MAY 1957 TWO SHILLINGS

# Wireless World

ELECTRONICS
Radio - Television



FORTY-SEVENTH YEAR OF PUBLICATION



# news

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WINDING WIRES

# Wireless World

ELECTRONICS, RADIO, TELEVISION

Managing Editor: HUGH S. POCOCK, M.I.E.E.

Editor:

H. F. SMITH

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MAY 1957

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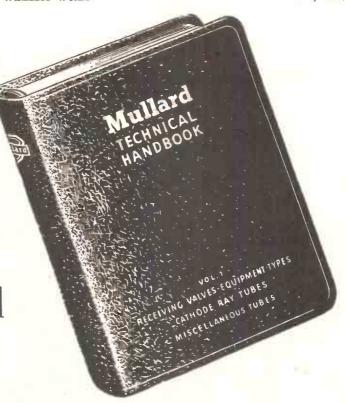
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# Wireless World

## Colour Fiasco

TWO months ago Wireless World expressed fears that the B.B.C. demonstrations of colour television which had recently been given might well have proved too successful. There was a risk that the high quality of the pictures transmitted and received under strictly experimental conditions might have inculcated a widespread idea that the N.T.S.C. system used for the tests was good enough for a regular service for reception in the home. It would now seem we were not emphatic enough in urging that a decision to adopt the system for this country would be disastrous.

During the last few weeks many reports have come in from British observers of the highest competence on the failure of colour television in America. With singular unanimity, all the reports coming to our notice tell the same doleful story; technically, economically and industrially, the N.T.S.C. system is failing to live up to the high expectations expressed when it was first introduced. Indeed, there now seems to be a widespread lack of enthusiasm for colour in the U.S.A., and the reported change in attitude of R.C.A. appears to be particularly significant. Some views of British observers are summarized on p. 205 of this issue.

In spite of the growing tale of woe from America there is still a school of thought in this country which says, in effect, "Admittedly the N.T.S.C. system may have its weaknesses, but perhaps they can be overcome. In any case, nothing better offers itself at present; unless we adopt it there is no possibility of starting a British colour service in the foreseeable future." That attitude seems to represent an attitude of despair: Wireless World, resisting the temptation to make the vulgar retort "So what?" will merely offer the quotation: "The lesson of history is that mankind learns nothing from history."

That is not to say the B.B.C. experimental colour transmissions should cease; still less that research on the general problems of colour television should not be pressed forward as actively as national resources will allow.

We must go on trying to find basically new methods. But, to start even a restricted and experimental public service of regular N.T.S.C. transmissions at the present state of development would surely be a deplorable error.

The Television Advisory Committee is expected to issue a report before very long; it will be surprising—and disappointing—if the Committee does not reach the conclusion that further basic development is needed before any specific recommendation can be made on the colour system to be adopted for Great Britain.

# Editorship of "Wireless World"

THIS intrusion on a page usually reserved for the Editor's comment is explained by saying that it is now the Editor himself who is to be the subject of comment.

The present Editor, H. F. Smith, is vacating the editorial chair in May after 46 years in radio and 32 years on *Wireless World*. For over half that period he has been Editor and it may be said that since 1940 the journal has revolved around him as its axis.

This is a long span of service on a technical journal of any kind, and it is noteworthy that in our particular sphere the period covered has seen greater scientific progress and technological development than has ever been witnessed before in any branch of science.

To have conducted Wireless World during such a time with so much distinction is in itself a sufficient tribute to the retiring Editor, but we know that in addition his personality and his readiness to share his experience and knowledge with others has gained him a multitude of friends all over the world.

It is at his own wish that he is relinquishing the editorship on attaining the normal retiring age, but happily his connection with Wireless World is not to be abruptly severed, and he has been persuaded to continue for a time in a consulting capacity. He is to be succeeded as Editor by F. L. Devereux, who has a long and distinguished record of 33 years with Wireless World. H.S.P.

# French Components Show

HE radio exhibition held annually in Paris under the impressive title "Salon National des Fabricants de Piecès Détachées Radio, Accessoires, Tubes Electroniques et Appareils de Mesures," embraced a far wider field than hitherto and thus afforded an opportunity to assess the progress of development of a large section of the French radio and electronics industries.

So far as components are concerned the trends are very similar to those in Great Britain. Considerable progress has been made during the past year in the manufacture and application of transistors and several firms are now producing transistorized broadcast receivers, as typified by the C.S.F. "Translitor." This company also showed transistor power supply units, interchangeable with the normal batteries, for

military "Handy-Talkie" sets.

An interesting application for transistors was shown by Teppaz in the form of an a.c./battery record player. It has an 8-V synchronous motor, normally operated from the electric supply mains through a step-down transformer. For portable operation the 50-c/s supply for the motor is provided by a transistor oscillator taking d.c. power from a battery and using the motor windings for coils.

A number of new semi-conductor devices were shown by the French Thompson-Houston Company; one was a 2.5-W a.f. power transistor, and another a silicon-junction diode rated at 1.5 A at 50 c/s.

The use of solar power for operating transistor equipment was demonstrated by Westinghouse with a Zenith pocket receiver powered by 144 "Westaphot" cells and a floating 4.8-V battery. This sup-

plied 10 to 20 mA of current.

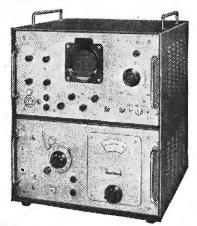
A new covering for instrument wires, described as "Carafil," was shown by S.C.F. It is very resistant to high temperatures and enables current loadings heavier than normal to be imposed on transformers and chokes, thus resulting in some reduction in size and weight.

Printed circuits are beginning to find applications in French electronic equipment, but there is little evidence that dip-soldering is in general use.

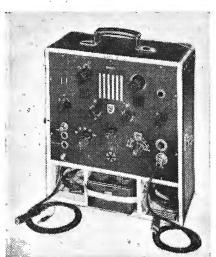
For some years past adjacent-channel interference on the broadcast bands has been combated by using rotatable frame aerials and many French receivers embody this feature; ferrite loops being the popular kind. F.M. has not, therefore, had the same attraction in France as an interference-reducing medium for broadcast; nevertheless f.m. sets and parts were well in evidence.

Radio-Celard of Grenoble combines the f.m. and loop-aerial solution to interference in the "Captefem" adaptor. This consists of an f.m. unit with a rotatable loop aerial feeding into the pick-up terminals of the broadcast receiver. On medium and long waves the loop is used as a low-impedance frame aerial followed by an r.f. stage and its output fed to the aerial terminal of the receiver.

The French electronics industry is now producing



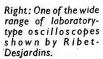
Above: "Spectrum Analyser" shown by Derveaux for general radar testing.

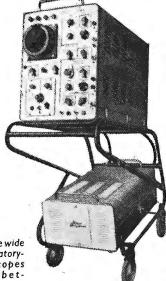




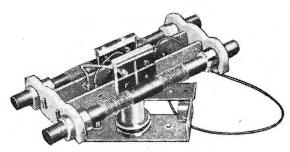
"Captefem" f.m. adaptor with rotatable loop aerial (Radio-Celard).

Left: Philips combined pattern generator and signal tracer covering television Bands I and III





WIRELESS WORLD, MAY 1957



Transco rotatable ferrite rod aerial.

a variety of test and laboratory equipment. For testing transistors, for example, C.R.C. have introduced the "Transigraphe GP70" which displays the family of curves for a p-n-p or n-p-n transistor directly on a c.r. tube. An optical attachment enables the displayed curves to be traced, by hand, on paper. Der-

veaux had a range of radar test sets covering 20 cm down to 8 mm, as well as a new spectrum analyser for general radar work. Ten different types of laboratory oscilloscope were shown by Ribet-Desjardins, the most elaborate going up to 50 Mc/s, having sweep speeds up to  $\frac{1}{100} \text{th} \, \mu \text{sec}$ , electronic switching and a delay line.

A.C. milli-voltmeters with input impedances between  $10 \, \mathrm{k}\Omega$  and  $1 \, \mathrm{M}\Omega$  and usable from  $20 \, \mathrm{c/s}$  to  $100 \, \mathrm{kc/s}$ , were shown by Ateliers DA et Dutilh. They employ a form of transistorized valve voltmeter

with a 6-V dry battery.

Television service equipment was represented on Philips' stand by an interesting combined portable signal generator covering Bands I and III and the customary i.f.s., and a signal tracer with loudspeaker. Equipment for testing bilingual TV speech channels, a system evolved for use in North Africa (see Wireless World Technical Notebook, February and March 1957), was shown by Société S.I.D.E.R.

# Colour TV in the Doldrums

HE general impression that American colour television is a complete failure was confirmed recently by C. O. Stanley, Chairman of Pye's, in an interview with Wireless World on his return from a visit to the U.S.A. One of the main reasons for the situation, said Mr. Stanley, was economic. Americans were not prepared to pay more than about 10 per cent above the cost of black-and-white receivers for colour sets—whereas in fact the colour sets were priced at 500 dollars (and subsidized at that) compared with the 160 dollars of equivalent monochrome receivers. The discrepancy was made worse by the fact that monochrome sets were falling in price anyway as a result of fierce competition and "distress merchandizing."

A second important reason for the situation was the poor technical quality of the pictures given by the N.T.S.C. system, especially in fringe areas and at the extremities of transmission networks. This applied to both colour and compatible black-and-white pictures. As a result, one could not help feeling that some American engineers were now beginning to doubt the wisdom of their having adopted compatibility in the first place, if one of the consequences was a loss of audiences to the broadcasting stations. Added to all this were the considerable difficulties of receiver adjustment and servicing—it was being said that an M.I.T. engineer was needed with every set installed! The actual programmes—about three hours per day—were, however, very good indeed.

The only real force behind colour television in America recently had been RCA, said Mr. Stanley, and one could not fail to observe that this organization had its plate full with some very serious lawsuits. At the same time, a business efficiency expert had been appointed president, and it might well be that the heavy financial leak due to colour television might stop RCA's interest in this project. If this happened it would put colour television on the ice for a considerable time.

On the question of single-gun tubes for receivers and other new components which would be required, it appeared that while the industry was in the doldrums in America nobody could spare the money to develop them—and the somewhat different receiver circuitry—for large scale production. The story might have been different had there been more time and freedom for independent lines of investigation into systems and display devices at the very beginning—but the over-hasty decision to get colour television going at all costs had now "queered the pitch." At the moment, it did not appear that singlegun receivers could be made any cheaper than those using the three-gun tube.

The American example, said Mr. Stanley, was a clear lesson to us that we ought to stop thinking about setting up a public service in Britain, and treat colour television purely as a laboratory problem. A satisfactory colour receiver could not at the moment be sold for less than £200 (excluding P.T.) and there was no reason to believe that British people would pay a greater proportion more for colour than the Americans—especially during the present period of rising prices.

These views were confirmed by L. C. Jesty, of Sylvania-Thorn, speaking with Dr. E. L. C. White at a recent I.E.E. informal lecture on colour television. He said there was practically no technical activity in the U.S.A. at the moment and no reference to colour in the recent I.R.E. Convention—except an account of what was happening in Europe. Mr Jesty's estimate of the desirable maximum price of a colour set was, however, somewhat higher than Mr. Stanley's—not more than two-thirds above the cost of a monochrome receiver.

It was generally agreed by other speakers that very little could be done until a really cheap and satisfactory colour display device had been evolved, and consequently all the present work on transmission systems could only be regarded as academic. One speaker in particular compared the progress of colour television with the history of colour photography and prophesied on that basis that we still have a long way to go. "We are now nearly through the era of the three-gun tube" he said—although Mr. Jesty had remarked earlier that the three-gun tube was still the backbone of colour television in the U.S.A.

# WORLD OF WIRELESS

#### International Acoustics Meetings

TWO recent Paris meetings of international committees dealt with acoustics. Among the subjects discussed at the meeting of the electro-acoustics committee of the International Electrotechnical Commission were lateral-cut commercial and transcription disc recording, methods of measurement of the electro-acoustical characteristics of hearing aids, sound systems, loudspeakers, ultrasonic therapeutic equipment, and sound level meters. The peutic equipment, and sound level meters. The eleven-man British delegation was led by R. S. Dadson (N.P.L.), and consisted of J. P. Ashton (Amplivox), R. A. Bull (Westrex), H. Davies (B.B.C.), Dr. G. F. Dutton (E.M.I.), N. Fleming (N.P.L.), S. Hill (S.T.C.), Dr. A. J. King (Metrovick), Dr. W. Summer (Barber Electrical Services), F. E. Williams (Post Office) and A. D. Falk (R.S.I.) liams (Post Office), and A. D. Falk (B.S.I.).

The second meeting, attended by delegates from 14 countries, including seven from Britain, was concerned with physical acoustics. A definition of the phon was agreed upon and will be circulated as a draft I.S.O. (International Organization for Standardization) recommendation. It is similar to that proposed some 20 years ago but never ratified.

#### Phenomenal Television Reception

NORMAN BURTON reports from Revesby, N.S.W., Australia, that since October last he has heard the B.B.C. television sound on 41.5 Mc/s some twenty times and the vision signal three times. On one occasion in November the vision signals were on peaks as strong as the local television station. Reception was confined to the 11 a.m. to 1 p.m. morning session of the London station and the B.B.C. has verified one transmission from a tape recording. Unfortunately the recorder was not always available and generally missing when signals were at their best.

The receiver was a Hallicrafter SX28 and the aerial, a 2-element one, constructed from details published in the August 1947 Wireless World.

### Marine Radar Training

COMMENTING in our December 1956 issue on what have been somewhat ironically called "radar assisted" marine collisions, we stated "as far as we know there has never been a case of collision which could be contributed to failure or lack of accuracy in the equipment itself. . . . By far the most prevalent cause of error is faulty appreciation of the displayed information." A step toward ending this unfortunate position has been taken by the Ministry of Transport and Civil Aviation by the introduction of a new regulation. It makes it compulsory for a deck officer in the British marine service to take an officially approved radar observer course before being issued with a certificate of competency as second mate (foreign-going) or mate (home trade).

The new regulation comes into operation on

June 1st.

#### Scottish Exhibition

THE biggest United Kingdom domestic sound and television exhibition yet held outside London opens at Kelvin Hall, Glasgow, on May 22nd for ten days. There will be nearly 60 exhibitors, including all the leading domestic receiver manufacturers. It may well provide a preview of the National Radio Show to be held at Earls Court in the autumn.

Although there will be considerable emphasis on television-about 100 receivers will be operating on the stands—the B.B.C. technical pièce de résistance will be a demonstration showing the benefits of v.h.f.

sound broadcasting.

1958 Exhibitions.—Soon after the list of exhibitors for the 1957 I.E.A. Exhibition had closed the date of the 1958 Show was announced-April 16th to 25th at Olympia. An Electronic Computer Exhibition, to oryanized handling equipment of all kinds, is being organized jointly by the Radio Communication and Electronic Engineering Association and the Office Appliance and Business Equipment Trades Association for November 28th to December 4th next year at Olympia.

Television Duty.—The additional £1 to be charged for television licences in August will not bring extra money to the B.B.C.; it is an excise duty added to the licence fee. Incidentally, under a new agreement which came into conscious April 1 tenth B.B.C. came into operation on April 1st, the B.B.C. will in future receive 87½% of the licence revenue after the Post Office has deducted "a sum equal to the expenses incurred by the P.M.G." in collecting the licence fees and investigating interference complaints.

B.B.C. Television Service.—When by the end of the year the B.B.C. has achieved its objective of providing a year the B.B.C. has achieved its objective of providing a television service to 98% of the population, it will then set about building "fill-up" stations for places within the general coverage area where reception is inadequate—such as Peterborough and Berwick. The Corporation will then extend the service to the highlands and islands outside the main service areas.

Hearing Aid Production.—As "purchasing agent" for the Ministry of Health, the Post Office has bought 800,000 "Medresco" hearing aids and 27M batteries for them since 1948, when the Dollis Hill Research Station produced the prototype. The Contracts Department of the Post Office along th ment of the Post Office also arranges for the repair of some 120,000 hearing aids a year.

Broadcast receiving licences in force in the United Kingdom at the end of February totalled 14,480,562. Of this number, 6,863,234 were for television and 304,307 for car radio sets. During February television licences in represent by 10,040. licences increased by 106,049.

Heaviside Lived Here.—Among a number of plaques to be erected by the London County Council to mark the former homes of famous people is one recording that Oliver Heaviside lived at 55, Plender Street, St. Pancras, London, N.W.1.

Purchase Tax on domestic sound and television receivers contributed over £40M to the national income in 1956.

Webbs Radio ask us to correct the price of the Eddystone 820 f.m./a.m. unit quoted in their advertisement on page 126. It should be £31 18s. West Wales will have a television service and a three-programme v.h.f. sound service from April 29th when the B.B.C.'s station at Blaen Plwy, near Aberystwyth, is introduced. The television station, operating in Channel 3 (vision 56.75 Mc/s, sound 53.25 Mc/s), started test transmissions on April 15th. It has an e.r.p. of 1 kW and will serve the coastal belt around Cardigan Bay. The v.h.f. sound transmitters will radiate on 88.7, 90.9 and 93.1 Mc/s, each with an e.r.p. of 60 kW. Aerials for both services are mounted on a 500-ft mast, and the transmissions are horizontally polarized.

Welsh I.T.A. Station.—The site at St. Hilary Down, near Cardiff, Glamorgan, chosen by the I.T.A. for its South Wales and West of England station, has now been approved by the Government. Objections had been raised by air services as it was considered the 750-ft mast would constitute a danger to users of the nearby Cardiff airport.

Plastics Convention.—Seventeen papers covering the latest extrusion and injection moulding techniques and recent developments in plastics materials will be delivered during the international convention being held in conjunction with this year's British Plastics Exhibition (Olympia, London, July 10th-20th). Although none of the lectures deals directly with plastics for electronics purposes, many of the techniques and developments covered are of general interest to the industry. Admission to the exhibition costs 2s 6d, but tickets for the convention are obtainable free from British Plastics, Dorset House, Stamford Street, London, S.E.1.

Automatic Measuring Equipment.—A conference is being organized by the Society of Instrument Technology to provide an opportunity for the users and makers of automatic measuring equipment, and those concerned with research and development in this field, to meet and discuss their work. This conference on automatic measurement of quality in process plants will be held at University College, Swansea, from September 23rd to 26th. Further information is available from the Society at 20, Queen Anne Street, London, W.1.

The Institution of Electronics has transferred its general headquarters from London to 78, Shaw Road, Rochdale, Lancs., the address of W. Birtwistle, who is now honorary general secretary. He will continue as honorary secretary of the northern division of the Institution and as organizer of the annual electronics exhibition held in Manchester.

1,700 miles on 2 Mc/s.—The radio officer of S.S. Spalake reports that on a voyage from Tobruk to Malta on March 10th he maintained direct radio-telephone contact on 2.182 Mc/s with Niton Radio (GNI); a distance of approximately 1,700 miles.

Courses for overseas specialists, being organized this year by the British Council in conjunction with universities, government departments and learned societies, include one on point-to-point radio services (April 28th to May 14th) and another on digital computers (October).

Electronics Centre.—Many of the Mullard exhibits mentioned in our review of the Physical Society's Exhibition are displayed at the technical information centre recently opened at Mullard House, Torrington Place, London, W.C.1. The floor space of the showrooms and demonstration room is 5,000 square feet, and there is also a cinema seating over 70.

Careers.—A well-illustrated informative brochure "Careers in the Telecommunication Industry," has been prepared by the Telecommunication Engineering and Manufacturing Association. It has been circulated to university appointments boards, technical colleges, public and grammar schools and youth employment offices, and is also available from the office of T.E.M.A., 40-53, Norfolk Street, London, W.C.2.

A summer school on instrumentation and automatic control is being organized by the Gloucester Technical

College for July 1st to 5th. A draft syllabus includes sections dealing with the basic theory of closed loop systems, servomechanisms and process control systems. Lecturers include Associate Professor E. B. Pearson (Royal Military College of Science) and Dr. G. L. d'Ombrain (Battersea Polytechnic).

"Marconi Instrumentation," the quarterly journal issued by Marconi Instruments, Ltd., which started ten years ago with an initial print order of 1,000 copies, now has a circulation of 16,000. Approximately 60% go abroad, including 3,500 to the U.S.A.

Plastics Year Book.—One of the most important features of the British Plastics Year Book, 1957, is the 142-page review of plastics patents. It contains all relevant patents issued last year, and as they are collected in subject groups, each with a potted specification, it provides a useful record of technical development in the industry. The 716-page Year Book also includes classified directories of manufacturers and proprietary names, a glossary of technical terms and a Who's Who. It is issued by our publishers and costs 2 guineas (postage 1s 9d).

#### FROM ABROAD

The net loss on all colour television activities of the Radio Corporation of America last year (including development, manufacture, training of technicians and provision of colour programmes) was nearly \$7M. Since the introduction in 1955 of the 21-in compatible colour receiver, only 102,000 have been sold.

Canadian TV.—The 518-page report of the Royal Commission on Canadian broadcasting records that 80% of the 16M population live within the service area of one or more of the country's 38 television stations. During the past four years the number of television receivers in use has increased tenfold and now totals 2,300,000. Of the 189 sound broadcasting stations in the Dominion, 167 are privately owned.

Marine Radar Conference.—An international meeting, to be held in Genoa from May 16th to 19th in preparation for the next International Meeting on Radio Aids to Marine Navigation, will consider problems relating to the design and construction of marine radar, and the use of radar at sea. Among those contributing to the conference are Colonel J. D. Parker (secretary general, International Maritime Radio Committee) and Captain F. J. Wylie (director, Radio Advisory Service).

Television in India.—The Indian Minister for Information and Broadcasting recently announced that preliminary arrangements have been made for the country's first television station to be built at Bombay. It will probably be ready for service next year.

Novel Aerial!—A crane near the Hamburg transmitting station was found to be acting as a tuned medium-wave aerial, so that the field of the high-power transmitter was causing dangerous r.f. voltages on the grab. Using a model of the crane it was possible to evolve an inexpensive means of reducing the r.f. voltage to a safe value. This consisted in joining two points on the crane by a free hanging wire through an adjustable capacitor (about 900 pF). The main body of the crane then completed a tuned rejector circuit.

Long-Distance TV Reception.—Membership of the American "Over 50TV DX Club," as its name indicates, is limited to those who have received 50 or more television stations. The top scorer in the club, which is sponsored by our New York contemporary Radio-Electronics, has logged 290 stations. This total has been reached in three years and includes stations in eight countries and 45 states.

Instrumentation.—An International Congress and Exhibition of Measuring Instruments and Automation is to be held in Düsseldorf, Germany, from November 2nd to 10th.

# **Personalities**

Air Vice-Marshal G. P. Chamberlain, C.B., O.B.E., the new deputy controller of electronics at the Ministry of Supply, has spent most of his Service career in signals. During and before the war he was with 16 and 18 Reconnaissance Groups, R.A.F., and was for some time in Australia on radar duties. His post-war service includes the directorship of Civil Air Operations at the Ministry of Civil Aviation, and after a tour of duty abroad took over the command of the R.A.F. Staff College at Andover. He is 52.

Major L. H. Peter, M.I.E.E., who, as announced last month, is the new president of the Radio and Electronic Component Manufacturers' Federation, has been with Westinghouse since the end of the first world war. In about 1926 he was made responsible for the development of metal rectifiers, and has successively held the positions of chief electrical engineer, chief engineer and, for the past ten years, chief development engineer. Major Peter was one of the six founder-members of the original Radio Component Manufacturers' Federation, and is also a member of the Rad.o Industry Council.

I. A. Smale, C.B.E., B.Sc., M.I.E.E., has retired from the position of engineer-in-chief of Cable and Wireless and has become technical consultant in telecommunications engineering to Marconi's W.T. Co. Mr. Smale, who is 62 and had been engineer-in-chief since 1948, was responsible for the development of long-distance c.w. relay stations as a means of overcoming unfavourable propagation conditions. He was also responsible for the design and manufacture of the first voice-frequency channelling system used commercially in this country. Mr. Smale was with Marconi's for ten years before he transferred to Cable and Wireless in 1929 where he was assistant e-in-c for 14 years.

Denis Taylor, M.Sc., Ph.D., head of the Electronics and Instrument Division at the Atomic Energy Research Establishment, Harwell, for the past 12 years, has been appointed a director and general manager of Plessey Nucleonics Limited. In addition he will become research executive of the Aircraft and Electronics Groups of the Plessey Company, and will be responsible for the co-ordination of the Company's nuclear programme. He takes up his new appointment on May 1st. Dr. Taylor, who is 46, was a member of Sir Robert Watson-Watt's team at the Bawdsey radar research station during the early part of the war, and for his "contribution to the development of radar installations" received a Government award. He later went to T.R.E., Malvern, where he became superintendent. Between 1931 and 1939 he held a number of university lectureships.



Major L. H. PETER



J. A. SMALE

E. W. Chivers. B.Sc., who for the past ten months or so has been principal superintendent of the electronics division of the Armament Research and Development Establishment (M.o.S.) at Fort Halstead, Sevenoaks, Kent, has been appointed deputy director of the establishment. He is 49. In 1947 he became superintendent of the Radar Research and Development Establishment at Malvern, and on the fusion in 1953 of R.R.D.E. and T.R.E. into the Radar Research Establishment was appointed deputy director of ground radar.

C. J. V. Lawson, M.I.E.E., the new engineer-in-chief, Cable and Wireless, was appointed deputy e-in-c only a few months ago. He was previously manager of the cable station and head of the school of telecommunication engineering at Porthcurno, near Land's End. He is 50. The new deputy e-in-c is A. H. Harris, who is 52. He joined the Eastern Telegraph Company in 1922 as a telegraph operator, and six years later was posted to the engineer-in-chief's department. He was transferred to C. & W. on the merger of British overseas telegraph undertakings in 1929.

Richard Arbib, this year's chairman of the R.E.C.M.F., is chairman and managing director of Multicore Solders, Ltd., which he joined some 20 years ago. He entered the radio industry in 1929 in the electrical reproducer department of H.M.V., later becoming advertising manager of that company.







RICHARD ARBIB

- J. M. Furnival, M.B.E., has retired from the position of general manager of Marconi Instruments, Ltd., which he has held since 1942. He will also be remembered for his pioneering work on the development of airborne radio equipment, including beam approach. He joined Marconi's W.T. Co. in 1919 for work in this field, and for some years was manager of the Company's aircraft wireless establishment at Hackbridge, Essex.
- S. W. Amos, B.Sc., A.M.I.E.E., a frequent contributor to Wireless World, has been appointed assistant editor in the Technical Instructions Section, B.B.C. He joined the Corporation in 1941, and after two years' experience as maintenance engineer transferred to the engineering training school as an instructor. Three years later he transferred to the Technical Instructions Section where since 1950 he has been chiefly concerned with the preparation of the four-volume B.B.C. engineering text book, "Television Engineering" (issued by our publishers).

Geoffrey E. Beck, B.Sc., A.M.I.E.E., author of the article on page 225, has been with Marconi's since graduating at Birmingham University in 1938. For ten years he was in the research division, for the major part of the time working on marine radar. Since 1947 he has been in the development division where he has been concerned with suppressed aircraft aerials. Last year he was appointed group leader of airborne navigational aid development.

# Inexpensive Pre-Amplifier

Simple Design for Use with Simple Pickups and Radio Tuners

By P. J. BAXANDALL, B.Sc.(Eng.)

HILST it is generally believed that presentday crystal pickups are somewhat inferior to the best moving-coil pickups from the point of view of quality of reproduction, the best of them, when properly equalized, are actually capable of giving results which, judged aurally, do not fall far short of the best obtainable.

Crystal pickups, moreover, have the undoubted advantages of low cost and large output, and this makes them very attractive when economy must be carefully considered.

With the above thoughts in mind, it was felt that a simple pre-amplifier for use with pickups such as the Cosmocord GP20 Hi-g, or Collaro Studio Transcription, and suitable for feeding the Inexpensive High-Quality Amplifier described in the preceding two issues, might appeal to some readers. The pre-amplifier is also suitable for use with radio tuners, and its distortion is low enough to enable full justice to be done to the best f.m. transmissions.

The circuit is shown in Fig. 1, from which it will be seen that the author's negative-feedback tone control is employed, the first half of the double triode operating as a straightforward amplifying stage. The tone-control circuit has been slightly modified, however, compared with the version

<sup>1</sup> "Negative-Feedback Tone Control," by P. J. Baxandall, Wireless World, Oct. 1952.

originally published, to enable a gain of approximately 3 to be obtained from this stage with the controls set for level response, instead of unity as in the original version. The price paid for the advantage of increased gain is a reduction in the available amount of treble lift, and to a lesser degree, of bass lift.

The performance of the tone control may be judged from Fig. 2, which shows the frequency response for various settings, measured between the grid of VIa in Fig. 1 and 15-ohm output terminals of the Inexpensive High-Quality Amplifier. advantage resulting from the increased gain of the modified tone-control circuit is that the previous stage is now required to supply so small an output voltage that its distortion, even with no feedback, is only a small fraction of 1%. The tone-control stage, having negative feedback, can supply the required output of 4 V r.m.s. on sine waves with a similarly low level of distortion, so that very low total distortion is obtained in a very economical manner. To achieve this low distortion in practical use, it is, of course, imperative for the volume control to be placed before the first stage, as in

The total gain, with the tone controls set for level response, is such that a sine-wave input to V1a grid of approximately 45 mV r.m.s. is required

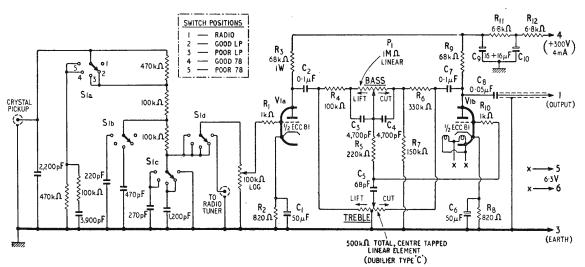


Fig. 1. Complete circuit of pre-amplifier. All resistors  $\frac{1}{2}$  watt  $\pm$  20%, and capacitors (other than electrolytic)  $\pm$  20%, except where otherwise specified. Mullard ECC81 may be replaced by 12AT7, Osram B309 or Services Type CV455. The numbers on the connections at the right-hand side of the circuit correspond with the numbers on the socket of the Inexpensive High-Quality Amplifier, described in previous issues. The equalizer circuit, to the left of the volume control, has been designed to suit the Cosmocord GP20 Hi-g pickup. Component values should preferably be within  $\pm$  10%.

to give an output of 5 watts from the main amplifier into a 15-ohm resistive load, i.e., an output from the pre-amplifier of 4V r.m.s.

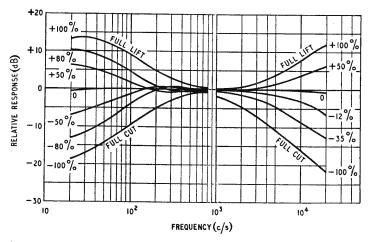
Due to Miller effect, the input capacitance of V1a is such that appreciable top loss will occur if the source has an effective internal resistance greater than  $100 \, \mathrm{k}\Omega$ ; this value gives a loss of about 1 dB at  $15 \, \mathrm{kc/s}$ .

The rest of the circuit consists of a passive network whose main function is to provide pickup equalization to suit standard recording characteristics, but it also allows additional top cut to be introduced when necessary, to improve results on worn or otherwise poor recordings. With further top cut from the tone-control, an asymptotic rate of cut of 12 dB/octave may thus be added to the equalizer characteristic if required; whilst this is less steep and the roll-off is more gradual than is obtained with filters of a more ambitious variety², nevertheless it will be found that poor recordings can be dealt with in quite a satisfactory manner.

The pickup equalization circuit differs from those previously published<sup>3</sup>, and has been adopted for the following reasons:—

(a) By placing a relatively large capacitor directly

"Gramophone and Microphone Pre-amplifier," by P. J. Baxandall, Wireless World, Jan. and Feb. 1955.
""Pickup Input Circuits," by R. L. West and S. Kelly, Wireless World, Nov. 1950.



Above: Fig. 2. Measured frequency response, between VIa, grid and output of Inexpensive High-Quality Amplifier, at various settings of the tone controls. The figures on the curves represent the percentage rotation of the knob on either side of the middle position.

Right: Fig. 3. Modified arrangement in which the gramophone equalizer and volume control are in the playing desk. The radio volume control may be fitted in the tuner unit and should have a value not greater than  $100k\Omega$ .

in shunt with the pickup, variations in internal capacitance from one pickup sample to another, and with temperature, are prevented from having a significant effect on the equalization characteristic obtained.\*

- (b) Due to the presence of the capacitor across the pickup, all impedances in the equalizer may be kept reasonably low, thus reducing the effect on the response caused by stray capacitances and so making the result almost independent of variations in layout.
- (c) The output impedance of the equalizer circuit is low enough to make it practicable, if desired, to place the equalizer and volume control in the playing desk and to connect it to the pre-amplifier via a low-capacitance screened cable up to 10 feet or so in length. By arranging matters in this way, the playing desk becomes a self-contained and fully equalized gramophone source, suitable for connection to any available amplifier capable of giving full output for a sine-wave input of  $100\,\mathrm{mV}$  r.m.s. or less, provided the input resistance of the amplifier is not less than about  $0.5/\mathrm{M}\Omega$ . To what extent this facility is regarded as advantageous depends, of course, on individual circumstances.
- (d) The values have been so chosen that approximately the same voltage is produced across the volume control on loud 78 r.p.m. records as on

loud LP records. This is not a vital point, but it is easiest for the user if about the same volume control settings are required with both types of record.

In the "Good LP" position of the equalizer switch, the equalization provided is intended to be correct for records made in accordance with the revised British Standard 1928:1955 LP recording characteristic4, which is now widely adopted by recording companies. Using the author's Cosmocord HGP 39-1 LP pickup head, which is not a specially selected one, the measured response, from pickup stylus to loudspeaker terminals, with the equalizer set to the "Good LP" position and the tone-controls set

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<sup>\*</sup> The advantage of placing a large capacitor in shunt with a crystal pickup was first pointed out to the author by G. B. Wellgate.

""Disc Recording Characteristics," by J. D. Smith, Wireless World, Nov. 1956. 470kΩ§ 100 k**Ω** ≷ ۷Ia R, GRAM RADIO 100k N 100kΩ § ۲ıc ΩMI RADIO TUNER CABLE  $R_2$ 270 pF 1,200 p F T50μF IN PLAYING DECK

View of prototype pre-amplifier with dust cover removed to show layout of components.

for level response, was within  $\pm 2\,\mathrm{dB}$  of the intended result over the frequency range  $50\,\mathrm{c/s}$  to  $10\,\mathrm{kc/s}$ . (The measurements were made using the British Sound Recording Association Test Disk No. PR.301, which is recorded to the C.C.I.R. 1953 characteristic, the measured results being corrected to allow for the difference between this characteristic and the revised B.S. 1928: 1955.)

In the "Poor LP" position of the switch, an extra top cut of approximately 6 dB at 10 kc/s is introduced.

In the "Good 78" position of the switch, the equalization is suitable for a recording characteristic

having 6 dB/octave asymptotes with corner frequencies at 250 c/s (bass cut) and 6 kc/s (top lift). This is considered to be a good compromise, and with judicious use of the tone controls when necessary, any normal 78 r.p.m. record can be well reproduced.

In the "Poor 78" position of the switch, an extra top cut of approximately 6 dB at 10 kc/s is introduced.

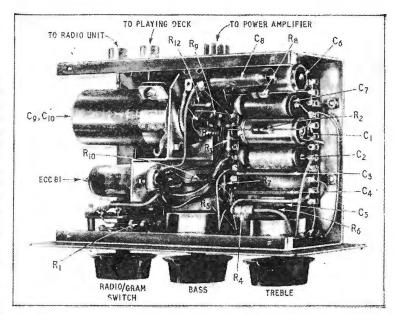
In the "Radio" position of the switch, a sine-wave input of about 45 mV r.m.s. is required for full output. Many radio tuners will give a larger output than this, and are designed to feed into a higher resistance load than  $100 \, \mathrm{k}\Omega$ ; in such cases a suitable resistor (e.g.,  $470 \, \mathrm{k}\Omega$ ) should be connected in series with the "Radio Input" socket.

If the equalizer circuit and gramophone volume control are put in the playing desk, a simple change-over switch, with positions labelled "Radio" and "Gram" will be required in the pre-amplifier, and the radio volume control may be fitted in the radio tuner unit. The unit photographed is intended for use in this way, the connections being shown in Fig. 3.

Fig. 4 shows an equalizer circuit performing the same functions as that included in Fig. 1, but designed to suit the Collaro Studio Transcription pickup, which responds fairly smoothly up to 15 kc/s under both LP and 78 conditions. The equalization provided is also reasonably accurate for the Collaro Studio P pickup.

In the "Poor 78" position of the switch, it will

In the "Poor 78" position of the switch, it will be seen that two additional top-cutting capacitors are introduced, giving an extra attenuation of about 10 db at 10 kc/s. By omitting the 150-pF capacitor, the attenuation is reduced to about 6 db, which is the same as for the GP20 Hi-g equalizer circuit; in general, however, it is considered to be advantageous to include this capacitor, as it gives an appreciable reduction in scratch, etc., on bad records.



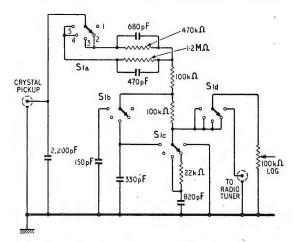


Fig. 4. Equalizer circuit designed to suit the Collaro Studio Transcription pickup. Component values should preferably be within  $\pm$  10%.

It may be worth mentioning that it appears to be a characteristic of present-day crystal pickups that the variations in frequency response and sensitivity between one sample and another of nominally the same model are rather greater than for some other types of pickup. Consequently the equalization circuits given may not be quite optimum for any particular sample of pickup, but the departure from ideal equalization is unlikely to be very noticeable audibly. In the unlikely event of insufficient amplifier gain being available for full volume with a low-sensitivity sample of pickup, the value of the capacitor connected across the pickup may be reduced a little; the accompanying slight loss of bass may be compensated by using the bass tone control.

Construction.—Various layouts are, of course, practicable for a circuit such as this, and the choice may

be left to the reader. The most economical arrangement would be to build the pre-amplifier, with or without equalizer, on the same chassis, suitably enlarged, as the main amplifier. Whatever is done, the following points should be watched:-

(a) The components associated with V1a grid circuit should be well separated from signal-carrying wiring in later parts of the circuit, otherwise the top response may be modified due to unintentional feedback via stray capacitances. Similarly the anode circuit wiring of V1b, i.e., that associated with R<sub>6</sub>, C7, R9 and C8, including the output lead and the lead to P2, should be kept well separated from the grid circuit components (R<sub>5</sub>, C<sub>5</sub> and R<sub>10</sub>) and their

(b) An ordinary black Bakelite valveholder should not be used if the lowest hum level is desired, but rather one of the light brown (nylon loaded plastic) variety; this will give less leakage current between heater and grid pins. A p.t.f.e. valveholder is an unnecesary extravagance at the signal level involved in this pre-amplifier. A further point is that the heater wiring should be twisted and kept as clear of the signal wiring as practicable.

(c) In the prototype unit, the valve and the 16+ 16μF capacitor have been mounted on a small subassembly resiliently attached to the main chassis using screws passing through soft rubber grommets. This reduces the risk that microphony in the valve may cause a howl to build up when the pre-amplifier is used close to a loudspeaker. Whilst it is probable that this precaution would normally be found quite unnecessary, it is nevertheless easy to take and at least can do no harm. Do not forget, however, to make an earth connection between the sub-assembly and the main chassis, otherwise, as the author discovered to his cost, there will be no h.t. decoupling and "motor-boating" will ensue!

(d) If the equalizer and volume control are incorporated in the playing desk, it is essential for them to be completely screened electrostatically. An ordinary tin box is perfectly satisfactory.

Testing.—After completion, it is desirable at least to check that the d.c. operating conditions in the two stages are reasonable. The cathodes should nominally (with 300—V h.t.) be at  $+1.6\,\mathrm{V}$  and the anodes at +115 V. Provided the measured values are within the limits 1.3 to 1.9 V and 80 to 150 V, and provided none of the readings is affected by operating the tone-control knobs, all may be assumed to be well in this respect.

The hum level, at the output of the Inexpensive High-Quality Amplifier, should be hardly any greater with the pre-amplifier connected than it is with the input to the main amplifier short-circuited; it should be only just audible with one's ear close to the loudspeaker in a very quiet room.

In the absence of facilities for frequency-response measurements, listening tests should be used to find out whether the controls are producing their intended effects. Turning the potentiometer knobs should not itself produce any noises from the loudspeaker, when no signal is applied.

## **Ouantum Amplifiers**

THESE amplifiers, with their attractive possibility of very low noise, are arousing increasing interest. They depend on the creation of a non-equilibrium distribution of energy between quantum states in atoms or molecules. Energy at the frequency of transition to the equilibrium state can be extracted by stimulation with an applied signal at the same frequency in the form of coherent radiation or of noise. According to the available energy, amplification or oscillation is possible.

What was apparently the first such amplifier was discussed by J. P. Gordon et al. in the Physical Review of August 15th, 1955. This uses an ammonia beam with electrostatically separated molecular energy states. The beam density must be small to prevent rapid spontaneous transition back to the equilibrium state. This severely limits the available energy to only about  $5 \times 10^{-10}$  watts. The authors coined the name "maser" (standing for "microwave amplification by stimulated emission of radiation") for such graphym amplifiers.

radiation") for such quantum amplifiers.

More attractive possibilities (discussed in a letter from M. W. P. Strandberg in the *Proc.I.R.E.* for January, 1957 and by Prof. N. Bloembergen in the *Physical Review* of Oct. 15th, 1956) are offered by proton or electron spin states in solids. The spin may be thought of an aredusing a magnetic moment that be thought of as producing a magnetic moment that can align itself with or against an applied magnetic field, thus producing two possible states. Non-equilibrium spin states can be prepared in several ways, the simplest being the application of a pulse of coherent radiation of the correct frequency cut off at a suitable phase. Spin densities much higher than those in ammonia beams are obtainable, and can be effectively increased still further by rapid cycling from the equilibrium to non-equilibrium states (e.g., at a typical radar p.r.f. of 10° c/s per sec.). Much slower spontaneous transition back to the equilibrium state (longer relaxation time) than in the ammonia beam can also be realized both for certain nuclear proton spin states and certain paramagnetic electron spin states. This gives a longer time for experiments on the non-equilibrium state, and moreover, the power requirements to produce saturation of this state are reduced. The transition frequency is proportional to the magnetic field, so that variation of this field offers wide-range tuning possibilities. By contrast the ammonia transition frequency that is used is fixed within a few Mc/s of its centre value (about 24 kMc/s).

A solid state "maser" using electron spins has recently been produced at the American Bell Laboratories by Dr. D. Scovil et al. It oscillates at X-band (9000 Mc/s) with a power of about  $2 \times 10^{-6}$  watts. Another experiment carried out in France (described by Combrisson et al. in Compt.Rend.Acad.Sci. of May 14, 1956) also used electron spins and a similar operaproduce oscillations, but some amplification was observed.

These quantum states are largely independent of thermal motion so that their noise can be equivalent to that at a very low effective temperature, only a few degrees above absolute zero. Noise is thus 20 to 30 dB down on that in normal receivers; and theoretical calculations indicate that sufficient gain can be realized to take advantage of this low noise figure. The consequent possibility that transmitter power could be reduced in this proportion (20 to 30 dB) without any decrease in effectiveness would revolutionize microwave technology. The equal possible increase in receiver sensitivity would be of tremendous value in the field of radio astronomy.

This low noise is also equivalent to operation with a very high Q-factor. For example, two of the original "masers" have been used to produce beats at 30 c/s with no apparent random phase variations. This indicates a stability to within a tenth of a cycle in 24 kMc/s!

# Physical Society's Exhibition

NEW ELECTRONIC DEVICES AND TECHNIQUES

Valves and allied devices shown at this exhibition will be described in the June Wireless World, while new test and measuring gear will be reported in the July issue.

THE dividing lines between pure and applied research and between research and development become increasingly difficult to draw in these days of intense activity in the physical sciences. In the Physical Society's catalogue there used to be a separate section for the research exhibits; now they are inextricably dispersed among the experimental, prototype and finished products of industry.

Applications of newly discovered physical effects are often thought of before the fundamental process has been fully explored, and research and development proceed on parallel lines. Nuclear resonance, for example, is already being used as a means of measuring magnetic flux, and in a portable fluxmeter shown by the Admiralty Signal and Radar Establishment is used to calibrate and stabilize the field of an electromagnet supplied from a 50c/s source. A regenerative receiver supplies a r.f. field at right angles to the magnetic flux and indicates precessional resonance of the proton nucleus of the hydrogen in water surrounding a search coil. There is a change in Q of the coil at resonance which is displayed as a pulse on an oscillograph trace. Changes in the magnetic field due to instability can be reduced by a factor of 60 by feeding back the pulses to the magnet power supply.

Frequency Standards.—A resonant transition between two energy states in atoms of the element cæsium in which the magnetic moment of the atom is reversed has been used by research workers at M.I.T. as a frequency standard of high accuracy (9192.63185 Mc/s) which is unaffected by external fields. By locking an oscillator to this frequency through a discriminator circuit it is possible to establish a time standard with a stability of 1 part in 10°. The Royal Aircraft Establishment showed a light portable version of the original M.I.T. apparatus which had

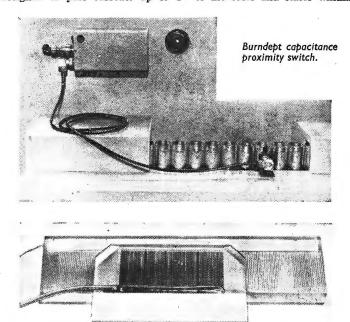
been constructed by Standard Telephones on a study contract for the Ministry of Supply.

Research and development are nowhere more closely associated than in the improvement and exploitation of special materials. Photoconductive cells, for the detection of infrared radiation, consisting of single crystals of indium antimonide, were shown by the Radar Research Establishment, while the Research Laboratories of the G.E.C. exhibited single-crystal cells of cadmium sulphide for the wavelengths of visible light in which variations in spectral sensitivity can be induced by various activation techniques. Large powder-layer cells of this material with a peak response in the spectrum of tungsten filament light were shown which if required can be designed to pass currents up to 1

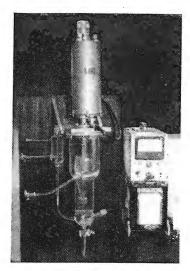
ampere for the direct operation of relays.

Length and Displacement.-Applications of electronic methods to the control of industrial processes, although sometimes complex, are essentially elaborations of simple basic principles. The measurement of length or displacement, for instance, can often be made in terms of capacitance, or by change of inductance when movement is imparted to the core of a coil. In the "Magna-Gage" shown by Southern Instruments a differential inductance transducer actuated by a probe is used as a sensitive feeler gauge; a 10-kc/s output from the transducer is amplified, rectified and applied to a centre-zero meter with a calibrated range of ±0.0005 in. The change of capacitance of a probe electrode is utilized in the Burndept proximity switch to detect the passage of opaque objects (e.g., metal cans) on a conveyor belt which, if touching, cannot be registered by conventional photoelectric counters.

For the accurate determination of position over a wide range, as in machine work tables, a form of linear resolver has been developed by Plessey in which the equivalent of the rotor and stator windings of



Plessey Linear Inductosyn scale and slider for automatic machine tool control.



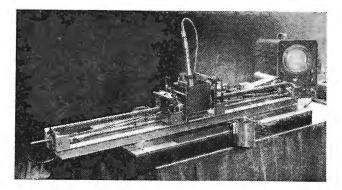
Pye liquid density indicator.

a rotary resolver are printed flat on superimposed slides. The pole spacing represents 0.1in and by interpolation settings to 0.0001 in can be repeated with an accuracy of 25 microinches. A somewhat similar principle is employed in a control rod position indicator demonstrated the U.K. Energy Atomic by Authority. Transducer coils spaced three to each interval of length (pitch) are influenced by steel collars attached to the rod. The output from one fixed coil is 120° out of phase with its neighbour and when each group is connected to the three stator windings of a synchro, 360° rotation is provided for each pitch (0.6 in). Settings are accurate to 0.02in in 25 inches.

Fluid Density.—The density of fluids is measured in terms of displacement in an instrument by Pye which uses an inductive transducer to register the height of a hydrometer float. Temperature compensation can be applied electrically when the concentration of saline solutions is to be controlled.

Absorption of gamma rays is the principle underlying the Ekco fluid density gauge. It can be used for liquids flowing in pipes of any material and will detect changes of density of 0.005.

Liquid Level. — Conventional methods cannot be employed when radioactive solutions are involved, and the problem has been solved by the Industrial Group, U.K. Atomic Energy Authority, by taking advantage of the change in low-frequency inductance of a coaxial line, consisting of a perforated stainless steel tube with centre rod, when the level at which it is short-circuited is



Ultrasonoscope automatic scanner for inspection of metal bars.

altered by the height of the conducting solution.

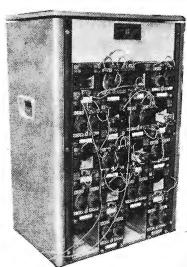
Magnetostrictive and Piezoelectric Transducers for the generation of ultrasonic vibration exploit the properties of a variety of materials from nickel to ceramics, and there was evidence of wider use of the latter class in many applications. Plessey, for example, have developed an ultrasonic abrasive drill using a cylindrical element of barium Increased efficiency of titanate. energy conversion is claimed for lead titanate/lead zirconate which are under development by Radio Heaters, Ltd. These materials also have higher thermal stability and can be worked with higher power loadings per cm<sup>2</sup> thanbarium titanate.

Ultrasonic testing of materials for flaws has been established for some time, and many portable instruments using manually operated test probes are available. A special installation for the continuous testing of metal bars was shown by Ultrasonoscope. The bar is immersed in a tank of liquid and scanned tangentially by a beam from a transducer which need not be in contact with the surface of the test piece. The dimensions of the tank and the spacing between transducer and specimen are chosen to place irrelevant return echoes outside the range of the oscilloscope time scale.

"Bender" elements consisting of ceramic strips backed by metal are used in relays developed by G.E.C. Research. They have the great advantage that, unlike magnetic relays, negligible power is required to hold the contacts closed.

Analogue/Digital Converters are used in measurement and control systems where the voltage output of a transducer, measuring some physical variable, has to be converted into digital form for numerical indication

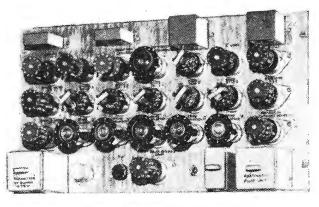
or feeding into digital data processing equipment. Many work on electromechanical principles, the usual method being to apply the analogue voltage to a self-balancing bridge incorporating a servo motor. The rotation of the motor in balancing the bridge drives a commutator system, and the brushes on this give digital signals representing the angular displacement and hence the amount of bridge unbalance caused by the applied voltage. An instrument in this category shown by I. Langham Thompson uses a uniselector as a combined servo motor and commutator. A purely electronic method well represented at the Exhibition was the so-called "subtractive comparison method," usually giving the result in binary notation. Here the input voltage is repeatedly compared with fixed reference voltages representing digits of the final answer. When the first reference is subtracted from the input, if the

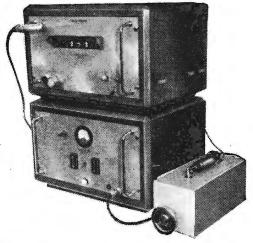


Metropolitan-Vickers d.c. analogue computer.

omputer.

WIRELESS WORLD, MAY 1957





Siemens-Ediswan transistor-driven Dekatron counter.

residue is positive a "1" digit is indicated and if it is negative a "0" is shown. The residue is then passed to the next digit stage, where the same process is performed, and so on. Elliott, Mullard and Southern Instruments all had converters of this kind, the Mullard device using transistor circuits and giving 8-digit binary indication.

Digital Indicators were very much in evidence, especially in association with the above-mentioned converters. The Langham Thompson equipment, for example, uses a new type of glow discharge tube for decimal numbers in which the numerals are formed by shaped wire electrodes placed one in front of the other. Each numeral lights up when an appropriate trigger voltage is applied to it. Other instruments used a new indicator made by Hilger and Watts. In this, each numeral is engraved on a Perspex plate, and the plates are stacked and illuminated from the edges by small lamps.

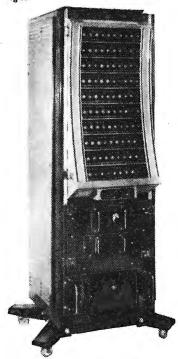
Analogue Computers on show this year included a new d.c. equipment made by Metropolitan-Vickers and compactness. notable for its Designed on the unit principle, the drift-corrected d.c. amplifiers are balanced and give two outputs of opposite sign, thereby reducing the number of amplifiers required for certain calculations. The machine is suitable for solving differential equations and studying servomechanisms by simulation. Elliott have further extended the range of possibilities of their well-known G-PAC d.c. machine with various new accessories including a function generator and an electro-mechanical servo multiplier.

Transistor Computing Circuits for digital work are becoming more prominent now that r.f. transistors

with 5-10-Mc/s cut-offs are allowing faster pulse rise times. Metropolitan-Vickers were not showing their new "950" transistor computer, but Ferranti had some interesting plugin transistor logical circuits performing simple operations at the high digit rate of 1 Mc/s. These do not employ conventional Boolean logic, but a so-called "ballot-box logic," transformers using small various input windings as the combining elements—the transistors merely acting as pulse amplifiers. The units are standardized and interchangeable and can readily be connected as adders, subtractors, etc. Mullard were showing logical circuits using both transistors and magnetic cores, the last-mentioned acting as two-state storage elements and the transistors as driving amplifiers. Usually, this type of circuit is limited by the magnetic cores to operation up to about 100 kc/s.

Pulse Counters of all kinds were to be seen in great profusion, mostly based on well-known techniques. There were, however, a few rather unusual examples. Siemens-Ediswan had an equipment in which Dekatron tubes were driven by pulses derived from transistor blocking-oscillator circuits-the h.t. for the Dekatrons being derived from a transistor "chopper" power supply so that the whole unit could run from only 20 volts. Mullard had a new transistor counter using r.f. junction types to permit working at the high p.r.f. of 1 Mc/s. A Dekatron counter designed for automatically printing out its figures on a roll of paper was displayed by Labgear, while another shown by Ericsson had a bi-directional facility—the glow discharge being moved either forwards or backwards according to the direction of rotation of a disc from which the

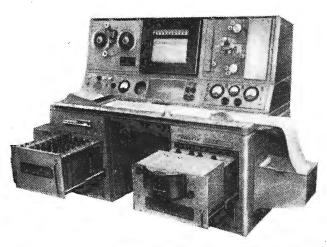
J. Langham Thompson digital indicator with strain gauge on the right.



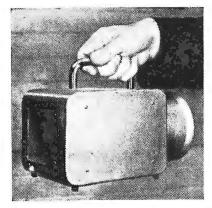
Philips pulse height analyser.

pulses were generated by an optical commutator.

Pulse Height Analysers are actually counters arranged to display the counts occurring at different pulse amplitudes. They are often used in conjunction with radiation detectors for examining radioactive materials, the pulse counts being plotted on a graph against amplitude levels. In the single-channel type, as shown by Isotope Developments, the gating of the pulses into the various amplitude levels is done by a bias control, which



Mervyn Instruments frequency/amplitude analyser for transducer signals, with magnetic-tape playback.



Right: Standard Telephones magnetic-cell storage system.



Polystyrene-copper artificial dielectric microwave lens (Admiralty Signal and Radar Establishment).

Redesigned 3-cm microwave course beacon receiver made by Elliott.

automatically moved slowly through the required range in synchronism with a pen-recorder chart. The number of counts obtained at each level is then indicated by the pen deflection at the corresponding position on the chart. In the multi-channel equipment demonstrated by Philips, however, there is a separate counter for each amplitude level (99 in all). Each incoming pulse is arranged to charge a storage capacitor to its peak value. The capacitor is then discharged in a series of accurately controlled steps, and the number of steps (which of course indicates the pulse amplitude) is used to work an electronic rotary switch which gates a count of one to the appropriate counter. The electronic rotary switch, incidentally, uses the new "trochotron" highspeed beam switching tube developed by Eriesson in Sweden.

Magnetic Matrix Stores, using tiny ferrite cores with rectangular hysteresis loops, are now being produced as complete units on a commercial basis by both Mullard and Plessey. In addition there were several experimental arrangements Mullard, for example, on view. showed how the magnetic cores could be switched directly by transistors -actually experimental high-frequency power types giving 2-µ sec pulses of 350-mA amplitude at a p.r.f. of 100 kc/s. The magnetic-cell version, however (using holes drilled in a block of ferrite), is more suitable for transistor drive because of the lower switching current required. S.T.C. demonstrated an example of this as part of an error-indicating telegraph system. The output signals were also amplified by transistors and fed into a simple transistorized logical circuit.

Ferroresonant Two-State Devices using ferrite-cored inductors were demonstrated by Mullard. In these the inductor is switched by a trigger winding from a high-current, low-inductance state, at which it resonates with a capacitor, to a low-current, high-inductance state, at which no resonance occurs (see our July, 1956,

issue). Apart from their reliability and robustness, these devices have the advantage over most other magnetic two-state elements that the stored information can be read out without erasing it at the same time.

Microwave Equipment.—It may be unusual to use a waveguide as a cable in a communications system; nevertheless Elliott employ one of circular section in a microwave telephone link they have developed. It operates on 8.5 mm using the H<sub>01</sub> mode of transmission and is said to have the very low attentuation of 2 dB per mile and be capable of carrying many hundreds of speech and television channels.

Elliott were also showing a redesigned version of their 3-cm microwave course beacon for guiding ships into harbour. The receiver now employs six transistor stages, gives an overall gain of 82 dB and is entirely self-contained with 4½ V battery, loudspeaker and receiving born.

A further development in the construction of microwave dielectric (Continued on page 217)

lenses was shown by the Admiralty Signal and Radar Establishment. This lens is made up from layers of a "mosaic" of small copper discs polystyrene film separated honey-comb grids of polybv styrene. Transmission losses are given at 0.5 dB per 100 layers at X-Band frequencies and the bandwidth is extremely wide. The density of the composite material is only one-fifth that of the natural dielectric.

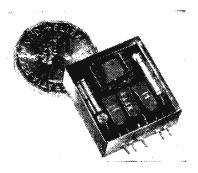
According to Mullard, a reasonably cheap way of constructing intricate sections of waveguide is to use a plastic form, give it a 40-thou. coating of silver, dissolve out the plastic and, after adding flanges and other items, fix it to a steel supporting yoke. Other examples of waveguide components were shown by Hilger and Watts and by Sanders Electronics; the latter firm had some improved versions of their "inexpensive" X- and J-Band (8 to 12 and 12 to 18 kMc/s repectively) waveguide test benches.

Materials with a high absorption characteristic over the range 2.5 kMc/s to 50 kMc/s are being produced by Plessey mainly for micro-"darkroom" applications. Grade AF10 and Grade AF11 are a kind of foam rubber made in 1-ft squares with one surface of cellular The cells provide a formation. graded transition from the impedance of free space to that of the highly attenuating material, and over the 10- to 50-kMc/s band absorption is of the order of 99.7%. A loaded rubber material, Grade M, is also available for shielding radomes when bench-testing radar scanners.

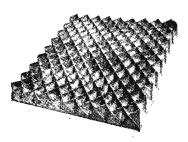
Transistor Components.—Further miniaturization of transistor components was the key-note of Fortiphone's exhibit this year. Encapsulation in epoxy resin is used extensively and, as an example of what can be achieved in this way, there was an encapsulated three-stage transistor a.f. amplifier which would lie on a penny without overhanging the rim of the coin. A new "Z" series transformers measures only  $0.575 \times 0.25 \times 0.25$  in overall and production has been made possible by a new technique in winding fine wires, such as No. 52 s.w.g.

Extension of the Plessey series of tantalum electrolytic capacitors now brings six different sizes into the transistor category. These range in size from a button type, no larger than a sixpence, to a tubular style of 0.08 in diameter and 0.1 in long. Capacitance range is from 0.25 to 750 µF and from 3 V working to 70 V with numerous intermediate values and working voltages.

Miscellaneous Equipment.—Two items of equipment not fitting into any particular category in this exhibition was a Radyne 1-kW induction heater, for "firing" the getter in thermionic valves and heating the electrodes during the "pumping"



Sub-miniature three-stage transistor a.f. amplifier (Fortiphone).



Plessey microwave absorbing material, Grade AF11.

process. A u.h.f. mobile radio-telephone for use in the 450- to 480-Mc/s band, made by Elliott, operates on a single crystal-controlled frequency. The transmitter output is between 10 and 20 watts, according to the radiated frequency, and the receiver is a double super-hetrodyne.

#### COMMERCIAL LITERATURE

Electronically Changed Transformer Taps to reduce the effect of mains voltage variations are discussed in a leaflet from Claude Lyons, Ware Road, leastet from Claude Lyons, Ware Road, Hoddesdon. Input changes of up to -20% or +10% from the nominal value are reduced to within ±5% of this value. The waveform is not distorted, and control is unaffected by frequency variations from 45 to 65 c/s. Alternative ratings of 2½ and 5 amps are available, and the power consumption is only 15 watts.

Quartz Crystals and Temperature Controlled Ovens in many different ranges are the subject of a leastet from Bulova Watch Co., 62-10, Woodside Avenue, New York. Individual frequencies range from 16 kc/s to 100 Mc/s and include standard crystals from 140 kc/s to 250 kc/s. Two of the six

and include standard crystals from 140 kc/s to 250 kc/s. Two of the six ovens permit control to within ½°C.

ovens permit control to within  $\frac{1}{2}$ °C.

Two Transistorized p.a. Amplifiers giving 10 or 15 watts output at 15 ohms impedance for 5 mV low impedance input are described in a leaflet from Lustraphone, St. Georges Works, Regents Park Road, London, N.W.1. Power consumption for either amplifier ranges from about  $2\frac{1}{2}$  watts (quiescent) to 20 watts (peak). The size is  $5\frac{3}{6}$ in ×  $3\frac{3}{6}$ in and the weight  $3\frac{1}{2}$ lb. New

microphones are described in another leaflet from the same company. These include a tubular hand microphone for close-talking in high ambient noise.

