TWO SHILLINGS

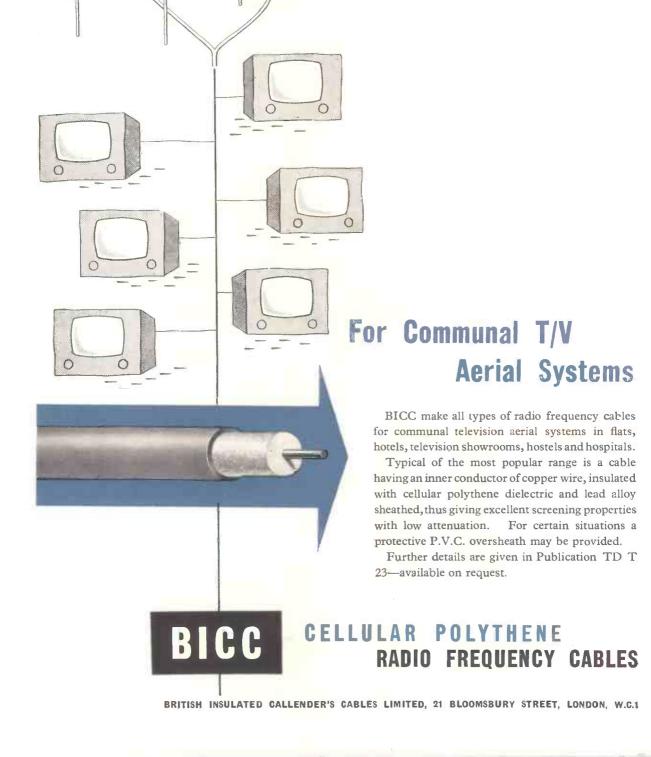
JANUARY 1957

Wireless World

ELECTRONICS Radio · **Television**



FORTY-SIXTH YEAR OF PUBLICATION



Wireless World

ELECTRONICS, RADIO, TELEVISION

Managing Editor: HUGH S. POCOCK, M.I.E.E.

Editor:

H. F. SMITH

Assistant Editor: F. L. DEVEREUX, B.Sc.

JANUARY 1957

In This Issue

- 1 Editorial Comment
- 2 Single Beam Colour Tube
- 4 World of Wireless
- 8 Limiters and Discriminators for F.M. Receivers. G. G. Johnstone
- 15 Portable Transistor Superhet. W. Woods-Hill
- 18 Resistance-Current-Voltage-Power Nomogram. B. E. Jackson
- 20 Is Radio Propagation Always Two-way? T. W. Bennington
- 22 Books Received
- 23 The Gated-Beam Valve. Lawrence W. Johnson
- VOLUME 63 No. 1
- Modernizing T.R.F. Television Receivers. P. F. Cundy
- PRICE: TWO SHILLINGS
- Short-wave Conditions 28
- FORTY-SIXTH YEAR
- Letters to the Editor 29
- 31 High-Quality Sound Broadcasting. G. H. Russell
- OF PUBLICATION
- Cascode Characteristics. W. Grant
- Editorial, Advertising and
- 36 Fish-Finding Asdic
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MULLARD COMPONENTS

Mullard pot cores and other Ferrox-

cube components, air-space trimmers,

Varite thermistors etc. are now avail-

able in small quantities for experi-

menters. For information regarding

the nearest source of supply please

enquire of Mullard Valve Sales Dept.

at the address below.

All resistors should be ± 5%

K

200mW Transistor



amplifier operated from a 6V supply

In a previous advertisement (June 1956) details were given of an audio amplifier using transistors, which derived its power from a nominal 4.5 volt battery. In portable equipment such as record reproducers, it is convenient to operate the amplifier from the same supply as the turntable motor, and since most portable motors operate from a 6 volt battery, the 200mW amplifier circuit has been adapted for use with this higher voltage.

The 4.5 volt and 6 volt versions are very similar in performance, except for the greater sensitivity of the latter. Both

are capable of an output of just over 200mW with 10% total harmonic distortion. In the 6V amplifier, the gain at 8kc/s and 50c/s falls 3dB below level response at 1kc/s.

The sensitivity of the 6V version is slightly higher than that of the original in spite of a higher series input resistance of $330k\Omega$. This can be attributed to the higher supply voltage. Since the output stage requires a lower driving current, and a higher voltage is available for the driver, a higher turns ratio can be used for the interstage transformer T1 and thus the stage to stage gain can be increased. The

basic sensitivity across the low impedance terminals YY is 3mV, compared with 6mV in the original, and across the high impedance terminals XX it is 400mV compared with 500mV.

The circuit and component values given in the accompanying diagram. Alternative high or low impedance inputs for crystal pickups or radio tuner are available at XX and YY respectively. The and driver stages (each using an OC71) are R-C coupled. and the driver stage is transformercoupled to the output stage which is a Class B push-pull arrangement of two OC72's

(sold in matched pairs as Mullard type 2-OC72).

Interstage Transformer

The turns ratio of the interstage transformer, T1, which is rated at 2mW, is $3.5:1\!+\!1$. The inductance of the primary should be 10H with a current of 15.mA d.c. flowing, and its d.c. resistance should be less than 200Ω . The resistance of each half of the secondary should be kept below 50Ω and the leakage inductance should be as low as possible. The d.c. currents in the secondary windings are balanced.

Output Transformer

The output stage is matched to the load by a push-pull transformer, T2, rated at 250mW. For a 3 Ω load the turns ratio is 4.9+4.9:1, for a 5 Ω load, 3.8+3.8:1, and for a 15 Ω load, 2.2+2.2:1. Each half primary should be capable of handling peak currents of 83mA.

The currents in each half of the primary will only be balanced if the transistors in the output stage are perfectly matched. At large-signal currents it is possible for the OC72's to be mismatched by as much as 35%, consequently the output

transformer should be constructed to allow for unbalanced currents.

The d.o. resistance of each half of the primary winding of T2 should be less than 3Ω and the total inductance should be greater than 0.5H.

The dynamic load for each collector of the push-pull stage should be 720. The d.c. resistance of the secondary winding should be less than 5% of the load resistance and the leakage inductance should be low.

The turns ratio of the output transformer, and the value of

the feedback resistor R13 for various loudspeaker impedances are shown in the top left hand corner of the diagram. The loudspeaker impedance must be quoted when the output transformer is ordered from the manufacturer.

Stabilisation

RI3 #

-K

Potential dividers R3, R4 and R7, R8 and emitter resistors R6 and R9 provide stabilised d.c. bias for the input and driver stages.

The effects of changes in the temperature of the surroundings, production spreads in the transistors, and deterioration of the

supply battery on the performance have been minimised by careful choice of the value of R11. The optimum value is $8.2k\Omega$, giving satisfactory performance under the conditions

likely to be encountered. Slightly lower distortion can be obtained by presetting the value of R11 to give quiescent curents of 0.5mA for each transistor at 20°C. The amplifier can be used safely in ambient temperatures as high as 45°C.

Negative feedback from the secondary of the output transformer is applied to the collector of the first OCTI by R13, whose value must be

whose value must be chosen to match the loudspeaker load, as shown in the table.

[3407]

Filter Components

An increase in battery impedance causes undesired feedback through the supply to the earlier stages and it results in considerable distortion in the output. This unwanted feedback is prevented by the filter network C4-R10.

Performance

Output Power

215mW at 10% total harmonic distortion

Frequency Response

Gain, at 50c/s and 8kc/s, is reduced 3dB below the response level at 1kc/s

Sensitivity (with nominal transistors)

3.0mV at the low impedance terminals YY 400mV at the high impedance terminals XX

Current Drain

5 to 6mA at zero signal

15mA with average music

75mA at maximum output with sine wave drive



INFORMATION THEORY AND BROADCASTING

Broadcasting techniques are now pretty well established, both on the engineering and programme sides. But, all the same, it might be a worth-while New Year's resolution for broadcasters to decide upon a re-examination of these techniques in the light of information theory. That theory, it will be remembered, did not originally concern itself with the *meaning* of the message or symbols transmitted. Of recent years, however, there has been a growing tendency to widen the scope of the theory, even to the extent of trying to fit the human mind into its place as a link of calculable capacity in a chain of communication.

There is already quite a formidable and highly esoteric literature on this widened aspect of information theory. "Formidable" seems to be a singularly appropriate word in this context; any attempt directly to apply the principles enunciated to say, the improvement of broadcast programme techniques, leads us into deep and turgid waters. But

even an unsuccessful attempt may bring up useful ideas.

For instance, the rate at which the human mind can assimilate information is always strictly limited, though it varies with the individual. This truism is brought out in an easily digestible form (though it must be admitted with no reference to information theory) in Professor Kapp's book* on technical writing. All the author's principles are applicable to some extent to the presentation of any kind of factual information (as opposed to imaginative writing or speaking) whether by the written or spoken word. The information in many broadcast talks seems to us to be presented at a rate that is far too high for the medium of communication. Some of them, indeed, can hardly be assimilated at a first reading when they are reprinted in *The Listener*, except perhaps by specialists.

What appears to be another fundamental misuse of broadcasting, considered purely as a means of communication, is the employment of it for disseminating information of purely local interest. Surely that is a function that can be much better carried out by local newspapers. The inhabitant of, say, a small town is almost certain to waste a vast amount of time in waiting for news of happenings in his own little community—if it ever comes. And, taking the South-Eastern broadcasting region of England, what common denominator of local interest can be found to link a London suburb, a New Town, a cathedral city

and a secluded village?

This technically indefensible use of the radio medium for parish pump broadcasting, though representing an error of principle, is not highly significant in volume. On the wider issue, much of the philosophy behind the concept of regional programmes, to which the B.B.C. has long been devoted, seems to be based on an almost equally serious misconception of the proper use of the radio medium. For a small country like England, surely radio is essentially adapted to distributing material of nation-wide interest. For example, a high proportion of listeners served on medium waves by the West Region must feel a much closer affinity with London than with the robust and rural West Country.

JANUARY 1957

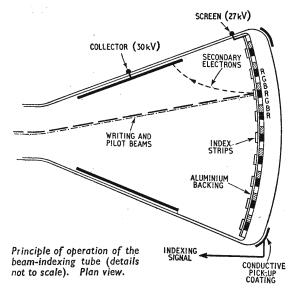
Vol. 63 No. 1

^{* &}quot;The Presentation of Technical Writing" by R. O. Kapp. Constable.

Single-beam Colour Tube

NE of the main brakes on the development of colour television at present is the absence of a really cheap and simple colour display device that will make possible a low-cost receiver. It is doubtful whether the well-known three-gun shadow-mask tube is the best basis for this. Not only do three guns add to the expense of manufacture but they bring with them all the problems of registration (which are by no means solved in existing designs) and necessitate two extra wideband video cutput stages capable of providing about 100 volts swing and a stable black level.

Fundamentally, what is required is a single electron gun controlled by a brightness signal, and a screen



consisting of a mosaic of differently coloured phosphor dots or strips, with some mechanism which ensures that the spot excites only appropriately coloured dots or strips depending on the colour

The Chromatron, or Lawrence tube, is one device

that goes some way towards the ideal (see July, 1953, issue, p. 329). Another, more recent, design is a single-beam tube developed by Philco in America which has hitherto been known by the code name "Apple." In this, as shown by the figure, the screen comprises a pattern of vertical phosphor strips arranged in the cyclic order R G B R G B, etc. There is no internal structure comparable with the shadow-mask in the three-gun tube or the colourcontrolling grid in the Chromatron, but on the inside face of the aluminium film backing the phosphor strips there are strips of magnesium oxide which register with a particular one of the phosphor strips.

The principle of operation here is that the incoming colour information is switched to modulate the tube according to the position of the beam. In other words, when the beam is passing across the red phosphor strip the red signal is switched to the electron gun, when the beam is on the green strip the green signal is switched on, and similarly with the blue

In order to do this, some means must be incorporated for continuously giving information on the position of the beam across the screen. This is achieved by means of a "pilot" beam (travelling parallel with the normal "writing" beam) in conjunction with the magnesium oxide strips on the screen. Magnesium oxide has a higher secondary emission coefficient than the screen's aluminium backing, so that when the pilot beam crosses the strips it produces a greater secondary emission current than from the aluminium between, and a regular pulsation is obtained. The secondary electrons are picked up by the conical collector electrode, which is at 30kV relative to the screen's 27kV.

The pulsation of secondary emission current generates a signal at the screen, which is taken off capacitively by an external conductive coating. This waveform is known as an "indexing" signal and is combined with the colour signal to gate the writing beam at appropriate moments to produce the desired colours.

In the absence of the colour signal the "Apple" tube produces a good black-and-white picture, simply because the writing beam energizes all the phosphors equally as it passes over them in rapid succession. No critical adjustments are required as in the three-gun tube, where the three separate beams must be correctly aligned and matched to give satisfactory colour-and monochrome-reproduction.

Tubes of this kind are known generally as "beam indexing" tubes. The main advantage claimed for the Philco version is that the task of maintaining tight tolerances is relegated to the manufacturing equipment rather than to the tube itself, where it would have to be faced every time a tube is made. Another important point is that no high-voltage power is wasted through interception or deflection of the beam by an electrode structure near the screen. Technicians in this country have, however, complained of a pattern of vertical dark lines on the picture which results from the screen construction. Full details of the tube have been published in the September, 1956, issue of Proc. I.R.E.

Tubeless Colour Television?

LOOKING forward beyond the single-beam tube and the flat tube (described last month), many people believe that the ultimate colour display will be a "picture-on-the-wall" device utilizing some solid-state phenomenon such as electro-luminescence. This method of producing light from phosphors by directly applied potentials* is now being actively investigated, mainly for lighting purposes and image intensification, but there is no doubt that the research workers have their eyes wide open for possible applications in television.

The problem of constructing such an electro-luminescent colour display was raised by a speaker at a recent Brit. I.R.E. lecture on the light amplifier given by Dr. T. B. Tomlinson of G.E.C. It has been discovered that

the light emitted from the phosphor can be made to change colour with different frequencies of a.c. excitachange colour with different frequencies, of a.c. excitation, and the speaker suggested that this effect might be exploited in some way. In reply Dr. Tomlinson said that the change with frequency could only be accomplished between green and blue, and in practice the method was only suitable for producing an overall colour change in complete sheets of phosphor.

He felt that a more likely solution would be a moscie.

He felt that a more likely solution would be a mosaic type of screen made up of phosphor dots of different electro-luminescent materials, with some arrangement for activating the dots separately in synchronism with the scanning process. A method which has already been suggested involves a matrix consisting of horizontal wires on one side of the screen and vertical wires on the other. Each phosphor dot is placed at the intersection point of an x wire and a y wire and, in theory, can be activated separately by applying the appropriate voltage to these electrodes. Apart from the elaborate and highspeed switching system required for scanning the matrix, one of the major difficulties, as Dr. Tomlinson pointed out, would be the inevitable stray cross-coupling between the electrodes.

Earlier, the lecturer had demonstrated electroluminescent panels of different compositions giving blue, green and orange lights. A good red, he said, was very difficult to obtain chemically. Other problems to be overcome were the low light efficiency and slow response time of the phosphors to activation, but the efficiency in particular was being steadily improved.

In discussing the light amplifier itself, Dr. Tomlinson thought that it might possibly be incorporated in the screens of conventional television cathode-ray tubes. This would make possible lower velocity electron beams and hence lower e.h.t. voltages and reduced scanning power. However, one speaker who had seen an American light amplifier in operation said that, although the amplification and picture quality were both good, there was a considerable time lag in response which would be a disadvantage on moving television images.

* See April, 1955, issue, p. 153.

Drilled-Ferrite Switching Circuit

AN unusual form of construction for two-state switching and computing circuits recently developed at the Radar Research Establishment consists of a block of ferrite with small holes drilled in it, with transistors mounted on top so that their leads pass directly through the holes. This has arisen from the need for switching circuits which are small, reliable and economical in operation.

The idea of using small, square hysteresis-loop ferrite cores, with transistors to drive them from one state of remanent induction to the other, is becoming quite a well-known technique. Unfortunately it brings difficulties in manufacture in that the tiny cores-which are only 2mm across—require a great many turns of fine wire to produce the necessary switching m.m.f. from the small transistor driving currents.

The desirable simplification is a one-turn winding, but to attain this it would be necessary to have a core shaped like a thin-walled tube which would be capable of being switched by a low m.m.f. In the absence of

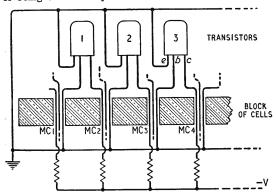


Fig. 1. Construction of transistor magnetic-cell two-state elements arranged as a shift register.

such cores on the market, the nearest practical altermative that can be switched by low currents is the "magnetic cell" or narrow hole drilled in a block of ferrite. This principle was described by D. S. Ridler and R. Grimmond at the recent I.E.E. Ferrites Convention (see December, 1956, issue, p.596), and the R.R.E. device was actually disclosed by G. H. Perry in a discussion following the paper.

Fig. 1 shows diagrammatically the construction of a

group of the transistor/magnetic-cell two-state elements

arranged as a shift register. The change of flux in each magnetic cell resulting from the switching action causes a current to be induced in a one-turn winding connected to the base of the associated transistor. The amplified current change at the collector is then passed through a single-turn winding of the next magnetic cell, which accordingly changes its state and applies an induced current to the next transistor . . . and so on. The action is initiated by a third single-turn winding in each magnetic cell, which serves to introduce shift pulses for moving the pattern of 0 and 1 digits along the length of the register.

The three pieces of 37 s.w.g. wire passing through each cell actually take the place of some 100 turns of 47 s.w.g. that are necessary on a conventional ferrite core performing the same action. The only disadvantage in using the magnetic cell is that it does not This means that the stored flux is largely dependent on the applied current, so that the two states are not so well defined and uncritical as in the ferrite toroidal core.

Equipments based on the transistor/magnetic-core element already give something like a 3,000:1 reduction in power consumption over valve circuits and about 100:1 reduction in size.

Student Exchange

SINCE the foundation of the International Association for the Exchange of Students for Technical Experience in 1948, nearly 29,000 students from 22 countries have taken advantage of the facilities provided by the Association whereby they can obtain practical experience abroad during the summer vacation. The 9th annual report records that in 1956 a total of 5,711 students went abroad under the scheme. By far the greatest number was from Germany (1,284) with Great Britain second (743). Sweden, who sent only 415 students abroad, received the greatest number (1,305) with Germany second (1,019). A total of 774 overseas students came to this country.

Although the radio and electronics industry is not given a separate classification—it is included in electrical engineering-it is obvious from the lists of the participating companies and research organizations in this country and abroad that a large number of them are in this field.

Details of the Association are obtainable from J. Newby, Imperial College, South Kensington, London.

WORLD OF WIRELESS

Radio Shows

WE HAVE often deplored the proliferation of exhibitions catering for radio and its electronics offshoots. Will the situation be eased by the dates of

some of the shows overlapping?

The Radio Industry Council has announced that this year's National Radio Show, which will again be held at Earls Court, London, will be from August 28th to September 7th with a preview for invited guests on the 27th. The static section of the S.B.A.C. Show at Farnborough, which has become the aeronautical radio exhibition, will be held from September 3rd to 9th with a preview on the 2nd.

The exhibition at which the marine side of the radio industry is usually well represented—the Engineering, Marine and Welding Exhibition—overlaps the National Radio Show still further, for it opens at Olympia on August 29th for fifteen days.

Audio Fair

ALL but four of the fifty-one exhibitors who have taken space at this year's Audio Fair will have de-

taken space at this year's Audio Fair will have demonstration rooms. The four-day fair will be held from April 12th to 15th, inclusive, at the Waldorf Hotel, Aldwych, London, W.C.2.

It is being run by Audio Fairs, Ltd., a non-profit-making company on which the following serve "on a purely voluntary basis": chairman, V. G. P. Weake (Pamphonic); vice-chairman, D. A. Lyons (Triv), M. I. Berry (Triv), I. H. Brooks (M.S.S.) (Trix); M. L. Berry (Trix), L. H. Brooks (M.S.S.), J. W. Maunder (Vitavox), H. V. Slade (Garrard), G. E. Spark (M.S.S.), T. R. Threlfall (Goodmans).



DOCTORS Bardeen, Shockley and Brattain (L to R), who jointly received the 1956 Nobel Physics Prize in Stockholm in December, photographed when they worked together on the development of the transistor at Bell Laboratories.

Organizational, Personal and Industrial Notes and News

G.E.C. Valve Policy

A FEW months ago the trade name of "Osram" valves was changed to "G.E.C." This foreshadowed a change in policy resulting from the acquisition by the General Electric Company of the share in the Marconi-Osram Valve Company formerly held by

In future, the M-O. Valve Company, which is now a wholly-owned subsidiary of G.E.C., will concern itself mainly with the manufacture of transmitting and special-purpose valves. Among the transmitting types will be klystrons, magnetrons, travelling wave tubes and backward wave oscillators, as well as valves for r.f. heaters. Receiving valves will include "reliable" and high-performance types in addition to audio amplifiers. Gas-filled valves such as thyratrons and xenon rectifiers represent an important side of the company's activities.

News in Morse

IT is some months since we published a schedule of the transmissions of English news bulletins prepared by the overseas press division of the Central Office of Information. For the bulletins to North America and the Far East an R.T.T. (printing radio telegraph) link, employing frequency-shift keying, is now used, and for a number of other areas the Hellschreiber method has taken the place of morse. There are, however, a number of areas for which morse is still used and below we give the latest schedule of these transmissions from Post Office The morse speed varies from 22 to 28 words a minute.

Region	Times (G.M.T.)		Call	Freq. (Mc/s)
Distant Europe	Monday Tues. to Sun.	0200-0430 } 0300-0530 }	GIQ25	5.365
Middle East	Monday Tues, to Sun.	0200-0430 0300-0530 }	GBB33	13.595
Caribbean	Mon. and Fri. Mon. to Fri. Mon. to Fri.		GIB36 GIB38	16.190 18.680
South America	Friday Mon. to Sat.	2015-2130 0115-0230	GIN31 GIS27	11.645 7.780
Africa	Mon. to Fri. Monday	0915-0945 2015-2100}	GAY40	20.100
South East Asia	Sunday Mon. to Sat. Mon. to Sat. Mon. and Sat.	1915-2115 1715-1800 1815-2215 1600-1715	GAY27 GAY33 GAY27 GAY33	7.447 13.665 7.447 13.665

PERSONALITIES

A.V-M. Raymond G. Hart, C.B., C.B.E., a member of Watson-Watt's Bawdsey team in 1936, has been appointed controller of engineering and equipment at the Air Ministry. In 1941 he went to the Air Ministry as deputy director of radar. He was subsequently concerned with the planning of the air signals in the invasion of Europe and became chief air signals officer at S.H.A.E.F.

Under the Department of Scientific and Industrial Research Act, 1956, which came into force on November 7th, a new research council has been formed in place of the former advisory council. Dr. H. W. Melville, F.R.S., is secretary of the council, and among the eleven members are Professor P. M. S. Blackett, F.R.S., (Imperial College) and Dr. Willis Jackson, F.R.S. (Metropolitan-Vickers).

R. H. Tizard, B.A., A.M.I.E.E., who had been superintendent of the Control Mechanisms and Electronics Division of the National Physical Laboratory, Teddington, since its formation in 1954, recently left to take up an appointment at the London School of Economics. He is succeeded by Dr. A. M. Uttley, who from 1940 until his present appointment was at the Radar Research Establishment (previously T.R.E.), Malvern. During the war he was concerned with the design of a number of synthetic trainers, and more recently was largely responsible for the functional design of TREAC, the electronic digital computer used in the Physics Department of R.R.E.

L. A. Woodhead, director and general manager of Cossor Instruments, Ltd., is the new chairman of the Electrical and Electronics Section of the Scientific Instrument Manufacturers' Association. He joined the parent company, A. C. Cossor, Ltd., in 1930 and during the war was in charge of the final test and inspection of valves and c.r. tubes at a large shadow factory.

William Culshaw, B.Sc., Ph.D., recently left the Radar Research Establishment, where he specialized in the field of microwave optics and later in millimetre wave magnetron development, and has joined the laboratories of the National Bureau of Standards at Boulder, Colorado. Dr. Culshaw, who joined T.R.E. in 1942, is in the N.B.S. Microwave Physics Section.

Dr. A. V. J. Martin, until recently editor of our French contemporary *Télévision*, has been appointed professor of electrical engineering at the Carnegie Institute of Technology, Pittsburgh, Pennsylvania.

L. S. Crutch, B.Sc., M.I.E.E., deputy chief engineer of Siemens Brothers and Company, which he joined in 1931, is appointed a director of the company. He has specialized in the development of telecommunication systems, and was for some years assistant chief engineer of Siemens' telecommunications department.

G. K. Nicholls, Assoc.I.E.E., has been appointed manager of the Cable and Wireless cable station and engineering school at Porthcurno, Cornwall, in succession to C. J. V. Lawson, recently appointed deputy engineer-in-chief.

I. C. I. Lamb, A.M.Brit.I.R.E., has been appointed engineer-in-charge of the recently opened I.T.A. station at Emley Moor, Yorks. Employed by the B.B.C. both before and immediately after the war, first as a maintenance engineer at Daventry and later in the research department, he subsequently went to Pye, Ltd. Last February he joined the I.T.A.

The announcement of the above appointment affords an opportunity to mention the engineers-in-charge of the first three I.T.A. stations. W. Woolfenden (Croydon), after service as a R.A.F. radar officer, went into industry for a short while before joining the B.B.C. in 1947. He has been with the I.T.A. since August 1955. N. G. Payne, A.M.I.E.E., was for 16 years on the maintenance staff of the B.B.C. before being appointed to Lichfield last February. W. H. Jarvis, A.M.I.E.E. (Winter Hill), was a marine radio officer from 1918 until 1935 when he joined the B.B.C. He was senior maintenance engineer at Alexandra Palace before joining the I.T.A. last April.

W. F. Harkness, who in the early days of broadcasting formed Electrical Appliances, Ltd., selling Eureka transformers, and after service with Cossor's went to the U.S.A. in 1939, has now retired and returned to this country. His address is 5, Dawson Place, London, W?



H. E. F. Taylor is the new secretary of the Radio Communication and Electronic Engineering Association in succession to Neill Christie. During the war Mr. Taylor was a lieutenantcolonel in the Royal Signals and was conwith cerned mostly long distance telecommunication projects. He has been a radio amateur for some 35 years and has operated in India with the call-sign VU2AT. His British call is G6HT.

L. Essen, D.Sc., Ph.D., A.M.I.E.E., who joined the National Physical Laboratory in 1929 and has been concerned with precise microwave measurements, in particular with the measurement of frequency and time, has been promoted to senior principal scientific officer in the scientific civil service. Dr. Essen, who is 48, recently developed a frequency standard, based on a resonance of the cæsium atom.

The B.B.C. has appointed G. K. Drake as engineer-in-charge of the television and v.h.f. sound broadcasting station at Blaen Plwy, Wales, and B. M. Britton as e-in-c of the Sandale, Cumberland, television station. Mr. Drake, who joined the Alexandra Palace television station in 1938, has been senior maintenance engineer at Wrotham, Kent, since 1949. Mr. Britton has been with the Corporation for 14 years.

T. P. Lynott, A.M.I.E.E., has been appointed chief engineer to Gardners Radio Ltd., of Somerford, Christchurch, Hants. Since 1947 he has been at the Atomic Energy Research Establishment, Harwell, as transformer design engineer, having previously been first with G.E.C. and then the directorate of instrument production at the Ministry of Supply. Mr. Lynott, who is 42, is chairman of the subcommittee of the Radio Components Standardization Committee of the Ministry of Supply dealing with transformers and chokes.

W. Grant, contributor of the article on page 33, studied at the Royal Technical College, Glasgow, for his B.Sc. in electrical engineering. During the war he was commissioned Electrical and Mechanical Engineer in R.E.M.E. He has since been undertaking research and development work and is at present with J. Stone and Company (Deptford).

OBITUARY

Air Commodore R. L. Phillips, C.B., C.B.E., who died on November 22nd at the age of 47, was associated with aeronautical radio for the major part of his career in the R.A.F. He had held the positions of Director of Radio and Director of Signals Policy at the Air Ministry.

The death is announced by the Canadian Department of Transport of G. C. W. Browne, retired controller of telecommunications, at the age of 66. He went to Canada from Ireland in 1912 and entered the Canadian Government Radio Service two years later. Since his retirement last year Mr. Browne had been acting as consultant to the Fowler Commission on Broadcasting in Canada.

George T. Clack, who for many years (until 1953) was honorary lecture secretary of the Television Society, died on November 17th at the age of 47. He had been with Bush Radio since 1939 where, as a senior laboratory engineer, he had been latterly primarily engaged on technical liaison work.

IN BRIEF

Receiving Licences.—During October the number of television licences current in the U.K. increased by 151,299, bringing the total to 6,291,072. The total number of broadcast receiving licences, including those for television and 310,301 for car radio, was 14,419,741.

Test transmissions from a 1-kW pilot transmitter will begin on March 1st from the site of the first Scottish I.T.A. station at Black Hill, Lanarks. The station will operate in Channel 10 (199.75 Mc/s vision and 196.25 Mc/s sound) although the carriers will actually be offset by -19.5 kc/s and -10.5 kc/s, respectively.

In preparation for the opening of the Scottish I.T.A. station at Black Hill, Lanarks., at the end of August, the programme contractors, Scottish Television, Ltd., are arranging a series of weekly exhibitions from February to June in the principal burghs to be served by the station. The Scottish Radio Retailers' Association is participating, and advice on the conversion of existing sets will be given to enquirers.

Lichfield Increased Power.—By adding 20-kW amplifiers to both the sound and vision transmitters at Lichfield the e.r.p. of the I.T.A. station was increased on November 23rd to 200 kW. Duplicate sets of transmitters were previously operated in parallel to bring the e.r.p. up to 100 kW. The spare sound and vision transmitters are now being kept as standbys in case of breakdown of the main equipment. All the transmitting equipment at Lichfield was designed and installed by Pye, Ltd.

The B.B.C.'s eighth v.h.f. sound broadcasting station, Holme Moss, was brought into service on December 10th. It is radiating a three-programme service on 89.3, 91.5 and 93.7 Mc/s with an e.r.p. of 120 kW. The six 10-kW transmitters (two for each service) were installed by Marconi's.

Four of the seven gold medals awarded to British manufacturers for goods displayed at the California State Fair, held in Sacramento in September, were won for radio and electronic equipment. Two of the medals went to Trix Electrical for their Trixonic amplifier 800 and record player A720, one to Pye for their "Leadsman" echo sounder, and one to Fonadek for their telephone amplifier. The medals were presented at a conference of the Dollar Exports Council by the Minister of Economic Affairs at the U.S. Embassy.

Sea-going trials of Gee (the Cossor hyperbolic navigational aid) have shown that sea-level ranges up to 200 nautical miles from coast chains can be relied upon. This was accomplished using the South Western chain which operates on a frequency around 25 Mc/s. The long range is attributed to tropospheric propagation.

Ferranti-Ekco Link.—Domestic radio and television receivers with the Ferranti trade mark will, in future, be marketed by a new company being formed by E. K. Cole, Ltd.

The scope of this year's Radio Society of Great Britain exhibition is to be widened considerably and the title changed to Radio Hobbies Exhibition. It will be held in October at Seymour Hall, Seymour Place, London, W.1, and is again being organized by P. A. Thorogood (G4KD), who is chairman of the London u.h.f. group.



JUBILEE of the invention of the triode valve by Dr. Lee de Forest is commemorated on this franking on a recent letter from the United States.

American Facts and Figures.—Dr. W. R. G. Baker, head of the General Electric Company's Electronics Park, at Syracuse, N.Y., in a review of the progress of the electronics industry, stated that one out of every forty jobs in the United States is in electronics, and that 75% of these did not exist ten years ago. Moreover, whereas the electrical industry in the States approximately doubles every ten years, the electronics industry is doubling every five or six years. Dr. Baker forecast that the use of semi-conductor equipment will increase 100% in the U.S.A. during 1957. Incidentally, during the past ten months the price of G.E. transistors has been reduced 35%.

"W.E." Editorials.—For nearly 30 years Professor G. W. O. Howe contributed editorials to our sister journal Wireless Engineer (now Electronic & Radio Engineer). An index to these contributions, including chronological, author and subject indexes, was compiled by Dr. A. J. Small, of the Department of Electrical Engineering at Glasgow University, some two years ago. An addendum bringing it up to date has now been prepared, and this, together with the original index (covering the period January, 1926, to March, 1955, the last of his regular editorials) is obtainable from Dr. Small, price 5s.

The Radio Trades Examination Board has issued a reminder that the closing dates for entries for this year's **Servicing Certificate Examinations** are January 15th for television and February 1st for sound receivers. Forms and regulations for the examinations, which will be held in May, are obtainable from the R.T.E.B., 9, Bedford Square, London, W.C.1.

Danish TV.—The information regarding Denmark included in the E.B.U. television map on page 605 of the December issue was incomplete. Three transmitters have been in use for the past eight months—Copenhagen (5 kW), Fyn, near Odense (5 kW) and Aarhus (2.5 kW).

"Audio-Frequency Response Measurements."—The equipment described under this heading in our December, 1956, issue was developed by the staff of Grundig (Great Britain), Ltd., in the company's laboratories.

Two nine-week courses on digital computers and on colour television will be held at the Southall Technical College, Middlesex, on Wednesday evenings, beginning January 16th. An eight-week course on experimental servomechanisms will also be held on Wednesday evenings, beginning February 6th. The fee for each course is £1.

A radio and television maintenance and servicing course will again be held during the spring term at the Wesley Institute, Wesley Road, London, N.W.10, on Monday evenings, beginning January 7th. (Fee £1.)

Transistors.—An evening course of eight lectures on transistor physics and transistor applications commences on Thursday, February 7th, at the South-East London Technical College, Lewisham Way, London, S.E.4. (Fee £1.)

Eight lectures covering the theory and practice of electronic instruments used in chemical analysis will be given at Battersea Polytechnic, Battersea Park Road, London, S.W.11, on successive Wednesday evenings commencing February 6th. (Fee £1.)

Most of the courses set out above deal with the technology of electronic communication. But, before information can be communicated, whatever the means, it must be clothed in words. To find the best words for the job becomes more and more difficult as the complexity of life increases. Managements of firms are realizing to an increasing extent that clear presentation of information, technical and otherwise, by their employees is important. Courses of instruction in various aspects of this subject are offered by Osmond Turner Mead Associates, of 3, Gower Street, London, W.C.1. A booklet describing the courses is issued.

BUSINESS NOTES

Vision and sound transmitters for the I.T.A. South Wales station are to be supplied by Pye. The equipment will be similar to that installed at Lichfield—20-kW vision transmitter and 5-kW sound transmitter with 5- and 1.25-kW standby equipment.

In the annual report of the Solartron group of companies it is recorded that sales increased from £152,300 in 1954 to £758,000 during the year ended last June. During the same period the staff has grown from 240 to 550, the average age being 33. A joint company (Industrial Automation Developments, Ltd.) has been formed by the Solartron Electronic Group, Ltd., and Scribbans-Kemp, Ltd., for research and development of automation in the food processing industries.

With the installation of Pye industrial television equipment at the airways terminal at Victoria, London, the announcer is both seen and heard. Pye industrial television equipment has also been installed by a firm of stockbrokers at the London Stock Exchange. It conveys by line to the company's offices a quarter of a mile away details of the constantly changing stocks and shares listed on the "board."

Within a few weeks of its announcement **Decca** true motion radar (TM 46) had been ordered for over one hundred vessels. Orders for all types of Decca marine radar now total more than six thousand—an increase of one thousand in about eight months.

A tour of U.K. ports is being undertaken by a demonstration caravan equipped with **Kelvin Hughes** marine gear, including the new Type 14 radar which has a slotted waveguide aerial. In January and February demonstrations will be given mainly in Northern Irish, Scottish and Welsh ports.

An order for the supply of fifty 10-watt f.m. mobile transmitter-receivers has been placed with Marconi's by the Metropolitan Police. Up to seven crystal-controlled channels are available within a 0.5 Mc/s section of the 70 to 100-Mc/s band.

A further fifty lifeboats of the Royal National Lifeboat Institution, making one hundred in all, are to be equipped with v.h.f. radio-telephone equipment by British Communications Corporation, Ltd.

The sales and service division of F. C. Robinson and Partners, at 122, Seymour Grove, Old Trafford, Manchester, 16 (Tel.: Chorlton 5366), will in future operate under the title of McKellen Automation, Ltd. The change does not affect the manufacturing operations at Cheadle of F. C. Robinson and Partners, of which F. P. McKellen (managing director of McKellen Automation) has been general manager for some years.

The sole manufacturing rights in Great Britain for the Bradford loudspeaker enclosure (of American origin) have been secured by **John Lionnet & Company** who have recently moved from the City to the West End. Their new address is 17, Charing Cross Road, London, W.C.2. (Tel.: Trafalgar 5575.)

An American patent (No. 254567), in addition to British patent No. 689695, has been granted to **Lustra-phone** for their noise-cancelling microphone (Type VC52).

Two members of Mullard Overseas, Ltd., have joined Mullard South Africa (Pty.), Ltd. They are T. W. Hogg, a commercial executive of the radio division, and R. E. Collins, of the electronic tube division, who is to organize a technical service department.

A kit of relay parts comprising seven coils (500 ohms to 20 K ohms) and a variety of contact banks has been produced by **Stevenage Relays**, **Ltd.**, associates of W. H. Sanders (Electronics), Ltd.

A large-screen television receiver without loudspeaker but with headphones for individual patients has been installed by Hadley Telephone & Sound Systems, Ltd., at the Royal Orthopædic Hospital, Birmingham. Lithgow Electronics, Ltd., sole representatives in the U.K. and Eire for the products of the Hewlett-Packard Company, of Palo Alto, California, have moved from Harrow to 198/200, Bath Road, Slough. (Tel.: Slough 21292). At their new office facilities are provided for demonstrating such H.P. equipment as electronic counters, signal generators, and oscilloscopes.

With the opening of Mullard's new headquarters at Mullard House, Torrington Place, London, W.C.1 (Tel.: Langham 6633), the various departments of the organization which have been in a number of separate buildings will be under one roof.

OVERSEAS TRADE

Equipment for the provision of direct radio-telephone links between the islands of San Miguel and Terceira, and between Terceira and Faial, in the Azores group, is to be supplied by Marconi's. Initially the links will carry seven speech channels and six voice-frequency telegraph channels.

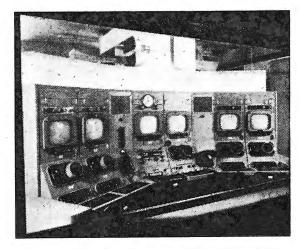
Electronic control equipment is being supplied by E.M.I. Electronics, Ltd., for an automatic conveyor system being installed by Geo. W. King, Ltd., of Stevenage, Herts., in the body-painting plant of a new Simca car factory at Poissy, France.

Solartron Incorporated has been formed to distribute and sell in the United States electronic equipment produced by the Solartron group in this country.

European Office.—Plessey International, Ltd., have opened an office at Singel 160, Amsterdam C, for the supervision of Plessey's interests in northern and central Europe.

This year's International Liege Fair, Belgium, will be held from April 27th to May 12th. Details of space available in the electronic section are obtainable from the U.K. representative, R. C. Liebman, 178, Fleet Street, London, E.C.4.

In order to overcome the delay caused by the recent New York dock strike Birmingham Sound Reproducers, Ltd., chartered planes to carry regular deliveries of record changers to the United States. American receiver manufacturers, who purchase \$100,000 worth of B.S.R. equipment a week, volunteered to help defray the extra cost involved.



EASE OF CONTROL is the keynote of the whole installation at the two television studios at Riverside, Hammersmith, recently brought into use by the B.B.C. This is especially true of the lighting which is remotely controlled from positions adjacent to the sound, vision and production control rooms. Facilities for electronic effects, such as inlay and overlay, are also provided. Marconi camera control equipment is shown here.

Limiters and Discriminators

I-Wide or Narrow Bandwidth: Basic Equivalent Circuits:

By G. G. JOHNSTONE, BSc.*

The Round-Travis Discriminator

W E shall begin by considering the bandwidth required in a discriminator, more especially in view of the arguments put forward by Prof. Arguimbau and his colleagues in favour of wide-band discriminators.

If two f.m. signals interfere, they may be on the same carrier frequency (i.e., co-channel) or on nearby carrier frequencies (i.e., adjacent channel). Briefly Arguimbau maintains that in the presence of co-channel or adjacent-channel interference, the interfering signal will produce unwanted audio output even when the difference between the frequencies of wanted and unwanted signals is above the audible limit. The two signals add together to produce a composite signal which varies in amplitude and frequency according to the relative magnitudes and frequencies of the two signals. This is

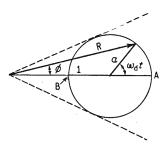


Fig. 1. Vector diagram of wanted signal (1) and interfering signal (a) with a small frequency difference.

shown in the vector diagram of Fig. 1, where the ratio of the amplitude of the unwanted signal to that of the wanted signal is a:1. The wanted-signal vector is assumed stationary and the unwanted-signal vector rotates at a relative angular frequency ω_d , which corresponds to the difference f_d between the frequencies of the two signals.

The magnitude of the resultant, R, varies between (1+a) and (1-a); this amplitude modulation can be removed by limiting and need not concern us further. The phase displacement (ϕ) of the resultant swings between the limits indicated by the dotted lines in Fig. 1. The phase displacement can be calculated and, since the instantaneous frequency shift is equal to $1/2\pi$ times the rate of change of phase angle, i.e., $f = \omega/2\pi$ and $\omega = d\phi/dt$ we can determine the frequency shift at any instant. The calculation is straightforward, but rather long, and it is sufficient for our purpose to note that the interfering frequency-modulated signal has the form shown in Fig. 2. The peaks at α occur when the vectors are in line as at A in Fig. 1; the peaks at β occur when the vectors have the position B in Fig. 1. The peak value of the frequency shift at α is given by $af_d/(1+a)$ and at β by $af_d/(1-a)$. Thus as the ratio of unwanted signal amplitude approaches that of the wanted signal a approaches 1

and the peak shift β becomes very large. The positive-going and negative-going excursions of the wave-form of Fig. 2 have a different form but the areas included between the curves and the horizontal axis are equal, the mean resultant frequency shift is zero and there is no d.c. component in the output of the discriminator, provided that the discriminator is linear over the range of frequency excursion.

The period of the wave of Fig. 2 is $1/f_a$ and, if the frequencies of the two signals differ by more than the highest audio frequency, there will be no audible output under the steady state conditions postulated. If the frequency difference is less than the highest audible frequency, there is a heterodyne whistle; this is true whether the discriminator is "wide-band" or not.

To carry the argument further, suppose the difference between the frequencies of the two signals exceeds the highest audible frequency and the discriminator is narrow band. As the unwanted-signal amplitude approaches that of the wanted signal the ratio a tends to unity and the peak frequency shifts become progressively larger, tending to a limit of $f_a/2$ in one direction and infinity in the other. We shall concentrate on the peak at β because this is always greater than that at α . For an idealized narrow-band discriminator characteristic of the type shown in Fig. 3, the peaks at β are "clipped" as shown in Fig. 4. The areas under the positive-

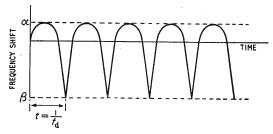


Fig. 2. Form of frequency modulation produced as a result of the conditions shown in Fig. 1.

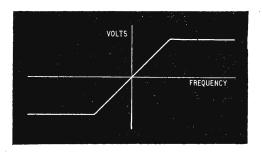


Fig. 3. Idealized narrow-band discriminator characteristic.

^{*} B.B.C. Engineering Training Department.

for F.M. Receivers

A GREAT deal has been written about the performance of various types of limiter and discriminator for use in f.m. receivers, but much of this information is contradictory and the choice of a limiter and discriminator for a particular application may appear difficult, particularly to the newcomer to the subject. It is the purpose of this and subsequent articles to discuss the performance of the basic types of limiter and discriminator in an attempt to clarify the subject.

The discriminators to be discussed fall into six classes: (1) the Round-Travis (2) the Foster-Seeley discriminator (3) the ratio detector (4) the locked oscillator (5) the phase-difference comparator and (6) the counter. Types (3)

(4) and (5) have a degree of inherent limiting action.

The types of limiter to be discussed comprise (1) the grid limiter (2) the anode limiter (3) the dynamic limiter and (4) the "clipper."

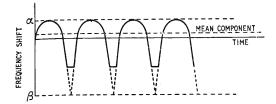


Fig. 4. Clipping of the frequency peaks by the characteristic of Fig. 3 results in a displacement of the average frequency.

going and negative-going portions of the waves are now no longer equal. There is a shift in the average frequency and a d.c. component in the output from the discriminator; it is shown in dotted lines in Fig. If now the unwanted signal is modulated, its frequency swings about the mean value and the difference between the frequencies of the two signals alters correspondingly. The waveform of Fig. 2 now becomes that shown in Fig. 5(a); for comparison the graph of the frequency difference is shown at Fig. 5(b). If now the waveform of Fig. 5(a) is "clipped" as indicated by the dotted line, the d.c. component has superimposed "blips shown in Fig. 5(c). These have the same repetition rate as the modulating signal, and have components at multiples of the modulating-signal frequency. This represents cross-modulation between the two received signals accompanied by distortion. With a "wide-band" discriminator there is no clipping and this effect does not occur.

We may summarize the conclusions of the previous paragraphs as follows. In receiving co-channel signals some interference is inevitable because the difference between the frequencies of the two signals must, for part of the time, lie within the audio frequency range; this effect occurs whatever type of discriminator is employed. The peak heterodyne output is given by $af_d/(1-a)$ which decreases rapidly as a falls below unity and the stronger signal rapidly "swamps" the weaker as the ratio of the amplitudes of the signals a departs from unity; this is, of course, the well-known "capture" effect,

For signals on adjacent channels the difference between the frequencies of two carriers is always greater than the highest audible frequency; there is no cross-modulation if a wide-band discriminator is employed. This is illustrated in Fig. 6 which

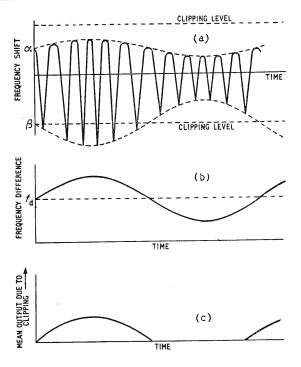


Fig. 5. (a) Waveform when the unwanted signal is modulated by a sine wave. The frequency difference is shown in (b), and the distortion product due to clipping is shown at (c).

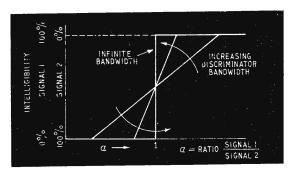


Fig. 6. Interference between signals on adjacent channels as a function of discriminator bandwidth.

shows that for an infinite bandwidth only the stronger signal is received even if its amplitude is only slightly greater than that of the other; but as the bandwidth is made smaller, the ratio of signal strengths for which interference is experienced becomes greater.

The behaviour of a discriminator toward ignition interference can be deduced by similar arguments.

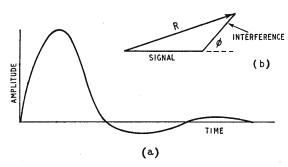


Fig. 7. (a) Waveform of i.f. output due to a pulse of interference and (b) vector relationship of signal and interference.

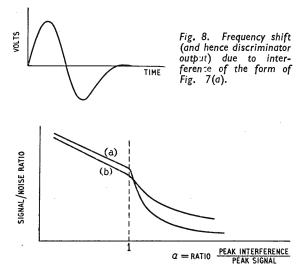
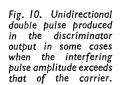
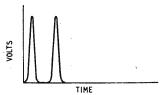


Fig. 9. Signal/noise ratio with impulsive interference for (a) wide-band and (b) narrow-band discriminators.





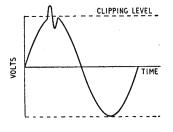


Fig. 11. When the interference pulse coincides with a peak of modulation, clipping may remove part of the pulse and increase noise.

The waveform of a pulse of interference is modified in the i.f. amplifier to a shape similar to that shown in Fig. 7(a). The shape of this pulse varies little with the source of the interference, but depends almost entirely upon the characteristics of the i.f. amplifier itself. The duration of the pulse is very short, approximately 7 microseconds for an i.f. bandwidth of 200 kc/s. The figure shows the envelope, which modulates a "carrier" at the centre trequency of the i.f. amplifier, which we shall assume equal to the signal carrier frequency. signal carrier and interference carriers may have any phase angle with respect to each other, because the exact moment of incidence of the interference pulse is fortuitous. Thus the signal and interrerence carriers add as shown in Fig. 7(b); the phase angle between the carrier vectors ϕ has been arbitrarily selected. The interference signal vector grows and decays as shown in Fig. 7(a). Consequently, if the ratio of peak interference envelope to the peak carrier is small, the phase angle of the resultant follows a wave similar in shape to that shown in Fig. 7(a). The rate of change of phase angle, and hence the frequency shift then follow a curve of the type shown in Fig. 8. When the number of tuned circuits preceding the limiter exceeds four, the maximum value of the frequency shift due to the interfering signal is given approximately by 4aF where a is the ratio of the peak value of the interfering signal to that of the carrier, and F is the bandwidth measured between 3-dB points. The audible noise output is proportional to the net area under the frequency-shift envelope, and hence to a. However, the area under the positive-going excursion is nearly equal to that under the negativegoing excursion and the net area is small. spectrum of this output rises linearly with frequency, and the output has the sound of a "click." If a succession of constant-amplitude impulses presented to the receiver, the magnitude of the output pulses varies with the relative phase angle between the carrier and the interfering signal at the occurrence of each impulse. If the amplitude of the interference signal is less than that of the carrier, a is less than unity and the signal-to-noise ratio falls linearly with a, as shown in curve (a) of Fig. 9. If the amplitude of the interfering signal exceeds that of the carrier, a is greater than unity and a new mechanism comes into play by which some of the output-signals have the form of sharp spikes, each pulse of ignition interference producing two spikes of the same polarity; as shown in Fig. 10. The net area beneath the curve is now no longer small. The spectrum of this waveform is level over the a.f. band and the output has the sound of a "pop." For such high-amplitude interfering signals, as the amplitude of the interfering signal is increased the signal-tonoise ratio falls abruptly and then levels off as shown in curve (a) of Fig. 9.

Consider the effect of reducing the discriminator bandwidth on impulsive interference of this type. If a is less than unity, and the signal is at one extreme of its frequency swing, one of the peaks due to impulsive interference in the discriminator output signal may be clipped as shown in Fig. 11. The net area increases and the signal-to-noise ratio is poorer than for a wide-band discriminator as shown in Fig. 9 curve (b). On the other hand, in the region where a is greater than unity, a reduction in discriminator bandwidth causes the amplitude of the

spikes (Fig. 10) to be reduced and the signalto-noise ratio is better than for a wide-band discriminator. Thus for impulsive interference a narrow-band discriminator is an advantage because the worsening of the signal-to-noise ratio in the region where this ratio is good in exchange for an improvement in the area where it is bad is in general desirable. Thus we may summarize the conclusions so far reached as follows:

(1) If the principal source of interference is co-channel and adjacent channel, a wide-band discriminator is best.

(2) If the principal source of interference is of the impulsive type, a narrow-band discriminator is best.

In this country cochannel and adjacent channel interference would not appear to present a serious problem, and hence ignition interference may be the principal type of interference to be overcome. In U.S.A., however, ignition interference is probably less troublesome than co-channel and adjacent-channel ference. Thus it would appear that

British and American practice in discriminator bandwidth may tend to diverge, with a tendency in Britain to use narrow bandwidth discriminators.

We shall now consider the performance of discriminators in detail and in the subsequent discussion we shall make extensive use of one or other of two equivalent circuit diagrams for the phase-difference discriminator transformer, Fig. 12(a), used in the Foster-Seeley discriminator and the ratio detector. These equivalent diagrams are shown in Figs. 12 (b) and (c), and their derivation is given in the Appendix. Depending on the constants of the original circuit only one of the two equivalents is physically realizable. The equivalent circuit for one special case reduces to two tuned circuits fed with equal currents, and resonant at frequencies equally displaced from the centre frequency of the transformer from which they are derived. Thus the Foster-Seeley and Round-Travis circuits shown in Fig. 13 have identical performances. This circuit transformation simplifies the analysis of the Foster-Seeley discriminator and the ratio detector and we shall analyse the performance of the Round-Travis circuit in detail in order to extend the results to the Foster-Seeley and ratio detector circuits.

Round-Travis Circuit. In this discriminator two

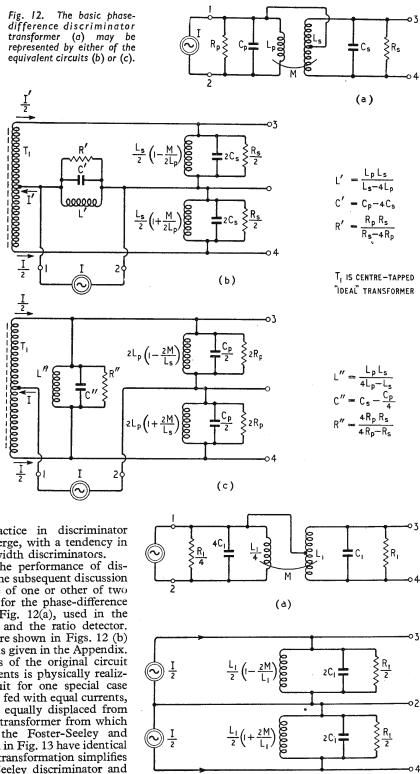


Fig. 13. Identical performances are given by these forms of (a) the Foster-Seeley and (b) the Round-Travis circuits

(b)

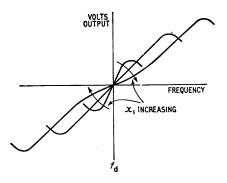


Fig. 14. Dependance of shape of discriminator characteris ic on the value of x_1 .

