

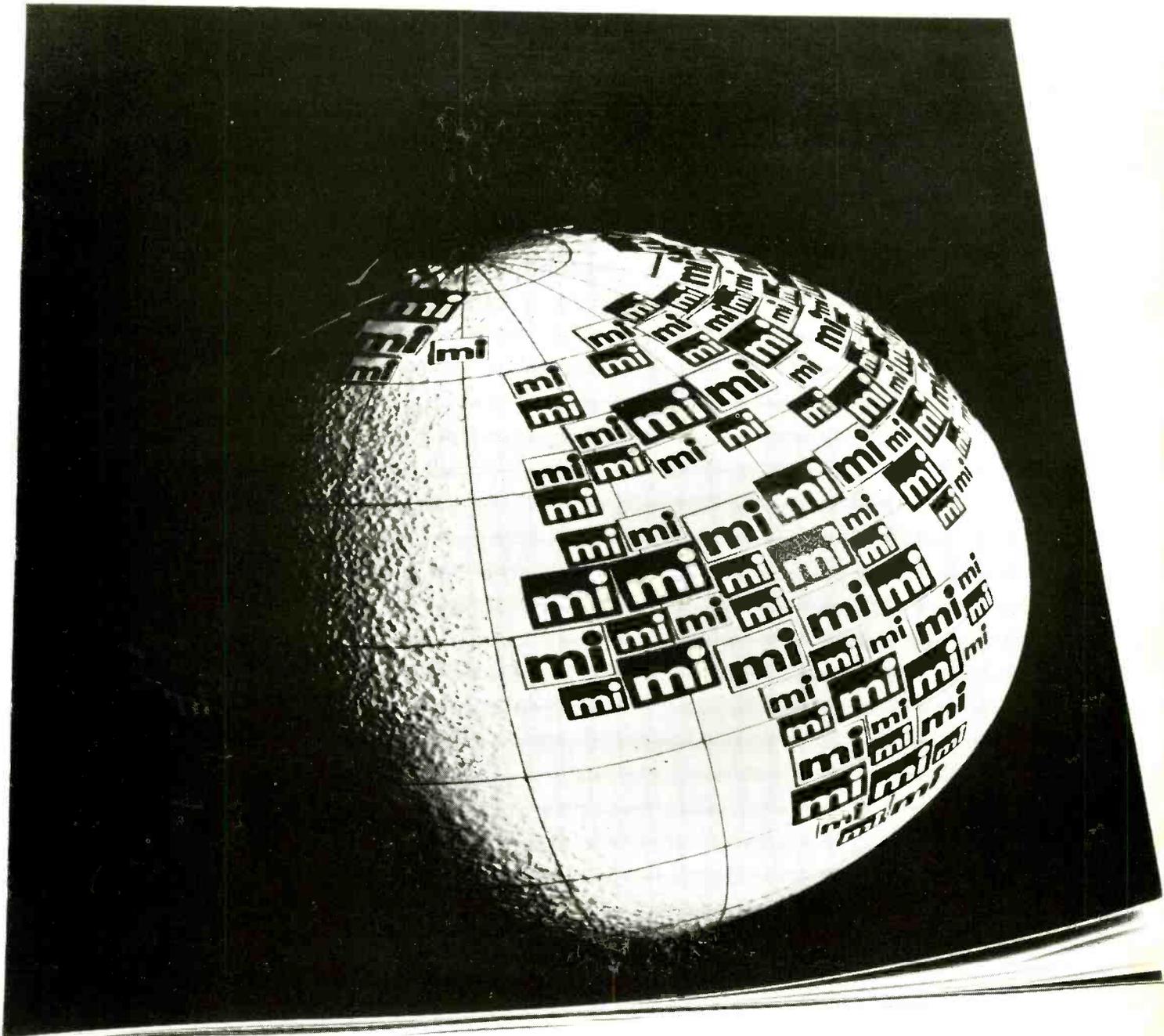
# wireless world

JANUARY 1975 25p

**Electronics and oil**  
**Silent stereo switch**



Australia	80 Cents	Malaysia	M\$ 2.60
Belgium	Fr. 52.00	New Zealand	78 Cents
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## Cover Story

Some Marconi Instruments are designed to be mobile. Others are not - but do a lot of travelling all the same. In fact, nearly three-quarters of **mi**'s total sales stem from export orders.

So there are plenty of people in Milwaukee or Mannheim or Melbourne or Montevideo who are just as discerning about Marconi Instruments as you are. And they're equally enthusiastic about **mi** service, too. We've service organisations in New Jersey, Munich, Paris and a whole lot of other

places to see to that.

There are **mi** distributors and representatives in more than 60 countries throughout the world and we have 14 associated companies in Africa, the Middle, Near and Far East, North and South America and Europe.

**mi**, then, doesn't only cover all the intricacies of planning and producing some of the world's finest electronic testing and measuring instruments . . . .

It covers the world, as well.

# **mi**: THE INTERNATIONALISTS

MARCONI INSTRUMENTS LIMITED

Langacres • St. Albans • Hertfordshire AL4 0JN • England • Telephone: St. Albans 59292 • Telex: 23350

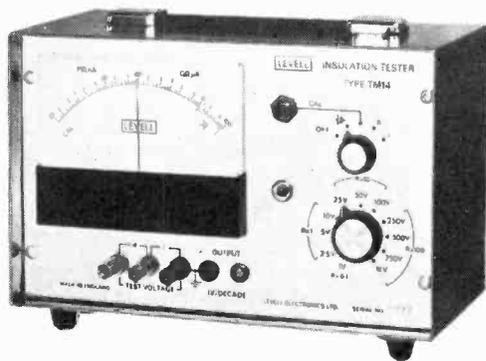
A GEC-Marconi Electronics company.

# LOW COST TESTERS



## LEVELL PORTABLE INSTRUMENTS

### INSULATION TESTER



A logarithmic scale covering 6 decades is used to display either insulation resistance or leakage current at a fixed stabilised test voltage. The current available is limited to a maximum value of 3mA for safety and capacitors are automatically discharged when the instrument is switched off or to the CAL condition. The instrument operates from a 9V internal battery.

#### RESISTANCE RANGES

- 10M  $\Omega$  to 10T  $\Omega$  ( $10^{13} \Omega$ ) at 250V, 500V, 750V and 1kV.
- 1M  $\Omega$  to 1T  $\Omega$  at 25V, 50V and 100V.
- 100k  $\Omega$  to 100G  $\Omega$  at 2.5V, 5V and 10V.
- 10k  $\Omega$  to 10G  $\Omega$  at 1V.

Accuracy  $\pm 15\%$  +800  $\Omega$  on 6 decade logarithmic scale.  
 Accuracy of test voltages  $\pm 3\%$   $\pm 50$ mV at scale centre.  
 Fall of test voltages  $< 2\%$  at 10 $\mu$ A and  $< 20\%$  at 100 $\mu$ A.  
 Short circuit current between 500 $\mu$ A and 3mA.

#### CURRENT RANGE

100pA to 100 $\mu$ A on 6 decade logarithmic scale.  
 Accuracy of current measurement  $\pm 15\%$  of indicated value.  
 Input voltage drop is approximately 20mV at 100pA, 200mV at 100nA and 400mV at 100 $\mu$ A.  
 Maximum safe continuous overload is 50mA.

#### MEASUREMENT TIME

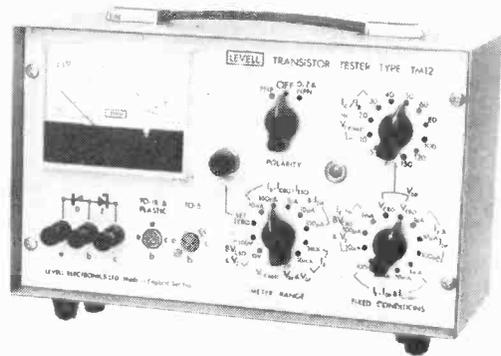
$< 3$ s for resistance on all ranges relative to CAL position.  
 $< 10$ s for resistance of 10G  $\Omega$  across 1 $\mu$ F on 50V to 500V.  
 Discharge time to 1% is 0.1s per  $\mu$ F on CAL position.

#### RECORDER OUTPUT

1V per decade  $\pm 2\%$  with zero output at scale centre.  
 Maximum output  $\pm 3$ V. Output resistance 1k  $\Omega$ .

type  
TM14 **£80**

### TRANSISTOR TESTER



Tests bipolar transistors, diodes and zener diodes. Measures leakage down to 0.5 nA at 2V to 150V. Current gains are checked from 1 $\mu$ A to 100mA. Breakdown voltages up to 100V are measured at 10 $\mu$ A, 100 $\mu$ A and 1mA. Collector to emitter saturation voltage is measured at 1mA, 10mA, 30mA and 100mA for  $I_C/I_B$  ratios of 10, 20, 30. The instrument is powered by a 9V battery.

#### TRANSISTOR RANGES (PNP OR NPN)

- $I_{CBO}$  &  $I_{EBO}$ : 10nA, 100nA, 1 $\mu$ A, 10 $\mu$ A and 100 $\mu$ A f.s.d. acc.  $\pm 2\%$  f.s.d.  $\pm 1\%$  at voltages of 2V, 5V, 10V, 20V, 30V, 40V, 50V, 60V, 80V, 100V, 120V, and 150V acc.  $\pm 3\%$   $\pm 100$ mV up to 10 $\mu$ A with fall at 100 $\mu$ A  $< 5\%$  +250mV.
- $BV_{CBO}$ : 10V or 100V f.s.d. acc.  $\pm 2\%$  f.s.d.  $\pm 1\%$  at currents of 10 $\mu$ A, 100 $\mu$ A and 1mA  $\pm 20\%$ .
- $I_B$ : 10nA, 100nA, 1 $\mu$ A ... 10mA f.s.d. acc.  $\pm 2\%$  f.s.d.  $\pm 1\%$  at fixed  $I_E$  of 1 $\mu$ A, 10 $\mu$ A, 100 $\mu$ A, 1mA, 10mA, 30mA, and 100mA acc.  $\pm 1\%$ .
- $h_{FE}$ : 3 inverse scales of 2000 to 100, 400 to 30 and 100 to 10 convert  $I_B$  into  $h_{FE}$  readings.
- $V_{BE}$ : 1V f.s.d. acc.  $\pm 20$ mV measured at conditions on  $h_{FE}$  test.
- $V_{CE(sat)}$ : 1V f.s.d. acc.  $\pm 20$ mV at collector currents of 1mA, 10mA, 30mA and 100mA with  $I_C/I_B$  selected at 10, 20 or 30 acc.  $\pm 20\%$ .

#### DIODE & ZENER DIODE RANGES

- $I_{DR}$ : As  $I_{EBO}$  transistor ranges.
- $V_Z$ : Breakdown ranges as  $BV_{CBO}$  for transistors.
- $V_{DF}$ : 1V f.s.d. acc.  $\pm 20$ mV at  $I_{DF}$  of 1 $\mu$ A, 10 $\mu$ A, 100 $\mu$ A, 1mA, 10mA, 30mA and 100mA.

type  
TM12 **£80**

## LEVELL ELECTRONICS LTD.

Moxon Street, High Barnet, Herts. EN5 5SD  
 Tel: 01-449 5028/440 8686

Prices include batteries and U.K. delivery, V.A.T. extra.  
 Optional extras are leather cases and mains power units.  
 Send for data covering our range of portable instruments.



Who else but the Italians could have produced the most sophisticated range of mixing and fading facilities ever offered in such a beautifully designed range of equipment.

Yet still apply the most precise and exacting manufacturing standards to provide the operational stability and reliability such complex electronics demand.

This is why we are able to guarantee all Goodmans/Galactron equipment for three years.

And your guarantee will be signed personally by the quality controller who tests it before it leaves the factory in Italy.

#### **Galactron Mk 10 Stereo Integrated Amplifier**

A remarkably compact pre and power amp combination with 90 watts RMS per channel. Features 5 mixable stereo inputs, 5 plug-in-modules—two of which can be cross-faded by slide potentiometer.

#### **Galactron Mk 16 Stereo/Quad Amplifier**

No comparable equipment has all these 3 functions. 5 inputs, independently mixable and equalised by plug-in modules. Twin graphic equalisers having

10 filters each ( $\pm 16\text{dB}$ ) at octave intervals from 32Hz to 16kHz. Plug-in quadrophonic decoder panels for discrete and matrix systems allied to 4 output level controls.

#### **Galactron Mk 100 Stereo Power Amplifier**

Originally designed as a monitor amp for recording studios, the Mk 100 is designed for use with the Mk 16 preamplifier. 100 watts RMS per channel output.

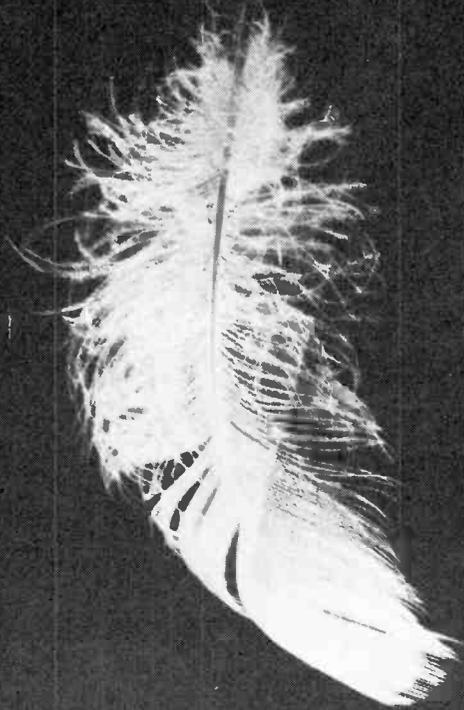
Full facts and figures are available from Goodmans Loudspeakers Limited, Downley Road, Havant, Hants.

 **Goodmans**  
**GALACTRON**

WW—080 FOR FURTHER DETAILS

WW—119 FOR FURTHER DETAILS ▶

  
A member of The Thorn Group



## Feathers and things

Take a diaphragm from a QUAD electrostatic loudspeaker. Let it fall and you can count up to ten before it reaches the ground. Try to do this with a cone from a moving coil speaker and you'll need a high speed computer to do the counting.

Remember all that stuff at school about kinetic energy? How heavy things are hard to start and

hard to stop? That's why a QUAD loudspeaker responds immediately to every nuance in the music. It's obvious when you think of it. It's even more obvious when you hear it.

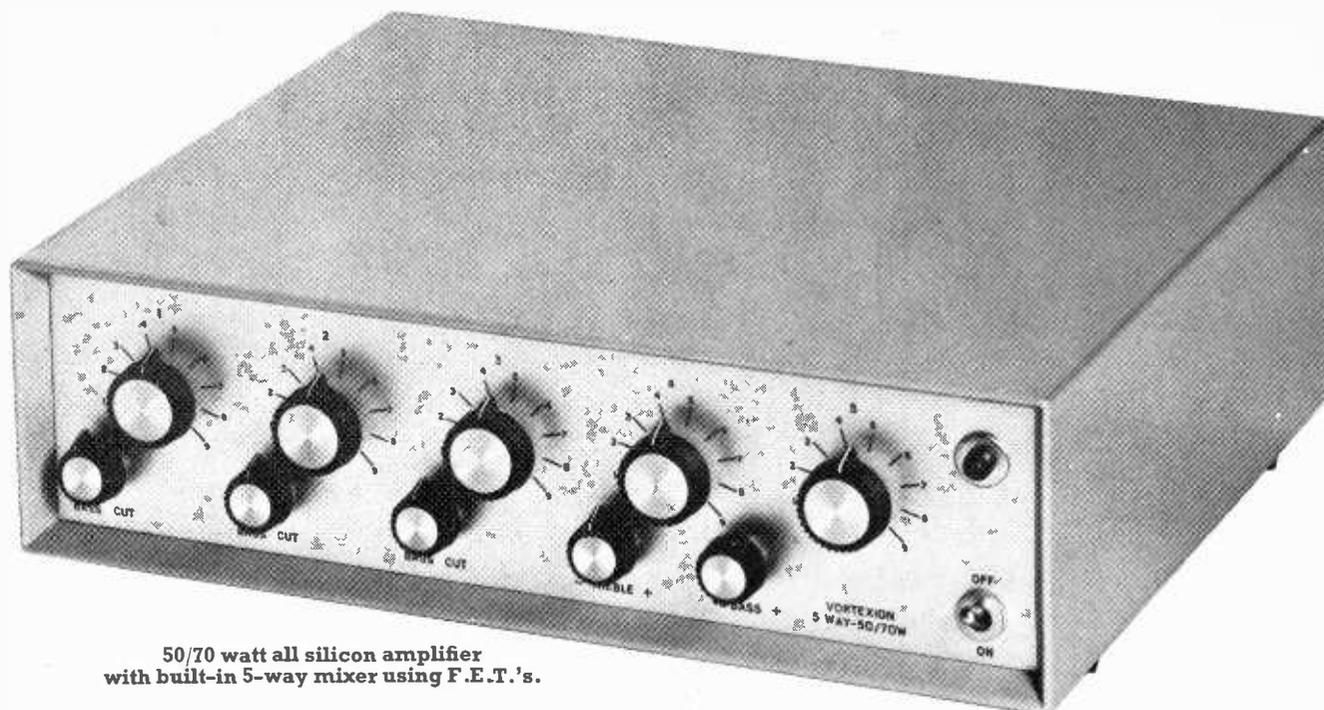
Send postcard for illustrated leaflet to Dept. WW Acoustical Manufacturing Co. Ltd., Huntingdon PE18 7DB. Telephone (0480) 52561.

# QUAD

Products of The Acoustical Manufacturing Co. Ltd.

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QUAD is a Registered Trade Mark



50/70 watt all silicon amplifier  
with built-in 5-way mixer using F.E.T.'s.

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VORTEXION Design and manufacture public address equipment to meet a range of specific requirements for AIRPORTS, HOTELS, THEATRES, GOVERNMENT AUTHORITIES, LOCAL AUTHORITIES, SUPERMARKETS, SCHOOLS, SPORTING COMPLEXES, POP GROUPS AND THE LOCAL VILLAGE HALL.

The high fidelity amplifier illustrated has bass cut controls on each of the three low impedance balanced line microphone stages and a high impedance gram stage with bass and treble controls, plus the usual line or tape input. All the input stages are protected against overload by back to back low self capacity diodes and all use F.E.T.'s for low noise, low intermodulation distortion and freedom from radio breakthrough.

A voltage stabilised supply is used for the pre-amplifiers making it independent of mains supply fluctuations and another stabilised supply for the driver stages is arranged to cut off when the output is overloaded or over temperature. The output is 75 % efficient and 100 V balanced line or 8-16 ohms output are selected by means of a rear panel switch which has a locking plate indicating the output impedance selected.

The mixer section has an additional emitter follower output for driving a slave amplifier, phones or tape recorder, output 0.3 V out on 600 ohms upwards.

**50/70 WATT ALL SILICON AMPLIFIER WITH BUILT-IN 4-WAY MIXER** using the circuit of our reliable 100 Watt Amplifier with its elaborate protection against short and overload, etc. To this is allied our latest development of F.E.T. Mixer Amplifier, again fully protected against overload and radio breakthrough. The mixer is arranged for 2-30/60  $\Omega$  balanced line microphones, 1-HiZ gram input and 1-auxiliary input followed by bass and treble controls. 100 volt balanced line output OR 5-15  $\Omega$  and 100 volt line.

**100 WATT ALL SILICON AMPLIFIER.** A high quality amplifier with 8 ohms-15 ohms or 100 volt line output for A.C. Mains. Protection is given for short and open circuit output over driving and over temperature. Input 0.4 V on 100 K ohms.

**THE 100 WATT MIXER AMPLIFIER** with specification as above is here combined with a 4-channel F.E.T. mixer. 2-30/60  $\Omega$  balanced microphone inputs, 1-HiZ gram input and 1-auxiliary input with tone controls and mounted in a standard robust stove enamelled steel case. A stabilised voltage supply feeds the tone controls and pre amps, compensating for a mains voltage drop of over 25 % and the output transistor biasing compensates for a wide range of voltage and temperature. Also available in rack panel form.

**20/30 WATT MIXER AMPLIFIER.** High fidelity all silicon model with F.E.T. input stages to reduce intermodulation distortion to a fraction of normal transistor input circuits. Standard model 1-low mic. balanced input and HiZ gram. Outputs available 8/15 ohms OR 100 volt line.

**CP50 AMPLIFIER.** An all silicon transistor 50 watt amplifier for mains and 12 volt battery operation, charging its own battery and automatically going to battery if mains fail. Protected inputs, and overload and short circuit protected outputs for 8 ohms-15 ohms and 100 volt line. Bass and treble controls fitted.

Models available with 1 gram and 2 low mic. inputs, 1 gram and 3 low mic. inputs or 4 low mic. inputs.

**200 WATT AMPLIFIER.** Can deliver its full audio power at any frequency in the range of 30 c/s-20 Kc/s. Can be used to drive mechanical devices for which power is 120 watts on continuous sine wave. Input 1 mW 600 ohms. Output 100-120 V or 200-240 V. Additional matching transformers for other impedances are available.

**F.E.T. MIXERS and PPM's.** Various types of mixers available. 3, 4, 6 and 8 channel with Peak Programme Meter. 4, 6, 8 and 10 Way Mixers. Twin 3, 4 and 5 channel Stereo, also twin 4 and 5 channel Stereo with 2 PPM's.

## VORTEXION

Vortexion Ltd., 257-263 The Broadway,  
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Telephone: 01-542 2814 and  
01-542 6242/3/4.  
Telegrams: "Vortexion  
London SW19"

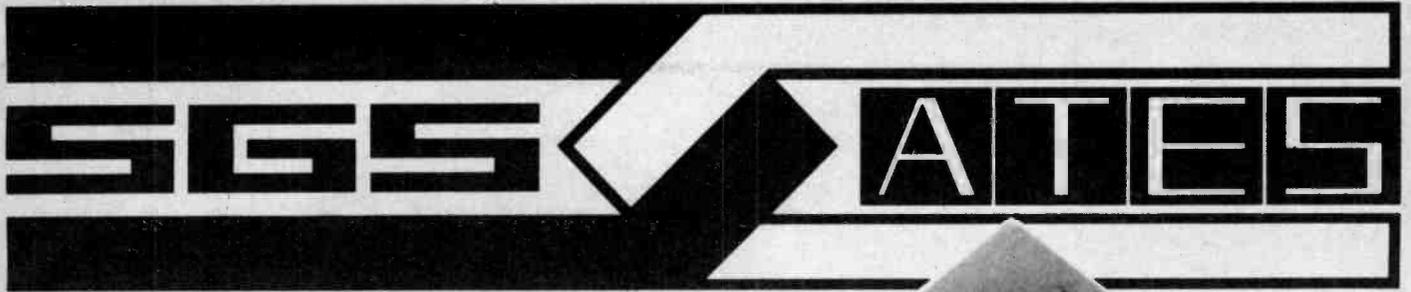
For further information and technical leaflets write to Vortexion

Name \_\_\_\_\_

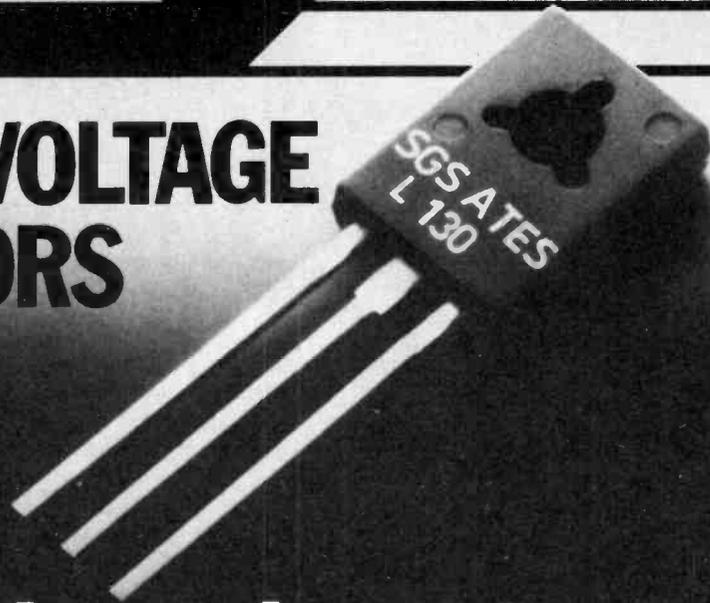
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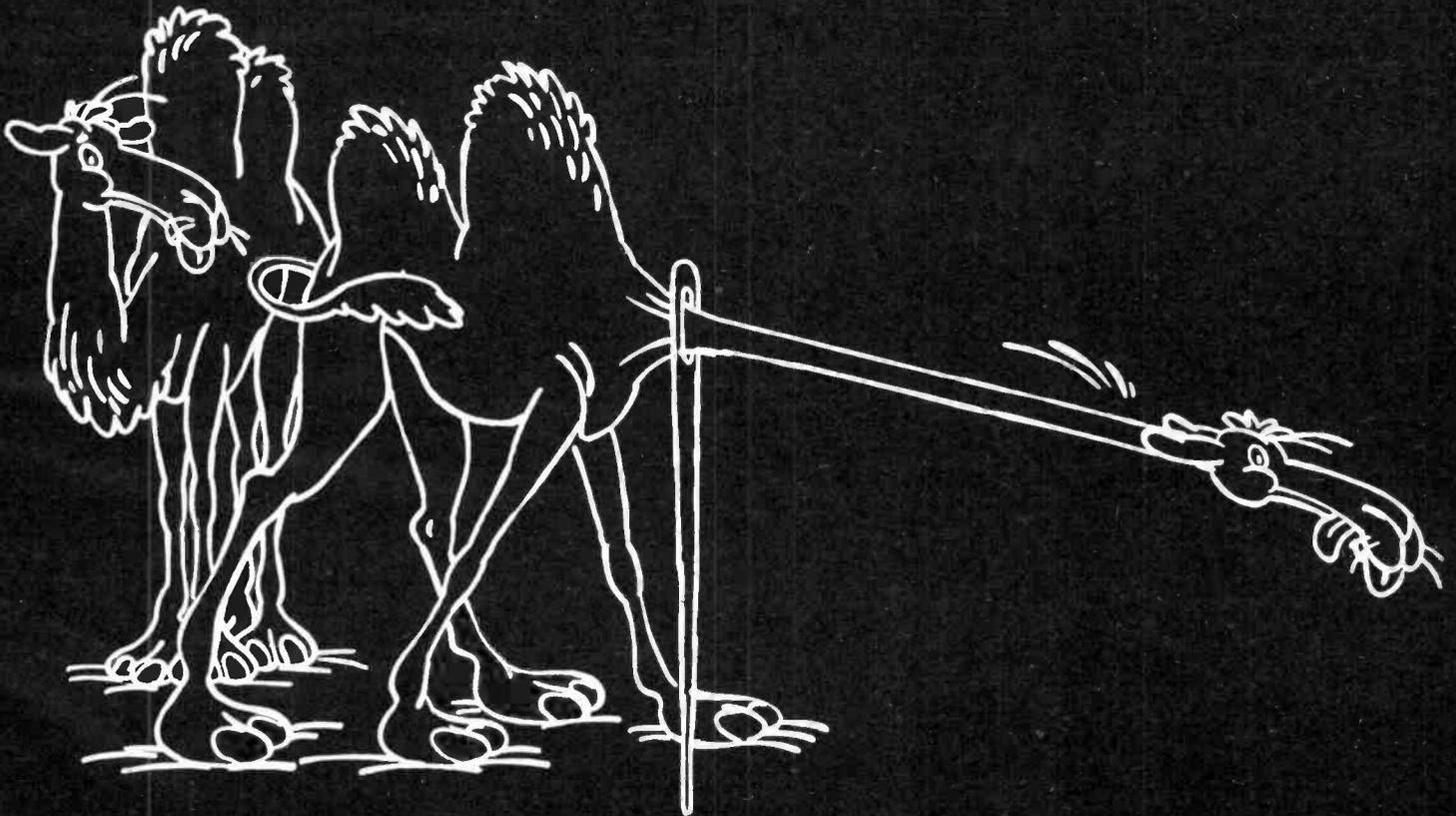
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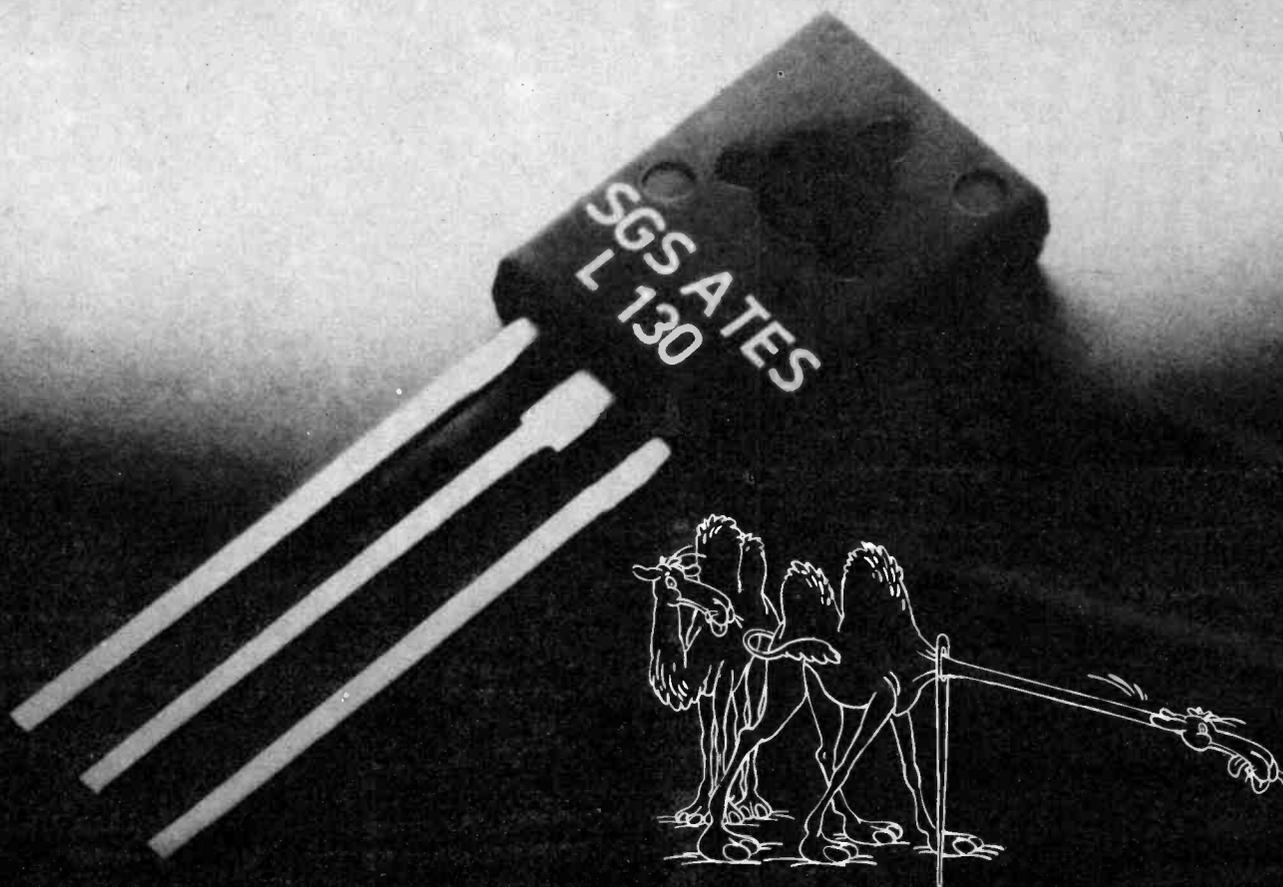
# PLASTIC VOLTAGE REGULATORS



## A regular and constant output



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## Bestselling voltage regulators now in plastic

Following the sweeping success of SGS-ATES' integrated fixed voltage regulators in TO-3 metal can, these circuits are now also available, ex stock, in SOT 32 plastic package.

Designated L129, L130 and L131, they are suitable for low cost applications in professional, industrial and consumer equipment requiring compact components with low/medium output current, such as

- desk calculators
- video displays

- computer peripherals
- touch tuning and remote control for TV sets
- TV subsystems, such as video IF, sound IF, sync and chroma stages

A particularly interesting area of application is in local regulation systems. The main advantages of this circuit technique over traditional single point regulation are the reduction in common ground and inter-circuit coupling, high noise immunity and the elimination of problems due to line voltage drops.

Special features of the circuits include

- tight tolerance on the output voltage
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The L129, L130 and L131 are designed to operate in the -20°C to +85°C temperature range. For the standard operating temperature range, 0°C to +70°C, these plastic voltage regulators are available with type numbers TDA1405, 1412 and 1415.

-20° to +85 °C	V <sub>o</sub>	I <sub>o</sub> reg. typical	0° to +70 °C
L 129	5V	850 mA	TDA 1405
L 130	12V	720 mA	TDA 1412
L 131	15V	600 mA	TDA 1415

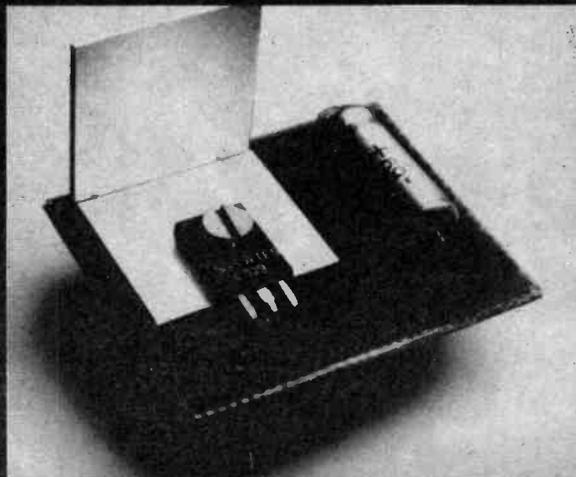


(United Kingdom) Ltd.

Distributors in the UK: Distronic Ltd., Harlow, 02796-32947 - Electronic Component Supplies Ltd., Windsor, 07535-68101 - Hawnt Electronics Ltd., Birmingham, 021-3594301 - ITT Electronic Services, Harlow, 02796-26777 - REL Equipment & Components Ltd., Hitchin, 0462-50551 - Quamdon Electronics Ltd., Derby, 32651.

WW-121 FOR FURTHER DETAILS

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# You could easily make our 12-speed chart recorder faster than you thought possible.

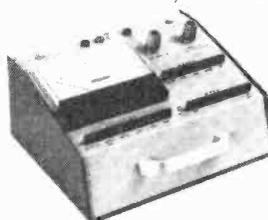
Send away for our 12-speed, 10" chart recorder kit—the IR-18M. And you'll receive a very clear, easy to understand instruction manual with it. Which explains every single step. To make light work of assembly and provide you with a high quality chart recorder a lot quicker than you thought.

And just look what you'll be getting. Multi-speed capability. With fast, pushbutton switch selection of speeds from 5 seconds per inch to 200 minutes per inch. To give you all the versatility you need.

You'll also get two input ranges, giving accurate voltage measurements of 1 millivolt and 10 millivolts full scale. Excellent repeatability. And a full scale pen response time of one second — comparing favourably with priced recorders. Take a look at the 1G-18 Solid State kit too. Outputs from 1Hz to 100KHz are available using repeatable

And its sine and square wave outputs are available simultaneously. With less than 0.1% sine wave distortion. And less than 50 ns square wave rise time.

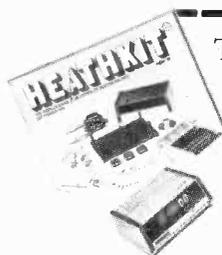
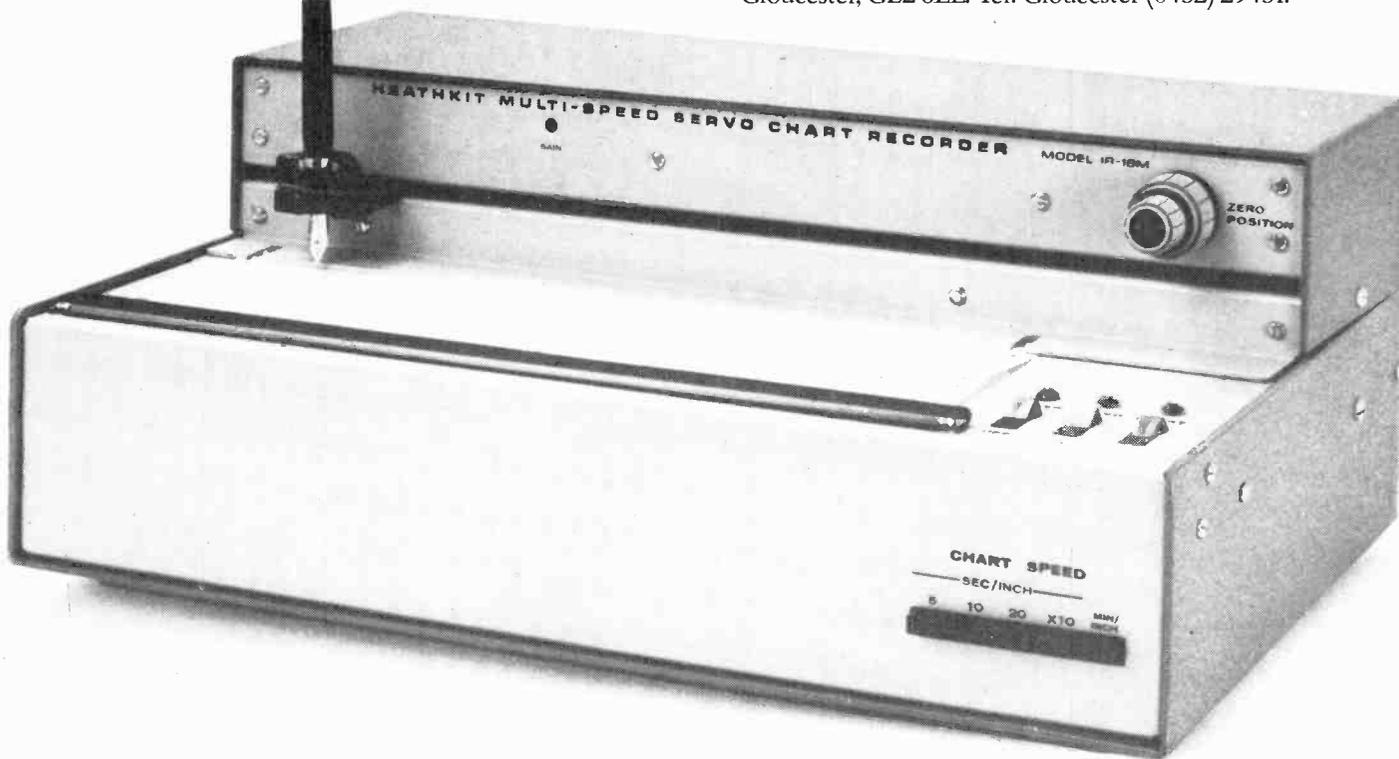
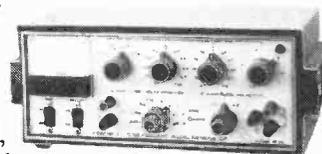
And, for quick accurate testing of diodes, FETs, transistors, SCRs and triacs, there's the IT-121 Tester kit.



You can see these and other Heathkit electronic kits at the London Heathkit Centre, 233 Tottenham Court Road. Or at our showroom in Bristol Road, Gloucester.

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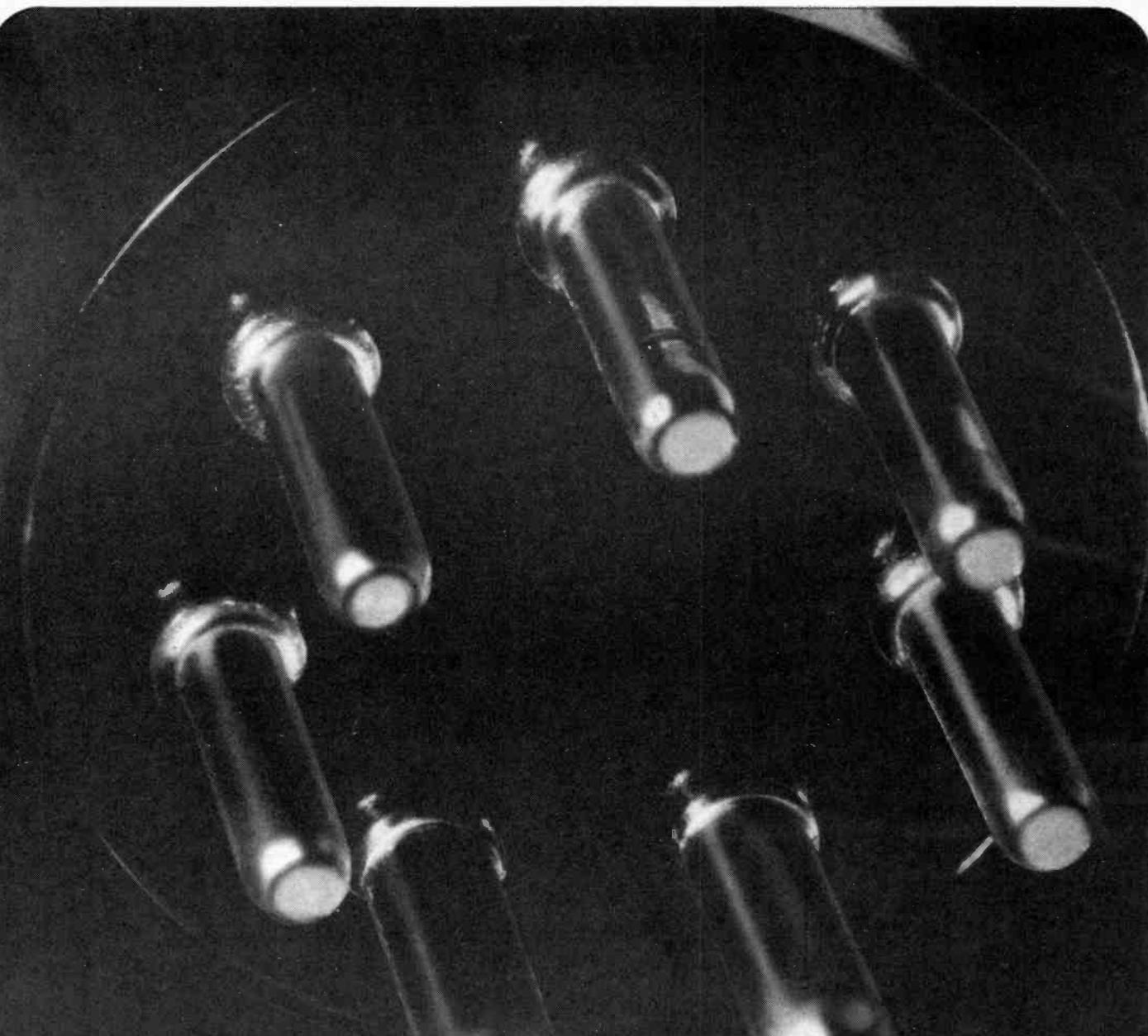
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Teonex offers more than 3,000 devices. They are competitively priced and they are superlative in performance, because the company imposes strict quality control. Teonex concentrates entirely on export and now operates in more than sixty countries, on Government or private contract. All popular types in

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**Electronic valves, semi-conductors and integrated circuits available only for export.**



## sounds international

WW—126 FOR FURTHER DETAILS



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The extra  
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It's a revelation, to watch a KEF speaker being made. No automated process, but one where the final result still depends on the hands that build it. And on the philosophy of the company . . . an exceptional concern that rejects cheaper materials or short cuts . . . searches always for design advances that lead to that ultimate in performance. A philosophy that takes care, even over the smallest details. Feed wires secured so that they never rattle. Ordinary wadding replaced by consistent pre-formed blocks of special acoustic foam. Every drive unit is KEF made, tested at every stage. Even the build-it-yourself Kefkits are individually tested in the correct enclosure. The next time you hear a KEF speaker you'll know why it sounds better. Return the completed coupon for detailed literature.

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the speaker  
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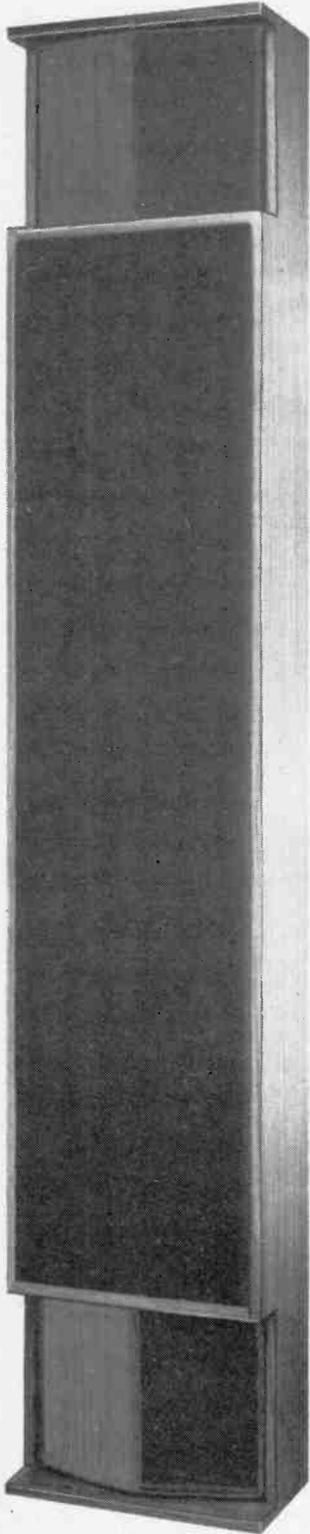
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WW-053 FOR FURTHER DETAILS

# audix

SOUND SYSTEMS AND ELECTRONICS

CL 750/H2 75 watts  
Theatre Column

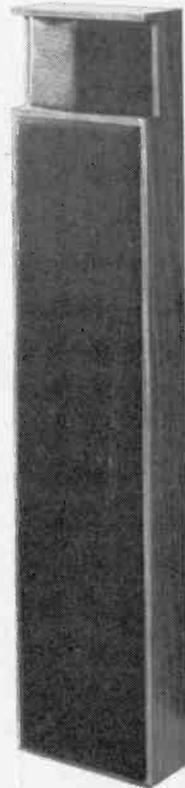


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A new exciting range of column loudspeakers, designed to combine excellent sound reproduction with good appearance and reasonable price. Cabinets are manufactured from heavy gauge afrormosia timber and are fitted with matched high quality driver units and 100 volt line transformers. The frequency response of the larger columns is maintained to the upper end of the audio spectrum by high frequency driver units, mounted in separate acoustic chambers. A forest green vynair grille completes the assembly and semi concealed brackets permit rapid installation.

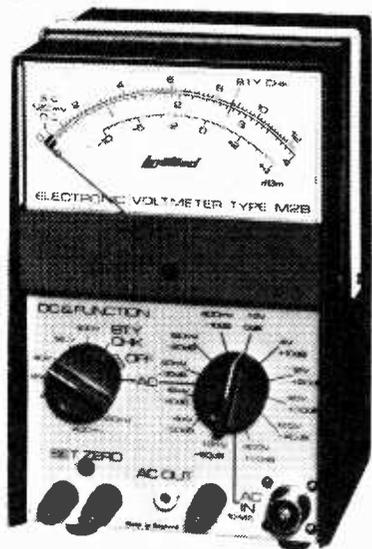
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MANUFACTURERS OF  
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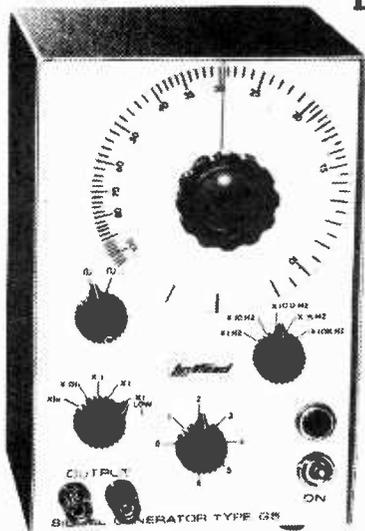
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(4 lines) (STD 0279)

WW—128 FOR FURTHER DETAILS

# Linstead Laboratory Instruments



**M2B** **WIDE RANGE MILLIVOLTMETER**  
High impedance millivoltmeter with 20 scales total measurement range 60 micro-amp a.c. to 400 volts d.c., 10-megohm input with overload protection and frequency range of 500 kHz.  
**£41.80**



**G5** **WIDE BAND SIGNAL GENERATOR**  
Sine-square wave wide band high power signal generator. 10 Hz-1 MHz. 0-6 volts r.m.s., 3 watts into 5 ohms incorporating short circuit protection.  
**NUFFIELD SPECIFICATION 181 £43.80**

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Denmark, Scarfysek, 13-15 Hjørringgade, DK 2100, Copenhagen.

Sweden, EMI Svenska A/B, Tritonvagen 17, Fack. 171 19 Solna 1.

Norway, EMI Norsk A/S, Postboks 42 Korsvoll, Oslo 8.

Malaysia, Laboratory Equipment Sdn. Bhd., P.O. Box 60, Batu Pahat.

Benelux, A.S.E. Ltd., Nationalestraat 38, B-2000 Antwerp.

WW-072 FOR FURTHER DETAILS

## Pin and varactor diodes for switching and tuning.

The types of PIN and varactor diodes listed here represent only a small part of the total AEI capability which includes devices widely used in both civil and military communications equipment. A number are available as DEF STAN types to Nato stock numbers.

With PIN diodes a wide range of silicon chips can be used in a number of outlines offering a large choice of switching speeds, breakdown voltage and resistance-vs-current values.

As for varactors, our diodes can be supplied singly, or in matched sets to a range of capacitance tolerances, breakdown voltages and Q's etc.

### PIN SWITCHING DIODES Miniature Epoxy-Package Diodes

Type No.	Package	V <sub>R</sub> (min.) V	R <sub>F</sub> (max.) ohms at mA	C <sub>d</sub> (max.) at 50V pF	Life-time (typ) μS	R <sub>th</sub> °C/W	High Rel. types
DC1016	36	250	0.75 at 100 5.0 at 5	0.7	1.0	40	*
DC1028A	08	250	1.1 at 100	0.45	0.7	350	**

\* available to DEF STAN specification.

\*\* available to commercial High Rel. specification.

### WIRE ENDED GLASS-PACKAGED DIODES

Type No.	Application	V <sub>B</sub> Volts	R <sub>F</sub> (max) at 100mA ohms	C <sub>d</sub> (max) at 100V pF	τ (typ) μS
DC2840E	General purpose	250	1.0	0.3	0.3
DC2825E	General purpose	200	1.0	0.4*	0.3
DC2841E	General purpose	200	1.5	0.4	0.3
DC2842E	General purpose	200	2.0	0.25	0.5
DC2843E	High speed	100	1.0	0.4	0.05
DC2844E	High speed	100	1.5	0.4	0.05
DC2845E	Long lifetime	150	3.5	0.3	1.5
DC2846E	Long lifetime	150	2.5	0.4	0.7

\* at -50V

### VARACTOR TUNING DIODES

Approximate frequency of application	C <sub>j</sub> (-4V) pF	Type No. (add suffix <sup>1</sup> )	Q(-4V) at stated freq.		Package
			Q	F(MHz)	
500 MHz to 10 GHz	2.2	DC4255B	500	50	35
	2.2	DC4265B	550	50	00
	2.2	DC4285B	550	50	06
	3.3	DC4256B	450	50	35
	3.3	DC4266B	500	50	00
	3.3	DC4286B	500	50	06
	4.7	DC4267B	450	50	00
5 MHz to 1 GHz	6.8	DC4210B	450	50	7
	15	DC4214B	400	50	7
	27	DC4217B	300	50	7
3 MHz to 100 MHz	47	DC4225C	140	50	14
	68	DC4227C	120	50	14
1 MHz to 30 MHz	80	DC4228C	100	50	14*
	100	DC4232B	200	10	18**
	120	DC4233B	200	10	18
	150	DC4234B	200	10	18
100 kHz to 5 MHz	210	DC4298	180 <sup>2</sup>	25	10
	270	DC4232C	750	1	78
	350	DC4299	200 <sup>2</sup>	25	10*
	350	DC4244C	500	1	78**

\* available to DEF STAN specification. \*\* available to commercial High Rel. specification.

Notes: <sup>1</sup>Suffixes A, B, C indicate MWV at 25°C of 30V, 60V, 90V respectively. Preferred types shown. <sup>2</sup> Measured at -8V

For full details of the complete range please write to AEI Semiconductors Ltd., Lincoln Telephone: 0522 29992, or call in at your local distributor.

**AEI**  
**SEMICONDUCTORS**

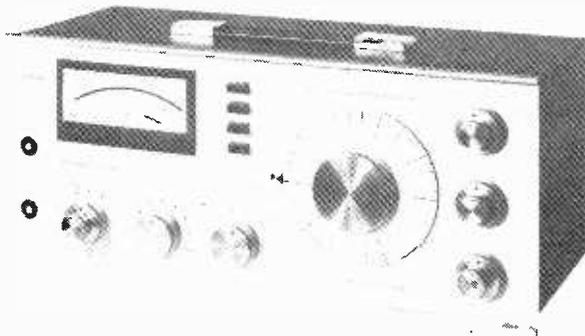
Part of GEC Electrical Components Group.

Also immediately available from: Black Arrow (Electronics) Ltd., Bristol (0272) 294313/Coventry Factors Ltd., Coventry (0203) 24091/Farnell Electronic Components Ltd., Leeds (0532) 636311/LST Electronic Components Ltd., Chelmsford (0245) 69543/W.S. McMillan & Co. Ltd., East Kilbride 38641/4./JVN Components, Bromley, Kent 01-464 1245/TI Supply Ltd., Slough 33411/SDS Components Ltd., Portsmouth 65311.

WW-111 FOR FURTHER DETAILS



## AUDIO MEASURING INSTRUMENTS



### LOW DISTORTION OSCILLATOR SERIES 3

A continuously variable frequency laboratory oscillator with a range 10Hz–100kHz, having virtually zero distortion over the audio frequency band with a fast settling time.

Specification:	
Frequency range:	10Hz–100kHz (4 bands)
Output voltage:	10 volts r.m.s. max.
Output source resistance:	150 ohms unbalanced (optional 150 ohms unbalanced, plus 150/600 ohms balanced/floating)
Output attenuation:	0–100dB (eight, 10dB steps plus 0–20dB variable)
Output attenuation accuracy:	1%
Sine wave distortion:	Less than 0.002% 10Hz–10kHz (typically below noise of measuring instrument)
Square wave rise and fall time:	40/60 n.secs.
Monitor output meter:	Scaled 0–3, 0–10, and dBV.
Mains input:	110V/130V, 220V/240V
Size:	17" (43cm) X 7" (18cm) high X 8 $\frac{3}{4}$ " (22cm) deep
Price:	150 ohms unbalanced output: £250 150/600 unbalanced/balanced floating output: £300

### DISTORTION MEASURING SET, SERIES 3

(illustrated above)

A sensitive instrument with high input impedance for the measurement of total harmonic distortion. Designed for speedy and accurate use. Capable of measuring distortion products down to 0.001%. Direct reading from calibrated meter scale.

Specification:	
Frequency range:	5Hz–50kHz (4 bands)
Distortion range (f.s.d.):	0.01%–100% (9 ranges)
Input voltage measurement range:	50mv–60V (3 ranges)
Input resistance:	47K ohms on all ranges
High pass filter:	12dB/octave below 500Hz
Power requirement:	2 X PP9, included.
Size:	17" (43cm) X 7" (18cm) high X 8 $\frac{3}{4}$ " (22cm) deep
Price:	£200

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**Bristol BS3 2HZ  
Telephone 0272 662301**

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Miniature and sub-miniature lamps are Vitality's speciality and the range available is one of the most comprehensive in Europe.

Write for the Vitality catalogue for full details on the range and application notes, or phone us if you have a special requirement for conventional or unusual environments, wherever a light source is needed for illumination, reference, indication or warning.

# Vitality Ltd

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Telephone: Bristol (0272) 294313. Telex: 449150

Farnell Electronic Components Ltd.

Canal Road, Leeds LS12 2TU

Telephone: Leeds (0532) 636311. Telex: 55147

Townsend-Coates Ltd., Coleman Rd., Leicester LE5 4LP

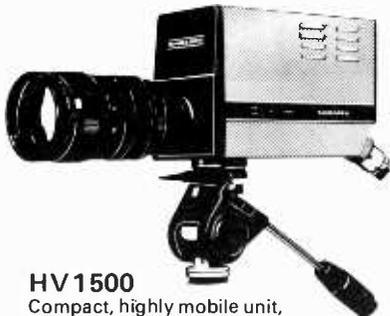
Telephone: Leicester (0533) 768561. Telex: 34321

Valiant Electrical Wholesale Company,

20 Lettice St., Fulham, London SW6 Tel: 01-736 8115

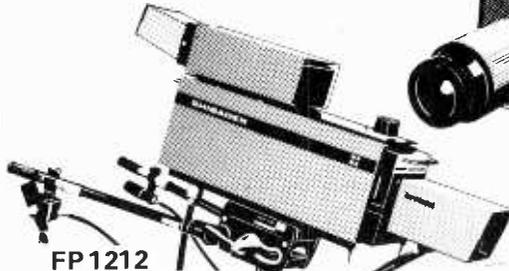
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# 5 good reasons why Shibaden colour cameras are the best!

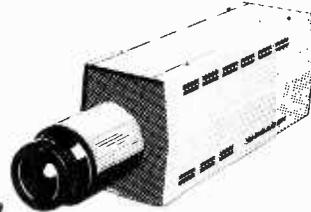


**HV 1500**  
Compact, highly mobile unit, the only colour CCTV camera available with a single one-inch filter integrated colour vidicon tube.

**FP 1500** As the HV 1500 but fitted with a 3" viewfinder for studio use.



**FP 1212**  
A one-inch three tube Plumbicon® Camera with freely detachable electronic viewfinder. Ideal for outside broadcast work and studio.



**HV 1100**  
An extremely compact, lightweight three tube colour TV camera ideal for surveillance and observation applications.



**FPC 1000**  
A vidicon/chal'nicon camera designed to meet all NTSC and PAL requirements.

® Trade Mark N.V. Philips

The Shibaden range of colour cameras are compact, easy to operate and versatile in their application through educational, medical, business and broadcasting studios. Shibaden Colour Cameras are designed with the customer in mind both from an application and performance stand point. They are fully backed by Shibaden's in-depth opto-electronic technology, which has proved to be superior through many years of application in a vast range of broadcasting equipment.

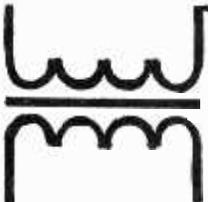
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*For further details on the Shibaden range of Colour Cameras, contact the Technical Service Department.*



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BROADCAST & CCTV EQUIPMENT MANUFACTURERS  
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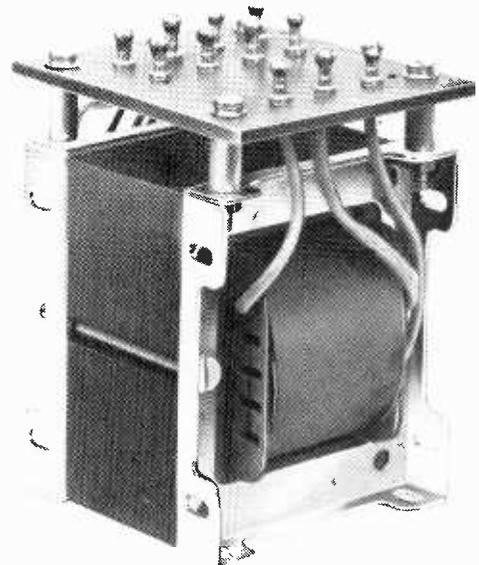
## transformers

mains, audio, microphone, ferrite core and other wound components

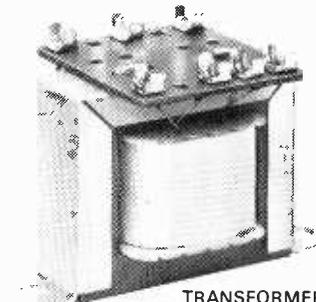
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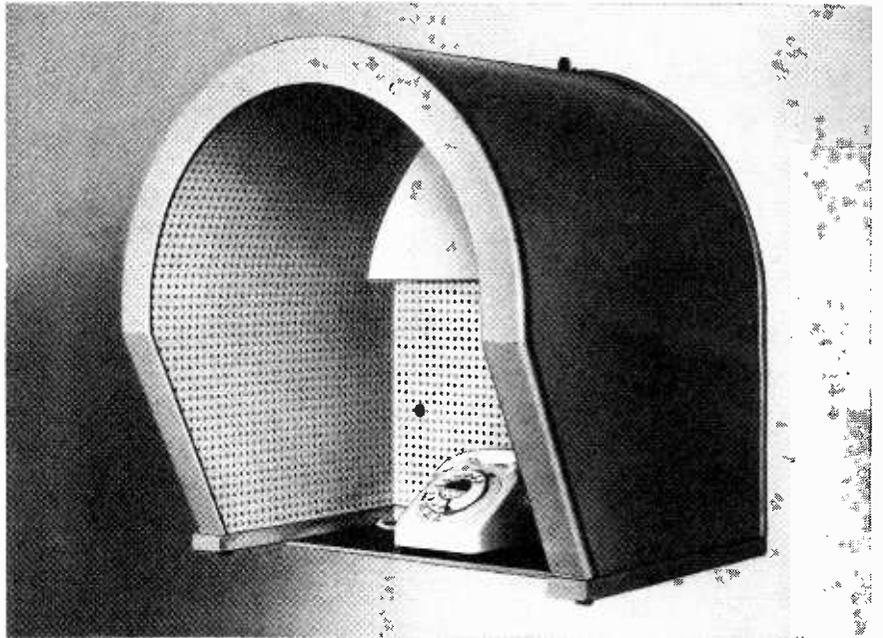
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# Whiteley

## Acoustic Hoods

These strongly made hoods for both outdoor and indoor use are designed to specifications which meet Post Office approval. Suitable for desk, shelf or wall mounting, they are available with or without internal light fittings and doors if required.



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McLennan Engineering are pioneering in the field of digitized liquid delivery. The equipment illustrated is suitable for medical, veterinary, chemical and general laboratory applications.

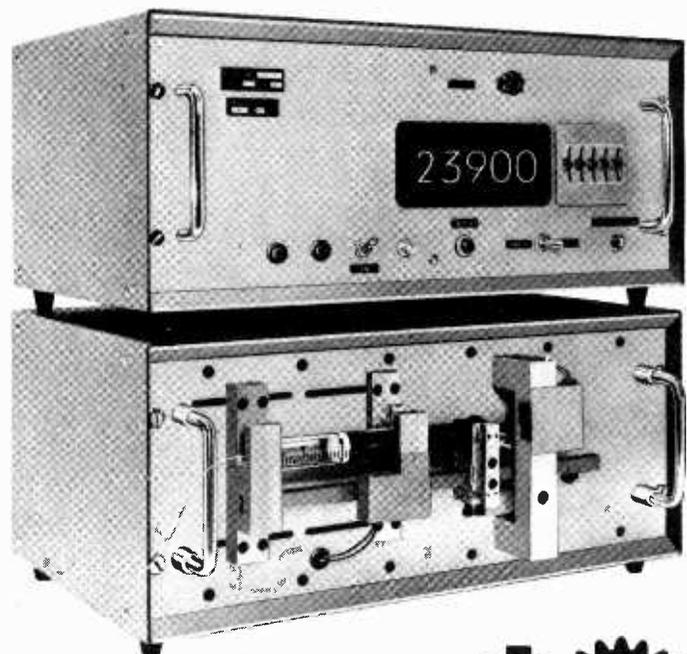
### DIGITAL SYRINGE TYPE DS110

Fluid pulse 1.0 or 10 micro litres  
Number of pulses presettable from 1–50,000  
Pulse rate 400Hz–1 Hz or .01 Hz in the case of frequency divider model  
Digital 'fluid delivered' display monitors output at all times  
External B.C.D. signals can programme the number of pulses  
Remote multiple syringe facility  
High reliability. Drive designed around Impex stepper motor system.

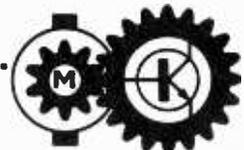
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If you have a problem in any of the above fields we shall be pleased to discuss your special requirements. Please get in touch – it costs nothing to talk.