Kit-Model Oscilloscope and Valve Voltmeter are described, with very full constructional details, in two brochures from Cossor Instruments, Highbury Grove, London, N.5. The oscilloscope P-amplifier sensitivity is variable up to 50 mV/cm with offerences response. 50 mV/cm with a frequency response 3 dB down at 5 c/s and 3 Mc/s. A calibrating voltage at 50 c/s is available. The valve voltmeter has fullscale ranges from 1.5 to 1,500 volts d.c. or a.c. As an electronic ohmmeter it or a.c. As an electronic ohmmeter it measures  $0.1\Omega$  to  $1,000\,\mathrm{M}\Omega$  with internal battery. On ranges up to 150 volts the frequency response is from 40 c/s to 1 Mc/s within  $\pm 10\%$ . Plugs and Sockets of the miniature "Jones" type. A new range under the name "Multicon" incorporating

many improved features is described in a comprehensive illustrated catalogue from Painton and Co., Kingsthorpe, Northampton.

Nickel Plating for engineers. A useful illustrated booklet of 72 pages, including surface preparation, commonly used solutions, plating procedures, plant required and mechanical properties of deposits and methods of testing them. From The Mond Nickel Company, Thames House, Millbank, London,

Marine Radiotelephones, suitable for small craft, incorporating direction finders and Consol meters. Transmiter: 17 watts output, crystal controlled on any eight channels between 1.6 and 6Mc/s. Receiver: sensitivity 8 V for 2019. 20dB signal/noise; d.f. facilities on all wavebands 150kc/s-3.8Mc/s. Equip-Equipment operates from 12V or 24V teries. Details on leaflets from Wood-son's Marine Radio Manufacturers, Details on leaflets from Wood-Greenbank Road, Aberdeen.

Rectiilinear Galvanometer Recorder, with two independent galvanometers and inking systems for side-by-side recording of two variables on a common time base. Sensitivity: 0.45in/100µA. Pen speed: 0.25sec/f.s.d. Ten chart speeds are available. Folder from Texas Instruments, 3609 Buffalo Speedway, Houston, Texas, U.S.A.

Potting Service, for development and production of resin-encapsulated electronic circuits and components.

tronic circuits and components, is out-lined in an illustrated brochure from Lion Electronic Developments, Lion Works, Hanworth Trading Estate, Feltham, Middlesex.

Wireless World, May 1957

#### ESPECIALLY OF INDUCTIVE CIRCUITS

O tell the truth, this was to have been "Blocking Oscillators." The general idea was that a blocking oscillator circuit, which looks one of the simplest oscillator circuits known, is made up of still simpler combinations of resistance and capacitance or resistance and inductance, whose principles are very familiar. By first quickly reviewing these principles, the explanation of the complete blocking oscillator circuit was to have been rendered foolproof (if you will pardon the implied insult).

In spite of the fact that the more knowledgeable the authority the worse the reputation he gives the blocking oscillator for obscurity, this is still roughly my plan. Where it came unstuck in detail was that some of the principles of simple combinations of resistance and inductance turned out to be considerably less familiar—to me, anyway—than I had supposed. So much so that I have had to abandon the quick preliminary review idea and expand it into a full topic, postponing the blocking oscillator until next time.

You will have noticed that I still reckon the behaviour of combinations of resistance with capacitance as familiar. But in case I am wrong about this—and for the sake of comparison with the inductive counterparts—I am going to review it all the same. There are various ways of doing it, but for the purpose in mind I think it will be best to look at the arrangement shown in Fig. 1.

Here C is supposed to start uncharged, at  $v_0 = 0$ . Unlike resistance, across which a voltage can jump instantly from one value to another, the voltage across a capacitance can only change gradually, as a result of a transfer of energy to its electric field, caused by the flow of current into it for a period of time. So immediately the circuit has been closed by moving the switch to A,  $v_0$  is still nil. The whole of V is therefore free to drive current through  $R_1$  and the amount of this current can be calculated by what is commonly though not very correctly referred to as Ohm's law— $i = V/R_1$ . This current starts to charge C, so  $v_0$  begins to build up.

Capacitance has its own "Ohm's law," namely, that the voltage across it due to Q amp-seconds that have flowed into it is Q/C. If our charging current

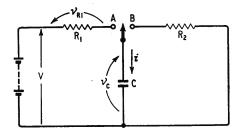
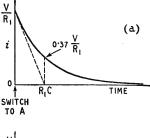
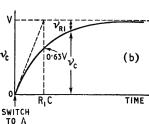


Fig. 1. The first experiment: C is charged by switching to A and then discharged by switching to B.

Fig. 2. Time curves of (a) current into and (b) voltage across C in Fig. I from the moment of switching to A. After a period equal to R<sub>1</sub>C (the "time constant") the charging process would have been completed if the starting rate had been kept up.





 $V/R_D$ , continued steadily for t seconds, C would thus be charged to

$$\frac{V/R_1 \times t}{C}$$
 volts

So we can calculate the particular time T which would have to elapse for C to be charged up to the full applied voltage V:

$$\frac{VT}{R_1C} = V$$
$$\therefore T = R_1C$$

This time T, sufficient for a capacitance to charge fully to any voltage applied through a resistance, if the starting current were maintained, is what is called the time constant; as we see, it is equal to the capacitance multiplied by the resistance, in ohm-farads or megohm-microfarads to give seconds.

Obviously the starting current is not maintained, for directly  $v_0$  begins to grow there is that much less of V to drive current through  $R_1$ . When C is half charged, only half V is available, so the current and hence the rate at which  $v_0$  grows is half what it was at the start. The graph of the current i thus has the peculiarity that the steepness of its slope at any point is proportional to its height at that point, as in Fig. 2(a). The name for this peculiarity is exponential. Its mathematical equation (but don't bother about it if you don't want to, for we shall not be using it) in this case is

$$i = \frac{\mathbf{V}}{\mathbf{R}_1} e^{-\mathbf{t}/\mathbf{R}_1 \mathbf{O}}$$

where e is the base of natural logarithms (2.718...etc.). According to the late Dr. Ohm, the voltage across a constant resistance is directly proportional to the current through it. Consequently the i curve, Fig. 2(a), will do also (to an appropriate scale) as a curve

of  $v_{R1}$ , the voltage across  $R_1$ . This is economy of effort.

The advantage of having a curve of  $v_{\rm R1}$  is that because  $v_{\rm R1}$  and  $v_{\rm C}$  everywhere add up to the constant voltage V, which is equal to the starting value of  $v_{\rm R1}$ , a curve of  $v_{\rm C}$  (Fig. 2(b)) can be obtained by the simple operation of turning the  $v_{\rm R1}$  curve upside-down. This is another economy of effort. The  $v_{\rm C}$  curve helps one to visualize the charging process, for it shows how V is shared from moment to moment between C and R<sub>1</sub>: at first, entirely across R<sub>1</sub>; then increasingly—but at a reducing rate—across C.

In both parts of Fig. 2 the starting slope of the curve is shown continued as a dotted line, to indicate the time constant,  $R_1C$  seconds. It turns out that in that time the curve has always gone just over 63% of the way towards its destination, leaving nearly 37% to go. In twice the time  $(2 R_1C)$  the  $v_0$  curve has  $0.37^2V = 0.135V$  left to go; in  $3R_1C$ ,  $0.37^3V = 0.05V$ ; and so on.

The gap never completely closes, but when it has become negligible we flip the switch over to B. The voltage applied through  $R_2$  is zero, so  $v_0$  (starting practically equal to V) changes via another exponential curve towards that value, as we see in Fig. 3(b). For the fun of it I have made  $R_2$  greater than  $R_1$ , so the time constant is greater, and more time is taken to go the statutory 63% of the way from starting to finishing voltage. Nevertheless, this dieaway or discharge has the same shape as the build-up, differing only in horizontal scale and in being upsidedown.

The discharge current, too, has the same shape as the charge, but because the current is in the opposite direction it must be reckoned negative (Fig. 3(a)). And besides the change of horizontal scale there is a change of vertical scale, for the higher resistance means less current.

So much for capacitance and the building up and releasing of its electric field. When we considered duality\* I mentioned that the great advantage of the idea was that it gave two sets of information for the price of one. (More economy of effort.) Having taken the trouble to work out what happens in circuits combining resistance and capacitance, say, one doesn't have to think it all out again for resistance and inductance. Inductance being the "dual" of capacitance, one can use the same formulæ, curves, etc., after having made the necessary exchanges with the other duals involved; e.g., current for voltage, and series for parallel.

This being so, there might seem to be little excuse for the principles of RL circuits being less familiar than the RC principles just reviewed. however, there are several excuses, not counting the one that lots of people still don't know about this new-fangled duality (actually, like most things, quite old). For instance, a strict dual of the circuit in Fig. 1 is not really practicable. In Fig. 1 there is no great difficulty in switching the charged C from A to B without anything much happening to it en route. But to transfer its dual—an inductor magnetized by current-intact from one circuit to another it is necessary to short-circuit it in such a way that the total resistance is zero. But whereas it is possible in practice to have a good approximation to a capacitance with no shunt conductance, one can only get a good approximation to an inductance with no series resistance by reducing its temperature to nearly 273°C below zero, which is inconvenient.

Yet another complication is mutual inductance, which has no counterpart on the capacitive side.

Still, we shall be able to trace an analogy with at least the first part of the Fig. 1 experiment if we adopt the arrangement shown in Fig. 4. With C we started from the fact that the voltage across it cannot be changed instantaneously; it is a measure of its electric field and has to be built up by current flowing in for a period of time. With L, the current through it cannot be changed instantaneously; it is a measure of its magnetic field, and has to be built up by applying an e.m.f. for a period of time. So immediately the switch in Fig. 4 has been closed there is no current through L. Consequently there is no current through R<sub>1</sub>, so no voltage drop across it, so the whole of V appears across L. That makes current begin to flow, and the current creates a magnetic field. The growth of this field induces a back voltage, which is the only thing the voltage applied to L So the current automatically grows has to face. at the rate which induces a voltage equal and opposite to the applied voltage. The inductance L in henries means the number of volts it induces when the current is changing at the rate of 1 amp, per second, or

 $V = L \times amps per sec$  So the current starts growing at V/L amps/sec.

Obviously it can't grow beyond  $V/R_1$  amps, because the whole of V would then be occupied in driving it through  $R_1$  and there would be nothing to spare for L. Let T be the time required for the

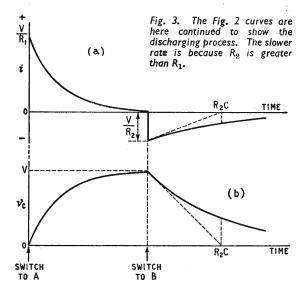


Fig. 4. Inductive counterpart of the first phase of the Fig. I experiment.

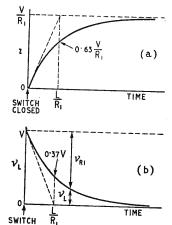
<sup>\*</sup>April 1952 issue, or Chap. 35 in "Second Thoughts."

Fig. 5. These current and voltage curves for Fig. 4 are the same as the voltage and current curves for Fig. 1 (shown as Fig. 2).

current to grow from nothing to this full amount  $V/R_1$ , if it were to keep up its starting rate, V/L. Then the rate of growth is equal to  $V/R_1$  divided by T:

$$\frac{\mathbf{V}}{\mathbf{L}} = \frac{\mathbf{V}}{R_1} / \mathbf{T}$$

$$\therefore \mathbf{T} = \frac{\mathbf{L}}{R_1}$$



This, then, is the time constant for the growth of current in a circuit consisting of L and R<sub>1</sub>. Note that the greater the resistance the *shorter* the time for the current to reach its full amount at the starting rate.

Just as the voltage across C could not keep up its starting rate of growth, but eased off into an exponential curve, so with the growth of current in L. Fig 2(b), in fact, would do equally well as a graph of current growth in an inductive circuit. And correspondingly Fig. 2(a) could just as well be a graph of voltage across the inductance during the same period. Clearly T is now the time for the current to reach 63% of its full value, or the transient inductive voltage to decline to 37% of its peak. For comparison with Fig. 2, the LR<sub>1</sub> circuit curves are shown in Fig. 5.

If we try to duplicate the second part of the Fig. 1 experiment with inductance we get into difficulties. Opening the switch in Fig. 4 would (theoretically) make the current change abruptly from its full V/R<sub>1</sub> amps to zero, which is what I said was impossible. It is impossible because an infinite rate of change of current would induce an infinite voltage. What happens in practice is that the voltage rises enough to produce a spark or arc at the switch points, which prolongs the decay of current for a short time after they have separated. If the inductance and the current are large, so that a lot of energy is stored, the result will be spectacular. I remember once in student days pulling out a plug connecting d.c. to the field windings of a large dynamo. If I had happened to be holding the metal parts with bare hands it would probably have been fatal. Nowadays the effect is employed to advantage in generating the thousands of volts needed for the cathode-ray tube in the domestic television set.

As already mentioned, the strict dual of the Fig. 1 circuit is impracticable, because it is not possible to have inductance even approximately devoid of resistance. Short-circuiting a real inductor doesn't keep the current flowing through it indefinitely, as it would it there were no resistance. So the usual Part 2 of the story is to suppose that V suddenly ceases to function, allowing L to "discharge" through R<sub>1</sub>. The result, of course, is an exponential decline in current, this current being driven through R<sub>1</sub> by the inductive "kick" caused

by that decline of current making the magnetic field linking L collapse. Having already extended Fig. 2 into Fig. 3, you should have no difficulty in extending Fig. 5 to cover this phase of operations, even if you didn't already know it. The time constant, of course, is unchanged, so except for being inverted the curves for this second phase are exactly the same as for the first.

Seeing that all real inductors have some resistance, it will be worth a few moments to consider what effect this resistance has on the voltage waveform one would actually observe in practice. In Fig. 6 the theoretical Fig. 4 is brought nearer reality by inserting r to represent the resistance of the coil. If could of course represent any added resistance as well. Clearly the current curve has the same shape as before, since r might be part of  $R_1$  for all the current knows about it. But to  $v_L$  shown in Fig. 5(b) there must be added a component proportional to the current i, as in Fig. 7(a).

If there were some inductance mixed up with  $R_1$ , its voltage waveform would cease to be an exact copy of the current, Fig. 5(a), and would be mixed with some of Fig. 5(b), as in Fig. 7(b). In fact, if the time constant of  $R_1$  and its inductance were made the same as that of r and L, the voltage waveforms of both would be flattened out, free of any transients, just as if there were no inductance anywhere, notwithstanding that the current waveform would still grow exponentially from zero.

And now we come to the bits that may not all be quite so familiar. For dealing with the blocking oscillator we shall have to take account of what happens when there is another circuit inductively coupled. To simplify matters let us suppose that the second coil in Fig. 8 has the same number of turns as the first, and that the coupling is 100%, which means that all the magnetic flux due to

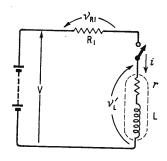


Fig. 6. A real inductor includes some resistance, shown here as r, as well as inductance L.

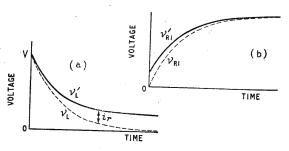


Fig. 7. (a) Showing how the curve of voltage across inductance (Fig. 5(b)) is modified by the resistance r in Fig. 6. (b) If some inductance were to be added to  $R_1$  in Fig. 4, the curve of voltage across it  $(v_{\rm R}_1)$  would be modified to such as  $v'_{\rm R}_1$ .

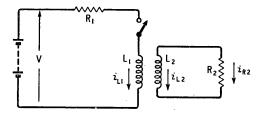


Fig. 8. Addition of a resistance-loaded secondary coil to the Fig. 4 experiment.

current in one coil links both equally. In practice this condition can be nearly attained by using a high-permeability closed iron core. (The amount of magnetic flux is then not strictly proportional to the current, but for our simple study we shall assume that the current is not large enough for this effect to be important.)

Suppose we now set up a voltage across  $L_1$ , say by closing the switch and starting a flow of current. The voltage thereby induced in  $L_2$  causes current to flow through  $R_2$ . This current also flows through  $L_2$ , and affects the flux and therefore the voltages induced. It looks as if we are faced with a vicious circle which will make calculating the upshot of the whole thing very complicated.

Thanks to our forethought in choosing equal turns and 100% coupling, however, it is actually quite easy. The result of these conditions is that whenever the amount of flux in the core changes, the change affects both coils equally, inducing equal voltages in them. And the flux that does this is not due to current in either coil separately, but the resultant of both currents. So it makes no difference to the behaviour of the system shown in Fig. 8 if the two coils are merged into one, as in Fig. 9. True, we can no longer distinguish between the two currents actually flowing in  $L_1$  and  $L_2$ ; we now know only the resultant of both, but since that is what creates the magnetic flux it is all we need. For example, if the current through L1 at any given moment is 3A and the current through L<sub>2</sub> is -2A (i.e., 2A in the direction opposing the flux due to the 3A), the equivalent is 1A through L. Note that the -2Ain L<sub>2</sub> goes through R<sub>2</sub> in the same direction as if +2A came direct from the source of the 3A, as shown in Fig. 10.

This amalgamation dodge is a great help. Instead of having to embark on a tricky lot of calculations, with secondary current affecting the flux due to the primary and hence the induced voltage, etc., we can see at once that when the switch in Fig. 9 is closed (and before current has had any time to build up through L) the current  $i=i_{\rm R2}={\rm V/(R_1+R_2)}$ , and the voltage  $v_{\rm L}$  is  ${\rm VR_2/(R_1+R_2)}$ .  $R_1$  and  $R_2$  act simply as a potential divider. After a long time, when the current through L is fully grown, so that the voltage across it—and of course across  $R_2$ —has died down to zero, V is occupied solely against the resistance,  $R_1$  so  $i=i_{\rm L}={\rm V/R_1}$ , and  $i_{\rm R2}=0$ . So the finishing line for current is the same as in Fig. 5(a), but the starting line for voltage is lower than in Fig. 5(b).

The only other thing we need know in order to complete the curves as modified by  $R_2$  is the time constant. Before going any farther, try guessing how  $R_2$  will affect it. My first line of argument was that loading a transformer secondary with resistance

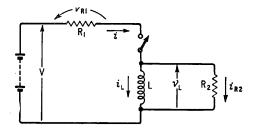


Fig. 9. On the assumption that  $L_1$  and  $L_2$  have equal numbers of turns, coupled 100%, Fig. 8 can be simplified by merging the two coils into one, as here.

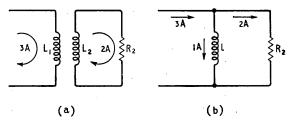
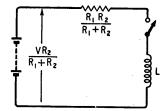


Fig. 10. This comparison shows how opposing currents through  $\rm L_1$  and  $\rm L_2$  are equivalent to their difference flowing through  $\rm L$ .

Fig. 11. For purpose of calculating the time constant, Fig. 9 can be further simplified by Thévenin's theorem to the same circuit as Fig. 4 but with different values.



makes the whole thing less inductive from the viewpoint of the supply; time constant is proportional to inductance, so connecting R<sub>2</sub> shortens it. Well, let's see.

But how? Even the simplified equivalent circuit, Fig. 9, doesn't give a very obvious lead towards how to set about it. Fortunately the problem is an easy one-if we remember Thévenin's theorem\*. According to this, the system to which L in Fig. 9 is connected can be replaced (so far as L is concerned) by a simple source and series resistance exactly as in our original inductive circuit, Fig. 4, in fact—in which the voltage of the source is what appears across the gap when L is removed, and the series resistance is the resistance that would be measured across that gap if any e.m.fs. ceased to act. We have already calculated the equivalent source voltage; it is of course the proportion of V that appears across the  $R_2$  part of the potential divider  $R_1 + R_2$ ;  $VR_2/(R_1 + R_2)$ . And the measured resistance is  $R_1$  and  $R_2$  in parallel:  $R_1 R_2/(R_1 + R_2)$ . So the circuit which is equivalent to Fig. 8 for the purpose of calculating the time constant is Fig. 11. Instead of L being divided by R<sub>1</sub> as in Fig. 4 it is divided by R<sub>1</sub> and R<sub>2</sub> in parallel—a lower resistance -so is greater as a result of connecting R2. I still find this rather surprising.

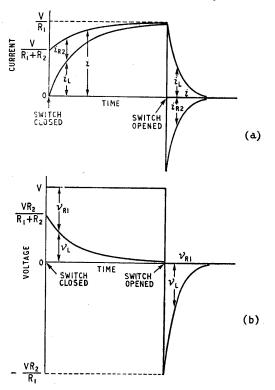
Although Fig. 11 is equivalent to Fig. 9 or 8 when the switch is closed, it obviously isn't when the switch is opened; for further consideration of our

<sup>\*</sup>March 1949 issue, or Chap. 32 of "Second Thoughts".

loaded transformer we revert to Fig. 9. You will remember that we couldn't draw curves or do any thing definite like that about the consequences of open-circuiting the simple inductor in Fig. 4, because theoretically it is impossible. The current through an inductive circuit cannot be changed instantaneously from one value to another. same applies when L2 is added. But when R2 is connected, Fig. 9 makes clear that the current through the inductor doesn't have to change suddenly even when the switch is flicked open; it can continue flowing—through R<sub>2</sub>. In fact, adding L<sub>2</sub> and R<sub>2</sub> to Fig. 4 provides a close analogy with the two-way switching in Fig. 1; the effective "charging" resistance in the "make" position is R<sub>1</sub> and R<sub>2</sub> in parallel, and the "discharging" resistance in the "break" position is  $R_2$ . The only thing is that the time constant in the second position is bound to be shorter, whereas with Fig. 1 we could do as we pleased.

If we look again at Fig. 8 instead of Fig. 9 we realize now that the current through  $L_1$  can cease instantly, without any nonsense about an infinitely high induced voltage. This is the second possibly surprising thing, because at first glance it seems to contradict a basic principle. It probably has a bearing on perplexities experienced in the study of blocking oscillators and pulse circuits generally. The explanation of the paradox, of course, is that the cutting off of current through  $L_1$  is exactly neutralized by an equal and opposite current change in  $L_2$ . In terms of Fig. 9, it means that there is no sudden change of current through L. Another way of putting it is that the magnetic energy built up by current in one winding of an inductor, and which would manifest itself as a flash or shock or the like if

Fig. 12. Current and voltage curves for the Fig. 9 circuit.



dispersed abruptly, can be safely and silently "discharged" by a pulse of current entirely in a separate winding.

Although so far everything has been going very smoothly, it is quite easy to trip up over the details; and as this is going to be the crux of the matter next month it will be worth recording graphically what we have found about the whole Fig. 8 experiment.

First of all we shall do it on the basis of the simplified circuit, Fig. 9, and then analyse the combined current through L into its separate  $L_1$ 

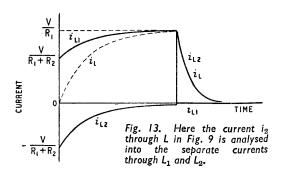
and L<sub>2</sub> components.

Let us deal first with the "switch closed" phase. We know (from Fig. 11) that the current  $i_L$  through L begins from zero and rises exponentially towards  $V/R_1$  with a time constant  $L(R_1 + R_2)/R_1$   $R_2$ , so that can be plotted (Fig. 12(a)). The corresponding voltage  $v_L$  can then be plotted, for the time constant is of course the same, and the starting point is  $VR_2/(R_1 + R_2)$ . Having settled L we must shift our attention back to Fig. 9 for  $R_1$  and  $R_2$ . Voltage V is easy, because it is constant. And the difference between V and  $v_L$  gives us  $v_{R1}$ . That completes the first half of the voltage diagram, Fig. 12(b). The current i follows from  $v_{R1}$ , being directly proportional to it (=  $v_{R1}/R_1$ ), so we can plot that. And since  $i_{R2} = i - i_L$ ,  $i_{R2}$  appears in Fig. 12(a) as the difference in level between the already plotted i and  $i_L$  curves.

Before opening the switch let us analyse  $i_{\rm L}$  into  $i_{\rm L1}$ , and  $i_{\rm L2}$ . This is easy if we remember that  $i_{\rm L1}$  is i (see Fig. 8) so can be plotted in Fig. 13 direct from Fig. 12(a). And  $i_{\rm L2}$  is minus  $i_{\rm R2}$ , so can also be derived from Fig. 12(a), or alternatively from the definition of  $i_{\rm L}$  as  $i_{\rm L1}+i_{\rm L2}$  (Fig. 10), curves of  $i_{\rm L}$  and  $i_{\rm L1}$  being already available. The interesting thing to note is that current springs instantaneously to the value  $V/(R_1+R_2)$  in both coils  $L_1$  and  $L_2$  directly the switch is closed; this is possible because the magnetizing effects of these currents exactly cancel out. Magnetic flux then grows gradually owing to  $i_{\rm re}$  increasing and  $i_{\rm re}$  dying away.

owing to  $i_{\rm L1}$  increasing and  $i_{\rm L2}$  dying away. When the switch is opened, i promptly ceases and remains ceased. So that current is easily shown in Fig. 12(a). And so is  $v_{\rm R1}$ in Fig. 12(b). The current flowing through L must at first be the same as it was just before the switch was opened —practically= $V/R_1$ . It declines exponentially to zero, with a time constant that is clearly  $L/R_2$ . That is less than with the switch closed, so we must show it dying away quicker than it grew. And because  $i_{\rm R2}=-i_{\rm L}$  we plot it as a perfect reflection of  $i_{\rm L}$ .

Right at the end there is a possible catch—or



even two catches—if we are over-confident. Our  $v_L$  is clearly the same thing as the voltage across  $R_2$ , and that (as every student of Ohm knows) is exactly proportional to  $i_{R2}$ , which we have plotted. So we must give  $v_L$  the same shape. But seeing  $i_L$  positive in Fig. 12(a), and perhaps with  $i_{R2}$ = $-i_{L2}$  still (though irrelevantly) in mind, there is just a chance that one might hastily show  $v_L$  positive in the second half, as in the first. If studying the directions of the arrows in Fig. 9 doesn't keep us correct in this matter, the fact that the voltage across L must clearly change sign when increase of flux changes to decrease will surely do so.

Even now one might be tempted to copy the first part of the  $v_{\rm L}$  curve in amplitude, though reversing it in sign. If so, we ought to be warned by seeing the negative "half-cycle" smaller than the positive, owing to its shorter time constant. The truth is, of course, that this shorter time constant means that

the flux is collapsing quicker than it grew, so the induced voltage is greater at "break" than at "make"; and if you work it out you will find that the negative peak of  $v_{\rm L}$  is equal to  ${\rm VR_2/R_1}$ . So what the negative half-cycle lacks in duration it exactly makes up in amplitude. That this is so can be seen even more directly by comparing the amplitude of  $i_{\rm R2}$  at "break" and "make."

The second part of Fig. 13 has no catches, for we have a curve of  $i_L$  in Fig. 12(a), and  $i_{L1}$  is zero all

the time, so  $i_{L2}$  must be the same as  $i_{L}$ .

If you are just beginning to get interested, you could do a little homework for next time by thinking out how these waveforms are modified if the ideal transformer we have been assuming is brought one step nearer reality by making its coupling a little less than 100%. This can be represented by a small amount of uncoupled inductance ("leakage inductance") in series with each winding.

# Third International Instrument Show

Exhibits by 54 Firms from Nine Countries

HIS exhibition of mainly electronic instruments, organized by B. & K. Laboratories, Ltd., differs from the too-many others in the field by its international character. It, therefore, provides an opportunity for inspecting apparatus much of which is unfamiliar, and for making comparisons with home products. The setting this year (March 25-29) at the Caxton Hall, London, enabled the exhibits to be examined in comfort.

The following report is confined to apparatus not seen at last year's Show. The nationality of the firms mentioned, where not stated, is American.

The Ampex Corporation specializes in tape recorders, but in contrast to last year's exhibits of sound recorders mainly for entertainment they demonstrated highly developed machines for data storage. One shown uses half-inch tape, with a choice of six speeds from  $1\frac{7}{8}$  to 60 in/sec, and up to 14 tracks. At the highest speed the frequency response is 100 to 100,000 c/s. By the use of multiplex, over 1,000 channels of simultaneous data can be recorded. In one of several available recording techniques, the small residue of variation inevitable with such a medium as plastic tape is excluded by recording a sinusoidal reference signal, the frequency of which can be stabilized to within almost any desired limits; the recorded data, in the form of frequency ratios relative to this standard, are immune from variations in tape speed. Such recording machines are now being widely used, especially in armament research and in conjunction with computers.

The same firm has produced, but was unable to spare a sample to show, a "Videotape" recorder for television, with a frequency response from 0 to 4 Mc/s. This machine uses 2-in tape at the remarkably low speed of 15-in/sec. Instead of a fixed recording head, producing a longitudinal track, four heads are mounted in a rotating drum and scan the

tape, which is brought into contact with the drum throughout its width. Sound is recorded conventionally along one edge of the tape, and there are two tracks along the other edge for cues and editing markers. The usefulness of such machines in television broadcasting is obvious, and it is understood that six are already on order for Britain.

A large proportion of the Bruel & Kjaer (Denmark) instruments on show were concerned with audio testing. As reported briefly last year, they are especially suitable for performing such tests rapidly and automatically, and this year the range has been extended. One key unit is a continuously motordriven beat-frequency oscillator, 20 to 20,000 c/s, the output of which, through the equipment under test, may be observed on a valve voltmeter scale, a longpersistence c.r. screen, a cartesian or polar recorded diagram, or any combination of these. Other instruments enable an output or response to be selectively analysed. By means of a mechanical coupling between the oscillator-recorder and a slowly rotating turntable, the automatic plotting of a microphone polar diagram was demonstrated. Reverberation diagrams of an auditorium over the whole a.f. range can be taken completely automatically. Hearing aids can be checked visually and/or on paper for amplitude/frequency characteristics in a few seconds; and, by successively coupling a selective detector to multiples of the source frequency, the various harmonic distortions can also be automatically plotted. One of the completely new instruments was for measuring the acoustic absorption coefficients and complex impedances of materials by standing waves in an acoustical transmission line.

Signal analysis by frequency scanning was shown by Panoramic Radio Products and by Kay Electric Co. The former have three models of scanning superhet receiver, with band frequencies of 200 kc/s, 1 Mc/s and 10 Mc/s; and the latter a sweeping oscillator within the band 10 to 350 kc/s, the repetition frequency being adjustable from 0.5 to 2 c/s.

Testing of the ability of electronic equipment to stand up to vibration is now of great importance, and perhaps the most massive exhibit in the Show was a "vibration exciter" by M. B. Manufacturing Co., capable of imposing a test force of up to 3,500lb over the range 2 to 2,000 c/s. This is not the largest by this firm, however; one model is rated at 12,500lb over the same frequency—nearly six tons!

Humidity is another factor in equipment testing, and hygrometers for measuring it are not on the whole very satisfactory. The introduction by El-Tronics of a plastic whose electrical resistance is proportional to relative humidity, the temperature coefficient being quite small, is, therefore, most interesting. Hygrometers embodying it were shown.

Work on colour television necessitates accurate measurements of phase angle. This is one important use of the Type 205A phase detector by Advance Electronics. A variable delay line is used to delay the unknown for a sufficient time to obtain a reading on an output indicator. The unknown phase angle or time delay is read off the dials of the delay line.

For providing action delay of the order of seconds, the relays by Electronic Speciality Co. are useful. They are available in three classes: less than 0.5 sec,

0.5 to 5 secs, and over 5 secs.

A number of new voltage stabilizers were to be seen, one by H. Struers (Denmark) being unusual in providing an electronically stabilized source of a.c. for heaters, etc., up to 4-5 amps in the range 5.8 to 8.2 volts, to limits of 3-4 mV. An h.t. stabilizer was convincingly demonstrated by rapidly varying the input voltage over 20 volts or more and showing that the variation in output voltage was 1 mV or less; this is achieved by a combination of saturated-iron and electronic techniques.

saturated-iron and electronic techniques.

The well-known "Unipivot" range of instruments by the Cambridge Instrument Co. (U.K.) has been extended by a r.f. milliammeter for use up to 10 Mc/s, having five vacuo-junctions selected by a

range switch without breaking the circuit.

Valve voltmeters shown last year were notable for low ranges—in one case reading down to fractions of a microvolt. This time attention was attracted by a model with five ranges, the lowest f.s.d. being 5 kV and the highest 100 kV. The most impressive parts, not surprisingly, are the terminals; they are both of e.h.t. type, for the instrument is arranged to measure the vector sum of two phases.

It was unfortunate that customs difficulties held up the appearance of a decade resistance box by Electro-Measurements, for they have brought a new look to this usually stereotyped piece of equipment by arranging as many as six decades concentrically. The dials can thus be easily handled and read off,

and much panel space is saved.

Progress in design and applications of transistors was noticeable; for instance, germanium tetrodes by Texas Instruments with a cut-off frequency as high as 200 Mc/s, and silicon transistors by this firm and also by Raytheon.

In the valve department, the most interesting examples were some of the types for microwaves. Several travelling-wave tubes for S-band and X-band were shown by Huggins Laboratories with a small-signal gain of 30-35 dB over a 2:1 frequency

band. The Sperry t.w. tube for the L-band (around 1,300 Mc/s) has a peak output of 7 kW, at which the gain is 34 dB. Sperry also showed a klystron power amplifier with a peak output of 15 kW at 2,700-2,900 Mc/s and examples of the new uses of ferrites in microwave circuits.

Other interesting microwave equipment included the standing-wave detector, by the P.R.D. Co., for 100 to 1,000 Mc/s. Instead of the lengthy slotted line usually needed for these frequencies, it is a compact unit weighing only 4½lb, consisting of a coaxial tee junction, a manually driven pick-up probe assembly and a normalizing standard reactance. The angle of reflection coefficient is directly read off a dial after it has been set to minimum indication on the associated meter. The De-Mornay Bonardi range of microwave equipment was notable for the very high frequencies provided for—from 5,800 to 90,000 Mc/s.

A noise-factor meter for both low and high radar frequencies was shown by Magnetic AB (Sweden). The source of noise is, for 5 to 300 Mc/s, a noise diode, and for 1,200 to 12,400 Mc/s a gas discharge tube. The source is electronically switched on and off, and the noise fed into the amplifier under test. A train of pulses of two different amplitudes, corresponding to noise-on and noise-off, is obtained, and the amplitude ratio is measured by an indicator directly calibrated in noise-factor dB. In this way it is possible to adjust equipment to minimum noise

CLUB NEWS

Birmingham.—J. Walker (G5JU) will demonstrate the Eddystone 888 receiver to members of the Midland Amateur Radio Society on May 21st. Meetings are held on the third Tuesday of each month at 7.30 at the Midland Institute, Paradise Street. Sec.: C. J. Haycock (G3JDJ), 360, Portland Road, Birmingham, 17.

Bury.—At the May 14th meeting of the Bury Radio Society M. Barnsley (G3HZM) will give a talk on direction finding. The club meets on the second Tuesday of each month at 8.0 at the George Hotel, Kay Gardens. Sec.: L. Robinson, 56, Avondale Avenue, Bury, Lancs.

Derby.—The Derby and District Amateur Radio Society's programme for May includes an open evening, sale of surplus gear, a visit to a place of interest, and the showing of the Mullard film strip "Indicating Instruments." Meetings are held each Wednesday at 7.30 at 119, Green Lane. Sec.: F. C. Ward (G2CVV), 5, Uplands Avenue, Littleover, Derby.



ARMORIAL BEAR-INGS have been granted to the British Institution of Radio Engineers. The shield, which is sur-mounted by the head of Mercury, alludes to Clerk Maxwelland Hertz and the subporters to the 7th Duke of Devonshire (who endowed the Cavendish Laboratory, Cambridge) and Earl Mountbatten, vice-president of the Institution since 1950.

# Airborne Doppler Navigation

Radio Application of Well-known Sound Effect

By G. E. BECK\*, B.Sc.(Hons.), A.M.I.E.E.

HE classical method of navigation is by steering a compass course, and using the ship's measured rate of progress along that course to fix its position. Allowance for the effects of sea currents and wind is based on their estimated values, and is corrected by occasional observations of the sun or stars. This is the "dead reckoning" which is always adequate for long voyages by sea.

When navigating in aircraft there is little time, and often no opportunity, to make the astronomical checks. But the wind velocity is so large a factor that dead-reckoning methods must take it into account. The compass heading differs from the track actually followed by the aircraft, and the speed over the ground is not equal to the speed through the air. Fig. 1 shows the triangle of velocities concerned.

The drift angle may amount to 30° for a moderately slow aircraft flying in a high wind, and so it is necessary to solve the triangle if navigation is to be accurate. The compass heading and the speed through the air are not enough by themselves.

This has led to navigation systems being devised which are based on radio transmissions from the ground, enabling the aircraft to fix its position at frequent intervals. For example; the radio compass giving bearings from m.f. transmitters, or by the hyperbolic systems such as Gee which lay down a signal pattern, and reference to appropriate charts gives the geographical position.

Self-contained Aids.—Difficulties of securing international agreement on the use of any one system, and the large capital cost of ground installations, make the idea of a self-contained navigational system on the classical model very attractive. For military use a ground-based system which would be prone to jamming, or unavailable over hostile territory, is not in any case a satisfactory solution.

One way out of this difficulty is to make use of the principle known as the Doppler effect. This is familiar, as stated by the Austrian physicist whose

<sup>\*</sup> Marconi's Wireless Telegraph Company, Ltd.

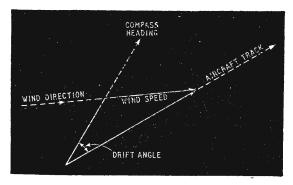


Fig. 1. Triangle of velocities for determining true course of aircraft.

name it bears, as the apparent change in pitch of a vibration, when its source is moving towards or away from the observer. The railway engine's whistle drops its note as the train passes the station and its advancing velocity is changed to a receding one.

In Doppler navigation a radio transmission replaces the sound. It is directed downwards from a radar set on the aircraft and the returned echo has its frequency measured. This frequency will be changed

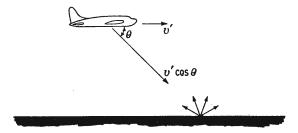


Fig. 2. The ground reflected signal has frequency difference proportional to the component of the aircraft speed in the direction of the radar beam.

from that of the outgoing signal by the Doppler effect, the difference being proportional to the component of the aircraft speed, in the direction of the radar beam<sup>1</sup>. (Fig. 2.)

The speed is that over the ground, which is one missing factor in the solution of the dead-reckoning calculation. The other factor, the drift angle, can be measured by a second beam directed laterally. This will give the sideways component of the aircraft's ground speed. Alternatively, the beam can be rotated until it lies in a direction for which the Doppler effect is a maximum. It must then lie along the track being followed by the aircraft, and the drift angle is directly measured by the azimuth angle between the beam and the aircraft fore-and-aft line. Compass heading, drift angle and ground speed are together sufficient for the navigation problem to be solved. It is in fact not necessary to determine the air speed or wind velocity.

The Doppler Equation<sup>2</sup>.—A picture of the mechanism by which the Doppler effect is produced can be made by referring to Fig. 3, where c is the velocity of propagation. The radar set moving with velocity v towards a target will transmit, in a time t, a wave which occupies a radial distance c.t.

This portion of the wave, which is approaching the target with velocity c + v, will be reflected in a time:—

 $\frac{c \cdot t}{c + v}$ 

<sup>&</sup>lt;sup>1</sup> British Patent No. 638167.

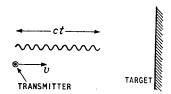


Fig. 3. Mechanism by which Doppler effect is produced.

During this time the radar set will have moved a distance:-

$$\frac{v.\ c.\ t}{c+v}$$

and so the last part of the echo will have this distance less to travel, and will take a time:—

$$\frac{v.\ c.\ t}{c+v}\cdot\frac{1}{c}$$
 less

 $\frac{v.\ c.\ t}{c+v}\cdot\frac{1}{c}\ \text{less,}$  that is, the echo will be received in a time:—

$$\frac{c \cdot t}{c + v} - \frac{v \cdot t}{c + v} = \frac{c - v}{c + v} \cdot t$$

In this time the number of cycles received will be the same as that transmitted in time t. Therefore the frequency observed will be (c+v)/(c-v)times the transmitted frequency.

For a transmitted frequency f, the frequency change is:-

$$\frac{c+v}{c-v} \cdot f - f = \frac{2v}{c-v} \cdot f \approx \frac{2vf}{c}$$

As shown in Fig. 2, the aircraft ground speed is v', where  $v' \cos \theta = v$  and so the measured Doppler frequency is:-

$$f_{\rm D} = 2\frac{f}{c} \cdot v' \cos \theta$$

This is the basic Doppler equation, from which the ground speed is derived by measurement of

 $f_{\rm D}$ . **Practical Figures.**—Some elementary calculations can be made to show the technical problems involved. For shallow angles of incidence  $(\theta)$  only a small part of the incident energy will be scattered back in the direction required for reception, while with a steep angle  $\cos \theta$  will be small, and the value of  $f_{\rm D}$  will be too small for precise measurement.

If  $\cos \theta = \frac{1}{2}$  is a suitable compromise, we have, for an aircraft speed of 600 m.p.h. or 1 miles per second:—

$$f_{\mathrm{D}} = \frac{f}{6 \times 186,000}$$

or about 1 part in 106 of the transmitted frequency

As a direct frequency measurement this would be difficult but by heterodyning the returned echo with the transmitter frequency,  $f_{\rm D}$  can be extracted as a beat note. Taking  $f=5.2\times10^9$  c/s (5.7 cm wavelength)  $f_{\rm D}\approx5$  kc/s, which is an audio frequency capable of precise measurement.

This waveband is a very suitable one in view of its propagation characteristics, the established airborne radars working in it, and the possibility of a narrow beam without excessive aerial size3.

A narrow beam is clearly necessary to give a finite value to  $\theta$  in the Doppler equation. Even with microwaves the width is not likely to be reduced below 3° or 4°, so that the Doppler frequency will not be a single tone, but a spectrum having a width, for a 4° beam centred on  $\theta = 60^\circ$ , of:  $\frac{\cos 58^\circ - \cos 62^\circ}{\cos 60^\circ} = 12\%$ 

$$\frac{\cos 58^{\circ} - \cos 62^{\circ}}{\cos 60^{\circ}} = 12\%$$

The Doppler frequency corresponding to the ground speed will be the centre of this spectrum, and one major technical problem is the measurement of this centre with sufficient accuracy.

Power Requirements.—Assuming a flat earth illuminated at vertical incidence by a transmitterreceiver at height h:-

$$rac{{
m P_R}}{{
m P_T}} = rac{{
m G^2 \lambda^2}}{16 imes \pi^2 (2 h)^2}$$

where

 $P_R$  = power received.

 $P_{\rm T}$  = power transmitted. G = aerial gain.  $\lambda$  = wavelength.

With an aerial gain of 120,  $\lambda = 5.7$  cm, h = 50,000 ft;—

$$\begin{split} \frac{P_{\scriptscriptstyle B}}{P_{\scriptscriptstyle T}} &= \frac{120^2 \! \times \! 5.7^2}{16 \! \times \! \pi^2 \! \times \! 10^{10} \! \times \! 30^{\cdot} \! 4^2} \\ &= \! 3.2 \! \times \! 10^{-10} \! = \! -95 \text{ dB}. \end{split}$$

Due to scattering and oblique incidence on the ground, the received signal will be less than this, and experimental results show4 that the additional loss is of the order of 50 dB.

The total system attenuation is therefore 145 dB at this altitude, and the transmitter power must be sufficient to give a detectable signal in these conditions.

Receiver Sensitivity.—The receiver noise power is  $0.4 \times 10^{-14}$  watts per Mc/s bandwidth. power is produced in the receiver input circuits at room temperature. This must be increased by the noise figure to find the signal required for unity signal/noise ratio at the second detector. Although the post detection signal/noise ratio can be greatly increased in view of the narrow band of audio frequencies which carries the Doppler information, intermodulation noise products prevent a much smaller signal being used.

For a 5.7-cm superhet receiver we assume a noise figure of 13 dB, a bandwidth of 1 Mc/s and the resulting signal power  $(P_R)$  required is  $8 \times 10^{-14}$  watts. The transmitter power is therefore 145 dB above  $8 \times 10^{-14}$  watts, or 25 watts.

Pulse Transmission.—The power suggested is not outside the range of modern microwave c.w. valves, but pulse methods are worth examining, in view of the established techniques using magnetrons for airborne use.

We must have a pulse repetition frequency high enough to avoid false Doppler signals from the p.r.f. or its harmonics. Also the time taken by the pulse to reach the ground and return prevents the echo, and the transmission, from being available simultaneously for the necessary heterodyning to extract the Doppler beat note. This last point is covered if we transmit pulses simultaneously in both forward and backward directions, and obtain the Doppler beat by mixing the two echoes1.

In the forward direction the frequency will be increased, and in the backward it will be decreased, by the amount given in the Doppler equation.

See "Radio and Radar Technique," A. T. Starr, p. 51 (Pitman).
 Hectronics, September 1955, p. 178.

<sup>4 &</sup>quot;Radar Echoes at Centimetre Wavelengths," Davies and Mac-Farlane, Proc. Phys. Soc., 1946, Vol. 58, p. 717.

The beat frequency will thus be twice that in a

"single-ended" system.

Assuming a top speed of 600 m.p.h. the Doppler frequencies will go up to 10 kc/s and the p.r.f. must then exceed 20 kc/s if neither the p.r.f. nor p.r.f. minus true Doppler signal is to give a false signal. This repetition rate is many times higher than in normal magnetron applications, and to avoid over-running the magnetron it has to be considerably de-rated, or run on an intermittent cycle. Twentyfive watts mean power at 20 kc/s p.r.f. with  $\frac{1}{2}$ - $\mu$ sec pulses implies a peak power of 0.6 kW. This is a modest size for airborne pulse magnetrons.

Presentation.—The measured Doppler frequencies can be shown directly to the navigator on a dial calibrated in ground-speed knots, and the drift angle similarly presented if a moving aerial system is used to set the beams along the aircraft's track line as described. Alternatively, if these quantities, together with compass heading, are fed into a simple computer, it will calculate the present position of the aircraft continuously. The results can then be shown as latitude and longitude, if the appropriate values are set in at the beginning of a flight.

For civil use more complex calculations are possible, relieving the navigator of much routine work. On a given flight plan the route and destination can be set in before take-off, and the calculations performed to show continuously distance to destination, departure from track, and estimated time of arrival.

Size and Weight.—An airborne equipment of the form described can be expected to weigh something of the order of 200 lb and consume 1 to 2 kW total power. The aerial system requires a radome, but since the beams are directed wholly downwards the scanner can be mounted within the airframe, with the radome flush with the skin. For the beam width discussed the aperture should not exceed

3ft in any dimension.

Accuracy.—To be of significant value, the computed accuracy of positions found by this deadreckoning technique should be within one or two per cent of the distance travelled. With 1% error, after a 2,000-mile flight the aircraft will know its position within 20 miles. At that stage the local air traffic control will have taken over and the longrange navigational aid is no longer required. A corresponding accuracy of e.t.a. is a major improvement on existing standards, and would greatly help the control of air traffic on the civil airways. But perhaps enough has been said of its possibilities to show that airborne Doppler equipment may be a major factor in long-range navigation.

#### WEATHER AIRBORNE RADAR

Storm Warning Indicator and Navigational Aid

WEATHER radar is an appropriate description for the Bendix Type RDR1 aircraft installation as its primary function is to give information regarding the nature of cloud banks along the flight path and advanced warning of hazardous areas where severe air turbulence is likely to be encountered. A secondary, but no less useful, function is the facility for mapping the ground along the flight path. This equipment was shown at Farn-

brough last year by Elliott Brothers but at the time it was not possible to give any details.

It operates in the X Band (3.2 cm) but, if required, it can be supplied for the C Band (5.5 cm). At these very short wavelengths a sheet of water shows black on the plan position indicator (p.p.i.), while land shows white and the terrain mapping facility provided by the 3.2-cm equipment thus enables rivers, lakes and coast lines, and after some experience mountains and high

ground, to be recognized and identified.

For mapping clouds a pencil beam is employed, but for terrain mapping the beam is converted into a "cosecant-squared" or fan-shaped one. This is effected by changing from horizontal to vertical polarization. Alone this would not affect the beam pattern, as a parabolic-dish scanner is employed. To the upper part of the dish, however, is fitted a grid composed of a series of vertical bars and with vertical polarization they behave as beam-diffusing reflectors, producing a fan-shaped beam in the vertical plane. They are unresponsive to horizontal polarization and the beam shape is then

determined by the characteristics of the dish alone.

Switching from horizontal to vertical polarization is effected by utilizing the Faraday rotation properties of certain ferrites on the application of a magnetic field. In this case the magnetic field is produced by passing a current through a coil wound over a section of the wave-guide feeding the aerial "head." Thus no mechanical switching is involved.

The RDR1 has the "Iso-echo" display feature with which the contour within the cloud where the greatest rainfall gradient prevails is outlined and the area en-closed is displayed on the p.p.i. as a black core. These cores represent the danger regions of the cloud bank to be avoided. This differentiation is achieved by arranging for reflected signals exceeding a certain intensity to show as black patches in the midst of the white patches

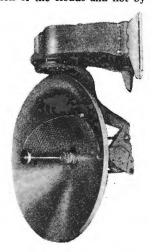
representing normal cloud echo signals.

Other information the aircrew can extract from a weather-radar display is the presence of hail. so correctly requires much experience in interpreting the p.p.i. display, as the presence of hail is deducible only from the edge formation of the clouds and not by

identifiable variation in the intensity of the returned echoes.

A condensed specification of the X-Band equip-ment is: 360° scanner rotation at 15 r.p.m. with 240° p.p.i. display; ±15° maximum vertical beam tilt; 0-20, 0-50 or 0-150 display; nautical miles 40 kW peak pulse power; 1.5µsec pulse 22in-diameter scanner.

The scanner of the Elliott-Bendix airborne weather radar. The grid for producing " cosecont-squared beam for ground mapping is shown.



# Limiting Factors in Gramophone

DEFORMATION AND WEAR OF GROOVE WALLS I.—PLASTIC

HE stylus tip in a gramophone pickup is usually spherical and much more rigid than the record, so that the problems of determining the deformation of the record groove wall have much in common with those associated with hardness tests such as the Brinell, in which a ball is pressed into the surface to be tested. Under light loads any material will deform elastically, giving a small area of contact. On releasing the load the material springs back to its original position undamaged. increasing load, the yield stress of the material will be reached and permanent plastic deformation will begin; on releasing the load the material will not return exactly to its original position, i.e. the record is damaged.

The equations for the elastic range are well known and were deduced by Hertz; they have been expressed in convenient form by Hunt1.

$$p_m = rac{0.45 \; \mathrm{E_1^{\S} \; W^{\S}}}{\mathrm{R}^{\S}}$$
or  $\mathrm{W} = rac{11 \; p_m^{\; 3} \mathrm{R}^{\S}}{\mathrm{E_1}^{\; 2}}$ 

Where  $p_m$  is mean bearing pressure between contacting surfaces in kgm/mm<sup>2</sup>

 $E_1 = E/(1-\sigma^2)$  E = Young's modulus of record material(kgm/mm<sup>2</sup>)

 $\sigma$  = Poisson's ratio of record material

W = Load on stylus in grams

R = Stylus radius in mils (0.001in).

Because of the complex stress system, yielding occurs at a value of  $p_m=1.1$  times the simple tensile or compressive yield stress of the material. Hunt<sup>1</sup> quotes 11 milligrams as the limiting load for no plastic deformation for a stylus of 1-mil radius on vinyl. Although the stylus is supported by both groove walls at low signal levels, at extreme amplitude or acceleration one wall will be taking most of the load. As this is applied at about 45° to the surface, the playing weight must be increased by  $\sqrt{2}$  before yielding can commence, i.e. to about 16 milligrams. In a modulated groove the stylus is in contact not with a flat surface but with concave and convex groove walls. This would reduce the load required for yielding by a factor of 0.77 if the driving wall were convex and the trace radius approached the stylus radius. However, at high frequencies where the trace radius may be small the inertia of the pickup will be a controlling factor rather than the stiffness, so that the load will be taken entirely by the concave outer wall (Fig. 1).

As the load on the indenter (stylus) is increased beyond the elastic range, yielding occurs not at the surface but below, at a distance of about half the radius of the circle of contact. With further increase in load, deformation will gradually spread throughout the area under the indenter. Eventually,

<sup>1</sup>Hunt, F. V. J. Audio Eng. Soc., Vol. 3, No. 1, Jan. 1955. <sup>2</sup>Davies, R. M. Proc. Roy. Soc., Vol. 197, A1050. 22 June 1949

plastic deformation of the surface will commence at the surface. With further increase in load, plastic deformation occurs over the whole of the area of contact (the condition has been termed "full plasticity") when the contact pressure is about three times the yield stress of the material. Further increase in load does not appreciably affect the contact pressure. This is the condition in normal identation hardness testing, where the load must exceed the minimum value for full plasticity for reliable hardness readings to be obtained.

From Hunt's results, the minimum load for full plasticity is 6-10 grams with a 1-mil stylus on a vinyl surface (Hunt's Fig. 2). Many commercial pickups therefore operate in the fully plastic range, and must cause considerable damage to the groove (Fig. 2). If each groove wall were deformed equally at all parts of the waveform, this would give no distortion and would not be serious. However, as the load is not taken equally by each wall, the deformation will be unequal, giving distortion of the waveform, with a decrease of low-frequency signals (where stiffness is operative) and an increase of high frequencies (where inertia is operative). Similar effects occur due to the elastic deformation of the groove walls, but in most if not all commercial pickups the elastic effects will be small compared with the plastic. A possible method of obtaining equal deformation of both groove walls would be to play the virgin record first at twice the normal tracking weight at a very low speed, so that the pickup arm could follow the whole of the wave form with negligible lateral loads, but this would hardly be practicable.

The ideal pickup would work entirely within the elastic range (16 mgm). Although it may not be possible to construct such a pickup it might still be possible to limit plastic deformation to the interior of the material, so that the surface of the grooves is undamaged<sup>3</sup>. The limiting tracking weight would be that at which plastic deformation just commenced at the surface. Unfortunately, this point cannot as yet be calculated. Under any stress

Barlow, D. A. J. Audio Eng. Soc., Vol. 4, No. 3. July 1956.

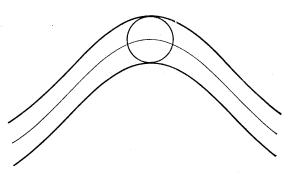


Fig. 1. Stylus supported by convex and concave groove walls.

Wireless World, May 1957

# Reproduction

system, all materials yield according to some function of the shear stress. The shear stress contours in a material under an indenter at the moment of sub-surface yielding are shown in Fig. 3; they will vary somewhat with the Young's modulus and Poisson's ratio of the material. The shear stress at the surface is 0.33 of the shear yield stress, and is proportional to the cube of the load while the whole of the material is elastic. To obtain surface yielding therefore, the load will have to be raised by some unknown factor, probably greater than (1/0.33)<sup>3</sup>, giving 0.3 gram for a flat surface, or 0.43 gram for a record groove.

As the record moves under the stylus, the system is not the same as the static indentation case so far considered. Poritsky<sup>4</sup> has shown, for cylinders in contact, that the effect of an additional tangential force, as represented by friction, is to shift the point of onset of yielding nearer to the surface. The influence of stylus-groove friction would doubtless be similar and would affect yield loads, but if friction is low, as is probably the case, the effect will be

Scratch Tests.—Hunt's scratch tests were conducted by dragging 1-mil and 3-mil radius styli over flat vinyl surfaces. No trace was detected below about 6.7 grams for the 3-mil stylus; the corresponding load for the 1-mil stylus should be 0.75 gram, but no tracks were detected below 1.5 grams, probably because of the difficulty of detecting such very fine traces. The limiting loads for plastic deformation just to appear at the surface with a 1-mil stylus will thus be between 0.3 and 0.75 gm for a flat surface, or 0.4 and 1 gm for a pickup, say, half a gram.

Shellac Records.—From hardness tests, the yield strength of shellac is about twice that of vinyl. From cantilever loading tests, the modulus of elasticity of shellac is about three times that of vinyl. The increased yield stress is therefore more than offset by the increased modulus, giving a smaller area of contact (and hence higher stresses) for a given load. The limiting load for no plastic deformation of shellac will thus be slightly less than for vinyl (for the same size stylus). For a 2.5-mil stylus the load will be about 90 milligrams, and the corresponding load for plastic deformation to just

Poritsky, H. J. Appl. Mech., Vol. 17, No. 2. June 1950

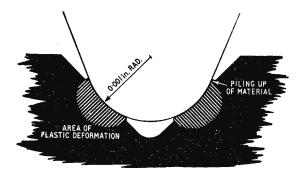


Fig. 2. Stylus-groove contact in the fully plastic range.

#### By D. A. BARLOW, M.Sc.

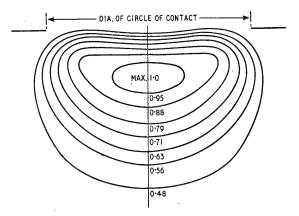


Fig. 3. Shear stress distribution in material under spherical indenter (after Davies<sup>2</sup>).

appear at the surface will be 1.75 grams. Loading tests on shellac with a 2.5-mil sapphire stylus showed tracks at less than 3 grams, corresponding to a pickup weight of about 4 grams. We may thus take the limiting load as about  $2\frac{1}{2}$  grams.

It will be noted that at low loads, for a given stylus, shellac will actually be damaged more than the vinyl, but around 15 grams for a  $2\frac{1}{2}$ -mil stylus the track width or damage will be similar for each material, and above this load the damage to shellac will be less—the track width will be about 0.7 of that on vinyl in the fully plastic range. Shellac is therefore the better material for the old type of heavy pickup, but vinyl will be superior for lightweight pickups. This would explain conflicting reports on the relative damage of vinyl and shellac discs. There is no technical reason why, in these days of lightweight pickups, 78 r.p.m. records should not be made in vinyl.

Deterioration on Repeated Playback.—When any material is deformed the area of contact increases, and, beyond the elastic limit, the material work hardens until it is able to support the load, unless the load is so high as to cause fracture. Once a record has been played at a given weight, provided that this is not too great, there will be no further plastic deformation on continued playback (at the same weight); the record will sound the same as at the first playing, although it may be heavily deformed, and there is no knowing what the virgin record would sound like. The claim that a certain record sounds the same after 1,000 playings as it did with the first playback does not mean that it is undamaged.

It used to be the practice of record companies to monitor the original wax or lacquer disc before plating to make the master. If the original has been damaged in this way, the final record will not sound any different for being played with a very light-weight pickup. It would be interesting to know if the record companies still monitor the original disc before plating now that the original recording is usually done on tape. If we are to take advantage

of very light-weight pickups which will not give plastic deformation of the surface not only must we purchase virgin records but it is essential that any monitoring at any stage during manufacture be done with equally light pickups (or with styli that

are weaker than the groove walls).

Nevertheless, with heavy pickups progressive deterioration does take place on continued playback. This is due to creep and fatigue. At high stresses the material continues to deform slowly, so that on repeated replay the groove continues to be deformed slightly each time. Fatigue is the fracture of a material by varying or repeated loads at stresses lower than the static strength. As the highest stresses are sub-surface, failure will take place by sub-surface cracking, giving flaking and pitting of the groove walls. This gives the increase in noise characteristic of heavily played records. It is interesting to note that Max<sup>5</sup> obtains this type of failure on repeated playback of polystyrene and occasionally vinyl records at 10 grams load with a 1-mil stylus. If there is a rest period between replays the material

partly recovers, and does not fail.

Wear.—Up till now we have been discussing damage or plastic deformation of perfect surfaces, although it is often referred to as wear. Wear may be defined as the attrition of contacting surfaces due to relative sliding. The nature of friction is as follows. Under light loads no two surfaces contact at more than a few high spots or asperities, however accurately thay may be finished. Local pressures at these asperities are therefore high, and ploughing, welding and shearing occur on relative motion. This is the normal mode of wear of styli. If there is no bulk surface plastic deformation of a record, the stylus is supported by the asperities, which may be stronger than the bulk material<sup>1,3</sup> and will give a lower rate of frictional wear of record and stylus than a heavier pickup working in the fully plastic range, where the whole of the mating surfaces are in intimate contact. Diamond is known to give lower coefficients of friction with most materials than sapphire or cemented carbide; it might therefore be expected to give less frictional record wear.

Noise.—The noise level will depend on the tracking weight of the pickup as well as on other factors such as sensitivity for degrees of freedom other than lateral. Also Hunt<sup>1</sup> has pointed out that there are the following components in the noise from a

gramophone record.

(1) Surface roughness. The grooves of modern records are very highly finished, the roughness as low as 50 A.U. (10<sup>-7</sup> mm). This is as low as is obtainable on the most highly finished surfaces. In the case of shellac, the filler is of course responsible for considerable roughness, and hence noise. This can be reduced somewhat by the use of superfine fillers.

(2) Welding and shearing of asperities.

(3) The associated plastic deformation. This may also give rise to noise as plastic deformation is not a continuous process, but on a microscale, it occurs by discontinuous slip.

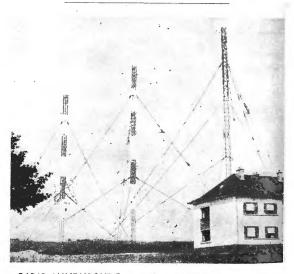
To reduce wear and noise, therefore, improvements can be made only to items (2) and (3), given a homogeneous record material. In addition to using a diamond stylus, the obvious method would be to use polytetrafluorethylene (p.t.f.e.) for the

record1 or the stylus, although its yield stress and modulus may be too low. This gives low friction with all materials, but if the pickup works in the fully plastic range a coefficient of friction of only 0.04 represents welding of stylus to groove over 25% of the contact area3. This will obviously give relatively high wear and noise level, so that the situation with more readily weldable materials. such as vinyl, can well be imagined. Polyethylene usually has a lower coefficient of friction than other plastics (apart from p.t.f.e.) but its yield strength and modulus may be too low; however, Smith has used polyethylene and reports that it gives a lower noise level than vinyl. Polyethylene is said to be too expensive for records; polytetrafluorethylene would be very much more so. It would be interesting to know what proportion of the cost of a record is represented by the plastic and its processing—it has been said that the cost of producing a record pre-war was about 3½d. If so, a more expensive plastic giving lower noise level could obviously be used without appreciably increasing the cost of a record.

Other possible means of reducing friction would be the use of graphite for styli, or porous metal or ceramic impregnated with graphite, oil or p.t.f.e.

Another method of reducing wear and noise due to items (2) and (3) would be by lubrication of the record<sup>1,3</sup>. For this purpose, a solution of calcium petroleum sulphonate in a light petroleum fraction has been suggested. This would be wiped on to the record immediately before each playing, the solvent evaporating and leaving an adsorbed film, only a few molecules thick, on the groove walls. This would probably give adequate boundary lubrication, and would not obscure the high frequencies. Flake graphite, as has been used in the past, would not be adsorbed on to the groove walls, and would have no effect other than to increase noise by reason of particles trapped under the stylus.

