inductance

Low self capacitance

Controllable air gap facilitating inductance adjustment

Self screening

Controlled temperature coefficient

Operation over a wide frequency range

Easily mounted

Mullard Mullard



- 'Ticonal' permanent magnets,
- 'Magnadur' ceramic magnets, Ferroxcube magnetic cores.

And NOW—a range of 'CERAMICAPS' for your

3 Storage Unit!

The LAB Continuous Storage Unit is widely acknowledged as the most efficient and convenient method of storing and selecting resistors. Now its usefulness is still further extended with the introduction of LAB pak'd 'Ceramicaps'.

> With the LAB Unit, research and experimental laboratories and small production groups have to hand immediately, a complete range of resistors and 'Ceramicaps', easily selected with card index simplicity from some 700 sorted and carded components. Empty cards

are merely replaced with full ones from stock.

The LAB unit is supplied FREE with initial purchase to your specification. Standard assortments available. Each LAB Unit can be used to store one type of component exclusively, or quantities of the complete range of resistors and 'Ceramicaps'. Full details and illustrated list will be sent on application.



CONTINUOUS

STORAGE UNIT

- ★ Continuous Storage for Resistors and 'Ceramicaps'
- * Values separately carded
- * Finger-tip Selection

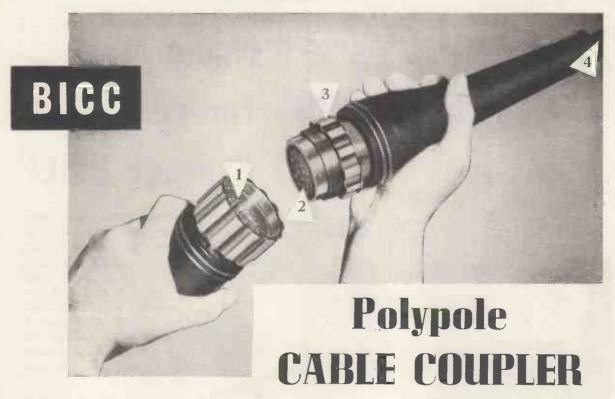
		RE.	SISTORS		
Ref.	Туре	Loading	Max. Volts	Range	Dimensions
T	‡ watt	† watt	250	10 ohms to 10	§" × 51"
R	y watt	l watt lerance avail	500 able ± 20%	megohms	3″ x 1″
		HIGH STAB	ILITY RES	ISTORS	
HS3		+ watt	750	l ohm to 500 megohms	1.1° x 0.1°
	T	olerance ava	ilable ±5%	, 2%, 1%	
	5 (WIREWOL			
			AMICAPS '		
	Tubula	rs 3 - 470 pf 500 - 5000 pf	Tolera	nces ±2%, 10% Hi-K	

The Lab Continuous Storage Units are available from your normal source of supply, but more detailed information can be obtained from

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50 ABBEY GARDENS LONDON N.W.8 Telephone: Maida Vale 5522



specialised remote control—centimetre radio links ground radar-outside broadcast television

BICC Couplers and Cables are intended for the outdoor inter-connection of equipment, such as that mentioned above. Each application calls for composite trailing cables containing both R.F. units and other polythene insulated conductors.

BICC Polypole Mark III Couplers are available in two versions, designed for use with two standard types of BICC outdoor trailing cables. The Mark IIIA cable and coupler incorporates three coaxial circuits, and the Mark IIIB three screened twin circuits. In addition, both cables contain three triplets and 21 other conductors.

The couplers are permanently moulded to the ends of the cable in the factory. This technique provides a remarkably robust coupler which is virtually free from the hazards of conductor breakages near to, or within the coupler.

If you are interested in the uses of BICC Polypole Cable Couplers, we will be pleased to send you further information.

Note these important features

The couplers are assembled with the conductors in tension to ensure that they each . contribute their share of the total strength.

engagement and withdrawal. The withdrawal. overall metal housing can also be easily replaced should it become daniaged.

Polythene injection moulding permits a watertight assembly.

The cable itself is designed with a symmetrical cross section to provide the greatest reliability under severe handling

Screwed lock rings

provide forced

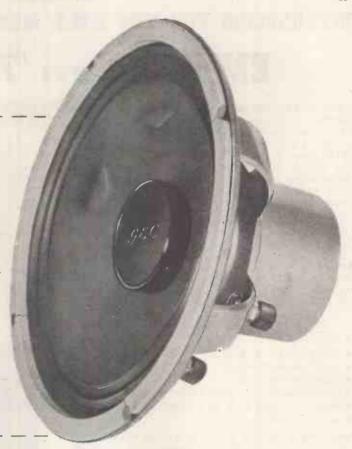




9 Octave

realism...

from a single unit



The G.E.C. metal cone loudspeaker gives lifelike reproduction of any type of sound over a range of 9 octaves. This includes the entire musical fundamental range together with overtones which give tonal quality and character to the performance of each musical instrument.

The sound engineer will appreciate the simplification and improvement in performance which has been achieved by combining the following attributes in a single unit.

- Smooth response over a range of nine octaves with extremely good low frequency response
- Negligible inter-modulation
- Unequalled transient response due to special coil and cone construction

£8.15.0

For the Home Constructor

This is a professional instrument and must be used under the correct conditions to obtain the optimum results. Cabinets have been specially designed for use with this loudspeaker, details of which will be available shortly.



Metal Cone Loudspeaker

INTRODUCING THE NEW E.M.I. MAGNETIC RECORDING TAPE

EMITAPE TYPE '77' AND '88'

E.M.I. with a small select team of scientists and research chemists pioneered the manufacture of Magnetic Recording Tape in this country, and due to the ever increasing demands for this tape by the famous studios of His Master's Voice, Columbia and Parlophone, etc., the British Broadcasting Corporation and leading Broadcasting Studios at home and abroad, the E.M.I. plant today is the largest and most up-to-date production unit in this country.

Unremitting research with this new development in electronics has produced: The magnetic recording tape by which all other tapes are judged.

EMITAPE is the universal tape, suitable for all types of Tape Recorders, whether they are single or twin track recording. The tape is readily joined and edited with the E.M.I. jointing accessories.

EMITAPE '88' SPECIAL FEATURES

- High Sensitivity
- Anti-static-P.V.C. Base
- High Tension Strength
- Freedom from Curl
- · Editing leader and trailer Strip
- Metallic Contact Strip on 5" spools for auto-stop
- New domestic plastic spool

EMITAPE is available wound on a range of five spools covering all professional and domestic hub machines. Spare empty reels are available in all sizes.

EMITAPE '77'

"Pen Tested" for Special Applications



Although manufactured under the same conditions as Type '88' and having all the special features, Type '77' undergoes an individual "Pen Test" examination for accuracy of sensitivity. Each reel is "Pen Tested" throughout its entire length to ensure a level of sensitivity not exceeding $\pm \frac{1}{2}$ dB, and an overall variation from reel to reel not greater than ± 1 dB. A typical example of a "Pen Tested" chart is given above.



Illustration of range of tape available in Type '77' and '88'

EMITAPE SPECIFICATION

Magnetic Properties:-

Coercive Force 270 Oersteds

Remanence 0.6 flux lines per 1" width

Sensitivity Uniformity for Type '77'

I Kc at optimum bias at 15" [sec.

- (a) Slow variation within one reel not greater than ± ½ dB on mean sensitivity
- (b) overall variation from reel to reel not greater than ± 1 dB on mean sensitivity
- (c) Instantaneous variation in sensitivity not greater than ⅓ dB

Sensitivity:-

The sensitivity for a given recording current is 8 dB above H50 tape.

Sensitivity of tape at 15"/sec.

I Kc ± I dB

10 Kc \pm 2 dB on sensitivity at 1 Kc.

15 Kc \pm 3 dB on sensitivity at 1 Kc.

Bias Ratio:

Optimum bias is 80% of that required for H50 tape

Print :-

At least 60 dB below test signal after close contact for 5 minutes at 70°F.

. Modulation Noise :-

At least 50 dB below peak mod. (2% total harmonics)

Basic Unweighted Noise:-

At least 65 dB below peak recording level

Tensile Strength:-

7½ lbs. per ¼" width

Elastic Elongation:—

At 1 lb. load — less than 0.5% (15 secs. application)

Yield Point:-

4½ lbs. per ¼" width

Recommended Operational Tension:-

3 ozs.

Longitudinal Temp. Coeff:-

4 x 10-5 per degree F.

Humidity Expansion:-

Negligible

PRICE



	REEL	LENGTH	TYPE 88		TYPE 77			
5"	DOUBLE SIDED PLASTIC SPOOL		3	600 ft.	88/6	1.1.0	77/6	1.10.0
7"	DOUBLE SIDED PLASTIC SPOOL	***		1,200 ft.	88/12	1.15.0	77/12	2.8.0
101"	NAB DOUBLE SIDED ALUMINIUM SPOOL			2,400 ft.	88/24N	4.3.0	77/24N	5.17.6
II.	EUROPEAN SINGLE SIDED ALUMINIUM SPOOL			2,400 ft.	88/24E	3.13.6	77/24E	5. 8.0
11.	EUROPEAN SINGLE SIDED ALUMINIUM SPOOL			3,250 ft.	88/325	4.11.0	77/325	6. 0.0

Send for illustrated brochure of Emitape Tope Accessories & Magnetic Tape Recording equipment to:-

E.M.I. SALES & SERVICE LTD., RECORDING EQUIPMENT DIVISION, HAYES, MIDDLESEX. Telephone: SOUTHALL 2468

ADVANCE COMPONENTS LTD., MARLOWE ROAD, WALTHAMSTOW, LONDON, E.17

Telephone: LARkswood 4366/7/8

7.5 to 250 Mc/s ON FUNDAMENTALS IN FIVE RANGES SINE AND SQUARE WAVE MODULATION R.F. OUTPUT 1 MV to 100 mV

Advance MODEL Q1 V.H.F. SIGNAL GENERATOR

£45
(List price in U.K.)

Again Advance lead the way—this time with a V.H.F. Signal Generator covering 7.5 to 250 Mc/s, a range that embraces Bands 1 and 2 and also the impending Very High Frequency Television Transmissions on Band 3. Moreover, this instrument is available at a price well within the reach of every service man. In the traditional Advance manner, this instrument is designed for simple operation and with a versatility that not only fulfils present needs, but anticipates the even more exacting requirements to deal with the television test problems of tomorrow.



Below ore some outstanding features:-

- WIDE RANGE—7.5 to 250 Mc/s
- SINE AND SQUARE WAVE
 MODULATION
- RELIABLE ATTENUATION
- LOW LEAKAGE—less than 3 microvolts
- TRULY PORTABLE—weighs only 17 lbs
- COMPETITIVE PRICE



The Q1 provides the ideal complement to the Model E2. These together give complete coverage from 100 kc/s to 250 Mc/s.

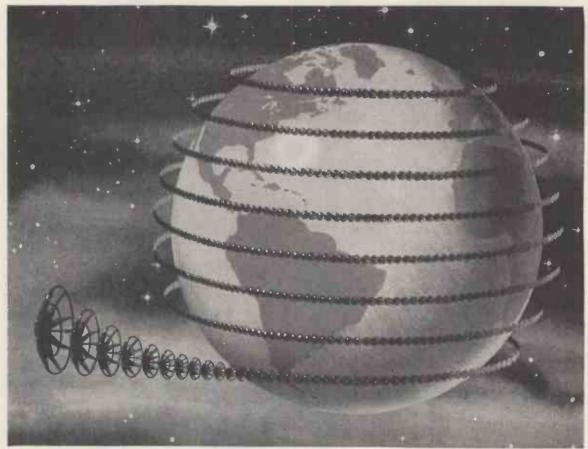
Telephone: LARkswood 4366/7/8

Full technical details available in Folder W23 on request.



Over 200,000 channel miles of RCA Microwave circuits actually in use

If all RCA MICROWAVE channels now in service were connected, they would circle Earth eight times!



Here is graphic proof that in the Microwave field, RCA's breadth of experience is unmatched. To date, RCA has installed Microwave circuits for teletype, telephone, program and control covering over 200,000 aggregate channel miles in 11 countries—a distance eight times the circumference of the globe.

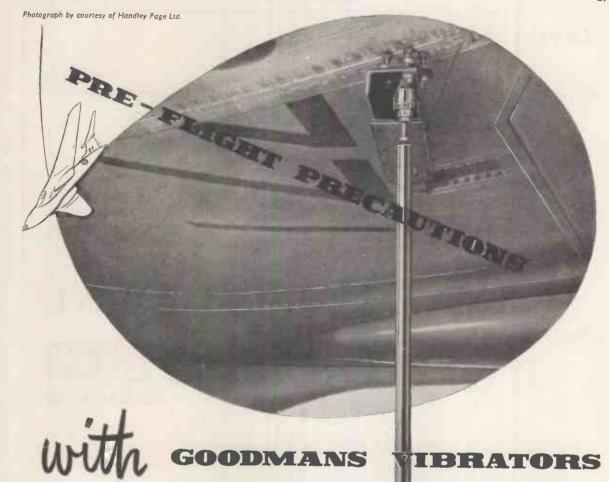
This unmatched record could be set only because RCA has been closely associated with Microwave since originating the radio relay principle 30 years ago. As a result, RCA Microwave is the last word in flexibility and versatility. It remotely controls many operations

such as pipeline stations for producers of crude oil and natural gas. It provides military or civilian agencies with multi-channel mobile communications equipment to meet emergency and special point-to-point requirements. And it serves the communications industry in countless ways.

Let RCA show you how its Microwave equipment can solve your problems at lower cost while providing superior performance. To aid you in surveys and installations, RCA Microwave experts are available. See your RCA distributor or write RCA today.

TMKS.4





The flight characteristics of a newly designed aeroplane are the subject of lengthy calculations before the first prototype is built. Whilst the mathematical calculations are themselve accurate, they are based, as in all design work, on several assumptions which have to be verified by a series of pre-flight tests.

One of these essential investigations is the Ground Resonance test, the purpose of which is to determine the various complex modes of vibration of the airframe structure. The frequency of the mode and the dynamic response at remote parts of the aircraft must be accurately determined. The information obtained together with the aerodynamic derivatives is used in predicting the critical 'futter' speed of the aircraft. The illustration shows one of the two Goodmans Model 8/600 Vibration Generators which were used to excite the Handley Page "Victor" for this very important

For wide frequency range vibration testing and dynamic response investigations, Goodmans Vibration Generators are an obvious choice. These units require no field excitation and provide a faithful reproduction of the input wave form. Industrial applications of controlled vibration are continually increasing; maybe it can serve you—in which case our unique experience is at your service.

The range includes models from the 8/600 shown, developing a force of \pm 300 lb., to the midget model, with a force of \pm 2 lb., for optical cell research and hairspring torque testing, etc.

Just another of the wide applications of Good-mans Vibration Generators. Full technical data available from Vibration Division"W"

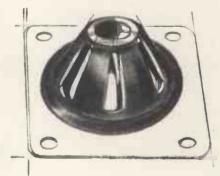
GOODMANS INDUSTRIES LIMITED, Axiom Works · Wemb'ey · Middx · Wembley 1200 (8 lines)

APPLICATION 95 SERIES 38



In this instance the Series 38 "Flexilant" Mounting protects a delicate instrument from vibration and shock. Other applications are manifold — from aircraft to power-station instrument panels: from ship's instruments to the protection of pyrometers in a steel works.

We produce a range of components that absorb vibration; eliminate noise; suppress shock. Our new catalogue lists all these for you.



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The 'PLAYTIME'

TAPE RECORDER

Carr. & Packing 12/6 Will provide endless entertainment at low costspare spools are only 26/6 for ONE HOUR'S playing time and are of specially high grade matched tape.

Take it with you!

to your friends and neighbours-to the office-to that rehearsal-to that wedding-anniversary or reunion-use it for every occasion.

M.O.S can offer you these EASY H.P. FACILITIES

Deposit 20% and 12 monthly payments of 46/9 if purchased complete with microphone and tape.



can offer you these

UNIQUE FEATURES!

- LIGHT IN WEIGHT-only 16 lbs.
- LOW IN PRICE—only 26 gns. or complete with high fidelity matched crystal microphone and ONE HOUR spool or laboratory matched tape for £31.4.6.
- SINGLE KNOB CONTROL by joystick for record, playback, rewind and fast forward without unlacing tape.
- SELF CONTAINED for Recording and Playback through any Radio or amplifier thus making possible high fidelity reproduction through the system used.
- PRECISION ENGINEERED CHASSIS resulting



in less than .1% wow and flutter and enabling operation in any plane.

- ONE HOUR'S PLAYING TIME on 600ft, spool.
- UNIFORM FREQUENCY RESPONSE between 60-6,000 c/s.
- COMPACT AND SMALL—overall size only $12\frac{1}{2}$ in. \times 10in. \times $4\frac{1}{2}$ in.
- ATTRACTIVE APPEARANCE-finished in 2tone leathercloth with detachable lid and handsome gilt fittings.
- FULLY AUTOMATIC operation and erasure.



See it and hear it at the RADIO CENTRE SUPPLY CO. MAIL ORDER

THE RADIO CENTRE

33 TOTTENHAM COURT ROAD . LONDON . W.I MUSeum 6667

THE POPULAR RECORDER at the POPULAR PRICE

THE TAPE RECORDER

Complete with Ronette Crystal Desk Microphone, 1,200ft. spool high coercivity tape, and take up spool.

TECHNICAL DATA

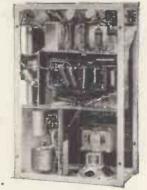
- INDEPENDENT BASS AND TREBLE CONTROLS FOR RECORDING AND PLAYBACK.
- Two speeds 3iln. and 7in. per sec.
- High quality Amplifier can be used quite independently for PA or gramophone record reproduction.
- Overall negative feedback.
- High flux speaker together with amplifier giving superb and brilliant reproduction.
- Instantaneous and positive braking. · High fidelity recording heads (twin tracks), automatic erasure.
- Powered by three high grade recording motors.
- Fast forward and rewind without unlacing tape.
- Precision engineering giving negligible wow and flutter.
- · Magic eye, recording level control.
- Speaker muting switch and provision for external speaker.
- Radio/Gram and microphone inputs.
- Size only 16?in. x 12in. x 5in. (without lid). Weight 33 lbs.
- MULLARD Miniature Valves.
- Attractive 2-tone leathercloth case with detachable lid with handsome gllt fittings.
- For use on AC mains 200/250 v.

TWO SPEED TAPE RECORDER



THE Tape Recorder for the Connoisseur who wants the best in Tape Recording. At 45 Gns. there is no better value. Now available with two speeds giving 2 HOURS' PLAYING TIME, the "EDITOR" combines the latest recording techniques with the advanced technical achievements of our research engineers.

Suitable for use with pre-recorded tapes, this wonderfully compact unit is amazingly simple to use for a hundred and one different recording purposes. Superb true balanced recording and listening can be obtained. The "EDITOR" is the smallest mains-operated Tape Recorder giving 2 HOURS' FULL PLAYING TIME.



THE HEART OF THE "EDITOR" The Precision Engineered Chassis

Custom-built and modern in styling, the "EDITOR'S" ingenious planned circuitry is built on a quickly removable, all steel frame -a remarkable development in chassis design construction. This skilful method of assembly facilitates ease of inspection. The chassis facilitates ease of inspection. The chassis can be withdrawn from the case in 30 seconds by removing only 4 screws.

. EASY H.P. TERMS Send only 20% deposit . with order, balance over any period up to 18 months. Add 15/- for carriage and packing.

YEARS' GUARANTEE with every Burgoyne Radiogram Chassis

(carriage and packing 7/6)

EASY H.P. TERMS

Send 20% deposit with balance spread очег period up to 18 months. With a push-pull output giving 8 watts of undistorted quality reproduction and using negative feedback, this fine chassis is supplied for those connoisseurs wanting only the best, at a price within their means.

TECHNICAL DATA

• Illuminated full vision coloured tuning scale 11½in. x

• Îlluminated full vision coloured tuning scale 11½in. x

• Îţin. • Negative feedback • 8 valves—6C9, 6F15,

• ÎLD20, 6L1 (2), 6P25, UU7 and 6MI • Separate bass and treble controls for cut and lift • Wavebands 16-50; 190
• S50; 1,000-2,000 metres • Magic eye tuning indicator and precision flywheel tuning • 8 watts push-pull output • Heavy gauge steel chassis, specially treated against corrosion • Special mains transformer with smoothing circuit reduces hum to a minimum • Clear long distance reception • Recommended for use with 10ln. or 12in. P.M. speaker • Speech coil impedance 3 or 15 ohms • Extension speaker sockets • Siz 9½in. high x 13in. wide x 8in. deep—chassis height 2½in.



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Telephone: MUSeum 6667.

THE RADIO CENTRE

To secure

* Low Deposit Terms

* Easy Payments * Personal Service * Infinite variety of equipment

M.O.S PERSONAL the CREDIT with

SEND OR BRING US YOUR ORDER TODAY WITH SECURING DEPOSIT. OUR RANGE OF MERCHANDISE IS UNSURPASSED AND A SELECTION IS GIVEN BELOW.

Please add sufficient to allow for carriage and packing.

TAPE RECORDERS AND DECKS

Cook Wains

The securing Deposit may be any amount convenient to the Purchaser but must be at least one-tenth of the Total of Cash Prices for any item or items (which may be grouped). The Balance remaining when the Deposit is subtracted from the Total Cash Price may be spread over 6, 12 or 18 months and for these periods the charges are on a sliding scale:

Cash Price

for 6 months add 2/- in the £ to Bal. ,, 12 ,, ,, 2/6 ,, ,, ,, ,, 18 ,, 3/6 ,, ,, ;,

LOUDSPEAKERS

To secure

Minimum Rates are necessary because administration costs are fixed for every transaction, no matter how small, and are as follows:-

20/- where the balance is £5 or under.

,, £10 ,, 40/-" £15 "

Cash Price

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	Cash Price	send only		Cash Price	send omy	Constitution with the state	00 5 0	10 0
Editor 2-speed	£47 5 0	£9 9 0	Wharfedale W.15C8 Wharfedale W.15	£17 10 0 £15 10 0	£1 15 0 £1 11 0	Connoisseur with 2 heads Decca X.M.S. with 2 heads	£9 5 6 £6 9 3	18 7 13 0
Ferrograph 2A	£79 16 0	£8 0 0	Wharfedale Super 12 CSAL	£17 10 0	£1 15 0	Acos HGP39/GP20 Arm Leak Ruby 78 r.p.m. or L.P.	£3 8 4 £11 11 0	13 0 7 0 £1 3 1
Vortexion Grundig TK9	£84 0 0 £88 5 0	£8 8 0 £6 16 6	Wharfedale W12CS Wharfedale W12	£9 15 0 £9 5 0	19 6 18 6	Ronette Miniweight with 2		
Grundig TK819	£99 15 0	£10 0 0	Wharfedale W10CS (B)	£12 6 6	£1 4 8	Ronette Miniweight super	£3 9 6	7 0
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Playtime	£27 6 0	£5 9 0	Wharfedale Super 8 CSAL	£6 13 3	13 4 12 8	CATHODE RAY TU	RES (Tolovis	ion)
Playtime with Microphone and Tape	£31 4 6	£6 5 0	Wharfedale Super 8 C8 Wharfedale Bronze 8	£6 6 7 £3 3 11	6 5	9in. Mullard, Mazda	£12 10 0	£1 3 0
Lane Tape Table Mk, 6	£18 10 0	£1 17 0	Wharfedale Super 5	£6 13 3	13 4	12in. G.E.C., etc. etc	£16 13 8	£1 13 4
Burgoyne 2-speed Deck Truvox Mark II	£13 19 6 £23 2 0	£1 8 0 £2 6 3	Wharfedale W5	£2 0 0	4 0	16in	£22 4 10 £23 12 8	£2 4 6 £2 7 3 £1 15 5
Wearite 2 A	£35 0 0	£3 10 0	Duplex	£22 11 0	£2 5 1	12ln. Aluminised types	£17 14 6	£2 7 3 £1 15 5 £2 1 0
Wearite 2B Wearite 2C	£40 0 0 £45 0 0	£4 0 0 £4 10 0	W.B. 12in. Concentric with	£23 16 0	£2 7 8	14in. Aluminised types 17in. Aluminised types	£20 10 0 £24 13 6	£2 1 0 £2 9 4 £1 6 0
			W.B. 10in. Concentric			E.M.I. 10in. MW6-2 Projection	£14 18 11 £8 6 10	£2 1 0 £2 9 4 £1 6 0 16 8
			W.B. 10in. Concentric with	£9 7 6			28 6 10	10 0
AMPLIFIERS AND A		S	W.B. Tweeter Unit	£10 15 6 £3 15 6	£1 1 7 8	TEST EQUIPMENT		
Leak TL/12 Point One	£28 7 0 £12 12 0 £28 7 0	£2 16 9	W.B. HF610 High Fidelity	£2 10 6	5 1	Advance Signal Generator	£19 19 0	£2 0 0
Leak Varislope	£12 12 0	£1 5 3	W.B. HF810 High Fidelity W.B. HF912 High Fidelity	£3 0 6 £3 9 6	6 1 6 11	Advance Signal Generator		
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Acoustical QUAD Mk. II Goodsell "Williamson"	£42 0 0	£4 4 0	W.B. HF1214 High Fidelity Goodmans Axiom 22	£9 15 6	£1 9 5	Advance Signal Generator	£28 0 0	£2 16 0
G.W.18	£33 5 0	£3 6 6	Goodmans Axiom 101	£6 12 1	13 3	Н1	£25 0 0	£2 10 0 £2 7 0
Goodsell "Williamson"			Goodmans Axiom 102 Goodmans Axiom 150 Mk.	£9 18 0	£1 0 0	AVO Model 8 Meter	£23 10 0 £19 10 0	£2 7 0 £1 19 0
G.W.12 Goodsell M.A.5./U.L	£27 10 0 £14 17 6	£2 15 0 £1 9 9	II	£10 5 6	£1 0 7	AVO Electronic Test Meter	£40 0 0 .	£4 0 0
Goodsell F/TC pre-amplifier Goodsell F/U/TC pre-ampli-	£10 10 0	£1 9 9 £1 1 0	Goodmans Audiom 60 G.E.C. Metal Cone BCS1851	£3 12 6 £8 16 7	17 3 17 8	AVO Universal Bridge AVO Signal Generator	£34 0 0 £30 0 0	£4 0 0 £3 8 0 £3 0 0
fler	£14 14 0	£1 9 5	Tannoy 15in. Dual Con-			AVO Universal Avominor	£10 10 0	£1 1 0
Goodsell P/F/A pre-ampli- fler	£20 0 0	£2 0 0	Tannoy 12in. Dual Con-	£33 10 0	£3 7 0	AVO Beavy Duty Meter	£5 5 0 £15 0 0	£1 1 0 10 6 £1 10 0
Bogers Senior Main Ampli-			centric	£27 10 0	£2 15 0	AVO Valve Characteristic		
fier Rogers Senior Control Unit	£28 0 0 £15 0 0	£2 16 0 £1 10 0	Lowther P.M.2	£35 0 0	£3 10 0	Meter	£60 0 0 £92 0 0	£6 0 0 £9 4 0
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Rogers Junior Mk. II am-	£14 0 0	£1 8 0	Regentone RP2 3-speed	£9 19 6	£1 0 0	Meters	£3 0 0	6 0
plifier	£9 0 0	18 0	Regentone HG23-speed and			Taylor 45B Valve Tester Taylor 66A Signal Generator	£25 10 0 £22 10 0	£2 11 0 £2 5 0
plifier	£12 17 6	£1 5 9	amplifier Regentone AHG2 3-speed	£15 15 0	£1 10 6	Taylor 75A 20,000 o.p.v.		
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Rogers RD Uniflex	£18 17 6	£1 19 9	Trixette A375 Auto 3-speed			Taylor 88A 20,000 o.p.v.	£15 0 0	£1 10 0
Lowther B5F Amplifier Lowther A105 Amplifier	£22 0 0 £35 0 0	£2 4 0 £3 10 0	and amplifier Volmar L425 3-speed Auto	£37 16 0	£3 15 7	Meter	£22 0 0	£2 4 0 £1 9 0
Lowther A15F Amplifier	£45 0 0	£3 10 0 £4 10 0	Amplifier	£24 13 6	£2 9 4	Taylor 110C Capacity Bridge Taylor 120A Universal	£14 10 0	£1 9 0
Lowther Bass/Treble Cor- rector B.T.2	£9 0 0	18 0				Meter	£9 10 0	19 0
Lowther Bass/Treble Corr- ector B.T.3	£9 9 0	18 11	GRAMOPHONE UN	IITS		Taylor 130A Insulation Tester	£15 0 0	£1 10 0
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	20 10 0		2010 Collaro AC/3/534 3-speed	£18 5 3	£1 16 6	Taylor 240A Pattern Generator	£14 0 0	£1 8 0
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Lowther LE1.2 Medium/	£22 7 9	£2 4 9	mixer	£16 10 0	£1 7 0	Pullin Universal series 100		
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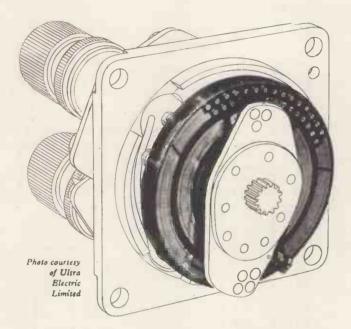


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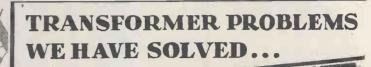
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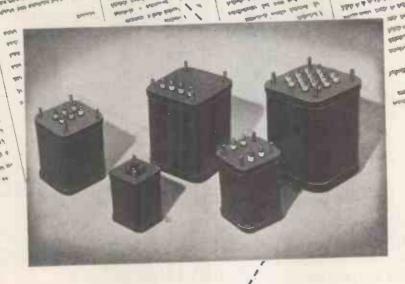
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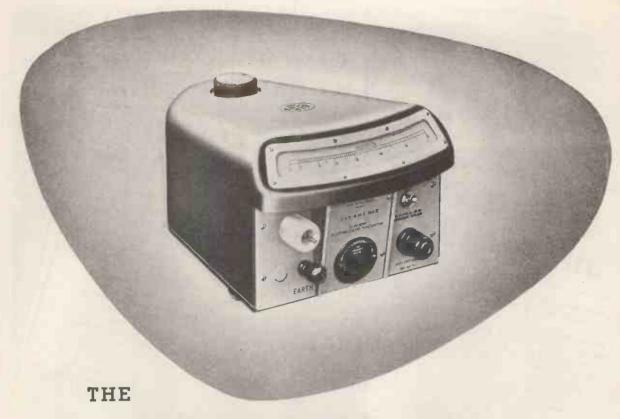
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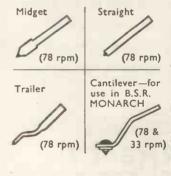


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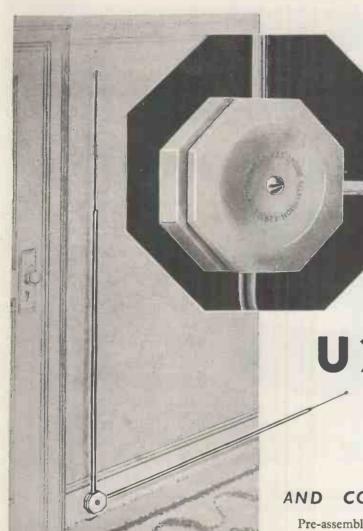
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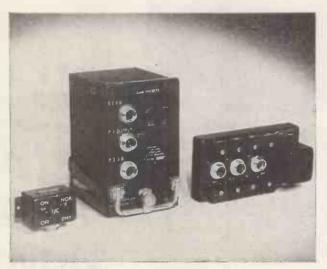
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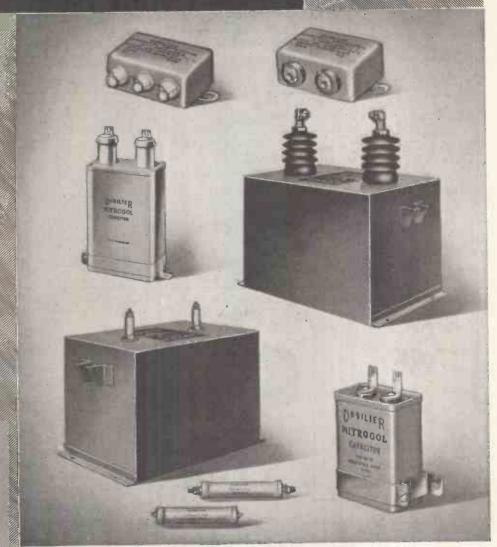
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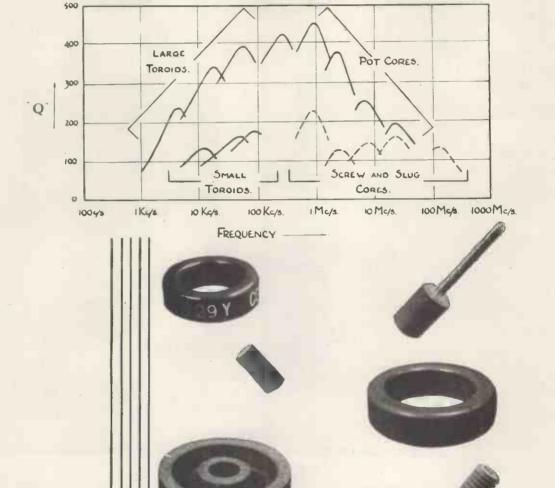
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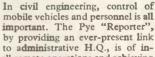








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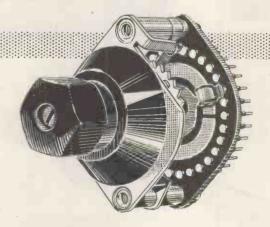
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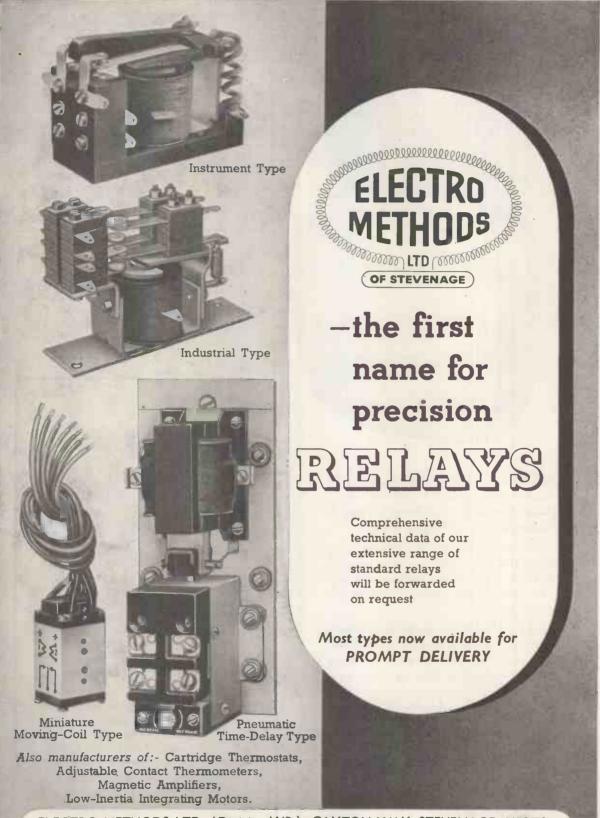
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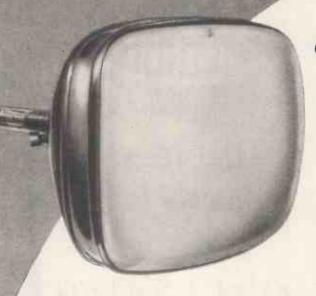
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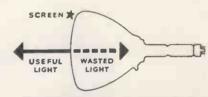
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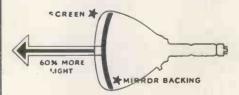
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WITHOUT ALUMINIZING

Without aluminizing, tubes waste half their light (see diagram above). To counteract this the brilliance must be increased and the tube life is shortened.