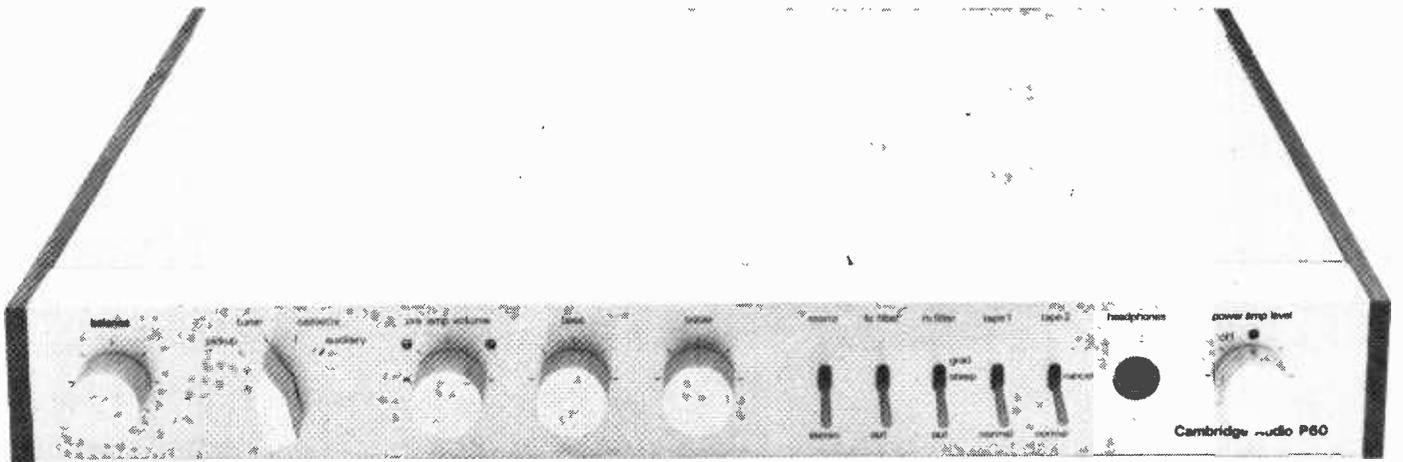


**McLennan Engineering Ltd.**  
CONTROL SYSTEMS AND COMPONENTS  
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\*Peak level indicator for tape recording.  
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International state-of-the-art circuitry from Cambridge Audio in Britain.

\*To the best of our knowledge these features have never been included in a comparable amplifier hitherto.



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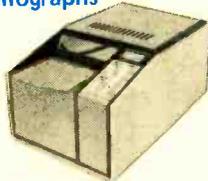
Address .....

WW15

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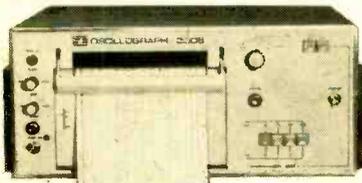
# SE Labs recorders

## Light-beam Oscillographs



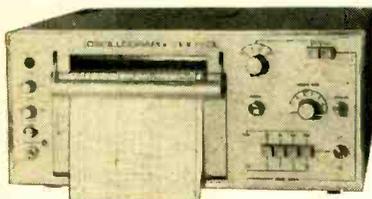
### SE692 Portable Recorder

6 channels on a four speed 92mm chart. Low cost galvanometers up to 2kHz. AC mains and/or dc power input. Only 2.2 amps and weighing in at 7.6 kg — a truly portable recording package at a good price.



### SE3006 U.V. Recorder

The best "all rounder" for simple straight forward recordings. No fuss no frills performance at a very economical price. 6 in. chartwidth up to 12 channels.

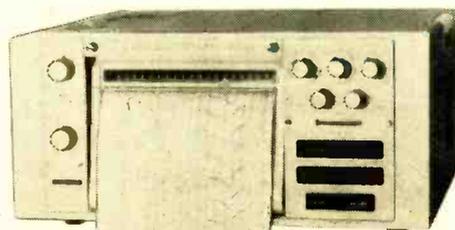


### SE3006DL U.V. Recorder

De-Luxe performance at low cost, 6 in chartwidth, 12 channels. Full facility unit.

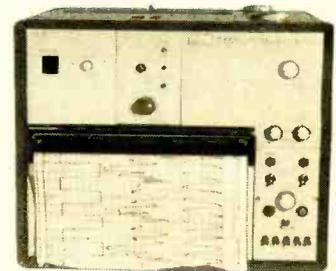
### SE6008 U.V. Recorder

Our latest model - superb performance at really economical cost. 8 in. chartwidth, servo drive to 4M/sec. Up to 25 channel capability, many, many novel features.



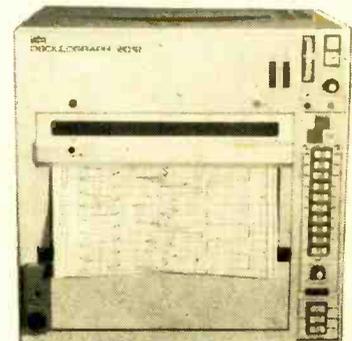
### SE3008 U.V. Recorder

Tried and proven model - a general purpose "workhorse". 8 in. chartwidth. 25 channels. Many options.



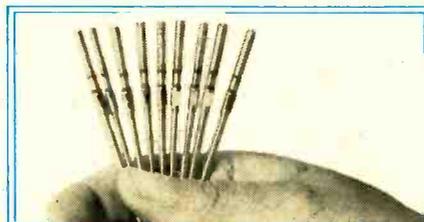
### SE2112U.V. Recorder

Another tried and proven model - 12 in. chartwidth economically priced. Many options available. Up to 50 channel capability.



### SE6012 U.V. Recorder

Our ultimate model - the latest technology coupled with years of experience. 12 in chartwidth 50 channels. 5M/sec forward, reverse drive, integral take up etc.

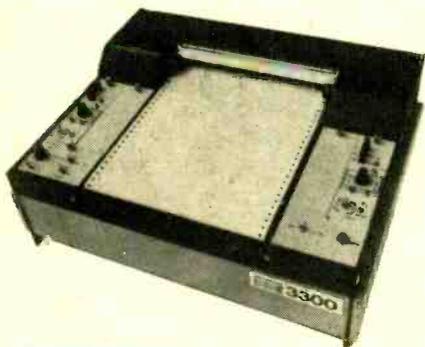


### Galvanometers

SE precision galvanometers provide these oscillographs with measurement sensitivities from  $0.8\mu\text{A/cm}$  to  $36\text{ mA/cm}$  and high fidelity recording capability from 0 to 8kHz.

# the image makers

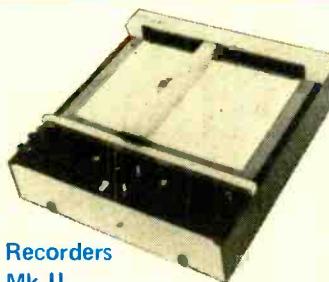
## Potentiometric Recorders



### SE3300 Series

A versatile series of recorders and modules for all applications of potentiometric recording. Single and two pen versions. A choice of writing mechanisms. Input modules for differing sensitivity requirements and many add on function modules eg. AC true RMS, integrating module, etc. Build up from a simple single channel unit to a complex 8 channel dot recorder!

Two new models for A3 operation to be announced shortly!



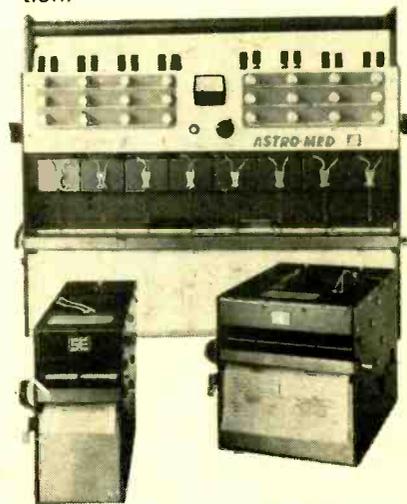
### X - Y Recorders SE225 Mk II

A general purpose X - Y recorder with a good specification at a realistic price. Choice of sensitivity configuration giving a maximum 0.05V/cm on an A4 chart. A compact unit with many features and a specification to equal more expensive recorders. Time base unit gives added versatility and there is also a chart adaptors available.

**Galvanometric Heat Stylus Recorders**  
Economical direct write units. Single double, triple channel recorders with vertical or horizontal chart travel. Frequency response to 100Hz Sensitivities 10mV/mm choice of chart speeds; full 50mm pen travel; available in OEM or cased configurations.

### Super 8

Superlative performance from this eight channel pen recorder. Unique variable drive from 0.25 to 100mm/sec. Frequency response to 100 Hz; Sensitivity 10mV/mm; channel width full 50 mm: OEM configuration.



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*For a small charge you can hire any of the instruments shown here; singly or as part of a system which we can design for you.*

*If you decide later to purchase the equipment, we can refund part of the hire fee to you.*

*You save your capital and space. You beat obsolescence.*

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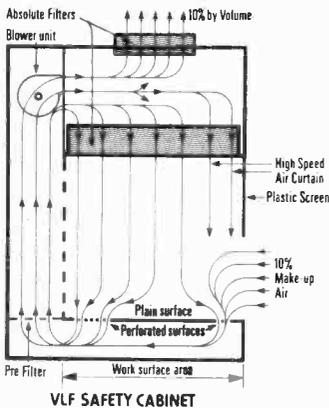
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# HEPAIRE PATHOLOGICAL



## SAFETY CABINET



### Positive Immunity

Cabinet design ensures full protection for operative plus sterile working conditions. Filtration efficiency 99.999% D.O.P. minimum on both main and dump filters. Minimum bench space required. Uses standard single phase electrics. Range of optional extras can be fitted. Extremely clean appearance.

### Designed for Safety

Cabinet of fully recirculating type as shown in diagram. 90% of air forced into plenum passes through main HEPA filter into working area and 10% is "dumped" through the HEPA filter in top of cabinet. 10% "make-up" air is drawn in through the open front of the cabinet and passes through the narrow perforated strip immediately in front of the work surface, thus forming a barrier between the working area and outside atmosphere and ensuring that "dirty" air cannot leak from cabinet.

For gassing out purposes the dump filter can be sealed by the blanking plate supplied and a separate screen clipped into place beneath the hinged front screen. Sterilising gas is introduced and extracted using the two gas taps provided.

Write for further technical details.



## HEPAIRE MANUFACTURING LTD

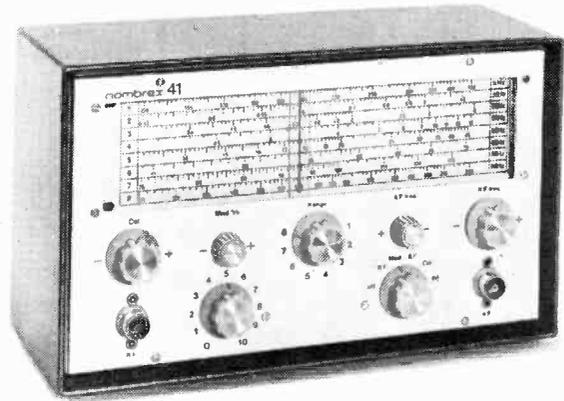
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PLUS 8% FOR V.A.T.

- ★ 150 KHz — 220 MHz on fundamentals.
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- ★ Spin-Wheel Slow Motion Drive 11 — 1 ratio.
- ★ Overall Accuracy — 2½%.
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- ★ Internal Crystal Oscillator providing calibration checks throughout all ranges.
- ★ Mechanical scale adjustment for accurate alignment against internal 1MHz crystal oscillator.
- ★ Powered by 9V Battery.

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Send for full technical leaflets.

Post and Packing 50p. extra.

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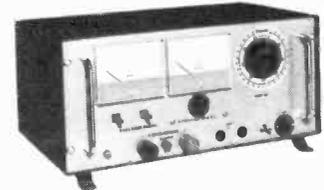
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## POWER UNITS

NOW AVAILABLE WITH 3  
VARIABLE OUTPUTS



Type VRU/30/25—£166.75 + 8% VAT

Input 200–250V. 50Hz  
or 100–120V. 60Hz to order  
Output 1: 0–30V. 25A. D.C.  
Output 2: 0–70V. 10A. A.C.  
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Other units are also available  
with outputs of:  
0–60V 12A.  
0–120V 6A.  
0–240V 3A.

ALL CONTINUOUSLY  
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# ANDERS MEANS METERS...

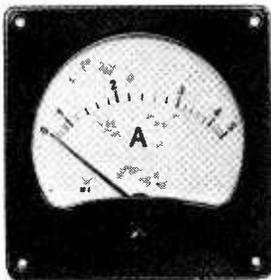
## PRESTIGE RANGE

- High accuracy and stability
- Clear Sperry Display
- Automatic zero-ing
- High noise rejection (78 db CMR)
- Extremely versatile
- Competitive prices.

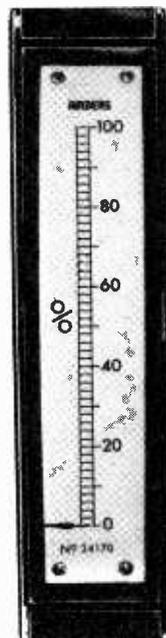


Anders provide what is probably the largest range of meters available from a single source in Europe: MC/MI, dynamometer, vibrating reed, electrostatic, etc. in over 100 case styles and sizes, a few of which are shown below.

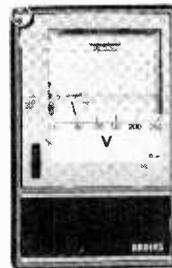
Popular models and ranges are stocked in depth while a specially equipped instrument department enables swift production of non-standard ranges and scales, to suit individual customer requirements, in large or small quantities.



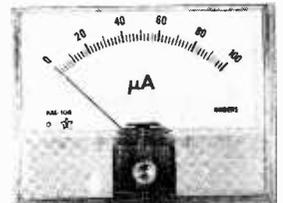
Vulcan Moving Iron. 4 models, 1.5", 1.8", 2.7", 3.7" scales. Voltmeters, ammeters and motor starting meters.



Profile 350 edgewise 4.3" scale. DC moving coil and AC moving coil rectified. Horizontal or vertical mounting.



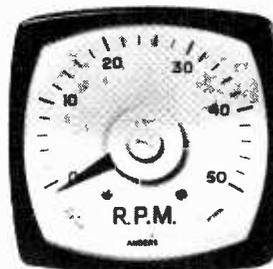
Recorders 60 or 120 mm. charts. Non-ink marking. DC moving coil and AC rectified.



Kestrel Clear Front. 7 models, 1.3" - 5.25" scales. DC moving coil, AC moving coil rectified, AC moving iron.



Regal Range 100° flattened arc. 2 models 2.5" and 3.2" scales. Taut band. DC moving coil and AC moving coil rectified.



Stafford Long Scale 240°. 6 models, 3.5"-11.5" scales. DC moving coil, AC moving coil rectified, AC moving iron. Also 98° scale.



Lancaster Long Scale 240°. 2 models, 4", 5.5" scales. DC moving coil and AC moving coil rectified.

Send for fully illustrated catalogue

**ANDERS ELECTRONICS LIMITED** 48/56 Bayham Place, Bayham Street, London, N.W.1. Telephone 01-387 9092.

Manufacturers and distributors of Electrical Measuring Instruments. Sole U.K. distributors of FRAHM Resonant Reed Frequency Meters and Tachometers. Manufacturers of purpose built electrical and electronic equipment to customers' requirements.

WW-117 FOR FURTHER DETAILS

# ALICE BROADCASTING GU 100



**£540** + VAT  
DELIVERY 6-8 WEEKS

The 'ALICE' GU 100 turntable unit is a console mounted 'SPARTA' GT-12-SY turntable complete with a 'STANTON' tone arm, less cartridge. This, along with a comprehensive 'ALICE' cue/pre-amp unit is mounted into a hand finished teak console built by our own craftsmen to standards that are hard to beat. Locking castors are used to allow the console to be easily moved to any required operating position.

## TECHNICAL SPECIFICATION

Input sensitivity	5 millivolts for 0dBm out at 1kHz.
Freq. response	to R.I.A.A. curve.
Output level	0dBm into 600Ω bal., other levels as requested.
	Outputs appearing on switch craft XLRs.
Stereo separation	70dB typical (electronics only).
Power requirements	240V 50Hz or 117V 60Hz.
Remote start	Relay operated.
Cue amp	5 watts RMS to internal speaker.
Turntable acceleration	less than $\frac{1}{16}$ turn to full rpm.
Turntable platter	European (flat platter).
	American (7" record centre well).
Platter weight	6 lb (2.75 kg).
Turntable speeds	45 & 33 $\frac{1}{3}$ rpm. 78 rpm available.
Console weight	106 lb (48 kg).
Dimensions	22 $\frac{1}{2}$ " deep, 24" wide, 32 $\frac{1}{2}$ " high to top of tone arm.

## OTHER ALICE PRODUCTS INCLUDE

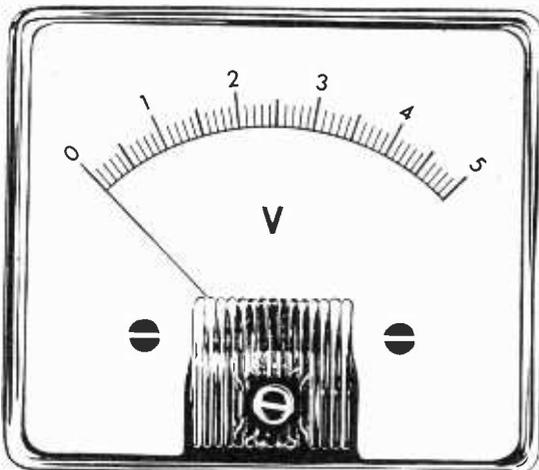
RACK MOUNTING DISTRIBUTION AMPS 6/24  
RACK MOUNTING TELEPHONE BALANCING UNIT  
RACK MOUNTING PRE-VIEW MONITORS  
BROADCASTING AND RECORDING CONSOLES, ETC.

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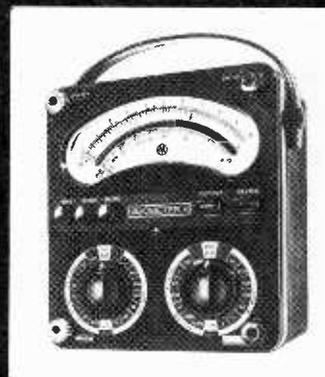
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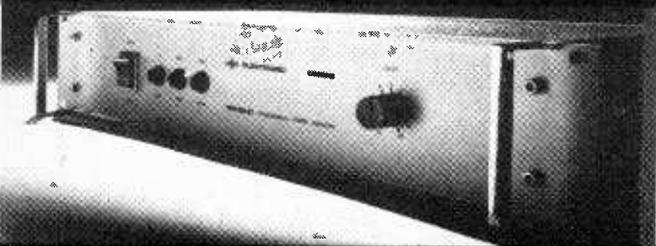
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Freq Response	$\pm 0.1$ dB 20Hz to 20KHz into 15 ohms. -1dB at 150KHz
Total harmonic distortion	Less than 0.04% at all levels up to 50 watts rms into 15 ohms
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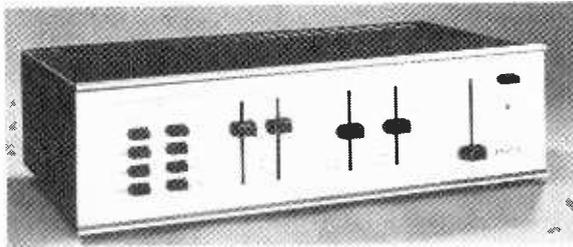
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**Power output.**

**Rated:** 50 watts average continuous power per channel, into any impedance from 4 to 8 ohms, both channels driven.  
**Maximum:** 90 watts average power per channel into 5 ohms load.

**Distortion.**

**Pre-amplifier:** Virtually zero. (Cannot be identified or measured as it is below inherent circuit noise.)  
**Power amplifier, at rated output:** Less than 0.02% (typically 0.01% at 1kHz).  
**at 25w output:** Typically 0.006%.

**Overload margin.**

Disc input 40 dB min.

**Hum and noise output.**

**Disc:** —83dBV Measured flat with noise bandwidth of 23kHz (ref. 5mV.)  
 —88dBV Measured with 'A' weighted characteristic (ref. 5mV.)  
**Line:** —85dBV Measured flat (ref. 100mV.)  
 —88dBV 'A' weighted (ref. 100mV.)  
**Size:** 17 inches × 4 $\frac{3}{4}$  inches × 11 inches deep overall.  
**Weight:** 21 lb.

Write or phone for leaflet which describes the design philosophy and conception of the HD250 together with a complete specification.

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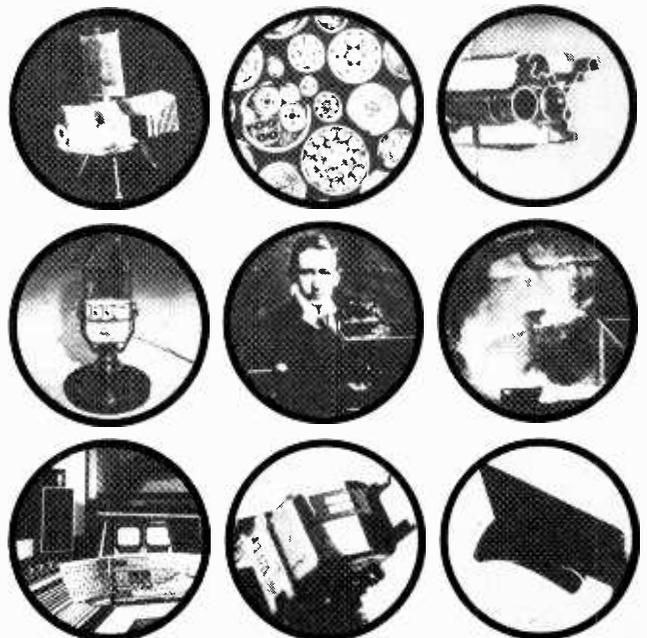
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(6 Position)

('WW' JUNE '73)

Exclusive Designer Approved Kits

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- VARICAP** tuning diodes in back to back configuration for low distortion.
- CERAMIC** filters for defined IF response.
- INTEGRATED** circuit IF amplifiers for reliability and excellent limiting/AM rejection.

- PHASE LOCKED** Stereo decoder with Stereo mute, see below
- LED** fine tuning indicators.
- PUSH BUTTON** tuning (with AFC disable) over the FM band (88-104).
- IC STABILISED** and S/C protected power supply.
- CABINET** double veneered against warp.

The Nelson-Jones Tuner has all of these features and many more, and more importantly the design is fully proven not just with a few prototypes but with many thousands of working tuners spread across the world.

Typ. Specn: 20 dB quieting 0.75uV. Image rejection —70dB.I.F. Rejection —85 dB

Basic tuner module prices start as low as **£12.31**, with **complete** kits starting at **£26.95** (mono) + P.P. 65p. and of course all components are available separately.

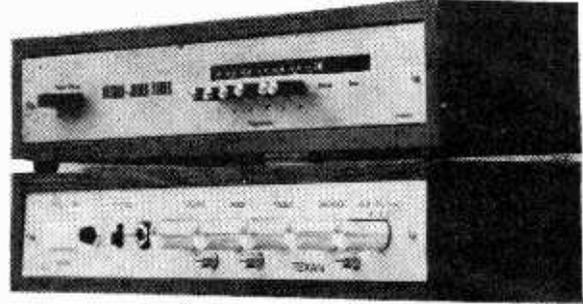
Our low cost **alignment service** is available to customers without access to a signal generator. Please send large SAE for our latest price lists which details all of the many options and special low prices for complete kits. All our other products remain available.

**PORTUS AND HAYWOOD PHASE LOCKED DECODER** (W.W. Sept. '70). Still the lowest distortion P.L. decoder available. THD typically 0.05% (at Nelson-Jones Tuner O/P level)! Supplied complete with Red LED.

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**PLEASE NOTE.** Existing tuners are readily convertible and kits/parts are available for this purpose.

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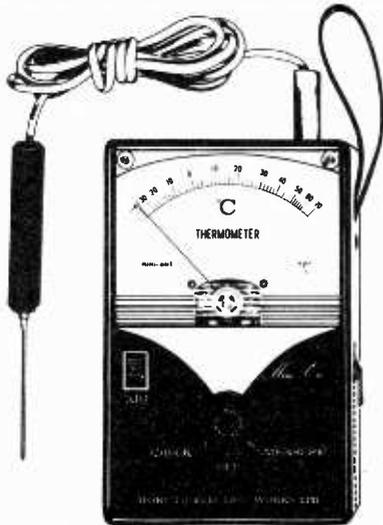
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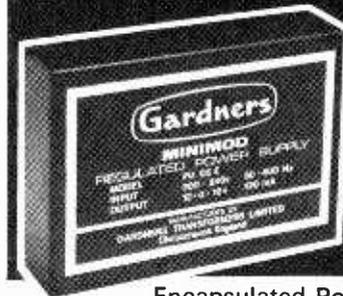
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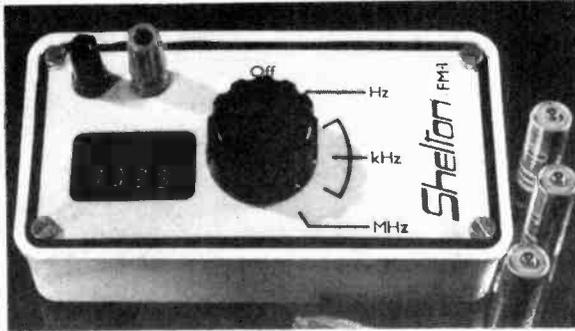
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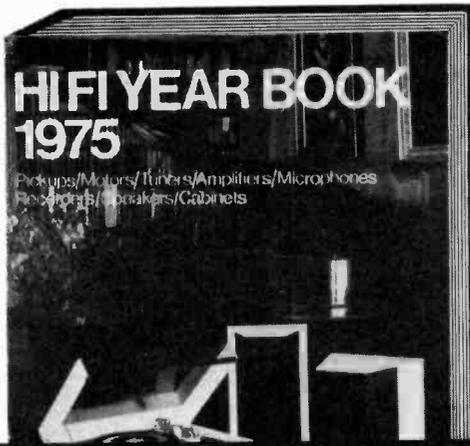
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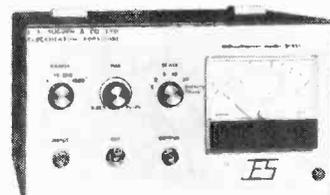
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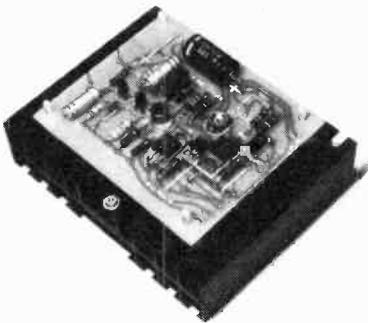
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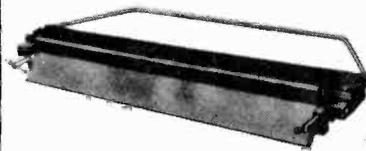
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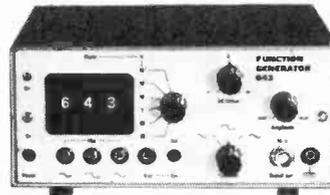
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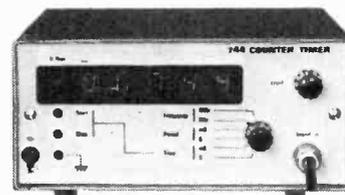
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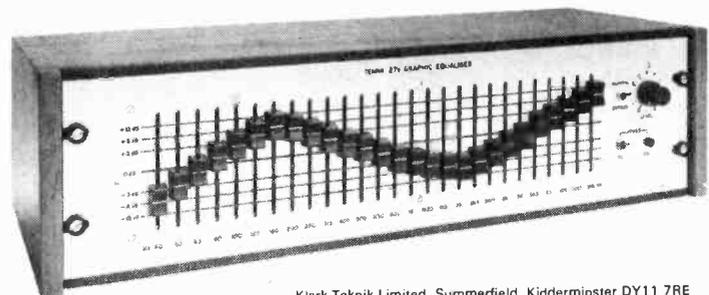
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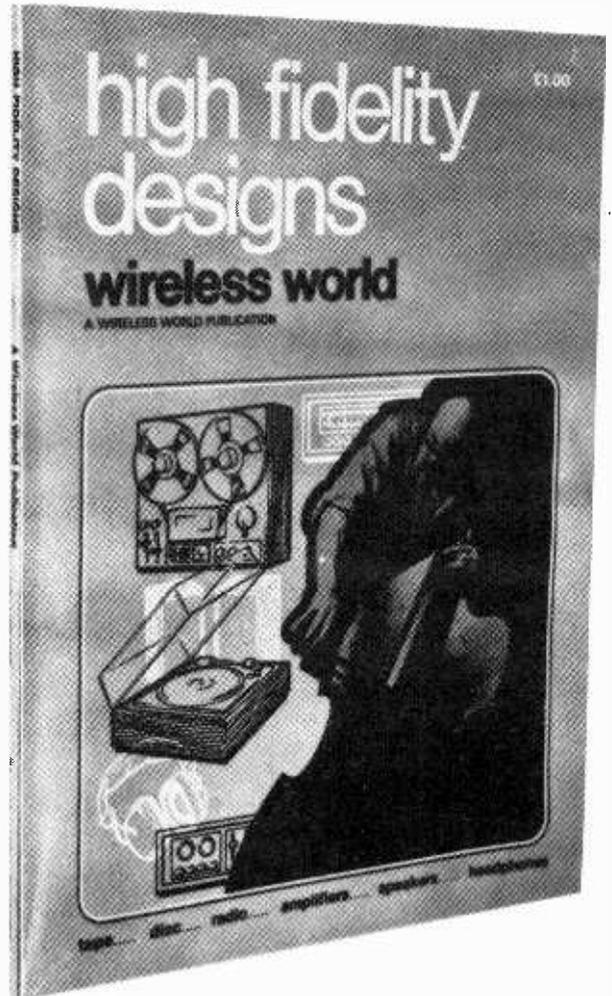


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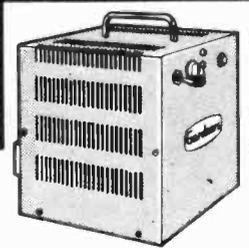
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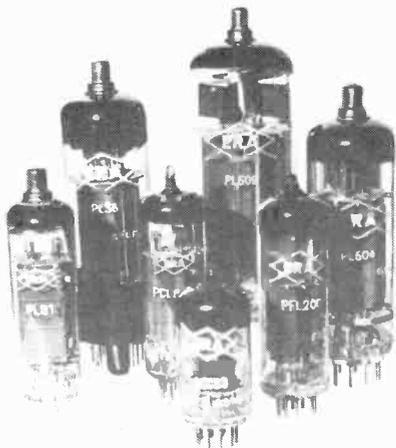


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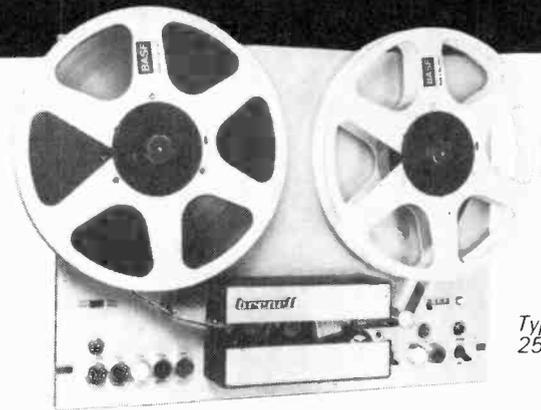
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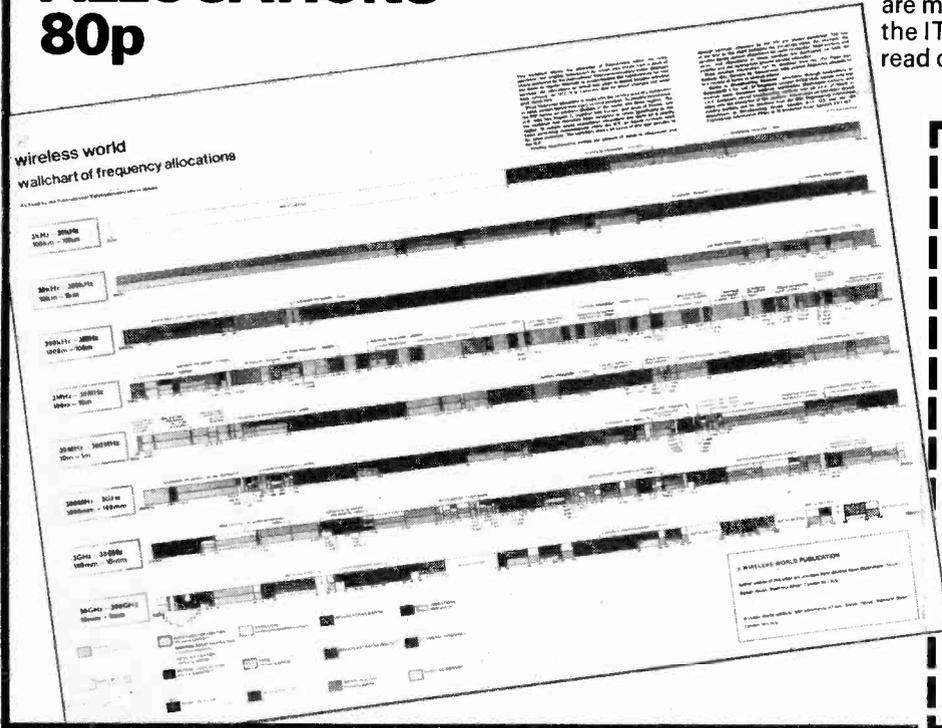


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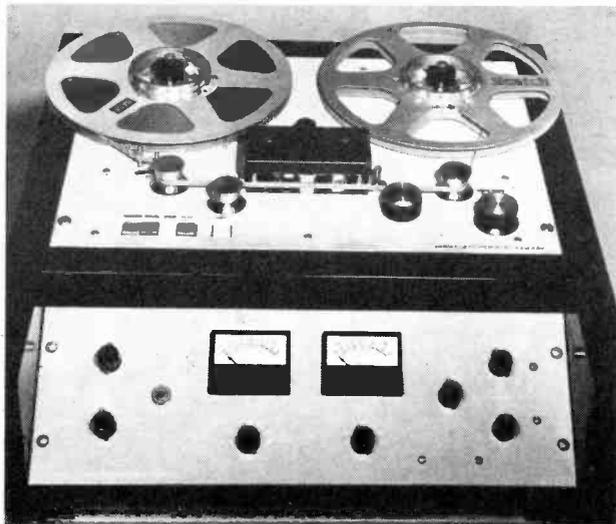
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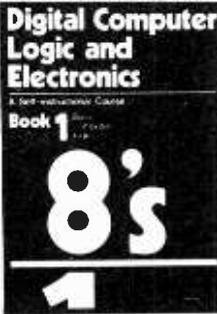
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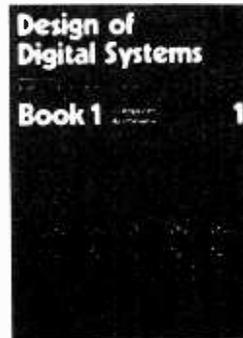
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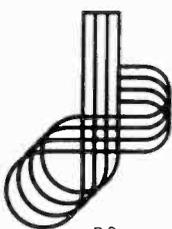
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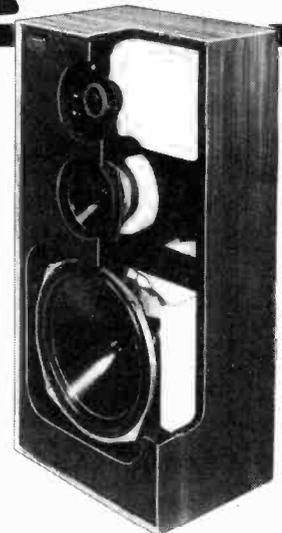
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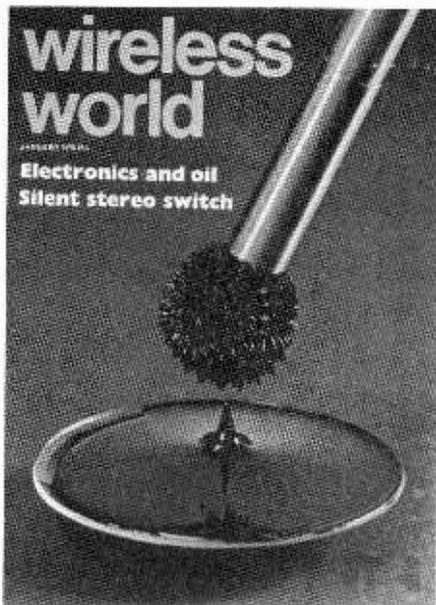


# wireless world

Electronics, Television, Radio, Audio

JANUARY 1975 Vol 81 No 1469

SIXTY-FIFTH YEAR OF PUBLICATION



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## Sharing the spectrum

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In the next two years the Annan Committee will be deliberating on the future of broadcasting in the UK. No doubt it will consider the amount and variety of broadcasting that we should have—bearing in mind the new channels in the broadcasting frequency bands that are likely to become available. But there ought to be another committee, with a wider brief, advising Annan on the amount of broadcasting usage of the radio spectrum there should be in relation to the needs of other users. Of course, the block allocations of frequencies for broadcasting, communications etc. are decided by international agreements, but there is still room for manoeuvre by individual national governments. For example the section of the v.h.f. band 87.5 to 100MHz is internationally allocated to broadcasting, but within the UK the section 97.6 to 102.1MHz is at present occupied by Home Office mobile radio users (the fire, ambulance and police services).

The new channels for broadcasting will be available for both sound and television. The mobile radio users mentioned above will be cleared from the 97.6 to 100MHz section, allowing one more national sound broadcasting network to be set up. Furthermore, the BBC, pointing to the even higher frequencies used for v.h.f. sound broadcasting in other countries, has said that "further clearance to 104MHz is most desirable". This would entail moving out the v.h.f. military communications at present in the section 102.6 to 104MHz. In television there is, of course, spectrum space available for a fourth national u.h.f. network (sometimes incorrectly called a "channel"), the use of which has yet to be decided; and when the present 405-line transmissions in bands 1 and 3 are shut down there will be room here for two more networks of near national coverage or a large number of local television stations. In general the broadcasters' attitude seems to be "we keep what we hold" but the BBC has publicly shown itself to be sensitive about the wasteful duplication of its sound (m.f./l.f. and v.h.f.) and television (v.h.f. and u.h.f.) programmes, which can only be justified on historical grounds and the laudable desire to keep faith with certain groups of listeners and viewers.

It is, of course, mainly the mobile radio manufacturers and users who are interested in these v.h.f. and u.h.f. parts of the spectrum. They are very much aware that in the USA the FCC has recently made available 115MHz of additional space for mobile users in the 900MHz bands. A bold suggestion from one British company is that the broadcasters might be prepared to surrender some of bands 1 and 3 "in exchange for the extended band 2".

The greatest problem of any spectrum advisory committee would be how to weigh against each other the requirements for spectrum space of very different types of users. How is society's need for entertainment, for example, to be balanced against society's need for telecommunications? Such value judgements are in fact already being made because they are implicit in the existing frequency allocations. But they are made under the influence of politicking by interested parties and to this extent it is doubtful if they reflect the true needs of society.

# Classifying f.e.ts

## "A unified view of the f.e.t. jungle"

by B. L. Hart

North East London Polytechnic

A field effect transistor (f.e.t.) is a semiconductor device in which the flow of charge carriers in a "channel" between two terminals, designated source and drain, is controlled by a transverse field resulting from the application of a potential difference between one of these terminals and a third, control, terminal known as the gate. This definition is a convenient starting point and can be extended to include those devices having two gates. The manner in which the control function is achieved, without the requirement of significant d.c. input power, permits a division of f.e.ts into two basic categories, each of which can be further sub-divided.

### Junction-gate f.e.t.

The voltage applied to the reverse-biased p-n junction associated with the gate terminal determines the thickness of the junction depletion layers and this alters the effective dimensions of the conducting channel. The conducting channel may be p-type or n-type material. The jugfet is also known as a j.fet, p-n f.e.t., and sometimes, confusingly, just f.e.t.

### Insulated-gate f.e.t.

The voltage applied to the gate terminal determines the charge induced in a semiconductor material which is electrically insulated from the gate. The induced charge can either establish a conducting channel where none existed before, which is the case with the p- and n-channel "enhancement-mode" devices, or modulate the conductivity of an already existing or built-in channel. This is the case with the p- and n-channel "depletion mode" devices.

Early igfets were made using established bipolar integrated-circuit processing technology and, as a result, had a metal gate and an oxide insulator. This led to the description most (metal oxide semiconductor transistor) or mosfet. Although metal and oxide are not always used mosfet has tended to be used interchangeably with igfet as a generic description of this device type. Cisfet (conductor, insulator, semiconductor) is, arguably, the best description of this group but because of past usage the former terms are unlikely to be displaced.

### General d.c. description

The pear-shaped symbol, shown at (a) opposite, represents an f.e.t. of unspecified type; the arrows represent the sign convention for positive  $I_{DS}$ ,  $V_{DS}$ ,  $V_{GS}$ . The relevant family of  $|I_{DS}|$  versus  $|V_{DS}|$  characteristics is shown at (b), opposite. It is apparent that  $|I_{DS}| \approx 0$  at  $V_{GS} = V_y$ ;  $V_y$  is thus a cut-in, cut-off, or a threshold-of-conduction voltage. For the jugfet,  $V_y$  is usually known as pinch-off voltage and written  $V_p$ , whilst for the igfet,  $V_y$  is normally referred to as the threshold voltage and written  $V_T$ . The form  $|I_{DS}| \approx 0$ , is used because  $V_y$  is often conveniently measured at some specified low leakage current level of a few  $\mu A$ .

When  $|V_{DS}| < |V_{GS} - V_y|$ , the f.e.t. operates in the pre-pinch-off, triode, ohmic, or voltage saturation region. For  $|V_{DS}| > |V_{GS} - V_y|$ , the f.e.t. operates in the pinch-off, constant-current, current-saturation, or pentode region and since the curves are parallel to the  $V_{DS}$  axis we can write an expression for  $I_{DS}$  which does not involve  $V_{DS}$ :

$$I_{DS} = \lambda (V_{GS} - V_y)^2$$

in which  $\lambda$  is a device parameter dependent on material type, doping level, and geometry. The polarities of the quantities in this relationship for the six possible types of f.e.t. are given in the accompanying table.

Device type	Carrier type	$\lambda$	$I_{DS}$	$V_{DS}$	$V_{GS}$	$V_y$
n-channel enhancement igfet	electron	+	+	+	+	+
n-channel depletion igfet	electron	+	+	+	+/-	-
n-channel jugfet	electron	+	+	+	-	-
p-channel jugfet	hole	-	-	-	-	+
p-channel depletion igfet	hole	-	-	-	+/-	+
p-channel enhancement igfet	hole	-	-	-	-	-

The device d.c. relationship with appropriate parameter signs is the basis of the f.e.t. classification chart opposite, which links the transfer characteristic with symbolic representation and a simple cross-section of device construction. Note that the device is only on and in the pinch-off mode for that part of the  $I_{DS}$ ,  $V_{GS}$  parabola which has a positive slope.

The symbols shown, though not used in

all f.e.t. literature, are strongly recommended because they permit instant recognition of device type without supplementary explanation. A thick continuous line connecting s and d indicates that for  $V_{GS} = 0$   $|I_{DS}| = |I_{DSS}| > 0$ . All devices so drawn are termed depletion f.e.ts. In some texts depletion-mode igfets are referred to as normally-on or depletion/enhancement devices, but this can be confusing and is not recommended. A thick broken line connecting s and d indicates that for  $V_{GS} = 0$ ,  $|I_{DS}| \approx 0$ ; as a result such a device has been referred to as a normally-off igfet.

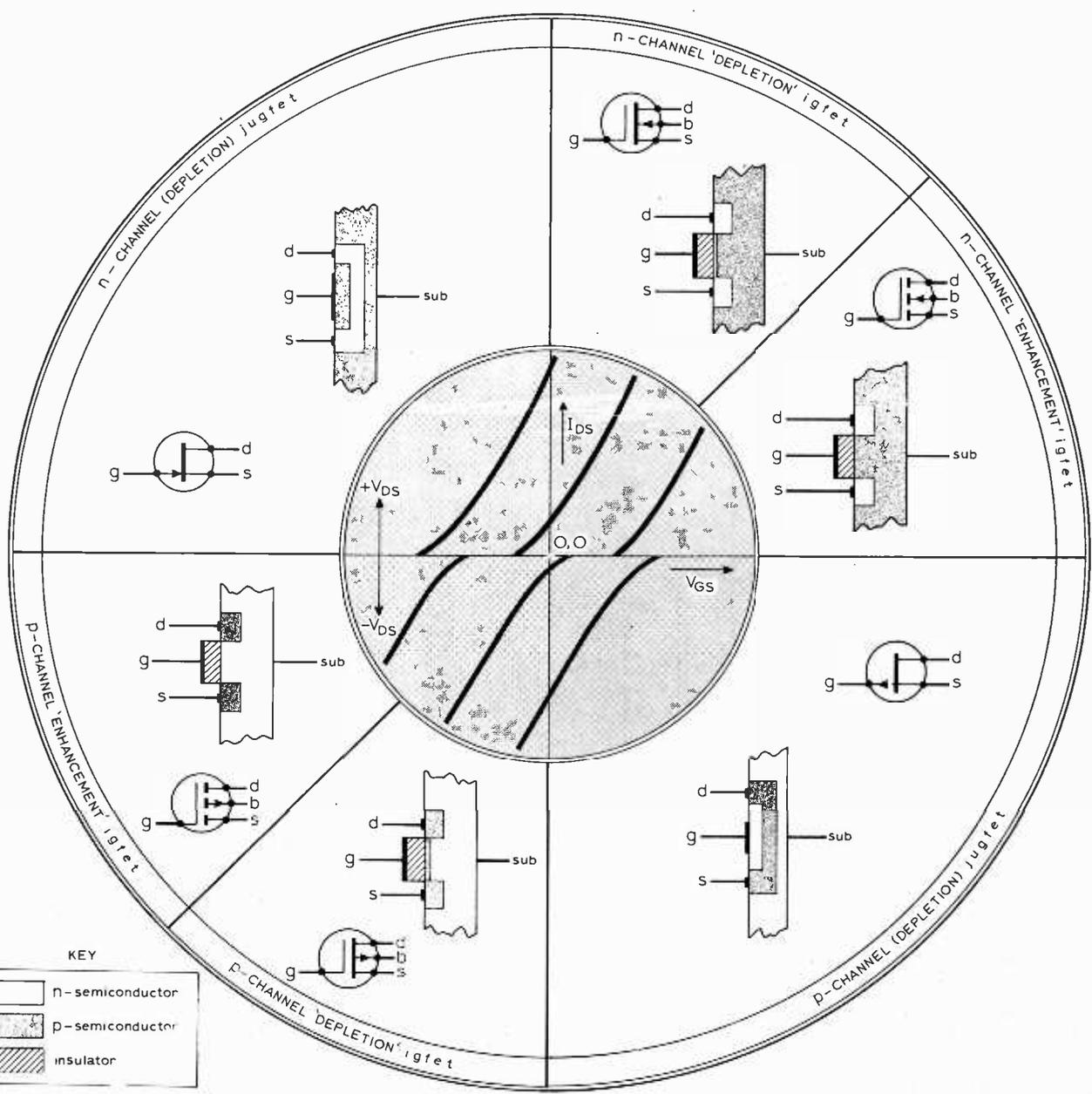
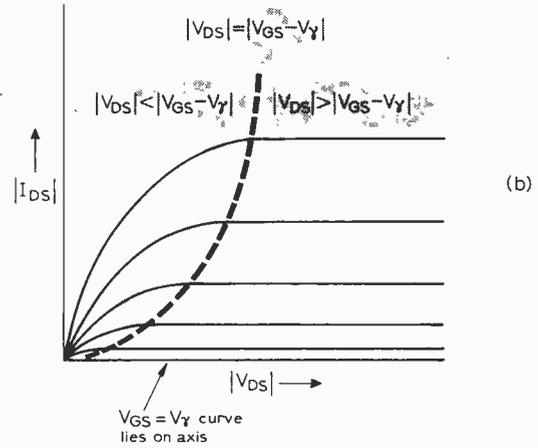
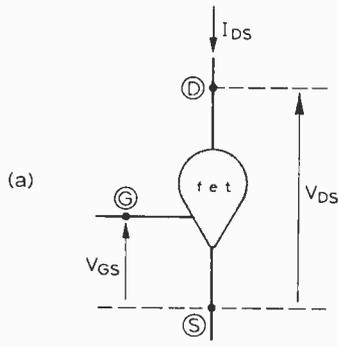
A horizontal arrow connected to a perpendicular line section indicates a p-n junction. The direction of the arrow is from p to n. Thus, an n-channel jugfet has a p-type gate. In the case of a p-channel enhancement igfet the arrow points from the p-type induced channel to the n-type substrate.

The horizontal section of the gate terminal is on the same level as the source. The igfet gate has a vertical section isolated from the rest of the device to emphasise the insulated nature of the terminal. The substrate, shown as b for bulk on the symbol, is sometimes internally connected to the source and in such cases the substrate is often not shown. When the substrate terminal is at the disposal of the circuit design engineer it must be connected to a potential which ensures that both the drain-substrate and source-substrate junctions never become forward biased. For n-channel igfets this is often, conveniently, the most negative potential in the circuit whilst for p-channel types the most positive potential in the circuit is appropriate.

Fig. 1. (a) F.e.t. of unspecified type, (b) Drain-source characteristics for (a).

Fig. 2. F.e.t. classification chart showing device inter-relationships.

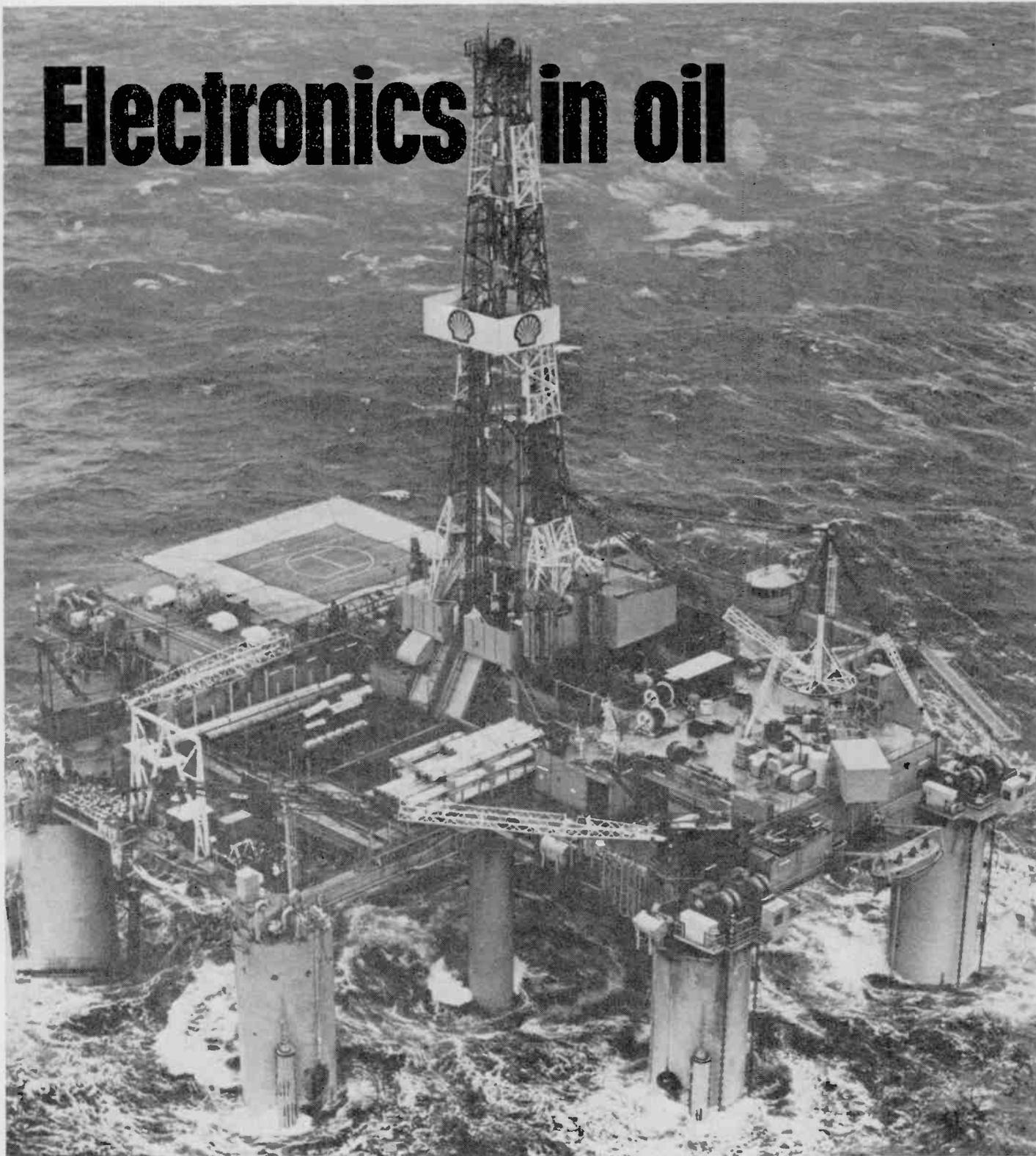
Transfer characteristics refer to "pinch-off" region. Channel type, whether initially "built-in", or induced always has the same polarity as the semiconductor material in contact with the source terminal.



KEY

	n-semiconductor
	p-semiconductor
	insulator

# Electronics in oil



Before we look at the role played by electronics and communications and how these systems are achieved, the scene must be set to reveal what conditions have encouraged the growth of the special and vital systems now in use for the discovery and recovery of undersea oil.

The type of drilling installation used (platforms, barges or ships on which drilling rigs are mounted) depends upon the depth of the sea and possible storm conditions. A jack-up unit—so called because the drilling platform is jacked up on legs (which rest on the sea bed) to above the water level—is normally used in less than 200ft of water. This type of installation is

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*Assistant Editor, Wireless World*

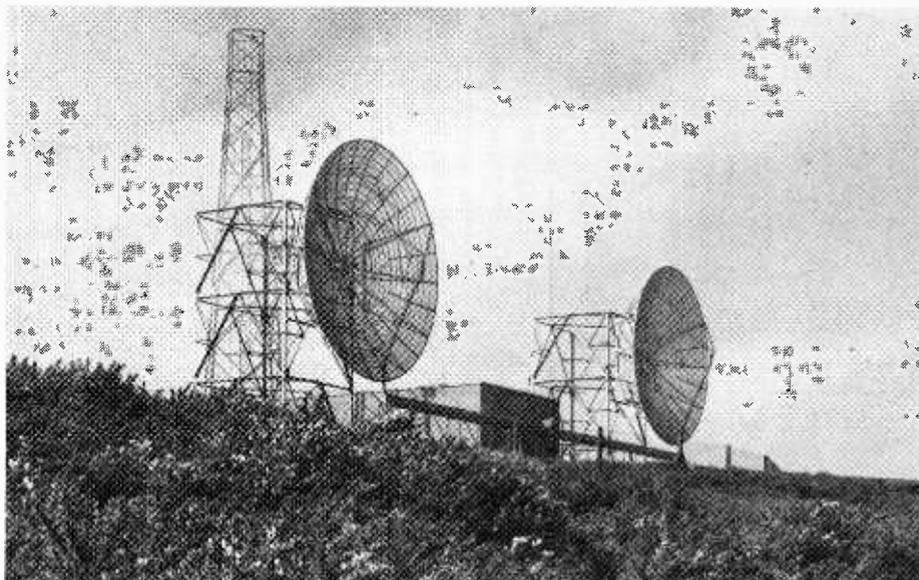
**A survey of the electronic systems used in the search for and recovery of oil under the sea—communications, telemetry, navigation and data collection with a brief look at special developments such as dynamic stationing of vessels and the national data buoy.**

highly stable but can be moved only in calm seas and wasted time in waiting for these conditions may therefore run into several weeks. In deeper water, which will be typical of most future UK offshore operations, a floating installation will have to be employed, either a drill ship or a semi-submersible. A drill ship is fitted with a rig which operates through an aperture in the middle of the vessel or, in some cases over the ship's side. A semi-submersible, as the name suggests, has submerged pontoons which support the working deck well above wave level.

Floating installations are normally anchored to the sea bed, although dynamic

*Tropospheric scatter aerials at Brimmond Hill which serve the B.P. platforms in the Forties Field (Marconi Communication Systems photograph).*

*Fig. 1. Tropospheric scatter link from the Phillips Group field production facilities at Ekofisk to the crude oil terminal facilities at Teesside (PS—pumping station).*



positioning (explained in detail later) by propellers appropriately oriented to counter the effects of wind and current is now used. However, in the waters around Scotland, where very high waves and winds may occur, keeping the platform in position is a major problem whatever method is employed.

Of the installations now available, only the semi-submersible can operate in Scottish waters during the winter months, and then only with difficulty; drill ships are less able to smooth out wave-induced vertical rig movements and can operate only during the summer season. To help overcome these difficulties, a new generation of large semi-submersibles is being built and the number of exploration installations at work in the UK sector of the North Sea is now about 25.

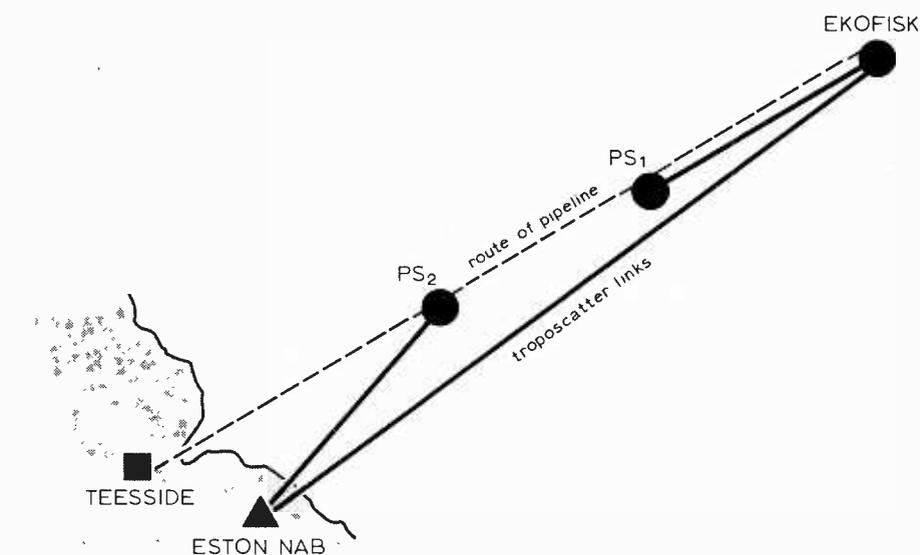
To put the cost of these operations into this background perspective, the new generation of installations will cost about £10m each to build, and with the associated supply boats, helicopters, etc, as much as £20,000 per day to operate. To drill a 10,000-ft well in 60 days, a company would have to lay out more than £1M.

In the North Sea, the ratio of successful wells to wells drilled is reasonably good (about one to six) but the ratio of commercially viable wells is only 1 to 20 or less, so that £10M–£30M may have to be spent on a drilling before a commercial oilfield is discovered. Luck enters into it as well. Some licensees may spend this sum of money and still find nothing. Finding a field is just the end of the beginning and two or three more wells at least have to be drilled to determine whether or not the field is commercial.

The cost rises rapidly in proportion to the water depth. In deep water (e.g. the 500 or 600 feet of water off the Shetlands), it could rise to more than £40M. No platform has yet been constructed in such a depth of water anywhere in the world, and, although it is technically feasible, the immense cost has prompted a search for alternative methods. An entirely new field of technology is therefore emerging encompassing such developments as completing the well under water (without the need for a fixed platform) by remote controls, or using two-man submarines fitted with remotely operated arms, or a diving bell which locks onto a capsule enclosing the wellhead, so enabling the technician to work as if on land.

### Communications

In the beginning, both needs and available facilities were simple—a straightforward radiotelephone link. Now the main service is provided by independent-sideband equip-



ment which caters for the simultaneous transmission of radioteleprinter on upper-sideband and radiotelephony on lower-sideband operating through special Post Office terminals at Humber and Stonehaven for rigs in the North Sea.

The radiotelephone and teleprinter are the two main types of communication link between the oil rig and the shore. A typical system supplied by Marconi Marine consists of independent-sideband or upper-sideband only installations. The former permits simultaneous operation of both radiotelephone (l.s.b.) and teleprinter (u.s.b.) while the latter system allows both types of transmission but requires switching from one to the other.

Frequency shift keying is a modulation method used for teleprinter operation. For the mark/space teleprinter code an audio tone is deflected from "side to side". The teleprinter however generates positive or negative d.c. for transmission and requires the same for reception. To convert from d.c. into frequency shift keyed audio tones and vice versa, a voice frequency telegraph unit is required. Automatic high-speed telegraphy, particularly when used for data telex transmission requires the highest

standard of accuracy possible. The Post Office's specification W6652 calls for the fitting of single-path error correction equipment. A technique for satisfying this condition effectively doubles up on the normal teleprinter code to provide a "checking" signal with which the required signal can be compared. The result is a substantial improvement in accuracy on noisy transmission/reception paths. Tropospheric scatter systems also play a large part in rig-to-shore communication, explained in detail later.

Most communications from the oil rig to its supply vessels are carried out via v.h.f. links, but while rig to ship communication requires frequency modulated v.h.f., rig to helicopter radiotelephony requires amplitude modulated v.h.f. Usually only one or two channels in the band 121–123MHz are necessary.

### Microwave systems

Telemetry systems provide vital information on the status of the pipeline, on supply, demand and product quality, providing control at any point. On land, telemetry information is generally carried over a conventional telephone circuit by connec-

tion into the local network, or provided by a special cable or radio-relay system. The communication link is vital, particularly in an emergency and the cable system must provide alternative routing and the radio relay system include independent standby equipment. Conventional relay links provide a solution to communication problems so long as the platform is within "line-of-sight".

Oversea paths are generally engineered with vertically spaced antennas to provide a diversity system, whereby when one antenna receives a low signal, the other is brought into use. The permissible offshore distance is thus dependent upon the available shore height and antenna spacing, the facility for both being strictly limited on most platforms because of the additional loading and hazard that the antennas present to helicopters. Whether the operating frequency is in the v.h.f., u.h.f., or s.h.f. band, the limit range for antenna heights of 30 to 60m will be 30 to 50km, a shore height of 300m extending the range to 80 to 100km.

Many offshore developments of which the North Sea is a particularly interesting example, are well in excess of the line-of-sight limit and the signal diffracted beyond the horizon is rapidly attenuated. As the diffraction loss becomes prohibitive in terms of effective radiated power, the scattered signal takes over. To provide the required service, typical data error rates must be in the order of not more than 1 in  $10^3$  for 99.99 per cent of the time.

North Sea scatter communications operate in the 2.5GHz band.<sup>1</sup> Six- and nine-metre paraboloids give gains of 41.5 and 45dB respectively, which with 1kW amplifiers produce effective radiated powers of 10 to 30MW. With modern uncooled parametric amplifiers having noise figures of

2dB, quadruple diversity receivers with i.f. combining and threshold extension techniques, an f.m. threshold of -140dB or better is achieved. A path loss of 250dB can be tolerated before the error rate becomes significant, corresponding to a range of 300km with the required 99.99 per cent circuit availability.

There is one outstanding problem affecting both radio relay and scatter communication links particularly relevant to the North Sea, the phenomenon of ducting. For short periods of time, signals far beyond the horizon may exceed the free-space value; the normally insignificant over-shoot to other stations may assume levels of serious interference. The distance between stations operating on the same frequency must ensure protection against both the scattered and the ducted signals.

Although the communication bands are very wide, the large number of users and the wide-band transmissions involved call for maximum economy in channel allocations. Thus many radio-relay systems carrying television and telephony traffic have a bandwidth of 30MHz, as wide as the whole h.f. band. The use of frequency diversity for both the line-of-sight and scatter links, occupying two channels for the same traffic, is being discouraged in favour of space diversity.

The scatter system often uses two antennas at each end, providing four physical paths. The two transmitters must be identified by the respective receivers by virtue of their different frequencies or, with single frequency links, the polarization of the two transmissions.

One of the latest troposcatter links is being established between the North East field called Ekofisk and the coastline near Teesside. The system provides for two 40ft dish antennas to be erected on the

800ft hill at Eston Nab along the coast just south of Teesside, with feedhorn arrays angled towards Ekofisk and towards one of two pumping stations, 70 miles off the coast. Similarly at Ekofisk, two 30ft dish aerials will be built with feedhorn arrays towards Eston Nab and towards the other pumping station, 70 miles from Ekofisk. Two 20-ft dishes will be installed at Pumping Station I and two 12-ft dishes at Pumping Station II both sited along the piping line. Each dish antenna will have two dual polarized feedhorns to provide for quadruple diversity operation—dual space and dual polarization techniques combined to provide four separate radio paths without using additional frequencies.

The main link is to provide a basis for 72 telephone or telegraphy channels, while the pumping stations' links will carry 12 channels with a capacity of 24. Both major stations will operate at 1kW transmitter power but the links with Pumping Station II will have 2W output from Eston Nab and 2W on the return path. Transmitted power from Ekofisk to Pumping Station I will be 20W.