<sup>6</sup>Smith, O. J. M. Audio Eng., Vol. 32, No. 9. Sept. 1948. (To be continued.)



RADIO LUXEMBOURG recently brought into service two new 100-kW transmitters at Marnach, about 40 miles north of the city. The original 100-kW transmitter is being transferred to the new site from which the three transmitters will then operate in parallel on 208 m.

Max, A. M. J. Audio Eng. Soc., Vol. 3, No. 2. April 1955

Plug-in Counter Units, designed on the "building block" principle so that a variety of different equipments can be assembled, have been introduced by Ericsson Telephones. Several ranges of units are available, covering counting speeds from 5c/s to 200kc/s. Below 5c/s the counting is done on electro-mechanical registers. Speeds up to 350c/s are obtained on Dekatron units with cold-cathode tube coupling stages. For speeds up to 20kc/s the Dekatron units have thermionic-valve driving stages, while binary units are used for counting speeds up to



200kc/s. Also available are input, output and control units, and a 1-kc/s valve-maintained tuning fork oscillator designed for timing and tachometry applications.

R.F. Absorption Matting of unusual composition has been developed by W. H. Emerson, A. G. Sands and M. V. McDowell, for use in anechoic chambers to facilitate indoor aerial measurements at lower frequencies. It takes the form of a loosely spun mat of animal hair impregnated with rubber containing carbon black. Reflection is minimized over a wide frequency range by graduating the amount of loaded rubber applied according to the depth of the mat. A 4-inch-thick mat absorbs as low as 1,000Mc/s and an 8-inch version well below 500Mc/s. Further details in D.S.I.R. unpublished report PB114686.

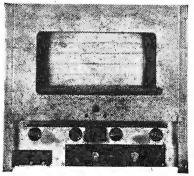
Multiplex Indication System using a single pair of wires has been developed by G.E.C. for checking the operating state of equipment remote from the control point. It utilizes up to twelve transmitter units, consisting of a.f. oscillators tuned to different frequencies, situated at various points along the wires, and a cabinet containing the corresponding receiver units. Each receiver comprises a band-pass filter, amplifier, detector and relay. Thus, when a particular a.f. tone comes on the line, switched by the associated piece of equipment, the correspond-ing receiver relay operates and shows which transmitter is working. A feature of the system is the use of transistors, and the battery power supply will run for six months on continuous load before replacement becomes necessary. In licating sig-



nals can be sent along wires of up to five miles in length.

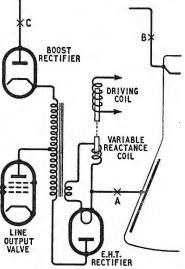
Titanium Oxide Rectifiers are being developed by A. E. Middleton, O. J. Mengali, L. R. Jackson and R. C. Sirrine to give degrees of rectification similar to selenium and germanium but permitting wider temperature variations. Films of oxide are formed on titanium conducting bases and have n-type characteristics. Point-contact rectification is obtained with tungsten, and junction rectification with copper and other metals. A junction rectifier using copper worked satisfactorily up to 280°C. Full accounts of the work are given in D.S.I.R. unpublished reports PB115426 and PB115427.

Trans-Atlantic Cable Monitoring, along the British section with bidirectional repeaters, is done by a swept frequency system using a different "marker" crystal filter in each repeater. The test signal, which sweeps through the entire carrier band in four seconds, is sent along the cable in one direction. Responses from the various filters (each on a different frequency) are frequency doubled and fed into the return channel. The timebase of the c.r.t. monitoring unit is synchronized with the frequency sweep so that the returned responses are displayed at various points along the horizontal race—the performance of each repeater being indicated by the vertical deflection signal. A feature of the display equipment, made by Kolster-Brandes (see illustration), is a "windowing" facility which facility which enables the operator to compare in magnified form the performance of each repeater with a reference signal.



The push-pull Y deflection output stage is arranged so that when the incoming signal falls outside certain limits (the "window"), the two valves cease to act as a normal amplifier and one of them becomes cut-off. These limits are set manually by the Y gain and shift controls.

Television E.H.T. Regulator, devised by John D. Burke, is intended partly for lengthening the life of e.h.t. rectifiers in line flyback systems and partly for increasing the possible current output and range of c.r.t. brilliance. According to Mr. Burke,

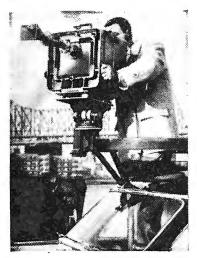


about one-fourth of service calls involve (or are exclusively for) the replacement of e.h.t. rectifiers. He maintains that breakdowns resulting from open- or short-circuited heaters or loss of cathode emission are caused by the rectifier heater growing cooler just when the picture brightness makes heavy demands for c.r.t. beam current. This appears to be inherent in the line flyback e.h.t. system. To combat the effect, the new regulator device has a coil in the rectifier's heater circuit, the reactance of which is varied by the c.r.t. beam current so that an increase of beam current causes an increase of heater current and vice versa. In one version a saturable reactor is utilized, with the beam current passing through the control winding. Another version, illustrated in the sketch, uses a movable armature which is pulled into a driving coil by increasing c.r.t. beam current (against the action of a spring or gravity). This armature is mechanically coupled to a movable core in the variable-reactance coil in such a way that increasing beam current reduces the reactance. The driving coil can be connected into the beam current circuit at any of the points A, B or C marked with a cross.

Fluorescent Noise Source, using a 6-watt fluorescent lamp coupled to a coaxial line, has been devised by M. Hill for monitoring purposes in radar equipments operating in the 400-Mc/s band. It is actually usable over a wide range of frequencies. Details are given in D.S.I.R. unpublished report PB118451.

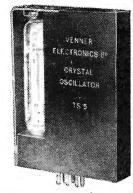
Super Elliptical Speaker, recently introduced in the U.S.A. by Rola, measures 14 inches in one direction and only 3 inches in the other. The ellipticity is accentuated in this fashion so that the speaker can be mounted at the front of a television receiver alongside the picture tube. The performance is claimed to be equivalent to that of an 8-inch circular model.

Miniature Aerial Horn, used by American broadcasting organizations in television "roving eye" microwave transmitters, makes the transmitter operator look very much like his colleague the cameraman. The broad beam of the horn aerial, compared with the parabolic "dish" normally used for this work, permits less critical sighting between the mobile transmitter and the fixed receiver. This is a distinct advantage in maintaining a good signal when the television unit is on the move and has to follow a circuitous route. The 8-inch-long horn (made by Narda) has a beam width of 20° vertically and horizontally. It



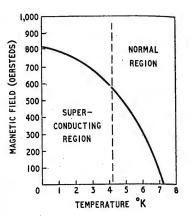
covers a frequency range of 5,850-8,200Mc/s and has a gain of 16.5dB.

Transistorized Crystal Oscillator made by Venner Electronics provides two outputs, one sine-wave and the other square-wave, at a frequency of 10kc/s. The circuit is potted in synthetic resin with the



exception of the crystal, which is replaceable. Actually, two types of crystal can be used in the device, one having a zero temperature coefficient between 15°C and 20°C so that maximum accuracy is obtained at room temperature, and the other a zero temperature coefficient between 40°C and 50°C for applications where the ambient temperature is of this order. The stability of the oscillator, at about the point where the zero temperature coefficient occurs, is of the order of 3 parts in 10°s. The supply voltage is nominally 10 but the unit will function satisfactorily with supplies from 4V to 12V. Incidentally, the oscillator can be used in conjunction with the transistorized plug-in decade counter described in our January issue.

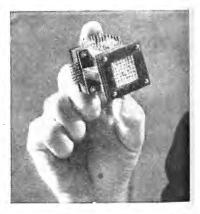
Superconductive Computer Elements, developed by D. A. Buck and called cryotrons," are the basis of a digital computing machine now being built by the A. D. Little company in Cambridge, Mass., U.S.A. The main advantages of the cryotron—virtually a 1-inch wire "core" carrying a small coil—are its extremely small size, simple construction and low power dissipation. In superconductivity, the resistance of a metal suddrops to zero when its temperature is reduced below a certain critical value (by immersion in liquid helium). The presence of a magnetic field makes this critical temperature even lower, and the graph shows how a field affects the onset of superconductivity for a "core" made of lead. Thus, a wire held at a constant low temperature can be switched between superconductivity and normal resistivity (up and down the dotted line) by means of an energizing coil-thereby providing a two-state device suitable for binary arithmetic. A flip-flop using two cryotrons is shown in the





lower diagram. If a current is established in one wire "core" it passes through the coil of the other and drives the second "core" into normal resistivity—the current continuing indefinitely because the energizing coils themselves are held permanently superconductive. Another pair of cryotrons is used to put the flip-flop into the desired state. Other circuits were published in the April, 1956, issue of Proc.I.R.E., where it was stated that a digital computer using cryotrons might be built into a 1-ft cube—excluding the refrigeration plant, of course!

Printed Matrix Store.—The accompanying picture shows the small size of the new RCA storage device based on the magnetic-cell principle which



was described in our February issue (p. 80). The unit stores 2,560 binary digits in a volume of only 2 cubic inches.

Unpublished Reports mentioned above come from various sources but can be obtained from the Technical Information and Documents Unit of the Department of Scientific and Industrial Research, 15, Regent Street, London, S.W.1.

# LETTERS TO THE EDITOR

The Editor does not necessarily endorse the opinions expressed by his correspondents

#### Colour Television Pitfalls

WHILST agreeing with the spirit of your editorial in the March issue, there are two comments with which I find myself in disagreement: (1) I do not believe it is true to say that the N.T.S.C. system was planned basically for use with the three-gun shadow mask tube, nor is tied to that tube. The system only assumes simil-taneous presentation of the red, blue and green components of coloured picture elements and, of course, can be used with several forms of display device (the right one not yet apparently thought of!). (2) The argument for compatibility that "a colour service would be economically impossible . . . unless it were receivable on existing black and white receivers," is, I think, misleading. If the public wished to see the transmissions in colour they would have to buy new colour television receivers. The cost of these receivers would be negligibly affected, whether or not they were designed to work on a compatible transmission system; i.e., compatibility does not materially affect economy from purely the receiver point of view.

As I see it, economies of compatibility relate almost entirely to the *transmission* side (for which, admittedly, we, as receiver owners, would have to pay indirectly. Apart from the fact that economy of "channel space" is an important consideration (i.e., a compatible system uses existing channels), there is also the fact that existing r.f. outlets—transmitters and aerials—can be used with very little modification. So also can long-distance cable

and radio links.

Studio equipment, colour cameras and the like would mean fresh capital expenditure whether the system was compatible or not and would not influence the argument

greatly one way or the other.

Having had a good deal of practical field experience of the difficulties with multipath distortion, fading, longdistance interference and other effects on present television and V.H.F. sound reception, I have lately been given to speculating whether it would not be a good idea to confine colour transmission to an almost completely "wired" system (i.e., co-ax run by the G.P.O.!). This would avoid the "ether-space" and many other problems and leave us free to optimize the system, at the same time giving reception free from defects of radiated transmission. Thinly populated areas could be catered for by radiation from Band IV low power relay stations.

Concerning "Cathode Ray's" and "Diallist's" conflicting opinions on the use of "monochrome," I agree with "Cathode Ray" that this is not the best word to use, but I can see nothing wrong with the word achromatic which—in the dictionary—is defined as "without colour." (By the way, grey is generally looked upon as achromatic as it is low intensity "white.")

D. W. HÉIGHTMÁN. Clacton-on-Sea.

### Etymological Inexactitude?

IT seems to me that, in their counter-attacks, "Free Grid" and "Diallist" have condemned themselves out

of their own pens.
"Diallist" agrees that white is a combination of all the colours of the spectrum, but argues that television "white" is a very pale grey, which he appears to suppose is fundamentally different. If so, I can only refer him to a reliable work on colour. He would have had a better case if the had made use of the fact that many set? case if he had made use of the fact that many sets' "whites" have a pronounced bluish tinge, but even so the spectral spread is pretty wide.

Both he and "Free Grid," whom I had long regarded as sound on etymology, take my breath away with their comments on "panchrome." Did the "fellow with little Latin and less Greek" also compile every reputable English dictionary, from the O.E.D. downwards?

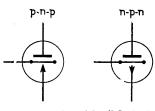
"Free Grid" says he has "by far the stronger case" in asserting that the word "data" is singular. I should

advise him to get measured for a larger size in hats, since he appears to know better than such authorities as the "Shorter Oxford English Dictionary," Eric Partridge, Sir Ernest Gowers, and H. W. Fowler.

It should take more than the misguided practice of some of the people in one small branch of knowledge expressed in English to enthrone an upstart solecism as a new accepted usage. "CATHODE RAY."

#### Transistor Symbols

IN your March issue, James Franklin fessed to an unconscious plagiarism of a transistor symbol that we have used. This we take as flattery. We have recently adopted the "open" type of the "open" type of symbol from the book



by Lo, Endres, et al. which was mentioned by "Cathode Ray" in your April issue as his personal preference (see accompanying sketch).

National Physical Laboratory, D. L. A. BARBER. Teddington, Middx. W. T. BANE. Teddington, Middx.

#### Beat Interference

IT is well known that since Winter Hill opened for service on Channel 9, Band III, reception of the Croydon I.T.A. station is often marred by co-channel interference in certain areas. My own observations show that when this interference is visible there is sometimes a pulsating variation of mean brightness level. This may or may not be accompanied by the more usual brightening of groups of lines, giving an impression of line pairing.

When the two stations radiate similar programme material a ghost or ghosts may also appear, depending on the intensity of the Winter Hill signal at this extreme range. When programme material is dissimilar—the "commercials," for example—the ghost(s) give place to two entirely different pictures, one usually weaker than

the other.

The pulsating lightening and darkening of the picture experienced here at times is not unlike the conditions related by your contributor in the March issue, James P. Grant. I am therefore led to believe that his trouble could be a form of this co-channel interference. In support of this view, I notice that a line connecting this town with Winter Hill passes through Croydon; similarly, a line from Cawsand and Kingsand to Holme Moss would pass through Hessary Tor.

These two latter stations share Channel 2, Band I,

and, I believe, always radiate the same programme material. The trouble, says Mr. Grant, is always present when Hessary Tor is transmitting, but then so is Holme Moss transmitting at those times. He also says there is no recorded signal in the band when Hessary Tor is silent, but again, Holme Moss would also be off the air at those times.

As Mr. Grant seems to have secured the active cooperation of the B.B.C. in investigating his problem,

Wireless World, May 1957

could he not prevail upon them to cut the Holme Moss carrier for a while during a morning or afternoon test transmission period, so that the effect on his reception could be observed. On the assumption that this has not been tried, it might give a lead, if not an answer

St. Leonards-on-Sea. W. E. THOMPSON.

#### Peak or R.M.S.?

IN your March issue Thomas G. Ward wonders whether recording equipment makers use peak reading meters for their quoted data.

Partly as the result of pioneer work by Stuart Ballantine, for over twenty years virtually all audio measurements in the U.S.A. have been made by average-reading meters, sine-wave-calibrated in equivalent r.m.s. voltage. This revolution was born of the discovery that amplifier. type average-reading vacuum-tube voltmeters had better linearity and much more sensitivity than the peak-reading type, and infinitely more stability than the r.m.s. vacuum-tube meter. "R.M.S." has become an obsolete cliché.

Today, such average-reading meters are universally used for recording tape and recorder measurement, as well as for virtually all other audio measurements. Since most models are good to several hundred kc/s, and some are accurate up to 4 or 5 Mc/s, they have also seen much r.f. use as well.

Audio Instrument Company, Inc., C. J. LeBEL. New York, U.S.A.

#### THE I.E.A. SHOW EXHIBITORS AT

AS its title implies, the Instruments, Electronics and Automation Exhibition (Olympia, May 7th to 17th) will include a considerable amount of equipment of interest to Wireless World readers. The show is promoted by five associations, among them the Scientific Instrument Manufacturers' Association and the British Electrical and Allied Manufacturers' Association. Although officially the radio and electronics industry is not represented, there are among the 200 exhibitors a considerable number (see below) of manufacturers in the industry, or whose products are used extensively in the manufacture of radio and electronic equipment.

A conference will be run in conjunction with the exhibition, for which tickets will be obtainable at the show. Each day will be devoted to a specific aspect of the industries covered by the exhibition—automation (8th), nuclear (9th), education (10th), medical (13th), industrial (14th), computer (15th), communications and navigation (16th). The morning session (from 11.0) will be devoted to a general review of the day's subject, whilst more specific techniques and applications will be covered in the

afternoon session (from 3.0) Some of the papers are listed below.

The exhibition opens daily (except Sunday) at 10.0, and closes at 6.0 except on the 10th and 15th, when it is open until 9.0. Admission, 2s 6d.

Name Stand Advance Components	934 936	Name Stand Fleming Radio	
Associated Automation	408 510 942A	G.E.C. General Radiological	406 703
B.T.H	309 515 933	Hilger & Watts Honeywell-Brown Hunt (Capacitors)	402 410 922
Belling & Lee	938 711 205	Kelvin & Hughes	310
British Physical Laboratories Brown, S. G	704	Lancashire Dynamo Electronic	501
Cambridge Instrument Co Casella (Blectronics)	601 412 945	Products Langley Livingston Laboratories	303 914 600
Cathodeon Cawkell, A. E. Cinema-Television Cooke, Troughton & Simms	501 716 913 806	Magnetic Devices	706 944 504 925
Cossor Crompton Parkinson Croydon Precision Inst. Co.	407 408 <del>9</del> 47	Metropolitan-Vickers Microcell Millett Levens	401 707 921
D.S.I.R. Dawe Instruments De La Rue Donvin Instruments Dubilier	502 939 209 925 908	Minerva Detector Co. Ministry of Supply Morganite Resistors Muirhead Mullard 305 & Murphy Radio	930 909 927 901 801 703
Ekco Electronics Elcontrol Electro Methods Electrofio Meters Co. Electronic Engineering Electronic Instruments	505 918 904 510 206 930 300	N.S.F. Nagard Nalder Bros. & Thompson Nash & Thompson National Cash Register Co. Nicholson, W. B. (Scientific Inst.)	919 216 603 105 311 515
Electrothermal Engineering Elliott Brothers E.M.I. Electronics English Electric Valve Co. Ericsson Telephones Evans Electroselenium Evershed & Vignoles	411 404 107 613 200 405	Painton & Co. Philips Electrical Plannair Power Controls Pullin, R. B. & Co. Pye, W. G. & Co.	211 910 604 706 925 501

Name Stand Racal Engineering Radiovisor Parent Robinson, F. C. & Partners	No. 932 923 212
S.T.C. Servomex Controls Short Brothers & Harland Siemens-Ediswan Sifam Electrical Instrument Co. Simmonds Aerocessories Smiths Industrial Instruments Society of Instrument Technology Solartron Southern Instruments Sperry Gyroscope Co. Sunvic Controls	307 900 106 507 808 903 929 101 503 100 203 506
T.C.C. Telephone Manufacturing Co. Turner Electrical Instruments 20th Century Electronics	602 201 937 946
Unicam Instruments	501
Victoria Instruments	925
Wayne Kerr Laboratories Wireless World and Electronic & Radio Engineer	304 941
Some Conference Papers  8th. "Computer controlled mad tools" by J. N. Toothill (Ferr. "Electronically controlled mad tools" by C. A. Sparkes (H. Kearns & Co.).  9th. "The place of analogue comp in reactor control" by J. W (Atomic Energy Authority).  10th. "The technologist—his training reward" by Dr. G. L. D'Om (Battersea Polytechnic). "Training for research" by D. Thompson (Scientific Instru Research Association).	and brain or. J. ment
13th. "Electronic instruments for clitests with radioactive isotopes." N. Veall (Guy's Hospital) and E Pulsford (Atomic Energy Autho 14th. "Instrumentation in the textile."	" by L. W. rity).
14th. "Instrumentation in the textile dustries" by J. E. Fielden (Fie Research).	elden
15th. "The electronic office" by Walter Puckey. "Production control procedusing a computer" by J. W. C (British Tabulating Machine Cd "Electronics in banking" by Temple (Lloyds Bank).  16th. "Communications and the fut by Sir Gordon Radley. "Recent developments in madar" by A. L. P. Milwright (I Naval Scientific Service). "Air navigation" by T. G. The Communication of the Communicatio	ure
(Deden Descend Establishment)	

Wireless World, May 1957

(Radar Research Establishment).

# Limiters and Discriminators for

# F.M. Receivers

3 (cont'd)—Practical Ratio Detector Circuits:

By G. G. JOHNSTONE, B.Sc.\*

Comparison of Foster-Seeley and Ratio Detectors

O extend the treatment to a practical ratio detector we shall next consider the case when the parallel resistance of the tuned secondary circuit  $R_{\rm s}$  is not infinite.

As before, the fundamental-frequency currents ( $I_{ab}$ ) flowing through the diodes are equal in magnitude, and the current in each diode is in phase with its applied voltage. Additionally, the current flowing through the resistive components  $R_s/2$  are also in phase with the applied voltage. These currents are given by  $2E_1/R_s$  and  $2E_2/R_s$  respectively. The equations relating the magnitude of the currents flowing must thus be modified as follows:

$$(I/2)^2 = E_1^2 Y_1^2 + (I_{ac} + 2E_1/R_s)^2 (I/2)^2 = E_2^2 Y_2^2 + (I_{ac} + 2E_2/R_s)^2$$

where  $Y_1$  and  $Y_2$  have the same meaning as formerly, i.e. they are the admittances of the reactive elements of the tuned circuits. Inserting the values for  $Y_1$  and  $Y_2$  and writing  $g_s=1/R_s$ 

$$E_1^2 [4C_s(\Delta\omega - \Delta\Omega)]^2 - E_2[4C_s(\Delta\omega + \Delta\Omega)]^2 + 4I_{ac} g_s(E_1 - E_2) + 4g_s^2(E_1^2 - E_2^2) = 0$$
As the diade rectification efficiency is assumed 100

As the diode rectification efficiency is assumed 100 per cent,  $E_1 = E_b + E$  and  $E_2 = E_b - E$ , where E is the a.f. output voltage.

Combining the expressions above gives

$$\frac{\mathbf{E}}{\mathbf{E}_b} = \frac{-\Delta \omega}{\Delta \Omega} \times 1 + (\mathbf{E}/\mathbf{E}_b)^2$$

$$\overline{1 + (g_s^2/4C_s^2\Delta\Omega^2) + I_{ac}g_s/(8C_s^2\Delta\Omega^2E_b) + (\Delta\omega/\Omega\Delta)^2}$$

In this expression, we can replace  $I_{ac}$  by  $2I_{dc}$ , and we can simplify the expression appreciably for initial examination by restricting consideration to the region where  $\Delta\omega/\Delta\Omega$  is appreciably less than unity,

i.e. to the working region near the centre frequency. The expression for E then becomes

$$\mathbf{E} = -\mathbf{E}_b \, \frac{\Delta \omega}{\Delta \, \Omega} \, \times$$

 $\overline{1+g_s^2/(4C_s^2\Delta\Omega^2)+g_sI_{dc}/(4C_s^2\Delta\Omega^2E_b)}$ 

To a first degree of approximation therefore, the output is linearly proportional to the frequency of the input signal. However, it can be shown analytically that if the input current (I) increases, then so does the direct current in the load,  $I_{dc}$ . This is apparent also from an inspection of the circuit. Thus we can draw the important conclusion that the audio output voltage decreases, as the input current in-

creases, and conversely. In this form the circuit is over-compensated. An examination of the expression above suggests a way out of this difficulty. If only part of the load voltage is "stabilized," i.e. shunted by a large capacitor,  $E_b$  will be no longer constant, and variations of numerator and denominator may be made to cancel. If a resistor  $R_m$  is inserted in series with each "battery" as shown in Fig. 10,  $R_L$  becomes  $R_m + R'_L$ , where  $R_L'$  is the resistance shunted by the large-value capacitor.  $E_b$  in the foregoing expressions must then be replaced by  $E_b' + R_m I_{de}$ , where  $E_b'$  is the new battery voltage, i.e. that developed across  $R_L'$ , no longer equal to the total load voltage. Inserting this value for  $E_b'$  in the expression above gives

$$E = -E_{b'} \frac{\Delta \omega}{\Delta \Omega} \times \frac{1 + R_{m} I_{dc}/E_{b'}}{(1 + g_{s}^{2}/4C_{s}^{2}\Delta \Omega^{2}) [1 + g_{s}I_{dc}/(g_{s}^{2} + 4C_{s}^{2}\Delta \Omega^{2})E_{b}]}$$

The factor  $1/E_b$  is the denominator can also be replaced by  $1/E_b'(1+R_mI_{dc}/E_b')$ , and provided the voltage  $R_mI_{dc}$  is small compared with  $E_b'$ , this can then be replaced by the first two terms of the series expansion, viz.

$$\frac{1}{{\rm E}_{b}{'}(1\,+{\rm R}_{m}{\rm I}_{dc}/{\rm E}_{b}{'})} = \frac{1}{{\rm E}_{b}{'}}(1\,-{\rm R}_{m}{\rm I}_{dc}/{\rm E}_{b}{'})$$

Then

$$E = \frac{-E_{b}'(1 + R_{m}I_{dc}/E_{b}') (\Delta \omega/\Delta \Omega)}{\{1 + g_{s}^{2}/4C_{s}^{2}\Delta \Omega^{2}\} \left[1 + \frac{g_{s}I_{dc}(1 - R_{m}I_{dc}/E_{b}')}{E_{b}' (g_{s}^{2} + 4C_{s}^{2}\Delta \Omega^{2})}\right]}$$

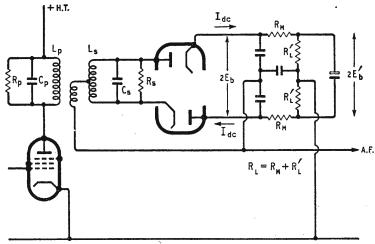


Fig. 10. Ratio detector with resistors  $R_m$  to improve a.m. suppression.

<sup>\*</sup> B.B.C. Engineering Training Department.

The output E is independent of  $I_{dc}$  to a good degree of approximation if

$$\begin{split} \mathbf{R}_{m} &= \mathbf{g}_{s}(1 - \mathbf{R}_{m}\mathbf{I}_{dc}/\mathbf{E}_{b}') \, / \, (\mathbf{g}_{s}^{\, 2} + 4\mathbf{C}_{s}^{\, 2}\varDelta\,\Omega^{2}) \\ \text{i.e. } \mathbf{R}_{m} &= \frac{\mathbf{g}_{s}}{\mathbf{g}_{s}^{\, 2} + 4\mathbf{C}_{s}^{\, 2}\varDelta\,\Omega^{2}} \cdot \frac{1}{1 + \mathbf{g}_{s}\mathbf{I}_{dc}/\{\mathbf{E}_{b}'(\mathbf{g}_{s}^{\, 2} + 4\mathbf{C}_{s}^{\, 2}\varDelta\,\Omega^{2})\}} \\ &= \frac{\mathbf{g}_{s}}{\mathbf{g}_{s}^{\, 2} + 4\mathbf{C}_{s}^{\, 2}\varDelta\,\Omega^{2} + \mathbf{g}_{s}\mathbf{I}_{dc}/\mathbf{E}_{b}'} \end{split}$$

This expression can be simplified by introducing the undamped Q value of the secondary circuit  $Q_s = R_s \omega_o C_s = \omega_o C_s/g_s$ . Then  $R_m = R_s/\{1 + (2Q_s \Delta F/f_o)^2 + R_s I_{dc}/E_b'\}$  This expression shows that complete a.m. rejection

cannot be achieved, since the optimum value of  $R_m$  depends on  $I_{do}$ , which varies during the a.m. cycle. We can make the output due to a.m. zero over a limited range about a selected value of  $I_{do}$ . It is usual to do this about the working point, when  $E_b'/I_{do}$  is equal to  $R_{L}'$ , the resistance in parallel with the stabilizing capacitor. Then  $R_m = R_{m \ opt} = R_s/\{1 + (2Q_s \Delta F/f_o)^2 + R_s/R_L'\}$ The effect of varying  $R_m$  whilst the total diode load remains constant is shown in Fig. 11, which shows

remains constant is shown in Fig. 11, which shows how the output varies with an a.m. input when the signal frequency is constant at a value near the centre frequency. The value of  $R_m$  is expressed in terms of  $U = R_m/R_L$ , where  $R_L = R_{L^{'}} + R_m$ . The factor U is equal to the fraction of the output voltage which is not stabilized. The optimum value of U corresponding to  $R_{m \ opt}$  calculated above is designated  $U_{opt}$ .

At this point it is convenient to introduce the "a.m. suppression ratio." This is a measure of the effectiveness of a f.m. detector in rejecting a.m. of the input signal. It is the ratio of the a.t. output due to f.m. to that due to a.m. when the input signal is modulated equally in depth by a.m. and f.m. The value of modulation depth employed is usually

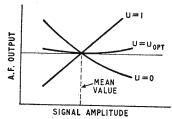


Fig. 11. Showing variation of a.f. output with input signal amplitude for a fixed frequency input signal  $(\Delta f small).$ 

30 or 40 per cent. Different frequencies are usually employed for the a.m. and f.m. components to facilitate measurement. Typical values for these frequencies are 100 c/s for the f.m. component, and 2 kc/s for the a.m. component. In a practical ratio detector the a.m. suppression ratio is between 20 and 30 db.

If now we return to the full expression derived earlier for E the a.f. output voltage, we can evaluate the distortion terms in the output. Substituting for the value of E<sub>b</sub> leads to the following expression for the a.f. output voltage E expressed as a fraction of  $\mathbf{E}_{b}{}'$ 

$$y = -Ax \frac{1 + B^2 y^2}{1 + ABx^2}$$

where  $y=E/E_{b}'$   $x=\Delta\omega/\Delta\Omega=\Delta f/\Delta F$   $A=(2Q_{s}\Delta F/f_{o})^{2}/\{1+(2Q_{s}\Delta F/f_{o})^{2}\}$   $B=R_{L}'/(R_{L}'+R_{m})$ . This is the fraction of the direct voltage at the diode output "stabilized" by

the electrolytic capacitor, and is equal to  $E_{b}'/E_{b}$ . If the graph of y against x is plotted, it has the form

shown in Fig. 12 for the portion of the curve in which we are interested.

The expression for y can be expanded as a power series, giving

$$y = E/E_b' = d_1(\Delta f/\Delta F) + d_3(\Delta f/\Delta F)^3 \dots$$
  
where  $d_1 = -A$   
and  $d_3 = A^2B (1 - AB)$ 

In order to use this expression to determine distortion terms, the value of  $\Delta F$  must be known. Except for the special case of  $R_s$  infinite, this is not equal to the half-bandwidth  $(\Delta F_p)$  measured to the turn-over point of the practical characteristic. However, in the process of deriving the expansion above, it emerges that the turn-over points of the characteristics occur at the values given by  $x_p^2$ 1/AB. As A and B are both less than unity, the measured half-bandwidth  $\Delta F_p$  is greater than  $\Delta F$ . In a practical circuit, if the measured half-bandwidth is found, △F can be found from

$$\Delta F = \Delta F_p \sqrt{AB}$$

The value of B can be calculated from the circuit constants. The value of A depends up  $\Delta F$ , and hence requires a knowledge of the answer. However,  $\Delta F$  can be found by successive approximations if the value of  $\Delta F_p$  is used instead of  $\Delta F$  to calculate A. This gives an approximate value of  $\Delta F$ , which can be used to determine A more accurately, and so on. In fact, the error introduced by using the first approximation only is generally small.

Alternatively, the value of  $\Delta F$  can be calculated from a knowledge of circuit values. Thus the resonance frequencies of the two tuned circuits given by  $1/2\pi\sqrt{(1 + M/2L_p)L_sC_s}$  $1/2\pi \sqrt{(1-M/2L_p)L_sC_s}$  respectively. From these expressions  $\Delta F/f_o = M/4L_p$ , whence  $\Delta F = Mf_o/4L_p$ 

If a tertiary winding or tapped primary circuit is employed, then  $L_p$  must be replaced by  $a^2L_p$ , and M by aM, giving

M by aM, giving  $\Delta F = Mf_o/4aL_p$ . The expression for the output voltage is given in terms of  $E_b$  and  $\Delta F$ . If it is required to determine the sensitivity of the circuit, we require an expression relating  $E_b$  to  $I_{in}$ . With a tertiary winding or tapped primary circuit, the equivalent circuit must be drawn with  $I_{in}$  replaced by  $a^{2}I_{in}$ .  $C_{in}$  by  $C_{in}/a^{2}$ . drawn with  $L_p$  replaced by a  $^2L_p$ ,  $C_p$  by  $C_p/a^2$ ,  $R_p$  by  $a^2R_p$  and  $I_{in}$  by  $I_{in}/a$ . We shall consider the signal frequency to be near the centre frequency. We can then ignore the effect of the reactive components of the tuned circuit connected between terminals 1 and 2 of the equivalent circuit. The dynamic resistance of this tuned circuit (R') is that which in parallel with  $R_s/4$  is equal to  $a^2R_p$  (see

$$\frac{1}{R'} + \frac{4}{R_s} = \frac{1}{a^2 R_p}$$

The impedance presented at the centre tap of the transformer T by the two tuned circuits and diode loads can be shown by an extension of the argument employed earlier to be

$$R_1 = \left(\frac{R_D}{\epsilon}\right) / \{1 + (2Q_w \Delta F/f_o)^2\}$$

where  $R_D/2$  is equal to  $R_L/2$  in parallel with  $R_s/2$ , i.e. the total damping applied to each of the two tuned circuits considered previously. The current flowing

Part 1), i.e.

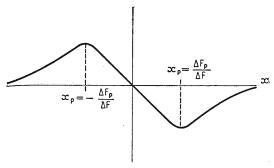


Fig. 12. Showing variations of output  $(y = E/E_b)$  against input signal frequency ( $x = \Delta f/\Delta F$ ).

to the centre tap of the transformer T is then given by

 ${\rm I}=\frac{{\rm I}_{in}}{a}\;\frac{{\rm R}'}{{\rm R}_1+{\rm R}'}$  The power delivered to the centre tap of the transformer is thus

$$P_{in} = \frac{1}{2}I^{2}R_{1}$$

$$= \frac{1}{2} \left( \frac{I_{in}}{a} \frac{R'}{R_{1} + R'} \right)^{2} R_{1}$$

This power appears in the diode load circuit and in the dynamic resistances (R<sub>s</sub>/2) of the two tuned circuits. Near the centre frequency, the voltage across each dynamic resistance is approximately E<sub>b</sub>, and hence the power dissipated in each resistance is  $\frac{1}{2}E_b^2/(R_s/2)$ . The power in each diode load is  $E_b^2/R_L$ , and hence

$$\frac{2E_b^2}{R_L} + \frac{2E_b^2}{R_s} = \frac{1}{2} \frac{I_{in}^2}{a^2} \frac{R'^2}{(R_1 + R')^2} R_1$$
But 
$$\frac{2}{R_L} + \frac{2}{R_s} = \frac{2}{R_D}$$

$$E_b^2 = \frac{1}{4} \frac{I_{in}^2}{a^2} \frac{R'^2}{(R_1 + R')^2} R_1 R_D$$

$$E_b = \frac{1}{2} \frac{I_{in}}{a} \frac{R'}{R_1 + R'} \sqrt{R_1 R_D}$$
This expression has its maximum value when

This expression has its maximum value when  $a = a_{opt}$ ; this value of a is given by

 $a_{op\,t}$ ; this value of a is given by  $1/a^2_{op\,t} = R_p\{1/R_1 - 4/R_s\}$  Using this value for a, and  $E_{b^{'}} = E_bR_{L^{'}}/R_L$ , gives the maximum value for  $E_{b^{'}} = E_{b^{'}max}$   $E_{b^{'}max} = \frac{1}{4} \frac{R_{L^{'}}}{R_L} I_{in} \quad \sqrt{R_pR_D/\{1 - (4R_1/R_s)\}}$  If as is usual,  $R_s/4$  appreciably greater than  $R_1$  then  $E_{b^{'}max} \approx \frac{1}{4} \frac{R_{L^{'}}}{R_L} I_{in} \sqrt{R_pR_D}$  and  $a^2_{op\,t} \approx R_1/R_p$  Near the centre frequency, the a.f. output voltage is given approximately by

$$E_{b'max} = \frac{1}{4} \frac{R_{L}'}{R_{r}} I_{in} \sqrt{R_{p}R_{D}/\{1 - (4R_{1}/R_{s})\}}$$

$$E_{b'max} \approx \frac{1}{4} \frac{R_L}{R_L} I_{in} \sqrt{R_p R_D}$$

given approximately by

 $E = -AE_b' \Delta f / \Delta F$ 

For maximum sensitivity,  $E_b$ ' should be large and  $\Delta F$  small. For  $E_b$ ' to be large  $R_p$  and  $R_D$  should be large. However, as we shall show next, the condition for good "downward" a.m. handling capacity requires R<sub>D</sub> small. Thus a practical design represents a compromise between these requirements.

To complete the investigation of the circuit, we shall evaluate the maximum "downward" a.m. handling capacity. With no a.m. present, the relationship between the peak value of the r.f. input current to each of the tuned circuits (I/2), when the signal frequency is near the centre frequency, is given by

 $\begin{array}{l} (\mathrm{I}/2)^2 = \mathrm{E}_b{}^2 (16\mathrm{C}_s{}^2 \varDelta \Omega^2 + 4/\mathrm{R}_\mathrm{D}{}^2) \\ = \mathrm{E}_b{}^2 16\mathrm{C}_s{}^2 \varDelta \Omega^2 \{1 + 1/(2\mathrm{Q}_w \varDelta \mathrm{F}/f_o)^2\} \end{array}$ 

When the diode current falls to zero, the value of the r.f. input current (I'/2) is given by

$$(I'/2)^2 = E_{b'}^2 16C_s \Delta \Omega^2 \{1 + 1/(2Q_s \Delta F/f_o)^2\}$$
 whence

$$\begin{split} m_{max} &= 1 - \text{I}'/\text{I} = 1 - \frac{\text{E}_b'}{\text{E}_b} \sqrt{\frac{1 + 1/(2\text{Q}_s \, \Delta \text{F}/f_o)^2}{1 + 1/(2\text{Q}_w \, \Delta \text{F}/f_o)^2}} \\ &= 1 - \frac{\text{R}_\text{L}'}{\text{R}_\text{L}} \sqrt{\frac{1 + 1/(2\text{Q}_s \, \Delta \text{F}/f_o)^2}{1 + 1/(2\text{Q}_w \, \Delta \text{F}/f_o)^2}} \end{split}$$

If  $2Q_s \Delta F/f_o$  is large, the expression simplifies to one similar to that given earlier for the case of R<sub>s</sub> infinite.

The value of  $m_{max}$  calculated above ignores the effect of the primary circuit, and in general this is not negligible. To evaluate this, consider the input impedance presented at the centre tap of the transformer T of the equivalent circuit. With no a.m. present, this is

 $R_1 = (R_D/4)/\{1 + 2Q_w \Delta F/f_o)^2$ Similarly, the impedance when the diode current falls to zero is

$$R_2 = (R_s/4)/\{1 + (2Q_s \Delta F/f_o)^2\}$$

If the values of  $R_1$  and  $R_2$  differ, then  $m_{max}$  is modified. This happens because the proportion of the input current  $(\hat{\mathbf{I}}_{in}/a)$  fed to the centre tap of the transformer T differs in the two cases. The effective impedance R' of the current source was shown earlier to be

$$1/R' = 1/a^2R_p - 4/R_s$$

Thus the proportion of the input current flowing to the centre tap when no a.m. is present is given by  $I = \frac{I_{in}}{a} \frac{R'}{R_1 + R'}$ 

$$I = \frac{I_{in}}{a} \frac{R'}{R_1 + R'}$$

and when the diode current falls to zero by 
$$I' = \frac{I_{in'}}{a} \qquad \frac{R'}{R_2 + R'}$$

Thus  $m_{max}$  is changed from the value calculated

$$\begin{split} m'_{max} &= 1 - \frac{\mathbf{I}_{in}^{'}}{\mathbf{I}_{in}} = 1 - \frac{\mathbf{I}^{'}}{\mathbf{I}} \frac{\mathbf{R}^{'} + \mathbf{R}_{2}^{}}{\mathbf{R}^{'} + \mathbf{R}_{1}} \\ &= 1 - \frac{\mathbf{R}^{'} + \mathbf{R}_{2}}{\mathbf{R}^{'} + \mathbf{R}_{1}} \frac{\mathbf{R}_{\mathbf{L}^{'}}}{\mathbf{R}_{\mathbf{L}}} \sqrt{\frac{1 + 1/(2\mathbf{Q}_{s}\Delta \mathbf{F}/f_{o})^{2}}{1 + 1/(2\mathbf{Q}_{w}\Delta \mathbf{F}/f_{o})^{2}}} \end{split}$$

Ratio Detector with Practical Diodes .- The analysis of the circuit operation with practical diodes, i.e. those with a rectification efficiency of less than 100 per cent is very complex, because the than 100 per cent is very complex, because the direct current component in the diode  $I_{dc}$  is no longer equal to half the peak value of the fundamental frequency a.c. component  $I_{ac}$ . If the diode efficiency is high, however, the assumption that  $I_{dc} = \frac{1}{2} I_{ac}$  may still be made with fair accuracy. The diode itself must then be regarded as a perfect diode in series with a resistor  $R_{di}$ . This resistance then forms part of the resistance  $R_m$  calculated earlier, and represents a minimum value below which  $R_m$  cannot fall. To calculate its value, we may note that cannot fall. To calculate its value, we may note that given an input peak voltage E the "perfect" diode delivers an output voltage E. A fraction of this voltage, ηE, appears across the true load resistance  $R_{L}$ , where  $\eta$  is the diode rectification efficiency.

The remainder of the voltage  $(1-\eta)$  E, appears across the fictitious resistor  $R_{di}$ . Hence

$$\eta \; rac{\mathrm{E}}{\mathrm{R_L}} = rac{1 - \eta}{\mathrm{R}_{d\,i}} \cdot \; \mathrm{E}$$
 $\mathrm{R}_{d\,i} = rac{1 - \eta}{\eta} \, \mathrm{R_L}$ 

It is the fact that  $\eta$  varies with the input signal level which limits the useful range of input signal levels which the detector can handle satisfactorily.

Normally,  $\eta$  tends to a constant value as the input signal increases, and the circuit constants are adjusted for this value of  $\eta$ . At low input signal levels, however,  $\eta$  decreases appreciably, and the a.m. suppression ratio is seriously impaired. Thus there is a lower limit of input signal which the detector can handle satisfactorily. It is apparent that, for best performance high-efficiency diodes should be employed.

Unbalanced Effects.—In the presence of amplitude modulation, a ratio detector exhibits an "unbalance effect." This is an output due to the a.m. which is constant at all frequencies in the working range. This effect has a number of causes, which are not indicated by the preceding analysis because of the simplifying assumptions made. The causes include variations of diode input capacitance with signal amplitude, the finite impedance of the tuned circuits to harmonics of the current flowing in the diodes, and inadequate decoupling of the diode loads at r.f. The last cause produces an effect which opposes that due to the first, and hence some reduction of the a.m. output may be obtained by using relatively small decoupling capacitors. The second cause can be minimized by using a large value of secondary circuit tuning capacitance. This tends to

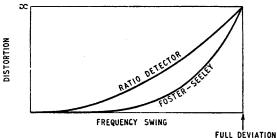


Fig. 13. Showing how distortion varies for ratio detector and Foster-Seeley circuits having equal distortion at full deviation.

produce low values of  $R_s$ , the dynamic resistance, and hence tends to lead to low sensitivity. A compromise is thus necessary, and a value of 50pF is usually employed. The a.m. output can, however, most easily be reduced by unbalancing the two diode-load circuit resistors,  $R_m$ . The foregoing analysis suggests that these should be equal; if, however, their sum is kept constant, while they are altered individually, substantial reduction of the a.m. output is then obtained.

Time Constant of Load Circuit.—The foregoing analysis was based upon the assumption that the time constant of the load circuit was very large, so that the load circuit could be replaced by a battery for the purposes of analysis. Unfortunately, if the time constant of the circuit is made very large, the tuning characteristics of the receiver are affected. The receiver then behaves like a conventional a.m.

receiver in which the a.g.c. time constant is too long; there is an appreciable lag between adjustment of the tuning control and the return to stable operating conditions. The tuning has then to be adjusted very slowly. To avoid this effect, the load timeconstant has to be shorter than is desirable. In practice a compromise value of time constant of the order of 0.1 to 0.2 seconds is usually employed Such a circuit ceases to behave like a constantvoltage battery when the input is varying at a slow rate, and there is a slow variation of the output signal in accordance with the signal variation. This is especially noticeable if "flutter" due to signal reflections from an aircraft occurs. This flutter generally begins to be noticeable when the flutter rate is about 0.5 c/s; the flutter rate increases, as does also the amplitude of the "flutter," until the flutter rate rises to value when the load time-constant is sufficient to suppress the variations. To counter this effect, an effective fast-acting a.g.c. system is required. A suitable control voltage is available from the load circuit itself, and this is usually employed. The a.g.c. system also has the desirable effect of equalizing the audio output from input signals of unequal amplitude.

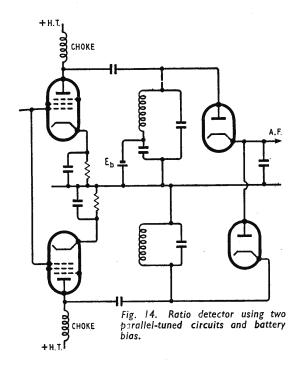
Variants of the Ratio Detector Circuit.—A number of variants of the ratio detector circuit have been described from time to time. The most common of these employ two tuned circuits instead of the phase-difference transformer. Two such circuits, shown in Figs. 14 and 15, are described by Paananen. In the circuit of Fig. 14, two tuned circuits are driven from two valves with the input grids connected in parallel, to supply equal currents to the tuned circuits. A battery is employed instead of the selfbiasing circuit. In the circuit of Fig. 15, a low impedance source (a cathode follower) is used to drive two series-tuned circuits; the "battery" voltage is provided by the cathode bias of the cathode follower. This circuit may be described as the dual of that of Fig. 14, in that a constant voltage is fed to two series-tuned circuits instead of a constant current to two parallel-tuned circuits.

# Comparison of the Foster-Seeley and Ratio Detector Circuits

A comparison of these two circuits depends critically upon the requirements of the detector in a receiver. These may be stated as (a) low distortion (b) good "downward" a.m. handling capacity (c) good a.m. suppression ratio (d) driving voltage required and (e) wide-band characteristics. On the score of low distortion, the Foster-Seeley circuit is better than a ratio detector of comparable bandwidth, although not necessarily better than a wide-band ratio detector.

The two circuits differ appreciably in the way in which the distortion varies with the signal frequency swing. In the Foster-Seeley circuit, the distortion at optimum adjustment increases with the fourth power of the swing; in the ratio detector it increases with the square of the swing. Thus if both circuits are adjusted to give equal amounts of third-harmonic distortion at full deviation, their characteristics at smaller frequency swings will be different. This is shown in Fig. 13.

In respect of "downward" a.m. handling capacity, the two are not strictly comparable, since in the Foster-Seeley circuit this maximum "downward"



a.m. handling capacity is proportional to the amount by which the input signal exceeds the "threshold" input required by the limiter. In the ratio detector, the maximum "downward" a.m. handling capacity is a fixed quantity. In general a detector should be capable of handling "downward" modulation of the order of 50 per cent, and both circuits can normally achieve this.

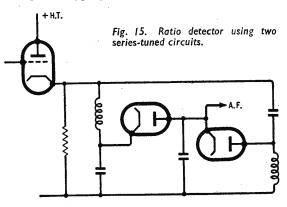
The a.m. suppression ratio required in a receiver depends upon the type of interference encountered. To deal satisfactorily with all types of interference a ratio of 35-40 dB would appear to be necessary. The Foster-Seeley circuit preceded by a limiter has a ratio of the order of 40 dB. The ratio detector, in practice, appears to have a ratio of the order of 20-30 dB. This is not sufficient for all types of interference, and is perhaps the most serious limitation of the circuit. The ratio can be increased by employing a limiter preceding the detector, but if this is done a relatively large input signal to the stage is required. This offsets one of the major attractions of the ratio detector, the smaller number of valves required in a receiver. A hybrid arrangement, in which the preceding valve functions as a high-level limiter, may go some way to improving performance, but there may be difficulties in areas of low field strength. Alternatively, a diode dynamic limiter may be added to increase the a.m. suppression ratio, but this generally leads to some loss of overall gain.

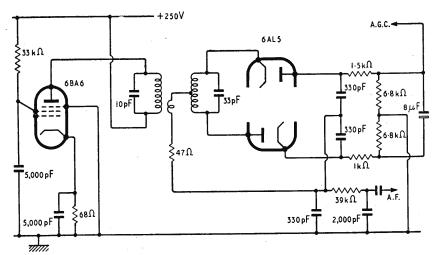
The driving voltage quoted differs for the two cases. With a Foster-Seeley circuit, there is a "threshold" at which the limiter commences to function satisfactorily. Below this threshold the a.m. suppression ratio is poor, the "downward" a.m. handling capacity zero, and the a.f. output varies approximately linearly with the input signal amplitude. Above the threshold, the a.m. suppression ratio rises rapidly to an approximately constant value, and the a.f. output tends to a constant value. The "downward" a.m. handling capacity rises linearly

with the ratio of input signal amplitude to threshold amplitude. In a ratio detector there is a "threshold" of a different type. This occurs when the input signal falls to the point where the diode efficiency begins to fall off. Below this threshold the a.m. suppression ratio and "downward" a.m. handling capacity decrease steadily. Above this threshold the a.m. suppression ratio and the "downward" a.m. handling capacity tend to constant values. The a.f. output, however, is proportional to input signal mean amplitude at all amplitudes except below the "threshold" where it falls somewhat more rapidly than the input signal mean amplitude.

The minimum input signal for satisfactory operation with a Foster-Seeley circuit is thus fairly well defined. If the circuit is to handle "downward" a.m. to a modulation depth of 50 per cent, this requires the input signal to the limiter to be approximately twice the threshold input. In a practical circuit, this corresponds to an input signal of some two volts at the limiter grid. The "threshold" input signal with a ratio detector is usually stated as the input voltage required at the grid of the i.f. stage feeding the detector, and this may be of the order of 20 mV. At this figure, however, the a.f. output may be appreciably below that of the Foster-Seeley circuit, and as a basis of comparison the ratio detector driver input, for an output comparable to that of a Foster-Seeley circuit, is perhaps better. A typical practical figure for the ratio detector on this basis of comparison is some 100 mV, the a.f. output being then approximately 1 volt peak. The overall gain from the aerial input to the driver/limiter grid is thus less by a factor of approximately 20 in a receiver employing a ratio detector than that in a receiver employing a Foster-Seeley circuit, and may enable an i.f. stage to be omitted. However, this saving may not be possible if the a.m. suppression ratio of the ratio detector has to be supplemented.

If a wide-band detector is required, the ratio detector would appear to be most satisfactory. It was stated in Part 2 that the Foster-Seeley circuit may suffer from "diagonal clipping," which occurs if the time-constants of the diode loads are so great that the envelopes of the signals applied to the diodes can fall faster than the rectified output falls. With increasing bandwidth the input signal envelope can fall progressively more rapidly and hence with a Foster-Seeley circuit, the diode loads must be reduced progressively with increased bandwidth. This leads to appreciable design difficulties. The ratio detector, however, can be made free from "diagonal clipping" as in the circuits of Figs. 14





Circuit values used in ratio detector described by Seeley and Avins (RCA Fig. 16. Review, June 1947).

and 15. With increased bandwidth, the "downward" a.m. handling capacity decreases, and hence a wideband ratio detector must be preceded by an efficient limiter.

# Theoretical and Practical Results

To illustrate the order of accuracy of the preceding analysis, the practical results can be compared with those given for a published design. The design chosen is that due to Seeley and Avins, described in the RCA Review, June 1947. The circuit diagram is shown in Fig. 16.

The rectification efficiency of the diodes was estimated from published data to be 0.8 approximately. The value of  $R_{di}$ , the equivalent inherent resistance of each diode, is thus found to be  $2 k\Omega$ . This gives the mean value of  $R_m$  of the practical circuit as  $3.\overline{25} \text{ k}\Omega$ . The calculated value is  $3.2 \text{ k}\Omega$ .

The measured a.g.c. voltage is 2.5 volts for an r.f. input of 100 mV to the grid of the 6BA6. This is equal to  $E_b'$ . Assuming the 6BA6 to have a mutual conductance of 4.3 mA/V, the calculated value of  $E_b'$  is 2.3 volts. The measured value of the " downward " maximum a.m. capacity is 70 per cent; the calculated value is 70 per cent also.

To evaluate sensitivity and distortion, the values of A and B are required. From circuit values B = 0.68. The value of A is calculated to be 0.83, given the measured halfbandwidth  $(\Delta F_p)$  of 175 kc/s. The value of  $\Delta F$  is then 135 kc/s approximately.

Taking  $E_{b}$  as 2.5 volts, the a.f. output voltage is given

by 
$$E = 0.0154(\Delta f) + 2.7 \times 10^{-7}(\Delta f)^3$$
 . . . where  $\Delta f$  is measured in kc/s.

With an input signal of 75 kc/s deviation, i.e.,  $\Delta f = 75 \cos \omega t$ 

$$E = 1.06 \cos \omega t + 0.03 \cos 3 \omega t \dots$$

The calculated r.m.s. fundamental frequency a.f. output is 0.75 volt; the measured value is 0.7 volt. The calculated third harmonic distortion is 2.0 per cent (r.m.s.); the measured total harmonic distortion is 2.5 per cent (r.m.s.).

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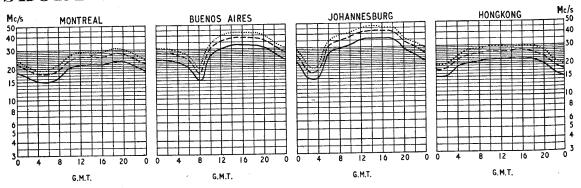
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#### SHORT-WAVE CONDITIONS

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# **Portable Transistor Receiver**

By S. W. AMOS\*, B.Sc. (Hons.), A.M.I.E.E.

HE junction transistors which have been available in this country for a few years have been mainly a.f. types with alpha cut-off frequencies not exceeding 0.5 Mc/s. Though perfectly suitable for use in audio amplifiers, these are far from ideal for use in r.f. or i.t. amplifiers or as frequency changers and it has not therefore been possible to construct satisfactory superheterodyne receivers using such transistors in all stages. A number of circuits for transistor superhets have been published but these have relied on the use of low intermediate frequencies such as 315 kc/s, and/or oscillators which operate below the signal frequency. Low intermediate frequencies increase the danger of image interference and low oscillator frequencies make ganging of oscillator with signalfrequency circuits difficult.

The alpha cut-off frequency quoted by transistor manufacturers is the frequency at which the current gain of the transistor, when used as a commonbase amplifier, is 3 dB down compared with the low-frequency gain. However, for a satisfactory performance from a common-base amplifier the alpha cut-off frequency must be at least twice the operating frequency: thus if the intermediate frequency is 465 kc/s an alpha cut-off frequency of at least 1 Mc/s is required. For reasons given later common-emitter operation is generally preferred, and for satisfactory performance in this mode the alpha cut-off frequency must be higher still. Thus transistors intended for use in i.f. stages usually have alpha cut-off frequencies in the range 1 Mc/s to 5 Mc/s. The requirements of the trequency changer are even more stringent because the transistor used in this position must be capable of oscillating at 2 Mc/s when the receiver is tuned to the high-frequency end of the medium waveband: transistors intended for such applications may have alpha cut-off frequencies as high as 8 Mc/s. Recently transistors of this type—known as r.f. transistors—have been introduced. With them it is now possible, for the first time, to construct a superheterodyne receiver with transistors in all stages which will operate over the full medium waveband (550 kc/s to 1.6 Mc/s) using the conventional intermediate frequency of 465 kc/s.

### Low Running Costs

This article describes the design of a portable battery-operated receiver of this type using a total of seven junction transistors (four a.f. types and three r.f. types) and one point-contact diode. The power output is more than 300 mW and the sensitivity is such that, even with a ferrite-rod aerial, the output stage can be overloaded on Brussels and Hilversum

SENSITIVE SUPERHETERODYNE CIRCUIT INCORPORATING R.F. TRANSISTORS

GENERAL PRINCIPLES OF DESIGN

when the receiver is used in the London area. The receiver operates from a 4.5- or 6-volt battery. Such a receiver offers a number of advantages over the conventional portable 4-valve battery-operated superhet and it is interesting to compare the two receivers. Perhaps the most outstanding difference between them is in efficiency, i.e., the ratio of the power delivered to the loudspeaker to the power taken from the batteries. For the transistor set this approaches 60 per cent at maximum volume, nearly six times the maximum likely to be obtained from the most economical valve receiver. As a result the transistor set is more economical to operate. For example, the receiver to be described takes an average current of 25 mA and 6 volts and a type PP1 battery costing three shillings has a life of 150 hours when discharged for four hours per day. The running cost is thus less than one farthing per hour and if larger batteries are used it is even less. For a valve set a typical running cost for both l.t. and h.t. is one penny per hour although for the most economical receivers using valves with 25-mA filaments, a value as low as 0.6 pence per hour is claimed. Thus the transistor set is cheaper to run by a factor of at least 3 and probably nearer 4 or 5 even though it gives two or three times the power output of a valve receiver and has better sensitivity. In addition the transistors are, of course, much smaller than valves, making possible very compact receivers; they are non-microphonic and have a longer life than valves. Their life is not unlimited (as has sometimes been suggested) but decreases as the operating temperature rises. Used in a receiver of the type to be described they should have a life many times that of valves. To offset these advantages the transistors are slightly more noisy than valves and at present they are more expensive.

Most battery-driven portable receivers have 4valve superhet ciruits basically similar to those employed in mains-driven receivers but their performance is, in general, inferior because of the lower gain of battery valves and because the frame or ferrite-rod aerials of portable receivers do not give so good a pick-up as an outdoor aerial. This limitation in performance is usually accepted because, in spite of it, the sensitivity is usually adequate for the reception of the local stations even when the receiver is used in an untavourable situation. Moreover, an improvement in performance would require additional stages of amplification and, in a

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battery superheterodyne receiver the frequency changer and i.f. stages account for a large fraction (between one-quarter and one-half) of the total power consumption. Thus extra stages must inevitably cause a significant increase in h.t. and l.t. drain. There is no need to accept such a limitation in the performance of a transistor receiver because the current taken by the early stages is a much smaller fraction of the total current drain and the increased consumption due to any added transistors is negligible. Thus there is no need to limit the number of stages on the grounds of running costs and the receiver can be given the maximum sensitivity likely to be required.

The required sensitivity was estimated by comparison with a mains-driven superhet recently described by the author<sup>1</sup>. This receiver needs a signal of approximately 20  $\mu$ V (modulated to a depth of 30 per cent) at the output of the medium-wave ferrite-rod winding to give 300 mW output and it was decided that the transistor set should give its maximum output for a smaller voltage at the output medium-wave winding. High sensitivity is of little use, however, unless it is accompanied by high

selectivity.

#### Class A or Class B?

We shall now consider the broad principles of design of a superheterodyne transistor receiver, beginning with the output stage. Here a choice has to be made between class-A and class-B operation. The quality of reproduction obtainable with a class-B stage is probably inferior to that from a class-A stage but it can be improved by negative feedback. However, too much importance should not be attached to this point; the small loudspeaker and limited baffle area of a portable receiver inevitably impose limitations of the quality realizable. A class-A stage could be only a single transistor and this can be RC-coupled to the previous stage; a class-B stage needs two transistors operating in push-pull and requires some form of phase-splitting device, such as a transformer with a centre-tapped secondary winding, between it and the previous stage. Moreover a class-B stage necessitates thorough decoupling of the supply to the frequency-changer and i.f. stages to prevent feedback of harmonics of the a.f. output and consequent distortion—we shall return to this point in Part 2. Thus the first cost of a receiver with a class-B stage is higher than that of a receiver with a class-A stage. However, the collector dissipation in a class-A stage is a maximum in the absence of a signal. Such a stage is more likely to suffer from thermal runaway with possible damage to the transistor than a class-B stage, and circuit precautions will be necessary to prevent this. This subject and that of protective circuits will also be discussed more fully in Part 2.

#### Efficiency

The running cost of a battery-operated receiver is probably more important than the first cost and depends on the efficiency of the output stage which in turn depends on the shape of the characteristics of junction transistors. The characteristics of an output transistor are illustrated in Fig. 1. They are practically

straight, parallel and equidistant: moreover, the knee of the characteristics occurs at a very low collector voltage which means that the signal-frequency voltage generated across the transistor during amplification can nearly equal the battery voltage. As a result the efficiency of a transistor, i.e., the ratio of output power to the power taken from the battery, is near the theoretical maximum which, for class-A operation, is 50 per cent. This applies only on peak audio signals for which the transistor delivers its maximum output. If the output is not at maximum (and for music and speech signals the average level is below the maximum level for a considerable fraction of the total time) the average efficiency is much less than 50 per cent. For a class-B stage the efficiency does not vary greatly with the amplitude of the input signal and in practice can exceed 70 per cent. Moreover a class-B stage is a quiescent system; that is to say the collector current is very small in the absence of an input signal but rises with increase in input signal Thus the relative economy of the class-B output stage is greater than the ratio of the two efficiency figures suggests and the running cost of a receiver with a class-B stage is much less than that of a receiver with a class-A stage delivering comparable output power.

Thus the choice between class-A and class-B output is influenced by the relative importance of first cost and running cost. If running costs must be low a class-B stage is preferable. If running costs are not so important a class-A stage is preferable. It does not follow, of course, that a transistor set with a class-A stage will be expensive to run. Because of the superior characteristics of transistors it must be more economical than a valve set. As an illustration a transistor operating with, say, 22.5 volts supply can give an output of 100 mW for a collector current of 10 mA; this is approximately the power output of many valve receivers operating with 67.5-volt batteries. The transistor set requires no elaborate filtering of the supply to the early stages and the total battery drain is unlikely to exceed 12 mA at which even small cells should give a This could form the basis of a reasonable life.

simple and compact superhet receiver.

#### Choice of Circuit

However, most of the transistors at present available in this country are intended for operation at lower collector voltages such as 6 or 9 volts. At 6 volts a class-A output stage must consume 33 mA to give an output of 100 mW. For such a stage the collector dissipation is 200 mW in the absence of an input signal. With little choice of output transistors at the moment, no type could be found which is suitable for such an application. Most of the available transistors are rated for dissipations of 100 mW or less and it was decided to use two of these in class-B push-pull for the output stage. From these it is possible to obtain more than 300 mW output without exceeding the maximum collector dissipation. The collector current rises to over 100 mA on programme peaks but the average is 25 mA, less than that required by a class-A stage to give 100 mW.