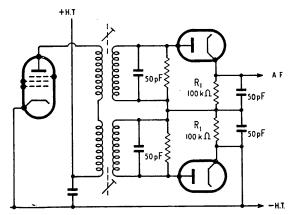


Fig. 15. Basic practical Round-Travis circuit.

tuned circuits are employed, one tuned to a frequency slightly above the centre frequency and the other tuned to a frequency an equal interval below the centre frequency. This circuit has appeared in a wide variety of forms, the variations being principally in the method of applying the signals to the two circuits. We shall consider the circuit in its general form, where the driving stage is represented by a constant current generator, as shown in Fig. 13.

We can write the response of a tuned circuit, comprising L, C, and R in parallel as

$$\frac{1}{Z} = \frac{1}{R} + \frac{1}{j\omega L} + j\omega C$$

In the frequency range near resonance (ω_0) we can write ω as $(\omega_0 + d\omega)$, where $d\omega$ is small compared with ω_0 . Using this substitution we can make the approximation that

approximation that
$$\frac{1}{Z} = \frac{1}{R} + 2j d\omega C = \frac{1}{R} + 2j \frac{d\omega}{\omega_0} \cdot \frac{1}{\omega_0 L}$$

$$= \left(1 + \frac{2j d\omega}{\omega_0} \cdot \frac{R}{\omega_0 L}\right) / R$$
If we let $x = 2Q d\omega/\omega_0$, where Q is $R/\omega_0 L$, then $Z = R/(1 + ix)$
in which x is a variable directly proportional to

in which x is a variable directly proportional to the frequency shift.

If one tuned circuit is tuned above the centre frequency and displaced by an amount $x = x_1$ and the other is tuned below and displaced by an amount $x = -x_1$ we can represent the impedance of the two circuits at any frequency in the neighbourhood of the

centre frequency by $Z_1 = R/[1+j(x-x_1)]$ and $Z_2 = R/[1-j(x+x_1)]$ respectively.

The two diodes rectify the voltages developed across each tuned circuit independently, as shown in Fig. 15, and for 100% rectification efficiency, the output voltage is equal to the difference between the peak values of the voltage developed across each tuned circuit. If I is the peak value of the input current the output voltage is given by

 $E = IR[\{1 + (x - x_1)^2\}^{-\frac{1}{2}} - \{1 + (x + x_1)^2\}^{-\frac{1}{2}}]$ A family of curves for various values of x_1 , is shown in Fig. 14. These are the output-voltage frequencyshift curves for the discriminator, and ideally should have a linear region about the centre frequency. As shown in Fig. 14, for small values of x_1 the characteristic has continuous curvature and small peak separation. Larger values of x_1 give better linearity and greater peak separation, but above a critical value of x_1 the characteristic develops a kink near the centre frequency. Thus there would appear to be an optimum value of x_1 .

The expression for E given above can be expanded as a series in ascending powers of x. The expansion is symmetrical about x = 0, and contains odd powers of x only. We can thus write

 $E = a_1x + a_3x^3 + a_5x^5 \dots$

The first term represents the required output, i.e., an output varying linearly with frequency shift. The other terms indicate non-linearity, producing harmonic distortion and intermodulation in the output. This distortion can be minimized by making a_3/a_1 ,

 a_5/a_1 , etc., as small as possible. The evaluation of a_1 , a_3 , a_5 in terms of x_1 is straightforward but tedious. The values of the first three coefficients are:

Three coefficients are:

$$a_1 = 2x_1(1 + x_1^2)^{-\frac{5}{2}}$$

$$a_3 = x_1(2x_1^2 - 3)(1 + x_1^2)^{-\frac{7}{2}}$$

$$a_5 = \frac{1}{4}x_1(8x_1^4 - 40x_1^2 + 15)(1 + x_1^2)^{-\frac{13}{2}}$$
From these expressions we have

$$a_3/a_1 = \frac{1}{2}(2x_1^2 - 3)/(1 + x_1^2)$$

 $a_5/a_1 = \frac{1}{8}(8x_1^4 - 40x_1^2 + 15)/(1 + x_1^2)^2$ To minimize distortion, we can choose the value of

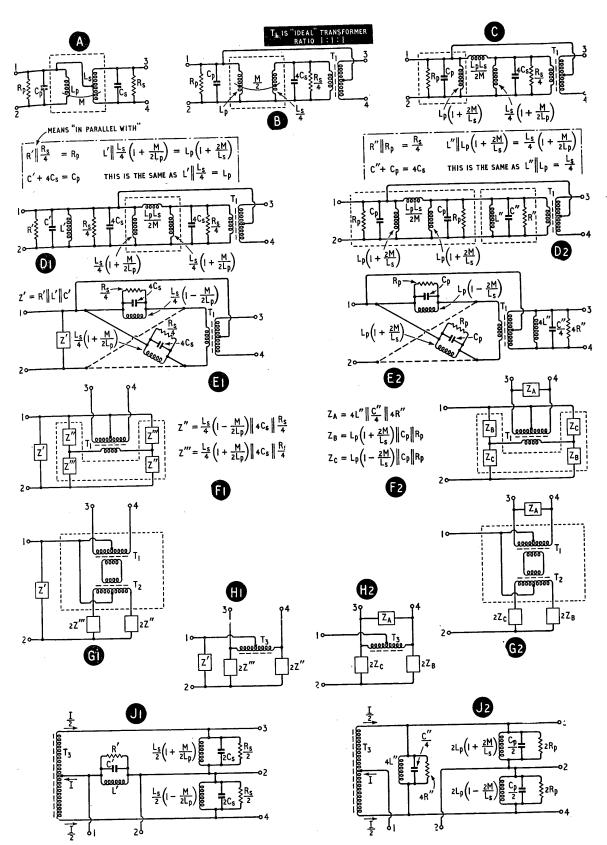
APPENDIX

THE derivation of the equivalent circuit for a phase difference discriminator transformer, Fig. A on the opposite page, is obtained by the successive manipulation of the portions enclosed by dotted lines. In Fig. B the secondary circuit comprising L_s, C_s, R_s is transferred to the primary side of the "ideal" transformer T1; this transformer has a centre-tapped secondary, providing the two voltages of opposite polarity in series with the primary voltage. In Fig. C, the "T" network is converted to " π " form. In Fig. D1 the terminations of the " π " network are made equal. If the terminations are made equal to the secondary components, the sequence follows through Figs. D1 to H1, and if to the primary components through Figs. D2 to H2.

In Fig. E, the " π " network is translated to a lattice by means of Bartlett's Bisection Theorem. Figs. F show Figs. E re-drawn. Figs. G show Figs. F re-arranged by the introduction of transformer T2, also of 1:1·1 ratio. Figs. H are Figs. G with transformers T1 and T2 combined into transformer T3. Figs. J show Figs. H re-drawn.

The derivation of these againstant circuits is

The derivation of these equivalent circuits is an extension of the treatment due to H. Marko (Frequenz, January, 1952).



Wireless World, January 1957

 x_1 which makes one of these ratios zero; it is usual to make $a_3 = 0$, because this is the dominant distortionproducing term for values of x less than unity. This gives $x_1 = \sqrt{1.5}$, and the expression for output voltage becomes

$$E = IR(0.62x - 0.055x^5 \dots)$$

For this value of x_1 , the useful extent of the characteristic is limited to values of x of less than unity. This is illustrated in the calculation below where it is shown that the distortion rises steeply for greater values of x.

To evaluate the distortion likely to be obtained with this circuit arrangement, we shall consider an input signal frequency-modulated by a signal of frequency f_a to a maximum swing of f_s kc/s on each side of the centre frequency. The value of x corresponding to f_s is represented by x_s and is given by $x_s = 2Qf_s/f_0$. Substituting the value $x_s\cos\omega_a t$ for x in the expression above gives

 $E = IR(0.62x_s \cos \omega_a t - 0.055x_s^5 \omega_a t ...)$ We can expand $\cos^5 \omega_a t$ by means of the identity $\cos^5 \theta = \frac{1}{16} (\cos^5 \theta + 5 \cos^3 \theta + 10 \cos \theta)$ which gives

$$E = I R[0.62x_s \cos \omega_a t - 0.0034x_s^5 (\cos^5 \omega_a t + 5\cos 3\omega_a t + 10\cos \omega_a t)]$$

$$= IR [(0.62x_s - 0.034x_s^5) \cos \omega_a t - 0.017x_s^5 \cos 3\omega_a t - 0.0034x_s^5 \cos^5 \omega_a t)]$$

The amplitude of the fundamental-frequency component is less for an ideal characteristic but the reduction is small and will be ignored, the values of x_s being limited to approximately unity. percentage of third-harmonic distortion is then given

by
$$\frac{0.017 \times 100}{0.62} x_s^4$$
, and the percentage of fifth

harmonic is one-fifth of this figure. For $x_s = 1$, there is 2.7 per cent third-harmonic and 0.54 per cent fifth-harmonic distortion. The magnitude of the harmonic distortion is proportional to x_s^4 , and thus falls rapidly if a lower value of x_s is considered. Thus reduced distortion can be obtained by using a lower value of x_s , but this in turn means a smaller output at the fundamental frequency.

With a broadcast signal, the frequency deviation is fixed at 75 kc/s. If it is desired to operate the discriminator with 75 kc/s corresponding to $x_s = 1$, the parameters of the circuit are determined by the relationship $x = 2Q \, df/f_0$. With $df = 75 \, \text{kc/s}$ at x = 1, and a centre frequency (f_0) of 10.7 Mc/s, the value of Q is 71. The resonant frequencies of the two tuned circuits are given by 10.7 $(1\pm\sqrt{1.5/142})$ Mc/s, i.e., $10.7 \text{ Mc/s} \pm 92 \text{ kc/s}$. Such a discriminator would have very little margin to allow for oscillatorfrequency drift and mis-tuning and a value $x_s = 1$ corresponding to 100 kc/s would be better. The corresponding to 100 kc/s would be better. circuit parameters are then Q = 53 with the resonant peaks at $10.7 \text{ Mc/s} \pm 123 \text{ kc/s}$. For such a discriminator at 75 kc/s deviation the third harmonic distortion is 0.84 per cent and the fifth harmonic 0.17 per cent. If we assume that the two tuned circuits each employ a capacitor of 50 pF, the dynamic resistance, $R = Q/\omega C$ of the circuits is approximately $53 \times 300 = 16 \text{ k}\Omega$. The input current, I, is the peak value of the fundamental-frequency component in the output of the preceding limiter stage; a typical value is 1 mA. The peak audio output is given by $0.62 \text{ IR } x_8$ and in the example chosen, x_s for 75 kc/s deviation is 0.75, giving a peak audio output of approximately 7.5 volts. The inductance

required to resonate at 10.7 Mc/s with 50 pF is 4.45 μH; final adjustment of the resonant frequencies of the two circuits is made by means of dust-iron cores in the inductor formers. To secure the correct value of Q, the usual procedure is to design the coils for a higher value of Q than required and add damping resistors. The diode detectors provide part of this damping equivalent approximately to $R_1/2$, where R_1 is the value of each diode load resistor. The basic practical circuit is shown in Fig. 15; coupling windings to the two inductors are employed to isolate the tuned circuits from the h.t. supply. In practice, additional precautions are necessary to eliminate the effect of the primary circuit capacitance.

The Round-Travis circuit offers no real protection against amplitude modulation. The audio output is proportional to Ix, where I is the input current, and x is a measure of the frequency shift. If there is amplitude modulation the magnitude of I varies, but if x = 0, i.e., if the signal is at the centre frequency there is no output due to a.m. For any other value of x, i.e., if the signal is mistuned or frequencymodulated, there is an output due to the amplitude modulation. Because the output is proportional to Ix the a.m. and f.m. signals are multiplied together and there is complete cross modulation. Thus a circuit of this type must be preceded by a limiter stage.

(To be continued.)

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Residual Magnetism in Recording Heads

MOST tape recorders incorporate a long-time-constant smoothing circuit in the h.t. supply to the bias oscillator to ensure that the h.f. current in the record/replay head dies away slowly when the instrument is switched off. This is necessary because any "d.c." component of remanent magnetism in the head is known to cause an increase in background noise from the tape.

Unfortunately, the amplitude of h.f. bias for best results from the point of view of either low distortion or high recording level is much less than is necessary to drive the core to a state of magnetic saturation, so that if by any mischance the magnetic state is carried beyond the maximum represented by the bias the head will not be automatically demagnetized.

Fortunately, the head can easily be demagnetized by field and then removing it slowly. This field can conveniently be provided by a small 50-c/s transformer with an air gap arranged to coincide with the gap in the recording head, but it is not too easy to devise suitable means with conventional components, due to the

wright and Weaire have recently developed a "defluxer" for this purpose in which projecting poles are arranged to give easy contact with the face of the record/playback head. The transformer is housed in a cylindrical case which falls conveniently to hand, and a Press-button switch is provided for operation.

The "de-fluxer," which can also be used for selective

erasure when editing tape records, costs £2 10s.

Portable Transistor Superhet

Home, Light and Third

With Currently Available Junction Types

By W. WOODS-HILL*

HEN it was discovered that Standard Telephones & Cables were in quantity production of a 500-kc/s junction transistor, it occurred to the author that if one of these could be made to oscillate up to 750 kc/s, then a medium- and long-wave superhet could be designed along the lines of the American "cigar case" portables. These vary in size from 6in \times 4in \times 2in to 5in \times $3\frac{1}{2}$ in \times $1\frac{3}{4}$ in.

The S.T.C. type TS3 transistors show a serious loss of gain above 450 kc/s, but if a low intermediate frequency of 275 kc/s is used, then sufficient gain can be obtained to drive the output stages. There is no problem about low-frequency amplification at 10 kc/s, and the 50 milliwatts required for normal room listening is within their power rating.

First attempts to make an oscillator of any frequency using some of the circuits described in American literature were disappointing. None of the six transistors available showed the slightest inclination to oscillate with the tuned circuit included in its emitter lead.

At last it was decided to revert to valve techniques, and a good beefy feedback winding was provided from the (output) collector to the oscillatory circuit. The last-mentioned had a direct (a.c.) connection back to the (input) base, and because the base has a rather low impedance this connection was tapped about \(\frac{1}{3}\) from the bottom. There was an immediate improvement, and oscillations were detected (a sound broadcast receiver does a good job as a wavemeter). Apart from altering the feedback tap on the oscillator coil so that it was just oscillating strongly enough at the high-frequency end of the band, and, of course, trimming off turns so that it covered the right frequency, no major alteration has been made to the circuit, which is shown in Fig. 2.

Various tapping points were provided on the coil

at 20, 40 and 60 turns, and it was found that all the six transistors provided could be made to oscillate up to 750 kc/s by increasing the feedback (more turns), and two of them above 750 kc/s. The better one of these two was earmarked for use in the receiver.

It is a good idea to build this oscillator on a tagboard and establish that it is functioning correctly and giving the right frequency coverage, rather than build the set "all in one go," because the parts used are small and difficult to alter in confined spaces.

The coil winding data in the table will give a frequency variation from 720 kc/s to 330 kc/s. This coverage, when used with a

275-kc/s i.f., will give the receiver a frequency range on medium waves from 330+275=605 kc/s to 720+275=995 kc/s. This includes the Third Programme at 640 kc/s, and the Home Service (Brookmans Park) at 900 kc/s.

Notice that this local oscillator is producing the 275-kc/s i.f. by oscillating below instead of above the signal as in the more conventional superhets. This will introduce a slight complication in the tracking arrangements—but a complication that is well worth while when it is realized that little selection of transistors is needed. In point of fact it is the fundamental reason why a superhet receiver covering most of the medium-wave band can be built using low-frequency currently available transistors.

The frequency changer is a quite straightforward stage consisting of a common (earthed) emitter amplifying stage (Fig. 1), where the signal at the aerial coupling winding is applied to the base, along with a small amount of r.f. from the local oscillator picked up by returning the bottom of the coupling winding to earth *via* two turns (L₃) wound round the earthy end of the oscillator coil.

Aerial Design

The ferrite aerial needs some explanation because it contributes greatly to overcoming the trouble in tracking.

Very roughly it can be said that the amount of signal picked up by a ferrite aerial is proportional to the bulk of ferrite enclosed by the tuning coil. That is to say, for maximum signal strength measured at the coupling coil the correct number of turns to resonate with the tuning capacitor should be loosely

^{*}The British Tabulating Machine Company.

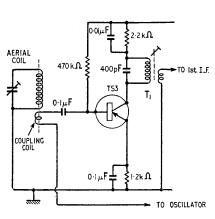


Fig. 1. Frequency changer circuit, showing input from oscillator.

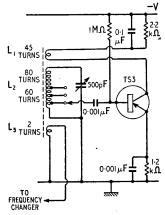


Fig. 2. Oscillator circuit with output to frequency changer.

Wireless World, January 1957

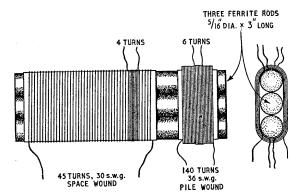


Fig. 3. Construction of the ferrite rod aerial, showing numbers of turns.

wound over the whole length of the rod. To obtain maximum bulk of material without excessive length three ferrite rods are stacked one above the other.

A certain price has to be paid for this increase in signal, inasmuch as the Q and selectivity of the circuit will be considerably reduced. On the other hand, to simplify tracking problems (which in this case can be stated as the aerial circuit failing to stay accurately in step with the local oscillator), what is wanted is a broad-band low-Q circuit which will ensure the signals are not seriously attenuated despite mistuning of the aerial circuit.

The ferrite rod aerial consists of three Ferroxcube rods of $\frac{5}{16}$ in diameter (Mullard type FX1495) and three inches long stacked one above the other and bound with Sellotape to hold them in place.

As shown in Fig. 3, the medium-wave winding consists of 45 turns of 30 s.w.g. insulated copper wire wound reasonably loosely, starting 1 inch from one end and occupying about 2 inches. This forms the tuning coil. The coupling winding consists of 4 turns of the same gauge wire wound in between the turns of the tuning coil, starting about 5 turns up from the bottom.

The last winding is the long-wave coil and is pile wound to cover about half an inch of rod right on the end farthest from the m.w. coil. This winding consists of 140 turns of 36 s.w.g. enamel- and cotton-insulated copper wire. The coupling coil here consists of 6 turns of the same gauge wire.

All these windings should be temporarily held in place and prevented from unwinding by small pieces of Sellotape stuck over the first and last turns of each.

As the electrical properties of ferrite rod vary slightly from sample to sample, adjustments to the number of turns may be necessary to optimize the frequency coverage and the rod should be tested before finally binding the whole length from end to end with tape. If the coils have been wound on a former of cartridge paper, so that the rods are a loose fit inside, then final adjusting of the tuning and tracking can be done by moving the coils along the rods. The centre of the rods gives maximum inductance.

The aerial has been made this shape to fit across the case of the receiver, and as it is possible that lengths this size may not be available, a word on how to cut the ferrite will not be out of place. The rod to be cut should be placed on a flat surface and held by hand. A nick should be made with a hack-

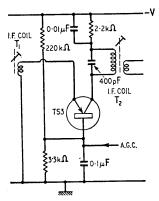


Fig. 4. An i.f. stage, showing the a.g.c. connection.

saw or Abrafile on opposite sides and then the rod broken simply by attempting to bend it by hand. This material is extremely brittle and any attempt to hold it in a vice or pliers will usually cause it to break at any other place but that required.

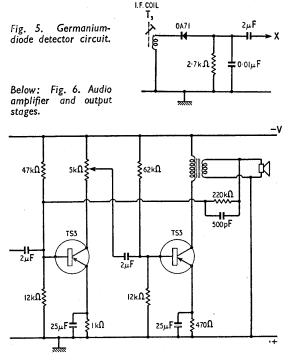
Coming now to the i.f. section, the frequency of 275 kc/s chosen was the result of a compromise between a high i.f. to

reduce whistles to a minimum and a low one that would give a useful gain from the transistors (which is well down at 500 kc/s).

The transistors were tried in a common (earthed) emitter circuit, which is theoretically capable of higher gain per stage than the common-base circuit finally chosen, but so much trouble was encountered due to instability (feedback within the transistor) and so many components were needed to neutralize this tendency to instability under varying battery voltages and temperature changes, that the loss in gain was considered a small price to pay. The circuit adopted is shown in Fig. 4.

I.F. Transformers

Because the input impedance of the transistors is so low compared with their output impedance, to obtain a correct match from stage to stage the i.f. transformers must give a ten-to-one reduction in



WIRELESS WORLD, JANUARY 1957

turns from primary to secondary. In fact the primaries have 330 turns while the secondaries have 33 turns. A slight increase of stage gain can be obtained by increasing the secondary turns, but above this excessive damping of the previous i.f. resonant circuit may occur and result in a decrease in gain. The secondary should be wound on the former first and the primary on top.

The detector circuit, shown in Fig. 5, is quite straightforward, consisting of a point contact germanium diode, Mullard OA71, connected as a

half-wave rectifier.

Because the input impedance to this stage is considerably higher than that of the common-base i.f. transistor stage, the secondary winding of the third and last i.f. transformer is increased from 33 turns to 50, so that a higher stage gain is available on this than the previous ones.

It should be noted that the 2.7-k Ω diode load is returned to earth, but in the full circuit diagram (Fig. 7) it is returned to the base of the first i.f. transistor to provide a.g.c. action. Whilst testing the i.f. stages it is best to return the resistor to earth because confusing results can be obtained with

strong signals.

A good way of adjusting the i.f. section is to build it as a separate exercise, complete with detector, and if no signal generator or oscilloscope is available, to connect a pair of headphones to point X and earth in Fig. 5, connect an aerial via a 25-pF capacitor to the first i.f. tuned circuit, and trim up on any available signal or noise within the range of the i.f. trimming (about \pm 25 kc/s).

The low frequency part of the receiver consists of two common-emitter transistor stages RC-coupled from the diode detector, with negative feedback applied at high and low frequencies.

Notice in Fig. 6 that the coupling capacitors should not be reduced much below $2 \mu F$ or a serious loss

at low frequencies will result. The 5-k Ω potentiometer used as a volume control forms part of the first amplifier collector load.

The negative feedback is taken from the speech coil of the loudspeaker, so that it covers distortion introduced by the loudspeaker transformer as well as that from the two low-frequency stages. Connection of this negative feedback should be left to the last, and if oscillations occur the sense of the transformer speech-coil winding should be reversed.

A miniature speaker transformer of the type usually sold with the $2\frac{1}{2}$ -in and 3-in speakers gives a tolerable match to the output stage as soon as the negative feedback is connected, but those patient enough can dismantle this and increase the secondary turns by 20% to improve the match.

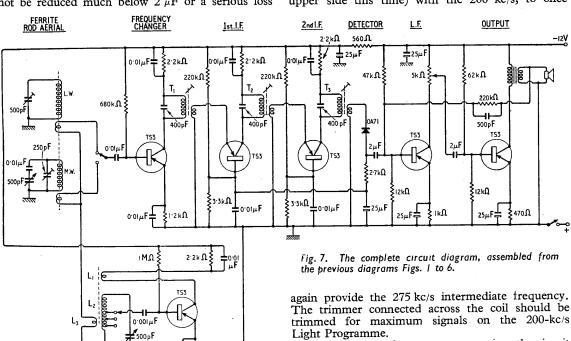
Complete Circuit

The complete design has been broken down into four separate stages because, to anyone tackling transistors for the first time, the effects caused by wiring mistakes or faulty components are unfamiliar, and can lead to the disconnection of each main portion as the only means of identifying whence the trouble originates, whilst in a thermionic-valve superhet the nature of the fault gives an immediate clue.

Notice in Fig. 7 how the long-wave coil of the ferrite rod aerial is brought into circuit by the coupling coil and the switch. When this winding is brought into circuit no alteration has to be made to the oscillator. A quick look at the frequencies involved will show why it is not necessary.

If reception is required on long waves of, say, the 200-kc/s Light Programme (which is the main reason for providing this range), then if the local oscillator is tuned to 475 kc/s, it will beat (on the upper side this time) with the 200 kc/s, to once

Coming now to the actual construction, the circuit was first built on a standard double-row tag strip with 30 tags down each side. As all resistors were



Wireless World, January 1957

OSCILLATOR

COIL WINDING DATA

Oscillator Coils

Former:— Aladdin ½in diam., 1in long with dust core.

L₁ ... 45 turns 36 s.w.g. cotton covered, wound

on first.

L₂ .. 140 turns 36 s.w.g. cotton covered, tapped at 20, 40 and 60 turns, pile wound next.

L₃ ... 2 turns 36 s.w.g. cotton covered, wound on last.

I.F. Transformers

Former:— Aladdin 4in diam., 1in long with dust core.

T₁ & T₂.. Secondary: 33 turns 36 s.w.g. cotton covered, single layer, wound on first. Primary: 330 turns 36 s.w.g. cotton

covered, pile wound on top.

T₃ .. Secondary: 50 turns 36 s.w.g. cotton covered, single layer, wound on first.

Primary: 330 turns 36 s.w.g. cotton covered, pile wound on top.

1/8 watt (mainly Erie type 16) and the largest fixed capacitor was a $25-\mu F$ miniature cathode bypass, no component short of the tuning capacitor needed any other support than that provided by soldering it into circuit. This enables all the units—i.f. stages, oscillator, frequency changer, output—to be tested under portable conditions before attempting to miniaturize.

Incidentally, if one decided to stop at this stage of development, having, say, built the receiver on two 6in tag strips, it would make a handy and economical portable, especially if a push-pull output stage using Mullard OC72 transistors were added.* Such an output stage would provide ample output to drive a 6in loudspeaker.

*See "Transistors for the Experimenter" booklet, obtainable free from Mullard. Note that the OC72s require only 6V. Suitable transformers can be obtained from Sobell.

It is not possible to be dogmatic about the final form of construction possible because this depends so much on each person's access to materials and miniature components. It can be stated, however, that the author has built two versions of the circuit shown. The first is constructed around the magnet of a 6-in loudspeaker utilizing full-size components throughout, with a push-pull output stage. This set is in constant use, and has a cabinet measuring The power supply consists of 7in \times 7in \times 3in. three flat 4.5-V torch batteries connected in series, and as these are designed to supply up to 300 mA to a bulb, the 25 mA average current drawn by the set is a very light load and many months of use can be obtained from three-shillings-worth of batteries.

The second version of the set is in a case measuring $5\text{in} \times 3\text{in} \times 2\text{in}$. The loudspeaker is a $2\frac{1}{2}$ -in Elac type and the supply battery is a 15-V hearing-aid (or flash-gun) type which drops to about 10V on load. Needless to say, this is the single-ended version of the circuit.

The author would like to advise readers again to be sure they have mastered the intracacies of the circuit before attempting to build it in a $5 \text{in} \times 3 \text{in}$ case, as the components will have to be packed side by side and sometimes in layers to get them all in.

Finally, the author was not in a position to evaluate the performance of the set in technical terms, but the following remarks will give readers a clue. Overloading of the output stage was possible in the London area on both the Third and Home Services, so long as the receiver was not used in a metal-framed building. The long-wave Light Programme was considerably weaker, presumably because the transmission originates in Droitwich. On the other hand, reception on this long wave was more consistent and suffered less from the screening effects of buildings. The volume level is more than adequate for listening in a room with no background noise, but if one wishes to hear the set above, for example, the conversation in a crowded room, then it is worth while adding the push-pull output stage.

Resistance - Current - Voltage - Power Nomogram

By B. E. JACKSON, B.Sc.*

ROBLEMS involving the relationships between the parameters resistance, current, voltage and power are constantly having to be worked out in electrical and electronic work. In most cases speed rather than accuracy is required. Therefore, a nomogram or a slide-rule-type calculator can profitably be employed.

Nomograms have had limited usefulness in this field in the past because (a) they have related only three of the four variables or (b) two settings of the rule have been required for a complete solution of the problem.

The nomogram presented here has the advantage that only one setting of the rule on the two known parameters is required to give the solution of the two unknowns.

For the convenience of those engaged in electronic

* Dominion Laboratory, Department of Scientific and Industrial Research, Wellington, New Zealand.

work the resistance scale is laid out in "preferred" values of resistors in addition to the ordinary logarithmic scale divisions.

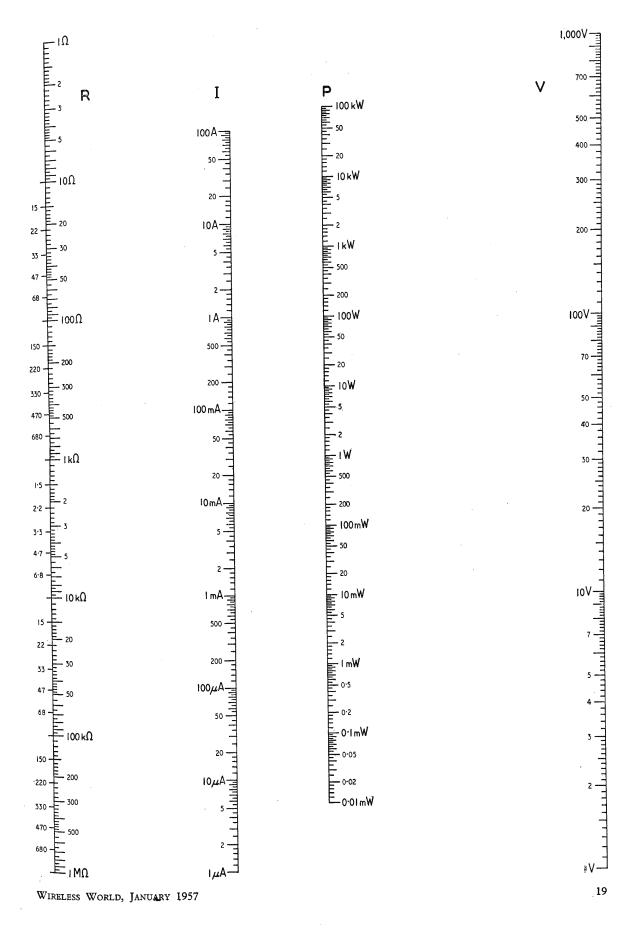
Of course, the nomogram can also be used in place of a slide rule for the occasional multiplication or division of numbers not connected with voltage, resistance, etc. For example, the product of two numbers can be read off the V line by setting the rule over the two numbers on the R and I lines respectively.

The use of the nomogram is so straightforward that only one example need be given:—

Q.—What is the current passing through a 10-kilohm resistor and what is the power dissipated when the voltage across it is 150 V?

A.—Lay a rule across the nomogram intersecting the R line at 10 kilohms and the V line at 150 V. Read off the current from the I line equal to 15 mA and the power off the P line equal to 2.25 W.

WIRELESS WORLD, JANUARY 1957



Is Radio Propagation

Non-Reciprocity and Circuit Asymmetry in Short-Wave Communication

HE old-time radio operator used a simple rule for his guidance in the establishment of communication with a distant station: "If I can hear him, he can hear me." To that, of course, should have been added a proviso regarding the necessity for exact similarity between the radiated power of his and the distant station, but, as it was, his rule often worked. Was it then based upon any scientific principle, or was it merely a piece of professional folklore? Some interesting experiments have recently been carried out which throw some light upon this, until lately, largely unsettled question.

Reciprocity in Radio Communication .- The meaning of the reciprocity theorem, as applied by Carson¹ to radio communication, may be expressed as follows: "If an electromotive force of a certain magnitude inserted in one aerial causes a current to flow at a certain point in a second aerial, then the same voltage applied at this point in the second aerial will produce the same current, both in magnitude and phase, at the point in the first aerial where the original voltage was applied." According to the statement of reciprocity by Sommerfeld2 this will happen regardless of the electrical properties and geometry of the intervening media and of the form of the two aerials. From this we should expect radio transmission in opposite directions over a distance to be truly reciprocal, as is the case with electrical phenomena in other forms of network, provided that no change occurs in the intervening medium with time. There is, in fact, no reason to doubt that the reciprocity theorem is true when applied to groundwave transmission, and it is only when sky-wave transmission occurs, where propagation is via an ionized medium in the presence of a magnetic field (the earth's), that it does not really hold. And in this latter case, which is that obtaining for all longdistance short-wave communication, though the possibility of non-reciprocal effects was realized by Carson, it does not seem to have been confirmed by experiment until recently.

It can be shown, however, that in certain special cases the theory of reciprocity should not hold. One of these is that where the wave travels through an homogeneous ionized medium along a magnetic meridian; i.e., along the direction of the magnetic lines of force, in which case the polarization of the wave twists in an anti-clockwise direction as it travels along, and, moreover, twists in the same direction whether going or coming, so to speak. The direction of twist is determined by the direction in which the magnetic force is acting, and not by the direction of propagation of the waves. In this case, if the direction of polarization of the wave when it leaves the transmitting aerial is the same in both the "go' and "come" directions then the propagation is still reciprocal, but if it is different in the two cases propagation is not truly so, there being a phase change at one end as compared with the other. It is even possible to find a case where the polarization changes are such that propagation is only possible at all in one direction. But these special cases may possibly have small significance in practical communication.

Of course if the "go" and "come" paths by way of the ionosphere were different in practical cases, as has sometimes been postulated, then the possibility of non-reciprocal effects would become more obvious, for there could be a differential factor in the ionospheric absorption for the two directions. However, it does not seem likely that waves travelling in opposite directions would, in fact, traverse different paths, and, therefore, that there would be differences in wave attenuation due to absorption.

In short, the possible effects of non-reciprocity in long-distance short-wave communication are by no means easy to assess, though, from operational data which has accumulated over the past several years, there is now no doubt at all that there can be differences in the performance of a radio circuit in the two opposite directions when the transmitting and receiving equipments at the two ends are similar. In other words, the rule of the old-time radio operator is not, essentially, a good one.

Tests for Reciprocity.—An experiment made to test the reciprocity of the 420-mile transmission path between Slough and Inverness by the D.S.I.R. has been described by Meadows3. Elaborate precautions were taken to ensure that the observed effects were due to the intervening medium, and not to any apparatus contributions. Pulse transmissions were used on a frequency of approximately 5.1 Mc/s, these being transmitted from and received at both terminals, the same aerial at each end being used both for transmitting and receiving, being switched from transmitter to receiver at the pulse repetition frequency. The received pulses were displayed on cathode-ray tubes, and the Inverness display was relayed by line to Slough, so that the two patterns could be visually compared there, and differences between the fading patterns of the ordinary E and F ray echoes observed. This was considered to be a sensitive test for non-reciprocity.

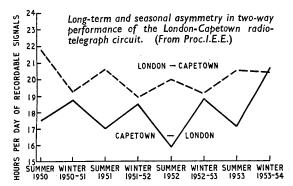
During about 15 hours of observation spread over 13 days definite non-reciprocal effects were observed for only about 1 per cent of the time. It was considered that this being so for this short path more pronounced non-reciprocal effects might occur on long-distance circuits, though probably they would be of short duration.

The results of a test for non-reciprocity over long-distance circuits are given by Laver and Stanesby⁴, who describe those obtained from a carefully controlled experiment conducted by the Post Office Engineering Department. The tests were made separately between the United Kingdom and the United States and between the United Kingdom and Australia on frequencies between approximately 11 and 14 Mc/s. At each end of these two circuits a single aerial was used, switchable to a transmitter or to a receiver tuned to the same frequency. Un-

Always Two-Way?

By T. W. BENNINGTON*

modulated carrier was transmitted alternately for two minutes from either end of the circuit. output signals from the receivers were recorded and the results were expressed in terms of circuit loss, the aim being to obtain the loss difference between transmission over each circuit in one direction and that in the other. At times there was no significant loss difference, but quite often for periods of a few hours loss differences, indicating non-reciprocal transmission, did occur. On the average the loss was greater for transmission from the United Kingdom to the United States and to Australia, than for transmission from those two countries to the United Kingdom. At times the loss difference for transmission in the opposite directions rose to values of the order of 5 to 10 dB. The reality of the test



results seems to be well proved by the fact that on some days no appreciable loss difference occurred, though on the previous days, with test conditions exactly the same, considerable loss differences occurred persistently.

These two valuable experiments, one over a relatively short and one over two long transmission paths, do therefore seem to prove that non-reciprocal effects are of some importance in long-distance communication via the ionosphere. They do not fully show, however, to what phenomenon the non-reciprocal effects are due, nor indicate the long-term significance of such effects. We may perhaps tentatively conclude that true non-reciprocity may not be the *major* cause of the operationally observed differences in long-distance circuit performance in opposite directions.

Circuit Asymmetry.—It has for some long time been realized that, since the distribution of atmospheric noise is not uniform over the earth's surface, but tends to be greatest in the equatorial land regions, and to vary at all places with time of day and season, the signal/noise ratio for a signal of given field-strength must vary for different geographical locations. That being so it follows that, quite apart from the effects of non-reciprocity, the

performance of a radio circuit would not necessarily be the same in two opposite directions if judged on the basis of the signal/noise ratio at the receiver inputs. Or, to put it into operational terms, the percentage of time for which a long-distance radio circuit was "commercial" or "uncommercial" would not necessarily be the same at the two opposite circuit terminals even if the transmitting and receiving equipments were identical. As has been said, such circuit performance differences have long been noted, and more light has now been thrown upon the subject by a recent study made by Humby and Minnis⁵. In order to distinguish it from the effects of non-reciprocity they have called the phenomenon in question "circuit asymmetry."

In examining the performance of a number of long-distance circuits, in terms of the number of commercial hours per day or days per month, they found that, in the cases where one terminal was in the northern and one in the southern hemisphere, a circuit performance deterioration in occurred during local summer. Since the time of local summer in these cases is displaced by six months as between the two opposite circuit terminals, this means that the performance varies in anti-phase at the two terminals over the year. Even if no other difference were present this leads to a differential in the circuit performance as between the "go" and "come" directions; in other words, to a seasonal asymmetry. (See accompanying diagram.) But, superimposed on this, there may be a consistently worse performance in one direction than in the other; i.e., a long-term asymmetry. Where both terminals were in similar latitudes in the northern hemisphere, where the seasons are coincident at the terminals, there was no evidence of seasonal asymmetry, though a component of long-term asymmetry might still be present.

These results are exactly what would be expected from a consideration of the likely signal/noise ratio, taking into consideration the local variations in atmospheric noise. This is, of course, much higher in summer than in winter, and varies geographically in a manner such that, generally speaking, its intensity is an inverse function of latitude. Thus, even with non-directional aerial systems such asymmetrical conditions would occur. But the communication systems in question used relatively sharply directional aerials, "beamed" in the direction of the distant terminal, and the authors have probed the matter further in view of this.

In considering the diurnal variations in circuit asymmetry, over several circuits where one terminal was in the United Kingdom and the others at places near or south of the equator, they found a marked tendency for the asymmetry to increase; i.e., circuit performance at the United Kingdom end to deteriorate, at a certain time GMT for each circuit, which time varied for the different circuits so as to become systematically later as the circuit direction varied from the east towards the west. This

^{*} Research Dept., British Broadcasting Corporation.

was particularly marked in the northern summer. The time of this increase in circuit asymmetry was, in fact, found to be at approximately similar values of local time at the distant terminal; i.e., between about 1850 and 2020 Local Mean Time. The implication was that towards and after local sunset at some place within the main beam of the receiving aerial, in the direction of the distant terminal, there was a significant increase in the atmospheric noise, such that the signal/noise ratio at the United Kingdom end of the circuit sharply decreased, and that as the sunset line moved from east to west over the circuits so the circuit asymmetry increased at increasing values of GMT, according as the direction of the circuit became farther to the west.

Atmospheric noise should be regarded as being primarily a meteorological phenomenon, being due to the lightning strokes in thunderstorms. The conditions for the production of thunderstorms are intimately bound up with the heating of the air by conduction from the earth under the influence of the sun's rays. Thus peak thunderstorm activity occurs in the late afternoon and evening, and, when the ionospheric conditions for the transmission of the noise over a distance are taken into account, it appears that a directional receiving aerial would tend to pick up the highest level of noise from an area lying slightly west of the sunset line. This enabled the authors to locate approximately the position of the noise sources responsible for the deterioration in circuit performances at the United Kingdom end of the circuit, for each of the circuits being examined, and a scrutiny of the receiving

operator's logs confirmed that there was an increase in the atmospherics at about the times expected.

Thus, it may be concluded, there is, at certain times of day, a deterioration in circuit performance over long-distance circuits in the direction in which reception is taking place in local summer, thus leading to a pronounced tendency for circuit asymmetry to occur. In addition, there may be long-term asymmetry, due to consistent differences in the local noise levels and, possibly, to other differences in conditions at the receiving terminals. Of the two effects of non-reciprocity and circuit asymmetry it would seem that the latter is responsible for the *major* differential effects observed in practice for transmission in opposite directions over a circuit, at least when the two terminals are located in widely different latitudes.

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BOOKS RECEIVED

Vacuum Tube Circuits and Transistors by L. A. Arguimbau. New edition of textbook dealing with the circuitry of radio communications, now including chapters on transistor devices and circuits by R. B. Adler. The treatment throughout is based on fundamental physical principles. Pp. 648+IX; Figs. 612. Price 82s. Chapman and Hall, 37, Essex Street, London, W.C.2.

Quartz Crystals as Oscillators and Resonators by D. Fairweather, A.M.I.E.E. and R. C. Richards, Assoc.I.E.E. Monograph on the types of crystal cuts available and their practical applications in the control of frequency, with particular reference to preferred circuits and their design. Pp. 54; Figs. 52. Price 7s 6d. Marconi's Wireless Telegraph Co., Ltd., Chelmsford, Essex.

Proceedings of the Conference on Radio Interference Reduction (Chicago, December 1954). Subjects discussed include techniques for suppression in motor cars, aircraft and ships; design of screening; susceptibility of receivers to pulse interference; spurious radiation from transmitters; corona interference in aircraft; measurement techniques. Pp. 352+V; Figs. 170. Price \$6.00. Armour Research Foundation, Dept. E, 10 W. 35th Street, Chicago, Illinois.

Television Programming and Production by Richard Hubbell. Revised and enlarged third edition of a handbook on camera technique, staging and sound effects written primarily on the basis of American practice, with a chapter on British television programmes. Pp. 272; Figs. 18. Plates 117. Price 32s. Chapman and Hall, 37, Essex Street, London, W.C.2.

Basic Electricity by P. B. Zbar and S. Schildkraut. Instruction manual for a series of laboratory experiments to familiarize radio technicians with measurements on simple d.c., a.c., and r.f. circuits. Pp. 84; Figs. 113. Price 13s. McGraw Hill Publishing Co., Ltd., 95, Farringdon Street, London, E.C.4.

Handbook of Basic Circuits by M. Mandl. Selection of 136 basic circuit elements, arranged in alphabetical order for easy reference, indicating their application in sound or television receivers and describing their purpose and function. Appendices give block diagrams of representative complete equipments. Pp. 365; Figs. 164. Price 52s 6d. The Macmillan Company, 10, South Audley Street, London, W.1.

Profitable Radio Troubleshooting by W. Marcus and A. Levy. American treatise on servicing from both the technical and business points of view. Pp. 330; Figs. 153. Price 34s. McGraw Hill Publishing Co., Ltd., 95, Farringdon Street, London, E.C.4.

Commercial Broadcasting in the British West Indies. Detailed account produced by Central Rediffusion Services, Ltd., of the organization and distribution of programmes in the main islands by medium-wave, v.h.f. and wire. Pp. 91; Figs. 31. Price 5s. Butterworth Scientific Publications, 88, Kingsway, London, W.C.2.

Dictionnaire Français-Anglais, by H. Piraux. Complementary volume to the English-French dictionary previously published, giving equivalent terms relating to electronic and electrotechnical subjects. Pp. 186. Price 960 Fr. Editions Eyrolles, 61, Boulevard St. Germain, Paris, 5.

RCA Transmitting Tubes. Manual of valve characteristics covering anode, ratings up to 4 kW, with an introduction on circuit design considerations and recommended operating conditions. Pp. 257. Price 12s. RCA (Gt. Britain), Ltd., Lincoln Way, Sunburyon-Thames, Middlesex.

The Gated-Beam Valve

By LAWRENCE W. JOHNSON* Its Use as Limiter and Discriminator for Frequency Modulation Reception

ADVANCES in the art of frequency modulation reception seem all too often to come about only as a result of advances in allied, higher-powered fields. Exceptions to this rule do exist—for example, the M.I.T. work on multi-path transmission^{1,2}—but it is safe to say that if it were not for radar and television, the low-noise front ends and compact i.f. amplifiers used in modern f.m. receivers would not be available. It is the purpose of this paper to describe the 6BN6 gated-beam tube, a television development which bears out the original contention. To the designer of f.m. tuners and receivers it brings a very useful tool in improving performance or in lowering price, whichever objective may be the more important.

The 6BN6 was developed in the laboratories of the Zenith Radio Corporation, by a group led by Dr. Robert Adler, and was first put into production by the General Electric Company (U.S.). The basic ideas were not new, but Adler's work seems to have been the first to combine them all successfully. The prime purpose of the development appears to have been the simplification of the sound channel of television receivers. When the 6BN6 is so used it takes the place of the limiter, discriminator, and first audio stages, and at the same time eliminates the rather complicated phase discriminator or ratio detector transformer, substituting in its place a simple inductor resonant at the intermediate frequency3,4. The resulting f.m. detector does not meet the requirements set forth for an exceptionally high capture ratio², but its performance equals or surpasses that of the commonly encountered ratio detector or single-limiter/discriminator. In some high-quality f.m. tuners the 6BN6 is employed as a broad-band limiter only, and is followed by a separate broad-band detector to assure a good capture ratio.

Counter Discriminators

Understanding the operation of the 6BN6 is not difficult if one falls back upon previously explained phenomena and circuits. Roddam⁵ and Scroggie⁶ have done much to familiarize readers of this journal with low-frequency versions of the counter type of discriminator, which presents several intriguing advantages, but also imposes limitations on bandwidth because of the necessarily low intermediate frequency. The 6BN6 may be thought of as a way of utilizing the same general principle as that of the counter discriminator, at an almost arbitrarily high intermediate frequency. This last-mentioned property might seem to provide a large advantage over other counter-discriminator systems in that an excellent capture ratio would seem to be within reach. That this is not completely true will be discussed in detail later; envelope for envelope, however,

*Hewlett Packard Company, Palo Alto California.

the 6BN6 still provides several points of superiority over practical counter detectors.

The conventional counter detector utilizes the principles of pulse position modulation (p.p.m.); it is supposed, ideally, to put out one pulse for each cycle of the incoming frequency-modulated voltage. It is assumed that the output pulse will have a standard height, duration, and shape, regardless of the input frequency and amplitude. The resulting train of pulses, identical in all respects save spacing, can be passed through a low-pass filter, at the output of which will appear the desired audio signal representing the demodulated wave. Fig. 1 shows an f.m. wave and an idealized counter detector's action. It is only a simple step to consider instead a system where the "duty cycle" (ratio of pulse duration to the full repetition period) instead of pulse spacing is varied. This is the scheme which the 6BN6 detector employs. Current pulses are formed which have standard height, rise time, and fall time; they vary in both width and spacing, but the significant fact is that the duty cycle, nominally 25% with no modulation, is made to vary in accordance with the deviation of the instantaneous input frequency from the fixed intermediate frequency. As before, the current pulses are passed into a low-pass filter, which yields an output proportional to duty cycle, thus conveying the desired modulation intelligence.

Dual Control Grids

The details of the manner in which the 6BN6 accomplishes these functions are fairly straightforward. For the present let it suffice to say that the 6BN6 has two control grids, well-shielded from each other, both of which are capable of cutting off anode current, and whose dynamic ranges are both quite small. Thus an alternating voltage on either electrode of a few volts amplitude, peak-to-peak, will cause

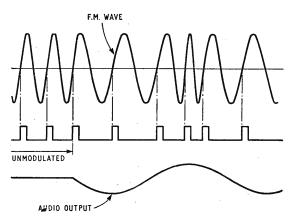


Fig. 1. Principle of the pulse counter detector.

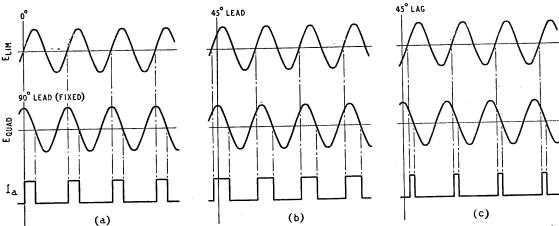


Fig. 2. Variation in pulse duty cycle for changes of phase between the limiter and quadrature grids. Anode current is assumed to flow only when both grids are positive.

pulses of anode current to flow as the electrode voltage is carried from cut-off to saturation and back. For reasons that will be clear later, the closer of the two grids to the cathode is called the limiter grid, and the other is called the quadrature grid.

Suppose now that an unmodulated signal is applied to the limiter grid, and that the same signal, advanced in phase by 90 degrees, is applied to the quadrature grid. (The reason for the name may now be growing apparent.) If the amplitudes of the two voltages are sufficient, either by itself would suffice to form pulses of anode current, and if one or the other were of zero amplitude, the other would cause the anode current duty cycle to be 50%. Fig. 2(a) shows how, with the application of voltages 90 degrees apart, the anode current duty cycle would be reduced to 25%. For simplicity, current is assumed to reach the anode only during the portion of the signal cycle when both grids are positive.

What happens if the phase of the voltage applied to the limiter grid is varied, while that of the voltage applied to the quadrature grid is kept steady as in the initial example? If the phase of the limiter grid voltage is advanced by 45 degrees, the anode current pulses will be as shown in Fig. 2(b); the duty cycle has been increased to 37½%. Alternatively, if the phase of the limiter grid voltage is retarded by 45 degrees, the anode current pulses will be as shown in Fig. 2(c); now the duty cycle has been decreased to $12\frac{1}{2}\%$. Bear in mind that Fig. 2 is for a voltage of constant frequency and unchanging phase applied to the quadrature grid, with variation only of the phase of the voltage applied to the limiter grid; these conditions are exactly what might be encountered in a phase detector. That is, such a circuit would provide a d.c. output that would vary in proportion to the phase difference between a variable-phase carrier-frequency input and a fixedphase carrier-frequency reference input. The line between phase and frequency is a hazy one; if, for example, one speaks of a continuously changing phase, one may equally well speak of a frequency shift. Thus it is that phase detectors and frequency modulation detectors often have very similar circuits.

The 6BN6 phase detector can be used almost without change as a frequency modulation detector; it is necessary only to arrange somehow to supply an appropriate reference voltage to the quadrature

grid. The signal to be detected will be applied to the limiter grid; a convenient result of the narrow dynamic range of the limiter grid is that amplitude modulation of the input signal will have little effect on the timing of the anode current switching.

Practical Circuit

Fig. 3 shows the circuit actually used in the 6BN6 f.m. detector. The representation is drawn in the fashion of a pentode; more physical detail will be given later. The limiter grid is that nearest the cathode, while an accelerator or screen grid is between the limiter and quadrature grids. The signal to be detected is connected to the limiter grid, a moderately-high-Q resonant circuit is connected to the quadrature grid, a typical screen grid voltage is applied to the accelerator, and to the anode are attached a load resistor, an integrating capacitor (to earth), and a coupling capacitor (to the audio amplifier). With this circuit configuration, consider the situation when a signal is applied of the same frequency (the intermediate frequency of the receiver)

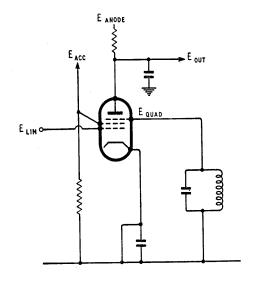


Fig. 3. Basic circuit of gated-beam limiter discriminator.

WIRELESS WORLD, JANUARY 1957

as that to which the coil in the quadrature grid circuit is tuned. Under these conditions there is space charge coupling to the quadrature grid circuit as a result of the pulses of current passed by the limiter grid. There results a current in the quadrature grid circuit whose frequency is that of the current pulses, and whose amplitude is broadly frequencydependent. Thus there is produced a voltage from quadrature grid to earth at the input frequency, of amplitude sufficient to carry the quadrature grid considerably past the cut-off and saturation limits, so that the pulses of beam current produced by the limiter grid will be further modified before they become pulses of anode current. Just how they are modified is determined by the phase difference between the limiter and quadrature grid voltages. The quadrature grid circuit situation is analogous to that of a parallel resonant circuit fed through a small capacitive reactance; at resonance the voltage across the resonant circuit leads the current by 90 degrees, and at frequencies near resonance the lead angle is given by an approximation quite accurate for frequency deviations of 75 kc/s or less, and for The approxiquadrature inductor Qs of 35 or less. mation states that

$$\phi = \frac{\pi}{2} - 2Q \cdot \frac{\Delta f}{f_0}$$

where ϕ is the lead angle in radians, Q is the figure of merit of the quadrature coil, f_0 is the intermediate frequency to which the quadrature coil is tuned and Δf is the deviation of the input frequency from f_0 .

Linearity

From this relation it is clear that the anode current duty cycle is 25% when the input frequency is equal to the intermediate frequency. And further, as the input frequency is varied, it is clear that the phase difference varies in a linear fashion, producing a linear variation in duty cycle of the anode current pulses, along the lines of what was described earlier for the 6BN6 phase detector; for a frequency above the intermediate frequency, the duty cycle is less

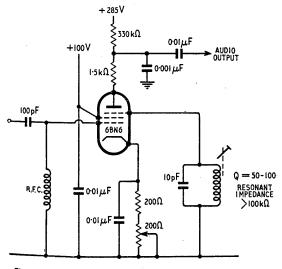


Fig. 4. Practical circuit with component values for the 6BN6 valve.