#### Accuracy in navigation

Marine seismic surveys are the commonest method of initiating exploration for offshore oil or gas fields which are indicated by certain geological formations. Sound waves are transmitted through the water and sea-bed and the reflections are recorded and analyzed to give a picture of the geological structure. The most favourable sites to drill and the depth at which prospective reservoir rocks are expected to occur are indicated by this picture, taken in conjunction with any other available information such as data on regional geology.

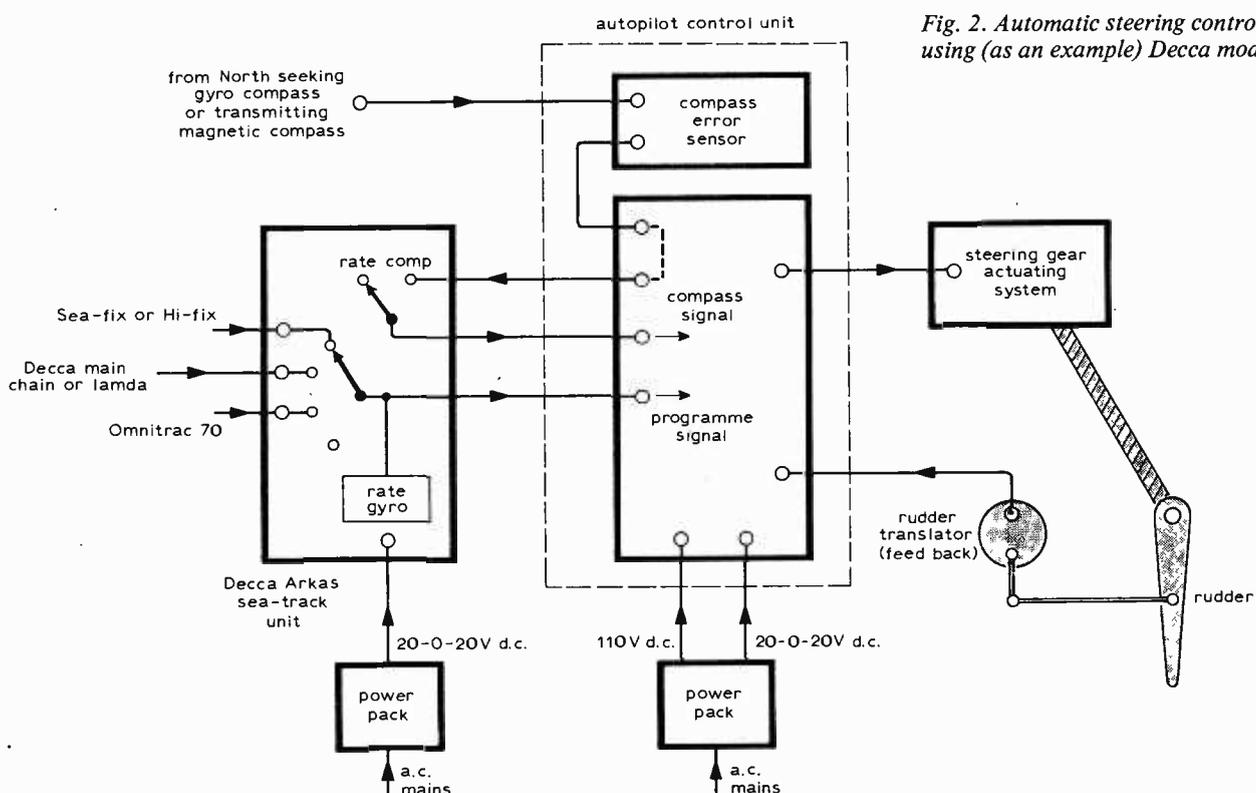


Fig. 2. Automatic steering control system using (as an example) Decca modules.

During the survey procedure it is essential that the area surveyed should be fixed and marked accurately, hence use has to be made of an accurate navigational system so that the survey ships know where they are, coupled with an equally accurate underwater system to define the limits of the area surveyed and to enable ships and drilling rigs to return to the same spot each time.<sup>2</sup>

Accurate navigation when reasonably close to the land can be obtained by a radio hyperbolic or ranging system. There are a number of such systems on the market, but in the North Sea surveys are often carried out using the Decca Survey Hi-Fix system. The present system consists of three shore stations working in the band 1700 to 2000kHz. All three use the same frequency and transmit one after another. Receivers on board the survey ships measure the phase difference of the received continuous wave from two of the stations and so position themselves on a hyperbola. Then a further hyperbola is obtained using the third station and one of those already used. Where the two curves intersect is the ship's position. Hi-Fix has a range of about 150 miles and will produce a position accurate to within two metres under optimum conditions. Decca Survey have just developed an even more accurate system, known as Hi-Fix 6. This consists of up to six stations on-shore, all employing the same frequency.

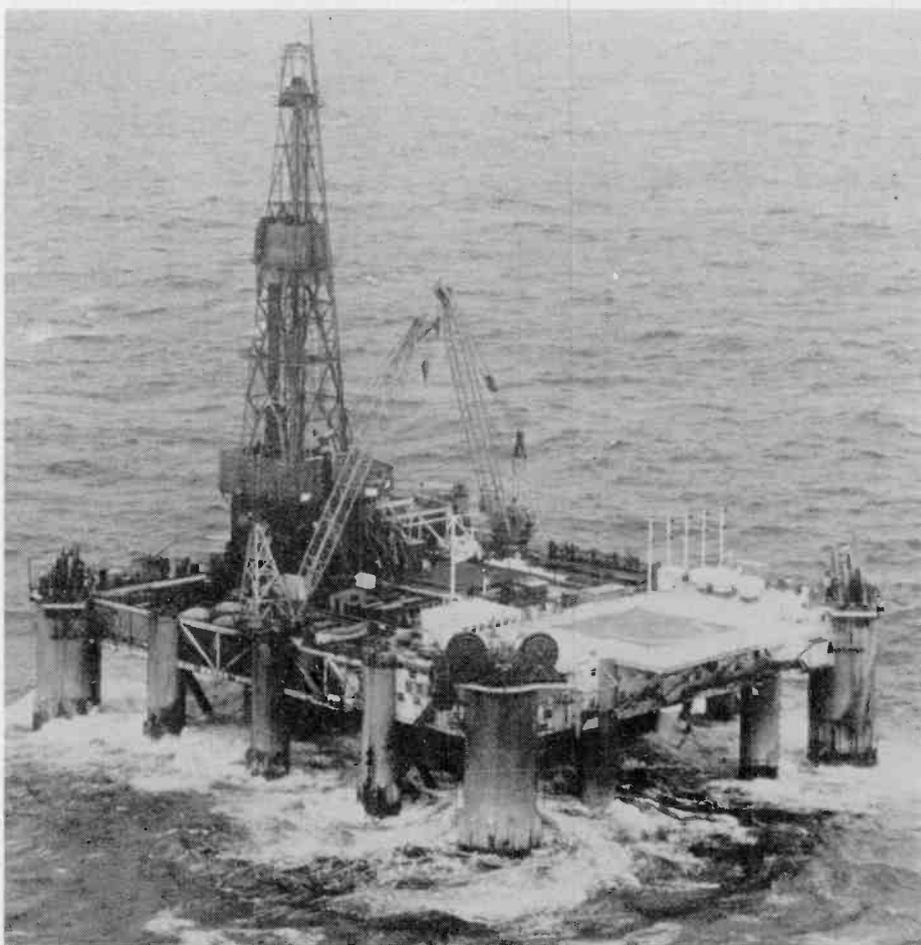
For underwater fixing some form of transducer that can be activated by a ship's sonar is used. Such a system is particularly valuable when working at the limit of a radio hyperbolic system. Two or more transponders may be laid on the sea floor in known positions and ships interrogate them with their sonars. The transponders are triggered off and transmit return pulses. By measuring the time between the transmission of a pulse of energy and the reception of the transponder's return and noting the bearing on which the transmission was made, the ship's bearing and distance from the transponder can be deduced and thus the ship's position. By using more than one transponder a check can be made and an accurate position found. The transponders have a life of three to three and a half years and can be laid permanently in selected positions as navigational beacons, either for use when surveying or for positioning rigs or platforms.

To obtain an overall picture of the seabed the sonars used usually project their beams sideways and downwards and scan the bottom as their parent ship moves along. They will produce contour maps of the seabed and will show up such things as cables, wrecks, pipelines and areas of rock.

A hydrographic sonar, designed by the Admiralty Research Laboratory is being developed by Marconi Space and Defence Systems and is capable of producing both horizontal and vertical plan views of the seabed. The depth of objects on the seabed can be determined to an accuracy of within two feet to ranges of 200 yards.

#### Rig manoeuvres

It is possible to manoeuvre a drilling rig or ship into position without human interven-



tion, thereby increasing the accuracy of manoeuvres. A system made by Decca Survey and known as Dynafix uses shore stations up to 40 miles distant and processes their signals in such a way that they are used to operate specially fitted manoeuvring propellers.

Dynamic positioning of a drilling, whereby the vessel is held in position over the well without the use of anchors, was first used in drilling for oil in deep water early in 1972. This was achieved by Sedco 445, a drillship designed to Shell specifications and equipped to conduct world-wide drilling operations in water depths of about 2000 feet. Dynamic positioning enables the drillship to hold its position despite wind, waves and tides. Eleven sideways-acting propellers and two main screws are controlled by two computers in keeping the ship over the hole while drilling takes place.

The method and systems were pioneered in the United States by the Shell Oil Company. Its work with dynamic positioning began in 1961 when it participated in the development of a manually controlled drillship. In the same year it developed the first automatically controlled dynamic positioning system in the core drilling vessel Eureka.

Sedco 445 provides laboratory space for drilling, electrical logging, mud logging, diving, petroleum engineering, and geological and management services, all of which are designed to be independent of shore support. However, for emergency supplies, timely re-stocking, personnel access and safety stand-by the drilling unit is provided with a helicopter deck and will be accompanied by a large crew-standby boat and a work boat. Two acoustic reference systems measure vessel's position with respect to beacons at the wellhead. As a backup and for use during certain operations, two tiltmeters are used either on a taut

line to bottom over the side or on a guideline. Two gyro compasses measure heading for control. Two anemometers measure wind velocity and direction with respect to the ship and permit the control system to command an immediate and opposite thrust.

To assure the highest reliability complete backup equipment is provided throughout the dynamic stationing system. Two Honeywell computers are used; while only one of them at a time is issuing commands to the thrusters, both are continuously receiving data from position and environment sensing instruments, comparing them for validity, performing the control calculations and checking each other. Control automatically transfers to the standby computer on failure of the operating unit.

The computer's thrust commands are sent to thyristor modules which provide variable voltage d.c. power to reversible speed standard traction motors.

Sedco 445 can be navigated by satellite.<sup>3</sup> Conventional navigational positioning systems use stationary wave patterns generated by fixed, land-based, radio transmitting stations, and have an accuracy of about 25 to 50 metres. However, they are limited to a range of about 200 miles from shore.

The Navy Navigation Satellite System (NNSS) consisting of orbiting satellites and accompanying ground facilities was made available for non-military use in 1967. NNSS enables work to be carried out quickly and conveniently—the vessel Lady Glorita using satellite navigation as its prime positioning system was able to carry out a seismic survey off Guyana in only four days, whereas the setting up of a conventional positioning system could have taken more than a month of expensive preparation. On a *moving* ship, given an accurate knowledge of the vessel's true

speed and course, an accuracy of about 100 metres can be obtained, with the added advantage of not being limited to a range of 200 miles from the shore.

The equipment needed to operate satellite navigation is portable and self-contained aboard ship. It consists basically of two radio receivers, a small computer equipped with teletype print-out facilities and a reference oscillator. The system measures the v.h.f. radio signals transmitted from one of the orbiting satellites and, using the Doppler principle, computes the latitude and longitude of the signal receiver. NNSS has five satellites orbiting the earth at an altitude of about 600 miles. They travel at a speed of about 16,500 miles per hour. The satellites are in polar orbit and their orbit planes are at angles of about 45° from each other.

Each satellite is transmitting continuously two related stable frequencies at 150 and 400MHz, while every two minutes it gives an accurate time check and its orbital position at that time. A ship with the necessary receiving equipment can compare the signal it receives from the satellites with the shipboard oscillator, which is fixed to a frequency slightly offset from the one transmitted by the satellite. The shipboard receiver measures the Doppler frequency by observing the changing relationship between the incoming frequency and the stable reference.

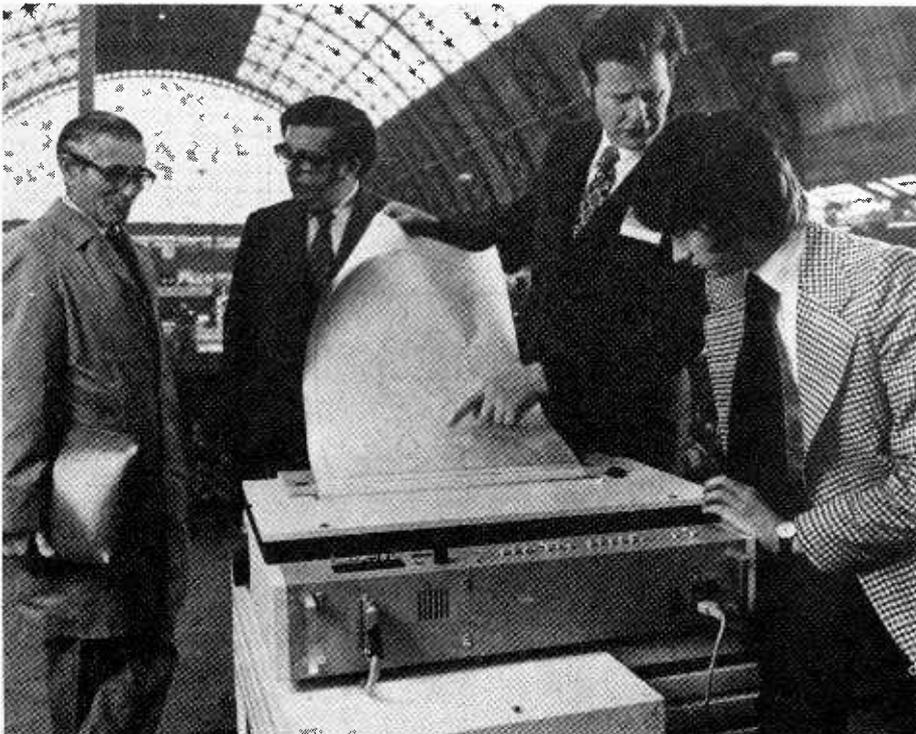
Satellite navigation is still in development. At its present state, it is unlikely to be used as the sole or primary means of navigational positioning except for cases such as seismic ships on roving commission. However, when combined with sonar Doppler into an integrated navigation system and used in shallow water, satellite navigation has shown that it has great potential for location fixing offshore work in the oil industry. (An article on satellite navigation by the NNSS will be published in the February issue.)

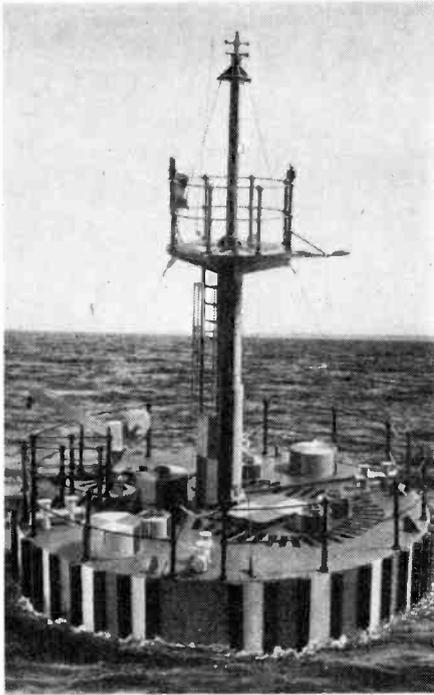
### New weather buoy

The national Data Collection Buoy, presently being manufactured by the Seatek consortium, is to be placed on station in the North Sea in summer 1975.

The 7.6-metre-diameter wave-riding welded steel buoy is to act as a development platform for oceanographic and meteorological sensors. These include air temperature, barometric pressure, wind speed and direction, humidity, rainfall and visibility. Sea-bed pressure instruments, connected to the buoy by cable, are included in the range of oceanographic sensors, and these will help produce storm surge warnings. Other sensors include acoustic and electromagnetic current meters near the ocean surface, and current speed and direction monitors at three sub-surface positions. One hundred

*Reception of worldwide weather chart transmissions of the international meteorological services demonstrated by the EMI Weatherfax system at the 1974 Offshore International Exhibition, London.*





Artist's impression of the UK national data buoy D.B.1.

data channels are provided, some 50 being used by the initial suite of sensors. Measurements can be made at any time within the one-hour cycle, and then stored ready for the hourly transmission. A 1MHz temperature compensated crystal oscillator provides not only the high accuracy clock (ten seconds per year) for automatic control but also a basic input to synthesize all frequencies required within the transmitter.

A six-watt transmitter at 4163.5kHz feeds a ten-metre whip antenna and is used in conjunction with space-diversity reception at Lowestoft. The A9J emission is a modification of the Piccolo system with one audio tone per decimal digit.

A slow morse call sign (2NI02) precedes a synchronizing signal, followed by three sequential scans of the data channels. Each channel uses three decimal digits to provide 0.1% resolution and each digit is transmitted as a tone lasting 300ms.

Every third hour an additional 20-minute transmission of buoy heave, pitch, roll and compass data provides high-frequency wave information. A fuel supply of 400kg of propane on the buoy will last two years and the data handling equipment is designed to operate unattended for at least six months, but the oceanographic sensors may require more frequent visits due to fouling by marine growths.

#### Under-sea production

Research into the development of deep sea production facilities is being pressed forward in parallel with progress in drilling techniques in the deep oceans. Such facilities can either be on the sea floor or on the surface. Oil companies are exploring both routes in seeking solutions to the problems involved. The objective involved with the surface method when oil is found in commercial quantities

is to get the oil from the well to the surface as simply as possible, put it through production facilities on the surface and transport it away by tanker. This technique calls for man-controlled, remotely actuated devices, using electronic tools where necessary and embodying the means to feed continuous data on what is happening below however there must be human access to the seat of the trouble—either by miniature submarines with mechanical arms or, dependent on depth, divers.

If large oilfields are found in very deep water far from shore, floating storage will have to be provided. A concept envisaged by the Shell companies is the use of a huge floating tube, the shape of a fisherman's float, suspended vertically in the water and with a storage capacity of perhaps 300,000 barrels (about 40,000 tons), linked by lines to the wellheads on the ocean floor. In very deep water, dynamic stationing equipment similar to that installed in the "445" would keep it in position.

A programme to build a complete oilfield on the seabed without any surface platforms and in deeper water than any existing wells is under way at Lockheed Petroleum Services. Several major oil companies are financing the programme. This gives a good indication of their interest in the project which is pioneering a range of subsea equipment to extract oil in up to 3,000ft of water. This is eight times deeper than any present oil well and yet is within a water depth where surveys indicate there could be major petroleum reserves in several areas throughout the world including the North Sea. A well-head on the sea floor is enclosed in a dry one-atmosphere, steel cellar which houses the

equipment normally carried on surface platforms. It is serviced by engineers who travel to it in a one-atmosphere capsule from a surface support vessel. The capsule docks with the seabed cellar and engineers open a hatch to gain access and carry out their work in shirt-sleeve conditions with fresh air and electrical power supplied by umbilical cable from a surface support vessel. Lockheed is developing the system.

As a final note and with the sort of developments just mentioned in mind, there still remains a market of over £2,000M in production wells and transportation over the next ten years and also on the many offshore and on land services associated with the oil business. Although much of the initial demand of the oil industry has been met by American and European suppliers, the United Kingdom's offshore oil business is a vast and expanding market that will stretch into the 1990s, and Britain now has not only the opportunity of rising to self-sufficiency in fossil fuels by the 1980s but also to evaluate the opportunities and establish itself as a major world supplier of products and services to the offshore industry. A report is due for publication in March by Industrial Market Research Ltd, London, containing up-to-date information on product and service opportunities in North Sea oil developments.

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1. Anderson, E. W., "Microwave Communication Systems for the Offshore Oil and Gas Industry", *Mariner*, July/Aug. 1973, p.8-10.
2. Marriott, J., "Accuracy and instrumentation in offshore oil developments", Offshore International Exhibition and Conference publication, Oct. 1974.
3. "Satellite navigation", *Shell Magazine*. Vol. L11, No. 749, p.109, 110.



# News of the Month

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## ITU first l.f./m.f. conference session

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Further to the news item published in our December 1974 issue, the following is a summary of the conclusions reached by the first session of the regional administrative l.f./m.f. broadcasting conference which was "to prepare the technical and operational criteria which will serve as a basis for the preparation by the Second Session . . . of frequency assignment plans for the l.f./m.f. broadcasting bands in Regions 1 and 3".

For ground-wave propagation, the curves of the International Radio Consultative Committee Recommendation 368-2, which cover propagation at low and medium frequencies for different values of ground conductivity, were adopted by the conference. The conference decided that any new frequency plan should be based on the continued use of double sideband amplitude modulation with full

carrier and rejected proposals for a reduced value of modulation bandwidth. Similarly, proposals to base planning on high degrees of signal compression, thereby improving protection against interference, were rejected by the conference because of the allegedly adverse effect upon reception quality. No upper limit on the radiated power of individual transmitters has been recommended but use should be made of directional antennae to reduce power in those cases where assignment incompatibilities cannot be resolved by any other means.

The conference decided that for most purposes a protection ratio of 30dB against interference from other transmitters operating in the same channel should be adopted. A consensus was quickly reached that the channel spacing should be uniform throughout the whole of Regions 1 and 3 and that the carrier frequencies should be integral multiples of the channel spacing. The revised channelling in the m.f. band will start with a carrier frequency of 531kHz and proceed in 9kHz steps up to the highest channel with a carrier frequency of 1602kHz. The l.f. band remains unchanged with its present 9kHz channelling and carrier frequencies which are not integral multiples of the channel spacing.

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## Liquid crystals for electron observation

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A simple technique has been developed for the observation of electron pulses flowing through an integrated circuit. The technique employs liquid crystals. Conventional i.c. test equipment determines whether an i.c. is functioning properly but is of little value in determining exactly why and where it has failed. With the new

technique, developed by RCA, it is possible to observe where the electron flow has been interrupted at a defect. This is made possible by the normally clear liquid crystal which reflects or refracts light when stimulated by an electric current.

A drop of nematic liquid crystal is placed on the surface of the i.c. so that all the rod-like molecules align in the same direction. The i.c. is placed in a conventional microscope and illuminated by light passed through a set of polarizers arranged so that none of the light reaches the microscope's eyepiece under normal conditions. However, when the i.c. is operating, the refractive index changes caused by the electrons' electric fields allow light to pass through the polarizers and, in effect, give the viewer a "live" picture of the pulses or signals flowing in the i.c. The circuits can be examined at various speeds and at normal operating voltages—eight to ten volts for m.o.s. circuits and as low as two or three volts for bipolars.

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## Paging the dead

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A news release we recently received indicated that paging equipment installed at the South Essex Crematorium has contributed towards the efficiency of the organization. According to Multitone Electric, "the smooth operation of a crematorium in every detail is imperative by the very nature of the function which it discharges . . . At the South Essex Crematorium there was an additional problem in that the administrative offices are situated at the entrance to the grounds, some distance from the crematory itself. The new Multitone paging system has made things very much easier, however, "by ensuring that all key staff can be contacted immediately wherever they are". It is envisaged that the next application of radio paging will be its use by mediums to take some of the routine hard work out of their endeavours.

*Laser system installed at the Beckman Instruments, Glenrothes, Scotland factory for resistance and functional trimming of their d.i.p. resistor networks, ladder networks and hybrid microcircuits.*




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## Quadraphonic cassettes

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Although details had not reached this office at the time of going to press, we have heard that BASF has been experimenting with the duplication of quadraphonic cassettes. Unfortunately none of the output from the German duplicating plant appears in the UK so it is unlikely that such cassettes will be offered for sale here, unless one of our own duplicators follows suit.

It is believed that the extra information is recorded on the standard track format, but matrix encoded using the SQ system. Although such an arrangement is perfectly feasible, it is possible that the phase stability of the cassette recording process may have to be of an order higher than most average domestic machines to achieve acceptable decoding. Should the

recordings be of such a type, standard add-on decoders, or those built-in to amplifiers may prove quite suitable for use with this type of recording. Further details will be published as they become available.

## New communications device

A control unit has recently been introduced which dispenses with space-wasting racks of switching and exchange equipment and condenses what would normally be a roomful of equipment into a space no larger than a small filing cabinet. The unit, MFC, was announced by Pye Business Communications as a new master control unit for its M100 speech intercom.

The MFC allows almost limitless expansion of M100 intercom systems while no conventional exchange or switching is required. The calling station initiates a pulse sequence which is in turn decoded by the receiving station. The control unit is constructed on a "plug-in" card principle, station capacity being decided by the number of cards employed.

When a call is initiated, the system memory is interrogated to confirm the availability of the required station and to evaluate the fastest method of connection. Should the called number be engaged, the system is able to keep trying the number every six seconds for up to 90s to obtain a connection, or even arrange for it to call you back later. Extra features include automatic call transfer, three callers on line at once, connection to public address or pocket paging systems and the calling of all stations at once for emergency use.

## Parrot power

After decades of experience, the engineers and researchers at Austral Standard Cables Pty, Sydney, Australia, could perhaps be excused for believing they had overcome almost every conceivable environmental challenge that could confront the industry. The sad truth is that the ASC people recently have been given the bird. Over several years they successfully wrestled with problems of cable moisture permeation, submarine cable protection, electrical interference, assorted "gremlin-inspired" technical difficulties and termite attacks. The termites were beaten when they introduced nylon-sheathed cable. Now another menace has arisen in Western Australia. "Iron beaks" have been pecking through cables (Integral Bearer Cables) at Mt Newman, W.A., causing shorts and interference within a mining company's domestic communications network. ASC supplied most of the cable when this private telephone system was commissioned in 1968 and since then has met substantial orders for extension and upgrading of the network. The system's radiotelephone signals link

both the Newman township and mine to the PMG exchange at Port Hedland, 265 miles to the northwest.

In such a communications complex, any pests which mutilate part of the network obviously are unwelcome. The birds have concentrated on a relatively small stretch of line. They land on the bearer wire, bend under and peck right through the polythene-sheathed cable. The ASC planners in Melbourne don't claim to have a quick remedy for the problem, but have suggested that brass tape may stop the birds. It has been urged that for ease of handling and installation poly-sheathed cable be lashed on site to the bearer wire with brass tape. If that doesn't stop the parrots, ASC's engineering services may be in for some overtime.

## Colour TV examination

The Radio, Television and Electronics Examination Board is introducing a certificate of competence in colour television servicing. The qualification has been established in response to demand from the industry to provide a recognized certificate in this field which is issued on passing a comprehensive practical test. It is open to those who have already established themselves in the servicing of colour television receivers, who hold a recognized technical qualification and who have had a minimum of one year's full time gainful experience. The award will take the form of a certificate and personal identity card issued by the Board.

The examination is a problem-solving exercise in which the candidate has to identify the problem and obtain the relevant test information. There is a limit on time (five faults in two hours) and the candidate is required to work on more than one type of receiver, designated in advance. Setting up of pre-set controls also forms part of the test. In addition to the practical assessment, a short written

test is concerned with safety and installation. The practical test involves fault-finding to component level and the candidate is to state correctly the symptom, the fault area, the stage and the component.

## TV deliveries down

Deliveries to UK distributors of UK made and imported colour television receivers reached 153,000 in September—a 41% decrease on September 1973 (259,000), according to the latest statistics compiled by the British Radio Equipment Manufacturers' Association. This brought the total for the first nine months to 1,638,000, a fall of 18% compared with the same period of 1973 (2,005,000). The share of imports of colour sets has fallen in the January to September period to 21% from 25% during the same period in 1973.

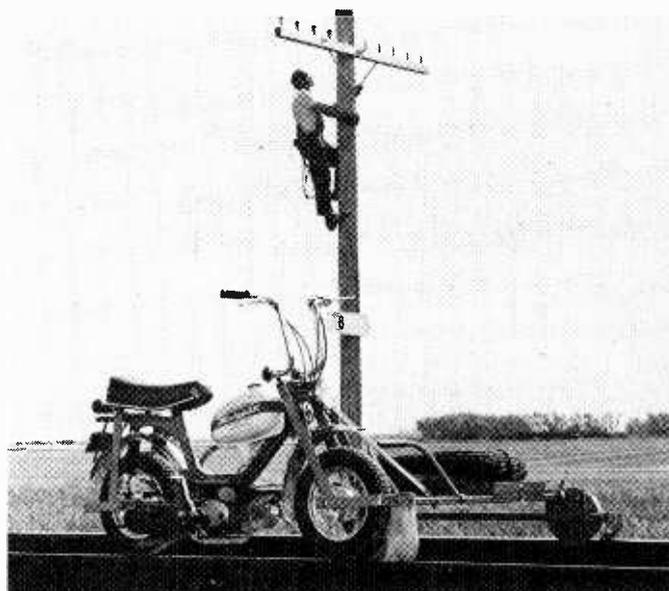
Total monochrome television deliveries for September of 72,000 brought the total for the year to 611,000, a fall of 44% compared with January to September 1973 (1,084,000). These figures are details of deliveries of UK made and imported deliveries, including those to rental and relay companies.

## Briefly

**The journal you like.** More and more people are reading *Wireless World*. At the time of going to press the estimated circulation for 1974 was an average of 65,723 copies per month (to be confirmed by the Audit Bureau of Circulations). This was 5,000 up on the 1973 figure of 60,528 per month.

**RTS Hon. Sec. retires.** The retirement of Charles Marshall as honorary secretary of the Royal Television Society was recently marked at a society luncheon in London. Mr Marshall who is head of public relations at Mullard had held the post for 13 years.

*Something new in telecommunications maintenance—a "Tra-k-art" has been introduced by Canadian Pacific Rail. It is a 48cc motorcycle and sidecar adapted to run on a railway track*



# Circuit Ideas

## Control of a binary counter for division by one or two

This circuit provides a method of switching division by two into or out of a stream of clock pulses. The output is in phase with the input, and free from spikes due to race problems, which may occur with conventional gating methods. Only one D-type flip-flop and one inverter are used.

The logic circuit is shown below; action is as follows.

**Control low; input low**

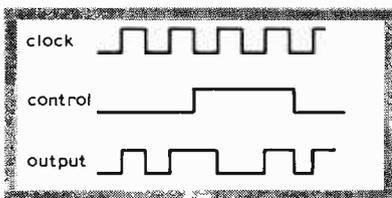
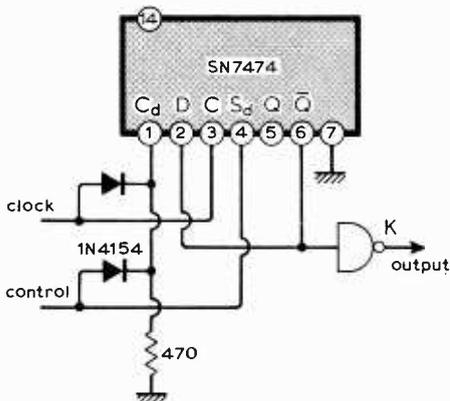
$C_d$ ,  $S_d$  both low, Q and  $\bar{Q}$  both forced high.

**Control low; input high**

$C_d$  high;  $\bar{Q}$  goes low (complement of Q).

**Control high**

$C_d$  and  $S_d$  are both high. At the positive edge of the clock, the D input is trans-



ferred to Q. This is the normal connection for division by two, using a D flip-flop. An inverter is added to restore the phase. Note that  $K \neq Q$  in the divide by one mode, since Q is held up, by  $S_d$  low. Hence the use of the inverter.

J. M. Firth,  
National Research Council,  
Ottawa.

## Passive solid-state antenna switch

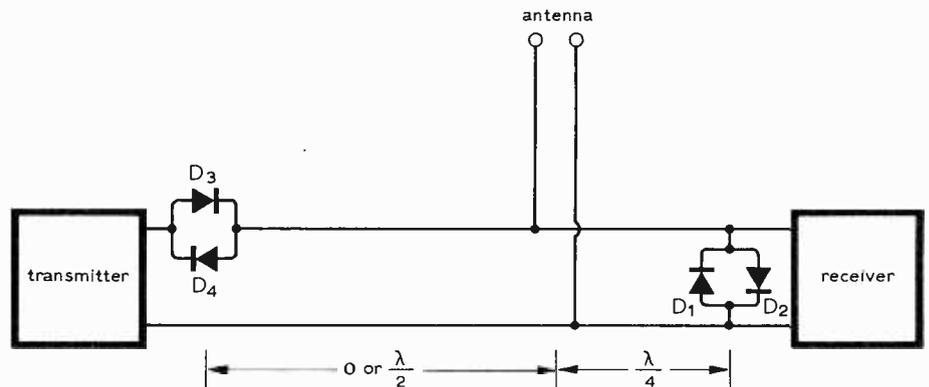
A lot of antenna switch schemes have appeared in the past, but all used complicated tuned circuits and lots of diodes, or vacuum tubes that required high-voltage supplies. This circuit uses only two pairs of silicon diodes, one pair ( $D_1$  and  $D_2$ ) which effectively shorts the receiver input during transmission, and the other ( $D_3$  and  $D_4$ ) which disconnects the transmitter during reception.

Because of the high power from the transmitter,  $D_3$  and  $D_4$  conduct, and the power flows towards the antenna. Likewise,  $D_1$  and  $D_2$  in the receiving branch also conduct and put a short circuit across the line at the receiver (only 0.6 volts appear across  $D_1$  and  $D_2$ ), thereby protecting the input

circuits of the receiver. As the short circuit is a quarter wavelength from the T-junction, the impedance in parallel with the antenna line at the junction is very high and does not affect the power travelling toward the antenna.

During reception, the impedance at the T-junction looking toward the transmitter is infinite because there is an open circuit half-a-wavelength away caused by non-conducting  $D_3$  and  $D_4$ . Looking toward the receiver there is a matched line, so all the power from the antenna goes into the receiver. The diodes are high-frequency switching diodes with current ratings depending on the transmitter power. The line is the same as the one used to feed the antenna.

Alejandro Lieber, LUI FCR,  
Edinburgh.



## Click-free switching for audio filters

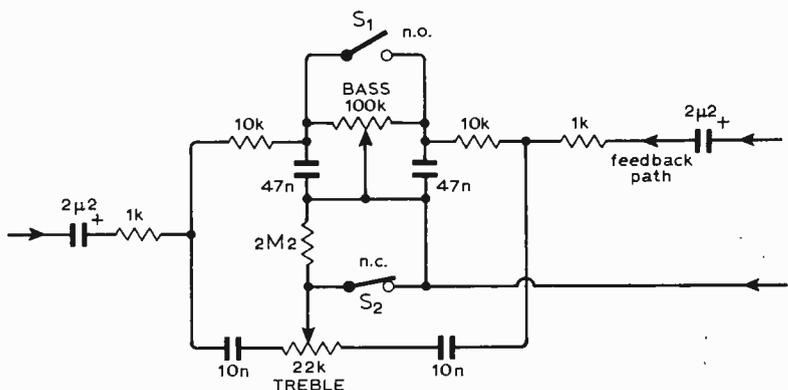
It's often required in mixing consoles and other audio equipment to be able to insert a correction network for comparison purposes without producing transients or changes of level. The diagram shows how this can be achieved with a familiar Baxandall network, though of course the idea is applicable to other filters.

With  $S_1$  open and  $S_2$  closed, the circuit functions normally, but if the switch positions are simultaneously reversed, the response remains flat, regard-

less of the positions of the pots. The centre-frequency gain remains unchanged since the network is symmetrical and, furthermore, phase shift is unaltered.

The main value of this type of switching, however, is that with the controls in the flat position, there is no transient interruption of the signal, and with no d.c. in the network, no clicks either.

J. S. Wilson,  
Amersham,  
Bucks.



# Charge-coupled devices

## 2—Techniques for making two-, three- and four-phase devices

by John Mavor

University of Edinburgh

In part 1 of this series of articles, the charge-coupled device concept was examined in relation to the simplest device embodiment; the three-phase single-level metallization structure (Fig. 1). Although c.c.d. structures are conceptually simple and essentially compatible with standard m.o.s. transistor processing, they do have an Achilles' heel. For acceptably high charge-transfer efficiency to be obtained, the formation of the very narrow inter-electrode gaps (gate-to-gate spacings) must be produced.

Another important limitation to the simple, single-level metallization c.c.d., caused by the existence of the gaps, is that of stability and, ultimately, its long-term reliability.

For efficient transfer of charge carriers in c.c.d.s, it was shown in part 1 that the silicon surface, just below the silicon-silicon dioxide interface, must be completely depleted between adjacent gates. Now for the silicon surface to be depleted, a voltage of a correct magnitude and polarity for repelling the substrate majority carriers must be applied across the insulator. For a given oxide thickness, a higher-doped substrate (with more majority carriers) will require a larger applied gate voltage than with lower doping (less majority carriers). For lightly-doped substrates of  $20\Omega\text{cm}$  ( $\sim 10^{15}/\text{cm}^3$ ) about 10V is required to allow a depletion layer depth into the silicon of  $1\mu\text{m}$ . Because complete depletion is required between electrodes for good efficiency the gap length ( $t$  in Fig. 1) must be less than  $3\mu\text{m}$  in practice.

For integrated-circuit processing using conventional photolithography,  $3\text{-}\mu\text{m}$  gaps are possible but not always easily reproducible with high yield in a production environment. As the device yield will suffer, fabrication cost will inevitably rise. The problem of producing narrow gaps results in the increased probability of alignment errors in connection with masking. Also the masks which are used to define the gaps must be kept particularly clean and replaced frequently to avoid bad definition of the gaps. However, although the masks may be in good order, it is necessary to use a careful photoresist-etching step to actually produce the narrow metal gaps.

Although single-level metal c.c.d.s with acceptable yields may be fabricated, their performance may vary either after encapsulation or during life tests. For gaps of  $3\mu\text{m}$  or less, the substrate surface potential in the gap region is determined mainly by the fringing fields caused by the gate potentials. However, any charge present in the gaps, which could vary in location and size, will cause a second-order variation in device performance. This charge is due mainly to

- the "fixed", positive, surface-state charge,  $Q_{SS}$ , which exists just within the oxide near the silicon-silicon dioxide interface
- a charge component due to the "fast" surface states,  $N_{SS}$ . Their density varies with the size of the depletion region. These states have a major effect on the dynamic transfer of charge in the c.c.d., and
- any contaminant ions (usually sodium) which may be mobile within the gate insulator.

Any variation in location or size of these charge contributions will result in potential barriers and wells being formed in this region, Fig. 2. Although a value of gate-to-substrate voltage can usually be chosen to reduce charge loss owing to this variation, the required bias voltage for this condition to occur will change with time. Thus, c.c.d.s with even partly exposed gate oxides have inherently unstable operating characteristics.

### Oxide growth conditions

Processing investigations on single-level metallization structures have produced satisfactory gate insulator growth conditions to reduce instabilities. Although more elaborate gapless techniques have been developed to improve c.c.d. performance and produce stable devices suitable for systems applications, great care must be exercised whenever the gate insulator (oxide) is grown. Some of the steps which are normally taken in a c.c.d. process are

- The use of particular crystal-orientation substrates to reduce the minimum obtainable values of  $Q_{SS}$  and  $N_{SS}$ .
- Stringent cleaning procedures to prepare the surface of the substrate, prior to oxidation.
- Furnace tubes are either double

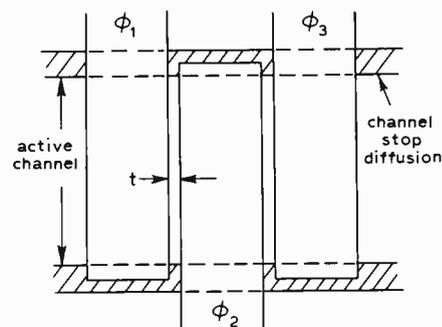


Fig. 1. Plan view of three-phase, single-level metal c.c.d. showing channel-stop diffusions. Difficulty in obtaining reproducible electrode gap width ( $t$ ) of less than  $3\mu\text{m}$  led to the "resistive sea" modification of Fig. 4.

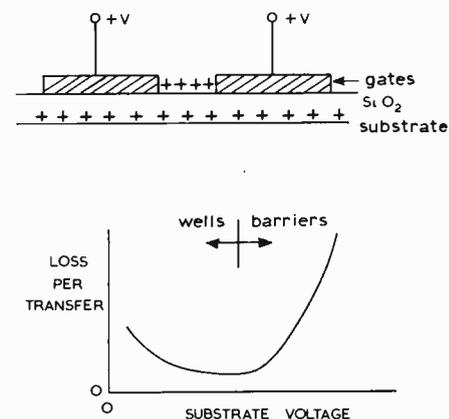


Fig. 2. Variation in size or location of change in the electrode gaps ( $t$  in Fig. 1) forms potential barriers or wells. Charge loss can be minimized by suitable choice of substrate voltage, but required value changes with time.

walled, or are steamed out continuously to prevent ionic contamination.

- The use of specific growth conditions to provide low  $Q_{SS}$  and  $N_{SS}$  values, e.g. "dry" thermal oxide grown at  $1050^\circ\text{C}$ . Conditions should be achieved for which both  $Q_{SS}$  and  $N_{SS}$  are at minimum values.
- Following oxide growth, a high temperature step in an inert atmosphere (say nitrogen), plus a low

temperature (450°C) anneal; the former to reduce  $Q_{SS}$ , the latter to minimize  $N_{SS}$ .

- A phosphorus gettering step is often used to reduce the mobility of any mobile ions present in the gate insulator.
- Oxides are sometimes grown with a trace of HCl present, so that the contamination ion concentration is reduced.

### Channel confinement

To avoid the loss of the signal charge which has been introduced into the c.c.d. depletion regions, it is necessary to introduce a barrier to the charge around the periphery of the clocked gates. Two methods are immediately available from integrated circuit technology.

**Thick oxide isolation.** In m.o.s. fabrication a thick oxide called the "field" is used to prevent the formation of parasitic transistors. The field oxide is normally deposited by chemical vapour deposition, and is typically 1- $\mu\text{m}$  thickness. For the c.c.d. example, if the gates are taken over the edge of the field and down on to a thin oxide well, then c.c.d. action will only occur within the confines of the well. The two main disadvantages of this isolation method are that an extra processing step is required to deposit the field oxide, and that the thin gate metal required for the production of narrow inter-electrode gaps can easily break at the corners of the step in the oxide between the thick and thin transition.

**Channel-stop diffusion.** When a highly doped ring of diffusion surrounds, but just underneath, the periphery of the c.c.d. gate area proper, then no charge loss can occur (see Fig. 1). For an n-type substrate, the  $n^+$  doped-up edge of the c.c.d., owing to the channel stop, cannot support a depletion region which would otherwise cause charge loss.

The disadvantage of this technique is that an additional diffusion must be made; however, no field oxide is required. Fig. 3 shows the basic processing steps used to fabricate a simple p-channel c.c.d. A further processing step is usually used to passivate the device, by coating the aluminium transfer electrodes with a vapour-deposited silicon oxide—Fig. 3(c).

### N versus P-channel c.c.ds

Charge-coupled devices—formed on n-type substrates, already studied in part 1, have certain disadvantages over the performance of p-types, for a given gate arrangement.

For p-channel, n-type substrate, devices, the channel must always be maintained in depletion. Otherwise the signal minority carrier charge, which is only located in the depletion region wells, will be lost. n-channel devices have a built-in surface depletion region owing to the positive  $Q_{SS}$  charge which is located in the gate insulator (see Fig. 2). The  $Q_{SS}$  charge tends to enhance the surface charge level in p-channel devices but deplete the surface in n-types.

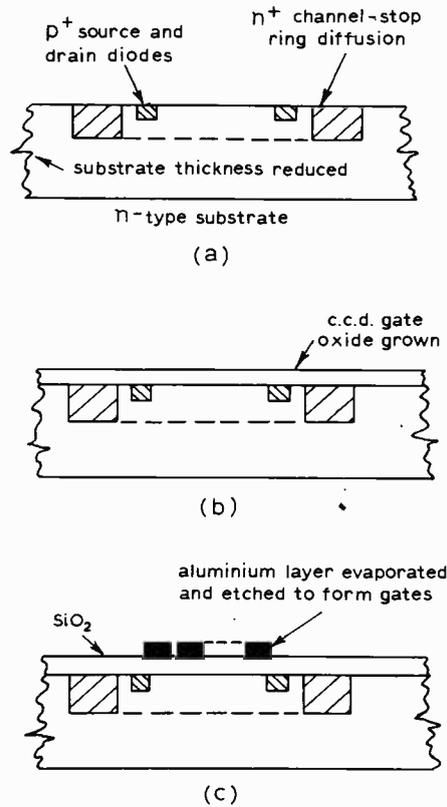


Fig. 3. Basic single-level metal c.c.d. process steps: (a) drain, source and channel-stop diffusions, (b) gate-oxide grown, and (c) aluminium layer evaporated and etched to form individual gates.

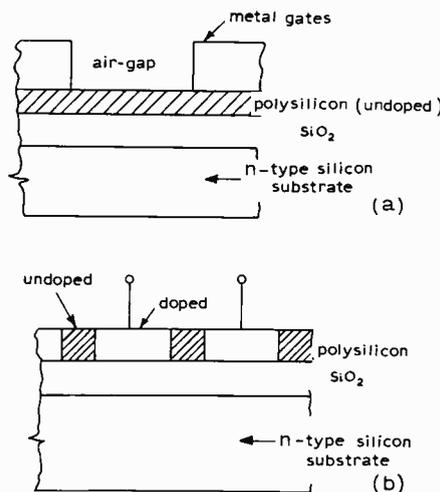


Fig. 4. Two alternative c.c.d. structures to Fig. 1, for metal gates (a) or polysilicon gates (b).

Carrier mobility in an n-type substrate is higher than for p-types. This means that the ultimate speed limitation on an n-channel c.c.d. is inherently higher than for a p-channel device.

Finally, a p-channel device has a higher  $V_T$  than an n-channel device. This is an important consideration for both on-chip and also commercially available clock generators.

### Modifications to single-level metal structure

Both an increased stability of the c.c.d. structure, and a reduction in the need for

narrow gaps can be achieved by using the "resistive sea" process modification<sup>1,2</sup> which comes in several forms. For example Fig. 4(a), useful for metal gates, and Fig. 4(b), useful for polysilicon gates. The polysilicon is lightly doped or used as grown (undoped). However, its conductance is higher than the gate insulator so that it acts effectively as a conductor, and helps to stabilize the surface potential against variations in charge within the insulator.

An advantage of this process is that the inter-electrode gap can be increased substantially for the same operating performance of a narrow gap structure. However, the high-resistance conductor and the distributed, associated gate capacitance, makes the gap look like an electrical RC transmission line. The characteristic delay associated with this equivalent circuit for the gap may severely limit the high frequency performance, even though the doping level of the polysilicon has been increased to reduce the delay to a practical minimum. This resistance between the gates presents an increased differential loading on the pulse generators which are driving the c.c.d.

### Gapless c.c.d. structures

The solution to the instability problem, coupled with increased performance, can be achieved by using overlapping, or gapless gate techniques. There is usually also a slight easing of the alignment tolerances. The penalty to pay, normally, is a multi-level gate arrangement which involves a more involved processing schedule. Fig. 5(a) shows how a three-phase, improved c.c.d. can be fabricated using doped polysilicon to produce a gapless gate arrangement<sup>3</sup>. Each gate overlaps, or is overlapped by, the next gate. A similar approach to this for the formation of the gates can be used to form a four-phase c.c.d. (see later). In this structure, the gates can be made by evaporated metal, and/or polysilicon gates<sup>4,5</sup>.

### Two-phase c.c.ds

The main attractions of a c.c.d. which can be operated by a two-phase clock are the simplified clocking arrangement, and for a given gate length, a two-phase structure may take up less area. Directionality of charge flow can be obtained by a variety of techniques.

**Stepped-oxide structure.** Frequently the two levels of conductors (gates) are produced by a stepped-oxide structure<sup>6,7</sup>, Fig. 6(a), or by the two-phase clocking of a four-phase c.c.d.<sup>8</sup>, which has been fabricated with a deposited oxide and a thermally grown oxide, Fig. 6(b). These structures have the effect of producing gates with alternatively high, then low gate capacitances. Consequently, when the maximum value of the gate voltage on each phase is equal, then the size of the depletion regions (or the well depths) will have two values owing to the different gate insulator fields. This results in charge always propagating in one direction.

Essentially, the main disadvantage of a two-phase structure is that the charge-carrying capability, otherwise known as the dynamic range, is reduced for the same gate voltage size as in a three-phase structure. For a gate voltage,  $V_g$ , the charge-carrying capability,  $Q$ , of a c.c.d. can be written<sup>9</sup>

$$Q = C (V_g - V_T)$$

per unit gate area, where  $C \propto 1/t$  is the capacitance per unit area of an oxide of thickness,  $t$ .  $V_T$  is the threshold voltage for the m.o.s. capacitor formed by a c.c.d. gate, its oxide and the substrate beneath it. It can easily be seen from this equation, that the charge-carrying capability increases by either increasing the gate voltage, or reducing the gate-oxide thickness. Notice that if charge is introduced into the oxide (see Fig. 6(e))  $V_T$  will change its value, and so will the charge-handling capacity of the c.c.d.

**Ion-implanted barriers.** The complex processing of a two-level metallization technique can be eliminated by using an implanted barrier to achieve directionality<sup>10</sup>, Fig. 6(c). This technique has two potential advantages over other two-phase c.c.d. structures in that it provides a fairly large dynamic range and the length of a shift-register bit is just larger than two gate lengths (say  $< 20\mu\text{m}$ ). However, using ion-implanted substrates does not solve the requirement for an overlapping gate arrangement to achieve high charge transfer efficiency.

**D.C. offset voltage.** Asymmetry in the depletion region depths can be obtained by using two-level clock amplitudes across a single-level metallization structure. However, rather than having to generate this clock pulse train, it is easier to have each of two clock phases connected to consecutive pairs of gates, but incorporating a d.c. bias to one gate of each pair, Fig. 6(d).

**Fixed oxide charge.** When additional charge is introduced into the oxide of an m.o.s. capacitor the threshold voltage is altered. For a single-level metallization c.c.d. structure, when a charge is introduced into the insulator of alternate gates, the depletion regions will be different under consecutive gates. This will result in two-phase operation, when pairs of gates—each pair having a corresponding insulator region with, and without introduced charge—are clocked.

Additional charge may be introduced conveniently when the gate insulator comprises two insulators, Fig. 6(e), having different conductivities, e.g. silicon nitride covering silicon dioxide (m.n.o.s.). When pulsed with a voltage, the m.n.o.s. capacitor threshold voltage changes<sup>11</sup> in value and sign under certain conditions. This shift in threshold voltage is due to charge which accumulates at the nitride-oxide interface owing to tunnelling currents through the very thin ( $\sim 50 \times 10^{-10}\text{m}$  gate oxide). The charge density should remain constant at the interface for many years when the applied insulator

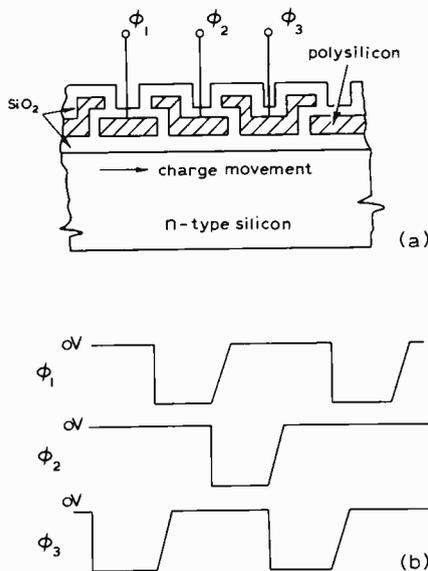


Fig. 5. Gap problem is avoided in this gapless technique, at the expense of more complicated processing. This can also be applied to four-phase devices.

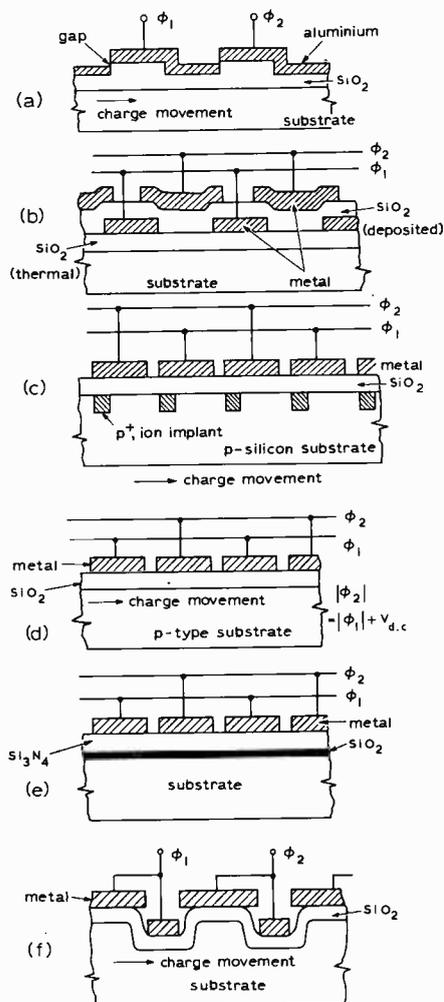


Fig. 6. Two-phase c.c.d. structures: stepped oxide (a), deposited oxide (b), ion implant (c), d.c. offset (d), m.n.o.s. (e), and profiled silicon (f).

voltages remain at normal c.c.d. clock levels<sup>12</sup> ( $< 20\text{ V}$ ).

This m.n.o.s. technique has been used to form a single-phase c.c.d.<sup>13</sup>, by introducing two levels of charge into the gate insulator. The device performance can be electrically programmed.

**Profiled substrates.** The necessary small lateral spacing between gate electrodes can be achieved by etching holes, say,  $0.2$  to  $0.3\text{-}\mu\text{m}$  deep in the silicon substrate, Fig. 6(f). Metal, evaporated during some stage of the process, will form breaks at the discontinuity in silicon surface levels. Two- or three-phase devices can be made by this technique<sup>6</sup> by selectively connecting the multi-level gates.

**Four-phase c.c.ds**

Superior clocking performance can be achieved using four-phase c.c.ds<sup>3,4</sup> (Fig. 7). They employ two-level conductor arrangements, which provide all the advantages of a sealed channel technology. Four gates are used to form one bit of a c.c.d. analogue shift register. (This is also the area required for some two-phase devices.) The four-phase structure, being symmetrical, is thus electrically bidirectional and when the clock pulse train is reversed, the signal charge will propagate back along the c.c.d.

To understand the reason for this action, it is helpful to visualize the signal charge as being transferred along the device in a series of depletion-region wells, under the control of gate potential. Given a choice, signal charge will start to fill the deeper adjacent well. In three- and four-phase structures, which are both symmetrical in design, the direction of signal charge propagation is determined solely by the clocking sequence. Correct clocking operation for three-phase devices requires one phase being switched off slowly, as the next gate phase is switched on. Polarity of the clock pulses is also important, and depends on whether the substrate is p- or n-type.

**Fabrication of four-phase c.c.ds**

**Silicon gates.** Four-phase devices are often made using basically a standard silicon-gate m.o.s. process. The gate structure avoids critical mask-alignment problems by using an overlapping gate arrangement, Fig. 7(b). —The gate oxide is thermally grown under stringent conditions for low  $Q_{SS}$  and  $N_{SS}$ .

—A polysilicon layer is then formed on the top of the oxide and doped to achieve low resistance gates.

—The doped polysilicon layer is etched to form individual gates.

—The slices are then placed again in an oxidation furnace to form a top insulator.

—Then aluminium is evaporated over the surface of the oxide and selectively etched to form the overlapping gates.

A further layer of polysilicon could be used to replace the aluminium (see Fig. 5). This last-mentioned gate structure is

particularly useful for imaging applications, because the polysilicon gates are transparent (200-nm thick), whereas metal gates of practical thickness would reflect light.

**Anodized aluminium.** In one process<sup>5</sup>, c.c.ds are made by anodizing first-level aluminium gates, which are first evaporated on a thermal oxide. The oxide of aluminium, which is formed over the surface of the aluminium, provides the insulation between the two-levels of the metal gates—see Fig. 7(a). Anodization is performed at temperatures which will not affect the previously evaporated aluminium gates. A deposited oxide, at say 400°C, could also be used to form the intergate insulator. Alternatively, a refractory metal that forms a controllable, good quality grown oxide could be used. Molybdenum is a possibility, but its oxide is fairly uncontrollable in thickness.

Fig. 7(c) shows the normal clocking arrangement for a four-phase n-channel device. Signal charge resides in turn in the depletion region under each of the four gates. An alternative and most useful arrangement is called double clocking: Fig. 7(d). This is possible where the gate oxide under each gate is the same thickness and the gate areas are similar. The advantages of this clocking sequence are:

- The clocks are on for twice the normal duration, therefore twice the normal amount of charge can be propagated, leading to a larger dynamic range than normal.
- Efficiency increased because the area under an electrode is without carriers for a shorter time than normal.
- The possibility of simpler clocking because each pair of clocks, e.g.  $\phi_1$  and  $\phi_3$ ,  $\phi_2$  and  $\phi_4$ , are mirror images.
- The clock breakthrough can be significantly reduced because of the mirrored clocks.

**Buried-channel c.c.ds**

**Basic device.** Surface-channel c.c.ds suffer from the fact that charge moves at the surface of the silicon, in intimate contact with the fast surface states. Unfortunately, the density of these states cannot be reduced beyond a certain minimum value, and interaction with these states is a major contribution to the charge transfer efficiency. In a buried-channel device<sup>14,15</sup>, Fig. 8, the depletion region well starts to form below the surface, within the bulk of the semiconductor. The shape and location of the depletion region, and, consequently, where the signal charge resides, is determined by several factors: the doping level and profile of the substrate; the oxide thickness; and the applied voltage. Because the charge is made to move within the semiconductor, only bulk trapping centres affect  $\eta_T$  (these are normally at a low density as compared to  $N_{SS}$  surface values). The carriers can move at higher velocities within the bulk because the bulk mobility is larger than the surface, inversion layer value. However, the charge handling capacity of the buried-channel

c.c.d. is lower than the surface version, owing to the larger effective distance of the charges to its gate electrode.

**Construction.** Buried-channel devices are usually made on n-type silicon layers on top of p-type substrates. The n-type layer is usually either ion-implanted with an n-type dopant, or epitaxially grown in an r.f. reactor.

The gate arrangements for buried-channel devices are usually three- or four-phase schemes which have been described

earlier. Fig. 8 shows a simple buried-channel c.c.d. with a three-phase gate arrangement. Four-phase devices can in some circumstances be driven by sine-wave clocks at 5 or 6 volts peak-to-peak. This development is most significant for the advanced high-frequency applications of c.c.ds.

**Testing**

At the end of the fabrication process, the finished slice contains perhaps hundreds of potentially working c.c.ds and m.o.s.ts. Before the wafer is scribed-up to produce individual chips, the circuits are d.c. tested. A test computer is often used to control the current and voltage sources used in the test, set the test limits on the detectors, and store the test data in a memory which can be read-out at a later time.

The parameters which are usually monitored to determine the d.c. performance of the chip, and thus the probability that the circuits will work under dynamic conditions, are simple continuity tests (forward biasing diode junctions); the gate oxide breakdown voltage (usually measured on the clock phases); a test to establish if any shorts exist between clock phase lines, and the source and drain diode reverse leakage. A c.c.d. chip which fails any of these d.c. tests is rejected by inking the offending device with the prober "inker" and removing it after the slice is scribed.

**Chip cost and yields**

The chip cost calculation has basically three components:

- wafer processing cost—including labour and overheads;
- yield—proportional to the number of photoresist-masking steps required to fabricate the silicon slice, and
- area per bit required for a particular structure, which is a function of the number of bits in the device.

As the fabrication cost of a chip, and therefore the c.c.d. cost, depends exponentially on the chip area it is necessary to aim for a square layout. This has led to making c.c.d. shift registers, with many bits, in a serpentine shape and in some cases to serial-parallel-serial memory layouts<sup>16</sup>.

**Future developments**

The commercial future of c.c.ds largely depends on the degree of process compatibility with existing standard m.o.s. processes; especially silicon-gate m.o.s. devices. The applications areas where this is particularly relevant is in the mass-memory market, where the cost per bit is a crucial parameter and high yields are essential. However, there will undoubtedly be applications, especially in the specialized military system area, where high component costs can be tolerated and therefore where non-standard processes are acceptable. A full treatment of the progress of c.c.ds in penetrating specific application areas will appear in later parts of this series.

As regards future developments in

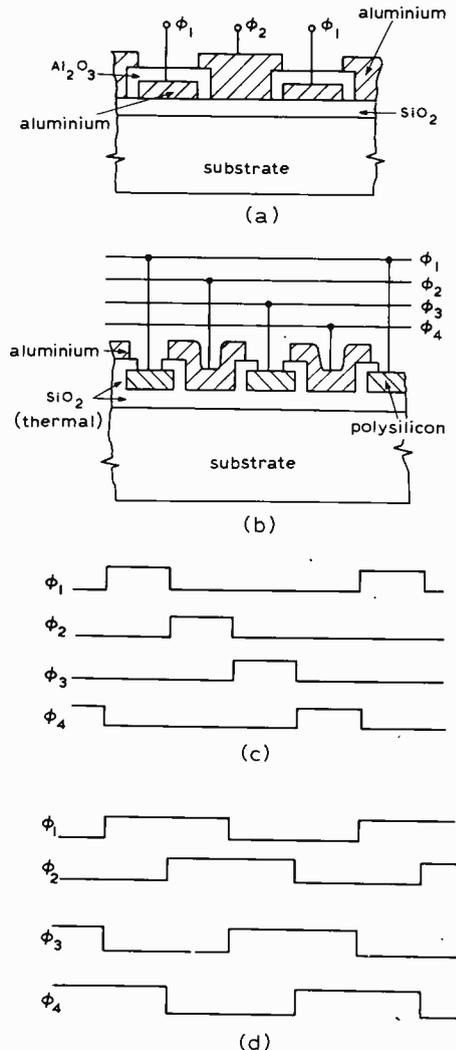


Fig. 7. Four-phase overlapping-gate c.c.ds can have anodized aluminium gates (a), or polysilicon ones (b)—especially useful in imaging devices because of their transparency. Double clocking (d) allows twice the charge to be propagated and increases efficiency over normal clocking (c).

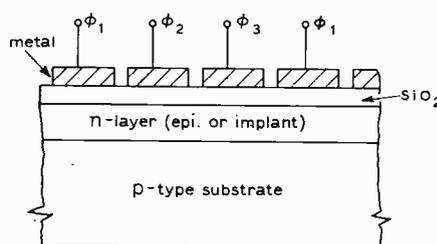


Fig. 8. In buried n-channel c.c.ds, carriers can move faster within the bulk because mobility is larger than the surface value.

c.c.d. technology, new techniques for producing sub-micron inter-electrode gaps, such as by electron-beam lithography, will undoubtedly have an important influence on device structures and therefore result in improved performance. Another possibility is fabricating devices in materials other than silicon. Silicon technology is established; and the processes for growing stable oxides and making good diodes is well understood.

However, materials exist which potentially offer improved c.c.d. performance, if a suitable technology based around the new material existed. A prime example is gallium arsenide. It has a mobility about four times higher than for silicon. Thus, c.c.ds based on gallium arsenide should have a significant speed advantage. Its optical properties compared with silicon make it an interesting proposition for imaging applications. However, before gallium arsenide devices become widely available the cost of the starting material will have to drop substantially, and the high surface state density, which occurs with this material, will have to be reduced by further research.

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# Conferences & Exhibitions

## LONDON

**Spectrum Utilization in Radio Communication**  
Feb. 11-14 Savoy Place  
(IEE Conference Department, Savoy Place, London WC2R 0BL)

**Low Light and Thermal Imaging Systems**  
Mar. 4-7 Savoy Place  
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**Satellite Communication Systems Technology**  
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**Intermag 1975**  
Apr. 14-17 Imperial College  
(The Secretariat, Intermag 1975, c/o Institute of Physics, 47 Belgrave Square, London SW1X 8QX)

**Static Electrification 4th Conference**  
May 5-8 CEGB Headquarters  
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**Antennas for Aircraft and Spacecraft**  
June 3-6 Savoy Place  
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**Film 75**  
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**Optical Fibre Communication**  
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**Signal Filtering**  
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**BANGOR**  
**Instrumentation in Oceanography**  
Sept. 23-25 Univeristy College  
(IERE, 8-9 Bedford Square, London WC1B 3RG)

**BIRMINGHAM**  
**Advances in Automatic Testing Technology**  
Apr. 15-17 Birmingham University  
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**CAMBRIDGE**  
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**European Electronics Circuit Techniques**  
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**Aerospace Instrumentation Symposium**  
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**Engineering Uses of Coherent Optics**  
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**HATFIELD**  
**Theory and Applications of Walsh Functions**  
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(P. D. Lines, Dept. of Electrical Engineering, Hatfield Polytechnic, PO Box 109, Hatfield, Herts)

**LOUGHBOROUGH**  
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# Letters to the Editor

## "SETTLING TIME" IN AUDIO AMPLIFIERS

In an earlier article in your pages<sup>1</sup> I noted that there appeared to be a relationship between the tonal quality of an audio amplifier and the type of transient response of the amplifier following a step function input under reactive load conditions. This was more noticeable with complex l.s. systems, which might be presumed to offer more highly reactive load impedances at certain parts of the frequency spectrum, than with simple l.s. configurations.