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6 fully equipped cathode ray tube service depots provide better, quicker tube testing should the need arise. Stocks of tubes are available in 26 Ediswan Offices. Only Ediswan give such complete backing to the Trade.

RV9

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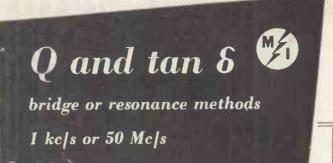
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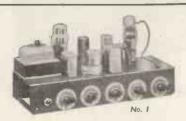
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3-SPEED GRAM UNIT MODEL "T" with new type turnover pickup head, £10/12/8, post 2/6.

MODEL TA as above, but with plug-in turnover head, £10/16/-, or with two separate high fidelity Acos HGP35 heads, £12/15/6. Unit less heads, £8/11/-, post 2/6. Heads,

42/3 each, post 1/-.
MODEL TB as above, but with long pickup arm. Less

heads, £8/11/-, post 2/6.
Heads to fit this unit: Decca XMS, 55/-, Decca Crystal, 35/-, Garrard Standard Magnetic, 25/-, miniature magnetic

Heads to fit this unit: Decca XMS, 55/-, Decca Crystal, 35/-, Garrard Standard Magnetic, 25/-, miniature magnetic low impedance, 25/-, miniature magnetic high impedance, 35/-. Post on heads 1/-. Unit can be supplied with any combination of above heads and is carefully adjusted for stylus pressure on despatch.

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high, lift-up lid with piano
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Unit or Auto-changer, Amplifier, Pre-amplifier, and Radio
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Va (min) 10.8 kV	Va (min) 11 kV
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Both tubes are provided with an external graphite coating, and have a scanning angle of 70°

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Model	12	9	6	- 6A	11
Volts	6 12 24-27½	6 12 24-27½	6	6	6
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Bt. Dia.	3/16 (push-on)	5/32 (push-on)	1/16 (fixed)	3/32 (push-on)	5/32 (push-on)
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NOVEMBER, 1954

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A portable panclimatic battery or mains operated valve voltmeter for laboratory or field use.

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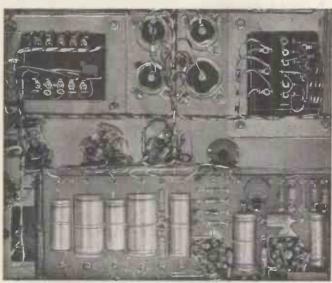
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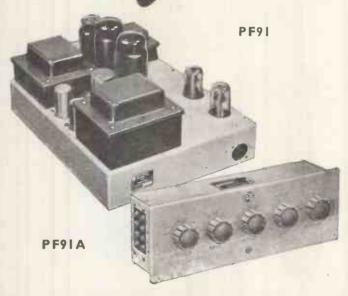
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The PF 91 amplifier, with the PF 91A remote control unit, is a versatile and practical combination for those who demand realism in sound reproduction from record players, tape recorders, microphones or radio tuners.

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I.F.s. 465 k/c. Permeability-tuned with flying leads. Standard size | \(\frac{1}{6}\)in. \(\times\) 1\(\frac{1}{6}\)in. \(\times\) 1\(\frac{1}{6}\)in. For use with OSMOR coilpacks and others, 14\(\frac{1}{6}\) pair. Midget I.F.s. 465 k/c. \(\frac{1}{6}\)in. \(\times\) 2\(\frac{1}{6}\)in. \(\times\) 2\(\frac{1}{6}\)in. \(\times\) PREALIGNED. 1/6 extra, both types.

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"No Compromise" TRF Tuner. "Midget Mains Receiver." Sensitive 2-valve Receiver. Television Converter (special coils in cans available), Midget sensitive T.R.F., etc.

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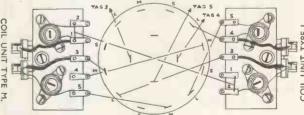
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Please let us know your requirements — send us your problems.



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Please send for our data sheets which include full details of all the above to:

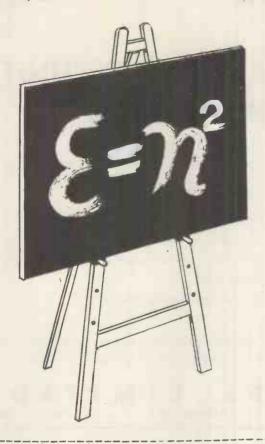
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	5 v. 2 amps.	16/9
	FS2, 250-0-250 v. 80 m/a FS30, 300-0-300 v. 80 m/a., 21/ FS3, 350-0-350 v. 80 m/a.	21/-
	FS1, 250-0-250 v. 80 m/a., 21/ FS3, 350-0-350 v. 80 m/a. FS10, 300-0-300 v. 80 m/a., 21/ FS3, 350-0-350 v. 80 m/a. FS2.X. 250-0-250 v. 100 m/a., 23/ FS75, 275-0-275 v. 100 m/a. FS30.X. 300-0-300 v. 100 m/a., 23/ FS3 X. 350-0-350 v.	23/-
	100 m.a.	23/-
	100 m.a. All the above have 6.3 4-0 v. at 4 amps., 5-4-0 v. at 2 amps. FS43. Output 425-0-425 v. 200 m/a., 6.3 v. 4 amps., C.T. 6.3 v. 4 amps., C.T. 5 v. 3 amps. Fully shrouded FS50. Output 450-0-450 v. 250 m/a., 6.3 v. 2 amps., C.T. 6.3 v. 4 amps., C.T. 5 v. 3 amps. Fully shrouded F35X. Output 350-0-350 v. 250 m/a., 6.3 v. 6 amps., 4 v. 8 amps.,	47/6
	FS50. Output 450-0-450 v. 250 m/a., 6.3 v. 2 amps., C.T. 6.3 v.	
	4 amps., C.T. 5 v. 3 amps. Fully shrouded	67/6
	4 v. 3 amps., 0-2-6.3 v. 2 amps. Fully shrouded	65/-
	F35 X. Output 350-0-350 v. 250 m/a., 6.3 v. 6 amps., 4 v. 8 amps., 4 v. 3 amps., 0-2-6.3 v. 2 amps. Fully shrouded. FS160 X. Output 350-0-350 v. 160 m/a., 6.3 v. 6 amps., 6.3 v. 3 amps., 5 v. 3 amps. Fully shrouded FS43 X. Output 425-0-425 v. 250 m/a., 6.3 v. 6 amps., 6.3 v. 6 amps., 5 v. 3 amps. Fully shrouded	44′-
	6 amps., 5 v. 3 amps. Fully shrouded	63/6
		26/6
	3 amps, Halfshrouded.	27/9
	3 amps. Fully shroughd	29/6
	HS150. Output 350-0-350 v. 150 m/a., 6.3 v. 3 amps., C.1. 5 v. 3 amps. Halfshrouded. F36. Output 250-0-250 v. 100 m/a., 6.3 v. 6 amps., C.T. 5 v. 3 amps. Fully shrouded. FS120. Output 350-0-350 v. 120 m/a., 6.3 v. 2 amps., C.T. 6.3 v. 2 amps., C.T. 5 v. 3 amps. Fully shrouded. FS256. Output 250-0-250 v. 80 m/a., 6.3 v. at 6 amps., 5 v. at 3 amps. Fully shrouded	29/9
	3 amps. Fully shrouded	
	3 amps. Fully shrouded PRI/I. Output 230 v. at 30 m/a, 6.3 v. at 1.5/2 amps. FS150. 350-0-350 v. 150 m/a, 6.3 v. at mmss, 5 v. 3 amps. FS150.X. Output 350-0-350 v. at 150 m/a, 6.3 v. at 2 amps. C.T. 6.3 v. at 2 amps. C.T. 5 v. at 3 amps. Fully shrouded The above have inputs of 200/250 v.	21/ - 31/6
	FS150X. Output 350-0-350 v. at 150 m/a., 6.3 v. at 2 amps. C.T. 6.3 v. at 2 amps., C.T. 5 v. at 3 amps. Fully shrouded	31/6
	The above have inputs of 200/250 v.	
	OUTPUT TRANSFC RM IRS	2.4
	MIDGET OP. $5,000\Omega$ to 3Ω	3/9 3/9
	8,000Ω to 3Ω MOP1. Ratios 26, 46, 56, 66, 90, 120-150 m/a. max. current, C.T. for Q.P.P. Class B, etc. Secondary 2/4 ohms. Top panel,	
	and clamped, each. OP10. 10/15 watts output. 20 ratios on Full and Half Primary OP30. 30 watts output, 20 ratios on Full and Half Primary Williamson's O.P. Transformer to Author's specification	5/6 17/9
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	Chokes for Williamson's Amplifier, 30 H. at 20 m/a	16/6
	FILAMENT TRANSFORMERS All 200/250 v. Input.	
		96
	F3. 6.3 v. @ 2 amps. F4. 4 v. @ 2 amps., 7/6. F6. 6.3 v. @ 2 amps. F6X. 6.3 v. @ 0.3 amps., 5/6. F12X. 12 v. @ 1 amp. FU6. 0-2-4-5-6.3 v. @ 2 amps., 10/ F12. 12.6 v. tapped 6.3 v.	7/6 8/ -
		16/6
	F24, 24 v. tapped 12 v. @ 3 amps. F29, 0-2-4-5-6,3 v. @ 4 amps., 18/9. FUI2. 0-4-6.3 v. @ 3 amps. FU24, 0-12-24 v. @ 1 amp	23/6 17/6
	FU24. 0-12-24 v. @ 1 amp	17,6
	F5. 6.3 v. @ 10 amps. or 5 v. @ 10 amps., or 12.6 v. @ 5 amps., or 10 v. @ 5 amps. F6/4. Four windings at 6.3 v. tapped 5 v. @ 5 amps. each, giving by suitable series and parallel connections up to 6.3 v. @	34/-
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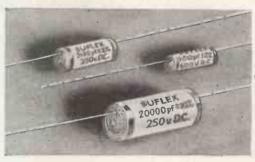


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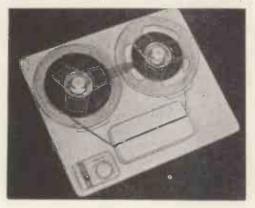
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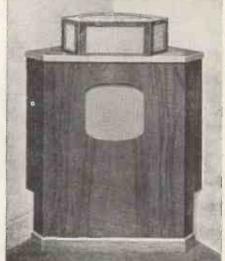
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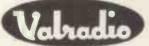
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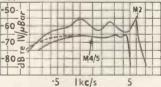
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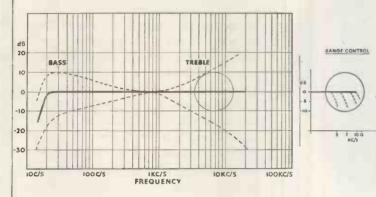
MODEL M.4/5: Illustrated: 0.4 to 5 Kc/s: weight §-oz. M5 similar to M4 with polythene membrane for close-speaking applications. (Std. Z = 600 ohms)

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DESIGN FEATURES OF HIGH FIDELITY REPRODUCERS



Frequency response of "H.M.V." Model 3001. Response of the main amplifier is shown by the full line; maximum variations given by the bass and treble controls are shown dotted. The inset shows the cut-off positions of the frequency range selector.

Two alternatives usually confront the designer of high fidelity record reproducing equipment. He can specify separate units for loudspeakers, pre-amplifier, power amplifier and turntable assembly; or he can incorporate all the units in one self-contained cabinet. Both systems have obvious merits, and both have their drawbacks, but when normal domestic conditions have to be taken into account, the latter course is usually the more acceptable, providing the cabinet is kept down to reasonable proportions.

The design of a self-contained reproducer of high fidelity standards raises problems not encountered when the separate unit method is adopted. Since a relatively large acoustic output and freedom from acoustic feedback and noise are basic requirements of high fidelity reproduction the principal problems the designer has to overcome concern the loudspeaker enclosure and the turntable and pick-up assembly. The way in which "His Master's Voice" engineers have overcome these problems is evidenced in the design of the new high fidelity reproducer, Model 3001, and the techniques and principles enumerated in this article have been tried and proven by the results achieved by that equipment.

results achieved by that equipment.

Model 3001 uses two special 13½" elliptical cone units, each covering its natural frequency range and mounted at an angle of 5°-7°. Consequently a greatly improved propagation of the high frequencies has been achieved.

Both these units have a high flux density and both are fitted with aluminium cone centres for increased output in the upper register. One of them has a specially designed speech coil, which sustains the upper response of the unit well into the normally accepted "high fidelity range", and the other has an improved low resonance cone and coil assembly which provides a clean bass response down to 30 c.p.s. The loudspeaker enclosure provides the maximum volume compatible with a cabinet of reasonable size and is fully lined with sound absorbing material and acoustically curtained to avoid standing waves and reflections. Throughout, the enclosure is constructed of

heavy cored timber to reduce vibrations and resonances to negligible proportions.

The net result of these features is a loudspeaker system having a good damping factor, wide angled distribution of the higher frequencies, a frequency range of 30-18,000 c.p.s. and a good mean spherical response.

Of necessity, the turntable and pick-up are mounted in close proximity to the loudspeakers. The dangers of sound coupling and mechanical coupling will be apparent. In Model 3001 the turntable and pick-up are mounted in a separate compartment that is completely insulated from the loudspeaker enclosure. This is achieved by mounting the entire assembly on a two stage mechanical filter, which comprises a special metal framework, spring mounted and mechanically loaded to bring its natural resonance down to the order of 10 c.p.s. or lower. In this way, both sound coupling and mechanical coupling are virtually eliminated.

Having dealt with some of the special problems of a self-contained reproducer, the general problems of high fidelity reproduction still remain. The requirements and features mentioned here are again all realised in Model 3001.

remain. The requirements and features mentioned here are again all realised in Model 3001. Taking the amplifier system first: the main amplifier must be capable of a large output with no more distortion than 0.1% total, and the frequency response should be flat from 20 to at least 20,000 c.p.s. if realism and good transient response are to be attained. This standard of performance is best achieved by using a balanced drive and push-pull output arrangement, preferably with triode or triode-connected valves, and a large multi-sectioned output transformer having high primary inductance and very low leakage reactance. A generous measure of negative feedback is of course essential.

arrangement, preferably with triode or triode-connected valves, and a large multi-sectioned output transformer having high primary inductance and very low leakage reactance. A generous measure of negative feedback is of course essential.

The pre-amplifier, which will normally incorporate the tone controls, should be characterised by high sensitivity, low noise and hum, and negligible distortion. Special low noise valves are desirable, and so is a balanced input to reduce the effect of stray magnetic fields. Tone controls must be flexible and simple to operate. There should be separate bass and treble controls giving maximum variations of about 30db at 50 and 10,000 c.p.s. respectively. An additional and extremely useful refinement is a frequency range selector comprising bridged "T" filters with cut-off frequencies at considered points, thus allowing optimum results to be obtained from all records whatever their age or condition (see graph).

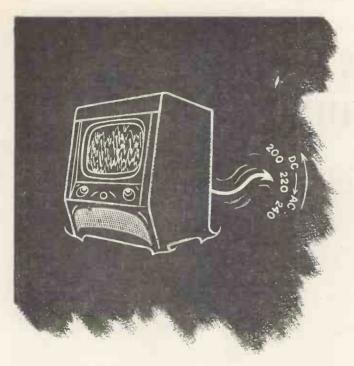
The motor unit must be free from rumble and wow and be capable of providing an absolutely constant speed. Fine speed adjustment is best achieved by an eddy-current device. Needless to say, the motor unit must be resiliently mounted. The pick-up should be an electro-magnetic component of good basic design, the chief requirements being low playing

The pick-up should be an electro-magnetic component of good basic design, the chief requirements being low playing weight, wide frequency response with resonances well controlled and outside the audio range, and preferably, an efficient hum-bucking arrangement. The stylus should be diamond for L.P. reproduction; sapphire is suitable for 78 r.p.m. records.

A high fidelity equipment whose design takes into account all the features and requirements outlined here will be capable of extracting full value from modern recordings.

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4.50mH 00000

great and conflicting claims for various systems only add to the confusion. However, it is now generally accepted that it is preferable to employ separate radiating sources for the various registers comprising the audio spectrum. The primary reason for the preference of a multiple system of this type is that extremely low distortion can be obtained, combined with a very wide frequency coverage. Since each of the sound sources is a specialist in its own part of the range, the combination can give a performance which is unattainable with a single source.

Any number of sources may be employed, but in the interests of simplicity and economy

the number is usually restricted to two or three at the most. In a "Twin" system, both radiators may be incorporated in a single unit (as in the well-known Goodman's Axiom 150 Mk. II and Axiom 22 Mk. II), or they may comprise two separate units.



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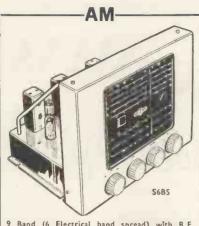
4.50 mH

received such praise that we are making public the full details of the system.

The Bass Unit should be mounted in an enclosure which will ensure adequate loading down to the lower end of the range and we shall be pleased to forward details of a specially designed cabinet, on application.

The Treble Unit should be mounted on a small open baffle, which need not be more than two feet square. Bass and Treble Units should be positioned as close together as possible.

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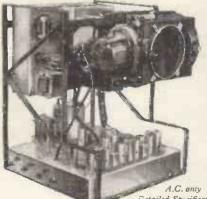
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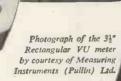
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1A3	3C24	6B5 6B6G	6P7G	7N7 7 Q7 7 R7 7S7	1723	78	809	4021A	CMV8 CMV28	DL63	EY51 EZ40
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1A5GT	3C45 3CP1	007	0070	1981	10 10:	80/S	81 ₀ 811	4045A	UAS	DL82 DL92	EZ40 FG17 FG27A FG67 FX215 G650 GDT4B GEX04 GEX34 GEX34 GEX34 GEX45/1 GEX54 GEX54/2
1A7G	3CPI	6B8	6Q7GT	78.7	19AQ5 19E2	80/3	011	4046A	CV3	DI 00	FGGGA
1A7GT	3D6/1297	6B8G	6R7	787	19E2	81	813	40004	CVO	DL93	FORM
1A7GF 1E23	3DP1	6B8G 6B8GT	6R7G 6R7GT	7W7 7¥4	19X3	82	814	4060A	CV24 CV43	DF83	Fu67
1B27	3FP7	6BA6	6R7GT	7¥4	19Y3	83	815	4205E	CV 43	DL94	FX215
1C5G	3LF4	SRES	6S7	- 724	21A6	83V	816	4212E	CV52	DRM1B	G650
1C5GT	3Q4	6BE6 6BG6G	6SA7	8D2	23D	84	826	4260A	CV57 CV58	DRM2B	GDT4B
1D5	3 Q 5G	6BH6	6SA7GT	8D5	24G	RRI	828	4313C	CV58	DRM3B	GEX00
	3Q5GT	6BJ6	6SC5	9D2	25A6/G	90 (1)	829A	4328D 4378	CV64	E4448	GEX34
1D6	26201	0000	0200	802	OF A COM	100TH 117L7GT 117N7GT 117Z6GT 210HL	829B	4378	CV67	E1148 E1155	GEX35
1D8/GT	384	6BR7	6SC7GT	9D6	25A6GT	100114	9538	4000	CV72	E1116	CEZ44/1
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1E7GT	4C27	6BW6 6BW7	6SF5	10	25L6GT	117N7GT	832	5763	CV75	E1190 E1191 E1192	GEA45/1
1F5G 1G4GT	4029	6BW7	6SF7	10 Y	25SN7GT	117Z6GT	832A	7193	CA83	E1191	GEX04
1GAGT	4D1	SRYS	6SG7	10D1	25¥5	210HL	833/833A	7475	CV85	E1192	GEX54/3
1G5G	4J53	6C4	6SG7 6SB7	11D3 11D5	25Z4G	210SPG	836	8011	CV88	E1231	GEX54/3 GEX54/4 GEX54/5
1G6/G/T	4THA	6C5	6SH7GT	1105	25Z5	210SPT	937	8012A	CV92	E1248	GEX54/5
TOOLOT	4TPB	905 C	68J7	12A6	DETERC.	210VPT	838	8013A	CV100	E1254	
1H5G	TIPB	6C5G 6C5GT	0047	12A6GT	25Z6G 25Z6GT	212E	841	8016	CV101/9	E1265	GEX84
1H5GT	5AP1	acout.	6SJ7G T	124001	252001	215P	843	8010	CV100 CV101/2 CV118 CV119 CV125	E1192 E1231 E1248 E1254 E1265 E1266 E1271 E1273	GEX64 GEX66 GEX69 GL486A GL451 GT1G GU20
1H6G	5A/102D	6C6 6C21	6SJ7¥	12A8GT	27	2131		8019 8020	CV 110	E1200	CEVES
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11.D5	5CP1	6D6	6SN7GT	12AT7	33	22 0P	863	9003	CV174	E1323	GTLC
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TLMD	0C/45UA	6E6	0061AT	10 4 77	35 A5 35L6GT	231D	866A	ACA/PEN	CV415	E1379	GTISO
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1N5GT	5FP7	6F5	68T7 6T7G	12AU7 12AX7 12BA6 12BE6	35T	250TH 262A/B	9003 K	AC4/PEN ACP4 ACT6 ACT17	CV987 CV988 CV1481 CV1583 CV1588 CV1596	E1480	H63 HD14 HF30
1P5GT 1Q5GT	5GP1	6F5G 6F5GT	6 T 7G	12BE6	35TG	ZOZA/B	869B 872A	AUTO	04490	E1468 E1474	2500
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17	5 X 4 G	SFSGT	8W7G	12K7GT	39/49	0100	931A	VE ATOT	D1	EB91 EBC3 EBC33	E POIA
2A3	5 ¥ 3 G	6F8GT 6G5G	6X4	12K8	40	323A 327A		ARP3 ARP4	77.5	EBC33 EBC41 EC54 ECC81 ECC82 ECC83 ECC91 ECH22	HP210 HR210 HR210 KMV6 KR3 KR6/3 KRN2 KT2 KT2
2A4G	5Y3GT	6G6G	6X5	12K8GT 12Q7GT	41	327A	954	AKP4	D15 D41	EBC41	E M v O
2A5	5Y4G	6 H 6	6X5G	12 Q7GT	41MP	328A/4328A	955	ARP13 ARP38	D41	EU54	ER3
2.8.6	5 Z 3	6H6G	6X5GT	128A7	41MPT	337A	956	ARP38	D42 D43 D63	ECC81	EE6/3
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9B7	5Z4G	6J5	6¥7G	12SC7	41MXP	357A	958A	AT4	D63	ECC83	KT2
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2C26A	6A3	6J5G 6J5GT	6Z5 7A2 7A4	128H7 12SJ7	42	337A 354V 357A 368A 380A	991	ARS6 AT4 AT15 AT40	DA30 DA60	ECH22	
20201	6A6	6J6	784	19617	42SPT	388A	1299A	ATP4	DA60	ECH35	KT30
2C34 2C40	6A7	6J7	7A5	128J7GT	43	394 A	1616	ATS70	DA90 DA100 DAF91	ECH35 ECH42 ECL80 EF22 EF36	KT30 KT31 KT32
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2C43	6A8G 6A8GT	6J7G 6J7GT	7A6 7A7	125K7GT	45SPEC	450TL 703A	1600	AU7	DAFOI	EF22	KT33C KT44 KT61
2D21	DASGT	6J 7GT	7A7	125K/UI		705A	1622 1624	A771	DDR25	EE36	WTAA
2E22	6AB7 6AB8	6J8G	7B6	12SL7GT	46	703A	1024	AZ1 AZ31	DET5	EF37	WTG1
2J21A	6ABS	8K8G	7B7 7B7E	12SN7GT	50C5 50CD6G 50L6GT 50Y6GT	707A/B 708A	1625 1626 1629 1635	AZ31	DET9	EAF OF A	WMOR
2J34 2J36	6AC7	6K6GT	7B7E	128Q7 128Q7GT	50CD6G	708A	1628	AZ41		EF37A EF39	F 100
2336	6AF6G	6K7	7RP7	12SQ7GT	50L6GT	709A	1629	B21 B30	DET12	EF39	E 171.
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2148	6AG7	6K7G 6K7GT	7C4 7C5	12SR7 12U5G	53.A	713A 714A¥	1642 1648	BL63	DET19	EF50	KT66 KT71. KTW61 KTW62 KTW63 KTZ41 KTZ63 KTZ73
2J48 2J54	6AJ7	8K8	708	12X3	53KU	717A	1648	BT45		EF54	KTW63
2J54B	6AK5	6K8 6K8G 6K8GT	707 7D5	1274	54	723A/B	1815	C5B C1C	DET25	EF80	KTZ41
2X2/879	6AK6	SESCO	7705	14B6	57	724A	1851	CIC	DF91	EF91 EF92	KTZ63
ZAZ/879	OAT F	6L5G	NT N	14E7	58	725A	1960	COA	DF92	EF92	KTZ73
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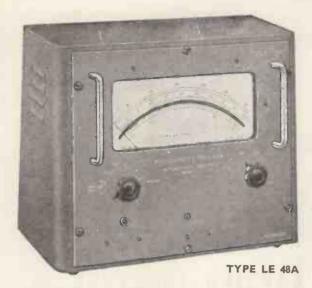
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350-0-350, 80 mA., 6.3 v. @ 4 a., 5 v. @ 2 a	19/6
200-230-250 output 3 v30 v., @ 2 a	17/6

	KECT	IFIERS	
	E.H.T. Penc	il Type S.T.C.	
Type K3/25	650 v.	1 mA	4/7
. K3/40	3.2 kV.	1 mA	6/-
,, K3/45	3.6 k♥.	1 mA	8/2
., K3/50	4 kV.	1 mA	8/8
,, K8/100	8 kV.	3 mA	14/8
., N3/160	12 kV.	1 mA	21/6
., K3/180	14.4 kV.	1 mA	24/6
		pe S.T.C.	
Type RM1	125 v.	60 mA	41-
,, RM2	125 v.	100 mA	4/6
., RM3	125 v.	125 mA	5/6
. RM4	250 v.	250 mA	18/-
		Full Wave	
6 v. l amp			41-
			8/-
			10/9
			15/-
B	ATTERY	CHARGERS	
200-250 V. A.	C. Will cha	rge 2 v., 6 v. and 12 v.	Car
		ed in strong metal cas	
		mored enemal Size	

long, 3½in. wide, 3½in. high.
Guaranteed 12 mths. The
above unit is manufactured
by PREMIER and does not contain Ex-Govt. components. Plus 2/6 39/6 post and pkg.

BATTERY CHARGER KITS

All incorporate metal rectifiers. Transformers are suitable for 200/250 v. A.C. cycle mains.

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9½ × 4½ × 2in...
10 × 8 × 2½in...
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All the components to build the above unit, 22/6, plus All the components to 1/6 pkg. and postage.

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bolt, 4BA nut.
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Installation instruction leadet included.
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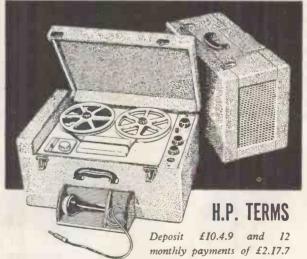
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carriage 5/-.
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	in.
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3.5 A	21 × 21 R.F. Thermo 7/6
4 A	21 × 21 R.F. Thermo 7/6
20 A	21 round M/C 8/6
40 A	21 round M/C 8/6
5 m.A	31 round 7/6
6 m.A	31 round 16/9
50 mg A	21 × 21 M/O 7/6
20 V	21×21 M/C 6/6
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Valve line-un 6817, 8V6 and 6 x 5, FOR A.C.
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Complete with one standard and one long playing head,
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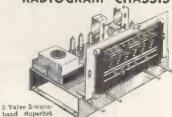
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VALVE LINE-UP: 787. 7B7, 7C5, 7C5, 7Y4, 3 WAVE-BANDS, Long, Medium and Short. CONTROLS Tuning, wave change, volume tope control only off Gram Position on Switch. Pick-up and Extension Speaker Sockets Incorporated. For use on 200/250° v. AC. mains. DIMENSIONS: Width, 16in., Height 13in., depth 8in.

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Advance P.1 Sig. Gen	£19 19	o o	£4 19	9	€1	8	-1
Packing and Carriage	7	6			00 =		-
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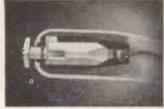
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Wireless World

RADIO, ELECTRONICS, TELEVISION

44th YEAR OF PUBLICATION

Managing Editor: HUGH S. POCOCK, M.I.E.E.

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H. F. SMITH

NOVEMBER 1954

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VALVES, TUBES & CIRCUITS

23. MINIATURE VALVES WITH 25mA FILAMENTS

The Mullard range of low-consumption valves for all-dry battery receivers consists of four types, the DK96, DF96, DAF96, and DL96, mounted on the standard B7G base. The filaments are economically rated at 1.4V, 25mA. The DL96 output pentode has two such filaments which are normally operated in parallel.

The filaments in a receiver using these four types may be fed in three alternative ways: (i) in parallel; (ii) in pairs in a 50mA chain, with the odd filament (say the DAF96) shunted by a 5% tolerance resistor to maintain the correct filament current; (iii) in a 25mA chain. The third method is suitable for ABC receivers with separate h.t. and l.t. batteries; but the variation of cathode current in the output valve, which can occur when the batteries are at different

stages of exhaustion, must be limited. For this purpose a special filament chain has been devised, of which full particulars are given in the Additional Notes.

For mains operation, supply variations should be allowed for by presetting the filament current (by means of a variable portion of the dropping resistor) to $24\text{mA} \pm 2\%$ at nominal mains voltage.

The valves are designed for optimum performance with a 90V supply; but there is no serious loss of sensitivity in the amplifier stages at voltages down to 67.5V, as the recommended screen-grid voltages of the amplifier valves are about 65V. In the output stage, however, the loss of power caused by battery exhaustion is more marked with lower nominal battery voltages.

The Mullard DK96 is a heptode frequency changer in which the first two grids form the oscillator, and the third grid is the signal grid. The optimum conversion conductance is $300\mu A/V$, and the cathode current is 2.4mA at an oscillator voltage of 4.0V r.m.s. The variable-mu characteristic gives good cross-modulation and allows the use of AGC. The screen-grid voltage is about 65V, but in ABC receivers it should be adjusted to give 0.6mA anode current at zero bias.

A tuned-grid oscillator circuit is recommended, with the earthy end of the oscillator grid resistor taken to the positive side of the filament. Feedback should be derived from the oscillator anode, with the feedback winding of the oscillator coil preferably series-fed, especially at the higher frequencies.

The DK96 is not suitable for use above 20Mc/s. Pulling at frequencies above 10Mc/s should be reduced by capacitive neutralisation between the oscillator and signal grids.

The Mullard DF96 is an IF amplifier with a mutual conductance of $750\mu A/V$ at a cathode current of 2.2mA. It is suitable for AGC operation, as its grid base has been lined up with that of the DK96. The DF96 and the DK96 can be operated with a common screen-grid dropping resistor; but in ABC receivers this is allowable only if the two filaments are in parallel or if the control-grids are biased to their respective filaments. In all circuits, however, a common screen-grid resistor allows the relatively high screen-grid current of the DF96 to affect the gain of the DK96, and thus to increase the spread in the overall sensitivity of the receiver.

The Mullard DAF96 is a pentode AF amplifier with a detector diode. A voltage gain of 60 is obtainable when the detector presents a source impedance of $500 \mathrm{k}\Omega$, and a voltage output of $5.0 \mathrm{V}$ r.m.s. is obtained at 3% distortion. If the valve is used as a triode, the gain is about 11 and the voltage output is $5.0 \mathrm{V}$ r.m.s. at 2% to 3% distortion.