TABLE I

6BN6—Limiter-Discriminator Characteristic	s and Typical			
Operation				
Input-signal centre frequency	10.7 Mc/s			
Frequency deviation	\pm 75 kc/s			
Anode supply voltage	285			
Anode voltage	122			
Accelerator voltage	100			
Cathode-bias resistor (variable)*	200 to 400 ohms			
Anode load resistor	330,000 ohms			
Anode linearity resistor	1500 ohms			
Integrating capacitor	0.001 μF			
Coupling capacitor	0.01 μ F			
Minimum signal voltage for limiting action (r.m.s.)†	2,0			
Average d.c. anode current	0.49 mA			
Accelerator current	9,8 mA			
Input signal level for a.m. rejection adjustment*	2.0 volts			
A.M. rejection at $E_{sig} = 2.0$ volts (r.m.s.) A.M. rejection at $E_{sig} = 3.0$ volts (r.m.s.)	20 dB			
A.M. rejection at $E_{sig}^{sty} = 3.0 \text{ volts (r.m.s.)}$	29 dB			
Total harmonic distortion	1.6 %			
. Peak audio output voltage	16.6			
*The cathode resistor should be adjusted for maximum a.m.				
rejection in the output of the limiter discriminator stage at the				
specified signal level. a.m. rejection is measured with an applied				
signal containing 30% a.m. and 30% f.m.				
†At signal levels above specified value, limiting	g is within \pm 2			

than 25%, and for a frequency below the intermediate frequency, the duty cycle is greater than 25%. This fortunate situation has resulted from quadrature circuit phase changes resulting from forced oscillations excited therein by means of space charge

coupling from the beam current.

As before, the desired audio signal can be recovered by means of an integrator or low-pass filter. Appropriate choice of low-pass filter components can provide simultaneous de-emphasis, yielding further simplification of the circuit. The values shown in the detailed circuit of Fig. 4 are designed to com-75-microsecond pre-emphasis, pensate for the standard in the U.S. Also shown in Fig. 4 is an additional linearity resistor between anode and integrating capacitor. This resistor, by permitting an appreciable component at carrier frequency to exist at the anode, modifies the phase and amplitude of the quadrature grid voltage by feedback through the quadrature-grid-to-anode capacitance in such fashion as to improve linearity considerably. This resistor also has some effect on the amplitude of the output voltage, and on the a.m. rejection capabilities of the circuit, so that its value represents compromise between conflicting requirements. Table 1 gives the characteristics and typical operation furnished in the manufacturer's technical data manual7, from which the circuit of Fig. 4 was

Simple Adjustment

Alignment of the circuit turns out to be admirably simple. The quadrature coil is tuned for maximum audio output, and the cathode resistance is adjusted for optimum a.m. rejection. Both these adjustments can be made without a signal generator; in fact the latter is very easily made when receiving a weak station in the presence of impulsive noise interference. It is important to note that symmetry of the tuning characteristic will be adversely affected unless anode current without signal equals anode current with an unmodulated signal. Thus the use of other supply voltages than those listed will require that the value of anode resistor be adjusted. It is desirable in addition that the accelerator be fed from a low impedance source.

A cross section of the 6BN6 electrode structure is shown in Fig. 5. Note that the limiter grid is almost

completely enclosed by a structure at cathode potential, which in turn is almost completely surrounded by the accelerator. Note also that the anode and quadrature grid are almost completely enclosed in another structure at cathode potential. With such a structure it should not be surprising that the direct capacitance between quadrature grid and limiter grid is less than 0.004 pF. The limiting action of both grids is accomplished by means of carefully planned electron-optical conditions. Either grid will draw no more than 0.5 mA no matter how far positive it may be driven, and the box structure, combined with the sheet-beam resulting from careful electrode layout, yields a sharp cut-off characteristic. In fact, as long as the signal applied to the limiter grid is above about two volts r.m.s., the space current which passes out of the accelerator is carried rapidly from zero to the saturation value; consequently the name limiter grid is justified, for any larger amplitude of input voltage will only sharpen the transition from zero to the saturation value.

The Q of the quadrature coil can vary between fairly broad limits. On the one hand, it must not be too sharply tuned, or the amplitude of the quadrature voltage may drop off at large deviations, and the phase deviation may depart from linearity. On the other hand, it should not be too broad, since there is then danger of insufficient quadrature grid voltage as a result of the reduced quadrature coil voltage. As a practical matter to insure continuity of operation with valve replacement, the manufacturer recommends that a total of at least 10 pF of capacitance be used across the quadrature coil. Needless to say, careful shielding of the quadrature circuit is necessary, especially from the input circuit to the limiter grid. Broadening the quadrature coil tuning will aid in broadening the bandwidth of the 6BN6 detector, but it appears that the practical upper limit will still not permit its use in a design which calls for a two- or three-megacycle detector bandwidth. Nevertheless the circuit fits well the requirements of low cost receivers, since it will still provide a greaterthan-normal bandwidth while providing a high output voltage, thus contributing to the simplicity and low cost of such a receiver while keeping quality reasonably high.

Use as Limiter

The characteristics of the limiter grid suggest that the 6BN6 can be profitably employed as a pure limiter. This is in fact the case. For use as a limiter the manufacturer suggests that the quadrature grid should be connected to the anode if the maximum amplitude of output voltage is desired, or to earth if limiting on the smallest possible input signal is Particularly desirable in a limiter is the characteristic of the 6BN6 that results from its electron-optical design; limiting does not depend on flow of grid current, nor in any way on biases determined by signal levels. Thus there are no time constants associated with the limiting action, which cannot be said to be true of the familiar pentode limiter, or even of some diode limiters. Thus the 6BN6 provides improved immunity from impulse interference and from rapidly changing signal levels, in contrast to the pile-up effect characteristic of pentode limiters. These several advantages have led to the appearance of the 6BN6 as a limiter in several high-quality f.m. receivers. It may be that

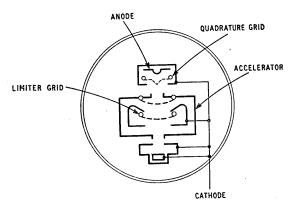


Fig. 5. Cross-section of electrode structure in the 6BN6 valve.

its failure to appear as a limiter-discriminator in inexpensive tuners is attributable to a stigma based on its television cost-cutting background. Such a reluctance is certainly not justified, since the 6BN6 when properly used can out-perform the presently popular ratio detectors and discriminators used in inexpensive equipment.

A detailed study of the gated-beam limiter at M.I.T.8 bears out the conclusions stated above about the excellence of its properties. The study recommends separate control of the biases on limiter and quadrature grids for optimum adjustment of limiting characteristics. This appears to be desirable because of variations in characteristics from valve to valve. Cascaded 6BN6 limiters with earthed quadrature grids were used in the Cross-Paananen receiver developed at M.I.T. 9,10, and mentioned in an earlier article in this journal².

A recently announced R.C.A. development¹¹ seems to be very similar to the 6BN6 detector circuit described above. The circuitry is essentially identical, but the operation differs in that the detector is normally oscillating, and only for strong signals does the oscillation cease. For weak signals the action is along the lines of the locked-oscillator detector, developed and used some years ago¹². There is no indication that the 6DT6, the special pentode developed for this circuit, possesses the electron-optical limiting characteristics of the 6BN6. It is possible that a marriage of the two schemes, combining the good features of both, would prove interesting. Presumably such an approach would involve modifying the 6BN6 circuit so that it would oscillate for low values of input signal.

D.C. Component

There is a characteristic of the 6BN6 detector that may be considered by some to be a disadvantage. There is present at the anode a d.c. voltage which varies in the fashion required for control of an automatic frequency control circuit, except for the fact that the voltage level for centred tuning is not zero but is instead of the order of 100 volts. This makes difficult, but not impossible, the job of designing an a.f.c. circuit, the need for which might better be counteracted by devoting care to the design of the local oscillator.

Tuning meters can easily be used with the 6BN6 circuit; the limiter grid current, never greater than one half milliampere, is a wonderfully sensitive

aid in tuning weak stations, while for strong stations the grid current of the preceding intermediate frequency amplifier stage—which would be the logical source of automatic gain control voltage in a 6BN6 receiver—provides a sensitive indicator. The provision of a zero-centre on-channel indication falls in the same category as providing a.f.c., however.

Modification of existing equipment to employ the 6BN6 as a limiter-detector is quite practical, and

in most cases will yield an improvement.

Existing limiters can be converted to additional intermediate frequency amplifier stages by appropriate adjustments of their operating conditions, and the discriminator or ratio detector transformer can often be converted into a driver transformer for the 6BN6 limiter grid. Room for a shielded quadrature coil must be located. The d.c. resistance in the 6BN6 limiter grid circuit should be kept under 200 ohms, lest the flow of grid current upset bias conditions. The results of such a modification will generally be as follows: sensitivity will be increased, noise rejection will be improved, alignment will be easier, and tuning will be easier. This last feature is perhaps as welcome as any of the others. It results from the fact that the broader-than-usual bandwidth of the 6BN6 detector effectively eliminates the threepoint detection usually encountered, substituting instead a broad region of smooth tuning with noisy regions on each side which result from slope detection in the intermediate frequency amplifier and consequently present a highly amplitude-modulated signal to the limiter grid. This tuning characteristic makes it convenient to design an inter-station squelch circuit activated by the super-audible components present in the inter-station noise.

In closing it might be noted that many applications other than those mentioned have been found for the 6BN6. It is useful as a clipper, square-wave generator, frequency multiplier, gated amplifier, coincidence circuit, slicer, or multivibrator. And finally, it seems to be the only tube which can be self-biased to anode-current cut-off.

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Modernizing T.R.F. Television Receivers

By P. F. CUNDY, A.M.I.E.E.

OLLOWING the article by G. J. Conway in the November, 1956, issue, it is worth while considering another method of converting Channel-I "straight" vision receivers to Crystal Palace single-sideband transmissions, and at the same time introducing Band III reception.

In simple terms this method is to change all sound channel circuits and traps from 41.5 Mc/s to 38.15 Mc/s, the vision circuits from 45-48 Mc/s to 34.65-37.65 Mc/s, and to add a multi-channel tuner in front. The previous signal-frequency sound and vision stages are thus converted to the standard recommended British intermediate frequencies, and any tuner with the "standard" i.f. output will do.

This treatment can be applied to "straight" sets in each of the following circumstances:—

(1) Upper-sideband types.

(2) Double-sideband types.

(3) Lower-sideband types when a simply added Band-III converter cannot be used because of 45 Mc/s re-radiation from the receiver or because of direct 45 Mc/s pick-up.

In most cases the existing trimming arrangements on the sound channel cater for the change from 41.5 Mc/s to 38.15 Mc/s (which is about 8%) and this is also true of the sound traps. Sets of type 2 and 3 would have had sufficient sound attenuation in their existing trap circuits to make alterations (other than tuning) unnecessary.

In general, type 1 receivers will need at least one additional sound trap. This can be made and fitted in exactly the same manner as described by Conway, but, of course, designed to resonate at 38.15 Mc/s.

With the vision circuits, the change in frequency required is up to 22% and this is usually well outside the range of the existing trimming facilities. The simplest way to lower the frequency of these circuits is by additional capacitance. A value of 6.8 pF is the best starting point and capacitors of this value should be connected from anode to earth and from grid to earth of each valve handling vision-frequency signals. Care must be taken that these capacitors and the leads to them are positioned so that the anode-to-grid capacitances of the amplifying valves are not augmented by excessive external feedback, or stability will suffer.

During alignment it may turn out that the 6.8-pF capacitor is either too large or too small. In this case it should be changed for a 4.7-pF or a 10-pF capacitor, but 6.8 pF will be right for at least 75%

of the requirements.

The added capacitance increases the selectivity and this could be troublesome. It is not worth while, however, changing damping resistors where they exist and are $10\,\mathrm{k}\Omega$ or less. To any circuits which in the original condition were not provided with damping resistors, values of $15 \,\mathrm{k}\Omega$ or $22 \,\mathrm{k}\Omega$ may be

On the question of alignment procedure it is impossible to give any specific advice. If carried out by somebody who has an instinct for this kind of thing it is not difficult, but in the absence of an oscilloscope and sweep generator it can be tedious. A good starting point is to align all circuits on 34.56 Mc/s and then raise the frequency of twothirds of them slowly, leaving one-third at about 36.15 Mc/s and pushing the remaining one-third as near 37.65 Mc/s as possible without running into sound-on-vision. It should be borne in mind that the sound rejectors may require some re-adjustment in the process.

Acceptable performance should always be achievable, with bandwidths of 2 Mc/s in all cases and 2.5 Mc/s quite often. Users of the well-known Pye 45 Mc/s strip will find the conversion satisfactory, and because of the large number of tuned circuits it is possible to avoid the use of sound traps. Responses 3 dB down at 37 Mc/s, 15 dB down at 37.5 Mc/s and 30 dB down at sound carrier frequency can be achieved by tuning adjustment alone.

Gain lost in adding capacitors and damping resistors to amplifying stages will be more than made up by the tuner. Since few of the receivers will have provision for any form of a.g.c., adjustment of contrast control on changing channels will usually be

necessary.

Good results have been obtained with the conversion of several receivers, both commercially-made and home-constructed. The Cyldon "Teletuner" and home-constructed. has been used successfully, and also the G.E.C. type BT205 adaptor and a home-built tuner.

Transatlantic Television

BRIEF mention was made in last month's "World of Wireless" of the successful reception of B.B.C. television transmissions in the United States. Since then, further details of the reception arrangements have been given to Wireless World by Dr. H. R. L. Lamont, European technical representative of the Radio Corporation of America.

The main receiving aerial is a horizontally polarized rhombic (mounted on 50-ft wooden poles) with an overall length of 329ft. The side angles are 142° and the side lengths 173ft. The aerial is designed for our Channel 1, with the main lobe 7° above the for each in the great circle azimuth of London. The far end is terminated in 800 ohms with the near end working into a 50-ft length of tapered impedance matching transformer. This feeds through approximately 100-ft of 300-ohm balanced line to the receiving equip-

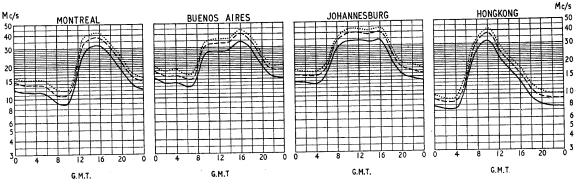
From the transmission line a 300- to 75-ohm balun, having less than 1 dB loss, a standing-wave ratio of less than 1:1.2 and a balanced to unbalanced ratio greater than 18 dB, is used. The pre-amplifier has a noise factor of 5 dB or less and a gain of approximately 25 dB. A network designed to reduce interference from strong offchannel stations is in the circuit after the pre-amplifier. Thereafter, the signal is fed to two Ekco T283 receivers. Two receivers are used because, with weak signals and intereference, optimum sound tuning does not always correspond to optimum picture tuning. Both receivers been equipped with cathode-follower output systems, vision being taken from the second detector and sound from the loudspeaker speech coil circuit. The vision signal is then fed to a microwave relay system for transmission to the NBC Laboratory in New York, a distance of 70 miles from the receiving station at Riverhead, Long Island. Sound is conveyed by line.
In New York another Ekco receiver with an additional

amplifier having a gain of approximately 10 to 1 is installed. Output from the amplifier is d.c.-restored by means of a diode where it is applied to the regular vision amplifier within the receiver. The received picture is then re-televised by a Vidicon camera chain operating from an RCA sync generator. The camera utilizes a 25-mm, fl.4 lens, and with this lens is capable of 600-line

horizontal resolution.

Although recognizable signals have been received there has been considerable interference and multipath effects.

Prediction for January **CONDITIONS** SHORT-WAVE



THE full curves given here indicate the highest frequencies likely to be usable at any time of the day or night for reliable communications over four longdistance paths from this country during January.

Broken-line curves give the highest frequencies that

will sustain a partial service throughout the same period.

****** FREQUENCY BELOW WHICH COMMUNICATION SHOULD BE POSSIBLE FOR 25% OF THE TOTAL TIME

- PREDICTED AVERAGE MAXIMUM USABLE FREQUENCY

- FREQUENCY BELOW WHICH COMMUNICATION SHOULD BE POSSIBLE ON ALL UNDISTURBED DAYS

WIRELESS WORLD, JANUARY 1957

LETTERS TO THE EDITOR

The Editor does not necessarily endorse the opinions expressed by his correspondents

Is Distortion Unpleasant?

AS A. J. Hickman points out (December, 1956, issue), one can get used to anything: vibrato, dominant seventh chords, even deliberately mistuned "jazz" pianos, are

sought after and give pleasure if not overworked.

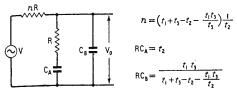
The point is that all these effects are under the control of the musician, but the products of non-linearity

are not. Hindhead.

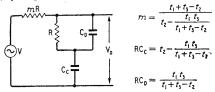
HENRY MORGAN.

Disc Replay Equalizers

THE article by J. D. Smith on "Disc Recording Characteristics" in the November 1956 issue gives incorrect formulae for the components of the combined network in Fig. 3. It can be shown that the correct formulæ should be as follows:-

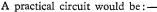


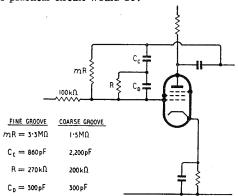
Another network which will give an identical frequency response curve is:-



The error in Mr. Smith's formulæ may explain why his feedback circuit shown in Fig. 4 does not appear to conform to the combined network diagram.

It can be easily demonstrated that the frequency response $V_{\scriptscriptstyle 0}/V$ of the combined networks above is exactly the same as the variation with frequency of the impedance seen looking back into the output terminals of the network, so that these networks can be used directly in the feedback loop of an amplifier to get the desired replay characteristic. A third network is also available giving the same impedance variation.





If the gain of the valve is not enough to prevent the bass response from flattening off due to the feedback becoming inoperative, then the value of mR may be increased or even omitted. E.M.I. Studios, London, N.W.8.

W. H. LIVY.

The Author Replies:

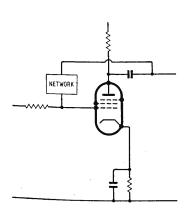
YOUR correspondent is quite right in taking me to task for misquoting the formulæ in Fig. 3. It will be noted that the expressions I gave are in fact approximations to the correct ones, since that for n may be rewritten as

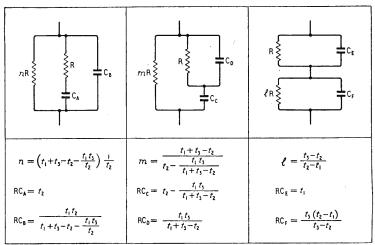
$$n = \left(\frac{t_3 - t_2}{t_2}\right) \left(1 - \frac{t_1}{t_2}\right)$$
 which reduces to $\frac{t_3 - t_2}{t_2}$, as given, when $t_1 \ll t_2$. In either case $RC_B = \frac{t_1 t_3}{n t_0}$. Since Fig. 3.

is intended to illustrate formal networks, I must apologize for quoting the approximate formulæ.

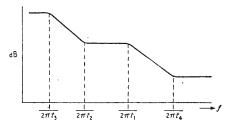
The approximation is valid when pre-emphasis is applied sparingly, as has been the practice in the past but which is scarcely true with the B.S.S. characteristics: the approximation is fair for the coarse groove case but somewhat gross for fine groove. The major maccuracy is in the limitation of bass boost and does not exceed 2 dB, which for many purposes is sufficiently accurate.

The circuit of Fig. 4 of my article is not derived





directly from this combined network. Only two of the required time constants, t_1 and t_2 , are included in the feedback network itself; the third appears by virtue of the finite gain of the valve which limits the bass boost. (If a circuit is to be used for equalizing several characteristics, some of which require less boost, this can be reduced by means of R_s .) There is a fourth time constant, t_1 , due to the fact that the h.f. cut does not continue indefinitely. Hence, the overall response is of the form:—



In practice, this highest time constant is not observed since it occurs beyond the pass-band of the amplifier. The conditions giving the three plateau regions were shown in Fig. 5. It is clear that the design of the equalizer involves a knowledge of the gain of the stage and even then is not quite straightforward because the feedback network provides frequency-dependent loading on the anode circuit, so modifying the response in a manner which tends to increase both the bass boost and treble cut and should be allowed for (most readily by experiment).

Note that under the bass boost condition the stage is working without feedback so that the maximum midband gain is realized. Against this it must be admitted that the limiting boost is dependent on valve parameters and therefore liable to change with ageing, etc.

The two practical circuits cannot be directly compared as they fulfil different operational requirements. The one given by your correspondent employs more feedback and hence gives equalization accurately controlled by the network elements, but at the expense of overall gain. In many instances, greater gain is required and this is achieved by raising the network impedance until the bass boost is limited by the available valve gain and not by the network itself. Under these conditions it is often convenient to include redundant resistors in order to avoid the use of inconveniently large values and the circuit may then take a form similar to that which I gave (which is in fact a derivative of the third network given in Mr. Livy's letter).

Watford.

J. D. SMITH.

Scale Distortion Again

"M. G. L." ends his review of a high-fidelity test record (December issue) by saying of loudness controls that they try "to reproduce an orchestra as it would be heard a long way away with the frequency balance as it would be audible much closer; and this cannot possibly lead to natural results."

The problem of scale distortion (loss in the ear of bass and treble at loudness levels less than natural) cannot be solved by ignoring it. The Fletcher and Munson curves show the loss of bass to approach 14 dB per octave at very low levels, and compensation is essential to hear the bass at all. Reproduction of an orchestra at full volume cannot be tolerated in ordinary rooms, and would be unnatural anyway. Reduction by ordinary (uncompensated) volume-control in effect removes the orchestra "a long way away" with loss of bass and treble, and makes the music thin, monotonous and tiring to listen to.

Reduction by compensated volume—so-called loudness—control effectively leaves the orchestra at its proper distance, but playing quieter (or with fewer members, if you will) as would be expected within the confines of an ordinary listening room, and therefore IS more natural.

Absolute fidelity in the home cannot be hoped for, due to the many well-known causes, but compensation for scale distortion is a valuable aid to the illusion of naturalness and the pleasure of listening—the real aim. Walsall, Staffs.

STANLEY MAY.

The Reviewer Replies:

I CANNOT agree with Stanley May's statement that "reproduction of an orchestra at full volume cannot be tolerated in ordinary rooms and would be unnatural anyway." The aim of correct reproduction is surely to produce in the ear the same sound pressures as would be produced in the ear in the concert hall. Subject to the usual distortions this can be achieved, and in the opinion of many people, including myself, leads to the most natural results. Many of us who share a belief in this standard think that music is often reproduced too loud by "hi-fi" addicts.

If an orchestra were to play quietly or with fewer members in the concert hall, owing to the scale distortion Mr. May mentions, the frequency balance heard would be different from that of a normal orchestra. Thus, even if for some reason we wish to reproduce our music as it would be played by such a smaller orchestra at the same distance as usual, it would be unnatural to compensate in the living room for a change which would

remain uncompensated in the concert hall.

It is, however, possible that reproduction sounding like an orchestra which is the wrong size and has an incorrect frequency balance may be preferable to reproduction sounding like an orchestra of correct size and balance which is too far away. If we are restricted to these alternatives there may be some justification for Mr. May's use of a "loudness" control, but neither of these alternatives attempts to provide the correct reproduction that can to a large extent be achieved.

M. G. L.

The UL Circuit

I NOTED Grant's application (September, 1956, issue) of the UL circuit to single-sided pentodes with some interest. My company suggested this to a magazine editor here in the U.S. and he turned down the suggestion with the argument that it would not pay commercially since

there is a patent licence problem.

A tap is required on a small and low-cost output transformer, and an engineer at one of the transformer companies was of the opinion that the tap cost would exceed that of an RC network for a conventional inverse feedback loop. Hence the UL circuit for a single-sided pentode doesn't seem to appear commercially attractive. However, in my opinion, it should work out better than an RC loop since there should be less trouble with poor "phase bandwidth" produced by a cheap output transformer.

TED POWELL.

Great Neck, L.I., U.S.A.

Audio Demonstrations

THE letters from C. Streatfield and H. Glover published in your October issue criticize the Radio Show demonstrations of sound-reproducing equipment and, in particular, the choice of programme material.

Perhaps the manufacturer who has the listener's ear for only a few minutes can be forgiven for trying to produce impressive rather than natural sounds. But if a test of naturalness is required, I, personally, remain convinced that speech is the best material. When well reproduced at the correct volume level the illusion of reality is, to me at least, greater than with other sounds well reproduced. But equipment which produces impressive bangs, crashes and tinkles doesn't necessarily seem to reproduce speech naturally.

London, N.W.7. W. J. CLUFF.

High-Quality Sound Broadcasting

G. H. RUSSELL Assoc.Brit.I.R.E.

THE USE AND MISUSE OF V.H.F.

HE main justification for v.h.f. sound broadcasting is the poor reception conditions in the lower frequency bands. At the same time, it offers an unprecedented opportunity for giving sound broadcasting a new lease of life. This can be done only, of course, by taking full advantage of the potentialities of v.h.f. and in particular the wide audio frequency range that it makes possible.

In this context it is illuminating to compare the following separate statements taken from a new report* on v.h.f. sound broadcasting in Europe.

"The programme input throughout is designed for a frequency band of from 30 to 15,000 c/s with all corresponding requirements of quality."

"Nor will any changes be made in the line network; most of the lines at present rented . . . transmit frequencies up to about 8,000 c/s, and the cost of increasing this bandwidth (except in the case of short lines to local transmitting stations) would be prohibitive."

The first comes from the German contribution and is representative of the attitude of all but one of the

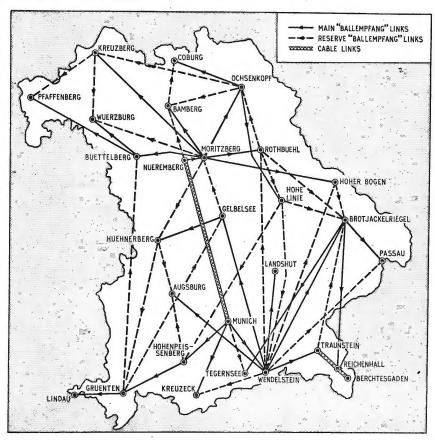
broadcasting European authorities who have launched v.h.f. broadcasting schemes. Even a small country like Austria is busy improving the studio equipment to extend it to 15 kc/s. The second quotation, one regrets to say, is from the B.B.C. contribution.

The attitude of the B.B.C. to this question of the upper audio frequency limit is incomprehensible. If they had said that a restriction to 8,000 c/s was an unfortunate temporary limitation and efforts to increase this limit substantially would be made as soon as possible, it would have been under-

Except for the links between the studios at Munich and Nueremberg, and between three stations in the southeastern "peninsular" the whole v.h.f. network of 28 stations in the area covered by Bayerischer Rundfunk operates on the system of direct rebroadcasting.

standable. Have the possibilities of unattended microwave links been examined? And has the question of direct re-broadcasting, which can be implemented at the cost of one aerial and one receiver per transmitter, been considered?

This system of direct re-broadcasting is being used extensively in Western Germany where it is known as Ballempfang. Indeed, it is also used by the British Forces' Network in that country.† The basis of the system is that signals from the originating station are received at the site of the nearest transmitter(s) where the demodulated signal is used to modulate the transmitter. Alternatively, the signal need not be demodulated but merely frequency transposed and re-radiated; this is called Umsetzer. It is self-evident that the cost of such a system will be only a fraction of that incurred by microwave or



^{* &}quot;The Present Position and Prospectives of V.H.F. Sound Broadcasting in Europe." Document Tech. 3068/E, published by the European Broadcasting Union.
† See Wireless World, February 1956.

cable links. The quality of the service rests upon that of the receiver at each station and the Germans claim that, with the receivers used, it is impossible to detect any degradation in quality even after six successive transmissions and re-transmissions.

One of the most complicated of these networks is that used by the Bavarian broadcasting authority and this is shown in the illustration. It is obvious that there are limits to the use of this system where a number of networks are used over a wide area involving many transmitters. Under these conditions one could conceivably arrive at the position where interference from another network could become a problem. In fact, this position has already arisen in Germany and, in future, cable links will be resorted to as the networks expand. Even so, all the cable links between transmitting stations and the extensions to the studio centres will eventually be able to transmit frequencies up to 10-11.2 kc/s.

Why Not in This Country?

It is realized that with its present network of v.h.f. stations it would be impossible for the B.B.C. to employ Ballempfang. However, the ultimate aim is for about 30 stations to cover the country with a three-programme service, and it would be encouraging to know that the B.B.C.'s intention was to use direct re-broadcasting and/or radio links to give us the kind of reproduction of which v.h.f. is capable. High-quality transmission might re-create public interest in sound broadcasting and stop the rot to television.

In Italy v.h.f. broadcasting is spreading fast,* but for a rather back-handed reason. Like our own B.B.C., the Italian authorities decided to place the v.h.f. sound and television transmitters on the same sites. Initially, it was proposed to proceed at a fairly leisurely pace determined by the rate at which a coaxial cable network could be laid. However, the public demand for television proved so impatient that it was decided to abandon the coaxial link in favour of microwave radio links. This enabled the authorities to bring into service simultaneously all the television transmitters initially projected and, in addition, the service has been extended to 83% of the population instead of the 54% originally planned.

In order to bring the v.h.f. sound broadcasting service into operation equally quickly, direct re-broadcast links are used in all but a few cases where microwave links are again resorted to. It is interesting to note the operational system evolved on the various transmitting sites. These sites are divided into three categories: main, secondary and satellites, of which there are 19, 16 and 48, respectively. This classification has nothing to do with the importance of the stations but with staffing. Thus, the main stations are fully and continuously manned; the secondary stations have a permanent caretaker with a team of engineers in attendance for short periods; and the satellites, which are automatically switched on and off, have no permanent staff. There is a lovable Latin touch to the monitoring system adopted for the satellite stations. A local big-wig in the nearest town, such as the policeman or postman, is appointed to If the transmission should fail, he can this task. bring in a reserve transmitter by remote control, after which it is his duty to telephone a report to the nearest main station.

While on the subject of radio links, it is notable

that Denmark is considering the possibility of combining both sound and television links with those for the multi-channel telephone circuits. This would enable common power supplies to be used with a consequent saving in cost.

Comparative Costs

In the E.B.U. Report a number of countries have given details of actual or probable costs of implementing v.h.f. networks. These are not of general interest except in the case of Sweden where an interesting cost comparison is made between v.h.f. transmission and wire distribution. Three proposals are put forward:

- (a) A national f.m. network reinforced by wire distribution where reception is poor;
 - (b) National wire distribution; and
- (c) F.M. transmitters for densely populated areas with wire distribution elsewhere.

The estimated cost for each of these schemes is £56M, £81M, and £52M, respectively. There does not seem to be much to choose between them. However, when the cost to the listener in new receivers or connecting cords for wire distribution is added, the picture becomes very different. This adds a further £115M, £8M and £95M, respectively. In spite of the economic factors, the Swedes have decided to adopt proposal (c), mainly on the grounds that radio distribution would enable a second programme to be brought to the densely populated areas much sooner than if wire distribution only was used.

Without wishing to resurrect the now very dead f.m. versus a.m. controversy, it is illuminating to compare the Swedish and British approaches to alternative systems. The figures presented to our Television Advisory Committee dealt with the capital cost of erecting and maintaining the transmitters only and left out the cost to the listener entirely. As can be seen from the Swedish figures, this cost can represent a substantial charge on the national income. It is to be hoped that on any future similar occasions which may arise this important factor will not again be omitted.

Before leaving the subject of wire broadcasting, it should be mentioned that no reference is made to it in the Swiss contribution despite the fact that Switzerland already has a first-rate network. Nevertheless, a network of f.m. transmitters is to be erected.

Because of the complex network of v.h.f. transmitters in Western Germany, v.h.f. portables and v.h.f. car radio have become popular. A further interesting development in Germany is the marketing by several firms of receivers that are able to receive television sound in addition to Band II transmissions. The purpose underlying this is that the addition of a simple vision-only receiver converts it into a combined sound and television receiver. It should, of course, be noted that the German television system uses f.m. sound and, furthermore, that v.h.f. sound broadcasting came before television in Germany.

A final note with a dreadful warning from Germany. The use of a 10.7-Mc/s intermediate frequency with poorly protected oscillators has resulted in "a critical situation so far as the final development of the v.h.f. network is concerned." There appear to be four million such receivers in use in Western Germany. No further comment is necessary.

WIRELESS WORLD, JANUARY 1957

^{*} Italy now has 102 transmitters in service.

Cascode Characteristics

GRAPHICAL METHOD OF CONSTRUCTION

By W. GRANT, B.Sc.

HE derivation of cascode characteristics by the use of the mathematical formulæ is a useful method of estimating the working parameters rapidly. It can, however, be misleading and a graphical approach presents a clearer picture and may lead to a

better appreciation of the cascode mode of operation. The static I_a/V_a curves of "single" valves are drawn with V_a and V_g stated relative to the cathode. The static curves of valves in the cascode connection are likewise stated relative to the cathode of the lower section. Fig. 1(a) shows the connection of two triodes in cascode indicating the voltages to which reference will later be made and the currents which do or may flow. Since the purpose is to derive the static characteristics no anode load is shown. Fig. 1(b) shows the d.c. voltage vectors for the general case.

In straight cascode operation V_{gc} is fixed and for the purpose of measuring the static curves V_{g1} may be fixed at each of several values while V_{ac} is varied in steps over the working range at each fixed value of V_{g1} , or vice versa. The curves of Figs. 5(b) and (6b) were measured using the first of these alternatives.

Figs. 2(a) and 2(b) show the I_a/V_a curves of two triodes. Fig. 2(a) will be considered to represent the lower section and Fig. 2(b) the upper section of a cascode pair of which the I_a/V_a curves are displayed in Fig. 3 and are derived as follows.

It will be seen from Fig. 1 that

$$V_{a1} = V_{k2} = V_{gc} - V_{g2} \tag{1}$$

 $\begin{array}{c} V_{a1} = V_{k2} = V_{gc} - V_{g2} & \text{(1)} \\ \text{and} \quad V_{a2} = V_{ac} - V_{k2} = V_{ac} - V_{gc} + V_{g2} & \text{(2)} \\ \text{Equation (1) defines the constancy of } V_{a1} \text{ and } V_{k2} \end{array}$

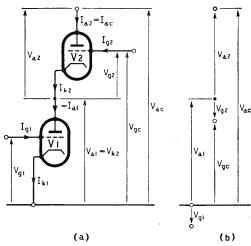


Fig. 1. (a) Cascode arrangement with voltage and current symbols used in the text. (b) Voltage vectors.

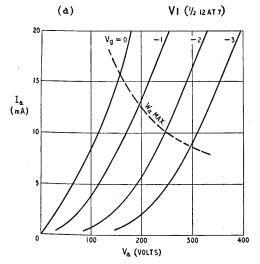
(the origin of the I_a/V_a curves of the upper section) for any constant value of V_{g2} . These two deductions from equation (1) make the graphical determination of cascode characteristics rapid and simple. routine is tabulated below. The "something over" and "somewhat" become self-evident as the tabulation proceeds.

(1) Set out the I_a axis to a value equal to I_{a1} at V_{a1} equal to the proposed V_{gc} and something over, and the V_a axis to the supply voltage available, say 500 V. (2) Erect the I_{a1}/V_{a1} curves (marking them lightly) for all relevant values of V_{g1} up to a value of V_{a1}

somewhat exceeding V_{gc} .

(3) Since $V_{k2} = V_{gc}$ when $V_{g2} =$ zero, erect the I_{a2}/V_{a2} curve for $V_{g2} =$ zero taking V_{gc} as the origin of the curve.

(4) Mark off on the curve of step (3) the currents



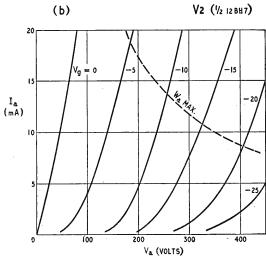


Fig. 2. (a) and (b) Representative characteristics of two dissimilar triodes.

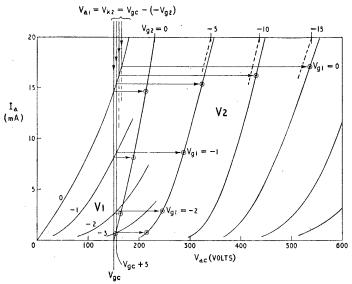
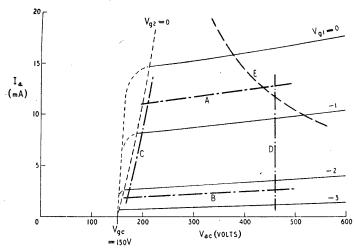


Fig. 3. Construction of cascode characteristics. Note that the curves of VI are the same as in Fig. 2 (a), but that the origins of the V2 curves are successively displaced to the right by increments equal to the bias V_{a2} .



 I_{a1} at $V_{a1} = V_{gc}$ for $V_{g1} = zero, -1, -2$ volts, etc.

(5) Choose a convenient value of V_{g2} , say -5 volts, and erect the I_{a2}/V_{a2} curve for $V_{g2} = -5$ taking $(V_{gc} + 5)$ as the origin, (6) Mark off on the curve of step (5) the currents I_{a1} at $V_{a1} = (V_{gc} + 5)$ for $V_{g1} = \text{zero}, -1, -2$, etc. Steps (5) and (6) are to be repeated for larger values of V_{g_2} , making the appropriate adjustments in the origins of the I_{a2}/V_{a2} curves, until the defining points are plotted as far as desired or the data allows.

(7) Join up all points corresponding to $V_{g1} = \text{zero}$, those corresponding to $V_{g1} = -1$, and so on.

Carrying the argument to the left of the curve $V_{g2} = zero$ (step 3) it is seen that V_{g2} becomes positive and I_{a2} becomes less than I_{a1} by I_{g2} . Given the I_a/V_a data in the V_g positive region and also the I_g/V_g data for the upper section, the curves may be completed. Such data is published for very few valves so all that can be said is that I_{a2} falls off in some unknown fashion. This is seldom of importance since the area is valueless for linear amplification.

The working boundaries are marked

on Fig. 4: they are:-

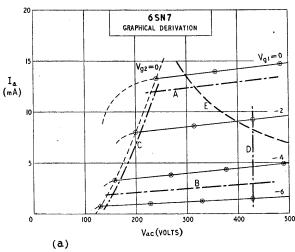
A, the onset of grid current, I_{g1} , in the lower section. This is a strict limit if the grid is returned to chassis through a resistor but may, of course, be relaxed if the return is through a coil of negligible resistance.

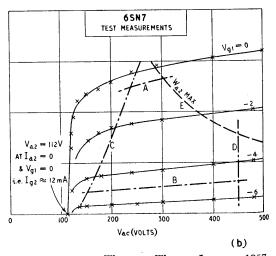
B, the limit of linearity of V_{g1} . This is variable and depends on the degree of distortion which can be tolerated.

C, the onset of grid current, I_{g2} , in the upper section. This is a limit to be respected as $I_{a2} = I_{a1} - I_{g2}$.

Left: Fig. 4. Complete curves developed by the method of Fig. 3 with the addition of working boundaries for linear operation.

Characteristics of a 6SIN7 Below: Fig. 5. cascode stage; (a) graphical construction (b) measured.





WIRELESS WORLD, JANUARY 1957

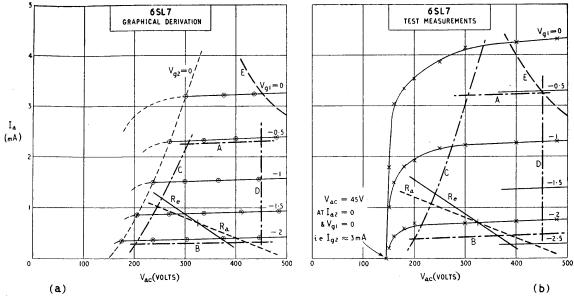
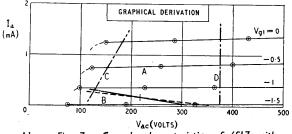


Fig. 6. (a) Graphically constructed, and (b) measured characteristics of 6SL7 cascode stage for $V_{uc} = 150V$.



Cascode characteristics of 6SL7 with Above: Fig. 7. $V_{gc} = 75V$.

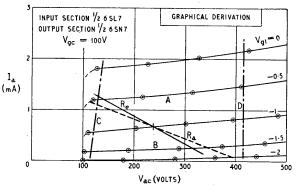
Right: Fig. 8. Demonstrating the advantage of a lowimpedance "upper" section $(VI = \frac{1}{2} 6SL7, V2 = \frac{1}{2} 6SN7)$ $V_{gc} = 100V.$

D, V_{ac} max. = (for all practical purposes) V_{gc} + rated V_{az} max. which in normal usage denotes the maximum supply voltage. Some liberty can usually be taken with this limit, but on the other hand noise is liable to increase with V_a and this should be taken into account in low-level stages.

E, W_{a2} max. This is for all practical purposes the

 W_{a2} univershifted by V_{gc} . Fig. 5(a) presents the graphical derivation of the characteristics of a 6SN7 cascode stage, and Fig. 5(b) displays the results of test measurements made on a 6SN7 valve of RCA manufacture chosen at random. The agreement of the two curves is good and any load line chosen from the derived curves is satisfactory when transferred to the measured curves, if permissible tolerances are borne in mind.

Fig. 6(a) presents the graphical derivation of the characteristics of a 6SL7 cascode stage, and Fig. 6(b) the results of test measurements. The agreement is good for μ and, although the measured valve runs at a higher current, g_m is only 15% high. Again, any load line chosen from the derived curves is satisfactory when transferred to the measured curves. A load line $R_e=150~k\Omega$, representing the following grid resistor $R_g=400~k\Omega$, in parallel with the anode load $R_a = 250 \text{ k}\Omega$, is drawn on both curves.



This demonstrates the importance of adjusting such critical circuits to designed anode current rather than to grid bias voltage.

Low values of V_{gc} are sometimes useful. Fig. 7 shows the cascode characteristics of a 6SL7 at $V_{gc} = 75$ V when, with an anode resistor of 1 M Ω and following grid resistor of 2 M Ω , the gain is approximately 400 and the safe peak output voltage is at least 60 V.

Fig. 8 shows that there are advantages in using an upper section of low impedance if the largest possible output voltage is required with modest h.t. supply and values of R_a and following R_a appropriate to an output stage.

The graphical determination of the cascode curves, given any pair of triodes, is quickly made and presents a clear picture of the properties and limitations of that cascode pair. The determination of the cascode characteristics by the use of formulæ is less accurate unless tediously repeated for many points from data which have in most cases to be found by measurements made on the triode curves. The formulæ, however, do supply the quickest estimation of the dynamic properties of a cascode pair provided the appropriate values are inserted. It is easy to choose the appropriate values by reference to the foregoing.

The general formulæ are included here for completeness; subscripts 1, 2 and c denote respectively lower section, upper section and cascode.

$$\mu_2 = \mu_1(\mu_2 + 1)$$
 (3)

$$g_{mc} = g_{m1} \frac{\mu_2 + 1}{(\mu_2 + 1) + \frac{r_{a1}}{r_{a2}}} \dots$$
 (5)

It is as plain as an outdoor aerial that the analogy with tetrodes must be neither taken for granted nor pressed too far.

The author wishes to record his debt to the Principal of Woolwich Polytechnic for experimental facilities, and would refer readers to the article by "Cathode Ray" on "The Cascode," W.W., Aug. 1955, p. 397, and to the articles mentioned therein.

Fish-Finding Asdic

ECHO sounders, designed primarily to show depth of water, have been used extensively in fishing vessels to detect shoals and even individual fish; but many valuable catches must have been missed because there has been no means of revealing fish other than those which pass immediately below the keel. By scanning in a horizontal plane with supersonic pulses, on the same principle as that used in the asdic submarine detection equipment, a much wider sea lane can be swept for fish.

Kelvin Hughes have now produced a prototype fisherman's asdic for this purpose with a range up to 2,000 yards which has given promising results in sea trials.

The pulse transmitter and receiver unit (transducer) is mounted on a vertical column working through a gland in the ship's hull and can be retracted into a fairing when not in use. It can be rotated by remote control in 5° steps and an automatic mechanism can be set to advance the bearing by this amount at each pulse when making a sweep. The beam width is 10° and the pulse train is at 50 kc/s (1 kW) with alternative durations of 1 and 10 milliseconds.

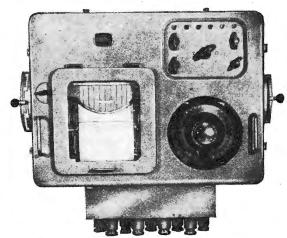
A heterodyne receiver circuit may be used with

headphones or loudspeaker for watch keeping, and the output can be switched to a recorder for accurate ranging when an echo is to be investigated.

Some degree of skill and experience is required if full advantage is to be taken of the information provided by this equipment. There are many sources of echoes, including scattering from the bottom, the water surface in rough weather, and the wakes of other vessels in otherwise smooth

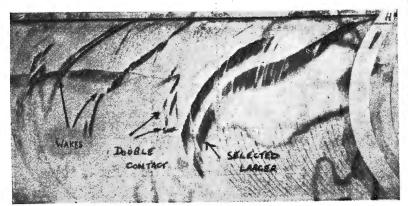
The accompanying specimen record shows, in the left-hand half, the traces of wakes which decrease in range until they are crossed (at the zero line running along the top). The horizontal echo running through the wake traces is from the sea bottom. In the middle of the picture may be seen the first contacts with two shoals followed by a change of range scale as the distance is closed: the difference in size of the shoals can be clearly seen. The curved dotted traces in the bottom right-hand corner are due to interference from the ship's echo sounder which was also working.

Given reasonable weather and intelligent operation, there is little doubt that this new equipment is capable of showing considerable economies in steaming time in search of fish, which will more than offset the initial cost (of the order of £2,500).



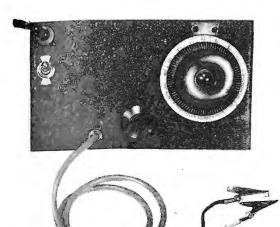
Wheelhouse control unit of the Kelvin Hughes fisherman's asdic. The beam bearing scale is on the right.

Shown on the right is the transducer unit which has a beam width of 10° at 50 kc/s. Below is a specimen chart showing two large fish shoals. The discontinuities are the result of alterations in the range scale.





WIRELESS WORLD, JANUARY 1957



Simple V.H.F. Test Oscillator

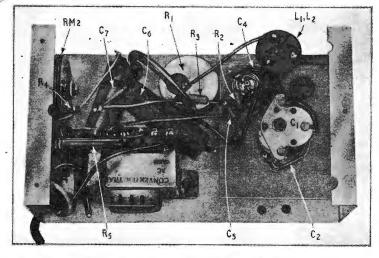
Minimum Requirement for Aligning an F.M. Receiver

By BERNARD DRIVER

HE lack of some form of signal generator can be an insuperable difficulty when contemplating the alignment of a v.h.f. receiver. It is, perhaps, not generally realized that a simple oscillator, as described in this article, if judiciously handled will enable a satisfactory alignment to be achieved.

The basis of the circuit, which is shown in Fig. 1, is that described by H. B. Dent in the December 1952 issue of *Wireless World*. Instead, however, of employing separate oscillator coils and valves for signal and intermediate frequencies a single Hartley oscillator is used, the 90-Mc/s range being pro-

vided by harmonics. Since modulation was not considered essential, the transitron modulator is omitted, but there is ample space for the additional valve and components inside the case, which measures $7\frac{1}{2}$ in $\times 4\frac{1}{2}$ in $\times 2\frac{1}{2}$ in, if the refinement is required.



General view of the oscillator removed from its case. All the components are readily identified.

The oscillator coil consists of 38 turns of 26 s.w.g. enamelled wire on a $\frac{1}{2}$ -in diameter former, tapped 7 turns from the earthy end. The r.f. output is taken from a separate pick-up coil, consisting of a further 3 turns, spaced $\frac{1}{8}$ in from the earthy end of the oscilla-

tor coil. Full winding details of the coil will be found in the article to which reference has already been made.

The valve is an acorn triode, Type 955, and in order to save space the connecting wires to the valve are soldered direct to the tips of the valve pins, a heat shunt being attached to each pin whilst applying the soldering iron. The writer has found that a sliver of ice is an efficient substitute for the crocodileclip type of heat shunt, where space does not permit the latter's use.

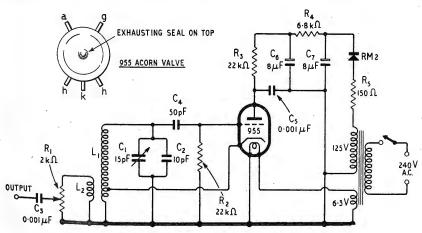


Fig. 1. Theoretical circuit diagram of the v.h.f. test oscillator.

WIRELESS WORLD, JANUARY 1957

The instrument can be calibrated with a fair degree of accuracy by the following method, which requires only a v.h.f. receiver capable of receiving the B.B.C. transmissions, and whose i.f. stages are approximately, at least tuned,

10.7 Mc/s.

The first step is to plot the oscillator dial readings against fundamentals in the range 9.5 to 12 Mc/s. Connect the output from the oscillator, with 2-k Ω potentiometer (R₁) at maximum, to the aerial socket of the receiver. If the receiver has an i.f. trap in the aerial circuit, short it out. Upon tuning C1 between maximum and minimum capacitance a number of responses will be heard. The i.f. fundamental can be readily identified since manipulation of the receiver tuning control will not tune it out.

The capacitance given for C₂ is approximate only, and if the fundamental cannot be found initially it may be necessary to try a different value capaci-

In the unit constructed by the writer, the calibrated portion of the scale occupies about 60 degrees only, and it might be found desirable to apply bandspreading by reducing the value of C₁ and increasing that of C₂. This would facilitate making, for example, a point-topoint measurement of a discriminator characteristic of sufficient accuracy to indicate quite a small degree of non-linearity. Figs. 3 and 4 are actual curves plotted with this oscillator.

Having noted the position of the i.f. fundamental on the oscillator tuning dial,

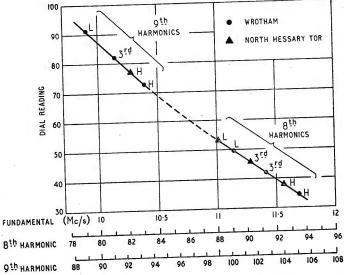
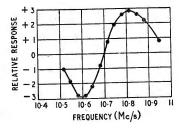


Fig. 2. Frequency calibration curve obtained by plotting the 8th and 9th harmonics of the oscillator beating with the Home, Third and Light programmes of Wrotham and North Hessary Tor. The fundamental is deduced from these readings.



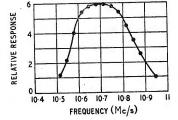


Fig. 3. A ratio-detector characterstic curve plotted with this oscillator.

Fig. 4. Overall frequency response of the i.f. amplifier of an f.m. receiver.

ACORN VALVE

Close-up of the coil showing the method of construction.

with the aerial as well as the oscillator output, connected to the receiver input socket as before, and with the receiver tuned to the Home Service, slowly increase C₁ until a beat note is heard in the loud-speaker. This will be due to the 9th harmonic of the oscillator fundamental beating with the broadcast signal. It is easier to tune the oscillator to the null point of this beat note when the broadcast carrier is not modulated, and it may be necessary to reduce the output from the oscillator to avoid swamping the receiver. Having found the null point, the oscillator dial reading may be plotted against the fundamental, which is f/9 where f is the carrier frequency. of the test signal.

Then tune the receiver to the Third and Light programmes successively, repeating the process outlined above by slowly increasing C1 to produce a beat note in each case, plotting the results after dividing the respective carrier frequencies by 9, as before.

Now reset the oscillator dial to the reading originally noted, giving the intermediate frequency of the receiver. Leaving the latter tuned to the Light programme, slowly decrease C, until the first beat note encountered above the intermediate frequency is heard. This will be the 8th harmonic of the oscillator fundamental, and when the null point has again been found, the dial reading may be plotted against frequency using the formula f/8. Retune the receiver to the Third and Home transmissions successively, reducing C_1 to produce beat notes and plotting the

dial readings as before.

By joining up the three points plotted from the 9th harmonic, and the three points plotted from the 8th harmonic, two curves will now be obtained, and assuming that the receiver has throughout been tuned to one or other of the transmissions from Wrotham, these will probably be similar to the curves shown by solid lines in Fig. 2. Here, however, additional points were obtained from North Hessary Tor.

It now remains to connect the two curves, as shown by the dotted portion in Fig. 2. This, as will be seen, is bound to be an approximation, but assuming a reasonably linear characteristic a fair degree of accuracy will be achieved if the dotted portion is drawn as a straight line. In addition, either end of the completed curve may be extended, if required, either notionally or by using as reference points the

carrier frequencies of any other receivable v.h.f. transmissions. A v.h.f. scale can be added along the base line of the calibration chart as shown in Fig. 2.

The frequency stability of the oscillator is good, apart from a slight positive drift which takes place during the warming-up period. As the extent of this drift depends largely on the nature of the coil former, compensation can be effected by selecting a negative temperature coefficient capacitor for C_2 , or possibly a combination of capacitors having negative and positive characteristics. The direction of drift can readily be ascertained by heterodyning a harmonic of the oscillator with a carrier of known frequency stability in the manner described earlier in this article. If, after setting C_1 to the null point, the frequency of the beat note changes, and it is necessary to decrease C_1 to restore the null point, the temperature coefficient of the circuit is clearly positive, and vice versa.