Shortly afterwards there appeared the now celebrated paper by Dr Ojala<sup>2</sup> which looked at the problem of the transient behaviour of audio amplifiers on a formal basis, and drew attention to the possibility of transient intermodulation phenomena when the rate of change of the input waveform applied to a feedback amplifier exceeded the possible rate of change of the feedback voltage (or current).

Recent work in the field of high-quality operational amplifiers has led to the widespread adoption and specification of the parameter "settling time" as a measure of the transient performance of such amplifiers under specified load conditions. This is defined as the time which elapses between the application at the input of the amplifier of a notionally ideal step function, and the "settling" of the output signal at a level which is, and remains, within some specified error band about its final output voltage.

I would like to suggest the extension of this concept to the field of audio amplifiers, as a means of defining the transient performance, partly because it is a readily visible and measurable thing—as an examination of the published "square wave" oscillographs in normal amplifier reviews will readily confirm—but principally because the argument suggests itself that when the output of an amplifier has "settled", steady state conditions, as defined by conventional t.h.d. and intermodulation distortion characteristics, must surely apply.

Following this argument, I would like to suggest, therefore, that the target for good-quality audio amplifier design should be

that t.h.d. should be, and remain, below 0.1% within the useful audio spectrum and the whole of the output power range, and also that the transient performance of the amplifier, under the anticipated "worst-case" reactive load condition, should be such that the output voltage settles within an appropriate error band (a realistic figure is probably  $\pm 0.5\%$ ) within a time which is short in relation to the highest frequency signal the amplifier is likely to be called upon to handle; 5 microseconds seems an appropriate value.

(If an input CR lag network is incorporated at the input of the amplifier, as part of the design, to limit the possible rate of change of the input voltage waveform—which may well be a prudent thing to do—the true settling time may be less than the apparent rise time, but can be derived from the difference between the measured rise time and that predictable from the effect of the input RC network.)

Apart from the questions which this hypothesis may raise in respect of the performance of available audio amplifier designs, it also raises a query as to the desirability in use of steep cut audio filters, which not only produce an increase in settling time when used, but also—demonstrably—will introduce colouration on a "white noise" signal, perhaps for this very reason.

J. L. Linsley Hood,  
Taunton,  
Somerset.

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## REDUCING AMPLIFIER DISTORTION

In his article in the October issue (page 367) Mr Sandman states that "In Fig. 1 the undistorted part of the output  $V_{in}R_2/R_1$  balances off at the junction of  $R_1$  and  $R_2$  to produce zero voltage, the only voltage to appear at this point being proportional to the distortion".

This statement is not strictly accurate. In Fig. 1, and in other circuits, the amplifier input is connected to the junction of  $R_1$  and  $R_2$ . It is obvious, therefore, that the undistorted component of voltage at this point cannot be zero. If it were, the amplifier would have no input and could produce no output. If  $A$  is large the voltage approximates to  $V_{in}R_2/AR_1$ ; it may well be that this is small compared with the distorted voltage fed back, but it can never be zero.

Referring again to Fig. 1, there is a point in the circuit at which the undistorted component of signal does balance to zero, to leave only a distorted component. This point is not at the junction of  $R_1$  and  $R_2$ , but is along  $R_2$  between the input and output of the amplifier  $A$ . To obtain a true balance to zero it is necessary to connect the input of  $A_2$  in

Fig. 2 to a tapping point on  $R_2$  instead of to the input of  $A_1$ . This point on  $R_2$  is critically dependent on the gain of  $A_1$ , however, and precise adjustment is needed to obtain the proper condition. As long as  $A_1$  is high enough, therefore, it is probable that Mr Sandman's non-critical arrangement is better in practice.

There is no mention in Mr Sandman's references to the work of W. Baggally ("Distortion cancellation in audio amplifiers", *The Wireless Engineer and Experimental Wireless*, August 1933, page 413). I referred to this in my letter in the April 1973 issue of *Wireless World*, page 192. In Baggally's scheme a phase-reversing main amplifier had a resistance with an adjustable tapping connected between its input and output. A non-phase-reversing amplifier was fed from this tapping and its output applied to the input to the main amplifier. Critical adjustments of tapping point and of subsidiary amplifier gain were required, which is probably why the circuit never achieved popularity.

W. T. Cocking,  
Ewell, Surrey.

### Mr Sandman replies:

The part of the article "It cannot be too strongly stressed . . ." (page 367) deals with the definition of distortion which I employ. Distortion includes frequency, amplitude, phase and non-linear distortion.

I am sure it is common ground that the output can be split up into two parts, undistorted

$$\left( V_{in} \frac{R_2}{R_1} \right)$$

and distorted  $V_D$ .

It follows that  $V_{in}$  and  $V_{in}R_2/R_1$  balance off to zero at the input to  $A_1$  and  $A_2$  and that the voltage at this point is the distortion ( $V_D$ ) attenuated by  $R_1$  and  $R_2$  (a small voltage). This attenuation is compensated by the gain of amplifier  $R_1', R_2'$  and  $A_2$  to produce  $V_D'$  (the error take-off voltage as I now define it) which is taken off the output appearing across  $R_L$ .

If Mr Cocking were to build Fig. 11 incorporating the corrections in *Wireless World*, November 1974, page 454, I am sure his doubts would be laid to rest.

Mr Baggally's scheme falls down on both the principles of "non-interaction" and "rigidity of interconnection".

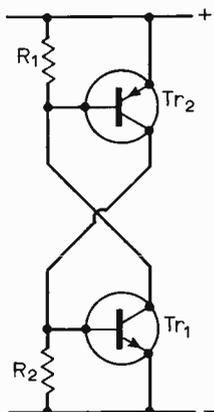
## CIRCUIT DIAGRAM LAYOUT

The article by Mr Amos on circuit diagram layout (November issue) was certainly welcome in these days of atrocities typified by his Fig. 9.

While agreeing with most of his recommendations, the golden rule I like to follow is to draw everything that is more positive "northwards" of everything that is negative, so that travelling from the bottom to the top of the paper each conductor is in order of potential above

earth. This makes it easier to understand the circuit once one has recognized it.

Therefore I totally abhor Mr Amos's Fig. 6 which, although it may be "clearly a multivibrator", is not easy to understand. I suggest the following drawing is preferable:



The crossover is preserved and so are the polarities. Caution is still needed, however, or, like Mr Amos, one might miss the fact that this *never* was a multivibrator, but is a bistable which self-destructs when triggered!

David Williams,  
London SE12.

Speaking as one who earns his daily bread in a world of circuit diagrams I must say I entirely agree with the admirable basic aims set out in your November 1974 editorial and the opening paragraph of Mr Amos's article on layout of circuit diagrams in the same issue.

However, I feel Mr Amos has missed the point in attempting to lay down standard circuit diagram patterns for every type of circuit. Since there are already countless different circuit configurations and new circuits are being designed every day, you can never hope to achieve a standard pattern for every circuit. The aim should be to assist a complete stranger to learn the function of a particular circuit configuration; if someone who is already familiar with the circuit can instantly stamp it with the name "Colpitts oscillator" (or whatever) then so much the better, but that should be a secondary aim.

I therefore suggest four basic rules for a good circuit diagram should be, in order of priority:

- (i) current flow vertically downwards;
- (ii) signal flow from left to right and top to bottom;
- (iii) minimize the number of bends in connecting lines;
- (iv) minimize the number of crossings of connecting lines.

I place (iii) above (iv) because a line is fairly easy to follow if it is straight, even if it does cross several others in its path.

In my experience, when one encounters a totally unfamiliar circuit configuration rule (i) is fundamental in attempting to understand its function. Fortunately nowadays most circuits are drawn to this convention, which enables one to visualize small voltage changes as "up or down" and to keep a clear track of the various

inversions a signal undergoes.

By this argument, Fig. 5 in the article is preferable to Fig. 6, contrary to Mr Amos's conclusions. Being able to stamp Fig. 6 with the name "multivibrator" does not help one to understand its operation, since it is unusual in that both transistors are on (or off) simultaneously.

Paul V. J. Adkins,  
Braintree, Essex.

*Mr Amos replies:*

I am glad that Mr Williams welcomed my article in general and I like his redraw of the multivibrator circuit. I am puzzled, however, by his final sentence which seems to imply that a multivibrator cannot be bistable. In fact electronic circuitry bristles with bistable multivibrators usually abbreviated nowadays to just bistables. I take Mr Williams's point about my Fig. 6; I have perhaps oversimplified this in order to emphasize my argument. In a practical version of the circuit current-limiting resistors are necessary.

Mr Adkins also advocates the "current downwards" approach in circuit diagram layout and I think this has much to commend it in digital circuits. My article was, however, chiefly devoted to analogue circuits as I made clear in my first paragraph and here I think it is preferable to aim at preserving the standard pattern for well-used circuits no matter what the direction of standing currents. This is also the view of BSI as made clear in Section B2 of the Guiding Principles of BS3939.

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## TRACKING FILTERS

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I was very interested in the article in your October issue by Messrs Knott and Unsworth, particularly in their implementation of the technique of 50Hz rejection with modern methods and their analysis of the performance of the filter.

One of the earliest examples of this method was described in 1953 by Beard and Skomal<sup>1</sup>. They used a switched capacitor storage system to reject 60Hz interference in a model of a geophysical prospecting situation.

The technique has also been widely used for rejecting all signals (as well as those from mains) which are not locked to the store switching rate. Three papers which have probably not received the credit they deserve, because of inaccessibility, are by G. Suryan<sup>2,3,4</sup>. He used a synchronous magnetic store and his analysis showed clearly its behaviour as a comb filter.

A switched capacitor store was introduced by me for rejecting 50Hz; and all other signals not locked to the switching cycle, in 1951 and described more fully in 1953<sup>5</sup>. Although the electronics are obsolete the account of the method may be of interest because it outlines some of the precautions against stray capacitances and capacitor leakage which are needed

if a stored waveform is to retain its shape. This technique has now become a standard method of examination in man for delay of conduction in diseased nerves. Also it is used for examining transmission in the auditory pathway in children who cannot communicate.

The technique is now usually implemented by purely digital methods, but there may still be a use for capacitor stores in special purpose applications. So it seems well worthwhile emphasizing the more general applications of a system such as that described by Knott and Unsworth. It can be easily used to extract the response of any system which can be stimulated at a fixed time in relation to the store switching cycle. Also, with digital switching, the occurrence of store switching cycles and locked stimuli may be irregular, if this is an advantage.

G. D. Dawson,  
Department of Physiology,  
University College London.

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## QUADRAPHONIC QUANDARY

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It would be pointless to make a *technical* reply to Mr Bauer's letter (September 1974) which concludes that it is sufficient for the producer and recording director to make and approve the SQ record and so "the various mathematical and philosophical arguments about quadrphony, therefore, become inconsequential".

How delightful! Quadrphony equals SQ. All controversial problems may now be set aside.

B. J. Shelley,  
Rome,  
Italy.

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## AMPLIFIER CLAIMS

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I have just noticed an advertisement in your May 1974 issue, placed by Radford Audio Ltd. I wish to make some comments on some of their claims, as they have made some very bold statements

which I doubt would stand the scrutiny of the Trade Descriptions Act.

First, their statement, "We believe no other amplifier in the world can match the specifications of the HD250". I don't believe that they have checked other makers' equipment from, say, the USA or Japan. There are several pre-amps and main amps made in both these countries that will equal it and better it by an easy margin—if the Radford specs are written in the same manner. They are not properly defined.

Secondly, to say distortion (pre-amp) is zero is a very bold statement, to say the least. According to the IHF method of measurement, the only true distortion figure to quote is what is called total harmonic distortion (t.h.d.) which is defined as including noise hum, all spurious and harmonics of the frequency being measured. Incidentally many British makers seem to "loophole" their way round amplifier distortion these days by stating only harmonic distortion, let alone which one! The reason for including noise is that all amplifying circuits add some noise which was not there on the original signal fed in, thereby distorting the original. (This I know is a hypothetical case.) So let's have a look at their case—making many assumptions. That the phono has a sensitivity of 2mV at 1kHz and the nominal output from the pre-amp is 1 volt, then the lowest distortion with reference to this can only be about 0.03%, not zero. The disc noise is given as -83dBV bandwidth limited to 23kHz, but with respect to what! The generally accepted method of quoting noise in Japan is on a wide band measurement up to 1MHz and against a nominal 2.2mV at 1kHz sensitivity, and for auxiliary or other high level inputs a reference of 150mV is used. Likewise whose "A" weighting do they mean? Overload margin of "disc" input is quoted at 40dB; nothing marvellous. I could find other points to grumble about in this advertisement.

Tim de Paravicini,  
Lux Corporation,  
Osaka, Japan.

*Reply from Radford Audio Ltd:*

Mr Paravicini's comments are a little inconsistent and misleading. Am I to understand that our current advertisements for the HD250 amplifier would not stand the scrutiny of the Trade Descriptions Act because the performance specification extracts appear too good to be true? If so, then how can it be that several pre-amplifiers and power amplifiers in USA and Japan "will equal it and better it by an easy margin"?

The phrase from our advertisement "We believe that no other amplifier in the world can match the specification of the HD250" is mis-quoted by him as "We believe no other amplifier in the world can match the specifications of the HD250". Mr Paravicini's plural specification is taken to mean "some specification details". The word "specification" (singular) means the totality of all specification detail. This includes visual presentation,

engineering design, quality of manufacture, servicability, facilities and functions available, flexibility in use, performance characteristics, etc. Mr Paravicini appears to have become enmeshed by his loose reading and colloquial popular hi-fi jargon.

In the advertisement it quite clearly states that the performance details quoted are extracts, and the specification is therefore not complete. In it readers are invited to write for a 12-page leaflet which describes the design details of the HD250, together with a complete specification. It is not possible or desirable to give a complete specification in an advertisement. Nor is it expected that our potential customers will purchase amplifiers by just reading the advertisement, or even after studying the leaflet, but only after hearing and comparing the HD250 with other amplifiers in the dealer's showroom.

The fact that we believe that the specification of the HD250 cannot be matched by any other *integrated* amplifier does not make it a claim or a fact. Nevertheless it is reasonable to expect that we have done some work to justify our opinion. Our belief is based on measurements carried out on amplifiers available in this country, and in America with similar test equipment and under similar conditions of test, and not by studying manufacturers' literature. Mr Paravicini compares the performance details of the HD250 quoted with unspecified separate pre-amplifiers and power amplifiers. Although it is generally accepted that it is not possible to obtain some performance parameters as good in integrated amplifiers as in separate pre-amplifiers and power amplifiers it does not alter the fact that we know of no other pre-amplifier with a better overall performance characteristic than the pre-amplifier section of the HD250 (the pre-amplifier section of the HD250 is now also available as a separate unit, namely the ZD22 Pre-amplifier Control Unit).

Concerning distortion. We do not claim that the harmonic distortion of the pre-amplifier section is an unqualified zero as he states. In general text we say that the distortion is "virtually zero" or qualified as in the advertisement "cannot be identified or measured as it is below inherent circuit noise".

The IHF method of specifying total residual background under dynamic conditions of distortion measurement as "total harmonic distortion" makes sense generally as this is what distortion measuring sets measure. If, however, after rejection of the fundamental test frequency by the d.m.s. there are no measurable or observable harmonics left—just the static inherent noise of the equipment under test plus measuring equipment noise if any—then to specify this residual as "total harmonic distortion" is nonsense in any language. When the IHF test specification was drafted such a condition was probably not envisaged. If the total harmonic distortion products generated by an amplifier at the working signal level do not add to the static inherent noise background, then the harmonic distortion can surely be said

to be "virtually zero". In the disc amplifier referred to, the harmonic distortion cannot be measured or detected at working signal level or even at 20dB above. It will be appreciated that distortion levels below 0.01% are largely academic in practical amplifiers for sound reproduction, but this does not prevent engineers from designing better and better amplifiers. The virtual elimination of harmonic distortion in audio amplifiers up to output stage clipping level is a logical target of development.

It is conventional when making distortion measurements with a d.m.s. to display the residual output, after fundamental rejection, on one trace of an oscilloscope and the fundamental on the other. This enables an assessment to be made of the harmonic distortion structure, the character and energy content of noise, crossover spikes, and spurious responses. The contribution of hum can be ascertained by using a 1kHz test signal with the 500Hz filter.

I am baffled by the statement that "British manufacturers seem to 'loop hole' their way around amplifier distortion by stating only harmonic distortion, let alone which one". One could gather from this remark that British engineers have a crafty way of eliminating hum, noise and a dominant second harmonic and quoting only a lower amplitude third harmonic. British manufacturers, in common with American and Japanese manufacturers, use conventional total harmonic distortion measuring equipment in development and do not generally use wave analyzers. As my company has supplied this type of equipment to the major audio manufacturers in this country (and the rest of the world) I am aware of the situation.

The "A" weighting characteristic is incorporated in standard noise measuring equipment and is also used by professional audio engineers in broadcast and recording studios. It was formulated to simulate the subjective hearing response in order to obtain significant noise figures. A bandwidth of 1MHz for audio and acoustical noise measurement is unrelated and misleading.

The 40dB disc overload margin is said to be "nothing marvellous". In itself it may not be extraordinary but if it is taken in conjunction with a noise level near the theoretical minimum and a "virtually zero" distortion at +20dB above operating level and an RIAA accuracy of  $\pm 0.2$ dB then that *is* something. In the HD250 sales leaflet it clearly states that the signal-to-noise ratio is greater than 83dB measured with a noise bandwidth of 23kHz when used with a 5mV output cartridge (1mV/cm/s at reference velocity of 5 cm/s). This figure is considerably better than in any other amplifier we have tested.

I am unable to appreciate the object of Mr Paravicini's letter. Is it intended to be a general tilt at British manufacturers? Is he worried about the advanced state of British audio and acoustical technology—or is it just "I am the greatest"?

A. H. Radford,  
Radford Audio Ltd,  
Bristol.

# Weather satellites ground station—3

## Conclusion of this series with the display electronics described in full

by G. R. Kennedy

The block diagram of the picture display system is shown in Fig. 22.

The scheme of operations is as follows. Assume an input signal from a tape recording of an APT satellite signal at a moment when the signal is in the peak white between picture condition. The signal clock rate is determined by the limiters feeding the phase-lock loop, which locks on to the input signal rate. The phase-lock loop v.c.o. will then follow the apparent input clock rate, within the tracking range limits, and hence take account of tape-recorder wow and flutter. The X ramp generator takes the p.l.l. v.c.o. frequency and produces a step-function

ramp from the buffered square wave signal locked to the input rate. Hence the X ramp also takes account of tape-recorder speed errors. It should be borne in mind that a step-function ramp generator for the X axis is superior to an analogue integrator ramp generator, for the former takes account of signal rate/phase changes cycle by cycle with the input signal, whereas the integrator sums the effect and due to the large time constant, may be lagging or leading the input-signal rate by flyback. This would give a ragged edge to the picture, and displacement of picture details.

The dividers count down the clock rate

in synchronism with any rate changes and accurately trigger the flyback of the X ramp generator.

The start-sync circuit is quiescent during most of the satellite signal sequence. When the 300Hz tone occurs, the circuit resets the decade counters in the divide chain to nine and the divide-by-12 counter to zero at the beginning of one of the 12.5ms black level periods in the five-second phasing period after the 300Hz tone. After 12 cycles of the signal frequency the divide-by-12 circuit changes state and sets the decade counters to zero, which resets the X ramp generator. The 12 cycles of the signal frequency delay the flyback

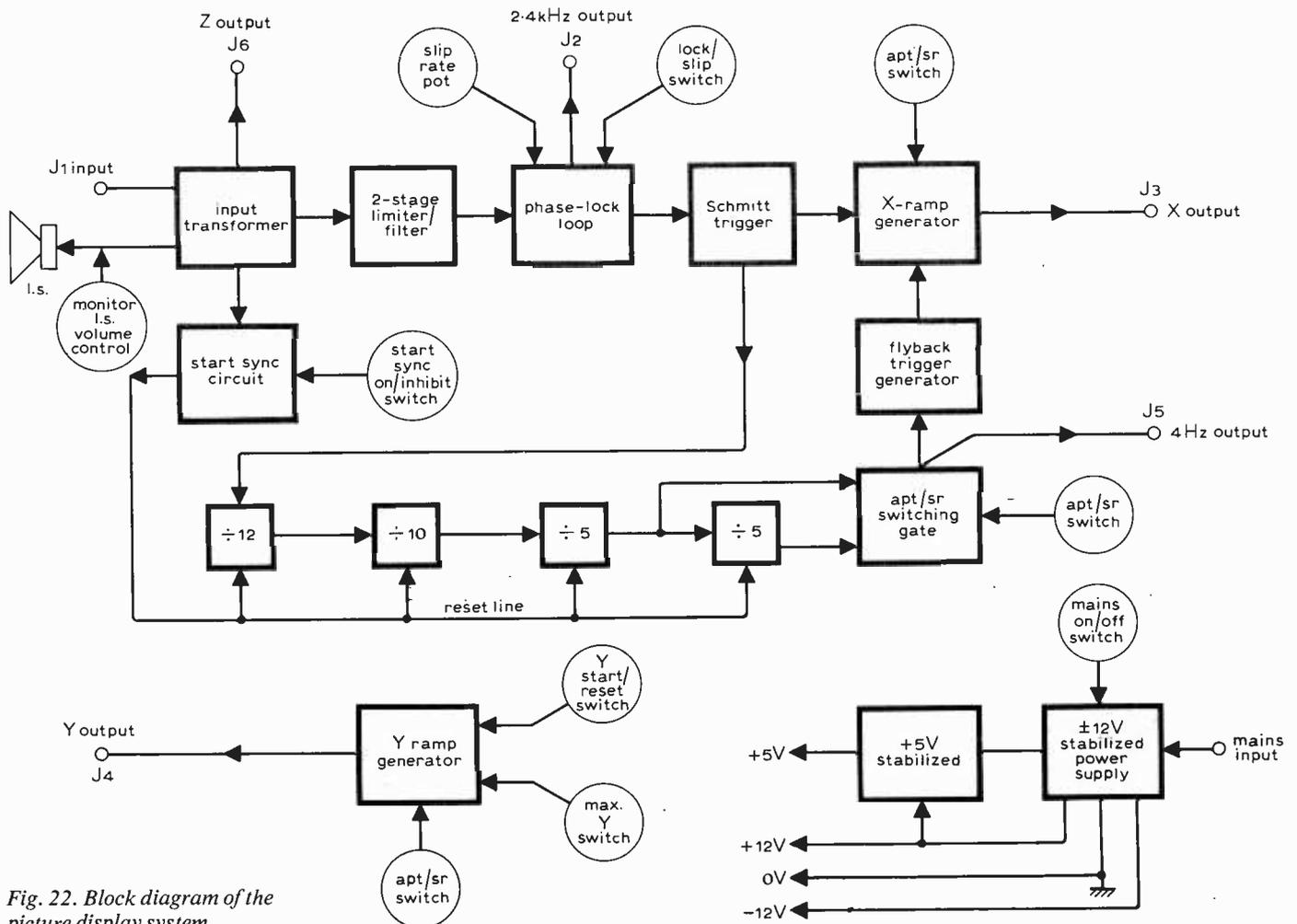


Fig. 22. Block diagram of the picture display system.

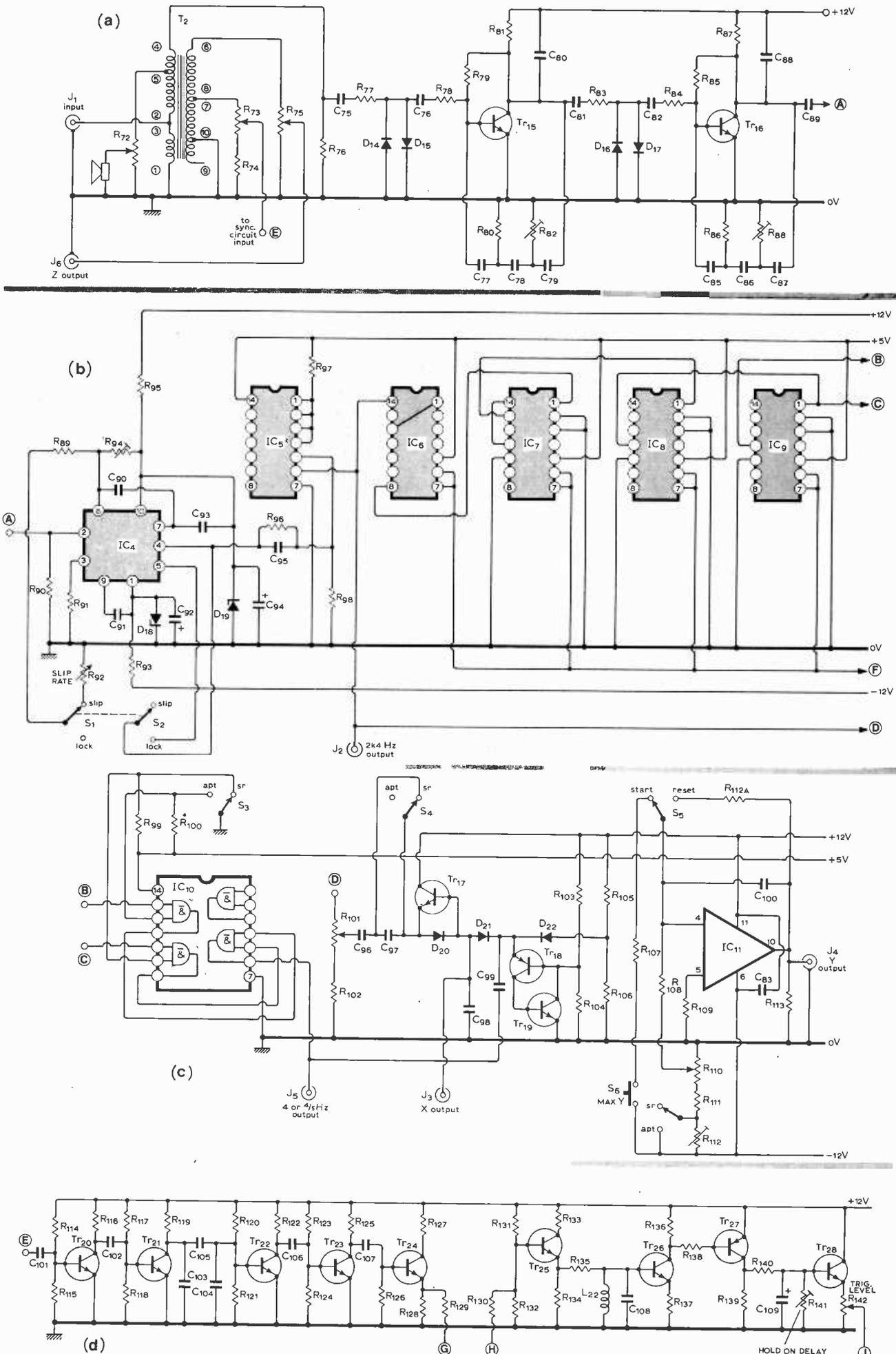


Fig. 23. Display electronics (a) input and limiter/filter stages (b) phase lock loop and divider stages (c) switching gate and ramp generators (d) start synchronizing circuit.

(and start) of the *X* ramp by six ms or so. This forces the *X* ramp to approximately midway through successive black periods in the phasing sequence and centres the picture *X* scan lines so that there is a white border down each side of the displayed picture. The sync circuit keeps the reset line at logic low during the rest of the picture, until it sees more than 1.5 seconds of 300Hz, whence the forcing action occurs again. The chances of the picture containing more than a few milliseconds of 300Hz waveform are remote, but the sync circuit can be manually inhibited, if so required.

In the case of SR pictures such as sent by NOAA-2 there is no interpicture period—the sequence runs continuously—and it is convenient to manually phase the picture for either visible or infra-red picture on the left-hand side, using the lock/slip and slip-rate controls. These unlock the phase-lock loop v.c.o. and allow the p.l.l. output frequency to lag the satellite sub-carrier frequency. In practice it is a matter of moments to manually phase up the picture by observing the picture formation, and by slipping the desired picture border to the left-hand side. The lock position is then selected, and the picture will stay phased. Using the proposed circuit, it would be relatively easy to detect the 23.3ms, 300Hz burst in the NOAA-2 sequence which precedes each IR and visible picture line scan. As it stands, the burst is too short for the circuit to respond, but by switching in increased gain for the SR position, forcing of the counters could be carried out. Also, the 600Hz burst every 30 seconds preceding an i.r. picture line scan could be detected using a 600Hz filter, and the display phased automatically for left-hand IR pictures. For SR pictures, which run continuously during a pass, the *Y* ramp generator is switched to run much slower than for APT pictures. The rate can be set by a preset potentiometer on the APT/SR switch to set the picture to the correct Index of Co-operation. It is for this reason that an analogue integrator is used for the *Y* axis ramp generator, and not a step scan generator.

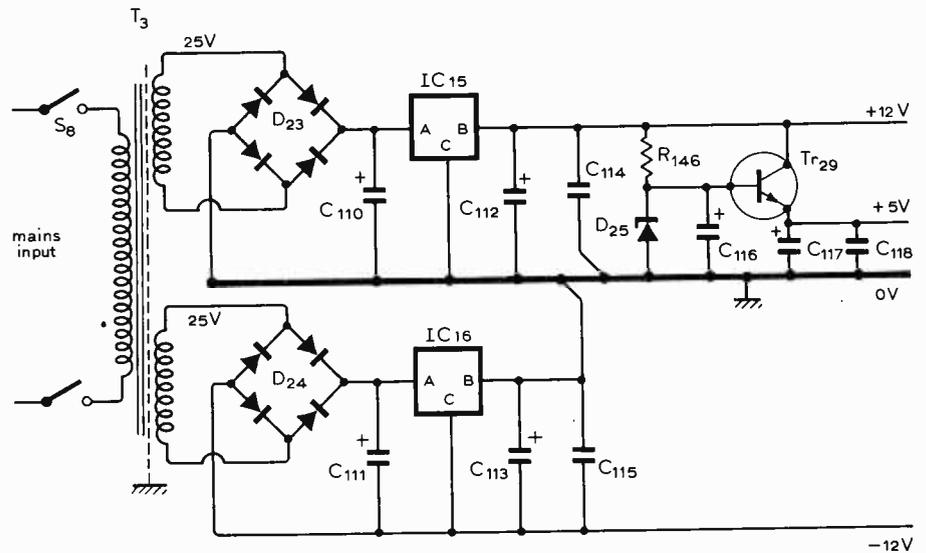


Fig. 24. Display electronics power supplies.

The complete display circuit is shown in Figs. 23, 24.

**Input stage:** the input transformer  $T_2$  is a multi-tapped standard speaker isolating transformer. The number shown refers to the tag number on this transformer. The outputs to the monitor loudspeaker, the sync circuit and to the *Z* axis output socket are variable by simple resistive coupling using potentiometers  $R_{72}$ ,  $R_{73}$ ,  $R_{75}$ . The voltage to the limiter is increased by auto-transformer action to double the input level. Shielding of the input transformer from any stray mains fields, particularly from the power supply transformer is essential to reduce 50 or 100Hz patterning on the displayed picture.

**Limiter/filter stage:** two similar limiters are used in series<sup>7</sup>. The input waveform is clipped on each half cycle by the opposed diodes  $D_{14}$  through  $D_{17}$  and amplified and filtered by  $Tr_{15}$  and  $Tr_{16}$ . The filter networks of  $C_{77}$ ,  $C_{78}$ ,  $C_{79}$ ,  $R_{80}$ ,  $R_{82}$  and  $C_{85}$ ,  $C_{86}$ ,  $C_{87}$ ,  $R_{86}$ ,  $R_{88}$  are simple 180° phase-shift lead networks across the amplifier transistors. For the simple circuit shown, and taking single

values for  $R$  and  $C$ , the filter frequency is very approximately given by  $f \approx 1/2\pi RC\sqrt{10}$

**Phase-lock loop:** an integrated circuit low frequency p.l.l. is used (Signetics NE565A). The usual detected output in unused, and the v.c.o. is RC coupled to the following buffer stage. To avoid feedthrough problems, and for simplicity the circuit has its own  $\pm 5$  volt supplies derived from the  $\pm 12V$  rails. The working point of the input is set by the bias resistors  $R_{90}$  and  $R_{91}$ .

The unlocked idle frequency is set by  $C_{91}$  and ten-turn trimming pot  $R_{94}$ . The internal v.c.o. output connection at pin 4 and the internal p.s.d. connection at pin 5 are broken and brought out to the lock/slip switch, which closes the servo loop for locked operation and opens it for slipping the picture sync. In the latter state the resistive loading of  $R_{89}$  and  $R_{92}$  are sufficient to alter the v.c.o. frequency.

**Schmitt trigger:** as mentioned earlier, a gate or emitter follower could perform as well as the Schmitt trigger. The purpose of the stage is to buffer the p.l.l. output and

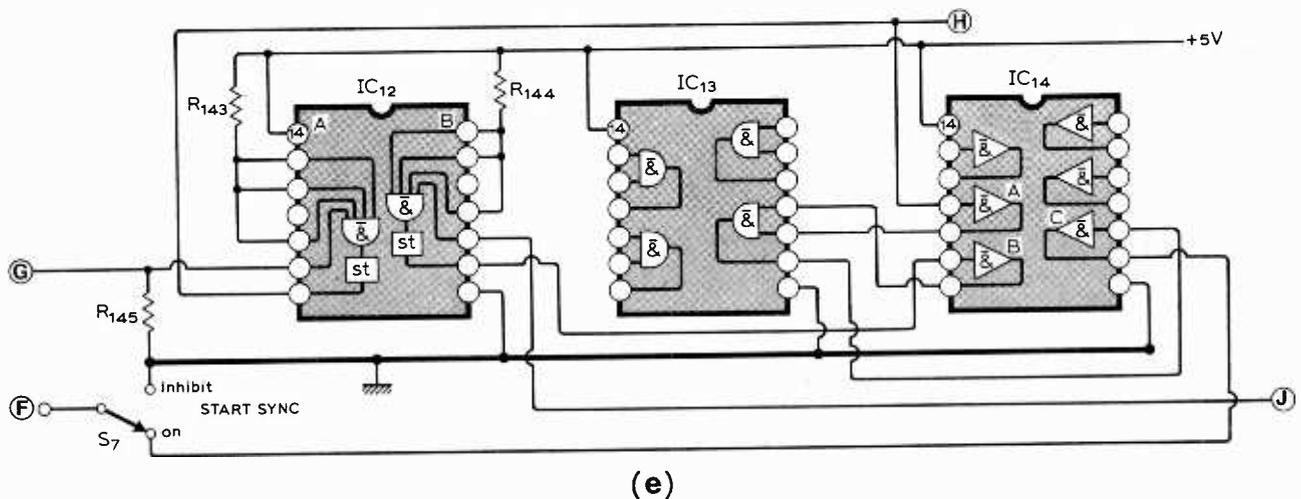


Fig. 23 (cont.) Display electronics (e) start synchronizing circuit.

allow fan-out to the ramp generator and dividers. The use of a digital i.c. gives a guaranteed and precise logic level output, and the dual nature of the NAND Schmitt trigger on the chip used allows for further development work.

**X Ramp generator:** The staircase ramp generator  $Tr_{17}$ ,  $D_{20}$ ,  $C_{97}$ ,  $C_{98}$  is a standard diode transistor pump. The step rise per input pulse of  $V_{in}$  is given by

$$V_0 = \frac{V_{in} C_{97}}{C_{97} + C_{98}}$$

assuming no loading of  $C_{98}$ . As it stands, the output across  $C_{98}$  is at very high impedance, and unless driving a high impedance device such as an oscilloscope amplifier, must be buffered. A simple f.e.t. source follower is suitable.

**Flyback trigger:** The voltage on ramp generator capacitor  $C_{98}$  is coupled via diode  $D_{21}$  to the complementary pair  $Tr_{18}$ ,  $Tr_{19}$ . In the quiescent state the anode of  $D_{22}$  is held at +8.7 volts,  $D_{22}$  is forward biased and  $D_{21}$  is reverse biased, since the ramp on  $C_{98}$  does not approach 8 volts. Diode  $D_{21}$  is a silicon diode and does not present any appreciable discharge path to  $C_{98}$ . Transistors  $Tr_{18}$  and  $Tr_{19}$  are off, since the 8.2V at  $Tr_{18}$  base due to potential divider  $R_{103}$ ,  $R_{104}$

is insufficient to forward bias  $Tr_{18}$  base/emitter diode with the forward conduction potential of  $D_{22}$  in series. When a positive trigger pulse arrives at  $C_{99}$  from the flyback trigger generator  $D_{22}$  cuts off,  $D_{21}$  remains cut off,  $Tr_{18}$  and  $Tr_{19}$  turn on and  $D_{21}$  conducts forwards. Capacitor  $C_{98}$  is rapidly discharged to the level of the sum of the forward bias potentials of  $D_{21}$ ,  $Tr_{18}$  and  $Tr_{19}$ . When no further charge is transferred through  $C_{99}$  the circuit returns to its former state.

**Divider stage:** the divider stage comprises four NAND digital i.c. counter chips: a divide-by-12; a decade counter; an identical counter connected for divide-by-five; and a further divide-by-five counter. All the counters have two input NAND gates for zero setting, and the decade counters have also a two input NAND gate for binary coded decimal nine setting. The divide by 12 zero reset line and the decade counter nine reset line are taken to the output of the start sync stage. The line

NAND GATE TRUTH TABLE

a	b	c
0	0	1
1	0	1
0	1	1
1	1	0

Fig. 25. APT/SR switching logic.

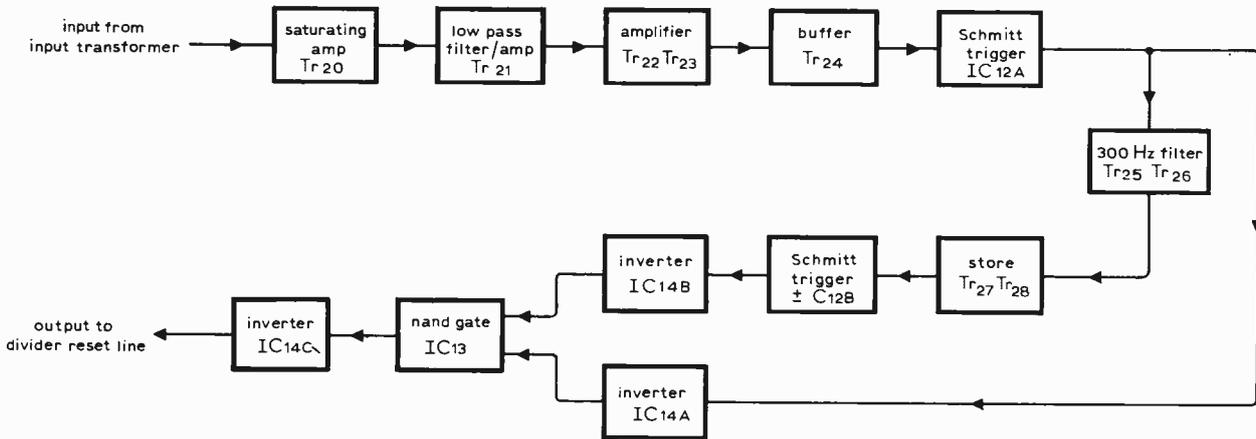
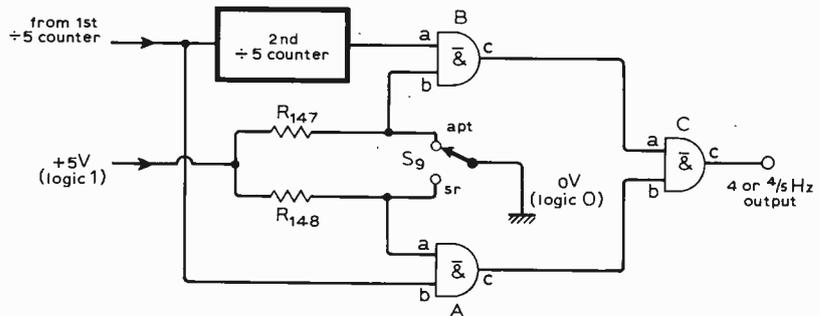


Fig. 26. Start sync circuit block diagram.

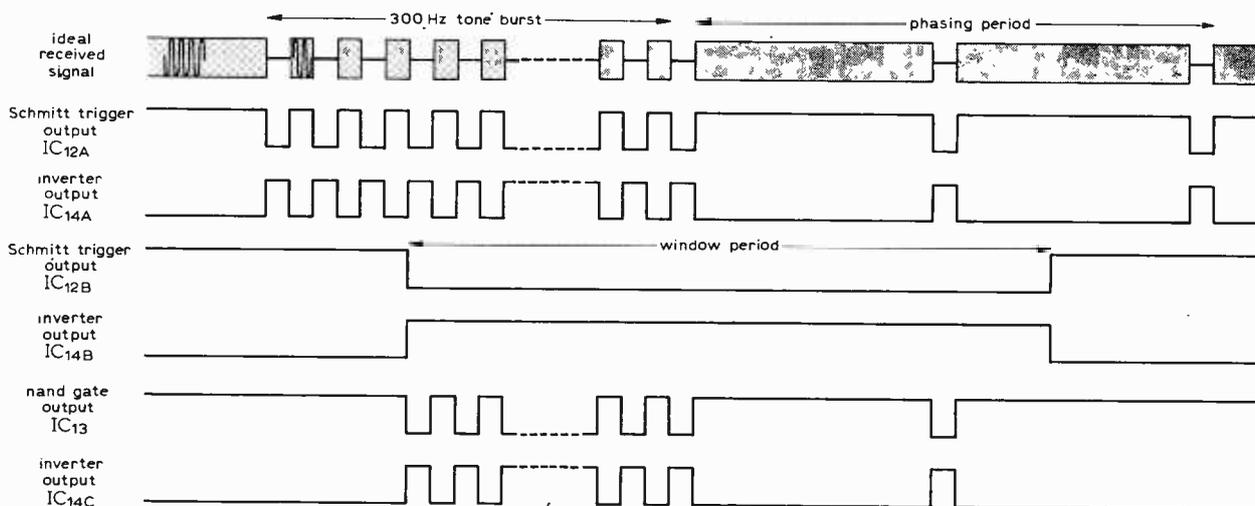


Fig. 27. Start sync circuit waveforms.

is normally held at logic zero, and the counters count conventionally.

**APT/SR switching gate:** the APT/SR switch circuit is shown separately in Fig. 25. Three two-input NAND gates are used, A, B and C. The input to the final divide-by-5 counter is fed in parallel to gate A. The output of the divide-by-5 counter is fed to gate B, and the outputs of the gates feed gate C. Both of the second unused inputs of gates A and B are held at logic 1 by a direct connection through  $R_{147}$  or  $R_{148}$ , but can be set to logic 0 by the APT/SR switch. If any NAND gate input is held at zero, no gate transmission can take place, and the output remains high. Hence, whichever gate is not held at zero conducts, and transmits the square wave input to the output, in inverted state. Since one gate is always held off at logic 1 output, gate C always toggles with the output of the other input gate, and inverts that output, returning the sign of the signal to that at the circuit input.

**Start sync circuit:** the block diagram of the start sync circuit is shown in Fig. 26, and the relevant waveforms in Fig. 27. Referring to the circuit Fig. 23(d), the input is taken from the input transformer via a potentiometer  $R_{73}$  and  $C_{101}$ . Transistor  $Tr_{20}$  forms a high gain saturated amplifier detector. The pi filter  $C_{103}$ ,  $C_{104}$ ,  $C_{105}$  removes the bulk of the 2.4kHz sub-carrier, and further amplification by  $Tr_{22}$  and  $Tr_{23}$  clips the detected signal to rapid transitions between high and low.

This signal is buffered by  $Tr_{24}$  and is converted to precise logic levels by Schmitt trigger  $IC_{12A}$ . The Schmitt trigger output is fed in parallel to an inverter  $IC_{14A}$ , one of six inverters on an inverter chip i.e., and to a 300Hz filter at  $Tr_{25}$ ,  $Tr_{26}$ . Components  $L_{22}$  and  $C_{108}$  are a circuit resonant at 300Hz of low  $Q$  due to the shunting effect of  $R_{134}$ ,  $R_{135}$  and  $R_{137}$  through  $Tr_{26}$  base/emitter diode. Transistor  $Tr_{26}$  collector drives the high gain p-n-p transistor amplifier  $Tr_{27}$ , which in turn feeds the capacitor  $C_{109}$ . When the potential at  $Tr_{26}$  base rises due to a 300Hz tone,  $Tr_{26}$  switches on, which switches  $Tr_{27}$ , which charges  $C_{109}$  by the potential due to the collector current of  $Tr_{27}$  through  $R_{139}$ .

The potential rises on  $C_{109}$  at a rate determined by its capacity, shunting components  $R_{139}$ ,  $R_{140}$ ,  $R_{141}$  and  $R_{142}$ , and by the length of the 300Hz burst. Hence the effect of the 300Hz burst is stored by  $C_{109}$ . Transistor  $Tr_{28}$  emitter follows the charge rise on  $C_{109}$  and depending on the value of potentiometer  $R_{142}$ , triggers Schmitt trigger  $IC_{12B}$ , the second half of a dual Schmitt i.c. chip. This Schmitt output is inverted by  $IC_{14B}$ , and the resultant signal applied to the second input of NAND gate  $IC_{13}$ , together with the inverted output of Schmitt trigger  $IC_{12A}$ . Due to the fact that Schmitt  $IC_{12A}$  output is normally high, and hence its inverted signal is normally low, NAND gate  $IC_{13}$  is normally disabled. When the input due to  $IC_{12B}$  via  $IC_{14B}$  goes high after a 300Hz burst, a window is created when gate  $IC_{13}$

can respond to its input from Schmitt trigger  $IC_{12A}$ , carrying detected signal information.

For the window period, the length of which depends on the length of burst the setting of the storage capacitor shunt  $R_{14}$ , and the Schmitt trigger lever  $R_{142}$ , the NAND gate responds to the detected signal information. The period after the 300Hz burst contains the 12.5ms black pulses, and the gate goes low during these periods. The inverted output of the gate through inverter  $IC_{14C}$  therefore goes high. This output is connected to the divider chain counter reset line, and forces reset during the black periods within the 300Hz store window. In practice, at the beginning of the window period, the 300Hz tone will still be running, since it is three seconds long, and the reset line will be activated for several of the 300Hz cycles. However, the counter will respond, as far as the picture display is concerned, to the last forced reset only.

**Y ramp generator:** the vertical ramp is generated by a conventional operational amplifier integrator,  $IC_{11}$ . The feedback integrating capacitor  $C_{100}$  is shunted by a low resistance  $R_{112A}$  during reset via switch  $S_5$ . The integrator potential is derived from the negative rail by dividers  $R_{110}$ ,  $R_{111}$  for APT and  $R_{110}$ ,  $R_{111}$ ,  $R_{112}$  for SR, selected by switching. Both inputs are biased by resistors  $R_{108}$  and  $R_{109}$ . Switch  $S_6$  is opened to allow linear integration of the potential on  $R_{110}$  wiper, with an optional negative potential being switched into the inverting input by  $S_6$  to set the integrator to maximum ramp voltage. The vertical output is taken across load  $R_{113}$  to earth. As the circuit stands it is manually controlled. The addition of gate control from the start sync circuit could be arranged relatively easily to automate the start/reset cycle.

**Stabilized power supplies:** the main stabilized power supply uses integrated circuit stabilizers. Two supplies are used and combined to give  $\pm 12V$  at 0.5A. The rail is fed to a simple series transistor stabilizer, comprising an n-p-n power transistor  $Tr_{29}$  with base potential stabilized by  $R_{146}$  zener diode  $D_{25}$  and is decoupled by  $C_{116}$  (Fig. 24).

#### Display device

The obvious display for the preceding circuitry is an oscilloscope. The basic requirements are: Z axis modulation capability; X axis input capability with stable d.c. coupled amplifier; Y axis stable d.c. coupled amplifier; small spot size; short persistence c.r.t. phosphor for photography, or long persistence for direct viewing; hum free supplies; and capability of disabling the beam blanking.

#### Display system operation

The display must first be set for X, Y and Z range limits. The X ramp is continuously available for setting up, as are the Y limits using S and S. On the oscilloscope the Z axis is the most difficult to set, due to the generally coarse controls for bright-

ness on most oscilloscopes. The inter-picture maximum brightness signal is useful for setting this level, but the overall dynamic range, as determined by  $R_{75}$ , is a matter of trial and error. Once set, the tape may be run until the 300Hz tone is heard on the monitor in the case of APT signals. The oscilloscope camera shutter, if used, can then be opened, and  $S_3$  switched to start. After the picture period, when the interpicture tone is heard, the shutter is closed and  $S_3$  switched to reset. In the case of SR pictures, as outlined earlier, the picture must be viewed, or a slave display arranged so that phasing can be carried out manually with the lock/slip switch  $S_{1,2}$ . The simplest way to set up the correct Index of Co-operation for the SR pictures is to count the telemetry "teeth" which occur every 25 lines, and to apply the empirical relationship

$$\frac{\text{width of actual picture (centimetres)}}{\text{telemetry "teeth" per centimetre}} = 2.6$$

Lastly, two practical points when using an oscilloscope for display can be useful. It may well be found that the X-axis amplifier is too insensitive for the generated X-ramp. One solution is to transpose the X and Y-axis outputs from the display electronics, since many oscilloscopes have a higher Y input sensitivity than X sensitivity, and the Y output of the display unit delivers a 0 to +11 volt ramp. Secondly, if the oscilloscope has a stable and accurate trigger circuit, the display unit step-derived ramp may be omitted and the oscilloscope internal timebase used to generate the X ramp. In this case, the 4 or 4/5Hz output is coupled to the oscilloscope external trigger input and the timebase speed adjusted to suit.

#### Appendix

**Capture and lock range for the Signetics NE565 phase lock loop.** If the external frequency determining components at pins 8 and 9 (Fig. 19, Part 2) are  $R_{53}$  and  $C_{67}$  respectively:

free running frequency  $f_o \approx 1.2/4R_{53}C_{67}$ . When the p.s.d. is in the limiting mode ( $V_m \gg 200mV$  pp) the lock range is given by  $2\omega_L = 2K_o K_d A\theta_d$

where  $K_o$  is the v.c.o. conversion gain,  $K_d$  is the p.s.d. gain,  $A$  is the amplifier gain and  $\theta_d$  is the maximum phase error for loop lock.

For the NE565 typical values are

$$K_o = \frac{50f_o}{V_{cc}} \text{ where } V_{cc} \text{ is the total voltage}$$

supply to the circuit,  $K_d = \frac{1.4}{\pi}$  volts/radian,

$A = 1.4$  and  $Q_d = \pi/2$  radians. Hence  $f_L \approx \omega_L/2\pi \approx 8 f_o/V_{cc}$  Hz either side of the centre frequency or a total range of  $2f_L \approx 16 f_o/V_{cc}$  Hz.

The capture range is given approximately

$$\text{by } 2\omega_c \approx 2\sqrt{\frac{\omega L}{\tau}}$$

where  $\omega_L$  is the one sided lock range

$$\omega_L = 2\pi f_L, \text{ and } \omega_c = 2\pi f_c$$

and  $\tau$  is the time constant of the loop filter.  $\tau = RC$  (C is the external filter capacitor on pin 7) with  $R = 3.6k\Omega$  (internally on the chip).

$$\begin{aligned} \text{Re-writing, } f_c &\approx \pm \frac{1}{2\pi} \sqrt{\left(\frac{2\pi f_L}{\tau}\right)} \\ &= \pm \left[ \frac{1}{2\pi} \sqrt{\left(\frac{16\pi f_o}{\tau V_{cc}}\right)} \right] \end{aligned}$$

Hz either side of centre or a total capture range of

$$f_c \approx \left[ \frac{1}{\pi} \sqrt{\left(\frac{16\pi f_o}{\tau V_{cc}}\right)} \right]$$

This approximation works well over narrow capture ranges when  $f_c < f_L/3$  but becomes too large as  $f_c \rightarrow f_L$ .

**Components list**

**Resistors—R**

Fig. 23(a)	72 1k	111 15k
	73 5k	112 100k
	74 33k	112A 100
	75 5k	113 10k
	76 10k	(d) 114 100k
	77 10k	115 1k
	78 10k	116 4.7k
	79 330k	117 100k
	80 10k	118 1k
	81 1.5k	119 4.7k
	82 10k	120 100k
	83 10k	121 2.2k
	84 15k	122 5.6k
	85 470k	123 100k
	86 10k	124 10k
	87 1k	125 3.3k
	88 10k	126 220k
(b)	89 47k	127 100
	90 330	128 1k
	91 330	129 2.2k
	92 1M	130 10k
	93 150	131 100k
	94 5k	132 100k
	95 150	133 100
	96 2.2k	134 1k
	97 470	135 1.7k
	98 1k	136 1.8k
(c)	99 330k	137 1k
	100 330k	138 100k
	101 5k	139 470k
	102 10k	140 10k
	103 470	141 250k
	104 1k	142 5k
	105	143 470
	106 1k	144 470
	107 1k	145 1k
	108 510k	Fig. 24 146 560,
	109 510k	Fig. 25 147 33k
	110 500, ten turn	148 33k

**Capacitors—C**

Numbers 83 and 84 are not included.

Fig. 23(a)	75 50n
	76 50n
	77 1.8p
	78 1.8p
	79 1.8p
	80 470p
	81 50n
	82 50n
	85 1.8p
	86 1.8p
	87 1.8p
	88 470p
	89 50n
(b)	90 1n
	91 32n
	92 150µ/15V
	93 100n
	94 150µ/15V
	95 47p
(c)	96 470p
	97 147p
	98 1.25µ
	99 680n
	100 6.8, mylar
	83 10n
(d)	101 100n
	102 10n
	103 220n
	104 1µ
	105 0.68µ
	106 150n
	107 680n
	108 320n
	109 10µ/25V
Fig. 24	110 10,000µ/30V
	111 10,000µ/30V
	112 400µ/35V
	113 400µ/35V
	114 10n
	115 10n
	116 10µ/30V
	117 400µ/35V
	118 10n

Fig. 24

**Diodes—D**

Fig. 23(a)	14 GEX34
	15 GEX34
	16 GEX34
	17 GEX34
(b)	18 MR56
	19 MR56
(c)	20 1N4001
	21 1N4001
	22 1N4001
Fig. 24	23 REL65
	24 REL65
	25 MR51

**Inductor—L**

Fig. 23(d)	22 500mH
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**Transistors—Tr**

Fig. 23(a)	15 2N2926
	16 2N2926
(c)	17 2N2926
	18 2N726
	19 2N706
(d)	20 2N2926
	21 2N2926
	22 2N2926
	23 2N2926
	24 2N2926
	25 2N2926
	26 2N2926
	27 2N2926
	28 2N2926
Fig. 24	29 2N3054

Fig. 24

**Integrated circuits—IC**

Fig. 23(b)	4 NE565A
	5 SN7413N
	6 SN7492N
	7 SN7490N
	8 SN7490N
	9 SN7490N
(c)	10 SN7400N
	11 SN72741N
(d)	12 SN7413N
	13 SN7400N
	14 SN7404N
integrated stabilizer	15 MVR-12V
integrated stabilizer	16 MVR-12V

**Transformers—T**

Fig. 23(a)	2 RS Components Ltd, universal speaker isolating transformer. Ratios w.r.t. i/p on pins 2 and 3.
	pin 5—1.375:1
	pin 4—2.0:1
	pin 6—1.575:1
	pins 7 and 8—0.475:1

Fig. 24 3 30V rectifier transformer.

**Author's biography**

Gerry Kennedy is a Higher Scientific Officer with the Science Research Council at the Appleton Laboratory, Chilbolton Observatory. His private project was started in the Falkland Islands with Nimbus 3 ice cover pictures. This work was continued on his return to the UK to encompass more recent satellites. He is a radio amateur with the call signs VP8LZ and G30GK.

**Corrections to Part 1**

- p.437, column 2, last line—diodes 3 to 13 (not 5 to 12).
- p.438, column 1, line 2— $D_7$  (not  $D_4$ )
- line 11— $R_7$  (not  $R_2$ )
- line 24— $R_8$  (not  $R_5$ )
- p.439, column 1, line 15— $Tr_2$  (not  $Tr_1$ )
- column 3, line 32— $L_5$  (not  $L_{10}$ )
- p.440, components  $R_7$ —1M (not 111)
- $C_{12}$ —1000 (not 1)
- $Tr_2$ —MS175TB (not 11S-1757B)

**Corrections to Part 2**

- p.488 col. 3 line 15—for  $R_3$  read  $R_{57}$ , line 16 for  $C_3$  read  $C_{69}$ , line 18 for  $C_6$  read  $C_{70}$ , line 19 for  $C_4$  read  $C_{71}$ , line 22 for  $C_4$  read  $C_{71}$ .
- p.489 picture is upside down and back-to-front.
- p.490 components list  $R_{70}$  is 250k.

**Acknowledgement**

The author would like to thank the Reverend Dr Paul Sollom OSB, of Douai Abbey for his encouragement and helpful advice, also NOAA for data supplied periodically and NASA for making the whole project possible.

**References**

- 7. Sollom, "Just Look at the Weather", *Radio Communication*, Radio Society of Great Britain, vol. 47, No. 12, Dec. 1971, p.823.

# The monostable . . . doth give us pause

Introducing set 19 of Circards

by J. Carruthers, J. H. Evans, J. Kinsler and P. Williams

*Paisley College of Technology*

Not quite the words of Hamlet, but delay is one outstanding property of the monostable circuit. De Bono, in *The Mechanism of Mind*, could be describing another function of the circuit when he writes, "a short-term memory is just a way of extending the influence of an event beyond the real time of its occurrence along the dimension of time", e.g. a monostable will accept a transition at its input and respond with an output pulse, but for a finite time. A more formal description of the monostable (sometimes called a one-shot) circuit is having one stable state in which it remains until triggered by an external signal into a quasi-stable state, where it remains for a time determined by circuit parameters and subsequently returns to its stable state. This basic action allows the monostable to be used for a variety of purposes such as lengthening, delaying and regenerating pulses, sequential timing and delay applications and frequency division.

The nature of the monostable circuits can be widely different because they can be designed using n-p-n and p-n-p bipolar transistors (in cross-coupled emitter-coupled and complementary modes), field-effect transistors, operational amplifiers, discrete and integrated-circuit logic gates, as well as purpose-designed monostable integrated circuits.

A very common type of monostable uses a cross-coupled configuration which can be thought of as being a modification of a symmetrical bistable where one resistive coupling is replaced by a capacitive coupling. Two can either be connected between the collector of a normally-off transistor to the base of a normally-on transistor, or between the collector of a normally-on transistor and the base of a normally-off transistor. Fig. 1 shows a circuit of the first type and Fig. 2 the associated current and voltage waveforms.

Transistor  $Tr_2$  is in a stable on state, until triggered, due to the base drive supplied through  $R_2$ . Transistor  $Tr_1$  is held in a stable off state as  $R_4$  is connected to  $Tr_2$  collector which is at the low saturation value of  $v_{ce2}$  and  $R_3$  is returned to the negative  $V_{BB}$  rail. When a positive-going trigger pulse is applied to  $Tr_1$  base via  $C_1$  this transistor turns on causing its collector voltage to fall to almost zero.

Because the charge on  $C_2$  cannot change instantaneously, this negative-going transition is passed to  $Tr_2$  base which switches off. The transistors remain in these states while the charge on  $C_2$  changes via  $R_2$  causing

$v_{be2}$  to rise exponentially towards  $+V_{CC}$ . When  $v_{be2}$  passes through zero and rises positively to a value depending on the type of transistor used, which causes base current to flow in  $Tr_2$ , this transistor begins

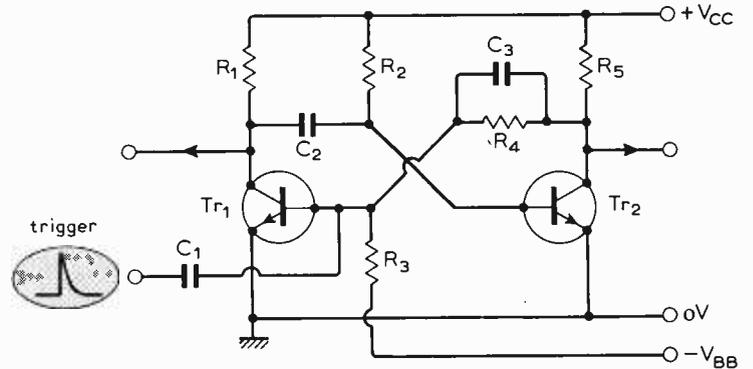


Fig. 1. A common monostable can be thought of as a bistable circuit with one resistive coupling replaced by a capacitive coupling. Two can be connected as shown.

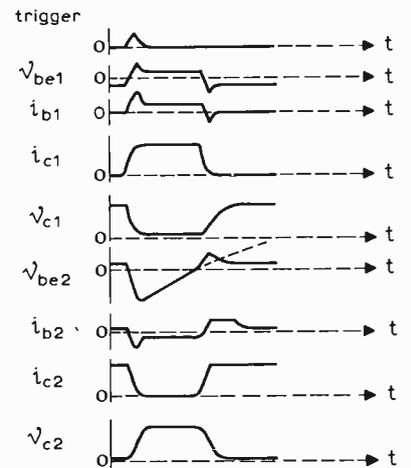
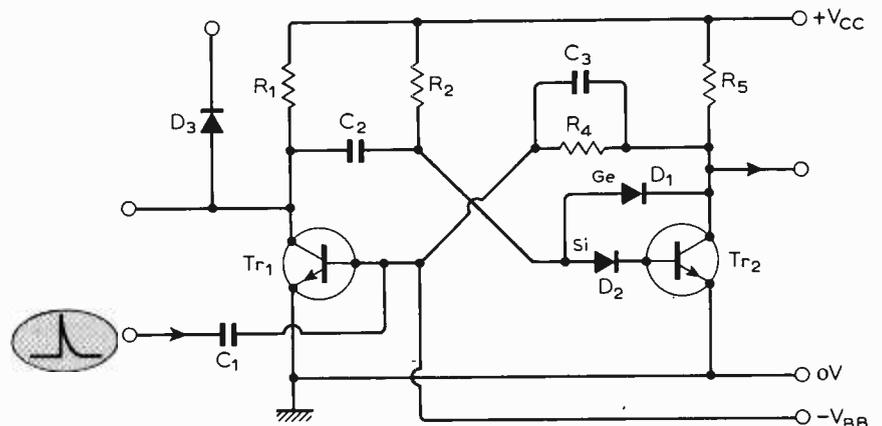


Fig. 2. Waveforms associated with circuit of Fig. 1.

Fig. 3. Switching speed of Fig. 1 circuit is improved by preventing saturation with diodes  $D_1$  and  $D_2$ . Clamping diode  $D_3$  reduces recovery time by connection to a supply less than  $V_{cc}$ .



to turn on. The resulting fall in  $V_{C2}$  is coupled to  $Tr_1$  base via  $C_3$ ,  $Tr_1$  beginning to turn off; the regenerative feedback via  $C_2$  and  $C_3$  causes the circuit to restore to its stable state of  $Tr_1$  off and  $Tr_2$  on, the capacitor  $C_2$  recharging through  $R_1$ .

The switching speed of this kind of circuit can be improved by using higher speed switching transistors in a non-saturating circuit. To prevent saturation, germanium diode  $D_1$  and silicon diode  $D_2$  can be added as shown in Fig. 3. When  $Tr_2$  begins to turn on, to return the circuit to its stable state,  $D_1$  will be reverse-biased until  $v_{C2}$  falls below  $(v_{be2} + v_{D2})$  causing the excessive base drive current, which would otherwise saturate  $Tr_2$ , to be diverted through  $D_1$ . Two series-connected germanium diodes can be used in place of the silicon diode  $D_2$ . The waveform at  $Tr_1$  collector can have a slow recovery time, especially when driving capacitive loads, and this can be reduced by the addition of the clamping diode  $D_3$  returned to a supply  $V_A < V_{CC}$ . The output voltage  $v_{C1}$  attempts to rise towards a higher value with  $D_3$  present but becomes clamped at  $(V_A + V_{D3})$  when  $D_3$  conducts.