With a bias resistor of $10M\Omega$ the detector load resistor should be limited to $500k\Omega$ to give minimum attenuation in the control grid input circuit and an adequate a.c. to d.c. load ratio. With a detector load resistor of $1.0M\Omega$ the bias resistor should be $22M\Omega$.

Anti-microphonic precautions are necessary only when the control grid voltage is less than 20mV for 50mW output.

The Mullard DL96 output pentode is designed for 90V operation; but the grid base at 67.5V is sufficient to allow operation at this lower supply voltage. A single valve, under Class A conditions with a 90V supply, will give a 200mW output at 10% total harmonic distortion for an input signal of 3.4V r.m.s. At 67.5V the output is reduced to 100mW.

Two valves may be used in push-pull, with the grid signal provided by a driver transformer, a centre-tapped choke, or a phase-inverter valve. The total cathode current of the two valves must not exceed 12mA. Class B operation, with all four filaments in parallel, gives, at 2% to 3% distortion, 440mW output at 90V and 235mW at 67.5V. The comparable outputs for Class AB operation, at 3% to 4% distortion, are 420mW and 220mW.

The Mullard DM70 subminiature tuning indicator, which has been described in Valves, Tubes, and Circuits Nos. 5 and 6, is suitable for use with these valves.

Reprints of this a lvertisement, with additional notes on the design of filament supply chains, a circuit for a four-value battery receiver, and value data, may be obtained free of charge from the address below.

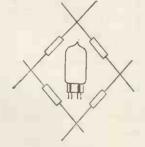




And detailed examination of the company's resources and experience in this field reveal that BRIMAR introduced:—

- the first mass produced aluminised cathode-ray tube;
- the first flat faced tube;
- the first 14" rectangular tube;
- the first 17" rectangular tube;
- the first 21" rectangular tube;
- the first electro-static tube.

Research and development to anticipate and meet the changing demands of the radio and electronic industries are integrated with modern manufacturing techniques in the production of BRIMAR cathode-ray tubes.



Consult BRIMAR

— the people who know — for your future equipment requirements

Standard Telephones and Cables Limited

Bring your equipment up to date with REPLACEMENT PICK-UP HEADS

If you already own a fine radiogram or record-player you now have the opportunity of rejuvenating it—of bringing it right up to date for a quite modest sum. Acos Hi-g crystal pick-ups are now available in a range of specially designed "plug-in" models to sult most famous

makes of record reproducing equipment. These Acos "Hi-g" pick-ups, you will find, represent a truly phenomenal advance in pick-up design—with regard to both reproduction and tracking characteristics (so important with many of the new microgroove recordings). Ask your Dealer!

MODEL **HGP 33-I** HGP 37-1 Collaro **HGP 33-I HGP 37-1** Garrard **HGP 39-1 HGP 35-1 HGP 41-1** HGP 45

HGP 33-1 Collaro. A Hi-g pick-up head incorporating the HGP 33-1 turnover cartridge for both standard and microgroove records. Will fit Collaro units RC 532; AC 534; AC3/534; 3/RC 532; and the Studio pick-up

HGP 37-1 Collaro. A Hi-g pick-up head Incorporating the HGP 37-1 turnover cartridge with cantilever sapphire styli. Designed for both standard and microgroove records. Will fit the above mentioned Collaro units.

Both models available in cream or walnut.

Ask for Data Sheets No. 4700 and 4800.

HGP 33-I Garrard. HI-g pick-up head incorporating the HGP 33-I turnover cartridge for both standard and microgroove records. Will fit Garrard units RC 75M; RC 80M; RC 90; RC 111; Model TA. HGP 37-I Garrard. A Hi-g pick-up head incorporating the HGP 37-I

HGP 37-1 Garrard. A Hi-g pick-up head incorporating the HGP 37-1 turnover cartridge with cantilever sapphire styli. Designed for both standard and microgroove records. Will fit the above mentioned Garrard units.

Ask for Data Sheets No. 4700 and 4800.

Hi-g pick-up heads incorporating cantilever sapphire styli. Separate heads for standard and microgroove records. Will fit the Acos GP 20 pick-up arm and the Garrard C type adaptor. Used on the following Garrard units: RC 72A; RC 75A; RC 80; and the model M unit. Can be used on any units which at present use the GP 19 heads.

Ask for Data Sheet No. 4400.

Separate plug-in type Hi-g heads for standard and microgroove records; fitted with cantilever sapphire styli. The crystal unit is identical to that of the HGP 39-1 above. Can be used on Garrard units RC 75M; RC 80M; RC 90; RC 111; and the TA player.

Ask for Data Sheet No. 4000.

Separate Hi-g plug-in type heads for standard and microgroove records incorporating the crystal unit as used in the HGP 39 pick-up head. Will fit Collaro units RC 532; AC 534; AC3/534; 3RC 532. Available in cream or walnut.

Ask for Data Sheet No. 4500.

Separate Hi-g pick-up heads for either standard or microgroove records. The crystal unit is identical to that used in the HGP 39-1 head. Will fit Garrard units RC 80; RC 72A; RC 75A; and the Model M player. Can be used on any unit which at present uses the Garrard C adaptor with GP 19 heads.

Ask for Data Sheet No. 4600.



... always well ahead

ACOS devices are protected by patents, patent applications and registered designs in Great Britain and abroad.

PRICE 32/6 (Plus 10/5 P.T.) for all types except HGP 39 models which are 32/- (Plus 10/3 P.T.)

"BELLING-LEE" NOTES

THREE - YEAR GUARANTEE AND INSURANCE

When we announced that we had increased our insurance cover on aerials from one to three years, dozens of letters came in from dealers asking for particulars, as they did not know of the existence of any insurance cover. This was most surprising in view of the fact that particulars have appeared on every piece of aerial literature issued by us for many years, and certainly on every instruction sheet. So that there need be no misunderstanding, we reprint the details of the cover below:—

INSURANCE COVER ON "BELLING-LEE" AERIALS

£1,000 against third party claims arising from personal injury or damage to property during the installation of "Belling-Lee" aerials by any dealer.

£1,000 against claims for damage to property arising from defective aerial material or faulty aerial workmanship for a period of three years.

£100 against claims for damage by lightning to the aerial system or receiver for a period of three years.

This insurance operates within the United Kingdom of Great Britain and Northern Ireland, from the date of purchase by the ultimate user, no matter where purchased.

The insurance cover applies only when the whole aerial, including mast, lashings and brackets, is manufactured by Belling & Lee, Ltd., and where there is no collateral insurance or after any existing cover has been exhausted.

MANUFACTURERS' THREE-YEAR GUARANTEE WITH "BELLING-LEE" AERIALS

If a "Belling-Lee" aerial (or part) is proved to be defective in workmanship or material within three years from date of purchase, the aerial (or part) will be replaced free of charge by the manufacturer.

CONNECTORS FOR 300 OHM FEEDERS

We understand that a large number of radio amateurs are changing over to 300 ohm feeders and we feel that the "Belling-Lee" plug and socket (L677/P and /J respectively);



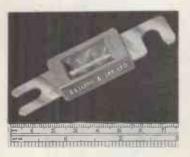
specially designed to snap onto ribbon feeder, is not as well known as it deserves to be. This was brought to our notice by several visitors to our stand at the Radio Show.

Provision is made to crimp the conductors into the spills.

Pins and sockets nominal lin. diameter spaced 0.312in.

SOCIETY OF BRITISH AIRCRAFT CONSTRUCTORS' EXHIBITION AT FARNBOROUGH

For the first time, we exhibited here, and quite shamelessly, we were fascinated by seeing so many "Belling-Lee" components on so much equipment designed to do such a wide variety of jobs. It was a very wonderful exhibition, but



we were far too busy ourselves to take full advantage of the opportunity to examine such an exhibition of instrumentation.

The organizers must be very gratified by the number of overseas visitors who came to the Display. At the official dinner the writer sat between a gentleman from Malaya and another from South Africa. Both were readers of this page.

Advertisement of BELLING & LEE LTD. Great Cambridge Rd., Enfield, Middx. Written 21st September 1934.

Coaxial coutlet sockets for one or

more installations



L.742 For use in demonstration rooms, workshops, etc., where up to six television receivers are required to operate at the same time without interaction. As the insertion loss at each outlet is considerable (25 dB), it should only be used where a high signal level is available.



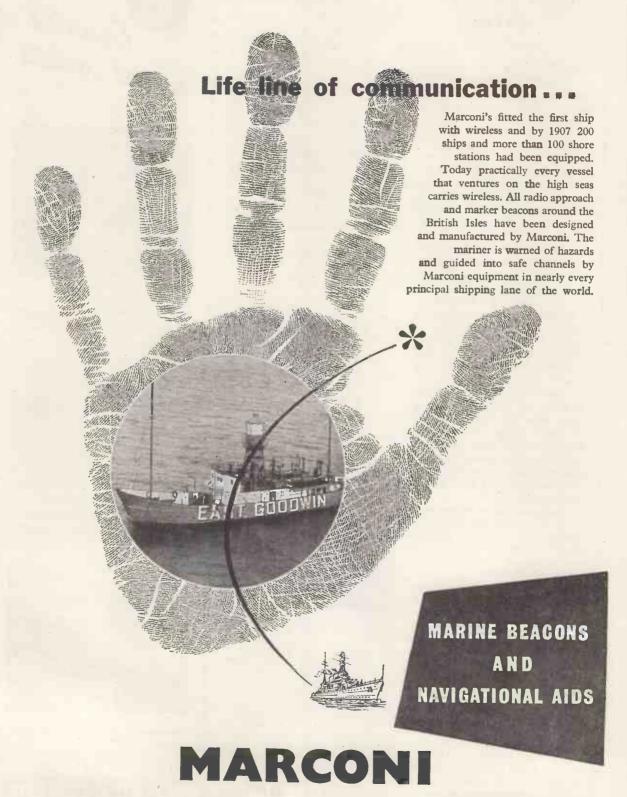
L.725/P. Padder network L.725/T. Termination network

Designed for skirting board termination of coaxial feeders up to 1 in. dia., supplied with termination or padder network, and gives an attenuation of 26 dB. Continuity of screening is provided by the bronze finished case.



L.735 A new, improved outlet box similar technically to L.725, but not supplied with termination or padder network. Accommodates 5/16ths in. dia. feeders. For use with the range of plugs L.1329/P, L.734 and L.781, and the "Belling-Lee" line attenuator.

BELLING & LEE LTD



MARCONI'S WIRELESS TELEGRAPH COMPANY LIMITED . CHELMSFORD . ESSEX

SUPERB E.M.I. EQUIPMENT

A TROLLEY MOUNTED PORTABLE OSCILLOSCOPE

TYPE WM.3.B. A compact general purpose D.C. Coupled portable Oscilloscope with facilities for rapid precision time and voltage Volts and time meter presentation - no measurements. calibration markers required. Displayed waveform measured by voltmeter bridge system (visual null balance). 9 range voltmeter gives high accuracy readings unaffected by amplifier gain or linearity. Dual 'Y' input paths with attenuators afford signal comparison and mixing facilities. Floating circuit enables AC/DC signals to be measured with respect to D.C. potentials within ±500V. Field of application - T.V. - Radar - Computers, and Industrial Electronics.

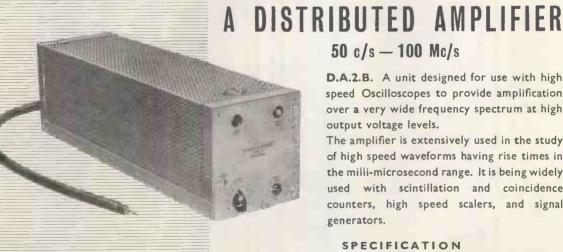
SPECIFICATION

C.R.T. E.H.T.								0.8 &	1.2 KV.
'Y' Amplifier					***		[D.C	6 Mc/s.
Max. Sensitivity	***		• • •		350 mm	/V (at	reduc	ed bane	dwidth)
Voltage Measurement \pm 10 mV $ \pm$ 500 V AC/DC \pm 2½% F.S.D.									
Time Measurem	ent				0.5 micr	osecon	ds —	4 milli-	seconds
Sweep Drive	1	Trigger	ed or r	ecui	rent, pl	nase and	freq	uency s	elected
Writing Speed			8	mill	i-second	ls/cm —	- L mi	croseco	ond/cm





FACTORIES



50 c/s - 100 Mc/s

D.A.2.B. A unit designed for use with high speed Oscilloscopes to provide amplification over a very wide frequency spectrum at high output voltage levels.

The amplifier is extensively used in the study of high speed waveforms having rise times in the milli-microsecond range. It is being widely used with scintillation and coincidence counters, high speed scalers, and signal generators.

SPECIFICATION

Input	Impeda	nce	•••		• • •		• • •	***	75 ohms	
Outpu	ıt İmpe	dance		***	•••				195 ohms	
Max.	Output	• • •	***						150 Vpp	١.
Bandy	vidth				• • •	50	c/s —	100 M	c/s (— 6db)
Phase	Respon	se			Sub	stanti	ally line	ar ove	er pass band	d
Gain									x 13	2

88



FEATURES

- Withstand overloads such as charging current of deformed electrolytic capacitors
- Instant starting no warming-up period
- Unlimited instantaneous overload
- Practically indestructible in service.
- No limit to size of reservoir capacitor
 - Simple wiring two connectors only.
 - Simple mounting no valve holder
 Small size...low weight
 - Low heat dissipation
 - Low cost

*RMS

RMA

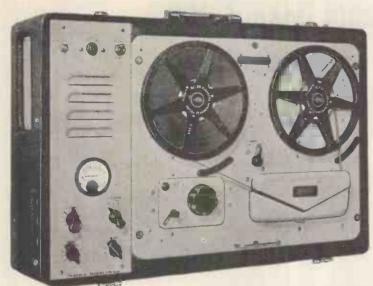
TYPE



Standard Telephones and Cables Limited

RECTIFIER DIVISION: Warwick Road, Boreham Wood, Hertfordshire

VORTEXION TAPE RECORDER



The amplifier, speaker and case, with detachable lid, measures $8\frac{1}{4}$ in. x $22\frac{1}{2}$ in. x $15\frac{3}{4}$ in. and weighs 30 lb.

 ★ The noise level is extremely low and audibly the hum level and Johnson noise of the amplifier, and deck are approximately equal. Only 25% of this small amount of hum is given by the amplifier alone.

★ Extremely low distortion and background noise, with a frequency response of 50 c/s.—10 Kc/s., plus or minus 1.5 db. A meter is fitted for the measurement of signal level and bias level.

Sufficient power is available for recording on disc, either direct or from the tape, without additional amplifiers.

★ A heavy mu-metal shielded microphone transformer is built in for 15-30 ohms balanced and screened line, and requires only 7 micro-volts approximately to fully load.

The .5 megohm input is fully loaded by 18 millivolts and is suitable for crystal P.U.s, microphone or radio inputs.

A power plug is provided for a radio feeder unit, etc. Variable bass and treble controls are fitted for control of the play back signal.

The power output is 3.5 watts heavily damped by negative feedback and an oval internal speaker is built in for monitoring purposes.

★ Facilities are provided for using the amplifier alone and using power output or headphones while recording or to drive additional amplifiers.

★ The unit may be left running on record or play back even with 1,750 ft. reels with the lid closed.

POWER SUPPLY UNIT to work from 12 volt. Battery with an output of 230 v., 120 watts, 50 cycles within 1%. Suppressed for use with Tape Recorder. PRICE £18 0 0.

TYPE C.P.20A AMPLIFIER

For A.C. Mains and 12 volt working giving 15 watts output, has switch change-over from A.C. to D.C. and "Stand-by" positions. Consumes only $5\frac{1}{2}$ amperes from 12 volt battery. Fitted with mu-metal shielded microphone transformer for 15 ohm microphone, provision for crystal or moving iron pick-up with tone control for bass and top. Outputs for 7.5 and 15 ohms. Complete in steel case with valves. **PRICE £30 16 0.**



Manufactured by

VORTEXION LIMITED, 257-263, The Broadway, Wimbledon, London, S.W.19

Telephones: LIBerty 2814 and 6242-3 Telegrams: "Vortexion, Wimble, London."

COSSOR presents Model 1052 double beam oscillograph

Two similar amplifier channels with ar. approximate gain of 2000 and an upper frequency response of 5 megacycles (—6DB) are features of this new Cossor Double Beam general purpose oscillograph. The repetitive or triggered time base has a sweep duration from 200 milliseconds to 5 microseconds.

The instrument will operate from power supplies of any of the various frequencies and voltages encountered in the Armed Services or from standard civil supply mains.

and Model 1433 voltage calibrator

Primarily designed to be used with the Model 1052 oscillograph the Cossor Voltage Calibrator Model 1433 provides an accurate means of calibration of input voltages to the plates or amplifiers of any oscillograph. Calibrating voltages are read directly from a wide scale meter without any computation being necessary. Measurements can be made to an accuracy of \pm 5% and the instrument can be used in any application where a source of accurately-known voltage is required.

Watch for the
NEW TELE-CHECK AND CRYSTAL
MONITORED MARKER GENERATOR
for Bands I and III

COSSOR ELECTRONIC INSTRUMENTS

Write for illustrated leaflets about both of these instruments

A. C. COSSOR LTD., INSTRUMENT DIVISION, DEPT. 1, HIGHBURY GROVE, N.5

Telephone: CANonbury 1234 (33 lines). Telegrams: Cossor, Norphone, London. Cables: Cossor, London

ALWAYS USE
COSSOR
TUBES &
VALVES

C.I.56

Five Advantages of the Clix TELEVISION TURRET TUNER

SPINDLE CONTROLLING SPRING OPERATING INDEXING OF DRUM AGAINST CENTRAL LOCATER SPRING - ON COVER ROTATING DRUM OR TURRET SPINDLE TO FINE ENCLOSED RADIATION HARD SILVERED PROOF COMPARTMENT FINE TUNING CONDENSER APERTURE FOR APERTURES FOR ADJUSTMENT OF INDIVIDUAL ADJUSTMENT HORIZONTAL OF RADIAL INDUCTANCE CERAMIC FEED THREADED BRASS INDUCTANCE CORES POLYSTYRENE RADIAL PAXOLIN HORIZONTAL COIL FORMER MICA - LOADED BAKELITE COIL SEGMENT

Full technical information and prices on request.

EDISWAN

THE EDISON SWAN ELECTRIC CO. LTD.

Member of the A.E.I. Group of Companies

Accurate switching
The rotating drum of the
Ediswan Clix Television Turret Tuner
indexes accurately to any of twelve
positions and re-sets precisely in these
positions after switching. No question

All circuits are adjustable with the unit in position in a Television receiver.

of mistuning after switching.

Adjustable cores to all inductances are easily accessible with the tuner in position in a Television receiver.

The tuner can, therefore, be set up or re-adjusted in its actual operating position.

Additional tuned circuits may be added at any time without removing the Tuner from the receiver.

The Ediswan Clix Tuner is designed so that additional coil segments can be added at any time while the tuner is in position in a receiver.

To tune to another channel the serviceman merely clips into position additional coil segments, carrying correctly wound coils, and trims them by the adjustable cores provided.

There is no need to dismantle the tuner or return it to the Factory for any part of this operation.

Wiring reduced to an absolute minimum thereby eliminating stray capacities.

Stray capacities between wiring can lead to serious mistuning on the very high frequencies of Television Band 3. The Ediswan Clix Tuner is designed so that wiring is reduced to an absolute minimum and materials are specially selected to overcome the problems of drift and instability encountered on these frequencies.

Suitable for mounting in deep or shallow chassis.

Four 4BA tapped holes are provided for mounting the Ediswan Clix Turret Tuner. If required, suitable mounting brackets can be provided for use in shallow chassis.

SOUND SALES LEADS WITH THE DX FOUR-F.M.

RADIOGRAM

This is a distinctly Hi-Fi Plus instrument combining F.M., Standard Broadcast Bands, AM/VHF, plus the ability to reproduce superbly your favourite long-playing or standard 78 records.

Achieved by the "A-Z"—F.M. Unit the "A-Z" Radio Unit and the phase invertor speaker. (Praised by Mr. P. Wilson of "The Gramophone" in his technical report) together with "A-Z" Junior Amplifier and the Collaro 3-speed



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The teaching methods are planned to meet modern industrial requirements.

We offer training in all subjects which provide lucrative jobs or interesting hobbies.

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ensure private and individual tuition. * Free advice covering all aspects of training is given to students before and after enrolment with us. * Equipment supplied upon enrolment and remains your property.

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SUBJECT(S) OF INTEREST NOV.

Banking

The only Postal College which is part of a world-wide Industrial Organisation

Marconi VHF Multi-Channel Equipment

TYPE HM 181



Multi-channel radio links are not only recognised economic alternatives to line and cable routes wherever the latter are costly because of intensive urban development or the wild nature of the terrain; they are frequently preferable in their own right. The type HM 181 equipment has been designed for comparatively simple schemes using two terminals working point-to-point or with a limited number of repeaters. It operates in the frequency range 150-200 Mc/s, employs frequency modulation and gives high performance with low distortion. It provides the following facilities:—

8, 16 or 24 channels.

Repeaters with easy channel dropping facilities.

Unattended operation.

Engineers' order wire.

Ease of access for maintenance.



MARCONI

COMPLETE COMMUNICATION SYSTEMS

Surveyed, planned, installed, maintained

MARCONI'S WIRELESS TELEGRAPH COMPANY LTD. · CHELMSFORD · E

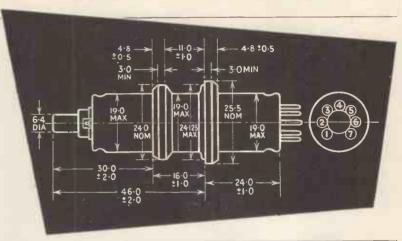
ESSEX

A NEW E.M.I. CENTIMETRIC VALVE

10 cms.
THREE BAND
KLYSTRON
2600-3700 Mc/s.

TYPE RK6112

This is a low voltage, reflex velocity modulated valve for use as a local oscillator in the 10 centimetre ("S") Band. It is of the plug-in type, with disc seals for resonator connection, and is Indirectly heated.



TYPE RK6112 SPECIFICATION

Power Output

100 mW minimum

Reflector Current

4 micro-amps max.

Frequency Range (with suitable cavity) Resonator Voltage #

2600 — 3700 Mc/s + 250 Volts Cathode Shield Volts

0 6:3 vales

Resonator Voltage *
Resonator Current
Reflector Voltage *
Range

+ 250 Volts
18 -- 34 mA
-- 55 to -- 350 volts

Heater Current 0.7 max.

* Measured with respect to Cathode



Write for particulars to-

E.M.I. FACTORIES LTD., HAYES, MIDDLESEX, ENGLAND

WESTON panel instruments

Both round and rectangular models of moving iron, moving coil, A.C. rectifier and H.F. thermocouple types are offered. In the range of rectangular instruments, which have been introduced to give the advantage of long, easily-read scales and to harmonize with rectangular panels, certain models are available with illuminated dials. Full particulars of types and ranges available are to be found in leaflets List Nos. W.1 and W.2, copies of which are available on request.

Larger instruments, both round and rectangular and for switchboard or panel mounting, are also available. These have scale lengths of 6" and 6\frac{1}{2}" respectively.



Rectangular panel instruments are available with scale lengths of 2.5", 3.2", and 4.2".
These offer the advantage of an increase in scale length of approximately 50% over their equivalent round models, for which they can be used as direct replacements using the same panel fixing holes.



Round models are housed in cases of 2", 2\frac{1}{2}" and 3\frac{1}{2}" diameter and have scale lengths of 7.", 2.1" and 2.8" respectively.

SANGAMO WESTON LIMITED

Enfield, Middx · Tel: ENField 3434 (6 lines) & 1242 (6 lines) Grams: Sanwest, Enfield

Scottish Factory: Port Glasgow, Renfrewshire. Port Glasgow 4|15|
Branches: London, CHAncery 4971 Glasgow, Central 6208 Manchester, Central 7904
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Bristol, Bristol 21781 Southampton, Soton 23328 Brighton, Brighton 28497

Newcastle-on-Tyne, Newcastle 26867 Nottingham, Nottingham 42403



TL/10 AMPLIFIER & "POINT ONE" PRE-AMPLIFIER



SPECIFICATION

A triple loop feedback circuit based on the famous TL/12. The output fransformer is the same size as in the TL/12.

Maximum power output: 10 watts.

Frequency Response: ± 1db 20 c/s to 20,000 c/s.

Harmonic Distortion: 0.1%, 1,000 c/s, 7.5 watts output.

Feedback Magnitude: 26 db, main loop.

Damping Factor: 25

Hum: -80 db referred to 10 watts.

Loudspeaker Impedancest 15 ohms, 8 ohms, and 4 ohms.

"POINT ONE" PRE-AMPLIFIER

The handsome gold escutcheon plate contributes to the elegant appearance, and blends with all woods.

Pickup
The pre-amplifier will operate from any pickup generally available in the world. A continuously variable input attenuator at the rear of the pre-amplifier permits the instantaneous use of crystal, moving-iron and moving-coil pickups.

Radio
The radio input sockets at the rear permit the connection of the LEAK V.S. turn unit. An input attenuator is fitted, H.T. and filament supplies are available from

Distortion
Of the order of 0.1%

Hum
Negligible, due to the use of recently
developed valves and special techniques.
Input selector

★ Input selector Radio, tape, records; any and all records can be accurately equalised.

* Treble
Continuously variable, + 9 db to - 15 db at 10,000 c/s

Bass Continuously variable, + 12 db to - 13 db at 40 c/s.

Continuously variable, 4 12 00 00 db at 40 c/s.

Volume Control and switch
The switch controls the power supply to the TL/10 power amplifier.

Tape Recording Jacks
An exclusive feature. Readily accessible jacks are provided on the front panel for secondary supplies with Tape Recorders. instantaneous use with Tape Recorders which have built-in (low level) amplifiers

* Write for leaflet W *

H. J. LEAK & CO. LTD., BRUNEL ROAD, WESTWAY FACTORY ESTATE, ACTON, W.3

'Phone: SHEpherds Bush 1173/4

Telegrams: Sinusoidal, Ealux, London

Cables: Sinusoidal, London

40 watt control unit, starter lamp, lamp holders, clips and diagram. Price, less observed to the control with the control of t Complete wiring diagram. Price, less tube, 22/6, plus 1/6 post. With tube, 30/-, plus 3/6 carr. NEW 5 AMP. THERMOSTAT (MINIATURE)



21" x 1" x 14" high Useful for the control of appliances such as convectors, gluepots, vulcanisers, hot plates, etc. This thermostat is adjustable to operate over the temperature range 50-550 deg. F., fitted with heavy (5 amp. A.C.) silver contacts size 1½in. long × ½in. wide, price 8/6, post 6d.; 1 amp. type, 3/6, 2 amp.

type, 5/6.

THE ELPREQ E.H.T.

GENERATOR



This is a made up unit working on the blocking oscillator/over-wound amplifying stage principle. It is of moderate power consumption (6.3 volt .8 amp. filament and approx. 59 mA. H.T.) and contains three of the latest BVA all glass valves. Output obtainable ranges from 6 kv. to 9 kv. with normal H.T. rail input by somewhat higher outputs can be obtained with higher H.T. supply.
Price 69/6. P. & P., etc. 5/-. BEDROOM-NURSERY MAINS MIDGET RADIO This is a made up unit working



All the parts, cabinet, valves, knobs, back—in fact everything will cost you only £3/15/- (plus 2/6 postage). The set is economical to run, too, for it uses only three valves in a special reflex T.F.R. circuit which gives ample power combined with good tone. Incidentally if you wish to give the sets to young children why not decorate the cabinet with a few suitable transfers? These can usually be obtained from local few suitable transfers? These can usually be obtained from local handicrafts shops. Circuiting and construction data free with the parts or available separately at 1/6.



Blanket. 27 yards of special heater wire and blueprint, 20/-Blueprint only 1/6. Alternatively make a Bed-Warmer. Constructional data 1/6.

TWO NEW CABINETS

THE BUREAU This is a really beautiful cabinet elegantly veneered in walnut and finely polished. The conand finely polished. The con-trol board, revealed when the front is dropped down is ample for the larger than average radio chassis or amplifier and alongside there is a space for a tape recorder or auto record a tape recorder or auto record changer mechanism. Both the radio board and the control board are left uncut to suit your own equipment. Size approximately 30in. high, 32in. wide, and 16in. deep. Price 16 guineas, carriage 12/6.



THE CONTEMPORARY

Also in the modern trend is this Also in the modern trend is this very stylish contemporary console. Veneered in oak with contrasting mouldings this has the "G" plan look and is ideal for use with this furniture or with other contemporary fittings or furnishings. The radio and motor board is uncut and its size 30in. X 151in. provides ample room for all equipment. Price £8/15/-. carriage etc., £8/15/-, carriage



-AMPLIFIER FOR TAPE RECORDERS

THE CLEVELAND "WIDE-BAND"

Designed in conjunction with Truvox engineers this high-fidelity amplifier ensures that best possible results are obtained from the amplifier ensures that best possible results are obtained from the Truvox Mk. III as well as from other go ut tape decks. Two input circuits are used—these have separate volume controls and so facilitate the mixing of programme matter. Miniaturized construction is used and the dimensions of the amplifier have been kept very small and in fact only approximately a 2in. section of the control panel and cabinet is required. The power pack also is on a separate chassis so that regardless of the type of cabinet, a position of minimum hum can be found. Hum level is very low at 50 db deeps for full output. down for full outport.

Applications additional to normal tape recording and reproducing

1. Radio amplifier for either direct listening or recording when used in conjunction with a crystal set or other tuner-detector.

2. Amplifier for direct listening of gramophone records or prerecorded tapes

3. Pre-amp, to boost the input to an existing amplifier.

TECHNICAL FEATURES

Two input jacks are provided, the first has a sensitivity of 1-micro volt for crystal microphone etc. The other for use with radio inputs and pickups has a sensitivity of 250 mv. The power output is 4 watts internally matched for 3 ohm loudspeaker. A magic eye is used to indicate depth of recording—the circuit of this, however is disconnected during replay. The frequency response of the amplifier is extremely wide, so ensuring that the best possible reproduction is obtained with modern tapes and heads. Using the Truvox heads the response is virtually level from 50 to 10,000 c.p.s. In addition to the two independent volume controls there is also a tone control and a master switch for record and replay. The amplifier is suitable for A.C. mains, voltages from 110 to 250. fier is suitable for A.C. mains, voltages from 110 to 250

Price £15. Hire Purchase terms if required—send a deposit of not less than 15% balance will then be spread over 12 months. Carriage and insurance 7/6. Delivery ex-stock. Demonstrations at all

THE TRUVOX TAPE DECK Mk. III/TR2U

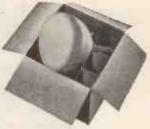
Correct directions for Pre-recorded Tapes.

Considered one of the best tape decks made, this incor-porates all the porates all the latest features and is ideal for serious work as well as for

Price 22 guineas.
Purchase terms if required, send a deposit of 15% or more, balance will be spread over months. Carriage and insurance 10/-.



FEW LAST



15in. MAGNETIC TELE-VISION TUBE

By famous maker. Specification Blue/White screen 9 Kv. ion trap triode, heater 6.3 v. at .55 amp., 50° deflection. New, with written guarantee. offered at approximately half price, £13/10/e each, plus 10/- carriage and insurance. H.P. terms, £4/10/- deposit and 12 monthly payments of 18/3. Limited quantity, so order immediately. mediately.

SLIDER RESISTORS

Heavy Duty Type

Size 7in. × 1½in. 11 ohms 4.5 amp., 22/-; Size 9in. × 11in. 1.2 ohms. 15 amp. 15/-; Size 13\in. × 1\in. 3 ohms 10 amp., 15/-.



£3/19/6 FEW Lectross warms room as it dries clothes, tumes, towels, etc. Size 3ft. wide, 3ft. high and 5in. deep. It has four stove

rails and works off A.C. or D.C. mains, consuming 650 watts. Fully guaranteed. Price £3/19/6.



CHASSIS ASSEMBLY

3 colour, 3 waveband scale covering standard Long, Medium, covering standard Long, Medium, and short wavebands, scale pan, chassis punched for standard 5 valve superhet, pulley driving head, springs, etc., to suit. Scale size 14½in. × 3½in. Chassis size, 15in. × 5in. × 2in. deep. Price 15/-, plus 1/6 post. Note: This is the one that fits our 39/6 table cabinet below.



THE WINDSOR STANDARD

This takes our Windsor 5 chassis and 6\(\frac{1}{1}\)in. speaker. It is a very nice job, walnut veneered and pleasantly polished. Size approximately 16\(\text{in.} \times 16\times 1. \times 7\times 1.

Offered at the particularly low price of 39/6, plus 3/6 post.

E. P. E. LTD

SEE OVER

OCCASIONAL RADIO



You will find that the building of our all-mains radio receivers is simplicity itself, and the more you make the less time each takes, everything down to the last nut and bolt is supplied, and everything fits together in a professional manner. The one illustrated above we call the "Occasional," in a choice of colours, Ivory or Walnut and the T.R.F. costs £5/15/- to make, H.P. terms being £2 deposit.

CONSTRUCTORS BARGAIN



Excellent rexine-covered cabinet -over production by one of our very famous makers. Complete with three-colour scale and metal chassis. Suitable for battery or chassis. Suitable for battery or mains receiver. Size approx. 13in. x 9\fin. x 6in. Limited quantity: price 17/6, postage 2/6.



RESISTORS
50 assorted 1 and 1 watt resistors,
Ranging between 10 ohm and
10 meg. ohm. (Our selection.)
Price 5/- pkt.