COMMERCIAL LITERATURE

Ferrite Cores for various applications, as well as irondust and flake-iron cores, are among the materials and components described in an illustrated brochure devoted to the products of the Chemical and Metallurgical Division of Plessey. Applications as well as physical properties and parameters are discussed. Obtainable from the Company at Wood Burcote Way, Towcester, Northants.

Germanium Diodes and Transistors.—The Telefunken manual mentioned in our last issue can be obtained from Tellux, West Mall Works, 27-29, Rabbit Row, London, W.8, who are agents for these products in Great Britain.

Components and Accessories, including coil packs and turrets, and drilled chassis and kits of parts for popular receivers and amplifiers. A general catalogue, with many detailed drawings, from Denco (Clacton), 357-9, Old Road, Clacton-on-Sea, Essex, price 9d.

Record Changer in which the required speed, record size and appropriate needle are all selected in one movement by a single control device. Improved version of an earlier model, with heavy turntable, new removable pick-up arm with ceramic crystal cartridge, and lower overall height. Brochure on the RTW-6 from Luxor Radio, Motala, Sweden.

Oscilloscope, with $3\frac{1}{2}$ -in p.d.a. tube, suitable for pulse and television work. The \tilde{Y} amplifier has a response to 6Mc/s with no overshoot or ringing and a sensitivity of 50mV per 0.8-cm graticule division. Time base, triggered or repetitive, variable from 0.2sec to 3μ sec. Specification and description on a leaflet from Telequipment, 313, Chase Road, Southgate, London, N.14.

Relays by various manufacturers, including aerial, co-axial, polarized, galvanometer and other special types. Illustrated leaflet giving brief specifications of about 70 different models, from Radio-Relais, 18, Rue Crozatier, Paris 12, France.

Low Frequency B.F.O. covering 2c/s to 4kc/s in two ranges, on logarithmic scale, which can be swept automatically at predetermined rate by flexibly coupling tuning capacitor to pen recorder or other motor. Automatic output regulator maintains constant output to within 1 or 2 dB. Output impedance 6, 60, 600 or 6000 ohms. Leaflet from B & K Laboratories, 59, Union Street, London, S.E.1.

Moulded Knobs, Handwheels and Dials.—An illustrated catalogue from the British Electric Resistance Co., Queensway, Enfield, Middlesex.

Television and F.M. Distribution System (Dumec) for hotels, showrooms, etc. A range of accessories, including attenuators, filters and outlet boxes, has been developed for extending the system and is described in a leaflet from Rainbow Radio Manufacturing Company, Blackburn, Lancs.

Equipment Handles of simple design in brass, chromium plated or gold oxidized, with 2 B.A. tapped holes. Leaflet from Harwin Engineers, 101-105, Nibthwaite Road, Harrow, Middlesex.

Instrument Control Knobs and general purpose types. An illustrated leaflet showing the range available from Uncles, Bliss and Co., New Parade, Cherry Orchard Road, East Croydon, Surrey.

Midget Prefabricated Cabinets (Widney Dorlec), made up from basic components of slotted corner rods, thin side panels to fit in the slots and thick top and bottom panels (see our April, 1956, issue, p. 179). Illustrated brochure and price list of the various components from Hallam, Sleigh and Cheston, Oldfield Road, Maidenhead, Berks.

Fractional H.P. Geared Motors for slow speeds between 0.2 and 840 r.p.m. Also centrifugal electric pumps, extraction fans, sump pumps, mains transformers (including variable types), meters, sliding resistors and synchronous timing devices. Illustrated leaflets from M.R. Supplies, 68, New Oxford Street, London, W.C.1.

Tape Recorder, two-speed, with 4-watt amplifier and three loudspeakers—a 6-in elliptical type with two $2\frac{1}{2}$ -in treble units. Frequency response 50c/s-9kc/s at $3\frac{3}{4}$ in/sec and to 13kc/s at $7\frac{1}{2}$ in/sec. Fast forward or rewind time: $1\frac{1}{2}$ minutes. Description and specification of Model TK8-3D from Grundig (Gt. Britain), 39-41, New Oxford Street, London, W.C.1.

Components and Accessories; an illustrated catalogue for November, 1956, from Radiospares, 4-8, Maple Street, London, W.1.

CLUB NEWS

Bradford.—The meeting of the Bradford Amateur Radio Society on January 15th will be held at the Bradford Technical College where Dr. G. N. Patchett will speak on television. On January 1st G. F. Craven will discuss automation, and on the 29th A. Davies (G3INW) will deal with simple receivers. These two meetings will be held at 7.30 at Cambridge House, 66, Little Horton Lane. Sec.: F. J. Davies (G3KSS), 39, Pullan Avenue, Eccleshill, Bradford, 2.

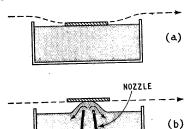
Leicester.—A symposium on mobile operation will be presented at the meeting of the Leicester Radio Society on January 14th. A fortnight later R. Macqueen (G3DVP) will speak about the Clapp V.F.O. on 28 Mc/s. Meetings are held at 140, Highcross Street. Sec.: J. Tranmer, 4, Grocot Road, Evington, Leicester.

Newbury.—At the meeting of the Newbury & District Amateur Radio Society on January 25th at 7.30 at Elliott's Canteen, West Street, L. A. Parnell (G8PP) will speak on world-wide commercial communication.

Wellingborough.—"Principles of radar" is the title of F. Wright's address to members of the Wellingborough and District Radio & Television Society at their meeting on January 3rd. On the 24th G. A. Wilford will deal with the principles of television. The club meets every Thursday at 7.30 at the Silver Street Club Room. Sec.: P. E. B. Butler, 84, Wellingborough Road, Rushden, Northants.

Technical Notebook

Improved "Dip" Soldering of printed circuits is offered by a new technique in which the work is not actually dipped as at (a) but passed continuously at 2-4ft per minute over a wave of molten solder forced up by a nozzle in the bath (b). This avoids the discontinuity of the dipping or rocking movements normally required and the consequent break in production flow. Fry's Metal Foun-



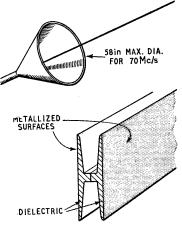
dries, who have introduced a machine embodying this idea, claim that it allows flexibility in the rate of production and the size of circuit boards. There is positive expulsion of flux gases, freedom from trapped flux which may prevent wetting, and a reduction of "icicles" and "bridging." The stream of solder is consistently clean, and, being continuous, prevents surface cooling, thereby allowing a lower working temperature or a shorter contact period.

Wide Magnetic Tape, 1 inch across, seen at a recent E.M.I. electronics exhibition, was stated to be suitable for recording television signals. The composition was slightly different from sound-recording tape. An experimental television-on-tape recording equipment is being developed by the B.B.C. Research Department and details can be expected within the next few months.

Symmetrical Transistors are rather rare devices in which the two outside electrodes have interchangeable roles. Each can act as either emitter or collector, depending on the polarity of the applied voltages. Only one commercially available version, the S.T.C. type TS4, appears in Wireless World "Radio Valve Data." Curiosity about possible applications was partly satisfied at the

recent I.E.E. Ferrites Convention, when D. S. Ridler and R. Grimmond described a transistor access selector for their new drilled-block ferrite storage device (see Dec., 1956, issue, p. 596). In this selector the symmetrical transistors are used for gating both positive and negative pulses.

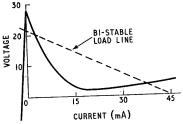
Open-sided Lines are the latest thing for simple and cheap transmission of r.f. energy. One example is a single-wire line connecting a remote aerial to a television distribu-tion system (Radio and Television News, Nov., 1956). The characteristics are those of a coaxial cable with its outer conductor at infinity, and wave propagation is largely axial. The line is connected to ordinary coaxial input and output cables by means of large metal cones (see sketch) which make the transition between the "outers" and the infinite spacing. Losses, which increase with bends, are 10-20dB per mile, and intermediate amplifiers are needed to cover the 15-mile stretch. Another example is waveguide of H-shaped cross-section, open at top and bottom (Electronic Industries, Nov., 1956). Intended for millimetre waves, it consists of a plastic moulding with metal-



lized coatings on the legs of the H (see sketch). Attenuation decreases with increasing frequency, and less than 0.1% of the energy travels outside of the guide. Fabrication and jointing are simple.

Negative-Resistance Transistor recently introduced by General Electric

in America has a characteristic like a point transistor that will give a regenerative switch-over action in bistable switching and computing circuits (see figure). At the same time it has the uniformity, stability and reliability of a junction type. The Unijunction transistor, as it is called, is made from silicon and so can be operated at high temperatures. Because of its characteristic it will do



the work of the two junction transistors normally required in a bistable trigger circuit. This should make possible a considerable simplification in the design of switching and computing equipments using large numbers of transistors, with consequent reduction of size and cost.

Binary v. Decimal notation was discussed by Dr. M. V. Wilkes at a recent I.E.E. meeting on data processing equipment. Many people have assumed that the decimal form is more suitable for data processing since very little computing is involved, and conversion to and from binary is a waste of time. Dr. Wilkes stressed, however, that a paramount problem in many data-processing systems is that of storing large quantities of information, and this can be done a good deal more efficiently by binary techniques.

Transistor Biological Amplifiers have distinct advantages over those using thermionic valves because of low microphony—normally a source of trouble on biological recordings. Moreover, their compactness allows them to be operated very close to the subject. This avoids the need for long input leads which can pick up interference and mask the required waveform. A four-stage transistor pre-amplifier for electromyography with a noise output of only 15µV is described by R. E. George in Vol. 7, No. 1 of the Proceedings of the Electro Physiological Technologists' Association.

Telephone-line possible by slow scanning, illustrates the communication theory principle that you can transmit a lot of information in a narrow-bandwidth channel if only you take sufficient time over it. In one system, developed by Thompson Products for transmitting still pictures of documents (Electronics, Nov. 1956), the scanning rate is 2-7 complete

WIRELESS WORLD, JANUARY 1957



pictures per second, and to allow for this a long-persistence c.r.t. is used at the receiving end. A horizontal resolution of 300 lines is possible with an 8-kc/s bandwidth. In the Bell Telephones "Picture-phone" system (see illustration) the camera scanning is comparatively fast at 20 pictures per second, but the actual transmission rate is only 1 picture in 2 seconds. The picture selected in each 2-second period is recorded on a magnetic drum, then, by means of gating and timing circuits, is "read" off at 1/40th of the recording speed, taking 2 seconds in transmission. This requires a line bandwidth of only 600c/s. At the receiving end are two storage type of c.r.ts, one of which builds up the incoming picture while the other displays the previous picture.

Silicon Transistors, capable of working at high temperatures (up to 150°C), are the next thing to watch for on the British market. Meanwhile, two new types have been introduced by Texas Instruments in the U.S.A.—the *n-p-n* 2N117 and 2N118. Suitable for high-gain, low-level applications, they have been designed to meet the stringent requirements of the U.S. Navy. The testing includes heat cycling four times from -55°C to +150°C and storage for 24 hours at 150°C.

R.F. Silicon Transistors of tetrode construction have also been developed by Texas Instruments, for working up to 100°C. In a single-stage amplifier, a gain of 15dB can be obtained at 30Mc/s. Details of gain tests in the 5-30Mc/s region are given by R. R. Webster in the Nov., 1956, issue of *Electronic Industries*.

Flying-spot Scanning, first introduced by Baird in the early days of television, is now coming back for colour television. This is because the development of sensitive photomultiplier tubes has made it possible to get video signals of good signal/noise ratio at the low light levels given by the scanning c.r.t. In the Du Mont "Vitascan" system, for example (I.R.E. Transactions PGBTS-6, Oct. 1956), clusters of

5-in photo-multipliers with colour filters are disposed about the studio, and can be arranged to get "lighteffects as if they were light sources. During scanning the studio has to be completely dark, but a form of lighting can be provided by puls-ing lamps in the frame suppression periods. The system is more suitable for low-cost industrial television, but has certain advantages for broadcasting; e.g., no high-power studio lighting and air-conditioning required, good colour match between different scanners (since the photomultipliers are common to them all) and short warm-up and adjustment time.

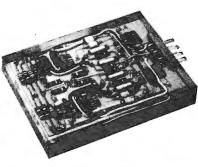
U.H.F. Receiving Valves for Bands IV and V are now coming on to the market—colour television and mobile

radio being two likely future applications. One might expect such valves to look rather unusual. In fact they are just like conventional B7G and B9A miniature types, ex-cept for the planar type of electrode structure inside. A recent one from G.E.C. is the A2521, a lownoise triode suit-



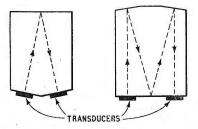
able for use as an r.f. amplifier in the 500-1,000-Mc/s region (see picture). Its slope is notably high at 12 mA/V, and the noise factor varies between 9 and 12 dB, depending on the frequency.

Transistor Decade Counter, made as a potted plug-in unit by Venner Electronics (see photograph) is notable for its small size $(4\frac{1}{2}$ in $\times 3\frac{1}{4}$ in $\times 3\frac{1}{4}$ in) and low consumption (160mW or 100mW, depending on whether it is used as a counter or as a $\div 10$



frequency divider stage). The circuit consists of four bi-stable trigger circuits with feedback and will operate at pulse input frequencies up to 30kc/s. A resetting facility (to zero or to nine) is included. The 86 components are mounted on a double-sided tagboard in the potting resin.

Folded Delay Lines of the acoustic-wave type are being developed by Bell Laboratories for giving long delays at radio frequencies (around 15Mc/s) in a relatively small space. The advantage over electrical delay lines is simply that acoustic waves travel some 100,000 times slower than electromagnetic waves, and this in itself



makes possible much smaller equipment. Solid blocks of vitreous silica are used, with quartz or barium titanote input and output transducers, and the folding of the wave path is achieved by reflections inside the specially shaped block, as shown in the sketches. One 990-µsec line utilizes 30 reflections to fold up some 12ft of wave path into a polygon 5½n in diameter. With a centre frequency of about 15.5Mc/s, this delay line has a bandwidth of over 4Mc/s.

Better reproduction from discs is offered by a tape-recording technique suggested by W. E. Gilson in Electronics for July, 1956 (p. 125). Signals initially recorded on magnetic tape are played back at half speed. The upper frequency limit is thus halved. These signals are rerecorded on an ordinary disc recorder which is also run at half speed. Effects such as cutter head resonance which normally cause distortion or loss at the higher frequencies will then occur outside the range to be recorded. On finally playing back the disc at normal speed the original signals are thus reproduced without distortion due to these effects.

Complications may, however, occur at the lowest recorded frequencies. The maximum amplitude that can be recorded on the disc is, of course, limited. Thus either the low-frequency turnover point for recording on the disc will be the same as usual, in which case this frequency will be twice the normal on final playback; or the disc recording must be made at half the usual level and the increase in noise may be troublesome. Distortion at the lowest frequencies on the disc recording must be more strictly controlled as this will be more objectionable on playback when the frequency is doubled. The disc recorder must be free from rumble even when played at half the normal speed, and, due to the re-recording, wow and flutter requirements will also be more stringent.

NEGATIVE RESISTANCE

By "CATHODE RAY"

A Mystery of the Backward Bending Curve

OME while ago Thomas Roddam posed a very interesting question*. Interesting, that is to say, to those who, like myself, are intrigued by questions which seem at first sight to imply something contradictory in accepted theory, but no doubt irritating to the "practical" folk who regard such things as mere hair splitting and a waste of time. Personally I don't think it is a waste of time, even for a practical man, to look into any apparent contradiction. If there really is something wrong with accepted theory, then the sooner it is put right the better; but if (as is considerably more likely) it is only our view of it that is wrong, then that is a good thing to put right, too.

Suppose we pass various amounts of current through a resistor, and in each case measure the voltage between its terminals; then (provided we take care to keep the temperature of the resistor constant) we usually find that a graph of voltage against current, such as Fig. 1, is a straight line. We conclude, as did Dr. Ohm long before us, that current and

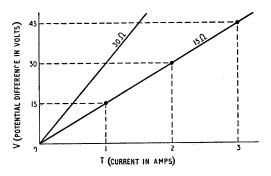


Fig. 1. Graph of voltage drop against current for ordinary linear (ohmic) resistance.

voltage are directly proportional to one another, so that the ratio V/I for any particular resistor is always the same, no matter what the values of V and I. This ratio has become quite well known as "resistance," denoted by R. We can easily see that with any given graph scales it is proportional to the slope of the graph. The line is, in fact, often regarded as representing the resistance. But for ordinary resistors there is really no need to make a graph; the value of R in ohms (i.e., volts per amp) provides all the needed information.

While this "law" established by Ohm still holds good for a sufficiently large number of parts of electrical circuits for it to be extremely useful, the number of parts for which it does not hold good has tended to increase rather noticeably of late. I have it on American authority† that already 7,000,000,000

valves have been manufactured, and every one of them flagrantly disobeys Ohm's law. So far only a very few million transistors have been produced, but Dr. Shockley has predicted an "explosive" increase very soon. And think, if you can, of all the metal rectifiers and neon tubes and Metrosils and much else. For any of these, the value of V/I varies with the values of V and I and also with the starting points from which they are measured; so the resistance is a variable, and a graph is necessary to provide full information about it. This is where the slope of the graph as a measure of resistance comes in useful, for the way in which the resistance varies can be seen at once from the variations in slope of the voltage/ current graph, without having to plot from it a resistance/current or resistance/voltage graph. (There is another way of reckoning the resistance at any point as the slope of the straight line drawn from it to the origin—but that is seldom used in practice.)

It is because of the curvature of their voltage/current graphs that electronic devices are called non-linear. But although their curves may vary from almost horizontal, meaning nearly zero resistance, to almost vertical, meaning nearly infinite resistance, it is usual for the slope to be everywhere upward from left to right‡, meaning that the resistance is always positive. There are, however, a few exceptions in which the slope bends over the other way, as in Fig. 2, so that over a certain range of current and voltage the resistance comes out negative.

Users of valves and other non-linear devices are commonly interested in what can be done with them

[‡] Assuming, of course, the standard practice of making the scale numbers increase positively to the right and upwards.

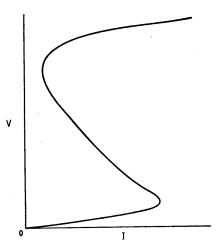


Fig. 2. Graph of voltage drop against current for one kind of non-linear (non-ohmic) resistance. The resistance varies with voltage, and over a certain range is negative.

^{* &}quot;Negative Resistance," Wireless World, July 1954, p. 336. † D. G. Fink, "Transistors v. Vacuum Tubes"; Proc. I.R.E.

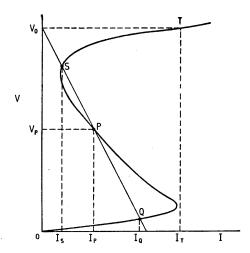


Fig. 3. Diagram combining graphs of non-linear resistance (as in Fig. 2) with linear resistance in series. In this case there are three ways (represented by P, Q and S) in which a total voltage V_0 can be shared between them.

in combination with a linear resistance connected as a load in series with a fixed supply voltage. This situation can conveniently be studied by drawing a "load line" on the same diagram as the valve curve, as for example in Fig. 3. The technique is well known, but for beginners I explained it in the July 1955 issue. The only point I need perhaps repeat here (in view of my having just said that a slope downwards towards the right represents a negative resistance) is that the load line sloping downwards towards the right does *not* mean that its resistance is negative. The apparent contradiction is because the point where the load line cuts the voltage scale (e.g., V_o in Fig. 3) represents the total fixed voltage applied to it and the valve in series, so the voltage across the load resistance is zero at that point and increases in the opposite direction to the scale numbering.

Because the valve and the load resistance are in series, the same current must flow through both; and so this amount of current on the diagram must apply to both curve and load line. At the same time the voltages across them must add up to the total V_o . These two facts can apply only to a point which is on both load line and curve at the same time as P in Fig. 3. This point indicates that the voltage across the valve is V_p , the voltage across the resistance is V_o - V_p , and the current through both is I_p -

Three-point Intersection

If this were a normal kind of valve, with resistance positive throughout, there could be only one point common to both its characteristic curve and any other positive resistance load line. But the valve we are considering is one of the exceptions with a stretch of negative resistance, which makes it possible for the load line to cut its curve at three points, as shown. In such cases there are two alternative currents, \mathbf{I}_q and \mathbf{I}_s , that could be driven through the combination by the same total voltage. At both of these other intersections the valve resistance is positive and the situation is entirely normal; the only question that arises is how the valve and resistor decide between them which point to occupy.

Actually they haven't much choice, because it is

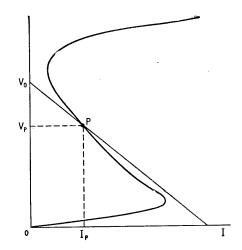
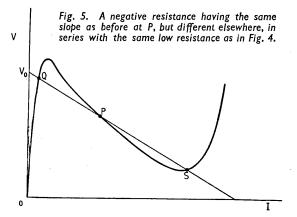


Fig. 4. Here the non-linear negative resistance of Figs. 2 and 3 is in series with a lower resistance, and there is only one way of sharing V_0 .



imposed on them from without by whoever is responsible for the arrangements for switching on. In the ordinary way, with the current growing from zero, it would rise to Q and stay there. But if now the resistor is short-circuited, changing the load-line slope to zero, the working point becomes unambiguously T. If the resistor is then unshorted the working point slides down to S.

So much for Q and S; but how can one get to P? It is not really very difficult; one just connects the junction of valve and resistor straight to a source of V_p volts. When this connection is broken the working point should remain at P. It we try it, however, we find it invariably flips over to Q or S. Why?

Most treatises beg this question by stating that P is an unstable working point. Before we try to find a real answer let us just look at Fig. 4, where our kinked valve curve appears yet again, this time in conjunction with a lower load resistance. Here, the negative resistance introduces no complication; there is no alternative to P as the working point, and only one value of current (I_p) can cause the total voltage drop to be V_0 .

Clearly, the situation changes from unstable to stable when the slope of the load line changes from greater to less than that of the valve at the point P. Next, let us give our attention to Fig. 5, where the slope of the load line is less than that of the valve at P, just as in Fig. 4, but where nevertheless there are three alternative points, and the situation is presumably unstable, as in Fig. 3. Experiment confirms this. If in each case the arrangement is switched on in such a way as to start it at point P, with a V/I characteristic as in Fig. 4, it stays there, but in Fig. 5 it flips across to Q or S the moment it is released. The point is—as T. Roddam pertinently asked—how does the circuit know, when it is set to point P, whether it is stable or unstable? If only the parts of Figs. 4 and 5 in the immediate neighbourhood of P are disclosed there is no difference whatsoever between the two diagrams.

The Working Point's Dilemma

I thought this a remarkably intriguing problem. Unfortunately, Mr. Roddam had to hurry on to the kernel of his article, which was the negative impedance converter, and so it appeared that the working point has to find out whether to say at P or not by doing tricks with a piece of string around a stick. The explanation, like most conjurors' explanations of how their tricks are done, left me wondering harder than ever; so, in case there were any other readers in the same state, I will offer my less elegant attempt to find the way.

The first thing is that theoretically a simple combination of positive and negative resistance must stay at P either way. The reason is that the only possible conditions are those represented in the diagrams by points common to both graphs—the valve curve and the load line. It is not possible to get from P to Q or S—or indeed anywhere—in such a way as to be on both graphs all the time. To move from P it would be necessary for the current or voltage or both to have two different values at the same place and the same time—which is absurd.

A way out is to alter the circuit. And perhaps it is high time to see a practical circuit diagram instead of just having to imagine a negative resistance. After my recent expositions you may expect a transistor as example, but point-contact transistors, which are the main ones with inherent negative resistance, are well on the way out. And since there must be many people to whom transistors of any kind are still something new and strange, I am first going back to the dynatron, which may seem a bit archaic to the younger readers, but at least is a valve.

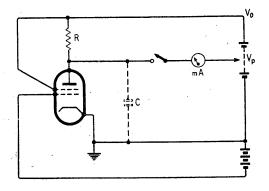


Fig. 6. Dynatron circuit for experimenting with the type of negative resistance graphed in Figs. 2-4.

As Fig. 6 shows it is tetrode, but *not* of the modern "kinkless" variety in which negative resistance is deliberately ironed out; rather, an old-fashioned "screen-grid" tetrode. The screen grid is held at a normal voltage, say 100; and if the anode voltage is varied from 0 to 100 the anode current traces out a curve like Fig. 2. This may not have been recognized as a dynatron curve, even by the old-timers, because it has been drawn with the voltage scale vertical instead of horizontal. The idea of departing from the usual custom was to follow Mr. Roddam in making slope represent resistance rather than conductance.

The reason for the abnormal behaviour of anode current while the anode voltage is varied between about 10 and 90 is that the electrons reaching the anode from the cathode have been given a boost on the way by the relatively high screen-grid voltage. So when they hit the anode they do so with such violence that they knock out some of the electrons already there. These "secondary" electrons are easily gathered in by the high positive screen-grid voltage against the feeble competition of the anode voltage. The result is that the more the anode voltage is increased the more violent the bombardment and the greater the number of secondary electrons, which all subtract from the normal anode current. In fact, it is quite usual for the net anode current to become actually negative over a certain When the anode is made range of anode voltage. nearly as positive as the screen grid, however, the secondary electrons have little or no inducement to leave, and the anode resistance becomes positive again.

One can—and usually does—produce one's negative resistance by means of positive feedback, but for the present purpose the dynatron has the great advantage that its negative resistance is practically constant at all frequencies right down to zero, and the circuit is almost ideally free from complications.

By choosing a suitable resistance for R, we can arrange that its line on the diagram cuts the valve anode characteristic curve in three places, as already discussed. And by joining a wire from the anode direct to a tap on the h.t. battery at the voltage of point P, we can bring the valve to that point. To make sure we are there, we can put a low-range milliammeter (mA in Fig. 6) in this wire and adjust the tap voltage until this meter reads zero. Seeing the wire is carrying no current, we might suppose that breaking the circuit would make no difference; but directly we do so, flip!—the current goes up or down, and we find it is at Q or S. How does it get over the hump in between?

Hidden Component

An explanation can be found in one of those "invisible components"—the capacitance of the anode to other electrodes. Most of it would be to the screen grid, but, since there is a fixed voltage between that and earth, the same results so far as voltage changes are concerned are obtained if all the capacitance (C in Fig. 6) is regarded as direct to earth; and it is rather easier to see what is going on that way.

However carefully we adjusted the voltage tapping, there would always be some current through that path when we opened the switch, if only as a result of the inevitable random fluctuations in circuits and valves. Suppose that just before breaking the meter

(Continued on page 45)

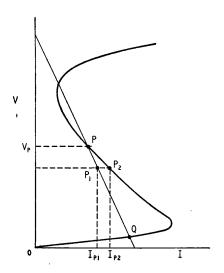


Fig. 7. Explaining the role of C in Fig. 6 in the instability of that circuit.

circuit there was a minute current flowing through it *into* the valve. The valve current would then be very slightly greater than through R; a condition represented rather exaggeratedly in Fig. 7 by points P₁ and P₂. The current through R would be I_{p1}; through the valve, I_{p2}; and the difference would be coming via the meter circuit. When the switch was opened there would be a sudden call for current to bridge the I_{p2}-I_{p2} gap.

bridge the I_{P_2} - I_{P_1} gap.

This is where C comes to the rescue. But it can deliver this current only at the expense of its own voltage. Its own voltage is the same as the anode voltage, so that begins to drop, and in so doing widens the gap between P_1 and P_2 . So more current is called for, and the gap widens more quickly. And so there is an accelerating movement towards Q. Directly P_2 gets past the "hump," the call for current, and hence the rate of voltage drop, begins to decline; until finally, at Q, there is no gap and no further drop in voltage.

With C of the order of 10pF, as it would normally be, the whole process is over in something like one microsecond, so it is difficult to follow by eye. This disadvantage can be overcome by augmenting C by a capacitor of say 16μ F. The slowed-down changes of current from it and also via R can then be observed on suitable milliammeters when the switch is opened after initial setting to as near P as possible. If the error in setting to P is on the other side, the system makes for S instead of Q.

Fair enough; but how about the original problem? How does the system know, at the moment of opening the switch, that the valve curve doesn't bend the other way, as in Fig. 8, which in the region of P is identical with Fig. 7? A rare fool it would look, after rushing madly down as before, to find that Q was non-existent and that the gap, instead of closing up, ever widened, while the scope for filling it by the voltage across C falling was strictly limited—and even reversed!

It appears, however, that this trap would be sprung before the start. For directly we tried to set it to P by connecting the junction of R and the negative-resistance device direct to a source of V_p, as we did in Fig. 6, we would be up against the fact that with

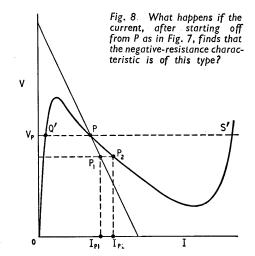
this other sort of negative resistance there would be a Q' and an S', to one of which the system would promptly go and stay. So our problem couldn't actually arise.

You may still feel, as I do, dissatisfied with this outcome, inescapable though it may be. It reminds one of the answer to the old problem of what would happen if an irresistible force encountered an immovable object—that there are no such things. You would like to know, I am sure, whether there is some fundamental difference between the negative resistances in Figs. 7 and 8 which makes itself felt at or near P, without having to go farther along to see which way the curve ultimately bends, and even without having to remember what kinds of difficulties there may have been in getting to P to start with.

An Odd Situation

We seemed to go some way to solving this mystery when we recognized the existence of C. It provided a most satisfactory explanation of our experimental results with the dynatron (Figs. 6 and 7). But it also seems as if it would lead to an extremely embarrassing situation if the negative-resistance slope happened to bend over the other way as in Fig. 8—a rapidly widening current gap to fill, and C at the end of its ability to supply it.

The best thing to do when theory predicts an absurdity like this is to try it in practice. This is where the old point-contact transistor comes in useful. Thanks to Mr. Betteridge of the G.E.C. I was able to obtain an experimental specimen, which



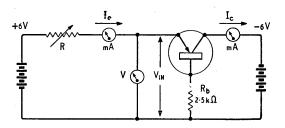


Fig. 9. Point-transistor circuit for providing negative resistance of the Fig. 8 type.

I connected in the simple common-base circuit shown in Fig. 9. Unlike the more usual common-emitter circuit (and the common-cathode valve circuit) its polarities are such that a bias resistance (Rb) causes positive feedback. Because each milliamp change in emitter current causes more than one milliamp change in collector current, the voltage drop in the emitter circuit due to the emitter-to-base positive resistance is more than offset by the reverse voltage drop across Rb due to collector current. By varying R, the relationship between input voltage Vin (measured on a currentless valve voltmeter V) and input current Ie was plotted, as in Fig. 10. Because the reverse drop across R_b was the main ingredient, Vin is wholly negative, but this doesn't matter; the shape of the curve is clearly of the Fig. 5 and 8

In Fig. 10 the load line for the particular value of R corresponding to 0.85mA and 2.0V is shown, giving the working point P. There is no alternative intersection to flip over to, so not surprisingly (from that point of view) this setting proved to be quite stable. But what, you may ask, about stray capacitance? Seeing that around P the relationship between negative and positive resistances is the same as in Fig. 7, which we found to be unstable, how (yet again!) does the system know itself to be stable?

One difference between the transistor circuit and the dynatron—besides the opposite curvature of the bends—is that the resistances are comparatively low, so very small capacitances have proportionately less effect; and another is that the amplification on which the transistor's negative resistance depends falls off at moderately high frequencies. So just to be sure that there was enough to make the thing unstable and start it off on an impossible journey I connected 300 µF across the input.

There was no doubt about the effect. The circuit didn't blow up, but all the meter pointers see-sawed

violently to and fro!

When I started, it was with the firm intention of arriving at a straightforward answer to the question. But the time is far spent, and so far from having cleared up that mystery we have unearthed another -what happens when the $300\mu F$ capacitor charge reaches one of the bends and finds it can (theoretically) neither go on nor can turn back, but somehow in practice does keep on turning? Come to think of it, there is yet With the help of Fig. 7 another. we saw theoretically how capacitance across the dynatron ensures instability when the series resistance is relatively high, by cumulatively widening the slightest current gap I_e(mA) Fig. 10. Actual input characteristic of an experimental circuit

between dynatron and resistance. When the experiment was made with an actual dynatron circuit, it behaved exactly as predicted by this theory. If now we consider in the same way the diagram for a transistor with low resistance, Fig. 5, we find that the current into or out of a capacitance across the transistor necessitates a voltage change which drives the working point P_1 and P_2 towards P_2 , which means that the circuit is stable. In attempting to confirm this by experiment I found it quite a tricky business getting the low-resistance circuit anywhere near P_2 to start with, and the result was invariably the same: it ended up at Q or S. At no time did it show the slightest inclination to be stable. Why did experiment confirm the capacitance theory in a dynatron circuit and contradict it in a transistor circuit?

It looks as if I shall have to get next month's issue

to find out!

High-Remanence Tape

A NEW grade of "Scotch Boy" magnetic recording tape has been introduced by the Minnesota Mining and Manufacturing Company which is of particular interest to high-quality enthusiasts. It is known as No. 120 and has a remanence of 0.9 lines compared with 0.6 lines for the No. 111 standard and No. 150 thin-based grades. The coercivity is 240 oersteds in all three cases.

The advantages conferred by the new tape are three-fold. There is a 3-dB increase of sensitivity for a given input, the maximum input for a given distortion level (1% 3rd harmonic) can be increased by more than 3 dB giving an overall gain at maximum of 6 to 8 dB, or, alternatively, the input can be reduced to a level which gives the same volume as would be obtained from No. 111, but with harmonic distortion reduced by approximately 12 dB.

Like the standard No. 111 tape, the new "High Output" grade is on 0.002-in cellulose acetate base and is available in four spool sizes between 600 and 2,400ft. The cost is about 10% higher than standard tape.

Dates for Your "Wireless World" Diary

ANNOUNCEMENTS have already been made of the dates of many of this year's exhibitions and conventions, but for the convenience of readers we give below a list of the principal events in 1957.

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March 5-7		л.с.i.		v Exhibition	Television Society Royal Hotel, Wob
March 25-28	/.t. ···			Exhibition	Physical Society E Royal Horticultur
April 8–11		e, Park	Hous	w (R.E.C.M.F.) e and Park Land	Grosvenor House London, W.I.
April 9-13	•••	E.E.)	(A.S.	ers' Exhibitior don, S.W.5.	Electrical Enginee Earls Court, Lond
April 12-15	•••	•••	•••	 London, W.C.2.	Waldorf Hotel, L
May 7-17	•••	tion Sh	itoma 	ctronics and Ann, W.14.	Instruments, Elections Olympia, London
•				10w (R,I.C.) sgow.	Scottish Radio Sh Kelvin Hall, Glass
June 28–July 2		nation	Autor	Electronics in	(Brit. I.R.E.) King's College, C
July 10-20	ster.	 Manches	ition logy,	ctronics Exhib nce and Techno	Institution of Electronic College of Science
July 10-20	•••	•••	v. 14.	Exhibition* mpia, London, V	British Plastics E: Grand Hall, Olyn
Aug. 28-Sept. 7	•••			Show (R.I.C.)	National Radio S Earls Court, Lond
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Oct. 23–26			G.B.	endon W L	Radio Hobbies Ex
(hibitions,	iese ex	with th	ction	held in conjun	*Conventions are

WIRELESS WORLD, JANUARY 1957

as in Fig. 9.

JANUARY MEETINGS

LONDON

8th. I.E.E.—"A theoretical and experimental investigation of anisoperimental investigation of aniso-tropic-dielectric-loaded linear electron accelerators" by R. B. R. Shersby-Harvie, L. B. Mullett, W. Walkinshaw, J. S. Bell, and B. G. Loach at 5.30 at Savoy Place, W.C.2. 9th. Brit. I.R.E.—A programme of films on radio and electronic engineer-ing at 6.30 at the London School of Hygiene and Tropical Medicine, Keppel Street, W.C.1.

Street, W.C.1. 9th. Rad Radar Association.—"The problems and techniques of high energy physics" by J. R. Atkinson (Glasgow University), at 7.30 at the Anatomy Theatre, University College, Gower University University

10th. Society of Instrument Technology.—"Electronic automation of machine tools" by F. T. Lett at 7.0 at Manson House, Portland Place, W.1.

11th. Television Society.—"Auto-

natic gain control circuits in television receivers" by S. N. F. Doherty and P. L. Mothersole (Mullard) at 7.0 at 164 Shaftesbury Avenue, W.C.2.
18th. B.S.R.A.—"Hearing aids and audiometers" by S. Kelly at 7.15 at the Royal Society of Arts, John Adam Street, W.C.2.

the Royal Society of Arts, John Adam Street, W.C.2. 23rd. I.E.E.—"Junction transistor bootstrap knear sweep circuits" by K. P. P. Nambier and Dr. A. R. Boothroyd; "Design considerations for junction transistor oscillators for the by F. Oakes; and "Minority carrier storage in semi-conductor diodes" by

storage in semi-conductor diodes" by J. C. Henderson and Dr. J. R. Tillman at 5.30 at Savoy Place, W.C.2.
24th. Television Society.—Fleming Memorial Lecture—"Luminescence" by H. G. Jenkins (G.E.C.) at 7.0 at the Royal Institution, Albemarle Street, W.1. (Admission by ticket only.)
24th. Physical Society.—"Detection and measurement of vibration" by M. L. Parsey at 5.30 at Imperial College, Imperial Institute Road, South Kensington, S.W.7.
25th. R.S.G.B.—Presidential address

S.W.7.

25th. R.S.G.B.—Presidential address followed by "Miniature aerials" by F. Charman (G6CJ), at 6.30 at the I.E.E., Savoy Place, W.C.2.

29th. I.E.E.—Discussion on "The performance of d.c. amplifiers with special reference to the use of transistors" opened by K. Kandiah and Dr. G. B. B. Chaplin at 5.30 at Savoy Place, W.C.2.

30th. Brit, I.R.E.—Battery operated equipment: "A.M.-F.M. receivers" by R. A. Lampitt and J. P. Hannifan; and "Radioactivity Instruments" by K. E. G. Perry at 6.30 at the London School of Hygiene and Tropical Medicine, Keppel Street, W.C.1.

ABERDEEN

9th. I.E.E.—"Colour television" by Dr. G. N. Patchett at 7.30 at the Caledonian Hotel.

CHELMSFORD

15th. I.E.E. (Students).—"Autofollowing radar systems" by J. A. Barber at 7.0 at the Public Library.

DUBLIN

17th. I.E.E.—"The use of radio for communication links" by D. McKenna at 6.0 at the Physical Laboratory, Trinity College.

DUNDEE

10th. I.E.E.—"Colour television" by Dr. G. N. Patchett at 7.0 in the Engineering Department, Electrical Queen's College.

EDINBURGH

11th. Brit. I.R.E.—"Potted components and assemblies" by H. G. Manfield at 7.0 at the Department of Natural Philosophy, University of

GLASGOW

17th. Brit. I.R.E.—"Industrial applications of high-speed pen recorders" by R. Kasler at 7.0 at the Institution of Engineers and Shipbuilders, 39 Elmbank Crescent.

HANLEY

18th. I.E.E.—"Digital computers" by Dr. S. H. Hollingdale; and "Power system engineering problems with reference to the use of digital-com-puters" by C. Robinson and D. H. Tompsett at 7.0 at Twyford Scout Hall.

22nd. I.E.E.—"Germanium a n d silicon power rectifiers" by T. H. Kinman, G. A. Carrick, R. G. Hibberd and A. J. Blundell at 6.30 at 1 Whitehall

LIVERPOOL
2nd. Brit. I.R.E.—"Instrumentation for frequency modulation" by D. R. Willis and A. G. Wray at 7.0 at 1 Old Hall Street.

23rd. I.E.E.—"The electronic control of machine tools" by N. Milne at 6.0 at the Temple, Dale Street.

LLANDARCY

23rd. Society of Instrument Tech-ology.—"Present and future trends in nology.electronic instrumentation" by R. J. Redding at 7.0 at the Training Centre of the National Oil Refineries, Ltd.

MANCHESTER

3rd. Brit. I.R.E. and Junior Institution of Engineers.—"Projection television receivers" by I. Somers at 6.30 in the Reynolds Hall, College of Tech-

nology, Sackville Street. 11th. Institute of Physics.—"Ferromagnetism and magnetic materials" A. E. De Barr at 6.45 at Bragg Building, Manchester University.

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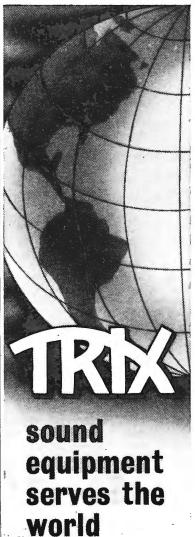
21st. I.E.E.—"Electronics and automation: some industrial applications" by Dr. H. A. Thomas at 6.15 at King's College.

PORTSMOUTH
14th. I.E.E. (Students).—"Digital computers and how they may help the engineer" by Dr. M. V. Wilkes at 6.30 at the C.E.A., High Street.

TREFOREST

16th. Brit. I.R.E.—"Radio techniques in Post Office engineering" by C. T. Lamping at 6.30 at the Glamorgan Technical College.

R. G. Russell-Bates at 7.15 at the Technical College, Wulfruna Street.



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Do We Want Colour?

A QUESTION one is pretty well certain to be asked during any conversation about television with nontechnical folk is: When are we going to get colour TV? Or, the inquirer may put it in the more impatient form: When are we going to have colour TV? It was the same, one gathered, in the United States in the days when only the black-and-white picture was available. Everyone professed eagerness to have colour; but when it came along it was to prove just about the greatest flop in the history of American big business. Those who had seemed so ardently to desire it developed a sales resistance that even the most high-pressure salesmanship couldn't break down. Some months ago it was estimated that there were possibly 100,000 colour receivers in use in the whole length and breadth of the U.S.A.; but a recent investigation by an American magazine puts the total no higher than 75,000. It can hardly be the prices of such sets that have been the snag. These have been brought down from about \$1,000 to the neighbourhood of \$750 or so, and there must be plenty of Americans well able to afford that. One hears of coming models which are to be priced at \$500 or less, but I doubt whether even they will get things really going.

Still Too Complicated

No, the trouble has been, and still is, that colour receivers are complicated boxes of tricks, needing constant adjustment. You can't just sit at your ease and watch. You've got to be continually jumping up from your chair to twiddle knobs for the colours to remain anything like right. Nobody wants exasperating "entertainment" of that sort, and I'm sure that if colour television using any system yet developed became a reality in this country it would flop here as monumentally as it has on the other side of the Atlantic. After all, the monochrome picture isn't all that unsatisfactory, or there wouldn't be well over 6,000,000 sets in use here, or some 34,000,000 (I think that's the figure) in the United States. I know I'd far rather have a good black-and-white picture and a set seldom needing anything but to be switched on and off than a coloured one (rather crude and garish at the best of times) produced by a set which called for constant attention. Them's my sentiments, anyhow; yours, of course, may be quite different.

Basic Inventions Needed

The present position of colour seems to me to be comparable with that of monochrome television when Baird had developed it as far as the scanning disc and neon lamp stage. That had little or no entertainment value and sales were small. For colour to be a success basic new inventions are needed. The flat c.r. tube with its "built-in" frame screen now being developed by Dr. Gabor may be one of these, if, as one hopes, it comes up to expectations when it reaches its final form. But others, too, are wanted if the colour receiver is ever to be as simple to operate as the monochrome and to be as suitable for use by the ordinary non-technical viewer. I've no doubt whatever that such inventions will be made; but when that'll be no one can say. Hence, no one can even attempt to answer the question: When are we going to have colour TV?

The Power of Suggestion

Talking of colour television reminds me that many people reported that they had seen colours on their black-and-white screens when the I.T.A. recently tried out a scheme of colour-by-suggestion. When I was last in London, shortly before this was written, two or three friends (whom I shouldn't have thought prone to imagining things) were in no doubt whatsoever that they had received pictures with distinct traces of colour while watching the B.B.C.'s experimental colour transmissions. Perhaps if the powers-that-be suggest hard enough that our present "penny plain" transmissions are really "tuppence coloured" there'll be no need to develop a genuine colour system!

V.H.F. Catching On

FROM what I hear in talks with people of all sorts and conditions, the v.h.f./f.m. broadcasting service seems to be gradually catching on, though it hasn't yet become as popular as it deserves. I don't think that quite enough publicity has been given to the freedom from interference and the silent background that can be given by a good v.h.f. receiver, provided that it's been properly installed. And I think it a pity that more manufacturers remain unconvinced that there's a big potential

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market for the press-button, or selector-switch set, pre-tuned to the Home, Light and Third Programmes. Nor, again, has sufficient prominence been given to the much superior quality obtainable. In these days, when Hi-Fi is all the rage, one would have thought that first-rate v.h.f. sets would sell like hot cakes. I'm all for omitting the long- and medium-wave ranges altogether; but, as the Editor pointed out a month or two ago, the public generally insists on being able to receive commercial transmissions from the Continent.

The Aerial Problem

Some folk, too, don't like the idea of adding yet another aerial to the not-very-beautiful arrays which already sprout from their roofs. Unless you're in a wireless shadow a simple dipole is all that is needed up to ranges of 45-50 miles at any rate. If your TV transmitter is vertically polarized such a dipole can often be fixed inconspicuously to the mast carrying the H, X, K or what not. In some areas where the television transmissions are horizontally polarized the one aerial array may serve perfectly well for both television and v.h.f. sound. I'm pretty sure that it will in the Norwich area, for instance; but I haven't yet been able to find out for certain, for at the time of writing we're still eagerly awaiting the début of Tacolneston as a v.h.f. broadcasting station. Another great help towards solving the aerial problem, at shortish ranges anyhow, may be the use of built-in ferrite rods.

A Spot of Bother

ONE doesn't envy the I.T.A. its job of trying to provide a good service in that TV spot of bother, the Sheffield area. Some parts of it lie in valleys; some are amongst the hills; many are heavily built up. But it's such a populous and important place that the I.T.A. must feel compelled to do everything possible to give it a satisfactory commercial service. B.B.C. is more fortunate, for the site of Holme Moss is higher and its carriers lower than that of Emley Moor. Even so, there are many Channel 2 black spots in and around Sheffield. On Channel 10 things are much more difficult, for its carriers are so much more liable to be blanketed by hills or tall buildings and to suffer the reflections which give rise to ghosts. It may be that Emley Moor's aerial, 1,250ft above sea level, and its 200-kW e.r.p. won't provide all the answers, and the only thing for some districts will be a "piped" service.



Microromeos

LOVE is a delicate subject which I had always thought to be completely outside the scope of this journal, but the impact of modern technology seems to have altered all that. Love seems well on the way to becoming merely a specialized branch of electronics, and will, I suppose, eventually be measured in microromeos or microcasanovas.

I have already referred to Dr. Grey Walter's recent pronouncement that it would be possible to pick out people who would make compatible marriage partners by examining their

encephalograms.

Now we have Gerald Sykes speaking in the Third Programme on the subject of "Technology and Love." Mr. Sykes is an American and therefore would probably be more familiar with wolf whistles than with heterodyne whistles. It appears that, according to Mr. Sykes, to understand what love is we need to study the psychology of Freud and Jung, and this leads us rather away from electronics into the jungle of the "id" and the "superego."

But we are brought sharply back

But we are brought sharply back to the electronic fold by the latest suggestion that the electronic computer can solve all problems of love and lead to happy marriages. Apparently all that is needed is to feed into a computer the necessary data about any budding Benedick and his Beatrice and it will decide whether or not they are suited to

each other.

I don't think it will be nearly so simple as it is made out to be, for such a lot will depend on the experts who have to decide what is the proper data the computer needs before it can make its calculations. Having decided on the data, the experts then have to turn it into the special binary lingo of the ACE. Personally I would far sooner trust the old-fashioned "Aunty Gertie" who solves love's problems in certain of the more romantic of our women's magazines.

I sincerely hope the day is far distant when W.W. publishes some book like "Second Thoughts on Love Theory," by "Cathode Ray."

Fiat Justitia

WE hear of such extraordinary things being accomplished by electronic computers that it surprises me that more attention has not been paid to them by the medical profession.

Surely a machine could be designed which, when fed with the requisite numerical data concerning bodily temperature, blood pressure

and so on, could make a swift calculation and diagnose the complaint. At the same time it might indicate the correct antidote.

Without doubt such a machine is a possibility of the future and I am very surprised that this doesn't seem to be realized in medical circles. Maybe it is because doctors have a vested interest in keeping any form of mechanical medico off the market. Doctors would, however, always be wanted to feed accurate data to the machine.

Another class of person which has neglected its possibilities is represented by the various Mesdames Estelles who haunt our seaside piers and funfairs. An electronic prognosticator would not put them out of business. They would still be wanted to feed all the enquirer's personal details to the machine to enable it to work out the positions of the planets and other heavenly bodies at the precise moment of birth.

A most important potential field of operations for the computer is surely in our magisterial courts. We often read of the great divergence in the penalties imposed by different benches for the same offence. A wife beater, for instance, who is arraigned before a bench of hard-bitten married men may incur little more than a mild "tut-tut" of reproof from the long-suffering chairman. If, however, he has the ill-luck to appear before a women stipendiary or a bench on which women predominate he can thank his lucky stars that the death penalty is ultra vires for magistrates. An electronic computer when fed with

the correct data on the crime and the prisoner's previous record would unerringly deliver a just and equitable sentence.

TV on Trains

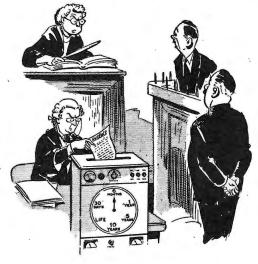
I WAS interested to read recently of the television demonstration given on two specially equipped excursion trains in Scotland. The programmes in each case came from the Guard's van which had been turned into a small studio. No attempt was made to relay ordinary broadcast TV programmes but the demonstration was none-the-less interesting as showing what we can expect in a few years' time.

It would not surprise me if TV eventually became available on all long-distance trains. Would it be possible to use the adjacent telegraph wires for a carrier-current system? It would, of course, be rather like putting the cart before the horse to have TV on trains, as no serious attempt has yet been made in this country to provide ordinary sound programmes in our expresses; yet it has always seemed to me that it would be so easy to provide each passenger who wanted this service with a pair of headphones at an appropriate fee. A start could be made by having a disc jockey in the guard's van of each train; real radio could come later.

Another thing which is lacking in our trains, despite the electronic age in which we live, is means of making a telephone call. There has not even been an attempt to provide a *telegraphic* service, and personally I have been compelled to follow the example

of castaways on a desert island and enclose a message in a beer bottle obtained from the restaurant car. This I have had to throw out when passing through a station in the hope that some porter might pick it up, and usually I have not hoped in vain.

The method is, however, primitive and I hope that this TV demonstration will open the eyes of the British Railways' authorities to the possibilities of equipping trains with an up-to-date telegraph, telephone and television service. The profits might enable them to reduce fares.