Another method of reducing the recovery time is to include an emitter follower between  $R_1$  and  $C_2$  of Fig. 1, as shown in Fig. 4. As  $C_2$  is charged to almost the supply rail voltage, the emitter of  $Tr_3$  is normally close to  $+V_{CC}$ . The input trigger pulse switches the circuit to its quasi-stable state and as the charge on  $C_2$  changes, the emitter voltage of  $Tr_3$  rises above its base voltage ( $v_{C1}$  on) cutting the transistor off. When  $Tr_2$  again begins to conduct, the circuit returns to its stable state with  $C_2$  being rapidly recharged by the emitter current of  $Tr_3$ .

The output from  $Tr_1$  collector can be made to more closely approach a rectangular pulse by the inclusion of an isolation diode  $D_4$  as shown in Fig. 5. When  $Tr_1$  is on the collector current flows through  $R_1$  and  $R_7$  in parallel and a faster recovery time is achieved by making  $R_7 < R_1$  so that when  $Tr_1$  switches off  $D_4$  is reverse biased and  $C_2$  recharges more rapidly, through  $R_7$ , than in the circuit shown in Fig. 1. Other methods of triggering this type of monostable include negative pulses to either  $Tr_1$  collector or  $Tr_2$  base or positive pulses to the base of another transistor having its collector and emitter respectively connected to  $Tr_1$  collector and emitter.

Another form of the cross-coupled monostable is shown in Fig. 6, the major difference compared with the foregoing circuits being that  $Tr_1$  is on and  $Tr_2$  is off in the stable state. This is achieved by correct choice of the potential-dividing chain and by  $D_2$  being forward-biased via  $R_4$ , holding the base-emitter junction of  $Tr_2$  reverse-biased. A negative-going input trigger pulse causes  $Tr_1$  to switch off and hence  $Tr_2$  to switch on and to remain in that state as  $C_2$  charges, part of the charging current being base drive to  $Tr_2$ . Diode  $D_2$  is reverse-biased in this quasi-stable state which ends when the base drive to  $Tr_2$  has fallen to a level which will not maintain conduction. Transistor  $Tr_2$  then switches off causing  $Tr_1$  to return to the stable on state. No output is taken from  $Tr_1$  collector as a

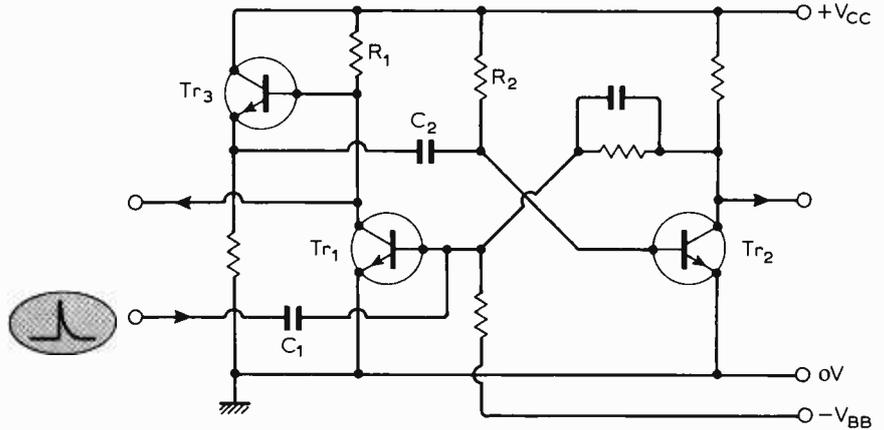


Fig. 4. Recovery time can also be reduced with an emitter follower between  $R_1$  and  $C_2$  of Fig. 1.

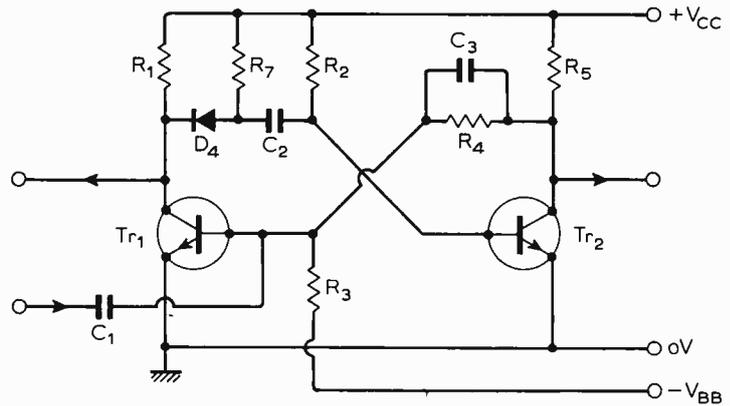


Fig. 5. Output from  $Tr_1$  is made more rectangular by isolation diode  $D_4$  and by making  $R_7 < R_1$ .

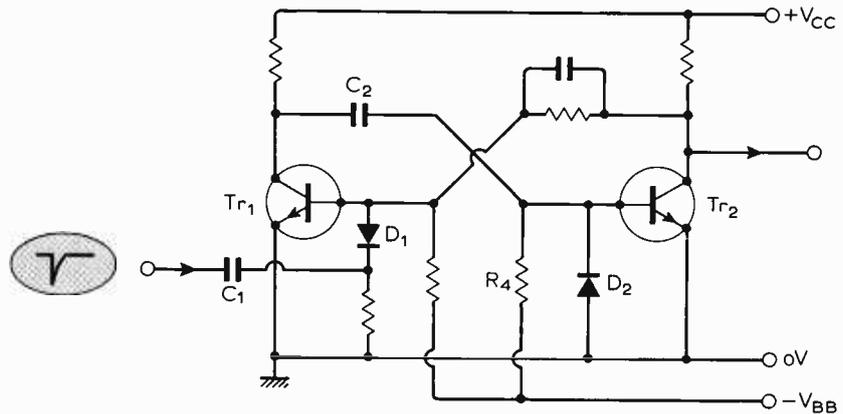


Fig. 6. In this variant of the cross-coupled monostable,  $Tr_1$  is normally on and  $Tr_2$  normally off. Note trigger is of opposite polarity. Circuit has much faster recovery time.

load at that point significantly changes the off time of  $Tr_2$ . This circuit has a much faster recovery time than the previous ones discussed.

A cross-coupled monostable which besides producing a time-constant-dependent output pulse may provide one due to the input pulse duration is shown in Fig. 7. In the stable state  $Tr_1$  is on and  $Tr_2$  is off, so when a short-duration trigger pulse is applied via  $D_1$  the circuit remains in its quasi-stable state for a time determined largely by  $C_1 R_3$ . However, when a long input pulse is applied,  $Tr_1$  will remain off until the input is removed even if  $C_1$  completes its discharge during that interval.

Fig. 8 shows an emitter-coupled monostable where  $Tr_2$  is on and  $Tr_1$  is off in the stable state. Compared with the cross-coupled circuits, this type has the advan-

tages of only using a single supply and providing an output which is taken from a point having no internal coupling. When a negative-going trigger pulse is applied to  $Tr_1$  collector via  $C_1$  it is coupled to the base of  $Tr_2$  which switches off. The emitter voltage falls allowing  $Tr_1$  to switch on for a time determined by that required for  $C_2$  to discharge sufficiently to allow  $Tr_2$  to begin to conduct. The emitter voltage then rises, causing  $Tr_1$  to begin to switch off, and the resulting rise in  $Tr_1$  collector voltage is coupled to  $Tr_2$  base which switches on, and  $Tr_1$  switches off to regain the stable state. Due to the presence of  $R_4$ , the output voltage swing does not approach  $V_{CC}$  and the recovery time is not very fast, as  $R_3$  should be greater than  $R_6$  to ensure the correct switching action. Recovery time can be improved by the

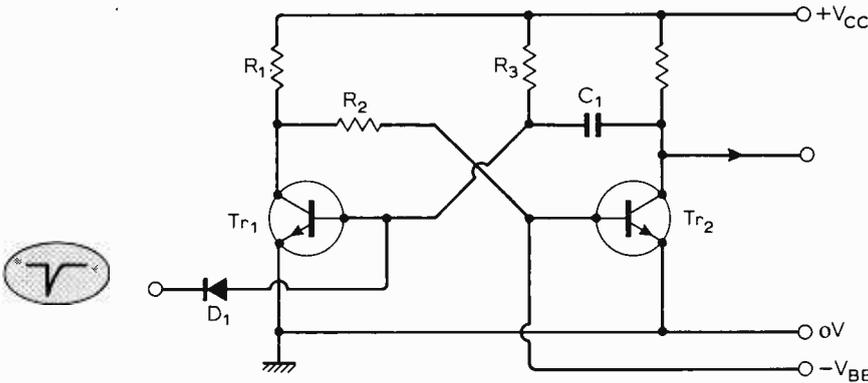


Fig. 7. This circuit produces an output pulse dependent on input pulse duration.

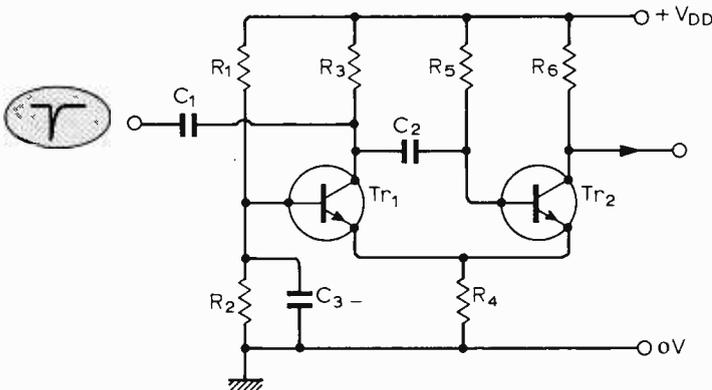
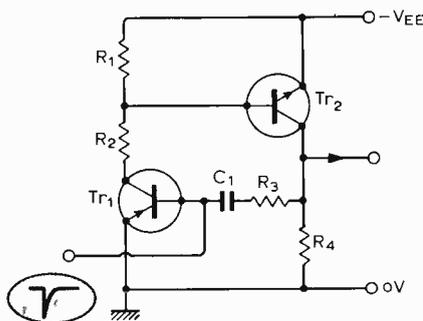
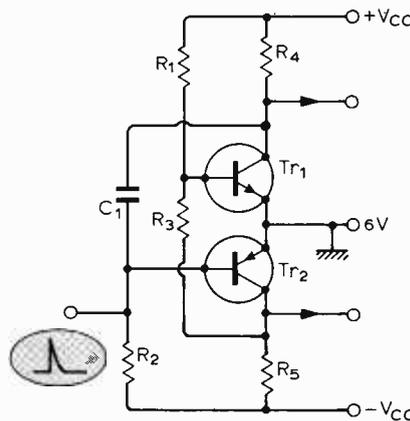


Fig. 8. Emitter-coupled circuit needs only one supply line and gives a more isolated output.



Complementary transistors enable both transistors to be normally off (Fig. 9, above) or normally on (Fig. 10, right). Opposite-polarity outputs are available from Fig. 10.



state.

Fig. 10 shows a complementary monostable in which both transistors are on in the stable state, and which provides a pair of opposite-polarity outputs simultaneously. A positive-going trigger pulse applied to  $Tr_2$  base turns both transistors off and after  $C_1$  charges sufficiently, through  $R_2$  and  $R_4$ , both transistors return to the stable on state regeneratively.

These and other types of monostable circuits are discussed in Circards, set 19, together with component values for tested circuits—see next column.

## Titles of cards in set 19 of Circards (available shortly)

- 1 discrete-component monostables
- 2 complementary circuits
- 3 op-amp/comparator types
- 4 t.t.l.-gate monostables
- 5 compensated c.m.o.s. circuits
- 6 emitter-coupled monostables
- 7 voltage-controlled monostables
- 8 long-delay circuits
- 9 dual monostable applications
- 10 high duty-cycle types

## What are Circards?

Circards are a new method of collating and presenting data about circuits in a compact and easily retrievable way. The sets of 203 × 127mm (8 × 5 in) double-sided cards are designed for easy filing in standard boxes and for easy access at the desk or at the bench, where transparent plastic wallets keep the cards in good condition.

Each card normally describes operation of a selected circuit, gives measured performance data and graphs, component values and ranges, circuit limitations and modifications to alter performance. Suggestions for further reading are included together with cross references to related circuits. The Circard concept was outlined more fully in the October 1972 issue of *Wireless World*, pp. 469/70.

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- 8 astable multivibrator circuits
- 9 optoelectronics: devices and uses
- 10 micropower circuits
- 11 basic logic gates
- 12 wideband amplifiers
- 13 alarm circuits
- 14 digital counters
- 15 pulse modulators
- 16 current-differencing amplifiers—signal processing
- 17 c.d.as—signal generation
- 18 c.d.as—measurement and detection

## Meetings

### LONDON

2nd and 3rd. IEE—"The why and how of telephone exchanges". Christmas holiday lecture by C. A. May at 14.30 at Savoy Pl., WC2.

6th. IEE—"Flat diaphragm loudspeakers" by J. W. Manger at 17.30 at Savoy Pl., WC2.

7th. IEE—"Protection performance as affected by the use of capacitor voltage transformers" by M. A. Hughes at 17.30 at Savoy Pl., WC2.

8th. IEE—Discussion on "Processor architecture for telecommunication switching" at 17.30 at Savoy Pl., WC2.

8th. IERE—"Train control developments on British Rail" by J. W. Birkby at 18.00 at 9 Bedford Sq., WC1.

8th. BKSTS—"The Turpin Colorflex system" by Gerry Turpin at 20.30 at NFT2, National Film Theatre, South Bank, Waterloo, SE1.

13th. IEE/IERE—"A review of electron microscopy" by Dr V. E. Cosslett at 17.30 at Savoy Pl., WC2.

14th. IEE—Colloquium on "Applications of active, digital and passive filters" at 10.30 at Savoy Pl., WC2.

14th. AES—"Practical design of magnetic heads" by Robert B. Dyer at 19.15 at the IEE, Savoy Pl., WC2.

15th. IEE—"Charge-coupled devices and their application" by D. Burt at 17.30 at Savoy Pl., WC2.

15th. IERE/RINav.—Colloquium on "Advances in airborne equipment for navigation and flight control" at 10.30 at the Royal Aeronautical Society, 4 Hamilton Pl., W1.

15th. IERE—"Good quality reception from medium-wave broadcasting" by Dr R. C. V. Macario at 18.00 at 9 Bedford Sq., WC1.

15th. I.Phys.—One-day meeting on "Surface effects on semiconductor devices" at 10.00 at Imperial College, SW7.

21st. IEE—Colloquium on "Standardization in geographically distributed control and telemetry systems" at 14.30 at Savoy Pl., WC2.

21st. IEE/IERE—"Designing machines for people" by Dr C. R. Evans at 17.30 at Savoy Pl., WC2.

22nd. IERE—Colloquium on "Thermionic emission devices" at 9 Bedford Sq., WC1.

22nd. IEE—"How to see in the dark" by Dr R. M. Hodgson at 18.30 at Savoy Pl., WC2.

23rd. IEE—"Control of distributed parameter systems" by Prof. P. C. Parks at 17.30 at Savoy Pl., WC2.

27th. IEE—"Digital systems for sound programme transmission" by J. W. H. O'Clarey at 17.30 at Savoy Pl., WC2.

28th. IEE—"The design of precision coaxial power meters" by Dr A. E. Fantom at 17.30 at Savoy Pl., WC2.

28th. IEE—"The ESRO orbital test satellite" by Dr P. Bartholome at 17.30 at Savoy Pl., WC2.

29th. IEE/IERE—"Sensing, sizing and sorting of cells: the laser sorter" by D. F. Capellaro at 17.30 at Savoy Pl., WC2.

29th. IERE—"Speech engineering" by Dr A. J. Fourcin at 18.00 at the Haldane Theatre, Wolfson House, Stephenson Way, NW1.

### BIRMINGHAM

15th. IERE/RTS—"The status of British broadcasting" by C. B. B. Wood at 19.00 at the A.T.V. Centre, Broad Street.

22nd. SERT—"Liquid crystal displays and their applications" by G. P. Stenning at 19.00 at the Byng Kenrick Suite of the University of Aston, Gosta Green.

### BRIGHTON

9th. SERT—"Principles of video tape recording" by R. A. Bravery and K. G. A. Whittington at 19.45 at the TV Studio, Sussex University.

### CHATHAM

21st. IERE—"Quadraphonics" by Dr K. Barker at 19.00 at the Lecture Theatre 18, Medway and Maidstone College of Technology, Maidstone Road.

### CHELMSFORD

15th. IEE—"C-MOS and its applications" by R. Henderson at 18.30 at the King Edward VI Grammar School, Broomfield Road.

### HALTON

16th. IEE/R.Ac.S.—"Radar and meteorology" by Prof. E. Shearman at 19.30 at Kermode Hall, R.A.F. Halton, Bucks.

### LEATHERHEAD

15th. IEE—"Man-made, God-made" by Prof. E. R. Laithwaite at 19.30 at C.E.R.L. Offices, Kelvin Avenue.

### LLANDAFF

15th. SERT—"The Pye 110° colour chassis" by P. E. Gibbs at 19.15 at Llandaff College of Technology.

### MANCHESTER

23rd. SERT—"Mobile radio equipment" by M. Howard at 19.30 at the Granada Building, College of Building, Hardman Street.

### MORDEN

29th. IEE—"Developments in superconductivity techniques" by J. A. Baylis at 19.00 at Merton Technical College, Morden Park, London Road.

### READING

6th. SERT—"Colour television" at 19.30 at The Technical College.

20th. IEE—"Concorde systems design" by H. Hill at 19.30 at the University, Whiteknights Park.

23rd. IERE—"Optoelectronic devices" by M. Miller at 19.30 at the J. J. Thomson Physical Laboratory, University of Reading, Whiteknights Park.

### SALISBURY

27th. SERT—"TEC, ERB and the technical engineer" by A. J. Kenward at 19.30 at Salisbury College of Technology.

### SOUTHAMPTON

22nd. SERT—"Philips video tape recorder" by R. Adams at 19.00 at the College of Technology, East Park Terrace.

*Tickets are required for some meetings; readers are advised therefore to check with the society concerned.*

## Wireless World lectures

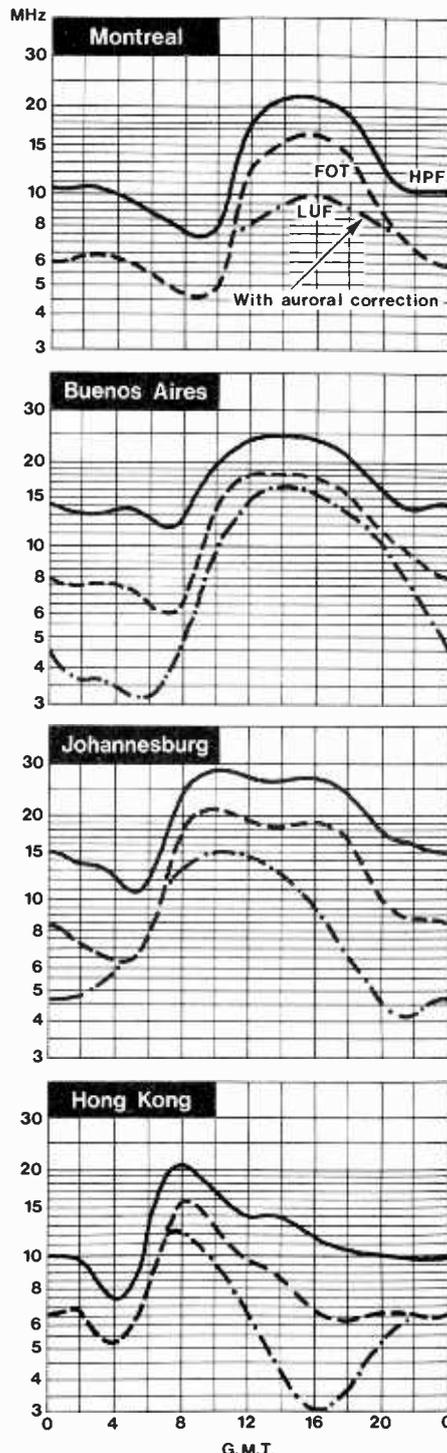
H. W. Barnard, who was editor of our journal from 1965 until 1973, has been approached several times by societies, clubs and other organizations in the field of radio and electronics to address their members. With 48 years experience of *W.W.*, he is in a unique position to give a picture of the development of communications, broadcasting and the growth of "electronics" and it occurs to us that many other people would like to listen to an illustrated talk on this most fascinating subject.

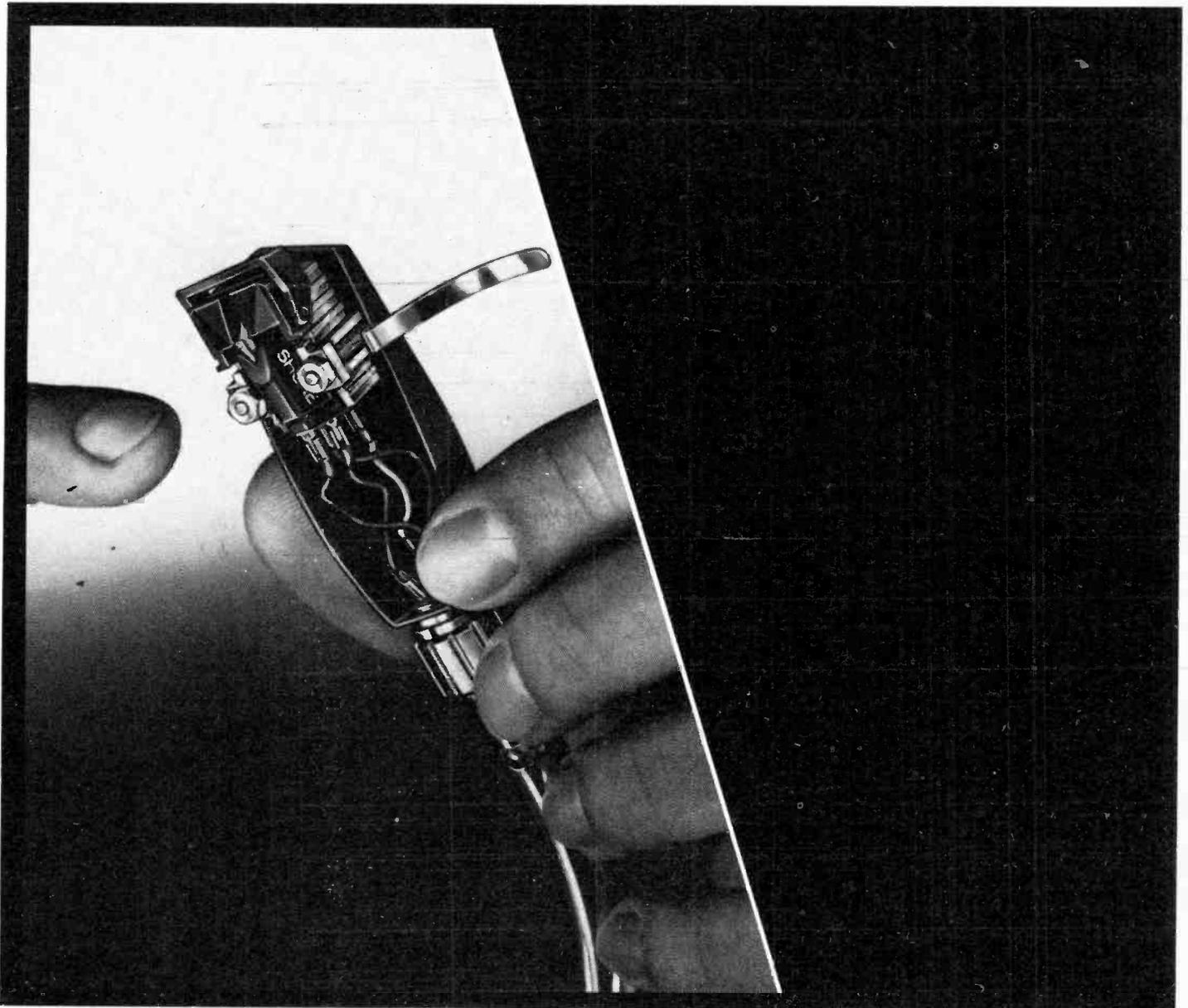
If, therefore, secretaries of such bodies would like to write to us, we will try to arrange for Mr Barnard to give a lecture.

## HF predictions

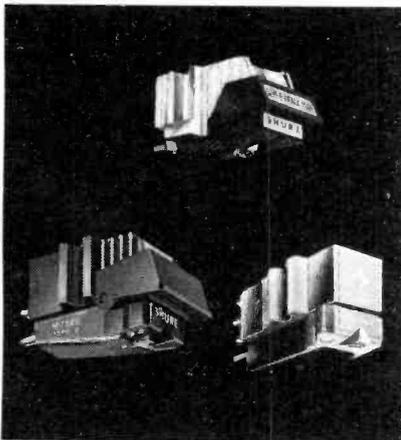
Solar Index is now less than 10 and will remain so throughout the year with the end of the current sunspot cycle expected in August. As their number decreases sunspots tend to concentrate at low solar latitudes, then when the number increases the new spots appear at high solar latitudes. Minima are therefore used to mark the duration of a cycle as they are much more clearly defined than maxima.

A year of poor communication conditions can be expected especially during summer months as HPFs and FOTs will be at their very lowest.





## The heart of hi-fi.



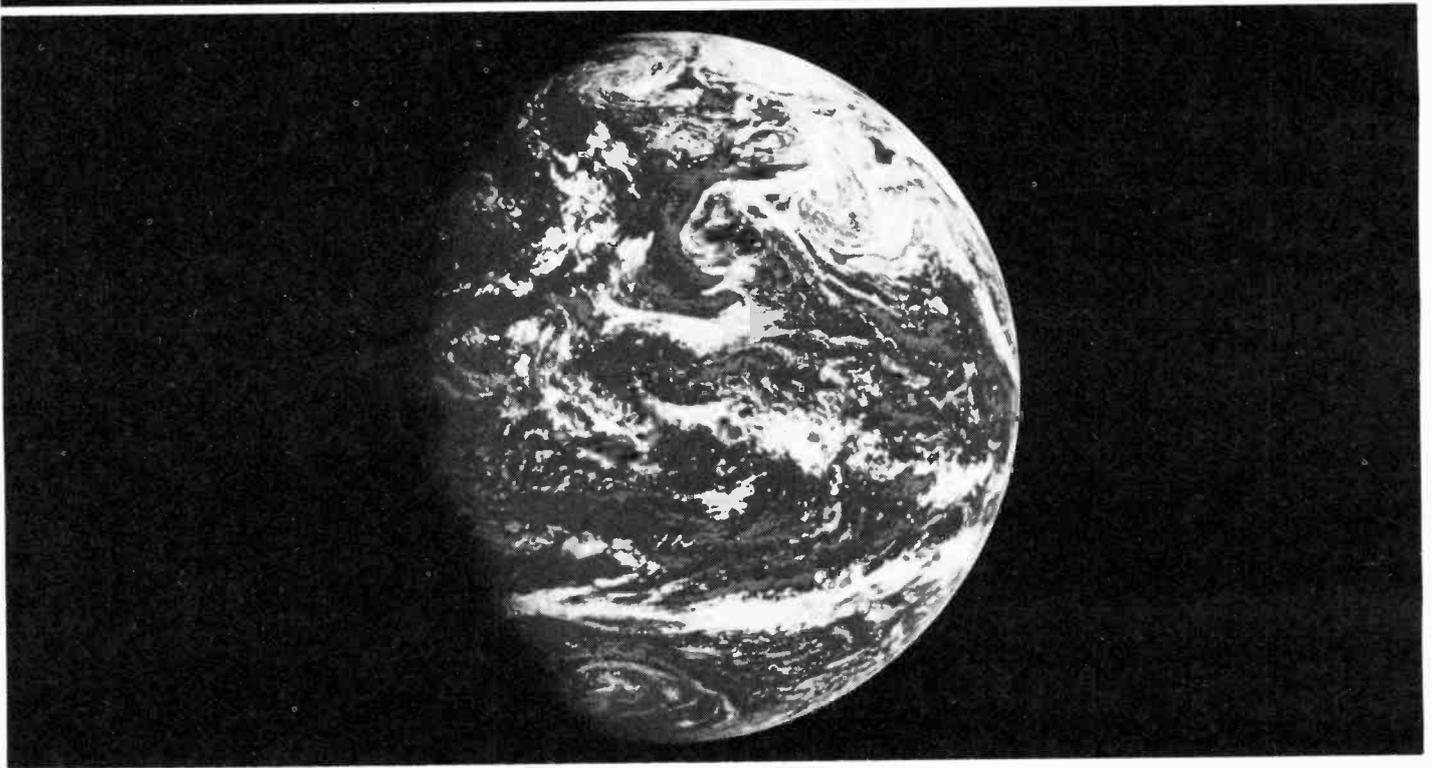
Beauty is truth, truth beauty. The fact is that all too few music lovers realise that while certain high fidelity components can be less than best, there is one component that cannot endure a sacrifice in quality: the cartridge. Because the hi-fi cartridge functions as the *source of sound* (the point at which the recording is linked with the balance of the hi-fi system), its role is absolutely critical. Just as the camera can be no better than its lens, the finest hi-fi system in the world cannot compensate for an inferior cartridge. Suggestion: For a startling insight into the role of the cartridge in the overall hi-fi system, and a breathtaking re-creation of your favourite recording, see your nearby Shure cartridge dealer. He'll introduce you to the Shure cartridge that is correct for your system and your exchequer. Or, next best, send for our brochure:

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WW—106 FOR FURTHER DETAILS

# Silent switch for stereo-pair comparisons

by K. Moulana, B.Sc.

University of Surrey/BBC Research Department

**Design and printed circuit construction details are given for an f.e.t. electronic switch designed to meet stringent requirements.**

During the course of a project the need arose for a silent switch with the following specification: an on/off ratio greater than 70dB; a switching time as fast as possible without introducing any audible transients; remote control switching facility by means of a single, mechanically silent on/off switch; output clipping level not less than +10dBm into 600 ohms; overall unity gain into 600 ohms; an input impedance greater than 50kΩ over the frequency range 30Hz to 15kHz; output impedance of 600 ohms ± 2% over the above frequency range; amplitude/frequency response ±0.2dB over the above frequency range; hum and noise not greater than -70dBm over a 15kHz bandwidth and a total harmonic distortion not greater than 0.5% and void of high order harmonics.

A preliminary survey showed that a unit satisfying the above requirements was not readily available on the market and, therefore, one had to be designed. However, before the actual design procedure which was adopted is outlined, a brief study of the underlying requirements may serve as a useful introduction.

When a programme is switched by mechanical means, transients of two different kinds are transmitted through the system. The first type is caused by the rapid change in the d.c. at the point of switching which of course leads to an audible thump. The second and less objectionable variety is the result of terminating an a.c. signal when its waveform is not passing through zero.

In order to eliminate transients caused by changes in d.c. levels, either the signal carrying part of the circuit must be electrically isolated from the switching section, or measures must be taken to ensure that the d.c. biasing potentials remain unchanged at the instant of switching.

In the past, the majority of transient free switches employed a light-sensitive resistance as the signal carrying element, and the luminance of a lamp to control the degree of attenuation required. The main disadvantage of light-operated

switches is that they are not fast enough, because an incandescent lamp has a decaying luminance after the current through it has been stopped. In fact, the decay rate is inversely proportional to the normal standing current through the lamp; even with low current lamps the decay time is too long. Up to now, such switches have, in addition, suffered from poor on/off ratios whenever small size, low current and hence low power lamps have been used. It should be pointed out that in recent years light emitting diodes have also been used instead of incandescent lamps.

The other group of silent switches or electronic attenuators often used may be conveniently classified under the heading of d.c. modulators. Such circuits are essentially amplitude modulators under various disguises. The programme signal is injected into the otherwise carrier input

and a d.c. potential is used instead of the modulation signal to control the amplitude of the programme. Basically, these circuits make excellent electronic attenuators over a finite range, and with additional refinements high on/off ratio switches can be designed. Unfortunately, the use of the above technique to achieve the desired specification would have resulted in a fairly complex circuit unless integrated circuits were employed. Furthermore, during the designing stages (two years ago) the author could not find any i.c. modulator or attenuator that would meet the requirements. Therefore, the only feasible alternative was to use an f.e.t. as a voltage controlled resistor which in fact constitutes the basis of the present design.

If an f.e.t. is biased near the origin of its output characteristics, the channel behaves like a pure resistance whose value is a function of the gate voltage. In other words, the device becomes a voltage controlled resistor. With suitable circuit arrangements, this property can be put to use as the basis of a transient free switch.

Essentially, an f.e.t. is used in conjunction with a resistance to form a voltage controlled potential divider shown in Fig. 1. When the f.e.t. is conducting,  $V_{GS}$  is zero and the channel resistance,  $r_{DS}$ , is a minimum and therefore:

$$\frac{E_o(\text{on})}{E_i} = \frac{R_L}{R_L + r_{DS \text{ min.}}}$$

If  $V_{GS}$  is greater or equal to the pinch-off voltage of the f.e.t.,  $r_{DS}$  becomes a maximum and thus:

$$\frac{E_o(\text{off})}{E_i} = \frac{R_L}{R_L + r_{DS \text{ max.}}}$$

For a 2N3819 junction f.e.t.,  $r_{DS}(\text{min})$  and  $r_{DS}(\text{max})$  are of the order of 100Ω and 10MΩ respectively. If  $R_L$  is set at 3.3kΩ, an on/off ratio of 70dB is achieved for the voltage controlled potential divider.

Let us now consider the biasing arrangement for the f.e.t. If the device is biased at the origin of the output charac-

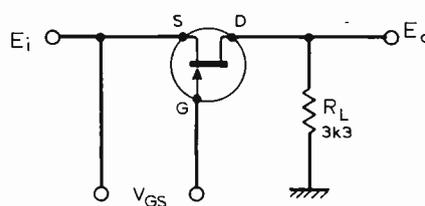


Fig. 1. An n.f.e.t. used as a voltage controlled resistor.

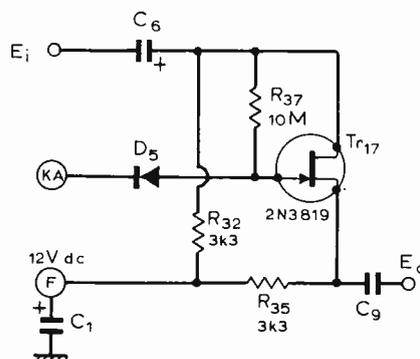


Fig. 2. Biasing arrangement for a symmetrical junction f.e.t.

teristics, the a.c. signal will swing symmetrically about that point, implying that the output characteristics of the f.e.t. must be symmetrical about the origin over the working range required. A symmetrical junction f.e.t. fulfils this requirement for small excursions about the origin of its characteristics.

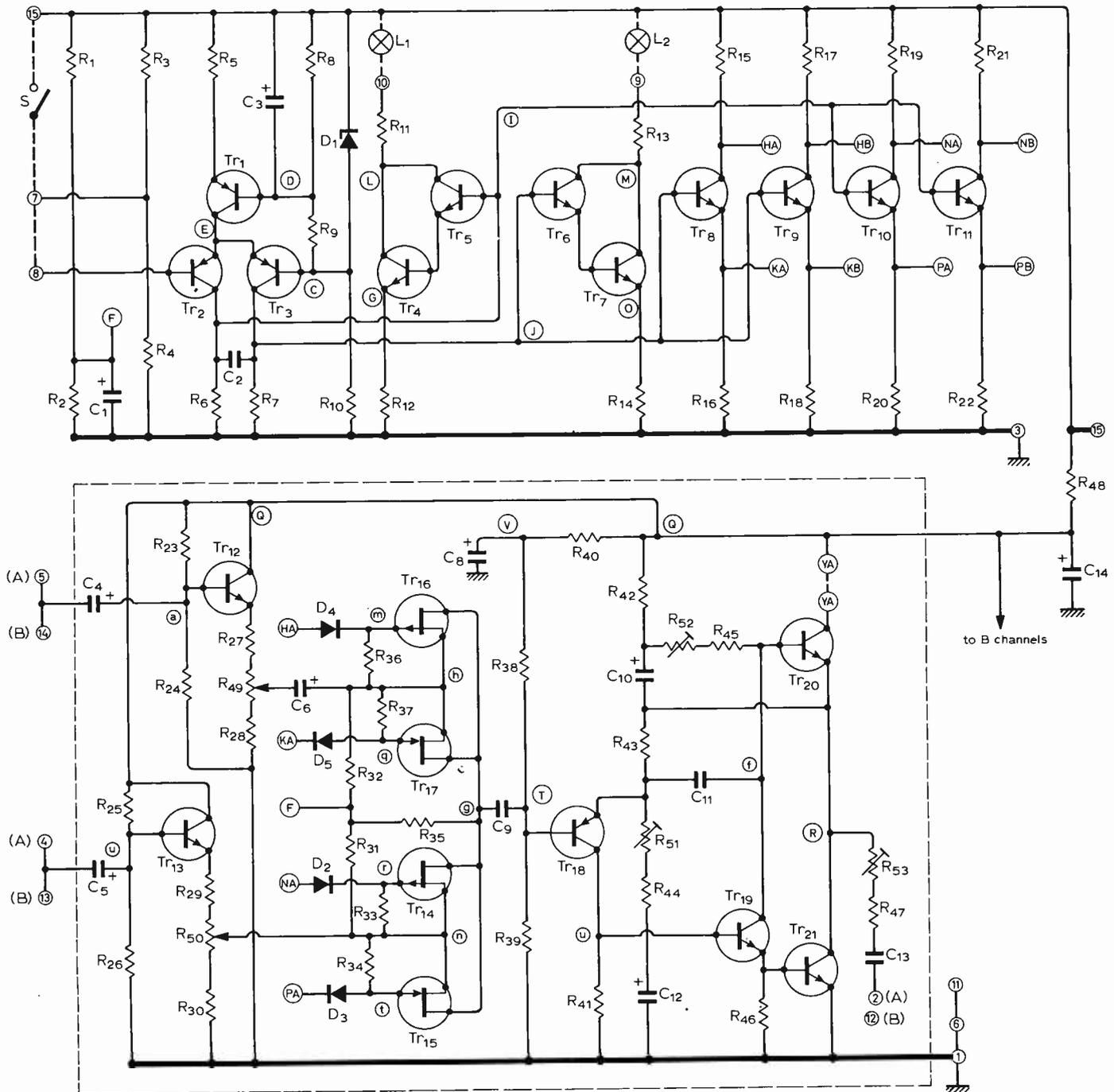
Fig. 2 shows the basis of the biasing arrangement for a symmetrical junction f.e.t. The source and drain are both held at 12V through  $R_{32}$  and  $R_{35}$  because the drain current is zero. When point KA is open circuited or at 12V,  $V_{GS}$  becomes zero because the current through  $R_{37}$  is zero, and the f.e.t. is switched on. The function of  $D_3$  is to protect the gate against excessive forward bias. Taking KA to a voltage greater than the pinch-off voltage of the device, switches the f.e.t. off. In the actual circuit, point KA is in fact taken to earth.

So far as signal transmission is concerned, point F should ideally be at a.c. earth. In practice, the resistive path between F and true earth must be very small in comparison to  $R_{32}$  at the lowest frequency of interest, because the two form a potential divider between the input and true earth, and hence a fraction of the a.c. signal always present at the input leaks through to the output via  $R_{35}$ , thus reducing the on/off ratio. In the actual circuit, a 5000 $\mu$ F capacitor couples F to

earth giving a theoretical leakage factor of about -70dB at 40Hz.

Using a single f.e.t., signals of the order of -30dBm can be passed without exceeding the distortion limit when the device is conducting. For larger swings, the incremental value of the channel resistance will no longer be the same as its d.c. resistance. In other words, the channel resistance will change during the actual a.c. cycle which of course leads to distortion. The effect can be minimized by using two complementary f.e.t.s in parallel so that the change in the channel resistance of one is compensated by the other hence reducing changes in the total resistance during the a.c. cycle. The complementary changes in resistance is due to the fact while one f.e.t. is forward biased, the other is reversed biased and the incremental value of the channel resistances are in the opposite sense for the two biasing

Fig. 3. Complete circuit for one channel of a stereo pair. Parts enclosed in the broken line are repeated for the B channels. Points marked with identical letters are connected together. Circled numbers refer to pin connections and operating voltages as shown in the table of voltages.



modes. The use of a complementary pair of f.e.t.s was found to increase the signal handling capability by some 20dB.

Fig. 3 shows the complete circuit of the stereo silent switch. Transistors  $Tr_{14}$  and  $Tr_{15}$  form the switching elements for the A channel of a stereo pair, while  $Tr_{16}$  and  $Tr_{17}$  serve the A channel of a second stereo pair. The circuit for the B channels is identical to that enclosed by the broken lines. Resistances  $R_{31}$ ,  $R_{32}$  and  $R_{33}$  maintain the drains and sources of the four f.e.t.s at about 12V. Resistor  $R_{35}$  also acts as the a.c. load for both A channels. When points HA and KA are at about 12V, f.e.t.s  $Tr_{16}$  and  $Tr_{17}$  are switched on, and the signal present at their sources is developed across  $R_{35}$ . When point HA is at 24V and KA is at zero volts,  $V_{GS}$  for both  $Tr_{16}$  and  $Tr_{17}$  becomes greater than their corresponding pinch-off voltages and, therefore, they are both switched off. Furthermore, at any given time if  $Tr_{16}$  and  $Tr_{17}$  are conducting,  $Tr_{14}$  and  $Tr_{15}$  will be cut off and vice versa. Therefore, the signal developed across  $R_{35}$  is either that belonging to the A channel of one stereo pair or the corresponding signal of the other stereo pair. The advantage of this arrangement is that only one subsequent amplifier (consisting of  $Tr_{18}$  to  $Tr_{21}$ ) is required for two independent channels. However, the required d.c. switching for f.e.t.s  $Tr_{16}$  and  $Tr_{17}$  is done by means of the phase splitter  $Tr_8$  which itself is driven by the differential amplifier consisting of transistors  $Tr_1$ ,  $Tr_2$  and  $Tr_3$ . When  $Tr_{16}$  and  $Tr_{17}$  are on,  $Tr_{14}$  and  $Tr_{15}$  should be off and, therefore, points NA and PA are driven by the phase splitter  $Tr_{10}$  which is in turn driven in opposition to  $Tr_8$  by the differential amplifier.

The remaining a.c. carrying part of the circuit is fairly straightforward. The two input signals present on the bases of transistors  $Tr_{12}$  and  $Tr_{13}$  are attenuated by 20dB before entering the switching elements in order to reduce harmonic distortion. The switching mode ensures that only one of the two input signals appears across  $R_{35}$ . The amplifier that follows the switching elements compensates for the initial 20dB attenuation and therefore maintains the overall unity gain required. The amplifier proper is of the class A push-pull variety, the operation of which has been explained frequently in the literature.

The d.c. switching and indicating section was designed to operate by means of a single on/off switch  $S$ , which could also be paralleled with a second on/off switch to facilitate remote control switching. The differential output state of the amplifier  $Tr_1$  to  $Tr_3$  is governed by switch  $S$ , provided the base of  $Tr_2$  is connected to the junction of  $R_3$  and  $R_4$ . This corresponds to linking pins 7 and 8 on the printed circuit board. Alternatively, the switching could be done by an external d.c. signal of about 4-5 volts negative with respect to the 24V supply rail. In that case, the switching voltage should be applied directly to the base of  $Tr_2$  with pins 7 and 8 isolated from each other. The magnitude of this switching voltage was chosen with t.t.l. compatibility in mind.

Lamps  $L_1$  and  $L_2$  are indicators for the

### Component list

Resistors: 1/8W,  $\pm 2\%$  unless otherwise stated.

$R_1$ & $R_2$	10k $\Omega$	$R_{23}$	150k $\Omega$	$R_{39}$	560k $\Omega \pm 5\%$
$R_3$	30k $\Omega$	$R_{24}$	330k $\Omega \pm 5\%$	$R_{40}$	220k $\Omega$
$R_4$	82k $\Omega$	$R_{25}$	150k $\Omega$	$R_{41}$	27k $\Omega$
$R_5$	1.5k $\Omega$	$R_{26}$	330k $\Omega \pm 5\%$	$R_{42}$	100k $\Omega$
$R_6$ & $R_7$	15k $\Omega$	$R_{27}$	4.7k $\Omega$	$R_{43}$	47k $\Omega$
$R_8$	10k $\Omega$	$R_{28}$	680 $\Omega$	$R_{44}$	2.2k $\Omega$
$R_9$	5.6k $\Omega$	$R_{29}$	4.7k $\Omega$	$R_{45}$	18k $\Omega$
$R_{10}$	3.9k $\Omega$	$R_{30}$	680 $\Omega$	$R_{46}$	100k $\Omega$
$R_{11}$	$\frac{1}{2}W, 160\Omega \pm 5\%$	$R_{31}$ & $R_{32}$	3.3k $\Omega$	$R_{47}$	560 $\Omega$
$R_{12}$	1W, 270 $\Omega \pm 5\%$	$R_{33}$ & $R_{34}$	10M $\Omega \pm 10\%$	$R_{48}$	27 $\Omega$
$R_{13}$	$\frac{1}{2}W, 160\Omega \pm 5\%$	$R_{35}$	3.3k $\Omega$	$R_{49}$ & $R_{50}$	470 $\Omega \pm 10\%$
$R_{14}$	1W, 270 $\Omega \pm 5\%$	$R_{36}$ & $R_{37}$	10M $\Omega \pm 10\%$	$R_{51}$	1k $\Omega \pm 10\%$
$R_{15}$ - $R_{22}$	120k $\Omega$	$R_{38}$	680k $\Omega \pm 5\%$	$R_{52}$	100k $\Omega \pm 10\%$
				$R_{53}$	100 $\Omega \pm 10\%$

### Capacitors:

$C_1$	500 $\mu$ F/12V	$C_6$ & $C_7$	50 $\mu$ F/12V	$C_{11}$	33pF
$C_2$	1 $\mu$ F	$C_8$	4 $\mu$ F/25V	$C_{12}$	50 $\mu$ F/12V
$C_3$	30 $\mu$ F/6V	$C_9$	1 $\mu$ F	$C_{13}$	100 $\mu$ F/25V
$C_4$ & $C_5$	4 $\mu$ F/25V	$C_{10}$	10 $\mu$ F/12V	$C_{14}$	500 $\mu$ F/25V

### Semiconductors:

$D_1$	BZY88, C3V3	$Tr_5$ & $Tr_6$	2N930	$Tr_{16}$	2N3820
$D_2$ - $D_5$	1N916	$Tr_7$	2N2219A	$Tr_{17}$	2N3819
		$Tr_8$ - $Tr_{13}$	2N930	$Tr_{18}$	2N3702
$Tr_1$ - $Tr_3$	2N3702	$Tr_{14}$	2N3820	$Tr_{19}$ - $Tr_{21}$	2N930
$Tr_4$	2N2219A	$Tr_{15}$	2N3819		

### Lamps

$L_1$ & $L_2$	6V, 40mA
---------------	----------

two stereo-pair programmes. When  $S$  is open,  $L_1$  lights and signals present at input pins 4 and 13 pass through to the output pins 2 and 12 respectively. Conversely, the closed position of the switch corresponds to  $L_2$  lighting and the signals at pins 5 and 14 appearing at output pins 2 and 12 respectively.

Finally, the 1 $\mu$ F capacitor  $C_2$  is used to reduce the change-over speed at the output of the differential amplifier. In this way, transients otherwise generated by rapid switching of the a.c. signals are subjectively eliminated. Note that this capacitor alone determines the switching speed of the complete unit.

### Construction

All components of the stereo silent switch except the two lamps and switch  $S$  are mounted on a printed circuit board shown in Fig. 4. The corresponding component layout is outlined in Fig. 5 which is immediately followed by relevant explanatory notes and the line-up procedure.

During assembly, it should be observed that the capacitor  $C_2$  is not in physical contact with the resistor  $R_{12}$  because the latter generates a certain amount of heat.

The length of the wires connecting switch  $S$  to the circuit are not critical. In fact, the circuit operates satisfactorily with remote control wires ten meters long. However, should the casing of switch  $S$  chosen be connected to any one of its pins, measures must be taken to eliminate the possibility of an inadvertent contact between the casing of that switch and earth. Otherwise, either a short circuit is created across the d.c. supply line, or a 21V reverse bias will be imposed across the base to emitter junction of  $Tr_3$ .

### Operating voltages

Point	$S$ open	$S$ closed
1, 3, 6 & 11		0 Volts
7	17.6	24.0
8	17.6	24.0
9	24.0	17.8
10	17.8	24.0
15		24.0
C		20.8
D		21.9
E	18.3	21.4
F		11.8
G	10.7	0
HA & HB	23.7	12.4
I	11.9	0
J	0	11.9
KA & KB	0.14	11.4
L	11.4	24.0
M	24.0	11.4
NA & NB	12.4	23.7
O	0	10.7
PA & PB	11.4	0.14
Q		23.0
R		11.5
T		8.8
U		1.14
V		19.4
a		14.8
f		12.1
g		11.8
h		11.8
m	23.4	12.3
n		11.8
q	0.43	10
r	12.3	23.4
t	10	0.43
u		14.7

### Performance tests

Objectively, the unit meets the required specification initially outlined. Total harmonic distortion, for example, is in fact less than 0.2% from 30Hz to 15kHz for an output level of +10dBm into 600 $\Omega$ . The distortion is predominantly second harmonic and its magnitude decreases with reduction in the output level.

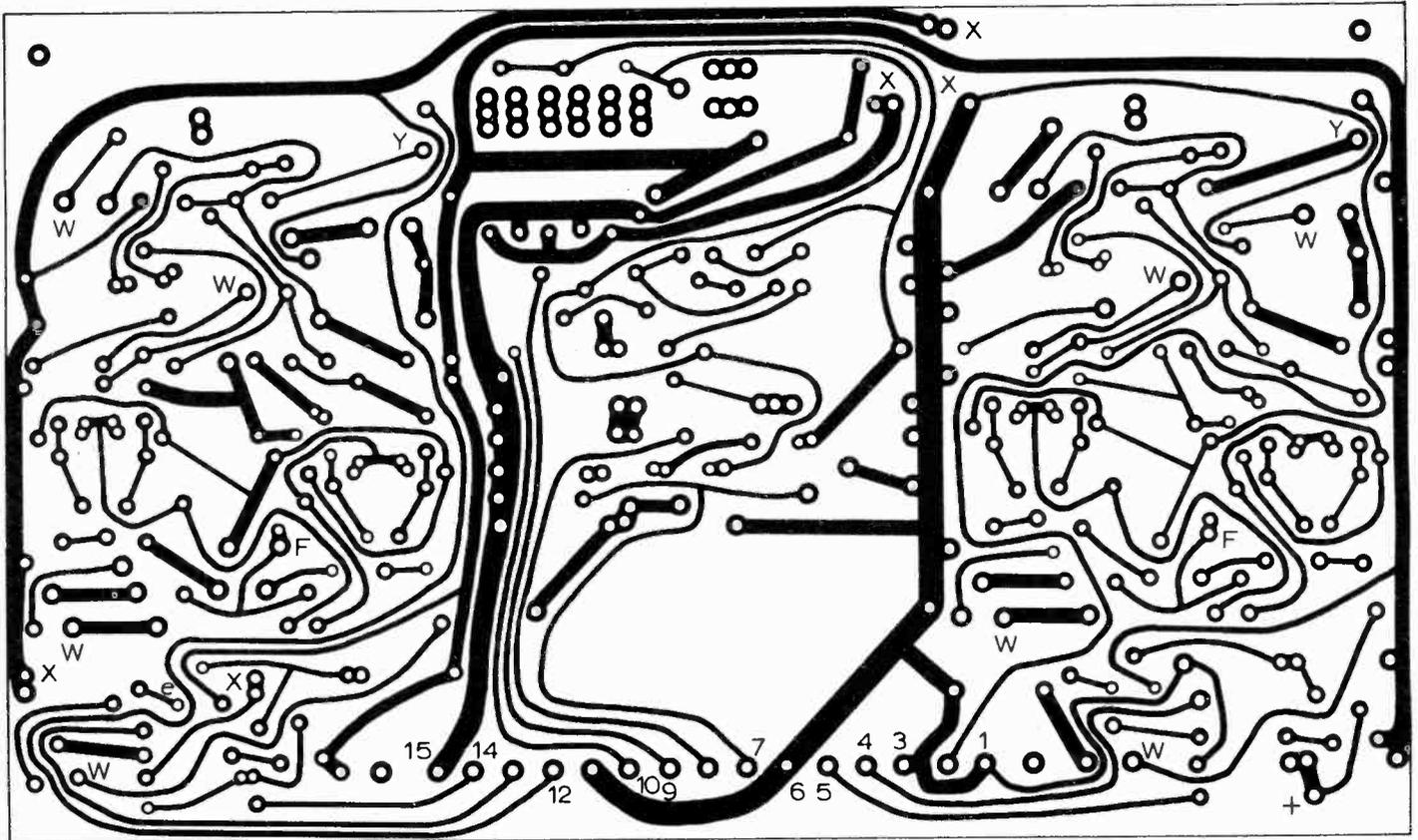


Fig. 4. Printed circuit layout of silent switch.

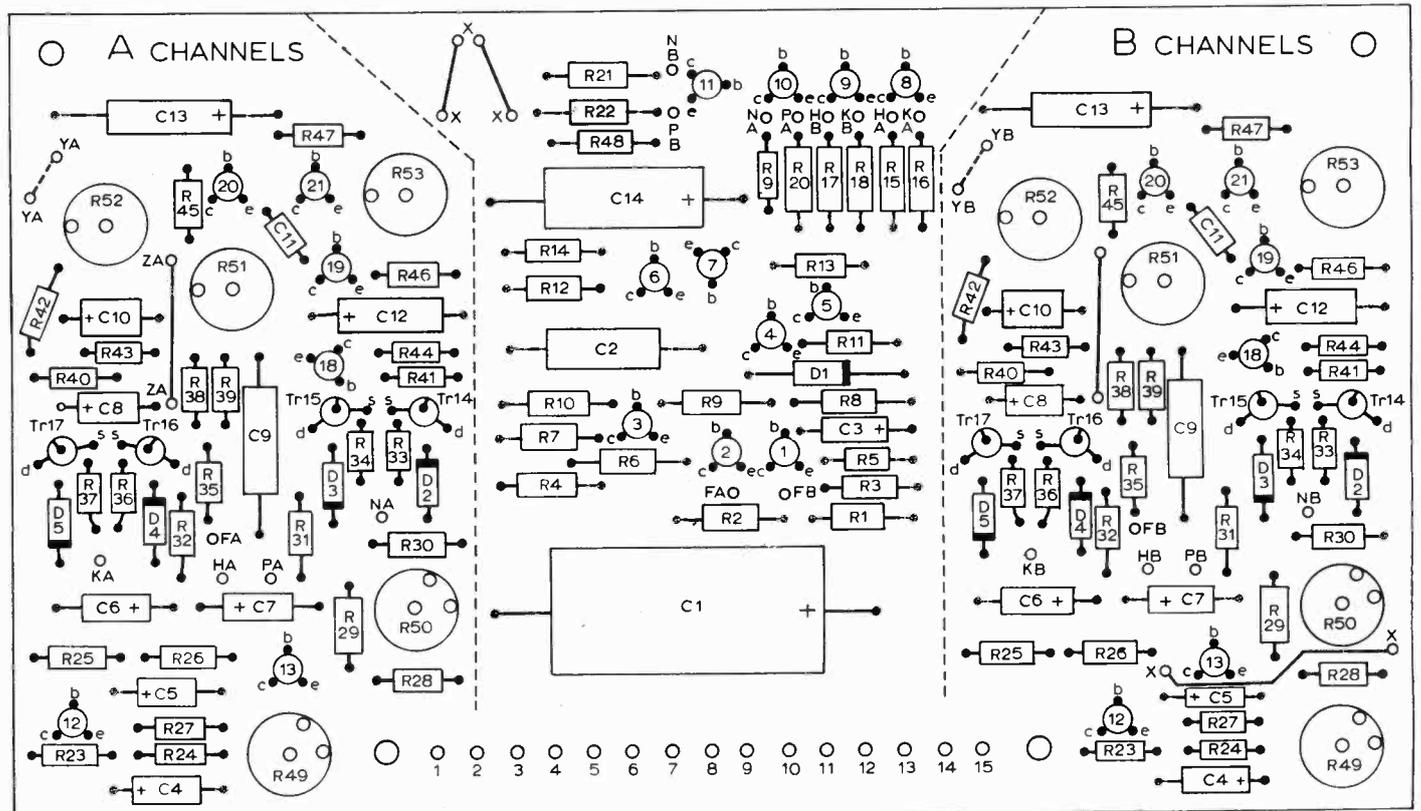


Fig. 5. Printed circuit component layout.

The d.c. switching and indicating section components are placed in the middle of the board. Components belonging to the signal carrying parts of the circuit are positioned to the left and right of the board for the A and B channels respectively. External Connections. Connect points marked X to each other as indicated. DO NOT connect points Y at this stage. Connect the following: HA to HA, KA to KA, NA to NA, PA to PA, FA to FA, ZA to ZA, etc.

Line-up Procedure. With no signal applied, connect an ammeter between points YA. Adjust  $R_2$  so that the ammeter reads 12mA. Remove the ammeter and connect points YA together. Set  $R_{53}$  to obtain an output impedance of 600Ω. Terminate the output (pin 2) with a 600Ω load. Apply a 1kHz, -10dBm signal (via a 100μF capacitor with its positive end connected to the circuit) to either end of  $C_9$ . Adjust  $R_{51}$  to obtain +10dBm at the output. Connect pins 7 and 8 together. Apply a 1kHz, +10dBm signal

to pin 4 (the input). Adjust  $R_{50}$  so that the output is at +10dBm. Apply a 1kHz, +10dBm signal to pin 5. Close switch S (see circuit diagram). Adjust  $R_{49}$  so that the output is also at + dBm. Repeat the same procedure for the B channels. Pins 1 to 15 are laid out for connection to a Pantone 15 pole plug type 73/10/1501/10.  $Tr_{20}$  and  $Tr_{21}$  should be matched.

The switching speed of the unit was measured in terms of a parameter called parameter implies "Fade-in" as well as time taken for the output level of the switch to change by 60dB. Note that the parameter implies "Fade-in" as well as "Fade-out". This mode of measurement was adopted in preference to the other criteria generally used because it is subjectively meaningful and compatible with the properties of human hearing as well as other parameters in acoustical engineering. The justification generally accepted is that a 60dB reduction in the sound pressure level of a programme makes it inaudible under average conditions. A figure of  $25\text{ms} \pm 20\%$  was obtained as the Fade-Time of the silent switch.

Subjectively, the switching was found to be free from transients for all programme materials including pure tone. Nevertheless, in order to investigate the subjective detectability of the actual transition, the same programme was fed to both inputs and the switch was operated so as to create a momentary interruption. The degree of the impairment caused by the transition was then judged by a few observers experienced in sound quality evaluations. It was found that the detectability of the transition was dependent on the programme used and the relative instant at which the switch was actuated. For speech and music if the change-over was made during the momentary silences of the programme, then the transition was not noticeable. However, if switching was done during the existence of a continuous passage, then the interruption was found to be noticeable but quite acceptable. The same judgment was also passed when continuous signals such as pink noise or pure tone were used.

Two units were manufactured, both of which were in continual daily use for about 14 months with satisfactory performance. The few problems encountered during this period were minor ones and their corresponding remedies have already been mentioned.

It is perhaps worth mentioning that during the designing stages, attempts were made to add electronic fading facility to the unit. Unfortunately, it was found that using f.e.t.s as the fading element, realization of a unit capable of low distortion performance during an entire fade, in addition to high on/off and signal to noise ratios, was not really possible. However, the author has since designed a four-channel modulation type electronic fader, the details of which will hopefully be published soon!

#### Acknowledgement

The above paper presents an engineering aspect of a Ph.D. project financed by the University of Surrey but carried out at the BBC Research Department. I would like to thank both bodies for making this rather unusual but most productive arrangement possible.

## Literature Received

#### APPLICATION NOTES

We have received a copy of the 256-page Sescosem linear i.c. application manual, Vol. 1, *Les amplificateurs operationnels*. The manual is published in French only. There are companion volumes on voltage regulators and active filters. Editions Radio, 9 rue Jacob, 75006 Paris, France. . . WW417  
A Precision Monolithics leaflet on the realization of a high-speed, eight-bit a-d converter is available from Bourns (Trimpot) Ltd, Hodford House, 17/27 High Street, Hounslow, Middlesex TW3 1TE. WW418  
The British Standards Institution have recently published BS5102, "Phenolic resin bonded paper laminated sheets for electrical applications," which gives requirements for six types of sheet material and test methods. Copies are available at £4 from BSI Sales Department, 101 Pentonville Road, London N1 9ND.

A chart has been prepared by ERMA to provide information on the correct way to crimp a variety of r.f. connectors, using ERMA hand crimping tools. ERMA Ltd, Mount Pleasant, Alperton, Wembley, Middlesex. . . WW419  
A bulletin (No. 2) is available from Qantex on the recovery of phase-encoded digital signals on magnetic tape in the ANSI four-track,  $\frac{1}{4}$ -in, 1600 bits per inch format. North Atlantic Industries Inc, Qantex Division, 200 Terminal Drive, Plainview, NY, USA. . . WW420  
GIM have sent us a copy of their application note on the AY-5-9100 microcircuit for use in push-button telephone systems. The publication provides circuit information on the use of the i.c. in mains diallers, line-powered instruments, re-dialling and card-reading telephones and repertory diallers. General Instrument Microelectronics Ltd, 57-61 Mortimer Street, London W1N 7TD. . . WW421

#### EQUIPMENT

A brochure is available describing the interfaces produced to enable Datalab 900 transient recorders to work with computers, punches, typewriters and other peripherals. Data Laboratories Ltd, 28 Wates Way, Mitcham, Surrey CR4 4HR. . . WW408  
Descriptions of paging systems, both loop and radio types, are contained in a publication from Sales Office, Multitone Electric Company Ltd, Underwood Street, London N1. . . WW409  
We have received a leaflet on the Nea Lindberg 1kVA static inverter, which provides a 50Hz, 220V sinusoidal output at up to 4.6A from 20-30V d.c. Efficiency is 75%. Avel-Lindbert Ltd, South Ockendon, Essex. . . WW410  
Teradyne have produced a book entitled "High-volume testing for electronic device users" which is mainly concerned with the use of Teradyne automatic test equipment in the inspection of devices and assemblies. The publication costs £1 from Teradyne Ltd, Clive House, 12 Queens Road, Weybridge, Surrey.

A brochure on the CILCOM 1600 system for the conversion of magnetic tape computer output into a film record (COM for Computer Output onto Microfilm) has been sent to us by UCC/Computer Instrumentation Ltd, School Lane, Chandler's Ford, Eastleigh, Hants. . . WW411  
The 1974/75 brochure of Pickering pickup cartridges is now available. The brochures are published in two editions, with six languages in each, and are obtainable from Highgate Acoustics, 38 Jamestown Road, London NW1 7EJ. . . WW412

We have received a brochure on the range of equipment marketed by Telephone Rentals, which includes telephones, data communications, staff location, time control, production control and fire and security equipment. Telephone Rentals Ltd, 197 Knightsbridge, London SW7 1RL. . . WW413  
Ship-borne and shore station radio-telephone equipment is described in a brochure (RF-201M) sent to us by Harris Corporation, 1680 University Avenue, Rochester, New York. Specifications of six basic models are included. . . WW414  
SE Labs have published the latest in a series of Complete Guides, this time to oscillographs, ultraviolet and other types. SE Labs (EMI) Ltd, North Feltham Trading Estate, Feltham, Middlesex TW14 0TD. . . WW415  
Labgear have published a brochure on television and f.m. radio reception equipment, v.h.f./u.h.f. distribution equipment and television test instrumentation. Labgear Ltd, Abbey Walk, Cambridge CB1 2RQ. . . WW416

#### PASSIVE DEVICES

Beckman have produced a 12-page booklet describing their range of Resnet resistor networks in various packages. Beckman Instruments Ltd, Components International, Queensgate, Glenrothes, Fife, Scotland. . . WW406  
Sprague have produced a wall-chart which gives brief details of a range of aluminium electrolytic capacitors. Sprague World Trade Corporation, Färberstrasse 6, 8008 Zürich, Switzerland. . WW407

#### ACTIVE DEVICES

Mullard have sent us a copy of their newly published 1974/75 data book. Valves, c.r.t.s, semi-conductors, resistors, capacitors, i.c.s and assemblies for entertainment purposes are briefly described. The publication is available from booksellers or from Technical Press Ltd, Freeland, Oxford OX7 2AP at 40p.

Microwave Associates Ltd have sent us three leaflets, on a Gunn diode local oscillator for a 9470MHz centre frequency (MA87635), the MA7701C series of tunnel diode detectors and a range of p-i-n diodes (Bulletin 4306). Available from Microwave Associates, Dunstable, Beds. . . WW401  
Siliconix have sent us their latest short-form catalogue, which includes information on junction f.e.t.s and dual-gate mosfets, a  $3\frac{1}{2}$ -digit a-to-d converter, a triple op-amp and new driver gates. Siliconix Ltd, 30A High Street, Thatcham, Newbury, Berks RG13 4JG. . . WW402  
ITT have produced a booklet on m.o.s. devices entitled "Everything you wanted to know about m.o.s.". It explains the pros and cons of the process and there is a glossary. ITT also have their new short-form semiconductor catalogue. ITT Semiconductors, Footscray, Sidcup, Kent.