The output transistors can be operated in commonbase, common-emitter or common-collector circuits. In a common-base amplifier the current gain of the transistors is less than unity and high gain is possible

<sup>&</sup>lt;sup>1</sup> Amos, S. W., "Economy in Receiver Design," Wireless World, Aug., 1956.

only by using high load impedances and these are inconvenient in an audio output stage. The choice is thus between common-emitter and commoncollector and in this receiver, as in most transistoroperated equipment, common-emitter working is preferred because of its higher gain. There is some distortion and a minimum of about 6 dB of feedback is advisable to improve linearity.

The maximum power output obtainable from a class-B push-pull pair is approximately four times the maximum permissible collector dissipation for each transistor, and if this is taken as 85 mW-a typical value—the power output is  $4 \times 85 = 340$  mW. This peak power is equal to VI/2 where V is the peak collector voltage and I is the corresponding peak collector current. If P is the power

$$I = \frac{2P}{V}$$

$$I = \frac{2 \times 340}{6} \text{mA}$$

For 340-mW output and a 6-volt supply  $I = \frac{2 \times 340}{6} \text{mA}$ = 110 mA.

The optimum load for each transistor is given by

$$\frac{V}{I} = \frac{6}{110 \times 10^{-3}} \text{ohms}$$
= 55 ohms

giving a collector-to-collector load of 220 ohms. From this the turns ratio for the output transformer can be calculated. If the loudspeaker is of 3 ohms impedance the ratio is given by  $\sqrt{(220/3)}:1$  which equals 8.5:1.

#### **Driver Stage**

If we take the current gain of the common-emitter output transistors as 50, the input current required for maximum output is approximately 2 mA. This is supplied by a driver stage, also common-emitter, coupled to the output stage by a transformer with a ratio of 1:1, the secondary winding being centretapped. Thus a 1-mA peak swing is required from the driver stage: the collector current for this stage must hence be at least 1 mA and is adjusted to at least 2 mA to allow a safety margin. If the current gain of the driver stage is also 50, an input current of 20  $\mu$ A is needed for maximum output. input resistance of common-emitter stages is usually or the order of  $1 k\Omega$  and the peak input signal required at the base of the driver stage is hence  $20 \times 10^{-6} \times 10^3 = 20$  mV. This could be supplied directly from the diode detectors but to obtain the gain from the pre-detector stages necessary to give the desired sensitivity at least three i.f. stages would be necessary. Some difficulty is likely to be experienced in stabilizing such an i.f. amplifier. Moreover, the gain of one a.f. stage is higher than that of one i.f. stage. It is therefore preferable to use three a.f. stages rather than three i.f. stages. The a.f. amplifier so obtained is very sensitive, requiring less than 1 mV input for maximum output, but the sensitivity is reduced by negative feedback applied from the secondary of the output transformer to the emitter of the first a.f. stage. This improves the linearity of the a.f. amplifier and also increases the input resistance of the first a.f. stage; a useful feature because, for a given degree of peak clipping in the detector stage, it permits the use of larger diode loads than would otherwise be possible.

The first a.f. stage is direct-coupled to the detector to give amplified a.g.c. Such amplification is necessary because it is impossible to obtain a large enough control voltage directly from the diode detector. There is a step-down ratio in the i.f. transformer coupling the final i.f. amplifier to the detector and the peak voltage swing at the collector must necessarily be less than the battery voltage: thus the signal delivered to the diode must be small and in fact is inadequate for giving effective a.g.c.

By using a three-stage audio amplifier the required sensitivity can be achieved with two i.f. stages and we will now consider the problems which arise in the i.f. section of the receiver. These differ markedly from those encountered in the i.f. section of a valve receiver. For example, the i.f. transformers in a valve receiver can be designed without regard to the input and output impedances of the valves with which they operate because the impedances are too high to have significant effect on the transformer performance. In a transistor receiver the damping due to the transistors has a very great bearing on transformer design: in fact, the input and

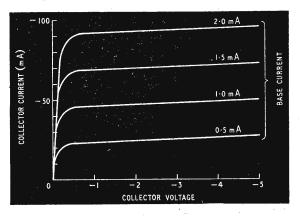


Fig. 1. Collector-current/collector-voltage characteristics for an open transistor.

output resistances largely determine the design and performance of the transformers.

These resistances depend, of course, on the type of amplifier used and here there is the usual choice between common-emitter and common-base circuits. In i.f. amplifiers general opinion is not so unanimously in favour of common-emitter working as in a.f. amplifiers. For a given alpha cut-off frequency a common-base amplifier will operate up to higher frequencies than a common-emitter amplifier and, where cut-off frequencies are low, the use of this type of amplifier is justified. However, the application of standing bias and a.g.c. bias to such an amplifier is difficult: if the base is connected to the positive terminal of the battery supply a yet more positive voltage is needed for the emitter bias. A common-emitter amplifier is more convenient to bias, and, as manufacturers steadily raise the cut-off frequencies of transistors, this type of amplifier is likely to become standard in time. If the emitter is connected to the positive terminal of the battery supply, the negative terminal can be used as a source of negative bias for the base. This mode of operation is used in the i.f. amplifier and in fact in all the stages of the receiver to be described.

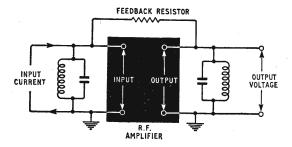


Fig. 2. Block schematic diagram for method of obtaining bandpass characteristics by means of negative feedback.

The i.f. amplifier provides most of the selectivity of the receiver and it was decided that four tuned circuits with an effective Q value of at least 100 were necessary to provide the desired selectivity. This is better than in many valve receivers where working Q values are commonly of the order of 70.

These four circuits can be arranged as a succession of single-tuned circuits or can be grouped to form two double-tuned circuits. Both arrangements give the same skirt selectivity; i.e., the same slope of response curve outside the pass band. However, a cascade of single-tuned circuits inevitably gives some side-band cutting, the extent of which can easily be calculated as follows. A single-tuned circuit resonant at 465 kc/s and with a Q of 100 has an effective bandwidth of 465/100 = 4.65 kc/s; that is to say the response is 3 dB down at 2.3 kc/s from the centre frequency. Four such circuits would therefore give a loss of 12 dB at this fre-

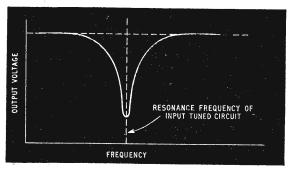


Fig. 3. Response of circuit of Fig. 2 when output load is a pure resistance

quency, making reproduction very low-pitched. It is better to group the tuned circuits into pairs, coupling the members of each pair to give a bandpass response. Such an i.f. amplifier can be designed to give a substantially level response over the required pass band thus making possible better reproduction than is obtainable with single-tuned circuits. This is, of course, the basis of design of valve superheterodyne receivers where one double-tuned circuit is used to couple the frequency changer to the i.f. amplifier and a second is used to couple the i.f. amplifier to the detector.

In the transistor receiver the design is not so straightforward. Two i.f. amplifiers require three inter-stage couplings, and introduce the problem of including two bandpass filters without using a further tuned circuit or an aperiodic network for one of the couplings.

One possibility is to use only one bandpass filter and two single-tuned circuits. The two singletuned circuits will each give a loss of 3 dB at 2.3 kc/s mistuning giving a total of 6 dB. This can be offset by over-coupling the two tuned circuits forming the bandpass filter so that they give a response with "rabbit's ears" which neutralize the loss of the single-tuned circuits to give an overall response flat up to, say, 3 kc/s off tune. This is, however, an impractical solution. The peaks are usually of differing heights. Moreover, if the damping imposed by a transistor on one of the tuned circuits in the bandpass filter should change for any reason say due to an alteration in a.g.c. bias applied to itthe Q of the circuit will alter and so will the height of the peaks. There will thus be significant changes in the shape of the pass band with changes in signal strength.

The solution adopted in this receiver is based

on an idea described by Jewitt2 which enables a bandpass response to be obtained from two singletuned circuits which are separated by an amplifier. The explanation of the circuit can be followed from Fig. 2 which illustrates such an amplifier in block schematic form. The input tuned circuit forms the lower arm of a negative feedback potentiometer and therefore frequency-discriminating feedback is applied to the amplifier. Feedback is at maximum at the resonance frequency, less at frequencies slightly displaced from resonance and is practically nil at frequencies remote from resonance. If the amplifier has a load independent of frequency, such as a pure resistance, its frequency response will show a dip at the resonant frequency of the input tuned circuit as shown in Fig. 3. When the load resistor is replaced by a parallel tuned circuit the overall frequency response becomes a combination of the dip due to the input tuned circuit and a hump due to the frequency-selective load circuit. Depending on the degree of feedback this response can be flat-topped (corresponding to critical coupling in a conventional bandpass

quency. The effect of adjusting the feedback frac-<sup>2</sup> Jewitt, H. S., "Wide-band I.F. Amplifiers," Wireless World, Feb., 1954.

filter) or can have two peaks corresponding to greater-

than-critical coupling. It is useful to remember

that critical coupling is obtained when the feedback is adjusted to give 6 dB loss at the mid-band fre-

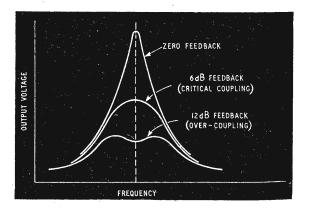


Fig. 4. Response curves of circuit of Fig. 2 for three degrees of feedback.

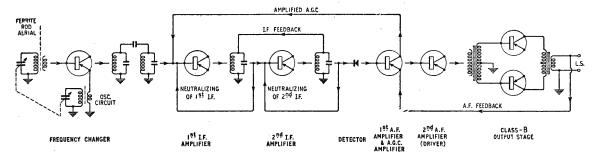


Fig. 5. Skeleton diagram of transistor receiver.

tion on the overall frequency response is illustrated

in Fig. 4.

The third and fourth tuned circuits in the receiver i.f. amplifier are arranged to form a feedback amplifier of this type. The first and second tuned circuits are arranged as a conventional bandpass filter with top-end capacitance coupling. This is illustrated in the block schematic diagram of the receiver in Fig. 5. The coefficient of coupling used in the first bandpass filter must be chosen with care because the first i.f. amplifier is controlled from the a.g.c. line and the damping it imposes on the second tuned circuit can vary. If the coupling is made critical when damping is at maximum, "rabbit's ears" will develop when damping is reduced. It is better therefore to arrange to have critical coupling when damping is a minimum. When damping increases the coupling then becomes less than critical but the response is still single-peaked though the bandwidth is less than it was. means that the receiver pass band varies with the received signal strength. This could be presented as a design feature—an automatic bandwidth control-but the truth is that the variations in band-Ideally the bandwidth are difficult to avoid. width should be independent of signal strength but if some variation is inevitable then it is better that the bandwidth should increase rather than decrease with increase of signal strength and it is fortunate that this is, in fact, what happens. bandwidth is a maximum on local stations where best quality is required and a minimum on weak signals from which quality is often marred by noise and sideband splash.

#### **I.F.** Circuits

We now come to the design of the i.f. circuits themselves. In addition to providing the required selectivity these must also match the cutput resistance of one transistor (approximately  $30 \text{ k}\Omega$ ) to the input resistance of the following one (approximately  $1 k\Omega$ ) in order to provide maximum gain. They must in fact behave as matching transformers and have a turns ratio given by  $\sqrt{(30 \text{ k}\Omega/1 \text{ k}\Omega)}$ : 1; i.e., approximately 5.5:1. The connections of collector and base to the tuned circuit must hence be chosen to give this turns ratio and to give the desired working Q value of 100. One possibility is to connect the transistors to tapping points on a parallel-tuned circuit as suggested in Fig. 6. The steady voltages on collector and base differ and blocking capacitors must be used to transfer signals from the tuned circuit to the transistors.

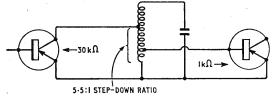


Fig. 6. Use of tappings on parallel-tuned circuit to match the output resistance of one transistor to the input resistance of the next.

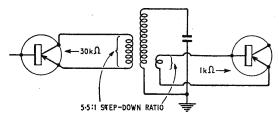


Fig. 7. Use of primary and tertiary windings to match the output resistance of one transistor to the input resistance of the next.

A better method is to employ separate windings for collector and base as in Fig. 7. the tuned circuit thus has three windings; a primary connected to the collector, a secondary which is tuned to 465 kc/s by a parallel capacitor and a tertiary which is connected to the base. The turns ratio of primary to tertiary must be 5.5:1; we now have to determine the turns ratio of primary to secondary. determined by the permissible damping of the tuned circuit. If the secondary circuit has a high Qsay 300—the ratio of primary to secondary turns can be so chosen that the damping due to collector and base together brings the Q down to one-third of its original value; i.e., to 100. On the other hand if the undamped Q is only 150 the damping must be much lighter to give a working Q of 100. Both arrangements give the same selectivity but the gain is higher with the higher initial Q. Webster<sup>3</sup> has shown that if the Q is reduced to half there is a 6 dB loss relative to the maximum gain theoretically possible. If the Q is reduced to one-third the loss is 4 dB and if it is reduced to one-quarter the loss is only 2.5 dB.

For maximum gain therefore it is best to design for the highest undamped Q but there are then large changes in damped Q and therefore in the i.f. response curve when the damping due to the transistors alters

<sup>&</sup>lt;sup>3</sup> Webster, R. R., "Designing I.F. Transistor Transformers," Electronics, Aug. 1955.

as a result of a.g.c. action. A compromise is required and it is probably best to accept the 6-dB loss and to arrange that the Q is reduced to half by transistor damping. The removal of one source of damping due to a.g.c. can then at worst cause only a 32 per cent change in damped Q. In the receiver to be described two losses of 6 dB each are suffered by adopting bandpass circuits and it was decided to use undamped Qs of 300, which are reduced to 100 by transistor damping. The change in Q due to removal of damping due to one transistor is then 50 per cent but this is allowed for, as mentioned earlier, by arranging that the bandpass filters are never more than critically coupled.

The output capacitance of a transistor in a commonemitter circuit is of the order of 30 pF but can vary by as much as 18 pF with the bias current. Hence the i.f. transformers must be so designed that these variations do not significantly alter the tuning. This requires that the equivalent capacitance across the primary winding should be large enough to swamp possible output-capacitance variations. If we decide that mistuning shall be limited to one-half per cent (2.3 kc/s in 465 kc/s) the capacitance change must be less than one per cent. If the output capacitance changes by 18 pF, the equivalent primary capacitance should not be less than 1800 pF: in fact it is 3200 pF.

The frequency changer stage can be a self-oscillating mixer requiring only one transistor or can consist of a separate oscillator and mixer which requires two transistors. The two-transistor circuit

has slightly higher conversion gain and has the advantage that a.g.c. can be applied to the mixer stage. However, the gain of the receiver is quite adequate with a self-oscillating mixer and, to economize in first cost, this form of circuit was adopted. Not all r.f. transistors are successful as frequency changers: some which are quite satisfactory as i.f. amplifiers fail to oscillate or oscillate only over part of the band. Careful selection is thus necessary to find a suitable transistor for this position. Some transistors are marketed specifically as frequency changers and with these no difficulty has been found in securing a good performance over the whole of the medium waveband.

In addition to giving complete medium waveband coverage the receiver was designed to receive the Light Programme transmission on 200 kc/s. This was achieved, as in another receiver described by the author<sup>4</sup>, by adding sufficient parallel capacitance to the medium-wave oscillator circuit to bring the resonance frequency down to 665 kc/s when the tuning capacitor is at its mid-setting. The switch used also selects a fixed-tuned long-wave winding on the ferrite rod. No difficulty was experienced on maintaining oscillation at 665 kc/s in spite of the reduced L/C ratio.

A block schematic diagram of the complete receiver is given in Fig. 5 showing the links between the stages for a.f. feedback, i.f. feedback, neutralizing and a.g.c. A full circuit description will be given in a later issue.

# PLOTTING EYE MOVEMENTS

A Method Depending on the P.D. between Cornea and Retina

MUCH has been heard of motion study for the reduction of manual fatigue in repetitive manufacturing operations, but less of eye fatigue in tasks calling for visual concentration on, say, a number of dials or meter readings. If the operator's eye movements could be

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Equipment for electro-oculography made by E.M.I. for the Naval Motion Study Unit of the Admiralty Research Laboratory.

analysed it should be possible to devise an arrangement of the indicators which requires the minimum effort for supervision,

Optical methods, such as corneal reflections and cinematography, have in the past been used to plot movements of the eyes when the subject has been set a visual task, but these have left something to be desired either on the score of convenience or accuracy. A new method depends upon the fact that a difference of potential exists between the cornea and the retina of the eye. If electrodes are applied to the surface of the face adjacent to the eye, any movement from a median position can be resolved into horizontal and vertical components from the alteration in potential of the skin electrodes, which are disposed in pairs on lines which would intersect at the centre of the iris.

The results may be plotted by a pen recorder or displayed in two dimensions on a cathode-ray tube—a method developed by Dr. N. H. Mackworth of the M.R.C. Applied Psychology Research Unit, Cambridge. The potential differences are small, 15 to 20 \(mu\) per

The potential differences are small, 15 to  $20~\mu V$  per degree of movement of the eye, and special twin-channel d.c. amplifiers have been developed by E.M.I. Electronics, Ltd., for this application with gains of the order of 10,000. Feedback is frequency-dependent and is designed to reject mains interference while preserving a short rise time for step changes of input. Each amplifier is provided with a backing-off circuit to compensate for standing potentials, which vary between individuals, at the arbitrary "zero" position of the eye. Zero drift in the amplifier is less than  $20~\mu V$  in 30 minutes.

<sup>&</sup>lt;sup>4</sup> Amos, S. W., "Design for a Car Radio," Wireless World, Dec., 1956.

# Manufacturers' Products

# NEW ELECTRONIC EQUIPMENT AND ACCESSORIES

# V.H.F. Measuring Sets

TWO self-contained, portable frequency meters for accurate measurement of frequency up to 1,000 Mc/s have been introduced by Telemechanics, Ltd., 3, Newman Yard, Newman Street, London, W.1. One, the Type 7474, covers 20 to 250 Mc/s and the other, Type 7475,



Telemechanics Type 7475 v.h.f. measuring set.

85 to 1,000 Mc/s using the fundamental and harmonic frequencies of the internal oscillator in each case.

Signals are picked up by a short aerial, heterodyned to zero beat and the frequency read off tabulated charts, housed in the drop-down cover, from dial readings. An accuracy of 0.002% at 25°C is claimed.

The sets can be used also as radiation-type signal

The sets can be used also as radiation-type signal generators with or without modulation at 1,000 c/s. While normally battery operated, provision is made for substituting a mains power unit if required. The price of each model is provisionally fixed at £245.

### Record Handling

A USEFUL tool for holding gramophone records has been produced by Claravox Products Ltd. This enables

records to be gripped by rubber-covered tongs at the edge and in this way the delicate playing surface of long-playing records can be protected against dust-collecting fingerprints. This instrument will perhaps be of most use in withdrawing records from their envelopes; if this is done by hand alone it is difficult to avoid touching the playing surface. Care must be taken to avoid flexing the record about the clamp—neglect of this precaution with shellac records could lead to breakages.

The instrument is called a Miragrip, the price is 18s 6d, and the address of the makers is 465 Walsgrave Road, Coventry.

### "Semi-Communications" Receiver

THE illustration shows a broadcast set having the rugged qualities, precision tuning and many features of a communications receiver. It is the new Eddystone Model 870 and as it is designed for operation on 110 V or 200/250 V d.c. or a.c. supplies it is particularly suitable for use on board ship. In addition to medium- and long-wave bands the set has two short-wave ranges, covering between them 1.95 to 18 Mc/s.

The circuit is reasonably orthodox and consists of a heptode frequency changer; pentode i.f. (465 kc/s); d-d-triode, detector, a.g.c. and a.f. and a tetrode, with negative feedback, feeding a built-in loudspeaker. An i.f. rejector is embodied in the aerial circuit and a filter in the mains leads to smooth out any "roughness" in ships' electric supplies. Thermistors and fuses safeguard the valves and the set.

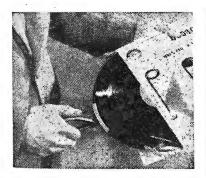
Like other Equipment sets the dial occupies the full width of the front and a long pendant pointer traverses the four full-length, frequency-calibrated scales as well as a special logging scale.

as a special logging scale.

Just above the last-mentioned is a small window through which is viewed a vernier logging scale which, used in conjunction with the coarse logging scale, enables the dial settings of stations to be recorded precisely for future occasions. This is invaluable on the very crowded short-wave bands.

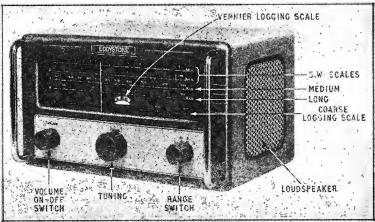
The "870" is housed in a two-tone grey metal cabinet measuring  $11in \times 6\frac{1}{8}in \times 8\frac{1}{4}in$ , it weighs  $11\frac{1}{2}$  lb and has tropical finish throughout.

The makers are Stratton and Co., Ltd., Alvechurch Road, West Heath, Birmingham, 31, and the price is £24 plus £10 16s U.K. purchase tax.



Claravox Products "Miragrip."

Eddystone Model 870 broadcast receiver.



WIRELESS WORLD, MAY 1957

# News from the Industry

R.E.C.M.F. Council.—At the annual general meeting of the Radio and Electronic Component Manufacturers' Federation on March 19th the representatives of the following firms were elected to the 1957/58 council: the representatives' names are in parentheses. Colvern (H. J. Mildren), De La Rue (C. R. Jennings), Garrard (H. V. Slade), Gresham Transformers (J. P. Coleman), Morganite Resistors (J. Thomson), Multicore Solders (R. Arbib), N. S. F. (K. G. Smith), Painton (C. M. Benham), Plessey (P. D. Canning), S.T.C. (E. E. Bivand), T.C.C. (W. F. Taylor), T.M.C. (E. Lawrence), Bulgin (A. F. Bulgin), Belling and Lee (E. M. Lee), A. H. Hunt (S. H. Brewell) and Wingrove and Rogers (A. J. D. Dobie). The chairman is Richard Arbib and the vice-chairman K. G. Smith.

A. B. Metal Products, Ltd., of Abercynon, Glamorgan, has been acquired by Gas Purification and Chemical Company. A. B. Metal Products have recently concluded an agreement with Standard Coil Products Inc., of Illinois, permitting them to manufacture under licence a "revolutionary type of television tuner." It is expected to be in production by the autumn. Among the companies already in the Gas Purification group are Grundig (Great Britain), tape recorders; Wolsey Television, aerials; Electric Audio Reproducers, sound reproducing equipment; Staar Electronics, record players; Kingsway of London, audio equipment; and Besson and Robinson, relays.

Peña Copper Mines, Ltd., are entering the field of electronics and have arranged to acquire an interest in three companies. The first to be announced is Peto Scott Electrical Instruments, Ltd., of Weybridge.

H.M.V.-Ferguson Merger.—A new company is being formed jointly by Electric & Musical Industries, Ltd., and Thorn Electrical Industries, Ltd., for the design and marketing of all domestic sound and television receivers under the Ferguson, H.M.V. and Marconiphone trade-marks. Production will be mainly centred at the Thorn factories at Enfield, Middlesex, and Spennymoor, Co. Durham.

E.M.I. Records, Ltd., has been formed by Electric & Musical Industries to co-ordinate the production, manufacture, marketing and distribution in this country and abroad of H.M.V., Capitol, Columbia, M.G.M., Parlophone and Regal-Zonophone records.

A modified version of the "Radiopage" r.f. induction staff-locating system (see W.W., July, 1956) has been purchased from British Communications Corporation by the Royal Navy for operational trials as a flight-deck communications system in aircraft carriers. Key men in the flight deck party will carry miniature receivers with earpieces in their noise-excluding helmets. As transmissions are not radiated outside the immediate area of the flight deck, secrecy requirements are fully met.

Technical Manuals.—British manufacturers obtaining contracts with the U.S. Department of Defense, which call for literature to U.S. specifications, may like to know an American company, Warner New York Corporation, is prepared to assist directly or indirectly in the preparation of such literature. Information is obtainable from the

general manager, Alfred Dinsdale (a contributor to Wireless World), at 750, James Street, Syracuse, 1, New York.

Data Recording Instrument Co., Ltd., with works at Hanworth Trading Estate, Feltham, Middlesex, has been formed to make components for computers. The company is initially concentrating on magnetic recording and reading heads. Among the directors are J. P. Coleman, founder and managing director of Gresham Transformers, and a director of Lion Electronic Components, and Dr. C. B. Speedy.

Murphy v.h.f. radio-telephone equipment, including a base station (MR862) and eight mobile units (MR800), has been installed for the South Devon Water Board by R. B. Holman, radio dealers, of Kingsbridge and Salcombe, Devon.

The manufacturers of Raymond and Beethoven television receivers have made arrangements with **Direct TV Replacements** (134-136, Lewisham Way, London, S.E.14) for them to manufacture replacement components for all models other than the current range. The main components included are e.h.t. line output transformers, frame transformers and deflector coils. Direct TV Replacements already have similar arrangements regarding Baird, Etronic and R.M. Electric receivers.

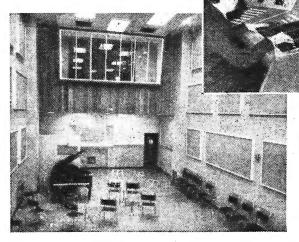
#### WORKS EXPANSION

A five-storey building in Liverpool, with a floor space of 55,000 square feet, has been purchased by Automatic Telephone & Electric Company to expand production in the electronics field. This is in addition to the company's main factory at Strowger Works and several other smaller factories in the area.

Building has started on a new 45,000-sq ft factory at Martin Street, Airdrie, for the Pye subsidiary, Pye Scottish Telecommunications, Ltd. The present factory employs about 130 and produces 1,000 broadcast receivers a week, of which roughly one-third is exported. The new factory, which should be ready next March, will employ over 400.

Fringevision, Ltd., television aerial manufacturers, of Elcot Lane, Marlborough, Wilts., are extending their factory buildings; when completed, floor space will be trebled to 15,000 square feet.

Trix Electrical Company, of Maple Place, London, W.1, have acquired additional factory premises at Wish Road, Eastbourne, for the production of sound reproducing gear.



PHILIPS new recording studio at Stanhope House, Stanhope Place, London, W.2, can be booked by organizations or individuals for all types of recording. From the console (inset) the recording engineer has complete remote control of the recording facilities, which include tape and

#### NEW ADDRESSES

Modern Techniques (S. Korobuk, Ltd.), makers of Motek tape recorders, have closed their factories in north London and have moved to larger premises at Wedmore Street, London, N.19. (Tel.: Archway 3114.)

Tellux, Ltd., distributors of Telefunken receivers, components (including transistors) and accessories, have moved from Kensington to 146, New Cavendish Street, London, W.1. (Tel.: Langham 2411.)

Telerection, Ltd., aerial manufacturers, of Cheltenham, Glos., have opened a wholesale depot at 149, Lower Cheltenham Place, Bristol. (Tel.: Bristol 57888.)

The new address of the Bristol depot of Aerialite, Ltd., is Portland House, Portland Square. (Tel.: House, Portla Bristol 26130.)

#### OVERSEAS TRADE

Provisional figures for the radio industry's exports in February are the highest on record for that month -£3.62M-and £400,000 more than in January.

South Africa has been added to the list of countries-including Australia, New Zealand, India, South America and Eire—in which E. K. Cole have financial interests in manufacturing companies. The export of goods from the U.K. to each of these countries is restricted. The new member of the Ekco overseas companies is Kruger & Wilson, Ltd., which represents them in South Africa and the Rhodesias.

The complete nucleonic instrumentation and control circuitry for the first experimental atomic reactor to be exported from this country is being supplied by Ekco Electronics, Ltd. The equipment is for the Australian reactor to be built at Lucas Heights, near Sydney.

S.H.F. Radio Network.—The installation of a chain of radio stations between Osaka and Fukuoka, Japan, covering a distance of nearly 400 miles, has been completed by Standard Telephones and Cables through their associates, the Nippon Electric Company, of Tokio. The network, including eleven intermediate repeater stations operating in the 3800-4200-Mc/s band, provides for three two-way channels. One will be used for a television link, another for 240 telephone channels, and the third kept as a stand-by for either television or telephony.

Milan Fair.—Among the 400 exhibits selected by the Council of Industrial Design for the Board of Trade's stand at the International Samples Fair, Milan (April 12th to 27th), is the Ekco portable television set. The Pye "Jewel Case" portable cound receiver Ekco 1245. set. The Pye "Jewel Case" portable sound receiver, Ekco U245 medium- and long-wave table receiver, and a portable electric gramophone Electric by Audio Reproducers, are also included.

F.M. Transmitters.—The Swedish Royal Board of Telecommunications has placed orders with Marconi's for the supply of twelve 5-kW frequencymodulated v.h.f. broadcasting transmitters together with three combining units. One transmitter has already been supplied and is in operation at Ostersund.

Two transmitters (5 and 7.5 kW) have been ordered from Marconi's for the Aden broadcasting service. They are due to be brought into service this summer.

Guy Barreyre, of 114, Rue Dantes Destouches, Port-au-Prince, Haiti, would like to represent a leading United Kingdom manufacturer of domestic broadcast receivers.

An order for tens of thousands of Monarch automatic record changers has been placed with Birmingham Sound Reproducers, Ltd. by a German radio manufacturer.

# MAY MEETINGS

LONDON

London U.H.F. Group.-2nd. "Amateur television convertor for u.h.f." by a member at 8.0 at the Bedford Corner Hotel, Bayley Street, W.C.1.

6th IFR—Discussion on "The

ford Corner Hotel, Bayley Street, W.C.1.
6th. I.E.E.—Discussion on "The
co-ordination of education and practical training in sandwich courses"
opened by C. Grad and A. Draper at
6.0 at Savoy Place, W.C.2.
6th. Institution of Post Office Electrical Engineers.—"The Rugby 'B'
h.f. radio transmitting station" by A.
Cook and L. L. Hall at 5.0 at the
I.E.E., Savoy Place, W.C.2.
15th. I.E.E.—"Transistor circuits
and applications" by A. G. Milnes at
5.30 at Savoy Place, W.C.2.
22nd. Brit.I.R.E.—"Barium titanate
storage cells" by G. Campbell at 6.30
at the London School of Hygiene and
Tropical Medicine, Keppel Street,
W.C.1.

23rd. I.E.E.—"General applications of digital computers" by Dr. A. D. Booth at 6.30 at Savoy Place, W.C.2. 25th. London U.H.F. Group.—U.h.f.-v.h.f. convention from 10.0 a.m. at the Bonnington Hotel, Southampton Row.

MALVERN

3rd. Brit.I.R.E.—"Marine radar" by H. R. Whitfield at 7.0 at the College of Electronics.

RYDE (Isle of Wight)
9th. I.E.E.—"Colour television"
by C. J. Stubbington at 6.30 at the Ryde Castle Hotel, The Esplanade.

TORQUAY

9th. B.S.R.A.—"A quart in a pint pot: the development of a loudspeaker" by A. R. Neve at 7.30 at Callard's



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Wireless World, May 1957

# RANDOM RADIATIONS

# By "DIALLIST"

# The Kingsand Effect

SEVERAL interesting letters have reached me on the subject of the Kingsand Effect, which was described on p. 102 of the March issue. One of my correspondents, M. E. Northey, lives at Belstone, near Okehampton, close to the 1,000ft above m.s.l. contour. He is only 12 miles from North Hessary Tor, but obtains very poor reception from that station. His home is three miles from Steeperton Tor (1,739ft) and one mile from Belstone Tor (1,568ft). The direct line from his aerial passes between the two over an intervening ridge. He obtains a venetian blind type of patterning which travels upwards over the picture, one line taking about three seconds to move from bottom to top. Then after a period varying from  $2\frac{1}{2}$  to  $3\frac{1}{2}$  minutes on different days the pattern changes its direction and travels downwards. There is some variation in the brightness, though this is not as a rule very pronounced. Mr. Northey mentions that Dartmoor is very rich in metallic deposits (it was for centuries an important tin-mining area) and wonders whether this might be the reason for the reflections that give rise to the interference. I suppose that's a possibility; but I'm more inclined to think that the French TV transmitter at Caen may be responsible. Its 819-line transmissions cover the whole of our Channel 1 and a good deal of Channel 2, the latter being the one used by North Hessary Tor. My correspondent mentions that he has occasionally heard French speech.

# Sunspots to Blame

Mr. Northey wonders whether Holme Moss, also on Channel 2, could not be the culprit. There have, if I remember aright, been complaints of interference due to this station at surprisingly great distances. If it is the offender in the present case, the effect would undoubtedly be due to the freak long-distance reception so frequently reported during the present sunspotty period. This doesn't seem unlikely since very good reception is sometimes obtained at Belstone from Sutton Coldfield, which is 145 miles away. I suppose

that when we have passed the sunspot maximum and begin to get nearer and nearer to the minimum, interference at great distances will become steadily less and less. Let's hope so anyhow.

#### Poor Fish!

WHEN you think of the relentless way in which they're harried day in, day out, night in, night out all through the year, you might be tempted to wonder that there are any fish left, particularly in such hardfished waters as those that surround these islands of ours. The modern trawler (which costs almost as much as a destroyer of yesteryear) carries a remarkable amount of electronic equipment. One gadget in particular, the fish-finding echo-sounder, is a very deadly weapon. It can be set to give distant "views" of quite large areas of water as the ship steams along in search of her quarry. Then when the right indications are seen it can be switched so as to show a close-up of a limited area. From the size of individual members of the shoal, their formation and their movements the fish can be identified with something like certainty by a practised eye. If they're of the kind wanted, down goes the trawl and a good catch is a certainty.

# For It Again

And now one reads of still another anti-fish device, which has given very promising results in experimental trials by Pye. It consists of a torpedo-shaped case, containing a device working on echo-sounding principles by transmitting a.f. pulses down towards the sea bed. It is towed by a helicopter, flying low over the surface, and signals from it travel up leads incorporated in the towing cable to a display unit in the aircraft. The big advantage is this. To make use of her fish-finding gear a trawler has to steam at no very great speed and it may be hours, or even days, before a shoal of worth-while size is found. The helicopter travels much faster and in a given time can cover a far greater expanse of water with her towed locator. As soon as she has a find, she transmits the position to the fleet which she serves and the hunt is on without a moment's waste of time. This is but one of a number of applications of echosounding from the air, which include salvage work and mine detecting. Electronic gadgets aren't always used to catch fish. Much use is made by marine biological establishments of the underwater television camera for the study of the breeding places and breeding habits of fish, so as to en-

#### ILIFFE Net Βv TELEVISION ENGINEERING: Principles and Practice. Volume III: Waveform Generation. S. W. Amos, B.Sc. (Hons.), A.M.I.E.E. and D. C. Birkinshaw, M.B.E., M.A., M.I.E.E.... 30/-30/11 TELEVISION RECEIVING EQUIPMENT. W. T. Cocking, 30/-4th Edition 31/6 13/6 18/6 RADIO VALVE DATA: Characteristics of over 2,500 Valves, Transistors and C.R. Tubes. Compiled by Wireless World ... SECOND THOUGHTS ON RADIO THEORY. "Cathode Ray" 5/7 25/of Wireless World 26/2 25/-26/6 25/-25/9 12/6 13/3 Sixth Edition ... ... ... ABACS OR NOMOGRAMS, A. Giet

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Wireless World, May 1957

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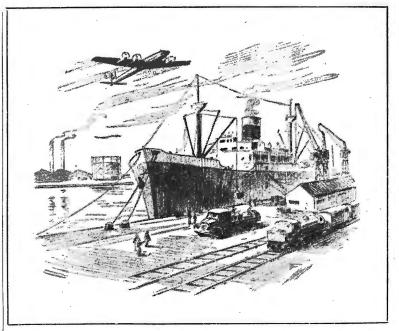
# Keeping Up With the Joneses?

THE tendency is for the living rooms of to-day to be quite small compared with those of years ago; yet one finds people going in for larger and larger TV screens. How many homes do you know in which people have 17-inch or 21-inch sets and can't (at any rate, in winter time) sit far enough away from them to rid the picture of lininess? I know quite a few. There's an idea amongst the uninitiated that you see more on a large screen than on a small one. You don't, of course, and if you sit at the proper viewing distance from each, a 12-inch screen gives exactly the same sized image on the retina as one with a larger screen. With a 405-line standard a useful rule of thumb is that for people with normal vision the minimum viewing distance in feet is half the screen size in inches. You can sit nearer than that with the 625-line standard used in most continental countries which have television services and still nearer to a screen displaying the admirable French 819-line picture. I hear that 30-inch c.r.t.s are appearing in America. If they are developed here there'll be a rush for them by the 14-inch Browns, who want to go one better than the 17-inch Robinsons and the 21-inch Joneses! But how are they going to contrive an eye-to-screen distance of 15 feet in their bungalow?

# Where Your Money Goes

A KIND reader sends me a copy of the Post Office Engineering Union's Journal, which gives an interesting account of the way in which the £3 that we pay for our combined sound and television licence is absorbed. The G.P.O.'s share is 4s, which seems modest when you come to think that it pays not only for the work of issuing the licences, but also for the services of those most helpful and obliging P.O. engineers who come to our aid when we're troubled by interference. The Government's whack is 5s 4d, which, I imagine, just goes into the general kitty. The B.B.C. gets what's left, £2 10s 8d, of which 16s 11d is applied to sound broadcasting and £1 13s 9d to television.

The figure quoted by "Diallist" at the top of the second column of p. 200 last month should have been £2 12s 6d.—Ed.





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# By FREE GRID

# Why 0-V-1?

I WONDER how many readers under thirty years of age will have any idea what 0-V-1 means? Very few I think, and yet in the twenties and early thirties this piece of shorthand was as well known as the vital statistics of film stars are to-day.

For the benefit of the new generation I would like to explain that in pre-superhet days this trinity of symbols told us at a glance the number of valves, if any, the set contained, their functions and if the set used a valve (V) or a crystal (C) as a rectifier. A 0—V—1 set therefore had no r.f. stage, used a valve recti-

fier and had one a.f. stage.

I am moved to discuss this question because this method of describing a set is used in a recent issue of the Russian journal Radio. There is nothing strange about the 0 and the 1 being used as the Russian numerals are the same as ours. But the Russian word for valve is "lampa" and one would therefore have expected the Cyrillic equivalent of the letter L—a slight variant of the Greek lambda-to have been

It cannot be doubted that the readers of this Russian journal fully understand the meaning of the expression 0—V—1 or the editor would not permit his contributor to use it. But probably some of the Russian readers don't understand what the "V" stands for; in that respect they are no more ignorant than many people in this country who could not say exactly what Latin words are represented by £sd—especially the s.

# R.I.C. Please Copy

ON SEVERAL occasions I have pointed out the difficulties of trying to choose between the various makes of any particular product shown at the National Radio Show. Suppose, for instance, I want to buy a tape recorder. When I go to the radio show I naturally want to look at all

Taking no chances

the various makes and compare one with another as we do the horses in the paddock at Ascot before we place our humble bets.

But at the radio show the state of affairs is quite different from that prevailing at Ascot. Having seen one tape recorder I have got to fight my way through the crowds to the far end of the exhibition hall to the stand of the manufacturer of the second instrument on my list.

I have often advocated that while each radio manufacturer continued to have a stand of his own as at present there should be other stands on which all tape recorders, all f.m. receivers, all television receivers, etc., of whatever make, be grouped to-gether. Visiting the Ideal Home Exhibition a few weeks ago, I found that the electrical industry had done this very thing.

Each of the large manufacturers had his own stand on which he showed the usual motley collections of cookers and kettles. But in addition there was one very large stand run by the electrical industry on which all makes of water heaters, cookers, and so on, were grouped together. I was able to compare one with another in comfort.

Actually I was told this stand was run by the Electrical Development Association. Why have we no similar organization in the radio industry? If we have, then its publicity man ought to be sacked, as I have never heard of it.

# **Statogenetics**

I HAVE received some interesting data from a South African radio engineer regarding the use of a dangling chain for conducting to earth the static charge on the body of a car about which I wrote in

In the Kimberly district, which is 4,000 feet up and where the air is very dry, static discharges are one of life's bugbears, and my correspondent mentions that when his wife brushes her hair it

results in crackling static. Over a quarter of a century ago I referred in these columns to a similar sort of thing happening when a lady removed her silk stocking and I reproduce my sketch in the next column.

Actually the same problem arose many years later when TV came to the fore. Considerable interference was noticed in the vicinity of a well-known school when

several hundred pairs of stockings were whisked off at bedtime. It was at first proposed to stop the trouble by encasing the dormitories in earthed wire netting, but it was thought that uncouth people of the sort who are fond of expressions with a double meaning might refer to the school as the "bird cage." The prob-



Shocking

lem was, however, instantly solved when the headmistress installed TV for her own use. The girls were sternly ordered, sub pæna, to remove all statogenic garments in slow

My Kimberly reader tells me that anybody alighting from an unearthed car obtains quite a healthy shock as the dry climate results in the building up of a strong static charge. At one time all motor vehicles carried a dangling chain but nowadays the problem is solved by using tyres processed with more carbon in the rubber, so greatly reducing their insulating properties. I am interested to learn, however, that car sickness from static build-up has not been heard of by my correspondent. This confirms my own view that the vogue for this malady in this country is due solely to suggestion.

# Wot! No F.M. Aerial?

WHILE prowling through the Ideal Home Exhibition I was interested to note that on the full-sized houses erected in the vast exhibition hall TV aerials were fitted. But not one of the houses I examined had a horizontal dipole for v.h.f. sound broadcasting.

This set me examining houses in the Greater London area, and I have been astounded at the scarcity of v.h.f. aerials. I am perfectly aware that in most London districts Wrotham comes in well without the help of an outdoor dipole. So does television in many London districts, but the majority of people use an outdoor

Can it be that, unlike TV, a v.h.f. aerial has no snob appeal?

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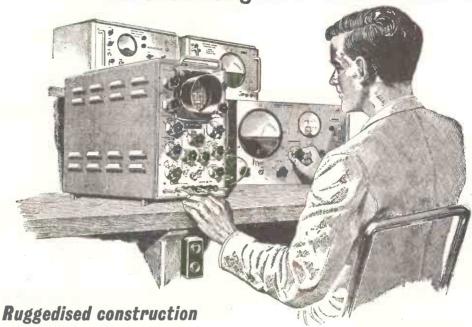
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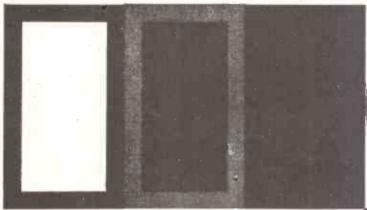
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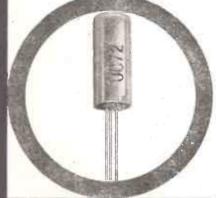
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Seven pages of data and curves on the OC72 and full information on other Mullard transistors are readily available upon request.

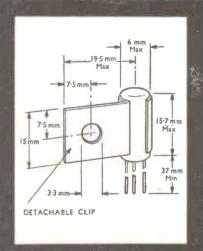
#### ABRIDGED DATA

Max. collector voltage*		
Max. collector current	250mA peak	125mA average
Max. power dissipation at 45°C:		
Without heat sink	75m W	
With heat sink		
Min. cut-off frequency		
(in grounded base condition		
$at 6V, I_c = 10mA$ )	350kc/s	

\*In grounded base or in grounded emitter with a base emitter resistance of less than  $1,000\Omega.$ 

### CHARACTERISTICS OF MATCHED PAIRS

(Two transistors in class "B" push-pull: gr	ounded	em	itter)
Output (without heat sink)			275m W
H.T. voltage	+ + + +	x 3/5	6V
Quiescent H.T. consumption			3mA
Load impedance (collector to collector)			Ι 40Ω
Full drive collector current (peak)			125mA
Full drive collector current (average)			40 m A
Total harmonic distortion (full drive)		0.00	9%
Total harmonic distortion (50mW output)	9.674		5%



See Mullard valves and tubes on Stand No. 305 at the Instruments, Electronics & Automation Exhibition, Olympia—7th to 17th May.

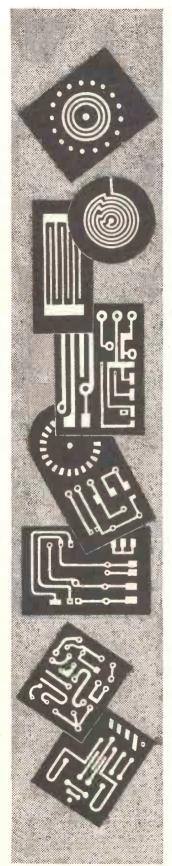




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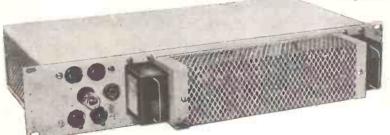
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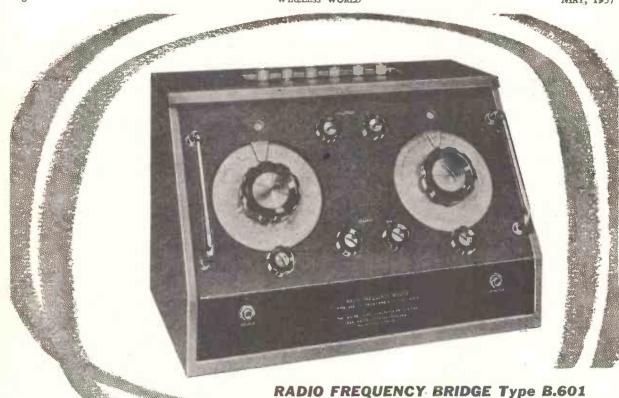


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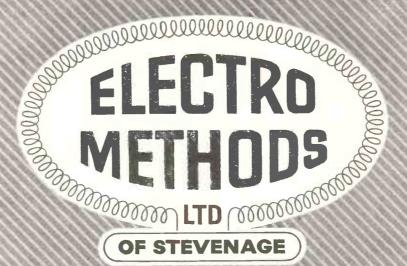


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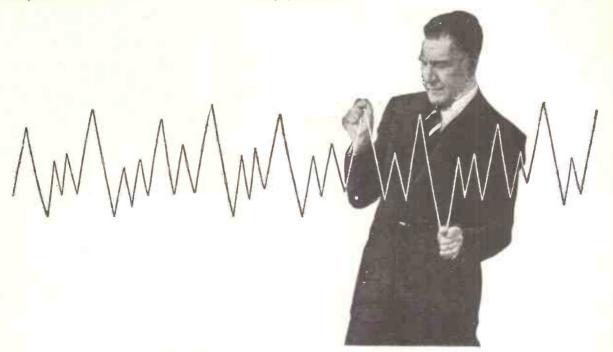
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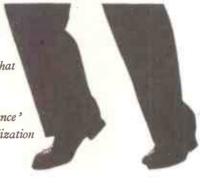
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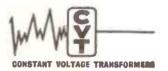
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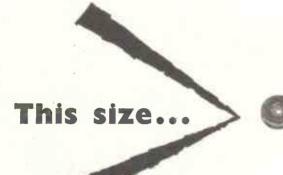
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# ...and smaller!

This is a small carbon track Precision Resistive Element a mere 10 mm. in diameter—but it isn't the smallest which can be produced by Plessey at Swindon. Neither is it the largest. They range up to 4" in diameter and, in their various forms, cover a wide field of applications.

By a recently developed technique, it is now possible to join straight Precision Resistive Elements to form electrically continuous tracks of several feet in length. Such tracks are used in automatic machine tool control. The track itself, normally carbon type, can alternatively be produced in a silver loaded, high conductivity material for multi-pole switches or commutators. These are suitable for continuous high-speed rotation and have an extraordinarily long life. Products of this type have many applications in spheres of telemetering, computers and instrumentation.

# Plessey

# **Precision Resistive Elements**

are employed in these important applications ...

Guided weapons
Machine tool control
Movement indication and control
Liquid level control and remote indication
Continuous rotation potentiometers
Sine cosine potentiometers
Precision potentiometers with special laws
Tagless track potentiometers
Stepped attenuators
Strain gauges
Pressure sensitive elements

COMPANY MEETING

# MARCONI'S WIRELESS TELEGRAPH YEAR OF PROGRESS

# SIR GEORGE H. NELSON'S REVIEW

The 59th annual general meeting of Marconi's Wireless Telegraph Co., Ltd., was held on March 14th in London.

Sir George H. Nelson, Bt., F.C.G.I., M.I.Mech.E., M.I.E.E., chairman, in the course of his speech, said:—

No Company can hope to maintain world leadership without making a substantial contribution to research, and it is with pride that I tell you of our expanding research effort, already the greatest of its kind in Europe. New and important extensions to our research laboratories will come into use during 1957.

#### FRUITS OF RESEARCH

Our scientists and engineers have achieved very significant results for the future in many fields.

Firstly, in the communications field we have made very great advances in microwave radio links. Our latest link will carry no less than 600 telephone channels, or alternatively a television signal in black and white or in colour.

Secondly, advances have been made in the Ionospheric Scatter technique of radio communication. This Very High Frequency system enables a useful number of messages to be transmitted simultaneously over longer distances than was hitherto possible and at all times of the day. Previously communication was often lost over long periods.

Lastly, in the vitally important field of air navigation we are now able to reveal that we have been in the fore-front in developing and manufacturing a revolutionary airborne navigational aid of great accuracy, known as the Doppler Navigator. This device gives a continuous pinpoint plotting of an aircraft's position to a high degree of accuracy without using any ground based aids.

Reviewing now your Company's main lines of activity I would comment as follows:—

#### SPREAD OF TELECOMMUNICATIONS

We have received orders for Ionospheric Scatter equipment from the Ministry of Supply for a new communications system between the United Kingdom and Malta.

During 1956, we strengthened still further our position in the field of microwave links, and installations are proceeding all over the world.

In Nigeria, we have been awarded an additional contract for maintaining the extensive Marconi multi-channel network and for establishing a Training College, under the auspices of our own Marconi College, for the advanced training of Nigerian technologists.

#### GROUND RADAR FOR MILITARY AND CIVIL USE

We have developed and put into production a series of very efficient high power early-warning radars, and a further range of new equipment is under development.

Your Company has always been a pioneer in the field of specialised radar display equipment. Our present programme is geared to meet the ever increasing demand created by the problems of supersonic flight and the advent of guided weapons upon the subsequent presentation of the radar information.

#### AIR SAFETY IN THE JET AGE

Our "Doppler Navigator" has given outstanding operational service with the Royal Air Force, and orders have been received from Commonwealth Air Forces.

We have been eutrusted by B.O.A.C. with the preparation of a radio system for their Comet IV aircraft, and I would add that this installation will be one of the most complete ever undertaken for an air-line operator.

Our Transmitter/Receiver has been chosen for B.O.A.C.'s long-range Britannia airliners on which will also be installed a pair of our famous radio compasses.

#### TELEVISION

The most outstanding event of the year in this field was the inauguration of television services in yet another continent—the Commonwealth of Australia. This great task was completed in time for the Olympic Games in November, and all reports speak of the high quality of the pictures transmitted. I am proud to say that Marconi's were responsible for four of the first six stations, two in Sydney and two in Melbourne, the total value of these contracts amounting to approximately £1,000,000.

In Denmark, the last of the first three stations, with their Marconi vision and sound transmitters and aerials, was completed last year.

At Home, work completed for the B.B.C. in 1956 included the transmitters and much other equipment for the new Crystal Palace station, and cameras and other equipment for the new Riverside Studios in London.

For the I.T.A., the completely Marconi-built and equipped station for the North of England at Winter Hill and Emley Moor, came into operation in 1956, both completed in a remarkably short time. We have also been awarded the contract for the transmitting equipment for the I.T.A.'s Scottish Station, due for completion this summer. Large Commercial Television studio centres were completed at Manchester, Birmingham and London for which your Company provided a large part of the equipment.

In the B.B.C.'s recent colour television demonstration for the Houses of Parliament the transmitting and camera equipment were of Marconi design and manufacture as also were those used for the regular trial transmissions during the year.

#### 40 VHF TRANSMITTERS FOR THE B.B.C.

Our new range of VHF F.M. transmitters has put us in a strong position in this field, and important orders have been received, including one for 12 transmitters for Sweden. At home, we completed the installation of no less than 40 of these transmitters at seven different sites for the B.B.C.

During the year we installed two high power transmitters for the new Baghdad station; nine for the Paradys station in South Africa; three for Cyprus and others for Ghana and Denmark. Orders are in hand for transmitters for the Sudan, Aden, Sarawak and Brunei, once again emphasising the world-wide nature of our business.

#### CONFIDENCE IN THE FUTURE

We are very much alive to growing competition overseas, but with our wealth of research, development and production facilities, we can face the future with every confidence.

The report and accounts were adopted.



Delaron

(by De La Rue)

# does a double act for you

You already know DELARON as a laminated insulant of precisely known dielectric values and mechanical properties which fully meet all British Standard and Ministry specifications at every grade. It is used as a controller of electricity, from loudspeaker spiders to insulating washers.

But do you know about the second half of the double act by DELARON laminates?

In its copper-clad form it is the basis of most of the printed circuits in radio, television, radar and electronic computors—the new, simpler and cheaper method of circuit manufacture.

You should use DELARON laminates. For information, advice and service get in touch with Dept. D8G, Thomas De La Rue & Co Ltd., 84-86 Regent Street, London, W1.

for the closest approach to the original sound



QUAD II

**AMPLIFIER** 

The criterion, as always, is that the reproduced sound shall be the closest approach to the original — that the enjoyment and appreciation of music may be unimpeded. This is reflected throughout the design of the QUAD II. It is reflected, too, in the straightforward and logical system of control, achieved without the sacrifice of a single refinement or adjustment capable of contributing to the final objective.



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the design, development and manufacture

of loud-speakers for all purposes . . . world

famous for quality of reproduction, sensi
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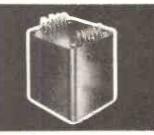


re specifying



TRANSFORMERS

Left: Potted Compound Filled Transformers. A wide range of capacities for transformers and chokes. Complete reliability. Suitable for exacting industrial and climatic conditions.



Above: Cast Resin Transformers. Give complete mechanical and climatic protection for core and windings. Good heat dissipation.

Bottom Left: Shrouded and Open-Type Transformers. Combine first-class engineering with a popular highly competitive product. Vacuum impregnated and rigidly tested.

WODEN TRANSFORMER CO. LTD

Catalogues available on request.

WODEN TRANSFORMER CO.LTD

MOXLEY ROAD
BILSTON - STAFFS

# Question "Why don't dealers stock and recommend our Amplifiers and Tuners, etc?" Answer "Because they cannot afford to as we give their discount to YOU (the public)."

This direct trading explains why our products, though in the top class, are so much cheaper than our competitors.

What we are and what we do.

Firstly we are quite large manufacturers of Audio Amplifiers, Radio Feeder Units, Tape Recorders, Portable Record Players, Speaker and Amplifier Cabinets and custom built Complete High Fidelity Radio and Record Reproducers.

Secondly we are Retailers of Gramophone Units, Autochangers, Speakers, Tape Recorders, etc., etc.

We recommend only that which we know to be of good performance and of sound construction. We are not in the group of traders who sell job lines at apparently low prices because they are obsolete or faulty. On the other hand our finances are such that we do not have to sell you an expensive article if we know that a less expensive unit will do your job perfectly.

If any reader should have his mind set on a high-priced amplifier of

another make and would like to save money if possible, we should like to make the following clear-cut offer: If he buys one of our "Symphony" Amplifiers or Tuners and is not entirely satisfied with it he may return it for full credit against any other amplifier or tuner on the market. It should be emphasised at this stage that we can supply any Amplifier, Radio Tuner, etc., advertised.

Our Chief Engineer, who is operating a Technical Guidance Service, is available daily including Saturdays from 10 a.m. to 6 p.m. or will deal with enquiries by return of post.

Our new illustrated Catalogue and supplement will be a great boon to our new injustrated Catalogue and supplement will be a great boon to those desiring quality equipment for modest expenditure. Send two 2½d. stamps for your copy now. It may well save you pounds! All our equipment is on demonstration at our showroom in conjunction with a variety of Pickups, Speakers, etc. If you can possibly call we shall be pleased to see and help you. H.P. facilities available.

It is essential to mention "Wireless World" when requesting Catalogue or when ordering.

# WE ARE HOLDING OUR OWN AUDIO FAIR IN OUR DEMONSTRATION ROOMS

The New No. I "SYMPHONY" AMPLIFIER MARK III is a 3-channel 5-watt Gram/Radio Amplifier MARK III is a 3-channel 5-watt Gram/Radio Amplifier with astonishingly flexible tone control. You can lift the treble, the bass, or—and here is the unique feature—the middle frequencies to suit your own ear characteristics and the record or radio programme being heard. It is thus possible to arrange the frequency-response of the amplifier to a curve equal and opposite to the resultant curve of the other items in the chain so what finally registers in the brain is as per original. This flexibility of control is even more important than the nominal linear response of the amplifier, as the pick-up speaker, etc., are not linear. Independent Scratch-Cut is also fitted and special negative feedback circuit employed. The Amplifier not linear. Independent Scratch-Cut is also fitted and special negative feedback circuit employed. The Amplifier can accommodate a wide variety of records from old 78s can accommodate a wide variety of records from old 78s to new L.P.s., and there is full provision for Radio Tuner, Tape take-off and Playback. It is available to match 2/3 or 15 ohms speakers. Price 12 gns. (carriage 7/6). Fitted in portable Steel Cabinet. 2 gns. extra.

The New No. 2 "SYMPHONY" AMPLIFIER MARK III, as No. | but with 10-watt Push.

watt Push-Pull triode output and triodes throughout. Woden mains and output transformers and choke. Output tapped 3, 7.5 and 15

ohms. Pro-

Tuner and Tape. Competes with the most expensive amplifiers on the market yet costs only 16 gns. (carriage 7/6). Fitted in portable Steel Cabinet, 2 gns. extra. "SYMPHONY" AMPLIFIERS WITH REMOTE CONTROL



Both the above model Amplifiers are available with all controls on a separate Control Panel with up to 4ft. flexible cable which simply plugs into the amplifier Enables the Amplifier proper to be sat in the bottom of a cabinet whilst the controls are mounted conveniently

higher up. Extra cost 2 gns.
No. 1 "SYMPHONY" F.M. TUNER. High grade
Instrument with extremely silent background. Based on the

latest type of permeability tuned Coil Assembly of advanced design housed in anti-radiation shroud giving extreme sensitiextreme sensitivity and high music/noise ratio. Suitable for amplifiers in the highest fidelity class. £15/8/-.



class. £15/8/-.
Power Pack £3/7/6. Magic eye £1 extra if required.

N.R.S. EMPRESS FM/VHF TUNER/ADAPTOR Fine little job. Will plug into any radio and add F.M. £13/15/-. Magic eye assembly £1 extra if required. Ditto mounted in beautiful dark walnut cabinet complete with magic eye 17 gns. Carriage 7/6.

tions o our Long. Medium and Short wave Superhet AM Tuner and our No FM Tuner. Separate Coil Assemblies and IFs Fully self-powered on one chassis.



26 gns. "SYMPHONY" AM/FM RADIOGRAM CHASSIS "SYMPHONY" AM/FM RADIOGRAM CHASSIS Mk II. Very high grade Radiogram Chassis incorporating the Long, Medium, Short and VHF Bands; nine valves including new fan-type, built-in Magic Eye; push-pull output for high quality reproduction. Input sensitivity adequate for Studio. Professional quality (P) and transcription (PX) pick-up cartridges. New type ultrasensitive, anti-radiation, no-drift F.M. front-end; built-in ferrite rod A.M. aerial; plug-in F.M. indoor dipole aerial supplied free. Negative feedback; 15 ohms tapped 3 ohms output; entirely new-look German-type dial and knobs in gold, brown and cream, measuring 15in. x 6in. gold, brown and cream measuring 15in. X 6in. horizontally. Depth front to back 8in. An extremely attractive up-to-the-minute instrument, Price complete with 10in. Goodmans Loudspeaker. 26 gns., plus carriage 10/-. Alternatively, allowance made on standard speaker against a more expensive, high fidelity speaker. Delivery from stock.

RECOMMENDED GRAMOPHONE UNITS COLLARO 4-SPEED SINGLE PLAYER AC4/564,

New model RC456, 4-speed mixer changer £13/17/-NEW MODEL GARRARD RC88 AUTOCHANGER £15/11/4. RC98 £17/10/3. Prices les's head.

Variety of pickup cartridges available in Garrard shell to fit. Leaflets on Collaro and Garrard Gram. Units on

LENCO GL50. 4-speed continuously variable from above 78 r.p.m. to below 16 r.p.m. Special Autostop. Price with Studio "O" or "P" head or Goldring Model "500" variable reluctance head, £21/17/10.

LENCO GL55, as above but without pickup and auto-stop but fitted with special device for Groove Location and knob which completely disengages drive-wheel. Suitable for use with any pickup, especially transcription types and B.J. Arm. Price £17/10/4. Immediate delivery guaranteed.

ENCLOSURES TO GOODMANS "SHER-WOOD" DESIGN. Walnut or mahogany, complete with Acoustical Resistance Unit, 19 gns., or less A.R.U., 16½ gns. MIDAX/TREBAX CABINET. To match "Sherwood' (Viscount) 8 gns.

"SYMPHONY" BASS REFLEX CABINET KITS. "SYMPHONY" BASS REFLEX CABINET KITS.
30in. high, consist of fully-cut \(\frac{2}{2}\)in. thick, heavy, inert, nonresonant, patent acoustic board, deflector plate, felt, all
screws, etc., and full instructions. 8in. speaker model,
85/—, 10in speaker model, 97/6. 12in. speaker model,
£5/7/6. Carriage, 7/6. Ready built, 15/— extra.
As above but fully finished in figured walnut veneer
with beautiful moulding and speaker grille. 10in. £11.
12in. £11/10/—. Other veneers to order.

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DEPT. WW., 11, KINGS COLLEGE ROAD, ADELAIDE ROAD, LONDON, N.W.3. Phone: PRImrose 3314 Tubes. Swiss Cottage and Chalk Form Buses: 2, 13, 31, 113 and 187 CONSOLE AMPLIFIER
CABINETS. 33in. high, lift-up
Ild with piano hinge, take Tape
Deck, Gram Unit or Autochanger,
Amplifier, Pre-Amplifier, and
Radio Feeder Unit, finished
medium walnut veneer. De
luxe version, price 12 gns. medium wainut veneer. De luxe version, price 12 gns. Oak or mahogany veneers and special finishes to order. Carriage according to area. We will quote by return.