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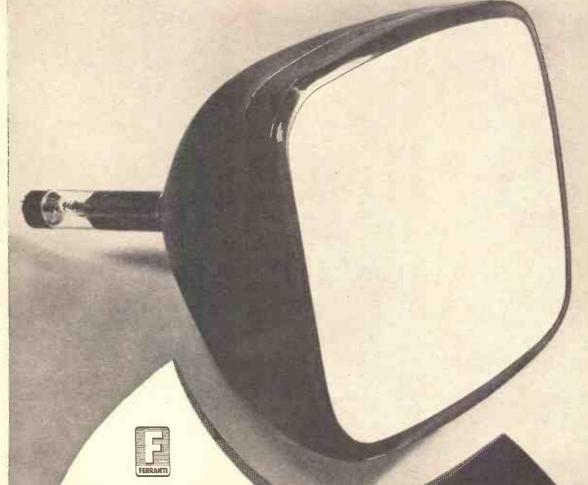
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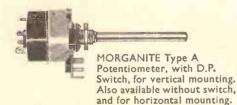
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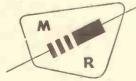
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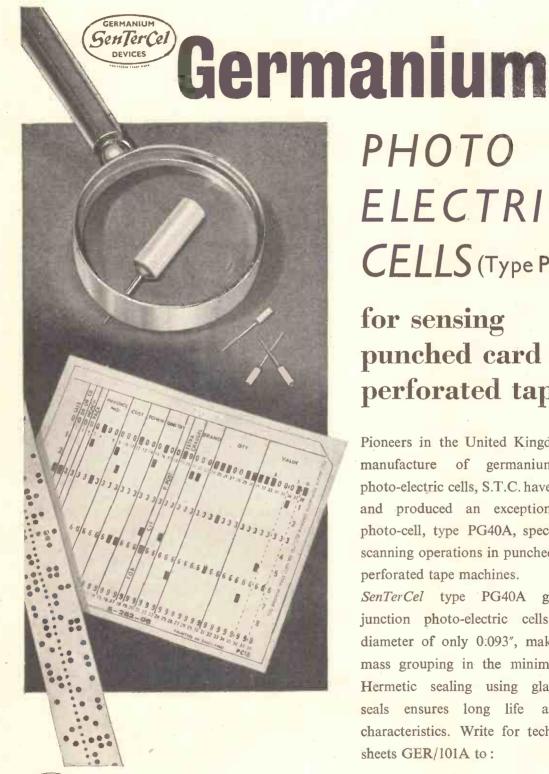


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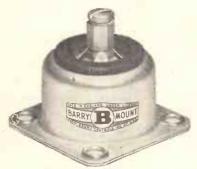
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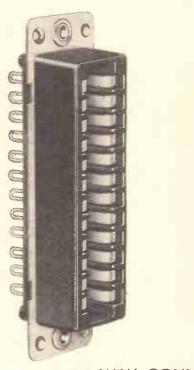
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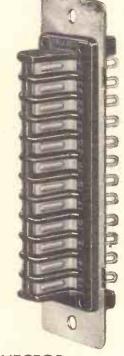
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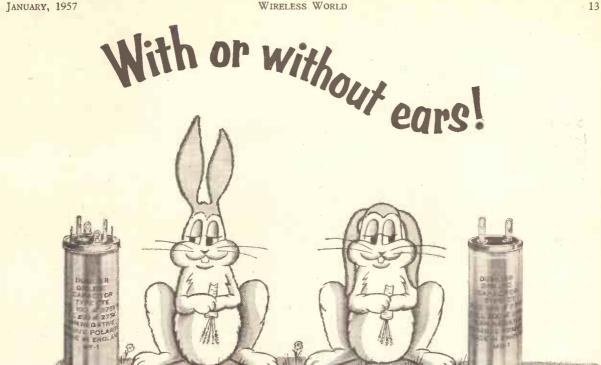
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Capacitance (μF)	D.C. Wkg. Voltage	Dimensions	Ripple Current (mA)
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50	280	3" x 1 3"	500
100	280	2" x 18"	550
50—100	350—280	3" x 13"	500—200
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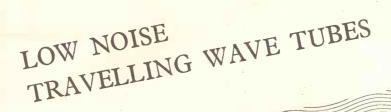
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	N.1002	Low Noise	2000	ımW	10	24	550	200μΑ	200
	N.1004	Power	4000	4W	- 1	21	2600	20mA	450
	N.1005M	Low Noise	4000	ImW	11	22	360	200μΑ	350
	N.1013	Voltage Amplifier	2000	200mW	20	32	650	4mA	300
	N.1017M	Low Noise	1200	ImW	10	20	700	200µA	200
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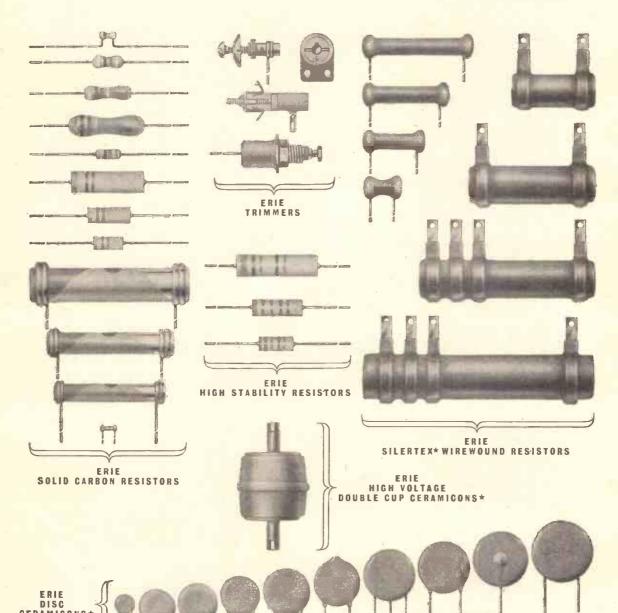
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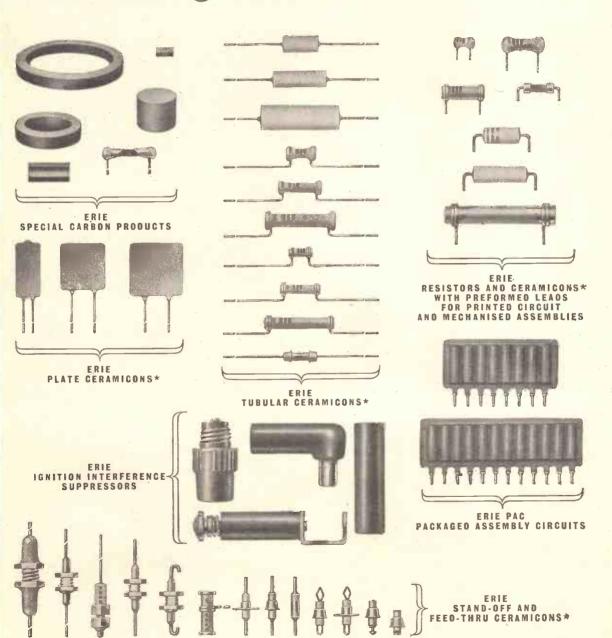




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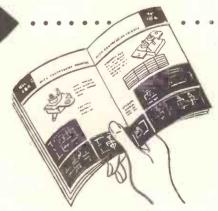
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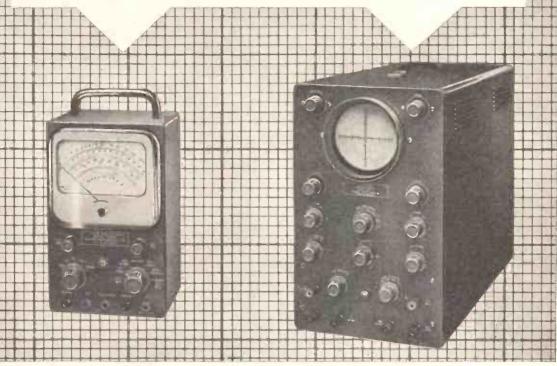


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Type A, No. 2.

Type A, No. 2.

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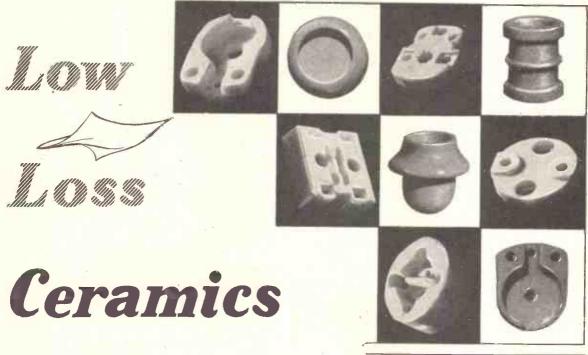
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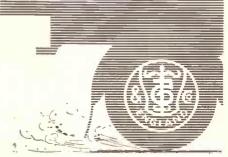
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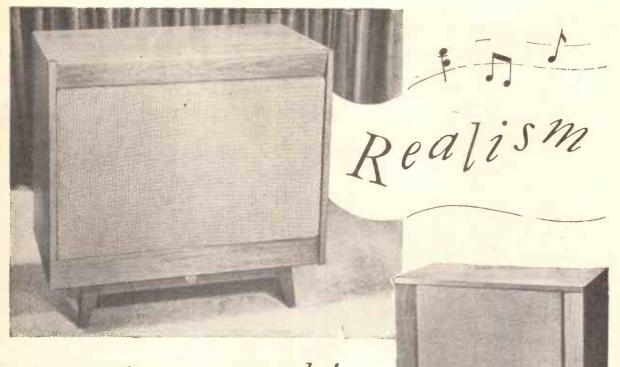


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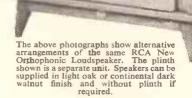
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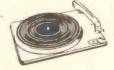
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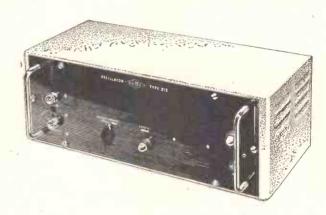
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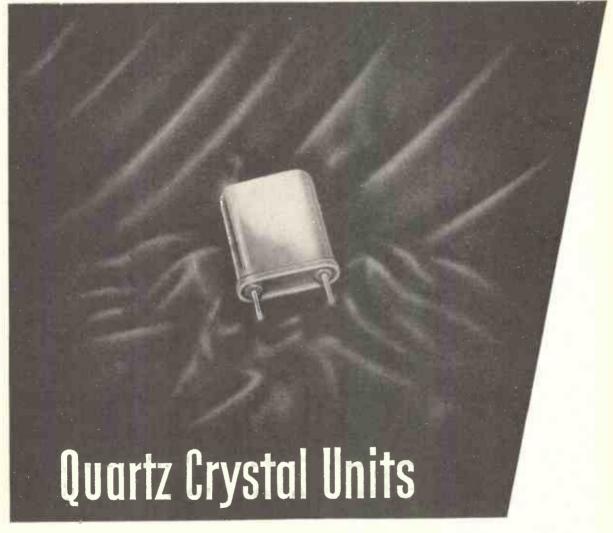
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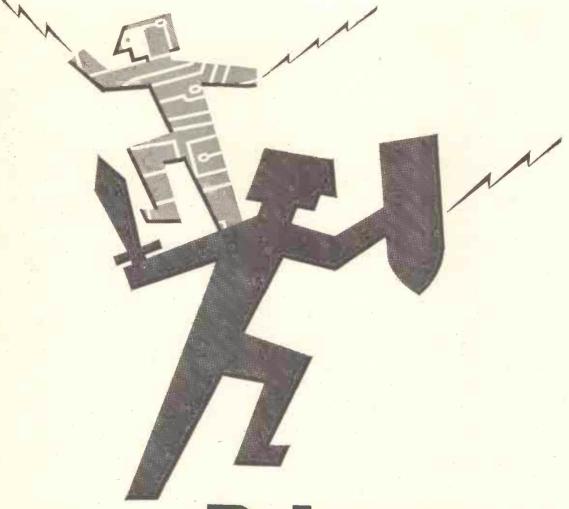


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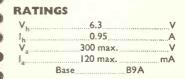


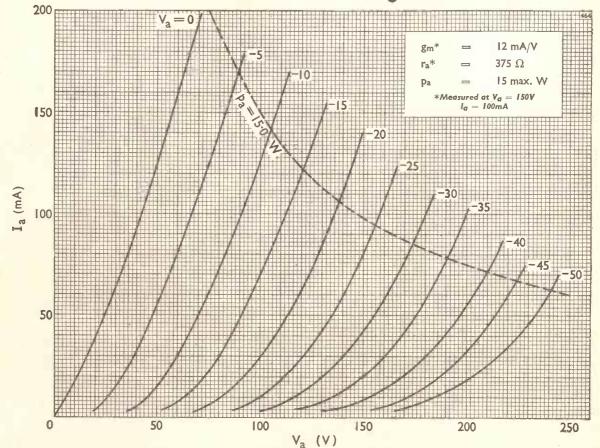
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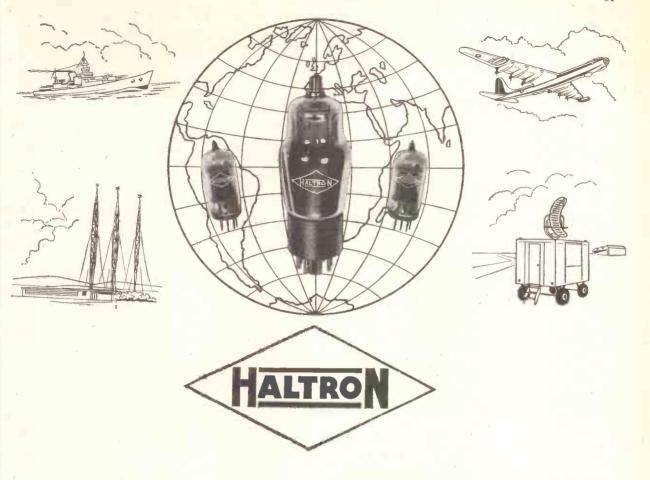
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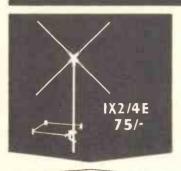


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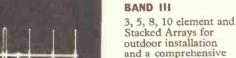


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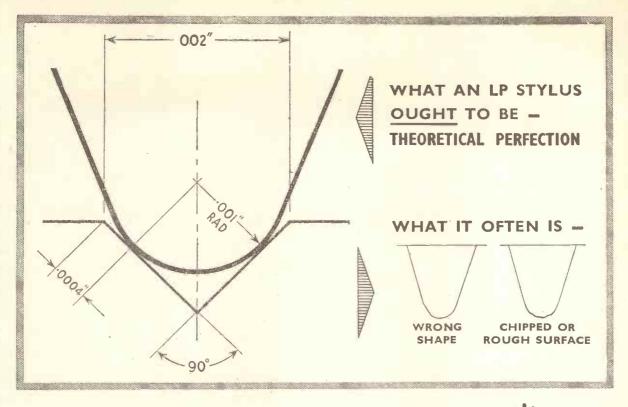


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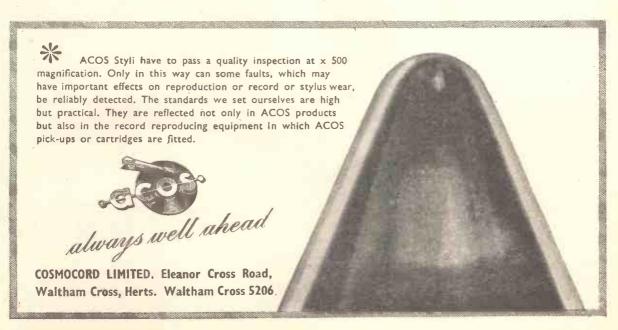
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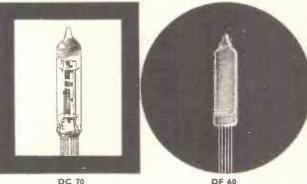


REPLACEABLE STYLI, AS FITTED TO ALL ACOS CRYSTAL AND CERAMIC PICK-UP CARTRIDGES HAVE PERFECT SHAPE, SIZE AND FINISH



For all portable telecommunications equipment

directly-heated





DF 61

space saving

Manufacturers of almost every type of telecommunications equipment in which space is a limiting factor will welcome this newly extended range of Mullard directly-heated subminiatures. Their diameter, which is of the same small order as other components, facilitates tight packing in "sandwich" and other types of assembly.



DF 62

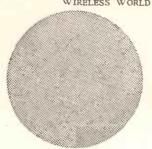
weight saving

Due to their small size, these robust valves offer special weight saving advantages which are particularly valuable in relation to certain types of specialised battery powered equipment such as 'Hand-Talkie' and 'Walkie-Talkie'. They will operate efficiently from comparatively small battery supplies and so allow the overall weight of equipment to be kept to the minimum.

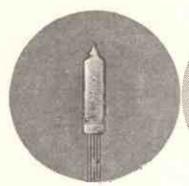


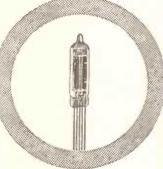
DL 70

Brief technical details are given on the page opposite—more comprehensive information on these and other Mullard subminiature valves is readily available.



subminiatures





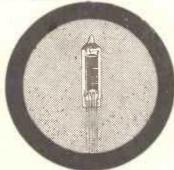


ABRIDGED DATA

DL 73

Commercial Type No.	Services Type No.	American Equivalent	Description	Filament		Typical Characteristics									
				Vf (V)	lf (mA)	Va (V)	Vg2 (V)	~Vgl (V)	ia (mA)	lg2 (mA)	gm (mA/V)	gl-g2		Special Notes †	
DC70	CV2275	_	U.H.F. Triode	1.25	200	150		4.5	14.5	_	3.75	15(µ)	4.0	Pout = 0.55W at 500 Mc/s as class "C" osc.	
DF60	CV2254	5678	R.F. Pentode	1.25	50	67.5 45.0	67.5 45.0	0	1.8	0.48	0.82	=	1000	_	
DF61	CV2371	_	R.F. Pentode	1.25	25	67.5 45.0	67.5 45.0	0	1.7	0.45	0.95 0.75	21	1600 1400	4.0 2.6 = -Vg for 100: reduction in gm	
DF62	CV2237	IAD4	R.F. Pentode	1.25	100	45.0	45.0	0 *	3.0	0.8	2.0		500	_	
DF63*	_	_	Variable-mu Pentode	1.25	25	67.5	67.5	0	1.7	0.49	0.85	_	1600	-Vgl=14V for 100:1 reduction in gn	
DL69	CV2361		A.F. Output Pentode	1.25	25	90	90	2.5	1.75	0.4	0.85		800	P _{out} = 50mW.	
DL70	CV2105	_	R.F. Output Pentode	1.25	110	135	90	7.5	7.5	1.5	1.9	6.5	150	Pout = 0.45W at 200 Mc/s as class "C" amp.	
DL73	CV2299	_	R.F. Output Pentode	1.25	200	100	100	9.0	15	3.8	2.5	6.0	16	Pout = 1.2W at 200 Mc/s as class "C" amp.	
DL620	CV2238	5672	A.F. Output	1.25	50	67.5	67.5	6.5	3.25	1.1	0.65	_	110	P _{out} = 65mW.	

- * At present only sample quantities of this type are available.
- *With 2MΩ grid resistor.
- †The power outputs quoted in the last column are not necessarily under conditions given for Typical Characteristics.





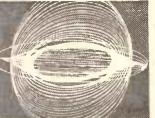
COMMUNICATIONS AND INDUSTRIAL VALVE DEPARTMENT



DL 620

PLACE, LONDON. HOUSE, TORRINGTON

Champion | High-Fidelity unit equipment for the home



Model 853 Power Amplifier

Champion proudly introduce the latest developments in HI-FI unit equipment



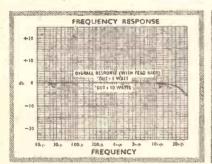
The complete power amplifier for use with either of the 2 other models (853A or 854). It is supplied in a beautifully finished cabinet which can be placed on a side table or bookshelf and will blend harmoniously in any room.

TECHNICAL DETAILS

The amplifier is based on a circuit developed by Mullards incorporating an ultra linear output-stage and contains a Power Supply for a Pre-amplifier and F.M. Tuner.

Maximum power output 11 watts. Frequency Response 1 watt within 1 db. 10 cis— 20,000 c/s—at 10 watts within 1 db. 30 c/s— 15,000 c/s.

Output impedance (Speech Coil): 15 ohm or 3.75 ohm. Mains Supply: 200-250 valts. 50-60 c/s A.C. or 100-130 volts. 50-60 c/s A.C. Sensitivity: 40 mV.



Model 853A Pre-Amplifier Control Unit



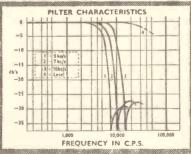
The Pre-Amplifier comprises a low noise, low distortion amplifier with tone controls and low pass filters. The first stage gives balanced compensation for five recording characteristics used by the leading recording companies in England and the U.S.A. This is effected by the use of frequency selective negative feedback. The tone control circuits give continuously variable control of both bass and treble frequencies.

TECHNICAL DETAILS

Input selector.

(1) Tape/Radio Replay.
(2) R.I.A.A.
(3) A.E.S. and R.C.A. ORTHO.
(4) Col. L.P. and F.F.R.R.
(5) N.A.R.T.B. and H.M.V. L.P.
(6) British 78 R.P.M.
(7) Meraphana

Microphone. (1) Microphone.
Treble and Bass Control.
Volume Control.
Low Pass Filter, Switched
10 K c/s. 7 K c/s. 5 K c/s
level. Dimensions 15" x
4½" x 4½".



The new Champion High-Fidelity Equipment is designed to bring to every home where music is enjoyed and appreciated, a new conception of listening. In ultimate form High-Fidelity is reproduction exactly as the artist recorded it.

> Model 854 Pre-Amplifier and F. M. Tuner



The Master Control comprises a low noise, low distortion tone control pre-amplifier and a sensitive VHF/FM tuner covering the frequency range 88-95 Mc/s, housed in a handsome cabinet matching the Main Amplifier Model 853.

TECHNICAL DETAILS

Input Selector.
(1) Mains OFF Switches off mains to Power Supplies in Model 853.
(2) FM Tuner.
(3) L.P. Records, Sensitivity 50 mV.
(4) 78 Records, Sensitivity 60 mV.
(5) Tapel Radio Replay, 100 mV.
(6) Microphone, Sensitivity 10 mV.
Volume Control.
Treble and Bass Controls

Volume Control.
Treble and Bass Controls.
Tuning Control.
Tuning Indicator,
Magic Eye. Mullard EM
81. Dimensions 15" x 8½"
** 01"

 $x 9\frac{1}{2}$ ". 23 gns. + 10 gns. P.T.

With the Champion High-Fidelity you will become aware of a new excitement in music; surprised and delighted to hear with extraordinary realism your favourite works, which before lacked clarity.

ELECTRIC CORPORATION

London Office & Showrooms: 8 Eccleston Street, S.W.1. Works: Newhaven, Sussex.

TONE CONTROL CHARACTERISTICS FREQUENCY



New channelling and specification standards for mobile radio are being introduced in the United Kingdom and many parts of the world. The "Ranger", Pye's latest V.H.F. mobile, has been designed to anticipate these and will, in fact, meet specifications for the next ten years. The Pye "Ranger" therefore combines superlative performance with the maximum technical life. No matter what your channelling requirements the Pye "Ranger" will meet them.



3 amplitude modulated versions are available

W = 100 Kc/s. channelling for aeronautical and multicarrier schemes.

N = 60 Kc/s., 50 Kc/s. or 40 Kc/s. channelling.

VN=30 Kc/s., 25 Kc/s. or 20 Kc/s. channelling.

The Ranger has been designed to meet the following leading specifications.

U.S. Federal Communications Commission
Canadian R.E.T.M.A.
Canadian Dept. of Transport

British G.P.O. existing and proposed specifications

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Pye Limited, Mexico City.

Pye Limited, Tucuman 829, Buenos Aires, Argentina.

PYE LIMITED

Phone: Teversham 3131

Pye Radio & Television (Pty.) Ltd. Johannesburg, South Africa,

Pye Canada Ltd., 82, Northline Road, Toronto, Canada.

> Pye Pty. Ltd., Melbourne, Australia.

CAMBRIDGE

Messrs. Telecommunications, Jamestown Road, Finglas, Co. Dublin.

> Pye Ltd. Auckland, C.I., New Zealand,

Pye (France) S.A. 29Rue Cambon Paris Ier

• ENGLAND

Cables: Pyetelecom, Cambridge



INSTRUMENTS

ADMITTANCE BRIDGE TYPE B.801

1 Mc/s-100 Mc/s

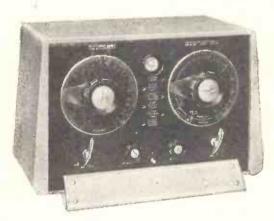
For balanced and unbalanced measurement.

Susceptance: Equivalent Conductance: 0-100 mmho. to ±230 pF.

Accuracy: $\pm 2\%$, ± 0.5 pF. Accuracy: ±2%, ±0.1 mmho. This is one of a range of bridges for use with external source and detector for the measurement of aerials, cables, feeders, and a variety of components and materials between 15 kc/s and 250 Mc/s. Bridge sources and detectors are available for use between 1-100 Mc/s and 50-250 Mc/s.

PRICE £150 NET EX WORKS





COMPONENT BRIDGE TYPE B.121

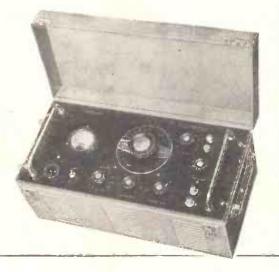
A general purpose 50 cps 3 terminal transformer ratio arm bridge for the measurement of Resistance, Capacitance and Inductance in the ranges 3-100 M Ω , 1 pF-100µF and 100 mH-10,000H, accuracy ±2%. Direct readings of the resistive and reactive components of impedance and facilities for "in situ" measurements are notable features.

PRICE £60 NET EX WORKS

AUDIO WAVEFORM ANALYSER **TYPE A.321**

A portable instrument to measure the relative levels of the components of a complex waveform over a range of 75 db between 50 c/s and 20 kc/s. Input impedance $100 \text{K}\Omega$ unbalanced or $> 25 \text{K}\Omega$ balanced. In transportable case as shown, or for standard 19" mounting.

PRICE £250 NET EX WORKS



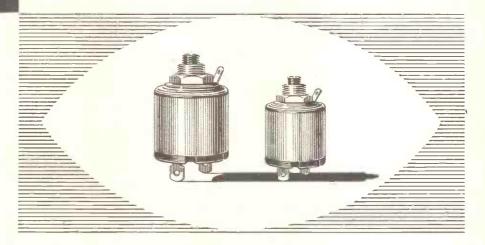
HIGH EFFICIENCY POT CORES

CAN NOW BE ADJUSTED.....

AFTER MOUNTING

OVER AN AVERAGE RANGE OF 10%

WITH A SETTING ACCURACY OF .5%



These new Mullard 14mm and 18mm pot cores are completely self contained, simple to mount and easily adjusted after mounting. Unique features include single hole fixing and two or four way terminal plates. Adjustments of inductance are made by means of a screw which varies the position of a magnetic shunt in the centre of the core; in many cases this eliminates the need for trimming capacitors. Designers will see from the brief characteristics listed here that Mullard adjustable pot cores are particularly suitable for use in high grade communications equipment, tuned circuits and filter networks. Those requiring further technical details are invited to write to the address below.

14mm Pot cores

 18mm Pot cores





'Ticonal' permanent magnets Magnadur ceramic magnets Ferroxcube magnetic cores



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Prompt delivery

Credit Terms:
9 monthly payments of £3.15.0

Unique Offer: You can part exchange an old TAYLOR instrument for a new one. Write for details.

VALVE TESTER

Model 45C

A comprehensive valve tester to measure the mutual conductance of most types of British, American and Continental receiving valves. Measures over 4,000 different valves, simple and rapid operation. 4in. scale moving coll meter.

Mutual Conductance: Two ranges: 0-3 mA/V. and 0-15 mA/V.

Cathode Leakage: Tests for Heater/Cathode insulation up to 10 megohms.

Emission: Rectifiers and Diodes can be tested for emission.

Inter-Electrode Shorts: Short circuits between electrodes are shown on the meter.

Heater Continuity: Meter indicates continuity of heater or filament.

Gas Tests: Press-button "gas" tests show abnormal positive or negative grid current.

T.V. cathode ray tube adaptor, model 445 available.

Hire Purchase Terms Also Available

INSULATION TESTER Model 130A

For workshop tests and component checking

This mains operated ohmmeter covers insulation and medium values of resistance. It is light and portable.

Meter: 4in. scale Taylor Moving Coil meter with knife-edge pointer.

Sensitivity: 50µA.

Ranges: (1) 20 ohms to 100K. ohms at test pressure of 50 Millivolts.

(2) 200K. ohms to 1,000 megohms at test pressure of 500 volts.

Accuracy: On each range 10% of centre scale values.

Overload Protection: Instantaneous Meter overload protection on all ranges.

Press Switch: Disconnects meter when rapidly charging capacitors for test,

Power Supply: 115V or 200/250V A.C., 40/100 c/s. Dimensions: $8 \times 5\frac{3}{4} \times 4\frac{1}{2}$ in. Weight: $5\frac{3}{4}$ lb. (2.6 Kg.)

Write for details of these and other models

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Prompt delivery

Credit Terms:

9 monthly payments of £2.0.0



PRESSURE UNIT

SPECIFICATION

Power Handling Capacity

10 watts peak

Voice Coil Impedance 15 ohms

Frequency Response 120-9000 c.p.s. Flux Density 12,000 gauss

Flux Density
Pole Piece

1.5in.diameter

PRICE £6.10.0

Specially designed and developed to meet the need of the P.A. Engineer requiring a compact, efficient unit combining good tone with average handling capacity, at a price that will make the "small" installation a profitable proposition.

HIGH SENSITIVITY. Heavy cross-sectioned cup with latest anisotropic alloy CP magnet.

PHASE EQUALISING THROAT. One-piece zinc based alloy die-casting.

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SPRING LOADED TERMINALS. Ensure quick and positive line termination.

WEATHERPROOF. Totally enclosed, ensuring protection when in exposed position, watertight gland cable entry.

Manufactured in Gt. Britain by

DIMENSIONS

> DC 12 PRESSURE UNIT (WITH TRANSFORMER) As DC 10 but fitted with totally enclosed 100 v line transformer tapped 2.5, 5, 8 and 12 watts. Price £7.10.0

Rola Celestion Ltd.

FERRY WORKS THAMES DITTON, SURREY

Telephone: EMBerbrook 3402

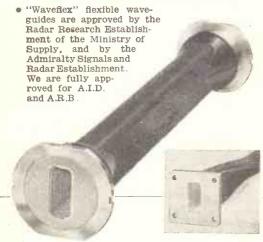
"Waveflex" Flexible Waveguides FLEXIBLE and TWISTABLE

-Precision built for

long and reliable service

CHECK THESE EIGHT "STAR" POINTS:-

- Two types:—
 Flexible—twistable
 Flexible—non-twistable
- The high quality of "Waveflex" waveguides is maintained because all production operations from selection of correct materials to final testing are completed within the one organisation.
- Specially produced by an exclusive method of convoluting strip metal.
- The 'Neoprene' rubber sheath which is moulded and bonded to the guide, has been specially produced to give flexibility at extremely low temperatures.
- WG.16 twistable waveguides are designed to take a plus or minus 30 degree twist per foot.
- A standard range of "Waveflex" waveguides is made in lengths from 3" to 36" fitted with standard flanges. We shall be interested to investigate special guides to meet particular requirements.
- "Waveflex" flexible waveguides to match rigid guides in WG. 10, 15 and 16 are in production, the final range will also include WG. 11, 18 and 22.



HERE ARE THE TEST DETAILS

A typical specification of WG. 16. V.S.W.R. '97 minimum per. end termination. Attenuation '15 DB/ft. maximum. Band width 8.2 to 10.7 k.m. c/s. Monitoring tests are carried out on a unique rig which flexes and/or twists the "Waveflex" guides many hundreds of thousands of times to ensure reliability in use.

WAVEFLEX

Full technical details from:-

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One of the Tecalemit Group of Companies.





CUTTERHEAD



These units are a development from our type "D" feedback cutterhead and have similar mechanical and electrical constants but are operated from a single winding. They may be used in conjunction with any high grade power amplifier.

SENSITIVITY—3 volts input for 1 cm/sec at 78 R.P.M.

IMPEDANCE—15 ohms at 1000 c/s
FREQUENCY RESPONSE—±3db—50 c/s to 10 Kc
6db at 20 Kc

DISTORTION—2% at 1000 c/s
WEIGHT—6½ oz (184 grams)
STYLUS HOLE—0.064" or 0.0625" as required
FITTING—Direct mounting on Presto and similar
machines

* Also available n horizontal form, type C/H

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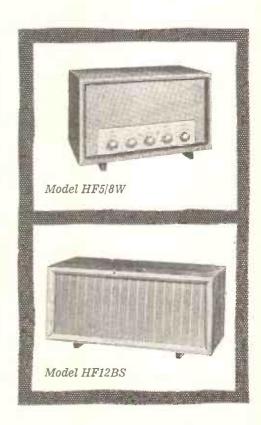
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Western Hemisphere. Reeves Equipment Corp., 10 East 52nd St. New York 22, N. Y. Australian Agent. Simon Gray Pty. Ltd., Elizabeth St., Melbourne C.I Australia.

New Low Price HIGH for the home

The Pye HF5/8 is a new, reasonably priced amplifier specially designed for use in the home, with peak output of 8 watts. Features: "loudness control" which correctly accentuates bass and treble at low volume levels; 4 plug-in inputs; 5 pick-up compensators; 4 record re-play characteristics; infinite damping factor. Harmonic distortion at 1 Kc/s: less than 0.3% overall at 5 watts output. Noise and Hum: main amp. better than 70 db's—overall, better than 55 db's.

The new Pye 12 watt Bookcase Speaker—equally at home in the drawing room or bedsitter—brings high fidelity to the ordinary listener at a price he can afford. Extremely compact, it comprises two matched 8 high flux speakers with special cones, operating in parallel and specially mounted in an acousspecially mounted in an acoustically designed chamber to give optimum performance. Fundamental resonance 60 c.p.s. Flux density 9,500 gauss. Frequency range (in Cabinet) 40—13,000 c.p.s. Impedance: 15 ohms. Power handling capacity: 12 watts. Finished in walnut veneers.





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SONIXGRAM

A COMPLETE DOMESTIC HIGH FIDELITY SYSTEM

Truvox TR7U Mk.111 Tape Unit

PABO-I Tape Pre-Amp and

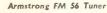
Colloro 2010 Transcription Gramophone Unit

Armstrong AM44 Tuner

● Variable Selectivity ● 4 wavebands • Magic Eye Tuning . Infinite Impedance Detector • Cathode follower £19/17/-Output

Armstrong Alo Amplifier & Control Unit

• 10-12 watts ultralinear • 0.1% total harmonic at 8 watts . Within 1 dB 15-30,000 eps . 4 input positions . Equaliser . Filter . Se; arate Bass and Treble controls £29/10/~



· Permeability Tuning · Freedom from Drift . Magic Eye Tuning . 3 position HT Supply Socket . Automatic Limiting £22/1/-

Armstrong Labyrinth Loudspeaker Enclosure

Revolutionary new design offering hiff reproduction from a cabinet small enough to blend into any home, Goodmans AUDIOM 60 (Bass Cone). Plessey Alumínium Foice Offerble Unit with fully matched Cross-over Network.

Complete \$30.

All units are available separately, and in various combinations in the Sonixgram

Price (COMPLETE) £200

ARMSTRONG WIRELESS & TELEVISION CO. LTD. WARLTERS RD., HOLLOWAY, LONDON, N.7. Tel. NORTH 3213/4

PRECISION High Fidelity

4 SPEED TRANSCRIPTION UNITS WITH VARIABLE SPEED ADJUSTMENT.

MAIN FEATURES

- Speed continuously variable from 29 r.p.m. to 86 r.p.m. Pre-set adjustable "click-in" position for 78, 45, 33\frac{1}{2} and 16 r.p.m. Playing old celebrity discs requiring speeds above 78 r.p.m. Tuning record pitch to a musical instrument. Correcting for mains frequency variations.
- Accurately balanced heavy precision made turntable eliminates Wow and Flutter.
- Unique VERTICAL EDGE-DRIVE PULLEY principle eliminates Rumble.
- Less than 1% change in speed for up to 13% change in Line Voltage. Large resilient 4-pole constant velocity
- motor. 0
 - Model G.L.50/4 and G.L.56 fitted with weight adjustable precision Pick-up-Arm
 with plug-in shell, incorporating the
 Superb Goldring Variable Reluctance Cartridge No. 500.

TYPE GL50/4 Low Loading velocity operated Price £15.15.0 Automatic Stop P.T. £6.2.10

TYPE GL55. Without Pick-up. FITTED WITH BAND LOCATION DEVICE Price £12.12.0 P.T. £4.18.4

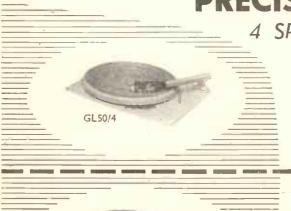
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DIAMOND STYLUS EXTRA

£3.15.0 P.T. £1.9.3

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GL55

REPLACEMENT



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Model 5in. G Price 25/8 inc. P.T.



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Model 8in. C Price 31/11 inc. P.T.



7x 4in. G Elliptical Price 25/8 inc. P.T.



Model 10in. C Price 39/9 inc. P.T.



10 x 6in, C Elliptical Price 39/6 inc. P.T.



ELMAG High Fidelity Units

Designed to give good quality at domestic volumes. For a power output stage providing more than 4 watts, 2 or more speakers are recommended.

Flux Density 8,000 gauss (27,500 Maxwells). Frequency Response 40-12,000 c.p.s.

9 x 5in. Model 59T. Price 38/2 inc. P.T.
All prices are for speakers without transformers.

TRADE TERMS: 331%

ELECTRO ACCIUSTIC INDUSTRIES LTD

STAMPORD WORKS REGED LANE TOTTERHAN HIS THE Telephon BOOM STORE

OHMS? RATING? **TOLERANCE?**

.... it's easy with



Continuous Storage Units



Thousands of LAB Continuous Storage Units are daily solving the problem of control and storage of the great range of resistors. Compact, and capable of storing up to 720 separate resistors, LABpak make selection positive, simple and speedy. Now that Ceramicaps, Histabs and Wirewound resistors have been added to the carded range, the usefulness of LABpak storage units is enhanced.

FREE with any purchase of the LABpak range, these units are the complete answer to the storage problems of small production units, laboratories, etc.

MAKE UP YOUR ORDER TODAY - DELIVERY EX-STOCK

All LABpak resistors are carded in ohmic value, rating and tolerance, colour indexed and tabbed for easy selection.

The LAB Continuous Storage Units are available from your normal source of supply, but more detailed information and literature can be obtained from:

THE RADIO RESISTOR CO. LTD.

50 ABBEY GARDENS . LONDON . N.W.8 Telephone: Maida Vale 5522



HARTLEY-TURNER SOUND EQUIPMENT LOUDSPEAKER **ENCLOSURES**

Now available in either assembled or in kit form to reduce freight charges for export orders, the Hartley-Turner "Boffle" is the answer to the need for economy in space and cost without sacrifice in quality.

Designed specifically for the types 215 and 315 Hartley Loudspeakers but equally suitable for any other high quality 10" or 12" loudspeakers, these enclosures utilise a special acoustic filter which enables the performance of an infinite baffle to be obtained from a unit only 18" cube.

Prices

In Kit Form

шл	XII FORIII,		
	Type 1.K. for 10 Loudspeakers	" diameter	£8 . 10 . 0
	Type 2.K. for 12 Loudspeakers	" diameter	£8.10.0
Ass.	embled,		
	Type 3.A. for 10' Loudspeakers	diameter	£9.0.0

H. A. HARTLEY CO. LTD.

£9.0.0

Type 4.A. for 12" diameter

Loudspeakers

66, WOODHILL, WOOLWICH. LONDON, S.E.18.

Phone: Woolwich 2020. Ext. CB32

Build yourself a 75 gns Radiogram for

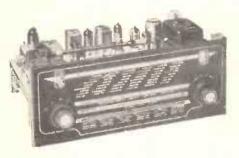


£54-7-6

CABINET CAT. NO. CAB/03

A magnificent Bureau-type Cabinet of the very highest quality in specially selected Walnut veneered exterior, Light Sycamore interior with Rexine lining to match. Outside dimensions, length 34in., depth 17½in., height 23in. Sloping control game on right-hand side annow. 33in. Sloping control panel on right-hand side approx. 16in. x 10½in. Removable approx. 15½in. x 15in. Packing and carriage 25/-. Removable baseboard on right side

Or on Credit Terms. CASH £17-6-6



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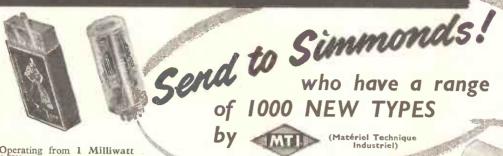




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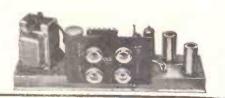


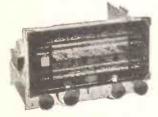
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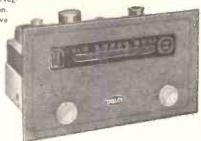
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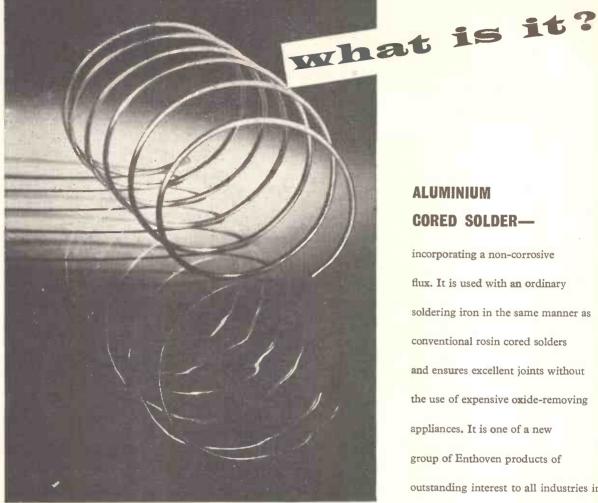
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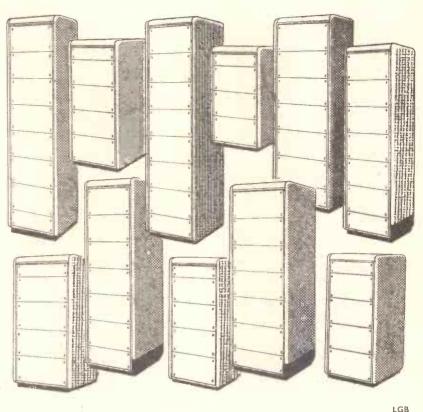
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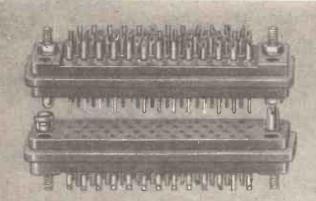
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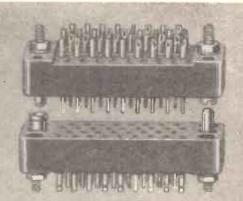
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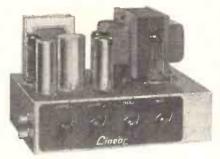
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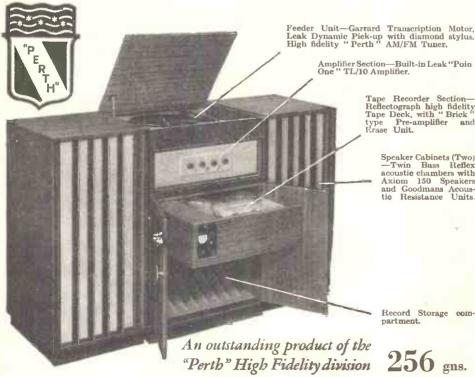
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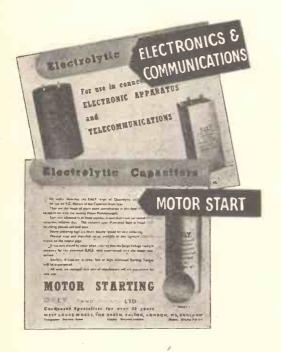


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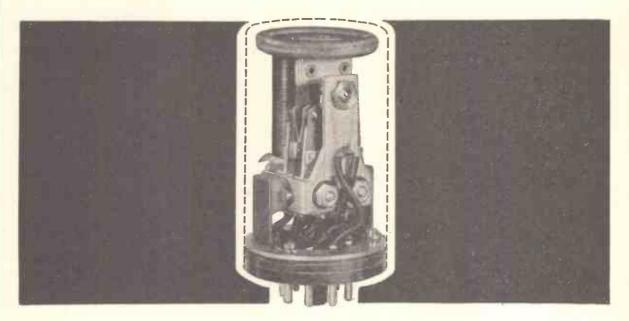
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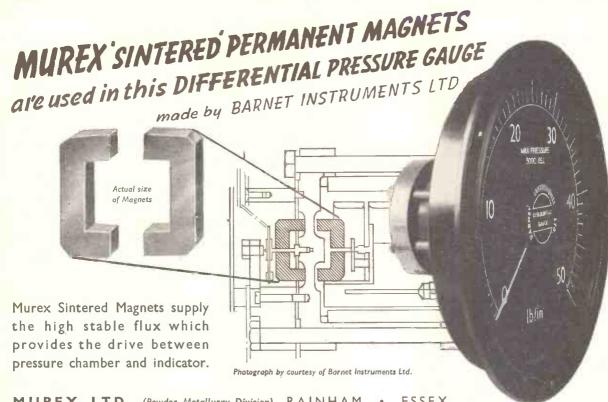
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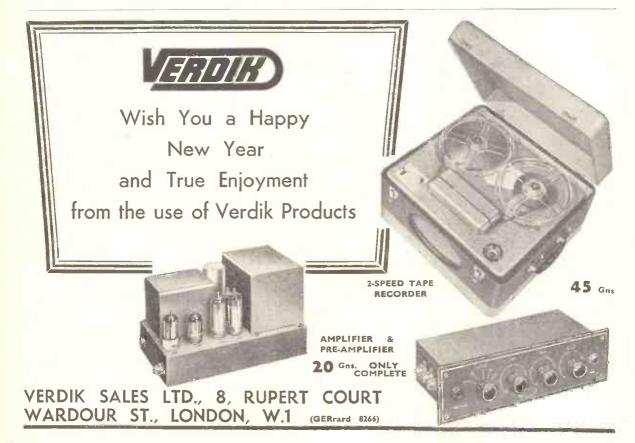
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another make and would like to save money if possible, we should like to make the following clear-cut offer: If he buys one of our "Symphony" Amplifiers or Tuners and is not entrely satisfied with it Symphony Amplifiers of Luners and is not entury satisfied with the may return it for full credit against any other amplifier or tuner on the market. It should be emphasised at this stage that we can supply any Amplifier, Radio Tuner, etc., advertised.

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It is essential to mention "Wireless World" when requesting Catalogue or when ordering.

The New No. I "SYMPHONY" AMPLIFIER MARK III is a 3-channel 5-watt Gram/Radio Amplifier with astonishingly flexible tone control. You can lift the treble, the bass, or-and here is the unique featuretreble, the bass, or—and here is the unique teature—
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amplifier to a curve equal and opposite to the resultant
curve of the other items in the chain so what finally
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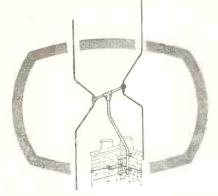
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	£	5.	d.		£	в.	d.		£	ß.	d.
Editor 2-speed Standard	50		0	123/3		4		46/8	50	8	0
Editor Super Hi-Fi	65		0	159/1	82	11	0	60/4	65		0
Playtime (complete)	31	4	6	76/4	15	12	6	29/-	31	4	6
Playtime Plus	36	15	0	89/10	18	8	0	34/-	36	15	0
Sound	57	15	0	142/-	28	17	6	53/-	57	15	0
Sound Cadet	40	19	0	103/-	21	0	0	39/-	40	19	0
Vortexion 2A	84	0	0	205/4	42	0	0	77/10	84	0	0
Vortexion 2B	99	0	0	242/-	49	10	0	91/9	99	0	0
Ferrograph 2A/N or 2A/NL	79	16	0	195/1	89	18	0	741-	79	16	0
2A/NH	90	6	0	218/6	45	3	0	83/8	90	6	0
Collaro Tape Transcriptor	20	0	0	48/11	10	0	0	19/2	20	0	0
Wearite 2A Tape Deck			0	85/7	17		0	32/5	35		0
Truvox Tape Deck	24	3	0	57/1	12	1	6	22/8	24	3	0
Lame Mk. VI Deck	18	10	0	45/8	9	5	0	17/11	18	10	0
Gramophone Motor Unit	S										
Garrard BC98 Changer	19	7	7	47/4	9	13	9	18/8	14	6	0
Garrard RC120 Changer	12	12	4	31/4	6	6	2	13/-	9	1	6
Collaro RC54 Changer	13	17	0	34/1	6	18	6	14/-	10	0	0
2010 and Pickup (T)			0	47/8	9	15	0	18/11	14	-1	6
2010 less Pickup (T)	14	18	0	36/5	7	9	0	14/11	10	15	0
Connoisseur Variable (T)	28	11	4	71/-	14	5	8.	26/6	20	0	0
		8	2	66/7	13	4	1	24/6	19	0	0

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Model	Pi	rice		De	pos	it	Paym	ents	of
820	€38	0	0	£4	6	8	€4	6	8
840A	€55	0	0	£6	8	4	£6	8	4
750	£78	0	0	'£9	2	0	£9	2	0
888	£110	0	0	£13	16	8	£13	16	8
680X	£120	0	0	£14	0	0	£14	0	0

Cash price if paid in 6 months by Banker's order. Carriage paid per passenger train

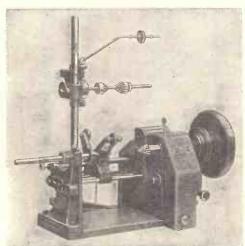
Model 840A is for A.C. or D.C. 110/250 v.; 750 and 680X 110/240 v. A.C. These sets are the choice of the discerning professional and amateur users. Descriptive literature gladly forwarded.

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TECHNICAL DATA

on the NEW Type 515 Oscilloscope

DC-TO-15 MC PASSBAND

High in performance, but low in size, weight, and cost, the Type 515 fits a relatively new requirement area. Besides its extra capabilities in applications requiring vertical response out to 15 megacycles, it occupies less space and is easier to handle than most other general-purpose laboratory oscil-

loscopes.

VARIABLE VOLTS/CM
5
10
20
.2
UNCAUSRATED

Risetime of the dc-coupled vertical amplifier is less than 23 millimicroseconds. Sensitivity is accurately calibrated, 0.1 v/cm to 50 v/cm in nine steps. A variable control adjusts the sensitivity between calibrated steps and out to 125 v/cm. To help avoid accidental inaccurate readings, a warning light indicates an uncali-

light indicates an uncalibrated condition when the variable control is in use. A balanced network delays the signal 0.25 μ sec to permit observation of the leading edge of the waveform that triggers the sweep. Direct input capacitance of approximately 36 $\mu\mu$ f is reduced to approximately 10 $\mu\mu$ f by use of the 10x attenuator probe supplied with the instrument.

SIMPLIFIED SWEEP CONTROL

All 22 of the Type 515's accurately calibrated sweeps are selected by the same control knob. This knob also indicates the sweep time-per-centimeter when the 5x magnifier is in use, making mental calculation of time intervals unneces-

sary. The normal sweep is expanded to 50 centimeters by the magnifier, and the horizontal-position control has sufficient range to display any 10 centimeters of the magnified sweep. To maintain uniform bias on the control grid of the cathode-ray tube for all sweep speeds and repetition rates, the unblanking waveform is dc-coupled.

Calibrated fixed sweeps extend from 0.2 µsec/cm to 2 sec/cm. A variable control makes the sweep range continuous from 0.2 µsec/cm to 6 sec/cm. Here again a warning light indicates an uncalibrated condition when the variable control is in use.

AUTOMATIC TRIGGERING

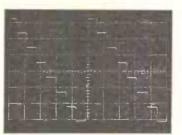
Automatic triggering is a real convenience in a great many oscilloscope applications. This one position, without further adjustment of the triggering controls, permits signals of widely differing frequencies and amplitudes to initiate the sweep, and provides a reference trace on the screen in the absence of an input signal. The automatic circuit operates at a natural rate of about 50 cycles, but synchronizes readily with incoming signals from 60 cycles to 2 megacycles.

Triggering versatility is one of the many highly-useful qualities of the Type 515. You can trigger the sweep from either the positive or negative slope of an internal, external, or line-voltage signal. On any of these signals, you can trigger the sweep at a selected amplitude level. You select

either ac or dc-coupling through the trigger circuitry. You can synchronize the sweep with sine-wave signals up to and beyond 20 megacycles. You can block out the low-frequency component of a composite signal, permitting the high-frequency component to trigger the sweep. These complete triggering facilities make possible a steady display of just about any signal you are likely to encounter.

LARGE DISPLAY AREA

A full 6-centimeter by 10-centimeter linear display can be presented on the screen of the new Tektronix cathode-ray tube, Type T55P, developed especially for this instrument. Characteristics of this new tube help make possible the



wide signal-handling range and excellent transient response of the Type 515. Accelerating potential is 4000 volts. A T55P2 is normally supplied, but a P1, P7, or P11 screen is available on request at no extra cost.

PORTABILITY

It's a bit unusual for higher performance to come in an oscilloscope that's smaller and lighter than previous models. But this combination of compactness and performance makes the Type 515 most convenient for those more-exacting field applications. Handling ease and simplified controls are characteristics also desirable in the increasing number of production-line test stations where high performance is a new requirement. The Type 515 weighs only 40 pounds and measures 93/4" wide, 131/2" high, 211/2" deep.

OTHER CHARACTERISTICS

Many of the other features you'd expect to find in any Tektronix Oscilloscope are part of the Type 515. Square-wave amplitude calibrator, sweep sawtooth and gate available at front panel, illuminated graticule, and electronically-regulated power supply are some of the "standard equipment". New style cabinet with removable sides speeds any maintenance that may be necessary.

TYPE 515...\$750 (F.O.B. Portland, Oregon) **£290.0.0** (Delivered in England)

The above prices are exclusive of duty.