Booklet . . . WW403  
Catalogue . . . WW404  
A wall-chart from RCA presents mechanical and electrical information on their range of linear integrated circuits and includes a cross-reference between the RCA products and twelve other types. There is a list of application notes. RCA Ltd, Solid-state—Europe, Sunbury-on-Thames, Middlesex. . . WW405

#### GENERAL

The "Handbook of Electrical Connectors" has been published by Pye Connectors Ltd, Hitchin Street, Biggleswade, Beds. It is a loose-leaf folder in which is collected all the information on Pye's various types of connector, including the printed-circuit variety. . . WW422

The solenoids in the Magnetic Devices range are described in a short-form catalogue which gives salient mechanical and performance information. Magnetic Devices Ltd, Exning Road, Newmarket, Suffolk. . . WW423  
A catalogue of small mechanical components and p.c.b. furniture is published by Dieter Assman Electronics Ltd, Victoria Works, Water Lane, Watford, Herts. The company markets the products of the German Assman KG company. No price list is provided. . . WW424

# Research Notes

## Enter the white hole

If a black hole in astronomy is a star which has collapsed to nothing then a white hole is the reverse, that is, matter which suddenly appears at a point in space. While there is no observational evidence that such a thing happens it is always of interest to astronomers to theorize about such things. Three Indian astronomers have been doing so. They conclude that the appearance of a white hole would be marked by a great burst of radiation, mostly at very short wavelengths (X-rays and gamma rays). The radiation is not very different from what is actually observed from certain types of galaxy, so the possibility that white holes exist in reality as well as in theory is open.

*Nature*, Oct. 18, 1974, vol. 251, p.590.

## Thermistor-stabilized oscillators

Low-distortion RC oscillators in which lamps or thermistors are used to stabilize the level of oscillation tend to suffer from "amplitude bounce". Any small disturbance to the circuit, such as the manipulation of a tuning control, causes the amplitude to jump about. Usually the effect dies away but in bad cases the bounce continues indefinitely, so that the output of the oscillator becomes an amplitude-modulated sine wave.

It has been known for a long time that bounce is an inherent property of low-distortion oscillators and gets worse as the distortion of the maintaining amplifier is reduced. (Some commercial oscillators can be operated in two modes: a low-distortion mode for use when purity of waveform is important and a "fast-settling" mode for such work as measuring frequency responses where bounce is a nuisance.) In a thorough analysis, P. L. Taylor of the University of Salford shows that even a small amount of amplifier distortion (0.1% third harmonic) damps the bounce by a large factor (16) compared with the ideal case of a distortionless amplifier. Bounce in practice is less than predicted by simple theory, probably because the usual assumption that the temperature is uniform throughout the thermistor bead is in practice invalid. Non-uniformity changes the

effective thermal time constant, which is an important quantity in the bounce equation.

Distortion is caused by the thermistor itself heating and cooling a little during each half-cycle of oscillation. The distortion is worst at the lower frequencies (0.1% at 10Hz in a typical circuit). The distortion can be reduced (at the expense of increased bounce) by putting resistance in series with the thermistor.

*Proc. I.E.E.*, Aug., 1973, vol. 120, no. 8.

## Power from ocean waves

An Edinburgh scientist says that if the energy in the Atlantic waves which approach Britain's western shores could be extracted along a frontage of a few hundred kilometres it would be enough to supply the present power needs of these islands.

Most proposals for extracting energy from sea waves make use of the up-and-down boat-bobbing movement as the wave passes a floating object. This, however, does not extract the maximum amount of energy, because the particle motion in the wave itself is not up and down but circular. A mechanism has been tested in the laboratory which makes use of the circular motion. It has rollers of egg-shaped cross-section which rotate, turning first one way then the other as the wave passes. A floating breakwater containing these structures should extract nearly all the wave energy, leaving calm water on the shoreward side.

The intermittent flow of wave energy poses problems in conversion to steady electrical supplies. One possibility is to use the waves to drive, first, a pump which would build up a head of liquid then allow the liquid to escape steadily, driving a turbo-generator. Development of the idea is to be supported by a government grant.

Dept. of Mechanical Engineering, Univ. of Edinburgh.

## First binary pulsar

The big radio telescope at Arecibo, Puerto Rico, has discovered a pulsar which is one partner in a double star, the other being an ordinary star. The ordinary star has not yet been detected, but its presence is deduced from the way in which the pulsar's period is Doppler-shifted every few hours, as it moves away from the earth then towards the earth in a highly elliptical orbit.

This discovery is of interest for the light it may cast on supernova explosions. Pulsars are currently thought to be neutron stars, small, very dense objects which may well be all that is left of a supernova. The fact that a normal star might have continued to exist in close proximity to a supernova in this present example lends support to the idea that the X-ray-emitting binaries recently discovered are also made up of supernova remnants.

## Watching high-speed transistors in slow motion

The scanning electron microscope has been used for some years to image transistors in operation. Changes in the potential of the transistor surface affect the electron beam

and are therefore visible on the microscope's "TV screen". The University College of North Wales, Bangor, has a method of "strobing" its scanning electron microscope at up to 10GHz, making it possible to "freeze" high-speed events in the transistor under examination.

## Sunspots, Jupiter, and earthquakes

1982 should be a bumper year for sunspots—and earthquakes. So say J. Gribbin and S. Plagemann ("The Jupiter Effect," Macmillan, London). The basic idea is that the number of sunspots is affected by the gravitational pull of the planets on the sun; this is increased when two or more planets are in line. In 1982 all the planets will be in line, for the first time in 179 years. Sunspots are known to affect the climate on earth, and the authors argue that this in turn will produce a slight perturbation of the earth's rotation and trigger off any incipient earthquakes.

Meanwhile, astronomers and radio-propagation experts will be checking up on another sunspot relationship just reported by G. M. Brown of the University College of Wales, Aberystwyth. Solar activity produces ionospheric currents which interfere with the horizontal component of the earth's magnetic field. The field on a normal "quiet" day goes through a minimum at about 11.00 hours local time. However, there are also "abnormal quiet days" when the effect takes place at some quite different time. Examination of magnetic records for England (which go back to 1885) shows that these abnormal quiet days go through a cycle like the sunspots, but with a maximum which occurs at sunspot minimum. What is more to the point, for ionospheric predictions, is that the "AQD" count seems to be a good measure of the intensity of the sunspot maximum which will follow it, in about six years.

*Nature*, Oct. 18, 1974, vol. 251, p.594.



*If a ship fitted with this Kodan radio buoy sinks, the buoy surfaces and transmits a distress signal for over 48 hours.*

# Computer monitoring of TV signals

An experimental digital system for the monitoring of unmanned television transmitters.

by J. Schaffer, B.Sc., A.R.C.S.

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Present methods of monitoring the quality of a television signal are almost invariably based on measurements of Insertion Test Signals (ITS). These signals are inserted into the field blanking interval of the signal, and usually accompany it from point of origin (studio) to destination (domestic TV receiver).

Over recent years the forms of the ITS have been agreed both nationally and internationally, and are shown in Fig. 1. Certain technical quality parameters based on the ITS are listed in Table 1.

Practical techniques for measuring the quality parameters may be divided into two categories—manual and automatic. Manual methods use oscilloscopes with special graticules for the measurement of white bar tilt and 2T pulse *K* factors; for differential phase and gain, vectorscopes or special purpose measuring instruments are used. Manual measurement of non-linearity is made with a differentiating filter acting upon the staircase waveform backed by a high gain amplifier<sup>1,2</sup>.

Automatic measuring methods may be sub-divided into the usual two categories of analogue and digital. There are now available automatic analogue machines<sup>3,4</sup>, which evaluate many of the parameters listed in Table 1. It is expected that auto-

matic methods will predominate as more automatic correcting and control equipment is brought into service. The output signals (direct voltages) from these analogue machines are used to raise alarms or to actuate local control equipment should any of the quality parameters fall outside

certain pre-set limits. In addition, the analogue outputs may be converted into digital form by a digital voltmeter and the digitized data telemetered to a central control room. At the control room the received data may be used merely for record purposes, or to decide whether

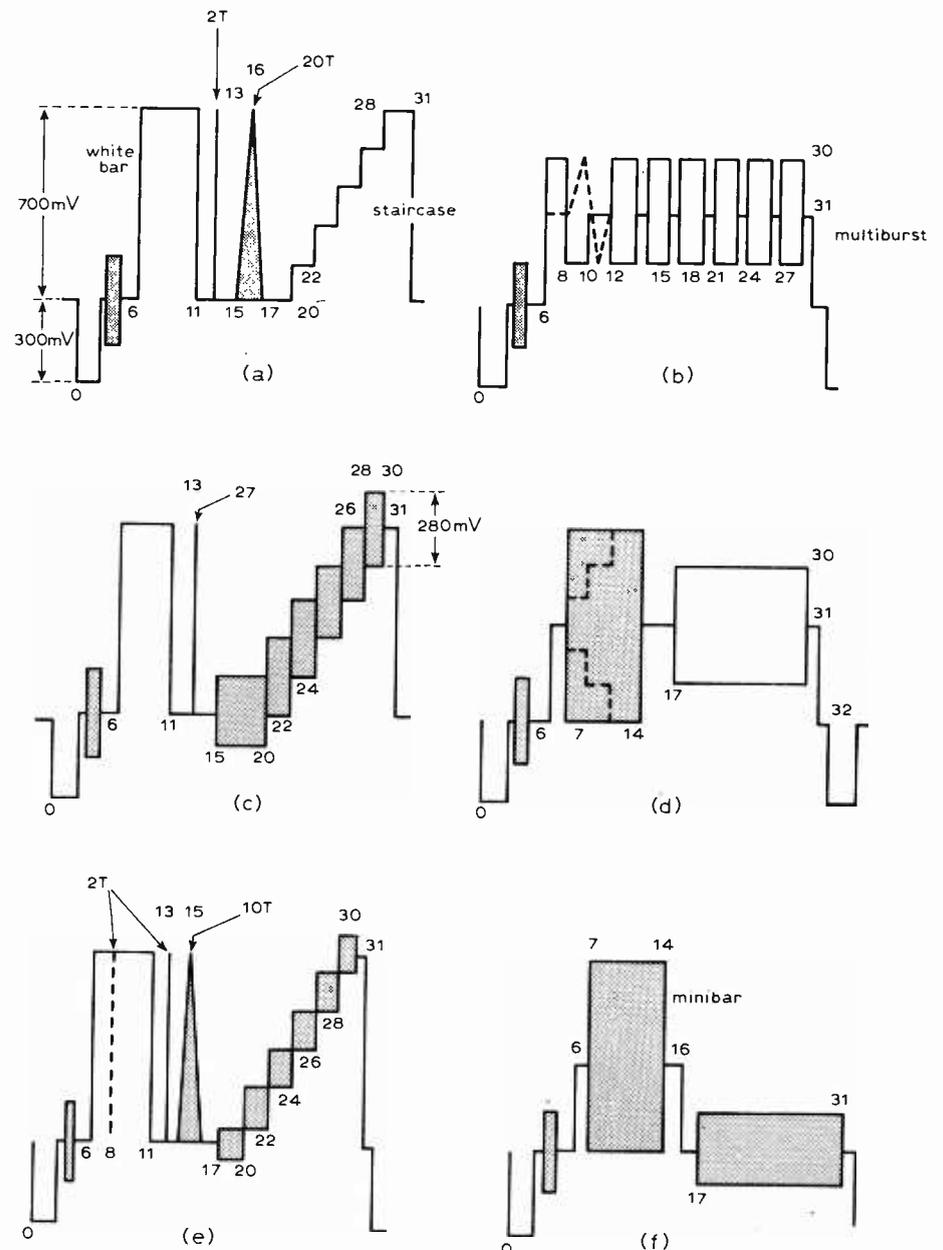


Fig. 1. International Test Line Signals a, b, c and d, inserted on lines 17, 18, 330 and 331. The National Test Line Signals a and b are inserted on lines 19 and 32, and lines 20 and 335.

Table 1

Quality Parameter	Waveform Used
Insertion gain	White bar
White bar tilt	White bar
Pulse to Bar <i>K</i> factor	White bar and 2T pulse
Non-linearity	Staircase
Differential gain	Staircase with superimposed sub-carrier
Differential phase	Staircase with superimposed sub-carrier
Chrominance luminance delay	10T or 20T pulse
Chrominance luminance cross talk	Mini bar
Chrominance luminance gain	Mini bar

remote control equipment should be actuated.

As far as is known there are no digital machines commercially available at present. There is, however, an experimental digital system, developed by the Independent Broadcasting Authority, which is being used to monitor unmanned television transmitters. This system has been undergoing field tests since November 1972 at the Lichfield control and monitoring centre of the Independent Broadcasting Authority<sup>5</sup>.

In its mode of operation, off-air signals are received at the monitoring centre from the unmanned transmitters in the vicinity, each transmitter being serviced in turn. After the received signal has been amplified and demodulated by a high-quality receiver, the ITS is extracted and applied to a fast sample-and-hold circuit backed by a fast analogue-to-digital converter. Evaluation of the quality parameters from the resulting digital data is performed by a general purpose digital computer. Results of the field tests show that good agreement is obtained with both manual measurements and with automatic analogue measurements. The off-air system of monitoring has the advantage that the main capital cost is concentrated at one location—the monitoring and control centre—giving a lower overall cost than a monitoring system using automatic measuring machines at each unmanned site.

Generally the signal-to-noise ratios met in off-air monitoring are poor compared to those met in on-site monitoring. Consequently the computer programmes which derive the quality parameters have been designed to operate in conditions of high noise by using averaging techniques to improve the signal to noise ratio<sup>6</sup>.

In passing it is worth noting that the relatively poor noise performance of analogue machines prevents their use in similar off-air monitoring systems.

Although the field tests have shown that adequate performance is obtained with off-air signals received at Lichfield, it was envisaged that cases would occur where the received signal-to-noise ratios would be too low for the system to operate, particularly where the unmanned station and the monitoring and control centre were located in hilly areas, or in conditions of severe co-channel interference.

To cover such cases the Independent Broadcasting Authority initiated the development of a digital telemetry system which could be dovetailed with the off-air monitoring system, using, as far as pos-

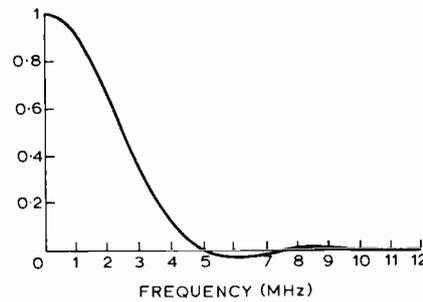


Fig. 3. Spectrum of the 2T pulse.

sible, common digital hardware and software. The function of the digital telemetry system would be to transmit measurements made at the "difficult" sites back to the monitoring and control centres using either the public switched telephone network or private telephone lines.

### Design of the digital telemetry system

An important factor in the design of the telemetry system is the need to minimize the cost of the measuring equipment installed at the sites to be monitored. Consequently it would seem that only the simplest measurements and processes should be undertaken on-site, with the bulk of the data processing carried out by the relatively expensive equipment at the monitoring and control centre. Unfortunately, it is found that this strategy dictates long data transmission times and a slow system response.

This can be seen by taking as an example the measurement of r.m.s. noise. To obtain a good estimate of noise about 200 samples need to be taken at a nominally constant part of the television waveform (preferably during the "quiet line"). If these samples are digitized by an eight-bit analogue-to-digital converter, the total number of bits equals 1,600, and the time taken to transmit these bits over a 50-baud (bits per second) channel is 32 seconds. Coupled with the transmission time of the ITS data, which would be at least as long, it is seen that the total data transmission time is in the order of minutes. This time may be reduced if, instead of transmitting raw data, a small amount of digital processing is performed upon the data prior to transmission. A block diagram of a measuring system, incorporating the above ideas, is shown in Fig. 2.

Circuit design was begun using read-only memories (ROMs) to determine sample timings and random access

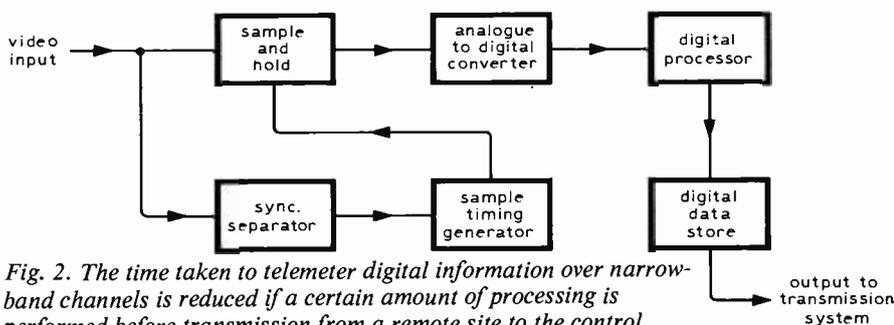


Fig. 2. The time taken to telemeter digital information over narrow-band channels is reduced if a certain amount of processing is performed before transmission from a remote site to the control centre.

memories (RAMs) to hold the data prior to transmission—data processing was carried out by an adder/subtractor unit made up in t.t.l. It was soon realized that the design was merely reproducing, at a high cost, circuitry that was already available in commercial microcomputers, and the original development policy was abandoned, subsequent development being based on the use of a microcomputer containing a single chip four-bit central processing unit.

The need for cheapness also limits the performance of the analogue-to-digital converter employed. Some converters are able to convert in fractions of a microsecond and form the heart of equipments such as DICE<sup>7</sup>. Unfortunately these fast converters are too expensive for this application and a cheaper, slow converter was used, which converts to eight bits in about 12 microseconds. Using a slow converter means that only a small number of samples can be taken in the 64-microsecond duration of each insertion test signal.

In practice, programming the microcomputer is simplified if only one sample is taken during each ITS, i.e., a sample rate of 25Hz or 50Hz. At this point it may be well to recall the well-known Sampling Theorem which states that a band limited signal may be reproduced, without error, from samples taken at a rate of at least twice the bandwidth of the signal. Sampling at field or picture rate would therefore apparently limit the bandwidth of the measurements to either 12.5Hz or 25Hz. This limitation is overcome by employing strobing techniques identical to those used in sampling oscilloscopes<sup>8</sup>, wherein the sample timing is advanced, between samples, by an amount not greater than half the period of the maximum frequency contained in the signal.

### Measurement theory

**Luminance parameters.** Sufficient samples need to be taken at various points along the ITS to provide the required data for calculating the luminance quality parameters: white bar amplitude, white bar tilt, 2T pulse response, and luminance non-linearity.

Measurement of white bar height and tilt requires four samples to be taken at appropriate points along the waveform. The accuracy of measurement is limited by the quantization errors of the analogue-to-digital converter, and may be estimated as follows. If the input signal is 1 volt peak to peak and it occupies, say, 0.7 of the full range of an eight-bit analogue-to-digital converter (thus allowing for a possible 3dB increase in input signal level without overloading the converter), then the picture component would span  $0.7 \times 0.7 \times 255 = 125$  quantization levels where the number 255 corresponds to the highest level of an eight-bit converter ( $=2^8 - 1$ ). The measuring error for each sample due to quantization is  $\pm \frac{1}{2}$  level; therefore the maximum error in bar height is  $\pm 1$  level since two measurements are used to evaluate the white bar height. The

fractional error is  $\pm 1$  in 125 or about  $\pm 0.8\%$ . Error in tilt measurement expressed as a percentage of white bar height is likewise  $\pm 0.8\%$  maximum. These errors are usually quite acceptable for most television measuring purposes. In the case of luminance linearity, measured on the staircase, the situation is somewhat worse. Each staircase riser height is approximately 25 quantum levels and the error of  $\pm 1$  level corresponds to an error in the measurement of luminance linearity of 8%, a performance which is not satisfactory. Improved accuracy may be obtained by adding small amounts of noise to the signal and averaging over many samples<sup>6</sup> or by superimposing sub-carrier on the staircase and averaging over four, or multiples of four fields.

For the 2T pulse, samples need to be taken at timing intervals short enough to permit the pulse to be reconstituted from the samples according to the Sampling Theorem. In Fig. 3 is shown the spectrum of the 2T pulse, from which it is seen that there is little energy beyond 5.0MHz, implying that the sample intervals should not exceed 100nanoseconds.

As mentioned above, strobing techniques are used to obtain these short timing intervals, the samples, which in real time repeat at picture intervals (40 milliseconds), being advanced by the required sampling intervals until the whole of the 2T pulse is covered. For reasons associated with the evaluation of the colour components of the Insertion Test Signal, the timing increments are derived from 13.5MHz oscillator giving a minimum timing increment of 74.1 nanoseconds and a bandwidth of 6.75MHz. The total number of pulses used for strobing the 2T pulse is 27, covering 2 microseconds, including a half microsecond allowance for timing errors in the location of the 2T pulse. In a similar manner, by strobing the line sync. pulse it is possible to measure sync., pulse amplitude, duration and rise times.

**Colour components.** At first glance the use of strobing techniques for evaluating chrominance data appears to be invalidated by the changes in sub-carrier phase which occur from field to field. Fortunately in the case of the PAL system these phase changes may be put to good use. It can be shown<sup>9</sup> that the phase of the sub-carrier component of the Insertion Test Signal, when referred to the preceding line sync. pulse, varies from field to field in multiples of 90 degrees. Taking line 19 as reference, the relative phases are:

Line No.	19	332	19	332	19	332	19	332
Phase	0	90.3	270	0.3	180	270.3	90	180.3

and so on, repeating in an eight-field sequence.

Suppose the amplitude of the Insertion Test Signal at a time relative to line sync. is given by:

$$v = v_L + v_c \sin(2\pi f_{sc} t + \phi),$$

where  $f_{sc}$  is the sub-carrier frequency,  $v_L$  is the luminance amplitude,  $2v_c$  is the peak to peak sub-carrier amplitude, and  $\phi$  is an arbitrary phase angle. Then it follows that the ampli-

tudes of four consecutive samples, taken at picture rate, have the values:—

$$\begin{aligned} v_n &= v_L + v_c \sin \theta \\ v_{n+1} &= v_L - v_c \cos \theta \\ v_{n+2} &= v_L - v_c \sin \theta \\ v_{n+3} &= v_L + v_c \cos \theta, \end{aligned}$$

where  $\theta = 2\pi f_{sc} t + \phi$ .

In these equations it is assumed that samples are confined to either odd or even fields; the method may therefore be applied directly to the International Insertion Test Signals which differ on odd and even fields. (It is also possible that future UK practice will be to use insertion signals from different origins on odd and even fields.) The amplitude and phase of the sub-carrier and the luminance amplitude may be easily derived from these samples by forming the variables:

$$\begin{aligned} v_I &= v_n - v_{n+2} = 2v_c \sin \phi, \\ v_Q &= v_{n+3} - v_{n+1} = 2v_c \cos \phi, \\ v_T &= v_n + v_{n+1} + v_{n+2} + v_{n+3} = 4v_L, \end{aligned}$$

giving  $v_L = v_T/4$ ,  $\tan \theta = v_I/v_Q$ ,  
 $v_c = \frac{1}{2}\sqrt{v_I^2 + v_Q^2}$ .

When evaluating chrominance-luminance delay the 10T pulse is strobed, groups of four phase samples being taken at each sampling point. The microcomputer is programmed to calculate the values of  $v_I$ ,  $v_Q$  and  $v_T$ , and it is these values which are telemetered. At the monitoring and control centre, the luminance amplitude  $v_L$  and the chrominance amplitude  $v_c$  are first evaluated. The values of  $v_L$  and  $v_c$  are then filtered in identical digital filters, in order to reduce noise and quantization errors and the luminance and chrominance 10T pulses are reconstituted according to the Sampling Theorem. A further computer algorithm then evaluates the relative delay between the two 10T pulses.

Unfortunately when evaluating differential gain and phase from the staircase waveform, the above equations when used directly, result in excessive quantization errors. With an eight-bit a.d.c. the 140-millivolt peak to peak sub-carrier superimposed on the staircase waveform spans approximately 25 quantum levels. The maximum quantization error in either  $v_I$  and  $v_Q$  is 1 quantum level corresponding to an amplitude error of 4% and a possible error in differential gain of 8%. Maximum phase errors are about 1/25 of a radian or  $2\frac{1}{2}^\circ$  approx., resulting in a possible error in differential phase of  $5^\circ$ .

A method has been devised which reduces these quantization errors by a process of summing a multiple of samples at each staircase level. At each staircase level, the sampling point is progressed along the sine wave by a small angle  $e$ , the values of  $v_I$  at each sampling point being added together to give a total  $S$ ; likewise the values of  $v_Q$  are added together to give a total  $C$ . If for each staircase step a total of  $n$  groups of four-phase samples are taken, it can be shown by summing sine and cosine series that

$$S = 2v_c \sin(\theta + \left[\frac{n-1}{2}\right]e) \frac{\sin ne/2}{\sin e/2}$$

$$C = 2v_c \cos(\theta + \left[\frac{n-1}{2}\right]e) \frac{\sin ne/2}{\sin e/2}$$

The relative sub-carrier phase and amplitude are again easily evaluated from  $S$  and  $C$ .

The luminance value  $L$  is equal to the sum of the sample values divided by  $4n$ . In these sums quantization errors tend to cancel whereas the signal components reinforce. Although it has not been found possible to evaluate the errors theoretically, practical errors are approximately 1 degree in differential phase, 2% for differential gain, and 1% for luminance non-linearity. These values apply for  $n=8$  corresponding to 32 samples being taken at each staircase level.

The required phase progression  $e$  is automatically obtained by deriving the sample timings from a 13.5 MHz oscillator, the output of which is divided by 864 to line frequency, and locked to the line synchronizing pulses. The resulting value of  $e$  is equal to  $-5.3^\circ$ . Other timing oscillator frequencies are possible,  $\frac{\sin ne/2}{\sin e/2}$  should not be small and that the division ratio to line frequency should be easy to realize in practice.

The analysis of the staircase waveform requires a well-defined sequence of sample timings. On a given step, a set of four-phase samples is taken at a constant time relative to the preceding line sync. pulse; the sample timing is then advanced by three cycles of the 13.5 MHz oscillator and another set of four-phase samples taken and so on until a total of  $n$  four-phase samples have been taken. The sample timing is then advanced to the next staircase step and the process repeated. The timing of each group of  $4n$  samples is made constant relative to the staircase risers, so that transients associated with staircase transitions, or tilt across the steps, affect each group of readings equally. Consequently in the above formulae the value of  $\theta$  varies with the step number, and correction angles must be applied when evaluating differential phase. The values of the correcting angles are given by  $\theta n = 2\pi f_{sc} nT$ , where  $T$  is the time separation between the steps (4.00 microseconds) and  $n$  is the step number (1 to 5) whence

$\theta_1$	$\theta_2$	$\theta_3$	$\theta_4$	$\theta_5$
-84.4	+11.2	-73.2	+22.4	-62.1

Another group of colour measurements often required is the amplitude, position, and rise and fall times of the colour burst envelope. The phase sequence of the colour burst differs from that of the Insertion Test Signals by virtue of the phase alternation which is inherent in the PAL system, and it is not possible to use the above method without modification. It can be shown<sup>10</sup> that the phase of the colour burst, relative to line sync, on a given line and the corresponding line in the next field takes one of two phases  $180^\circ$  apart. Quadrature phases are only obtained when the samples are taken on

pairs of lines half a field apart, for example lines 19 and 175. The sub-carrier amplitude may be evaluated from samples taken on these lines using the previous formula and by strobing the sampling point through the colour burst the required information may be obtained.

**Noise measurement.** Signal-to-r.m.s.-noise ratio is an important measure of signal quality. As indicated previously, about 200 samples taken at a nominally constant part of the signal, are required to obtain a good statistical estimate of the noise. It is of course possible to programme the microcomputer to compute the r.m.s. value of the samples directly, but the relatively complex squaring programme involved in this computation may be avoided by making use of a relationship<sup>11</sup> between the mean square  $P$  and the mean deviation from the mean  $d$ , possessed by Gaussian (normal) noise:

$$d^2 = \frac{2}{\pi} P.$$

Using this relationship it may be shown<sup>12</sup> that the signal-to-noise ratio ( $S/N$ ) in dB is given by:

$$(S/N) = 20 \log_{10} \left( \frac{2.B.m}{\pi.S_m} \right),$$

Where  $B$  is the white bar amplitude and  $S_m$  is the telemetered noise word formed by adding the magnitudes of the differences between consecutive noise samples for a total of  $m+1$  samples.

For an eight-bit analogue-to-digital converter this method of noise measurement is accurate for signal-to-noise ratios less than approximately 49dB.

### Hardware

A block diagram of experimental equipment operating according to the above concepts is shown in Fig. 4. The video signal is clamped and applied to the input of the sample and hold circuit. Timing information from the microcomputer is compared, in a ten-bit comparator, with

the state of a divide-by-1,024 counter driven by 13.5 MHz crystal oscillator. When coincidence occurs a pulse is generated which, after gating by the output of a second comparator, actuates the sample and hold circuit. The second comparator ensures that sampling occurs only during the line selected by the microcomputer. Synchronism between the sequence of operations within the microcomputer and the television waveform is maintained by the line 3/316 signals applied to the microcomputer.

The microcomputer itself, as used in the experimental equipment consists of a single-chip four-bit central processing unit, four ROM and four RAM packages and about 30 t.t.l. packages which are used for control purposes. The ROMs have a total capacity of 1,024 programme steps and the total RAM capacity is 1,280 bits.

### Programming the microcomputer

As a first experimental application of these ideas, it was decided to programme the microcomputer to analyze the staircase waveform. The flow diagram of this programme is shown in Fig. 5, which is seen to consist of a main programme and a measuring subroutine labelled LABA. The main programme after defining the starting time for the scan at black level jumps to the measuring subroutine LABA.

On rejoining the main programme after completing sub-routine LABA the process is repeated for the next step and so on, until the five steps are scanned. At this point the processed measuring data are held in the RAM store and would, in the final system, be read out into the telemetry channel. However in the present experimental system the data are read out directly onto paper tape using a routine labelled PUNCH.

The heart of the staircase programme is the sub-routine LABA. This routine organizes the arithmetic operations made upon the digital measurements in accor-

dance with the foregoing equations. On entering the routine the sample counter is incremented, followed by a test to determine whether the sample count is a multiple of four. If so the sample timing counter is incremented by three which results in the sample timing being advanced by three cycles of the 13.5MHz oscillator for each group of four samples. A test for the presence of the line three signal on an input line of the computer follows.

If the line three signal is not present the microcomputer enters a sub-loop which it can leave only on the presence of the line three signal. The latest timing information as determined by the state of the timing counter is then entered on to the ten output lines which are connected to the timing comparator in the measuring circuitry.

At this point in the programme, a delay is inserted which ensures that the a.d.c. data accepted is derived from a sample taken at the new sampling time. The amount of delay required is estimated by dividing the c.p.u. instruction cycle time (which for this microcomputer is approximately ten microseconds) by the difference between the times that the sample timing data are outputted ( $T_1$ ) and the timing ( $T_2$ ) of the sample in line 19. The time difference between line three and line 19 corresponds to 102 instruction cycles: 16 instruction cycles are taken up between the detection of line three and  $T_1$ , and the delay must therefore be at least 86 instruction cycles. In practice the delay is made up by traversing a loop of 32 instruction cycles five times, giving a total delay of 160—well in excess of the required delay. It is permissible to waste programme time in this way since there is room for approximately 4,000 instructions in the 40 millisecond interval between samples, whereas only 50 are used in the present programme.

After the a.d.c. output has been accepted, one of six RAM locations con-

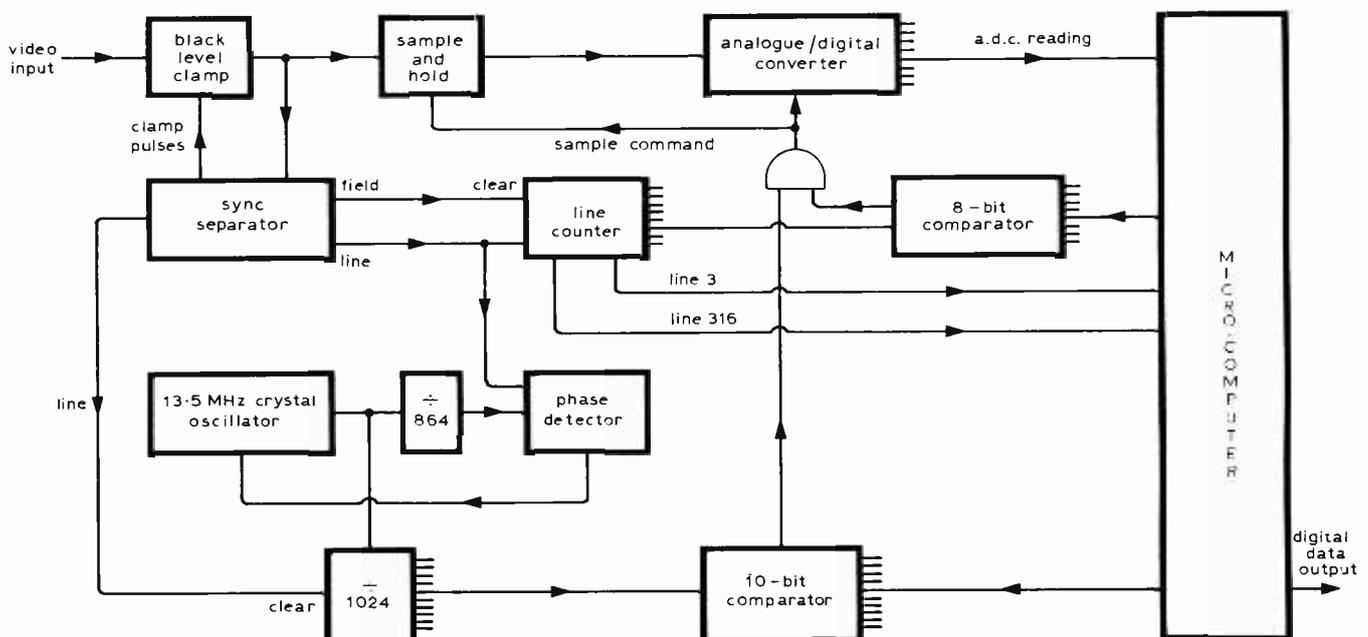


Fig. 4. Measurement, timing and processing system used at the remote site.

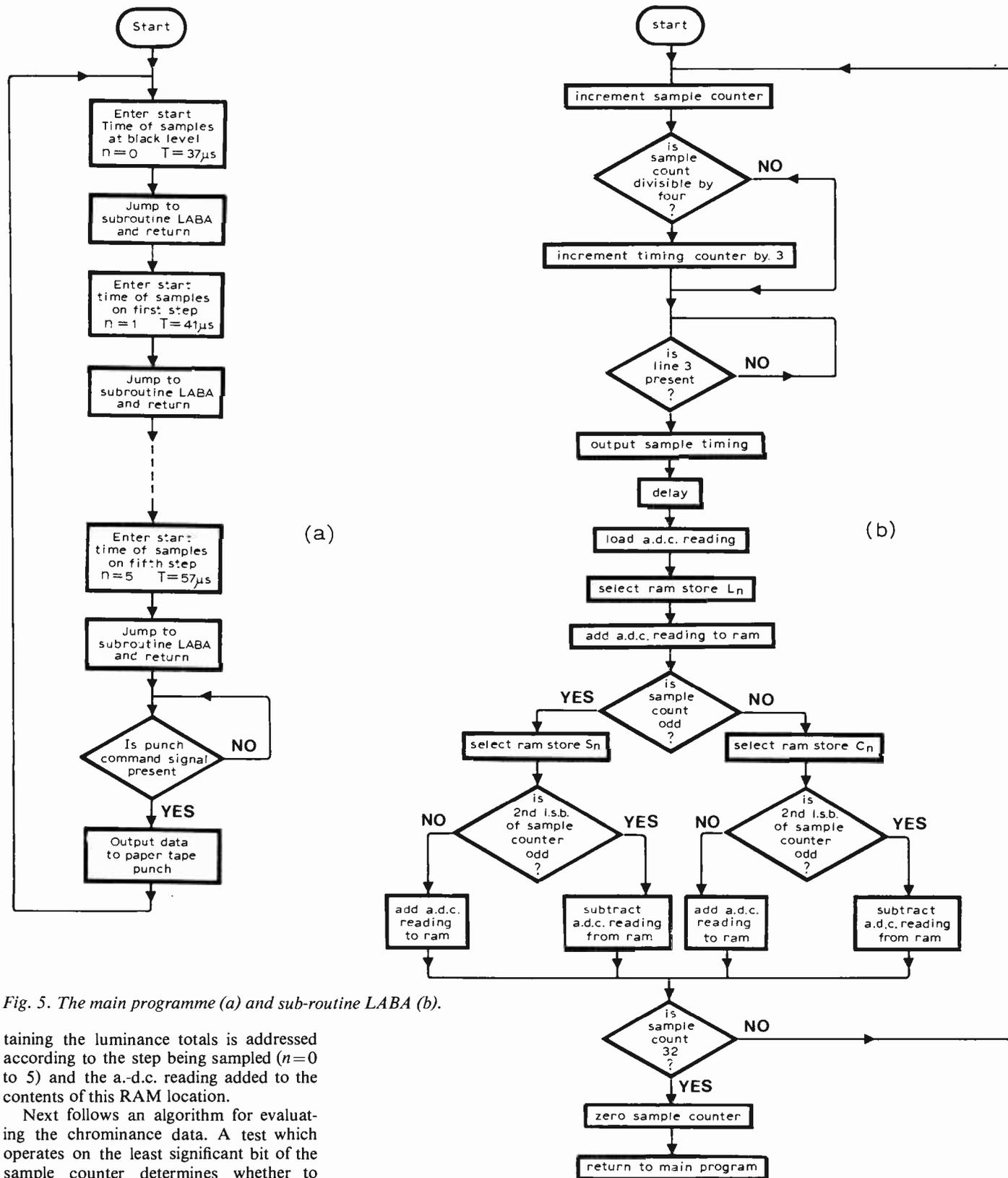


Fig. 5. The main programme (a) and sub-routine LABA (b).

taining the luminance totals is addressed according to the step being sampled ( $n=0$  to 5) and the a.-d.c. reading added to the contents of this RAM location.

Next follows an algorithm for evaluating the chrominance data. A test which operates on the least significant bit of the sample counter determines whether to address the  $S_n$  or  $C_n$  RAM location. A further test on the second least significant bit of the sample counter determines whether the a.-d.c. reading is to be added or subtracted from the RAM store addressed.

Finally a test is made to check whether the samples taken total 32. If so the main programme is rejoined after zeroing the sample counter. In the subroutine LABA there are two nested subroutines LABT and LABS, which respectively add and subtract the a.-d.c. readings from the appropriate RAM locations. These subroutines are necessary, for although the

c.p.u. possesses add and subtract machine instructions which occupy single instruction cycles, these instructions operate only on four-bit words, whereas in this application, to prevent overflow, 16-bit words are used. That 16-bit words are required may be seen by considering the contents of the luminance store when sampling the fifth staircase step. Peak white corresponds to a quantum level of about 180, giving for the total luminance content,  $32 \times 180$  or 5760, which in binary notation becomes the 13-bit word

1011010000000. The basic word length of the c.p.u. is four bits and any arithmetic operation on a 13-bit word must necessarily involve four operations in cascade giving a working word length of 16 bits.

For chrominance measurements the 140-millivolt peak-to-peak chrominance amplitude on the staircase for the UK signal corresponds to 25 quantum levels, giving possible maximum values  $S$  and  $C$  of approximately  $25 \times 32$  or 800, which in binary notation becomes the ten-bit word 1100100000. A difficulty now arises

because the values of *S* and *C* may be negative and a sign bit must be added. Further, if the higher level of subcarrier for the international test signal is taken into account, and a one-bit margin against overflow is allowed the total number of bits required for the chrominance values *S* and *C* also equals 13. The net result is that both luminance and chrominance working word lengths are 16 bits long.

The subtraction operation in the c.p.u. uses two's-complement arithmetic requiring the 16-bit *S* and *C* words to be interpreted in the following way. The 16th most significant bit (sign bit), if zero, signifies a positive number, with the remaining 15 bits regarded as a normally weighted binary number. If the sign bit is unity the number is negative, the magnitude of the number being equal to the binary complement of the remaining 15 bits plus one.

The next step in programming is to transform the flow diagram into a series of instructions using the instruction set belonging to the c.p.u. The c.p.u. here used has a set of 45 instructions, examples of which are:

- ADD —Adds two four-bit numbers with carry
- SUB —Subtracts two four-bit numbers with borrow
- INC A—Increment contents of register A
- LD X —Loads contents of register X into the accumulator

Completion of this stage of programming results in a series of machine instructions which are next translated into machine code. This translation is simple, since each member of the instruction set corresponds to a unique eight-bit machine code word. In machine code the programme consists of a sequence of eight-bit words; it is these words which are written in order into the Read Only Memory (ROM).

The task of programming the micro-computer is eased by using assembler and simulator programmes designed by the microcomputer manufacturer. With these programmes, which are accessed via computer time-sharing services, the micro-computer programmes may be checked for correct operation prior to entering them into the ROM, thereby decreasing the cost and time of programming. A product of the assembler programme is a paper-tape which contains the micro-computer programme as a sequence of machine code instructions. This tape is used in a special machine to programme the ROM automatically.

**Results**

Measurements made with the staircase programme may be taken to indicate the performance of the monitor based on this work since it involves appreciable on-site processing of the raw data and produces three quality parameters.

A single read-out from the staircase programme consists of 18 measurements made up of six sets of values *L<sub>n</sub>*, *S<sub>n</sub>*, *C<sub>n</sub>*, where *n* varies from 0 to 5. On paper tape these values are recorded as 36 words, each word having a length of eight bits.

**TABLE 2**

Col 1	2	3	4	5	6	7	8	9	
<i>n</i>	<i>L<sub>n</sub></i>	<i>S<sub>n</sub></i>	<i>C<sub>n</sub></i>	<i>R<sub>n</sub></i>	<i>A<sub>n</sub></i>	$\theta$	$\theta'$	$\theta_n$	$\theta_r$
0	1829	-8.7	-184	—	204	+25.3	0	0	0
1	2579	-176	+111	750	208	-57.8	-83.1	+84.4	+1.3
2	3330	+121	+165	751	205	+36.2	+10.9	-11.2	-0.3
3	4075	+153	-140	745	207	-47.5	-72.8	+73.2	+0.4
4	4818	-155	-139	743	208	+48.1	+22.8	-22.4	+0.4
5	5555	-124	+167	737	208	-36.6	-61.9	+62.1	+0.2

**TABLE 3**

Col 1	2	3	4	5	6	7	8	9	10	
<i>n</i>	<i>L<sub>n</sub></i>	<i>S<sub>n</sub></i>	<i>C<sub>n</sub></i>	<i>R<sub>n</sub></i>	<i>A<sub>n</sub></i>	$\theta$	$\theta'$	$\theta_n$	$\theta_r$	$\theta_r'$
0	1819	-162	+61	—	173	-69.4	0	0	0	0
1	2452	+79	+153	633	172	+27.3	+96.7	+84.4	+181.1	+1.1
2	3078	+145	-93	626	172	-57.6	+11.8	-11.2	+0.6	+0.6
3	3700	-107	-137	622	174	+38.0	+107.4	+73.2	+180.6	+0.6
4	4327	-125	+120	627	173	-46.2	+23.2	-22.4	+0.8	+0.8
5	4949	+131	+112	622	172	+49.5	+118.9	+62.1	181.0	+1.0

A typical set as read off from paper tape and converted to decimal notation is shown in Table 2. In column four of this table are evaluated the relative riser amplitudes, and in columns five and six the chrominance amplitude and phase. After normalizing to the phase at black level and correcting by  $\theta_n$  the final phase is shown in column nine.

Non-linearity is given by

$$NL = 100 \frac{(R_{MAX} - R_{MIN})}{R_{MAX}} \text{ per cent}$$

= 1.9%.

Differential gain is given by the largest in magnitude of

$$100 \frac{(A_n - A_0)}{A_0} \text{ per cent}$$

= 2.0%

Differential phase is the largest in magnitude of  $\theta_r$

= +1.3°.

To give an idea of the repeatability of the measurements, results from the same signal measured at a level of -1.5dB are given in Table 3.

These results give

NL = 1.8%

Differential gain = +0.6% or -0.6%

Differential phase = +1.1°.

In evaluating differential phase in this case, an additional correction had to be made in column ten to compensate for the 180° ambiguity in the evaluation of arctangents. This correction is not always necessary but depends on the particular point in the eight-field sequence at which the summations of *S* and *C* commence.

Tables 2 and 3 show that the maximum difference in phase at each staircase step between these two sets of measurements is 0.9°, which is typical of results obtained.

Detailed measurements to determine the accuracy of the monitor in the presence of random noise have not been made. However it is expected that the effects of random noise will be reduced in the same manner as quantum noise, and the

accuracy will not be significantly impaired for signal-to-random-noise ratios exceeding about 46dB.

**Acknowledgement**

This work was carried out whilst the author was employed by the Independent Broadcasting Authority, and the author wishes to thank the Director of Engineering of the Independent Broadcasting Authority for permission to publish this article. The author also wishes to acknowledge the important contribution made by Mr John Moore (formerly of the IBA now of Sumlock Anita Ltd) in producing the original programmes.

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# Twin voltage stabilized power supply

A simple high-quality practical design

by J. L. Linsley Hood

The classical series voltage stabilizer system using thermionic valves is shown in Fig. 1, and most transistor operated stabilized supply circuits are simple derivatives of this, of the form shown in Fig. 2. In both cases the h.t. output voltage is varied by altering the setting of  $R_1$ . Among the snags of this arrangement is the fact that the lowest output voltage at which the stabilized output can be obtained is roughly equal to the reference voltage  $V_{ref}$ .

If a stable negative reference voltage is available, the circuit can be rearranged as shown in Fig. 3, to give an output variable down to 0V. The performance of the stabilizer arrangement in this circuit has also been upgraded by including a monolithic op. amp. integrated circuit in the control loop, and a conventional "constant current" current limiting circuit has been included in the form of  $Tr_3$ . With some form of Darlington transistor arrangement as  $Tr_1$ , this type of circuit forms the basic layout of the bulk of normal stabilizer arrangements.

However, as it stands, this circuit arrangement suffers from three significant drawbacks. These are: (1) the forward bias applied to the series pass transistor,  $Tr_1$ , cannot be greater than the input-to-output voltage drop less the base-emitter potential(s) of  $Tr_1$ . Consequently, the value of  $R_1$  must be kept fairly low if adequate base bias current is to be provided for  $Tr_1$ , which lowers the loop gain and increases the quiescent dissipation in  $Tr_2$ . Also, since at higher currents there will be some ripple on the input supply voltage, the forward minimum voltage drop must in fact be larger than simple calculations would suggest if output ripple is to be avoided; (2) since the operation of the current limit circuit is to "steal" the base current from  $Tr_1$ , and this current must flow in the output circuit, this sets the lower limit at which the short-circuit output current can be set; (3) under short-circuit conditions, the portion of the stabilizer which provides the high loop gain is removed from useful participation in the operation of the circuit, and in consequence, the output current under these conditions is much less well stabilized than when the circuit

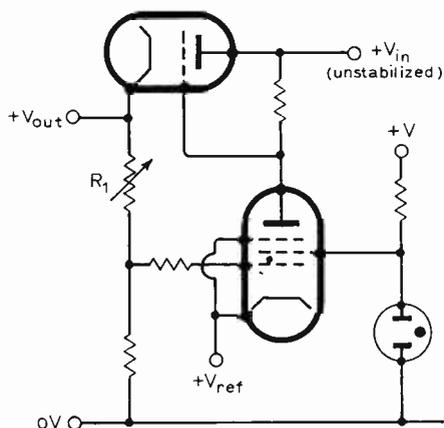


Fig. 1. Traditional "series" valve voltage stabilizer.

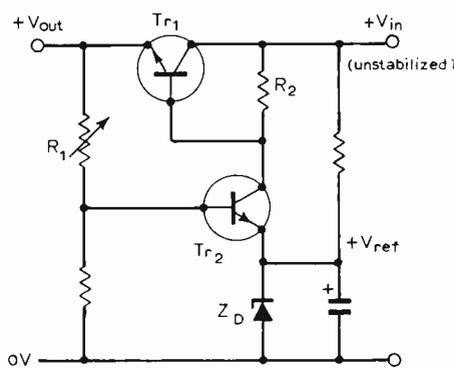
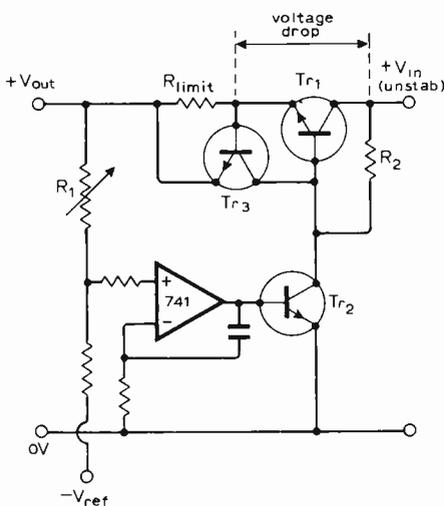


Fig. 2. Conventional transistor voltage stabilizer circuit derived from Fig. 1.



is acting as a voltage controlled arrangement.

These snags can be removed if the circuit is rearranged as shown in Fig. 4. In this the forward bias of the pass transistor  $Tr_1$  is obtained from the zero volts line, and is, in consequence, the whole of the input supply potential. Also, the amplifier transistor,  $Tr_2$ , now is required to pass current only when the load current requires it, and the static dissipation of the device is consequently much less. (The use of the pass transistor in this mode is probably due to Owen<sup>1</sup>.) As before, an operational amplifier is used to increase the

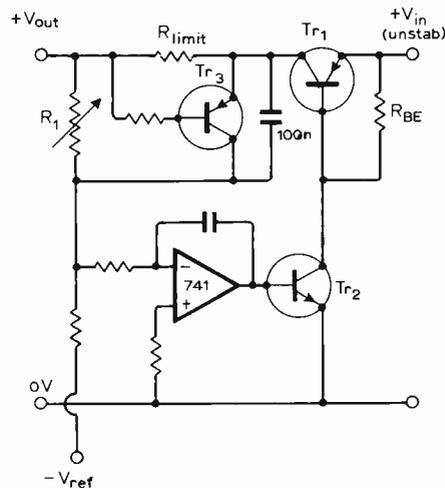


Fig. 4. Rearranged stabilizing circuit with  $Tr_3$  and op-amp inverted. The circuit of  $Tr_3$  is rearranged below to give re-entrant current limiting.

Fig. 3. Improved transistor stabilized supply with current limiting circuitry and op-amp to increase loop gain.



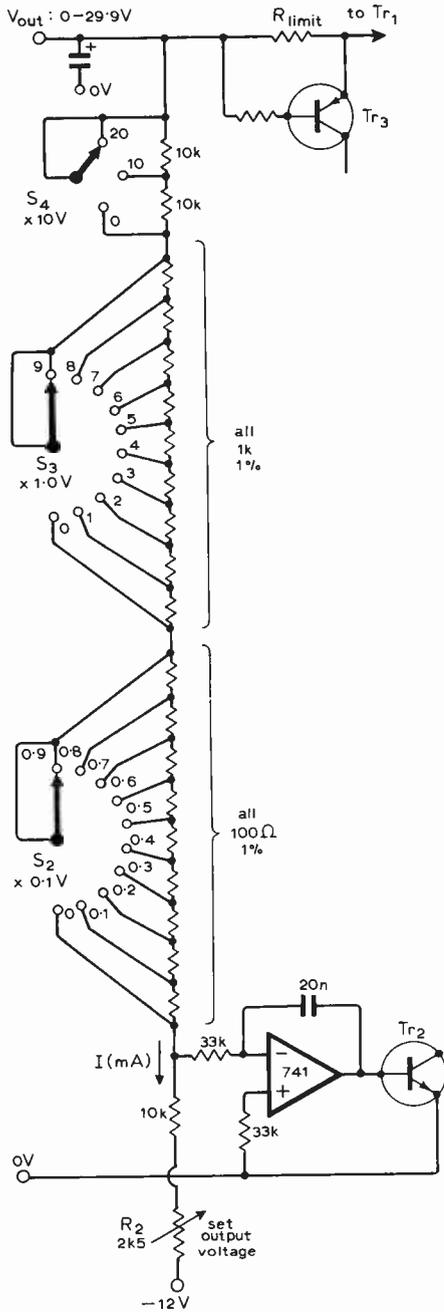


Fig. 6. Circuit configuration to give precise switched output voltages.

any h.f. noise and to assist in avoiding loop instability. Their stored energy should not be an embarrassment under short circuit conditions.

An interesting further possibility exists in the case of any supply circuit having a negative reference voltage line, and that is as shown in Fig. 6. If the current drawn from the reference supply is set to be precisely 1mA, by means of the preset  $R_2$ , the output voltage can be adjusted in 0.1-, 1-, and 10-volt increments by the switches  $S_2$ ,  $S_3$  and  $S_4$ , with the output voltage as accurately set as the precision of the resistors allows.

**Reference**

Owen, T. R. E., "Circuit Ideas" *Wireless World*, May 1971, p234.

# Teletext receivers

Engineers are now turning their minds to the design of receivers for Teletext, the unified Ceefax/Oracle system of information display now being experimentally transmitted (November issue, p.441). B. S. Barnaby of GEC and G. O. Crowther of Mullard presented a paper at the International Broadcasting Convention in London on the receiver techniques needed to take advantage of the transmissions, pointing out that the design philosophy that is eventually adopted will have been decided by economic factors, and that if it is not found possible to bring the cost of the extra circuitry down to an acceptable level then Teletext will probably not succeed. They also recognize that large-scale integration will play a vital part in this exercise, though it seems likely that even larger-scale integration, bringing the cost down further still, will have to wait until the system has been accepted before semiconductor companies will feel impelled to spend several million pounds on the development.

Two possibilities exist: an add-on unit, with a tuner, i.f. and modulator, to feed the aerial socket of a receiver; and a combined television/Teletext receiver. With the former, one is not restricted to the television channel being used; while the latter, though cheaper, is a little restrictive.

The memory part of the circuit is, perhaps, the thorniest problem, and two techniques are considered—the shift-register and RAM, both of the large-scale m.o.s. type. The shift-register is a possibility, even though there is no random access, as transmission and use of the digital information is serial in form, as is shift-register operation. The authors conclude that the RAM offers the best chance of success in both cost and

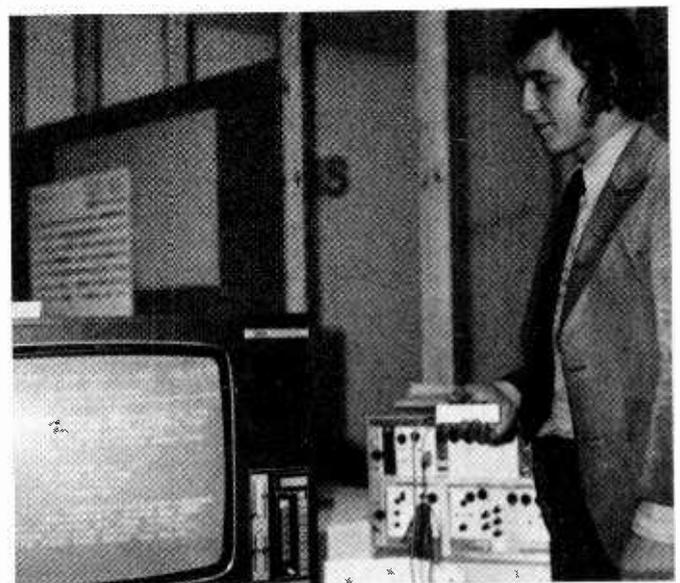
ease of access, although the standard RAM does have binary organization, which is a slight disadvantage. The dynamic type of "refreshed" memory is acceptable with the information flow presented to it.

The data acquisition part of the decoder, which consists of instructions for the display character ROM and address information, will possibly be realized in the t.t.l. family of devices, because the data clock rate—nearly 7MHz—is a little high for m.o.s. techniques. The user, incidentally, will be able to select the required page number by means of either a thumbwheel switch or a calculator-type keyboard. It seems probable that some sort of remote control device (ultrasonic?) would eventually be used.

The display section uses the coded signals to produce the video character signals and the timing. The character-memory, which produces characters in response to the transmitted instructions, is a "read-only" type (ROM), in the m.o.s. technique. Characters are on a  $7 \times 5$  matrix, and the rather restricted character-forming facilities can be improved, at no expense in bandwidth, by using raster interlace to "fill in the corners". Upper- and lower-case characters can be generated, but a lower-cost, upper-case-only ROM gives a slight cost reduction. Timing circuits are in large-scale m.o.s. modules.

The test transmissions are to last two years, and one hopes that manufacturers will have the next generation of l.s.i. circuits well considered before the end of this period, because the smaller-scale devices now available could lead to an overall decoder cost of up to £150, depending on whether "combined" receivers or add-on units are used.

*The BBC "Ceefax" information display system was publicly demonstrated for the first time on our Audio Fair stand. A Wireless World staff member, Mike Sagin, demonstrates the equipment: the decoder can be seen in the centre. This is a BBC laboratory prototype—much larger than a commercial unit will be.*



# World of Amateur Radio

## Oscar 7 up and working

The seventh amateur-radio space satellite, Oscar 7, was successfully launched into orbit on November 15, exactly 25 months after the launching of Oscar 6 which is still functioning, although to a restricted timetable. The new satellite—by far the most ambitious of the series—carries two linear repeaters: one (built in West Germany) that accepts signals on 432.125 to 432.175MHz and retransmits them on 145.975 to 145.925MHz; the other provides a similar service to Oscar 6, accepting signals in the 144MHz band and retransmitting them on 29.4 to 29.5MHz. The two transposers operate on alternate days. The anticipated 2304MHz beacon could not be carried (apparently it proved impossible for the Americans to obtain permission to use this frequency in space) but it carries beacons on 29.50, 145.98 and 435.10MHz. A feature of the new satellite is the use of circularly-polarized aerials for 144 and 432MHz. The orbit is very similar to that of Oscar 6 (sun synchronous).

## The president from Wales

When, on January 17 at Cardiff Castle, Cyril Parsons, GW8NP, formally takes over the insignia of president of the Radio Society of Great Britain he not only makes history as the first person with a "GW" (Wales) call sign to hold this office but is likely to find that, figuratively at least, the chain is not growing any lighter. For amateur radio, both in the UK and in many other parts of the world, is going through a period of uneasy change at a time when rapid inflation is undoubtedly pressing hard on many long-established societies. Although financially the RSGB has had two good years, undoubtedly costs are rising at a pace that is difficult to match with subscriptions; like many London-based societies there are persistent suggestions that a move to the provinces might reduce running costs. Again, amateur radio itself is increasingly subject to pressure to expand by making it ever easier to become an operator, yet experience has shown that where licences are easy to obtain they are valued less and tend to result in a form of Citizens Band approach to the hobby.

But in Cyril Parsons the national society will have as president someone who while clearly accepting that the hobby must be ready to change, does so from the viewpoint of one with a knowledge of experimental radio stretching back more than 50 years to the time when at the age of 14 he obtained (through a guardian as was then necessary) an "Experimental Receiving Licence" and soon progressed from a crystal receiver with loose-coupled aerial to a more sophisticated three-valve receiver using French R valves. By the end of the twenties an early interest in high-quality reproduction was reflected in constructing experimental moving-coil loudspeakers that did away with the need for an output transformer by winding 4000-ohm speech coils (centre-tapped) and with a machined steel pot wound with wire capable of taking the necessary two amps to excite the gap.

Then, after an interval in which motor-cycles and hydroplane racing played a part, Cyril Parsons came back to radio experimentation in 1934 with the call 2BPN, becoming GW8NP in February 1937. He was one of the considerable number of pre-war amateurs who joined the RAF Civilian Wireless Reserve in 1938 and was mobilised just before the outbreak of war in September 1939. He served as a Staff Signals Officer, retaining his interest in the Air Force for more than ten years after the war in the Royal Auxiliary Air Force with such units as No 3615 Fighter Control Radar, finally stepping down with the rank of Hon. Wing Commander and the Air Efficiency Award and Bar. From 1946 he was also again very active in amateur radio.

Cyril Parsons takes office at a time when there are a record number of over 20,000 licensed amateurs in the UK but with mode and band rivalries hardening and signs of differences of opinion between those with Class A and Class B licences. While by European standards the numbers here are large, there are today over 400,000 amateurs (about three-quarters of them in code-free categories) in Japan with an average age of 22 years. In the United States there are some 250,000 licensed operators (about 180,000 'active' stations) but with a growing belief that the FCC is shortly to introduce a new structure giving more facilities to code-free categories, including operating rights above 29MHz. American amateurs are still puzzled at the recent unexpected decision of FCC to waive logging requirements.

A difficult maze for the new president to find his way through.

## Commonwealth microwave record?

Murray Willis, ZL2THW, and Neil Lambert, ZL2TGC, established on August 12, 1974 a New Zealand record for 3.3GHz of 144 miles. This is 46 miles better than the current UK band record and may well be a Commonwealth record. Equipment at both ends was a CV237 feeding a 3ft dish aerial and using f.m. (transmitter power

60mW) with signals "59" both ways.

From New Zealand's *Break-in* also comes news that a 28.17 MHz beacon station (ZL2MHF) is being installed by the very active Upper Hutt branch of NZART on Mount Climie. This follows an approach some time ago by the RSGB enquiring whether a ten-metre beacon could be installed in New Zealand to help propagation studies. There are over 20 v.h.f. beacons in Region 3.

## Amateur television

The experiment of holding the 1974 British Amateur Television Club's convention at Rugby was a qualified success, with some disappointment in the attendance of about 100 members for what was a most interesting day. Among the demonstrations were those of the BATC "outside-broadcast" vehicle "Monoculus", microwave and fibre optic experimental equipment, low-definition television and slow-scan television. Bob Roberts, G6NR, continues at president with Don Reid taking over as chairman from Malcolm Sparrow.

An experimental, low-definition, mechanical television system by D. C. Hodges, G6MXY/T, uses 30 lines at the high rate of 50 pictures/second (to allow the use of standard monitors) based on a Nipkow disc running at 3000rpm.

## In brief

Almost 6,000 people attended the 1974 ARRA amateur radio exhibition at the Granby Halls, Leicester . . . The RSGB Education Committee is presenting one of the Christmas holiday lecture demonstrations at the Science Museum. This will be at 11am and 3pm on Saturday, January 4. Ticket applications to J. D. Freeborn, Lecture Service, Science Museum, South Kensington, London SW7 2DD . . . During the period May 16 to October 10 the Australian amateur VK3CZ heard on 1.8MHz a number of North and South American amateurs but the only European amateur heard was the Czech station OK1DOK (August 6) although the German commercial station DHJ (commonly used as a Top Band "DX beacon") was heard on many occasions . . . The March and District Amateur Radio Society emerged as overall winner of the 1974 VHF National Field Day. This was held under extremely bad weather conditions but nevertheless attracted 115 entries for operation on 70, 144, 432 and 1296MHz. Runners-up were Southampton RSGB Group . . . M. Hawkins of Chelmsford won the 1974 Direction Finding Contest as the first to locate three 1.8MHz hidden transmitters . . . The RSGB affiliated societies contest is being held on January 11 to 12 (a changed date) . . . Quote from Don Keith, WA4BDW: "So long as we depend on the publicly-owned frequencies for amateur radio's very existence we had better make sure the public knows who we are and what we do."