NORDYK CABINETS. Spea-NORDYK CABINETS. Speaker Enclosure £5/17/6. Table Model Amplifier/Gram Unit Cabinet £5/19/6. Table Model Tape Recorder Tape Amplifier or Radio Tuner Cabinet £5/19/6. Record Storage Cabinet holding 150 records £4/17/6. All above cabinets measure (internally) cabinets measure (internally) 19in, wide x 13in, high x 13in, deep and finished in polished walnut, thus enabling a complete installation to be built up unit by unit in matching style cabinets and added to as required.

We can supply Amplifiers We can supply Amplifiers, Tuners, Gram units, Tape Decks and speakers mounted in these cabinets. Examples on demonstration.

TAPE RECORDER DEPT. We are specialists in the supply of tape gear for use in conjunc-tion with High Fidelity Equip-ment. We are familiar with all worth-while Tape Recorders and Decks on the market and are in a unique position to advise on Tape Recorders, Tape Decks, Tape Amplifiers and Tape Pre-Amplifiers and give unbiased opinions and demonstrations. All those intending buying a Tape Recorder or adding Tape facilities those intending buying a Tape Recorder or adding Tape facilities to their present systems are advised to consult us before spending money, as we might well be able so save you money and dissatisfaction. Call for a demonstration, or write.

THE "SYMPHONY" DE-LUXE TAPE RECORDER.
2-speed twin-track, microphone, radio and gramophone inputs. Facilities for playback through high quality internal elliptical speaker or through external high fidelity speaker or through external high fidelity amplifier. Automatic head demagnetisation. Wide frequency range heads. Wide frequency range heads. Housed in handsome polished walnut cabinet. Fantastic value for money at 49 gns. or 9 monthly for money at 49 gns. or 9 monthly payments of 6 gns. Plus carriage and packing £1. Full details in catalogue. Also available with built-in revolution counter for 52 gns. or 9 monthly payments of £6/13/-. Recommended microphones: Ronette 5742 at £10/4/- or \$53 at £2/15/-.

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STRENGTHENED EXTRUDED ALUMI-NIUM COVER WITH RIGID CABLE CLAMP, TOP OR END CABLE ENTRY

**OPTIONAL LATCH PREVENTS** ACCIDENTAL DISENGAGEMENT AVAILABLE FOR ALL COMBINATIONS



MASK TO PROTECT PINS OF PANEL-MOUNTED PLUG

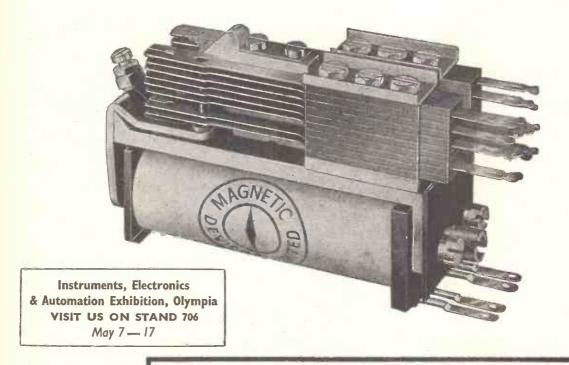
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# series 305 relay



#### P.O. 3000 RELAY

This Relay is the well known P.O. 3000 Relay and can be supplied with coils wound for standard voltages up to 250 volts D.C.

Contact assemblies are available up to six pole changeover and alternative rivets can be supplied to suit varying duties. The Series 305 Relay can be slugged for make or break action and ooils can be vacuum impregnated for tropical and humid conditions.

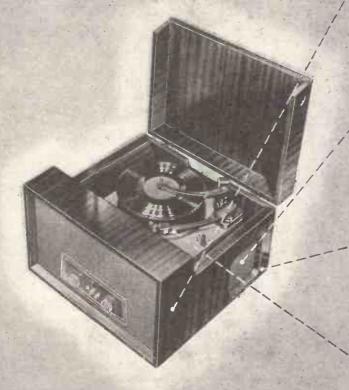
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# SUPER BLACK BOX



An outstanding new high fidelity record reproducer

#### AMPLIFIER

Valves: EL34, 2 EF86, EZ81. SINGLE-ENDED ULTRA-LINEAR output stage having 22db negative feedback overall, which gives 8 watts with 0.5% distortion.

Frequency response:
7cps-75Kcps±1db,followedby
continued fall outside this range.
Steep cut filter:

Out, 9Kc, 6Kc, 4Kc. For operation from 110-120 volt or 200-250 volt. 50 cycles AC. Facility for radio tuner via rear input socket (sensitivity 300 mv. across 100,000 ohms to give 8 watts output).

#### SPEAKER SYSTEM

Complete cabinet forms bass reflex chamber of 2½ cubic feet. Two 6½ in. P.M. speakers operating in parallel, plus Pye Electrostatic speaker with curved surface 16" wide across the front of the cabinet, which operates from 5Kc to above audibility.

#### CABINET

Extremely strong rigid cabinet (\$\foats^2\$) available in two attractive colour schemes—the traditional cabinet is finished in rich dark walnut veneers with contrastinggrille clothin pastelblue. Available in Contemporary styling with contrasting cream lid and crimson lining. Pushbutton controls for amplifier. Dimensions: 12\footnote{x}'' (32.4 cms.) Width 19\footnote{x}'' (50.2 cms.) Depth 19\footnote{x}'' (48.3 cms.)

#### RECORD PLAYER

Collaro transcription cartridge in 4-speed auto/manual player unit. Tropicalized version also available with ceramic cartridge.

Pye Limited, Auckland, C.I., New Zealand.

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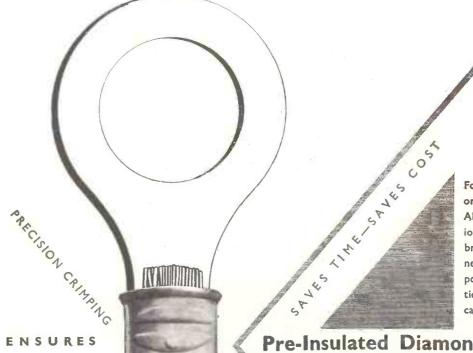
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# modern solderless terminations



For single terminations or complicated cables, AMP Solderless Precision Crimp methods are bringing to Industry a new high standard of positive wire termination. Wherever electrical termination is em-

#### Pre-Insulated Diamond Grip

TLOIDS HUMAN ERROR PER PECT LERNINGTON The AMP solderless method meets wire termination specifications in foreign countries. Use of the AMP AIDS EXPORTS method will enable you to compete in world markets, it is

ployed there are AMP methods, AMP terminals and AMP tools to cut cost, reduce human error and speed the job to keep pace with fastest production schedules. Write or 'phone us NOW for further information.

#### IMPORTANT ADVANTAGES

- 1. Electro-tinned high conductivity copper in one-piece construction. Termination completed in a single operation.
- 2. Plastic insulation permanently bonded to terminal barrel.
- 3. Serrated terminal barrel ensures maximum area of contact and great tensile strength.
- 4. Wire and terminal are compressed into a solid, homogeneous mass, ensuring maximum conductivity and resistance to corrosion.
- 5. Circumferential insulation support permits flexing of the cable without damage to the conductor or fraying of the insulation.
- 6. A wide variety of tongue shapes and stud hole sizes. Terminals and tools have matching colour coding for positive cable size identification.

particularly significant that AMP systems are standard practice in the U.S.A.

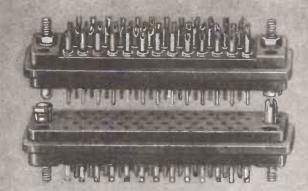


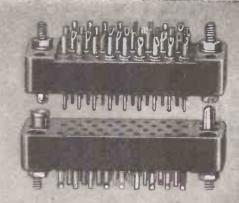
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London Sales Office: DEPT. 15, 60 KINGLY STREET, LONDON, W.1. Telephone: REGENT 2517-8 and 3681-2-3

Works: SCOTTISH INDUSTRIAL ESTATES, PORT GLASGOW, SCOTLAND

AP 323/48





These Units are ACTUAL SIZE —made under U.S licence from Winchester Electronics Inc.

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CONNECTORS

CURRENT CARRYING CAPACITY: 7.5 amps

BREAKDOWN VOLTAGE BETWEEN CONTACTS: (at sea level) 7-contacts: 3.1 kV 14 up to 50-contacts: 4.0 kV

AVERAGE MATING AND UNMATING FORCE (per contact): 8 oz.

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RIGID ALUMINIUM HOODS WITH CABLE-CLAMPS (vibration locks optional) FOR COMPLETE SERIES

SERIES 'MRE' with 7, 14, 18, 26, 34 & 50 contacts

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GOLD-PLATED CONTACTS

made from spring-tempered phosphor-bronze
provide low contact-resistance,
prevent corrosion and facilitate soldering.

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provide high arc-resistance, high dielectric and mechanical strength.

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Model 5in. G Price 25/8 inc. P.T.



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10'x 6in. C Elliptical Price 39/6 inc. P.T.



**ELMAG High Fidelity Units** 

Designed to give good quality at domestic volumes. For a power output stage providing more than 4 watts, 2 or more speakers are recommended.

Flux Density 8,000 gauss (27,500 Maxwells). Frequency Response 40-12,000 c.p.s.

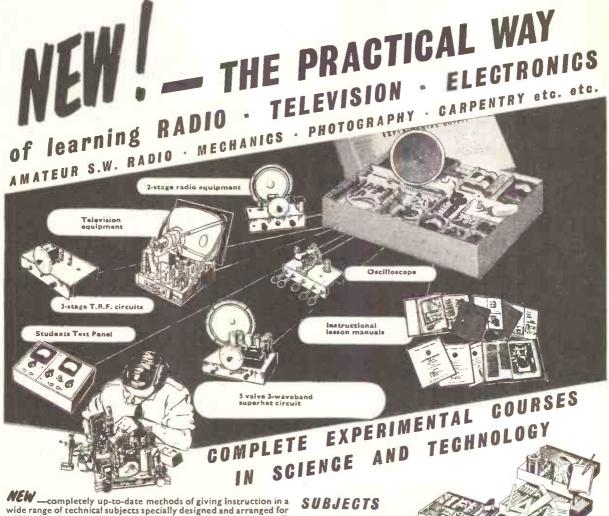
9 x 5in. Model 59T. Price 38/2 inc. P.T.

All prices are for speakers without transformers.

TRADE TERMS 331%

ELECTRO ACOUSTIC INDUSTRIES LTD

STANFORD WORKS RENED DANE TOTTERBAND WIS THE TOTAL



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NEW experimental outfits and lesson manuals are despatched on enrolment and remain the student's property. A tutor is allotted to each student for personal and individual tuition throughout the course.

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COURSES FROM 15/-PER MONTH E.M.J. INSTITUTES, Dept. 127x, London, W.4 NAME (if under 21) ADDRESS I am incerested in the following subject(s) with/without equipment We shall not warry you with personal visits

-Part of "His Master's Voice", Marconiphone, etc. etc.

#### 

# Single pillar lampholder supplied completely prewired with 3 ft. leads ready for immediate installation. Reference No. 80/10/0155

# Thorn pillar lampholders for the illumination of instrument panels...

Originally designed for aircraft control panels (and widely used throughout the British aircraft industry) these Thorn pillar and bridge piece lampholders are of universal application for industrial use wherever instrument panels require illumination. A full range of these components is available.

# . and bridge pieces

The special advantage of Thorn pillar and bridge pieces is their notable economy of panel space and the clear illumination they provide. Wiring arrangements are extremely simple and bridge pieces can be quickly added to existing control panels without any difficulty.



Bridge pieces are supplied with double entry leads for emergency stand-by lighting if required.

#### The present range of bridge lighting units is as follows:—

TYPE A	Mk. G4B Gyro Compass	4 lamps
TYPE B	Artificial Horizon	2 lamps
TYPE C	Large S.A.E. Case (4BA screws)	2 lamps
TYPE D	Small S.A.E. Case (4BA screws)	2 lamps
TYPE E	Horizontally mounted Double Desynn	2 lamps
TYPE F	Large S.A.E. Case (2BA screws)	2 lamps
TYPE G	Small S.A.E. Case (2 BA screws)	2 lamps
TYPE H	Large Air Ministry Case	2 lamps
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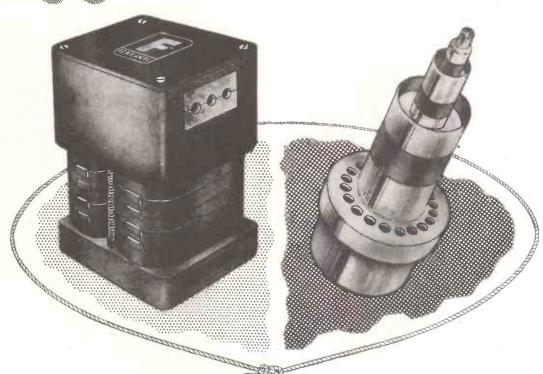
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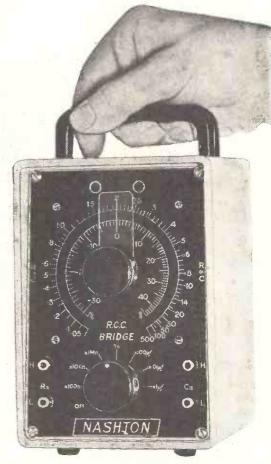
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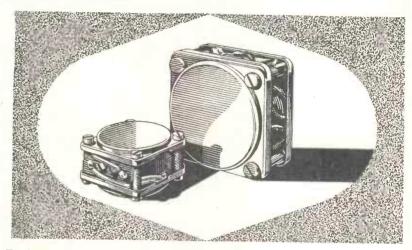
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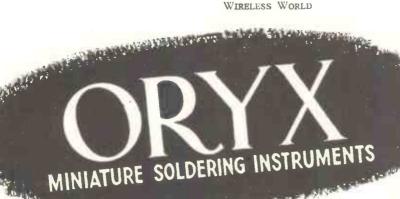
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Model 6



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Designed for high-speed soldering Prevents on production lines. fatigue by operators and damage to surrounding components. volts only.



Mod.	Consumption	Bit Dia.	Weight	Length	Price	Sp. Bits
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12	12 watts	3 in.	1 OZ.	6in.	25/-	2/-
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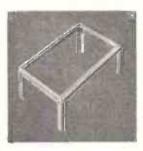
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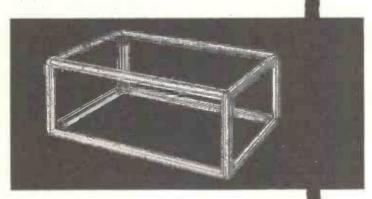




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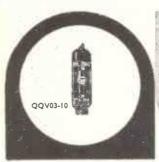
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# a transmitting all communications

WIRELESS WORLD









alye Output Power in Watts	Type Number	20	30	40 50	50 80	00	200	300		10 00 800 700 900	2	2000	40 3000
10,000-0	TY7-6000A		-4-										
10,000.0	TY7-6000W					Į.							
6,900.0	TY6-5000A		-	-			- +						
6.900-0	TY6-5000W		-	++	+++		- +						
4,100.0	QY5-3000A -	-	-	-	+++		- +	1					
4,100.0	QY5-3000W -	-	-	+	++++		-+	1					
1,690.0	TY4-500	-		1	1	-			1 1			-	
1,440-0	TY4-350				-+11		1						
1,000.0	QY4-250			-	+++	(a)						da -	
900 - 0	QY4-500A			++			-+						
845.0	TY3-250			++									
390-0	TY2-125	-	-			-	-					100	
375.0	QY3-125	_		11		-	_	1					
280-0	QY3-65			-	+		-+						
195.0	QV1-150A	-		+ +		_			+-			4	
90.0	QQV06-40A								+-				
87.0	QQV07-40			11	1 1 1 1								
52.0	QV06-20						·						
48.0	QQV03-20A		-	1									
- 27.0	TD1-100A			100	1111		-		-	++++			
2,6 • 0	QQV04-15				1111		-+-						- 1
23.0	TD04-20			++		-			1			-	
16.0	QQV03-10			1									
10-0	QV03-12	-	-		+		•						
7.9	QV04-7												
6.0	QQV02-6			1	1111	-							
2.8	TD03-10	_		+					+++				. —
2.0	TD03-10F	-		-	++++			-	+++			+	-
0.02	TD05-12			11									
		20	30	50	70 90		200	300		700 90		2000	3000

# valve range for equipment

This extensive range of work-proven transmitting valves fills the wide and diverse needs of communications equipment manufacturers. The performance of this valve group extends to frequencies as high as 3,000 Mc/s for 0.5W and to powers up to 6.9kW at lower frequencies.

The Mullard technical advisory service is always at the disposal of manufacturers to answer questions relating to the applications and suitabilities of these valves.

#### **Transmitting Valve Data**

The chart on the left has been compiled to acquaint designers with the range and scope of Mullard transmitting valves available for communication purposes, and to facilitate the selection of suitable types for given applications. The power quoted is the maximum valve output available with Class C telegraphy operation up to the frequency indicated by the junction of the solid and broken lines. The extent to which a valve may be used at higher frequencies with reduced ratings is given by the broken line.

More detailed information may be obtained from a leaflet on this range of valves and from individual data sheets—all of which are available on request at the address below.

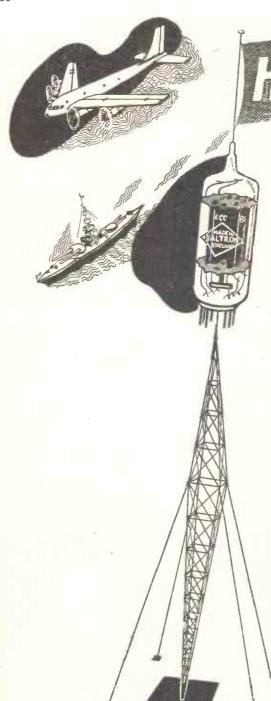






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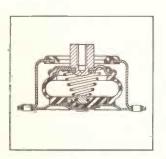


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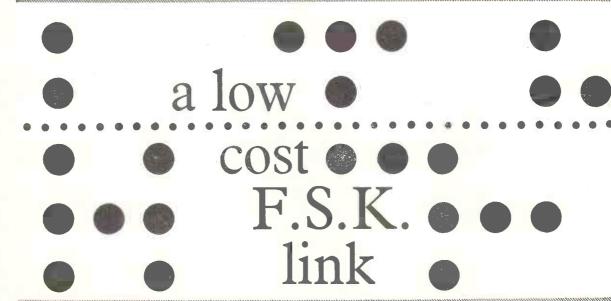


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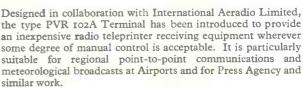
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## Plessey

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nator.

Rapid diversity switch action on small signal differential over wide range of inputs. Complete supression of weaker diversity signal.

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All frequencies from 25 to 174 Mc/s.

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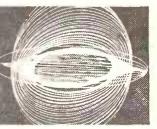
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Model 853 **Power Amplifier** 

Champion proudly introduce the latest developments in HI-FI unit equipment



The complete power amplifier for use with either of the 2 other models (853A or 854.) It is supplied in a beautifully finished polished wood cabinet which can be placed on a side table or bookshelf and will blend harmoniously in any room.

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Maximum power output 11 watts. Frequency Response at 1 watt within 1 db. 10 cls - 20,000 cls - at 10 watts within 1 db. 10 cls - 20,000 cls.

Output impedance (Speech Coil): 15 ohm or 3.75 ohm.

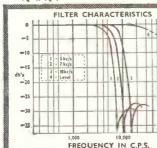
Mains Supply: 200-250 volts.
50-60 cls A.C. or 100-130 volts. 50-60 cls A.C.

FREQUENCY RESPONSE

FREQUENCY

m-10

-20



Model 853A Pre-Amplifier **Control Unit** 



low distortion amplifier with tone controls and low pass filters. The first stage gives balanced compensation for five recording characteristics used by the leading recording companies in England and the U.S.A. This is effected by the use of frequency selective negative feedback. The tone control circuits give continuously variable control of both bass and treble frequencies.

#### TECHNICAL DETAILS

Input selector.

Input selector.
(1) Tape Radio Replay.
(2) R.I.A.A.
(3) A.E.S. and R.C.A. ORTHO.
(4) Col. L.P. and F.F.R.R.
(5) N.A.R.T.B. and H.M.V. L.P.
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(2) FM Tuner.
(3) L.P. Records,
(4) 78 Records,
(5) Tape|Radio Replay,
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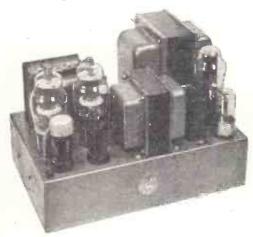
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Input Sensitivity: 1 Volt for full output into 4 or 16 ohm load.

Frequency Response: Flat 40-20,000 c/s (-1.5 db at 32 c/s; -4db at 30 Kc/s).

Hum Level: -80 db at 20 Watts.

Additional Power Supplies: 6.3 V. at 1 A., 300 V. at 5 mA. (stabilised), 6.3 v. at 2 A., 300 V. at 25 mA.

Chassis Size: 12in. × 8in. × 8in. high. Weight: 27 lb.

Power Requirements: 100-125 V. A.C. or 200-250 V. A.C., 50-60 c/s.

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. . . you will realise that Grampian high fidelity equipment gives you the nearest approach to "Concert hall-listening" in your own home. You will, for instance, appreciate the extraordinary delicacy of reproduction achieved by their new 12in. loudspeaker. A great deal of research and new manufacturing methods were necessary to produce a speaker unit with such an extended audio frequency coverage at such a reasonable cost.

# GRAMPIAN 12" SPEAKER UNIT

Type 1255/15

 Frequency Range
 20-15,000
 c.p.s.

 Voice Coil Impedance:
 1 jin.

 Voice Coil Impedance:
 15 ohms.

 Fundamental Resonance:
 40 c.p.s.

 Power Handling Capacity:
 10 watts.

 Flux Density:
 14,500 lines per sq. cm.

 Total Flux:
 130,500 lines per sq. cm.





CYCLES PER SECOND INPUT \(\frac{1}{2}\) WATT
RESPONSE CURVE for speaker unit 1255/15



Full details from:

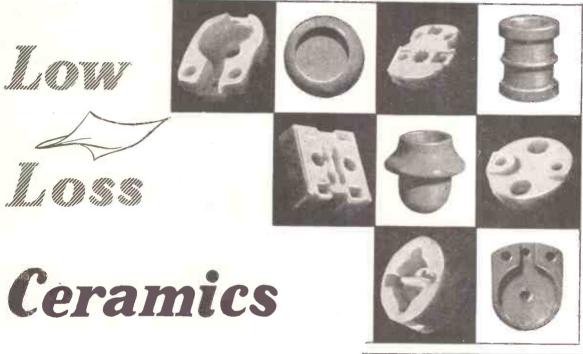
A specially designed reflex cabinet suitable for either corner or side of room is now available as an easy-to-assemble kit of parts, complete with grille material ready to assemble, stain and polish. Although it is primarily intended for use with the Type 1255/15 speaker the cabinet will give excellent results with other units of similar specifications.

Deferred terms available if desired for both speaker and cabinet kit!

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Makers of quality high fidelity equipment 17 HANWORTH TRADING ESTATE, FELTHAM, MIDDLESEX Telephone Feltham 2657/8

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#### BRIEF SPECIFICATION

Output: 10 watts (nominal), 20 watts peak. Frequency Response: 10-100,000 cps, with 1 dB 15-30,000 cps. Distortion: Less than 0.1%. Damping Factor: 40. Hum Level: better than 80 dB down. N.F.B.: 3 loop, main overall loop 28 dB from testiary winding of output transformer. Senitivity: 18 mV (Gram input A) for 10 watts. Spare power supplies: 320 V at 60 mA and 6.3 V at 2 amps.

#### CONTROLS

I. INPUT-MIC, RADIO, TAPE, GRAM (in conjunction with 4 position pick-up matching selector). 2. EQUALISER—6 position. 3. FILTER—6 switched positions. 4 and 5.—BASS and TREBLE (both lift and cut 15 dB). 6. VOLUME.

### announcing the NEW Armstrong A10

HIGH FIDELITY AMPLIFIER

now even better than the original Armstrong A10

FOR 5 GOOD REASONS!

- INCREASED SENSITIVITY—enabling low output magnetic pick-ups to be fed directly into the control unit without recourse to step-up transformers
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- A Additional EQUALISING positions
- Latest EL 34 output valves

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ADDRESS

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#### RR Series 102 RECORD REPRODUCER

Home Model A high performance portable tape recorder for use in the

home and incorporating a number of features normally fitted only in professional equipment. Separate Record and Playback Amplifiers

> All signals from the two built-in speakers are from the tape via the playback head and amplifier.

The input signal and playback signal from the tape can be directly compared by a "Break-in" switch.

Record Level Meter

Fast forward, slow-return type. Push-pull supersonic bias oscillator This feeds a Reflectograph Type H.E. Ferrite core erase head.

Playback and Record characteristics Strictly to C.C.I.R. recommended

specifications. The electronic section utilises the "Brick" form of construction.

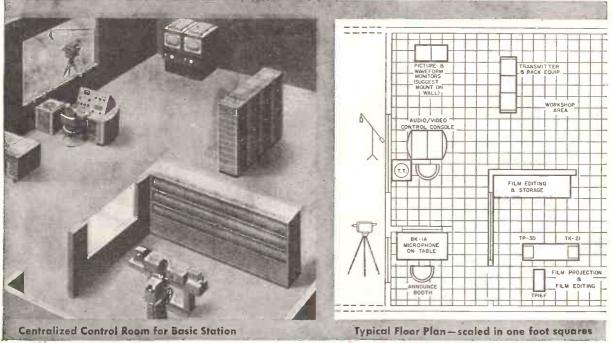
RUDMAN DARLINGTON (ELECTRONICS) LTD

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# RCA BASIC TELEVISION STATION

provides complete facilities for versatile programming with minimum investment



**EQUIPMENT "PACKAGE"** for basic TV station consists of an RCA vidicon film camera chain, picture and waveform monitoring facilities, 16-mm film projector, slide projector, multiplexer, studio synchronizing generator, master audiovideo switching console, stabilizing amplifier, turntable, microphone, transmitter, antenna, audio editing equipment, spare parts, installation tools and materials.

A complete television broadcasting "package", comprised of equipment basic to all television stations, is offered by RCA to those planning television broadcasting on a small but highly efficient scale. The Basic Television Station enables the broadcaster to start programming with a relatively small investment, and reduces operating costs to the minimum.

All units in the "package" meet RCA's world-famous standards of good engineering for high quality performance. Proved and tested in the field, this equipment assures continuous, dependable service with minimum operating and maintenance personnel. The Basic Television Station offers many important advantages:

**ECONOMICAL ONE-MAN OPERATION**... One man can easily operate all program controls which are located in the unique two-section Audio-Video control and switching console. The operator of this centralized

control can also handle any additional live and film cameras that might be added later.

**PROGRAMMING VERSATILITY**... The RCA Basic TV Station provides facilities for: Network or incoming "off-air" satellite programs; local 16-mm programming; local film and slide programs; local live programming.

**EASILY EXPANDED** ... "Matched" design permits quick and easy expansion—without obsoleting the basic equipment. "Matched" live camera and remote pickupfacilities can be added when desired; or an increase in power can be made at a later date with RCA "Add-On" Amplifiers or higher power transmitters.

See your RCA Distributor for additional information on the RCA Basic Television Station. Or write Dept. TV-49-D RCA International Division, Radio Corporation of America, 30 Rockefeller Plaza, New York 20, N. Y., for free booklet giving complete details.

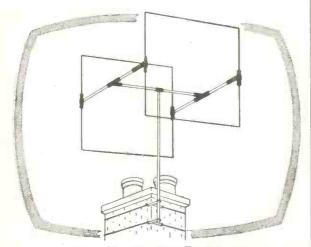


RCA INTERNATIONAL DIVISION

#### RADIO CORPORATION of AMERICA

30 Rockefeller Plaza, New York 20, N. Y., U. S. A. Trademark ® Registered

# for Band I



# the LABGEAR BI-SQUARE outdoor

The most remarkable advance in aerial design. Only half the size of ordinary Band 1 arrays, the BI-SQUARE is light in weight, easy to erect and gives 11-12dB gain. Factory pre-assembled and supplied complete with 12 ft. mast and double chimney lashings.

Model 110 (head only) £6.10.0

Model 110/X3 (Complete) £10.17.6

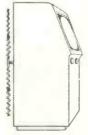
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# First of its kind The Spiral

Another new Labgear development! Designed to meet the demand for a neat, unobtrusive aerial for Bands I and III, the Spiral has a range of approximately 10 miles and is supplied ready to plug into the set.



Send now for Labgear Wall Chart giving complete details of all aerials for B.B.C., I.T.A. and V.H.F./F.M.

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# LOUD SILENCE

#### Connoisseur equipment will reproduce silence -as well as music.

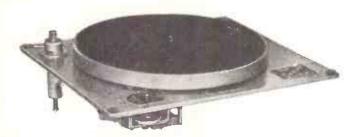
The ability of hi-fi equipment to reproduce silence is perhaps a keener test of its quality, than is its ability to reproduce a full orchestra in spate.

When you are listening to Connoisseur equipment a pause is a pause—an interval of silence. It is silence you can hear.

This is why. Connoisseur equipment is designed by a perfectionist. It is built under his close supervision.

The Connoisseur transcription motor is a fine job, possessing outstanding qualities and unique features. On all three speeds there is a 4% variation which is obtained without braking action. The motor is synchronous and will maintain its synchronisation with up to 25% variation in line voltage. Price £20 plus £8/11/- tax.

The Connoisseur Pick-up is made like a watch—a precision instrument with a downward pressure of only 4 grams. It has a frequency range from 20 to 20,000 cycles at 33½ r.p.m. The armature retracts into the head if accidentally dropped and the coil is perfectly screened by a magnet to minimise hum.



Prices: Pick-up complete with 1 head fitted with Diamond Armature £8/19/- plus Purchase Tax £3/16/6. Head only £6/12/- plus Purchase Tax £2/16/5. Replaceable Armature System £4/10/- plus Purchase Tax £1/18/6.

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PATENTED DESIGN

CENTRE POLE moving coil meters

The movement consists basically of a centre core magnet surrounded by a soft iron ring, where the coil revolves around the magnet.



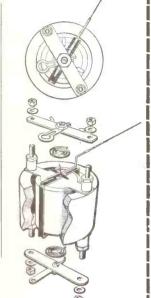
We manufacture a comprehensive range of moving coil meters, with nominal scale lengths from 2" to 5".

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#### IMPORTANT ADVANTAGES

- 1 Torque over power ratio at least twice that of conventional movements.
- 2 Extreme robustness.
- 3 Very high sensitivity (commencing from 5 micro-amps).
- All 4 High degree of accuracy. Taylor meters are made to B.S.89/54 Industrial Limits.
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- 7 Exceptional coil clearance. Trouble-free gap.
- 8 Inherent magnetic shielding.
- 9 Patented anti-parallax mirror scales.
- 10 Overload protection. Meters can withstand 10,000% overload-



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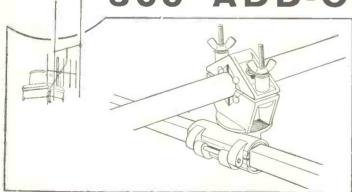
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# '360' ADD-ON AERIALS



#### NOTE THESE PLUS FEATURES

- 360 degrees orientation in all 3 planes irrespective of angle of stand-off arm
- Type "A" is adjustable to fit stand-off arms or masts  $\frac{7}{6}$ in, to  $\frac{1}{2}$ in, or Type "B" which is adjustable to fit stand-off arms or masts 1\frac{3}{8}in. to 2in. (Please specify when ordering).
- Attaches aerial direct to stand-off arm or mast thus eliminating unnecessary sag (no extra arm required).
- Locks positively at any angle, in any situation.

## WITH FULL ORIENTATION

Fitted in seconds for any angle any direction.

The Wolsey "Add-on" aerials, incorporating the new '360' clamp can be mounted in apposition to the stand-off arm and provide unlimited orientation in every direction.

Available in

BAND III aerials, 3, 5 and 8 elements and BAND II aerials, "H" type and Yagi 4.

#### AND NOTE THESE RETAIL PRICES

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360/Y3 . . . . 27/6 360/FMH . . . . 50/-360/FMY4. . . . 65/-360/Y5 . . . 40/-

\*360/Y5WS. . 42/6 (Wide spaced) 360/Y8 . . . . 55/-

When ordering, please specify for which diameter of stand-off arm required:  $A = \frac{7}{8}"$  to  $1\frac{1}{8}"$ ,  $B = 1\frac{3}{8}"$  to 2".

\*A chimney-lashed wide-spaced 5 element Yagi incorporating a '360' clamp is also available (Y5WSL, price £3.10.0 retail).

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Quality of recording . . . economy of recording . . . You can have both, with 'SCOTCH BOY' magnetic tapes. Choose from Britain's only comprehensive range, and get the tape that exactly suits the job you want to do.

And remember to get 'SCOTCH BOY' No. 41 splicing tape for joining your edited tapes: it's specially made for the job! If your machine takes  $5\frac{3}{4}$ in. spools, ask for "Continental size". Your 'SCOTCH BOY' supplier will help you.





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-choose the *right* tape for the job!

#### standard 'SCOTCH BOY' 111

magnetic tape with accetate base Probably the most famous recording tape in the world, 'scorror Boy' 111 has a high reputation for clarity of reproduction, and for freedom from background noise. It has become the criterion for judging fidelity. (Coloured brown for easy identification)

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SCOTCH'S BOY TRADE

magnetic tape

does the job BETTER!

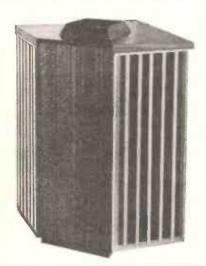


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Amplifiers by Messrs. Acoustical, Leak, Pye and Lowther.

Speakers by Wharfedale, Goodmans, Pye and Lowther. Tuners by Chapman, Jason, etc.

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Suppliers to Govt. Depts., B.B.C., Tech. Colleges, Leading Manufacturers & Research Laboratories



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## AM and FM plus Pre-amplifier

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During 1956 we have moved into a larger, better equipped factory and have been able to enlarge our scope of manufacture.

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Incorporating AM Medium Wave and Long Wave, and the full VHF, FM band PLUS a really comprehensive Control Unit with: 5 Inputs, Tape Output, Amplifier Output at 200 m/v, 3 switched Mains Outlets, Bass and Treble Controls, Roll off filter, Rumble filter, Volume Control PLUS the CHAPMAN Compensator accurately following the famous Fletcher Munson Loudness Contours for realism at low level listening.

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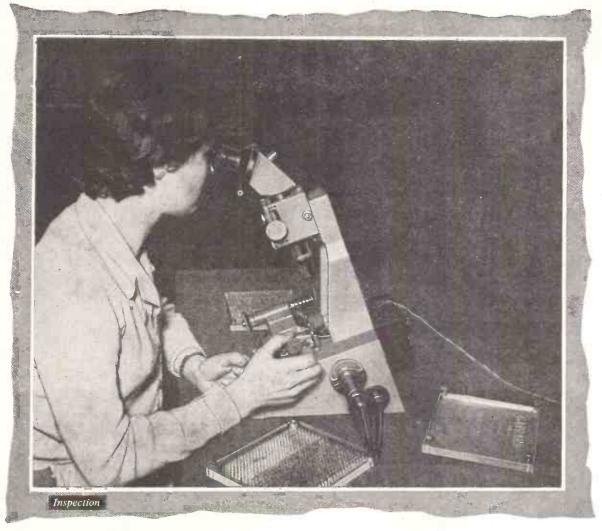
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#### needs

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Amplifiers	£	8.	d.	s. d.	£	8.	d.	s. d.	2	9.	d.	
Quad Mark II	42 28	7	0	102/8 69/4	21 14	3	6	38/1 26/3	42 28	7	0	
W.B.12 Hi-Fi	25 18	18	0	61/1 46/5	12 9	10	0	23/4	25 18	18	0	
E.A.R. Mullard 610 Rogers Senior Rogers Junior	19 42 26	0	0	48/10 102/8 63/7	9 21 13	19 0	0	18/4 38/2 24/2	19 42 26	19 0 0	0	
Rogers Junior Rogers Minor Mark III E.A.R. 750	14	0	0	35/7 24/4	7	0	0	14/2 10/5	14	9	. 0	
R.C.A. Hi-Fi Amplifier and Pre-Amp.	48	0	0	117/4	24		0	44/6	48	0	0	
Grampian 5-10-B	27	0	0	66/-	13	10	0	25/1	'27	0	0	
F.M. Tuners												
Quad Tuner F.M	30	9 10	0	74/6 86/10	15 17	4 15	6	28/3 32/11	21	0	0	
Rogers F.M.	24	17	0	60/9	12	8	6	23/3	17	10	0	
Jason Switched F.M	16 16	12 16	7	41/5	8	6	4	16/5	11	19	3	
Ferguson F.M. Tuner Chapman F.M. 85	25	4	0	61/8	12	12	ő	23/6	18	0	ó	
Chapman F.M. 81	22	i	0	53/11	11	0	6	20/5	15	15	0	

# Personal Credit Plan

Speakers		8-	d.	в. d.	£	ß.	d.	s. d.	£	Б.	đ.
Wharfedale W.16 C8 Wharfedale Super 12 CSAL	17 17	10 10	0	43/4		15 15	0	16/6 16/6		10 10	0
Wharfedale W.12 C8	10	5	0	27/3	5	2	6	11/1	10	5	0
Wharfedale Golden 10	8	0	11	21/3	4	0	6	9/2		15	0
Wharfedale Super 8 CSAL	7	6	11	19/8	3	13	6	8/7	5	5	0
Wharfedale SFB/3 Complete											
Speaker Unit		10	0	96/6		15	0	36/8	39		0
G.E.C. Metal Cone	9	5	0	23/11	4	12	6	10/2		13	7
Goodmans 150 Mark II	10		9	28/5		. 8	0	11/6	10		9
Audiom 60 (12in.)	9	2	9	23/8		11	0	10/1	9 15	2 9	9
Axiom 22	15	9	0	38/9	√4	14	6	15/4	TĐ	Я	U
Tonnesisting Units											
Transcription Units		_					1				
Garrard 301	26	8	2	64/7	13	4	1	24/6	19	0	0
Connoisseur (T)	28 19	11	4	69/9 47/10 ·		15	8	26/6 18/11	14	0	6
Collaro 4T200 with PU Collaro 4T200 without PU	14			37/7	7	10	0	14/11		15	0
Lenco GL 55	17	10	4	43/5		15	2	17/1		12	0
Lence GL 56	23	7	0	56/6	11		6	22/-	16		0
Lenco GL 50/4		17	10	53/7		18	11	20/9	15		0
Woollett	21	0	0	51/4	10	10	0	20/-	15	10	0
Pickups											
Goldring L.56/500	6	19	0	18/10	3	9	6	8/4	5	0	0
Goldring L.56/500/SD	111	16	4	30/8				12/5		10	0
Complete Collaro O. or P. Head	5			14/5		10	3	6/8		12	6
Complete Garrard TP1210	5	4	- 3	14/9	2	12	2	6/10	3	15	0
Leak standard with diamond LP			_			_	_			_	
and Std. Head		4		49/5	10	8	5	19/5 8/1	14	14	8
B.J. with Shell and C.12 Head	6	12	0	18/1 69/9	14	5	6	26/6		0	0
Connoisseur	28	¥Τ	0	99/9	1.0	Đ	U	20/0	20	0	v

If any of your requirements are not mentioned, please ask for details. We can supply your need whatever it is on easy "M.O.S. Personal Credit Plan" terms. Please add extra to your initial deposit to allow for carriage and packing.

Did you go to the Audio Fair? Remember, you can buy anything you saw there on the M.O.S. Personal Credit Plan.

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The Radio Centre

MAIL ORDER SUPPLY CO.

PRECISION High Fidelity

#### SPEED TRANSCRIPTION

WITH VARIABLE SPEED ADJUSTMENT. MAIN FEATURES

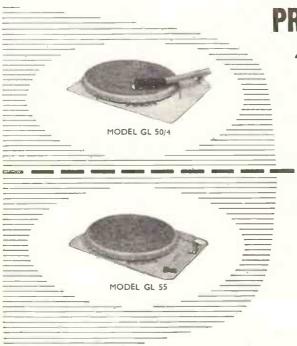
- Speed continuously variable from 29 r.p.m. to 86 r.p.m. Pre-set adjustable "click-in" positions for 78, 45, 33\u00e4 and 16 r.p.m. Playing old celebrity discs requiring speeds above 78 r.p.m. Tuning record pitch to a musical instrument. Correcting for mains frequency variations.
- Accurately balanced heavy precision made turntable eliminates Wow and Flutter.
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- Less than 1% change in speed for up to 13% change in Line Voltage.
- Large resilient 4-pole constant velocity motor.
- Revolutionary Revolutionary new devaccurate groove selection. device
- Model GL 56 is fitted with weight adjustable precision Pick-up-Arm with plug-in shell, incorporating the Superb Goldring Variable Reluctance Cartridge No. 500.

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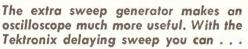


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START THE OSCILLOSCOPE SWEEP WITH THE FIRST TRIGGER RECEIVED AFTER A CONTROLLABLE TIME-DELAY PERIOD.

This is an important reason for the extra sweep generator and its associated pickoff circuit in Tektronix Type 545 and Type 545.

associated pickoff circuit in Tektronix Type 535 and Type 545 Oscilloscopes. Triggering the delayed sweep by the observed signal guarantees a jitter-free display... ideal for examination of time-modulated pulses and signals with inherent jitter.

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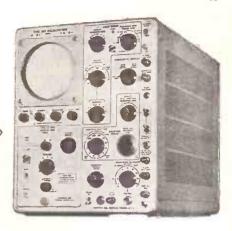
MAKE MORE ACCURATE TIME-INTERVAL MEASUREMENTS.
A calibrated ten-turn time-delay control divides each of the twelve delay ranges into a thousand units. Range accuracy is within 1%, incremental accuracy on any range is within 0.2% of full scale.

TRANSFER PART OF A DISPLAY TO A FASTER SWEEP. By initially displaying a signal on the extra, delaying sweep, and then transferring it to the main oscilloscope sweep. a continuously adjustable horizontal expansion can be obtained. Degree of magnification is determined by the time/cm ratio between the two sweeps. The average jitter of 1 part in 25,000 permits practical use

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ARM THE OSCILLOSCOPE SWEEP FOR TRIG-GERED ONE-SHOT OPERATION. A front-panel pushbutton or an electrical signal from a remote location can be used instead of the internal delayed trigger to arm the sweep. After the button is

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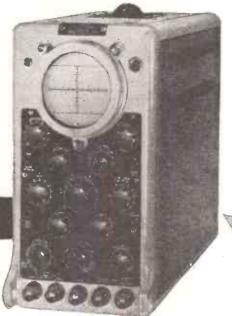
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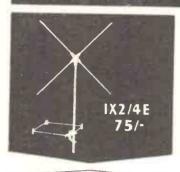
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BAND



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Type H.F. 1012 10" unit, die cast, 12,000 gauss magnet, cambric cone. 10
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c.p.s. Bass resonance
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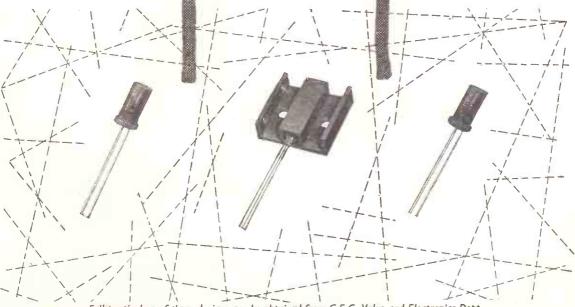
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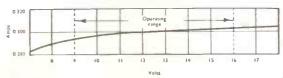
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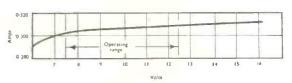
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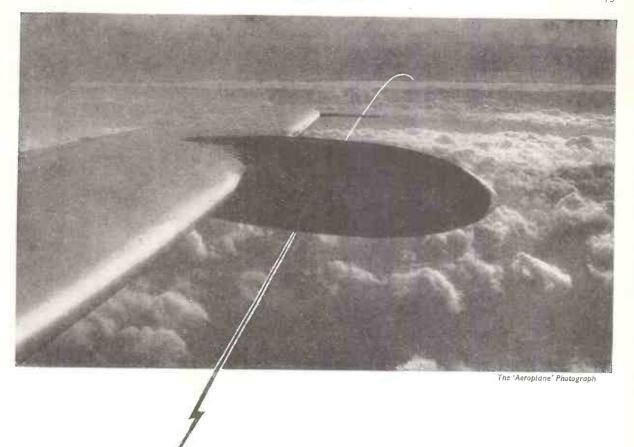
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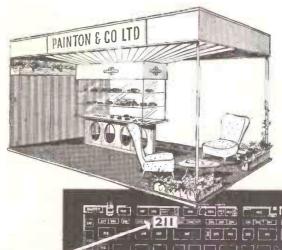
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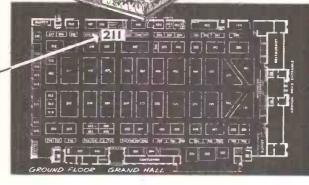


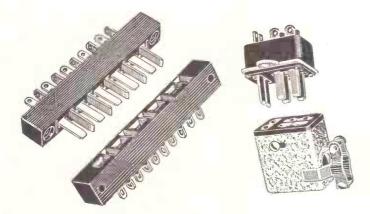
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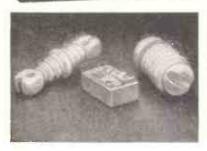
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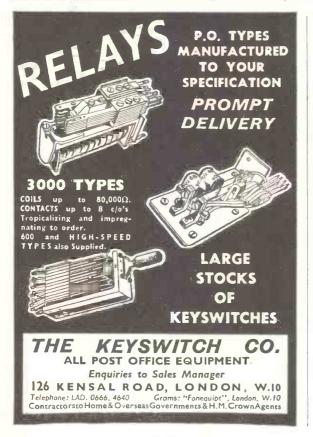


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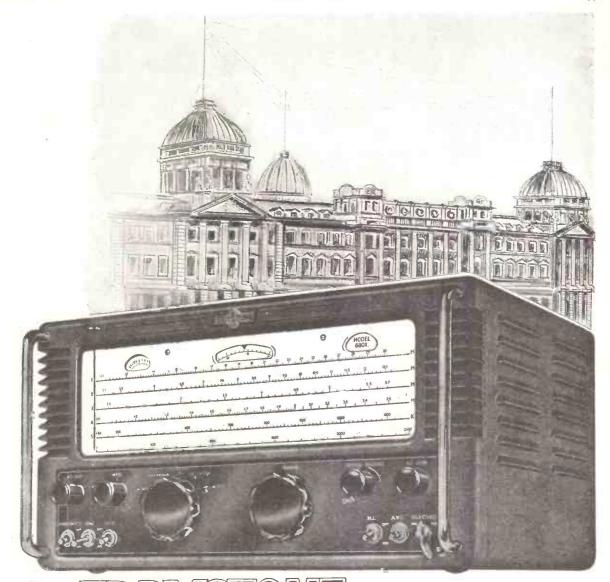




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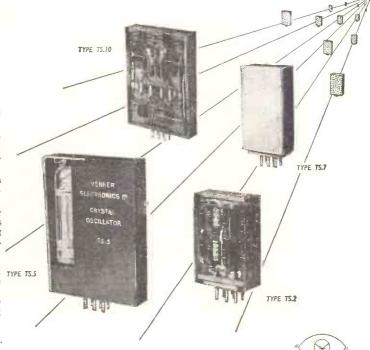
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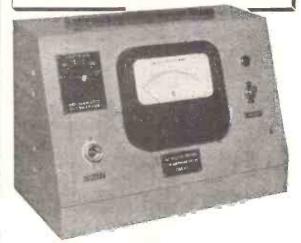
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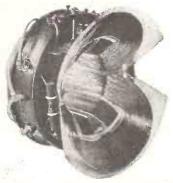


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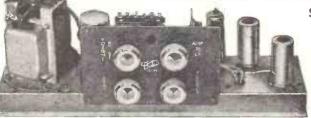


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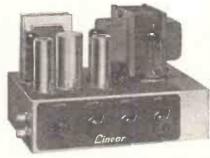
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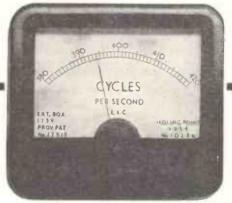
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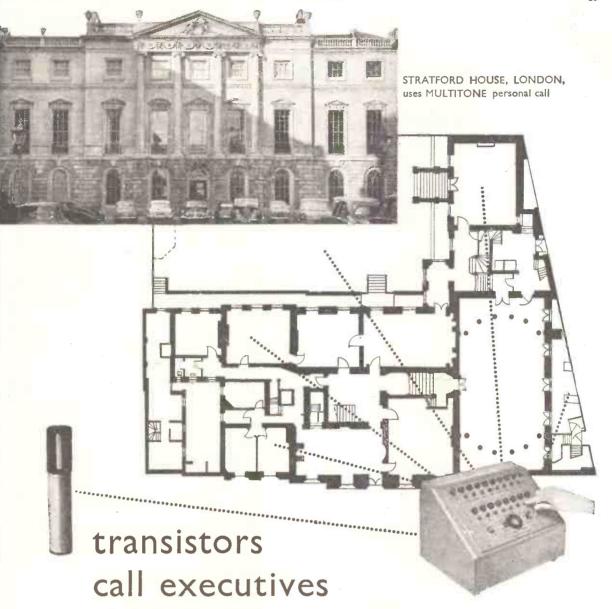


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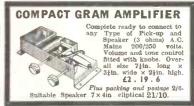
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MAY 1957

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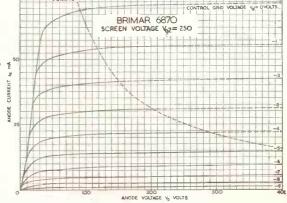
The Brimar 6870 is a Trustworthy screened pentode with a high mutual conductance and low control grid to anode capacitance, and is intended for use as a small R.F. power amplifier up to 150 Mc/s, or as a video amplifier. In the latter application advantage may be taken of the fact that the valve has higher anode dissipation and cathode current ratings than an ordinary high slope R.F. pentode, so that lower values of anode load resistance may be used for a given voltage output. This means that the valve can work into higher load capacitances without loss of bandwidth, or alternatively may be used over a wider band with a given load capacitance. The valve is fully Trustworthy and is eminently suitable for mobile equipment.

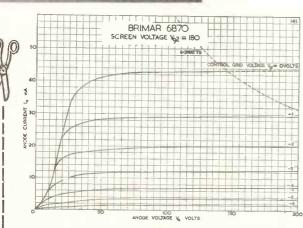
#### TYPICAL CHARACTERISTICS

Anode voltage Screen voltage Autobias resiste Anode current Screen current	, or 			 (	180 180 56 25 3.5	250 volts 250 volts 120 ohms 25 mA 3.5 mA
	And	ual con de impe	edance		9.0 170	8.5 mA/V 230kilohms
141	( p	er ampli		 * * *	35	35
		trol Gr == 100 μ.			-9	— 13.5 volts

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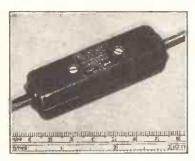
We always get 'needled' when we think of the harm done to good music and to good records by *some* cartridges, when we can do the job so well. You see, we are Type 65-1, the medium-output member of the Acos family. Our proper place is a good record player or radiogram. Our characteristics are linear, our frequency range is wide, and our g is high.

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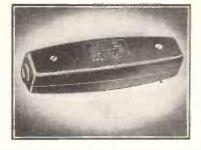


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Effective on bands I and III.

Owing to the high frequencies involved, any band III filter should be fitted inside the appliance, as an external filter would tend to radiate interference.

These internal inductors must be fitted in pairs inside the casing, in series with the brush leads.



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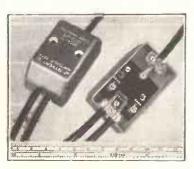


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#### "BELLING-LEE" NOTES

#### BAND III IN SCOTLAND

We have just returned from a trip to Dundee where a film strip lecture was delivered to about 135 members of the trade. We learnt that in parts of Dundee, and certainly along the north bank of the Tay estuary, reception of the test card from the I.T.A. test trans-mitter was considered to be very We were particularly pleased about this as there had been some criticism, and we were quite disturbed. We sold the transmitter to the I.T.A. prior to its use at Emley Moor and, although we erected the small I.T.A. aerial at Blackhill, we are no longer responsible either for manning or maintenance, and all queries relating to the test transmissions should be addressed to I.T.A. and not to us.

Dundee is a fringe area for Blackhill, and if the test card is being received there, there isn't much wrong with the transmitter, in fact we sent a telegram to I.T.A. congratulating them upon the results.

We also saw results in Glasgow, but even using a high gain aerial the picture was very noisy although well and truly locked.

There seems to be a feeling that the test card should be equal in quality to entertainment value. It should always be remembered that the purpose of the transmitter is to enable dealers and others to carry out conversions and to line up band III aerials, and viewed in this way the transmitter is doing its job. The only thing to bear in mind is that where a picture is excessively noisy the noise might be concealing a ghost, in such cases extra care should be taken. In the picture we saw in Glasgow a ghost was obvious even through the noise.

In the "Belling-Lee" lectures given in Edinburgh and Glasgow, Mr. A. P. Hale, A.M.I.E.E., repeatedly gave it as his opinion that there would be considerable difficulty in obtaining a good band III picture in certain parts of these towns. It is unlikely that indoor aerials will give a satisfactory picture except perhaps in the eastern suburbs of Glasgow and other very favourable sites.

Advertisement of BELLING & LEE LTD.
Great Cambridge Rd., Enfield, Middx.
Written 25th March, 1957

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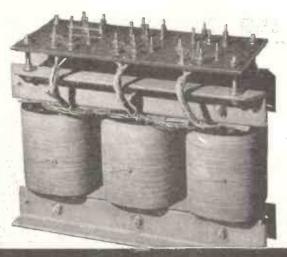
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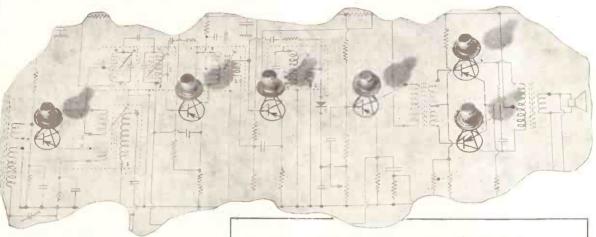
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APPLICATION CHARACTERISTICS Average frequency cut-off 5 Mc/s. Amplifier Frequency Average frequency cut-off 8 Mc/s. Changer/ Oscillator Intermediate Average current gain 30. L.F. Stage Intermediate L.F. Stage Average current gain 66. **♦** Output Stage Maximum collector dissipation (absolute) 115mW at 35°C ambient. Maximum junction temperature (absolute) 70°C. \* The XCIOI is also available Thermal resistance in free air 0.3°C/mW. in matched pairs for push-pull Thermal resistance with appropriate heat sink 0.21°C/mW.

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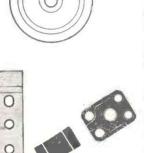
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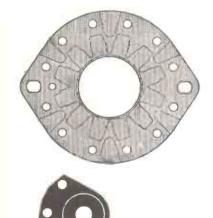
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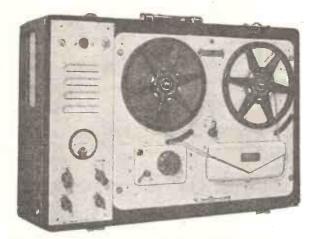
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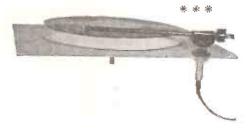
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The full test report appeared in the February, 1957 issue of "Wireless World," pages 22 and 23.







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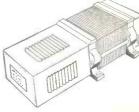




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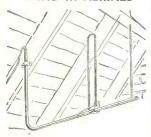
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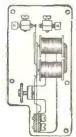
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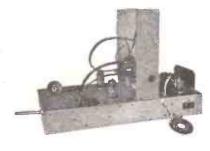
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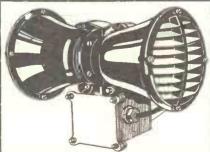
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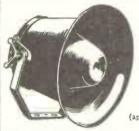
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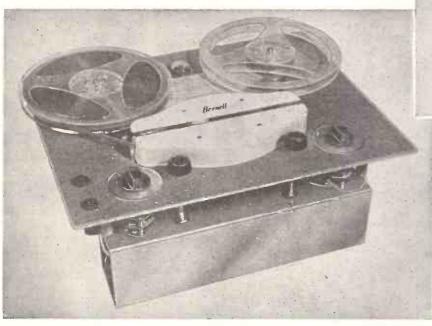
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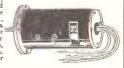
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MAINS BLOWERS, 2007250 v. A.C./D.C., ‡-amp., 5,000 r.p.m., consists of the motor with stached encibed fan, end funnel littake t‡lin, da., side outlet lib. x ²im., plinth blues 5tin. x ½im., dishe blue crackle and die cast aluninium, size overall 9lin, long, ¼im. wide, 5in. high, weight 7 ½b., a very superior blower, offered at a fraction of oeignal code, new unused, 25/c.

SLYDLOK FUSES, 250 v. 15 amp. type, end and back connection, new unused, fraction of original cost, 1/\*, post 4d.; 10/\*, doz., post 1/9.

BATTERIES, radio layer type, by famous maker, fully guaranteed by us, 120-v. size 3in. × 2in. × 1in. new unused 2/6, post 1/\*. Cartons of 6 batteries, 12/\*, post 2/6. Ditto, 22 v. size 3iin. × 2iin. × 2iin. × 2iin. (A/\*, post 1/\*). Cartons of 3 batteries, 12/\*, post 1/9.

4/\*, post 1/9.

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TELEPHONE SETS, consists of 2 combined microphones and receivers, which when wired up with ordinary twin flex, provide perfect 2-way communication, excellent results up to 1 mile have been reported, self-energised, no battery required, price the 2 instruments new unused, 7/8, post 1/3, twin P.V.C. 14/36 flex up to 300ft, lengths at 1d. per ft.

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## THIS MONTH'S 'SUPERIOR' BARGAIN!

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RADIO/GRAM CHASSIS ASSEMBLY

PRICE

- £4 5 0 CONTAINING: \* Punched chassis, Back-plate, etc. Size 12"x7"x8". \* Multi-colour Glass Dial L.M.S.G.
- L.M.S.G.

  Drive Drum and Spindle.

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Output Transformer, Twin Gang (500 pF) Con-Twin Gang (500 pF) Condenser.

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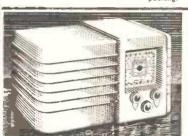
Theoretical circuit and rough component layout free with each



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Metal chassis punched for 4-valve (B.9.A) superhet and fixing brackets.

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Ideal for midget construction. Available in Walnut or Green. Size 12in. long, 7in. high, 5½in. deep. Complete with handle, back, dial and two knobs.

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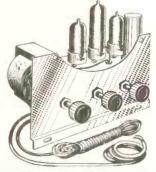
An elegant cabinet in richly figured walnut veneer, internal panels in polished sycamore. A drop front lid covers a sloping, uncut control panel (18in. long × 10tin. high) slongside which is an uncut baseboard (18tin. long × 13tin. back to front). The inside of the drop front lid is panelled in beige leather-tete. In the lower part of the cabinet are two large storage cupboards (13tin. are two large storage cupboards (13tin. high, 7tin. wide, 16tin. deep). The lid and cupboard handles are in chased Florentine bronze. Overail dimen-Florentine bronze Overall dimensions (33in. high, 34in. long, 164in. deep).

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THREE VALVE (EBC41, EL41, EZ41). Ideal for use in a low priced record player. Output approx. 2 watts. Two controls—volume and tone. Mains transformer and fully iteolated chaesis, less output transformer which is available separately. Overall size approx. 6 ½n. ×2; m. PEICE 23/19/8 plus 2/8 postage and peacing. 2-3ohm O/F transformer 6/- extra.



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Revine covered cabinet suitable for housing speaker and amplifier in end Adjustable compartment. motor board 14jin. ×12jin. Internal clearance from tid to base of cabinet Two colour covering in blue and grey or wine and grey rexine. Handle fittings, locks and hinges are in gilt with a solid white plastic handle. Overall size 18in. long, 9\frac{1}{2}in. high. 13\frac{1}{2}in. back to front.



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The SPEAKER ENCLOSURE on the left is based on a simplified Horn principle, whereby the sound waves from the back of the speaker are driven over a barrier and out a secondary effluent on the far side. In consequence the bass response is quite remarkable for an enclosure of this size. Price £5/17/6. ● The LEGS cost 32/6 a set and can be fitted to any of the units, thereby converting it into a cabinet. The GRAM UNIT (upper right) is suitable for every turntable (including auto-change and Transcription) and there is room beneath for most amplifiers, and possibly even an f.M. tuner. • The RECORD STORAGE UNIT (lower right) will hold 150 records (including 12in, L.P.s in their sleeves) and costs £4/17/6. • The PLINTH is 9/6 extra.

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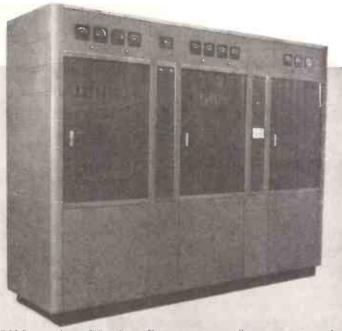
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ET-18 Front and rear sliding doors offer easy access to all components, any of which can be quickly replaced without disturbing any other components.

...Substantially reduces installation and operation costs

...Designed to permit personnel with limited technical experience to perform routine operations

... "Split-Cycle" cutoff protection and automatic re-application

... Entirely air-cooled

RCA-ET-18...designed for high efficiency operation...delivers 15 KW output within the frequency range of 3.2 to 24 mc. Modern high-gain screen-grid type tubes enable a substantial reduction in the number of stages of power amplification, afford high stability of operation without the need for neutralizing adjustments.