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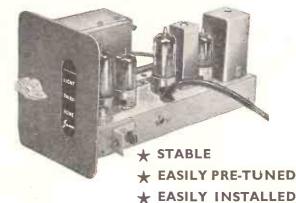
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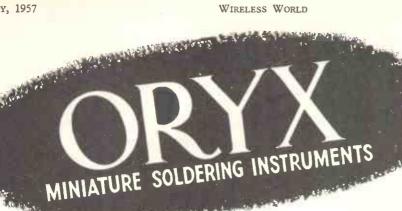
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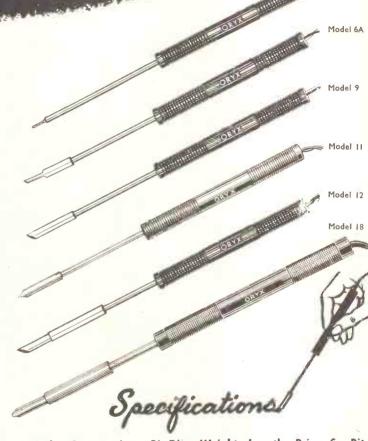
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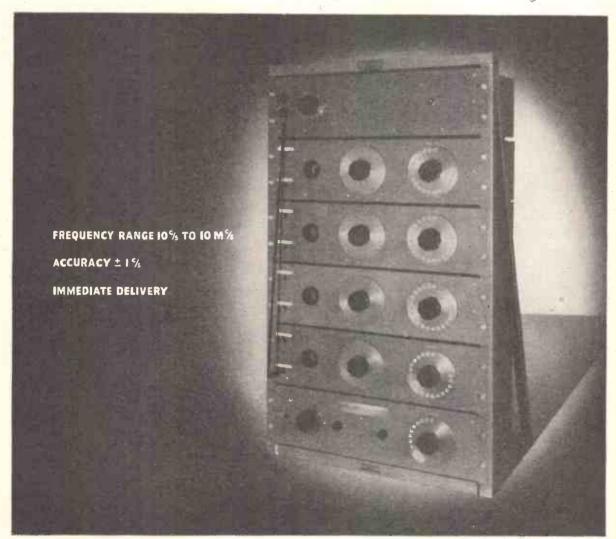
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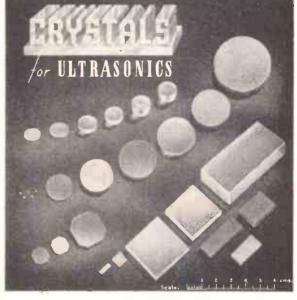
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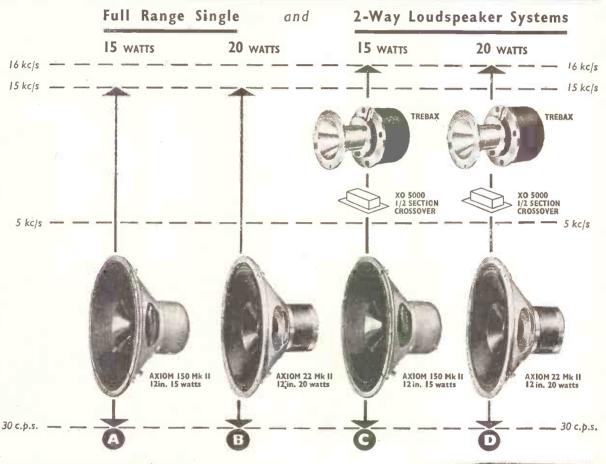


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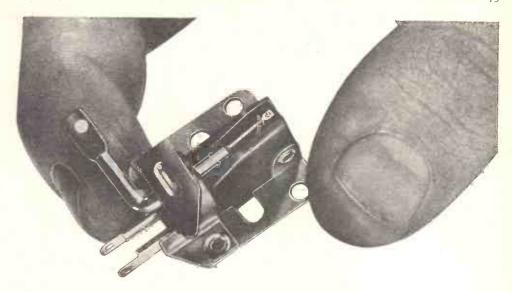
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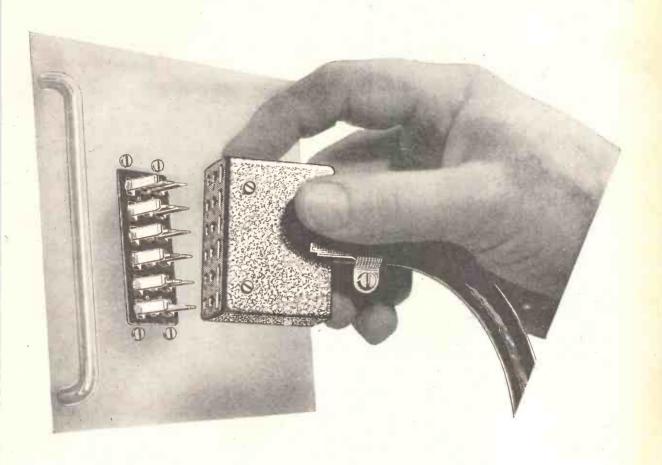
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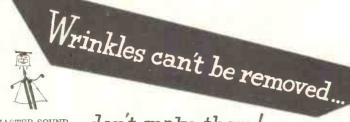
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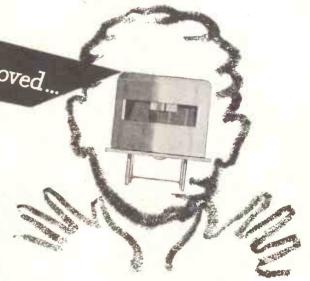


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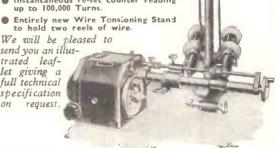
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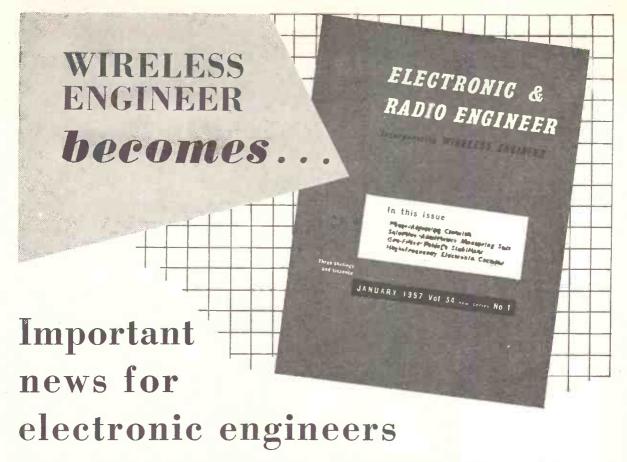
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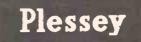
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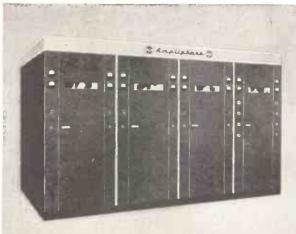
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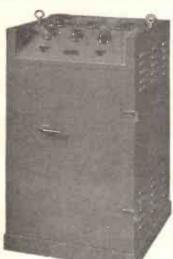
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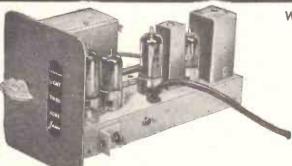
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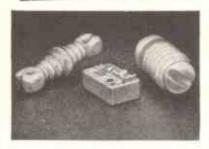
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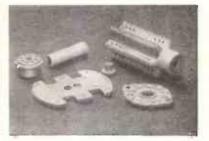
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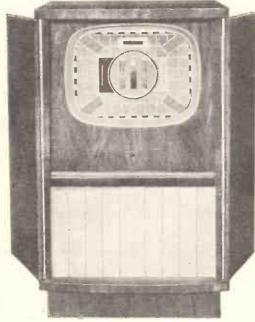
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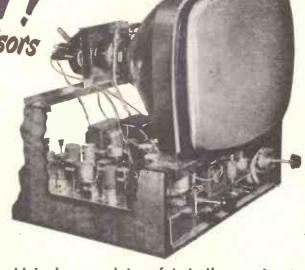
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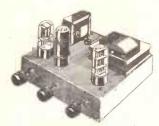
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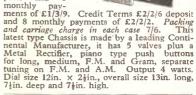
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All primaries are tapped for 200-230-250 v. mains 40-10 cycles. All primaries are screened, SP175B, 175-0-175, 50 mA., 4 v. @ 1 a., 4 v. @ 2-3 a. SP350A, 350-0-350, 100 mA., 5 v. @ 2-3 a., 6.3 v. SP350A, 530-0-350, 100 mA, 4 v. @ 2-3 a., 4 v. @ 3-3 a., 4 v. @ 3-3 a., 4 v. @ 3-5 a., 5 v. @ 2-3 a. 6.3 v. @ 2-5 a. 6.3 v. @ 3-5 a., 5 v. @ 2-5 a. 6.3 v. @ 3-5 a., 5 v. @ 2-5 a. 6.3 v. @ 3-5 a. 7 v. @ 2-5 a. 6.3 v. @ 3-5 a. 7 v. @ 2-5 a. 6.3 v. @ 3-5 a. 7 v. @ 2-5 a. 6.3 v. @ 3-5 a. 7 v. @ 2-5 a. 6.3 v. @ 3-5 a. 7 v. @ 2-5 a. 6.3 v. @ 3-5 a. 7 v. @ 2-5 a. 6.3 v. @ 3-5 a. 7 v. @ 2-5 a. 6.3 v. @ 3-5 a. 7 v. @ 2-5 a. 6.3 v. @ 3-5 a. 7 v. @ 2-5 a. 30/-52/6 22/6

PUSH-PULL OUTPUT TRANSFORMERS, 2×6V6 into

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mplete, ready to connect to any ype of Pick up and Speaker (3 ohms) A.C. Mains 200/250 volts. Volume and tone control fitted with knobs. Overall size 7\fin. long × 3\fin. wide × 2\fin. high. 62.19.6

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THE LATEST TYPE 17" RECTANGULAR TUBE MW43/64 BY TELEFUNKEN AT 217 (INC. TAX) POST AND
PACKING 21/- EXTRA.

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Type LSH100		Price 21/-
Type LSH518		Price 17/6

LATEST B.S.R. MONARCH 4-SPEED AUTOCHANGER

Designed to play 12in., 10in. and 7in. Records inter mixed in any order at 16, 33\(\frac{1}{2}\), 45 or 78 r.p.m. Capacity 78 r.p.m. Car 10 Records. 10 Records. New reversible Dual Stylus Crystal Plck-up, for use on 100/250 v. 50 cycle A.C. mains, £9/15/-plus packing and postage 5/-. Deposit 25/- a 8 monthly payments of 25/-.



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manuacturer with crystal turnover head, for use on 100-250 v. 50 cycle A.C. mains. £6/19/6. Plus pkg, and carr. 5/-.

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Plus 5/- packing and carriage. TUNING CONDENSERS (SMALL TYPE) 2-gang .0005 mfd, with trimmers, 5/-

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ITEM PLAN			DEPOSIT		MONTHLY PAYMENTS			DEPOSIT		MONTHLY					
Premier Bureau Cabinet Premier Bureau de Luxe Cabinet Rogers Amplifier and Pre-amp. Mullard EA.R/8/10 Mullard EA.R/8/10F Leak TL10 Garrard Transcription Type 301 less F/U Garrard Transcription Type TA/AO Unit	£ s. 12 12 17 6 26 0 18 18 24 3 28 7 26 8 11 6	d. 0 6 0 0 0 0 3	£ 1 2 3 2 3 3 1	12 3 4 7 0	d. 0 4 6 3 6 0 7	(8) (8) (8) (8) (8) (8) (8) (8) (9)	2 3 2 2 3 3	12 2 1 4 6 19 9 5	d. 60065908	13 9 12 14 13	6 13 1 9 2 3	d. 0 0 3 3 0 0 7	£ (8) (12) (12) 1 (8) 1 (12) 1 (12) 1 (12) 1 (6) 1	8 2 6 4	a. 3 1 0 3 4 4
Garrard Transcription Type TA/AC/DC Unit Garrard Changer Type RC80M AC/DC Garrard Changer Type RC98H AC Leneo-Transcription Unit Model F50-2 complete with P/U Goodmans Axiom 102 Speaker Goodmans Axiom 150 MK. 1 Goodmans Axiom 22 MK. 2	19 10 26 3 19 17 21 16 10 7 10 15 15 9	5 7 2 9	1	9 5 9 14 5 7	2 5 1 6 0 1	(8) (8) (8) (8) (8) (8)	2 2 1 1	10 9 13 6 7	0 1 0 3 6 4 8	13 9 10 5 5		9 4 8 9	(10) 1 (12) 1 (9) 1 (12) 1 (6) 1 (6) 1 (8) 1	4 4 0 0 1	2 8 4

207 EDGWARE RD., LONDON, W.2. Tel: AMBassador 4033 and PADd ington 3271

Tel: AMBassador 4033

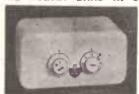
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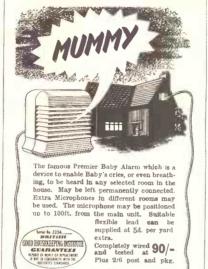
THE WOLSEY BAND III CONVERTER



This Converter has been designated to receive alternative programmes on Band 3 Channels 6 to 13, selection of Channel being made by rotation of Switch Knob. Mains supply 200/255 v. A.C. only. The high

only. The high gain of this Converter (minimum 20dB) together with low gain of this Converter (minimum 206B) together with low noise factor ensures rood picture quality. A variable gain control makes it possible to balance a Band 1 and Band 3 signal inputs to the receiver. Any single channel Receiver of either T.R.F. or Superhet design may be fed from the Converter. Separate input sockets are provided for Band 1 and Band 3 inputs. Cash price £9/19/6. Credit Terms deposit £1/5/6 and 8 monthly payments of £1/5/6. IMPOBTANT, please state your Band 1 station. Packing and Postage 3/e extra.

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JUNCTION TRANSISTORS 10/- EACH



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A NEW SPEAKER **ENCLOSURE**

A really elegant cabinet in well figured walnut veneer. Suitable for housing Goodmans Audiom and Axiom speakers.



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GOODMANS ACQUISTICAL UNIT. Type 172ARU #2/15/4

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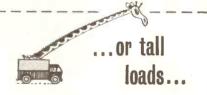
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At the B.S.R. works, teams of highlytrained inspectors eliminate after-sale problems before sale. At every manufacturing stage each single component must pass their exacting tests; then, after assembly, pass even more stringent tests.

Thus, many manufacturers report that not only is the Monarch free of after-sale worries, but it has also minimised their own inspection problems.

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Manarch UA8

Worlds finest four Speed Autochanger



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Wireless World

ELECTRONICS, RADIO, TELEVISION

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JANUARY 1957

In This Issue

- 1 Editorial Comment
- 2 Single Beam Colour Tube
- 4 World of Wireless
- 8 Limiters and Discriminators for F.M. Receivers. G. G. Johnstone
- 15 Portable Transistor Superhet. W. Woods-Hill
- 18 Resistance-Current-Voltage-Power Nomogram. B. E. Jackson
- 20 Is Radio Propagation Always Two-way? T. W. Bennington
- 22 Books Received
- 23 The Gated-Beam Valve. Lawrence W. Johnson

VOLUME 63 No. 1

27 Modernizing T.R.F. Television Receivers. P. F. Cundy

PRICE: TWO SHILLINGS

- 28 Short-wave Conditions
- FORTY-SIXTH YEAR
 - OF PUBLICATION
- 29 Letters to the Editor
- 31 High-Quality Sound Broadcasting. G. H. Russell
- - 33 Cascode Characteristics. W. Grant
- *** * * * ***
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- 40 Technical Notebook

36 Fish-Finding Asdic

- 42 Negative Resistance. "Cathode Ray"
- 47 January Meetings
- 48 Random Radiations. "Diallist"
- 50 Unbiased. "Free Grid"

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200mW Transistor



amplifier operated from a 6V supply

In a previous advertisement (June 1956) details were given of an audio amplifier using transistors, which derived its power from a nominal 4.5 volt battery. In portable equipment such as record reproducers, it is convenient to operate the amplifier from the same supply as the turntable motor, and since most portable motors operate from a 6 volt battery, the 200mW amplifier circuit has been adapted for use with this higher voltage.

The 4.5 volt and 6 volt versions are very similar in performance, except for the greater sensitivity of the latter. Both

are capable of an output of just over 200mW with 10% total harmonic distortion. In the 6V amplifier, the gain at 8kc/s and 50c/s falls 3dB below level response at 1kc/s

The sensitivity of the 6V version is slightly higher than that of the original in spite of a higher series input resistance of $330k\Omega$. This can be attributed to the higher supply voltage. Since the output stage requires a lower driving current, and a higher voltage is available for the driver. a higher turns ratio can be used for the interstage transformer T1 and thus the stage to stage gain can be increased. The

basic sensitivity across the low impedance terminals YY is 3mV, compared with 6mV in the original, and across the high impedance terminals XX it is 400mV compared with 500mV.

The circuit and component values given in the accompanying diagram. Alternative high or low impedance inputs for crystal pickups or radio tuner are available at XX and YY respectively. The input and driver stages (each using an OC71) are R-C coupled, and the driver stage is transformercoupled to the output stage which is a Class B push-pull arrangement of two OC72's

(sold in matched pairs as Mullard type 2-OC72).

Interstage Transformer

The turns ratio of the interstage transformer, T1, which is rated at 2mW, is 3.5:1+1. The inductance of the primary should be 10H with a current of 15.mA d.c. flowing, and its d.c. resistance should be less than 200Ω . The resistance of each half of the secondary should be kept below 50Ω and the leakage inductance should be as low as possible. The d.c. currents in the secondary windings are balanced.

Output Transformer

The output stage is matched to the load by a push-pull transformer, T2, rated at 250mW. For a 30 load the turns ratio is 4.9+4.9:1, for a 5Ω load, 3.8+3.8:1, and for a 15Ω load, 2.2+2.2:1. Each half primary should be capable of handling peak currents of 83mA.

The currents in each half of the primary will only be balanced if the transistors in the output stage are perfectly matched. At large-signal currents it is possible for the OC72's to be mismatched by as much as 35%, consequently the output transformer should be constructed to allow for unbalanced currents.

The d.c. resistance of each half of the primary winding of T2 should be less than 3Ω and the total inductance should be greater than 0.5H.

The dynamic load for each collector of the push-pull stage should be 72Ω . The d.c. resistance of the secondary winding should be less than 5% of the load resistance and the leakage inductance should be low.

The turns ratio of the output transformer, and the value of

the feedback resistor R13 for various loudspeaker impedances are shown in the top left hand corner of the diagram. The loudspeaker impedance must be quoted when the output transformer is ordered from the manufacturer.

Stabilisation

Potential dividers R3, R4 and R7, R8 and emitter resistors R6 and R9 provide stabilised d.c. bias for the input and driver stages

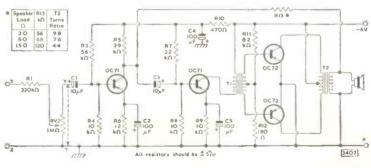
The effects of changes in the temperature of the surroundings, production spreads in the transistors, and deterioration of the

supply battery on the performance have been minimised by careful choice of the value of R11. The optimum value is $8.2k\Omega$, giving satisfactory performance under the conditions

likely to be encountered. Slightly lower distortion can be obtained by presetting the value of R11 to give quiescent curents of 0.5mA for each transistor at 20°C. The amplifier can be used safely in ambient temperatures as high as 45°C.

Negative feedback from the secondary of the output transformer is applied to the collector of the first OC71 by R13,

whose value must be chosen to match the loudspeaker load, as shown in the table.



MULLARD COMPONENTS

Mullard pot cores and other Ferrox-

cube components, air-space trimmers,

Varite thermistors etc. are now avail-

able in small quantities for experi-

menters. For information regarding

the nearest source of supply please

enquire of Mullard Valve Sales Dept.

at the address below.

Filter Components

An increase in battery impedance causes undesired feedback through the supply to the earlier stages and it results in considerable distortion in the output. This unwanted feedback is prevented by the filter network C4-R10.

Performance

Output Power

215mW at 10% total harmonic distortion

Frequency Response

Gain, at 50c/s and 8kc/s, is reduced 3dB below the response level at 1kc/s

Sensitivity (with nominal transistors)

3.0mV at the low impedance terminals YY

400mV at the high impedance terminals XX

Current Drain

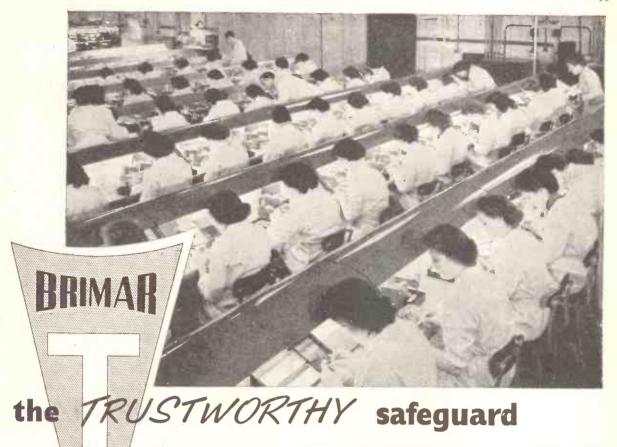
5 to 6mA at zero signal

15mA with average music

75mA at maximum output with sine wave drive



T.S.D. DATA and PUBLICATIONS SECTION, MULLARD LTD., MULLARD HOUSE, TORRINGTON PLACE, LONDON, W.C.1



Communications and Industry

The special Trustworthy high quality valves have been designed to give maximum efficiency with reliability—most valuable in equipment required to operate for lengthy periods unattended. Primarily established to meet Service requirements, the Trustworthy techniques, including shock and vibration tests, have been extended to include many commercial types. The accompanying table shows the range of industrial "T" valves. These can also be supplied with flying lead, or flying lead valve assemblies for chassis mounting, the information on which can be obtained on application.

Most types are available within a reasonable period. In many instances additional types can be made available for special applications.

INDUSTRIAL T RANGE

Code	Equivalent Commercial Type Code	Function	Base
5726	6AL5	Double Diode Short Bulb	B7G
6058	6AL5	Double Diode	B7G
6516	6AM5	Power Pentode	B7G
6064	6AM6/8D3	High Slope R.F. Pentode	B7G
6066	6AT6	Double Diode Triode	B7G
5749	6BA6	Vari Mu R.F. Pentode	B7G
5750	6BE6	Heptode Mixer	B7G
6059	6BR7	Low Noise A.F. Pentode	B9A
6061	6BW6	Output Beam Tetrode	B9A
6132	6CH6	Video Output Pentode	B9A
6100	6C4	Triode Amplifier	B7G
6180	6SN7GT	Low Mu Double Triode	Octal
6063	6X4	Full Wave Rectifier	B7G
6065	9D6	Vari Mu R.F. Pentode	B7G
6060	12AT7	High Slope Double Triode	B9A
6067	12AU7	Low Mu Double Triode	B9A
6057	I2AX7	High Mu Double Triode	B9A
6158	13D3	Special Purpose Double Triode	B9A
6062	5763	V.H.F. Beam Tetrode	B9A
6157	R17	Half Wave Rectifier	B9A
6443	R18	Half Wave Rectifier	B9A
6LGA	6L6GA	Output Beam Tetrode	Octal
25L6GT	25L6GT	Output Beam Tetrode	Octal
6042	25\$N7GT	Low Mu Double Triode	Octal
50C5	50C5	Output Beam Tetrode	B7G



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Regd. Office: Connaught House, 63, Aldwych, London W.C.2

FOOTSCRAY

SIDCUP

KENT + FOOtscray 3333



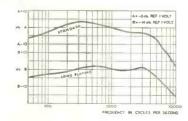
In a previous announcement we showed how ACOS GP61 Ceramic Pick-up Cartridges had passed the official BSI Test No. BF.2011, Class 112, "Basic Climatic and Durability Test for components for radio and allied equipment". Now our own laboratories have gone even further with climatic tests—and added a punishing mechanical test too. These new tests, which covered a batch of GP61s, gave average results as follows:—

RESPONSE SHAPE

16 hours at Minus 10°C (14°F) in water No change No change No change Vertical drop from 2in. 10,000 times (at 50 times per minute) No change No change

Manufacturers who fit the GP61 Ceramic know where they are. It is, demonstrably, a most robust cartridge for all climatic conditions.

It has a smooth response, low harmonic and intermodulation distortion, high needle tip compliance replaceable "X500" styli and very good output.



The ACOS GP61 CERAMIC pick-up cartridge fitted with 'X500' styli is the high performance cartridge for manufacturers with world markets.



ACOS devices are protected by patents, patent applications and registered designs in Great Britain and abroad.

"BELLING LEE" NOTES

Why do "Belling-Lee" T.V. aerials stand up straighter longer than most? Because after they leave the laboratory with the desired electrical characteristics, mechanical engineers set to and build them so that they will withstand the extreme rigour of our climate, and so that the factory is able to make them at a fair price. We do not expect a physicist specialising on aerial designs to be as good at mechanical designs as an engineer who specialises in that work.

Pre-production samples are tested by the laboratory and by a field research team and not until the results compare favourably with the original laboratory model

do we go ahead.

But what a lot of "know-how" is employed at every stage; windage, weight (plus ice and snow) and resistance to corrosion. How many users know that dangerous corrosion is retarded by the use of identical metals, and where dissimilar metals have to be used; in the choice of those with a low potential difference?

"Belling-Lee" try to avoid the use of steel parts, and where they must be used they are suitably treated. It is common knowledge that the component parts of an aerial lock together after a few weeks in the open. The white powdery coating that forms is generally aluminium carbonate or aluminium oxide and is in itself generally harmless. It only takes a minute to rub some grease on to mating parts to ensure easy dis-

mantling at any time.

"Belling-Lee" do aim to strike a happy balance between electrical and mechanical performance, and that is why some of our aerials cost a few shillings more, but what is so galling is to know that production is sometimes held back to achieve one or two dBs improvement, and that only an infinite percentage is installed with the knowledge and care to take advantage of this extra efficiency. For example, neighbours in identical houses using identical aerials and receivers can easily get widely different results because one of them is receiving an out-of-phase reflected signal, giving a weak picture. Even moving the aerial a few feet might help. This is another example of "probing the roof" for optimum results.

Advertisement of BELLING & LEE LTD.
Great Cambridge Rd., Enfield, Middx.
Written 19th Nov. 1956

BELLING - LE T.V. INTERFERENCE FILTERS

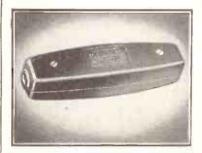
FLEX LEAD FILTERS

L. 13 4 For 2-core cables 2 amp. 250 v.

L. 1316 Complete with 6ft. 2-core cable 2 amp.

This small flex lead filter (L.1314) is designed for the suppression of interference at television frequencies only, and for insertion in the flex lead within 6in. of the offending component of an appliance. The most convenient form of filter which can be readily serviced, it is complete with terminals and cord grips, etc. Three-core cables may be fitted, by-passing the earth

The type moulded into a 6ft. 6in. length of cable (L.1316) is intended for use by electrical appliance manufacturers as an integral part of the appara-tus, although it may be used to replace an existing cable. These flex lead filters may be used in conjunction with the plug L.1308 which has a built-in filter efficient on the medium and long wave-

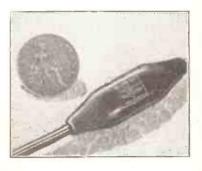


L. 1308 5 amp 3-pole Mains suppressor plug 200-250 v. a.c./d.c.

Where an appliance is suspected of or known to be creating electrical interference on the long and medium wavebands, the interference can usually be filtered or reduced by the insertion of this mains plug. This is designed for fitting to the free end of the flex lead, replacing the normal type of 5 amp 3-pole plug generally used.

Appliances likely to cause mainsconducted interference are hair dryers, refrigerators, washing machines, food mixers, fans, small motors, small drills, grinders, lathes, etc., actuated by commutator motors.

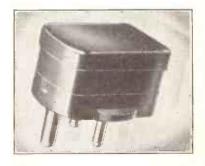




L.799 (2- or 3-core) 2 amp. Inductor and capacitor filter 250 v. a.c./d.c.

Effective at band I television frequencies and short and medium wavebands.

This is designed for connection in the lead of domestic electrical equipment such as hair dryers, vacuum cleaners, sewing machine motors, electric fans, etc., and to be truly effective must be fitted within 6in. of the connections of the motor in the appliance.

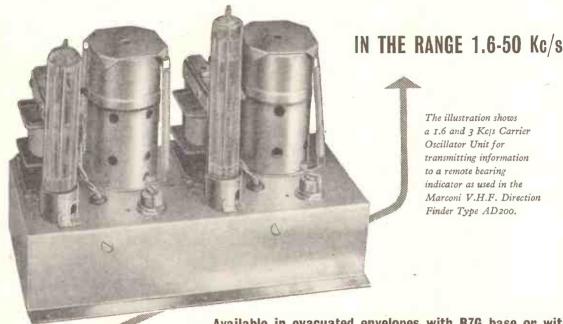




GREAT CAMBRIDGE ROAD, ENFIELD, MIDDX:, ENGLAND

Telephone: Enfield 3322 · Telegrams: Radiobel, Enfield

MARCONI LOW FREQUENCY CRYSTALS



The illustration shows a 1.6 and 3 Kc/s Carrier Oscillator Unit for transmitting information to a remote bearing indicator as used in the Marconi V.H.F. Direction Finder Type AD200.

Available in evacuated envelopes with B7G base or with flexible leads for connection into the circuit

Among the many uses for this type of crystal are the following:

> SPEECH INVERSION **OSCILLATORS**

CARRIER CHANNELLING **EQUIPMENT**

RANGE CALIBRATORS

TIMING APPLICATIONS ETC.

Flexure mode crystals are suitable for a wide variety of applications where an oscillator of good stability and small size is essential. They cover the frequency range 1.6 to 50 Kc/s with a point of zero temperature coefficient in the range o°-40°C. The bar in XY flexure used between 1.6 and 12.0 Kc/s has the great advantage of a low temperature coefficient in the region of room temperature.



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MARCONI'S WIRELESS TELEGRAPH COMPANY LIMITED CHELMSFORD, ESSEX. Telephone: CHELMSFORD



STROBOSCOPES For all applications

HIGH POWER STROBOSCOPES for the measurement of speed and observation of rotary and reciprocating mechanisms.

GENERAL PURPOSE TYPE 4

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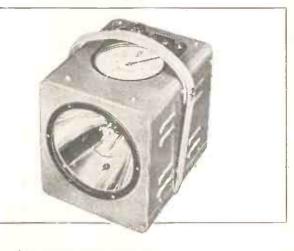
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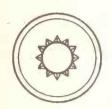


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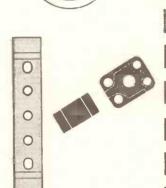
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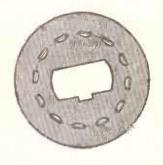




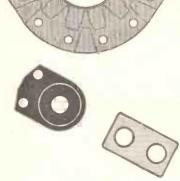
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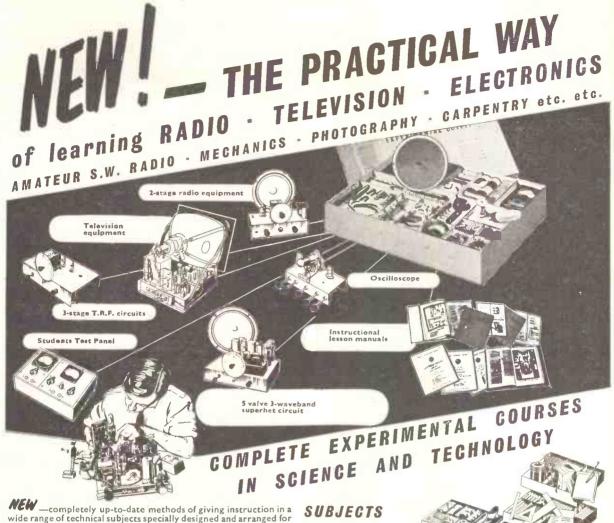




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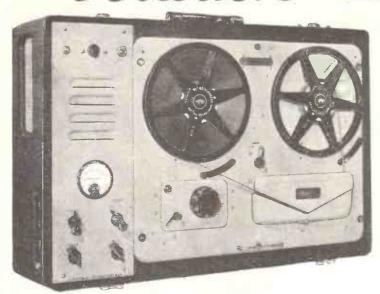
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The amplifier, speaker and case, with detachable IId, measures $8\frac{1}{4}$ in. x $22\frac{1}{2}$ in. x $15\frac{3}{4}$ in. and weighs 30 lb.

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★ A lower bias lifts the treble response and increases distortion. A high bias attenuates the treble and reduces distortion. The normal setting is Inscribed for each instrument

★ The distortion of the recording amplifier under recording conditions is too low to be accurately measured and is negligible.

★ A heavy mu-metal shielded microphone transformer is built in for 15-30 ohms balanced and screened line, and requires only 7 micro-volts approximately to fully load. This is equivalent to 20ft. from a ribbon microphone and the cable may be extended 440 yds. without appreciable loss. ★ The .5 megohm input is fully loaded by 18 millivolts and is suitable for crystal P.U.s, microphone or radio inputs.

A power plug is provided for a radio feeder unit, etc. Variable bass and treble controls are fitted for control of

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The power output is 3.5 watts heavily damped by negative feedback and an oval internal speaker is built in for monitoring purposes.

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One milliwatt output on 600 ohm line (,775V) for an input of 30 micro-volts on 7.5-30 ohm balanced input.

Output balanced or unbalanced by internal switch. The meter reading is obtained by a valve voltmeter with I second time constant, which reads programme level, and responds to transient packs.

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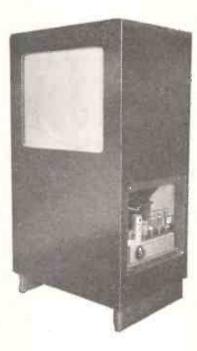
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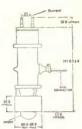
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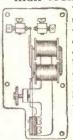
rotate a heavy scanner, reflector, beam array, etc., etc.

Item 2, known as Indicator 1-221-A is the remote controller which enables the azimuth position of Tower 24A to be controlled from a remote point. Conversely, it enables the cator contain selsyn transmitter/receivers and it is these that provide the impulses which cause the aerial to rotate backwards or forwards. The equipment intended for 117 voit A.C. mains but will operate from our mains it connected through step down transformer of 1 K.W. rating.

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Special discount of £5 for cash with order or C.O.D. If both units purchased together.

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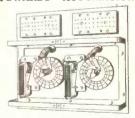
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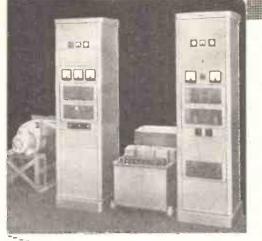
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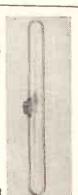
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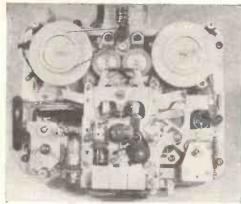
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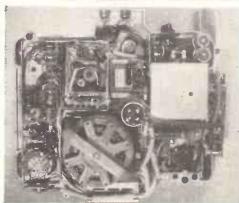
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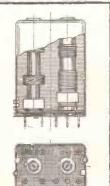
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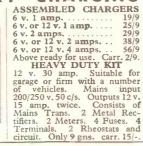
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8 mfd. 450 v	1/9	16 mfd. 350 v.	1/11
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16μF 350 v	2/3	16 mfd. 500 v.	3/9
16μF 450 v	2/9	32μF 350 v	2/11
16μF 500 v	3/9	32 mfd. 450 v.	4/9
8-16μF 500 v.	4/11	100 mfd, 450 v.	2/9
		8-8μF 450 v	
25μF 25 v	1/3	8-16μF 450 v.	2/11
50μF 12 v	1/3	16-16μF 450 v.	3/11
50 mfd. 25 v	1/9	$32-32\mu F 350 \text{ v}.$	4/9
50μF 50 v	1/9	$32-32\mu F 450 \text{ v}.$	5/9
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100 mfd. 12 v.	1/9	V	7/6
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6,000 mfd. 6 v.	3/11	275 v	6/11
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design of 3 valve 200-250 v. A.C. Mains selenium rectifier. For inclu-

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300-0-300 v. 150 mA., 4 v. 3 a	9/9
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Potted 41-31-3in	11/9
460 v. 200 mA., 6.3 v. 5 a.	22/9

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Fully shrouded upright. Primary 200-230-250 v. Sec. 425-0-425 v. 150 mA. 6.3 v. 3 a., 5 v. 3 a., 33/9. Clamped type 325-0-325 v. 100 mA., 6.3 v. 3.5 a., 5 v. 2 a. Wearite 19/9. 230-0-230 v. 60 mA., 6.3 v. 2.5 a. Midget, 2½ x 3 x ½jin. approx., 11/9. Post 2/9 on any of above.

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250-0-250 v. 100 mA., 6.3 v4 v. 4 a., c.t.,	0-
0-4-5 v. 3 a	25
250-0-250 v. 100 mA., 6.3 v. 4 a., 5 v. 3 a.	23
250-0-250 v. 100 mA., 6.3 v. 6 a., 5 v. 3 a.,	
for R1355 conversion	31
300-0-300 v. 100 mA., 6.3 v. 4 a., 5 v. 3 a.	23
300-0-300 v. 100 mA., 6.3 v. 4 v. 4 a., c.t.,	
0-4-5 v. 3 a	26
350-0-350 v. 100 mA., 6.3 v. 4 a., 5 v. 3 a.	23
300-0-300 v. 130 mA., 6.3 v. 4 a., c.t., 6.3 v.	
1 a., suitable for Mullard 510 Amplifier	33
350-0-350 v. 100 mA., 6.3 v4 v., 4 a., c.t.,	
0-4-5 v. 3 a	26
350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.	33
350-0-350 v. 150 mA., 6.3 v. 2 a., 6.3 v.	
2 a., 5 v. 3 a	33
425 0 425 v. 200 m. 4 6 2 v. 4 c. c.	33
425-0-425 v. 200 mA., 6.3 v. 4 a., c.t.,	

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260-0-260 v. 70 mA., 6.3 v. 2 a., 5 v. 2 a.
350-0-350 v. 80 mA., 6.3 v. 2 a., 5 v. 2 a.
250-0-250 v. 100 mA., 6.3 v. 4 a., 5 v. 3 a.
300-0-300 v. 100 mA., 6.3 v4 v. 4 a.,
c.t., 0-4-5 v. 3 a
350-0-350 v. 100 mA.,6.3 v. 4a., c.t.,5v. 3a.
350-0-350 v. 100 mA., 6.3 v4 v. 4 a.
c.t., 0-4-5 v. 3 a
350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.
E.H.T. TRANSFORMERS, 2,500 v.
5 mA., 2-0-2 v. 1.1 a., 2-0-2 v. 1.1 a.,
for VCR97, VCR517

6.3 v. 6 a. . . . 12 v. 3 a. or 24 v. 1.5 a. . . 17/6 17/6

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All with 200-230-250 v. 50 c/s. Primaries:
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0-9-15 v. 6 a., 23/9. 25/9 31/-23/9 23/9 9/11 33/9

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Midget Battery Pentode 66:1 for 3S4, etc.
Small Pentode 5,000Ω to 3Ω
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Multi-ratio 40 mA. 30:1, 45:1, 60:1,
90:1, Class B Push-Pull
Push-Pull 18 Watts 6V6 to 5 ohms
Push-Pull 10-12 Watts 6V6 to 3Ω or 15Ω
Push-Pull 10-12 Watts to match 6V6 to
3-5-8 or 15Ω
Push-Pull 15-18 Watts, sectionally wound,
6L6, KT66, etc., to 3 or 15 ohms
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A6 ULTRA LINEAR R.S.C. 30 WATT **AMPLIFIER**

NEW 1956 DESIGN. HIGH FIDELITY PUSH-PULL UNIT EMPLOYING SIX VALVES. Tone Control Pre-amp stages are incorporated. Sensitivity is extremely high. Only 30 millivolts minimum input is requirefor full output. THIS ENSURES THE SUITABILITY OF ANY TYPE OR MAKE OF MICROPHONE OR PICK-UP. Separate Bass and Treble controls give both "lift" and "cut" with ample tone correction for long playing records. AN OUTPUT SOCKET WITH PLUG IS INCLUDED FOR SUPPLY OF 300 v. 20 mA. and 6.3 v. 1.5 a. FOR A RADIO FEEDER UNIT. Price in kit form with easy-to-follow wiring diagrams. ORNS. incorporated Sensitivity is extremely high.



Type 807 output valves are used with High Quality Sectionally wound output transformer specially designed for Ultra Linear operation. Negative feedback of 17 D.B. in main loop. CERTIFIED PERFORMANCE FIGURES ARE EQUAL TO MOST EXPENSIVE UNITS AVAILABLE. Frequency response ± 3 D.B., 30-20,000 c/cs., 12 D.B. "lift" at 50 c/cs., 30-20,000 c/cs., 12 D.B. "lift" at 12,000 c/cs., Hum and noise 70 D.B. down. Good quality reliable components used. Chassis finish blue crackle. Overall size 12 × 9 × 9in. approx. Power consumption 150 watts. For A.C. mains 200-230-250 v. 50 c/cs. Outputs for 3 and 15 ohm speakers. EQUALLY SUITABLE FOR THE CONNOISSEUR OR FOR LARGE HALLS, CLUBS, or OUTSIDE FUNCTIONS. IDEAL FOR USE WITH MUSICAL INSTRUMENTS SUCH AS STRING BASS, ELECTRONIC ORGAN, GUITAR, etc. FOR DANCE

12-WATT AMPLIFIER

NEW 1956 MODEL AS HIGH-FIDELITY PUSH-PULL AMPLIFIER WITH "BUILT-IN" TONE CONTROL, PRE-AMP. STAGES

GONTROL, PRE-AMP. STAGES

High sensitivity. Includes 5 valves (807 outputs), High Quality sectionally wound output transformer, specially designed for Ultra Linear operation, and reliable small condensers of current manufacture. INDIVIDUAL CONTROLS FOR BASS AND TREBLE "Lift" and "Cut" Frequency response ± 3ds. 30-30,000 e/cs. Six negative feedback loops. Hum level 71 db. down. ONLY 70 millivoits INPUT required for FULL OUTPUT. Suitable for use with all makes and types of pick-ups and practically all micronhones Comparable with the very best designs. For STANDARD or LONG PLAYING RECORDS. For MUSICAL INSTRUMENTS such as STRING BASS. GUITARS, etc. OUTPUT SOCKET with plug provides 300 v 20 mA. and 6.3 v 1.5 a. For supply of a RADIO FEEDER UNIT. Size approx. 12-9-7in. For A.C. mains 200-230-250 v. 50 e/cs. Output for 3 and 15 ohm speakers. Kit is complete to last mit. Chassis is fully punched. Full instructions and point-to-point Wiring diagrams supplied.

Unapproachable value at £7/15/- or factory built



R.S.C. TA1 HIGH QUALITY TAPE DECK AMPLIFIER
FOR ALL DECKS WITH HIGH IMPEDANDE RECORD/PLAYBACK AND
ERASE HEADS. Such as Lane, Truvox, etc., or matched to low impedance
crase heads as fitted latest COLLARO TAPE TRANSCRIPTOR. Chassis
size 127-751n. Overall size 127-764in. For 230-250 v. 50 e/cs. A.C. mains.
Output for standard 2-3 ohm speaker. Only 15 millivoits input required for
full recording. Only 2 millivoits minimum innut required from recording head.
Magic Eve recording level indicator. Provision for feeding P.A. amplifier.
Can be used as gram. amplifier with input of 0.75 v. R.M.S. Negative feedback equalisation. Linear frequency response ± 3 D.B. 50-11,000 c/ce.
Facilities for recordings at 15in., 71in. or 38in.
Facilities for recordings at 15in., 71in. or 38in.
of a knob. When switching from record to
playback position automatic demagnetisation of
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PERFORMANCE IS COMPARABLE WITH UNITS

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H.M.V. LONG PLAYING RECORD TURNTABLE COM-PLETE WITH GRYSTAL PICK-UP (SAPPHIRE STYLUS), Speed 33† r.p.m. BRAND NEW. CARTONED. Only £3/19/6 (approx. balf price). Carr. 5/- (for 200-250 v.

R.S.C. 4-5 WATT HIGH GAIN AMPLIFIER TYPE A5

highly sensitive 4-alve quality amplifier or the home, small valve quality ampliner for the home, small club, etc. Only 50 milli-volts input is required for full output so that it is suitable for use with the latest high-fidelity pick-up heads in addi-tion to all other types of



tion to all other types of plot-ups and practically all mikes. Separate Bass and Treble controls are provided These give full long playing record equalisation. Hum level is negligible, being 71 D.B. down, 15 D.B. of negative feedback is used. H.T. of 300 v. 26 mA. and L.T. of 6.3 v. 1.6 a. is available for the supply of a Raddo Feeder Unit or Tape Deck pre-amplifier. For A.C. mains input of 200-230-250 v. 50 c/s. Output for 2-3 oths speaker. Chassis is not alive. Kit is complete in every detail and includes fully punched chassis (with baseplate) with the blue hammer tinsh, and point-point wiring diagrams and instructions. Exceptional value at only 24/15/c, or assembled ready for use 25/extra, plus 3/6 carriage.

R.S.C. A7 3-4 WATT QUALITY AMPLIFIER

R.S.C. A7 3-4 WATT QUALITY AMPLIFIER
A bighly sensitive 4-valve amplifier using negative feedback
and having an excellent frequency response. Fre-amplifier
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Bass and Treble controls giving full tone compensation for
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output. Fully isolated chassles with baseplate For AC.
Complete kit of parts with point-to-point wiring diagrams
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22/6 extra.

D. M. Sneekers nearwareand of Science and S

P.M. Speakers recommended for use with above amplifiers.
Plessey 10in. 3 ohm with high flux density magnet. Only 28/9.

P.M. SPEAKERS. 2-3 ohm, 5in. Goodmans, 17/9, 7 × 4in. Elliptical, 19/6, 64in. R.A., 15/9, 8in. Rola 19/9, 10in. R.A., 26/9, 12in. Plessey, 29/11. 12in. Plessey 15 ohms. 10 watte 3 gns.

GARRARD 3-SPEED AUTOMATIC RECORD CHANGERS.

Latest Model Mixer Type RC110. Fitted high fidelity turnover crystal pick-up head with dual point sapphire stylus. Baseboard size 14 x 12 lin. height above, 4in, Below, 21in. For 200-250 v. A.C. Brand new cartoned. Limited number. Only £7/19/6, plus 3/6 carriage.

LINEAR MINIATURE 4/5 WATT QUALITY AMPLIFIER. Suitable for use with Garrard B.S.R. or any other record playing unit, and most microphones. Total negative feedback 18 db. Separate Bass and Treble Controls. For convenience when mounted in cabinet, mains switch is incorporated in control. For A.C. mains input of 200-250 v. 50 c.p.s. Output for 2/3 ohm speaker. Three miniature Mullard valves used. Size of unit only 6 x5 x5 gin. high. Chassis is fully isolated from mains. Guaranteed 12 months. Only £5/19/6.

MICROPHONES. High fidelity crystal types. Acos 33-1 hand or desk type, 50/-. Plezzo with heavy floor base and telescopic stem, £6/19/6:

ROTARY CONVERTERS. 200 watts. Input 12 v. D.C. Output 230 v. 50 c/cs. A.C. Only 7 gns. Carr. 7/6.

PLESSEY DUAL CONCENTRIC 12 in. P.M. SPEAKERS



(15 ohms), consisting of a high quality 12in. speaker, of orthodox design supporting a small elliptical speaker ready wired with choke and condensers to act as tweeter. This high fidelity unit is highly recommended for use with our A8 or any similar amplifier. Rating is 10 watts. Price only

LINEAR "DIATONIO" 10-WATT HIGH FIDELITY AMPLIFIER. Incorporating pre-amp. For A.C. Mains input 200-230-250 v. 50 c.p.s. A compact attractively finished unit with two separately controlled inputs, and outputs for 3 and 15 ohm speakers. Separate Bass and Treble controls. Five latest type miniature Mullard valves. Only 12 Gns. Carr. paid. Send S.A.E. for leaflet.

W.B. "STENTORIAN" HIGH FIDELITY P.M. SPEAKERS. HF1012, 10 watts, 15 ohm (or 3 ohm) speech coil. Where a really good quality speaker at a low price is required, we highly recommend this unit with an amazing performance, £4/10/8. Please state whether 3 ohm or 15 ohm required.

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Design of a high quality Radio Tuner Unit (specially suitable for use with any of our Amphifiers). A Triode Heptode F/changer is used. Pentode I.F., and double Diode Second Detector. Delayed A.V.C. As./Orid F/C Coupling is by botton end Condenser Coupling giving freedom from alignment broubles when As. of varying lengths and capacity are used. Both Frequency Changers and I.F. valves are A.V.C. controlled from the very low distortion Double Diodes so arranged that very high Percentage modulation of the Transuitter can be handled without distortion. The Feed for the delayed A.V.C. is arranged so that A.V.C. distortion is avoided. The W. Ch. Sw. Incorporates Gram. position. Controls are Tuning W., Ch. and Vol. Output will load most Amphifiers requiring 500 M.V. Imput depending on Ae. location. Only 250 v. 15 m.A. H.T. and L.T. of 6.3 v. 1 amp. required from amplifier. Size of unit approx. 9-6-7in. high. Send S.A.E. for Illustrated leadet. Total building cost is 241.51/-. Point-to-point wiring diagrams and instructions. 2/6.

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Still available. Our very popular Gram
Chassis replacement Kit. For long,
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ACOS TYPE 7 Crystal Microphone Inserts. Brand New, 7/6 each, post



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Based on the booklet by Data Publications Ltd., 2/- post free, including our individually priced Parts List. Highly sensitive free from drift. Incorporates 4 vaives 64.M6 and 2 specially graded G.E.O. Crystals. The kit supplied includes drilled chassis with tuning condenser, scale calibrated in m/cs., and attractive bronze stovenamelled front plate already mounted (illustrated). From plate size 8in. × 5in. chassis 7in. × 4jin. × 1jin. Complete standard kit £6/15/- plus 2/6 P. & P. Fringe area kit £7/15/-, plus P. & P.

FM POWER PACK KIT. We can now supply complete kit for power pack suitable for the above F.M. tuner or any other similar type. Price for the complete kit is 37/6 only, or 52/6 for ready assembled unit. This pack is extremely small, incorporating valve rectifier type 6X4 and built on chassis size only 6×4×1/in. Optional extra for power pack. Bulgin Octal Plug 2/3.

THE T.S.L. FM TUNER!

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We can now supply this FM/YHF adaptor either in kit form or fully assembled, wired and tested. Our price for the ready-built unit, which incorporates its own power supply is £13/15/- only, tax paid, plus 5/P. & P. or H.P. terms. Magic tye tuning indicator, just plug in, 19/- extra. Or the kit complete as specified £10/19/6 plus 3/6 P. & P. The booklet "FM TUNER CONSTRUCTION" (32 pages) with full technical data and point-to-point wiring diagrams together with our separately priced parts list, is available at £/6 post free.



THE T.S.L. AM/FM CHASSIS !

Exceptional value. Covers L.M. and S.W. plus PMI 8-valve push-pull output. Ferriter od aerial. Valve line-up ECO85, ECR81, EF89, EABC80, ECC82, two 6BW6s plus 573 large full-vision dial, size 143 x 6in. Chassis size, overall: 15 x 73 x 8in. high. Tax paid, 25 guiness, plus 5/7 ascing and carriage. A supplementary extra is made eye EM34, complete with escutcheon and fixing cable at 26/-. H.P. terms available. Demonstrations at 18 Tottenham Court Road!

INTRODUCING THE NEW T.S.L. FM TUNER UNIT.

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This compact unit with built-in power supplies has been designed by craftsmen to standards which will satisfy the most critical enthusiast. Brief specifications: Valve line-up: ECC86.
2-EF89, EABC80, 6X4 and EM80. Overall size: 10 jun. W. No Jin. H. v5 jin. D. Dial size 10 jun. W. s Jin. Attractive phastic dial in Black and Gold with easy-to-read calibration. Controls switch. OFF FM & GRAM. and tuning. Pre-set gain control at rear of chasis. Connections: Convention stopped to study the socket. 300 of the arrangement of chasis. Connections: Convention stopped to study the socket. 300 of the set gain control at rear of chasis. Frice £17/10/p. plus 5/p. F. & T.

THE DULCI FM TUNER. Incorporates own power supply, suitable for use with any amplifier. Valve line-up. ECC85, two EF89, EABC80, 6X4 and EM80 indicator! Overall size: 9 × 6 × 5 in. high. Pre-Budget price £16/16/-, plus 5/- P. & P. Illustrated leaflet available, also H.P. terms.

THE R.E.F. 1-VALVE RECEIVER. All-dry battery operation, for use with headphone: The complete kit is available at 42/-, less batteries plus 2/- F. & F. or full instructions at 9d. post free.

COLL PACKS. Manufacturers' Surplus. Miniature size, only $2\frac{1}{2}$ in. $\times 2\frac{3}{2}$ in. $\times 1\frac{3}{2}$ in. deep Iron-cored. For L., M. and S.W. with gram. position. Switch has 2in. spindle. Absolutely brand new, complete with circuit. Frice only 27/6. plus 1/6 P. A. P. A. spindle.

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38.0 34.5 38.0 34.5 19.5 16.0 19.5 16.0 TT16S TT16P Series Parallel 10.5 14.0 10.5 14.0 Series Parallel The second series of the serie TT13P

JUST ARRIVED!

The "Imperial" AM/FM Radiogram Replacement Chassis. Overall measurements 13in. × 6in. × 7nn. high. Dial cut-out required only 10in. × 2jin. Covers long, medium and F.M. Features include very attractive black and gold dist and gold dial. 4-button, pu°h button unit. gram position. separate FM

separate FM tuning, con-tinuously variable tinuously variable-tone control, A.C. mains 110/230 v. Valve line-up EI-11, ECG85, EABC80, EF89, ECH81, plus metal recti-fier. Frice complete \$16/19/6 tax paid. H.F. terms available.

6v. VIBRATOR PACK RCA
Input 6 v. Output 300 v. at 80 ma, D.C. fully smoothed. Incorporates 6-pin Vibrator, OZ4A Rectifier, heavy duty transformer, etc. Variable output. Dimensions 4×4½×6in. Brand new. Limited quantity only. 35/- plus 2/- P. & P.

SPECIAL PURCHASE! MANUFACTURER'S SURPLUS

Owing to favourable purchase: MANUFACTURE 200/250 v. can offer strictly limited quantity of these handsome chassis. AC/DC 200/250 v. for Medium and Long Waves, plus gram position. Incorporates own frame aerial. Valve line-up: U107, N108, DH107, W107 and X109. Overlach assis size 12 x5½ x7½in. hlgh. Attractive bronze dial with gold and cream lettering. Dial size 11½ x 4½in. Scale length 7½in. Logging scale provided. Price £7/19/56 only, tax paid, plus 3/6 P. & P. H. terms, £4 deposit plus four monthly payments of 22/-



Splendid unrepeatable offer!! Dulci F.3 Radiogram chassis

We have been very fortunate in being able to obtain a limited quantity of this well known and highly efficient chassis which we are able to offer at a greatly reduced price.