PAT HAWKER, G3VA

# New Products

## Mini oscilloscope

A miniature battery/mains-powered oscilloscope, the A1010, measures only 5.5 × 13.5 × 19cm. The y amplifier has a 10MHz bandwidth, a 10mV/division sensitivity and the pre-amp stage can be isolated for use in conjunction with the external sweep input. The input attenuator is switched to give ×1, ×10 and ×100 with a maximum input of 350V a.c./d.c. The time-base is continuously variable on each of three switched ranges from 1µs to 1s/division. Built-in batteries provide four hours' operation before recharging is necessary, which takes place automatically when the instrument is powered from external 240/110V a.c. or 12V d.c. supplies. Lawtronics Ltd, 139 High Street, Edenbridge, Kent TN8 5AX.  
**WW313 for further details**

## Sweep generator

The model 7271 linear/logarithmic sweep generator offers sine, square, triangle, pulse and ramp waveforms over the range 0.0001Hz to 20MHz. The sweep width is set by two controls—one for start

frequency and the other for stop, over a three-decade range. The internal sweep generator, having a range of sweep times from 1000s to 100ns, may be triggered manually or externally. The pulse generator has variable pulse width and repetition rate which can be set independently. Several choices of d.c. offset, for vertical positioning of the waveform, are offered as well as a voltage-controlled offset for remote control. Dana Electronics Ltd, Collingden Street, Luton, Beds.  
**WW306 for further details**

## Optical transmission system

A fibre-optic data transmission system comprising an emitter, lightguide, and receiver is capable of transmitting a 16-bit digital word or one analogue signal with a 12-bit accuracy. With an additional multiplexer, 16 analogue signals may be transmitted at the same accuracy. Plug-in p.c. cards are also available to expand the transmission capacity in steps of 32 bits up to a maximum of 320 bits. The system, which is noise immune, can operate over distances up to 100 metres. Triskelion AG, Leimatt 1, 6317-Oberwil/ZG, Switzerland.  
**WW305 for further details**

## Function generator

The latest function generator from the Heath/Schlumberger range of assembled instruments is the SG-1271. The instrument will provide sine, square, or triangle waveforms over the frequency range 0.1Hz to 1MHz. Frequency selection is by means of six variable ranges. The output delivers a 10V peak-to-peak signal into a 50 ohm load. A calibrated step attenuator adjusts from 0 to 50dB in 10dB steps with a variable attenuator providing up to 20dB attenuation in each step. Frequency accuracy for the generator is ±3% with wave-

form symmetry within 10%. Heath (Gloucester) Ltd, Bristol Road, Gloucester, GL2 6EE.

**WW302 for further details**

## Static-protection aids

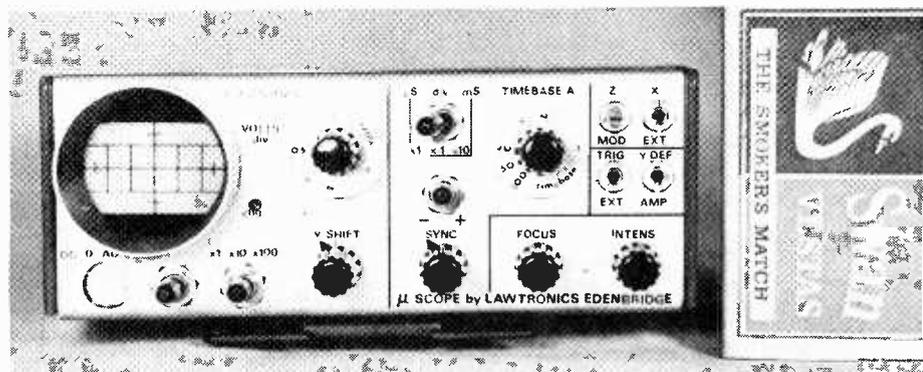
A range of materials and accessories for the handling of devices sensitive to electrostatic-discharge damage is available from Semicomps Ltd. The range, which is constructed from electrically conductive material, includes items such as aprons, wrist straps, shoes and stool covers. The material is also available in 4ft × 8ft sheet form for bench tops and foam sheets for shorting component leads. Semicomps Ltd, Northfield Industrial Estate, Beresford Avenue, Wembley, Middx.  
**WW303 for further details**

## Pushbutton potentiometer

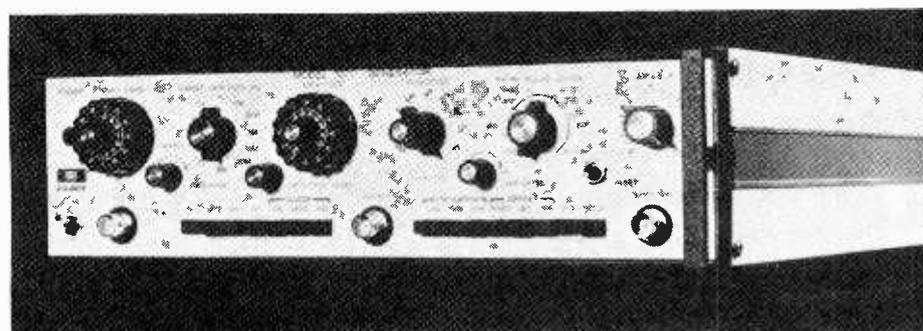
A potentiometer, known as the 3680 knobpot, combines an incremental decade resistance-element with a digital display and pushbutton section in one package. Ratings for the device are a temperature coefficient of 100 p.p.m./°C, resistance tolerance of ±1.0%, resolution of ±0.1% and a power rating of 2W. Bourns Trim-pot Ltd, Hodford House, 17/27 High Street, Hounslow, Middx.  
**WW307 for further details**

## Surge suppressor

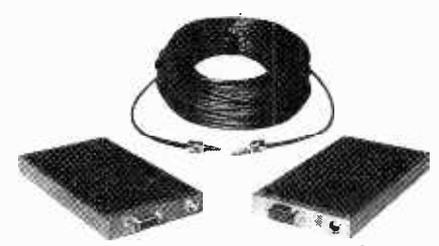
A voltage-dependent resistor has been developed by Mullard for the suppression of mains-borne transients. The resistor, type 2322 594 53912, is made from zinc-oxide and has a higher degree of non-linearity than the usual silicon-carbide-based components. Whereas the current through silicon-carbide components is proportional to the fifth power of the applied voltage, this figure becomes the



**WW313**



**WW300**



**WW305**



**WW302**

35th power for zinc-oxide types. In normal operating conditions with a 240V a.c. supply the zinc-oxide v.d.r. dissipates a few milliwatts, an increasing voltage causes a rapidly falling resistance to effectively short circuit the transient. Under surge conditions the v.d.r. can pass currents of 100A. Mullard Ltd, Mullard House, Torrington Place, London WC1E 7HD.

WW301 for further details

### Multiplying oscilloscope

In addition to a full range of facilities, the Philips PM3265 dual-trace oscilloscope possesses a multiplying mode in which signals from both amplifiers are multiplied and displayed on one trace, the other displaying one of the original signals. The multiplying bandwidth is 100MHz, which means that power products in high-speed logic circuitry can be displayed. Bandwidth of the y amplifiers is 150MHz at 5mV per cm and operating modes are A, B, chopped, alternate, added or multiplied. The horizontal deflection is by a delayed time-base, the delaying and delayed sweeps appearing apparently together, although, in fact, on alternate sweeps. Triggering, in a variety of modes, is workable with a signal up to 300MHz. A 8x10cm screen is provided, the 20kV accelerating potential making for a bright, sharp trace, which is stable with variations in beam current. Pye Unicam Ltd, York Street, Cambridge CB1 2PX. WW315 for further details

### Instrument modules

A recently introduced instrument module system from Metrowatt comprises basic frame sizes ranging from volumes of 300 c.c. up to housings of 3500 or 10,000 c.c. Most of the frames are divided into two subframes. The upper frame accepts the

display movement and offers a variety of control layouts. There is also a choice of lower frames for various battery sizes and types. Blank circuit cards are available for all frame sizes together with ancillary components such as battery connectors, jacks and safety switches. Metrowatt UK Ltd, York House, Stevenage Road, Hitchin, Herts SG4 9DY.

WW308 for further details

### Peak-reading voltmeter

The Semikron peak-reading storage voltmeter will read the maximum transient voltages on a line in any given period. The transients to be measured are selectable by filters for duration and amplitude. The instrument has six voltage ranges from 30 to 10,000V and an input impedance of 10M $\Omega$ . A minimum pulse width is selectable from 1, 10 or 100 $\mu$ s and a selectable storage time from 1 to 20s and infinity. The voltmeter is mains or battery powered with an automatic-charge circuit for the latter. An automatic reset facility is provided, so that if the meter is connected to a suitable recorder the voltmeter will give a history of supply variations. Semikron UK Ltd, Brewhouse Lane, Hertford.

WW312 for further details

### Optical tachometer

Using the Power Instruments optical tachometer it is possible to take measurements up to two feet away from a revolving mechanism. The instrument uses the principle of a collimated beam and a high-speed response phototransistor. A small piece of reflective tape is attached to the rotating component, and the instrument receives only its own light to provide a reading. The instrument is self-calibrating from any fluorescent light operating from 50 or 60Hz. Four ranges, from 0 to 30,000

r.p.m., are provided on the tachometer which has a claimed accuracy of 1 $\frac{1}{2}$ % of f.s.d. The instrument is battery powered and measures approximately 5x7 $\frac{1}{2}$ x2 $\frac{1}{2}$ in with a 24in probe cable. Electronic Brokers Ltd, 49/53 Pancras Road, London NW1.

WW300 for further details

### Moisture-proof switch

A moisture-proof switch called the E7240A, is rated at 10.1A, 186W, 115/250V a.c., and is claimed to operate immersed in water. The switch measures approximately 1x $\frac{7}{8}$ x $\frac{1}{2}$ in with 10in, 14-gauge leads. The one-off price is £0.60 from Cherry Electrical Products UK Ltd, Lattimore Road, St Albans, Herts.

WW309 for further details

### Frequency-to-voltage converter

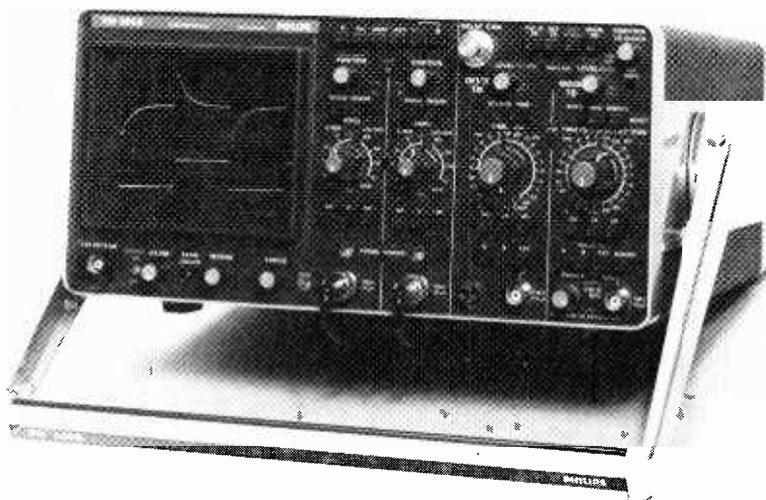
Teledyne Philbrick have introduced a 10kHz frequency-to-voltage converter. The device, which is known as the 4714, has a 1mV to 10V output directly proportional to a 1Hz to 10kHz input frequency. A non-linearity of 0.08% of f.s. in four decade ranges is claimed for the device which is priced at £19.75 one off, from Teledyne Philbrick, Heathrow House, Bath Road, Cranford, Hounslow, Middx.

WW310 for further details

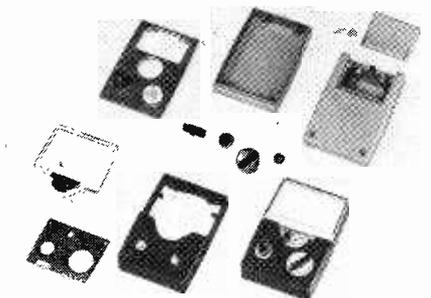
### Miniature power supply

A d.c. power supply in a d.i.l. package provides outputs of 5 or 12V at 1W. The total volume of the package, which fits into a standard i.c. socket, is 0.3 cubic in. Isolation is provided and the source is short-circuit proof with an automatic reset. TI Supply, 165 Bath Road, Slough, Bucks SL1 4AD.

WW311 for further details



WW315



WW308



WW312

## Audio fair new products

### Three-head cassette deck

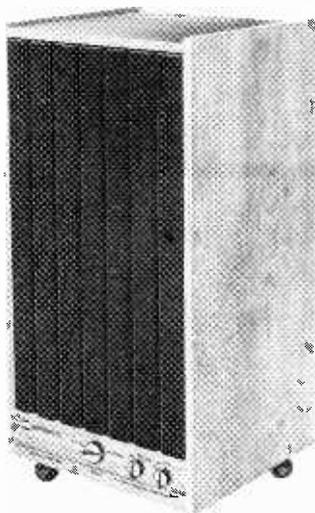
Teac showed an unexpected new model of a three-head cassette tape deck at the Audio Fair. Designated the A-850 this machine is placed upright, thus occupying only the depth of a shelf. Three d.c. motors provide forward drive and fast wind functions via logic-controlled solenoid operation. In common with Sony and Nakamichi, dual capstans are used to improve control of the tape across the heads. Dolby noise reduction is included and calibration controls and a built-in test oscillator provide the flexibility to get the best out of all tapes. Separate three-position bias and equalization switches, a peak-reading facility for the VU meters and full microphone/line mixing are included among the facilities. Price will be about £400. Acoustico Enterprises Ltd, Unit 7, Space Way, North Feltham Trading Estate, Feltham, Middlesex TW14 0TZ.

WW327 for further details

### Omni loudspeaker

The Omni TL6 "monitor" loudspeaker is designed to leave the listener with many options as to the kind of loudspeaker used. Using five drive units, with mid-range and h.f. units in both the front and rear, it is possible to operate in the forward-radiating mode or in the "omnidirectional" mode by adjustment of the level controls.

In the bass region there is a choice of mode brought about by mechanically



WW320

operated flaps which alter the loading of the bass unit, from a quarter-wave design to either a distributed port or damped labyrinth.

Crossover frequencies are 400Hz and 5kHz using 12 and 18dB/octave slopes. Mid- and high-frequency unit controls are switched with constant-resistance and Zobel impedance correction networks. Sensitivity in the direct mode, all controls set level, is quoted as 80dB/watt. Distortion is claimed to be less than 1% above 65Hz for 90dB s.p.l. (at 1kHz). Maximum amplifier rating should be 20 watts (into 8Ω) and maximum power handling figure is 50 watts. Ambionic Sound Reproducers Ltd, Omal House, North Circular Road, London NW10 7UF.

WW320 for further details

### Belt-drive turntable

With much of the emphasis on direct-drive turntables at the top end of the market, it is unusual to see a competitive new belt-drive turntable. Sansui showed such a product, the SR-313, and claim that it can out-perform many types of direct-drive units. Complete with tone-arm, the SC-38 induced magnet cartridge, plinth and cover, the unit offers the following manufacturer's specification. Signal-to-noise ratios: >50dB, frequency response: 20Hz-20kHz, ±3dB, wow and flutter: <0.06% w.r.m.s. Approximate price is £142.86 plus v.a.t. Vernitron Ltd, Thornhill, Southampton.

WW323 for further details



WW327

### Professional CD-4 demodulator

A new high-performance CD-4 demodulator for professional use was demonstrated by JVC. Designated CD4-1000, it features lower distortion and improved signal-to-noise than the consumer model. The carrier-channel circuitry has been improved by use of a "crosstalk-cancelling" circuit; the a.n.r.s. circuit has been upgraded to the standard of the recording circuit. Two switched filters are included—one giving a 3dB loss at 18Hz, the other giving a 6dB loss at 10kHz, with a slope of 6dB/octave. Harmonic distortion quoted for the baseband channels is 0.03% (1kHz). No distortion figures are issued for the carrier channels. Baseband amplitude frequency response can extend to 20kHz (-3dB). Victor Company of Japan Ltd, 1, 4-chome, Nihonbashi-Honcho, Chuo-ku, Tokyo 103.

WW324 for further details

### Dolby cartridge recorder

The 3M Company made quite a showing with a new range of equipment selected from the American Wollensak range. The first is an eight-track cartridge recorder, designated the Wollensak 8075 and is unique in as much as it is the first Dolby cartridge machine to be marketed in the UK.

In addition, a cassette deck based on the well-known Wollensak mechanism was shown, the model 4766. Again, this machine has Dolby noise reduction, plus a claimed wow and flutter of 0.07% w.r.m.s., twin VU meters and peak overload indicators. 3M United Kingdom Ltd, 3M House, Wigmore Street, London W1A 1ET.

WW321 for further details (8075)

WW322 for further details (4766)



WW323

## Mini loudspeaker

An interesting design produced by Technics is the SB30 loudspeaker system. This consists of one full-range 9cm loudspeaker mounted in a closed cabinet measuring only 10.3 × 18.1 × 12.7cm. Maximum input power to the nominal 8Ω unit is 20W and 1W will produce 86dB at a distance of 1m on axis. The weight of each speaker is 1.5kg and the claimed frequency range is 50Hz to 20kHz, no limits being specified, however. Price is £15 each plus v.a.t. National Panasonic (UK) Ltd, 107-109 Whitby Road, Slough, Berks, SL1 3DR. WW328 for further details

## New valve amplifiers

One of the most surprising new products at Olympia was the Lux MQ-80 valve stereo power amplifier from Lux (perhaps not so surprising on reflection). A twin triode tube 6336A is used per channel at the output stage in a push-pull circuit. The output transformer in each output has bifilar windings to ensure maximum coupling with no leakage inductance. The transformer design also permits a claimed frequency response extending up to 200kHz. Main specifications are: Power output: 40W (8Ω, each channel, both driven); t.h.d.: below 0.5%; frequency response: 10Hz to 60kHz (-1dB); damping factor: 15 (8Ω load); residual noise: below 0.5mW. Price £398 plus v.a.t.

Associated with this power amplifier is the Lux 35/II valve pre-amplifier (£298 + v.a.t.). Howland West Ltd, 3-5 Eden Grove, London N7 8EQ.

(Howland West state that they do not keep these models as stock items but will order on request.)

WW329 for further details

## Calibration cartridge

Wilmex, distributors of Stanton cartridges, showed the model 681 EEE which is claimed to represent a "state of the art" standard in magnetic cartridges. The stylus tip is a low mass (two-thirds the mass of its predecessor) nude diamond, 0.2 × 0.7 mil elliptical type. Frequency response: 10Hz-12kHz, ±0.5dB, overall, 10Hz-22kHz. Nominal output for 5cm/s recorded velocity: 3.5mV ± 2dB, channel separation: 35dB, tracking force: 0.75-1.5g, total cartridge mass: 5.5g. Wilmex Ltd, Import Division, Compton House, New Malden, Surrey KT3 4DE. WW326 for further details

## New Brahms speaker systems

An enclosure added to the Brahms range of loudspeakers is the SAL 3000, a design which incorporates an 8in bass unit with an aluminium voice coil and rubber-roll suspension. It has a one-inch dome high-frequency unit mounted in a cabinet which measures 48 × 27 × 25cm. Power handling is rated at 30W and nominal impedance is 4-8Ω. Each cabinet weighs 9.5kg and teak or walnut is the

choice of cabinet finishes. The manufacturers claim a good stereo image and a flat response to 22kHz. Price is £29.50 each plus v.a.t.

The new Windsor loudspeaker system also has two units but the bass unit is a 10in neoprene doped cone mounted in a larger cabinet measuring 61 × 33 × 28cm. Finishes are also similar and the price £34 each plus v.a.t. Brahms also had a new range of German loudspeakers manufactured by Schilling on view at Olympia, which is due for release during January. These are similar in operating principle to the Sonab surround sound loudspeakers and the range consists of four models which range in price from £31.93 to £95.81 plus v.a.t. Brahms Manufacturing and Development Co, Unit E, Rochester Airport, Maidstone Road, Rochester, Kent ME1 3QJ. WW325 for further details

# Solid State Devices

The names of suppliers of devices in this section are given in abbreviation after each entry and in full at the end of the section.

## Switching power-transistors

Three new series of switching transistors from Sescosem are constructed using the triple-diffused technology and have ratings for  $V_{CEO (rms)}$  from 90 to 500V at maximum collector currents from 15A to 30A.

WW350 for further details Sescosem

## Quad opto-isolator

The 1LQ74 is a quad opto-isolator in a 16-pin d.i.l. package. Each channel has a typical isolation resistance of 100MΩ and a minimum breakdown voltage of 1500V. The coupler costs £2.87 for one-off and £1.65 for 1,000-off quantities.

WW351 for further details Jermyn

## 80V op-amp

An op-amp designated the HA2-2645-5 is capable of operating from ±40V power rails. The device, which incorporates an output current limiter, will deliver an output swing of up to ±35V at ±10mA with a bandwidth of 4MHz. Offset voltage is typically 2mV and offset voltage drift is typically 15μV/°C. The op-amp costs £2.65 in 100+ quantities.

WW352 for further details Memec

## Step-recovery diodes

The 5082-0800 series of step-recovery diodes has been designed for use in high- and low-order harmonic generators. The

diodes have typical outputs of 0.3W from 10 to 20GHz and 6W from 3 to 5GHz. Junction capacitance for the two ranges is 0.1pF minimum and 3.5pF maximum respectively. Transition times range from 50ps to 250ps.

WW353 for further details Hewlett Packard

## Buffer register

The AMI S1709 buffer register contains 13 parallel-in/parallel-out shift registers plus the control logic necessary to achieve a first-in/first-out memory configuration. External control signals allow cascading of several register arrays and the device may operate with independent input and output data rates. The S1709 is supplied in a 24-pin d.i.l. package and costs £8.69 for 100+ quantities.

WW354 for further details GDS

## Liquid-crystal driver

A b.c.d.-to-seven segment latch/decoder/driver called the MC14543 is designed for use with liquid-crystal readouts. The device is constructed using c.m.o.s. and offers direct l.e.d. driving capability, latch storage of code and readout blanking on all unpermitted combinations.

WW355 for further details Lock

## Suppliers

Hewlett-Packard Ltd, 224 Bath Road, Slough, Berks SL1 4DS.

GDS (Sales) Ltd, Michaelmas House, Salt Hill, Bath Road, Slough, Berks.

Lock Distribution, Neville Street, Middleton Road, Oldham, Lancs OL9 6LF.

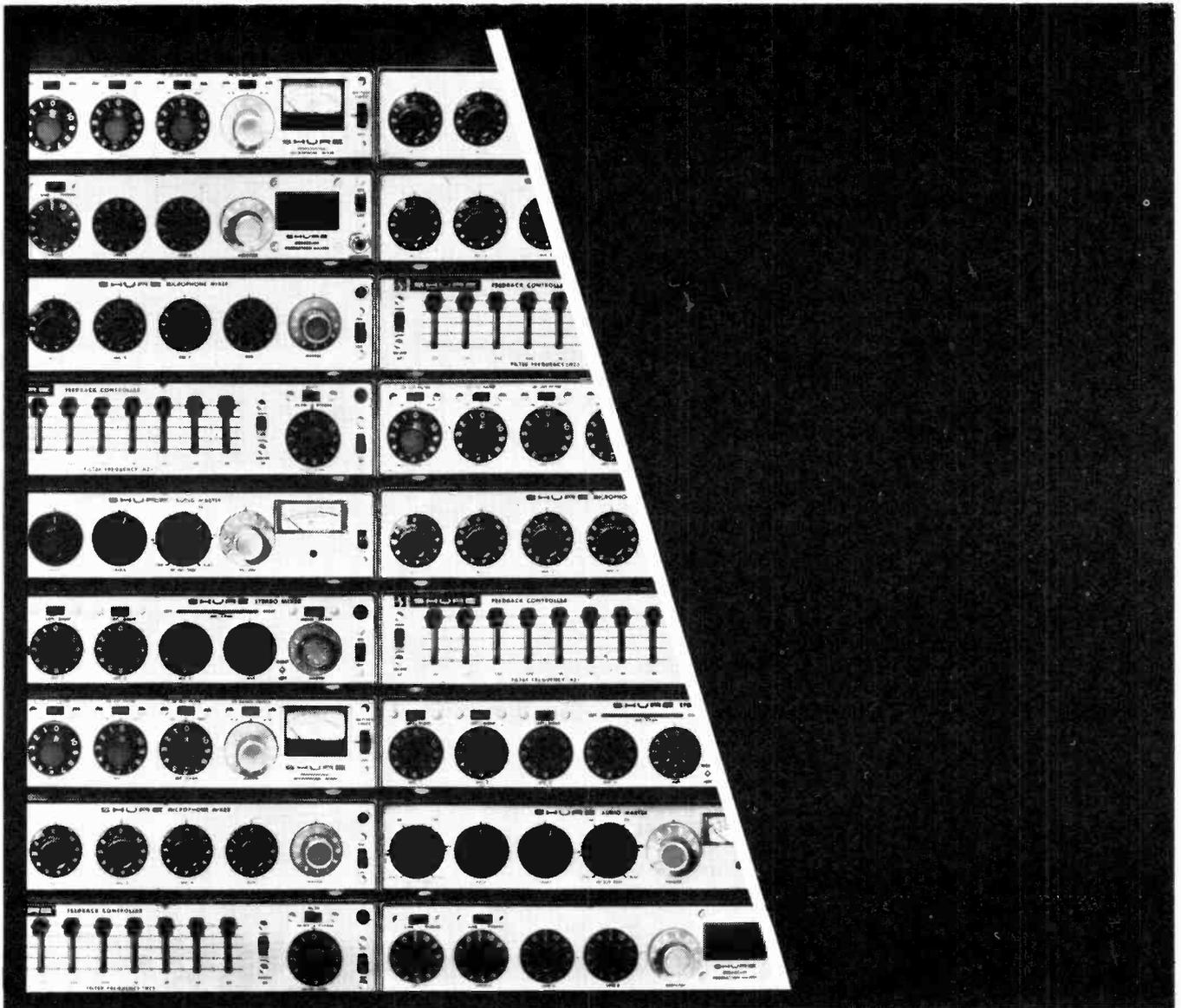
Memec Ltd, The Firs, Whitchurch, Aylesbury, Bucks.

Jermyn Distribution, Sevenoaks, Kent.

Sescosem, 50 rue Jean Pierre, Timbaud, BP120, 92403 Coubevoise, France.

## Semiconductor service

Amateur constructors and servicing technicians can now obtain small quantities of semiconductor devices at manufacturers' list prices from the distributor Semicomps through a new service started by its subsidiary SCS Components. The range available includes all discrete and integrated semiconductors from Mullard, Motorola, Signetics, General Instrument (Microelectronics), G.I. (UK), Ferranti, RCA, Monsanto, and Mostek. Data sheets are free on request. Passive components from Mullard, Seatronics and Centralab will be added to the range later. A catalogue is available free. SCS Components is at 5c Northfield Industrial Estate, Beresford Avenue, Wembley, Middlesex, HA0 1SD, telephone 01-903 3168.



# It's a mod. mod. modular world.



The fact is that all too few music lovers realise that while certain high fidelity components can be less than best, there is one component that cannot endure a sacrifice in quality: the cartridge. Because the hi-fi cartridge functions as the *source of sound* (the point at which the recording is linked with the balance of the hi-fi system), its role is absolutely critical. Just as the camera can be no better than its lens, the finest hi-fi system in the world cannot compensate for an inferior cartridge. Suggestion: For a startling insight into the role of the cartridge in the overall hi-fi system, and a breathtaking re-creation of your favourite recording, see your nearby Shure cartridge dealer. He'll introduce you to the Shure cartridge that is correct for your system and your exchequer. Or, next best, send for our brochure:

Shure Electronics Limited  
 Ecclestone Road, Maidstone ME15 6AU  
 Telephone: Maidstone (0622) 59881

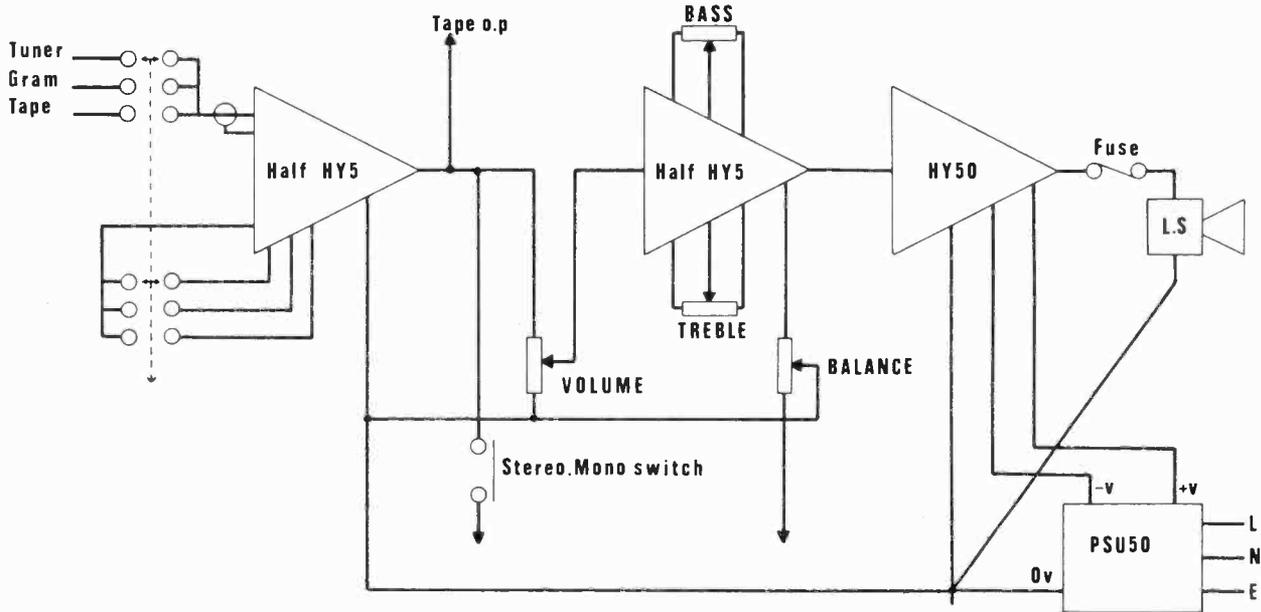


WW-095 FOR FURTHER DETAILS

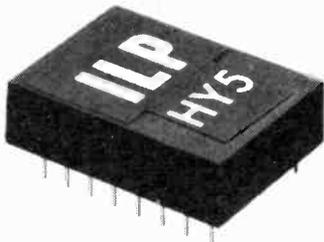


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# SHEER SIMPLICITY!



*Mono electrical circuit diagram with interconnections for stereo shown*



The HY5 is a complete mono hybrid preamplifier, ideally suited for both mono and stereo applications. Internally the device consists of two high quality amplifiers—the first contains frequency equalisation and gain correction, while the second caters for tone control and balance.

**TECHNICAL SPECIFICATION**

**Inputs**

- Magnetic Pick-up 3mV, RIAA
- Ceramic Pick-up 30mV
- Microphone 10mV
- Tuner 100mV
- Auxiliary 3-100mV
- Input impedance 47kΩ at 1kHz.

**Outputs**

- Tape 100mV
- Main output 0db (0.775 volts RMS)

**Active Tone Controls**

- Treble ±12db at 10kHz
- Bass ±12db at 100Hz

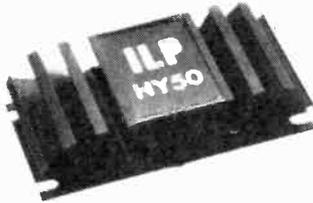
**Distortion**

- 0.05% at 1kHz
- Signal/Noise Ratio 68db
- Overload Capability 40db on most sensitive input

**Supply Voltage**

- ±16-25 volts.

PRICE £4.50 + 0.36 V.A.T. P & P free.



The HY50 is a complete solid state hybrid Hi-Fi amplifier incorporating its own high conductivity heatsink hermetically sealed in black epoxy resin. Only five connections are provided: Input, output, power lines and earth.

**TECHNICAL SPECIFICATION**

- Output Power 25 watts RMS into 8Ω
- Load Impedance 4-16Ω

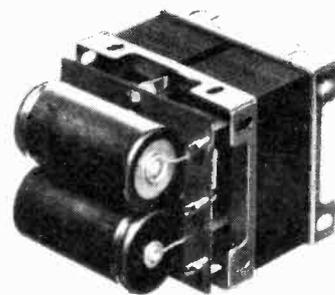
- Input Sensitivity 0db (0.775 volts RMS)
- Input Impedance 47kΩ

- Distortion Less than 0.1% at 25 watts typically 0.05%

- Signal/Noise Ratio Better than 75db
- Frequency Response 10Hz-50kHz ±3db

- Supply Voltage ±25 volts
- Size 105 x 50 x 25 mm.

PRICE £5.98 + 0.48 V.A.T. P & P free.



The PSU50 can be used for either mono or stereo systems.

**TECHNICAL SPECIFICATIONS**

- Output voltage 25 volts
- Input voltage 210-240 volts
- Size L. 70, D. 90, H. 60 mm.

PRICE £5.00 + 0.40 V.A.T. P & P free.

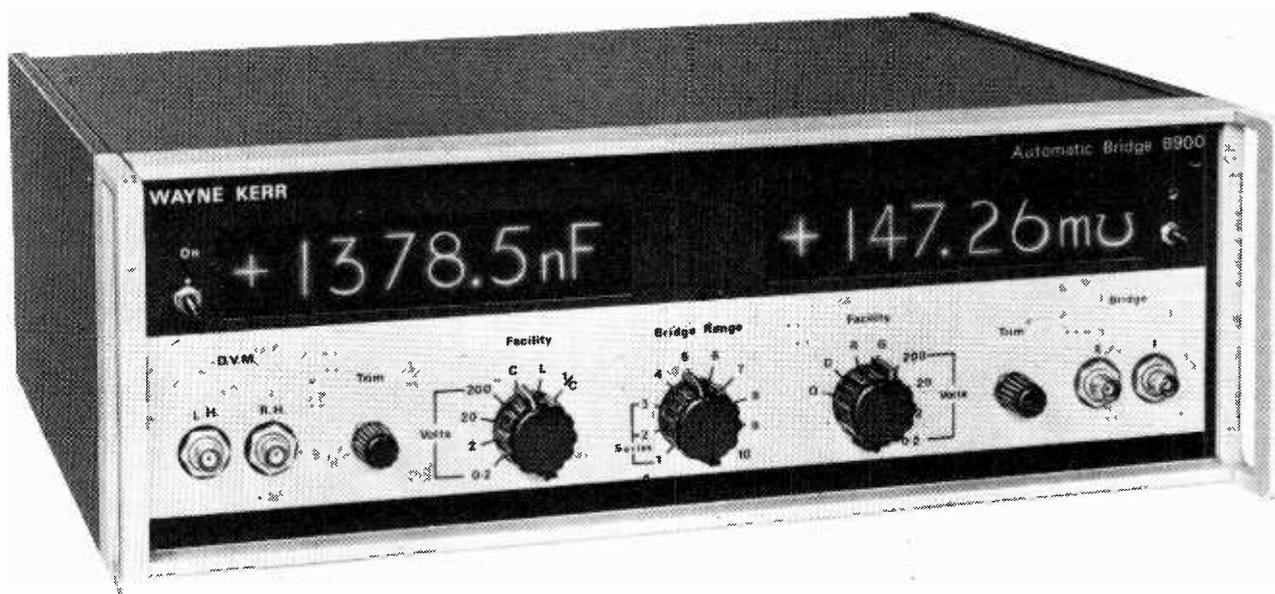
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WW-086 FOR FURTHER DETAILS

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For the attention of Mr. \_\_\_\_\_

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WW—Jan

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**WAYNE KERR**  
 A member of the Wilmot Breedon group.

WW—129 FOR FURTHER DETAILS

TTL 74 SERIES INTEGRATED CIRCUITS table with columns for part number, price, and description.

LINEAR ICs table listing various integrated circuits like CA3046, LM301, etc.

SIGNAL DIODES, RECTIFIER DIODES, ZENER DIODES table listing diode types and prices.

SPECIAL OFFERS FOR POPULAR TRANSISTORS table listing transistor models and prices.

BRIDGE RECTIFIERS table listing diode bridge components.

SCR-THYRISTORS table listing thyristor components.

OPTO-ELECTRONICS table listing light-dependent components.

TGS GAS SENSOR table listing gas sensor components.

Table listing various electronic components and their prices.

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TRANSISTORS table listing various transistor models and prices.

DIODES table listing various diode models and prices.

THYRISTORS, TRIACS AND TRIACS WITH TRIGGER table listing thyristor and triac components.

Table listing various electronic components and their prices.

Notes: All prices are in pence per unit. First price in each group is thyristor, second is triac, third is triac with trigger.

INTEGRATED CIRCUITS table listing various IC models and prices.

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3.3 63	6p	100 4	6p
4.7 63	6p	100 10	6p
6.8 40	6p	100 25	6p
6.8 63	6p	100 40	6p
10 25	6p	100 63	15p
10 63	6p	150 6.3	6p
15 18	6p	150 15	6p
15 40	6p	150 25	6p
15 63	6p	150 40	14p
22 10	6p	150 63	16p
22 25	6p	220 4	6p
22 63	6p	220 10	6p
33 6.3	6p	220 15	6p
33 18	6p	220 25	14p
33 40	6p	220 40	16p
33 63	6p	220 63	15p
47 4	6p	220 63 25p	15p
47 10	6p	330 4	6p
47 25	6p	330 10	6p
47 40	6p	330 15	14p
47 63	6p	330 63	28p
47 63	6p	330 63 28p	4700 4 28p

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BC108	10p	OA200	7p
BC109	13p	OC71	20p
BC109C	15p	SC146D	88p
BC142	23p	T1S43	28p
BC143	26p	WD05	30p
BC147	10p	WD4	33p
BC148	10p	1N914	4p
BC149	12p	1N4001	6p
BC168C	12p	1N4002	6p
BC169C	12p	1N4003	7p
BC178	17p	1N4004	7p
BC182L	10p	1N4005	8p
BC183L	12p	1N4006	8p
BC184L	12p	1N4007	9p
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Plastic-topped plug	5p
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Chassis socket single	4p
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P360 3-pin 1.5A chassis plug with line socket	30p
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### TRANSFORMERS

LT700 min. output. Pri. 1k2; Sec. 50 200mA	50p
Sub-min mains 6-0-6V 100mA	95p
12-0-12V 50mA (Size both approx. 30X27X25mm)	95p
Min. mains 0-6V 500mA, 0-6V 500mA	£1.36
0-12V 250mA, 0-12V 250mA	£1.36
0-20V 150mA, 0-20V 150mA	£1.36
0-24V 125mA, 0-24V 125mA	£1.36
Mains MT3AT; Sec. 12-15-20-24-30V 2A	£3.60
Mains MT206AT; Sec. 0-15-20V 1A, 0-15-20V 1A	£3.98

### ORGAN CONSTRUCTION

A Full-Scale Electronic Organ that you can build to your own specification.

#### FULL CONSTRUCTIONAL DETAILS IN OUR LEAFLETS

Leaflet MES 51: price 15p, describes a fully polyphonic basic organ which can later be used as the basis of a large sophisticated instrument.  
 Leaflet MES 52: price 5p, continues the description of the MES 50 series organs and shows you how to add a second keyboard with lots more stops.  
 Further leaflets to follow at approx. two-monthly intervals.



### THE AMAZING DMO2

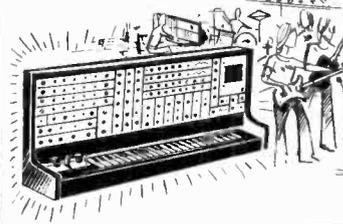
A ready-built, tested and guaranteed digital master oscillator. Accurately generates the top 13 notes for your organ system and reduces the complete tuning of your organ to ONE SIMPLE adjustment. New design gives selectable C to C output ranges of (approx.) 4k to 8k (highest) or 2k to 4k or 1k to 2k, etc., right down to 16Hz to 32Hz! And this new compatible design is even smaller; only 3.5in. X 3.7in., including gold-plated edge connexion.  
 DMO2 includes: built-in variable depth and rate frequency shift tremulant.  
 DMO2 £12.25 DMO2T £14.25  
 SAJ 110: 7-stage frequency divider in 14-pin DIL package. Sine or square wave input. Square wave output may be converted to saw-tooth. £2.63 each or 6 for £14.14 or 12 for £25.

### ORGAN COMPONENTS

Keyboards high quality, fully sprung.  
 Flat-front 48-note F to E £15.88  
 Sloping-front 49-note C to C £15.88  
 Sloping-front 61-note C to C £20.35  
 Swell pedal with 10k log. pot £3.95  
 \*Spring line unit (short) £7.59  
 \*Spring line unit (long) £7.59  
 \*Reverberation driver module £5.34  
 \*S.a.e. please, for full details: leaflet MES 24.  
 Gold-clad phosphor-bronze wire 30p per yd.  
 Palladium earth bar 15p per octave length  
 Contact blocks 2-make (GB2) 22p  
 Stop tabs, rocker type, not engraved (white, red, grey or black) with DPDT switch 49p

### "ELECTRONIC TODAY INTERNATIONAL" 4600 SYNTHESISER

We stock all parts for this brilliantly designed synthesiser. This includes all the PCBs, metal-work and drilled and printed front panel giving a truly professional finish. Authoritative opinions agree the ETI International Synthesiser is technically superior to most of today's models. Complete constructional details in our booklet, available shortly. S.a.e. please, for price lists and specification.  
 We also stock all parts for the P.E. Synthesiser and Minisonic.



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## TRANSFORMERS

### CASED TRANSFORMERS

Housed in smart resin-coated steel cases, with 3-core power cable and outlet socket, fused primary winding. Isolation types are fitted with 3-pin outlet sockets, and are available with 110 volt or 240 volt output (Please state). Auto types are fitted with 2-pin flat style sockets up to 500 VA, 3-pin sockets from 750 to 3000 VA. See Auto and Isolation sections for prices.



### SAFETY ISOLATING

Prim. 120/240V. Sec. 120/240V. Centre Tap with screen

VA (WATTS)	REF No.	Cased	Open	Price	Post
60	149	7.35	0.80	4.00	0.38
100	150	8.22	0.80	4.60	0.52
200	151	10.20	0.80	7.40	0.52
250	152	11.68	0.80	8.88	0.85
350	153	14.10	0.80	10.80	0.80
500	154	15.80	0.80	12.38	1.00
750	155	26.83	1.00	18.72	1.20
1000	156	32.19	1.00	26.50	1.20
1500	157	38.18	1.00	30.34	O.A.
2000	158	45.20	2.40	34.68	O.A.
3000	159	66.50	2.40	53.35	O.A.

### MINIATURE & EQUIPMENT

VOLTS		MILLIAMPS		TYPE	PRICE	Post
Sec. 1	Sec. 2	Sec. 1	Sec. 2	No.	£	£
0-3	0-6	200	—	238	1.23	0.10
0-6	0-6	500	500	234	1.30	0.10
0-6	0-6	1000	1000	212	1.95	0.22
0-9-9	—	100	—	13	1.23	0.10
0-9	0-9	330	330	235	1.43	0.10
0-8-9	0-8-9	500	500	207	1.75	0.22
0-8-9	0-8-9	1000	1000	208	2.30	0.30
0-15-15	—	40	—	240	1.23	0.10
0-15	0-15	200	200	236	1.30	0.10
0-20-20	—	30	—	241	1.23	0.10
0-20	0-20	150	150	237	1.30	0.10
0-15-20	0-15-20	500	500	205	2.47	0.38
0-20	0-20	300	300	214	1.72	0.22
0-20	—	3500	No Screen	1116	3.00	0.40
20-12-20	—	700	—	221	2.31	0.30
0-15-20	0-15-20	1000	1000	206	3.22	0.38
0-15-27	0-15-27	500	500	203	2.73	0.38
0-15-27	0-15-27	1000	1000	204	3.52	0.38

### 12 and 24 VOLTS PRIMARY 200-240 Volts.

VA	AMPS	TYPE	PRICE	Post
12V	24V	No.	£	£
0.3	0.15	242	1.34	0.22
0.5	0.25	111	1.38	0.22
1	0.5	213	1.58	0.22
2	1	71	2.22	0.22
4	2	18	2.58	0.38
6	3	70	3.80	0.42
8	4	108	4.20	0.52
10	5	72	4.80	0.52
12	6	115	5.01	0.52
15	8	17	6.22	0.52
20	10	115	9.47	0.69
30	15	187	11.95	0.97
40	20	232	13.26	1.00
60	30	226	15.30	1.10

### 30 VOLTS

PRIMARY 200/240V	SECONDARY 12, 15, 20, 24, 30V.	Ref.	Price	Post
AMPS		No.	£	£
0.5	112	1-72	0.22	
1	79	2-21	0.38	
2	3	3-26	0.38	
3	20	4-10	0.42	
4	21	4-68	0.52	
5	51	5-80	0.52	
6	117	6-50	0.52	
8	88	8-50	0.67	
0	89	8-47	0.67	

### 60 VOLTS

PRIMARY 200/240V	SECONDARY 24, 30, 48, 60V.	Ref.	Price	Post
AMPS		No.	£	£
0.5	102	2-33	0.30	
1	103	3-00	0.38	
2	104	4-57	0.42	
3	105	5-20	0.52	
4	106	6-89	0.52	
6	107	11-17	0.67	
8	118	14-19	0.97	
10	119	15-47	0.97	

### 50 VOLTS

PRIMARY 200/240V	SECONDARY 19, 25, 33, 40, 50V.	Ref.	Price	Post
AMPS		No.	£	£
0.5	124	2-08	0.38	
1	126	2-96	0.38	
2	127	4-63	0.42	
3	125	6-84	0.52	
4	123	7-94	0.67	
5	40	8-85	0.67	
6	120	10-15	0.82	
8	121	13-58	1.00	
10	122	18-15	1.00	
12	189	16-00	1-10	

### AUTO TRANSFORMERS

VA (Watts)	Ref. No.	PRICE Cased	PRICE Plugs 2 & 3 pin	PRICE Open	Post
Tapped at 115, 220, 240 Volts					
20	113	3.00	0.15	1.55	0.30
50	150	4	0.15	3.98	0.39
150	200	65	0.15	4.50	0.40
300	300	66	0.15	5.28	0.52
500	500	67	0.15	8.29	0.67
750	750	83	0.15	12.56	0.82
1000	1000	84	0.15	15.70	0.82
1500	1500	93	0.15	19.88	1.50
2000	2000	95	0.15	30.10	1.44
3000	3000	73	0.15	43.58	1.90

### BATTERY CHARGER TRANSFORMERS

	Price	Post
	£	£
2 Amp 2-6-12 Volts	2.45	.35
4 Amp 2-6-12 Volts	3.29	.35
6 Amp 6-12 Volts	4.95	.50
12.5 Amp 2-6-12 Volts	7.80	.68

RECTIFIERS NOT INCLUDED

**NEW PRODUCTS!**  
Available shortly  
*Don't chance it!*  
*isolate it!*

**"SPASH PROOF" SAFETY TRANSFORMER**  
750 VA Isolation Unit (Interwinding Screen)  
Housed in a tough Fibreglass case, with carrying handle. Complete with heavy duty 3-core power cable, splash proof outlet plug and socket, internal fuse, 110 Volt and 240 Volt version available.  
**PRICE £26.20**  
**CARRIAGE £1.30**

### BRIDGE RECTIFIERS



ONE AMP	Price	TWO AMP	Price
50 P.I.V.	0.25	50 P.I.V.	0.35
100 P.I.V.	0.25	100 P.I.V.	0.40
200 P.I.V.	0.28	200 P.I.V.	0.45
400 P.I.V.	0.30	400 P.I.V.	0.50
<b>FOUR AMP</b>		<b>SIX AMP</b>	
100 P.I.V.	0.55	50 P.I.V.	0.65
200 P.I.V.	0.59	100 P.I.V.	0.70
400 P.I.V.	0.65	200 P.I.V.	0.80
600 P.I.V.	0.75	400 P.I.V.	0.90

### 1/4 WATT CARBON FILM RESISTORS

1/4 watt at 70°C E 12 range 100-1MΩ. ±% tol. above 470 KΩ 10% tol. at 95p per 100.

### POWER UNIT TYPE A125

Supplying 6 or 9 Volt DC at 200 mA.  
In moulded case forming a 2 pin 5 A mains plug.  
2 metre output lead with 4-way multiplex giving 2.1 and 2.5 mm sockets and 3.5 mm plugs.  
Price £2.25. Post 10p.

### POWER UNIT Type CC12-05

Output switched 3, 4.5, 6, 7.5, 9 and 12 Volts at 500 mA D.C. Operates from 240 V mains suitable for Radios, Tape Recorders, Record Players etc.  
Size: 7.5 x 5.0 x 14.0 cm. Price £3.95. Post 25p.

**NEW!**

### 2" AND 4" PANEL METERS



2"		4"	
SIZE: 60mm High X 45mm Wide X 40mm Deep.	Movement	SIZE: 110mm High X 82mm Wide X 43mm Deep.	Movement
0-50 micro A	1250	0-50 micro A	1400
0-100 micro A	580	0-100 micro A	730
0-500 micro A	170	0-500 micro A	200
0-1 mA	170	0-1 mA	200
0-5 mA	170	0-5 mA	200
0-10 mA	6	0-10 mA	6
0-50 mA	0.5	0-50 mA	0.5
0-100 mA	0.5	0-100 mA	0.5
0-500 mA	0.5	0-500 mA	0.5
0-1 AMP	0.5	0-1 AMP	0.5
0-2 AMP	0.5	0-2 AMP	0.5
0-25 Volt	15K	0-25 Volt	15K
0-50 Volt	50K	0-50 Volt	50K
0-300 Volt	300K	0-300 Volt	300K
g Meter	170	g Meter	200
VU Meter	5250	VU Meter	5250

VU Meters are complete with detectors. Modern view.  
Price 2" £3.15 Post 10p. Price 4" £3.95 Post 10p. Lamps 55p per set.

### C1000 MULTI-METER

Special Offer NOV. AND DEC. ONLY

Compact General Purpose Mini Multimeter  
Input Resistance 1000 ohms per volt.  
Ranges: AC Volts 0-15 50 250 1000 Volts  
DC Volts 0-10 50 250 1000 Volts  
DC Current 0-1 mA 0-100 mA  
Resistance 0-150K ohms  
Size 60 x 24 x 90 mm  
Complete with: Batteries, Test Prods, Instructions.  
Special price £3.20 Post 20p.



### MINIATURE NEONS

6 mm dia. 12 mm length. Leads length approx. 20 mm. Recommended ballast resistor 150K ohms for 240 Volt operation. Price: Packet of 10 for 50p Postage 10p.



### ELECTRONIC MAINS TIMER

A reliable unit ideal for timing Bathroom/Toilet Ventilators, Stairway/Cloakroom Lighting etc. Gives up to 30 mins. delay before switching off. Delay: 1-30 mins. adjustable. Max Load: 400 VA or 1000 Watts resistive. Ivory Case: 3 1/2" x 3 1/2" x 2 1/2". Fitting Instructions included. Price: £5.80. Post 20p.



### MAINS KEYNECTOR

The safe, quick connector for electrical appliances. 13 Amp rating, fused will connect a number of appliances quickly and safely to the mains, ideal for testing, demonstrating, window displays, etc. Warning Light, interlocked to prevent connecting when live.  
Trade Price: £2.95. Post 25p.



### C1001 MULTIMETER

Input Resistance 20,000 ohms per volt  
Overload protection  
250 uA movement, clear scale  
Ranges—AC Volts 0-10, 50, 250, 1000V  
DC Volts 0-5, 25, 125, 500, 2500V  
DC Current 0-50 mA  
Resistance 0-60 Kohms 0-6 Mohms  
Decibels -20 to +22 db  
Carrying Case, Test Prods and Batteries included.  
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PLEASE ADD 8% FOR VAT

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HIGH PERFORMANCE PHASE LOCKED LOOP  
(as in 'W.W.' July '72)

### MOTOROLA MC1310P EX STOCK DELIVERY SPECIFICATION

Separation: 40dB 50Hz-15kHz. Distortion: 0.3%  
I/P level: 560mV rms. O/P level: 485mV rms per channel.  
Input impedance: 60KΩ. Power requirements: 8-16V at 16mA.  
Will drive up to 75mA stereo 'on' lamp or LED.

**KIT COMPRISES FIBREGLASS PCB**  
(Roller tinned). Resistors, I.C., Capacitors,  
Preset Potm. & Comprehensive Instructions

**LIGHT EMITTING DIODE**  
Suitable as stereo 'on' indicator for above

**ONLY WHY PAY MORE?**  
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**RED 29p**  
**GREEN 59p**

**MC1310P only £3.15 plus p.p. 6p**

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As the supplier of the first MC1310P decoder kit, of which we have sold literally thousands, our customers can benefit from our wide experience.

V.A.T.

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Ten inputs. Four output groups. Four limiters. Base, mid, treble EQ. Balanced inputs. Modular construction. Headphone monitoring.

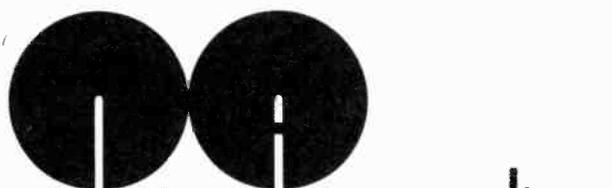
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**BARGAIN PACK PEP3—£4.90**



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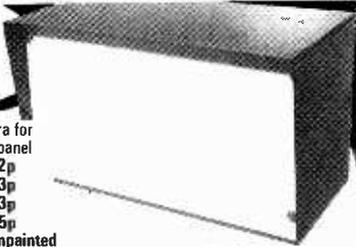
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AZ31 0-60	EABC80	EOH35 1-50	EZ81 0-31	PC86 0-65	PFL2000-70	PY801 0-55	UP89 0-50	5Y3GT 0-85	823 1-30	30FL14 0-80	2AF1 4-00
AZ41 0-70	EAF2 0-30	EOH42 0-85	EZ90 0-45	PC88 0-65	PC900 0-55	SP41 3-00	UL41 0-85	5Z4G 0-65	824 1-30	30L14 0-85	2AF1 4-00
CLB31 1-40	EAF42 0-70	EOH81 0-35	EH90 0-60	GC080 0-55	PC084 0-45	SP61 0-75	UL84 0-50	6/30L2 0-90	825 1-30	30L17 0-85	3BP1 4-50
CL33 1-60	EAF801	EOH83 0-50	EL33 2-00	GC230 0-65	PC088 0-55	T41 1-00	UY41 0-55	6AL5 0-30	826 1-30	30P12 1-00	3PD1A 4-00
CY31 0-60	ECB33 1-00	EOH84 0-50	EL34 0-70	GC232 0-65	PC098 0-55	U25 1-00	UY85 0-45	6AQ5 0-50	827 1-30	30P19 0-85	3EG1 8-00
DAF91 0-40	ECB33 1-00	EL27 0-50	EL41 0-90	GC234 0-75	PC098 0-40	U25 1-00	VF43 1-25	6AS7 1-00	828 1-30	30P21 0-85	3FP7 2-00
DAF96 0-60	ECB41 0-75	EL28 0-50	EL42 1-85	HLA1DD 0-70	PCF80 0-65	U404 0-75	VR75/30	6AT5 1-00	829 1-30	30P21 1-10	3GFL1 1-10
DCC90 1-35	ECB81 0-40	ECLL80 0-45	EL84 0-35	0-70	PCF801 0-60	U801 1-18	VR105/30	6AU6 0-50	830 1-30	30P21 1-10	3GFL1 1-10
DF91 0-40	EBF80 0-40	EL91 1-00	EL91 1-00	HN309 1-50	PCF802 0-55	U801 1-18	VR105/30	6AV6 0-50	831 1-30	30P21 1-10	3GFL1 1-10
DF96 0-60	EBF80 0-40	EL91 1-00	EL91 1-00	HN309 1-50	PCF802 0-55	U801 1-18	VR105/30	6BA6 0-38	832 1-30	30P21 1-10	3GFL1 1-10
DK91 0-60	EBF89 0-32	EL96 0-80	EL96 0-80	KT61 2-00	PCF806 0-90	U801 1-18	VR105/30	6BE6 0-45	833 1-30	30P21 1-10	3GFL1 1-10
DK92 1-00	ELB81 2-00	EL96 0-80	EL96 0-80	KT61 2-00	PCF806 0-90	U801 1-18	VR105/30	6BH6 0-75	834 1-30	30P21 1-10	3GFL1 1-10
DK96 0-75	ECOC4 1-00	EP41 0-75	ELM80 2-00	KT781 (7C5)	PCF808 0-90	U801 1-18	VR105/30	6BT4 0-55	835 1-30	30P21 1-10	3GFL1 1-10
DL92 0-50	ECOC8 0-45	EP52 1-30	EM80 0-55	1-30	PCLR2 0-45	PL802 1-00	YR3 0-50	6BQ7A 0-55	836 1-30	30P21 1-10	3GFL1 1-10
DL94 0-48	ECOC8 0-38	EP80 0-35	EM81 0-40	KT88 2-90	PCLR3 0-70	PY32 0-63	YR5 0-40	6BR7 1-20	837 1-30	30P21 1-10	3GFL1 1-10
DL96 0-55	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6BW6 1-00	838 1-30	30P21 1-10	3GFL1 1-10
DM70 0-70	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6BW7 1-00	839 1-30	30P21 1-10	3GFL1 1-10
DY807 0-45	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	840 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	841 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	842 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	843 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	844 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	845 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	846 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	847 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	848 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	849 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	850 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	851 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	852 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	853 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	854 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	855 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	856 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	857 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	858 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	859 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	860 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	861 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	862 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	863 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	864 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	865 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	866 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	867 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	868 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	869 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	870 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	871 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	872 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	873 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	874 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	875 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	876 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	877 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	878 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	879 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	880 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	881 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	882 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	883 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	884 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	885 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	886 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	887 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6C4 0-40	888 1-30	30P21 1-10	3GFL1 1-10
DY802 0-47	ECOC8 0-38	EP85 0-45	EM84 0-40	KTW61 1-50	PCLR4 0-50	PY33 0-63	YR5 0-40	6			

Available in a range of six sizes in 21-gauge Zintec with blue Acrylic texture. Front panels white Zintec steel or PVC/Aluminium.

**CONTIL TEXTURED CASES**

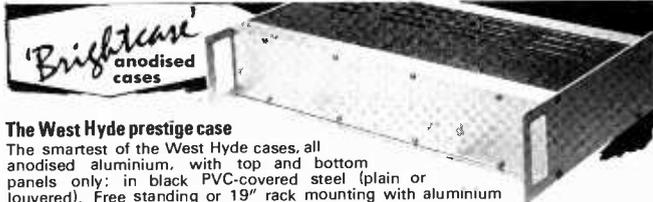


Width	Depth	Height	No.	Case cost	ali. panel
7"	5"	5"	755	£6.02	12p
8	6	7	867	£7.11	23p
9	7	5	975	£7.11	23p
12	7	7	1277	£8.10	15p
12	7	7	1277	£6.11	unpainted
16	12	7	16127	£11.30	35p
19	10	10	191010	£15.35	—

Extra for

Less for quantities. Prices include steel panel with feet and screws. P. & P. and 8% VAT.

Prices correct to Dec 1974.



**The West Hyde prestige case**

The smartest of the West Hyde cases, all anodised aluminium, with top and bottom panels only: in black PVC-covered steel (plain or louvered). Free standing or 19" rack mounting with aluminium brackets. Supplied ex-stock, fully assembled, with SS Pozidriv screws.

Brightcase	1 off	Pr. Brackets	Extra for Louvres
BC21 (3 1/2" whole rack)	£13.43	86p	79p
BC22 (3 1/2" half rack)	£10.91	86p	79p
BC31 (5 1/2" whole rack)	£15.46	£1.22	79p
BC32 (5 1/2" half rack)	£12.77	£1.22	79p

Prices include panels, feet, P. & P. and VAT. State whether 1/4, 1/2 or full panels required. Prices correct Dec 1974

**The new Oryx 50** is temperature controlled, light, small, easy to handle, rapid heating and high performance. It has a temperature control within ± 2C and adjusted in seconds whilst running to any value between 200C and 400C. Long life iron-coated tip as standard (11 sizes available).



**ORYX 50 TEMPERATURE CONTROLLED IRON**

**ORYX SR3A DESOLDERING TOOL**

**Oryx De-Soldering Irons**—small model SR3A instantly removes solder from printed circuits, etc., accurate, reliable, simple. PTFE nozzle. Larger instrument SR2 gives more suck, less recoil as only piston moves.



De-Soldering Tools  
SR3A £5.02  
SR2 £6.58  
Oryx 50 Iron  
1 @ £6.53  
Safety Stand £2.45  
Prices include P. & P. and 8% VAT. Prices correct Dec. 1974.

Lower prices for quantities

**WH Printed Circuit System**

is simple, inexpensive, and fits into low-cost West Hyde cases. The System comprises six cards (two styles, three sizes), connectors and five types of board guide. Connectors are double-sided and all contacts gold-plated. Shown: Mod-301 case with boards 421, guides 311, 21-way connectors. Prices Mod-301 (including chassis) £4.06; Connector 21-way

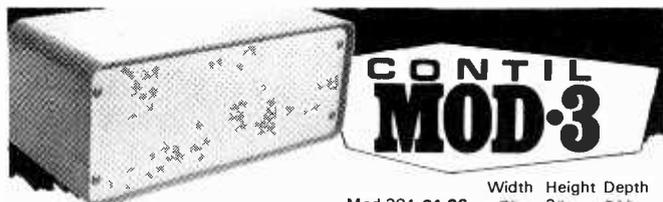


84p; Boards 421 & 422 £1.11. (up to 8 DILS on each board); Card guide pairs 311 £1.78. Prices include P. & P. and 8% VAT. Much less for quantities.

**LEDs** with chromium-plated screwed case suitable for 5.5 mm. hole or unmounted LEDs 3.2 mm. dia. 1 off inc. P & P and 8% VAT

Cased red	54p	w/o case	27p
Cased green	64p	w/o case	43p

Much less for quantities. Send for catalogue. Prices correct Dec. 1974.



Mod	Case cost	Width	Height	Depth
Mod 301	£4.06	7"	3"	5 1/4"
Mod 302	£4.25	7"	4 1/2"	5 1/2"
Mod 303	£4.80	7"	6"	5 1/2"
Mod 304	£4.80	11"	3"	5 1/2"
Mod 305	£5.70	11"	4 1/2"	5 1/2"
Mod 306	£6.57	11"	6"	5 1/2"

Contil Mod-3 cases are in six sizes and offer the manufacturer of small instruments an attractive low cost case available ex-stock. Made in blue PVC-coated steel and complete with front and rear panels and chassis, they are light, strong and rigid. PCB and PSU mounting systems available.

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### AUDIOTRONIC Model ATM1

Top value 1,000 opv pocket multi-meter. Ranges: 0/10/50/250/1,000 Volt AC and DC. DC current 0-1mA/100mA. Resistance: 0/150k ohms. Decibels: -10 to +22dB. Size 90 x 60 x 28mm. Complete with test leads.

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Jewel movement, attractively moulded case with edgewise ohms adjustment. Ranges: 0.3/1.5/15/300/1200V AC. (2500 opv). 0.6/30/300/600V DC. (5000 opv). 0.300 uA/0.300mA DC. Resistance: x 10 & x 100. -10 to +16dB. Supplied with battery test leads and data booklet. Size: 121 x 73 x 29mm.

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### MODEL TH12

20,000 opv. Overload protection. Slide switch selector. 0/0.25/2.5/10/50/150/1000V DC. 0/10/50/250/1000V AC. 0/50uA/25/250mA DC. 0/3k/30k/300k/3 Megohms. -20 to +50dB

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A versatile, accurate measuring instrument. 20,000 opv. 0/5/25/100/500/1000V DC. 0/10/50/250/1000V AC. 0-50uA/250mA. 0-20k/2 Megohms.

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20,000 opv DC. 8000 opv AC. Mirror scale 6/3/12/30/120/600V DC. 3/30/120/600V AC. 50/600uA/60/600mA. 10/100K/1 Meg/10 Meg Ohm. -20 to 46dB.

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### UA4323 MULTIMETER

20,000opv. Simple unit with audio/IF oscillator. Suitable for general receiver tuning. Ranges: 0.5/2.5/10/50/250/500/1000V DC. 2.5/10/15/50/500/1000V AC. 0.05/0.5/5/50/500mA DC. Resistance: x 10, x 100, x 1,000, x 10,000 (50k, 500k, 5kQ, 50kQ centre scale) Battery operated. Size: 160 x 97 x 40mm. Supplied in carrying case complete with test leads.

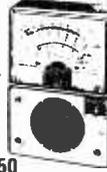
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### HIOKI 730X

30,000 opv. Overload protection. 6/30/60/300/600/1200V DC. 12/60/120/600/1200V AC. 60uA/300mA. 2K/200K. 2 Meg Ohm. -10 to +63dB.

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### UA4324 MULTIMETER

High sensitivity, overload protected. 20,000opv. Ranges: 0.6/1.2/3/12/30/60/120/600/1200V DC. 3/6/15/60/150/300/600/900V AC. Current: 0.06/0.6/6/60/600mA/30A DC. 0.3/3/30/300mA/3A AC. Resistance: 25/500 ohms/0.5/5/50/500k ohms/5 Mohms. Decibels: -10 to +12dB. Size 167 x 98 x 63mm. Supplied complete with test leads, spare diode and instructions.

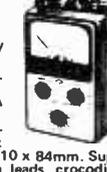
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### UA435 MULTIMETER

20,000opv. Ranges: 75mV/2.5/10/25/100/250/500/1000V DC. 2.5/10/25/100/250/500/1000V AC. Current: 50uA/1/5/25/100mA/0.5/2.5A DC. 0.5/25/100mA/0.5/2.5A AC. Resistance: 0.3/3/30/300k ohms. Size: 25 x 110 x 84mm. Supplied complete with leads, crocodile clips and steel carrying case.