SERVICE DATA

SERVICE DATA

100 service sheets, covering British receivers which have been sold in big quantities, and which every service engineer is ultimately bound to meet. The following makes are included: Aerodyne, Alba, Bush, Cossor, Ekco, Ever-Ready, Ferguson, Ferranti, G.E.C., H.M.V., Kolster-Brandes, Lissen, McMichael, Marconi, Mullard, Murphy, Philco, Philips, Pye, Ultra. Undoubtedly a mine of information invaluable to all who earn their living from radio servicing. their living from radio servicing. Price £1 for the complete folder. Our folder No. 2 consists of 100 data sheets covering most of the popular American T.R.F. and superhet receivers "all dry" etc. which have been imported into this country. Names include Sparton, Emmerson Admiral, Crossley, R.C.A., Victor, etc. Each sheet gives circuit diagrams and component values, alignment and component values, alignment procedure, etc. etc. Price for the folder of 100 sheets is £1. Post free.

MINIATURE



The Elpreq Miniature Telvisor uses standard conventional circuitry, employing a total of 13 valves and 2 crystal diodes. The cathode ray tube used is a 2½in. Service type V.O.R. 139A, which has a standard equivalent and will therefore always be obtainable. The layout is extremely clean, straightforward, and professional. The wiring, whilst naturally being a little more intricate due to miniaturisation, is nevertheless completely turisation, is nevertheless completely accessible, and very good results have been obtained.

The total cost, if you have to buy every part, would come to £16.£17, but you may have many of the components already in stock as only standard conventional components are used. A carrying case, similar to the artist's litustration above, will be approximately 9½in. x 8in. x 6in. (Internally). Full construction data, layouts, diagrams, templates, etc., running into some 50 to the control of th templates, etc., running into some 50 sheets, is available, price 5/-, post

ORTABLE BATTERY RADIO ALSO CONTAINING DATA FOR CONVERSION TO THE PICNIC PLAYER

FEW REMAIN

This cabinet is offered below cost. It is suitable for a televisor using tube sizes varying from 12in. to 17in., its overall dimensions being 3ft. 5in. high, 1ft. 4in. deep. 1ft. 10in. wide. It Is complete with plywood back and "Bowler Hat." Originally made for a very expensive televisor and really good quality. Unrepeatable. Offered at £7/5/- or £2/8/4 dep., carriage, packing, etc., 12/6. Note: These are cut for 12in. tubes, but the holes for the controls are not drilled.





SEND 2/6 to-day for constructional booklet entitled "STROLLER"

CENTIMETRE RADAR TRANSMITTER RECEIVER

new and complete tains magnetron, rhumba-tron, spark gaps, wave guides, Government over £100 each to make.

assorted 1 watt resistors. watt resistors, Ranging be-tween 10 ohm to 5 meg. ohm. (Our selection.) Price 7/6 pkt. Post 6d.



L.T. RECTIFIERS
All recently manufactured and
guaranteed. All full Wave Bridge
type. CIRCUIT DIAGRAM
INCLUDED.

5-12	volt-1	amp.	7/6
	volt-2		11/6
	volt-4		17/6
	volt-6		27/6



COIL PACK Long, medium, short wavebands. With necting gram. Price 19/6. Post 6d.

H.T. RECTIFIERS
FAMOUS SELENIUM
"SENTERCEL."
All are this year's stock—for higher voltages join two or more in series.

R.M. 1.	125V.	60Ma.	3/9
TANAL TO	ALJY.	ooivia.	3/7
R.M. 2.	125V.	100Ma.	4/2
ALIAVA: A:	14J V .	IOUIVIA.	~4/2
R.M. 3.	125V.	120Ma.	5/9
ACIATA. J.	123 V .	IZUIVIA.	2/2
R.M. 4	250V.	250Ma.	16/-
TATIANT A	230 V.	2301V1d.	10/-

PORCELAIN STAND OFF INSULATORS

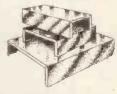
threaded Price 6/doz.



HEATER TRANSFORMERS
All 200-240 Volt working.
6.3V 14 amp. 5/9
6.3V 3 amp. 9/6
2V 3 amp. 7/6
4 and 6V 2 amp. 7/6
Special Type over wound to give normal H.T. and with primary tapping 6.3V. and 2.3 amp.—9/6.



CONNECTING WIRE SNIP P.V.C. insulated 23 s.w.g. copper wire in 100 ft. coils, 2/9 each. Colours available: Black, Brown, Red, Orange, Pink, Yellow, White, Transparent. 4 coils for 10/-



BLANI 18 S.W.C											
$7 \times 3 \times 2$	٠				٠				٠	٠	3/9
91 × 41 × 21											5/-
10 × 8 × 21											5/6
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10 × 51 × 21				٠	٠	٠	۰		٠	٠	5/-
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12 × 9 × 2}											7/-
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14 × 10 × 3											7/9
16 x 10 x 3		١,									8/3
16 × 12 × 3			4	4	٠		٠	٠		٠	8/8
19 × 9 × 24											8/3
											10/-

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INSTANTUS Creenhouse Heate

INSTANT HEAT CONVECTOR

CONVECTOR
The heater with the lowest
possible thermal capacity, 4ft.
long; made from heavy gauge
sheet steel (galvanised), 1 kw.,
suitable A.C. or D.C. Price only
£2 or with thermostat £3/15/-.
Note: The thermostat mounts
separately and will control up to three heaters.



EX-ROYAL NAVY SOUN POWERED TELEPHONE SOUND

These require no batteries, and will go for long periods without attention. Complete with generator and sounder which gives a high pitched note, easily heard above any other noise. Also fitted with an indicator lamp which in quiet situations can be used instead of the sounder, or where several h'phones are used together will indicate which one is being called. Size 7\(\frac{2}{3}\times \text{in}\times \text{y}\times \text{in}\times, \text{wall}\times \text{min}\times \text{discate the min}\times \text{di office, warehouse, factory, garage, etc. Price 57/6 each, plus 4/6 carriage.

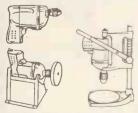
MULTIMETER KIT



All the essential parts, including 2in. moving - coil meter, selected resistors. wire for shunts, 8-

point range selector, calibrated scale, stick-on range indicator and full instructions for making are available as a kit, price 15/-, plus 9d. post and packing.

SENT FOR £1 ONLY BLACK AND DECKER ELECTRIC TOOLS



in. drill, £5/19/6 or £1 deposit Bench stand for drill £3/7/6— Lathe stand for drill, £5/5/- or £1 deposit. The three items supplied for £14/12/- or 43/- deposit.

INFRAY THE LAMP

room or other place where air temperature is low as it emits Infra-Red Rays which not only warm you but relieve pain, if you have any, and keep you healthy. Means real comfort in bed or in work-

Economical because its ravs warm

Economical because its rays warm you and not the room.

Costs only \(\frac{1}{2}\)d. per hour to run (electricity at 1d. per unit).

Works off lighting circuit (full instructions supplied).

Instructions supplied).

Absolutely safe for continuous
burning, no health or fire risk.

Ideal for many other uses: over pet's basket—rearing pup, chicks
—over desk—work bench, etc.

Completely and unconditionally guaranteed for five years.

All complete and ready to work. Price 36/-, post and pkg. 2/-.

Money refunded in full if after seven days' trial you are not completely satisfied. Please state mains voltage.

SUPERHET RADIO BY BEETHOVEN NOW AVAILABLE FOR LONG, MEDIUM and SHORT WAVES



Extremely well built on chassis size approx. 9½×7½×8½ using only first-class components, fully aligned and tested, 110-240 volt A.C. mains and tested, 110-240 volt A.C. mains operation. Large clear edge-lit dial. Three wave bands covering Long, Medium and Short waves. Complete with five Mullard valves, frequency changer, double diode triode, pentode output and full wave rectifier. Complete with Rola loudspeaker ready to operate. Special cash-with-order price this month, £8/17/6, carriage and insurance 7/6. Hire purchase terms £3 deposit, balance over 12 months.

THE WOLSEY 54

A really fine ready built modern Superhet at the remarkable price of £8/19/6 or £3 deposit, balance over twelve months.

The Wolsey 54 is an A.C. mains superhet employing latest

mains supernet employing latest circuitry covering long and medium wave bands in an ultra modern case with illuminated dial—overall size approximately 11\perp x x 8—complete ready to work—twelve months' guarantee.

Really beautiful walnut veneered and polished cabinet for only 39/6 if purchased at the same time as the Beethoven 5 valve superhet chassis (illustrated above). Bought separately the price of the cabinet is 49/6. H.P. deposit on cabinet and chassis is 32/cabinet and chassis is 32/-



CONSTRUCTOR'S PARCEL Contains cabinet as Wolsey 54.
drilled metal chassis—dial—
pointer, etc., 29/6. All other components available total cost £5.
Data 1/6 (free with component).

THE CLEVELAND "ORGANTONE"

The Cleveland "ORGANTONE" is a 5-valve 3-wave band superhet covering long wave (1020-1,875 metres), medium

long wave (1 020-1, 875 metres), medium wave (187-545.5 metres) and short wave (16-50 metres). Built to a very stringent specification, it attains a high level of performance both with regard to sensitivity and fidelity.

Osram all-glass miniature valves are employed throughout and low loss iron cored coils in both aerial and oscillator sections together with permeability tuned I.F.'s account for an excellent signal to noise ratio. Full A.V.C. is applied to both frequency changer and I.F. stages, and particular care has been taken to ensure freedom from frequency drift. frequency drift.

frequency drift.

The output stage utilises variable negative feedback for sone control, and, but for standard pentode correction, no cut in the ordinary sense is applied. A gram, position is provided on the wave change switch and reproduction of records is particularly good. An amply proportioned power transformer with a primary tapped for 110-280 voits gives complete isolation from the mains.

Chassis size is 12in. × 7ln. × 7ln. —Scale size is 10in. × 4in.

This receiver has been tested in particularly difficult areas and its stability and noise rejection have produced exceptional results. It is an instrument which could fairly be described as a custom-built chassis.

Price £11/10/- or £3/168 deposit—carriage, etc., 7/6.

A circuit diagram and photograph available price 2/- post free.

VARIABLE POWER
RESISTORS
Mounted on substantial framework, overall dimensions approximately 11×3½×6in. high, 25 amps. 4 ohms. Quite suitable for rewinding for other values, power rating exceeds 250 watts. Adjustment is by twisting protruding knob which is the only part that needs to show in front of panel. Price 17/6, carriage and packing. 2/- extra.

HEAVY DUTY MAINS
TRANSFORMERS
400-0-400 at 200 m/a. with two
4-volt L.T. windings, both rated
at 6 amps. A really massive
job made for services equipment—
limited quantity 19/6 each.

TRANSFORMER
LAMINATIONS
Ideal for making up experimental
and special purpose jobs. Price
1/6 per lb. or 1/6 per dozen pairs
(approximately 48 required for
lin. stack), size 4½in. × 4in.
(approx.). Small size, suitable
for output transformers, etc.
price 6d. per dozen pairs.

BREAKDOWN UNIT

BREAKDOWN UNIT Unit for breaking down, offered at little over the price of the \$\frac{g}{1}\$in. Aladdin Coil Formers. Note: all parts can easily be removed as they nut and bolt together. The unit contains:—6 Aladdin \$\frac{g}{1}\$in. coil formers with dust cores.

6 metal cans for above coil formers.
1 4-position 12-pole switch.

formers.

1 4-position 12-pole switch.
6 miniature R.F. chokes.
2 25 mfd. 25 v. electrolitic.
30 paper tubular condensers.
002 to 1 mostly for 450 v.
56 carbon resistors value from 1-watt to 2-watt.
2 medium size R.F. chokes.
7 moulded octal valve holders.

7 moulded octal valve holders. 1 moulded diode valve holder. 20 mica condensers (moulded, silver and ceramic).

silver and ceramic).
7 insulated top caps for valves.
4 components strips (1 40-way,
111-way, 15-way, and 13-way).
1 very useful chassis size 18×5×
3½in. Plus dozens of nuts, bolts,
screws, washers and other useful
items such as ½in. spindle extender, etc., etc.
Price 7/6, post and packing 2/6.

MAKING A CONVECTOR HEATER?
250-watt elements ideal for use with home built convectors, towel rails, airers, etc. Price only 2/6 each, post and pkg. 6d.

METERS FOR BATTERY

CHARGERS

2in. square Bakelite cased meter reading 0-5 amps. Price 9/6, post and packing 9d.

CHANGER TRANSFORMERS

9 v. 6 15 v. secondaries, suitable for 6 v. and 12 v. batteries. Charging rate up to 6 amps. Amply rated, price 21/6, post and packing 2/6.

UNIVERSAL METER 2-milliamps moving coil move-ment. Complete with sheet of printed scales, covering most ranges of volts, milliamps, amps. Price 9/6 post and packing 9d.

VALVES FOR V.H.F.
Type C.V. 64 and C.V. 186
Magnetrons unused and guaranteed. Price £2/10/-, post and
insurance 10/-.

HEAVY DUTY CHOKE
300 milliamps, 7 henrys, 50 ohms.
D.C. Size approximately 4½ × 4½ × 3in. New, not Governmen;
surplus, price 10/-, plus 2/post and packing.

SEE PREVIOUS PAGES DE DE DE LE PROPERTO DE LA CONTRACTION DEL CONTRACTION DE LA CONTRACTION DE LA CONTRACTION DE LA CONTRACTION DE LA CONTRACTION DE LA CONTRACTION DE LA CONTRACTION DE LA CONTRACTION DE LA CONTRACTION DE LA CONTRACTION DE LA CONTRACTION DE LA CONTRACTION DE LA CONTRACTION DE LA CONTRACTION DE LA CONTRACTION DE LA CONTRACTION DE LA CONTRACTION DE LA CONTRACTION DE LA CONT



Price this monta 15 gns.,

carr. etc. 12/6-also

heing 15%

5-WAVE BAND ASSEMBLY



5-wave coil pack for up to 11 mtrs., with R.F. stage, three-gang tuning condenser, slow motion drive, I.F. transformers and numerous other parts, make a really fine receiver. Price £6, plus 10/- post and insurance. Note: The above are new, but removed from chassis.

ELECTRICAL BARGAINS In addition to our large range of radio accessories we also carry a good stock of electrical wiring accessories; details of a few of these can be found below:—

T.R.S. CABLES, 250 v. CLASS
1/.044 Twin flat 9d
3/.029 Twin flat 1/-
3/.029 Twin with earth 1/3
3/.020 3 Core flat 1/6
3/.036 Twin flat 1/4
3/.036 Twin with earth 1/7
3/.036 3 Core flat 2/-
7/.029 Twin flat 1/0
7/.029 Twin with earth 1/11
7/.036 Twin flat 2/9
7/.036 Twin with earth 3/3
7/.064 Twin flat 4/9
LEAD-COVERED CABLES
250 - CTASS

3/.029 3 Core 2/3 2/8 3/3 7/.064 Twin CLIX 15 AMP. FOOT PLUG



SOCKETS HICRAFT

Flush type for skirting, 5 amp. 3-pin shuttered, 1/3 each; ditto with switch, 2/3

LAMP HOLDERS
Bakelite, 1/- each or 10/6 doz.
Bakelite skirted Batten holder, 1/6 or 15/- doz.

Bakelite type threaded, for §in. with HO. skirt, 1/6.



5 AMP. SURFACE SWITCHES HICRAFT OblongBrown Plastic 1-way 1/3 each. Oblong White Plastic 1-way,

MadetoB.S.S. specification, shuttered in m o u l d e d Bakelite case,

8/6 each.

Oblong Brown 2-way				each
Oblong White 2-way				23
Round Brown 1-way				33
Round White 1-way				99
Round Brown 2-way			1/6	23
Round White 2-way			1/6	33
	*	10	* = * = = =	

15 per cent. discount if bought in dozens in dozens.

EMPRESS CONSOLE

AVAILABLE BUREAU TYPE

cabinet is undoubtedly a beautiful piece of furniture. It is elegantly veneered ex-It is elegantly veneered ex-ternally in figured walnut, internally in white sycamore. The radio section is raised to convenient level but is not drilled or cut. The lower deck acts as the motor-board again, acts as the motor-board again, is uncut, it measures 16 × 14 and has a clearance of 5in. from the lid. There is a compartment for the storage of recordings. Overall dimensions of this essentially modern cabinet are 3ft. wide, 2ft. 8in. high, and 1ft. 4½in. deep.



Ref

3-wave (L. M. & S.) 5-valve £12 12 0 Ref B3 Pushpull 6-valve 3-wave.... £15 15 0 Ref. B3PP Pushpull with R.F. stage 3-wave 7-valve 6-wave L.M. and 4 short waves (band spread)

DULCI RADIO CHASSIS

Complete range of these famous receivers now available at all our branches—cash or Hire Purchase demonstrations gladly given.

15 15 18 15 15 B3PP/RF 0 **B6** B6PP 18 18 0 23 2 0 B6PPRF All available on H.P.-deposit 15 per cent, balance over 12 months.

MULLARD AMPLIFIER

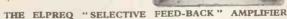
A High Quality Amplifier designed by Mullard engineers. Robust high fidelity, with a power output exceeding 10 watts and a harmonic distortion less than .4% at 10 watts. Its frequency response is extremely wide and level being almost flat from 10 to 20,000 C.P.S.—three controls are provided and the whole unit is very suitable for use with the Collaro Studio and most other good pickups. The total cost of the amplifier is around £11. For 30/- extra a unit completely made up and tested can be supplied. Carriage in either case is 10/- extra. Data will be provided with all orders for components. Send for the "Mullard Amplifier Shopping List." Shopping List.

CHASSIS BARGAIN

7-valve pushpull radio chassis with approximately 7 watts output—designed for high quality gramophone reproduction but equally good on radio—covers long, medium and short wave bands—uses latest midget B.V.A. valves and most up-to-date clrcuitry—price only £12/15/-, or in fine walnut veneered cabinet, £14/14/—carriage and insurance 10/- extra.

GRAMOPHONE AUTO **CHANGER COLLARO 3/521**

The latest three-speed type with the famous "Studio" turn-over pickup. Price £11/10/0, carriage etc.





The amplifier is fitted with independent bass and treble control, both connected through different feed-back loops so that no "cut" at all in the ordinary sense is applied. The variation which can be achieved, by applying various degrees of negative feed back in the higher and lower ranges of the sound strata will accommodate all strata will accommodate all individual tastes.

We strongly recommend a 12in. speaker in order to make

the fullest use of the instrument's potentialities. Booklet and set of components available at once at £3/19/6, post, etc., 2/6. Booklet separate 1/6. 12in. speaker to suit £3, post free if bought with amplifier. Now, available, ready to work, 20/- extra.

PRECISION EQUIPMENT LTD. ELECTRONIC

249, Kilburn High Road, Kilburn. (Openi ng shortly.)

Middlesex. Phone: RUISLIP 5780 Half-day Wednesday. Post orders should be marked "Dept. 2" and addressed to our Ruislip dept.

42-46 Windmill Hill, Ruislip 152-153 Fleet Street, E.C.4. Phone: CENTRAL 2833

Half-day Saturday.

STAR
71° diameter by
6° deep Price 7/6
ea. Post etc. 1/3. SENIOR
Ilif diameter by
4 deep. Price
13/6 each. Post
etc. 1/9. JUNIOR 61° diameter by 31° deep. Price 7/3 each. Post etc. 1/3. BIJOU 5½° diameter by 2° deep. For 40/60 watt lamps. Price 6/6 each. Post etc. 1/3.

LIGHT WEIGHT REFLECTORS Ideally suitable for all purposes where the intensification of elec-tric illumination or infra red is required. The material used is light-weight alu-minium, highly polished. All are pierced for Stan-dard Lampholder. STAR

LIGHT WEIGHT

Post etc. 1/3.

BELL
51 diameter by
5 deep. Price
6/3 each. Post
etc. 1/3.

1" MICROMETER Exceptional purchase Exceptional purchase enables us to offer a lin. precison micrometer at the very low price of 10/-. A micrometer is an essential part of an engineer's equipment. You will have found the need for one on many occasions in the past for measuring wire gauge, etc. Price 10/- post free.

NOTE: We now have a waiting list for this, orders In rotation.



Veneered & polished — less glass, makes ideal extension

speaker cabinet for 12in. Price 19/6. plus 3/6 carr.

SOMWEAVE



This really lovely loud-speaker fab-ric we offer at approxi-mately a third of today's cost.
It is 42in.
wide and
Our Price
is 12/- per
y ar d or anels 12in.

x 12in., 1/9 each. This is also very suitable for covering plain wooden cases, for portable radio amplifiers, etc.

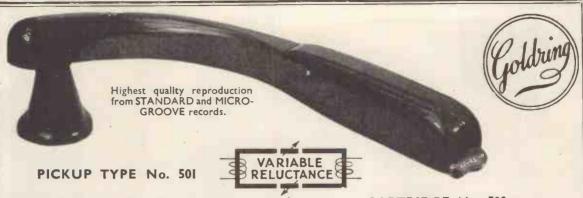
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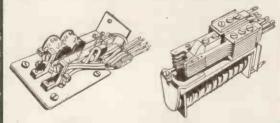
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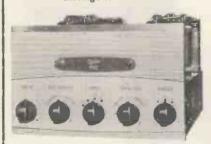
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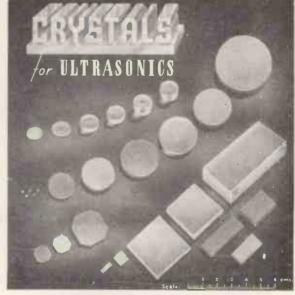


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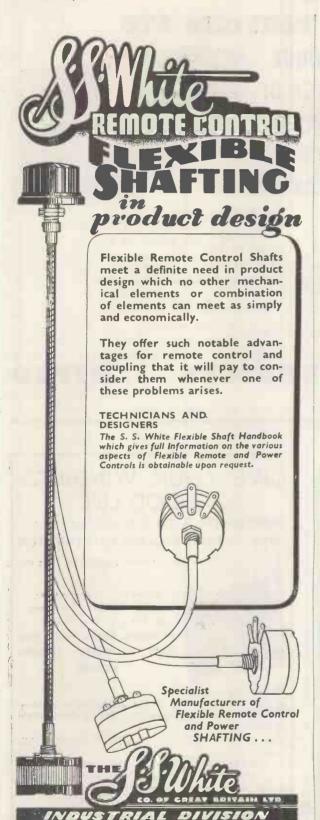
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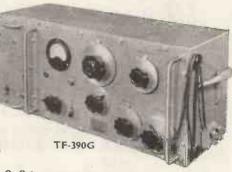
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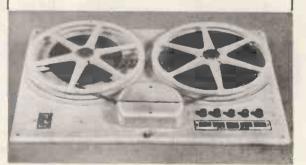
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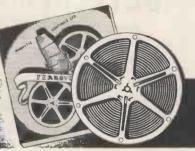
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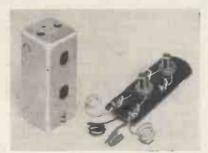
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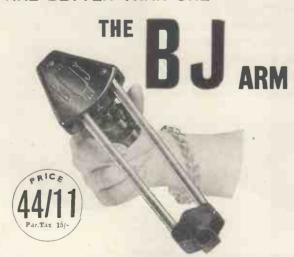
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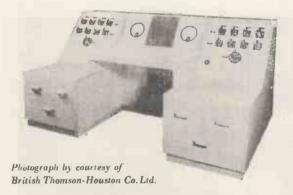
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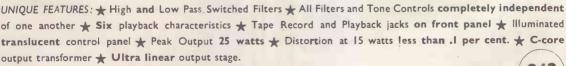
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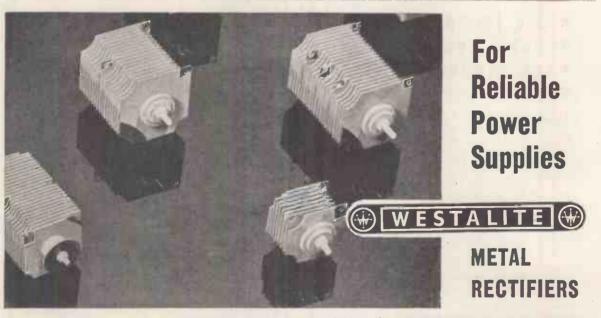
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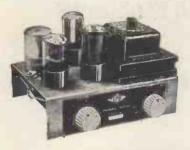
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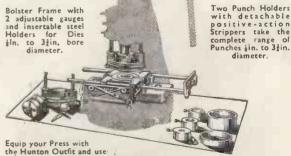
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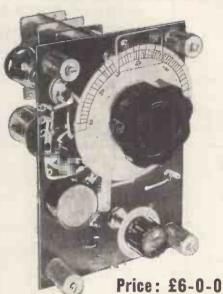
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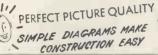
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It is suitable for use with any type of High Fidelity Amplifier.

The descriptive manual, including circuit and Component Layout etc., is available for 1/6.

THE COMPLETELY ASSEMBLED CHASSIS, ready for use, aligned and tuned

£B/17/6 (plus 6/- carriage and insurance).

THE NEW DENCO ULTRA MIDGET SUPERHET COIL PACKS

A COMPLETE KIT OF PARIS 10 By HIGH GAIN AMPLIFIER for operation on A.C. or D.C. Mains, 200-250 volts.

This amplifier will give 3 watts output for the small input voltage of only 75 millivolts, and is therefore suitable for use with any type of pick-up from the crystal type to the miniature H/F Magnetic type.

A tone control is incorporated and the quality produced is excellent. The overall size of chassis is 9 in. × 5 in. × 7 in. and valve line-up 25 75 -6 sH7-25 L6.

Price of complete kit, including drilled chassis and valves, £4/2/8, plus 63 in. P.M. (which fits on chassis), 16-7, or 8in. P.M. (18/2). Price of fully assembled chassis ready for use, £5/5/- (plus cost of speaker).

Copy of assembly instructions and components price list available for 1/3.

MODEL CP4/L. A 4-station "Pre-set" unit providing any 3 stations on medium waveband and one station on long wave, price £1/13/4.

MODEL CP4/M. A 4-station "Pre-set" unit which provides any 4 stations on medium waveband. Price £1/13/4.

The above are supplied fully wired leaving only four connections to be made.

The above are supplied than when earling only the tions to be made.

MOBEL CP3/370PF and CP3/500PF. Completely wired 3 waveband Coil Packs for use with either 350 PF or 500PF condensers. Coverages 190-550 metres, 800-2000 and 15-50 metres. Prot £2/2/8.

An attractive Dia and Drive Assembly is available for 25/-.

Overall size of each unit 3½in. x 2½in, x 1/1n. deep.

BATTERY CHARGER KITS

All kits are for A.C. Mains 200-255 volts. They comprise a Metal Rectifier and Transformer, tapped for 6 or 12 volt charging, and a tapped Resistor, with Selector Switch, to enable the charging rate to be varied. A M/coll meter 5 amp. max., 13/6 extra. For 6 or 12 volt batteries at max. 1 amp. £21/7/6 For 6 or 12 volt batteries at max. 2 i amp. £25/5/3 For 6 or 12 volt batteries at max. 4 amp. £23/2/6 An easily followed Wiring Diagram is included with each kit.

FILAMENT TRANSFORMER

BRAND NEW C.R.T. MASKS Latest aspect ratio for 12in. "Round" tubes, finished Ivory (plus 1/- postage) 12/6 SPEAKER BARGAINS PLESSEY, 10in. 3 ohm V/coil
TRUVOX 12in. 3 ohm V/coil
BOLA, 12in. 3 ohm V/coil
BAKERS, 12in. 15 ohm V/coil
GOODMANS, 12in. 15 ohm V/coil
(Carriage and Ins. 1/6 extra). £1/5/0 £2/9/6 £3/19/6 £4/15/0 £5/5/0

THE NEW W.B. "STENTORIAN" HI FI SPEAKERS ARE IN STOCK

Model H.F. 6-inch Model H.F. 9-inch Model H.F. 8-inch Model H.F. 10-inch £2/10/6 £3/7/0 £3/0/6 £3/13/6 These speakers are of the very latest design and provide quality reproduction for the lower-price range, 3 or 15 ohm models are available.

£47/5/0 £23/2/0 £68/5/0

RECEIVER CHASSIS

Modernise your old Radiogram

RECORD PLAYERS

COMPLETE RADIOGRAM EQUIPMENT-QUALITY AT LOW COST

STERN'S DESIGN FOR HOME CONSTRUCTORS The "SUPER-SIX"

compact and highly efficient superhet Radio-Radiogram chassis of outstanding quality.

YOU CAN BUILD IT FOR £10/7/6 Including the OCTAL VALVE LINE-UP. (£12/7/6 with the miniature valves)

We will supply it assembled and READ Y FOR USE for

£13/13/0 (Plus 7/6 Carr. & Ins.) H.P. Terms £3.10.6. deposit and 12 months at 19/-

Incorporating the new B.V.A. Miniature Valve Line-up.
This receiver is designed to the very latest specification
and provision is made to incorporate either the standard Octal
Valve Line-up or the new B.V.A. range of miniature valves. Great
stention has been paid to the quality of the reproduction of both Radio reception and Record
playings, and excellent clarity of speech and music is obtained.

A few brief details. playings, and excei:
A few brief details.
Covers 3 waveb.
Employs 6 valve
Incorporates del
A 4 position Tor
Has independen
Size of Assemble

A few brief details.

Covers 3 wavebands 18-50 metres, 190-550, and 800-2,000 metres.

Employs 6 valves having PUSH-PULL for 5-6 watts output.

Incorporates delayed A.V.C. on all wavebands and pre-selective feedback.

A 4 position Tone Control operates on both Radio and Gram.

Has independent mains supply socket for a Record Player.

Size of Assembled Chassis 12in. x 8 in. x 8 in. Dial aperture 8 jin. x 4 jin.

For operation on A.C. mains 200-250 volts 50 cycles.

THE INSTRUCTION and ASBEMBLY MANUALI s available for 2/-, it contains very detailed practical drawings and circuit diagrams and a complete Component Price List.

THREE COMPLETELY ASSEMBLED ALL-WAVE SUPERHET CHASSIS

Model B.3, A 5-valve 3-waveband Receiver.

Model B.3.P.P. A 6-valve 3-waveband Receiver with PUSH-PULL OUT-

PUT.

Model B.3,P.P./R.F. A 7-valve 3-waveband Receiver incorporating an R.F. stage with PUSH-PULL OUTPUT.

The three Receivers are for operation on A.C. mains 100/110 volts and 200/250 volts, and employ the very latest ministure valves. They we designed to the most modern specification, great attention having been given to the quality of reproduction which gives excellent clarity of speech and music on both gram. and radio, making them the ideal replacement chassis for that "old Radiogram." etc.

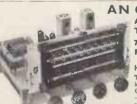
Brief specifications: Rodol B.3.—Valve line-up, 6BE6, 6BA6, 6AT6, 6BW6, 6AZ—wave-bard coverage short 16:50 medium

3E6, 6BA6, 6AT6, 6BW6, 6X4—wave-band coverage short 16-50, medium 187-550, long 900-2,000 metree. Controls: (1) volume with on/off; (2) tuning (flywheel type); (3) wavechange and gram; (4) Tone Control (operative on gram, and radio). Negative feedback is employed over the entire audio stages. Chassis size: 11 x 7½ x 8½in. high. Dial size 8½ x 4in. Price complete and READY FOR USE. excluding speaker 2[21/12]- (cerr-certainty-certa excluding speaker £12/12/- (carrand ins. 7/6 extra).

H.P. Terms: £3/4/- deposit, 12 months at 17/8.

months at 17/8.

Model B.3.P.P. This model is two B.3 Receiver but incorporates two B.3 Receiver but incorporates two in really excellent quality reproduction up to approximately Model B.3. P.P.R.F. This model is similar in appearance and has same waveband coveringe as the Model B.3. Dut in addition it incorporates an R.F. 8TAGE together with PUSH-PULL OUTPUT, employing a total of 7 vaives with two type 6BW6 in Push-Pull. This makes for a really sensitive receiver with genuine quality reproduction. Price £18/18/- (plus 7/6 carr, and ins.) or £4/13/- deposit, 12 months at £1/6/9.



AN OUTSTANDING OFFER A BULK PURCHASE ENABLES US TO OFFER THIS "PUSH-PULL" 7 VALVE SUPERHET RECEIVER

For only £12/19/6 (Carr. and Ins. 7/6 extra.).
H.P. Terms £3/4/6 Dep. 12 months at 18/4.

These receivers Model AW3-7 are made by a well-known set manufacturer and incorporate the latest Osram Valve Line-up of X79—W77—DH77—H77—U78 and two N78's in Push-Pull for approx. 7

—U78 and two N78's in Push-Pull for approx. 7
watts output.
They cover 3 wavebands 18-50 metres, 190-550 and
the Wavechange Switch.
They cover 3 wavebands 18-50 metres, 190-550 and
the Wavechange Switch.
They make an excellent replacement Badiogram Chassis having a P.U.
connection on the chassis. Extension speaker connection is also provided.
Overall size of chassis: 12In. long x 7th. x 6th. high, dial aperture
8½in. x 4½in. (Dial Escutcheon available for 4/9).
THEEB RECEIVERS ARE BRAND NEW AND FULLY GUARAN(a) With Model
(b)
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(c)

109 and 115 FLEET ST., London, E.C.4. Phone: CENtral 5812/3/4 This AUTOCHANGE UNIT by a famous Manufacturer

is offered for £11/10/0 (Plus 7/6 Carr. & Ins.)

Hire Purchase Terms £2/17/6 Dep. and 12 months at 16/4.

(Normal price is £16/10/-).

 These units will autochange on all three speeds, 7in., 10in. and 19h

• They play MIXED 7in. 10in. and 12in. records.