Specification:
Three waveband: iong 1,000-2,000
metres: medium 187-540 metres; short
16-50 metres. Valve line-up: X79,
6BA6 or W7A7, 5AT8 or DH77, EL84
or N709, 6X4 or U78.

Four controls, tone/on-off.

Volume wavechange.

Volume wavechange.

Tuning: output 4 watts matched to 3-5

Chine Incorporates latest Ferrite Rod runing; output 4 watts matched to 3-5 ohms. Incorporates latest Ferrite Rod Acrial. Pick-up sockets and mains supply for Gram motor. Overall dimensions: 12in. L. × 7in. D. × 7jin. H. Attractive dial with red, gold and green lettering on black background, Size 11jin. × 4jin. Price only £10/5/- plus 3/6 P. & P.

MINIATURE CRYSTAL/TRANSISTOR RECEIVER!!!

A kit for building this very sensitive receiver employing the very latest miniature transistor and Germanium Diode, powered by a small torch battery, for headphone reception, is now available. Assembly is very simple and NO EXPERIENCE IS NECESSARY!!!

At time of going to press no price has been finalised, but it is expected to be under 40/- absolutely complete including a pair of suitable high resistance headphones. A stamp will bring full details.

TRANSISTORS!!! (Special Offer)

Now available, manufacturers surplus transistors. Suitable for use in Audio stages, etc., and for experimental purposes. P.N.P. type. Only 10/- each, post free.

AM/FM KIT

AM/FM KIT
Introducing the JASON AM/FM KIT for medium waves and F.M.
As illustrated this is a very high quality chassis incorporating 8 of the latest miniature valves, plus DM70 nugic eye with output available for Olisasis colless output in the with own built-in power pack at \$13,1096 only. These are high fidelity units and exceptional value at these prices which include all required components and full constructional details, Fully illustrated Data Booklet with full construction details, plus individually priced component list, available per return of post at 2/- post free. Both plus 3/6 P. & P.

DULCI H4T AM/FM TUNER

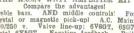
DULGI H4T AM/FM TUNER
This unit has been designed for Quality Reproduction and built to the highest technical standards. Contains own power supplies. Brief specifications: four wavebands: VHF 87-101 mc/s. Short, 16:50 metres. Medium, 187:540 metres. Long, 1,000:2,000 metres Intermediate Frequencies: 10.7 mc/s. and 471 Kc/s. Full A.G.C. on all A.M. Bands and amplitude limitation on F.M. Band. Three controls: ON/OFF, Volume, Tuning and Wave-change. Valve line-up: COSE, ECHSI, EF99, EABCS0, EMS0 and EZS0. Attractive dial in Black with Red. Green and Gold lettering, size 11½in. × 5½in. Chassis size (overall) 121n. W. × 7½in. H. Spin. D. A low impedance of 47K olim output makes matching to amplifier non-critical. Weight 12th. Price is £20/17/-. plus 5/- P. & P.

DULCI AM/FM CHASSIS H4

Hustrated leafet available. L., M. and Short Waves plus F.M. This is a quality chassis 6 latest B.V.A. Mullard Valves. including magic eye. High Q inductances throughout, also Ferrite rods. Price is £24/6/- cash—or H.P. terms

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amplifier can be supplied assembled, tested, and ready use at £5/5/-P. and Hearing plus P



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Our advantageous H.P. terms are available on any single item over £5. Let us have your

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THE "ECONOMY FOUR" T.R.F. KIT. A three-walve plus metal rectifier receiver. A.C. mains 200/250 v. Medium and Long waves. We can supply all required components right down to the last nut and boit. Valve line-up 6K7, 8J7 and 6V6. Chassis ready drilled-Cabinet. We can supply all required components right down to the last nut and bolt. Valve line-up 6K7, 637 and 6V6. Chassis ready drilled-Cabinel size 12in. long by 6in. high by 5in. deep—Choice of ivory or brown Bakelite, or wooden walnut flinish cabinet. Complete instruction booklet with practical and theoretical diagrams. Each component brand new and tested prior to packing. Our price £5/10/- complete—Remember this set is being demonstrated at our shop premises! We proudly claim that our fully illustrated instruction booklet is the most compensation of the premises of the property of the premises of the property of the premises of the property of the premises of the p



cking and carriage for complete kit.

THE "SUPERIOR" FOUR RIT. Our new four-valve receiver. A.C. mains, 200/250 v. M. and Long waves. As with our very successful "Economy Four" all lequired components as supplied. Valve line-up: 2 5807, 6 X56T and 6 V6GT. Chassis ready drilled. Cabinet size 104 in. × 10in. wide. Maximum depth at base 5 in. tapering to 34 in. at top. Slophing front. Very attractively finished in light walmut and peach. Each component brand new and tested prior to packing. Complete instruction booklet with practical and theoretical diagrams is provided. Booklet available at 1/6 post free. Our price for complete kit, £6/9/6! Please add 2/6 packing and carriage. If preferred, we can supply Cabinet Assembly only, comprising Cabinet and bracket wave-change switch, dlal, pointer, drum pulleys drive spindle, drive spring and knobs, at 45f-, plus 2/6 packing and carriage. N.B.—Our kits are even supplied with sufficient solder for the job.

N.B.—All our T.R.F. Kit circuits now include specially wound Dence "Max-Q" coils on polystyrene formers, improved performance! Price remains the same.

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		METE	RS	
F.S.D.	Size	Type	Fitting	Price
50 microamp	D.C. 2in.	M.C.	R.P	
50 microamp	D.C. 5in.	M.C.	Rectangular	
50 microamp	D.C. 4in.	M.C.	Rectangular	
50 microamp	D.C. 31in.	M.C.	F.R	95/-
100 microamp	D.C. 24in.	M.C.	F.R	
200 microamp	D.C. 2in.	M.C.	F.R. (Tropicalised)	30/-
200 mloroamp	D.C. 31in.	M.C.	F.R	
500 microamp	D.C. 21n.	M.C.	F.R	
1 mA.	D.C. 2ln.	M.C.	F.R	17/6
1 mA.	D.C. 2ln.	M.C	F. Sq	22/6
1 mA.	D.C. 2in.	M.C.	F. Sq. (1954 manufacture	
			Elliott)	25/~
1 mA.	D.C. 2lin.	M.C.	Desk Type	30/-
50 mA.	D.C. 2in.	M.C.	F. Sq	
500 mA.	D.C. 2lin	M.C.	F.R	
.5 amp.	R.F. 2in.	Thermo	F. Sq	
1 amp.	R.F. 21in.	M.C.	F.R	10/-
120-0-120 amp.	D.C. 2in.	M.C.	F. Sq. (shunt required)	
150 amp.	A.C. 4in.	M.I.	R.P	
1 amp.	R.F. 21in.	Thermo	R.P	7/6
3 amp.	B.F. 2in.	Thermo	F. Sq	6/-
20 amp.	D.C. 2in.		R.P. (with shunt)	
25 amp.	D.C. 24in.	M.I.	F.R	
30 amp.	D.C. 24in.	M.I.	F.B	12/6
15 volt	A.C. 28 ln.	M.L.	F.R	
15-0-15 volt	D.C. 23 in.	M.C.	F.B	
300 volt	A.C. 2kin.	M.C.	F.R	
300 volt	A.C. 31in.	M.I.	F.R	
SPECIAL U.S. 0-	1 mA. 2kin, tak	en from equ	pment but perfect, 22/6 eac	h. R.P. =
Round Projection	a. M.C Movi	ng Coll. The	rmo = Thermo-coupled. F. b	3q. = Flush
Square. F.R =	Flush Round.	M.I. = Mor	ing Iron.	
METER RECTIF	ERS. 1 mA. by	G.E.C., at 6	/6, also 5 mA. by G.E.C., at	6/6.

METER SPECIAL. We have a limited quantity of aircraft electrical thermometers. Brand new, by Weston, 2hn moving coll meter, thush aquare fitting. These meters have a luminous scale graduated 40-140 degrees centigrade, but the full scale deflection is approximately 150 microamps! Price 12/6 each only, plus 1/- P. & P.

24 VOLT ROTARY CONVERTOR. Input | 24 v. D.C. Output 200/250 v. A.C. 100 watts. Complete in black steel box 18in.x11in.x1in. Weight approx. 30ib. Completely smoothed, incorporates Sodium Lamp transformer Brand new, 92/6.

HEADPHONES, Low resistance. Brand new ex-W.D. type CLR., 7/6 per pair, plus 1/6 p. 6 p. Brand new ex W.D. type DHR, 4,000 ohms, 15/- per pair. High resistance, 4,000 ohms brand new light-weight. 15/- per pair plus 1/6 p. & p.

TRANSISTORS! MULLARD TYPE O.C71 Available ex stock at new list price of 24/- each also O.C.71 at 21/- and O.C.72 at 30/-. All post free.

at 30/-. All post free.

No. 38 TRANSMITTER/RECEIVER
WALKIE-TALKIE. Range approx. 5
miles. Coverage 7.4-9 Mo/s. The set only
complete with valves at 25/-. in very
good condition. We also have available
"38" sets absolutely complete with
junction box, aerial, headphones, microphone, epare set of valves, with full
operating instructions, absolutely brand
new in original sealed packing cases, at
99/6 each complete station, plus 5/carriage. Export enquiries invited.

SPECIAL PURCHASE from Ministry BRAND NEW No 17 Mk. II TRANSMITTER/RECEIVER

Built into strong wooden cabinet 15in. x 14in. it into strong wooden capinet 13In. X 14In.

9in. Complete with headphones and crophone. Range 5-8 miles with simple ial. Frequency coverage: 44-61 mc/s. (5-7 metres). Uses standard 120 v. H.T. and 2 volt L.T. batteries. Complete with full operating instructions. 59/6, plus 3/6. C. & P. x 9in. Con microphone.

No. 17 Mk. II, as above, but secondhand, in good condition and complete, 45/- plus 3/6 C. & P.

HEAVY DUTY VARIABLE AUTO TRANSFORMER. Input: Variable from 110 to 250 voits. OUT-PUT: 110 and 280, at 1.2 kVA. Contained in grey metal case with carrying handle. Overall size: 101 W × 8ln. D, × 12ln. H Weight 1 qtr. 19lb. Brand new! £8/10/- pins 76 carriage and packing.

THE R.C. RAMBLER ALL-DRY PORTABLE RIT

Full assembly details with practical and theoretical diagrams can be supplied at 1/6 post free. This is a truly professional 4-valve superhet—all diry—for medium and long waves. A cream plastic top panel, with dial engraved in red and green adds to the very imposing appearance of this model which is housed in an attractive cream and grey leatherette covered attache-case type cabinet: measuring only 0ln. X 7ln. X 51ln. Weight less batteries 44lb., with batteries 64lb. This set really has everything. Bullt-in frame serial, high quality, extremely sensitive, and very adequate volume from the 5in. speaker. Valve line-up 374, 1R5, 185, 174. Also the required components, exactly as specified, including cabinet, can be supplied from stock at the special lacibusive price of £777/- plus 2/6 p. and p. (less hateries). Uses Ever-Ready 90 v. H.T. type B128 at 10/s. Also L.T. 1.5 v. A.D. 35 at 1/8.



RAMBLER MAINS UNIT! At last we are able to offer our special mains units kit for using our popular all-dry "Rambler" on A.C. Mains. Complete kit, which when assembled fits snugly into battery compartment, can be supplied at 47/6 plus 1/6 packing and postage. Price includes all required components, and full assembly instructions, N.B.—This unit is completely self-contained in a metal box measuring 7in. × 2½in. × 1½in. and is ideally suitable for ANY all-dry battery portable requiring 90 v. H.T. and 1.5 L.T.

THE R.C. 2 AMP, BATTERY CHARGER KIT, Our new 2 amp, charger kit is now available. Includes handsome well-ventilated black stove-enampled steel box; 27 ½m. × 3½m. Fully shrouded first quality transformer, brand new G.E.C. rectifier. Mains use, etc., or charging 6 or 12 v. batteries at 2 amp. Absolutely complete kit with full practical and theoretical instructions. Price 33/6 plus 2/6 P. & P. Can be supplied assembled and tested at 41/6 plus P. & P. Heavy duty crocodite clips suitable for car battery lugs, optional extra at 1/6 per pair. THE R.C. 2 AMP. BATTERY CHARGER

Input 200/250 v. Output 350-250 280 mA, 6.3 v., 8 a., 6.3 v. 2 a., 4 v. 7 a., 5 v. 2 a. Fully smoothed. Incorporates valve rectifier GZ32. Chassis measures 13 in. \times 7 in. \times 5 jin. \times \times 2 ib. Few only at 24/19/6, plus 3/6 p. and p.

MAINS TRANFORMER SPECIAL!
Primary: 10-0-200-220-240 v. Secondary
windings: 375-200-0-200-375 v. at 230 mA.
Double wound 230 v. at 6 amp. 6.3 v at
3 amp., 6.3 v. at 3 amp., 8 v. at 0.25 amp.
Unshrouded, fully impregnated dropthrough type. 50/-, plus 1/6 p.p.

FOUR-SPEED CHANGERS! The new B.S.R. 4-speed auto-changer in attractive cream and gold finish, now available from stock at £9/15/- only, plus 3/6 p. and p. H.P. terms available.

Special Purchase! RC.54. Special Purchase! Latest type 3-speed incorporating "T" type turnover head. Cream finish. Original manufacturer's cartons. Definitely the last few £8/19/6 only, plus 3/6 p. and p. H.P. terms available.

GARRARD 120H !!! 3-speed, mixer, anto-changer unit with crystal to head and saphire stylii. Provided with Manual control for single records. Frinished in Cream and Brown. Brand new in sealed manufacturers carton with fitting and operating instructions. 27/19/6 plus 5/- P. & P.

VALVES

We have perhaps the most up-to-date valve we have jet haps the most up-to-mate varye stocks in the trade. A stamp will bring complete list but the following is a selection only of brand new imported valve types. fully guaranteed. Purchase tax pald.

EABC80	10/-	DAF96	10/6	PL83	11/6
EAF42	10/-	DF96	10/6	PY80	10/6
EB41	7/6	DK92	10/6	PY81	10/-
EB91	7/6	DK96	10/6	PY82	9/6
EBC41	10/-	DL96	10/6	PY83	11 6
EBF80	11/6	or39/61		UBC41	
ECC81	9/-	of four		UCH49	211/6
ECC82	9/-	DM70	9/-	UF41	10/6
ECC83	9/-	EL41	10/6	UL41	10/6
ECC84	15/-	EL84	11/6	UY41	9/-
ECC85	10/-	EM80	9/-	6AQ5	8/6
ECF82	15/-	EY51	12/-	6AT6	
ECH42	11/6	EY86	14/6	6AU6	
ECH81	11/6	EZ40	8/6	6BA6	8/8
ECL80	11/6	EZ80	8/6	6BE6	9/-
EF41	10/6	PCF80	12/6	6BW6	8/6
EF80	10/6	PCF82	12/6	6X4	7/6
EF85	10/6	PCC84	12/6	35W4	7/6
EF86		PL81	13/6	50B5	10/-
EF89	10/-	PL82	10/6	50C5	10/-
in addit	ion w	e natur	ally h	ave all	usua1
surplus 1					76GT
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TELETRON BAND III CONVERTOR! Still

LOOK 11 1 A first class SIGNAL GENERATOR that VOU can afford. The "Weyrad" type S.G.M.1 covers 100 kc/s to 70 mc/s in 6 bands, on Fundamentals, with an accuracy better than ± 2%. Switched Audio Mod.: 500 c/s. For use on A.C. Mains 200/250 v. 50 cycles. Fully illustrated leaflet available. Price ONLY 212/10/- plus 2/6 P. & P. H.P. available.

RECORD PLAYERS CABINETS-to suit all types of single record and auto-changer units. Priced from 45/-. Send stamp for fully illustrated list.



Another Cabinet Bargami Special purchase of walnut trolley-type cabinets originally intended for use in projection T.V. Easily recognised as being of leading High Qua'tty manufacturer's stock. Can be easily adapted to house tape recorder, amplifier, radiogram, etc., etc. Measurements external 24 in. x 16 in. x 29 in. The whole is mounted on easters Unrepeatable bargain at £5/19/6 plus 10/- packing and carriage, We have a large selection of all type cabinets. A stamp will bring list.

CLYNE RADIO LTD

18, Tottenham Court Road. London, W.I. Stern SNEW!! "fidelity

TAPE RECORDER WITH EVERYTHING EXCEPT A HIGH PRICE

BEFORE CHOOSING YOUR RECORDER YOU MUST HEAR THIS NEW "fidelity" MODEL . . . IT HAS . . . THIS NEW "fidelity" MODEL . . . IT HAS . . .
The BRENELL 3-speed Tape Deck and a "fidelity" Tape Amplifier, based on a new design by the MULLARD TECHNICIANS and which we consider to be one of the best now available . . . Truly HIGH FIDELITY RECORDINGS are obtainable.

PRICE of COMPLETE RECORDER INCLUDING MOVING COIL MIKE and 1,200ft. REEL of TAPE

(Plus £1 carriage and insurance of which 10/- refunded on return of packing case.) CREDIT TERMS. Deposit £11/10/- and 9 monthly payments of £4/4/4. HIRE PURCHASE. Deposit £23 and 12 monthly payments of £2/2/8.

-HOME CONSTRUCTORS-YOU CAN BUILD THE COMPLETE RECORDER FOR

(Plus £1 carriage and insurance of which 10/- refunded on return of packing case.) CREDIT SALE TERMS. Deposit £10/12/6 and 9 monthly payments of £3/17/11. HIRE PURCHASE TERMS. Deposit £21/5/- and 12 monthly payments of

The BRENELL TAPE DECK and the "fidelity" TAPE AMPLIFIER are supplied tested and ready for use and the actual assembly of the recorder is extremely simple involving only a few connections for which a step-by-step chart is supplied.



★ High Quality Output Transformer by Gilson

 \star 3 Speeds, $3\frac{8}{4}$, $7\frac{1}{2}$ and 15in., TWIN TRACK

* Position provided for use as straight amplifier

* Efficient Tone Control arrangement

★ High-grade Components throughout

★ Two position equaliser for 34 and 71in.

Monitor and Extension Speaker Sockets are provided

* Beautiful styling of cabinet

IF YOU HAVE YOUR OWN CABINET WE WILL SUPPLY . . .

THE BRENELL TAPE DECK, the "fidelity" TAPE AMPLIFIER, MATCHED P.M. SPEAKER and 1,200ft. REEL PLASTIC TAPE.

CREDIT SALE TERMS. Deposit £9 and 9 monthly payments of £3/6/-. He Deposit £18 and 12 monthly payments of £1/13/5. HIRE PURCHASE TERMS. 於 £36'0'

(Plus £1 carriage and insurance of which 10/- refunded on return of packing case.)

TAPE RECORDER EQUIPMENT—IN STOCK . . .

- BRENELL 3-SPEED TAPE DECK (a) The "fidelity" TAPE AMPLIFIER (as used in above Tape Recorder), including matched P.M. Speaker £16/16/-£18/10/-(b) The TRUVOX MK. IH and MK. IV DECKS

- (from \$294/3)(c) The COLLARO TRANSCRIPTOR "TAPE
 DECK" \$20 (see note below)
 (d) The LUSTRAPHONEN MOVING COIL MIKE,
 HIGH IMPEDANCE, \$3/7/6
 (e) The ACOS CRYSTAL MIKE, HIGH IMPEDANCE, \$2/10/-
 - (b) The TRUVOX MODEL "C" TAPE AM-PLIFIER £17/17/-
 - The ARMSTRONG P.A.B.O. TAPE PRE-AMPLIFIER £12/10/- (suitable for nearly all

All types of PLASTIC TAPE by E.M.I., SCOTCH BOY and GRUNDIG, Standard and Long play ARE IN STOCK.

ARE IN STOCK.

NOTE. We recommend that a CORRECTLY MATCHED PREAMPLIFIER is purchased with the COLLARO Transcriptor. We can supply it with the preamplifier actually assembled on Tape Deck. \$37/10/-. HIRE PURCHASE and CREDIT TERMS are available on all above equ ment.

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STERN'S "fidelity F.M. TUNING UNIT A 5 Valve Tuner incorporating

£14/10/0

7/6 carr. & ins.)

(Plus 7/6 carr. & tins.)
TERMS: (a) H.P. Deposit £7/5/and 9 monthly payments of 18/4;
(b)Gredit Deposit £8/12/6 and 9 monthly payments of £1/6/7.
Provides "Hi-Fi" reproduction with any make of Amplifier
and many Radio Receivers. It incorporates ● The latest
Valve Line-up—ECOS5, 2 *ype EPS5, EF91 and EMS0.

A "Magic Eye" Indicator ● Power consumption is
1.7 amps. at 6.3 voits and 25 m/a. at 250 voits.

STERN'S "fidelity" COMBINED A.M. and F.M. TUNING UNIT

This is IDENTICAL 'o the Stern's F.M. Tuner illustrated above, but in addition incorporates the MEDIUM WAVE-BAND and thereby also provides a selection of foreign exteriors.

stations.

Price \$18/18/0 (Plus 7/6 carr and inv.)

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THE LEAK "TL/10" AMPLIFIER
and "POINT ONE" PRE-AMPLIFIER



Provides a maximum output of 10 waits, maintains in every respect the renowned Leak reception for precision engineering, fine appearance and fastidious wiring.

PRICE COMPLETE \$28/7/0

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TERMS: Credit: Deposit £?/?/- and 9 monthby payments of £2/11/4. H.F. Deposit
£14/4/- and 12 monthly payments of £1/6/-.
Send S.A.E. for fully illustrated leafiet.

STERN'S " COMPACT **AMPLIFIERS**

EXPRESSLY DEVELOPED FOR VERY HIGH QUALITY REPRODUC-



GEAM,
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PARTICULARLY
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FOR HIGH
QUALITY
REPRODUCTION
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The "Compact 5-2"

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A 2-stage high sensitivity amplifier having SDPAR-ATE BASS and TREBLE CONTROLS and designed to give up to approx. 5 watts with very pleasing quality. PRICE £5/15/-

The "Compact 5-3" A 3-stage version of the "5-2" model but in this case having an additional stage and incorporating negative feedback. PRICE £6/16/-

The Amplifiers are compact and very attractively designed having a "Hammered/Gold" finish with a fully engraved front panel by which the entire Amplifier is conveniently mounted into a Cabinet, occupying no more space than a conventional Tone Control Unit. Send S.A.E. for illustrated

POWER SUPPLY. Is obtainable from a small separate Unit which apart from supplying power to either Amplifier, also has additional supply available for a Radio Tuning Unit. PRICE (additional to above), £2/10/-.

Open Monday to Friday 9 a.m.-6 p.m. Saturday 9 a.m.--1 p.m.

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AMPLIFIERS PRE-AMPLIFIERS

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TUNING UNITS RADIO RECEIVERS

KITS OF PARTS FOR "Hi_Fi"

QUALITY OF THIS NATURE HAS NEVER BEFORE BEEN OFFERED AT SUCH LOW COST.



This is the very latest descripted to Mullard's specification, including the latest GILSON ULTRA LINEAR OUTPUT TRANSFORMER and the entire MULLARD Valve line up. ALL SPECIFED COMPONENTS are supplied. PRICE OF COMPLETE KIT OF PARTS \$\frac{21}{110}\$ (Pius 6)- carr. and ins.). \$\frac{25}{60}\$ (DIRECTE KIT OF PARTS \\
\text{CPIUS OF COMPLETE KIT OF PARTS} \\
\text{VIII IN THE FULL PREVIEW ACTION AND ADDITIONAL AN

STERN'S "fidelity" PRE-AMPLI-! FIER TONE CONTROL UNIT

"A design for the music lover"



THE full SPECIFICATION and BUILDING INSTRUCTIONS for these three Units are available for 1/6 each. THEY include COMPONENT PRICE LISTS and simple "wire-to-wire" PRACTICAL DIAGRAMS.

"HIGH OUALITY" 8-10 WATT AMPLIFIER

Price of COM-PLETE KIT OF PARTS (plus 5/- carr. £7/10/0 WE ALSO OFFER IT ASSEMBLED

A COMPLETE KIT OF

PARTS STERN'S

Has power sup-ply available for Radio Tun-ing Unit.

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This amplifier has proved one of the most popular models yet offered to the HOME CONSTRUCTOR. It provides really excellent reproduction up to 8 watts, employing 6V6's in push-pull and incorporating negative feedback. Provides for the use of both 3 and 16 ohm Speakers. The Complete SPECIFICATION and BUILDING INSTRUCTIONS are appliable for 1/8

Complete Struction and District and District and THONS are available to 1/8.

"Wire-to-Wire" Diagrams are included and all Components are available separately.

SPECIAL PRICE REDUCTIONS . . . FOR PURCHASERS OF A COMPLETE "HI-FI" AMPLIFIER

WE WILL SUPPLY (a) COMPLETE KIT OF PARTS to build THE MULLARD "5-10" MAIN AMPLIFIER and the STERN'S "fidelity" PRE-AMPLIFIER-TONE CONTROL UNIT for £16/16/- or we will supply THE TWO UNITS MADE UP and READY FOR USE for £19/19/-. Terms: Deposit £9/19/6 and 12 monthly payments of £1/16/7.

"MODERNISE YOUR RADIOGRAM" OLD

IT IS MUCH CHEAPER THIS WAY!!

THE LATEST DESIGN OF COMBINED AM/FM REPLACEMENT RADIOGRAM CHASSIS and a NEW 4-SPEED RECORD PLAYER

nely hand-made chassis providing really high quality A on both Radio and Gram.

PRICE

£26/15/0

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luxe" Chassis for those who want the highest possible quality



PRICE £29/8/0

(Plus 7/6 carr. and ins.).

TERMS: Credit Deposit £7/7/-and 9 monthly payments of £2/14/-. H.P. £2/14/-. H.z. £14/14/-

STERN'S NEW "Fidelity" COMBINED AM/FM RADIOGRAM CHASSIS RADIOGRAM CHASSIS RADIOGRAM CHASSIS RADIOGRAM CHASSIS RADIOGRAM CHASSIS REPROPERTY OF THE NEW MODEL "H" COMBINED AM/FM RADIOGRAM CHASSIS RADIOGRAM CHASSIS Pesigned for first rate reproduction of Radio

and Gram Records PRICE

£21/10/0

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payments from \$22/9/-. H.P. Deposit \$213/7/8 and 12 monthly payments of \$22/14/-. H.P. Deposit \$213/7/8 and 12 monthly payments of \$21/18/-. H.P. Deposit \$213/7/8 and 12 monthly payments of \$21/7/8.

BRIEFLY IT HAS:—

An 8 valve line up incorporating the latest MULLARD preferred-type valves. Provides complete coverage of the VHF/FM waveband plus the SHORT, MEDIUM and LONG waves. Has EL84's in Push-Pull, with negative feedback of 8 watts output. Employs "Pinno Key" Selector Switch and a Variable Tone Control. Contains of Feed output. Quiet action "Pinno Key" Selector Switch and a Variable Tone Control. Contains of Provides for use of either 3 or 15 ohm Speakers. Has El84's in Push-Pull, with negative selectors and separate Bases and Treble Controls. Quiet action "Pinno Key" Selector Switch and a Variable Tone Control. Contains of Provides for use of either 3 or 15 ohm Speakers. Has a provided, one for Crystal Pick-ups and the other for Magnetic Feed Tuning Indicator. Of Two Gram Inputs are provided, one for Crystal Pick-ups and the other for Magnetic Feed Tuning Indicator. Of Two Gram Inputs and EM80 Tuning Indicator. Of Output is 4 watts and any 3 or 15 ohm Speakers are not used. Connection of Sockets on the Chassis (a) Pick-up, (b) Extension Speaker, for 3 of 16 ohm types. Overall size 12 in. x 9 in. x 7 in. high, Dial size 11 in. x 5 in.

SEND S.A.E. IF FURTHER INFORMATION IS REQUIRED ON THESE CHASSIS.

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We recommend THE 8- or 10-inch W.B. STENTORIAN "Hi-Fi" MODELS. We have SPECIALLY REDUCED PRICES for purchasers of a CHASSIS and RECORD PLAYER (and SPEAKER if required). SEND S.A.E. FOR DETAILS.

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This latest B.S.R. MONARCH 4-SPEED AUTOCHANGER £7/19/6 (Plus 5/- carr. and ine.). • These units will autochange on all three speeds, 7in., 10in. and 12

in.

They play
MIXED 7in.

10in. and 12in. records of same speed.

They have separate sapphires for L.P. and 78 r.p.m.,
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Minimum baseboard size required 14×12fin. with
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GREATLY REDUCED PRICES

● TRANSCRIPTION UNITS. ● 3- and 4-SPEED AUTOCHANGER ● AUTOCHANGERS with MANUAL CONTROL POSITION, Send S.A.E. for ILLUSTRATED and DESCRIPTIVE LEAFLET.

SPECIAL CASH OFFER

A good quality 2 Stage (plus Rectifier) GRAM AMPLIFIER together with a 64m, P.M. Speaker and this attractive PORTABLE CASE.

ALL FOR ONLY 28/7/6. The Amplifier incorporates the latest B.V.A. Valves, types ECC83, EL84 with EZ80 Rectifier and has separate BASS and TREBLE CONTROLS. The CASE is attractively finished in Rexine, maroon and grey, and has space for almost any make of Autochanger.

We also sell the two separately:
(a) AMPLIFIER and 6 in. SPEAKER 24 12 6

(a) AMPLIFIER and 64 m. SPEAKER ... 24 12 6
(b) PORTABLE CARRYING CASE ... 23 17 6

FOR CALLERS ONLY We have in stock various KITS OF PARTS including P.M. Tuners, AM/FM Tuners, Midget Battery Portable and Mains Units, etc., etc. .. We also have the most comprehensive stock of WIRELESS and ELECTRICAL COMPONENTS.

STERN'S "SUPER SIX"

6 Valve 3 Wavehand Superhet

Provides good selection of stations and really good reproduction on both RADIO & GRAM.



PRICE \$14.0.0 (p'us 7/8 arriage and ins.

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BRIEF SPECIFICATION .



. . . you will realise that Grampian high fidelity equipment gives you the nearest approach to "Concert hall listening" in your own home. You will, for instance, appreciate the extraordinary delicacy of reproduction achieved by their new 12in. loudspeaker. A great deal of research and new manufacturing methods were necessary to produce a speaker unit with such an extended audio frequency coverage at such a reasonable cost.

GRAMPIAN 12" SPEAKER UNIT -

Type 1255/15

Frequency Range 20-15,000 c.p.s. Voice Coil Diameter 1%in. Voice Coil Impedance: 15 ohms. Fundamental Resonance: 40 c.p.s. Power Handling Capacity: .. 10 watts. Flux Density: 14,500 lines per sq. cm. Total Flux: 130,500 lines per sq. cm.





CYCLES PER SECOND INPUT & WATT RESPONSE CURVE for speaker unit 1255/15



A specially designed reflex cabinet suitable for either corner or side of room is now available as an easy-toassemble kit of parts, complete with grille material ready to assemble, stain and polish. Although it is primarily intended for use with the Type 1255/15 speaker the cabinet will give excellent results with other units of similar specifications. Price £11

Full details from:

Deferred terms available if desired for both speaker and cabinet kit!

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All your TV Components from one source

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Send headed paper for Trade Terms, C.W.O. or C.O.D.

Please add postage and packing (1/6 up to 10/-, 2/- up to £1, 2/6 up to £1). Ordering a number of items at one time will show a considerable saving. The minimum rate for postage and C.O.D. mrde by the G.P.O. is 2/6. All orders over £5 Packing and Postage Free.



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BUILD A RADIO FOR 37'6 or 47/6!



In response to many requests we now resent the double-triod "SKYPOCKET." a beautifully designed precision PCCKET." a beautifully designed precision PCCKET. RADIO. Can be built by anyone without any radio knowledge whatever—EVERY SINGLE PART TESTED BEFORE DESPATCH; our simple, pictorial plans take you step-by-step. This set has a remarkable sensitivity due to painstaking design and careful choice of component values. Covers all medium waves 200 to 550 Metres, including "Home." Light." Luxembourg, etc. Size only 5iln. x 3in. x 3in. in strong plastic case with panel, cover and station-printed invorine dial. A really personal pocket-radio WITH OWN DETACHABLE ROD AERIAL, uses personal phone, ideal for Bedroom, Garden, Holldays, Second-set, etc. Completely all-dry low consumption battery operation. Specially chosen high-efficiency coil. Average building time 1 hour. Total Building Cost-including Case, Double-Triode valves, etc., in fact, everything down to the last nut and both—ONLY 37/6 with plans. Postage, etc., 2/CO.D. 1/6 extra. (Parts sold separately. Priced Parts Lists, etc. 1/6). Demand is certain to te besyen—SEND TODAY In response to many requests we no present the double-triode "SKYPOCKET



Build this exceptionally sensitive twin triode ratio for the control of the contr

ORDERS DESPATCHED BY RETURN Limited SEND TODAY! ALL PARTS AVAILABLE SEPARATELY

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3-SPEED AUTO-CHANGERS BRAND NEW IN MAKERS' CARTONS



GARRARD RC.120/H. 3 speed. Complete with t.o. crystal pick-up. Incorporates manual and auto control enabling records to be played singly if desired. Cabinet space required: 14 x 12\frac{1}{2} x 4\frac{1}{2} in. above and 2\frac{2}{2} in. below. Cream/brown finish. Limited number only. List \(\frac{1}{2}\frac{1}{ £7.19.6 LASKY'S PRICE Carr. 3/6. Cabinets available.

GARRARD RC.80. Full length arm with two XMS heads or GC2 t.o. crystal head. List £20/15/-. LASKY'S PRICE £13.19.6

B.S.R. 4 Spd. with t.o. crystal pick-up. Incorporates auto and manual control enabling records to be played singly. LASKY'S PRICE £8.15.

T.O. CRYSTAL CARTRIDGES B.S.R. complete with two styli. LASKY'S PRICE 18/6, post free.

ACOS type HGP.37, as used in latest radiograms. L.P. and standard. Complete with styli, 22/-. Post 1/-.

DECCA PICK-UPS
3-speed with t.o. crystal head HI/G, and rest. Brown plastic.
LASKY'S PRICE 32/6. Post 2/6.

The New WEARITE "DE-FLUXER," 50/-. Post 2/6.

CONTINENTAL AM/FM **RADIOGRAM** CHASSIS LASKY'S PRICE £16.19.6

Very special offer of a limited number only at wonderful bargain price! Built throughout of latest high grade components. 5 valve plus metal rect., gram socket and switch, piano key wavechange tone control, independent AM/FM tuning. Covers med., long and V.H.F. wavebands. Valve line-up: ECC85, ECH81, EF89, EABC80, EL81. For A.C. mains 100-250 v.

SPECIAL P.A. OFFER!



TRUVOX "SENIOR" **SPEAKER** DRIVING UNIT (Pressure type) WELL BELOW HALF PRICE!

New and unused in makers' cartons. A P.M. moving coil loudspeaker driving unit with a power handling capacity of 15 watts peak. Provides substantially linear response from 200 to 10,000 c.p.s. With a 12ft. cinema horn the unit will reproduce down to 17 c.p.s. The Throat has an 18 t.p.i. thread with an external diameter of 1\frac{1}{6}in.

LISTED AT £7/15/-.

LASKY'S PRICE

59'6 Carr. 5/-.

LASKYS RADIO

TAPE DECK CASES ALMOST HALF-PRICE



Strongly made and finished with light grey leatherette with black/silver bands, finger-shaped handle for easy carrying, strong hinges and clasps. Pocket in lid strong hinges and clasps. Pocket in lid for tapes and spools, door for microphone, etc. Overall dim.: 15½in. long, 13¼in. wide, 9in. deep. Inside dim.: 14¾in. × 12¾in. × 5¾in. A real general purpose job; will take almost any type of Deck including Collaro Tape Transcriptor, also almost any type of Record Changer including RC.80, etc.

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LARGE SELECTION OF CABI-NETS for TV and radiograms, carrying cases for record players, tape recorders, etc. Your enquiries invited.

SINGLE RECORD PLAYERS



B.S.R. type TU.8, as illustrated.
3-spd. motor and pick-up with HGP.59
t.o. crystal complete with styli.

LASKY'S PRICE 92/6

Post 3/6.
Above motor and turntable less pick-up, 57/6. Post 2/6.

COLLARO RC.3/554, 3-spd. Single Record Player with Studio t.o. crystal pick-up and styli.

LASKY'S PRICE £6.10.

HI-FI SPEAKERS

Large stocks. Goodmans, Wharfedale, G.E.C., Lorenz, etc., including the new Wharfedale 3-speaker system new \SFB/3.

HI-FI AMPLIFIERS

Full range in stock. Quad, Rogers, Leak, R.C.A., Pamphonic, Unitelex, W.B., etc. Demonstrations at Totten-W.B., etc. Demo

IGRANIC JACK PLUGS, 2'6.

LASKY'S BATTERY PORTABLE FOR HOME CONSTRUCTION ON PRINTED CIRCUIT

You can build it complete with valves and for only

Post 3/6 extra.



10 STAR FEATURES make this the finest portable radio ever offered to the home constructor. Peak value for money has been achieved without any sacrifice of quality or design.

SIMPLICITY OF CONSTRUCTION. The use of all the latest innovations gives maximum simplicity of construction combined with fine quality performance. In particular, the PRINTED CIRCUIT greatly simplifies construction and completely eliminates the possibility of wiring errors. The veriest novice can build this portable radio easily and quekly and the cost complete, less batteries, is only £7/7/-. Plus 3/6 postage.

Demonstration models at both our addresses.

SEND FOR CIRCUIT DIAGRAM with assembly data, all instructions, illustrations and full shopping list. Price 1/6 post free. ★ PRINTED 7½in. × 2½in. CIRCUIT,

4-valve Superhet, med. and long waves.

Low consumption Double Battery Life.

* Ferrite Rod Internal Aerial. 3 or 5in. P.M. Moving Coil Speaker (your choice).

Brand new T.C.C. Capacitors.

Automatic Volume Control. New style Contemporary Case.

Lightweight and Handsome Appearance.

★ Every Component available separately.

YOU CAN BUILD A POWER SUPPLY UNIT FOR THIS PORTABLE.
For 200-250 v. A.C. mains. Made for the new low consumption valves. COMPLETE KIT containing printed circuit, brand new TCC condensers, latest STC metal rectifiers, all components, and full instructions, 45/-. Post 2/-. Also suitable for most other portables. Full details on request.

SEND 3d. STAMP FOR OUR LATEST BARGAIN LIST.

MORE MONEY-SAVING LASKY BARGAINS ON

LASKY'S. RADIO



A REALLY FIRST CLASS F.M. TUNER FOR HOME CONSTRUCTION ON A PRINTED CIRCUIT

Note these star features:—

* HIGH SENSITIVITY.

* ALL BRAND NEW T.C.C.
CONDENSERS.

AERIAL COIL AND R.F. COUPLING COIL PRINTED ON

CIRCUIT.
5 VALVES AND 2 GERMANIUM DIODES.

By the use of a printed circuit the I.F. and R.F. amplifiers are extremely stable at maximum gain and results are consistent on all tuners.

tent on all tuners.

Valve line-up:—

R.F. Amplifier, Z719 or EF80.

Mixer and Osc., B719 or EC85.

Ist I.F. amp., W719 or EF85.

2 Germanium Diodes GEX.34.

Driver Limiter, Z719 or EF80.

CAN BE BUILT FOR GINS.

Write for full instructions data and illustrations, 2/6 post free.

All parts available separately

All parts available separately



AM/FM TUNER

A super-sensitive Tuner for F.M. and medium waves. The complete parcel with power supplies, £13/19/6. Post 3/6 Data Book, 2/- post free.
All components available separately. Send for itemised price list. Chassis Assembly, 57/9, post 2/6. I.F. and Coil Set, 78/-, post 1/6.

5-Valve RADIO CHASSIS

1 deal as radio receiver for inclusion in a TV set. Brand new and unused. A.C./D.C. 200/250 v. I.F. 465 kc/s. A.V.C. 4 watts output, 3-station pre-set, frame aerial, fully aligned, chassis 10 x 5½in. max. height 5½in. Completely wired and ready for use with the addition of a speaker and output transformer. Two controls, volume and station switch. Valves used: 10Cl, 10F9, or UF14, 10LD11, 10P14, U404 or UY41. LASKY'S PRICE less valves. Post 3/6. 52/6

SAVE POUNDS! ORDER BY POST IF YOU CANNOT CALL

FAMOUS' MAKE TURRET TUNER



and 3. Valves used: PCC34, R.F. double triode, cascode R.F. amplifier, PCF30, triode pentode, f.c. and mixer. I.F. output 33-38 Mojs. Easily modified to other I.F. output Full instructions and circuit diagram

12 CHANNEL TUNERS

Famous make. Covers Bands I and III. Complete with valves EF80 and ECC81. Ceramic valve holders, finest quality components. Switch and fine tuning. I.F. output 20-25 Mc/s. Freq. coverage 50-87 Mc/s. and 175-213 Mc/s. Full details and effectual diagram supplied. LASKY'S PRICE
Post 3/6. KNOBS 2/9 extra.

79/6



BAND III CONVERTORS BELOW HALF-PRICE! COMPLETE WITH POWER SUPPLIES

Brand new, manufactured by one of the well-known Pye group. In attractive plastic case complete with three brand new Mullard valves: Cascode R.F. Amp PCC84, Osc. Mixer ECC81, Rectifier E290. Not a kit but complete with valves, ready for use. Original list price \$f90/9-

£9/9/-Post and Pkg.

JASON F.M. TUNER

Special parcel containing data book, chasels, front panel, dial, drive tuning condenser, full set of coils. I.F.s ration of the condenser full set of coils. I.F.s ration of the coils 2/- post free.

DATA EBOOK with price list 2/- post free.

Post 2/6

Note: This tuner uses 4-6AM6 and 2 crystals and can be built for £6/15/-, plus 3/6 post.

DULCI F.M. TUNER

Incorporates its own power supply and provides complete F.M. coverage. Operates with most radio receivers and any make of Amphifer. Valve line-up. EABCS0, ECOS5, two EFS9, 6X4 (Rect.), EM80 magic eye indicator. Dial 10½×6in. Overall size 9×6×5in. high. Complete. £17.10.0 Carr. & Pkg. 7/6.
DULCI AM/FM TUNER £20/17/-

METER BARGAIN

2½in. moving coil. Brand new micro-ammeters F.S.D. 0-750 micro-amps., 15 ohms. resistance 15/-. Post extra.

BUILD THIS FIRST-CLASS TAPE RECORDER AT MANY POUNDS SAVING

LASKY'S PORTABLE TAPE RECORDER KIT

Comprises:-

* Fully fitted portable case 59/6 ★ Latest type Truvox Deck 23 gns.

★ Tape Recorder Amplifier 12 gns. 7×4 Elliptical Speaker, 19/6 * 1,200ft. E.M.I. Tape,

* 7in. Plastic Spool, 4/6

LASKY'S PRICE COMPLETE KIT



36 GNS. Carr. & Pkg. 25/-.



LATEST BRENELL TAPE EQUIPMENT

Deck. 3-speed, 3 motors, record and play back. 18 gns.
Amplifier Mk. II. 5 watts, for use with 3 ohras speaker. Magic eye. 18 gns.
Carrying Case £4/18/-.
Complete equipment less mike, with tape, in carrying case ready for use.

Full details on request.

48 gns.

LASKY'S RADIO CONSTRUCTOR PARCELS



PARCEL No. 1

Contains everything to build a 4-valve 3-wave superhet for 200/250 A.C. mains. Uses &KS, &KT, &CT, &VG valves. Attractive wood cabinet, walnut veneer, or plastic cabinet as illustrated. Size 12×8§×5§in. deep. CAN BE BUILT FOR £7.19.6 Carr. and packing 2/6.

PARCEL No. 2

Contains everything to build a T.R.F. 3-valve set for 200/250 A.C. mains, medium and long wave. Uses 6KTG, 6JT, 6V6 and metal rectifiers. Neat plastic cabinet, walnut or ivory finish, or wood cabinet. can BE BUILT FOR £5.10.0 Carriage and packing 2/6

INSTRUCTION BOOK for either above sets 1/- post free. CABINETS ONLY, plastic or wood, 17/6. Carriage 2/6. All components available

Carriage 2/6. separately. **ALUMINIUM CHASSIS**

18 S.W.G. undrilled, 4 sides, 18 S.W.G. unarilied, 4 states, reinforced corners. Depth 2½ in. 6×4 4/-; 12×8 7/-; 16×10 8/3; 8×6 5/-; 14×9 7/6; 12×3 4/9; 10×7 6/-; 16×9 8/-; 12×6 6/6. Post 1/- per chassis extra.

LARGE RANGE OF TAPE DECKS

Collaro "Tape Transcripter." £20. Truvox 23 gns. Lane £18/10/-. Brenell 18 gns. Wearite £35 and £40.

SPECIAL OFFER TAPE DECK MOTORS

Anti-clockwise, shaded pole. Col-laro 25/-. Garrard 26/6. B.T.H. 28/6. Post extra.

NEW PLASTIC RECORDING TAPE

"Ferrovoice," on plastic spool, 1,200ft. Listed at LASKY'S PRICE 25/-

Post 1/-. Spare 7in. spools, 3/6.

Special Offer! Magnetic

Recording Tape, kraft base. On Cyldon metal spools: 1,200ft. 11/6; 600ft. 7/6 On plastic spools: 1,200ft, 12/6; 600ft. 9/6. PURETONE Tape on plastic spool, 1,200ft., 14/11 Post 1/- extra.
All makes of Tape includ-

ing thin long-playing. Also spools.

> GERMANIUM CRYSTAL DIODES

GEX.00 1/6 GEX.34 GEX.54 and OA71

FERRITE ROD AERIALS

Med. and long waves, wound ready for use. Each 6/9, post 1/-.

FERRITE ROD

5in. long, \$\frac{1}{2}in. diam., with full instructions for making a Ferrite road aerial, 2/6, post 1/-.

STANDARD 2-GANG CONDENSERS

.0005 mfd., with fixing feet. Each 5/11. Post 1/6.

MORE MONEY-SAVING LASKY BARGAINS ON NEXT PAGE

EVERYTHING FOR HOME CONSTRUCTOR & SERVICEMAN LASKYS

MAINS TRANSFORMERS

All 200-250 v. 50 c.p.s. primary, finest quality, fully guaranteed.

MBA/3. 350-0-350 v. 80 mA. 6.3 v. 4 a., 5 v. 2 a. Both filaments tapped at 4 volts. 19/6-

MBA/7. 250-0-250 v. 80 mA. 6.3 v. 3 a 5 v. 2 a. Both filaments tapped at 4 volts

0-10-120, 200-230-

AT/3. Auto trans. 0-10-120, 200-230-240 v. 100 watts. 19/6.

MT/340. Tapped input 200/250 v. 300-0-300, 100 mA., 5 v. 3 amp., 6.3 v. 1.5 amp. 16/6

MT/341. Tapped input 250-0-250, 120 mA... 6.3 v. 5 amps., fully shrouded. 27/6.

6-VALVE RADIOGRAM CHASSIS COMPLETE WITH VALVES

Famous Manufacturer's Surplus 6-valve 3-wave Superhet. 13-50 m. short. 200-550 m. medium. 1,000-2,000 m. long. Brand new Mullard valves: ECH42, EF41 L63, EB41, 6V6, g.t. EZ40 and finest quality components. Gram., switch, 465 Kc/s. I.F. tone control, three-colour dial-Overall size 13½ × 5in, height 12½in, Apcrture required for dial and controls 11 × 31in. Complete with valves, output trans. knobe etc

LASKY'S PRICE £10.19.6

Carriage and Packing 7/6 extra

5-VALVE RADIOGRAM CHASSIS complete with valves, £9/19/6. Carr. & Pkg. 7/6.

HI-FI ELECTROSTATIC **SPEAKERS** "TWEETERS" AT REDUCED PRICES

For high fidelity sound reproduction. Easy to fit to any radio, TV receiver or amplifier. Full data and circuit diagram supplied with each.

LSH75 For outputs up to 6 watts, 8/-.

For outputs of 10-12 LSH518. watts, 12/6.

LSH100. For outputs up to 20 watts 14/-.

Moving coil Tweeter. I.PH65. Imp. 5.5 ohms, freq. range 2,000-2,200, 50 c/s. For outputs up to 6 watts. 2½in. diameter, 39/6. All post free.

MOVING COIL P.M. SPEAKERS

3in. and 3½in., 19/6. 5in. | 6½in. | 8in. | 10in. | 12in. | 16/6 | 17/6 | 25/- | 32/6 | 29/6 61 in. with trans..... 21/-7 × 4in. Elliptical..... 19/6 10 × 6in. Elliptical.....

GOODMANS 12in. AUDIOM 50 P.M. SPEAKERS

10 watts. Limited number only. Listed at £6/15/-.

LASKY'S PRICE 97/6 Post free

16 METAL CONE **ENORMOUS SAVING!**

BRAND NEW AND PERFECT

Convert to big picture television at a price you can afford. Note especially that these are not "seconds" but perfect tubes without fault, and supplied in original cartons. Brief specification: 6.3 v. heater, ion trap, 14 Kv. E.H.T., wide angle 70 deg., standard 38 mm. decel hose mounts for and defect of the second standard s

neck, duodecal base, magnetic focus and deflection.

Maximum length 17 lin. Gives large 11 × 14 lin. black and white picture. GUARANTEED BY US FOR 3 MONTHS.

Full data, connections and suggested time bases supplied with every tube.

LISTED AT £23.9.10 LASKY'S PRICE £8.9.6

Carr. and Insur. 22/6 extra.

Masks, Anti-Corona, Bases and Ion Traps available.

FEW ONL ITIN. C.R. TUBEL

Type C17FM, rectangular, aluminised, 6.3 heater. Brand new and unused.

LASKY'S £14.19.6

Also, 14in. at £12/19/6. Carr. and ins. 22/6. Carr.

TRANSISTORS

Special Offer. Junction type suitable for use in local station receivers, amplifiers and pre-amplifiers, etc.

Each 10/-Post free.

MULLARD TRANSISTORS

OC70, 21/-. OC71, 24/-. OC72, 30/-

> BRIMAR TRANSISTORS

TS1, 18/-, TS2, 21/-, TS3, 24/-, TP1 or TP2, 40/-

TRANSCRIPTION TURNTABLES

by Lenco, Garrard, Collaro

RUSS RECEIVERS

Available on Easy Terms. In original wood transit cases. Used, Grade 1, £9/19/6. Used, Grade 2, £7/19/6. Carr. 12/6.

Power Pack and Output Stage with 61in. Speaker, 5 gns.



FAMOUS "912" AMPLIFIER AT BARGAIN PRICE

A high fidelity radio and record Amplifier based on the 912 circuit of the G.E.C. with the following controls: Volume, Bass, Treble, Treble Slope, Presence. PERFORMANCE

PERFORMANCE
Power output: 12 watts. Peak, 15 watts. Sensitivity: 100 millivolts for 12 watts. Noise and hum level: —85 db, on 12 watts. Freq. Response: ±1 db. 30 cps. to 25 kc/s. Distortion: 2nd Harmonic—7 watts output 0.1%, 10 watts 0.14%, 12 watts 0.2%.

Negative Feedback Applied: 12 db. Output Impedances: 3.75 and 16 ohms. Valve line-up: Z729, B309, two N709

LASKY'S

16 GNS. PRICE

Carr. extra. Demonstrations at Tottenham Court Road Full details on request.

* LASKY'S ANNOUNCE A PORTABLE GRAM AMPLIFIER KIT

Of very small dimensions and suitable for any type of mains operated portable Record Player. All brand new components, latest circuit technique. The price of the Kit, complete with valves, rectifier and 6 x 4in. elliptical speaker, will be under £4.

FILAMENT TRANSFORMERS

All 200-250 v. 50 c.p.s. prim	arv.
finest quality, fully guarant	eed.
6.3 v. 1.5 amp	
6.3 v. 3 amp	
6.3 v. 1 amp	4/6
0-30 v. 2 amp, tapped voltages 1	9/6

MAKERS' SURPLUS TV COMPONENT BARGAINS

	WIDE ANGLE 38 mm.	
	Line E.H.T. trans., terrox-cube	OF.
١	Line E.H.T. trans., ferrox-cube core, 9-16 kV	25/-
	trame	25/-
	Ferrox-cube cored Scanning Coils and Line Output Trans., 10-15 kV, EY51 winding. Line Trans.	
l	incorporates width and linearity control. Complete with circuit	
ı	diagram the pair	50/-
	Frame Output Transformer	6/6
l	frame	17/6
l	Frame or line blocking osc. trans-	4.00
ŀ	Focus Magnets Ferrox-dure	4/6
	P.M. Focus Magnets, Iron Cored	19/ 6 19/ 6
ı	Duomag Focalisers	22/6
	300 m/a. Smoothing Chokes	15/-
	Electromagnetic focus coil with	
	combined scan colls	25/-
	STANDARD 35 mm.	
	Line Output Transformers. No	
	E.H.T. Line Output Transformers 6.9 kV.	12/6
	Line Output Transformers 6.9 kV.	
	E.H.T. and 6.3 v. winding. Ferrox-cube	19/6
	Scanning coils. Low imp. line and	19/0
	frame	12/6
	Ditto hy Igranic	14/6
	Frame or line blocking oscillator	
	transformer	4/6
	Frame output transformer Focus Magnets:	7/6
	Without Vernier	12/6
	With Vernier	17/6
	Focus Coils, Electro-magnetic	12/6
	200 m/a. Smoothing Chokes	10/6

LASKY'S FOR **VALVES** 20,000 IN STOCK

Here are a vew examples of brand new surplus and imported valves:

	o t				
EB91 EB41 EABC8 EAF42	7/6 7/6 10/-	EV41 EF80 EF85 EF86	10/6 10/6 10/6 12/6	EY51 EC84 EY86 EZ40	12/6 11/6 14/6 8/6
EBC41	10/-	EF89	10/-	EZ80 PCF82	8/6
ECC85 ECC84	10/- 15/-	6K8 6V6	10/6 8/6	PCC84	12/6 12/6
ECC83	9/-	6K7	5/6	PL81	13/6
ECC82	8/-	607	10/6	PL82	10/6
ECC81	9/-	6B7	6/8	PL83	11/6
12AT7	8/6	5Z4	9/6	PYS0	10/6
12AU7	8/6	DAF9	6 10/-	6AT6	7/6
12AX7	9/6	DL96	10/-	6AT7	7/8
ECF82		DK96	10/-	185	7/6
ECH42		DF96	10/-	384	7/6
ECH8		Set of		1T4	7/8
ECL80	11/6	DM70	9/-	IR5	7/6

Also full stocks of B.V.A. Valves and C.B. Tubes at the new lower list prices. WRITE FOR COMPLETE LIST

Full details on request,

DATA BOOK and shopping list, 1/6 post free.