Compact in size for a transmitter of such high power, with a very minimum of adjustable control and tuning circuits, RCA ET-18 frequency-shift keyed radio-telegraph transmitter is economical to install and operate. The final rf power amplifier utilizes two long life RCA-6166 tubes. These tubes are air-cooled—keeping accessory and equipment housing requirements at a minimum in space and cost.

The "split cycle" protection circuits of the RCA ET-18 assure superior communications service. In the event of a fault the transmitter recycles itself in a split second. Indicator lights show where the fault occurred and remain on until manually reset. Vertical chassis construction eliminates heat pockets and subsequent damage common in older types of horizontal chassis transmitters.

Ask your RCA distributor for complete details and technical particulars about this equipment and other RCA communications and broadcast transmitters. Free booklet on RCA ET-18 FSK RADIO TELEGRAPH TRANSMITTER will be mailed on request. Write to Dept. HF-49-D, RCA International Division, Radio Corporation of America, 30 Rockefeller Plaza, New York 20, N.Y., U.S.A.



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## ADAPTATA

is the name of the new SONOMAG Pre-Amplifier recommended on page 238 of the November "Hi-Fi News" to those already owning Hi-Fi equipment and wishing to add tape reproduction of the same quality.

This is the ONLY pre-amp, at present available designed specially for the new Collaro Transcriptor, and rigidly fixed as a unit to it.

Demonstrations to all Hi-Fi enthusiasts of our pre-amp, used in conjunction with the Collaro Transcriptor Tape Unit, Collaro Transcription Motor, Leak Dynamic Pick-up and Diamond stylus, Leak Trough-line F.M. Tuner, Wharfedale Baffle 3-speaker system and Leak main amplifiers, will convince you of the fine standard of recording possible. Day, or evening (by appointment).

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In good working condition. PRICE

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Radar Test Unit for measuring relative output power and fre-quency of 3 cm. Radar systems. Consists of thermister type Power Meter, a co-axial line Frequency Meter, an R.F. Oscillator attenuator, and Choke coupling.

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#### M.I.T. Radiation Laboratories

#### Spectrum Analyser Type TSX-4SE

(3 centimetre)

The TSX-4SE Spectrum Analyser is an ultra-high frequency receiver



with an oscilloscope indicator, in which the local oscillator is frequency-modulated by a sawtooth voltage proportional to the sawtooth sweep on the oscilloscope tube. It is used for observing the spectra of the pulsed oscillators, tuning receiver local oscillators, adjusting defective r.f. components, measuring large standingwave ratios, and measuring the Q of resonant cavities.

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SPECIFICATION: Tuning range—8,630 Mc/s-9,550 Mc/s (723/AB klystron). Frequency calibration by means of a pip provided by a reaction type cavity wavemeter. I.F. frequency 20 Mc/s. Receiver band width 50 kc/s. Receiver gain 130 db, 4 I.F. stages, 3 video stages. Sweep frequency vairable from 10 to 20 cps. Attenuation graduated from 0-100 with calibration factor of 1.0 db/div. above 10.

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BC221 Range 125 kc/s — 20 Mc/s

Also in stock: U.S.A. BENDIX LM SERIES

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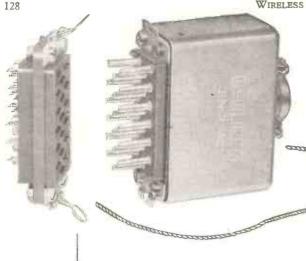
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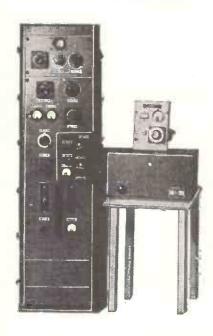
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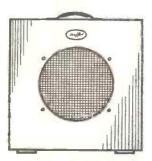
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Of very small dimensions: approx. 6½in. ×3½in., maximum height 5in. Utilises EL84 output and 6X4 rectifier, double-wound transformer, tone control, output transformer, and 7in. ×4in. elliptical speaker.

The T.C.C. Printed Circuit greatly simplifies construction and eliminates wiring errors.

LASKY'S PRICE for the complete Kit including valves, printed circuit, speaker, with full instructions, Post 2/6.

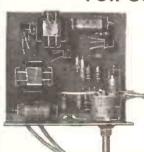
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stvli. Type 4/456, £9.7.0 £6.19.6 4-spd. Post 3/6.

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Size: 32in. ×31in. Height can be under lin. Uses our new hermetically sealed Transistors and operates from 6-volt battery

SEND FOR FULL DETAILS, CIRCUIT DIAGRAM AND SHOPPING LIST, 1/-.
Post free.

LASKY'S PRICE FOR THE COMPLETE including 4 Transistors, all brand new components, T.C.C. Miniature condensers, printed circuit and KIT latest full instructions.

Post 2/-. You can have a demonstration at either of our addresses and you will be amazed at the results!

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T.C.C. MINIATURE ELECTROLYTICS (low voltage for transistor working), all types in stock.

You have been waiting for a R.F. Transistor at a reasonable price. Here it is!

Lasky's now offer you a genuine R.F. Transistor, P.N.P. Junction Type, suitable for medium and low frequency oscillators, frequency changers, and I.F. amplifiers (up to 2 Mc/s), at only

Double spot-yellow and red

Also AUDIO P.N.P. Junction Type suitable for high gain and low frequency amplifiers, and for output stages up to 250 milliwatts, only each

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Special prices for quantities of 6 and over.

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\* HERMETICALLY SEALED AND UNAFFEC-TED BY TEMPERATURE VARIATIONS.





LARGE SELECTION OF 3- and 4-SPEED AUTO - CHANGERS. B.S.R., Garrard, Collaro, etc. Our stocks are constantly changing. See us for what you want.

CARRAND RC.80. 3-speed Auto-Changer. Full length arm with two XMS heads or GC2 t.o. crystal head. Brand new, in makers' cartons. List £20/15/-. GARRARD RC.80. 3-speed Auto-

LASKY'S PRICE £13.19.6 Carr.

B.S.R. 4 Spd. with t.o. crystal pick-up. Incorporates auto and manual control. Brand new, in makers' cartons. LASKY'S PRICE 48 15 0 £8.15.0 Carr. 5/-

relaxation multi-vibrator, oscillator, audio amplifier, oscillators, signal tracers, etc., etc., supplied with each

Full operating data and circuit diagrams for a simple

receiver, superhet, T.R.F.,

Transistor.

MORE MONEY-SAVING LASKY BARGAINS ON NEXT

# LASKY'S. RADIO



#### RONETTE "MINIWEIGHT" **CRYSTAL PICK-UPS**

CREAM PLASTIC ARM AND REST

Post 1/6. 17/6

CARTRIDGES complete with sapphire stylus, for use with ordinary radio sets and small amplifiers:—

N50/3, Standard, or L50/3, long playing, response up to 7,000 c.p.s. Each 19/6.

SPECIAL PRICE for Arm with 2 of Cartridges, 45/-

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PRINTED CIRCUIT VERSION OF G.E.C. 912 F.M. TUNER FOR HOME CONSTRUCTION.

Note these star features:-

- \* HIGH SENSITIVITY.
- \* T.C.C. PRINTED CIRCUIT. \* NEW T.C.C. CONDENSERS.
- \* AERIAL COIL AND R.F. COUP LING COIL PRINTED OF CIRCUIT.
- VALVES AND 2 GERMANIUM DIODES.

By the use of a printed circuit the I.F. and R.F. amplifiers are extremely stable at maximum gain and results are consis-

at maximum gain and results are c tent on all tuners. Valve line-up:—
R.F. Amplifier, Z719 or EF80.
Mixer and Osc., B719 or ECC85.
Ist I.F. amp., W719 or EF85.
2nd I.F. amp., W719 or EF85.
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CAN BE BUILT FOR (Including Valves)

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"BARONETTE" MIDGET RADIO CASES. Plastic, in cream, pastel pink or pastel green. Overall size: 8½in. wide, 4½in. deep, 5in. high.

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THE NEW BRENELL MARK IV TAPE EQUIPMENT

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Covering Channels 8-4 or 1-9, with provision for 10 more coil sets. 2 valves:-Mazda 30L1 cascode r.f. amp., Mazda 30C1 triode/pentode f.c. Complete with power supplies for 200-250 v. A.C. I.F. output 16-19 Mc/s., easily modified to other outputs. Full circuit diagram supplied. CE Post 2/-. £5 17 LASKY'S PRICE

Also available without power pack at 99/6.

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Truvox. 23 gns
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LARGE RANGE OF TAPE DECKS

#### TAPE RECORDERS

Large range, Elizabethan Truvox, Sound, Vortexion Brenell, etc.

TAPE DECK MOTORS Anti-clockwise, shaded pole. Col laro 25/-. Garrard 26/6. B.T.H 29/6. Post extra.

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"Ferrovoice," on plastic spool, 1,200ft. List, 32/6 LASKY'S PRICE 25 Post 1/-. Spare 7in. spools, 3/6.

SPECIAL OFFER! Mag netic Recording Tape, kraf On Cyldon meta base.

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PURETONE Tape or plastic spool, 1,200ft. 12/11 Post 1/- extra. All makes of Tape including thin long-playing.

7/9

#### TARE SPACE

	I WE F	-		91	г	P	91	ν	-0	
	plastic									3/
	metal									2/
	metal									1/
	plastic									3/
9in.	Ferrog	ra	1	١l	h					9/
	P									

### LASKY'S BATTERY PORTABLE FOR HOME CONSTRUCTION ON PRINTED CIRCUIT

You can build it com-

plete with valves and case for only

Post 3/6 extra.



SIMPLICITY OF CONSTRUCTION. The use of all the latest innovations gives maximum simplicity of construction combined with fine quality performance. In particular, the PRINTED CIRCUIT greatly simplifies construction and completely eliminates the possibility of wiring errors.

Demonstration models at both our addresses.

SEND FOR CIRCUIT DIAGRAM with assembly data, all instructions, illustrations and full shopping list. Price 1/6

POWER SUPPLY UNIT for the above and suitable for most other battery portables. Stabilised L.T., surge proof. Complete safety for the first time with battery valves on mains operation COMPLETE KIT, containing printed circuit. 45/-, post 2/-. Full details on request. For 200-250 A.C. mains.

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Full range in stock. Quad,
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Demonstrations at Tottenham

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Tottenham including the new Wharfedale 3-speaker system.



10 STAR FEATURES

- ★ PRINTED 7½in. × 2½in. CIRCUIT siz
- ★ 4-valve S/het, med. & long wave Valves
- Low consumption Double Battery Life. ★ Ferrite Rod Internal Aerial.
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- separately.

New TSL F.M. TUNER £17 10 DULCI F.M. TUNER DULCI AM/FM TUNER £20 17

BARGAINS ON MONEY-SAVING LASKY

#### & SERVICEMAN-EVERYTHING FOR HOME CONSTRUCTOR

#### JASON "ARGONAUT"

A super-sensitive Tuner for F.M. A super-sensitive Tuner for F.M. and medium waves. Complete parcel with power supplies, £13/19/6. Post 3/6. Data Book, 2/-. All components available separately. Chassis Assembly, 57/9, post 2/6. I.F. and Coil Set, 78/-, post 1/6.

#### JASON F.M. TUNER

Special parcel containing data book, chassis, front panel, dial, drive tuning condenser, full sets of coils. I.F.'s 68/9 ratio detector, etc. Post 2/6, DATA BOOK with price list 2/-. Note: This tuner uses 4-8AM6 and 2 crystals and can be built for £8/15/-, plus 3/6 post,



#### TRUVOX "SENIOR" SPEAKER DRIVING UNIT (pressure type)

New and unused in maker's rew and unused in maker's cartons. Power handling capacity 15 watts peak. With a 12ft. cinema horn will reproduce down to 17 cps. Listed at £7/15/-. LASKY'S PRICE Carr. 5/-. 59/6

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Few only left. Let us have your enquiry. Prices from £7/19/6.

TEST PRODS. Red and black, fused and retractable. Complete with Pair 2/11

#### MOVING COIL P.M. SPEAKERS

2½in., 3in. and 3½in., 19/6. 5in. | 6½in. |8in. | 10in. | 12in. | 19/6 | 17/6 | 21/- | 29/6 | 29/6 6½ in. with transformer .... 21/-7 × 4in. Elliptical ..... 19/6 10 × 6in. Elliptical ..... 32/6

#### GOODMANS 12in. AUDIOM 50 P.M. SPEAKERS

10 watts. Limited number only. Listed at £6/15/-. Limited number LASKY'S PRICE 97/6 Post free.

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Easy to fit to any radio, TV receiver or amplifier. Full data and circuit diagram or simplifies a supplied.
LSH75. For outputs up to 6 watts, 8/-LSH618. For outputs of 10-12 watts,
12/8.
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LPH65. MOVING COIL TWEETER. Imp. 5.5 ohms, freq. range 2,000-2,200 50 c/s. For outputs up to 6 watts. 2½in. diameter, All post free. 39/6.

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18 S.W.G. undrilled, 4 slides, reinforced corners. Depth 2\(\frac{1}{2}\)in. 6×4 4/-; 12×8 7/-; 16×10 8/3; 8×6 5/-; 14×9 7/6; 12×3 4/9; 10×7 6/-; 16×9 8/-; 12×6 6/6. Post 1/- per chassis extra.

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PARCEL No. 1 PARCEL No. 1
Contains everything to build a 4-valve
3-wave superhet for 200/250 A.C. mains.
Uses 6KS, 6KT, 6QT, 6VV valves. Attractive wood cabinet, walnut veneer, or
plastic cabinet as fliutarated. Size 12×6]
×5jin. deep. CAN BE BUILT FOR

Carr. and packing 2/6. £7.19.6

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PARCEL No. 2
Contains everything to build a T.E.F.
3-valve set for 200/250 A.C. mains, medium
and long wave. Usee 6K76, 647, 6V6 and
metal rectifiers. Near plastic cabinet,
walnut or ivory finish, or wood cabinet.
Walnut or ivory finish, or wood cabinet.
Size 12 ×6 ± ×6 ± n. deep.
CAN BE BUILT FOR
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INSTRUCTION BOOK for either above
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CARINETS ONLY plastic or wood 17/6.

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All components available separately.

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6.3 v. 1 amp. . . . . . . . 4/6 0-30 v. 2 amp. tapped voltages 19/6 ALL-DRY POWER UNITS

By Decca. Suitable for any battery radio using 1R5, 1T4, etc., 67½ volts H.T., 1½ volts L.T. Mains input 200-250 adjustable. In metal chassis with rubber feet and black plastic cover. Size: 7×5×1½in. Mains lead and onf switch. Complete with two metal rectifiers, ready for use. List £14/15/-.

LASKY'S PRICE Post 3/6

If too large to fit into your por-

If too large to fit into your portable, stand it on or by it.

#### HP TERMS AVAILABLE

on certain goods.

Write stating your requirements.



#### **FAMOUS AMPLIFIERS** BUILT ON T.C.C. PRINTED CIRCUITS

MULLARD 510, ready for use. Price according to trans-15 gns.

COMPLETE KIT and printed circuit, from 12 gns.

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Book of the Mullard 510, 3/6. Book of the Osram 912, 4/-.

#### 5-VALVE RADIOGRAM CHASSIS COMPLETE WITH VALVES

3-wave superhet, 16.50m., 200-250m., 1,000-2,000m. Brand new Mullard and Mazda valvea—6C9, 6F15, 6LD20, N108, U107. Overall dim.: 13in. long, 6in. deep, 7in. high approx. LASKY'S PRICE, complete \$7.19.6 with all valves, Carr. & Pkg. 7/6 extra. Price without valves, £5/4/-.

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2½in. moving coil. Brand new micro-ammeters F.S.D. 0-750 micro-amps., 15 ohms resistance. Post extra.

SPEAKER COVERINGS. Large stocks of Tygan and "Someweave" Speaker Cover-Tygan and "Someweave" Speaker Coverings. Any size piece cut. Send for samples

# GERMANIUN CRYSTAL DIODES GEX.00 1/6. GEX.34 3/6. GEX.54 and 0A74 5/-.

FERRITE ROD AERIALS

Med. and long waves, wound, ready for use. Each 6/9, post 1/-. FERRITE ROD

5in. long, \$in. diam.. with full instruc-tions for making a Ferrite rod aerial, 2/6, post 1/-.

STANDARD 2-GANG CONDENSERS
.0005 mfd., with fixing feet. Each 5/11.

#### LASKY'S FOR **VALVES** 20,000 IN STOCK

Here are a few examples of brand new surplus and imported valves.

ı	EB91	7/6	EV41	10/6	EY51	12/6
١	EB41	7/6	EF80	10/6	EC84	11/6
1	EABC86	010/-	EF85	10/6	EY86	14/6
Į	EAF42	10/-	EF86	12/6	EZ40	8/6
i	EBC41	10/-	EF91	9/6	EZ80	8/6
ı	ECC85	10/-	6K8	10/6	PCF82	12/6
ı	ECC84	15/-	6 <b>V6</b>	9/6	PCC84	12/6
ı	ECC83	12/6	6K7	5/6	PL81	13/6
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ı	ECC81	9/-	6 R.7	6/6	PL83	11/6
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1	ECL80	11/6		JI	IR5	9/6
1	Also ful	l stock	s of B.V.	A. Va	lves and	C.R.

Tubes at the new lower list prices WRITE FOR COMPLETE LIST.

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COMPONENT BARGAINS WIDE ANGLE 38 mm. Line E.H.T. trans., Ferrox-cube core, 9-16kV.
Scanning Colls, low imp. line and 25/-25/frame
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Complete with circuit diagram, the frame 50/-frame .....rame or line blocking osc. transformer 17/6 former
Focus Magnets Ferrox-dure
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Electromagnetic focus coll with
combined scan coils

STANDARD 35 mm.	
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All 200-250 v. 50 c.p.s. primary, finest quality, fully guaranteed.
MBA/3. 350-0-350 v. 80 mA., 6.3 v. 4 a., 5 v. 2 a. Both illaments tapped at 4 volts.

MBA/7, 250-0-250 v. 80 mA., 6.3 v. 3 a., 5 v. 2 a. Both filaments tapped at 4 volts.

AT/3. Auto trans. 0-10-120, 200-230-240 v. 100 watts. 19/8. MT/340. Tapped input 200/250 v. 300-0-300, 100 mA., 5 v. 3 amp., 6.3 v. 1.5 amp.

300, 100 mA., 5 v. 3 amp., 6.3 v. 1.5 amp. 16/6 MT/341. Tapped input 250-0-250, 120 mA., 6.3 v. 5 amps., fully shrouded. 27/6

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#### AT ENORMOUS SAVING

Convert to big picture television at a price you can afford. Note especially that these are not "seconds" but perfect tubes without fault, and supplied in original cartons. Brief specification: 6.3 v. heater, ion trap, 14 Kv. E.H.T., wide angle 70 deg., standard 38 mm. neck, duodecal base, magnetic focus and deflection. Maximum length 17 lin. Gives large 11×14 in. black and white picture. GUARANTEED BY US FOR 3 MONTHS.

Full data, connections and suggested time bases supplied.

LISTED AT \$23.9.10 LASKY'S PRICE £8.9.6

Carr. and Insur. 22/6 extra.

Masks, Anti-Corona, Bases and Ion Traps available.

LASKY'S (HARROW RD.) LTD.

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PRICE . . . Including CRYSTAL MIKE and 1,200ft. reel of PLASTIC TAPE.

OR £3 EXTRA WITH REV. COUNTER.

(Plus £1/10/- carriage and insurance, of which £1 is refunded on return of Packing Case.)

Stern) introduce...

A "fidelity" TAPE RECORDER WITH EVERYTHING - EXCEPT A HIGH PRICE

IT INCORPOATES: The NEW TRUVOX Mk. IV TAPE DECK together with the "fidelity" MODEL HF/TR2 TAPE AMPLIFIER (both fully described on this page), and a Rola 10×6in. P.M. speaker.

 BEFORE CHOOSING YOUR TAPE RECORDER YOU SHOULD HEAR THIS MODEL-TRULY "Hi-Fi" RECORDINGS ARE OBTAINABLE and it is comparable to much higher priced Recorders.

Alternatively send S.A.E. for ILLUSTRATED LEAFLET.

CREDIT SALE: Deposit £12/8/- and 9 monthly payments of £4/10/8. HIRE PURCHASE: Deposit £24/15/- and 12 monthly payments of £2/5/11.

YOU CAN BUILD A PORTABLE TAPE RECORDER OR INCORPORATE "TAPE" IN YOUR RADIOGRAM.

WE MAKE SPEC!AL PRICES TOP URCHASERS OF TAPE EQUIPMENT (i.e. buyers of Deck and Amplifier together, etc.,) SEND YOUR ENQUIRY TO US. H.P. and CREDIT SALE TERMS ARE AVAILABLE.

A COMPLETE KIT OF PARTS TO BUILD

The "fidelity" TAPE AMPLIFIER Model HF/TR2 including POWER SUPPLY UNIT

FOR \$12.0.0. (Plus 5/- carr. and ins.)

This amplifier has been expressly designed to meet the requirements of the enthusiasts for High Fidelity reproduction. It is based on a new design, completed by the Mullard Technicians and only really high grade components are incorporated, trull High High grade components are incorporated, trull High High grade components are incorporated. The High High grade components are incorporated at the High High grade components are incorporated at the High High grade components are incorporated and the many obstitution of the High High grade provided to enable it to be used as an independent Amplifier for Gramophone Records or Radio Tuning Unit. Overall size: Ilin.×Sin.x Sin. high. Suitable or nearly all makes of Tape Decks. When ordering, please advise make of deck in use THE ASSEMBLY MANUAL, PRACTICAL DIAGRAMS, etc. are available for 2/9 or nd S. A.E. brief details

WE ALSO SUPPLY THE HF/TR2 ASSEMBLED and READY FOR USE FOR 216.0.0 (Pins 6) carr. & ins.) B.P. TERMS: Depost £8 and 9 monthly payments of 21. (DEEDIT TERMS: Depost £4 and 9 monthly payments of 21.

#### THE NEW TRUVOX MkIV TAPE DECK

THIS IS UNDOUBTEDLY ONE OF THE BEST TAPE DECKS ON THE MARKET WE HAVE A FEW ONLY AVAILABLE

(Plus 10/- carr PRICE £27.6.0

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H.P. TERMS: Deposit £13/13/- and 12 monthly payments of £1/5/4.

H.F. TERMS: Deposit £13/13/- and 12 monthly payments of £1/5/4.

SPECIFICATION: ● 3 B.T.H. shaded pole motors with silent friction drive eliminating wow and illuter. ● Push button controls, electrically and mechanically interlocked (patented) ● Patented electric type push button controlled brake. ● Inching to assist editing tape loading on the drop-in principal: accommodation for rele of 7th. diameter ● Tracking sense. To British and American standards. ● Playing times: Up to 3 bours with L.P. Tape or 2 hours with Standard Tapes. ● Two tracks, side by side, with safety gap. ● Playing time indication by precision revolution counter or large visual type indicator plate, according to choice. Positive Azimuth adjustment of Record/Player Head. ● High Impedance Heads. ● The metal work is Gold Hammered finish. ● Overall size 14½ in × 12½ in., from top of face of panel. overall depth 5in

IV DECK CAN ALSO BE SUPPLIED INCORPORATING PRECISION REV. ER (ot \$30/9/-. H.P TERMS: Deposit £15/4/6 and 12 months of £1/8/3. The MR. IV DECK CAN COUNTER for 230/9/~. CREDIT SALE: Deposit £7/12/3 and 9 months of £2/15/-.

#### STERN'S "COMPACT **AMPLIFIERS**



### Stern's "fidelity" F.M. TUNING THE ARMSTRONG MODEL AF105 AM/FM UNITA 5-Valve

Tuner incorporating the latest Mullard Permeability Tuned
 Unit Price assem bied less Power Supply:

£14.10.0 (Plus 7/6 carr. and ins.)

The "Compact 5-2"

The "Compact 5-2"

EXPRESSLY DEVELOPED FOR VERY HIGH QUALITY REPRODUCTION OF GRAM. RECORDS AND PARTICULARLY SUITABLE FOR HIGH QUALITY REPRODUCTION OF THE FM. TRANSMISSIONS.

A 2-stage high sensitivity; The "Compact 6-2" manufiles.

PRODUCTION OF THE F.M. TRANSMISSIONS.

A 2-stage high sensitivity
amplifier baving SEPARATE BASS and TREBLE
CONTROLS and designed
to give up to approx. 5
watts with very pleasing an addition elements the MEDIUM WAVEstage and incorporating
quality. PRICE £8/6/E8/6/E8/6/E8/16/E8/16/E8/16/ENUMED SUPPLY Levels from a small result of the stage and incorporating
quality. PRICE £8/6/E8/16/ENUMED SUPPLY Levels from a small result of the stage and incapant of the stage and incorporating the

POWER SUPPLY. Is obtainable from a small separate TERMS:—(a) H.P. Deposi. £9/9/- and 10 monthly pay-Unit which apart from supplying power to either Ampli — ments of £1/1/-; (b) Credit Deposit £4/15/- and 9 fier, also has additional supply available for a Radio — monthly payments of £1/14/7. Send S.A.E. if further Tuning Unit. PRICE (additional to above), £2/10/- data required.

Developed to meet the needs of those require really high quality radio and record reproduction

but who, for reasons of expense or lack of room in existing or proposed cabinets, cannot consider the normal high-fidelity system. The A.F.105 is as good as, or better than, all but the most expensive Amplifiers, and Associated units. Independent and continuously variable

Associated units. Independent and continuously variable Bass and Treble controls give a wide range of control. SEND S.A.E. FOR DETAILS.

PRICE £37 (Plus 7/6 Carr. and Ins.) CREDIT SALE TERMS: Deposit £9/5/- and 9 monthly payments of £3/7/10.
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> Open Monday to Friday 9 a.m .- 6 p.m. Saturday 9 a.m.-1 p.m.



**AMPLIFIERS** PRE-AMPLIFIERS

### HIGH FIDELITY ... HOME CONSTRUCTO

**TUNING UNITS** RADIO RECEIVERS

"Hi-Fi" ENTHUSIAST COMPLETE KITS OF PARTS FOR

QUALITY OF THIS NATURE HAS NEVER BEFORE BEEN OFFERED AT SUCH LOW COST.



THE in SPECIFICATION and BUILDING INSTRUCTIONS for these three Units are available for 1/6 each. THEY include

STERN'S "fidelity" PRE-AMPLI-FIER TONE CONTROL UNIT

"A design for the music lover"



This is the very latest design and needs no recommendation from us. Our Kit is complete to Mullard's specification, including the latest GILSON ULTRA LINEAR OUTPUT TRANSFORMER and the entire MULLARD Vaive line up. ALL SPECIFIED COMPONENTS are supplied.

PRICE OF COMPLETE KIT OF PARTS \$11/11/0 FOR USE, £8/-/- (Plus 5/- carr. and ins.).

Briefly it has inputs for all types of MICROPHONES, HIGH and LOW GAIN PICK UPS and a RADIO TUNING UNIT. It incorporates (BRAM EQUALISING CONTROL WILL OF SEARCH CONTROLS AND A TROLL (b) STEEPOUT FILTER; (c) Continuously OUTPUT CONTROL which enables its use with any type of MICROPHONES, and a RADIO TUNING CONTROL (c) CONTROL WILL OF SEARCH CONTROLS AND A TROLL (d) STEEPOUT FILTER; (c) Continuously OUTPUT CONTROL which enables its use with any type of MICROPHONES, HIGH and LOW GAIN PICK UPS and a RADIO TUNING CONTROL.

(d) STEEPOUT FILTER; (c) Continuously OUTPUT CONTROL which enables its use with any type of MICROPHONES, HIGH and LOW GAIN PICK UPS and a RADIO TUNING CONTROL.

(e) STEEPOUT FILTER; (c) Continuously OUTPUT CONTROL which enables its use with any type of MICROPHONES, HIGH and LOW GAIN PICK UPS and a RADIO TUNING CONTROL.

(e) STEEPOUT FILTER; (c) Continuously OUTPUT CONTROL which enables its use with any type of MICROPHONES, HIGH and LOW GAIN PICK UPS and a RADIO TUNING CONTROL.

(e) STEEPOUT FILTER; (e) Continuously OUTPUT CONTROL which enables its use with any type of MICROPHONES, HIGH and LOW GAIN PICK UPS and a RADIO TUNING CONTROL.

(e) STEEPOUT FILTER; (e) Continuously OUTPUT CONTROL which enables its use with any type of MICROPHONES, HIGH and LOW GAIN PICK UPS and a RADIO TUNING CONTROL WILLIAM CONTROL

COMPONENT PRICE LISTS and simple "wire-to-wire" PRACTICAL DIAGRAMS.

A COMPLETE KIT OF PARTS STERN'S "HIGH OUALITY" 8-10 WATT **AMPLIFIER** Has power sup-ply available for Radio Tun-ing Unit. Price of COM-PLETE KIT

(plus 5/-carr. £7/10/0 and ins.). WE ALSO OFFER IT ASSEMBLED

and BEADY FOR USE for £9/10/0 this amplifier has proved one of the most popular models yet offered to the HOME CONSTRUCTOR. It provides

yet offered to the HOME CONSTRUCTOR. It provides really excellent reproduction up to 8 watts, employing 8V8's in push-pull and incorporating negative feedback. Provides for the use of both 3 and 16 both 3 peakers. The Complete SPECIFICATION and BUILDING INSTRUCTIONS are available for 1/16.
"Wire-to-Wire" Diagrams are included and all Components are available senarately.

are available separately.

SPECIAL PRICE REDUCTIONS . . . FOR PURCHASERS OF A COMPLETE "Hi-Fi" AMPLIFIER

WE WILL SUPPLY (a) COMPLETE KIT OF PARTS to build THE MULLARD "5-10" MAIN AMPLIFIEE and the STERN'S "adelity" PRE-AMPLIFIER TONE CONTROL UNIT for \$16/16/- or we will supply THE TWO UNITS MADE UP and READY FOR USE for \$19/19/-. Terms: Deposit \$29/19/6 and 12 monthly payments of \$1/16/7.

#### MODERNISE YOUR OLD RADIOGRAM"

and Gram.

FRICE

£26/15/0

(Plus 7/6 carr.

TERMS: Credit Deposit £6/14/-and 9 monthly

payments from

£2/9/-. **H.P.** Deposit£13/7/6

Deposit£13/7/0 and 12 monthly

IT IS MUCH CHEAPER I THIS WAY!!

THE LATEST DESIGN OF COMBINED AM/FM REPLACEMENT RADIOGRAM CHASSIS and a NEW 4-SPEED RECORD PLAYER

A genuinely hand-made chassis providing really high quality on both Radio



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STERN'S NEW "Fidelity" COMBINED | THE NEW ARMSTRONG P.B.409 AM/FM | AM/FM RADIOGRAM CHASSIS RADIOGRAM CHASSIS luxe" Chassis for those who want the highest possible quality



Dep. £14/14/-and 12 monthly payments of £1/7/3. BRIEFLY IT HAS:—

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An 8 vaive line up incorporating the latest MULLARD preferred-type vaives, • Provides complete coverage of the VHF/FM wavehand plus the 8H0 RT, MEDIUM and LONG waves. • Has EL44's in Push-Pull, with negative feedback of 6 watte output. • Employs "Piano Key" Selector Switch and a Variable Tone Conirol. • Contains Gram input socket for both Crystal and Magnetic Pick-ups. • Provides for use of either 3 or 15 ohm Speakers. • Has Grey Tuning Indicator. • Two Gram Inputs are provided, one for Crystal Pick-ups and the other for Magnetic Picks one of Crystal Pick-ups and the other for Magnetic Picks one of Crystal Pick-ups and the other for Magnetic Picks one of Crystal Pick-ups and the other for Magnetic Picks one of Crystal Pick-ups and the other for Magnetic Picks one of Crystal Pick-ups and the other for Magnetic Picks one of Crystal Pick-ups and the other for Magnetic Picks one of Crystal Pick-ups and the other for Magnetic Picks one of Crystal Pick-ups and the other for Magnetic Picks one of Crystal Pick-ups and the other for Magnetic Picks one of Crystal Pick-ups and the other for Magnetic Picks one of Crystal Pick-ups and the other for Magnetic Picks one of Crystal Pick-ups and the other for Magnetic Picks one of Crystal Pick-ups and the other for Magnetic Picks one of Crystal Pick-ups and the other for Magnetic Picks one of Crystal Pick-ups and the other for Magnetic Picks one of Crystal Pick-ups and the other for Magnetic Picks one of Crystal Pick-ups and the other for Magnetic Picks one of Crystal Pick-ups and the Other Picks one of Crystal Picks one of Crystal Picks one of Crystal Picks one of the VHTP Picks on the Control Picks of Control Picks on the Other Picks on the Other Picks on the Other Picks on the BRIEF SPECIFICATION :-

STERN'S "SUPER SIX"

6 Valve Waveband Superhet

PRICE

£29/8/0

(Plus 7/6 carr. and ins.).

TERMS: Credit Deposit £7/7/and 9 monthly payments of £2/14/-. H.P. Dep. £14/14/-

Provides good se-lection of stations and really good reproduction on both RADIO & GRAM.

PRICE S14.0.0 (Plus 7/6 carriage and ins.) CREDIT TERMS: Deposit £3/10/- and 9 monthly payments of £1/5/8. H.P. TERMS: Deposit £7 and 10 monthly payments of 16/-.

payments of 16/-.

\*\* Delayed AVC on all wavebands

\*\* Preselection feedback

\*\* Preselection feedback

\*\* Modern valve line-up: 12AH8, 6BA6, 6AT6, two 6AQ5s
and 5Z4 (or OCTAL VALVE equivalents)

\*\* Push-pull output gives approx. 6 watts

\*\* Connections on chassis for extension speaker, gram.
and mains supply to gram.

\*\* Coverage 18-30 metres, 190-560 and 800-2,000

\*\* Overall size 11 x 77 x 84in. higb, dial 84 x 44in.

\*\* A bronze dial escutcheon is available for 4/6.

\*A bronze dial escutcheon is available for 4/6.

SEND S.A.E. IF FURTHER INFORMATION IS REQUIRED ON THESE CHASSIS.

To complete a GENUINELY HIGH QUALITY RADIOGRAM... we recommend THE NEW COLLARO MODEL 456 4-speed Autochanger, and if a LOUDSPEAKER is required.

We recommend THE 8- or 10-inch W.B. STENTORIAN "Hi-Fi" MODELS. We have SPECIALLY REDUCED PRICES for purchasers of a CHASSIS and RECORD PLAYER (and SPEAKER if required). SEND S.A.E. FOR DETAILS.

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● They play
MIXED 7m.,
10th. and 12th. records of same speed.

● They have spearate supphires for L.P. and 78 r.p.m.,
which are moved into position by a single switch.

● Minimum baseboard size required 14×12jin., with
height above \$\frac{1}{2}\text{in.}\$ and height below baseboard \$\frac{2}{2}\text{in.}\$ A
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#### RECORD PLAYERS THE VERY LATEST MODELS ARE OFFERED AT GREATLY REDUCED PRICES

● TRANSCRIPTION UNITS. ● 3- and 4-SPEED AUTOCHANGERS ● AUTOCHANGERS with MANUAL CONTROL POSITION. Send S.A.E. for ILLUSTRATED and DESCRIPTIVE LEAFLET.

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FOR CALLERS ONLY

We have in stock various KITS OF PARTS including F.M. Tupers, AM/FM Tupers, Midget Battery Portable and Mains Units, etc., etc., ... We also have the most comprehensive stock of WIRELESS and ELECTRICAL COMPONENTS.

### SPECIAL CASH ONLY OFFER!!



PLIFIER together with a 64in. P.M. Speaker and this altractive PORT-ABLE CASE.

ALL FOR ONLY £8.7.6. The Amplifier incorporates the latest B.V.A. Valves, types ECC83, EL84, with EZ80 Rectifier and has separate BASS and TREBLE CONTROLS. The CASE is attractively finished in Rexine, maroon and grey, and has space for almost any make of Autochanger. We also sell the two separately:

(a) AMPLIFIER and 6 in. SPEAKER .... £4 12 6 (b) PORTABLE CARRYING CASE 23 17

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### 18. TOTTENHAM COURT ROAD, LONDON, W.1

MUSeum 5929/0095 (50 yards only from Tottenham Court Road Tube)

All post orders please to: -24-26. HAMPSTEAD RD., LONDON, N.W.1

EUSton 5533/4/5

THE R.C. 2 AMP. BATTERY CHARGER THE R.Q. 2 AMP. BATTERY CHARGER KIT. Insaludes handsome well-rentited black stove-enamelled steel box, size; 7½in. × 3½in. × 3½in. × 1½in. × 1

TRANSISTORS — MULLARD TYPE 0.C.71. Available ex stock at new list price of 24/- each, also 0.C.70 at 21/- and 0.C.72 at 30/-. BRIMAR T.S.I. 18/-. All post free.



#### THE JASON FM TUNER

Based on the booklet by Data Publications Ltd., 2/- post free, including our individually priced Parts List. Highly sensitive, free from drift. Incorporates 4 valves 6AM6 and 2 specially graded G.E.C. Crystals. The kit supplied includes drilled chassis with tuning condenser, scale calibrated in mc/s., and attractive bronze stove-enamelled front plate aircady mounted (illustrated). Front plate size 6in. × 6in. × 6in. Chassis 7in. × 4in. × 1in. Complete standard kt. 26/15/- plus 2/6 P. & P. Fringe area kit £7/15/- plus P. & P.

FM POWER PACK KIT. We can now supply complete kit for power pack suitable for the above F.M. tuner or any other similar type. Price for the complete kit is 37/6 only or 52/6 for ready assembled unit. This pack is extremely small, incorporating valve rectifier type 6X4 and built on chassis size only 6×4×14in. Optional extra for power pack. Buigh Octal Plug 2/3.

THE T.S.L. FM TUNER
We can now supply this PM/VHF adaptor either in kit form or fully assembled, wired
and tested. Our price for the ready-built unit which incorporates its own power supply
is 213/15/- only, tax paid, plus 5/- P. & P. or H.P. terms. Magic eye tuning indicator,
just plug in 19/- extra. Or the kit complete as specified 210/19/6 plus 3/6 P. & P.
The Booklet "PM TUNER CONSTRUCTION" (32 pages) with full technical data and
point-to-point wiring diagrams together with our separately priced parts list is available
at 2/6 post free.

THE T.S.L. AM/FM CHASSIS 1957 Model
9-valve Superhet with F.M./VHF Band (4 wavebands). Push-pull output. Slow motion
tuning drive. The tone controls have been given an extra wide range to embrace all
types of recordings. A.C. 200/250 voltes, 50 cycles only. CASH £27/8/J.- Packing and
carriage 7/6. H.P. terms available. Demonstrations at 18 Tottenham Court Road.

SEND FOR DETAILS OF OUR NEW AM/FM CHASSIS "THE CAVALLER." This wonderful offer includes THREE LOUDSPEAKERS at an ALL-IN price of ONLY £25, plus 7/6 C. & P. H.P. Terms available.

7/6 C. & P. H.P. Terms available.

INTER-DUCING THE NEW T.S.L. FM TUNER UNIT

This compact unit with hull-tin power supplies has been designed by craftsmen to standards which will satisfy the most critical enthusiast. Brief specifications: Valve line up: ECCS5, 2-EFS9, EABCS0, 634 and EMS0. Overall also: 10½ M. v. Spin. H. v. Spin. D. Dial size 10½ M. v. Spin. M. v. Spin. D. Dial size 10½ M. v. Spin. M. v. Spin. D. Dial controls: Switch, OFF FM & GRAM. and tuning. Fre-set gain control at rear of chassis. Connections: Co-axial output socket, 300 obm serial input socket and pick-up input socket on rear of chassis. Price £17/10/- plus 5/- P. & P.

-DULCI-

All Dulci products available ex stock Illustrated leaflets and H.P. terms

Hustrated leaners and R.F. cama available. Dulei F.M. Tuner at £16/16/-. AM/FM Chassis H4 at £24/6/8. Each plus 5/-p. & p. Demonstrating at Tottenham Court Road |

ANNOUNCING OUR NEW F.M. TUNER

AMNOUNGING OUR NEW F.M. TUNER KITI (printed circuit)
This is our printed circuit version of the Osram 91.2 P.M. Tuner—using T.C.C. printed circuit and condensers, incorporating 5 valves and two germanium diodes. Attractive black and gold dial, with gold escutcheon plate. Dial aperture only 5×2in. Osram F.M. booklet plus our additional instructions and individually priced components list-2/6 post free or the Kit absolutely complete at 28/8/plus 2/6 P. & P. Aligament service available if required. We are demonstrating at 18 Totenham Court Road!

TELEVISION TURRET TUNERS 12
CHANNEL—"BRAYHEAD"
We have six types now available from stock, to cover Bands I and III—fully illustrated and descriptive leader available on request. Each unit is fully aligned and thoroughly tested before despatch. Valves employed are PCF80, PCC84 for AC/DO and ECF80 and ECC83 for AC/DO Series 168 19.5 16.0 Parallel 198 10.5 16.0 Parallel 198 10.5 14.0 Parallel 198 10.5 14.0 Parallel We have a large selection of in-built converters for all areas from 92/6: also serials, low-lose co-axial cable at 9d. per yd. Are you on our mailing list? illusta.

abile on aligned and despatch. Valve.

PCC84 for AC/DU

ECC84 for AC. Pric
2/6 P. P. All

Type Sound M/05

358 38.0

168 19.5

- P. 10.5

- O.5

- O.5

- O.5

- O.5

- O.5

- O.7

-

ANOTHER CARINET BARGAIN-

EXCLUSIVE 1
This cabinet as illustrated below was originally manufactured for Decca, Ltd., as the price well in excess of our selling price with in excess of our selling price with the p



#### SPECIAL PURCHASE! MANUFACTURER'S SURPLUS

Owing to favourable purchase we can offer strictly limited quantity of these handsome chassis. AC/DC 200/250 v. for Medium and Long Waves, plus gran position. Incorporates own frame aerial. Valve line-up: U107, N108, DH107, W107 and X109. Overlat chassis size 12x5;x7;in. high. Attractive bronze dial with gold and cream lettering. Dial size 11;x 4;in. Scale length 7;in. Logging scale provided. Price £7/19/56 only, tax paid, plus 3/6 P. & P. H.P. terms, £4 deposit plus four monthly payments of 22/-

Splendid unrepeatable offer !! Dulci F.3 Radiogram chassis We have been very fortunate in being able to obtain a limited quantity of this well known and highly efficient chassis which we are able to offer at a greatly reduced price. Definitely the last few!

Specification: Three wavel Specification:
Three waveband: long 1,000-2,000
metres; medium 187-540 metres; short
16-50 metres. Valve line-up: X79,
6BA6 or W7A7, 5AT6 or DH77, EL84
or N709, 6X4 or U7S.

Four controls, tone/on-off Volume wavechange.

Tuning: output 4 watts matched to 3-5

Tuning: output 4 water matched to 3-3 ohms. Incorporates latest Ferrite Rod Aerial. Pick-up sockets and mains supply for Gram. motor. Overall dimensions: 12ln. L. × 7ln. D. × 7lin. H. Attractive dial with red, gold and green lettering on black background. Size 11\(\frac{1}{2}\)in. × 4\(\frac{1}{2}\)in. Frice only £10/5/- plus \$\frac{3}{2}\)if P. & P.

JUST RELEASED!!!
THE NEW R.C. TRANSISTOR/CRYSTAL RECEIVER KIT

THE NEW R.C. TRANSISTOR/CRYSTAL RECEIVER KIT
This receiver, covering medium waveband, which can be assembled in about 1 hour, will give amazing volume and tonal quality when used in conjunction with a good aerial and earth. Incorporating PNP Transistor and Germanium
Diode. For headphone reception.
Included with the kit of parts is a landsome plastic case in black and white, measuring #4 x/2; 1/lin. This case accommodates the complex for the control of the control of

AM/FM KIT



#### PRE-SET TUNER UNIT

(Manufacturer's surplus)

(Manufacturer's surplus)

This is a two valve (THA1, VP41) superhet tune unit covering, in original stage, two pre-set stations: Light and flome Service, with provision for adding a third station. Station selection is by means of an attractive illuminated Perspex knob. A small modification, the addition of a Germanium dioce, is all that is required to enable this unit to be used in conjunction with any amplifier or tape recorder capable of supplying the necessary power; 200 v. D.G. Alternatively built-in power supplies may be added. This is an exceptionally well made unit producing a "clean," good quality output. Dimensions of Tuner: 9in. L.x3jin. W. x7itn. I. overall. Unit only 45/- plus 2/6 P. & P. We can also supply all the components for built-in power pack with full modification details at 20/-.

THE R.C.3/4 WATT AMPLIFIER RIT
Compare the advantages!

Treble, bass AND middle controls. For
crystal or magnetic pick-up. A.C. Mains
200/250 v. Valve line-up: 6V66T, 68.0.

metal 6&56T. Nevative feedback. Built
on stove enamelled steel chassis, measuring
only Sin. x 4in. x 21in. Four engraved
cream knobs are included in the price of
the complete kit with all necessary practical
and theoretical diagrams at £4/5/- only,
plus 2/6 packing and post or Instruction Book
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Post This 1/-. free. amplifier can be supplied be supplied assembled, tested, and ready for use at £5/5/-plus P. and P. Hearing is believing.



Our advantageous H.P. terms are available on any single item over 45. Let us have your

Please add postage under £1, or Cash with order, C.O.D. charge extra-open 9 a.m. to 6 p.m. Monday to Friday. Sorry but we close I p.m. on Saturday.

THE "ECONOMY FOUR" T.R.F. KIT. A three-valve plus metal reotifier receiver. A.C. mains 200/250 v. Medium and Long waves. We can supply all required components right down to the last nut and bolt. Valve line-up 6K7, 647 and 6V6. Chasels ready drilled. Cabinet size 12in. long by 6in. high by 5in. deep—Cholce of ivory or brown Bakelite, or wooden walnut finish cabinet. Complete instruction booklet with practical and theoretical diagrams. Each component brand new and tested print to nack. with practical and theoretical diagrams. Each component brand new and tested prior to packing. Our price 25/10/- complete—Remember this set is being demonstrated at our shop premises! We proudly claim that our fully illustrated instruction booklet is the most comprehensive available for this type of receiver—Booklet available at 1/6 post free, allowed if kft is purchased later. Plus 2/8 packing and carriage for complete kit.

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cking and carriage for complete kit.

THE "SUPERIOR FOUR" KIT. Our superior four-valve receiver. A.C. mains, 200/250 v. M. and Long waves. As with our very successful "Sconomy Four" all required components as supplied. Valve line-up: 2 8-367, 6 X567 and 6 V6GT. Chassis ready drilled. Cabinet size 10\(\frac{1}{2}\)in. A 10in. with. Maximum depth at base 5in. tapering to 3\(\frac{1}{2}\)in. at top. Sloping front. Very attractively finished in light wainut and peach. Bach component brand new and tested prior to packing. Complete instruction booklet with practical and theoretical diagrams is provided. Booklet valiable at 1/6 post free. Our price for available at 1/6 post free. Our price for availabe at 1/6 post free. Our price for complete kit, £6/9/6 Please add 2/6 packing and carriage. If preferred, we can supply Cabinet Assembly only, comprising Cabinet and bracket wave-change switch, Caoinet and bracket wave-change switch, dial, pointer, drum pulleys drive spindle, drive spring and knobs, at 45/-, plus 2/6 packing and carriage. N.B.—Our kits are even supplied with sufficient solder for the job.

N.B.—All our T.R.F. Kit circuits now include specially wound Denco "Max-Q" coils on polystyrene formers, improved performance Price remains the same.

#### SURPLUS BARGAINS-METERS

		00111 -00	DAILON	142-11515173	
	F.S.D.	Size	Туре	Fitting	Price
	50 microamp	D.C. 4in.	M.C.	Rectangular	. 110/-
	50 microamp	D.C. 31in.	M.C.	F.R	
	100 microamp	D.C. 2½ in.	M.C.	F.R	
	200 microamp	D.C. 2in.	M.C.	F.R. (Tropicalised)	. 30/-
i	200 microamp	D.C. 31in.	M.C.	F.R	
ľ	500 microamp	D.C. 2in.	M.C.	F.R	
ı	1 mA.	D.C. 2in.	M.C.	F.R.,	
	I mA.	D.C. 2in.	M.C.	F. Sq	
ı	1 mA.	D.C. 2tn.	M.C.	F. Sq. (1954 manufacture b	У
ı				Elliott)	. 25/-
ļ	1 mA.	D.C. 21in.	M.C.	Desk Type	. 30/-
ĺ	50 mA.	D.C. 2in.	M.C.	F. Sq	. 8/6
ł	100 mA.	D.C. 21in.	M.C.	F.R	. 10/6
į	.5 amp.	R.F. 2in.	Thermo	F. Sq	. 6/6
i	1 amp.	R.F. 21in.	M.C.	F.R	. 10/-
ı	120.0.120 amp.	D.C. 2in.	M.C.	F. Sq. (shunt required)	. 15/-
ı	150 amp.	A.C. 4in.	M.I.	R.P	. 45/-
ı	I amp.	R.F. 2½in.	Thermo	R.P	. 7/6
ı	3 amp.	R.F. 2in.	Thermo	F. Sq	. 6/-
ı	20 amp.	D.C. 2in.	-	R.P. (with shunt)	. 10/6
ı	30 amp.	D.C. 21in.	• M.I.	F.R	
ı	15 voit	A.C. 2½in.	M.I.	F.R	
Į	15-0-15 volt	D.C 24in.	M.C.	F.R	- 17/6
į	300 volt	A.C. 2½in.	M.C.	F.R	35/-
ı	300 volt	A.C. 31in.	M.I.	F.R	. 30/-
ı	SPECIAL U.S. 0	-I mA. 2lin. take	en from equipm	nent but perfect, 22/6 each.	R.P. =
ı	Round Projectio	n. M.C Movin	g Coil. Therm	o = Thermo-coupled. F. Sq.	== Flush
ł	Square. F.R. =	Flush Round, I	M.I. = Moving	Iron.	

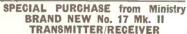
METER SPECIAL. We have a limited quantity of aircraft electrical thermometers. new, by Weston, 2in, moving coil meter, flush square fitting. These meters have a luminous scale graduated 40-140 degrees centigrade, but the full scale deflection is approximately 150 microampsi Frice 12.66 each only, plus 1/-. P, & P.

METER RECTIFIERS. 1 mA. by G.E.C. at 6/6, also 5 mA. by G.E.C. at 6/6.

#### **SPECIAL PURCHASE!!** LIMITED QUANTITY ONLY

A.A. PREDICTOR MK. I—OSCILLO-SCOPE No. 11. This ex Govt. unit readily lends itself economically to

readily lends itself economically to conversion to oscilloscope for domestic use. For Lib volt or 230 v. 50 cycle A.C. mains—comprising 24in. C.R.T. Type ACR10—45F91, ESC33, 8J5, 6X56T, SU2150 A and EA50. Continuously variable and stepped attenuator on Y amplifier. Internal X and Y shifts. Brightness and focus controls. Time base speeds can be increaseed by simple modification to cover 3 of s to 30 kc/s. Overall measurements of chassle as illustrated are 7in. high, 12in. deep and 19in. long. This unit, which is of recent manufacture and absolutely brand new, is offred at £12/10/- plus 15/- packing and carriage. This is a fraction of original cost and a bargain not to be missed! Circuits and full details are supplied.



TRANSWIIIEK/KEUELYER
Bulli into strong wooden cabinet 16in × 14in × 9in.
Complete with headphones and microphone. Range
5-8 miles with simple aerial. Frequency coverage44-61 mc/s. (5-7 metres). Uses standard 120 v. H.T.,
and 2 volt L.T. batteries. Complete with full operating
instructions. 59/6, plus 3/6 C. & P.
No. 17 Mk. II, as above, but secondhand, in good condition and complete. 45/-, plus 3/6 C. & P.

MAINS TRANSFORMER—SPECIAL Bemoved from chassis but clean and guaranteed. 200/240 v. Input. 350-0-350 at 250 m/a. 6.3V. 8 amps. 6.8V. at .6 amps. 5 at 3 amps. Only 30/- plus 1/6 P. & P.

BEACON TX/RX. (Mint condition.) BEAUON TEMES. Amn condition.)
Comprising: Transmitter/receiver unit, telescopic antenna, pair lightweight headphones, co-ax. cable, connecting leads, plugs etc., contained in excellent quality haversack. Supplied complete with valvess 5-8A5, 3-185, 1-1R5, 2-2v. vibrator packs, also comprehensive illustrated manual. Frequency coverage: 214-224 Mc/s. Size: 13in. x 10m. x 5in. Weight: 28ib. Limited quantity only at 72/6, plus 2/6 0. & P.

THE R.O. RAMBLER ALI-DRY PORTABLE KIT
Full assembly details with practical and theoretical
dagrams can be supplied at 1/6 post free. This
is a truly professional 4-valve superhet—all
dry—for medium and long waves. A cream
plastic top panel, with dial engraved in red and
green adds to the very imposing appearance of
this model which is housed in attractive cream
and grey leatherette covered attache-case type
cabinet, measuring only 9ln. x 7in. x 5lin.
Weight less batteries 4lb., with batteries 6jlb.
This set really has everything. Built-in frame
aerial, high quality, extremely sensitive, and very
adequate volume from the 6in. speaker. Valve
line-up 3V4, 1R5, 185, 1T4. Also the required
components, exactly as specified, including
cabinet, can be supplied from stock at the special
inclusive price of 27/7/- plus 2/6 p. and p. (less
batteries). Uses Ever-Realy 90 v. H.T. type
B126 at 10/-. Also L.T. 1.5 v. A.D. 35 at 1/6.
RAMBLER MAINS UNIT! At last we are able to offer our
specialmains units kit for using our popular all-dry "Ramblar" on A.C. Mains. Complete kit, which when assembled
fits saugly into battery compartment, can be supplied at 47/6 plus 1/6 packing and postage.
Price includes all required components, and full assembly instructions. N.B.—This unit
is completely self-contained in a metal box measuring 7in. x 23in. x 13in. and is ideally
suitable for ANY all-dry battery portable requiring 90 v. H.T. and 1.5 L.T.

THE R.E.P. 1-Valve RECEIVER. All
LOOK 1 L. A. first-class SIGNAL THE R.C. RAMBLER ALL-DRY PORTABLE KIT

THE R.E.P. I-Valve RECEIVER. All-dry battery operation, for use with headphones. The complete kit is available at 42/-, less batteries plus 2/- P. & P. or full instructions at 9d, post free.

COLL PACES. Manufacturers' Surplus. Miniature size, only  $2 \pm in \times 2 \pm in \times 1 \pm in$  deep. Iron-cored. For L. M. and S.W. with gram position. Switch has 2in. spindle. Absolutely brand new, complete with circuit. Price only 27/6 plus 1/6 P. & P. A snip.

RECORDER AMPLIFIER

RECORDER
(Well known manufacturer's surplus.)
This is a brand new a mplifier designed for use with a famous wire recorder. A simple modification is fication is all that is re-

floation is all that is required to make this unit ideal to make the control of the

VALVES: We have perhaps the most up-to-date valve stocks in the trade. A stamp will bring complete list but the following is a selection of brand new imported valve types, fully guaranteed. P.T. paid. 18 a selection of braind new intervalve types, fully guaranteed. P.T. EABCS0 10/- DAF96 10/6 PLS1 EAF42 10/- DF96 10/6 PLS2 EB91 7/6 DK92 10/6 PYS8 EB91 7/6 DK96 10/6 PYS8 EBC41 10/- DL96 10/6 PYS9 EBC41 10/- DL96 10/6 PYS9 EBC41 10/- DL96 10/6 PYS9 EBC90 10/6 PYS9 EBC9 10/6 PY80 9/-PY81 10/-BBC41 10/- DL96 10/6 PY81 10/- BBF80 11/6 or 39/6 per PY83 11/6 ECC91 9/- set of four UBC41 10/6 ECC91 9/- bet of four UBC41 10/6 ECC93 9/- DM70 9/- UCH2 11/6 ECC93 9/- EL41 10/6 UF41 10/6 ECC93 10/- EL42 10/6 UL41 19/- ECC95 10/- EL42 10/6 UL41 19/- ECC95 10/- EL42 10/6 UL41 19/- ECC95 10/- EL42 11/6 EA76 3/- ECH4311/6 EY81 11/6 6A76 3/- ECH4311/6 EZ90 8/6 6BA6 8/6 ECL90 11/6 EZ90 8/6 6BA6 8/6 ECL90 11/6 EZ90 8/6 6BA6 8/6 EF41 10/6 EZ91 9/6 EBW6 8/6 EF41 EF41 10/6 EZ91 9/6 EBW6 8/6 EF55 10/6 PCF90 12/6 50X4 7/6 EF65 12/6 PCF92 12/6 5085 10/- In addition we naturally have all usual surplus types available such as 6V6CT, etc. All in our valve price lists PY82 PY83 UBC41 UCH2

LOOK!!! A first-class SIGNAL GENERATOR that YOU can afford. The "Weyrad" type S.G.M.1 covers 100 ke/s to 70 mc/s in 6 bands, on Fundamentals, with an accuracy better than ±2%. Switched Andio Mod. 500 c/s. For use on A.C. Mains 100/250 v. 50 cycles. Fully illustrated leaflet available. Price ONLY \$12/10/plus 2/6 P. & P. H.P. available.

GRAMOPHONE MOTORS are in SHORT SUPPLY ! COLLARO AC.3/554: Three speed, single

player for A.C.mains 200/250v., c r e a up, inc porating the well-

known high output "T" type head. Strictly limited quantity at £6/19/6 plus 3/6 p. and p.

FOUR-SPEED CHANGERS The new FOUR-SPEED CHANGERS The new B.S.R. 4-speed auto-changer in attractive cream and gold finish now available from stock at £8/15/- only, plus 3/6 p. and p. HP. terms available.

THE "R.C. STALLION." THE "K.C. STALLION." This is the latest addition to our range of gramophome amplifiers and is supplied complete with high flux Sin. P.M. speaker and baffle. Incorporating three octal-type valves, 807, 6V2 - 1027.

Incorporating three octal-type valves, 6027, 6V6 and 6X5, this robust and well made unit is ideal for use in the larger type of record allows.

larger type of record player or radio-gram, and is equally suitable for use in conjunction with a radiol feeder unit. Separate bass and treb, e controls are provided, also provision a made extension speak. A control of the control



10in. CABINET SPEAKER. Idea! for P.A. etc. Comprises solid wood cabinet complete with carrying bandle. Painted dark brown; with built-in good quality 10in. P.M. speaker, 3 ohm speech coil, complete with lead and Igrante Jack plug. Brand new. Price only 45/-, plus 3/6 P. & P.

### /NE RADIO

18, Tottenham Court Road, London, W.I.

### There is always a fine selection of equipment at

#### LABORATORY RESISTANCE

BRIDGE BRIDGE A Standard Resistance Box containing 22 hand-wound non-inductive resistance coils of manganin (co-efficient of expansion ance coils of manganin (co-efficient of expansion .000006) which provides a 1 to 11.110 ohm standard at 60°F in 1 ohm steps for meter calibration, etc. The coils are connected to heavy machined brass blocks in which shorting plugs are arranged to form the two ratio arms and variable arm of a Wheatstone bridge.

The ratio arms of x 1/100, x 1/10, x 1, x 10 and x 100 enable the variable arm to measure by direct comparison unknown resistances between .01 and 1,111,000 ohms.

Heavy brass binding posts, an infinity plug, battery

between .01 and 1,111,000 ohms. Heavy brass binding posts, an infinity plug, battery and galvo keys, and ratio arms isolating link incorporated. New in teak box with operating instructions and explanatory circuits. Size  $54 \times 6 \times 8$  in.: £2/10/-, plus 5/- p.p. Size  $10 \times 64 \times 64$  in.: £3/10/-, plus 8/6 p.p. (Larger unit is of superior finish with ebonite insulated shorting plugs.)



2in. Magslips 50V 50 Cycle A.C. transmitter and receiver units. Accurate to 1/10th of 1°. Guaranteed in good working order. Price 30/pair, plus 3/- p.p.



#### AN/APN.1 TRANSDUCER

This Unit consists of Magnet and Coil which is attached to an aluminium diaphragm suspended freely and perforated to prevent air damping. Mounted on a Ceramic cover which sits over the diaphragm is a form of 2-gang capacitor which has a swing from 10-50 pF.

The above unit is used as part of Wobbulator described on page 252 of the June "Wireless World." Price 7/6 p.p.

#### COWL GILL MOTOR

THE PERFECT BEAM ROTATOR. This motor was designed to run on 24 volts D.C. but will successfully operate on 6 or 24 volts D.C./ A.C. if the magnetic clutch is removed (not needed for use in conjunction with Beam rotating, as reduction gears are sufficient to stop

There is a limit switch incorporated which allows rotation of  $2\frac{1}{2}$  turns in either direction (co-axial cable can be used instead of slip rings on mast). Speed can be varied by voltage input. Easily waterproofed for exterior use. Size 12in. L. × 4in. Dia.,  $\frac{1}{2}$ in. splined drive. Price 25/- each, plus 3/- p.p.

#### I.F. AMPLIFIER UNIT

460 kc/s with IT4. Brand new and boxed. Fully screened in plug-in box. Size  $2\frac{1}{2} \times 1 \times 4\frac{1}{2}$ in. Price, with circuit, 10/= each, plus 1/= p.p.

#### RADIO ALTIMETER

5 mA panel mounting meter, 3in. dia., 8in. circular scale. Large magnet. Scale easily removable leaving finished faceplate for re-calibration. Basis for sensitive portable multimeter. Brand new, boxed, 7/6 post free.



#### **BOOST GAUGES**

2in, dia.; suitable after minor adjustment as car induction manifold meter. 2/6 p.p.

#### BENDIX INVERTER

Type 12123-1-A. 24 volt D.C. input. 115 volt 3 phase 400 cycle .5 amp. Size 9in. long, 4in. dia., 6in. high including connector box and voltage regulator. Price £4 each, plus 5/- p.p.

#### BENDIX TRANSMITTERS TYPE T.A.12B

Master oscillator type transmitter. Four-channel 40W. operation, provides telephone, CW or MCW in frequency ranges of 300-600 kc/s, 3-4.8 Mc/s, 4-6.4 Mc/s, 4.37-7 Mc/s. Each of the 4 channels has its own oscillator and uses a 12SK7. The IPA stage consists of an 807 while the PA is two 807s in parallel. Size  $10\frac{1}{2} \times 6\frac{3}{4} \times 15\frac{1}{2}$ in. Price £3/15/-, plus 10/- carriage.

#### R.F. UNITS

R.F.25 40-50 Mc/s. Switched Tuning. Valved ..... 9/6 each R.F.26 50-65 Mc/s. Variable Tuning. Valved. Damaged dials .. 20/- each Perfect dials ...... 25/- each Packing and postage 3/- each type.