• They have separate sapphires for L.P. and 78 r.p.m., which are moved into position by a simple switch.

Minimum baseboard size required 14in. × 12½in., with height below haseboard 2½in. A bulk purchase enables us to offer these BRAN NEW UNITS at this exceptional



The COLLARO 3RC/521 3-SPEED AUTO CHANGE UNIT H.P. Terms £2/10/0 Deposit £9/19/6 (Plus 7/6 Carr. & Ins.) and 11 months at 15/9

Normal price £18/10/-.

Complete which High Fidelity Crystal "Turnover" Head which incorporates separate stylus for L.P. and 78 r.p.m. Records.

Will autochange on 7in-10in, and 12in, records not inter-mixed.

 Minimum Baseplate size
 15in. x 12in., with height above
 4in. and below baseplate 3in. • Minimum

Brand new in Maker's Cartons, complete with Mounting instruc-



We have the NEW ARMSTRONG CHASSIS—see over

A Replacement RADIO-RADIOGRAM CHASSIS



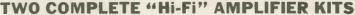
MOBL AW3-5. A 5-Valve Superhet Receiver covering the standar awayebands, 16-50 magnetic standard awayebands, 16-50 magnetic standard awayebands, 16-50 magnetic standard awayebands, 16-50 magnetic standard awayebands, 16-50 magnetic standard awayebands, 16-10 magnetic standard standard awayebands, 15-6 magnetic standard standard awayebands, 15-6 magnetic standard awayebands, 15-6 magnetic standard awayebands, 15-6 magnetic standard awayebands, 15-6 magnetic standard s

SPECIAL REDUCTIONS FOR COMPLETE EQUIPMENT

SUMMARY

(a) With Model 'E3 chassis. (b) , B3PP (c) , B3PP/RF (d) , Super str (e) (f) (a) With Modei (b) ,, ,, (c) ,, ,, (e) , , , AW3-5 £21 (f) , , AW3-7 £23 An additional charge of 10/- is made in each case to co

and KITS





A HIGH QUALITY 8-10 WATT AMPLIFIER THE IDEAL' AMPLIFIER FOR GENERAL HOME USE AND FOR SMALL HALLS, ETC.

Price of COMPLETE KIT including Valves and Drilled Chassis, etc. £7/10/0 (Plus 2/6 Carr. & Ins.).

We will supply it Com pletely Built for £9/10/0 (Plus 3/- Carr. & Ins.).

Designed for high quality reproduction up to an output level of 10 watts, having 6V6s in Push-Pull and incorporating negative feedback. It is suitable for use with all types of Pick-ups and most types of microphones and the output transformer provides for use of 3 and 15 ohm speakers.

- Valve line up 6J5, 68N7, 5Z4, with 6V6s in push-pull.

 The undistorted output level of up to 10 watts is produced from an input of .25
- volts. First class reproduction of Radio (where a Tuning Unit is used) and Record Playing. Separate Bass Boost and Treble Controls provide an excellent range of frequency
- Separate Bass Boost and Treble Controls provide an excellent range of frequency control.
 Very satisfactory results are obtained with an average type of high impedance Moving Coll or Crystal Microphone, a clear speech level of approx. 5 watts output being obtained.
 Power supplies (HT and LT) are available for a Tuning Unit.
 For operation on A.C. Mains 200-250 volts 50 cycles.
 THE ARSEMBLY MANUAL is available for Ij- and includes detailed layouts and com-

The NEW "LEAK" TL/10 AMPLIFIER "POINT ONE" PRE-AMPLIFIER

This Amplifier has a maximum output of 10 watts and maintains in every respect the world renowned LEAK reputation for precision engineering; fine appearance and fastidious wiring. The Pre-Amplifier will operate from any make or type of pick-up. A continuously variable input attenuator at the rear of the Pre-amp, permits the instantaneous use of crystal, moving iron and moving coll pick-ups. H.T. and L.T. Radio Tuning Unit. An input attenuator is fitted. S.A.E. for descriptive leaflet.

PRICES :

- (a) The COMPLETE AMPLIFIER WITH PRE-AMPLIFIER, £28/7/0, or £7/2/0
- Deposit and 12 months at £2.

 (b) The TL/10 Main AMPLIFIER ONLY: £17/17/0 or £4/7/0 Deposit and 12 months at £15/4.

 (c) The "POINT ONE" PRE-AMPLIFIER ONLY: £10/10/0 or £2/12/6 Deposit and 12 months at 15/-.

A BULK PURCHASE ENABLES THIS SPECIAL PRICE REDUCTION OF THE EAMOUS

SHAFTESBURY PORTABLE AMPLIFIER



Suitable for home use and small Halls. His matched inputs for both Record Players and Microphone. Also provides for the "mixing" and "isading" of both Gram, and speech as requested.



COMPRISING

(a) A 4 Valve High Gain Amplifier for use on A.C. or D.C. mains 200-250 volts with 5 watts output. Incorporating independent Volume Controls for Mike and Gram, either of which can be faded at will, a variable Tone Control and independent input sockets for Mike and Gram.

(b) A Transverse Carbon microphone which obtains its polarizing current from the amplifier—no batteries are necessary.

(c) An Sin. Goodmans P.M. Speaker with the "Ticonal" magnet for first-class reproduction.

THE COMPLETE EQUIPMENT is all contained in the PORTABLE CARRYING CASE

Having been reduced from £30/9/-. HIRE PURCHASE TERM DEPOSIT £4/10/0 and 12 monthly payments of £1/5/6 blight in weight © Easy to CARRY © CENUINELY PORTABLA illustrated leaflet containing free data is available on receipt of S.A. HIRE PURCHASE TERMS

A 12 Watt "HIGH FIDELITY" Push-Pull AMPLIFIER

Push-Pull AMPLIFIER
Comprising a Main Amplifier Chassis a Remote Control Pre-Amplifier-To Control Unit. The remote control unit measures only 7in. × 4in. × 2in. and contains four controls, being: Bass-Treble-Volume and a Radio, Grain, Microphone Switch control. It incorporates its own feedback circuit on the Bass Channel. Loop negative feedback is employed on the Main Amplifier which has a valve line up of 635-687-504 with two PX25's in push-pull and 635 and 68N7 are used in the remote control unit. THE COMPLETE KIT IS AVAILABLE FOR \$144/0/0

AVAILABLE FOR £14/0/0 (Carr. & Ins. 3/- extra).
THE COMPLETE UNIT ASSEMBLED

AND READY FOR USE £17/0/0 (Carr. & Ins. 5/- extra).



A 4-VALVE QUALITY "PUSH-PULL" 6-8 watt AMPLIFIER

AMPLIFIER

for use on A.C. mains. Incorporating Negative Feedback. Filter
Input Circuit and employing 6V6s in PushPull. A simple arrangement is provided to enable either a magnetic, crystal or lightweight pick-up to be used, and is suitable for use with Standard or long-playing records. A tone control is incorporated, and the lo-watt outmatch 2 to 15 ohm speakers. The overail size of the assembled chassis is 10in. X supplied. Price, including drilled chassis and valves, of complete kit, 26/17/6. Price of assembled chassis, supplied ready for use, £8/12/6. Plus 5/- Carr. & Ins. Full descriptive leaflets are available separately for 1/-.

WE HAVE IN STOCK THE NEW COLLARO "TRANSCRIPTION" RECORD PLAYERS

Model 2000 comprises the Transcription Motor and Turntable complete with 3-speed Gear and Switch mounted on a banjo type unit plate. Price 213/9/6. H.P. terms—Deposit £3/7/- and 12 monthly payments of 19/. Model 2000 has the same specification as the Model 2000 except that it is mounted on a rectangular unit plate and is equipped with the STUDIO "P" HIGH FIDELITY PICK-UP HEAD. Comprising a special low resonance arm and special bearings.

PICA-OF HEAD. Compraing a special low resonance arm and special bearings. Price 21847-9posit 24/14/9 and 12 monthly payments of 21/5/4. An Illustrated leafet is available on receipt of S.A.E.

ROGERS-RD BABY de Luxe MK II AMPLIFIER with RD JUNIOR Mk II

£23 / 0 / 0 (Plus 7/6 Carr. & Ins.)

H.P. Terms: £5/15/- Deposit and 12 months at £1/12/4.

A medium-priced 8-10 watt push-pull de Luxe Amplifier of very attractive appearance and embodying a high standard of workmanship. Complete performance data is available. Please send 8.A.E.

THE COLLARO MODEL 3/514 3-Speed Non-Auto Change Unit

- £7/19/6 (Plus 6/- Carr. and Insur.) Normal Price £12/17/6 Complete with High Fidelity Crystal "TUENOVER" Head which
 incorporates a separate stylus for L.P. and Standard Records.
 Will play 7 inch, 10 inch and 12 inch Records.
 Brand New and Complete with mounting instructions.





separately, 37/6.

BATTERY PORTABLE



THE "MINI TWO-THREE"

An "Alldry" Battery Portable of midget size, 6 in x 4 in. x 3 in. designed to cover medium wave-band 190-559 metres, with use of short trailer aerial.

short trailer aerial.

The simple design of this Receiver is so arranged that either a 3-valve set or a 2-valve (afterwards easily converted to the 3-valve) can be

converted to the 3-valve) can be made.

Consists of a T.E.F. circuit using a regenerative detector with H.F. stage and a high gain output pentode. Valve line up IT4—IT4—DL94.

The 2-valve set can be completely built for £4/3/6 (less case) and the 3-valve for £5/3/- (less case). Each price includes valves, speaker and reference of the decision of th

"PERSONAL SET" BATTERY ELIMINATOR

A complete Kit of parts to build a Midget A complete Kit of parts to build a M
"Alldry" Battery Eliminator, g
approx. 69 volts and 1.4 volts.
This eliminator is for use on A.C.
mains and is suitable for any
4-valve Superhet Receiver requiring H.T. and L.T.
voltage as above, or
approx. to 69 volts.
The Kit is quite easily and
outch't assembled and is

The Art is quice resort and is quickly assembled and is housed in a light-duminium case size 4½1n. ×1½in. ×3½in. Price of complete Kit with easy-to-follow assembly instructions, 42/6. In addition we can offer a similar COMPLETE KIT to provide approx. 90 volts and 1.4 volts. Size of assembled unit 71n. ×2½in. X1½in. Price 47/6.

A COMPLETE "CAR RADIO" FOR THE HOME CONSTRUCTOR 114in. × 42in. × 34in.

11½in. × 4½in. × 3½in.

A design of a complete 5-VALVE

SUPPERET RECEIVER employing an R.F. Stage, and incorporating a separate VIBRATOR PACK size 4½ × 2½

× 6½in. for use on 6 or 12 volt D.O. supplies.

We can supply all components to build this complete Receiver and Vibrator Pack including a Metal Case, Valves, Drilled Chassis and 5in. P.M. Speaker for £13/9/8. (Carr. and Ins. 5/6 extra.) Or the Receiver Components for £9/19/6 and the Vibrator Components for £9/10/-.

This is NOT an EX-GOVT. Receiver, it is a new design employing new Components Send 2/8 for the complete set of ASSEMBLY INSTRUCTIONS, CIRCUITS and PRACTICAL LAYOUTS, including a complete individual Component Price List.

THE NEW ARMSTRONG F.C.48

OUTSTANDING FEATURES INCLUDE :--

- 8 Valves including 2 double Triodes.
- 8 Watts output from push-pull tetrodes. Heavy negative feed back is used resulting in negligible distortion and high damping factor.
- Provision for using F.M. adaptor to receive the present high quality transmissions from Wrotham and the new B.B.C. V.H.F. stations.
- An accessible socket at rear provides the power supply for this unit.
- Independent controls give BASS and TREBLE lift and cut with unique Thermometer visual indicator.
- · Gram position on wavechange switch.
- 4 wavebands Coverage 16-51, 50-120, 190-550, 1000-2000 metres.
- Large four-colour illuminated dial.

CASH PRICE COMPLETE and READY FOR USE £23/18/0

(Plus 7/6 Carriage and Insurance).

H.P. Terms, Deposit £5/18/- and 12 months at £1/13/9.

"MINI-TWIN" 1-VALVE BATTERY SET



A design of a simple 1-valve 2-stage Battery Receiver, giving excellent results on medium and long wavebands and having exceptionally low battery consumption.

Drilled chassis and practical diagrams make it the ideal set for the beginner to build. The complete chassis, including valve, can be built for 37/6, plus 8/11 P/Tax, the attractive plastic case is 9/6.

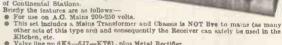
37(6, plus 8)11 F/Tax, the attractive plastic case is 9/6. and suitable beadphones, 14/9.
The complete assembly instructions, layouts and a component price list are available for 1/6.
This Receiver also performs excellently, without modification, as a tuning unit, and, in addition, with simple modifications for which a complete diagram is provided, makes a first-class pre-amplifier for pic k-up or microphone.

109 and 115 FLEET LONDON. E.C.4 Phone: CENTRAL 5812-3-4

!!!CONSTRUCTORS!!!

A NEW SUPERHET TRANSPORTABLE THE "SUPER THREE"

Designed for local station reception without the use of an external aerial. This design provides for a 2 valve (plus Metal Rectiler) Superhet Receiver incorporating a Frame Aerial for "room to room" use, provision is also made for a short external aerial, if required, for the reception of Continental Stations.



Kitchen, etc.

Kitchen, etc.

Valve line up 6K8—637—KT61, plus Metal Rectifier.

The L.F. Transformer is supplied "pre-aligned" and thereby ensures extreme simplicity of Tuning—in fact, more simple than most T.R.F. Receivers.

Compact and easy to build simple "point to point" practical diagrams are supplied with a completely drilled chassis.

se complete Receiver Chassis can be built to cover the diagrams are supplied with with a complete Receiver Chassis can be built to cover the £6 . 6.6 Medium Waveband only for

Or to cover both Long and Medium Waves for

£6 . 16 . 3 If the Receiver is first built to cover the Medium Waveband, Long Waves can be added at any time, separate diagrams are provided for this purpose. The attractive Polished Wood Cabinet 11½ inches wide, 8½ inches high and 6 inches deep illustrated above is The CONSTRUCTOR'S MANUAL is available for 1½-, this shows the component prices, which are all available for separate purchase.

DUAL-CHANNEL PRE-AMPLIFIER and TONE CONTROL UNIT

This comprehensive PRE-AMPLIFIER and TONE CONTROL UNIT provides a full control of base and treble in conjunction with a main Volume/Mixer Control. CONTROL

It can be used with any amplifier and with any pick-up, the range of frequency control provided by the unit affording ample compensation for all types of pick-up and all natures

of pick-up and all natures of recordings, i.e., English, American and long-playing, without recourse to pick-up correction. The extreme flexibility of the bass and treble control is such that the level of bass and treble can be set to mit any conditions irrespective of the volume output of the amplifier. Response characteristics are given in 12-wast amplifier advi. The unit measures only 7in. x 4in. x 2in., including self-contained power supply and can be accommodated either on or away from the main amplifier, i.e., on the front panel of a cabinet or any other position. Price including drilled chassis, valves (68N7 and 615), £31.69, Complete assembly data are available separately for 1/-. Completely assembled and ready for use, £515/-.

AN AMAZING OFFER! A COMPLETELY ASSEMBLED

VALVE T.R.F. CHASSIS

Including a 5in. P.M. SPEAKER and VALVES

FOR ONLY £6/9/6

This receiver is of the very latest design and is for use on A.C. or D.O. Mains. It covers both Long and Medium Wavebands, and includes the modern BVA miniature valves. The line up being 12 BA6-12AT6-12A6-35W4.

12AT6—12A6—35W4. It incorporates Permeability Tuned Coils, thus ensuring excellent selectivity and sensitivity. The overall size of the complete chassis including speaker is 104in. X 44in. X 64in. An attrative Bakelite Ivory-finished Cabinet size 14in. X 54in. X 61in. is available for 16/8 (plus 2/6 carriage and insurance).



RADIO **TELEVISION**

MONEY BACK GUARANTEE GOODS OF QUALITY PROMPT DESPATCH

RECORD PLAYERS

. MONTPELIER RISE, 34 LONDON ' N.W.11.

Telephone: MEADWAY 1736.

AMPLIFIERS

TERMS OF BUSINESS: Cash with order (or C.O.D. Post Items only); all orders for small items totalling over £2 post free, unless otherwise

BUILD YOUR OWN RADIO!



We can supply all the parts (including valves, 5in, moving coil speaker, cabinet, chassis and everything down to the last nut and boit) to enable YOU to build a professional-looking radio. The chassis is punched and drilled ready to mount the components. There is a choice of any of three attractive cabinets 12in, long, 5in, wide by 6in. high, as follows; either ivory or brown bakelite, or wooden, finished in walnut. Complete and easy-to-follow point-to-point circuit wiring diagrams supplied.



MODEL I T.R.F. RECEIVER

This is a 3-valve plus metal rectifier T.R.F. receiver with a valve line up as follows: 6K7 (HF), 6J7 (Det.) and 6V6 (Output). The dial is illuminated and when assembled the receiver presents a very attractive appearance. Coverage is for the Medium and Long Wave Bands. Operates on 200/250 volts A.C. Mains.

Plus 2/6 Packing Carriage, Insur

ALL COMPONENTS SUPPLIED ARE GUARANTEED FOR ONE YEAR

NOTE: We would respecifully suggest to those interested in building this receiver that they send for OUR Instruction Booklet. Intending constructors can then judge for THEMSELVES now comprehensive this Booklet is.

Instruction Booklet and priced Parts List available separately at 1/s. This money will be refunded if circuit diagram is returned as NEW within 7 days.

MAINS NOISE SUPPRESSOR KIT

Consisting of 2 specially designed chokes and 3 condensers. Extremely effective, outs out all mains noise. Can be assembled in existing receiver or separately as desired. Complete with circuit diagram, 4/11, plus 1/- P.C.

BATTERY CHARGER KIT

Incorporates metal rectifier. Transformer is suitable for A.C. mains 200/250 volts. Charges either 12, 6 or 2 volt secumulator at 1 amp. Complete with circuit diagram. Price 19/11, plus 1/6 post and packing.

This is a powerful midget 4-valve plus metal rectifier Superhet Receiver with a valve line-up as follows: 683, 687, 697, 698. The dial is illuminated and coverage is for the Short Wave bands between 16-50 metres, the Medium Wave bands between 190-450 metres, and the Long Wave bands between 1,000-2,000 metres. Operates on 200/250 volts A.C. meins. **MODEL 2 SUPERHET RECEIVER**

Insur. £5 . 10 . 0 Plus 2/6 Packing Carriage and Insur. £7 . 1

T.R.F. RECEIVER We can supply this Receiver ready built at £8/15/6, plus 3/6 p.c. Plus 2/6 Packing £7.19

THE LATEST RANGE OF W.B. H.F. SPEAKERS
Incorporating the NEW Composite Cone
W.B. 6lin. H.F., 10,000 lines, 3 ohms £2 10 6
W.B. 8lin. H.F., 10,000 lines, 3 ohms £3 0 6
W.B. 9lin. H.F., 12,000 lines, 3 ohms £3 7 0
W.B. 10lin. H.F., 12,000 lines, 3 ohms £3 13 6
(Also available 15 ohms (mped.)

ELECTROLYTIC CONDENSERS
BRAND NEW!

ntd. 500 volt. Aluminium Container. Height 8 mfd. 500 volt. Aluminium Container, Height 2 x 1 in. dia. Price 1/2 each, 12/- per doz., 140/- per gre Height 21in

WE CARRY LARGE STOCKS OF COMPONENTS AND WELCOME YOUR ENDUIRIES

4 watt AMPLIFIER KIT

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PRICE Plus 2/6 PACKING. CARRIAGE & INSUR. 5 . 0

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The Output Transformer supplied is for use with a loudspeaker of 3 ohms impedance, and we would suggest that
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as follows: Sin., 60/6; Sin., 67-; 10in., 73/6. All plus
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Circuit Diagrams only, available separately at 1/-.
To those who require this Amplifier ready-built we can
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HIGH SPEED and A.C. to 400 VOLTS

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MAJOR TYPE 6×1½×1½ ins. 3 ohms operates on 3/6 Vo. D.C. 500 ohms operates on 18/24 Vo. D.C. 1,000 ohms operates on 100/110 Vo. D.C. 2,300 ohms operates on 200/230 Vo. D.C. 17/6, Post and Packing, 9d.

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Send your enquiries for all Radio and Electrica; goods, especially those in short supply. NEW VALVES

We have probably the largest variety of valves in the country. Let us know your requirements.

AVO METERS IN STOCK

Signal Generator, Mains and Battery ______£30 Models 0 0 Valve Characteristics Meter £60 0 0

Also full range TAYLOR METERS. List on request

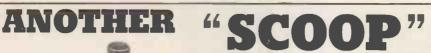
VALVE MANUALS Mullard 5 0 Osram 5 0 Brimar No. 5 5 0 Mazda, Part 2 2 0 Sound Reproduc-tion by F. H. Brittain, D.F.H.... 2 6 Postage 6d. each extra.

Leak TL/10 Amplifier and "Point One "Preampli-fier complete£28 7 0 Chapman Tuning Units £17 6 Leak Tuning Unit £35 6 3 Grundig Tape Recorder £68 5 0
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Terms C.O.D. or Cash with order. Goods offered subject to being unsold and to price alteration.

PROPS: ARTHUR GRAY, LTD. GRAY HOUSE, 150-152 CHARING CROSS ROAD, TEMple Bar 5833/4 and 4765. Cables: TE LONDON, W.C.2 Cables: TELEGRAY, LONDON



A COMPLETE 5 VALVE RADIO CHASSIS

BRAND NEW AND UNUSED AC/DC Mains 200/250 volts

69'6

LESS VALVES Postage 3/6d. extra.

COMPLETELY WIRED AND READY FOR USE, WITH THE ADDITION OF A SPEAKER AND OUTPUT TRANSFORMER.

Two controls only: Volume and Station switch.

Valves used: 10C1 freq. changer, 10F9 or UF41 I.F. Amp., 10LD11 AVC and Det., 10P14 output, U404 or UY41 rect.

YOU CAN FIT THIS UNIT INTO YOUR EXISTING T.V. RECEIVER FOR RADIO RECEPTION

Circuit diagram supplied. Available separately at 1/6d.

PRICE COMPLETE WITH VALVES £5 · 19 · 6

THE IDEAL SECOND SET

A Cabinet will be available shortly

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TERMS AVAILABLE

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Send for pro-

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★ I.F. 465 Kc/s.

* 4 Watts output.

A.V.C.

* 3 Station Pre Set.

* Frame Aerial.

* Fully aligned.

★ Size of chassis only $10'' \times 5\frac{1}{2}''$ max. height 5½"

TEST SET TYPE 28
P.R.F. Output Meter. Contains 0-50
microamp—2½ inch moving coil meter.
Mounted in strong metal case, size
6in. high, 3½in. wide, 3in. deep.
Complete with all plugs and cables.
Supplied in wood transit case, hinged
lid (ideal for tool box) size 11 ×
9½ × 5½ inches. Rubber padded
fitments fitments.

IDEAL FOR CONVERSION INTO MULTIRANGE TESTMETER LASKY'S PRICE 30/6 39/6 Carriage 3/6.

PORTABLE RECORD PLAYERS Single speed auto changer, with amplifier. In case. A FEW LEFT AS PREVIOUS ADVT. AS PREVI Carriage 10/6d

SUPERHET COIL PACKS
With Circuit.
No. 1. L.M.S.G. Size: $4\frac{3}{7} \times 5 \times 2\frac{1}{7}$ in.
With $\frac{1}{7}$ in. spindle. 19/6.
No. 2. M.S.S. Size: $4 \times 4 \times 3$ in.
With $\frac{1}{7}$ in. spindle. 16/-.
Both for use with 465 Kc/s. I.F.

MODULATION INDICATOR TYPE 2. Frequency 3,000-6,000 Kc/s. Contains 0-500 microamp meter, 2½ inch moving coil. Fitted in metal carrying case with leather handle. Size 11½ × 7 × 6½ inches. IDEAL FOR CONVERSION TO MULTIRANGE TESTMETER, VALVE VOLTMETER, ETC.

LASKY'S PRICE 45/-. Carriage 3/6 extra.

FILAMENT TRANSFORMERS 200-250 v. primary 50 c.p.s. 6.3 v. 1.75 a. 6.6. 6.3 v. 3 a., 9'6.

PERSONAL CALLERS ONLY

Tane Recorder Amplifiers. 6 valves. Fully assembled and wired. Untested, and faults may be present. LASKY'S PRICE £4/19/6.

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"Stalwarı." 12in. 15
ohms impedance. Frequency response 3013,500 c.p.s. Power
handling capacity 15
watts, peak A/C. PRICE
£5/10/-.

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ohms impedance. Reentry cone. Frequency response 18-17,000
c.p.s. Power handling capacity 15 watts, peak
A/C. PRICE £8/10/-. CARRIAGE 3/6 per
speaker extra.

speaker extra.
(H.P. Terms available).

STILL ANOTHER SUPER BUY

Tape Recorder Heads By "Phidelity" High imped-

ance, single hole fixing. Size lin. diam., Jin. high. Twin track.

Record/playback. 22/6d.

Low impedance erase. 22/6d.
FAR BELOW ACTUAL MANU-FACTURING COST, LESS THAN HALF USUAL PRICE.
Limited Quantity only.

CAR RADIO SPECIAL—PARTLY ASSEMBLED CAR RADIOS

Small size case, 12 × 4 × 6in. Will fit most cars. For either 6 or 12 volts, depending on vibrator. Chassis supplied with 5 octal valve holders, medium wave aerial and oscillator coils output transformers, volume control, sundry resistances and condensers, dial and knobs. Case finished in brown crackle. Dial calibrated 150-550 metres, 5 valves to suit. One each, either GT or metal; 6SA7, 6R7. 6V6, 6K7 0Z4. LASKY'S PRICE £5/5/-. Carriage 5/- extra. Or less valves, 69/6. Carriage 5/- extra. Other chassis in various conditions of completion are available for expressions. conditions of completion are available for personal callers only.

CIRCUIT for 5 valve car radio, using above chassis. PRICE 1/6.

"THE HARROW" Baffle Radio Cabinet



Build a second set to be proud of. Pleasing design cabinet, with drilled chassis, dial, drilled chassis, dial, driveand back. Finished in satin mahogany veneer. Outside dims.: 17½in. wide, 11½in. high, 5in. deep.

LASKY'S 36/6

36/6 PRICE PRICE
Carriage 2/-.
Receiver design uses
2-6K7, 6V6 and 5Z4.
Total cost to build is
less than £5/10/-.
Circuit for receiver I/6.

CAR RADIO AERIALS 2 section, chrome, 75 inches. Side fitting. 15/-. Post 3/6

RADIO CABINETS

Size: 12in. wide, 6 in. deep, 8in. high. Finished in medium walnut veneer, with high polish. Complete with back, chassis, and dial.

LASKY'S PRICE 16/11. Carriage 2/6 extra.



R.1155 RECEIVERS

NOW AVAILABLE ON H.P. TERMS

BRAND NEW BEFORE DESPATCH

These well-known Ex-Air Ministry Receivers need no further introduction. Supplied complete with 10 valves and full circuit data.

LASKY'S PRICE BRAND NEW £11.19.6

Secondhand. Specially Selected. Grade 1 £9.19.6 £7,19,6 Secondhand. Grade 2

Carriage 17/6 per receiver extra. including 10/- returnable on case.

ASSEMBLED POWER
PACK/OUTPUT STAGE FOR
R.1155 RECEIVER
For use on 200-250 v. A.C. mains.
Complete with 2 valves. In metal
case size: 12 x 7 x 5 ½in.
LASKY'S PRICE, 79/6. Carr. 5/-.
Power Pack as above. Fitted with
6½in.p.m. speaker.
LASKY'S PRICE £5/5/-. Carr. 5/-.

A LASKY'S RADIO ADVERTISEMENT. SEE OVER.



LASKY'S T.V. CONSTRUCTORS' PARCELS.

LASKY'S T.V. CONSTRUCTORS' PARCELS.

No. 1 WIDE ANGLE PARCEL.
Containing ferroxcube line E.H.T. transformer, ferroxcube scanning coils, frame output transformer, p.m. focus unit, frame blocking osc. transformer, 14, 16 or 17-inch mask and glass, width and linearity controls. Also the following valves:—614gt, 6CD6, 6AL5, 2—6AM5 (N78), 3—12AU7.
Full circuit.
LASKY'S PRICE FOR THE COMPLETE
COMPLETE
68/15/11
Carriage 3/6 extra.

No. 4 Complete set of metal-work. Unassembled. Comprising main chassis, tube supports and valve-holders. (Less sound-vision chassis.) PRICE 25/-. Carriage 3/6 extra.

No. 5 SPECIAL PARCEL. Comprising line output transformer (Non E.H.T.) frame output transformer, scanning coils, line and frame blocking oscillator transformers, large 250 m/a, smoothing choke

LASKY'S PRICE 44/6 POST FREE.

CRYSTAL DIODES. type, wire ends. 1/6 each. Higher Grades Available. 12 Assorted for 30/-. Post Free. 1/6 each.

LIMITED QUANTITY ONLY

COLLARO 3-SPEED AUTO CHANGERS. Model 3RC/521. New and unused in maker's carton.

Cream or fawn finish. Complete with hi-fi-delity "studio turn over crystal pick-up.



LASKY'S \$9.19.6 Carriage Free.

12 VOLT-4 WATT MOBILE

BRAND NEW AND UNUSED KT.61 output. Complete with power unit and synchronous vibrator (Wearite type QFA/12), and all valves. Fitted with rubber covered heavy duty battery lead.

By famous manufacturer, in handsome metal cabinet, grey crackle finish. Size: 10in.x6in.x8in. Output impedance 3 ohms. With the addition of a suitable loudspeaker, this is ready for operation. Finest quality components throughout. Robustly constructed for rough handling. Complete with carbon hand-mircophone with screened lead.

Can also be used as a power pack and output

Can also be used as a power pack and output

stage for a car radio. OR LESS MICROPHONE LASKY'S PRICE, £7.19.6

COMPLETE

Carriage 5/- per unit extra.



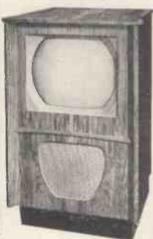
SPECIAL OFFER MAGNETIC RECORDING TAPE

6d.

Kraft base. 1,200ft. reels, 17/3.

CABINETS TELEVISION

THE ROTHESAY



ank shade. Inte top is inch thick. Fitted with gold anodised speaker grille. The C.R.T. aperture frame is detachable, supplied to suit any size tube to order. Full length doors if required can be supplied with the cabinet. Veneered both sides, and polished to match the cabinet, they will be mounted with full length piano hinges. Outside dim. 34½in. high, 21½in. wide, 21½in. deep. Inside dim. 18½in. wide, 19½in. deep. Size of top 22½in. × 21½in. Thickness. in. NOTE THESE GENEROUS SIZES.

GENEROUS SIZES.

LASKY'S £9.19.6 Carriage 15/- extra.

This cabinet is really the last word in outstanding glass, castors, shelf, bearers, C.R.T. Absolutely rigid construction throughout with the finest laminated woods, wenered in walnut, polished light, medium or dark shade. The top is inch thick. Fitted with gold anodised speaker grille. The C.R.T. aperture frame Can be supplied with cut-out for is detachable, supplied to suit any size tube to order. extra cost.

Now supplied complete with mask, glass, castors, shelf, bearers, C.R.T. neck end protector, back, speaker fret and baffle board. Finished in beautiful figured medium, light or dark walnut veneer, with high order to structor T.V. receivers, including the vision," "Tele-King," "Magnigiew," "Wireless World," etc. Can be supplied with cut-out for 14in., 16in. and 17in. C.R. tubes at no suit any size tube to order.

£6.19.6

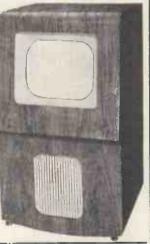
An allowance of 4s, 6d, will be made if the mask is not required. Inside Dimensions: Depth 16½in.; width 17½in.; height 28in. Overall height 32in. and width 18¼in. WHY NOT CONVERT YOUR TABLE RECEIVER TO A CONSOLE MODEL? Adaptor frames for fitting 9in. or 10in. C.R. tubes can be supplied if required.

required.

LASKY'S PRICE £8.10.0

H.P. Terms. Deposit £2/17/-, plus carriage. Balance plus charges spread over 12 months.

THE DE-LUXE



3-WATT AC/DC MIDGET **AMPLIFIERS**

ELECTROLYTIC CONDENSERS **ALL BRAND NEW**

H.P. TERMS. Deposit £3/10/plus carriage charge. Balance plus charges spread over 12

months.
The Rothesay cabinet with doors. Price £14/9/6.

8 mtd. 450 v.w	1/9
16 mfd. 350 v.w	2/6
16 mfd. 500 v.w	3/6
20 mfd. 500 v.w	3/6
30 mfd. 450 v.w	3/3
60 mfd. 350 v.w	3/11
64 mfd. 450 v.w	3/11
150 mfd. 350 v.w	3/6
400 mfd. 150 v.w	2/6
8 + 8 mfd. 450 v.w	3/6
8 + 16 mfd. 450 v.w	4/3
12 + 12 mfd. 350 v.w	2/6
16 + 16 mfd. 350 v.w	3/6
16 + 16 mfd, 450 v.w	4/6
20 + 20 mfd. 275 v.w	2/-
60 + 100 mfd. 350 v.w.,	7/6
32 + 32 mfd., 450 v.w.,	5/11
MANY OTHER SINGLE	
MULTIPLE CONDENS	
IN STOCK.	