H.P. TERMS AVAILABLE Write stating requirements.

BAND III AERIALS. All types, outdoor or indoor, also Diplexes, Crossover Boxes, Co-axial Plugs, Socket and Cable.

TWO ADDRESSES FOR PERSONAL CALLERS
OPEN ALL DAY SATURDAY EARLY CLOSING: THU EARLY CLOSING : THURSDAY

42 TOTTENHAM COURT ROAD, W.1.

Nearest Station: Goodge Street, MUSeum 2605

370 HARROW ROAD. PADDINGTON, W.9.

(Opposite Paddington Hospital) LAD 4075 and CUN 1979

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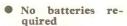


LASKY'S (HARROW RD.) LTD.

There is always a fine selection of equipment at

A room - to - room telephone . . .

Ideal for two-way conversation, house-to-garage or internal communication.



No soldering required

Just connect it up and it works

The sets consist of 2 high-quality microphone/receivers (new and boxed) and 15 yards of twin wire,

> COMPLETE FOR 8/6 plus 1/- postage



INVERTERS

Miniature 3-phase (ex-compass unit) 24V input with 17V 3-phase, 400 c/s output. These have been used by model makers as motors and are known as the "5/- Motor." Will run quite successfully on 12 volts. 5/- plus 2/- p.p.



AN/APN.1 TRANSDUCER

This Unit consists of Magnet, and Coil which is attached to an aluminium diaphragm suspended freely and perforated to prevent air damping. Mounted on a Ceramic cover which sits over the diaphragm is a form of 2-Gang capacitor which has a swing from 10-50 pF.

The above unit is used as part of Wobbulator described on page 252 of the June "Wireless World." PRICE 7/6 p.p.

RECTIFIERS

Chassis cooled, brand new, 125 volt, 80 mA., 4/9 p.p.; 250 volts, 50 mA.

BATTERY CHARGING LEADS

2 yds. of cab tyre twin cable, and 2 large crocodile clips; new and boxed. 3/- p.p.

HEATER TRANSFORMERS

6.3 volt, 1½ amp. Brand new, 6/6 each plus 1/- p.p.

THROAT MICROPHONES

Type T30. U.S. Manufacture. Complete with elastic strap. Lead terminating at 2-pin plug PL.291, and socket JJ-048. New and boxed, 3/- each, post paid.

SMALL MAINS TRANSFORMERS

Input 230 volt 50 cycles, output 250 volt 40 mA., 6.3 volt 1.5 amp. Size 3.9in. \times 2.4in. \times 2in. Ideal for TV converters. Price 12/6 each, plus 1/- p.p.

CHARGER TRANSFORMERS

For 6 or 12 volt. 230 volt 50 cycles input, 9 and 17 volt 3 amp. output. Price 15/6 each, plus 1/- p.p.

TRANSMITTER Type T1131-L

Frequency 100 to 156 Mc/s. Output 50 W. Crystal controlled. 200-240 v., 50 c.p.s. Power supply. Housed in 6ft. standard on 19in. rack. In new condition complete with valves.

Send for full details.

MAINS POWER UNIT Type 234

(For use with Receiver R1392) Double Smoothed 200-250 v. 50c Input. 240 V. 100 mA. 6.3 at 6 amps. with Volt Meter reading input and output voltages. Size: 19in. × 10in. × 6½in. Standard Rack Mounting. Price £4/10/each, plus 7/6 carriage.



BENDIX TRANSMITTERS

TYPE T.A. 12B Master oscillator type transmitter. 4 channel 40 W. operation provide telephone, CW or MCW in frequency ranges of 300-600 kc/s, 3-4.8 Mc/s, 4-6.4 Mc/s, 4.37-7 Mc/s. Each of the 4 channels has its own oscillator and uses a 12.SK.7. The IPA stage consists of an 807, while the PA is two 807s in parallel. Size 104in. × 64in. × 154in. Price £3/15/-, plus 10/- carr.

2in. MAGSLIPS

50 V. 50 cycle transmitter and receiver units. Accurate Guaranteed good working order, 35/- a pair, plus 3/- p.p. Accurate to 1/10th deg.

STUD STITCHES

20 segment 5/16in. studs, base 5in. square with handle and housing. New and boxed. 5/- each, plus 1/6 p.p.

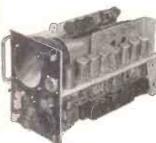
SPECIAL OFFER

MALLORY VIBRATOR PACKS

12 volt, 150 volt 40 mA. Brand new and boxed, size 5½in. × 5½in. × 3in., 12/6 each p.p.

TYPE 62A INDICATORS

Ideal for conversion to oscilloscopes, T.V. units, etc. Containing VCR.97, 12 VR.91 (EF.50), 2 VR.54 (EB.34), 3 VR.92 (EA.50), 4 CV.118 (SP.61). Slow-motion dial, 13 Pots and scores of useful components. Size 8½ × 11½ × 18in. In wooden packing case, £3, carriage 7/6.



CATHODE RAY TUBE TYPE 3.BP.I.

With Mumetal screen and base. 3in. short persistence tube. 2./-plus 2/6 p.p.

POST OFFICE COUNTERS

500 ohm, 4 figure, no reset; size $5 \times 1\frac{1}{2} \times 1$ in. 5/- each, p.p.

EARPIECES

2,000 ohm C.H.R. or balanced armature type, low resistance single units 3/6 each, plus 6d. p.p.

INDICATOR LAMPS

American panel type complete with 6V bulbs in set of 4, 3 green jewels and 1 red jewel, 10/6 post paid.

All these fine offers are on display at



PROOPS BROS. LTD. -The Walk-around Shop

R.F. UNITS

R.F.24 20-30 Mc/s. Switched Tuning. Valved 9/6 each.

R.F.25 40-50 Mc/s. Switched Tuning. Valved, 9/6 each

Packing and postage 3/- each.



CR.300/1 RECEIVER & POWER SUPPLIES

Available for callers only.

2 METRE RECEIVER Type R1392

Air Tested

15 Valve Superhet

Frequency 95-150 Mc/s

(2 to 3 metres)

Valve line-up: 1st and 2nd R.F. Amp. VR.136 (EF.54), 1st Local Oscillator VR.65 (SP.61), 2 Oscillator Multipliers VR.136 (EF.54). 3 I.F. Amp. VR.53 (EF.39). A.G.C. 6Q7. Output 6J5. Muting

VR.92 (EA.50). Noise Limiter VR.92 (EA.50). B.F.O. 6J7. Mixer VR.136 (EF.54). De Mod. 6Q7.

Slow motion tuning, normally crystal controlled, or tunable over 95-150 Mc/s. Power supply required: 240-250 volts at 80 mA. 6.3 volts at 4 amp. Size 19in. × 10in. × 10in. Standard Rack Mounting.

Complete with valves and circuit diagram, checked and £6/19/6 Air Tested. Packing and carriage 17/6, 10/- returnable on

APQ.2. RADAR/JAMMING UNIT

Freq. 450-710 Mc/s. Containing 931a Photo Multiplier Cell complete with resistance network and light proof box. Wide band amplifier 2 6AC7. 1 6AG7. 2 388a. This unit is similar to the A.P.Q9 Jamming Unit. Brand new £5 plus 10/- carriage.

MORSE SIGNALLING LAMPS

(Aldis type) 5in. dia. with sighting arrangement, 2 handles, keying switch, and 2 yards cable. In wood carrying case, 10/- plus 3/- p.p.

MINIATURE I.F. STRIPS

Size 103 × 21 × 3in. Frequency 9.72 Mc/s. 2 EF.92s and 1 EF.91 I.F. amps. EB.91. DET/ AGC. EF.91 AGC. Amp. and EF.91 Limiter. Circuit supplied.

Price 8/- less valves. Post paid.

BUZZERS

6 volt A.C. with tone adjuster, size 2 × 1 × 2½in., 4/- p.p.

BOOST GAUGES

2in. dia.; suitable after minor adjustment as car induction manifold meter. 2/6 p.p.

RIII5 RECEIVERS

Air Tested, in good secondhand condition. Price £6/5/-, plus 10/packing and carriage.

3 cm. TEST SET

TYPE 263

Containing transmission type w/meter complete with detector unit 9280-9480 Mc/s, attenuator unit, 2 coaxial to waveguide feeders, impedance matching unit. medium power dummy load, standing wave indicator with lock using CV.263 indicator valve, metered indicator unit, various connectors. Suitable for testing medium and low power radar installations Price £20 carriage paid.



WAVEMETER TYPE W.1310

Coverage 155 to 230 Mc/s. continuous, complete with Test Prod. Input 230 v. 50 cycles. New condition, £3/10/-, plus 7/6 carr.

BLOCK CONDENSERS

8 mfd. 600 v. W., 5/6 each, post paid. 4 mfd. 400 v. W., 4/- each, post paid.

DESYNN TYPE Antenna or Beam position indication

This comprises a Transmitter unit and Indicator which will operate on 12 or 24 volts D.C. and will indicate with instantaneous and smooth pointer movement. The Transmitter is a specially designed potentiometer and will operate the Receiver on a simple three-wire system and the receiver in this instance is calibrated in Gallons but dial could be easily altered to indicate a 360 Deg. sweep. Transmitter and Receiver with full instructions. Price 12/6 post paid.

I.F. AMPLIFIER UNIT

460 Kc/s with IT4. Brand New and Boxed. Fully Screened in plug-in Box. Size 2½in. × 1in. × 4½in.

Price, with circuit, 10/- ea., plus 1/- p.p.



RADIO ALTITUDE METERS

5 mA. Basic movement, 3in. dia. circ. scale with approx. 300 deg. sweep. 6/- each, plus 2/- p.p.

TWIN COUNTERS

(Gallons gone) 24V, reading 4 figures and reset contained in housing, size 4in. dia. by 5in. long, 15/- plus 2/- p.p.

NICKEL IRON CELLS

1.2 volt, size 3½in. × 2¾in. × 1in., unfilled 5/- each, plus 1/- p.p.

OCTAL PLUGS

(Bulgin bakelite type), 2/6 each p.p.

POWER UNIT Type 173

24 Volt D.C. Input, 120V, 60 mA. Output. Containing Vibrator Transformer, 12 Volt Vibrator, two 120 Volt Selenium Rectifiers. Chokes and Condensers. Size 10 lin. × 6in. × 3in. Price 12/6 post paid.



NOTE: Carriage prices quoted apply only to England and Wales.

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NOTE: Orders and Enquiries to Dept. "W". Shop hours 9 a.m. to 6 p.m.—Thurs.: 9 a.m. to 1 p.m. OPEN ALL DAY SATURDAY. Telephone: LANgham 0141

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12A TOTTENHAM ST. NEAR GOODGE STREET STATION (OPPOSITE HEALES)

LONDON W.1 LTD

PHONE-LANGHAM 7391-2

BUSINESS-9-6 HOURS



HEAD-PHONES DLR No. 2 Low Res. Balanced Arm_turas. 10/6 per

. & P. 1/6.

SPECIAL OFFER o. 5 BALANCE ARMATURE Brand new. Price 3/6 each or No. INSETS. f2 per doz.

These can be put to many uses, i.e. microphones, intercom., etc.

25 ohm 25 w. wire wound POTS (U.S.A.). Price 4/6 ea. Post and packing 9d.

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Single phase motors suitable for tape re-corders, radiograms, workshops, etc., etc. Has many uses. Reversible 200-230 v., versible 200-230 v., 5in. oz torque 1,400 r.p.m. Capactor start. Weight 41b. Length overall 5in. spindle both ends. \$\frac{1}{2}\text{in.}\text{Yin.}\text{Price.}\text{Price.}\text{Price.}\text{Price.}\text{Price.}\text{Price.}\text{Price.}\text{Price.}\text{True.}\text{Vin.



COLLINS CHOKE. 8 Henrys 160 ohms impedance 100 m.a., completely shrouded. Price 9/- each. Post and packing 2/6.

TUNEON INDICATOR NEON LAMPS. 200/ G.E.C. Worked in series with 300 K. res. Preach or 24/- per doz. Post and packing 6d. each. 200/260

AIRCRAFT LANDING BULBS. 10 wired in series, ideal for some photography. Total wattage output 2,000 w. Price 4/6 each or 48/- per doz. Post and packing 1/- each

PILOT LAMP HOLDERS. M.B.C. fitting U.S.A. Similar to Bulgin type. Price 30/- per doz. or 2/9 each.

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American Bulbs 6-8 v. .25 amp., M.Bc., 6/- per dozen. 12-16 v. .1 amp., M.Bc., 6/- per dozen. 12-16 v. . 7/6 per dozen. Post free.

807 VALVES Brand new. Individually boxed. 5/- ea P. & P. 6d. Special prices for quantities.



27 v. input output 7,000 r.p.m. at 0.63 amp. 12 v. input. output 2.800 r.p.m. at 0.57 amp. 6 v. input. output put, output 380 r.p.m. at 0.5 amp. Price 17/6. P. & P. 2/-.

TYPE 3,000 POST OFFICE RELAYS

Surplus to Ministry Requirements, the following are a few of the relays which we can supply ex stock We build relays to your specification and would be pleased to receive enquiries for prompt quotation and delivery. Prototypes 7/14 days.

Table 1	20	E L
Coil Resistance	Price	Each 8/-
6.4	2M	
100	2M, IM.P.	12/-
i00	3M	10/6
100	4B.P.	22/-
200 1±in. H.S.	20.	11/6
200 lain. H.S.	4C.	14/6
200	IC.P.	12/-
200 + 200	4C.	12/-
300 Igin. T.S.	2M, IC, IC.P.	20/-
310 lin. T.S.	2K.	9/-
335 ½in, H.S.	1B.P., 1B.	12/6
500 Adjustable Residual	6C.	16/6
500 Anode trip relay		12/6
500	2M, 2C.	12/6
500	211.	9/6
500	1B.T., 3M.T.	14/6
500 ! ½ in, T.S.	2K.	13/6
500	4C.P.	32/6
500	414.T.	13/6
500 + 500 ½in, H,S.	4C.	15/-
500+500	IM, IM.P.	13/6
765	3M, 3B.	13/6
1,000	IM.P.	13/6
1,000		Price
1.000	on applic	
1,000		15/-
1,000		13/6
1,000	3C.P., 3K.P.	
1 000	on applic	ation
1,000	2M, 1B, 1C, 2C.P.	25/6
1,000	2B, 2M.	13/6
1,000	3M.T.	13/6
1,000	IB, IM.	11/-
1,000	1M, 1B.	11/-
2.000	2M.T.	13/6
2,000	IM.P.	15/6
2,000	2C.	13/6
4,000	2M.	14/6
6,500	IC.	17/6
20.000	6C.	25/-
For orders under £2 ple		,
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SIEMENS HIGH SPEED RELAYS 250 ohm. double coil. Price 8/6 each.



250 watts at 25 amps. Resistance 0.4 ohms. Suitable for charging Both brand new. Price 12/6.

I ohm at 125 watts

Post 3/-

ROTARY TRANSFORMER TYPE 47



20 watts, 9 volt input, gives 450 v. out at 50 mA. Spindle both ends. Brand new and boxed. Price 35/- including post and packing.

AMERICANI MICA CONDENCERS

PAT	TERICAIN	MICA COI	ADI	1425	14.3
Descr	iption	F	er	doz.	Each
.001	350 v.	V.D.C. Farado		3/4	4d.
.01	1,000 v.	V.D.C. Corne Dubilier	all	10/6	1/1
.001	1,200 v.	V.D.C. Farado	n	10/6	1/1
.01	1,200 v.	V.D.C. Farado	n	12/-	1/3
.0001	2,500 v.	V.D.C. Farado	n	12/-	1/3
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Post and packing 1/- per doz. or 3d. each. Please enquire for sizes not stated as we have many in stock.

ROTARY TRANSFORMERS
Delivery Ex Stock. Quotations on application



H.T.31 Input 11.5 Output 250 v. at 125 mA.

H.T.32 Input 11.5 v. Output 490 v. at 65 mA.

H.T. 11, 11.5v. in., out 365 v.-310 v., 30 mA. Fully tropicalised if required.

MICROPHONE ADAPTORS. In 3½ ×3½ ×1½in. polished steel case complete with 6-pin interior Jones plug and socket. Price 5/-. Post and packing 1/6.

PHILLIPS CONCENTRIC TRIMMERS. 2-8 P.F. Price per doz. 6/6, and 3-30 PF. Price per doz. 8/8. Post and packing 1/- per doz.

HEADPHONES. Type H.F.38. American lightweights-Western Electric. Inc. lead with P.L.354 plug. Price 9/- inc. post and packing.

BELLING LEE INSULATED TERMINALS. With caramot washer. Prioe 1/6 each or 15/- per doz. Post and packing 1/- per doz.

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Dulcie Kenton, etc. Highly pollshed walnut. Price 12/6 each. Post and packing 2/6.



Price 37/6 ca. P. & P. 2/-. D.C. Input 27 volts at 1.75 amps. D.C. Output 285 volts .075 amps. Can be supplied in 12 volt at extra cost.

PLEASE SEND FOR LISTS. All the above special prices quoted for quantities. Please call and see our varied stock,

MAINS TRANSFORMERS

Primary, 200-250 v. P. & P. 2/-. 300-0-300 100 mA., 6 v. 3 amp., 5 v. 2 amp., 22/6.

Semi-shrouded drop-through 380-0-380 v., 120 mA., 6.3 v. 4 amp. 5 v. 2.5 amp., 22/6.

Drop thro' 350-0-350 v. 70 2.5 amp. 5 v. 2 amp., 14/6. . 70 mA., 6 v.

Chassis mounting or drop thro'. Pri. 110-150 v. Sec. 350-0-350, 250 mA., 6.3 v. 7 amp., 6.3 v. 0.5 amp., 5 v. C.T., 0.5 amp. 4 v. 3 amp. P. & P. 3/6. 32/6.

Chassis mounted and fully shrouded, 80 mA. 6 v. 3 amp., 5 v. 2 amp., 14/6. Drop thro' 270-0-270 60 mA., 6 v. 3 amp., 11/6.

250 v. 350 mA., 6.3 v. 4 a., twice 2 v. 2 a., 19/6.

Auto-trans. Output 200-250 H.T. 500 v. 250 mA., 6 v. 4 a., twice, 2 v. 500 v. 250 2 a., 19/6.

Auto-trans. Input 200-250. H.T. 350 v. 350 mA. Separate L.T. 6.3 v. 7 a., 6.3 v. 1½ amp., 5 v. 3 amp., 25/-. P. & P. 3/-.

F. & F. 3/-.

Mains transformer, fully impregnated.

Input 210, 220, 230, 240. Sec. 350-0-350
100 mA, with separate heater-transformer.

Pri. 210, 220, 230, 240 sec.
6.3 v. 2 amp., 43 amp., 4 y.
6 amp., and 5 v. 2 amp., 30/-. P. & P.

350-0-350 75 mA, 6.3 v, 3 a, tap 4 v-6.3 v. 1 a., 13/6.

500-0-500 125 mA. 4 v. C.T. 4 a., 4 v. C.T. 4 a., 4 v. C.T. 2.5 a., 27/6.

500-0-500 250 mA. 4 v. C.T. 4 a., 4 v. C.T. 5 a., 4 v. C.T. 4 a., 39/6.

R. & T.V. Energised 6½in. Speaker, with O.P. trans. field coil. 175 ohm, 9/6. P. & P. 2/6.

R. & A. 61in. M.E. Speaker, with O.P. trans. field 440 ohms, 10/6. P. & P. 2/6.

Volume Controls. Long spindles, less switch, 50K, 500K, 1 meg., 2/6 each. P. & P. 3d.

Volume Controls. Long spindle and switch, \(\frac{1}{2}, \frac{1}{2}, 1 \) and 2 meg., \(4/\)- each. 10K and 50K, \(3/\)6 each. \(\frac{1}{2} \) and 1 meg., long spindle, double pole switch, miniature, \(5/\)-. P. & P. 3d. each.

Trimmers. 5-40 pf., 5d. 10-110, 10-250, 10-450 pf., 10d.

Twin Gang .0005 Tuning Condenser 5/-. With trimmers, 7/6.

Twin Gang .0005, with feet, size $3\frac{1}{4}$ × $3 \times 1\frac{1}{2}$ in., 6/6. 3-gang .0005, with feet, size $4\frac{3}{4}\times 3\times 1\frac{1}{2}$ in., 7/6.

T.V. Cois, moulded former, iron-cored wound for re-winding purposes only. Ali-can 1½ × 1½in., 1/- each. 2 iron-core Ali-can 2½ × ½in., 1/6 each. The above coil formers a suitable for the "Wireless World" F.M. tuner.

Used Metal Rectifier, 250 v. 150 mA., 6/6. Metal Rectifier, 250 v. 45 mA., 6/6.

Metal Rectifier, RM2, 125 v. 100 mA. 3/6.

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3-SPEED AUTOMATIC MIXER CHANGER

Will take 10 records, 7in., 10in. or 12in Mixed, turnover crystal head, brand new, current model. A.C. mains 200/250 v. (list price £14/10/-).

£7 - 19 - 6 P. & P. 3/6.

COMMERCIAL TELEVISION-CONVERTER

SUITABLE ANY T.V. using lower side band NO ALTERATIONS TO SET

Complete with bullt-in power supply, 230-250 v. A.C. mains. Case 53in. long, 3in. wide, 4in. high. Incorporating gain control and band switch.

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Plus Post & Packing 2/6.



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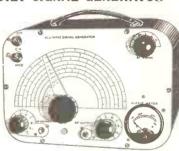


sing 211. Moving con interact, scale candidated in A.C./D.C. 0-10, o-100 and 0-500. Milliamps 0-10, 0-100 ohms 0-10,000. Front panel, range switch, wire wound pot (for ohms zero setting), two toggle switches, resistors and meter Point-to-Point wiring diagram 1/-. Free with complete kit.

Complete in case, grey 19/6 P. & P. 1/6.

COMPLETELY BUILT SIGNAL GENERATOR

Coverage 120 Kc/s.-230 Kc/s., 300 Kc/s.-900 Kc/s., 900 Kc/s.-2.75 Mc/s., 2.75 Mc/s.-8.5 Mc/s., 8 Mc/s.-28 Mc/s., 16 Mc/s.-56 Mc/s., 24 Mc/s.-84 Mc/s. Metal Mc/n. 94 Mc/n. 94 Mc/n. Metal case 10 n. x. 6½ n. x 4½ n. x 4½ n. s. 6½ n. x 5½ n. s. 6½ n. x 5½ n. g. x 2½ n. x 2½ n. g. x 2½ n. x output and moving coil output meter. Grey hammer finish case and white panel. Accuracy plus or minus 2%. \$4/19/6. or 34/- deposit and 3 monthly payments 25/*. P. & P. 4/6 extra.



T.R.F. KIT IN PLASTIC CABINET

3 valve plus metal rectifier, A.C. mains 200-250 v. Medium and long waves. In pastel blue or brown. Valve line-up: 2 VR658 and VT52. Size 15\frac{1}{2}\text{in. long by 9in. high by 7in. deep.}

£3-19-6 P. & P. 4/8

A point-to-point wiring diagram, 1/6. Free with complete kit.

All parts supplied separately.

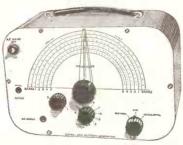
SIGNAL & PATTERN GENERATOR

Coverage 7.6 Mc/s-210 Mc/s. in five bands, all on fundamentals, slow motion tuning, audio output, 8 vertical and hofizontal bars, logging scale. In grey hammer finished case with carrying handle. Accuracy ± 1%.
A.C. mains 200-250 v.

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P. & P 5/6.

Or £3 deposit. P. & P. 5/6 and 3 payments of 30/-.



RADIO AND T.V. COMPONENTS (ACTON) LTD. 23 ACTON HIGH STREET, LONDON, W.3

GOODS NOT DESPATCHED WHERE CUSTOMS DECLARATION IS APPLICABLE Terms of Business: Cash with order. Where post and packing charge is not stated please add 1/6 up to 10/-, 2/- up to £1, and 2/6 up to £2. All enquiries S.A.E., lists

Germanium Crystal Diode, 1/6, post

Line O.P. Transformer in aluminium can mounted in rubber, 12/6. Line and E.H. T. Transformer, 14 Kv., using ferrocart core, complete with line and width control, and corona shelds US? rectifier winding, 35/-.

Line and E.H.T. Transformers, 9 Kv. using ferrocart core, complete with built-in line and width control. Mounted on small all-chassis. Overall size $4\frac{3}{4} \times 1\frac{1}{4}$ in. EV51 rec. winding, 27/6. Scan coils, low line low impedance frame, complete with frame transformer to match above 27/8. P. & P. 2/-.

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As above, but complete with line and frame blocking transformers, 5 Henry 25 mA. choke, 100 mfd. and 150 mfd. 250 wkg. 380 mA. A.C. ripple, \$2/9/6. P. & P. 3/-.

P.M. Speaker, 63 in. closed field, 18/6. 8 in. closed field, 20/6. 10 in. closed field, 25/-. 12 in. closed field, 25/-. P. & P. on each 2/-

Extension Speaker, in polished walnut complete with Sin. P.M. P. & P. 3/-. 24/8

COLLARO **RC54**

3-speed automatic changer, current model. Brand new. 10 records mixed. Studio "O" pick-up. model. Brand new. mixed. Studio "A.C. mains, 200-250 v.

£7-19-6 P. & P. 5/-.

Standard Wave Change Switches. 4-pole, 3-way, 1/9; 5-pole, 3-way, 1/9; 3-pole, 3 way, 1/9; 9-pole 3-way, 3/6. 3-pole, 3 way, 1/9; 3-pole 3-way, 3/6. Miniature type, long spindle, 3-pole, 4-way, 4-pole 3-way and 4-pole 2-way, 2/6 each. 2-pole 11-way, twin wafer, 5/-; 1-pole 12-way single wafer, 5/-. P. & P. 3d.

Ion Traps for Mullard or English Electric tubes, 5/-, post paid.

Standard 465 Kc. iron-cored I.F.s., 4 × 1½ × 1½in., per pr., 7/6.

1,200tt. High Impedance Recording Tape on plastic spool, 12/6. Plus 1/- P. & P.

Miniature wire ends moulded. 100 pf. 500 pf. and .001, each 7d.

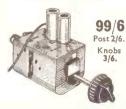
Combined 12in. mask and escutcheon in lightly tinted Perspex. New aspect edged in brown. Fits on front of cabinet, 12/6. As above for 15in. tube, 17/6.

Frame Oscillator Blocking Trans., 4/6. Line Osc. Blocking Trans., 4/6

Wide Angle P.M. Focus Units. Vernier adj. state tube, 15/-.

P.M. Focus Unit for Mullard tubes with vernier adjustment. P. & P. 2/-, 15/-.

FAMOUS MAKE TURRET "TELETUNER"



Covers all Channels, Bands I and 3. Valves used: PCC84, R.F. double triode, cascode R.F. amplifier. PCF80, triode pentode f.c. and mixer. I.F. output 33-38 Mc/s. Easily modified to other I.F. outputs. Full instructions and circuit diagram supplied. Complete with 12 Coil Sets.

16 16

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PAMPHONIC were the first and only company at the last Radio Show to feature Absolute Fidelity equipment fitted neatly into furniture.

All wires, amplifier, gramophone turntable and radio equipment were housed without any alteration whatever in standard G. Plan furniture.

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Absolute Fidelity equipment for fitting in furniture can be selected from the following models:

- Am plifier 1002 with pre-amplifier 1002A control unit High Fidelity, 25-watts output. 28 gns., and pre-amplifier
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Pamphonic	lou	dspė	ake	rs	are
created for					
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perfect ton	al bala	ance.			
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Victor Senior 15 w., 55 gns. Victor Junior 55 gns. 10 w., 35 gns.

TWO OTHER UNITS in the popular Pamphonic range are the Westcott and Pandora record reproducers. The Westcott contemporary in design conte ducers. The Westcott con-temporary in design, price oak finish £49/10/11 and sapele mahogany £50/13/tax paid.

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THE NEW AXIOM ENCLO-SURES built to the specification of GOODMANS.

Completely Fitted comprising 12in. Axiom No. 150 Mk. II. Speaker, The Axiom No. 150 Mk. II. Speaker. The Acoustic Resistance Unit and Cabinet to Messrs. Goodmans specification. Lined and Quilted with lin, cotton felt and constructed of \$\frac{2}{2}in. Weyrock.

Cash price £28/9/6 or £4/4/6 deposit and

9 payments of 58/I monthly. Cabinet only £14/18/6 or £2/5/- deposit and 9 payments of 30/4 monthly. Delivery 12/6 cash or terms.

In oak, walnut or mahogany veneers, finished to required shade.

Also in Corner Cabinets 20/- extra.

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PARABOLIC REFLECTORS up to 9ft. dia. LOUDSPEAKER HORNS, Etc., Etc. POWER **PRESSWORK** 250 to capacity, including Hydraulic ton GENERAL SHEET METAL WORK, ARGON, ARC & OXY-ACETYLENE WELDING

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This well-known R/T Transceiver is offered complete with Valves, High Resistance Headphones, No. 3 Handmike and Instruction Book giving complete details and circuit, contained in strong cabinet. Variable tuning.

Frequency Range: 44.0 to 61 Mc/s. Range approximately: 3 to 8 miles. Power requirements: Standard 120 v. H.T. and 2 v. L.T. Ideal for Civil Defence and communications

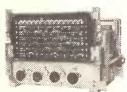
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Calibrated Wavemeter for same 10/- extra.

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16-50 metres short wave. 187-550 metres medium wave. 900-2,000 metres long wave. Flywheel Tuning. Negative Feed Back. Valves 6BE6, 6AT6, 6BW6,

Wave change and Gram. Chassis 11in. x 7½ in. x 8½ in

£9 - 5 - Od. Carr. 5/-.

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Manufactured by well-known manufacturers. ABSOLUTE BARGAIN

GARRARD 3-SPEED AUTO-CHANGER

Plays mixed records. Complete with turn-over Crystal pick-up. Cream & Brown Enamel finish. Brand new in original cartons. (List price £14/13/0.)

£7.19.6 carr. 3/6

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Plays mixed records. Complete with H.G.P. 37 Crystal Pickup. Finished in Hammered Gold.

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SPECIAL REDUCTION FOR SETS OF VA	LVES
1A7GT, IN5GT, 1H5GT, 1A5GT (or 1Q5GT or 3Q5GT)	37/6 Set
10 EF50 (Ex-Brand New Units) 5/+ each	45/- "
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DK96, DF96, DAF96, DL96	32/6
6K8G, 6K7G, 6Q7G, 25A6G, 25Z5 (or 25Z6G)	37/6
12K8GT, 12K7GT, 12Q7GT, 35Z4GT, 35L6GT (or 50L6GT)	37/6
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JUNCTION TYPE (Red-Spot) (P.N.P.)
OFFERED AT LESS THAN HALF-PRICE.

Designed for A.F. application up to 800 Kc/s and are suitable for use in amplifiers, Signal Tracers, Local Station Receivers, Radio Control, Oscillators, Transistor Voltmeters, Baby Alarms, Microphone Pre-Amplifiers, etc.

10/- each.

(Tested and complete with Data & Circuits)

N.B. These Transistors may be used in place of Mullard OC71 or similar Transistors.

Please note that these Red Spot Transistors are ideal for most circuits includ-ing "WW." Pocket Transistor Receiver and Transistor Amplifier. All Tran-sistors are British Manufactured and Guaranteed. Send for Circuits and Data

PRE-SELECTED TRANSISTOR SIX PUSH-PULL PORTABLE SUPERHET

Just switch to your favourite Station. No tuning, no aerial or earth. Pre-select 3 stations. Complete with all components and six Transistors 7×4 Elliptical speaker. Teletron Superhet Coils and I.F.T.s. Powered by $7\frac{1}{2}\times d$ dry battery which lasts for months. I50 Milliwatts output. All the above with Circuits, etc. £9 - 0 - 0 Carr. paid.

Or with Matched Mullard OC72's (200 Milliwatts Output) and 7 x 4 Elliptical High Resistance Speaker 30/- extra.

Suitable Plastic Cabinet easy to assemble 18/6.

Call and hear demonstration model working. Ideal as a car radio.

SPECIAL OFFER

Set of four Transistors including one R.F. Transistor... 42/6 Set of six Transistors including one R.F. Transistor...

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Complete Kit with 2 Transistors, Components, with Circ 42/6

TRANSISTOR SQUARE WAVE GENERATOR

Ideal for signal tracing.
Complete Kit with 2 Transistors, Components and Circuit.
25/-.

62A INDICATOR UNIT

Containing VCR97 with Mu-Metal Screen 21 Valves: 12-EF50, 4-F961, 3-EA50, 2-EB34. Plus Pots., Switches, H.V. Cond., Resistors, Muirhead S/M Dial. Double Deck Chassis and Crystal. BRAND NEW ORIGINAL CASES, 67/6. Carr. free.

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Unit contains VCR517 Cathode Ray Sin. tube, complete with Mn-Metal screen, 3 EF50, 48F91 and 1 5 U4G valves, 9 wirewound volume controls and quantity resistors and condensers. Offered BRAND NEW (less relay) at 67/6. Flus 7/6 carr. "Radio-Constructor" scope ofrcuit included,

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Brand new miniature I.F. Strip size 10\(\frac{2}{3}\)in. × 2\(\frac{1}{3}\)in. × 3\(\frac{1}{3}\)in. high. Valve line-up: 2-EF92 3-EF91 and EB91. With circuit. With valves, 45/- (less valves 8/- Post free). This I.F. Strip is part of above equipment.

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Bendix type, for TA-12, push-pull 807's to plate and screen modulate two 807's in parallel, 15/-. Collins type, 20 watts, 807 to 807, 12/6.

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Complete with 6 valves: 3 12SK7, 1 12K8, 1 12SR7, and 1 12A6. Size 5in. x 5\$in. x 11\$in. deep. In very good condition Less dynamotor. FREE CIRCUIT WITH EACH SET. BC453 (the famous Q5'er), 190-550 Kc/s., 59/6. BC454, 3-6 Mc/s., ... 27/6. NEW, BOXED BCXXX (Trawler band), 15-3 Mc/s., 75/-. COMMAND TRANSMITTERS. Complete with 2 1625 (12 x 807). 1 1676 1 1679 and Crystal

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Consists of 2 valve oscillators (ARPI2's) (one with pitch control), for I or 2 operators (ARPI2's) (one with pitch flas provision for creating a true of the case I2\frac{1}{2}in. x 10in. x 8in. vw. 16lb. Complete with valves, le.ds. 2 keys, 7-way terminal board, circuit and instructions, but less batteries and phones. Wr. 16lb. Complete with valves, le.ds. 2 keys, 7-way terminal board, circuit and instructions, but less batteries and phones. South sets. SNIP, 19/6.

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100 Microamp.
D.C. M/C 2in.
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Of the OBSOLETE Type 3339

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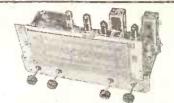
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Send S.A.E. for illustrated leaflet, or 1/3 for 14-page booklet which gives technical information, circuits, etc., and is supplied free with each receiver.

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F.S.D.

50 microamps D.C. 500 microamps D.C.

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METERS SIZE AND TYPE PRICE 2½in. Flush circular 2in. Flush square 2in. Flush square 2½in. Flush circular (blank scale)

500 microamps D.C. 2in. Flush square 1 ma. D.C. 2in. Flush square 10 m.a. D.C. 2½in. Flush square 150 m.a. D.C. 2½in. Flush square 200 m.a. D.C. 2½in. Flush circular 24 amp. D.C. 2½in. Flush circular 20 amp. D.C. 2in. Proj. circular 20 amp. D.C. 2in. Proj. circular 30-0-30 amp. D.C. 2in. Proj. circular 30-0-30 amp. D.C. 2in. Proj. circular 30-0-310 amp. D.C. 2in. Flush circular 30-0-310 amp. D.C. 2in. Flush circular 30-0-310 amp. D.C. 2in. Flush circular 30-0-310 amp. D.C. 2½in. Fl 22/6 10/6 7/6 15/ironin. Proj. circular electro-9/6 2 Kilovolts A.C. ... 2½in. 300 volts D.C. 2in. Flush square

Enquiries invited for types not listed, 7-14 days delivery on "specials".

L.T. HEAVY DUTY TRANSFORMERS. Ex-Admiralty, with 20 v. 50 cycles primary. I. Secondaries 5, 10, 15, 20, 25 30 volts at 5 amps. ONLY 29/6. 2. Secondaries 7, 14, 21, 28 volts at 12 amps. ONLY 42/6. (postage on either 2/9).

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Frequency coverage 16-150 Mc/s. BRAND NEW IN MAKER'S ORIGINAL TRANSIT CASES, with instruction manual. For normal A.C. mains operation. A unique opportunity to acquire Laboratory Equipment at a fraction of original cost. ONLY

159 RECEIVER UNIT. Contains I each valve, types EF50, EAS0, SP61, RL37 and 24 v. selector switch. ONLY

RCA 8in. P.M. SPEAKER, mounted in heavy black crackled metal cabinet with chromium grill, and padded feet.
Size Ilşin. w. × 10şin. h. × 6in. d.
Ideal for use with receivers or as an
extension. BRAND NEW IN
MAKER'S CARTONS. ONLY 45/-.

100 MICROAMPS METERS. 2½in. circular flush mounting. Widely 100 MICROAMPS METERS. 2 jin. circular flush mounting. Widely calibrated scale of 15 divisions marked "yards" which can be rewritten to suit requirements. These movements are almost unobtainable today and being BRAND NEW IN MAKER'S CARTONS are a snip at ONLY 42/6.

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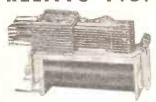
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F.S.D. 100 Microamp 250 ,, (multirange s 500 ,, (scaled 0/15 1 Milliamp 30 ,, 100 ,, 200 ,,	2in. KV)2in. 2in. 2½in. 2½in. 2½in. 2½in.	Type MC/FR MC/FR MC/FR MC/FS MC/FR plug type MC/FS Elliott 5Q/87 MC/FR MC/FR MC/FR MC/FR	Price 50/- 55/- 27/6 18/6 27/6 12/6 12/6
500 ,, 20 Amp.	2½ in. 2½ in.	MC/FR MI/FR	12/6 25/-
25 ,,	2½in	MI/FR DC	7/6
50 ,,	5in.	MI/PR	60/-
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10 ,,	$2\frac{1}{2}$ in.	MCR/FR	30/-
20 ,,	2in.	MC/FS	10/6
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300 ,,	2lin.	MI/FR	25/-
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2,000 volt	$2\frac{1}{2}$ in.	ES/FR	40/-

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TELEPHONES—SOUND POWERED—NO BATTERIES REQUIRED.

Just connect with twin flex for clear speech. Transmitter/receiver units 9/- per pair. Twin flex 44d. yard. Post 1/-.

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Throat Microphones, American surplus. Complete with strap, lead and plug type T30B 3/- set High Resistance Phones, 4,000 ohms. Complete with Jack

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SMALL MAINS TRANSFORMERS
Suitable for
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SPECIFICATION OVERALL SIZE
Primary: 250 v. 60 (20mp Construcc/s. 20mp Construction 3.9 x 2.4 x
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Primary: 200-220-240 v.

Primary: 200-220-240 v.

Secondary: 30 v. 2 amp.

Secondaries: 350-0-350 v. 80 M/A, 0-6.3 v. 4 amp., 0-5 v. 2 amp., both tapped at 4 v., each 19/6

2/- Packing and Post on above trans-

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★ Tuneable over Band III range
★ Single knob channel changing

★ 4-valve circuit
 ★ Hammer-tone bronze finish

NOTE THE PRICE-26/15/-Fully guaranteed against faulty workmanship or materials (other than valves) for 12 months.

The unit uses B.V.A. valves. Guaranteed for 90 days.

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WAVE CHANGE SWITCHES	ETC.	
3 pole, 4 way	2/9 ea.	
4 pole, 3 way	2/9 ea.	
4 pole, 1 way	1/9 ea.	
1 pole, 12 way	2/9 ea.	
2 pole, 6 way	2/9 ea.	
TRF Switch 2 pole Changeover	1/6 ea.	
3 pole, 3 way, 3 bank	1/9 ea.	
2 pole, 5 way, 3 bank	2/- ea.	
4 pole, 2 way, 3 bank	1/6 ea.	
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2 pole, 2 way	1/9 ea.	
Yaxley type, 1 pole, 9 way	1/9 ea.	
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ROTARY SWITCH 4 position, 30 amp. 3/- ea. SPINDLE COUPLERS

Mixed sizes 6d. doz GRID CAPS Octal Push on type 6d. doz. British screened type 3d, ea.

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ALL PM TYPES LESS TRANSFORMER

Waterhouse 5in. unit 17/6 ea. Plessey 6 in. unit . . 18/6 ea. R. & A. 8in. unit . . 18/6 ca. Plessey 12in. unit . . 35/- ea.

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R. & A. 6 in. unit, mains energised, 600 ohms field Plessey Sin. unit, mains energised, 600 ohms field Goodmans or Lectrona Sin. unit with output trans-former 21/6 ea.

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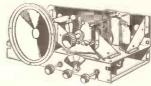
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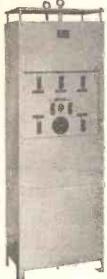
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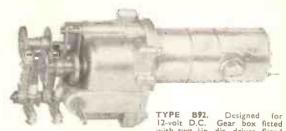
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Completely enclosed slider control 65/-, 300 ohm. I A. Geared drive with control handle 35/-, 500 ohm. 2-0.36 A. Geared drive 27/6, 1100 ohm. 0.4 A. Horizontal sweep. Control 17/6, 100 ohm. 0.4 A. Horizontal sweep. Control 17/6, 100 ohm. 1.6 A. enclosed slider control, 25/-, 2,6 ohm. 8.5 A. Geared drive with handle 25/-, 5.3 ohm. 8 A geared drive 27/6, 7.5 ohm. 4 A. slider control 17/6. O.4 ohm. 25 A. geared control 17/6. I ohm. 12 A. slider control 12/6. 50 ohm. I A. gear control 10/6. 12in. field rheostats 38 ohm. 5.6 A. res. out 2.1 A. res. on 45/-. 95 ohm. 3.3 A. no control but fitted with adjustable tappings 22/6. 850 ohm. 0.55 A. completed enclosed fixed res. 17/6, P.P. on all resistors 2/6, many other types available. Let us know your requirements.

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5/-. Pri. 230 v. sec. 50 v. 30 amps., £6/10/-, carriage 7/6. Pri. 230 v. sec. 50 v. 20 amps., £5/5/-, carriage 7/6. Variable voltage regulator transformers input 230 v. output 57.5 v. to 230 v. in 16 equal steps at 21amps., £10/10/-, carriage 10/-. Occasionally we have limited supplies of constant voltage transformers and variacs; give us a ring we may be able to assist you with your requirements. Sterling Equipment wire PVC stranded copper 7/36, 500 yard drums assorted colours 32/6, postage 2/6. Twin PVC Bell Wire 0.024 23 S.W.G., 220 yard coils. 25/-, nostage 2/-.

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Overall size of motor and gearbox $4\frac{1}{4} \times 2\frac{1}{4} \times 2$ in. Will operate on slightly higher voltage A.C. Mounted on metal box size $5\frac{1}{2} \times 4\frac{1}{2} \times 2\frac{1}{4}$ in which

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TESTERS REQUIRED

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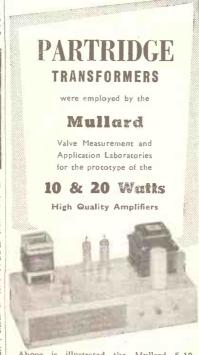
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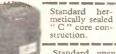
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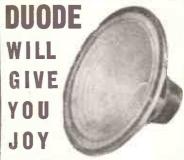
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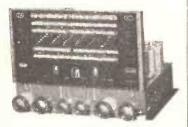
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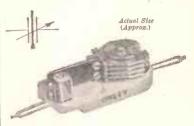
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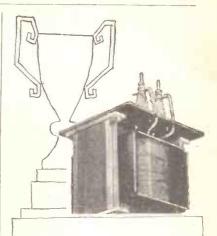
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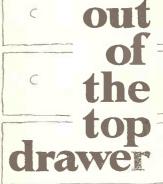
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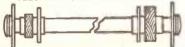
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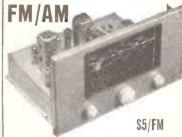
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INDEX TO ADVERTISERS

Altham Radio Co	Page Page	Painton & Co., Ltd.
Alluco, Alu	Gabriel Manufacturing Co., Ltd. 4 Galpins 16 Gee Bros., Radio, Ltd. 14 General Electric Co., Ltd. 29 Gilfillian, R., & Co., Ltd. 16 Gilson, R. F., Ltd. 16 Glaser, L., & Co. 16 Goldring Manufacturing (Gt. Britain) Ltd.	Power Controls, Lt1 2
Anders Electronics, Ltd. 48 Antex 67 Antiference, Ltd. 32 Appointments Vacant 152, 153, 154, 155, 156, Arcolectric Switches, Ltd. 157, 171, 172, 173 Arnestrong Wireless & Television Co., Ltd. 460, 161 Ashworth, H. 161 Aspden, W. 171 Automatic Coli Winder & Electrical Equipment Co., Ltd., The A.W.F. Radio Products, Ltd. 142	Ltd. 4 Goodmans Industries. Ltd. 7 Grampian Reproducers, Ltd. 42, 13 Gray, Arthur, Ltd. 8 Gray, Arthur, Ltd. 8 Grighth, Hansen (Recordings), Ltd. 7 Grundig (Gt. Britain), Ltd. 11	Radio & T.V .Components (Acton), Ltd. 137 Radio Component Specialists
Balun, Ltd	Hall Electric, Ltd.	Radio Striply Co (Leeus), Ltd. 146 Radio Traders, Ltd. 146 RCA, Great Britain, Ltd. 24 Rogers Development Co. 76 Rola Celestion, Ltd. 41 Rollet, H. & Co., Ltd. 170 Rudman, Darlington (Electronics), Ltd. 116 Runbaken 118
Cover ii	Igranic Electric Co., Ltd. 12 Iline & Sons Ltd. 88, 95, 15 Imhof, Alfred, Ltd. 88, 95, 15 International Correspondence Schools	Samsons Surplus Stores 151 Sangamo Weston, Ltd. 110 Savage Transformers, Ltd. 163
British National Radio School 84 British Physical Laboratories 82 British Thomson-Houston Co. Ltd. 114 Brookes Crystals. Ltd. 70 Brown. S. C., Ltd. 68 Bultin. A. F., & Co. Ltd. Edit. 49 Bull. J., & Sons 122 Bullers, Ltd. 90	Jason Motor & Electronic Co	Smith, H. L., & Co., Ltd. 166 Smith, W. H. & Son, Ltd. 25 Smith, W. H. & Son, Ltd. 35 Sonomag, Ltd. 76 Specialist Switches 17 Specto, Ltd. 35
C. & G. Kits 120 Candler System Co. 164 Cathodeon Crystals, Ltd. 27 Cementation (Muffelite), Ltd. 11 Champion Electric Corporation 36 Chapman, C. T. (Reproducers), Ltd. 165 Cirlema Television, Ltd. 20 City Sale & Exchange, Ltd. 89 Classic Electrical Co., Ltd. 86 Ciyne Radio, Ltd. 126 Cosmocord, Ltd. 35 Cossor, A. C., Ltd. 19 Coventry Radio 164	Kolectric, Ltd.	Standard Telephones & Cables, Ltd. 10, 99, 106 8 Stern Radio, Ltd. 128, 128 Stern Transformers, Ltd. 128, 128 Stewart Transformers, Ltd. 88 Sugden, A. R., & Co. (Engineers), Ltd. 128 Sutton Coldfield Electrical Engineers
City Sale & Exchange, Ltd.	Lewis Radio Co. 16 Light Soldering Developments. Ltd. 16 Linear Products, Ltd. 16 Linear J., & Co. 16 Lithgow Electronics. Ltd. 17 Lockwood & Co. (Woodworkers), Ltd. 17 Long Playing Record Library Lowther Mfg. Co. 17	2 Taylor Electrical Co., Ltd. 448 Taylor Tunniciff (Refractories), Ltd. 224 Technical Ceramics, Ltd. 77 Tektronix Inc. 66 Telegraph Condenser Co., Ltd. Cover it Telegraph Construction & Maintenance Co., Ltd. 818 Telegraph Construction & Maintenance Co., Ltd. 818 Telegraph Construction & Maintenance Co., Ltd. 818
Dallmeyer, J. H., Ltd. 167 Dally (Condensers), Ltd. 56 Davies, A., & Co. 170 De La Rue, Thomas & Co. Ltd. 28 Denco (Clacton), Ltd. 52 Dependable Radlo Supplies 136 Direct T.V. Replacements 130 Dixon, L., & Co. 166 Dixon's Electronics 168 Domestic Direct Sales, Ltd. 47 Dubiller Condenser Co. (1925), Ltd. 13	Magnetic Devices, Ltd.	4 .
Direct T.V. Replacements 130	Marconi Instruments, Ltd. Marconi's Wireless Telegraph Co., Ltd. Martin, J. H. 102, 14 Mathew Bros 1	2 Universal Book Co. 17(9 Universal Electrical Instrument Corpn. 14' Universal Electronics 14'
Dubiller Condenser Co. (1925), Ltd. 13 Duke & Co. 150 Dulci Co., Ltd., The 50 Dude Natural Reproducers 160	McMurdo Instruments Co. Ltd. Mercia Enterprises, Ltd. Midland Instrument Co.	0 Valradio, Ltd. 77 2 Verdik Sales, Ltd. 55 0 V.F.S. Wholesale Services, Ltd. 144 8 Vitality Bulbs 14 9 Vortexion. Ltd. 105 5
E.K.E. 171 Electrical & Wireless Supply Co. 142 Electro-Acoustic Developments 166 Electro-Acoustic Industries, Ltd. 45 Electro-Methods, Ltd. 53 "Electronic & Radio Engineer" 79 Electronic Instruments (H'ton) Ltd. 86 Electronic Precision Equipment 112, 113	Mills, W 1 Modern Blook Co 1 Modern Electrics, Ltd. 1 Morganite Resistors Ltd. 1 M.R. Supplies, Ltd. 1 M.S. Recording Co., Ltd 1 Mullard, Ltd. 3, 34, 35, 39, 49, 1 Mullard, Ltd. Cover Multicore Solders, Ltd. Cover Multicore Electric Co., Ltd 1 Murex, Ltd. 1	Whiteley Electrical Co., Ltd 5
Electro-Winds, Ltd. 120 E.M.I. College 110 E.M.I. Electronles, Ltd. 105, 107, 173 E.M.I. Institutes 105, 107, 173 E.M.I. International, Ltd. 16C E.M.I. Studios, Ltd. 148 English Electric Valve Co. Ltd. 15 Enthoven Solders, Ltd. 6, 51 Erie Resistor, Ltd. 167 Eta Tool Co. (Leicester), Ltd. 64 Excel Sound Services, Ltd. 138	Neo Electrical Industries, Ltd. 1 Northern Radto Services	Young C H
Erie Resistor, Ltd. 16 17 Eta Tool Co (Leicester), Ltd. 64 Excel Sound Services, Ltd. 138	Oddie, Bradbury & Cull, Ltd. 1. Osmor Radio Products, Ltd. 1. Oxley Developments Co. 1	00

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in μF.	Volts D.C.	Length	Diameter	Type No.
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4	4	5"	1/8	CE58AA
2	8	5//	1"	CE58A
1	12	5"	1" 8 1" 8	CE58B
0.25	25	5/8	1/8	CE58C
6	3	9 "	-18	CE68AA
10	3	9"	-18	CE68AA
1	25	9 " 16 " 16 " 16 "	-18	CE68C
8	6	11/1	-2	CE69A
4	12	11"	.2	CE69B
32	1.5	11"	1"	CE67
8	15	11"	1"	CE67B

Capacity in μF.	Peak Wkg. Volts D.C.	T.C.C. Type No.			
100	6	CE59AE			
50	12	CE59BE			
25	25	CE59CE			
12	25	CE59C			
5	50	CE59D			
12	50	CE59DE			
6	100	CE59EE			
4	150	CE59FE			
2	200	CE59GE			

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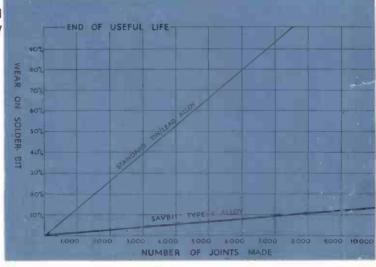
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