#### COMMUNICATIONS RECEIVER

(General Electric, U.S.A.) Highly sensitive receiver 1,500 to 9,000 kc/s (200-232) metres continuous coverage with overlaps in 4 channels. 3 I.F. stages, 2 R.F. stages and I.F. break-through trap. B.F.O. and O/P. Valve line-up: 5 12SK7s, 12K8, 12SR7, 12A6. Neon static in antenna circuit. Fully valved, £8/10/-, plus 10/- pack. and carr.

### **EDDYSTONE 358**

#### **COMMUNICATIONS RECEIVERS (B34)**

Range 40 kc/s to 31 Mc/s covered with 10 plug-in coils; only 4 coils available covering 1,250-2,100 kc/s, 2,100-4,500 kc/s, 4,500-9,000 kc/s, 9,000-22,000 kc/s. Selectivity: 2 kc/s at 2.5 db down; 55 kc/s at 35 db down; 150 c/s at 4 db down. Supply required: 6V 1.4A; 175/200V 65mA. CIRCUIT: variable mu pentode H.F. Amplifier, Triode-Hexode frequency changer, two I.F. Amplifiers (450 kc/s), A.V.C./Detector/A.F. Amplifier, output stage, B.F.O. Valve check Meter. £7/-/- without power supply. Plus £1 packing and carriage.



#### BEACON RECEIVER BC1206A

Covering 200-400 kc/s. Valve line-up: 6K7 RF; 6SA7 frequency changer; 6SK7 I.F. amplifier; 6SQ7 det; 28D7 O/P.

This was designed to run on 24/28V D.C. HT/LT. Excellent basis for car radio; size 6 × 5 × 4in. Good working order. £3/5/each, plus 5/- carr:

#### APQ.2. RADAR/JAMMING UNIT

Freq. 450-710 Mc/s. Containing 931a Photo Multiplier Cell complete with resistance network and lightproof box. Wide band amplifier. 2 6AC7, 1 6AC7, 2 388a. This unit is similar to the APQ.9 Jamming Unit. Brand new £5, plus 10/- carriage.

#### RECEIVER UNIT Ex 1143A

10:72 Mc/s, I.F.s: Frequency 100-120 Mc/s., suitable for conversion to 2 metres and Wrotham.

Owing to a large purchase we can offer these units fully valved, with circuit diagram at 25/- each, plus Valve line-up: 3/- post/packing. (4) EF50, (1) EL32, (2) EF39, (1) EBC33, (1) EA50.



#### U.S.A. ALTITUDE SWITCHES

Totally enclosed incremental network of 14×2.5K ohms 10% 1 watt resistors on two bank 11 way Yaxley type switch unit. Insulated mounting range and handsome glass covered dial with large central switch knob covering 11 positions in steps of 25 "feet." Rear socket, 4 connections to network and earthing point for screening. 3in. dia. × 5in. long. Brand new, boxed. 4/-post free.

All these fine offers are on display at 👈



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### The Walk-around Shop

#### ABSORPTION WAVEMETER

Easily converted to 2 metres or 70 cm. In Copper-plated metal cas  $3\frac{1}{4} \times 4\frac{1}{4} \times 5\frac{1}{9}$ in. with dial calibrated 0-100 and 80 v. Neon tube. Coverage approx. 190-210 Mc/s. New, 6/6 each, post paid.

#### RELAYS

Sensitive Single Pole change-over 2,000 ohm Coil. 10 volt D.C. Mounted on insulated base  $2\frac{1}{2} \times 2\frac{1}{2}$  ×  $\frac{1}{2}$  merican manufacture. New and boxed. Price 12/6, p.p.

4 Pole change over. Miniature Relay 200 coil. 24-27 volt D.C. Size  $1\frac{1}{2} \times 1\frac{1}{2} \times 1$  American manufacture. Price 7/6, p.p.



#### E.M.I. TEST EQUIPMENT FOR AMATEURS

E.M.I. 1ESI EQUIPMENT FOR AMATEURS

SPOT FREQUENCY MARKER. Type AD/U405. Operating on a frequency of 1 Mc/s and generating harmonics at 1 Mc/s intervals up into the V.H.F. range.

V.H.F. GRID DIP OSCILLATOR. Type AD/U406. Frequency may be varied over the range 65-150 Mc/s and accuracy is within ±2% at all frequencies within this range. Consumption 0.3 Amp. at 6.3V and 3mA at 150-250V. A stabilised power supply is not essential.

ABSORPTION WAVEMETER. Type AD/U408. This consists of a variable tuned circuit, across which is connected a germanium crystal in series with a 500 microammeter. Frequency range is continuous from 1.6-30 Mc/s. Accuracy is within ±2%.

V.H.F. ABSORPTION WAVEMETER AND FIELD STRENGTH METER. Type AD/U409. Of similar design to the Absorption Wavemeter, but for operation in the frequency range 65-150 Mc/s, accuracy being within ±2% over the specified range. The external coupling element consists of a single turn loop connected to the instrument by 2ft. of co-axial cable. A terminal is provided for the connection of a short rod aerial, to enable comparative field strength checks to be made, and, using such an aerial, the instrument can also be used as a carrier shift indicator, as a check on over-modulation of transmitters. The case, finished in pale green, with rubber feet, measures 8½ × 4½ × 2½ in.

GENERAL PURPOSE POWER SUPPLY UNIT. Type AD/U410.

23th. GENERAL PURPOSE POWER SUPPLY UNIT. Type AD/U410. L.T. supply being isolated from earth. A separate H.T. "On'Off" switch is provided. Input: 200-250 volts, 50 cycles A.C. only. Output: 6.3 volts at 2 amps. approx. and 250 volts at 60mA (unstabilised). Dimensions:  $8\frac{1}{2} \times 4\frac{3}{2} \times 5\frac{1}{2}$ in.

All Above Units New and Boxed

AD/U 405-406-408-409 ... £3/10/- each AD/U 410 Power Unit ... £4 each

Postage and packing 3/-.

#### HEATER ELEMENTS

230 volt 500 watt. Size 10½in. long, 1½in. wide, ½in. deep. This unit is totally enclosed and could be termed a Black Heater. Flanges turned up at either end, drilled for ½in. clearance makes easy fixing. Superb element for heating greenhouses, the home (preventing freezing, etc.). Price 5/- each, post paid.

#### BAND PRECISION WAVEMETER

2,900 to 3,150 Mc/s. TEST SET 288 A.M. Ref. 108B/6161. Comprising exceptionally rugged silver-plated Wavemeter Type 1665, resiliently mounted and directly tuned by 1½in. dia. calibrated micrometer with 6¾in. thimble scale. Temperature correction for micrometer attached. Resonance indicated on 100 microamp meter. Equally suitable for laboratory using milliwatt powers or, with loose coupling, for high powers. UR21 connecting cable and coupling probe supplied. Brand new in robust moisture-proof case with jacking-off screws and tool. Price £15, plus £1 packing and carriage.

#### GYRO UNIT AND INVERTER

Inverter: 12 volt D.C. input, 3 phase 190 cycle output. (These inverters can be used successfully as 12 v. D.C. Motors for Models). Gyro Unit: operates on 3 phase output from Inverter. Peak speed 11,400 r.p.m. Caged. Precision made equipment. These units are ideal for experimenting and demonstration purposes. Size: Inverter 4×3×3in.; Gyro 4in. dia. incl. cage. Price 12/6 per

pair, plus 3/- p.p.

#### **HEATER TRANSFORMERS**

6.3 volt, 11 amp.; brand new 6/6, plus 1/- p.p.

#### SMALL MAINS TRANSFORMERS

Input 230V 50 cycles, output 250V 40 mA, 6.3V 1.5A. Size  $3.9\times2.4\times2$ in. Ideal for TV converters. Price 12/6 each, plus 1/- p.p.

#### CHARGER TRANSFORMERS

For 6 or 12 volt; 230 volt 50 cycles input, 9 and 17 volt 3 amp. output. Price 15/6 each, plus 1/- p.p.

#### POWER UNIT Type 173

24 volt D.C. input, 120 v., 60 mA. output. Containing Vibrator Transformer, 12 volt Vibrator, two 120 volt Selenium Rectifiers. Chokes and Condensers. Size  $10\frac{1}{2} \times 6 \times 3$ in. Price 12/6, post paid.



#### POST OFFICE COUNTERS

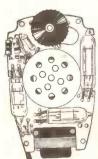
3 ohm, 4 figure no reset; size  $5 \times 1\frac{1}{2} \times 1$ in. 5/- each p.p.

#### STUD SWITCHES

20 segment hin. studs, base 5in. square with handle and housing. New and boxed, 5/- each, plus 1/6 p.p.

SPECIAL OFFER-MALLORY VIBRATOR PACKS 12 volt, 150 volt 40 mA. Brand new and boxed, size  $5\frac{1}{2} \times 5\frac{1}{2} \times 3$ in.

#### Make a miniature POCKET RADIO



high " O " Incorporating technique using the New Ferrite rod. Made possible by simple conversion of an ex-Govt. Hearing Aid. Size 33in. x 21in. x 1in.

Technical Details. A Germanium Diode Detector circuit followed by the existing 3 valve Amplifier, giving adequate amplification throughout the medium wave band.

This conversion can be carried out in approximately 30 minutes.

SEE and HEAR this Miniature POCKET RADIO demonstrated. THE COMPLETE KIT OF PARTS includes a Type OL10 Hearing Aid (with Crystal microphone) in perfect working order with miniature earphone and moulded ear insert attached; ferrite rod, germanium diode, components, circuit diagram and full instructions

PRICE £2 6s. Od. post paid

ALL COMPONENTS SOLD SEPARATELY

Deaf Aid Unit with earpiece.. Plastic Ear mould ...... £1 15 Ferrite Rod 0 Ferrite Rod Conversion Components ....
Batteries 1.5 v. L. T. (Type D 18)
30 v. H.T. (Type B 119) ... 4

NOTE: As the crystal microphone is not used in the Pocket Radio, it can, if desired be used as a general microphone and it does not require a matching transformer.



NOTE: Carriage prices quoted apply only to England and Wales.

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### (RADIO) LIMITED Phone: GERRARD 8204/9155 Cables: SMITHEX LESQUARE 3-34 LISLE STREET, LONDON, W.C.2

#### AMERICAN LIGHTWEIGHT **HEADPHONES**

Magnetic type, resistance 50 ohms. Fitted with rubber earmoulds to fit inside the ear. Best quality, ideal for communication receivers, etc., supplied with lead, brand new, 15/- each P.P. 1/6.

BENDIX COMMAND TRANS-MITTERS. Complete with all valves and crystal. Coverage 2.1 to 3 Mc/s., 29/6 each. Coverage 4 to 5.3 Mc/s., brand new, 29/6. P.P. 3/-.

HEAVY DUTY L.T. TRANSFORMERS. Input 230 volt 50 cycles. Output 17.5 volts 35 amps. (service rating, OK 50 amps). Brand new, 72/6 each. P.P. 5/-.

#### 0/1 MA. METERS



Brand new moving coil meters, round flush mounting with 2½in, scale, calibrated 0/300 volts. Price 25/- each. P.P. I/-.

8 MFD. PAPER CONDENSERS. Brand new TCC. Visconol type, 750 volts working, 5/6 each. P.P. 1/-.

COPPER AERIAL N 300ft, reel, 3/6. P.P. I/-. WIRE. Ex-U.S.A.,

HEAVY DUTY SLIDER. I ohm 12 amps. Brand new, 6/6. P.P. 1/9.

#### **HEAVY DUTY MAINS** ISOLATING TRANSFORMERS

Specification:—Primary 230 volts 3 amps. Second rry 230 volts 3 amps. (Service rating, OK 5 amps.), Ideal for laboratory or workshop use. Supplied brand new in original transit cases, £6/10/- each. P.P. 10/-.

INSTRUMENT POTENTIOMETERS.
Brand new Colvern type. 100,000 ohms, 10 watts, 3½in. dia. Ideal for bridges, etc., 10/6 each. Ditto, twin gang, 5,000 ohms, 10/6 each. P.P. 1/6.

450 KC/S B.F.O. UNITS. Brand new and complete with 1S5 valve, fully screened in aluminium case only 8/6 each. P.P. I/-.

#### **ROTARY CONVERTORS**

Input 24 volts D.C. Output 230 volts 50 cycles, 100 watts, Supplied brand new, 92/6 each. P.P. 5/-. Supplied brand

#### ALUMINIUM CHASSIS

Best quality, 18 s.w.g. Four sided, reinforced corners. reinforced corners. 3/6  $10\frac{1}{2} \times 7\frac{1}{2} \times 2\frac{1}{4}$  in. 5/3  $7\frac{1}{2}$  in.  $5\frac{1}{2} \times 2\frac{1}{4}$  in. 5/3  $1\frac{1}{2} \times 7\frac{1}{2} \times 2\frac{1}{4}$  in. 6/9  $1\frac{1}{2} \times 7\frac{1}{2} \times 2\frac{1}{4}$  in. 6/9 Postage 1/- all sizes.

POST OFFICE RELAYS AND POST OFFICE RELAYS AND KEY SWITCHES. Extensive stocks available at "CHEAP" prices. Ali enquiries welcomed. Special American relay offer. Type I, 3,500 ohm coil, I pr. c/o contacts, I2 v. 6 mA., 5/6. Ditto 6,500 ohms., 2 mA., 6/6. P.P. I/-.

#### A.C. MAINS BLOWER MOTORS

220/230 volt 300 watts. 1½in, diameter outlet. Housed in metal box and fitted with dust filter pads. Supplied complete with 4 spare filters, 2 way outlet adaptor and 2 lengths of hose. Brand new only and 2 lengths of hose. £4/19/6 each. P.P. 7/6.

#### **EX-NAVY SOUND POWERED TELEPHONES**



This type requires no batteries to operate and can be fitted in moments. Uses hand generator for calling, giving an extremely loud buzzing note, and also a neon indicator. Ideal for field activities, factories, office, etc. Only 45/- each. P.P. 4/6

#### AMERICAN MULTI-RANGE TESTMETERS

KANGE ITSIMELERS
1,000 ohms per volt, 400 microamp basic movement.
Ranges as follows: A.C. and D.C. volts, 0 to 5,000
volts in 6 switched ranges. D.C. current, 1 mA.,
10 mA., 100 mA. and 1 amp.
Resistance measurement from .1 ohm to 1 megohm.
Decibels from — 10 db. to + 15 db.
The instrument is housed in a polished wood case,
complete with leather carrying handle, test prods
and battery. Gauranteed perfect order and tested
before despatch. Price £5/19/6 each. P.P. 3/-.

#### MODULATOR 67



These bargain instruments contain a
COMPLETE A.C.
MAINS POWER PACK. Input 230 volts 50 cycles. Out-230

put 350 volts. 120 mA. and 6.3 volts 50 cycles. Output 350 volts. 120 mA. and 6.3 volts 5 amps. Choke and condenser smoothed and uses 5Z4 rectifier. (Transformer actually 200 mA.) Also included in the unit are 11 other valves, 5 SP61, 1 VR116, 2 EB34 and 3 EA50, and many other useful components, pots, resistors, switches, etc. Size of case 18 x 9 x 71, which is finished in grey. Supplied brand new, 49/6 each. P.P. 7/6.

#### **COSSOR DOUBLE BEAM** OSCILLOSCOPE, TYPE 339A

Operation 110/200/250 volts A.C. Ten time base positions, 6 cps. to 250,000 cps. Input frequency range, 10 cps to 2 Mc/s. Offered in perfect operational condition, fully tested, £27/10/- each. P.P. £1.

#### **AMERICAN GEARED MOTORS**



American 24 volt D.C. motors with built-in precision gearbox giving twin outputs 20 r.p.m. outputs 20 r.p.m. m. Will also operate and 6 r.p.m. Will also operate on 12 v. giving reduced out puts. Size 7in, x 13in. Shaft puts. Size 7in. x 13in. Shaft dia. 4in. Supplied brand new only 29/6 each. P.P. 3/-.

#### **MARCONI SIGNAL GENERATORS TYPE 390-G**

Frequency coverage 16 to 150 Mc/s in switched ranges. 200/250 volt A.C. mains 50 cycle operation. Supplied brand new in original transit cases complete with calibra-Supplied tion charts, instructions and compliment of leads. £25 each. P.P. £1. Other types in stock

#### AMERICAN ROTARY GENERATORS

Input 12 volt D.C. Output 250 volts 80 mA. Fitted with blower attachment which can be easily removed if desired. Brand new 22/6 each. Ditto with 6 volt input 22/6 each. P.P. 3/-.



#### AMERICAN BEACON TRANSMITTER/RECEIVERS

RT 37/PPN-2. Brand new and boxed, complete with instruction book, Equipcomplete with instruction book. Equipment comprises transmitter/receiver with 9 valves (5 3A5, 3 1S5 and 1 1R5), with built-in 2 v. vibrator power pack, spare vibrator, head-set, connector leads and 10ft. collapsible aerial. Frequency coverage 214/238 Mc/s. Price 72/6 each.

L.T. TRANSFORMER BARGAIN. Input 200/250 volts. Output tapped, 3, 6, 9, 12 24 or 36 volts 5 amps., 35/- each. P.P. 3/-BARGAIN CABLE CLEARANCE. 23/36 BARGAIN CABLE CLEARANCE. 23/36
3-core rubber mains flex, silk maroon covered, 12 yds. 9/-, 100 yds. 59/6. Twin mains 10 amp., twisted, plastic or rubber, 12 yds. 9/-, 100 yds. 59/6, 75 ohm coax cable.

\$\frac{1}{2}\$ in. 6/6 12 yds. Twin transparent mains 3amp. flex, 2/6 12 yds. Plastic 6 core flex, 15/50 amp. 3amp, flex, 15/- 12 yds.

#### A.R.88 WAVECHANGE **SWITCHES**

Ceramic, 8 bank, 6 position, complete with screens. Brand new and boxed 17/6 each. P.P. 2/6.

CRYSTAL MICROPHONE INSERTS Sensitive, ideal for amplifiers, tape recorders, etc., 4/6 each. P.P. 6d.

SMOOTHING CHOKE SNIP. Brand new parmeko chokes. 5 henry, 200 mA. Res. 50 ohms. Only 5/6 each. P.P. I/6. MODULATION TRANSFORMERS. Collins type, potted. Push-pull 807 to parallel 807, 20 watts audio. Brand new, 12/6 each. P.P. 1/6.

#### WESTON DUAL RANGE **OHMMETERS**

American test instruments by two famous American test instruments by two famous manufacturers. Incorporates a 21in. moving coil meter, ranges 0-2,000 and 0-200,000 ohms. Price 39/6 each, brand new with leads and leather carrying case. P.P. 2/6.

INSTRUMENT TRANSFORMERS. Type INSTRUMENT TRANSFORMERS. Type I.—Parmeko. Input 230 volts. Outputs 195 volts 85 mA. tapped 130 v. and 65 v. 6.3 volt 5 amp., 6.3 volt. 3 amp. Price 14/6. P.P. 1/6. Type 2.—Midget. 220/240 volt input. Output 200 volts 25 mA. and 6.3 volt 1 amp. Price 10/6. P.P. 1/-. Midget rectifier to match, 7/6.

#### **6 VOLT VIBRATOR PACKS**

6 volt D.C. input. Output 120 volts 30 mA. Fully smoothed, uses standard Mallory 4-pin vibrator. Compact in size. Supplied brand new and boxed, 12/6 each. P.P. 2/6.

JACKSON SHORT WAVE VARIABLES 75 pF. with twin ended spindle, 2/- each. Twin gang 100 pF., 3/6. P.P. 1/-.

#### **HALLICRAFTER S.36A** RECEIVERS

Frequency coverage 27 to 143 mc/s. A.M. or F.M. Built in "5" meter, operation 110/230 volt A.C. Supplied brand new in original cases £45 each P.P. 15/-.

HEADPHONE ADAPTORS. Ex-U.S.A. High to low impedance matching, brand new 1/3. P.P. 6d.

#### **50 MICROAMP METERS**

A  $2\frac{1}{2}$ in, flush mounting meter housed in a grey instrument case, complete with a chrome handle. Resistance A 2½ in, illush mounting meter housed in a grey instrument case, complete with a chrome handle. Resistance 800 ohms. Supplied brand new and tested, 59/6 each. P.P. 3/-.

#### WANTED. ALL TYPES OF COMMUNICATION RECEIVERS, TEST EQUIPMENT AND VALVES. HIGHEST CASH PRICES PAID.

#### **POWER UNIT TYPE 3**

complete A.C. mains power input 200/250 volts. Output 250 volts D.C., 100 m/a and 6.3 volts 4 amps, Fitted with H.T. voltmeter and current meter. Fully smoothed, choke and paper condensers, Housed in case for 19in, rack mounting. Sur in brand new condition, 72/6 Housed in grey counting, Supplied each.

### CHARGING AND MODEL TRANSFORMERS 1. Pri. 200/250 v. Sec. 3.5, 9 or 17 v. I amp.,

2. Pri. 200/250 v. Sec. 3.5, 9 or 17 v. 2 amp., Pri, 200/250 v. Sec. 3.5, 9 or 17 v. 4 amp., 4. Pri. 200/250 v. Sec. 6.3 v. 3 amp., 8 v. 1.5 amp., 9/6. 5. Pri. 200/250 v. Sec. tapped, 3, 4, 5, 6, 8, 10, 12, 15, 18, 20, 24 or 30 v. 2 amp., 18/6. P.P.

L.T. METAL RECTIFIERS Full wave and bridged. 12 v. 1 amp., 6/3; 12 v. 2 amp., 9/3; 12 v. 4 amp., 13/9; 12 v. 10 amp., 32/6; 24 v. 4 amp., 22/6; 1/- P.P. all

#### PANORAMIC ADAPTORS

Brand new and boxed Ex-U,S.A. For use with receivers having an I.F. of 455/475 kc/s., giving a bandwidth of 200 kc/s. 110/230 volt A.C. operation. Price £30 each. P.P. £1.

### ELECTROLYTIC CONDENSER BARGAINS

All new stock, 
2m. 450 v. 1/9 30 m. 450 v. 3/3 18  $\times$  16 m. 
2m. 500 v. 2/9 40 m. 450 v. 3/9 450 v. . 3/6 
2m. 500 v. 2/9 8  $\times$  2m. 450 v. . 3/6 
2m. 450 v. 2/9 8  $\times$  2m. 450 v. . . 3/6 
2m. 50 v. 3/3 8  $\times$  16 m. 500 v. 4/3 
2m. 25 v. 3/9 8  $\times$  16 m. 500 v. 4/3 
2m. 25 v. 4/8 50  $\times$  50 m. 360 v. 4/3 
25 m. 25 v. 19 275 v. 3/9 350 v. 4/3 
250  $\times$  220 m. 50 m. 12 v. 1/3 276 v. . 3/6 
6 v. . 2/6 500 m. 12 v. 1/3 276 v. . 3/6 
6 v. . 3/6 50 v. 4/3 6000 m. 6 v. 3/3 
6 d. P./P. on all types. All new stock.

500 PF. TUNING CONDENSERS Brand new single gangs, 3/6 each. Brand new 3 gangs, 6/6 each. Sub-miniature twin gang for transistors, 365 pf., 8/6. P.P. I/-.

#### ADMIRALTY REFLEX RE-ENTRANT P.A. LOUDSPEAKERS

Twin units. Impedance 3 ohms. Extremely sensitive and directional. Ideal for all outdoor work. Complete with 600 ohm line transformer. Price 32/6 each. P.P. 5/-.

DEAF AID EARPIECES. Brand new, 30 ohm res., 3/6. Lead, 1/-, P.P. 6d. I megohm pots w/switch, 1/-, Output transformer, 1/-, P.P. 6d.

#### METER BARGAINS

0/50μ amp. 2½in. Pj. MC	49/6
0/100µ amp. 2½in. F.M.M.C	39/6
0/50 M/amps, 2in, F.M.M.C	7/6
0/150 M/amps, 2in. F.M.M.C	6/9
0/200 M/amps, 2½in, F,M,M,C,	9/6
0/1 amp. RF, 2½in. Pi. T.C	5/-
0/4 amp. RF. 2in. F,M,T,C,	5/-
00/300 volt D.C. 2in, F.M.M.C	10/6
0/300 volt A.C. 21in, F.M.M.I	25/-
0/1,5 amp. A.C./D.C. 2in, F.M.M.I.	6/6
20/0/20 amp. Lucas car type	8/6
500/0/500μ amp. 2½in. F.M.M.C.	25/-
ALL NEW AND UNUSED	

2 m/a meter rectifiers S,T,C,..... 5/6

#### **R.1155 COMMUNICATION** RECEIVERS, MODEL L



Latest issue by the Ministry. Similar to the model N, incorporating the trawler porating the trawler band. Frequency cov-200-500 kc/s., erage, 200-500 kc/s., 600-1,500 kc/s., 1-5.3 mc/s., 3-7.5 mc/s., 7.5-18.5 mc/s. Supplied as

new, aerial tested and complete with illustrated descriptive leaflet. Price £12/19/6 each. P.P. 10/-.

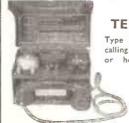
#### C.R. 91 COMMUNICATION RECEIVERS

Navy version of the AR.88.1.f. Receiver. Frequency coverage 75 kc/s, to 550 kc/s, and 1,5 mc/s-30 mc/s. on six bands.

Operation 110/230 volts A.C., speaker or phone output, variable selectivity, B.F.O. etc. Offered in first class condition, re-aligned and thoroughly tested. Price £45 each. P.P. 30/-

#### L.T. TRANSFORMER BARGAIN

Input 200/250 volts. Output 12 volts 5 amps, Brand new, 12/6 each. P.P. 2/6.



#### FIELD TELEPHONES

Type Don Mk. 5. Buzzer calling, Ideal for inter office or house communication. Supplied complete with two 1.5 volt cells. tested and

ready to operate. Price only 39/6 each. P.P. 3/-.

#### MARCONI U.H.F. SIGNAL **GENERATOR T.F. 517, MODULATION GENERATOR T.F. 675**

Complete station comprising TF 517 signal generator, frequency coverage 16-58 mc/s, and 150-300 mc/s, and TF.675 pulse modulator, repetition speed 50-3,000 cycles, pulse width 2-12.4  $\mu$  sec. Supplied brand new in original transit case with Instruction book and full complement of leads. £42/10/- each. P.P. 30/-.

#### MARCONI CRYSTAL CALIBRATORS

Frequency coverage 170/240 mc/s. Directly calibrated, accuracy .001%. Operation 200/250 volts A.C. Supplied complete with 5 mc/s crystal and spare set of 5 valves, in original transit case, brand new with instructions. £4/19/6 each. P.P. 10/-.

#### TRANSMITTER/RECEIVER No. 19, Mk. II



Equipment comprises 3 separate units built into one chassis and separate power pack. Specification: "A" set.

For R.T., C.W. or M.C.W. Range on R.T. 15 miles C.W. 50 miles. Superint receiver, 45 kg/s miles. Superint receiver, 465 kc/s, 57. 18. F. 38 kc/s, 58. Value ine-up 68.7; EFS 98.8 miles, EFS 99. 18. Superint receiver, 465 kc/s, 57. 18. F. 38 kc/s, 58. Value ine-up 68.7; EFS 98.8 miles, EFS 99. EFS 99 buffer, EB34 ADC, 807 P.A. "B" set, Transmitter/receiver 229/241 me/s, Local use up to 1 mile. Valve line-up; CV8, 2 68.7 and 69.6. Lucler Com. set. 2 valve A.F. amplifier for vehicle crew inter-communication. Valve line-up; 68.7 and 69.6. A 2 in. meter is built in reading L.T. and H.T. voltages, drive, etc. POWER UNIT. 12 volt D.C. input. Output 275 volts 110 m/a., and 500 volts 50 m/a. Equipment is of American manufacture and is supplied in good condition. Price, complete with power pack only £5/10/- each. P.P. 15/-. Less power pack, £4/19/6 each.

#### **POWER UNIT 234**

A complete A.C. mains power unit in grey metal case for 19in, rack mounting. Input 200/250 volts A.C. Output 250 volts 150 m/a. and 6.3 volts 6 amps. Double choke and condenser smoothed. Fitted with 2½in, moving iron meter for measuring A.C. input and D.C. output volts. Price 69/6 each, P.P. 8/6.

VARIAC TRANSFORMERS. Input 220 volts 50 cycles. Output variable from 200-240 volts 7.5 amps. Price 92/6 each. P.P. 5/-. TRANSISTORS. Brand new, equivalent to OC71, 10/-. Germanium crystal diodes, 10d.

SOUND POWERED EARPIECES. Can be used as a two-way communication, no batteries required. New, 3/6 each, P.P. 1/-,

#### DYNAMO EXPLODER UNITS

Used for detonating explosive charges. Operation is by hand generator, giving 1,800 volts D.C. across output terminals. Ideal also for use as photo flash generator. Supplied brand new only £3/19/6 each. P.P. 5/-.

HEATER TRANSFORMERS. Brand new. 230 volt input. 6.3 volt output 1.5 amps. 5/9 each. P.P. I/-.

SURPLUS SPEAKER BARGAINS

SURPLUS SPEAKER BARGAINS All new and unused Elac Sin. 3 ohm, 17/6; Elac 6½in. 3 ohm, 17/6; Elac 6½in. 3 ohm, 27/6; ROLA 7X4 elliptical 3 ohm, 18/6; Plessey 10X7 elliptical 3 ohm, 16/6; Plessey 10X7 elliptical 3 ohm, 27/6; Goodmans 3½in. 3 ohm, 17/6; Std. pentode o/p transformer, 4/6.

#### SMOOTHING CHOKES

ALL NEW AND UNUSED
G.B. 20h. 175 m/a., 10/6; Parmeko 8H.
250 m/a., 10/6; Parmeko 9H. 100 m/a.,
7/6; Parmeko 8H. 50 m/a., 5/6; Parmeko
C core, 4H. 22.5 m/a., 4/6; Collins 8H.
100 m/a., 8/6; Parmeko swinging choke,
3.6-4.2H. 250 m/a. 20H. no D.C., 10/6;
15H. 60 m/a., 5/6; STC 10H. 60 m/a., 4/6.

BAND III AERIAL BARGAINS. 3 element aerial, for wall mounting, complete with wall bracket and stand off arm, 360° rotation, 32/6 each. Ditto S element, 42/6. P.P. 3/-PDDYSTONE POWER UNITS. 200/250 volts input. Output 175 volts 65 m/a., and 6.3 volts 3 amps. Fully smoothed, 524 rectifier, 32/6 each. P.P. 4/6.

#### G.P.O. BELL UNITS No. 1

Supplied brand new in wooden box, complete with two bells, induction coil and condenser, 7/6 each. P.P. 2/6.

ROTARY CONVENTORS. Input 24 volts D.C. Output 50 volts A.C. 50 watts. Brand new, 29/6 each. P.P. 3/-. WAFER SWITCHES. Small. 2 p. 2 w. 1/6. 3 p. 4 w. 2/6. 4 p. 3 w. 2/6. 2 p. 6 w. 2/6. 1 p. 12 w. 2/6. Meter switch 2 p. 11 w 2 band, 2/6. Ceramic 4 p. 4 w. 2 bank, 3/6. Large Tx ceramic, 2 p. 6 w. 2 bank, 7/6.

#### **VALVE BARGAINS**

VALVE BARGAINS
Large stocks held. Few examples:
5V4 8/6, 6AG5 3/6, DK96 9/6, EY51 10,6,
EF86 12/6, 6V6 6/6, DL96 9/6, EF80 10/6,
EL84 12/6, 5U4 8/6, EX5 7/6, PX25 15/6,
DF96 9/6, ECF80 12/6, EZ81 10/6, 6H6
1/9, 6SN7 6/6, DAF96 9/6, ECF82 12/6,
ECC83 10/6, 616 3/6, KT66 12/6, DF91
7/6, ECC84 12/6, ECL80 11/6, 2D21
10/6, VUIII 1/9, EF39 5/6, ECH42, 10/6,
ECH81 10/6, EF37A 10/6.
ALL NEW AND GUARANTEED

Phone: GERRARD 8204/9155 Cables: SMITHEX LESOUARE STREET, LONDON, W.C.2

#### R. S. C. BATTERY CHARGING

**ASSEMBLED** CHARGER v. or 12 v. 2 amps. Fitted Ammeter and selector plug for 6 v. or 12 v. Louvred metal case, finished attractive hammer blue. Ready for use mains and output leads, Double Fused. 47/9



ASSEMBLED CHARGERS 6 v. l amp. 6 v. or 12 v. 1 amp. .. 25/9

EQUIPMENT

BATTERY CHARGER KITS Consisting of Mains Transformer F.W. Bridge, Metal Rectifier, well ventilated steel case, Fuses, Fuse-holders,

6 v. or 12 v. 1 amp. 25/9
6 v. or 12 v. 2 amps. 38/9
6 v. or 12 v. 2 amps. 59/9
6 v. or 12 v. 2 amps. 59/9
Above ready for use. Carr. 2/9.
HEAVY DUTY KIT
12 v. 30 amp. Suitable for garage or firm with a number of vehicles. Mains input 200/250 v. 50 c/s. Outputs 12 v. 15 amp. twice. Consists of Mains Trans. 2 Metal Rectifiers, 2 Metals Rectifiers, 2 Metals Rectifiers, 2 Rheostats and circuit. Only 9 gns. Carr. 15/
EX GOVT. MAINS TRANSFORMERS EX

All for A.C. MAINS 200-250v., 50 c/s. Guaranteed 12 months Assembled 6 v. or 12 v. 4 amps.



Fitted Ammeter and variable charge selector. Also selector plug for 6 v. or 12 v. charging. Double fused. Well ventilated steel case with blue hammer rinish. Ready for use with mains and output leads. Carr. 3/9. Or Deposit 13/9 and five monthly payments 13/9.

#### SELENIUM RECTIFIERS

APPELLIA11.	1/2 / 1 / 1   1   1   1   1
L.T. Types	6/12 v. 6 a 19/9
L.T. Types 2/6 v. ½ a.h.w. 1/9	6/12 v. 10 a 25/9
6/12 v. ½ a.h.w. 2/9	H.T. Type H.W.
F.W. Bridge Types	120 v. 40 mA. 3/9
6/12 v. 1 a 4/11	250 v. 50 mA. 5/9
6/12 v. 2 a 8/9	250 v. 80 mA. 7/9
6/12 v. 3 a 11/9	250 150 mA 9/9
6/12 v. 4 a 14/9	300 v. 250 mA. 12/11
CO-AXIAL CABLE.	75 ohms. lin., 8d. yard
Twin screened feeder, 1	
5 CORE FLEX. H	lenleys circular rubber
14/36. Each lead colour	coded. 1/6 yd.

DIAL BULBS, M.E.S., 8 v. 0.2 a., 6/9 doz. 6.5 v. 0.3 a., 5/9 doz. 2.5 v. 0.3 a. 3/9 doz. ELECTROLYTICS (current production).

NOT Ex	Govt.
Tubular Types	Can Types
8 mfd. 450 v 1/9 8 mfd. 500 v 2/6	16 mfd. 350 v. 1/I1 16 µF 450 v 2/9 16 mfd. 500 v. 3/9
16 μF 350 v 2/3	32μF 350 v 2/11
16μF 450 v 2/9	32 mfd. 450 v. 4/9
16μF 500 v 3/9	100 mfd. 450 v. 4/9 8-8 µF 450 v 2/9
8-16µF 500 v. 4/11	8-16 µF 450 v. 3/11
25μF 25 v 1/3	16-16 µF 450 v. 3/11
50μF 12 v 1/3	32-32 µF 350 v. 4/9
50 mfd. 25 v 1/9	32-32 µP 450 v. 5/9
50μF 50 v 1/9	100-100 mfd. 350 v.
100 mfd. 12 v. 1/9	64-120 mfd. 350
100 mfd. 25 v. 2/3	v 7/6
3,000 mfd. 6 v. 3/9	100-200 mfd.
6,000 mfd. 6 v. 3/11	275 v 6/11
Many others	in stock.

VOLUME CONTROLS with long spindles, all values, less switch, 2/9; with S.P. switch, 3/9.

EX GOVT. STEP UP/STEP DOWN
TRANSFORMERS. Double wound 80/100.
watts. 10-0-100-200-220-240 v. to 5-0-75-115125-135 v. or Reverse. Only 11/9, plus 2/9 post. GOVT. METAL BLOCK PAPER

	U	JNDI	NOEKO	
4 mfd.	500 v	2/3	10 mfd. 500 v	4/9
4 mfd.	1,000 v.	3/9	8-8 mfd. 500 v.	5/11
8 mfd.	500 v	4/6		
4 mfd.	400 v nlu	s 2 mf	d. 250 v.	1/11

EX GOVT. VALVES. VR137, EA50, EB34, 11d.; SP61 2/3; VS110 1/11; 6J5 3/9; 6V6G, 5U4G 7/9, 35Z4, 6X4 5/9; EF80 7/9.

EX GOVT. UNITS, type RDF1 in original scaled cartons with 14 valves including 5Z4G, etc., trans, L.F. choke, Rectifier, etc., etc. We cannot enter into correspondence regarding these units which represent a really exceptional bargain at 29/9. Carr. 7/6.

#### OIL FILLED BLOCK CONDENSERS

Bryce 11-7 mfd. 500 v. New unused Govt. surplus, only 5/9 each.

#### THE SKY FOUR T.R.F.RECEIVER



A design of a 3 valve 200-250 v. A.C. Mains design of v. A.C. Mains L. & M. wave T.R.F. receiver with selenium rectifier. For inclusion in inclusion in cabinet illustrain

ted above or walnut veneer-walnut veneer-wal ted above or walnut veneer-

#### EX GOVT. MAINS TRANSFORM All 230 v. 50 c/s. input 120-0-120 v. 40 mA. 250-0-250 v. 60 mA., 6.3 v. 3 a., 6.3 v. 1 TRANSFORMERS a. Potted 4½-3¼-3in..... 11/9

HEAVY DUTY OIL FILLED MAINS
TRANSFORMERS
Suitable welding or soil heating. With input Suitable welding or soil heating. With input of 200-250 v. 50 c.p.s., output is 12 v. 80-100 amps. Only £6/19/6, carr. 7/6.

### MANUFACTURERS SURPLUS TRANSFORMERS

TRANSFORMERS
Fully shrouded upright. Primary 200-240-250 v. Sec. 425-0-425 v. 150 mA. 6.3 v. 3 a., 5 v. 3 a., 33/9. Drop through type 250-0-250 v. 70 mA. 6.3 v. 3 a., 11/9. Postage on either type 2/9.

EX GOVT. SMOOTHING CHOKES
250 mA., 5 H., 50 ohms. 12/9
250 mA., 3 H., 50 ohms. 8/10 mA., 10 H., 50 ohms. 10/11
100 mA., 10 H., 100 ohms, Parmeko 6/9
100 mA., 5 H., 100 ohms, Tropicalised 3/11
50 mA., 50 H., 1,000 ohms. 6/9
L.T. type 1 amp., 2 ohms. 2/9

EX-GOVT. CASE. Well ventilated, black crackle finished, undrilled cover. Size 14—10—8½ ins. high IDEAL FOR BATTERY CHARGER OR INSTRUMENT CASE. COVER COULD BE USED FOR AMPLIFIER. Only 9/9, plus 2/9 post. SPECIAL OFFERS. Small 2 gangs .0005 mfd., 4/9. Electrolytics 32-32-32 mfd. 250 v. 2½ × 1½ ins., 2/9 each or in lots of six, 2/3 each.

#### TO MAINS CONVERSION UNITS

Type BM1. An all dry battery eliminator. Size  $5\frac{1}{2} \times 4\frac{1}{2} \times 2$  in, approx. Completely replaces batteries supplying 1.4 v. and 90 v. where A.C. mains 200-250 v. 50 c/s. is avilable. Suitable for all battery portable receivers requiring 1.4 v. and 90 v. This includes latest low consumption types. Complete kit with diagrams, 39/9. or kit with diagrams, 39/9. or ready for use, 46/9.



MINIATURE MOTORS. 24/28 v. D.C. or A.C. Size only 2½ x 1½ins. Spindle 1½ins. long, ½in. diam. Made by Hoover Ltd., Canada. Price only 9/9s. VIBRATORS. Oak 2 v. 7 pin. synchronous, 7/9.

M.E. SPEAKERS. 2-3 ohms R.A. 8in. Field 600 ohms, 11/9

Type BM2. Size 8 × 5½ × 2½in. Supplies 120 v., 90 v., and 60 v., 40 mA. and 2 v. 0.4 a. to 1 amp. fully smoothed THEREBY COMPLETELY RE-PLACING BOTH H.T. BAT-TERIES AND L.T.2V.ACCUMU-LATORS when connected to A.C. mains supply 200-250 v. 50 c/s. SUITABLE FOR ALL BATTERY RECEIVERS normally using 2 v. accumulator. Complete kit with diagrams and instructions 49/9 or ready for use 59/6.

T.V. CABINETS. For 15 16 or 17in. tube. Table model with doors, 79/6 carr. 7/6.

R. S. C. TR	AI	NSFORMERS	
FULLY GUARANTEED.	INTE	RLEAVED AND IMPREGNATED	
MAINS TRANSFORMERS Primaries 200-230-250 v. 50 c/s.		FILAMENT TRANSFORMERS Primaries 200-250 v. 50 c/s.	
FULLY SHROUDED UPRIGHT MOUNTI	NG	6.3 v. 1.5 a 5/9 0-2-4-5-6.3 v.	
250-0-250 v. 60 mA., 6.3 v. 2 a., 5 v. 2 a.,		6.3 v. 2 a 7/6 4 a	16/9
Midget type, 2½-3-3in	17/6	0-4-6.3 v. 2 a. 7/9 6.3 v. 6 a	17/6
350-0-350 v. 70 mA., 6.3 v. 2 a., 5 v. 2 a.	19/9	6.3 v. 3 a 8/11 12 v. 3 a. or 12 v. 1 a 7/9 24 v. 1.5 a.	17/6
250-0-250 v. 100 mA., 6.3 v4 v. 4 a., c.t.,	25/9	12 V. 1 a //9 24 V. 1.5 H.	1//0
0-4-5 v. 3 a	23/9	CHARGER TRANSFORMERS All with 200-230-250 v. 50 c/s. Prim:	aries.
for R1355 conversion	31/-23/9	0-9-15 v. 11 a., 11/9; 0-9-15 v. 3 a., 0-3.5-9-17 v. 3 a., 17/9; 0-9-15 v. 5 a.,	16/9:
300-0-300 v. 100 mA., 6.3 v. 4 a., 5 v. 3 a. 300-0-300 v. 100 mA., 6.3 v. 4 v. 4 a. c.t.,	- 1.	0-9-15 v. 6 a., 23/9.	17/7,
0-4-5 v. 3 a	26/9	ELIMINATOR TRANSFORMERS	
350-0-350 v. 100 mA., 6.3 v. 4 a., 5 v. 3 a. 300-0-300 v. 130 mA., 6.3 v. 4 a., c.t., 6.3 v.	23/9	Primaries 200-250 v. 50 c/s.	
1 a., suitable for Mullard 510 Amplifier	33/9	120 v. 40 mA., 5-0-5 v. 1 a	14/9 9/11
350-0-350 v. 100 mA., 6.3 v4 v., 4 a., c.t., 0-4-5 v. 3 a	26/9		7/11
350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.	33/9	OUTPUT TRANSFORMERS	

	350-0-350 V. 100 High, 0.3 V4 V., 4 a., C.l.,			-1
	0-4-5 v. 3 a	26/9	OUTPUT TRANSFORMERS	
	350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.	33/9	Midget Battery Pentode 66:1 for 3S4, etc.	. 3/6
	350-0-350 v. 150 mA., 6.3 v. 2 a., 6.3 v.	2010	Small Pentode 5,000 $\Omega$ to 3 $\Omega$	3/9
	2 a., 5 v. 3 a	33/9	Standard Pentode, $5,000\Omega$ to $3\Omega$	4/9
	425-0-425 v. 200 mA., 6.3 v. 4 a., c.t.,		Standard Pentode, $8,000\Omega$ to $3\Omega$	4/9
	6.3 v. 4 a. c.t., 5 v. 3 a., suitable		Multi-ratio 40 mA. 30:1, 45:1, 60:1,	417
	Williamson Amplifier, etc	49/9	90:1, Class B Push-Pnll	5/6
	450-0-450 v. 250 mA., 6.3 v. 6 a., 6.3 v.		Push-Pull 8 Watts 6V6 to 5 ohms.	8/9
	6 a., 5. v. 3 a	69/6	Push-Pull 10-12 Watts 6V6 to 3 $\Omega$ or 15 $\Omega$	
	TOP SHROUDED DROP-THROUGH TY			15/9
			Push-Pull 10-12 Watts to match 6V6 to	
	260-0-260 v. 70 mA., 6.3 v. 2 a., 5 v. 2 a.	16/9	3-5-8 or 15Ω	16/9
	350-0-350 v. 80 mA., 6.3 v. 2 a., 5 v. 2 a.	18/9	Push-Pull 15-18 Watts, sectionally wound,	
	250-0-250 v. 100 mA., 6.3 v. 4 a., 5 v. 3 a.	22/9	6L6, KT66, etc., to 3 or 15 ohms	21/9
	300-0-300 v. 100 mA., 6.3 v4 v. 4 a.,		Push-Pull 20 Watt high-quality section-	
	c.t., 0-4-5 v. 3 a	23/9	ally wound, 6L6, KT66, etc., to 3 or $15\Omega$	47/9
1	350-0-350 v. 100 mA., 6.3 v. 4 a., c.t., 5 v.			
ì	3 a	22/9	SMOOTHING CHOKES	
J	350-0-350 v. 100 mA., 6.3 v4 v. 4 a.		250 mA., 5 H., 100 ohms	11/9
ı	c.t., 0-4-5 v. 3 a	23/9	150 mA., 7-10 H., 250 ohms	11/9
J	350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.	29/9	100 mA., 10 H., 200 ohms	8/9
1	E.H.T. TRANSFORMERS, 2,500 v.		80 mA., 10 H., 350 ohms	5/6
ł	5 mA., 2-0-2 v. 1.1 a., 2-0-2 v. 1.1 a.,		60 mA., 10 H., 400 ohms	4/11
ı	for VCR97, VCR517	36/6	1 amp. 0.5 ohm L.T. type	6/6
-		-		310

#### R.S.C. A6 ULTRA AMPLIFIER LINEAR 30 WATT



12-WATT AMPLIFIER



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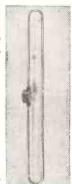
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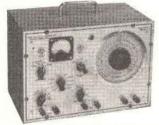
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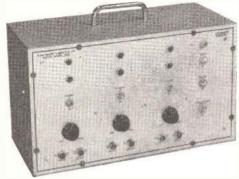
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X66, KTW61, DH63, KT63, U50	35/-	41	
DK96, DF96, DAF96, DL96	32/6	14	
6K8G, 6K7G, 6Q7G, 25A6G, 25Z5 (or 25Z6G)	37/6		
12K8GT, 12K7GT, 12Q7GT, 35Z4GT, 35L6GT (or 50L6GT)	42/6		
128A7GT, 128K7GT, 128Q7GT, 35Z4GT, 35L6GT or 50L6GT	35/-		

#### TRANSMITTER/RECEIVER SCR 522

Comprising the well known BC825 and BC824A. Units complete with 17 valves types 2-892, 3-12A6, 3-123G7, 3-903, 9002, 696G, 1216GT 12AH7GT, 12C3, 6857. The complete unit is in year good condition having very useful parts including Relays, Transformers, Condensers, etc. Less valves 45f-carr. 5f-. With valves £5f15f- carr. 5d.

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(150 MILLIWATTS OUTPUT)
Build this Push-Pull Amplifier which is ideal for Crystal or Magnetic Pick-up Amplification, Baby Alarm, Microphone Amplifier, etc.
Powered by 6-volt Dry Battery lasting for months.
Complete Kit of Farts including 4 Transistors and all Components with Circuit (less speaker), 24/10/~.

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RED-SPOT 800 kc/s Audio Frequency 10/-BLUE-SPOT 1.6 Mc/s Mixer and Frequency Changer 15/-WHITE-SPOT 2.5 Mc/s R.F. and I.F. Amp. ... ... 20/-

All Transistors are Tested and Guaranteed N.B. The Red-Spot is similar to Mullard OC71



#### PRE-SELECTED SEVEN TRANSISTOR PUSH-PULL PORTABLE SUPERHET

Just switch to your favourite Station. No tuning, no aerial or earth. Pre-select 3 stations. Complete with all components and seven Transistors, 7 x 4 Elliptical speaker. Teletron Superhet Coils and I.F.T.'s. Powered by 7½ v. dry battery which lasts for months. 150 Milliwatts output. All the above with Circuits, etc., £9/17/6 carr. paid.

ALL COMPONENTS SOLD SEPARATELY

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Suitable Plastic Cabinet, easy to assemble,

Call and hear demonstration model working



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THREE TRANSISTOR POCKET RADIO
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Pre-selected to receive the Light and Home Stations.
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ROTARY CONVERTERS. Input 24 volt D.C. Output 230 volt A.C. 50 cy, conservatively rated at 100 watts. Brand new in a strong ventilated metal case with switch, input plug and output socket, 105/-. Carr. 7/6.

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TRACER
Complete Kit with 2 Transistors, Components.
Phones with Circut & plastic case.
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Ideal for algrand tracing.
Complete Kit with 2 Transistory, Components, Circuit & plastic class.
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Containing VCB97 with Mu-Mctal Screen.
21 Valves: 12-EF50, 4-8F61, 3-BA50,
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Besistors, Muirhead S/M Dial, Double Deck
Chassis and Crystal.
BRAND NEW.
ORIGINAL CASES. 67/6. Carr. Iree.

#### INDICATOR UNIT TYPE 182A

Unit contains VCR517 Cathode Ray 6in. tube, complete with Mu-Metal screen, 3-EF50, 4-SF61 and 1-5U4G varves, 9 wrewound volume controls and quantity of resistors and condensers. Offered BRAND NEW (less relay) at 67/8. Plus 7/6 carr. "Radio Constructor" 'scope circuit insulated.

B.F.24. 10/-. R.F.25 12/6. R.F.26 25/-. Brand new with valves, carr 2/6

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MU-METAL SCREENS for
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VCR97. Slight-cut-off. Carr.2/3BPL. Brand new £2 0 0 £1 15 0 10 15 £1 10

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Brand new miniature I.F. Strip size 10\$in.x
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 67½ v. Size 2½ x 3½ x 2¾in.
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4-way Push Button Units 2/6 each. Knobs for same 3/- per doz. 5-way Push Button Units 5/6 each, complete with knobs. WEARITE COILS. PA4, PO4, PA5, PO5 1/3 each..... VALVE HOLDERS. Moulded B9A 7/6; B7G 6/-; Int. Oct. 9/-; VALVE HOLDER FITTED WITH LOWER CAN I/6 per doz. extra. Screening cans for B7G and B9A..... Paxolin V/H Int. Oct. B9A, B7G, 5/- per doz.; Eng. Oct., 5-pin, BELLING-LEE PLUGS AND SOCKETS, 5 pin 1/9; 7 pin 2/ 2/6 AIR-SPACED TRIMMERS, 5, 10, 1S, 20, 25, 50; and 75 of pre-set and spindle types 2/- each.. PYE PLUGS AND SOCKETS I/6 per pair, "Tee" pieced...each GROMMETS, I grs. assorted grommets, in. to lin....gross 8/6 POST OFFICE LAMP JACKS No. 10 I/- each.....doz. 9/-Lamp Covers for same......doz. P74 2-pin and sockets are now available 3/6 each. OUTPUT TRANSFORMERS. Multi-ratio 5/- each. WESTECTORS. WX6, WX12, W4 I/- each ......doz. SIGNAL LAMP HOLDERS. Panel mounting, complete with adjusting lampholder 2/- each ......doz.

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100 Microamp	2lin.		MC/FR	50/
250 ,, (multirange scale)	3½in.		MC/FR	55/
500 ,, (scaled 0/15 KV)	2in.		MC/FR plug ty	rpe 18/
1 Milliamp	2in.		MC/FS Elliot 5	Q/87 27/
30 ,,	2lin.		MC/FR	12/
100 ,,	2½in.		MC/FR	12/
20 Amp.	2½in.		MI/FR	25/
25	2lin.		MI/FR DC	7)
50 ,,	5in.		M1/PR	60/
50-0-50 Amp,	2in.		MC/FS	12/
15 Volt	2lin.		MI/FR	15/
20 .,	2in.		MC/FS	10/
40 ,,	2in,		MC/FS	10/
300 ,,	2in.		MC/FS	10/
300 ,,	2∮in.		MI/FR	25/
300 ,,	5in.		MI/PR	60/
CROSS POINTER METERS.		eparate	100 microamp	movements
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PORTABLE BLOWERS 200/250 v. AC/DC 300 watts with switch and lead

PORTABLE BLOWERS 200/250 v. AC/DC 300 watts with switch and lead 1½in. outlet 25, carr..7/6.

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mouth to ear, 18/-. Two pairs each complete with cord, plug and socke 27/6.

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BATTERY CHARGERS. Output up to 22 v. 10 amps., controlled by two 4-position rotary switches for fine and coarse control. Input 200/250 v. A.C. 50 cy., fused for A.C. and D.C., clear scaled ammeter. Brand new made by S.T.C. 217/10/-. Carr. 15/-.