Push pull, very high gain

4 valves: 2 UL41 in push pull, 1 UCH42 and 1 UAF42. Input voltage 100/110 AC/DC. Very easily converted to 230 volts. Supplied with circuit diagram and full details. Size:—

9 x 4 x 4 inches. Uses 2 metal rectifiers, 1 each RM2 and RM3 Ideal for ships' record players, tape recorders, home record players, tape recorders, home record players, tape larms, etc., etc. Supplied complete, fully assembled and wired, with 4 valves. Highest quality miniature components used throughout. An auxiliary 60 m/a. output is fitted, for use with a radio feeder. etc.

BRAND NEW AND UNUSED. IN MAKER'S CARTONS.



CARRIAGE FREE

C.R.T. Neck Protectors 2/6.

SPECIAL T.V. CONDENSERS 64 mfd. 450 v.w. 100 mfd. 450 v.w. 32 + 100 mfd. 450 v.w. 100 + 200 mfd. 350 v.w. 4/11 5/11

TABLE MICROPHONE STANDS. 2 Section Chrome. Heavy base. 12/6.

MICROPHONE FLOOR STANDS. 2 Section Chrome. Heavy Base. 35/-.

METROSILS. 10 Kv. 5/-.

BRIMISTORS. CZ.1 1/6 each. CZ.3 9d. each.

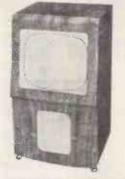
OUTPUT TRANSFORMERS Midget Pentode 3/6
Miniature Personal, 3S4, etc. 3/6
Standard pentode 3/11
Push-Pull 6V6 9/6
Multi Ratio, P.P. 12/6
Heavy Duty, P.P. 14/11

HE TELE KING

SUPERHET RECEIVE

WIDE ANGLE — LARGE SCREEN

Do you know . . . this famous and well tried home constructor set can now be built for £29'10'including valves. Only tube and cabinet extra.





MULTI CHANNEL TUNER FOR THE TELE KING WILL BE AVAILABLE SHORTLY.



EVERY COMPONENT CAN BE SUPPLIED SEPARATELY

Full constructional data, wiring diagrams and circuits.

Price 6/- FREE

WRITE NOW FOR OUR NEW TELE KING PRICE LIST. WE CAN SAVE YOU MONEY.

CHOKES 40 m/a. . . 3/3 120 m/a. 7/3 60 m/a. . . 3/11 200 m/a. 12/6 80 m/a. . . 4/11 250 m/a. 14/-

SPECIAL TRANSFORMER Secondary tapped as follows: 3, 4, 5, 6, 8, 9, 10, 12, 15, 18, 20, 24 and 30 volts at 2 amps. PRICE 17/6.

TELEVISION SELENIUM RECTIFIERS The very latest "Sentercell" S.T.C. range. S.T.C. range. K3/40, 3.2 kV
 K3/40, 3.2 kV
 9/

 K3/45, 3.6 kV
 8/2

 K3/50, 4.0 kV
 8/8

 K3/100, 8.0 kV
 14/8

 K3/100, 12.8 kV
 21/6

 K3/200, 16 kV
 26/

MANUFACTURER'S SURPLUS

R.F. E.H.T. OSCILLATOR
COILS
Doubler type, 6-9 kV. Uses 1 or 2
EY51's. LASKY'S PRICE 12/6.

HEARING AIDS

By well known manufacturer. In metal case 2½ × 4½ × 1in. Complete with batteries and 3 subminiature valves. Fitted with internal crystal microphone. Used and soiled condition. LASKY'S PRICE 39/6. Post 2/6. dition. LASKY'S PRICE 39/6. Post 2/6. Earpiece and Cord. For use with hearing aid. LASKY'S PRICE

INTERCOM. UNITS

4-station operation. For use on A.C./D.C. mains 200-250 volts. Complete, with 3 valves. Fitted in attractive ve plastic cabinet. MAS-UNIT £5/19/6. Carr. 5/- extra.

Extension Units, Price 21/- each complete. Carriage 2/- each extra.

P.M. LOUDSPEAKERS All with 3 ohm speech coil.
3½in., 14/6. 5in., 14/6. 8in., 19/11.
4in., 12/6. 6½in., 15/-. 10in., 19/6.

ENERGISED SPEAKERS 8in. with O/T 600 ohm field, 15/6 8in. less O/T 600 ohm field, 12/6 8in. less O/T 1,200 ohm field, 12/6. 6½in. with O/T 600 ohm field, 14/-.

SPECIAL OFFER. 12 INCH CATHODE RAY TUBES. Standard types, suitable for T.V. LIMITED QUANTITY. LASKY'S PRICE £12/19/6. Carriage and insurance 15/- extra.

ION	TRAPS.	All	types,	3/
	MOUR F			SS
	Actual s			
	in. × lin. Actual s			7/11
13i	n. x lin.		gut A	6/11
12in.	Actual	size 13	3in. X	
	in.׆in.			4/-
	Actual siz			3/-
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TRIPLEX DARK SCREEN FILTERS 15½ × 13½ × ½in. 9/6
Postage and packing 5/- per piece extra. (This charge is necessary owing to extra packing required).

PERSPEX IMPLOSION GUARDS, incorporating C.R.T. MASKS. Brand New LATEST ASPECT RATIO 910. 7/10in. 7/12in. 0ld Ratio 9/6
12in. Escutcheon mask, with
Perspex filter 12/6
14in. Rectangular 12/6
15in. Cream rubber 17/6
16in. Plastic, white 12/6
17in. Rectangular 15/-

TELESCOPIC
AERIAL MASTS
previously advertised Comte. LASKY'S PRICE 25/plete. LASKY'S Carriage 2/6 extra.

MANUFACTURERS' SURPLUS T.V. COMPONENT BARGAINS

WIDE ANGLE

38mm.			
Line E.H.T. trans., ferrox- cube core. 9-16 kV	25/-		
Scanning Coils, low imp. line and frame Frame Output Transformer	25/ - 10/6		
Scanning Coils low imp. line and frame	17/6		
Frame blocking osc. trans- former	4/6		
former, caslam cored Focus Magnets Ferroxdure	4/6 25/-		
P.M. Focus Magnets. Iron Cored Duomag Focalisers	19/6 29/6		
300 m/a. Smoothing chokes Electromagnetic focus coil,	15/-		
with combined scan coils	25/-		

AERIAL ROD SECTIONS Steel, heavily copper plated.

12in, long, in, diameter. Any
number may fitted together.

PRICE 2/6 per doz. POST FREE.

MAINS TRANSFORMERS
All 200-250 v. 50 c.p.s. primary
Finest quality, fully guaranteed,
MBA/3, 350-0-350 v. 80 mA.
6.3 v. 4 a., 5 v. 2 a. Both filaments tapped at 4 volts. An
ideal replacement trans. 18/-.

MBA/6, 325-0-325 v. 100 mA. 6.3 v. 3 a., 5 v. 2 a. With mains tapping board. Price 22/6.

MBA/7. 250-0-250 v. 80 mA. 6.3 v. 3 a., 5 v. 2 a. Both filaments tapped at 4 volts. 18/-.

MBA/8. SPECIAL OFFER Drop through type. 235-0-235 v. 60 mA. 6.3 v. 3 a., 12/6.

MBA/9. 400-0-400 v. 60 mA. 6.3 v. 1 a., 4 v. 2.5 a.Price 12/6. AT/3. Auto transformer. 0-10-120, 200-230-240 volts 100 watts Price 17/6.

CLOSED FIELD SPEAKERS 6\in. 18/6
8\in. round and 6\in. Eliptical.
19/11.

CTANDARD 25

ı	STANDARD 33M	ım.
	Line Output Transformers. No. E.H.T	12/6
	6-9 kV. E.H.T. and 6.3 v. winding Ferroxcube	19/6
I	Scanning coils. Low imp. line and frame Scanning Coils. Low imp.	12/6
ı	line and frame, by Igranic	14/6
l	Line blocking oscillator trans- former	4/6
	transformer	4/6 7/6
I	Focus Magnets: Without Vernier	12/6
	With Vernier Focus Coils. Electromagnetic 200 m/a. Smoothing chokes	17/6 12/6 10/6



SWITCHED TELETUNERS

Brand new. Instant and positive selection of any one of the 5 B.B.C. television channels, by a single control knob. Uses EF.80 or 6BW7

RF pentode and ECC81 or 12AT7

Double Diode Triode as frequency changer. Tuning is obtained by switching incremental inductances. Size 4½ × 2½ × 2½ in. Spindle 2½ in. long lin. diameter. I.F. Output 9.5-14 Mc/s., noise figure on all channels better than 10.5dB. I.F. rejection better than 45dB. on all channels. Power gain 24dB. LASKY'S PRICE, less valves, 12/6. POST FREE.

Complete with valves. 37/6.

TAPE RECORDER AMPLIFIERS. Complete with 5 valves: 2 65N7, 2 6V6, 1 5Z4. Twin inputs, also volume control and record level. On aluminium chassis, size 11½ ×2½ ×9in. Complete with valves and 8in. speaker. Totally enclosed in case. LASKY; PRICE £9/19/6. Less cover £8/15/-. Less cover and head lift trans-

Less cover and head lift transformer £7/15/-. Carriage 5/-per unit extra.

LASKY'S (Harrow Road) Ltd.,

370 HARROW RD., PADDINGTON, LONDON, W.9

(Opposite Paddington Hospital)

Telephone, all departments: CUNningham 1979/7214. Please Add a Reasonable Amount For Postage.

NE RADIO

MU5eum 5929/0095.

TOTTENHAM COURT ROAD, LONDON, W.1

All goods specially selected for quality and value. Prompt Service—Money-back guarantee—It will pay you to visit our new rebuilt shop premises. Situated 50 yds only from Tottenham Court Road Tube! (Genuine).

F.M.!! (Frequency Modulation)

We are pleased to announce our complete Kit for the "Denco" F.M. Feeder Unit.
This unit provides an A.F. output suitable for feeding into the audio section of a standard broadcast receiver where triode/pentode output are available. Within an average of 30 miles from a V.H.F. transmitter one I.F. stars stare should be adequate, but our complete Kit supplied includes all components and values for an extra I.F. stage if necessary, or if the unit is used at greater distances. Pull Constructional details, theoretical circuit, and point-to-point wiring diagram as a be supplied for 1/6 post free, or the complete Kit right down to the last nut and boit, at only £8/7/8, plus 2/9 backing and postage. This unit can be supplied if desired, ready assembled, sligned and tested, at £8/10/p plus 2/10 points of the post of the complete Kit right down to the last nut and boit, at only £8/7/8, plus 2/9 backing and postage. This unit can be supplied if desired, ready assembled, sligned and tested, at £8/10/p plus 2/9 backing and postage. This unit for a charge of 7/6. N.E.—Valve line-up is 6AM6, 12AH8, 2-6BA6 and 6AL5. Chassis measures only 6\text{im. X }\text{jin. X }\text{lin.


				METERS	
	F.S.D.	Size	Туре	Fitting	Price
	50 microamp	D.C. 2in.	M.C.	R.P	50/-
	250 microamp	D.C. 21in.	M.C.	F.B	401-
	500 microamp	D.C. 2in.	M.C.	R.P	13/6
	500 microamp	D.C. 2ln.	M.C.		18/6
	500 mlcroamp	D.C. 21in.	M.C.		35/-
	1 mA.	D.C. 2ln.	M.C.	F. Sq	17/6
	1 mA.	D.C. 2ln.	M.C.		15/-
	1 mA.	D.C. 21in.	M.C.		22/6
	1 mA.	D.C. 21in.	M.C.		27/6
	5 mA.	D.C. 2in.	M.C.	F. 8a	7/6
	10 mA.	D.C. 21in.	M.C.	R.P.,	8/-
	10 mA.	D.C. 2+in.	M.C.		10 -
	15 m.A.	D.C. 2in.	M.C.	F.R	7/6
	20 mA.	D.C. 2in.	M.C.	F.R	7/8
	50 mA.	D.C. 2in.	M.C.	F. 8q	8/6
	150 mA.	D.C. 2in.	M.C.	F. 8q	7/6
	200 mA.	D.C. 21in.	M.C.		10/-
	500 mA.	D.C. 2in.	M.C.	R.P	6/6
	500 mA.	D.C. 21 in.	M.C.	F.R	8/6
	0.5 amp.	R.F. 2in.	Thermo	F. Sq	4/6
	1 amp.	R.F. 24in.	Thermo	R.P	10/-
	3 amp.	R.F. 2in.	Thermo '	F. 8q	6/-
	5 amp,	D.C. 2in.	M.C.	F. 8q	13 6
	6 amp.	R.F. 24in.	Thermo	F.R	7/6
	20 amp.	D.C. 2ln.	_		10/6
	50-0-50	D.C.	M.C.	F. 8q	7/8
1	15 volt	A.C. 24in.	M.C.	F.R	10/-
	20 volt amp.	D.C. 2in.	M.C.	F. 8q	7/6
	15-0-15 volt	D.C. 21in.	M.C.	F.R 1	17/8
	150 volt	D.C. 2in.	M.C.	F.R 1	15/-
	300 volt	D.C. 2in.	M.C.	F. Sq	8/6
	R.P Rou	nd projection		Thermo = Thermo-couple.	
		h Square		M.C. — Moving Coil.	
	F.R. = Flus	h Round			

EX-W.D. CATHODE RAY TUBES. Guaranteed full picture. VCR97 at 40/-. VCR517C at 35/-. Also VCR139A—Ideal for oscilloscope 2\frac{1}{2}fin. screen at 35/-. We also have VCR97 with slight out-off, very suitable for oscilloscope, testing purposes, etc., at 15/- only. All those tubes are brand new, in original packing, and tested before despatch. Please add 2/6 packing and carriage for any of the above tubes.

R.F. UNITS. All new condition and complete. Case size 9½in. × 7½in. × 5in. Type 24.—20-30 Mc/s, 15/-. Switched Tuning. Type 25—30-50 Mc/s, 19/6. Switched Tuning. Type 27—65-80 Mc/s, 45/-. Variable Tuning. We have a limited supply of RF27 new condition and complete, but tuning dial damaged. Price only 30/- each. ALL these units Post Freel!

TEST METER—EX-ARMY. Direct readings 15 v. and 3 v. D.C., 6 mA. and 60 mA. D.C. current, 500 ohms and 5,000 ohms resistance ranges. Complete in bakelite case with web carrying strap, 19/8 plus 1/8 P. s. P.
T1154 TRANSMITTER UNIT. Medlum/high-powered for C.W.-M.C.W. R/T. 3 ranges, 10-5.5 McGs, 5-3.3 McGs, 500-200 KcGs. Absolutely complete, 4 valves, 2 meters, hundred of resistors, condensers, etc., in wooden transit case. Frice 39/8, plus 7/6 carriage and

D.C. TEST METER EX-AIR MINISTRY
D.C. TEST METER EX-AIR MINISTRY
TYPE E, BY AVO. Instrument size 4 lin. x
3 lin. x 1 lin. Black Bakelite case. Meeter
scale length 3in. B.C. voits, 2 v., 4 v., 20 v.,
40 v., 200 v., 1,000 v., 2,000 v.
D.C. current, 20 m.A., 100 m.A., 200 m.A.
2 amp., 20 amp. Resistance scale, 0-10,000
ohms. These meters have all been reconditioned, and are guaranteed perfect
Bupplled complete in leather carrying case at
£3/19/6, plus 2/- P. & P. Limited quantities.

Taching Templus. Brand new, tropicalised by Woden, for instrument work: Primary 0/110 v., 220/240 v., 380/440 v. Secondaries 0/10 v./20 v./30 v./60 v./230 v. do 3 o m.h. 6.3 v. 45 A., 6.3 v. 0.9 A. 7/8 ca only plus 1/6 P. & P. Limited quantities.

BII55A RECEIVERS guaranteed serviceable in original packing cases. £7/19/6. Fully assembled Power Pack and output stage, to ping straight into BII55 for A.C. 200/250 volts. at 79/6. We have a few brand new BII55A at £11/19/6, also in original packing cases—Deduct 10/- it purchasing either receiver together with power pack. Pins 10/- packing and carriage.

HIRE PURCHASE HIRE PURCHASE
We are pleased to announce advantageous hire purchase facilities on
any single Item over £10. Ask for
details, montioning what you are
interested in.

TAPE RECORDING EQUIPMENT. We can offer a well constructed cabinet handsomely finished in grey or brown restine made specifically to take Trivox or Weartte made specifically to take Trivox or Weartte Tape Decks Measures 221n. x 14in. x 9in. deep. Completely portable, shows attractive speaker grill at one end, to take 8in speaker. This cabinet is especially made to take in addition to the above decks, the very latest. ELPICO tape amplifier (Mk. V) at \$16.16.7. Price of cabinet 79/6, plus P. and P. N.B.—We can supply from stock the latest

24.47.
SPECIAL PURCHASE. We can offer strictly limited supply of "Limpet" telephone tape recorder attachments. Simply stile, rubber suction pad to base of telephone and plug in to input-jack on your tape recorder. This automatically records incoming telephone conversation. Our price absolutely complete with lead and jack plug. 17/6 only, post free!

free!
Manufacturer's surplus high-quality crystal
microphone type HM7 for hand or stand use.
A few only at 50/-, post free. We also have
a limited number of Ronette twin cell crystal
microphone inserts at 23/6.



Carrying cases in black leatherette finish. An extremely well-made case with chrome locks and corner pieces for extra strength. This cabinet will house any 12in. Hi-Fi speaker, but can be put to a number of uses. Front panel and lid are removable, and the cabinet is packed in a strong cardboard container for carrying purposes. Size: 18ijn. × 10ijn. × 16ijn. high, 55i-, plus 5i- post and packing.

45 Mofs PYE STRIP.—Brand new complete with 6 valves type EF50 and one EA50, 70i- only.

70/- only.

METER SPECIALI We have a limited quantity of aircraft electrical thermometers. Brand new, by Weston. 2ln. moving coli meter, flush square fitting. These meters have a luminous scale graduated 40-140 degrees centigrate, but the full scale deflection is approximately 150 microamps! Price 12/6 each only, plus 1/- P. & P. VIBRATOR PACK. Brand new, by Mallory, 12 voit input, 150 v. 40 mA. output. Complete with synchronous vibrator, 27/6.



SPECIAL PURCHASE! DECCA THREE-SPEED GRAM UNITS.

A three speed quality single player motor complete with 10in, turntable and A three speed quality single player motor complete with 10in. turntable and pickup, with the two famous firr magnetic plug-in heads type C and D, fitted with sapphire stylii. Latest Decca cantil-lever type counter-balanced pickup arm. Matches the circuit of almost any radiocramophone or record reproducer. The first step towards the achievement of high-fidelity reproduction when used with amplifiers specially designed for this purpose. Automatic stop of entirely new design. Base-plate measures 12in. × 11in. Height above motor board 2½in. and 3in. clearance required below. List price 213/1968. our price only 277/19/6 tax pad, plus 5/- packing and post. Cream finish. We can also supply this unit with the special "3-pin to ACOS" stappor and two GP19 heads. Price the same 27/19/61



VERY SPECIAL HIGH-QUALITY BADIO-GRAM GHASSIS. We have purchased a limited quantity of these chassis by Britain's leading manifacturers of quality radiograms. Circuit is a 3-waveband five-valve superhet with A.V.C. Valves 6K8 Grequency-changer 68B8G I.F. amplifier, detector and A.Y.C. 68L7GT. Combined pick-up amplifier and A.F. Amplifier on Radio and Gram. 6V6G, beam-power output tetrode; 5Z4G full-wave rectifier—Employing a special circuit for gramophone pre-amplification — A continuously variable tone-control provides ample treble correction without accentuating the base. Large glass dial, horizontal tuning measuring 11in. x 3lin. Chassis measurement: 14 lin. x 9in. x 8in. This is a superior chassis designed to sell originally in a Radiogram costing 279. Our price is \$11,1396 only, sax paid, plus \$6-packing and carriage. We will gladly demonstrate this chassis or any other working item from our stocks, to personal callers!



BATTERY CHARGER 6/12v. 4A. Attractive grey and red metal case. Fused in and out. Full charge or half charge. Complete with heavy duty crocodile clips. Not Ex-Govt. Fully guaranteed. 24/19/6.

LIGHTWEIGHT CRYSTAL HEADPHONES. Brand new, by Rothermel. List price 70/s. Our Price 25/-.!! Limited supply.

HEADPHONES. Brand new, ex-Govt., by 8. G. Brown. Type Cl.R. Low resistance, 7/6 per pair. Type CHR high resistance, 12/6 per pair. We can also aupply very special brand new American ex-Govt. light-weight high resistance phones by Trimm at 154/- per pair.

The R.C. RAMBLER ALL-DRY PORTABLE KIT

Full assembly details with practical and theoretical diagrams can be supplied at 1/6 post free. This is a truly professional -valve superhet—all dry for medium and long waves. A cream plastic top panel, with dial engraved in red and green, adds to the very imposing appearance of this model which is housed in an attractive cream and grey leatherette covered attachecase type cabinet, measuring only 9in. × 7in. × 5fin. Weight (less batteries) 4f lb.

7in. Weight (less batteries) 4{ lb. with batteries 64{lb. This set really has everything! Built - in Irame serial, high quality, extremely sensitive, and very adequate volume from the 5in. speaker. Valve line-up: 3V4, 1R5, 1S5, 1T4. All the required components. exactly as specified, including cabinet, can be supplied from stock at the special inclusive price of £7/7/- plus 2/6 P. & P. (less batteries). Uses Ever Ready 90 v.

type B126 at 9/3. Also L.T. 1.5 v. AD.35 at 1/4. N.B. When batteries are removed there is adequate space for mains unit which will shortly be made available.

will shortly be made available.

THE "SUPERIOR FOUR" KIT. Our new four-valve receiver. A.C. mains, 200/250 v. M. and Long Waves. As with our very unccessful. Economy Four" all required consumments are supplied. Valve line-up: 2.8807, 6.8507 and 807607. Chassis ready drilled. Cabinet size, 10½in. × 10in. wide Mainum depth at base, 5in., tapering to 3½in. at top. Bloping front. Very attractively finished in light wainut and peach. Each component brand new and tested prior to packing. Complete Instruction booklet with practical and theoretical diagrams is provided. Booklet available at 1/6, pout free. Our price for complete kit, 26/5/6/11 Please add 2/6 packing and carriage. If preferred, we can supply Cabinet, Assembly only, comprising Cabinet and bracket wavechange switch, dial, pointer, furm pulleys, drive spindle, drive spring and knobs, at 45/-pius 2/6 packing and carriage.

N.B.—Our Kits are even supplied with sufficient solder for the job!

THE R.C. GRAM REPL.

THE R.C. GRAM REPLACEMENT CHASSIS KIT

THE R.C. GRAM REPLACEMENT GHASSIS KIT

To meet the very great demand for this type of receiver, we have produced this unit. For Long. Medium, and Short Waves. Valve line-up: 6K8 Frequency changer, 6K7, I.F. Amplifier, 6Q7, 1st Audio, Detector and A.V.C., 6V8 Output, 6X5 Full-wave rectained. A wave and A.V.C., 6V8 Output, 6X5 Full-wave rectained black, red, green and gold dial, for horizontal tuning. Four controls are funding. L/M/S/Gram. Vol./on/orf. to are funding. L/M/S/Gram. Vol./on/orf. to are funding. L/M/S/Gram. Vol./on/orf. to are funding. L/M/S/Gram. Vol./on/orf. to are funding. L/M/S/Gram. Vol./on/orf. to are funding. L/M/S/Gram. Vol./on/orf. to are funding. L/M/S/Gram. Vol./on/orf. to a season by a simplified black, red, green and gold dial, for horizontal tuning. Four controls are funding. L/M/S/Gram. Vol./on/orf. to a season black in the season of the season by the season of the season o

plus 5/- carriage and packing.

THE "ECONOMY FOUR" T.R.F. KIT

A three valve plus metal rectifier receiver. A.C.
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THE R.E.P. ONE-VALVE BATTERY RECEIVER KIT. Simple one-valve all-dry battery receiver for headphones, easily built in one evening. All required components including headphones, can be supplied at inclusive cost of \$2/P. plus 2/P. p. & p. Operated by Ever Ready B14 type battery available at 7/9. Full assembly details available separately at 9d, plus 3d, post.

TELESCOPIO AERIAL MAST. Ex-R.A.P. dingby transmitter mast. Total length when extended, 17tt. Collapses into two sections each approx. 24in. Complete with dies and lashings, lightweight duratumin construction, diameter at thickest point, 14in. approx. tapering to \$\frac{1}{2}\text{in}\$. New condition. 32/6. Plus 2/* post and packing.

CO-AXIAL CABLE. Standard 80 ohms CO-AXIAL CABLE. Standard 80 ohms. brown, stranded centre conductor, 6d. per yard only! Not Govt. surplus. Min. 12 yds. We stock MIGROPHONES by Lustraphone, Rouette, etc., and have available, ex-stock, the New ACOS Crystal Microphone Type MIC 35-1 at 25/- and MIC 33-1 at 50/-.

BRANDENBURG E.H.T. UNITS. 6-9 kV., 6 gns.; 13-16 kV., 9 gns.; 6-9 kV. coil, 39/-; 10-15 kV. coil, 55/-. Wiring diagram supplied.

SPECIAL 111

DECCA LIGHTWEIGHT FICKUPS. Complete with either Standard or L.P. Crystal Cartridge insets. Complete with Rest and Tracking instructions. 32/8 plus 2/8 P. & P. Also their very latest type, as above, but with turn-over head, 47/8 only!

TWO GANG .0005 mid. Absolutely standard. with feet by Wingrove & Rogers. Long spindle, 6/6 each.
THREE GANG DITTO, less mounting feet,

6/6 only. 22 SET POWER UNIT NO. 4MK1 ZA10478-Complete with 4 metal rectifiers each 250 v. 60 mA. 2-12 v. 4 pin Mallery Vibrators, transformers, condensers, resistors, signal 1 amp. indicator, etc. etc., in good condition. Complete in metal box size 10 in. × 6in. × 8in. P. & P. Weight 19lb., 27/6, plus 5/-.

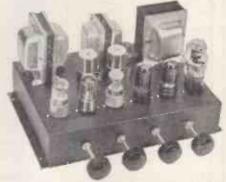
6ln. x 8ln. Weight 1915, 27/6, paus offer. x P. vALVES. We have a very comprehensive stock of special purpose surplus valves at competitive prices. A stamp will bring Valve Price List.

L.T. RECTIFIERS TYPE R.K. A newly manufactured range, guaranteed 12 months. 6 or 12 v. 1.5 a. 9/6 6 or 12 v. 1.5 a. 9/6 6 or 12 v. 2 a. F.W. bridge type 11/3 6 or 12 v. 4 a. F.W. bridge type 23/6 cor 12 v. 6 a. F.W. bridge type 23/6 CHARGER TRANSFORMERS. Input 230 v. 61/12 v. 2 a. F.W. bridge type 23/6 12 v. 6 a. F.W. bridge type 23/6 6 or 12 v. 6 a. F.W. bridge type 23/6 6/12 v. 2 a. 6/12 v. 4 a.

6/12 v. 6 a. 25/COIL PACKS MANUFACTURERS'
SURPLUS. Few only, iron-cored, 7 waveband (2 medium, 5 short waves), comprising
14 coils, trimmers, wave-change switch, etc.
etc., complete with copy of manufacturers'
original circuit, 50/- only, tax paid. Completely assembled. Suitable Glass Dial. 3/6.



"CONTEMPORARY." A well made cabinet in light wood, made especially to blend with this type of furniture. The motor board is uncut, and will accommodate most Radio Chassis and Auto-change units. Size: 30in. x 15in. x 29in, high. Price £9/15/¬, plus 10/- post and packing.



THE NEW R.C. HIGH-FIDELITY AMPLIFER. P.P. 6V6 output. Freq. 25–18,000 cps.—60db at 6§ watts. Treble boost and out—Bass boost—L.P. correction. Provision for Feeder Unit Max. UNDISTORTED OUTPUT 8§ watts. Frice 14 gns., plus 7/6. MOW AVAILABLE. Kit of Parts, complete with full flustrated instructions £11/19/6, plus 5/1-carriage. Illustrated booklet available separately at 2/6. Attractive metal cover, now available. With built-in carrying bandle, 19/6.
24 VOLT ROTARY CONVERTEE. Input 24 v. D.C. Output 269/260 v. A.C., ibs. P. 19/6.
24 VOLT ROTARY CONVERTEE. Input 24 v. D.C. Output 269/260 v. A.C., ibs. P. 19/6.
25 VOLT COUNTRY CONVERTEE. Input 24 v. D.C. Output 269/260 v. A.C., ibs. P. 19/6.
26 VOLT ROTARY CONVERTEE. Input 24 v. D.C. Output 269/260 v. A.C., ibs. P. 19/6.
26 VOLT COUNTRY CONVERTEE. Input 24 v. D.C. Output 4 watts. 2/3 ohm. Illin. × 8/in. Weight approx. Sidum Lamp transformer. Brand new 26/6.
26 Jin. × 19/6. December 20/6.
27 Jin. × 19/6. Volume and Tone Controls—Valve line up. 681.7, 6V6, 573—Engraved 11/2. Jin. × 19/6. Jin. × 19/6. P. Philips. Jin. × 19/6. STIPENDOUS HALF-PRICE OFFER II DECCA SINGLE SPEED RECORD PLAYING DESKS 33A. Easily converted to either Standard or L.P. Price with one crystal cartridge of either type. \$\frac{24}{19/6}\$. or with both cartridges, \$\frac{25}{19/6}\$. Plus 5/- P. & P.

WHIP AERIALS. All copper, 3 sections each of 4tt. Screw in, 7/6 complete. Ditto, but two bottom sections only at 4/6. Both plus P. & P. 1/6.

8 MFD. 1,200 v. PAPER BLOCK CONDENSERS. Size: 5in. x 4/in. x 3/in., 15/- eacb. Many others in stock.

prices.

CABINETS. We can supply a cabinet for every requirement, Table Model, Extension Speaker, Portable Player, Console, even for Projection T/V! Why not call and see us?

4-WATT 2-STAGE AMPLIFIER. Valve line-up: 616, EF87 and GZ32, complete with 10in. Mains Energised Speaker, 26(19/8, plus 5/- packing and carriage.



	RECTIFIERS
L.T. Types	H.T. Type H.W.
2/6 v. ½ a.h.w 1/9	120 v. 40 mA 3/11
6/12 v. ½ a.h.w 2/9	250 v. 50 mA 5/9
	250 v. 80 mA 7/9
F.W. Bridge Types	RM2 125 v. 100
6/12 v, 1 a 5/9	mA 3/11
6/12 v. 1\(\frac{1}{4}\)a 7/9	RM3 125 v. 120
6/12 v. 2 a 9/9	mA 5/9
6/12 v. 4 a 14/9	RM4 250 v. 250
6/12 v. 6 a 19/9	mA 11/9
6/19 10 - 00/0	200 975 m A 19/4

CO-AXIAL CABLE. 75 ohms lin., 7d yard. Or in 20yd, lengths, 6d. yd. Twin screened feeder,

6/12 v. 10 a..... 29/9

mA 11/9 300 v. 275 mA. 12/11

RHEOSTATS (VARIABLE RESISTORS)
2 ohms 5 amps, 6/9; 0.4 ohm 25 a., 8/9; 10 ohm
3 amps., 8/9; 60 ohms 1.5 amps, 14/9.

SILVER MIGA CONDENSERS. 5, 10, 15, 20, 25, 30, 35, 50, 100, 120, 160, 180, 200, 230, 300, 330, 400, 470, 500, 1,000 pfd. (.001µF), .002 mfd. (2,000 pfd.). All at 5d. each, 3/9 dozen one type.

DIAL BULBS, M.E.S., 8 v. 0.15 a., 6/9 do 6.5 v. 0.15 a., 6/9 doz. 4.5 v. 0.3 a., 6/9 doz.

ELECTROLYTICS (Current production)

	TAOT A	DA GOVE.	
Tubular Type	S	Can Types	
8μF 450 v	1/11	16 mfd. 350 v	1/11
8 mfd. 500 v	2/6	16μF 450 v	2/9
16μF 350 v	2/3	24μF 350 v	2/11
16μF 450 v	2/9	32μF 350 v	2/11
16μF 500 v	3/9	32 mfd. 450 v	4/9
24μF 350 v	3/3	64 mfd, 450 v	4/9
32μF 350 v	3/9	8-8μF 350 v	3/9
32 mfd, 500 v	5/9	8-8µF 450 v	3/11
8-16μF 500 v.	4/11	8-8 mfd, 500 v.	
25μF 25 v	1/3		4/9
50μF 12 v	1/3	8-16μF 450 v	2/11
50μF 50 v	2/3	16-16μF 450 v.	4/11
A		16-32μF 350 v.	4/9
Can Types		16-32 mfd, 450 v.	4/9
8 mfd, 350 v	1/3	32-32µF 350 v.	4,9
8 mfd. 450 v	2/3	32-32µF 450 v.	5/11
8 mfd. 500 v	2/9	ου-ουμι που v.	0/11

AMPLIFIER OR CHARGER CASES. Size 14% x 5% x 7½ in, high. Strongly made in perforated 5 x 7 in. high. Strongly made in steel. Grey enamel finish. Only 9/8.

VOLUME CONTROLS with long spindles, all values less switch, 2/9; with S.P. switch, 3/9.

wire wound Pots: 20 ohms, 500 ohms, 5K, 20K, 50K, 100K (medium length spindles), 2/9. 220 ohms, 2K, 10K, 20K, 50K, Preset type, 1/9 ea.

AMMETERS. Moving coil. 0-5 amps., 2in. scale, 11/9.

EX-GOVT. E.H.T. SMOOTHING CONDENS	ERS
25 mfd. 4.000 v. Blocks	4/9
.5 mfd. 2,500 v. Blocks	3/9
.5 mfd. 3,500 v. Cans	3/3
(common negative isolated)	9/6
1.5 mfd. 4,000 v. blocks	5/9

EX-GOVT. ACCUMULATORS with non-spill vents Unused and guaranteed. 2 v. 16 A.H., 5/9 each or 3 in wood carrying case 9×7×5in., 14/9, plus

EX-GOVT. BLOCK	PAPER CONDENSERS	
2 mfd. 800 v	1/9 4 mfd. 2,000 v.	6/9
4 mfd, 500 v	2/9 6-6 mfd, 500 v	5/9
4 mfd. 730 v	3/9 8 mfd. 500 v	5/9
4 mfd, 1,500 v	4/9 8-8 mfd. 500 v	6/1
	15 mfd. 500 v	7/9
4 mfd. 400 v. plus 2	2 mfd, 250 v. 1/11.	, i

EX-GOVT. AUTO TRANSFORMERS 50	c/s
Double Wound 0-230 v. to 15-10-5-0-195-	
215-235 v., 1,000 watts	27/9
Double Wound 220/240 v. input. Output	
57.5 v, to 230 v, 21 amps in steps of 11 v.	£6/15
Double Wound 10-0-200-220-240 v. to	
10-0-275-295-315 v. 1,000 watts	69/6
For 110-115 v. input or output primaries	
and secs., can be connected in series.	
0-110-190-230 v. 1.400 watts	49/6
0-110-180-400 A. T'100 Mgff2	40/0

M.E. SPEAKERS. All 2-3 ohms, 6\frac{1}{2}\text{in.} Rolafield 700 ohms, 11/9. 10\text{in.} R.A. field, 1,500 ohms, 23/9. 10\text{in.} R.A. field, 1,500 ohms, 23/9. SPECIAL OFFER. Mains Trans. 200-250 v. 50 c/s. Primary. Secs. 300-0-300 v. 150 mA. 6.3 v. 4 a., 5 v. 3 a., V.15 checuled depth brough 21/9. Half shrouded drop through, 21/9.

R.S.C. TRANSFORMERS

FULLY GUARANTEED, INTERLEAVED AND IMPREGNATED

MAINS TRANSFORMERS Primaries 200-230-250 v. 50 c/s.

300-0-300 v. 100 mA., 6.3 v. 4 v. 4 a. c.t., 0-4-5 v. 3 a 23/9 350-0-350 v. 100 mA. 6.3 v. 4 a., 5 v. 3 a. 22/9 850-0-350 v. 100 mA., 6.3 v. 4 v., 4 a., c.t., 0-4-5 v. 3 a 23/9 350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a. 31/6 350-0-350 v. 150 mA., 6.3 v. 2 a., 6.3 v. 2 a., 5 v. 3 a. 33/9

TOP SHROUDED DROP THROUGH TYPE

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a. 26/9

FILAMENT TRANSFORMERS Primaries 200-250 v. 50 c/s 6.3 v. 1.5 a..... 5/9 0-4-6.3 v. 2 a.... 7/9

CHARGER TRANSFORMERS All with 200-230-250 v. 50 c/s Primaries: 0-9-15 v. 1.5 a., 12/9; 0-9-15 v. 3 a., 18/9; 0-9-15 v. 6 a., 22/9; 0-4-9-15-24 v. 3 a., 22/9.

ELIMINATOR TRANSFORMERS

 OUTPUT TRANSFORMERS

 Midget Battery Pentode 66:1 for 3S4, etc.
 3/6

 Small Pentode, 5,000Ω to 3Ω
 3/9

 Standard Pentode, 6,000Ω to 3Ω
 4/9

 Standard Pentode, 8,000Ω to 3Ω
 4/9

 Standard Pentode, 10,000 ohms to 3 ohms
 4/9

 Standard Pentode, 10,000 ohms to 3 ohms
 4/9

 Multi-ratio 40 mA, 30:1, 45:1, 60:1, 90:1,
 5/6

 Push-Pull
 5/6

 Push-Pull 10:12 Watts 6V6 to 3Ω or 15Ω
 8/9

 Push-Pull 10:12 Watts 6V6 to 3Ω or 15Ω
 15/9

 Push-Pull 10:12 Watts to meth 8V6
 15/9

SMOOTHING CHOKES
 SMOOTHING CHOKES
 11/9

 250 mA., 3 H. 50 ohms.
 11/9

 150 mA., 7-10 H. 250 ohms.
 11/9

 100 mA., 10 H. 200 ohms.
 8/9

 80 mA., 10 H. 350 ohms
 5/6

 60 mA., 10 H. 400 ohms.
 4/11

 50 mA., 40 H. 1,000 ohms. Potted
 10/9

 20 mA., 30 H. 1,000 ohms.
 4/9

> EX. GOVT. MAINS TRANSFORMERS All 230 v. 50 c/s, input

MICROPHONE TRANSFORMERS

THE SKY CHIEF T.R.F. RECEIVER





A design of a 4-stage, 3 valve 200-250 v. A.C. Mains receiver with selenium rectifier. For inclusion in any of cabinets illustrated above. It consists of a variable Mu high gain H.F. stage followed by a low distortion grid detector triode. The next stage is a further triode amplifier with tone correction by negative feedback. Finally comes the output stage consisting of a parallel connected double triode giving ample output at an extraordinary low level of distortion. Point to point, wiring diagrams instructions, and parts list, 2/8. This receiver can be built for a maximum of £4/16/- including cabinet. of £4/16/- including cabinet.

P.M. SPEAKERS. All 2-3 ohms, 31in, Goodmans (Ex New Units), 10/9. 5in. Goodmans, 15/9. 6lin. Plessey, 16/9. 8in. Plessey, 15/9. 10in. R.A., 26/9. 10in. Plessey, 18/6. 10in. Rola with Trans., 29/8.



CASE, MAINS TRANS
FORMER, FULL WAVE METAL RECTIFIER
FUSE, FUSE-HOLDERS AND CIRCUIT
Any type assembled and tested for 6/9 extra

250-0-250 V. 40 mA., 6.3 V. 2 a.,	
5 v. 2 a	9/11
8.8 v. 4 a	9/9
	9,6
48 v. 1 a	
0-11-22 v. 15 a	35/9
0-11-22 v. 30 a	72/6
16-18-20 v. 35 a	79/6
7.7 v. C.T. 7 amps 4 times	25/9
460 v. 200 mA., 6.3 v. 5 a	27/9
365-0-365 v, 150 mA	8/9
300-0-300 v. 80 mA, 5 v. 3 a	8/11
278-0-278 v. 100 mA	
300-0-300 v. 150 mA., 610-0-610 v. 150 mA.,	-/-
	29/9
400 v. C.T. 150 mA. 4 v. 6 a., 6,3 v. 6 a.,	20,0
6.3 v. 0-6 a., 4 v. 6 a., 4 v. 3 a., 4 v. 3 a.,	
	00/0
4 v. 3 a., 5 v. 2 a	22/0
EX-GOVT, SMOOTHING CHOKES	
250 mA., 10 H. 50 ohms	14/9
250 mA. 10 H. 100 ohms	14/9
250 mA. 3 H. 50 ohms	8/9
150 mA, 10 H. 50 ohms	10/11
100 mA. 10 H. 100 ohms, Tropicalised	6/9
100 mA, 5 H. 100 ohms. Tropicalised	3/11
50 mA. 50 H. 1,000 ohms. Potted	9/11
	8/11
90/100 mA, 10 H, 100 ohms, Potted	8/9

EX-GOVT. TRANSMITTER-RECEIVER TYPE TR9D, complete with all valves, only 47/9, plus

L.T. type 1 amp.....

у. 6.	Call. 0/	
v.	CHASSIS	
9.	18 s.w.g. undrilled alu-	16 s.w.g. aluminium, re-
T E L	minium amplifier type	ceiver type.
E	(4-sided).	10101011
L	12in, × 9in, × 2½in, 6/11	12in, × 8in, × 2 in. 5/3
5	$14in. \times 9in. \times 2\frac{1}{2}in.$ 6/11 14in. × 10in. × 3in. 7/11	16in. × 8in. × 2½in. 7/6 20in. × 8in. × 2¾in. 8/11
ζ, Γ.	16in. × 10in. × 3in. 8/3	2011. A old. A 2511. 8/11
a,	18 s.w.g. aluminium re-	16 s.w.g. aluminium, am-
		-lifes tome 4 sided

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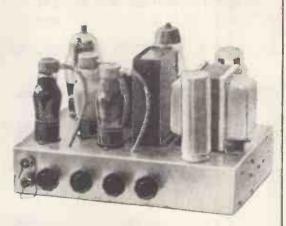
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Now firmly established and proving extremely popular, our AII Quality Amplifier we consider to be the best value in amplifiers offered to-day. The volume of its high fidelity reproduction is completely controllable, from the sound of a quiet intimate conversation to the full glorious volume of a great orchestra. Its sensitivity is so high that in areas of fair signal strength it can be operated straight from a crystal receiver. Entirely suitable for standard or long-playing records in small homes or in large auditoriums. For electronic organ or guitar or for garden parties or dance bands.

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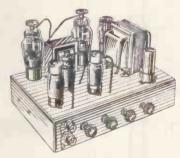


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All parts for an "All
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Complete with integral pre-amp. Tone control stage (as AII amplifier), using negative feedback, giving humproof individual bass and treble lift and cut tone control. Six Negative Feedback Loops. Completely negligible hum and distortion. Frequency response \pm 3 db. 30-20,000 c.p.s. Two independently controlled inputs. Six B.V.A. valves. A.C. mains 200-230-250 v. input only. Outputs for 3 or 15 ohms speakers. Kit of parts complete in every detail, \$7/19/6, plus 5/- carriage, or ready for use, 45/- extra. Descriptive leaflet 1/*.

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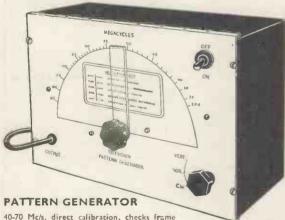
23. HIGH STREET, ACTON, W.3

(Opposite Granada Cinema)



COMPLETELY BUILT SIGNAL GENERATOR

Coverage 120 Kc/s-320 Kc/s., 300 Kc/s-900 Kc/s., 900 Kc/s.-2.75 Mc/s., 2.75 Mc/s.-8.5 Mc/s., 8.5 Mc/s.-25 Mc/s., 17 Mc/s.-50 Mc/s., 25.5 Mc/s.-75 Mc/s. Metal case 10 x 6} x 4in. Size of scale 6½ x 3in., 2 valves and rectifier. A.C. mains 230-250 v. Internal modulation of 400 c.p.s. to a depth of 30 per cent., modulated or unmodulated, R.F. output continuously variable 100 milli volts. C.W. and mod. switch, variable A.F. output and moving coil output meter. Black crackle finished case and white panel. Accuracy plus or minus 2%. £4/19/6, or 34/- deposit and 3 monthly payments 25/-. P. & P. 4/- extra.



40-70 Mc/s. direct calibration, checks frame and line time base, frequency and linearity,

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Both generators guaranteed for 12 months

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ALL COMPONENTS for:- OSRAM 912 AMPLIFIER and MULLARD 5 VALVE 10 WATT HIGH QUALITY AMPLIFIER. Send for priced parts list.

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as per our general list.

MULLARD " UNIVERSAL" LARGE SCREEN A.C./D.G. TELEVISOR. Denco drilled chassis with all mechanical parts, 53/6; FD12/4, duomag focaliser, 37/6; 14A/342 rectifiers, 37/2; Goldsman droppers DAS7/6, 8/9; DX35/6, 7/6. VA1008 varite res., 4/6. Other Denco parts, please see below.

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BC610 TRANSMITTERS with speech amplifier, aerial tuning unit, etc. Brand new

RCA TRANSMITTERS. Type ET-4336. Complete with original speech amplifier, crystal multiplier and VFO units. Unused and reconditioned. Can be supplied with very large quantity of spares.

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MULT! CHANNEL TRANSMITTER T-4/FRC, with modulators MD-1/FRC, 2 Mc/s to 18 Mc/s. Each channel 400 w. output. T.C.S.6 EQUIPMENT complete with antenna loading unit, remote control, microphone, etc. Brand new.

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METAL RECTIFIERS Type IB, D.C. output 10 amps at 22 v, input 220/250 v., 50 c/s.

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A large selection available for SCR399 (BC610), ET4336, SCR610, EE8 Telephones, and Tele-**SPARES** printers type 7B.

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Mains Transformer, fully impregnated, laput 210, 220, 230 and 240. Sec 600-0-600, 275 mA., and 200 v. at 30 mA., complete with separate heater transformer. Input 210, 220, 230, 240. Sec. 6.3 v. at 3 amp. and 5 v. 3 amp. 45/-.
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MAINS TRANSFORMERS, chassis, mounting, feet and voltage panel. Primaries 200/250.

350-0-350 75 mA. 6.3 v. 3 a. tap 4 v.

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9in. T.V. Cablnet, front in contrasting walnut veneurs, size 104 in. long, 112 in. high, by 124 in. wide. Complete with two pieces expanded aluminium in gold, 12 x 9in. and 5in. speaker baffle and chassis, 204-, post paid.

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6lin. M.E. Speaker, 1,000 ohm field,

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R. & A. T.V. energised 64in. speaker with O.P. trans., field coil 175 chms, 9/6. P. & P. 2/6.

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Volume Controls. Long spindle and switch, \$, \$, 1 and 2 meg., \$4/- each. 10K and 50K, 3/6 each. \$ and 1 meg., long spindle double pole switch, ministure, 5/-. P. & P. 3d. each.

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Line Cord, 2-way 0.3 amp., 60 ohms per foot, 1/3 per yard.

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Terms of Business : Cash with order. Despatch of goods within 3 days from receipt of order. Where post and packing charge is not stated please add 1/6 up to 10/-, 2/- up to £1, and 2/6 up to £2. All enquiries, S.A.E., lists 5d. each.

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T.V. CONVERTER for the new commercial stations complete with 2 valves. Frequency:-can be set to any channel within the 186-196 Mc/s. band. I.F.:-will work into any existing T.V. receiver designed to work between 42-68 Mc/s. Sensitivity:-10 Mu/v with any normal T.V. set. Input:-arranged for 300 ohm feeder. 80 ohm feeder can be used with slight reduction in R.F. gain. Circuit EF80 as local oscillator, ECC81 as R.F. amplifier and mixer. The gain of the first stage, grounded grid R.F. AMPLIFIER 10 db. Required power supply of 200 v. D.C. at 25 mA. 6.3 v. A.C. at 0.6 amp. Input filter ensuring complete freedom from unwanted signals. 2 simple adjustments only. £2/10/-. P. & P. 2/6.

HIGH-IMPEDANCE PLASTIC RECORDING TAPE, by famous manufacturer. 600ft. on sluminium spool, 8/-, 1,200ft. on aluminium spool, 17/6 post paid.

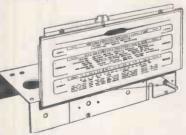


P. & P. 3/6.
AS ABOVE, complete with new 5in. speaker

AS ABOVE, complete with new 5tn. speaker to fit and O.P. trans., 37/6. P. & P. 3/6. With superhet chases. 83/8. P. & P. 3/6. Used metal rectifier, 230 v. 50 mA., 3/6, gag with trimmers, 6/6; M. & L. T.-R. S. Vibandi eventual formation of the second of th

P.M. 28/17/8. P. a.F. 3-CR100 Coll packs, 10-2,000 metres, in soiled condition complete with 4-gang tuning condenser. 19/6. P. & P. 3/6. CR100 Coll packs in first class condition less oscillator section, complete with 4-gang tuning condenser. 19/6. P. & P. 3/6. CR100 465 Kc, I.F.s, types 3, 4 and 5 and B.F.O., new condition, 7/6 each. 465 Kc Xtal for CR100, 12/6. 4-gang tuning condenser for CR100, 9/6.

ONSTRUCTOR'S PARGEL comprising chaesis 124 x 8 x 23 in., ead. plated, 18 gauge, vih., LF. and trana out-oute, back-plate, 2 supporting brack-ts, 3 ware-band scale, new wavelength stetions names. Size of scale 11½ x 44 in., drive sp., drum, 3 putleys, pointer, 3 bath badders, 5 par. LO. v/h., 4 knobs and pair of 460 LFs, bvin gang, 16 x 16 mfd. 350 wkg., mains trans. 250-250 60 mA., 54 v., 2 amp. 5 v. 2 amp. and 6 im. Ms. speaker with O.F. trans. 39/6. P. & P. 3/6.



Battery charger, input 230/250 v. output 6 and 12 volt 1 amp. Black crackle finished case size 10 x 6 x 4in. 21/-. P. & P. 3/-.

OUTPUT TRANSFORMERS. Standard type 5,000 ohms imp. 4/9; 42-1 with extra feed-back windings, 4/3. Miniature 42-1,3/3. Multi-ratio 3,500,7 000 and 14,000,5/6, 10-watt push-pull, 6V6 matching, 7/-. 90-1 3 ohm speech coll, 6/6.
PUSH-BACK CONNECTING WIRE. Doz. yds., 1/6. Post paid.
STANDARD WAVE-CHANGE SWITCEES 4-pole 3-way, 1/9; 5-pole 3-way, 1/9; 3-pole 3-way, and 4-pole 2-way, 2/6 each. 2-pole 11-way twin wafer 5/-; 1-pole 12-way single wafer 5/-, P. & P. 3d.

POTATO AND VEGETABLE PEELER

By famous manufacturer, capacity 41 lbs., complete with water pump. All aluminium construction, white stove-enamel finish. Originally intended for adaption on an electric food-mixer, can be easily converted for hand operation. 39/6. P. & P. 3/-.

PERSONAL SHOPPERS ONLY. 9in. Enlarger, 17/6; 12ln., 27/6. Germanium Crystal Diode, 1/6, post

141

paid. Used 9in. Tube, with ion burn, 17/6.

Used 9in. Tube, with ion burn. 17/6, post paid.

Line O.F. Transformer in aluminium can mounted in rubber, 12/6.

Crystal Set, weddim and iong wave, in plastic cabinet, 16/
Readphones, per pair 8/
Speaker Matching Unit on aluminium chasels, 3-15 ohms, reversible, 12/8.

Line and E.H.T. Transformer, 14 kV..

Line and E.H.T. Transformer, 14 kV. using ferrocart core, complete with line and width control, and corona shields, U37 rectilier winding, 35/-
Line and E.H.T. Transformer, 9 Kvi. Line and E.H.T. Transformer, 9 Kvi. using ferrocart core, complete with

using ferrocart core, complete with built-in line and width control, Mounted built-in line and width control. Mounted on small all-obassis. Overall size 4½ x1½ in. EV51 rec. winding, 27/6. Line and E.H.T. Transformer, 9 Kv., ferrocart core, EV51 heater winding, complete with scan colls and frame output transformer, and line and width control, £2,5/1. P. & P. 8/1. Scan Colla, low line low impedance frame, complete with frame transformer, to match above, 27/6. P. & P. 2/-.

Valve Holders, monided octal Mazda and loctal, 7d. each. Paxolin, octal Mazda and loctal, 4d. each. Moulded B7G, B8A and B9A, 7d. each. B7G moulded with screening can, 1/8 each. 32 mfd., 350 wkg. 21-16 x 24, 350 wkg. 41-4 mfd., 200 wkg. 1/3 40 mfd., 400 wkg. 16 x 8 mfd., 500 wkg. 3/8 16 x 16 mfd., 500 wkg. 5/9 16 x 16 mfd., 450 wkg. 3/9 32 × 32 mfd., 350 wkg. 4/-82×32 mfd., 350 wkg., and 25 mfd., 25 wkg. 8/6 11d. 1/-3/3 8 mfd., 350 v. wkg., tag ends 50 mfd, 25 v. wkg., wire ends 1/8 100 mfd., 350 wkg. 4/-100 mfd., 450 w. wkg., 280 mA., A.C. ripple 3/11 9/8 16+16 mfd., 350 wkg. 1/9 65 mfd., 220 wkg..... 1/6 7/6 50 mfd., 50 wkg. 1/9
Miniature wire ends moulded.
100 pf., 500 pf., and .001, ea. . . 7d.

100 pt., 500 pt., and .001, ca... 7d.
T.V. Filter in lightly thred Persper,
size 13\frac{1}{2} \times 11\times 3/16\lin., 4/6.
Combined 12\lin. mask and esenteheon
in lightly thred Perspex. New aspect,
edged in brown. Fits on front of
cabinet, 12/6. As above for 15\lin.
tube, 17/6.

tube, 17/6.
Frame Oscillator Blocking Trans., 4/6.
Line Osc. Blocking Trans., 4/6.
Tube Mounting Bracket, size 9½ × 4½in. 12in. tube clamps, 2/-.

12in. tube clamps, 2i-.
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except Mazda 12in., with adjustment, 15/-.

adjustment, 15/-.

P.M. Foeus Unit for Mazda, 12in., with vernier adjustment, 17/6.
Wide Angle P.M. Foeus Units, Vernier adj., state tube, 25/-.
Energised Foeus Coil, low resistance mounting bracket, 17/6.

Ion Traps for Mullard or English Electric tubes, 5/-, poet paid. 465 Kc. I.F.s, size 2½ x 1½in. Q.110, removed from American equipment

5/- per pair. Standard 465 Kc. iron-cored I.F.s, 4×1½×1½In., per pr. 7/6. Wearlte standard, iron-cored, 465 Kc. 1.F.s 3½×1½×1½in., per pr. 9/6.

1976. Pron-sored 465 Ke. Whistle Fliter, 2/8, 465 Ke. MIDGET I.F.s. Q.120 size 14m, long, lin. wide, jin. deep by very famous manufacturer. Pre-aligned adjustable iron-dust cores, per pair 12/6.

12:6.

Mains Droppers. 0.3 amp., 460 ohms, tapped 280 and 410, 1/6; 0.2 amp., 717 ohms, tapped at 100 ohms, vitreous, 1/6; 0.3 amps. 950 ohms, tapped 700 and 826, 2/6; 0.2 amp., 1,000 ohms, vitreous, tapped, 2/6; vitreous, 0.3 amp., 700, tapped 680, 640, 600, 3/6. P. S. P. on each 3d.

T.V. Width Controls, 3/6.

Prices slashed at Clydesdale

PLEASE NOTE. Carriage and Postal charges refer to the U.K. only. Overseas freight, etc., extra.

RECEIVER 6A. Channel checking unit working on 49-100 metres contains 5/VR91 (EF50). on 49-100 metres, contains 5/VR91 (EF50), 1/6K8, 1/VR55 (EBC33), 1/VR53 (EF39) valves. Thermal switch breaking at 85 degrees F., etc., etc. In Metal Case 8 in. x 7 in. x 10 in. CARRIAGE ASK FOR X/H477A.

29/6 each RECEIVER UNIT R3601. Ref. 10DB/6037. With valves: 2/VR136 (EF54), VR137 (EC52), 5/VR65 (SP61), 4/VR92 (EA50), VR91 (EF50), 6V6G, VU39A (R3), etc., 1.F. 13 mcs. Dim. 18in. x 9in. x 8in. Wgt. 38lbs. ASK FOR 20/6 CARRIAGE

39/6 each. X/H493

EX. U.S.N. TEST OSCILLATOR TS-24/ARR2 Low/High frequency battery powered for TBX alignment, H.F. signal 245 mcs. L.F. signal tunable 540 to 830 kcs. with valves 2-955 acorn triodes and clockwork time switch with calibrated diate 0/30 Min. Unit dim. 9½In. x 7½in. x 7in., finish black ASK FOR CARRIAGE 27/6 each

MONITOR CRYSTAL TYPE 2. 10T/11390. As used with the R1116 or R1082, less valves and crystals, but otherwise complete. Dim. $7\frac{1}{2}$ in. x 5½in. x 3½in. Plastic constructions, in transit case. ASK FOR POST 1/-5/- each. EXTRA X/H872.

POWER UNIT TYPE 266. In Transit Case, Input 80 v. 1.5 k/cps. A.C. Output H.T. 120 v. D.C. bias 3, and 9 v. L.T. 2 v. Smoothed and stabilised. Complete with 5U4G valve, VCI10 stabiliser, 12 v. I a. Metal Rectifier, etc., etc., in attractive metal case with handles. Dim. Ilin. x 9in. x 7in. ASK FOR CARRIAGE 22/6 each. X/E870.

STAINLESS STEEL AERIAL WIRE. 7/.015 in reels of approx. 1,600ft. made by Tem.co. ASK FOR 25/- per reel. PAID 25/- per reel.

AERIAL ROD. 15in. lengths, copper plates, steel tube, ferruled to interlock an Aerial of desired length.
3/16in. dla. ASK FOR X/H709.

3/16in. dia. ASK FOR X/H in. dia. ASK FOR X/H710. EITHER 4/6 dozen lengths. POST 6d EXTRA

RADAR REFLECTOR AERIAL MX/137/A.
Spider-Web mesh aerial in original moisture proof carton, with assembly instructions.
ASK FOR X/E175.

4/11 each. POST 9d.
X/E175.

PLOTTER FIELD MK. IV. Ref. O.S.739A. A precision made Protractor Unit, first class condition. With 2 scales 0-180 deg., moving crossarms, scaled 21-65, each 12jin. long. Straight edge base scaled 0-3500, length 25in. fully extended in soiled leather case 16in. x 5 jin. x 2in. ASK FOR X/H864. 9/11 each. PAID

ION TRAP MAGNET ASSEMBLY. Mfg. Surplus.

Type IT/6 by Elac for 35 mm. tube neck ASK FOR X/H919 2/6 each. POST 3d. 2/6 each. EXTRA CORD DRIVE SPINDLE. Ratio 6-1.

Reverse Vernier Drive, I.e. cord runs outside chassis. POST ASK FOR 1/- each or 3 for 3/- post paid.

ELECTROLYTIC CONDENSERS, Metal Can, Clip Mrg. Types.
Cap. 24-24 mfd. 450 v. D.C. wkg. Dia. Iĝin. x 2in.
ASK FOR 3/- each POST
X/H971. or 3 for 7/6 post pald. 3d. 3/- each or 3 for 7/6 post paid. Cap. 16-24 mfd. 450 v. D.C. wkg. Dia. 1 in. x 2 in. ASK FOR 3/- each POST X/H972. or 3 for 7/6 post paid, 3d. Cap. 8-16 mfd. 450 v. D.C. wkg. Dla. 18in. x 28in. ASK FOR 3/- each POST X/H918. or 3 for 7/6 post paid. 3d. Cap. 32 mfd. 450 v. D.C. wkg. Dia. 2in. x 4\fm\text{in.} With waxed cardboard cover and mtg. plate. ASK FOR I/9 each POST X/H852. or 3 for 5/- post paid. Cap. 8 mfd. 450 v. D.C. wkg. Dia. ¾in. x 2¾in. Tubular card covered wire ends. ASK FOR I/6 each POST X/H980. or 3 for 4/- post paid. 3d. PAXOLIN WAFER ROTARY WAVE-CHANGE SWITCH.

3 wafers each, 2 pole, 5 way. Dim. 3 jin. x 2 jin. 5 WAY GROUPBOARDS. Paxolin panel 2½in. x 2½in., with tags for mounting 5 condensers or resistors, two hole fixing.

ASK FOR 6d, each POST ASK FOR X/H981. or 3 for 1/6 post paid.

GO-AXIAL CABLE.
Any length supplies 52 ohms, 12 mm, dia, Price 5d, per yard. Minimum 12 yards at 5/- post paid. ASK FOR X/E987.

I.F. TRANSFORMER. 465 kc/s. standard type. Dim. 3\frac{1}{2}in. x 1\frac{1}{2}in. x 1\frac{1}{2}in. Pigtall and plain A.D.T. ASK FOR 8/6 per pair or 3 pairs for 22/6 post paid.

465 kcs. miniature type. Dim. 21in. x 11in. x 1in., plain permeability tuned. ASK FOR 9/6 ea 9/6 each

or 3 pairs for 25/- post paid

CLYDESDALE

Phone: South 2706/9 2, BRIDGE STREET, GLASGOW . C.5 BRIDGE STREET SUPPLY

2/6

5/-2/-

1/-

9d_ 8/6 2/-1/-

1/-

1/-

2/-

2/-

1/6

1/-

6d. 1/3

SAMSON'S==

X/H364

SURPLUS STORES

SPECIAL OFFER—OFFICE INTER-COMM. SETS. FAMOUS MANUFACTURER'S EXPORT SURPLUS. Includes Master and two extensions built in highly polished wood cabinets in Oak or Mahogany. Operates from 200-250 volts A.C. Valveline-up I UF41, UL42, and metal rectifier. The Master is designed to operate four extensions. Brand new in Maker's Cartons with Installation instructions, £8/19/6, originally sold at 16 gns. Extra Extensions 27/6 each. Illustrated in the September issue of "Wirreless World."

CONSTANT VOLTAGE TRANSFORMERS BY SOLA U.S.A. Pri. 90-125 volt or 190-250 volt. Sec. 115 v. at 2 KVA. Pri. and Sec. completely isolated. For 50 or 60 cycle operation. Approximate weight 200 lbs., £19/10/r each, £37/10/r per pair, carr. according to distance.

weight 200 los., £19/10/e each, £37/10/e per pair, carr. according to distance.

A.M. HT. TRANSFORMERS. Pri. 230 volt, Sec. 1,500 volt 1.6 KVA, 65/e, carr. 7/6. 1154 TX Transformers, Pri. 200-250 volt, Sec. 1250-1300 volt 350 volt MA, 35/e, Carr. 4/e.

SLIDING RESISTORS—ALL BY FAMOUS MAKERS. 20 ohms 7 to 1.5 amp. with geared drive, 37/6. 152 ohms 2 amp. with worm gear control, 32/6. 5.3 ohm 8 amp. with worm gear control, 27/6. 3.4 ohms 12 amp., 12/6. P.P. on all types 2/e.

LOW WATTAGE HEATERS. 230 volt, comprises high grade element built in brass cylinder. 350 watt, length 8in, dia. lin., 6/6. P.P. 6d. 250 watt, length 5in, dia. lin. 5/6. P.P. 6d. dlealfor drying cupboards, garage heaters, hot-houses, photographic purposes, etc. etc.

RESISTANCE MATS. Set of four, includes one 690 one 150 and two 80 ohms. Size of each mat 8 x 6\frac{1}{2}\text{in., 10/6 per set. P.P. 1/6.}

ARMY FIELD TELEPHONES TYPE DS. Buzzer calling. Complete with hand set and batteries, built in strong metal cases. Suitable for farms, building sites, workshops, etc., 49/6 each. Carr. 3/e.

ADMIRALTY SOUND POWERED HAND SETS. No batteries required, 17/6 each. P.P. 1/6.

ADMIRALITY SOUND POWERED HAND SETS. No batteries required, 17/6 each. P.P. 1/6.

TELEPHONE CABLE, single D3, one mile drums, 55/-. Carr. 5/-.

COMMANDO ASSAULT TELEPHONE CABLE. P.V.C. 1,000-yard drums, ideal telephone cable and very useful for the home and garden, 15/- per drum. P.P. 1/6.

= 169/171 Edgware Road, ===== London, W.2. Tel. PAD 7851

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All orders and enquiries to our Edgware Road branch, please. This is open all day Saturday.

LARGE OUANTITIES GUARANTEED UNUSED

COMPONENTS STILL AVAILABLE

2.000 CERAMIC VARIABLE CONDENSERS, split stator 15/15 pf. as illustrated in Sept. and Oct. issues EA.
2,000 CERAMIC TRIMMERS 22 pf., as described in Sept. and Oct. issues EA.
2,000 VARIABLE CONDENSERS, 100 pf., ceramic insulation VARIABLE CONDENSERS, in screening case, 50 pf. EA. 250 TRANSMITTER TANK CONDENSERS, split 250 TRANSMITTER TANK CONDENS
stator, as Illustrated in above issues EA.
1,000 CHARGING OR EARTHING SWITCHES,
30 amp. double pole, as previous issues EA.
1,000 COILS SLEEVING of one gross yards, permanoid
peribraid, systoflex, I mm. and 1.5 mm. PER COIL
5,000 STAND-OFF INSULATORS only miniature
Linch DOZ. 10/-1,000 POTS 100K, { spindle

500 POTS, I meg. EA. I,000 POTS, 3 gang each, 70K EA.
I,000 HUMDINGER POTS, 100 ohm. Miniature wire wound EA. 1,000 POTS COLVERN. 200 ohms 5 watts. wound, N.P. case EA.
1,000 WIRE WOUND POTS, 2,000 ohm 5-watts,

250 100K MINIATURE POTS EA. 10,000 YAXLEY TYPE 1-pole 6-way Switches, complete, less screws, with knobs EA. 1,500 WAVE CHANGE, 2-wafer 6-pole 3-way switches EA.

E. case

10,000 ERIE RESISTORS, 47K, 2-watt, boxed in 50's and 5's. ERIE RESISTORS, 1,200 ohm, ½ watt. Boxed in 50's. Also 33K 2 watt, 150K I watt, 22K I watt 70K I-watt; price 2 watt, 3d.; I watt, 2d.; ½ watt, Id. 800 Wire-wound Vitreous 10-watt wire ends, 500Ω EÅ.

MINIMUM ORDER 5/- ADD EXTRA FOR POSTAGE. **WOOLLEYS RADIO & ELECTRICAL SUPPLIES LTD.** 615, BORDESLY GREEN, BIRMINGHAM, 9. Phone: VIC 2078



I min. Piccadilly ◀---Tube Station.



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FOR ALL RADIO BARGAINS



Square Tube Station



DESK TYPE METERS. Fitted with 0/Imilliamp. first grade moving coll meter, with $2\frac{1}{2}$ in. scale, resistance 100 ohms. Brand new, 25/-.

CRYSTALS. R.C.A. 100 kc/s frequency, 3 pin plug in type. 15/- each.

CRYSTAL DIODES. Wire Ended G.E.C., I/6 each.