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604 7/-	12SG7 7/6	KTW63 8/6 KTZ41 6/- LP220 5/-	WEARIT
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604	12SG7 7/6 12SH7 5/6 12SJ7 8/- 12SK7 6/-	KTZ41 6/- LP220 5/- MH4 7/6 MH41 7/- N37 13/-	WEARIT Wearite "P" coils 3/- each. VR53(EF39) 6/6
604	128G7 7/6 128H7 5/6 128J7 8/- 128K7 6/- 128L7 7/6 128G7 8/6 128B7 7/6	KTZ41 6/- LP220 5/- MH4 7/6 MH41 7/- N37 13/- N78 12/6	WEARIT Wearite "P" coils 3/- each.  VR53(EF39) 6/6 VR54(EB34) 2/-
6BW7 10/- 6C4 7/- 6C5GT 6/6 6C6 5/-1 6C9 10/6 6D6 5/- 6F6G 7/6 6F6M 7/6	128G7 7/6 128H7 5/6 128H7 8/- 128K7 6/- 128L7 7/6 128Q7 8/6 128R7 7/6 1487 13/6	KTZ41 6/- LP220 5/- MH4 7/6 MH41 7/- N37 13/- N78 12/6 P61 3/9	WEARIT Wearite "P" coils 3/- each.  VR53(EF39) 6/6 VR54(EB34) 2/- VR55(EB633)
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\$BW7 10/- 6C4 7/- 6C5GT 6/6 6C6 5/-1 6C9 10/6 6D8 5/- 6F6G 7/6 8F6M 7/6 6F13 14/- 6F15 14/-	128G7 7/6 128H7 5/6 128J7 8/- 128K7 6/- 128K7 7/6 128G7 8/6 128G7 7/6 1487 13/6 15D2 7/9 20L1 12/6	KTZ41 6/- LF220 5/- MH4 7/6 MH41 7/- N37 13/- N78 12/6 PUI 3/9 P215 3/11 PENA4 15/-	WEARIT Wearite "P" coils 3/- each.  VR53(EF39) 6/6 VR54(EB34) 2/- VR55(EB053) 7/6
\$BW7 10/- 6C4 7/- 6C5GT 6/6 6C6 5/-1 6C9 10/6 6D6 5/-6F6G 7/6 6F6M 7/6 6F13 14/- 6F15 14/- 6G6G 4/6	128G7 7/6 128H7 5/6 128H7 8/- 128K7 6/- 128L7 7/6 128Q7 8/6 128R7 7/6 1487 13/6 16D2 7/9 20L1 12/6 20P5 11/6	KTZ41 6/- LP220 5/- MH4 7/6 MH41 7/- N37 13/- N78 12/6 PSI 3/9 P215 3/11 PENA4 15/- PEN26 5/- PEN26 7/-	WEARIT Wearite " P " coils 3/- each.  VR53(EF39) 6/6 VR54(EB34) 2/- VR55(EB053) 7/6 VR56(EF36) 6/- VR57(EK32) 8/- VR55(F861) 3/-
9BW7 10/- 604 7/- 6056T 6/6 606 5/- 609 10/6 609 10/6 676G 7/6 676M 7/6 6713 14/- 6715 14/- 6606 4/6 6H6 2/6	12807 7/6 12817 5/6 12817 8/- 12817 7/6 12817 7/6 12817 7/6 12817 7/6 12817 7/6 12817 7/6 12817 7/9 1487 13/6 1487 11/6 20P5 11/6 20F5 11/6	KTZ41 6/- LP220 5/- MH4 7/6 MH41 7/- N37 13/- N78 12/6 P41 3/9 P215 3/11 PENA4 15/- PENA5 5/- PENA6 7/- PENA6 7/- PFEN220 4/-	WEARIT Wearite "P" coils 3/- each.  VR53(EF39) 6/6 VR54(EB34) 2/- VR55(EB053) 7/6
\$\text{9BW7}\$ 10/- 6C4 7/- 6C56T 6/8 6C6 5/- 6C9 10/6 6D6 5/- 6F6G 7/8 6F13 14/- 6F15 14/- 6G6 4/6 6H6 2/6 815G 5/-	128G7 7/6 128H7 5/6 128H7 8/- 128K7 6/- 128K7 7/6 128G7 8/6 128E7 7/6 128G7 13/6 15D2 7/9 20L1 12/6 20P5 11/6 25U6GT 9/6	KTZ41 6/- LP220 5/- MH4 7/6 MH4 7/6 MH41 7/- N37 13/- N78 12/6 P41 3/9 P215 3/11 PENA4 15/- PEN26 5/- PEN26 7/- PEN20A 4/- PCC84 10/-	WEARIT Wearite "P" cols 3/- each. VR53(EF39) 6/6 VR54(EB34) 2/- VR55(EB053) 7/6 VR56(EF36) 6/- VR56(EF36) 3/- VR65(SF61) 3/- VR65(SP61) 3/- VR65(P61) 3/9
BW7 10/- 6C4 7/- 6C5GT 6/6 6C6 5/- 6C9 10/6 6D6 5/- 6F6G 7/6 6F6M 7/6 6F13 14/- 6G6G 4/6 6J56T 5/6 6J56T 5/6	12807 7/6 12817 5/6 12817 8/- 128K7 6/- 128K7 7/6 12807 7/6 12907 8/6 12987 7/6 1487 13/6 1497 12/8 2011 12/8 2015 11/8 25166T 9/6 25165 9/6	KTZ41 6/- LF220 5/- MH4 7/6 MH41 7/- N37 13/- N78 12/6 P01 3/0 P216 3/11 PENA4 15/- PEN26 5/- PEN46 7/- PEN290 4/- PCC84 10/-	WEARIT Wearite "P" coils 3/- each. VR53(EF39) 6/6 VR54(EB34) 2/- VR55(EB057)/6 VR56(EF36) 6/- VR57(EK32) 8/- VR65(F61) 3/- VR65(P61) 3/- VR66(P61) 3/- VR66(P61) 5/0 VR91(EF50) 4/-
,BBW7 10/- 6C4 7/- 6C5GT 6/6 6C6 5/-/ 6C9 10/6 6D6 5/- 6F6G 7/6 6F6M 7/6 6F15 14/- 6G0G 4/6 6H6 2/6 6J5G 5/- 6J5GT 5/6 6J5GT 5/6 6J5M 6/6	128G7 7/6 128H7 5/6 128H7 8/- 128K7 8/- 128K7 7/6 128G7 7/6 128G7 7/6 128G7 7/6 129B7 13/6 15D2 7/9 20L1 12/6 20P5 11/6 25Y6 9/6 25Y6 9/6 25Y6 9/9	KTZ41 6/- LF220 5/- MH4 7/6 MH4 7/6 MH41 7/- N37 13/- N78 12/6 P61 3/9 P216 3/11 PENA4 15/- PEN26 5/- PEN46 7/- PEN204 4/- PCG84 10/- PCF80 11/- PCF82 12/6	WEARIT Wearite "P" colls 3/- each. VESS(EF39) 6/6 VR54(EB34) 2/- VR55(EB605) 7/6 VR55(EF305) 8/- VR55(EF305) 3/- VR55(EF30) 3/
\$\\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\	128G7 7/6 128H7 5/6 128H7 8/- 128K7 8/- 128K7 6/- 128Q7 8/6 128B7 7/6 128B7 7/6 1487 13/6 15D2 7/9 20L1 12/6 20P5 11/6 2514G 9/9 2554G 9/9 2554G 9/-	KTZ41 6/- LF220 5/- MH4 7/6 MH4 7/6 MH41 7/- N37 13/- N78 12/6 P61 3/9 P216 3/11 PENA4 15/- PEN26 5/- PEN46 7/- PEN204 4/- PCG84 10/- PCF80 11/- PCF82 12/6	WEARIT Wearite "P" colla 3/- each. VR53(EF39) 6/6 VR54(EB34) 2/- VR55(EB605 7/6 8/- VR55(EB605 7/6 8/- VR55(EK50) 3/- VR55(EK5
,BBW7 10/- 6C4 7/- 6C5GT 6/6 6C9 10/6 6C9 10/6 6D6 5/- 6F6G 7/6 8F6M 7/6 6F13 14/- 6G96 4/6 6H6 2/6 8J5G 5/- 6J5GT 5/6 8J6M 6/6 6J6 6/-	12807 7/6 12817 5/6 12817 8/- 12817 8/- 12817 7/6 12807 8/6 12807 7/6 1487 13/6 15D2 7/9 2011 12/6 20P6 11/6 251660T 9/6 2575 9/6 2575 9/6 2575 9/6 2575 9/-	KTZ41 6/- LF220 5/- MH4 7/6 MH4 7/6 MH41 7/- N37 13/- N78 12/6 P41 3/9 P216 3/11 PENA4 15/- PEN26 5/- PEN46 7/- PEN204 4/- PCG84 10/- PCF80 11/- PCF80 11/- PCF82 12/6 PL82 10/- PL83 12/6	WEARIT Wearite "P" colla 3/- each. VR53(EF39) 6/6 VR54(EB34) 2/- VR55(EB605 7/6 8/- VR55(EB605 7/6 8/- VR55(EK50) 3/- VR55(EK5
### 10/- 604 7/- 6050T 6/6 6050T 6/6 606 5/- 609 10/6 6D8 5/- 6F6G 7/6 6F13 14/- 6G6G 4/6 6H6 2/6 6J5G 5/- 6J5GT 5/6 6J5M 6/6 6J6 6/- 6J7G 6/- 6J7G 6/-	128G7 7/6 128H7 5/6 128H7 8/- 128K7 8/- 128K7 7/6 128G7 8/6 128R7 7/6 128G7 13/6 1487 13/6 15D2 7/9 20L1 12/6 20P5 11/6 25Y5 9/6 25Y5 9/6 25Y5 9/6 25Y5 9/- 25Z5 9/- 25Z5GT 9/6	KTZ41 6/- LF220 5/- MH4 7/6 MH41 7/- N37 13/- N78 12/6 P61 3/0 P216 3/11 PENA4 15/- PEN26 5/- PEN46 7/- PEN220 4/- PCG84 10/- PCF89 11/- PCF82 12/6 PLS3 12/6 PLS3 12/6 PLS3 17/- PP23 17/-	WEARIT Wearite "P" colla 3/- each. VR53(EF39) 6/6 VR54(EB34) 2/- VR55(EB05) 6/- VR55(EF26) 6/- VR57(EK32) 8/- VR55(ASP1) 3/- VR65(P61) 3/- VR56(P61) 3/- VR51(EF56) 4/-
	128G7 7/6 128H7 5/6 128H7 8/- 128K7 6/- 128K7 6/- 128K7 7/6 128K7 7/6 128K7 7/6 128K7 7/6 1487 13/6 18D2 7/9 20L1 12/6 20P5 11/6 25Y55 9/6 25Y55 9/6 25Y55 9/9 25Z4G 9/- 25Z3GT 9/6 35L6GT 9/6 35L4G 9/- 35L6GT 9/6 35L4G 9/-	KTZ41 6/- LF220 5/- MH4 7/6 MH41 7/- N37 13/- N78 12/6 P61 3/0 P216 3/11 PENA4 15/- PEN26 5/- PEN46 7/- PEN220 4/- PCG84 10/- PCF89 11/- PCF82 12/6 PLS3 12/6 PLS3 12/6 PLS3 17/- PP23 17/-	WEARIT Wearite "P" colla 3/- each. VR53(EF39) 6/6 VR54(EB34) 2/- VR55(EB05) 6/- VR55(EF26) 6/- VR57(EK32) 8/- VR55(ASP1) 3/- VR65(P61) 3/- VR56(P61) 3/- VR51(EF56) 4/-
\$\text{9BW7}\$ 10/-\$ 6C4 7/-\$ 6C5GT 6/6 6C6 5/-1\$ 6C9 10/6 6D6 5/-\$ 6F6G 7/6 6F6M 7/6 6F15 14/-\$ 6G0G 4/6 6H6 2/6 6H6 2/6 6J5G 5/-\$ 6J5G 5/-\$ 6J5G 5/-\$ 6J5G 6/-\$ 6J6 6/-\$ 6J7G 6/-\$ 6K7M 6/6 6K7M 6/6	128G7 7/6 128H7 5/6 128H7 8/- 128K7 6/- 128K7 6/- 128K7 7/6 128C7 8/6 128E7 7/6 1487 13/6 18D2 7/9 20L1 12/6 20P5 11/6 25Y55 9/6 25Y56 9/9 25E4G 9/- 25Z5GT 9/6 35L6GT 9/6 35U4 9/- 35Z4GT 8/6	KTZ41 6/- LF220 5/- MH4 7/6 MH4 7/6 MH41 7/- N37 13/- N78 12/6 P41 3/9 P216 3/11 PENA4 15/- PEN26 5/- PEN46 7/- PEN204 4/- PCC84 10/- PCF80 11/- PCF82 12/6 PL82 10/- PCL83 12/6 PL82 10/- PCL83 12/- PCL83 12/- PCL83 12/- PCL83 12/- PCL83 12/- PCL83 12/- PCS60 10/- PY81 10/-	WEARIT Wearite "P" colla 3/- each. VR53(EF39) 6/6 VR54(EB34) 2/- VR55(EB05) 6/- VR55(EF26) 6/- VR57(EK32) 8/- VR55(ASP1) 3/- VR65(P61) 3/- VR56(P61) 3/- VR51(EF56) 4/-
BW7 10/- 6C4 7/- 6C5GT 6/6 6C6 5/-] 6C9 10/6 6C9 10/6 6F6G 7/6 8F6M 7/6 8F13 14/- 8F13 14/- 8G6G 4/6 8J5G 5/- 6J5GT 5/6 8J5M 6/6 8J6M 6/6 8J6M 7/- 6K8G 7/- 6K7G 5/9 6K7M 6/9	128G7 7/6 128H7 5/6 128H7 8/6 128H7 8/7 128K7 6/- 128L7 7/6 128G7 8/6 129G7 8/6 129B2 7/9 20L1 12/6 20F5 11/6 25T6 9/6 25T6 9/6 25T6 9/9 25LGGT 9/6 35LGGT 9/6 35LGGT 9/8 35LGGT 9/8 35LGGT 9/8 35LGGT 8/6 35U4 9/- 35ZGGT 8/6	KTZ41 6/- LF220 5/- MH4 7/6 MH41 7/- N37 13/- N78 12/6 P91 3/9 P216 3/11 PENA4 15/- PEN45 5/- PEN46 7/- PEN26 5/- PEN46 7/- PCF80 11/- PCF80 11/- PCF80 11/- PCF80 12/6 PL82 10/- PL83 13/11 PCS 12/6 PL83 12/- PCS 3/11 PCS 3/11 PCS 15/- PC	WEARIT Wearite "P" colla 3/- each. VR53(EF39) 6/6 VR54(EB34) 2/- VR55(EB05) 6/6 VR55(EF26) 6/- VR55(EB05) 3/- VR56(EF36) 3/- VR56(EF36) 3/- VR56(EF36) 3/- VR51(EF39) 3/9 VR51(EF59) 3/9 V
\$\text{9BW7}\$ 10/-\$ 6C4 7/-\$ 6C5GT 6/6 6C6 5/-1\$ 6C9 10/6 6D6 5/-\$ 6F6G 7/6 6F6G 7/6 6F15 14/-\$ 6G0G 4/6 6H6 2/6 6H6 2/6 6H6 5/-\$ 6J5G 5/-\$ 6J5G 5/-\$ 6J5G 6/-\$ 6J6 6/-\$ 6J7G 6/-\$ 6K7G 5/9 6K7G 6/9	12807 7/6 12817 5/6 12817 8/- 12817 7/6 12817 7/6 12807 8/6 12817 7/6 12807 13/6 12917 13/6 12917 13/6 12915 11/6 2011 12/6 2015 11/6 2016 11/6 2575 9/6 2576 9/9 25760 9/9	KTZ41 6/- LF220 5/- MH4 7/6 MH41 7/- N37 13/- N78 12/6 P91 3/9 P216 3/11 PENA4 15/- PEN45 5/- PEN46 7/- PEN26 5/- PEN46 7/- PCF80 11/- PCF80 11/- PCF80 11/- PCF80 12/6 PL82 10/- PL83 13/11 PCS 12/6 PL83 12/- PCS 3/11 PCS 3/11 PCS 15/- PC	WEARIT Wearite "P" coils 3/- each. VR53(EP39) 6/6 VR54(EB34) 2/- VR55(EBC53) 7/6 VR55(EBC53) 3/9 VR55(EBC1) 3/9 VR55(EP1) 3/9 VR55(EP1) 3/9 VR55(EP1) 3/9 VR55(EP1) 3/9 VR55(EP1) 3/9 VR51(EP1) 3/9 VR
	12807 7/6 12817 5/6 12817 8/- 12817 8/- 12817 7/6 12807 8/6 12807 7/6 1487 13/6 15D2 7/9 2011 12/6 20P6 11/6 25V5 9/6 25V5 9/6 25V5 9/6 25V5 9/6 35L6GT 9/6 35L6GT 9/6 35L6GT 8/6 ACG/FEN 8/6 ACG/FEN 6/6 ACG/FEN 6/6 ACG/FEN 6/6 ACG/FEN 6/6	KTZ41 6/- LF220 5/- MH4 7/6 MH41 7/- N37 13/- N37 13/- N38 12/6 P01 3/19 P216 3/11 PENA4 15/- PEN26 5/- PEN26 7/- PEN20A 4/- PCG84 10/- PCF80 11/- PCF82 12/6 PCL83 12/6 PCL84 12/6 PCL85 13/11 PCCL85 13/11 PCCCL85 13/11 PCCCL85 13/11 PCCCL85 13/11 PCCCL85 13/11 PCCCL85 13/11 PCCCC	WEARIT Wearite "P" coils 3/- each. VR53(EP39) 6/6 VR54(EB34) 2/- VR55(EBC53) 7/6 VR55(EBC53) 3/9 VR55(EBC1) 3/9 VR55(EP1) 3/9 VR65(EP1) 3/9 VR65(EP1) 3/9 VR65(EP1) 3/9 VR91(EP50) 4/- VR116 - 4/- VR115 - 4/- VR116 - 4/- VR1
## 10/- ## 10/	128G7 7/6 128H7 5/6 128H7 8/- 128K7 8/- 128K7 8/- 128K7 7/6 128G7 8/6 128E7 7/8 128E7 7/8 15D2 7/9 20L1 12/6 20P5 11/6 25Y6 9/8 25Y6 9/8 25Y6 9/8 25Y6 9/8 25Y6 9/8 25Y6 9/8 35L6GT 9/6 35L6GT 8/6 35L6GT 9/6 35L	KTZ41 6/- LF220 5/- MH4 7/6 MH41 7/- N37 13/- N78 12/6 P91 3/9 P216 3/11 PENA4 15/- PEN46 7/- PEN46 7/- PEN82 10/- PCF80 11/- PCF80 11/- PCF82 12/6 PL82 10/- PL83 12/- PL83 12/- PC285 3/11 PY80 10/- PY81 10/- PY83 10/- PY81 10	WEARIT Wearite "P" colla 3/- each. VR53(EF39) 6/6 VR54(EB34) 2/- VR55(EB05) 6/- VR56(EF36) 6/- VR57(EK32) 8/- VR56(EF36) 3/- VR65(EF36) 3/- VR65(EF36) 4/- VR91(EF50) 4/- V
,BBW7 10/- 6C4 7/- 6C5GT 6/6 6C9 10/6 6C9 10/6 6F6G 7/6 6F6M 7/6 6F13 14/- 6G6G 4/6 6J5G 5/- 6J5G 5/- 6J5G 5/- 6J5G 6/- 6J5G 7/- 6K7G 7/- 6K7G 7/- 6K7G 7/- 6K8G 7/- 6K8G 7/- 6K8G 7/- 6K8G 7/- 6K6G 7/- 6K6G 7/- 6K6G 7/- 6K6G 7/- 6K7M 6/9 6K8G 8/9 6K8G 8/9 6K8G 8/9 6K8G 9/- 6K8G 9/- 6K6G 7/- 6K7G 7/- 6K7G 7/- 6K7G 7/- 6K7G 7/- 6K7G 7/- 6K7G 7/-	128G7 7/6 128H7 5/6 128H7 8/- 128K7 6/- 128K7 6/- 128K7 7/6 128C7 8/6 128E7 7/6 1487 13/6 18D2 7/9 20L1 12/6 20P5 11/6 25Y55 9/6 25Y55 9/6 25Y55 9/- 25Z6GT 9/6 35L6GT 9/6 35L6GT 9/6 35L6GT 8/6 35W4 9/- 35Z6GT 8/6 35L6GT 8/6 ACG/PEN 8/6 ACG/PEN 8/6 ACG/PEN 8/6 ACG/PEN 8/6 ACG/PEN 6/6 ACG/PEN 6/	KTZ41 6/- LF220 5/- MH4 7/6 MH41 7/- N37 13/- N78 12/6 P91 3/9 P216 3/11 PENA4 15/- PEN45 5/- PEN46 7/- PEN46 7/- PCF80 11/- PCF80 11/- PCF80 11/- PCF80 12/6 PL82 10/- PCS0 3/11 PCS0 3/11 PCS0 15/- PY01 10/- PY02 12/6 PCS0 15/- PY01 10/- PY02 12/6 PCS0 15/- PY01 10/- PY03 12/- PY04 10/- PY05 3/11 H04 10/- U22 8/-	WEARIT Wearite "P" colls 3/- each.  VR53(EF29) 6/6 VR54(EB34) 2/- VR55(EB053) 7/6 VR55(EB053) 7/6 VR55(EB053) 7/6 VR55(EF21) 3/- VR55(EF21) 3/- VR55(EF21) 3/- VR55(EF21) 3/- VR55(EF21) 3/- VR56(F51) 3/- VR51(EF50) 4/- VR116 4/- VR136 6/6 VR516 4/- VR136 5/6 VR516 3/- VR156(F51) 5/6 VR156 3/- VR156(F51) 5/6 VR156 3/- VR156(F51) 5/6 VR516 3/- VR156(F51) 5/6 VR516 3/- VR516 3/- S/- VR516 3/- VR516 3/- S/- S/- S/- S/- S/- S/- S/- S/- S/- S
\$\text{9BW7}\$ 10/-\$ 6C4 7/-\$ 6C5QT 6/8 6C6 5/-1\$ 6C9 10/6 6D6 5/-\$ 6F6G 7/6 6F6G 7/6 6F15 14/-\$ 6G0G 4/6 6H6 2/6 6J5G 5/-\$ 6J5G 5/-\$ 6J5G 6/-\$ 6J6 6/-\$ 6J7G 6/-\$ 6K7M 6/9 6K8G 7/-\$ 6K8G 7/-\$ 6K8G 7/-\$ 6K8G 8/9 6K8G 8/9 6K8G 8/9 6K8G 9/-\$ 6L6 9/-\$ 6K77 7/-\$ 6Q7GT 9/-\$ 6R7 9/-\$ 6K4	12807 7/6 12817 5/6 12817 8/- 12817 8/- 12817 7/6 12807 8/6 12827 7/6 1487 13/6 15D2 7/9 20L1 12/6 20P6 11/6 25166T 9/6 25166 9/9 25786 9/9 25786 9/9 25786 9/6 35167 9/6 35467 9/6 35467 9/6 35467 9/6 35467 9/6 35467 9/6 35474 3/6 AC6/PEN 8/8 AC6/	KTZ41 6/- LF220 5/- MH4 7/6 MH41 7/- N37 13/- N78 12/6 P91 3/9 P216 3/11 PENA4 15/- PEN45 5/- PEN46 7/- PEN46 7/- PCF80 11/- PCF80 11/- PCF80 11/- PCF80 12/6 PL82 10/- PCS0 3/11 PCS0 3/11 PCS0 15/- PY01 10/- PY02 12/6 PCS0 15/- PY01 10/- PY02 12/6 PCS0 15/- PY01 10/- PY03 12/- PY04 10/- PY05 3/11 H04 10/- U22 8/-	WEARIT Wearite "P" coils 3/- each VR53(EF39) 6/6 VR54(EB34) 2/- VR55(EB05) 6/- VR56(EF36) 6/- VR57(EK32) 8/- VR56(EF36) 3/- VR56(EF36) 3/- VR56(EF36) 4/- VR51(EF56) 4/- VR51(EF36) 4/- VR
BW7 10/- 6C4 7/- 6C5GT 6/6 6C9 10/6 6C9 10/6 6C9 10/6 6F6G 7/6 8F6M 7/6 8F13 14/- 8F15 14/- 8G6G 4/6 8J5G 5/- 6J5GT 5/6 8J5M 6/6 8J5M 6/6 8J6M 7/6 8J6M 8/- 6K7G 7/- 6K7G 9/- 6K7G 9/- 6K7G 9/- 6K7G 9/- 6K7G 7/- 6K7 7/- 6K7 7/- 6K7 9/-	128G7 7/6 128H7 5/6 128H7 8/6 128H7 6/- 128K7 6/- 128K7 7/6 128G7 8/6 129G7 8/6 129B2 7/9 20L1 12/6 20F5 11/6 25F5 9/6 25F6 9/9 25L6GT 9/6 35L6GT 9/6 35L6GT 9/6 35L6GT 8/6 35E3 9/- 25Z6GT 8/6 35E3 9/- 25Z6GT 8/6 35E3 9/- 25Z6GT 8/6 35E44 9/- 35Z6GT 8/6 35E44 9/- 35Z6GT 8/6 35E44 9/- 35Z6GT 8/6 35E44 9/- 36Z6GT 8/6 35E44 3/6 36Z6T 8/6 35E45 9/- 36Z6GT 8/6 35E44 3/6 35E45 9/- 36Z6GT 8/6 35E46 10/6 3	KTZ41 6/- LF220 5/- MH4 7/6 MH41 7/- N37 13/- N78 12/6 P91 3/9 P215 3/11 PENA4 15/- PEN45 5/- PEN46 7/- PEN46 7/- PEN46 7/- PEN52 12/6 PCF80 11/- PCF80 11	WEARIT Wearite "P" coils 3/- each. VR53(EF39) 6/6 VR54(EB34) 2/- VR55(EB05) 6/- VR56(EF36) 6/- VR57(EK32) 8/- VR56(EF36) 3/- VR65(EF36) 3/- VR65(EF36) 4/- VR91(EF56) 4/- VR91(EF50) 5/- VR91(EF50) 5/- VR91(EF50) 5/- VR91(EF50) 5/- VR91(EF50) 4/- VR91(EF50) 5/- VR91(EF50) 4/- VR91(EF50) 5/- VR91(EF50) 4/- V
\$\text{9BW7}\$ 10/-\$ 6C4 7/-\$ 6C5GT 6/6\$ 6C9 10/6\$ 6D6 5/-\$ 6F6G 7/6\$ 6F6B 7/6\$ 6F13 14/-\$ 6G91 14/-\$ 6G6 4/6\$ 6J5G 5/-\$ 6J5GT 5/6\$ 6J5GT 5/6\$ 6J6 6/-\$ 6J7G 6/-\$ 6K7G 7/-\$ 6K7G 7/-\$ 6K7G 7/-\$ 6K7G 7/-\$ 6K8G 7/-\$ 6K8G 7/-\$ 6K8G 7/-\$ 6K8G 7/-\$ 6K8G 7/-\$ 6K8GT 9/6\$ 6L6G 9/-\$ 6L7 7/6\$ 6N7 7/-\$ 6Q7GT 9/-\$ 6SA7GT 8/-\$ 6SG7 7/6\$	128G7 7/6 128H7 5/6 128H7 8/6 128H7 6/- 128K7 6/- 128K7 7/6 128G7 8/6 129G7 8/6 129B2 7/9 20L1 12/6 20F5 11/6 25F5 9/6 25F6 9/9 25L6GT 9/6 35L6GT 9/6 35L6GT 9/6 35L6GT 8/6 35E3 9/- 25Z6GT 8/6 35E3 9/- 25Z6GT 8/6 35E3 9/- 25Z6GT 8/6 35E44 9/- 35Z6GT 8/6 35E44 9/- 35Z6GT 8/6 35E44 9/- 35Z6GT 8/6 35E44 9/- 36Z6GT 8/6 35E44 3/6 36Z6T 8/6 35E45 9/- 36Z6GT 8/6 35E44 3/6 35E45 9/- 36Z6GT 8/6 35E46 10/6 3	KTZ41 6/- LF220 5/- MH4 7/6 MH41 7/- MH41 7/- N37 13/- N78 12/6 P91 3/9 P216 3/11 PENA4 15/- PEN25 5/- PEN26 7/- PEN20A 4/- PEN20A 4/- PCF80 11/- PCF81 10/- PT82 9/- PT83 12/- PT83 1	WEARIT Wearite "P" coils 3/- each. VR53(EF39) 6/6 VR54(EB34) 2/- VR55(EB05) 6/- VR56(EF36) 6/- VR57(EK32) 8/- VR56(EF36) 3/- VR65(EF36) 3/- VR65(EF36) 4/- VR91(EF56) 4/- VR91(EF50) 5/- VR91(EF50) 5/- VR91(EF50) 5/- VR91(EF50) 5/- VR91(EF50) 4/- VR91(EF50) 5/- VR91(EF50) 4/- VR91(EF50) 5/- VR91(EF50) 4/- V
BW7 10/- 6C4 7/- 6C5GT 6/6 6C6 5/-] 6C9 10/6 6D8 5/- 6F6G 7/6 6F6M 7/6 6F13 14/- 6G6G 4/6 6J5GT 5/- 6J5G 5/- 6J5G 5/- 6J5G 5/- 6J5G 6/- 6J5GT 5/- 6J6 6/- 6J7G 6/- 6K7G 7/- 6K7G 7/- 6K7G 7/- 6K7G 7/- 6K7G 7/- 6K7G 9/- 6K7 7/- 6K7 7/- 6K7 7/- 6K7 7/- 6K7 9/- 6K7 7/-	12807 7/6 12817 5/6 12817 8/- 12817 8/- 12817 7/6 12827 7/6 12827 7/6 12827 7/6 1487 13/6 1487 13/6 2075 11/6 2075 11/6 2075 9/6 2575 9/6 2576 9/9 2526GT 9/6 3516GT 8/6 3525 9/- 2526GT 9/6 3516GT 9/6 3516GT 8/6 3525 9/- 5016GT 8/6 3527 9/- 5016GT 8/6 3527 10/6	KTZ41 6/- LF220 5/- MH4 7/6 MH41 7/- MH41 7/- N57 13/- N78 12/6 P91 3/9 P216 3/11 PENA4 15/- PEN26 5/- PEN26 5/- PEN26 5/- PEN26 10/- PCF80 11/- PCF80 11/- PCF80 11/- PCF80 11/- PCF80 11/- PCF80 11/- PCF80 3/11 PCF80 3/11 PX25 15/- PY80 10/- PY81 10/- PY81 10/- PY81 10/- PY82 9/- PY83 12/- PY83 12/- PY83 12/- PY80 10/- PY81 10/- PY81 10/- PY81 10/- PY82 9/- PY83 12/- PY80 11/- PY80 11/- PY81 10/- PY81 10/- PY81 10/- PY81 10/- PY82 11/- PY83 12/- PY80 11/- PY81 10/- PY81 10/- PY81 10/- PY81 10/- PY81 10/- PY82 11/- PY83 12/- PY80 11/- PY81 10/-	WEARIT Wearite "P" colla 3/- each. VR53(EF39) 6/6 VR54(EB34) 2/- VR55(EB67) 6/- VR55(EB67) 6/- VR55(EF36) 6/- VR55(EF36) 8/- VR51(EF56) 8/- VR156 6/- VR136
BW7 10/- 6C4 7/- 6C5GT 6/6 6C6 5/- 6C9 10/6 6D8 5/- 6F6G 7/6 6F6M 7/6 6F13 14/- 6G6G 4/6 6J5G 5/- 6J6G 5/- 6J5G 5/- 6J5G 5/- 6J5G 6/- 6J5G 7/- 6K7G 7/- 6K7G 7/- 6K7G 7/- 6K8G 7/- 6K8G 7/- 6K6G 7/- 6K7G 9/- 6K8G 9/- 6K8G 9/- 6K8G 7/- 6K7M 6/9 6K8G 7/- 6K7G 7/- 6K7G 7/- 6K8T 9/- 6K8G 7/-	12807 7/6 12817 5/6 12817 8/- 12817 8/- 12817 7/6 12827 7/6 12827 7/6 1487 13/6 15D2 7/9 2011 12/6 20P6 11/6 25V5 9/6 25V5 9/6 25V5 9/6 25V5 9/6 25V5 9/6 35L6GT 9/6 35L6GT 9/6 35L6GT 8/6 3523 9/- 35Z6GT 8/6 35Z3 9/- 35Z6GT 8/6 35Z3 9/- 35Z6GT 8/6 35Z3 10/6 35Z6GT 8/6 35Z6GT 10/6 35Z6GT 8/6 35Z6GT 10/6 35Z6GT 8/6 35Z6GT 10/6 35Z6GT 8/6 35Z6GT 8/6 35Z6GT 10/6 35Z6GT 8/6 37Z6GT 8/6 37Z6GT 8/6 37Z6GT 8/6 37Z6GT 8/6 37Z6GT 8/6 37Z6GT 8/6 37Z6G	KTZ41 6/- LF220 5/- MH4 7/6 MH41 7/- N37 13/- N78 12/6 P91 3/9 P215 3/11 PENA4 15/- PEN46 7/- FEN46 7/- FEN520 12/6 FEN520 12/6 FL83 10/- FUF83 12/6 FUF83 11/- FUF83 12/-	WEARIT Wearite "P" colls 3/- each VR54(EB34) 6/5 VR54(EB34) 6/5 VR54(EB34) 6/6 VR16 6/6 VR16 4/- VR136 6/6 VR16 4/- VR136 6/6 VR16 4/- VR137 5/6 VR16 4/- VR17 8/6 VR16 4/- VR17 8/6
\$\text{9BW7} \ 1.0\footnote{10}\$ \$\tag{6C4} \ 7\footnote{10}\$ \$\tag{6C5} \ 6\footnote{10}\$ \$\tag{6C6} \ 5\footnote{10}\$ \$\tag{6C6} \ 7\footnote{10}\$ \$\tag{6C6} \ 7\footnote{10}\$ \$\tag{6F6G} \ 7\footnote{10}\$ \$\tag{6F6G} \ 7\footnote{10}\$ \$\tag{6F6G} \ 7\footnote{10}\$ \$\tag{6F15} \ 14\footnote{10}\$ \$\tag{6H6} \ 2\footnote{10}\$ \$\tag{6H6} \ 2\footnote{10}\$ \$\tag{6H6} \ 2\footnote{10}\$ \$\tag{6H6} \ 2\footnote{10}\$ \$\tag{6H6} \ 3\footnote{10}\$ \$\tag{6H7} \ 6\footnote{10}\$ \$\tag{6K7G} \ 6\footnote{10}\$ \$\tag{6K3G} \ 7\footnote{10}\$ \$\tag{6K3G} \ 7\footnote{10}\$ \$\tag{6K3G} \ 7\footnote{10}\$ \$\tag{6K3G} \ 7\footnote{10}\$ \$\tag{6K7} \ 7\footnote{10}\$ \$\tag{6K7} \ 7\footnote{10}\$ \$\tag{6K7} \ 7\footnote{10}\$ \$\tag{6SH7} \ 7\footnote{10}\$ \$\tag{6SH7} \ 6\footnote{10}\$ \$\tag{6SH7} \ 6\	12807 7/6 12817 5/6 12817 8/- 12817 8/- 12817 7/6 12807 8/6 12807 8/6 12807 7/6 1487 13/6 15D2 7/9 20L1 12/6 20P6 11/6 25166T 9/6 25166 9/9 25766 9/9 25766 9/9 25767 9/6 35166T 9/6 35166 10/6 DE96 10/6 DE	KTZ41 6/- LF220 5/- MH4 7/6 MH41 7/- MH41 7/- N57 13/- N78 12/6 P91 3/9 P216 3/11 PENA4 15/- PEN26 5/- PEN26 5/- PEN26 10/- PCF80 11/- PCF80 11	WEARIT Wearite "P" colls 3/- each VR54(EB34) 6/5 VR54(EB34) 6/5 VR54(EB34) 6/6 VR16 6/6 VR16 4/- VR136 6/6 VR16 4/- VR136 6/6 VR16 4/- VR137 5/6 VR16 4/- VR17 8/6 VR16 4/- VR17 8/6
## 10/- ## 10/	12807 7/6 12817 5/6 12817 8/- 12817 8/- 12817 7/6 12827 8/6 12827 8/6 12827 7/6 1487 13/6 15D2 7/9 2011 12/6 2075 11/6 2575 9/6 2575 9/6 2575 9/- 25Z6GT 9/6 25Z6GT 9/6 35L6GT 9/6 35L6GT 9/6 35L6GT 9/6 35L6GT 9/6 35L6GT 8/6 35L6GT 9/6 35L6GT 9	KTZ41 6/- LF220 5/- MH4 7/6 MH41 7/- MH41 7/- N37 13/- N78 12/6 F91 3/9 P216 3/11 PENA4 5/- PENA6 5/- PENA6 6/- PENA6 7/- PENA20 10/- PCF80 11/- PCF80 11/- PCF80 12/- PCF81 10/- PL83 12/- PL82 10/- PL83 12/- PT82 3/11 PX25 15/- PT82 9/- PT82 9/- PT83 12/- PT81 10/- PT82 9/- PT83 12/- PT83 12/- PT83 12/- PT83 12/- PT83 12/- PT81 10/- PT82 1/- PT83 12/- PT83 12/- PT83 12/- PT81 10/- PT81 10/- PT82 1/- PT83 12/- PT8	WEARIT Wearite "P" coils 3/- each VR53(EF39) 6/6 VR54(EB34) 2/- VR55(EB50) 6/- VR56(EF36) 6/- VR57(EK32) 8/- VR56(EF36) 3/- VR56(EF36) 3/- VR56(EF36) 4/- VR51(EF50) 4/- VR51(EF50) 4/- VR51(EF50) 4/- VR51(EF50) 4/- VR51(EF30) 6/- VR
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BBW7   10 -   6C4   7 -   6C5   6 6   6C6   5 -    6C9   10 6   6D6   5 -    6F6G   7 6   6F6G   7 6   6F13   14 -    6G0G   4 6   6H6   2 6   6J5G   5 -    6J5G   5 -    6J5G   5 -    6J5G   5 -    6J5G   7 -    6K6G   7 -    6K7G   5 -9   6K8G   8 -9   6K7   6 -9   6SA7   8 -9   6SA14   5	12807 7/6 12817 5/6 12817 8/- 12817 8/- 12817 7/6 12827 7/6 12827 7/6 12827 7/6 1487 13/6 1487 13/6 1487 13/6 2075 11/6 2075 11/6 2575 9/6 25746 9/- 25246 9/- 25246 9/- 2525 9/- 2526GT 9/6 3546GT 9/6 3546GT 8/6 3525 9/- 5016GT 8/6 ATP4 3/6 DAP96 10/6 DH95 10/6 DH95 10/6 DH96 10/6 DH97 8/6 EABC80 10/- EAC91 7/6 EAF42 12/6 EB41 9/-	KTZ41 6/- LF220 5/- MH44 7/6 MH41 7/- MH41 7/- N57 13/- N78 12/6 F91 3/9 F216 3/11 FENA4 15/- FEN26 5/- FEN26 5/- FEN26 5/- FEN26 10/- FCF80 11/- FCF80 11/- FCF80 11/- FCF80 11/- FCF80 11/- FCF80 3/11 FCF80 3/11 FX25 15/- FY81 10/- FY82 9/- FY83 12/- FY83 12/- FY83 12/- FY83 12/- FY83 12/- FY83 12/- FY84 10/- FY85 15/- FY85 15/- FY86 10/- FY81 10/- FY82 9/- FY83 12/- FY81 10/- FY82 11/6 UB44 19/6 UB44 19/6 UB44 19/6 UB641 11/- UBF80 12/6 UGH42 12/6 UGH41 12/6 UGH41 12/6 UGH41 12/6 UGH41 12/6	WEARIT Wearite "P" colla 3/- each. VR53(EF39) 6/6 VR54(EB34) 2/- VR55(EB26) 7/6 VR56(EF26) 7/6 VR56(EF26) 7/6 VR56(EF26) 3/- VR51(EF26) 3/- V
## 10/- ## 10/- ## 6059T	12807 7/6 12817 8/6 12817 8/7 12817 8/7 12817 7/6 12827 8/8 12827 7/6 1487 13/6 18D2 7/9 20L1 12/6 20P6 11/6 25Y5 9/6 25Y5 9/6 25Y5 9/6 25Y5 9/7 25Z5GT 9/7 35L6GT 9/7 35L6GT 8/6 ACG/FEN 8/6 ACG/FEN 8/6 ACG/FEN 6/6 ACG/FEN	KTZ41 6/-  KTZ41 6/-  LP220 5/-  MH4 7/6  MH41 7/-  N37 13/-  N78 12/6  P81 3/9  P81 3/11  PBNA4 15/-  PENA4 15/-  PENA6 7/-  PENA6 7/-  PENA6 7/-  PENA6 7/-  PENA6 11/-  PCF80 11/-  PCF80 11/-  PCF80 11/-  PCF80 11/-  PCF80 15/-  PC82 12/6  PL82 10/-  PT82 12/6  PL82 10/-  PT83 12/-  PT93 3/11  PT93 12/-  PT93 3/11  LP4 10/-  US25 13/6  US29 15/-  US29 15/-  US40 11/6  US41 11/6  UBC41 10/-  UBC42 11/-	WEARIT Wearite "P" coils 3/- each "P" coils 3/- each "P" coils 3/- each "RE4(EB34) 2/- VR56(EB653) "/6 VR56(EB653) "/6 VR56(EB61) 3/- VR56(EB61) 3/- VR66(EB1) 3/- VR66(EB1) 3/- VR66(EB1) 3/- VR91(EF60) 4/- VR91 Sylvania "R92(EA50) 1/6 VR916 4/- VR913 6/6 VR16 4/- VR136 6/6 VR16 3/- VR16 4/- VR137 5/6 VR16/30 8/- VR16 3/- VR16
\$\text{9BW7}\$ 10/-\$ 6C4 7/-\$ 6C5QT 6/6 6C6 5/-1\$ 6C9 10/6 6D6 5/-\$ 6F6G 7/6 6F6M 7/6 6F15 14/-\$ 6G6G 4/6 6H6 2/6 8J5G 5/-\$ 6J6G 6/-\$ 6J6G 6/-\$ 6J6G 6/-\$ 6J6 6/-\$ 6J6 6/-\$ 6J6 6/-\$ 6J7G 6/-\$ 6K7G 5/9 6K7G 5/9 6K8G 7/-\$ 6K7G 5/9 6K3GT 9/6 6K8G 7/-\$ 6K3G 7/-\$ 6K7G 5/9 6K3GT 9/6 6K3GT 9/6 6K3GT 9/6 6K3GT 9/6 6K3GT 8/-\$ 6SB7 8/-\$ 6U5G 8/6	12807 7/6 12817 8/6 12817 8/7 12817 8/7 12817 7/6 12807 8/6 12807 8/6 12817 7/6 1487 13/6 15D2 7/9 2011 12/6 2012 11/6 2015 9/6 2575 9/6 2575 9/6 2575 9/6 2575 9/6 25746 9/7 25725 9/7 25725 9/7 25725 9/7 25725 9/7 25725 9/7 25725 9/7 25725 9/7 25725 9/7 25725 9/7 25725 9/7 25725 9/7 25725 9/7 25725 9/7 25725 10/7 2572	KTZ41 6/- LF220 5/- MH44 7/6 MH41 7/- MH41 7/- N37 13/- N78 12/6 F91 3/9 P216 3/11 PENA4 15/- PEN26 5/- PEN26 5/- PEN26 10/- PCF80 11/- PCF80 11/- PCF80 11/- PCF80 11/- PCF80 11/- PCF80 3/11 PCF80 3/11 PCF80 12/- PCF81 10/- PT81 11/- PT	WEARIT Wearite "P" coils 3/- each "P" coils 3/- each "P" coils 3/- each "RE4(EB34) 2/- VR56(EB653) "/6 VR56(EB653) "/6 VR56(EB61) 3/- VR56(EB61) 3/- VR66(EB1) 3/- VR66(EB1) 3/- VR66(EB1) 3/- VR91(EF60) 4/- VR91 Sylvania "R92(EA50) 1/6 VR916 4/- VR913 6/6 VR16 4/- VR136 6/6 VR16 3/- VR16 4/- VR137 5/6 VR16/30 8/- VR16 3/- VR16
## 10/- ## 10/- ## 6059T	12807 7/6 12817 8/6 12817 8/7 12817 8/7 12817 7/6 12827 8/8 12827 7/6 1487 13/6 18D2 7/9 20L1 12/6 20P6 11/6 25Y5 9/6 25Y5 9/6 25Y5 9/6 25Y5 9/7 25Z5GT 9/7 35L6GT 9/7 35L6GT 8/6 ACG/FEN 8/6 ACG/FEN 8/6 ACG/FEN 6/6 ACG/FEN	KTZ41 6/-  KTZ41 6/-  LP220 5/-  MH4 7/6  MH41 7/-  N37 13/-  N78 12/6  P81 3/9  P81 3/11  PBNA4 15/-  PENA4 15/-  PENA6 7/-  PENA6 7/-  PENA6 7/-  PENA6 7/-  PENA6 11/-  PCF80 11/-  PCF80 11/-  PCF80 11/-  PCF80 11/-  PCF80 15/-  PC82 12/6  PL82 10/-  PT82 12/6  PL82 10/-  PT83 12/-  PT93 3/11  PT93 12/-  PT93 3/11  LP4 10/-  US25 13/6  US29 15/-  US29 15/-  US40 11/6  US41 11/6  UBC41 10/-  UBC42 11/-	WEARIT Wearite "P" coils 3/s-each.  VR53(EF29) 6/6 VR54(EB34) 2/s-VR55(EB053) 7/6  VR55(EB053) 7/6  VR56(EF3) 3/9  VR55(EB05) 4/s  VR56(EF3) 3/9  VR56(EF3) 3/9  VR56(EF3) 3/9  VR56(EB1) 3/9  VR51(EB50) 4/s  VR51 S/4  VR51 S/4  VR51 S/6  VR52 S/6  VR52 S/6  VR52 S/6

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#### ALPHA 3 VALVE T.R.F. KIT £5.10.0

\* Easy to build.

\* Valves 6J7, 6K7, 6V6GT plus metal rectifier.

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Primary 200-200-240 v.
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M/A. 0-6.3 v. 4 amp., 0.5 v. 2
amp., both tapped at 4 v.
amp., both tapped at 4 v.
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ALL P.M. TYPES LESS TRANSFORMER

Waterhouse 5in. unit 17/6 ca. Plessey 61in. unit 18/6 ca. R. & A. 8in. unit 18/6 ca. Plessey 12in. unit 35/- ca.

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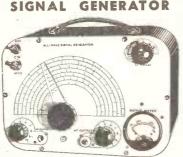
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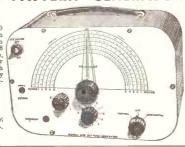
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In plastic cabinet comprising transistor, tuning condenser iron-cored coil, etc., 19/6 P. & P. 1/6.

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Comprising chassis, tuning condenser, coils, valves, valve holders, volume control, resistors, condensers, 19/6 Point to Point wiring diagram 1/-. plus 2/6 Free with kit. P. & P.

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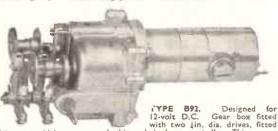
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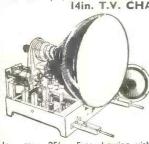
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T.V. CONSTRUCTOR CHASSIS SOUND AND VISION STRIP. 35/6. Tested working. Com vision strip LESS valves FREE drawing P. & P. 2/6 I.F.'s 16.5-19.5 Complete vision strip LESS valves FREE drawing P. & P. 2/6 I.F.'s 16.5-19.5 m/cs POWER PACK. 39/6. R.F. E.H.T. unit, tested working LESS valves FREE drawing Ins. Carr., 5/-.
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Complete with tube and spea-ker, modified ready working. Fully guaranteed for 3 months. demonstrated in our These are shops. LESS valves. As above with 5 valves £15/19/6. With all the valves £19/19/6. (Some delay on the latter). Ins., carr., tube incl., 25/-. Channels I and 2 only, but enquire for all other channels.

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6 valves. BRAND NEW. With tele-scopic aerial. V.H.F Many clients tell us they have successfully converted to has its in-Walky-Talky, Each structions. and Ins., 5/6.



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	EABC80	7/6	PL81	11/6	6X4	6/11	)
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	EB91	6/3	PL83	11/6	7C5	7/11 (	ļ
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1	ECC81	8/6	PY81	8/11	757	8/11	)
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)	ECF82	10/11	UY4I	7/11	12K8GT	12/6	ķ
	EF41	9/3	VUIII	1/6	12Q7GT	,	1
1	EF90	8/3	IR5	7/6		11/6	ì
í	EF86	11/6	185	7/3	25L6GT	8/11	١
	EF91	6/6	IT4	7/3	25Z4G	8/11	,
	EL41	9/11	354	7/6	35Z4GT	7/11 (	)
	EL84	10/6	3V4	8/3			١
Ĺ	EY51	9/11	5Y3GT	7/3	35L6GT	8/11	ľ
	EY86	10/3	5Z4G	8/3	30L1	11/9	Į
1	EZ40	7/11	615	2/11	807	3/11	3
	EZ80	8/3	6K7G	2/11	954	1/6	ĺ
	PCC84	9/11	6J7G	6/11	955	3/11	ļ
1	PCF80	10/-	6L18	12/11	956	2/11	)
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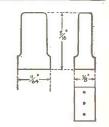
Pioneers in the field of crystal devices, British Thomson-Houston, by constant advances in manufacturing techniques, are able to supply transistors of unsurpassed quality at highly competitive prices.

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GT 1	0.8	20	-15	-10	50
GT 2	0-9	40	-15	-10	50
GT 3	1.0	65	-15	-10	50
GT:11	4.0	30	-15	-10	25
GT 12	6.0	40	-15	-10	25
GT 13	9.0	50	-15	-10	25

Ratings given pertain to ambient of 25°C:

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For Cathode Ray Tubes having Heater/Cathode short circuit for C.R. Tabes, with falling emission. Type A. Low leakage windings. Ratio 1: 1.25 giving a 25% boost on Secondary.

a 25% boost on Secondary.

2 volt 10/6 each
4 volt 10/6 each with Tag
6.3 volt 10/6 each with Tag
6.3 volt 10/6 each Panel and
10.8 volt 10/6 each Solder Tags
13.3 volt 10/6 each
Ditto with mains primaries 12/6 each.
Ditto with mains primaries 12/6 each.
Type B. Mains input 220/240 volts. Low Capacity. Multi
Output 2, 4, 6.3, 7.3 10 and 13 volts. Input has two taps
which increase output volts by 25%, and 50% respectively.
This transformer is suitable for all Cathode Ray Tubes.
With Tag Panel 21/- each.
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2 volt Tubes with falling emission. Input 220/240 volts.
Output 2-21-21-21-3 volts at 2 amps. With Tag Panel
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Output 2-25-27-27 to the state of the state

T.V. receivers having series connected heaters.

RESISTORS. All values. 10 ohms to 10 meg., ½ w. 4d.; iw., 6d.; 1 w., 3d.; 2 w., 1/-.

HIGH STABILITY. ½ w. 1%, 2/-. All preferred values 100 ohms to 10 meg., 5 wait 100 ohms to 10 meg. 5 wait 100 wait 100 ohms to 10 meg. 5 wait 100 ohms to 10 meg. 6 wait 100 w

I.F. TRANSFORMERS 7/6 pair 485 Kc/s Slug tuning Miniature Can 2½ × ½ in. × ½ in. High Q and good band width. By Pye Radio. Data sheet supplied.

Wearite M800 IF Transformers 465 ko/s 12/6 pair.

Weather mood of framsormers was keps 1276 pair.

HEATER TRANS. Tapped 200/250 v. 6.3 v. 14 amp., 7/6ALADDIN FORMERS and cores. Jin. 8d.; Jin., 10d.
Jin. FORMERS 5837/8 and Cans TY1/2. Jin. sq. × 2 Jin.
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SLOW MOTION DRIVES. Epicyclic ratio 6:1, 2/3.
TYANA. Midget Soldering Iron. 200/220 v. or 320/250 v.
16/9. SOLON MIGGET IRON. 25 w. 24/MAINS DROPERS. 3. x Jin. Three Adj. Sliders, .3 amp.
750 ohms, 4/3. 2. amp., 1,000 ohms, per 100t., 2 amp., 100 ohms, per 10ot, 2 way, 6d. per 10ot, 3 way, 7d. per 10ot.

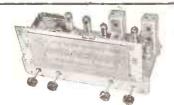
CRYSTAL MIKE INSERT by Acos
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Varied and interesting fields of work are open to men who wish to work on the development of electronic circuits and production test equipment. The scope of the problems cover from the development of simple valve and transistor circuits to the final design and assembly of equipment suitable for the automatic control of mechanical and electrical processes. The laboratory is associated with a factory manufacturing components vital to the further advance of communications equipment and is part of a large organisation. Applicants should be between the age of 22 and 35 years and should be of H.N.C. or degree Applications are also standard. invited from men with experience in electronics who are studying to achieve a recognised qualification and assistance will be given to complete the course. The position is permanent and a non-contributary pension scheme is in operation. A wide variety of accommodation can be offered to suitable applicants.

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The Nelson Research Laboratories of the English The Nelson Research Laboratories of the English Electric Company Limited invite applications from Physicists and Electronic Engineers for research and development on circuit techniques for Electronic Digital Computers. Previous experience in this field or on radar or transistor circuits would be an advantage, but suitable training will be given where necessary.

Candidates should have an appropriate degree or equivalent, but consideration will also be given to applicants having H.N.C. coupled with some previous experience of the subjects specified.

Applications, with details of qualifications and experience, should be sent to Central Personnel Services, 336/7 Strand, W.C.2, quoting Ref. W.W906C.

#### VACUUM TECHNOLOGIST

Aged 25-35, with some experience in construction of thermionic devices for small production unit working in this field, also:-

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> Electronic Instrument and Equipment Design. Electro Mechanical Design. Mass Production Test Equipment.

Excellent working conditions, attractive salaries will be offered to successful applicants.

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A number of appointments are available for interesting work providing and maintaining aeronautical telecommunications and electronic navigational aids at aerodromes and radio stations in various parts of the United Kingdom.

Applications are invited from men aged 19 or over who have a fundamental knowledge of radio or

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Salary £561 10s, at age 25 rising (subject to a practical test) to £671.

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Apply to the Ministry of Transport and Civil Aviation (ESB1/RT), Berkeley Square House, London, W.1, or to any Employment Exchange (quoting Order No. Westminster 5788).

#### TRINITY HOUSE LONDON

(a) ENGINEER (unestablished) required to undertake the planning and installation of a number of fixed site V.H.F. telephone links. A background of telecommunications experience including telephone switching, line transmission and V.F. telegraphy would be an advantage. Opportunities may also arise for other V.H.F. and U.H.F. development work.

Qualifications required are corporate.

Qualifications required are corporate membership of the Institution of Electrical Engineers or success in examinations recognised as granting exemptions from Sections A and B of the examination for corporate member-

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Applications should be made in writing to The Secretary, Trinity House, Tower Hill, London, E.C.3, not later than 6th May, and should state age, occupation, qualifications, experience, and enclose copies of testimonials.

#### **ENGINEERS**

Mechanical and Electrical and

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Required for work on development, circuit application and manufacturing of special radio valves including microwave devices.

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**MANUFACTURERS** VALVES FOR G.E.C.

#### MULTITONE ELECTRIC CO. LTD.

invite applications from Intermediate and Junior

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for work on the development and testing of an interesting range of new electronic projects. There are vacancies for engineers with a wide range of qualifications and experience up to and including H.N.C. standard. Experience of development work or fault-finding advantageous. Preferred age range 20/30 years but applications will also be considered from young men who have recently left school with Higher School Certificate in Science. Apply stating age and giving particulars of education, training and experience to 12/20, Underwood Street, London, N.1.



Seniors and Juniors required by The B.T.H. Co. Ltd., in Rugby, for development and production of Electrical Control Gear and its associated equipment.

Interviews arranged to suit applicant, including Saturday mornings.

Men with Electrical and/or Mechanical Draughting experience are invited to apply to:—

Engineer-in-Charge, Control Gear Drawing Office, The British Thomson-Houston Co. Ltd., Rugby.

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#### SCIENTIST OR TECHNICIAN

with experience in the manufacture of Electrolytic Capacitors required for Canadian Company. Good salary and prospects for suitable man. Write giving fullest details to

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5

#### **ELECTRONIC ENGINEERS**

The English Electric Company Limited have vacancies for Electronic Engineers to work, in the first instance, on maintenance and operation of digital computer installations. Training will be given, where necessary, in the appropriate techniques, and opportunities will exist for suitable candidates to transfer to research and development groups working on advanced types of computer.

Applications should be sent to:— Central Personnel Services, 336/7 Strand, W.C.2, quoting Ref. WW906B.

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Head of Department: D. O. Bishop, Ph.D., M.I.E.E.

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#### Nuclear Power Stations and Marine Propulsion Projects

The Nuclear Division of Elliott Bros. (London) Ltd., has vacancies for experienced Draughtsmen for work on electronic and mechanical design in connection with the control and instrumentation of nuclear reactors. The work is interesting and varied and provides an opportunity to participate in projects of great National importance.

All grades are required but H.N.C. or equivalent, together with suitable experience, is essential for senior posts. Previous Nuclear Energy experience is not essential.

Write giving full details of your career to Personnel Officer, Century Works, Conington Road, Lewisham, S.E.13.

THE ENGLISH ELECTRIC COMPANY LIMITED STEVENAGE, HERTS.

require

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for work in a variety of interesting aspects of an environmental testing programme. Experience in electronic and electrical equipment, together with theoretical qualifications of H.N.C. level or equivalent are desirable though not essential.

Applicants who possess the necessary imagination and initiative for this type of work are invited to write to the Personnel Officer, Development Wing, at the above address, quoting Ref. W.W.1318A.

#### BRITISH SOUTH AFRICA POLICE RADIO COMMUNICATIONS BRANCH TELEGRAPHIST

Applications are invited from unmarried men between the ages of 18 and 25 for appointment in the Radio Communications Branch of the British South Africa Police. Candidates should have reached a standard of education equivalent to General School Leaving Certificate and should be in possession of Post Office Certificate for radio telegraphists or its equivalent, and be able to transmit/receive Morse at the rate of 25 w.p.m. A knowledge of touch typing will be an advantage.

Commencing rate of pay according to qualifications held by candidate which will be assessed by a trade test.

Applications stating qualifications should be addressed to the Recruiting Officer, British South Africa Police, Rhodesia House, 429, Strand, London, W.C.2, who will supply further particulars on request.

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Experienced in one or more of the following:-

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Five-day week, good working conditions, single accommodation available.

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QUALIFICATIONS: The ability to design and develop equipment, and aggressively progress a project through to the stage where a model is made and the information is available for a production drawing office. Candidates should preferably be of degree standard, or, Corporate Members of one of the Professional Institutions, but consideration will be given to others who have considerable practical experience in the field. The ability to progress the project through to a satisfactory conclusion is the prime requirement. Due to expanding activities men with drive and initiative can be sure of progressive advancement.

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On well served transport routes.

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# Television Development and Test Equipment Engineers

A well known West London manufacturer requires Engineers for the development of black and white and colour television receivers and associated test equipment.

Vacancies exist for both Senior and Junior Engineers in the Television Development Department and for Junior Engineers in the Test Equipment Department.

Senior Engineers should have academic qualifications and several years' development experience. Junior Engineers require either academic qualifications or experience in development or equipment calibration and maintenance.

Progressive salary policy ensures rapid advancement for Engineers who show exceptional initiative and responsibility. All posts are permanent and carry the benefit of the Firm's Pension Scheme.

Please write fully, in confidence, stating age, qualifications and experience to Box No. 7441.

#### TEXAS INSTRUMENTS LIMITED

A new British Company

#### TECHNICAL SALES MANAGER

required to develop and integrate marketing programme of new U.K. subsidiary of Texas Instruments Incorporated world's leading transistor manufacturer. Duties include establishing technical sales department, analysis of markets, sales forecasting and planning, and accomplishment of established sales goals.

Should be persuasive and imaginative and familiar with the electronics industry and the application of semiconductor devices. Several years sales experience in electronics components preferred together with honours degree in engineering or physics.

Salary commensurate with age, ability and experience. This appointment offers an exciting future for the right man.

Reply to Box No. M.3014, JOHN HADDON & Co. LTD., 11/12, Salisbury Square, E.C.4.

#### Z & I AERO SERVICES LTD.

Fully Serviced and Guaranteed Test Equipment COMMUNICATION RECEIVERS & ACCESSORIES

MARCONI TF144G "STANDARD" SIGNAL GENERATORS, range 85 kc/s to 25 mc/s; output  $|\mu V$  to 1 volt; completely overhauled, with mains and output leads, £85.

MARCONI TF144F "STANDARD" SIGNAL GENERATOR, range and output as above. Complete with mains and output leads, fully overhauled, £70.

MARCONI TF390G SIGNAL GENERATOR, range 16 to 150 mc/s, indirect calibration, output  $|\mu \rangle$  to 100m $^{\circ}$ /s, internal modulation 400 c/s; complete with output lead and attenuator pad, £25.

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MARCONITF-675D MODULATION GENERATOR (Pulse Generator), for pulses from 2 to 12.5 µsec wide, repetition speeds from 500 to 3,000 c/s; output voltage 50 v. pos. peak. Power supplies 250 v. A.C., £23.

MARCONI CR-150 COMMUNICA-TION RECEIVERS, range 2 to 60 mc/s, in 5 bands; high sensitivity, selectivity and stability; dual superhet; Crystal Filter; Calibrating Crystal; "S" meter. Power requirements 300 v. H.T. and 6,3 v. L.T., £50. Mains operated Power Unit, £10.

HALLICRAFTER S-27 COMMUNICATION RECEIVER, range 27.8-143 mc/s, 110/230V, AM/FM; Checked, in good operating condition £25.

HALLICRAFTER S-36 COMMUNI-CATION RECEIVER, tropicalised version of S-27; Checked, in good operating condition, £30.



ARMATURE DROP TESTER (Ex A.M. Ref. 5G/549)

For testing Motor and Generator Armatures, max. dia. of commutator appr. 4in.; max. overall dia. 7in. max. length appr. 15in. PRICE £5/10/-.



#### 8" SCALE EDGEWISE METERS

Cross Coil (Balanced Type) Movement, three terminals. Resistance of each coil appr. 250 ohms. Sensitivity appr. 30 µA FSD. PRICE £7/15/-

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EVERSHED DUAL PEN VOLTAGE RECORDER, range 160 to 240 v. A.C. suppressed zero; spring clock driven; chart speed lin, per hour; chart width fin.; Moving Coil Rectifier Type Movement; basic movement has an appr. resistance of 1,000 ohms. The recorder can therefore be used as a milliammeter recorder with a range of from 10 to 15 milliamps. Complete with a supply of charts, pens, filler, ink, etc., £75.

EVERSHED DUAL PEN MILLIAM-METER RECORDER, 0 to 5 mA D.C., synchronous clock drive, chart width 6in, £75.

ELLIOTT BROS. MILLIAMMETER RECORDER. Single Pen, range 0 to 5 milliamps D.C., synchronous clock drive; chart speed 3in. per minute; chart width 6in. Complete with spare pens and chart, £45.

INSULATION TESTERS.
Evershed "Wee" Meggers, 500 v., in leather cases, £12/10/-.
Evershed 500 v. 40 megohm Meggers, £22/10/-.
Evershed 1,000 v. 100 megohm Meggers, £27/10/-.
Evershed 1,000 v. 200 megohms Bridge Megger, £55.
High Voltage Test Set, range 0 to 5 kV, A.C. and D.C., 250 v. mains operated, £25.

TS89/AP VOLTAGE DIVIDER, for extending voltage range of an oscilloscope; ratios 100 and 10 to 1; max. volts 20,000, £5.

AVOMETER MODEL 40 BAKELITE BACK CASES, 7/6. AVOMINOR UNIVERSAL FRONT PANELS, 7/6.

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Alkaline Cell for the above, £3/3/-.

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METER. Calibrated for Pt.Rh. (1600°C), Chromel/Alumel (1300°C) and Iron Constantan Thermocouples (1050°C), millivolt ranges 20 mV, and 60 mV. PRICE, complete with Weston Standard Cell, £35.

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Readers are warned that Government surplus Readers are warned that Government surplus components and valves which may be offered for sale through our displayed or classified columns carry no manufacturers' guarantee: Many of these items will have been designed for special purposes making them unsuitable for civilian use, or may have deteriorated as a result of the conditions under which they have been stored. We cannot undertake to deal with any complaints regarding any such items purchased. chased.

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[0095]

EAK TL/10 amplifiers with point one pre amps; £4/5 deposit and 9 payments of 57/7 monthly.

ROGERS junior with control unit; £3/18 deposit and 9 payments of 52/10 monthly; cash prices Leak £28/7, Rogers £26.

A. L. STAMFORD (Dept. LR.2), 20, College Parade, Salusbury Rd., London, N.W.6. [6915]

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HRO Rx's and colls in stock, also AR88, BC348R. CR100, etc.—Requirements please to R. T. & I. Service, 254, Grove Green Rd., London, E.11. Ley. 4986

15-watt Grampian amplifier with radio, with Decca corner speaker and Decca 3-speed record player, two pick-up heads; £40.—Ennor, The Moor, Falmouth. [6971

HALLICRAFTERS V.H.F. AM/FM receiver type S-36, 28 to 143 m/cs, 100/250 V. A.C., unused in makers packing with spare valves; £55.—Harris, 93, Wardour St., W.I.

valves; £55.—Harris, 93, Wardour St., V. [6918]

A MERICAN Stromberg-Carlson international battery operated, built-in loop aerial and short wave telescopic aerial, 2 speakers, world may not lid with time zones, instruction manual and log book, barometer, thermometer and humidity indicator on front tuning panel, set is only 6 months old, hardly used, will self to the first offer of £60.—Write R. Lynn, 45, Mecklenburgh Square, London, W.C.I. [6951]

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R.F. Unit No. 2 for Receiver R.209, comprises compact unit approx. 64\(^{\chi}\)\(\chi^{\chi}\)\(\



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for Special Applications



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Output transformer as specified for the Baxandall 5 watt Amplifier (featured in the March and April issues of this periodical). Price 36/-

This transformer is also available with G.O.S.S laminations (Type P4077). Price 42/6

#### **Type P4073**

A single ended 4 watt output transformer suitable for the Mullard 3 watt amplifier and the Mullard Tape amplifier. Type A. Price 45/-

#### **Type P4078**

Mains transformer as specified for the Collaro Tape Transcriptor. Price 50/-

Smoothing choke as specified for the Collaro Tape Transcriptor. Price 18/6

Many current amplifier designs, such as those published by Mullard and G.E.C., specify and approve Partridge Output and Mains transformers.

If there is any difficulty in obtaining specified transformers from your local dealer, please write direct to:



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LOUDSPEAKERS—SURPLUS AND SECOND-HAND
SECOND-HAND
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SECONDHAND

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BC221M frequency meter, new condition: [6973

A MATEUR selling test equipment, etc., bar-gain prices; send stamped addressed enve-lope for list.—Gilford, 22, Pembury Rd., Tonbridge, Kent. [6949

Tonbridge, Kent.

SignAL generators, oscilloscopes, output meters, valve voltmeters, frequency meters, multi-range meters in stock; your enquirtes are invited.—Requirements to R. T. & I. Service, 254, Grove Green Rd., London, E.11. Ley. 4986.

SURPLUS to requirements:—Radar dual-hand TV signal generator type 4/5, £50; Taylor 170A valve voltmeter, £15; Taylor 30A oscillo-scope. £15; Philips projection TV optical units (1800A) with CRT, £7.—Cosmic Radio, 6 & 8. Clifton Crescent, Birkenhead NEW COMPONENTS

TRANSISTOR transformers, interstate push-pull, 8/-; output ditto, 7/6, from manufac-turers, Osmabet, Ltd., 14, Hillside Rd., Tottenham. London. N.15.

CRYSTAL microphone inserts (Cosmocord Mic 6/4), still in steady demand by Hams and Sound Engineers; guaranteed newly made and boxed; 15/6 post free.—Radio-Aids, Ltd... 29, Market St., Wetford, Herts.

COMPONENTS—SURPLUS AND
SECOND-HAND
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Court Rd., London, W.I. Tel. Museum 

SOUTHERN RADIO SUPPLY, Ltd., 11, Little Newport St., London, W.C.2, See our dis-played advertisement, page 162.

#### Fidelia

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VHF/FM reception with low noise R.F. stage, variable selectivity, medium and long wavebands, negative feedback tone control circuit, having separate base and treble controls. Triode output stages. Tuning indicator. High quality gramophone amplification. Audio response ≥20-20,000 cycles.

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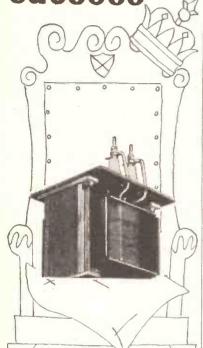
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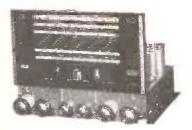
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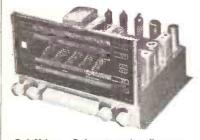
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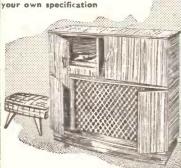
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[6933]

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Personnel Officer, McMichael Radio, Ltd., Wexham Rd., Slough.

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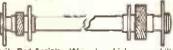
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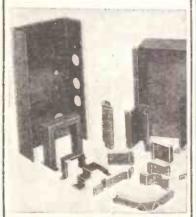
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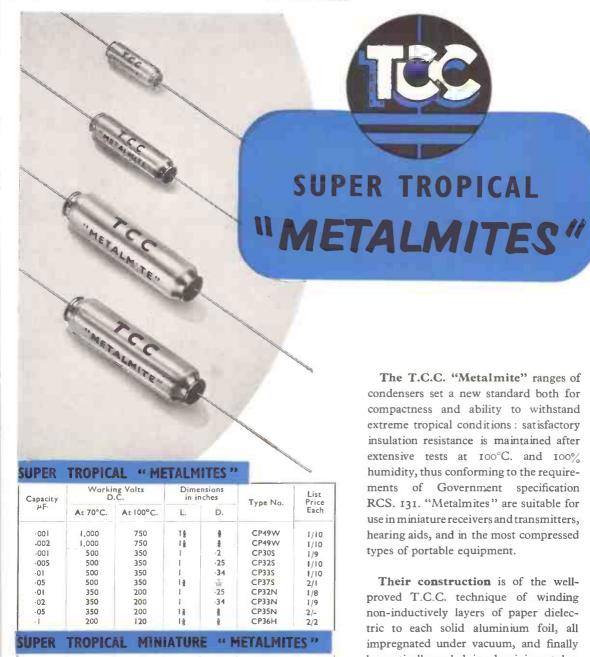
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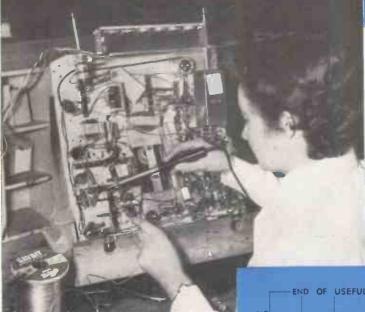
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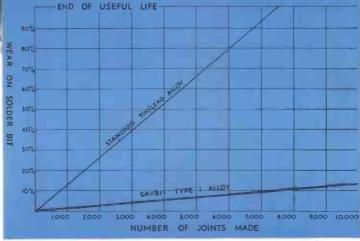
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