METER RECTIFIERS. Full Bridge 2 mA. S.T.C. Brand new, 5/6 each.

MIDGET IS WAY PLUGS AND SOCKETS non reversible, size 2in. x {in., 3/6 pair.

MICRO SWITCHES. Universal Changeover Type, size 2in. x \$in., 2/6 each, many other types available.

AMERICAN (SPRAGUE) CONDENSERS. Wire ended, .1 mfd., .01 mfd., .02 mfd., .05 mfd., .05 mfd., all at 9d, each,

NITROGOL CONDENSERS, 4 mfd. 4,000 volt working, size 9in. x 5in. x 3½in., brand new, 22/6 each. Mansbridge Paper Condensers, 4 mfd. 2,000 volt working, size 5in. x 5in. x 2½in., 7/6 each.



new and boxed. 9/6 each.

MULTI WAY TOGGLE SWITCH BOXES. Fitted with 16Toggle type switches, brand

AMERICAN ROTARY TRANSFORMERS. 12-volt D.C. input, output 255 volt 65 mA, size 4½in. x 2½in. Suitable for car radios or electric shavers. 22/6.

MUIRHEAD PRECISION BUILT KEY SWITCHES with Heavy Contacts. 8 pole 2-way. Brand new, 4/6 each, cost £2/15/- to make. Wonderful bargain.

CERAMIC TRANSMITTER SWITCHES. Extra heavy duty silver contacts, 3in. dia., I pole 6 way, 3 bank, 9/6. I pole 6 way 2 bank, 6/6 each. I pole 4 way I bank, 5/6 each.



H.R.O. 6-VOLT VIBRATOR POWER SUPPLY UNITS. Output 165 volt 80 mA. 6.3 volt @ 3 amps., 6X5 Rectifier, Choke and Condenser amoothed, cablnet size, 7in. x 7in. x

6in. supplied with clips and leads, brand new, 29/6 each.

CHOKES ALL EX-W.D.
20 Henry 120 mA. size 4in. x 3in. x 2½in., 10/6

each. 15 Henry 275 mA. size 4½in. x 4in. x 3in., 125 ohm, 10/6 each.

onm, 10/6 each.
Swinging chokes, 150 mA 4/20 Henry, size 3½in. x 3in., 7/6 each.
20 Henry 300 mA. 2,000 v. Insulation. Will pass 500 mA. 13/6 each.

TELEPHONE HANDSETS, Ex-American, Standard P.O. type, wonderful Instruments, 12/6 each.

R.1155 2-SPEED SLOW MOTION CON-DENSER DRIVES "A" type with double knobs, 3/6 each. MICROAMP METERS. 0/100. 2½in. flush panel mounting, scaled 0/1500 yards, first-grade instruments, brand new and boxed, 42/6 each.

ROTARY CONVERTORS. 12 volt D.C. input or 24 volt D.C. input, output 230 volt A.C., 50 cycle at Ministry rating of 100 watts, 92/6 each.

UNISELECTOR SWITCHES. 4 Bank Double Wipers, coll resistance 25 ohm., 25 position, 32/6 each. Brand new.

HEADPHONES. Brand new, Canadian, "Northern Electric," finest ever produced, 50 ohm coils, complete with P.O. Jack Plug, 10/6 pair.

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and other values, 2-3 wart, 2/- each, IOK Isolated Spindle	2/-	
500 ohms, IK, 20K, 25K, 50K, with spindle	3/-	
VICONTROLS WITH SWITCH: most values, B-NSF	2/6	49
V/CONTROLS: Less Switch, Preset and Spindle. MOST	-/-	.,
VALUES	1/9	
TWIN MIDGET GANGS, .0005, with trimmers, PERSPEX	-1	11
COVER	5/6	
COVER 4-WAY PUSH BUTTON UNITS, I/6 each PUSH BUTTON KNOBS.	15/-	doz
PUSH BUTTON KNOBS	3/-	uoz.
TAG STRIPS: 3-way 2/2 doz : 4 way 2/4 doz : 5 way 3/2 doz :	3/-	10
TAG STRIPS: 3-way 2/- doz.; 4-way 2/6 doz.; 5-way 3/- doz.; 7-way 4/- doz.; 28-way 12/- doz.		
ASSORTED PILOT LAMP HOLDERS	4/-	
ASSORTED PILOT LAMP HOLDERS FUSES 1½ in. Most values from 750 mA. to 10 amp. POINTER KNOBS. Small black, with line, ½in. hole	2/-	0.7
POINTER KNORS Small block wish line line hale	7/6	11
STANDARD ROLLND KNORS, Small Jin hole 4/-	.,0	*1
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WANDER DI LICE Red and Black	2/-	0.3
PHILIPS TRIMMED TOOLS	1/-	11 02.ch
BELLING & LEE, P/M FUSE HOLDERS, Type 1354	2/6	oa Cil
WEARITE COILS: Types PA4 PO4 PA5 PO5 1/3 each	12/-	doz.
VALVE HOLDERS: Moulded ROA 7/A. BTG ALL EESO		
6/-: ENGLISH OCTAL 3/- per doz SCREEN CANS		
for B9A B7G Alador : PAXOLIN B7G MAZDA Apin LIX	3/-	
PHILIPS TRIMMER TOOLS BELLING & LEE. PIM FUSE HOLDERS. Type 1356 WEARITE COILS: Types PA4, PO4, PA5, PO5, 1/3 each VALVE HOLDERS: Moulded. B9A, 7/6; B7G, 6/-; EF50, 6/-; ENGLISH OCTAL, 3/- per doz. SCREEN CANS for B9A, B7G, 6/- doz.; PAXOLIN—B7G, MAZDA 4-pin UX BELLING & LEE. PLUGS AND SOCKETS. Ex-Govt. BRAND NEW 5-pin, Chassis and Cable 7-pin	3/-	9.0
BRAND NEW 5-pin, Chassis and Cable, 7-pin	1/6	pair
BULGIN, P74, Plug and Socket, 2/6; P200, Plug and Socket,	.,5	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
2/-: Rotary Switches, \$ 255, 2/ Dolly Switches \$ 267, 2/		
2/-; Rotary Switches, S.255, 2/-; Dolly Switches, S.267, 2/-; Standard Switches, Ex-Govt., On-off	1/6	each
POST OFFICE LAMP JACKS. No. 10 1/2 each	9/-	doz
Lamp Covers for same	3/-	doz.
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OUTPUT TRANSFORMERS Multi Ratio 5/4+ Pentode	40	
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DRUM DRIVES 41in	1/	
DRUM DRIVES, 41in. WESTECTORS. WX6, WX12, W1, W12, W4, I/- each		
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SIGNAL LAMP HOLDERS P/M, complete with adjusting	10/	
1amp holders, I/9 each	18/-	10
AIR SPACE TRIMMERS. Preset and spindle types, 5PL,	161	
10PF, 15PF, 20PF, 25PF, 50PF, 75PF, 15/-; 100PF Preset, 1/6 each JONES PLUG AND SOCKETS. 4-pin, 2/6; 6-pin, 3/-;	15/-	25
0 min 3/4 10 min 4/ 12 min 4/ 12 min 2/6; 6-pin, 3/-;	7.1	
o-pin, 3/0; 10-pin, 4/-; 12-pin	6/-	pair
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SOLDER TAGS, 2/6 gross. SHAKEPROOF WASHERS	2/-	59 '
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doz., post 2/-.
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The famous ex-Bomber Command Receiver known the world over to be supreme in its class. Covers 5 wave ranges: 18.5-7.5 Mc/s, 7.5-3.0 Mc/s, 1,500-600 kc/s, 500-200 kc/s, 200-75 kc/s, and is easily and simply adapted for normal mains use, full details being supplied. Aerial tested before despatch. BRAND NEW AND UNUSED IN MAKER'S TRANSIT CASES, ONLY £11/19/6.
SLIGHTLY USED RECEIVERS. Grade I, also tested working

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DEDUCT 10/- IF PURCHASING RECEIVER AND POWER PACK TOGETHER.

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An 11-valve receiver, covering 100-124 Mc/s. Has large tuning dial with slow motion drive, R.F. and L.F. gain controls, phone and line output sockets, and 0-5 mA., tuning meter. In grey enamelled metal case with plated handles, size 18in. x 10in. X 11in. Complete with valves, circult diagram and calibration chart. IN BRAND NEW CONDITION IN MAKER'S TRANSIT CASES, ONLY, 79/6 (carriage 7/6). Also a few slightly used at 69/6, plus carriage

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Made for use with the R.1132.A, this is a standard rack mounting job to match the receiver, and is for 200/250 v. 50-cycle mains with outputs of 250 v. D.C. 100 mA., and 6.3 v. 4 amps. Fitted with H.T. current meter and voltmeter, this js a first-class unit, and can be used for a variety of receivers. Used, but tested working before despatch. ONLY 90/- (carriage, etc., 5/-). Connecting Cable with Jones Plugs for receiver and power unit. 10/-. and power unit, 10/-.

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		METERS	
F.S.D.	SIZE	AND TYPE	PRICE
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I ,,	D.C.	25in. Flush circular	
1 ,,	D.C.	21in. Desk type	
5 ,,	D.C.	2in. Flush square	. 7/6
100	D.C.	24in. Flush circular	. 12/6
150 ,,	D.C.	2in. Flush square	7/6
500	D.C.	21 in. Flush circular	
500 ,,	thermo	2in. Flush square	. 5/-
500	thermo	2in. Proj. circular	
20 amps.	D.C.	2in. Proj. circular	
40 amps.	D.C.	2in. Proj. circular	
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15 volts	A.C.	24in. Flush, circ., mov. iron	. 8/6
All meters B	rand N	ew in Maker's Cartons.	

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2½in. circular flush mounting. Widely calibrated scale of 15 divisions marked "yards" which can be rewritten to suit requirements. These movements are almost unobtainable today and being BRAND NEW'IN MAKER'S CARTONS are a snip at ONLY 42/6.

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500 K3/20 5/1 1260 K3/50 8/8 3600 K3/140 19/3 655 K3/25 5/8 1500 K3/60 9/8 4100 K3/160 21/6 755 K3/30 6/- 1780 K3/70 11/- 4660 K3/180 24/3 885 K3/35 6/10 2030 K3/80 12/4 5150 K3/200 26/- 12 V. D.C. at 1 amp., 6/6; 12 v. D.C. at 2 amp., 10/6, 9d. p.p. 12 v. D.C. at 3 amp., 15/-, p.p. 1/-; 12 v. D.C. at 4 amp., 17/6; p.p. 1/2 v. D.C. at 4 amp., 17/6; p.p. 1/2 v. D.C. at 4 amp., 17/6; p.p. 1/2 v. D.C. at 6 amp., 25/-, p.p. 2/-; 12 v. D.C. at 6 amp., 30/-, p.p. 1/2 v. D.C. at 6 amp., 30/-, p.p. 2/-; 24 v. D.C. at 6 amp., 31/-, p.p. 1/-; 24 v. D.C. at 6 amp., 30/-, p.p. 2/-; 24 v. D.C. at 6 amp., 35/-, p.p. 2/- VALVE TESTER, TYPE 4. 200/230 v. A.C. input. Ex-Govt., in good condition, with descriptive book containing circuit diagram of instrument and how to test valves from 1.4 v. to 40 v. With valve-holders for Brit., 4, 5, 7 pin and Octal, U.S., 5 and 7 pin, 1/Octal, side contact, large Brit., 4 and 9 pin. Acorn and diode. Housed in substantial wooden case. Price £7/19/6, carriage 10/- extra.

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VITAVOX PRESSURE UNITS. Heavy duty, P.M. 20 watts. To
fit the above horn. Brand new. £4/9/6, carriage 5/-.
ROTARY CONVERTERS. 12 v. D.C. input 230 v. A.C. output, at
100 watts. Brand new. £4/17/6. Ditto, 24 v., same price, carriage 7/6.
AN/APA-I CATHODE RAY INDICATOR AMPLIFIER UNIT.
Complete, comprising OF. 3BPI C.R.T., 7-65N7GT, 1-6H6, 1-6G6,
1-2X2, 1-6X5, valves. Bargain value, £4/19/6, plus 10/- carriage.
TUNING UNITS (EX-US.A.). Types available, T.U.5B., T.U.6B.,
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AC/DC SUPPLY UNIT. (S.T.C. SELENIUM RECTIFIER). Complete
with Mains Isolation transformer, fixed and housed in strong metal
cabinet. 250 v. A.C. to 200-220 v. D.C. @ 3-4 amps. Ready to use for
£6/10/10 only, carriage 10/-.

watts for 6L6 valves. To match, 3, 8 and 15 ohms. New and unused.

29/6, p.p. 2/6.
R.1155 COMMUNICATION RECEIVERS. Individually tested and despatched in good working order. Cases slightly soiled. £8/19/6,

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HOOVER I/6th H.P. MOTORS, 400/440 v. Three-phase, Standard shaft, 1,425 r.p.m. Brand new in original maker's cartons. £3/10/-,

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HALF MILE OF TWIN DON "8" TELEPHONE WIRE.
Brand new, on wooden drums, £2/12/6 per drum, carriage 10/-, England

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HIGH-VOLTAGE TRANSMITTING CONDENSERS. Hank

Pot Type (25 pf. 8 kV) (400 pf. 9.6 kV.) (500 pf. 15 kV.) (600 pf. 9.6 kV.)

(750 pf. 15 kV.). Any type, 3/6 each, p.p. 1/-.

CHROMIUM PLATED EXTENDIBLE AERIALS. Min. length

12in. Max. length 46in. Suitable for car radio aerials. 8/6 each, p.p. 9d.

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Type 3BPI, new and unused, with base and screen, 42/6, p.p. 2/-.

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Type CV 1526, 2½in., 4 v. filament, 3,000 v. anode, complete with base and mu-metal screen, 20/-, p.p. 2/6.
PHOTO ELECTRIC MULTIPLIER CELLS. TYPE 93IA. £2/10/-,

PHOTO ELECTRIC MULTIPLIER CELLS. TYPE 931A. £2/10/-, p.p. |/-. Also 931A complete on chassis with multiplier network and two 832 valve-holders, etc., £3/10/-, p.p. 2/-.
POWER UNITS. Type 3, made for use with the R.1132A, this is a standard rack mounting job to match the receiver and is for 200/250 v. 50 cycle mains with output of 250 v. D.C., 100 mA. at 6.3 v. 4 amps. £3/10/-, carriage. Power unit for Wireless No. 11, 12 v. D.C. input, 230 v. D.C. output at 30 mA., fully smoothed, 19/6, 2/6 p.p. Power unit ex-No. 19 Trans-receiver, 12 v. D.C. Input, 275 D.C. output at 100 mA., fully smoothed, 19/6, p.p. 4/-.
NO, 38 WALKIE-TALKIE TRANS-RECEIVER, in good condition (less external accessories), 35/-, p.p. 2/6.

(less external accessories), 35/-, p.p. 2/6, SIEMENS HIGH SPEED RELAYS. Twin 1,000 ohm coils, perfect

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MOVING COIL HEADPHONES. Brand new. 12/6 per pair, p.p. 1/BATTERIES H.T./L.T. Heavy duty layer type. 150v. tapped at
87v. H.T. L.T. 4½v. Perfect condition. Size 9½in. x 4½in. x 4½in. 4/6, p.p. 2/6,

15 LITTLE NEWPORT ST., LONDON, W.C.2.

BC.453 COMMAND RECEIVERS, new, with dynamotor, £5/5/-, RHEOSTATS. 12 v. 1A 2/6. 12 v. 5A 9/6.
MORSE KEYS. Bakelite fully enclosed, 3/6,
BENDIX SELSYN TRANSMITTER MOTORS, TYPE VIII.
A.C. 50 v. 50 cycle, 4ln. x 3½in. new. 27/6,
NEW FREQUENCY CRYSTALS. 9100 and 4500 kc., 10/6.
480-4800-2400-594-561-560H559 Kc. 6/6. ½in. space pins.
SETS OF 6. CARBON TWIST DRILLS. ½in. to ½in. or ½in.

SETS OF 6. CARDOL.

to 12 in. 3/6 set.

ARP12/YP23 VALVES, new, 4 for £1, 5/6 each.

PLESSEY T.V. PRE-AMPLIFIER. London band. Valve 6F13.

Complete, 25/6. VALVES. Lists supplied. CYLDON 5-CHANNEL PRE-TUNER. Gives 26 D.B. gain. Fit one of these to your T.V. for better pictures. I.F. Output 9.5-14 Mc/s., 15-22 Mc/s. With valves EF80, ECC81, 52/6. Less valves, 15/-NEW 0-100 MICRO-AMP. METERS. 4½in. Round flush mounting. Made by Ernest Turners. £3/12/6. MAINS TRANSFORMERS. Input 200/240 v. Output 350-0-350 or 250-0-250 volt 80 mA, and 4 and 6.3 v. 4 a. and 4 and 5 v. 2 a. Price 21/6. Input 200/240 v. Output tapped 3, 4, 5, 6, 8, 9, 10, 12, 15, 18, 20, 24, 30 volts, 2 amp., 21/6. Output 17-11-5 volts 5 amp., 22/6. Output 17-11-5 volts 1½ amp., 16/6. 6.3 v. 2½ a., 8/6. All with one vear's guarantee.

one year's guarantee. D.P.D.T. RELAYS. Operate at 200/300 volts D.C. 8/6. We can

supply any type of voltage and contacts at varying prices.

NEW SELENIUM RECTIFIERS. F.W. 12/6 volt 3 amps., 14/6; 4 amp., 22/6; 6 amp., 30/-; 1 amp., 8/6; 12 v. 100 mA., 3/-; 24 v. 2 amp., 30/-; H.W., 250 v. 100 mA., 9/-; 250 v. 275 mA., 17/6; 250 v.

GERMANIUM or SILICON CRYSTAL DIODES, 3/9.
M/C MICROPHONES with matched Trans., 15/6.
FL5 FILTER UNITS, 8/6. Same as FL8 but less switch.
TRI196 TRANSMITTER SECTION. New and complete but less valves. 4.6-6.8 Mc/s. Easily converted, 15/-. With valves TTII, EL32, EF50, £2.

All Carriage paid in the U.K. from Dept. W.W.

AR88LF in tip-top condition, £55.
U.S. ARMY FIELD TELEPHONES. TYPE EE8, £5/10/- each.
Carriage extra on above items.

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1070 Harrow Road, London, N.W.10

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College general-purpose units. MODEL
ACIOE, 4 valve 10 valts. Neg. feetback. \$210/7/6. MODEL A.015E.
6 valve, 11-16 vatt. Pf. portput. Reckback over 3 stages, \$14/14/4. MODEL,
ACIZE, 32 vatte Pf. poutput. Feedback over 3 stages, \$14/14/4. MODEL,
ACIZE, 32 vatte Pf. poutput. Feedback over 3 stages, \$19/15/-. MODEL,
ACIZE, 32 vatte Pf. poutput. Feedback over 3 stages, \$19/15/-. MODEL,
ACIZE, 32 vatte Pf. poutput. Feedback over 3 stages, \$19/15/-. MODEL,
ACIZE, 32 vatte Pf. poutput. Feedback over 3 stages, \$19/15/-. MODEL,
ACIZE, 32 vatte Pf. poutput. Feedvolume, and D.C./JAC. unine, 6 valve,
Pf. portput. Feedvalve, Pf. poutput of 9 vatts. This amplifier incorporates and 18 exciton OfTransformer. Variable feed-back from zero to 25 db. Output impedance
36 to 239 ohms. Complete chassis, \$2/14/14/-. Complete range of accessories available,
also tape recorders, amplifiers, etc. Stamp for list. All amplifiers ready for use and
carriage paid. Terms available.

20 WATT AMPLIFIER FOR 50/-

20 WATT AMPLIFIER FOR 50/-, less valves. Front panel 19in, wide for rack mounting 19in. deep. This unit is divided into 2 sections, the top section containing the amplifier and consisting of output transformers, valve-holders, etc., tone control, valve line-up 2 PX 25's, MBIL4 and a U14. Contains also a 3in. 0-200 milliamp meter, complete with input and loudspeaker sockets. The bottom portion contains the power supply unit for 200-250 v. mains and consists of mains transformer 500-0-500, 120 milliamp 3-4 volt heater windings, smoothing choke, condensers, variable resistances, etc., also power output for providing HT. and heater voltages for a pre-amplifier. Indicator light and on and off switch. Sold less valves, believed to be in working condition at our NEW PRICE of 22:10/-, carriage 15/6. The weight of this amplifier is approximately 50 ib.
AERIAL COUPLING UNIT. Type G. Ref. ZA.0843. Containing large inductances, variable transmitter type condensers, 0-1 ma., M.O. meter 2in. dis., indicator light, etc., with controls brought out to front panel 15 x 11in. Contained in metal bor 15 x 11 x 15in. deep with 24in. hinged lid, complete with circuit. In new condition, apart from external scratches to case. Price 27/6, carriage 6/6.
WIRE WOUND POTS. 10,000 ohms, 4in. dia., 34in. deep with wiper arm and 8in. spindle, new condition, diamantled form units, price 8/6, postage 1/c.
UNISELECTORS. Slemens ministure 3 banks of 10 contacts. 3 sets of wipers etc. 1276 degrees. Coil resistance 10 ohms. Stripped from new equipment. Price 27/6, postage 1/6.

set at 120 degrees. 27/6, postage 1/6.

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Novem	BER,	1954		
18 8.W.G. 20 8.W.G. 22 8.W.G. 24 8.W.G.				2/- 2/2 2/4
ENAMELLE 4 oz. Reels. 8.W.G. 16 18 20 22 24 26 28	Price 1/11 2/1 2/3 2/5 2/7	8.W.6 30 32 34 36	WIRI	Price 3/1 3/3 3/5 3/7 3/11
Aluminium Corners. A 6in. × 4in. > 8in. × 6in. > 10in. × 7in. >	Undrill tvailabl eiz (2)in.	e In the	he foll	lowing

6in. × 4in. × 2in 4/6 ea.
8in. x 6in. x 2 in 6/3 ea.
10in. × 7in. × 2 in 7/3 ea.
12in. × 8in. × 2 in 8/6 ca.
14in. × 8in. × 24in 9/6 ca.
16in. x 9in. x 2iin 12/- ea.
All are four sided-ideal for radio
receivers amplifiers power packs, etc.
SET OF VALVES. Ten VR91 (EF50)
valves. Ex-Brand new units, 6/- each,
45/- set.

GRAMOPHONE MOTORS, etc. Collaro AC37 Gramophone motor suitable for 100/120 v. 200/250 v. A.C. variable speed, complete with 10in. E.M.I. type urntable feit covered. Price, 46/- each

GOLDRING PICK-UP HEADS. Plok-up head type No. 112 (2,000 ohms.), complete with lead. Price 17/6 cach.

AMPLIFIER

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COMPARE THIS PRICE!

This is not a kit of parts but a well-built unit—read this specification.

- * 3 valves-6B8G, 6X5GT, 6V6GT. ★ Components 100%, only recently manufactured condensers used.
- * Strong chassis, sockets for all input and output leads.
- * Output 30 secondary.
- * Tone and volume controls.
- * Input for crystal or Hi-Fi magnetic
- * A.C. mains fully isolated.
- * Negative feed back.
 Price 79/6. Packing & Post 2/6.

JUNCTION BOXES
Type 5X/2234 20 Way..... 1/6 ea. PUSH BACK WIRE
Size 7/412. Available in
colours: Blue, Green, Red 24d. yd.

NYLON BRAIDED DRIVE CORD 25 yd. Reels 2/9 ea AMERICAN RELAY 45Ω Impedance with leads No. AZ0545 1/9 ea.

IRON LEADS Black and white flat iron leads, bonded ends 1/3 ea. POTENTIOMETER PANEL

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Potentiometers on Panel.
50ΚΩ SPS; 750Ω W.W;
25ΚΩ Carbon; 5ΚΩ W.W.
All with long spindle, with
leads of different colours
terminating in an 11 pin
plug surplus to leading T.V.
Makers Production Run



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SPECIAL PURPOSE VALVES VR53 6/6 CV286

					4.5		
	200	40.0		VR56	6/	VR54 2/-	
X2	5/-	VR150/30	9/	VR65A	3/6	VR57 8/	
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/R91	61-	CV173	10/-	955	4/9	TOLL LIST	

ION TRAPS

Type IT6 for Tubes with 35 mm. neck diameter 2/6 ea;

HEADPHONES-MICROPHONES, Etc. EX-GOVERNMENT HEADPHONES BY S. G. BROWN, etc.

CLR Low resistance type 120 ohms 7/6 pr. CHR High resistance type 4,000 ohms ... 11/- pr. 13/6 pr. DHR a super phone
American phones by Trimm Mfg. Co. of
Chicago, U.S.A., 1,200 ohms. each 1/9 ea. Throat microphones, American surplus.
Complete with strap, lead and plug type T308 4/- set
"Regent" Hand Microphone. Crystal insert, nickel chrome plated head, complete with lead and Jack plug, listed at 2 Gns. Our price 21/- ea.
Throat Microphones, type Za.21095.
2 units per box 1/8 per box
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HEATER TRANSFORMERS

30 v. Input 2 vo	olt .5 amp.		4/6
30 v. Input 2 vo	It 3.0 amp.	*********	7/9
130 v. Input 4 vo	olt 1.5 amp.		5/-
	olt 3.0 amp.		10/
230 v. Input 5 vo	olt 2.0 amp.		10/
230 v. Input 6.3 vo	olt .5 amp.		5/-
130 v. Input 6.3 vo	olt 1.5 amp.	*********	6/-
130 v. Input 6.3 vc			9/
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OUTPUT TRANSFORMERS

Multi Ratio suitable for all ordinary receivers giving six single ratios....... 6/6 ea.

CONTROL KNOBS in MODERN STYLING

Tastefully and clearly engraved in gold.
Size A. Diameter I in. Depth in.
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These Mouldings are available in two colours: Walnut and Ivory

They are suitable for use with \$\frac{1}{2}\ln spindles, and are simply and firmly held by means of a grub screw and locking nut.

Prices:
Type "A "-1/6 each.
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Type "B"—1/2 each.
Plain Knobs can be supplied in either size or colour: Price 1/- each and 8d. each respectively. Inscriptions available:—
RADIO: "Volume," "Vol/On-Off," "Wavechange," "Tuning," "S.M.L. Gram.," "Radio-Gram.," "Tone," "On-Off," TELEVISION: "Contrast," "Brilliance," "Brilliance," "Brilliance," "Focus," "Brightness." AMPLIFIER: "Treble," "Bass," (plus any of those shown above). TAPE RECORDER: "Record-Play."

ANOTHER LARGE PURCHASE OF COMPACT TELEVISION AERIALS BY ANTIFERENCE LTD.

Supplied complete with universal mounting and backplate in neutral brown finish. Overall length 5ft. 6in. Packed in carton 3ft. 4in. long. Complete with full instructions. Cat. No. CD4. Original price 50/-. Our 12/6 price

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This well-known cabinet of which thousands have been sold is ideal for every constructer. Complete with chassis, dial, backplate, cord drive, pointer and dial drum. Price 27/6 each.

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20H, 250Ω, 60 mA. Clamp	
construction 6/- ea. 10H, 200Q, 90 mA. Clamp	١,
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CHARGERS

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This attractive wainut finished cabinct is available for 6½n. or 8in. speaker units. Metal speaker fret, complete with back and rubber feet. 6½in. type: Measures 8½in. × 8½in. × 4½in. at base. Price 15/6 each.

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WIRE WOUND RESISTORS
Available in the following values:—
250, 500, 1000, 1500, 2000, 2500,
2500, 500, 10000, 15000, 20001,
25001, 35000, 50000, 68000, 1500000
Tolerance +-10%.
Ratings 5 watt, 1/s each. 10 watt
1/3 each. 15 watt 1/9 each.
1/3 each. 15 watt 1/9 each.
1/4 each. 200/250 v. Secondary 6.3 volt
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1/4 each. 200/250 v.

1/- each.
PENTODE OUTPUT TRANSFORMER.

1/- each.
PENTODE OUTPUT TRANSFORMER.
2/9 each.
MAINS DROPPERS
Dubliler type HY 71228 1350 Ω with
5 taps 2/6 each.
945Ω Dropper with 5 taps 2/6 each.
Vibrator Clips 4d. each.
Nitrogol Condensers, 12 mfd. 350 v.
Dropper with 5 taps 2/6 each.
Nitrogol Condensers, 12-mfd. 350 v.
Dr.C., 5/- each.
Etched Foil Electrolytic Condenser,
10 mfd. 4/ v. 4/- each.
By 10 mfd. 4/ v. 4/- each.
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By 10 mfd. 1/- each.
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By 10 mfd. 1/- each.
By 10 mfd. 250 v.
By 10 mfd. 250



R. & A. 10° unit21/6 ea. PENCIL RECTIFIERS

THE LATEST ELAC 4in. × 7in. ELIPTICAL UNIT 19/10 each.

ELAC 10in. Units 2 to 3 ohms 22/6

PLESSEY 10in. Lightweight. 19/6 TRUVOX BX11 12in. Light-

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ELAC 4in. Square type 4/03, 2 to 3 ohm

LECTRONA 6 in., With trans-ELAC 6in. Type 6/19, 2 to TRUVOX 6in. Water type, 1in. deep, 2 to 3 ohm 20/-1 jin. deep, 2 to 3 oma..... B. & A. 8in. Lightweight, 2 to 16/11 LECTRONA 8in. PM 2 to 3 ohms

K3/25, 5/8; K3/40, 7/6; K3/45, 8/2; K3/50, 8/8; K3/60, 9/8; K3/100, 14/8

SENTERCEL RECTIFIERS

RM1, 3/9 ea.; RM2, 4/2 ea.; RM3, 5/- ea.; RM4, 16/- ea.

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12 v. 1 amp., 1/6 ea.; 12 v. 1 amp. 4/6 ea.; 2 v. 1 amp., 3/- ea.; 250 v. 45 mA., 6/3 ea.; 250 v. 75 mA., 7/6 ea.; 300 v. 60 mA., 7/6 ea.

FULL WAVE TYPES

12 v. 1 amp., 4/9 ea.; 12 v. 2 amp., 8/- ea.; 12 v. 3 amp., 13/- ea.; 12 v. 5 amp., 18/- ea.

SPECIAL OFFER

Co-axial Cable

Best quality grade "A" cable solid
1/022 70 chms, 7½d, yd. Best quality
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FUSES

1, 1, 1, 2, 3, 5 amp. 11in. Standard Cartridge Fuses 3d. ea. Panel Mounting Press Switch 1/3 ea.

"SATCHWELL" THERMOSTAT

Complete with mounting bracket and including 2 space heating units 230 v. 35/- set

CARRYING CASE

TERMS: Cash with order or C.O.D. Postage and Packing charges extra, as follows: Orders value 10/- add 9d.; 20/- add 1/-; 40/- add 1/6; £5 add 2/unless otherwise stated. Minimum C.O.D. fee and postage 2/3.

MAIL ORDER ONLY

CHAMBERS, VICTORIA SQUARE, · LEEDS

WHEN ORDERING PLEASE QUOTE "DEPT. W.W."

BENSON'S'

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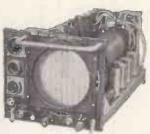
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[3539]

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Immediately. [3504]
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[3466

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[3557]
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Bridge Rd., London, S.E.I. Wat. 6944. [3585]

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RADUATES with an honours degree in physics or in electrical engineering are required by the British Thomson-Houston Co., Ltd., Rugby, for research in the field of high-power ultra high-frequency valves; applicants should write to the Director of Research giving their age, qualifications and college, quoting reference DR. [3529

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N.15. Sta. 7861-2. [3178]

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ENGINEERS required for maintenance and design of electronic test equipment, quality control and investigational work on thermionic valves; Inter B.Sc. or Higher National Certificate standard; apply giving full particulars of age, qualifications and experience to—Personnel Superintendent, The Edison Swan Electric Co., Ltd., Cosmos Works, Brimsdown, Enfield, Middlesex. [5480]

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dish Lane, Manchester, 16.

An opportunity occurs in progressive manufacturing concern in London area for engineer, aged 25/35, with electrical or physicist degree, on development and research work on high frequency telecommunication cable and associated testing equipment; salary will be commensurate with qualifications and experience.—Apply giving full particulars to Box 7677.
[3456]

ENGINEERS required for maintenance and design of electronic test equipment, quality control and investigational work on thermionic valves; Inter. B.Sc., or Higher National Certificate standard.—Apply, giving full particulars of age, qualifications and experience to Personnel Superintendent, The Edison Swan Electric Co., Ltd., Cosmos Works, Brimsdown, Enfield, Middlesex. [3628]

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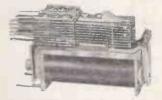
ELECTRICAL Engineer with University degree or equivalent qualification, required for development work on rubber and plastic insulated cables, with particular emphasis on telecommunications and radio frequency applications; experience in cable manufacture desirable but not essential; salary in accordance with experience and qualifications.—Apply to the Secretary, W. T. Glover & Co., Ltd., Trafford Park, Manchester.

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[5651]

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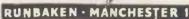
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Lavender Hill, S.W.11. [3548]

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15, Hill St., London, W.1.

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SENIOR engineer required for long term basic development of new types of radio communication equipment; attractive position for engineer of degree standard with interest in radio circuitry and components; the position is permanent and will carry a salary commensurate with the applicant's knowledge and experience; location in South London.—Apply in writing, stating age, education and salary required, to Box 8010.

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Hatfield Rd., St. Albans. [3463]

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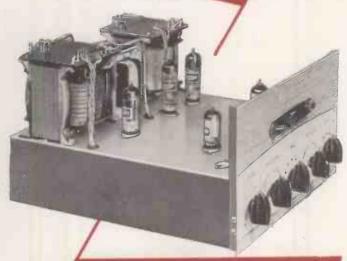
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