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### UA4312 MULTIMETER

extremely sturdy instrument for general electrical use. 6670opv. 0/0.3/1.5/7.5/30/60/150/300/600/900V DC & 75mV. 0/0.3/1.5/7.5/30/60/150/300/600/900V AC. 0/300uA/1.5/6/15/150/60/600mA/1/1.5/6A DC. 0/1.5/6/15/60/150/600mA/1.5/6A AC. 0/200/3k/30k ohms. DC accuracy 1%. AC 1.5%. Knife edge pointer, mirror scale. Complete with sturdy metal carrying case, leads and instructions.

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### U91 Clamp VOLT AMMETER

For measuring AC voltage and current without breaking circuit. Ranges: 300/600V AC. Current: 10/25/100/250/500A. Accuracy 4%. Size 283 x 94 x 36mm. Complete with carrying case, leads and fuses.

**OUR PRICE £13.50 P&P 30p**



### MODEL 500

30,000 opv with overload protection. Mirror scale. 0/0.5/2.5/10/25/100/250/500/1000V DC. 0/2.5/10/25/100/250/500/1000V AC. 0/50uA/5/50/500mA. 12A DC. 0/60k/6 mag/60 megohms.

**OUR PRICE £13.95 Carr. paid Case for above £1.75**



### HIOKI 750X VOLT-OHM-MILLIAMMETER

43 ranges: 0-0.3/0.6/1.5/3/6/12/30/60/150/300/600/1,200V DC. 0-3/6/15/30/60/120/300/600/1,200V AC. Current: 0-300uA/1.5/3/15/30/60/300mA/100A DC. Resistance: 0-3/300k/3/30Mohms. Decibels: -10 to +17dB. Output: 0-3/6/15/30/60/120/300V. Accuracy ± 3% DC, ± 4% AC. Sensitivity: 50,000 opv DC, 5,000 opv AC. 4 inch meter. Built in protection. Size: 57 x 102 x 153mm.

**OUR PRICE £11.95 P&P 40p**



### TMK MODEL TW50K

46 ranges, mirror scale. 50kV/DC 50kV/AC. DC Volts: 0.125/0.25/1.25/2.5/5/10/25/50/125/250/500/1000. AC Volts: 1.5/3/5/10/25/50/125/250/500/1000. DC current: 25/50uA/2.5/25/50/500mA/5/10A. Resistance: 50k/100k/1 Meg/10 Meg ohms. -20 to +81.5dB.

**OUR PRICE £12.50 P&P 20p**



### HIOKI MODEL 700X

100,000opv. Overload protection. Mirror scale. 0.3/0.6/1.2/1.5/3/6/12/30/60/120/300/600/1200V DC. 1.5/3/15/30/60/150/300/600/1200V AC. 15/30uA/3/6/30/60/150/300mA/6/12A DC. 2k/200k/2M/20M Ohms. -20 to +63dB.

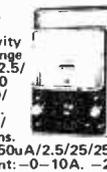
**OUR PRICE £14.95 P&P 30p**



### Model HT100B4 MULTIMETER

Overload protected, shock proof circuits. 9.5uA Meter with mirror scale. Sensitivity 100kV. Polarity change switch. Ranges: 0.5/2.5/10/25/50/100/200V DC. 2.5/10/50/250/1,000 Volts AC. DC resistance 0-20/200k/2/20 Meg. ohms. DC current: -10/250uA/2.5/25/250 mA/10A. AC current: 0-10A. -20 to +62dB. Operates from 2 x 1.5V batteries. Size: 180 x 134 x 79mm.

**OUR PRICE £17.50 P&P 40p**



### MODEL AS.1000 VOM

100,000 opv. Mirror scale. Built-in meter protection. 0/3/12/60/120/300/600/1200V DC. 0/6/30/120/300/600V AC. 0/10uA/6/60/300mA/12 Amp. 0/2K/200K/2M/200 Meg Ohm. -20 to -17dB

**OUR PRICE £17.50 P&P 30p.**



### MODEL C720ZEN

20,000 opv. DC. 10,000 opv. AC. Mirror Scale. 5/25/50/250/500/1000/2500V. DC. 10/50/100/500/1000V. AC. DC Resistance x 10, x 100, x 1000 (30k centre scale) DC Current 50uA/2.5mA/250mA. -20 to +68 dB

**OUR PRICE £6.50 P & P 30p**



### KAMODEN HM720B FET VOM

Input impedance 10 Megohms. Ranges: 0/2.5/10/50/100V DC. 0/2.5/10/50/250/1000V AC. 0/25uA/2.5/25/250 mA DC. 0/5k/50k/500k/5 M 500 Megohms

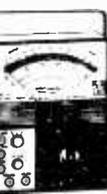
**OUR PRICE £21.00 P & P 40p**



### KAMODEN 360 MULTIMETER

High sensitivity. DC 100kOhm/V AC 10kOhm/V 5" mirror scale, overload protected. Ranges: 0.5/2.5/10/50/250/1000V DC. 0/5/10/50/250/1000V AC. Current: 0.01mA/0.5/5/50/500mA/10A. Resistance: 0.1/1/10/100 ohms/1/10/100k ohms/10/100M Ohms. Decibels -20 to +62dB. Battery operated. Size: 180 x 140 x 80mm. Supplied complete with test leads etc.

**OUR PRICE £17.50 P & P 40p**



### TMK MODEL 117 FET ELECTRONIC VOLT METER

Battery operated. 11 Meg input, 26 ranges. Large 4 1/2" mirror scale. Size: 149 x 117 x 60mm. 0.3-1200V DC. 3-300V RMS AC. 8-800V P-P. DC current 0.12-12mA. Resistance up to 2000M Ohms. Decibels: -20 to +51dB. Supplied complete with leads and instructions.

**OUR PRICE £18.50 P&P 20p**



### TMK 100K LAB TESTER

100,000opv. 6 1/2" scale. Buzzer short circuit check. Sensitivity 100,000 opv DC. 5kV/AC DC Volts: 0.5/2.5/10/50/250/1000V AC. 3/10/50/250/500/1000V DC. 10/100uA/10/100/100k/10 Meg/100 Meg ohms. Decibels: -10 to +49dB. Plastic case with carrying handle. Size: 190 x 172 x 99mm.

**OUR PRICE £19.95 P&P 30p**



### 370WTR MULTIMETER

Features AC current ranges. 20,000opv. 0/0.5/2.5/10/50/250/500/1000V DC. 0/2.5/10/50/250/500/1000V AC. 0/50uA/1/10/100 mA/1/10A DC. 0/100uA/1/10A AC. 0/5k/50k/500k/5 Meg/50 Meg. Decibels: -20 to +62dB.

**OUR PRICE £19.95 P&P 30p**



### KAMODEN 72.200 Multitester

High sensitivity tester. 200,000 opv Overload protected. Mirror scale. Ranges: 0/0.06/3/30/120/600/1200V DC. 0/3/30/120/600/1200V AC. 0/6uA/1.2mA/120mA/600mA/12A DC. 0/12A AC. -20 to +63dB. 0/2k/200k/2 Meg/200 Megohms.

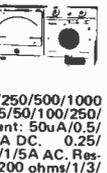
**OUR PRICE £22.50 P&P 30p**



### UA4317 MULTIMETER

High sensitivity instrument for field and laboratory work. Knife edge pointer. 86mm. mirror scale. Overload protection. Ranges: 100mV/0.5/2.5/10/25/50/100/250/500/1000V DC. 0.5/2.5/10/25/50/100/250/500/1000V AC. Current: 50uA/0.5/1.5/10/50/250mA/1.5A DC. 0.25/0.5/1.5/10/50/250mA/1.5A AC. Resistance: 0.5/10/100/200 ohms/1/3/30/300k ohms. Decibels: -5 to +10dB Battery operated. Size: 210 x 115 x 90mm. Supplied in carrying case complete with leads.

**OUR PRICE £16.50 P&P 40p**



### MODEL C7208FM

30,000 opv DC. 15,000 opv AC. 6/3/15/60/300/600/1200V. DC. 6/30/120/600/1200V. AC. DC Resistance x 10, x 100, x 1000 (50k centre scale) DC Current 30uA/3/30/600mA. -20 to +63dB.

**OUR PRICE £8.95 P & P 30p**



### MODEL UA4311 Sub-standard Multi-range Volt-Ammeter

Sensitivity 330 Ohms/Volt AC and DC. Accuracy 0.5% DC. 1% AC. Scale length: 165mm. 0/300/750uA/1.5/3/7.5/15/30/75/150/300/750mA/1.5/3/7.5A DC. 0/3/7.5/30/75/150/300/750mV/1.5/3/7.5/15/30/75/150/300/750V DC. 0/750mV/1.5/3/7.5/15/30/75/150/300/750V AC. Automatic cut out device. Supplied complete with test leads, manual and test certificates.

**OUR PRICE £52.00 P&P 50p**



### MODEL AF.105 VOM

50,000 opv. Mirror scale. Meter protection. 0/3/12/60/120/300/600/1200V DC. 0/6/30/120/300/600/1200V AC. 0/30uA/6/60/300mA/12 Amp. 0/10K/1m/10m/100 Meg Ohms. -20 to +17dB.

**OUR PRICE £12.50 P&P 30p.**



### LB3 TRANSISTOR TESTER

Tests ICD and B. PNP/NPN. Operates from 9V battery. Instructions supplied.

**OUR PRICE £3.95 P&P 20p**



### LB4 TRANSISTOR TESTER

Tests PNP or NPN transistors. Audio indication. Operates on two 1.5V batteries. Complete with instructions etc.

**OUR PRICE £4.50 P&P 20p**



### KAMODEN T735 TRANSISTOR TESTER

High quality instrument to test reverse leak current and DC current. Amplification factor of PNP, PNP, diodes, transistors, SCR's etc. 4 1/2" square clear scale meter. Operates from internal batteries. Complete with instructions, leads carrying handle.

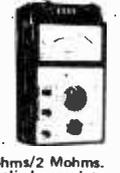
**OUR PRICE £17.50 P & P 40p**



### UA4341 Multimeter & Transistor Tester

27 ranges. 16,700opv. test reverse leak current and DC current. Amplification factor of PNP, PNP, diodes, transistors, SCR's etc. 4 1/2" square clear scale meter. Operates from internal batteries. Complete with instructions, leads carrying handle.

**OUR PRICE £17.50 P & P 40p**



### S100TR MULTIMETER TRANSISTOR TESTER

100,000opv. Mirror scale. Overload protection. 0/0.12/0.6/3/30/120/600V DC. 0/6/30/120/600V AC. 0/12/60uA/12/300mA/6/12A DC. 0/10k/1 Meg/100 Meg. -20 to +50dB. 0.01-0.2 MFD Transistor tester measures Alpha, Beta and ICD. Complete with instructions, batteries and leads.

**OUR PRICE £19.95 P&P 25p**



**ALL PRICES EXCLUDE VAT**

Also see following pages

SWR METER Model SWR3

Handy SWR meter for transmitter antenna alignment, with built-in field strength meter. Accuracy 5%, Impedance 52' Indicator 100uA DC. Full scale 5 section collapsible antenna. Size 145 x 50 x 60mm.



OUR PRICE £4.25 P&P 30p

C15 PULSE OSCILLOSCOPE

For display of pulsed and periodic waveforms in electronic circuits. VERT. AMP. Bandwidth: 10MHz. Sensitivity at 100kHz VRMS/mm: 0.1-25; HOR. AMP. Bandwidth: 500kHz. Sensitivity at 100kHz VRMS/mm: 0.3-25. Preset triggered sweep 1-3000usec. Free running 20-200 kHz in nine ranges. Calibrator pips. 220 x 360 x 430mm. 115-230V AC.



OUR PRICE £43.00 Carr. paid

RUSSIAN C116 Double Beam OSCILLOSCOPE

5 MHz pass band. Separate Y1 and Y2 amplifiers. Rectangular 5" x 4" CRT. Calibrated triggered sweep from 0.2usec. to 100 milli-sec/cm. Free running time base 50Hz-1MHz. Built-in time base Calibrator and amplitude Calibrator. Supplied complete with all accessories and instruction manual.



OUR PRICE £87.00 Carr. paid

MODEL TE15 GRID DIP METER

Transistorised. Operates as Grid Dip, Oscillator, Absorption Wave Meter and Oscillating Detector. Frequency range 40kHz-280MHz in six coils. 500uA meter. 9V battery operation. Size: 180 x 80 x 40mm.



OUR PRICE £17.50 P&P 30p

TRANSISTORISED L.C.R. A.C. BR/8 MEASURING BRIDGE

A new portable bridge offering excellent range and accuracy at low cost. Resistance: 6 ranges: 0.1 ohm-11.1 megohm + 1% Inductance: 6 ranges: 1 microhenry-111 henries + 2% Capacity: 6 ranges: 10pf-1110 mfd + 2% Turns Ratio: 6 ranges: 1:1/1000-1:11100 + 1% Bridge Voltage at 1.000cps. Operated from 9-volt battery. 100 microamp meter indication. Size 7 1/2" x 5" x 2"



OUR PRICE £25.00 P&P 30p

TE-200 RF SIGNAL GENERATOR

Accurate wide range signal generator covering 120 kHz-500 MHz on 6 bands. Directly calibrated. Variable R.F. attenuator audio output. Xtal socket for calibration. 220/240V a.c. Brand new with instructions. Size 140mm x 215mm x 170mm.



OUR PRICE £17.50 P&P 50p

TE22 SINE SQUARE WAVE AUDIO GENERATOR

Sine 20cps to 200kHz on 4 bands. Square 20 cps to 30 kHz. Output impedance 500 Ohms. 200/250V AC operation. Supplied brand new guaranteed, with instruction manual and leads.



OUR PRICE £24.95 P&P 50p

ARF 300 AF/RF SIGNAL GENERATOR

All transistorised compact fully portable. AF sine-wave 18Hz to 220 kHz. AF square wave 18Hz to 100kHz. Output Square/Sine wave 10V. P-P RF 100kHz to 200MHz. Output 1V maximum. 220/240V AC operation. Complete with instructions and leads.



OUR PRICE £37.50 P&P 50p

WALKIE TALKIES SKYFON NV7

Super low cost transmitter/receiver. 100MW with call buzzer and on/off volume control. 7 transistors. Telescopic rod antenna.



OUR PRICE £28.95 per PAIR P.&P 50p. NOT LICENSABLE IN THE U.K.

MODEL MG100 SINE SQUARE WAVE AUDIO GENERATOR

Range 19-220.000Hz Sine Wave 19-100.000 Hz Square Wave. Output Sine or Square wave 10v. P. to P Size 180 x 90 x 90mm. Operation 220/240V. A.C.



OUR PRICE £19.95 P&P 50p

POWER RHEOSTATS

High quality ceramic construction. Windings embedded in vitreous enamel. Heavy duty brush wiring. Continuous rating. Single hole fixing. 1/4" diameter shafts. Bulk quantities available.



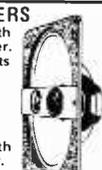
25 WATT 10/25/50/100/500/1000/2500 ohms. £1.15 P&P 10p

50 WATT 10/50/100/250/500/1500/5000 ohms. £1.62 P&P 10p

100 WATT 1/5/10/25/50/250/500/2500 ohms. £2.34 P&P 15p

EMI LOUDSPEAKERS

Model 350 13 x 8" with single tweeter/crossover. 20-20,000Hz. 15 watts RMS. Available 8 or 15 ohms.



OUR PRICE £7.50 each P&P 37p

Model 450 13 x 8" with twin tweeter/crossover. 55-13,000Hz. 8 watts RMS. Available 8 or 15 ohms

OUR PRICE £3.62 each P&P 35p

SPECIAL PURCHASE LIMITED QUANTITY!

Tannoy I2" DR/8 Bass Speakers 8 ohms. 30 watt. Heavy duty. ideal for Hi-Fi P.A. Group. OUR PRICE £12.50 P&P 50p.



PS200 Regulated POWER SUPPLY UNIT

Solid state. Variable output 5-20V DC up to 2 Amp. Independent meters to monitor voltage and current. Output 220/240V AC. Size: 190 x 136 x 98mm.



OUR PRICE £19.95 P&P 50p

AUDIOTRONIC LE-102A INTERCOM

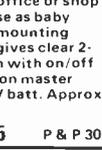
Beautifully made and finished in two tone ivory/buff, the LE-102A is useful in the home, office or shop and is suitable for use as baby alarm. Wall or desk mounting 57mm speaker/mic gives clear 2-way communication with on/off and volume control on master unit. Operates 9V batt. Approx 60ft lead.



OUR PRICE £3.95 P & P 30p

TRITON 4318 PORTABLE 8 TRACK CARTRIDGE PLAYER WITH MW/LW RADIO

Will play 8 track stereo cartridge monaurally. Channel selector switch. Covers medium and long wave bands Volume and tone controls. Earphone socket. Battery/Mains operation.



OUR PRICE £11.95 P & P 50p

EA41 REVERBERATION AMPLIFIER

Self contained, transistorised, battery operated. Simply plug in microphone, guitar etc. and output to your amplifier. Volume control and depth of reverberation control. Be walnut cabinet. 184 x 77 x 108mm.



OUR PRICE £7.50 P&P 30p

SPECIAL PURCHASES! RECORD DECK PACKAGE

by Famous Manufacturer GARRARD SP25 Mark 111 with G800 cartridge in luxurious plinth with cover. OUR PRICE £13.95 P & P 75p GARRARD SP25 Mark 111 Record deck fitted K5 40A cartridge. OUR PRICE £9.95 P & P 50p

LH025 STEREO HEADPHONES

Light weight headphones with padded ear pieces. 4/16 ohms 20-20,000Hz. Complete with 6' lead and plug.



OUR PRICE £1.97 P&P 30p

DH025 STEREO HEADPHONES

Wonderful value and excellent performance combined. Adjustable head band. Impedance 8 ohms. 20-12,000Hz. Complete with lead and plug.



OUR PRICE £2.25 P&P 30p

TE1035 Stereo HEADPHONES

Low cost with excellent response. Foam rubber earcups. Adjustable headband. 8 ohms impedance. Frequency response 25Hz-18kHz. Complete with cable and stereo jack plug.



OUR PRICE £2.60 P&P 30p

SDH8V MONO/STEREO HEADPHONES

Volume control for each channel. 4/16 ohms impedance. Frequency response 20Hz-18kHz. Complete with 10ft. coiled lead and jack plug.



OUR PRICE £4.97 P&P 30p

BH001 HEADSET and Boom Microphone

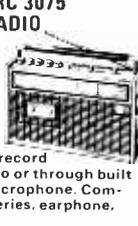
Moving coil. Ideal for language teaching. Excellent communications etc. Headphone impedance 16 ohms. Microphone impedance 200 ohms.



OUR PRICE £5.95 P&P 30p

HANIMEX HRC 3075 CASSETTE RADIO

Covers Medium and FM wavebands. Slider volume and tone controls. Battery/Mains operation. Will record direct from radio or through built in condenser microphone. Complete with batteries, earphone, and cassette.



OUR PRICE £24.30 P & P 50p

SPECIAL BARGAIN!! STEREOSOUND SPEAKERS

Matched pair of stereo bookshelf speakers. Deluxe teak veneered finish. Size: 368 x 229 x 190mm. 8 ohms. 8 watts RMS, 16 watts peak. Complete with Din lead.



OUR PRICE £12.95 PAIR P&P 50p

FM TUNER CHASSIS

6 transistor high quality tuner. Size only 153 x 109 x 63mm 3 IF stages. Double tuned discriminator. Ample output to feed most amplifiers. Operates on 9V battery. Covers 88-108MHz. Ready built, ready for use. Fantastic value for money.



OUR PRICE £8.95 P&P 20p Stereo Multiplex Adaptor £5.95 extra

SPECIAL OFFER! SAVE OVER 50%



AMSTRAD 8000/2 Stereo amplifier 7 watts per channel rms. Inputs for tuner tape, phono. Headphone socket. List price £29.95. OUR PRICE £12.95 P & P 60p

SPECIAL OFFER! CONVERT YOUR STEREO SYSTEM TO 4D SOUND FOR UNDER £16



Exclusive offer of GOODWIN 4-CHANNEL CONVERTER and a pair of AD15 10 watt 8 ohm bookshelf speakers enables you to add 4D sound to your existing system. Complete with simple connection details. Normal retail value £25.50. OUR PRICE £15.80 P & P £1. GOODWIN CONVERTER available separately £3.95 P & P 50p.

Model A1018 FMT TUNER

6 transistor high quality unit-3IF stages and double tuned discriminator. For use with most amplifiers. Covers 88-108MHz. Powered by 9V battery. OUR PRICE £13.50 P&P 30p Stereo multiplex adapter £5.95 extra.



ELECTRONIC CALCULATORS



We carry a tremendous range of both pocket and desk calculators from as little as £9. Owing to the demand it is not possible to include them in this advertisement, so send for our latest price list or call into any branch.

MINIATURE ORGAN MUSIC MASTER AM100

Spanning nearly two octaves, including semi-tones. This instrument will give hours of enjoyment to all the family. Beautifully finished. The keyboard range can be adjusted to be in tune with any instrument. Operates from internal 9V battery. Fitted with on/off switch, vibrato switch, earphone socket and external 9V D.C. socket. OUR PRICE £7.95 P&P 50p.



BINATONE DIGITAL CLOCK

Attractive ivory case. Large clear numbers for hours, minutes and seconds. A.C. 240V operation. Size approx. 6 1/2 x 3 x 3 1/2 inches. OUR PRICE £4.50 P&P 50p.



SINCLAIR IC12 INTEGRATED CIRCUIT AMPLIFIER

complete with printed circuit mounting board. OUR PRICE £1.50 P & P 15p.



SINCLAIR Project 80 Modules

240 Power Amp. £5.95 P & P 15p 260 Power Amp. £7.45 P & P 15p Stereo 80 Pre-Amp £13.95 P & P 15p Active Filter Unit £7.45 P & P 15p FM Tuner £13.95 P & P 15p Stereo Decoder £8.95 P & P 15p P25 Power Supply £5.95 P & P 30p P26 Power Supply £8.95 P & P 30p P28 Power Supply £8.45 P & P 30p Transformer for P28 £4.05 P & P 50p IC20 Stereo Amp. kit £7.95 P & P 15p P220 Power Supply kit £5.45 P & P 30p

SINCLAIR Project 80 Packages 2x240/Stereo 80/P25 £28.60 P & P 35p each 2x240/Stereo 80/P26 £31.30 P & P 35p each 2x260/Stereo 80/P28 £33.55 P & P 35p each

TE1021 Stereo Listening Station

For balancing and gain selection of loudspeakers with additional facility for stereo headphone switching. Two gain controls, speakers on-off slide switch, stereo headphone socket. OUR PRICE £2.25 P&P 15p



AUDIOTRONIC LOW NOISE CASSETTES

TYPE 5 10 25 C30 £1.57 £3.00 £7.08 C90 £2.24 £4.25 £10.00 C120 £2.73 £5.17 £12.24 P&P 3p each. 10 and over Post Free

MP7 MIXER-PREAMPLIFIER

5 Microphone inputs each with individual gain controls enabling complete mixing facilities. Battery operated. Size: 235 x 127 x 76mm. Inputs: Mics. 3 x 3mV 50k; 2 x 3mV 600 ohms. Phono. Mag. 4mV 50k; Phono Ceramic 100mV 1 Meg. Output 250mV 100k. OUR PRICE £8.97 P&P 20p



AUDIOTRONIC AHA101 Stereo Headphone Amplifier

All silicon, transistor amplifier operates from magnetic, ceramic or tuner inputs with twin stereo headphone outputs and separate volume controls for each channel. Operates from 9V battery. 4 INPUTS: 5mV and 100mV. OUTPUT: 50mV per channel. OUR PRICE £8.50 P&P 30p



HIGH QUALITY CONSTRUCTION KITS

WE ARE APPOINTED STOCKISTS AT Oxford Street, 42 & 257 Tottenham Court Road, 34 Lisle Street, 152, Fleet Street, 311 Edgware Road, CROYDON BIRMINGHAM KINGSTON LEICESTER NORTHAMPTON SOUTHEND TUNBRIDGE WELLS WOLVERHAMPTON branches, or by Mail Order.

All kits are complete with comprehensive easy to follow instructions and covered by full guarantee. Post and Packing 15p per kit.

- AF20 Mono amplifier..... £5 61 AF25 Mixer..... £3 29 AF30 Mono pre-amplifier..... £3 20 AF35 Emitter amplifier..... £2 42 AF80 0.5W mic. amplifier..... £4 86 AF305 Intercom..... £7 67 AF310 2 Mono Amplifier..... £7 55 M160 Multi-vibrator..... £2 18 M1302 Transistor tester..... £8 38 M191 VU Meter..... £5 37 M192 Stereo balance meter..... £5 93 LF380 Quadraphonic device..... £ 8 42 AT5 Automatic light control..... £3 75 AT30 Photo cell switch unit..... £ 6 68 AT50 400W triac light dimmer/speed control..... £ 5 18 AT56 2,200W triac light dimmer/speed control..... £ 6 75 AT60 1 channel light control..... £ 10 82 AT65 3 channel light control..... £ 16 52 GU330 Tremolo unit..... £ 8 10 HF61 Diode detector..... £3 87 HF65 FM transmitter..... £3 21 HF75 FM receiver..... £3 66 HF310 FM tuner..... £16 32 HF325 Deluxe FM tuner..... £26 33 HF330 Decoder (HF101/325)..... £10 55 GP310 Stereo pre-amplifier for use with 2 x AF310..... £22 98 GP312 Circuit board..... £10 02 GP304 Circuit board..... £5 33 HF380 lw/hf aerial amplifier..... £ 6 02 HF395 broadband aerial amp. £2 10 NT10 Stabilised power supply 100mA, 9V..... £ 6 27 NT300 Stabilised p. supply..... £13 16 NT310 Power Supply 240 V AC or 2 x 18 V D C at 2 amps..... £ 5 64 NT305 Voltage converter..... £ 5 64 NT15 Power supply 240V AC to 4.5/15V DC, 500mA..... £12 06

Amateur Electronics by Josty-Kit, the professional book for the amateur

covers the subject from basic principals to advanced electronic techniques. Complete with circuit board for AE1 to AE10 listed below. OUR PRICE £3.30 (No VAT) P&P 25p plus VAT.

- AE1 100mW output stage..... £1 55 AE2 Pre-amplifier..... £1 32 AE3 Diode receiver..... £ 2 05 AE4 Flasher..... £1 26 AE5 Astable multi-vibrator..... £1 14 AE6 Monostable multi vibrator £1 11 AE7 RC generator..... £1 08 AE8 Bass filter..... £1 05 AE9 Treble filter..... £1 05 AE10 CCIR filter..... £1 05

Also see previous page

ALL PRICES EXCLUDE VAT

# SEW PANEL METERS

**SEW PANEL METERS ARE STOCKED AT OUR 3 LISLE ST., 311 EDGWARE RD., & 152 FLEET ST., BRANCHES or order by post.**

USED EXTENSIVELY BY INDUSTRY, GOVERNMENT DEPARTMENTS, EDUCATIONAL AUTHORITIES ETC.  
Over 200 ranges in stock—other ranges to order. Quantity discounts available. Send for fully illustrated brochure.



**CLEAR PLASTIC MODEL SD640**  
Size: 85 x 64mm

50uA ..	£3.80
100uA ..	£3.75
200uA ..	£3.70
500uA ..	£3.65
50-0-50uA ..	£3.75
100-0-100uA ..	£3.70
1mA ..	£3.65
5mA ..	£3.65
10mA ..	£3.65
50mA ..	£3.65
100mA ..	£3.65
500mA ..	£3.65
1A DC ..	£3.65
5A DC ..	£3.65
10A DC ..	£3.65
5V DC ..	£3.65

10V DC .. £3.65  
20V DC .. £3.65  
50V DC .. £3.65  
300V DC .. £3.65  
15V AC .. £3.75  
300V AC .. £3.75  
VU Meter .. £3.90

**\*Items with asterisk are Moving Iron type, all others are Moving Coil**

**CLEAR PLASTIC MODEL SD830**  
Size: 110 x 83mm

50uA ..	£4.30
100uA ..	£4.25
200uA ..	£4.20
500uA ..	£4.15
50-0-50uA ..	£4.25
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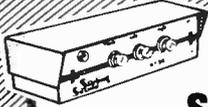
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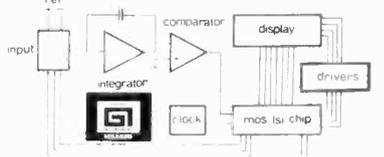
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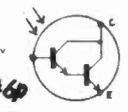
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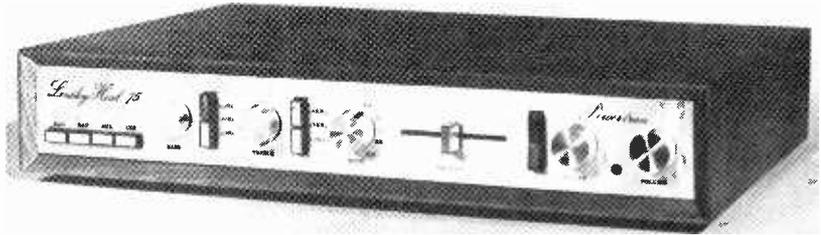
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## Hi-Fi News Linsley-Hood 75 W Amplifier Mk III Version (modifications as per Hi-Fi News April 1974)



Full circuit description in handbook (pack 15—price 30p)

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- NE561 PLL £3.15
- NE562 PLL £3.19
- NE565 PLL £2.69
- NE566 Gen £2.49
- NE567 code £2.69
- SN72709 709 29p
- SN72741 741 31p
- SN72748 748 36p
- SN76151 £1.20
- SN76660 FMIF £1
- SN76611 IF £1.25
- TAD 100 & IF £2
- ZN100E £3
- ZN402T £1.75
- ZN403 Servo £2.50
- ZN414 AM Rxf £1.09

#### SPECIAL OFFERS

- 741 29p MFC4000 35p
- 555 67p ZN414 £1.09
- BC107, BC108, BC109 9p ea
- 2N3055 39p Three for £1
- 115W/T03 or 90W plastic
- 2N3819E 16p 2N3053 17p
- BFY50/51/52/53 all 18p
- LA50Vrect 4p ea IN914 4p

#### Price each:-

- AC127/128 16p
- AC187/188 19p
- AD161/162 35p
- BC107/8/9 9p
- BC132/4/7 18p
- BC147/8/9 10p
- BC157/8/9 12p
- BC177/8/9 18p
- BC182/3/4 11p
- BC212/3/4 12p
- \*A or L
- BCY70/1/2 15p
- BD131/2 39p
- BFY50/1/2 18p
- BFY53 17p
- BSX20 12p
- MJE2955 95p
- MJE3055 62p
- MPU131put 49p
- OA91 8p
- TIP29A 48p
- TIP30A 57p
- TIP31A 61p
- TIP32A 73p
- TIP41A 78p
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- BZY88 400mW 9p
- ZENERS 9p
- BRIDGE RECT 4A 50V 20p
- GAS SENSOR £2
- GAS "KIT" £5
- TIP2955 90p
- TIP3055 55p
- TIS43 UJT 25p
- IN4001 4p
- IN4004 6p
- IN4148/914 4p
- 2N697 13p
- 2N706/8 10p
- 2N2646 49p
- 2N2904/5 20p
- 2N2926 royo 9p
- 2N3053 17p
- 2N3055 39p
- 2N3614 49p
- 2X3702/3 9p
- 2X3704/5 10p
- 2X3706/7 9p
- 2X3708/9 8p
- 2X3710/11 9p
- 2X3563/64 16p
- 2X3566/67 16p
- 2X3638 16p
- 2X3641/2 16p
- 2X3819E 16p
- 2X3832E 17p
- 2X3904/6 14p
- 2N4249 16p
- TAG 1/400 55p
- C107D1 SCR 4A/400V 55p
- SC146D TRIAC 10A 400V 75p

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- VERO PINSx36 25p.
- COPPER CLAD VEROBOARD 0.1"
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- DIL IC's BOARDS 6x4 1/2" £1.50
- 24 way edge connector 60p
- 36way 90P. PLAIN 3 1/2"x17 £1
- FACE CUTTER 43p. FEC ETCHANT

### DALOpen69p

- PRINTED CIRCUIT BOARD KIT £1.69
- COPPER BOARD 6x4" 40p.
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- HEATSINKS
- 5T/T05 & 18T/T018 5p ea.
- TV4 12p. TV3/T03 16p. 4Y1/T03 29p.

### CAPACITORS

- 22p to 0.1uf 4p ea. ELECTROLYTIC
- 25V 2/10/50/100uf 6p. 1000uf 20p
- PRESETS VERT: 5p. RESISTORS 5% 12p

### POTS AB or EGIN

- ROTARY: 12p. SWITCH 13p. DUAL 38p.
- SLIDERS: SINGLE 26p. DOUBLE 48p.
- SWITCHES: SPST 18p. DPDT 25p.
- MINI 4": SPST 39p. PUSH 59p.
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- DIN PLUGS all 13p ea. Sockets 9p
- TRANSFORMERS 1A 6/12V £1.34
- BHA 0002 MODULE 15WATT AMP £5
- EA1000 4W AF MODULE £2.49
- 8W/12V FLUORESCENT LIGHT £3.

### OIL sockets

- PROFESSIONAL GOLD PLATED & GREY NYLON. 8, 14 or 16 PIN. Only 15p each.

### LEDS 14p.

- MINI PIN SOURCE OR RED DIFFUSE
- LEDS. 209 STYLE. NO CLIP. 14P ea
- TIL209 RED LED & CLIP 17P ea
- BIG 1" RED LED & CLIP 18P ea
- ORANGE & GREEN LEADS:
- MINI 25P ea. BIG & CLIP 33P ea
- INFRA RED LED £1.2N5777 33P.
- PS12 PHOTO IC/amp/switch £1.

### DIGITAL CLOCK

- MOS INTEGRATED CIRCUITS.
- AY51224 4 DIGIT CLOCK supplied with 14pin socket & data £4.25
- MM5311/14 6 DIGIT CLOCK with 28 pin socket & data £7.50
- 3 DIGIT DVM AY53500 £7.50
- 4 DIGIT COUNTER/DRIVER £7.50

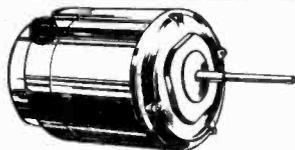
### CASSETTE mechanics £12.50

STEREO CASSETTE MECHANISM.  
As used in imported types costing £100. Only requires a case & electronics leads supplied. Send for data 15p.



- 7400 etc gates 16p
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- 74121 mono 45p
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- Full range in Cat.

WW-029 FOR FURTHER DETAILS



## "SLO-SYN" 3-LEAD SYNCHRONOUS STEPPING MOTOR

Type SS15. These fine motors are easily reversed, starting and stopping in less than 5° without electrical or mechanical braking. Simple relay circuit can be applied to give D.C., to winding for a maximum holding torque of 300oz/in in with 35v at 0.35amps through winding. For A.C. (synchronous) operation at 120v, 50Hz. Speed 60 rpm at 60Hz, 72 rpm. STEPPING. Holding torque at 60 steps per second—100 oz/in. Can be wired to give 100 or 200 steps per revolution with accuracy of 0.1° per step non-cumulative. Torque characteristics can be modified by simple R.C. circuits. Dimensions: dia. 4", body length 4 1/2", spindle length 2 1/2" x 1/8" dia. Weight 6 1/2 lbs. BRAND NEW in maker's packing. Offered at less than 1/2 maker's price. £15

### OPEN FRAME shaded pole GEARED MOTORS

(Dural gear case) 240 AC. 28rpm. NEW HIGH TORQUE, approx. overall size: 3 1/2" x 3 1/2" x 2 1/2" spindle 1/2" dia. as illustrated. £3. P. & P. 30p. Similar to above, 18rpm. £3. P. & P. 30p. 110rpm with pressed steel gear case (similar to above but slightly smaller). £3. P. & P. 30p.

### CARTER ELECTRIC

Similar to above with alloy gear case. 60 r.p.m. This item is ex-equipment but perfect. £1.95. P & P 30p.



### SMITHS RINGER-TIMER

Reliable 15 minute times, spring wound (concurrent with time setting) 15x1min divisions, approximately 1/2" between divisions. Panel mounting with chrome bezel 3 1/2" dia. £1.40. 15p. P. & P.

### FEW ONLY

Fully stabilised "Labgear" Power Supply Unit. Input 90-240v. 50Hz. Outputs 6v, 6a D.C., and 6v+2v, 100mA. Hum and ripple at full load—less than 3mV peak to peak. Stability improvement ratio for 15% mains change—1/1000. Output impedance 0.005 ohms. 9 1/2" x 9 1/2" x 12 1/2". Weight 20lbs. £26.00. Carr. & Pkg £1.50. In manufacturer's carton.

### "LABGEAR ELIMINAC"

P.S.U. 200-250v. 40/60Hz. Alternative outputs fully variable (variac incorporated). Output 1. 12v at 5a D.C. fully smoothed. Output 2. 12v at 8a D.C., with ripple content. Output 3. 20v at 10a A.C. 2 1/2" x 2 1/2" flush 0-20v D.C. mic meter. In attractive grey hammer finish case. In maker's carton. £27.50. Carr. & Pkg. £1.50.

### SHADED POLE MAINS MOTOR

A quality shaded pole motor. Open frame. 3" high x 2 1/2" x 2". Spindle 1" x 1/8". 1,420r.p.m. £1.95 P & P 20p.

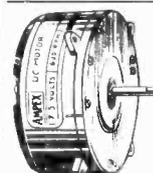
### SOLENOIDS by WESTOOL

240AC type MM6. 3lb. pull, 2 1/2" x 1 1/2" x 1 1/2". Travel 1". 90p each. P.&P. 10p.

240AC type MM4. 2lb. pull, 1 1/2" x 1 1/2" x 1 1/2". Travel 1" 70p each. P. & P. 10p. Quantity discounts: 10-50 10%. 50 upwards 25%

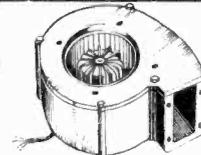
### MAINS SOLENOID

This little unit gives vertical lift of approximately 1" through hinged "elbow". Bracket incorporates 2 fixing screws. Length of arm, 2 1/2". 240V A.C. Pull at coil is approximately 1lb. £1. FREE P. & P. Special quotes for quantities.



### AMPEX 7.5v. DC MOTOR

An ultra precision tape motor designed for use in the AG20 portable recorder. Torque 450GM/CM. Stall load at 500ma. Draws 60ma on run. 600rpm ± speed adjustment. Internal AF/RF suppression. 1" dia. x 1 1/2" spindle. motor 3" dia. x 1 1/2". Original cost £16.50. OUR PRICE £3.30. P. & P. 25p. Large quantities available (special quotations). Mu-metal enclosure available. 75p each. FREE P. & P.



## ULTRA PRECISION CENTRIFUGAL BLOWER by Air Control Ltd.

30 segments individually balanced in heavy cast alloy case. 2,300 r.p.m. 240v A.C. Very powerful and silent running. 5 1/2" dia. 3" inlet dia. Outlet flange 3" x 2 1/2".

Limited number only £8.95 P & P 40p.

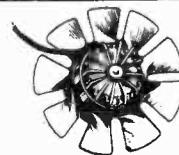
## SILVANIA MAGNETIC SWITCH

Now complete with reference magnet!

A magnetically activated switch, vacuum sealed in a glass envelope. Silver contacts, normally closed. Rated 3amp at 120v. 1amp at 240v. Size: (approx.) 1 1/2" long x 1" dia. Ideal for burglar alarms, security systems etc., and wherever non-mechanical switching is required. 10 for £2; P & P 15p. 50 for £8.80; 100 for £16.50. FREE P.&P. over 10.

## NORPLEX

The famous American fibre-glass copper-clad laminate. Finest quality with woven glass base of Epoxy-resin. Excellent Mech. and Elec. conductive properties. Heat resistant, ideal for P.C.'s etc. THIS IS A SPECIAL PURCHASE AND ONLY AVAILABLE WHILE STOCKS LAST! Sizes: 12" x 12", 24" x 12", 24" x 24", FULL SHEET 43" x 37" (11 sq. ft.). Single-sided Copper with thickness of 1/32", 3/64", 3/32". Also double-sided 1/32", 1/16", 3/32". £1 per sq. ft. Cut sizes (1-10 sq. ft.) 25p. P. & P. Full Sheet £8 each. Carr. £1 for 1st sheet plus 25p each additional sheet.



## FAN/BLOWER

Precision-built in Germany. Dynamically balanced mains unit (200/240) continuous rated, reversible 60MA on run. Size: 5 1/2" dia. x 2 1/2" deep. Back plate is tapped for 4 fixing screws (supplied). Well under maker's price at £3. P. & P. 20p. Similar unit to above but 7 1/2" dia. x 3" deep. £4.90. P. & P. 25p.

### ALL PRICES INCLUDE V.A.T.

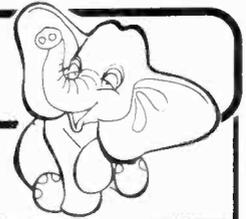
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### TEXAN 20 + 20 WATT IC STEREO AMPLIFIER

Features fibre glass PC board. Gardeners low field transformer. 6-ICs. 10 transistors plug diodes etc. Designed by Texas Instruments engineers for Henry's and P.W. 1972. Supplied with full chassis work, detailed construction handbook and all necessary parts. Full input and control facilities. Stabilised supply, overall size 15 1/4 in. X 2 1/4 in. X 6 5/8 in. mains operated. Free teak sleeve with every kit. **£31.00** (GB post paid). Built and tested **£37.50**



**STEREO FM TUNER**  
Features capacity diode tuning, led and tuning meter indicators, stabilized power supply—mains operated. High performance and sensitivity with unique station indication IC stereo decoder. Overall size in teak sleeve 8 in. X 2 1/4 in. X 6 5/8 in. Complete kit with teak sleeve **£21.00** (GB post paid). Build and tested **£24.95**

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<b>Amplifiers</b> (All single channel unless stated)	
4.300 9 volt 300 MW	£1.75
2004 9 volt 250 MW	£2.10
104 9 volt 1 watt	£3.10
304 9 volt 3 watt	£3.95
555 12 volt 3 watt	£4.10
555ST 12 volt 1 1/2 X 1 1/2 watt	£5.95
E1208 12 volt 5 watt	£5.10
608 24 volt 10 watt	£4.95
410 28 volt 10 watt	£4.95
620 45 volt 30 watt	£9.95
240 30/35 volt 15 watt	£5.45
Z60 45/50 volt 25 watt	£6.95
SA6817 24 volt 6+6 watt	£10.20

<b>Amplifiers with controls</b>	
E1210 12 volt 2 1/2 + 2 1/2 watts 8 ohms	£8.25
RE500 Mains 5 watts 4-16 ohms	£6.30
SAC14 Mains 7+7 watts 8 ohms	£11.75
SAC30 Mains 15+15 watts 8 ohms	£14.95
CA038 9 volt 1 1/2 + 1 1/2 watts 8 ohms	£6.95
CA068 12 volt 3+3 watts 8 ohms	£10.50

<b>FM Modules</b>	
Mullard LP 1186 FM tuner (front end) with data 10.7MHz o/p	£4.85
Mullard LP 1185 10.7MHz IF unit	£4.50
Gorier Permeability FM tuner (front end) 10.7MHz o/p	£4.20

<b>FM and AM tuners and decoders</b>	
FM 5231 (Iu 2) 6 volt FM tuner	£7.95
TU3 12 volt version (IFM use with decoder)	£7.95
SD4912 Stereo Decoder for Tu 3.12 volt	£7.95
SP62H 6 volt stereo FM tuner	£14.95
A1007 9 volt MW-AM tuner	£4.80
Sinclair 12/45 volt FM tuner stereo recorder for above	£7.45
A1018 9 volt FM tuner in cabinet	£13.95
A11005M (S) 9-12 volt stereo decoder FM for above	£7.50
1062 12 volt stereo decoder. General purpose	£6.50

<b>Preamplifiers</b>	
Sinclair Stereo 60 Preamplifier	£6.75
E1300 CART/TAPE/MIC INPUTS 9 volt	£2.85
E1310 Stereo 3-30mV mal cart 9 volt	£4.75
FF3 Stereo 3mV tape head 9 volt	£4.95
3402 Stereo 5-20mV Mag. cart. mains	£5.95
EQ25 Mono 3-250mV Tape/cart/flat 9 volt	£1.95
<b>Power Supplies—Mains input (*chassis-rest cased)</b>	
470C 6.75/9V 300mA	£7.80
with adaptors	£2.25
P500 9 volt 500mA	£3.20
HC244R 3/6/7 1/2 9 volt	£13.95
400mA stabilised	£5.50
*P11 24 volt 1/2 amp	£3.30
*P15 28 volt 1/2 amp	£3.30
*P1080 12 volt 1A	£4.70
*P1081 45 volt 0.9A	£7.80
P12 4 1/2-12 volt	£7.15
0-4-1 amp	£13.95
SE101A 3/6/8/12 volt	£12.75
1 amp stabilised	£12.75
P1076 3/4 1/2 6/7 1/2 9/12 volt 1/2 amp	£4.20
SE800A 1-15 volt 0-1A stabilised	£17.50

### 1250-watt Light

**Dimmer**  
£3.50 pp 20p  
MANUFACTURED BY ULTRA LTD  
Supplied with plate, knob + instructions.

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SR-2A 16 Projects	£7.70
SR-3A 100 Projects	£14.95
ST-45 45 Projects	£10.50
ST-100 100 Projects	£13.20

### Radionic Kits

X20 20 Projects	£5.70
X40 40 Projects	£12.75
X40A Add-on	£10.45

### Turner Kits

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50 in 1 50 Projects	£15.45
150 in 1 150 Projects	£23.65

### SINCLAIR MODULES AND KITS

ST80 stereo pre-amplifier	£11.95
Audio filter unit	£6.95
Z40 15 watt amplifier	£5.45
Z60 25 watt amplifier	£6.95
P25 power supplies for 1 or 2Z40	£4.98
P26 power supplies (STA3) for 1 or 2Z40	£7.98
P28 power supplies (STA3) for 1 or 2Z60	£7.98
Transformer for P28	£3.95
FM tuner	£11.95
Stereo decoder	£7.95
IC20 power amp kit	£7.95
PZ20 power supply for 1 or 2 IC20	£5.45

### Sinclair Project 80

<b>Package Deals</b> (Carriage/packing 35p)	
2 X Z40, S780, P25	£25.00
2 X Z60, S780, P26	£27.75
2 X Z60, S780, P28 +Trans.	£34.40
<b>Sinclair Special Purchases</b>	
* Project 80 stereo preamp/amplifier	£8.75 post 20p
* Project 605 kit	£19.95 post 25p
* Cambridge calculator kit	£13.50 post 15p

### EMI SPEAKERS Special Purchase

13 X 8 chassis speakers (carr/packing 30p ea or 50p pr) \*150 TC 10 watt 8 ohm twin cone **£2.20**

\*450 10 watt 4, 8, 15 ohm with twin tweeters and crossover **£3.85** each  
EW 15 watt 8 ohm with tweeter **£5.25**  
350 20 watt 8, 15 ohm with tweeter **£7.80** each  
\*Polished wood cabinet **£4.80** carr. etc. 35p each or 50p pair

### EXCLUSIVE 5 WATT IC AMPLIFIERS

Special purchase 5 watt output 8-16 ohm load, 30 volt max DC operation complete with data.  
Price **£1.50** ea or 2 for **£2.85**.  
Printed Circuit Panels **50p**.

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625-line receiver UHF transistors tuners FM. UK operation. Brand new. (Post/packing 25p each)  
TYPE C variable tuning **£2.50**  
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2 x 400mA/HR 50p p.p. 15p.

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for 8w fluorescent tube. Supplied with instr. and tube **£3.50** p.p. 30p.

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U4313 20KΩV with steel case	£12.50
U4317 20KΩV with case	£16.50
U4341 33KΩV plus transistor tester steel case	£10.50
U4323 20KΩV plus 1KHz 465KHz OSC with case	£7.70
ITH-2 20KΩV slim type TLI33D (L330K) 2KΩV robust	£7.50
TP55N 20KΩV (Case £2.00)	£8.25
TP510S 2KΩV	£5.25
TW20S 20KΩV	£10.00
TW50K 50KΩV	£11.25
EP10KN 10KΩV	£9.95
AF105 50KΩV De-luxe (Case £1.90)	£12.50
S100TR 100KΩV plus transistor tester	£22.50
New Revolutionary Supermeter 880R Multimeter	£18.50
*TE40 AC multivoltmeter	£18.75
† TE15 Grid dip meter 440KHz-28MHz	£19.95
† TE65 28 range valve voltmeter	£22.50
† TE200 RF generator 120KHz-500MHz	£18.95
† TX220 AF generator 20Hz-200KHz	£19.95
* HM350 In circuit transistor tester	£19.50
* C3025 De-luxe meter 1-300 MHz	£6.95
† T145 Compact transistor tester	£14.75
* C3042 SWR Meter	£5.75
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* SE400 Mini-lab all in one tester	£15.50
CI-5 Scope 500,000Hz (carr £1.00)	£43.00
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Marriot XRPS/7 1/2 track high	£2.50
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Marriot 1/2 tr. Erase 13 X 12E 343	£0.75
Marriot erase heads for XRPS 17/18/36 (XES)II	£0.75
R/RPI record/play 1/2 track	£0.45
H/RP single-track rec/play	£0.35
Bogen type UL290 erase	£1.50
ACY39	£0.78
AD149	£0.50
AD161	£0.44
AD162	£0.44
AF117	£0.24
AF118	£0.57
AF139	£0.20
AF186	£0.48
AF239	£0.44
ASY27	£0.33
BA15	£0.05
BAX13	£0.05
BC107	£0.14
BC108	£0.13
BC117	£0.14
1250R 12/55 2 p.c.o.	60p
1700R 18/24v 2 p.c.o.	p.p.
1800R 24v 4 p.c.o.	15p
2500R 18/24v 2 p.c.o.	
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1250R 12/55 2 p.c.o.	
1700R 18/24v 2 p.c.o.	
1800R 24v 4 p.c.o.	
2500R 18/24v 2 p.c.o.	
4000R 24v 2 p.c.o.	

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40p per pair p.p. 15p

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Plessey 5w Power Amp IC **£1.65** p.p. 15p

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£5.90 p.p. 25p  
TAA 960 40KHz AMP **£1.75** p.p. 15p

**VAT 8% EXTRA**  
Semi-conductors. Any one type or mixed SN 74 Series 'IC' 12 + EXTRA 10% 25 + EXTRA 15% 100 + EXTRA 20%

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SN7401N	0.16	SN7493N	0.70
SN7402N	0.16	SN7494N	0.16
SN7403N	0.16	SN7495N	0.80
SN7404N	0.26	SN7496N	0.95
SN7405N	0.22	SN7497N	3.87
SN7406N	0.42	SN74100N	1.89
SN7407N	0.42	SN74104N	0.58
SN7408N	0.28	SN74105N	0.53
SN7409N	0.28	SN74107N	0.45
SN7410N	0.16	SN74110N	0.58
SN7411N	0.25	SN74111N	0.86
SN7412N	0.30	SN74116N	1.89
SN7413N	0.36	SN74118N	0.90
SN7414N	0.36	SN74119N	0.68
SN7416N	0.36	SN74120N	0.95
SN7417N	0.36	SN74121N	0.50
SN7420N	0.16	SN74122N	0.70
SN7421N	0.33	SN74123N	1.00
SN7422N	0.25	SN74125N	0.65
SN7423N	0.37	SN74132N	0.72
SN7425N	0.37	SN74141N	0.90
SN7426N	0.37	SN74145N	0.75
SN7427N	0.37	SN74150N	1.75
SN7428N	0.40	SN74151N	1.00
SN7430N	0.16	SN74153N	0.95
SN7432N	0.37	SN74154N	1.00
SN7433N	0.37	SN74155N	1.00
SN7437N	0.37	SN74156N	1.00
SN7438N	0.37	SN74157N	0.95
SN7439N	0.37	SN74160N	1.00
SN7441N	0.92	SN74161N	1.38
SN7442N	0.79	SN74162N	1.38
SN7443N	1.27	SN74163N	1.38
SN7444N	1.27	SN74164N	1.75
SN7445N	1.60	SN74165N	1.76
SN7446N	1.89	SN74166N	1.80
SN7447AN	1.60	SN74167N	3.00
SN7448N	2.77	SN74170N	2.52
SN7449N	0.37	SN74171N	0.70
SN7451N	0.16	SN74174N	1.57
SN7453N	0.16	SN74175N	1.26
SN7454N	0.16	SN74176N	1.26
SN7455N	0.16	SN74177N	0.98
SN7470N	0.36	SN74180N	1.26
SN7472N	0.38	SN74181N	3.95
SN7473N	0.41	SN74182N	1.26
SN7474N	0.41	SN74186N	1.80
SN7475N	0.59	SN74185N	1.80
SN7476N	0.45	SN74190N	2.00
SN7480N	0.60	SN74191N	2.00
SN7482N	0.87	SN74192N	2.00
SN7483N	1.10	SN74193N	2.00
SN7484N	1.00	SN74194N	1.10
SN7485N	1.00	SN74195N	1.10
SN7486N	0.47	SN74196N	2.00
SN7489N	3.87	SN74197N	1.20
SN7490N	0.55	SN74198N	2.77
SN7491AN	1.00		

**G. F. MILWARD**

# ELECTRONIC COMPONENTS

Wholesale/Retail :

**369 Alum Rock Road, Birmingham B8 3DR. Tel. 021-327 2339**



## CALLING ALL INDUSTRIAL BUYERS!!



We are glad to say that it is now possible to supply from stock the following integrated circuits. **ALL ARE BRANDED, FULL SPECIFICATION** devices offered at unbeatable prices! This is **YOUR** chance to cut manufacturing costs and greatly increase profit margins!

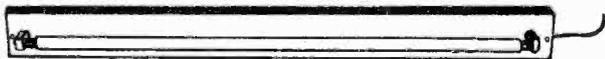
	1/99	100/499	500/1000		1/99	100/499	500/1000		1/99	100/499	500/1000
7400	£0-15	£0-125	£0-10	7442	£0-645	£0-43	7494	£0-495	£0-412	£0-33	
7401	£0-15	£0-125	£0-10	7443	£1-275	£0-85	7495	£0-63	£0-525	£0-42	
7402	£0-15	£0-125	£0-10	7445	£0-855	£0-57	7496	£0-72	£0-60	£0-48	
7403	£0-15	£0-125	£0-10	7446	£1-05	£0-70	74104	£0-315	£0-262	£0-21	
7404	£0-18	£0-15	£0-12	7446A	£1-05	£0-70	74105	£0-315	£0-262	£0-21	
7405	£0-18	£0-15	£0-12	7447	£1-05	£0-70	74107	£0-315	£0-262	£0-21	
7406	£0-375	£0-312	£0-25	7447A	£1-05	£0-70	74121	£0-315	£0-262	£0-21	
7407	£0-375	£0-312	£0-25	7448	£0-855	£0-57	74122	£0-45	£0-375	£0-30	
7408	10-15	£0-125	£0-10	7450	£0-125	£0-10	74123	£0-63	£0-525	£0-42	
7409	£0-15	£0-125	£0-10	7451	£0-15	£0-10	74141	£0-75	£0-625	£0-50	
7410	£0-15	£0-125	£0-10	7453	£0-15	£0-10	74151	£0-69	£0-575	£0-46	
7412	£0-195	£0-162	£0-13	7454	£0-15	£0-10	74153	£0-69	£0-575	£0-46	
7413	£0-345	£0-287	£0-23	7460	£0-15	£0-10	74155	£0-69	£0-575	£0-46	
7416	£0-345	£0-287	£0-23	7472	£0-255	£0-212	74156	£0-69	£0-575	£0-46	
7417	£0-345	£0-287	£0-23	7473	£0-153	£0-262	74160	£1-005	£0-837	£0-67	
7420	£0-15	£0-125	£0-10	7474	£0-315	£0-262	74161	£1-005	£0-837	£0-67	
7423	£0-27	£0-225	£0-18	7475	£0-465	£0-387	74162	£1-005	£0-837	£0-67	
7425	£0-27	£0-225	£0-18	7476	£0-315	£0-262	74163	£1-005	£0-837	£0-67	
7426	£0-27	£0-225	£0-18	7480	£0-435	£0-362	74166	£1-425	£1-187	£0-95	
7427	£0-27	£0-225	£0-18	7482	£0-75	£0-625	74174	£1-20	£1-00	£0-80	
7430	£0-15	£0-125	£0-10	7483	£0-125	£0-825	74175	£0-975	£0-812	£0-65	
7432	£0-25	£0-225	£0-18	7485	£1-275	£1-062	74192	£1-275	£1-062	£0-85	
7437	£0-27	£0-225	£0-18	7486	£0-315	£0-262	74193	£1-275	£1-062	£0-85	
7438	£0-27	£0-225	£0-18	7490	£0-465	£0-387	74198	£2-10	£1-75	£1-40	
7440	£0-15	£0-125	£0-10	7492	£0-465	£0-387	74199	£2-10	£1-75	£1-40	
7441A	£0-825	£0-687	£0-55	7493	£0-465	£0-387					

To secure the above prices, all orders for these devices must exceed £25 in total value. Price rating is established by TOTAL NUMBER OF DEVICES ORDERED. Any mix may be made. For special quotations for large orders ring 021-327 2339 NOW !!!

**MICROWAVE DEVICES**

CL8300	Gunn effect oscillator	9-4GHz	£40
CL8370	ditto	9-5GHz	£10
CL8380	ditto	10-5GHz	£10
CL8390	ditto	11-5GHz	£10
CL8430	ditto	9-35GHz	£40
CL8450	ditto	9-35GHz	£40
CL8470	ditto	9-35GHz	£40
BXY27	Varactor Diode. "S" Band. Cut-off	70GHz	£1
BXY28	Varactor Diode. Cut-off	100GHz	£1
BXY32	Frequency Multiplier. "X" Band	150GHz	£1
BXY35A/C	ditto	25GHz	£1
BXY36C/D	ditto	75GHz	£1
BXY37C/D	ditto	100GHz	£1
BXY38C/E	ditto	120GHz	£1
BXY39C/D	ditto	150GHz	£1
BXY40D/E	ditto	180GHz	£1
BXY41C/D/E	ditto	200GHz	£1

**12 VOLT FLUORESCENT LIGHTING**



Inverter transformers 13/15W (circuit included)	70p
"Current economy" transistor (600 ma.)	50p
"Maximum light" transistor (1-3A)	50p
Resistors/capacitors to suit	15p
Lampholders (long lead) (needed with cases)	Pair 30p
(short lead)	Pair 20p
White enamel case 21in (postage 30p)	70p
Tube. 21in-13W	45p
(Note: tube only supplied if case ordered, to prevent postal damage).	
13W fitting ready built and tested—including tube (postage 30p)	£3-75
Post/packing, 25p per order except where shown.	

**NEW! NEW! NEW! NEW!**

An aerosol spray providing a convenient means of producing any number of copies of a printed circuit both simply and quickly. Method: Spray copper laminate board with light sensitive spray. Cover with transparent film upon which circuit has been drawn. Expose to light. (No need to use ultra-violet.) Spray with developer, rinse and etch in normal manner. Light sensitive aerosol spray **£1-00** plus **50p** postage Developer and Etchant **50p** postage

Single-sided Copper-clad Fibreglass Board **75p** sq. ft. Double-sided Copper-clad Fibreglass Board **£1-00** sq. ft. Boards cut to any multiple of 6". Max. size 3' x 4'.

**1,000,000**

**POTENTIOMETERS**

We have bought a huge assortment of volume controls.

Pre-sets, sliders, etc. All are in manufacturer's original packing.

Manufacturing quantities of some types available.

Write or phone for details.

**Sample bag 100 mixed £2-50**

**ELECTROLYTIC CAPACITORS**

Several thousand of each of the following types. Silly price to clear!

**ALL NEW STOCK**

5µf 10V	35p dozen
10µf 10V	35p dozen
50µf 10V	35p dozen
100µf 10V	35p dozen
330µf 16V	45p dozen
330µf 25V	60p dozen
330µf 35V	80p dozen
2200µf 16V	£1 dozen
15000µf 25V	50p each

**HOBBY CORNER!**

**BRAN TUB !!!**

- ★ Resistors, Wire-wound and Carbon
- ★ Capacitors, Silver-mica, Paper, Ceramic, Polyester and Electrolytic
- ★ Controls, Volume, Pre-set, Carbon, Wire
- ★ Diodes, Silicon, Germanium, Zener
- ★ Transistors, Silicon, Germanium

All the above are new and unused stock.

We have made up packs of 2lb gross weight, all are different in content, and contain a mixture of components from the above list. This is a fantastic, unrepeatable offer that will enable you to get a good stock of spares at a tiny fraction of normal price!

To make things even more interesting — TWENTY OF THESE BAGS ALSO CONTAIN A POUND NOTE! TWENTY CUSTOMERS WILL BE VERY PLEASED INDEED!

And the price that we are asking? Only **£1-50** including both postage and VAT!

Rush your order now! This offer is only made to reduce our surplus stock! It is unlikely that in these days of rising prices we shall ever be able to repeat!

**£1** 100 1/2 WATT RESISTORS  
100 CERAMIC CAPACITORS  
100 DIODES

POSTAGE 25p  PACK No. 1

**£1** 100 RESISTORS  
100 CERAMIC CAPACITORS  
100 POLYSTYRENE CAPACITORS

POSTAGE 25p  PACK No. 2

**£1** 100 RESISTORS  
100 CERAMIC CAPACITORS  
50 MULLARD POLYESTER CAPACITORS

POSTAGE 25p  PACK No. 4

**£1** 20 ASSORTED UNUSED, MARKED, TESTED TRANSISTORS BC108 ETC.

POSTAGE 25p  PACK No. 5

**£1** 1 TRANSISTORISED SIGNAL TRACER KIT  
1 TRANSISTORISED SIGNAL INJECTOR KIT

POSTAGE 25p  PACK No. 6

**£1** 100 RESISTORS  
100 CAPACITORS (ASSORTED TYPES)

POSTAGE 25p  PACK No. 8

**REMEMBER! ALL GOODS PLUS 8% V.A.T.**

**G. F. MILWARD, 369 Alum Rock Rd., Birmingham B8 3DR. Postage (minimum) per order 25p.**

# SERVICE TRADING CO

## VARIABLE VOLTAGE TRANSFORMERS

Carriage extra

INPUT 230 v. A.C. 50/60  
OUTPUT VARIABLE 0/260 v. A.C.  
BRAND NEW. All types.  
200W (1 Amp) ..... £9.00  
0.5 KVA (Max. 2½ Amp) ..... £10.00  
1 KVA (Max. 5 Amp) ..... £14.70  
2 KVA (Max. 10 Amp) ..... £28.10  
3 KVA (Max. 15 Amp) ..... £31.25  
4 KVA (Max. 20 Amp) ..... £72.50  
(Max. 37.5 Amp) ..... £102.50  
1 Amp OPEN TYPE  
(Panel Mounting) ..... £9.00



## 300 VA ISOLATING TRANSFORMER

115/230-230/230 volts. Screened. Primary two separate 0-115 volts for 115 or 230 volts. Secondary two 115 volts at 150 VA each for 115 or 230 volts output. Can be used in series or parallel connections. Fully tropicalised. Length 13.5 cm. Width 11 cm. Height 13.5 cm. Weight 15 lb. SPECIAL OFFER PRICE Only £5.00. Carr. 80p.

## VENNER TIME SWITCH TYPE MSQP

200/250 Volt 2-ON/2-OFF every 24 hours at any manual pre-set time. 20 amp contacts. Fitted die-cast case. Tested and in good condition. £4.75 Post 25p.



## A.C. MAINS TIMER UNIT

Based on an electric clock, with 25 amp. single-pole switch, which can be preset for any period up to 12 hrs. ahead to switch on for any length of time, from 10 mins. to 6 hrs. then switch off. An additional 60 min. audible timer is also incorporated. Ideal for Tape Recorders, Lights, Electric Blankets, etc. Attractive satin copper finish. Size 135 mm X 130 mm X 60 mm. Price £2.00. Post 20p. (Total inc. VAT & Post £2.38).



## UNISELECTOR SWITCHES - NEW

4 BANK 25 WAY FULL WIPER 25 ohm coil, 24v. D.C. operation £6.90. Post 30p.  
8 BANK 25 WAY FULL WIPER 25 ohm coil, 24 v. D.C. £7.90. Post 30p.  
8 BANK 25 WAY FULL WIPER 24 v. D.C. operation £9.50. Post 40p.



## MINIATURE UNISELECTOR SWITCH

2 Bank, 12 position. 24 volt D.C. operation. Full wiper with ancillary contacts. NEW Price £2.50 Post 20p. As above but with 5 Bank, 12 position. Price £3.50 Post 20p.



PROGRAMME TIMERS 230/240 Volt A.C. 15 RPM Motors. Each cam operates a c/o micro switch. Ideal for lighting effects, animated displays etc. Ex equipment tested. 2 cam model £2.00 post 30p. 4 cam model £2.50 post 30p.

## VERY SPECIAL OFFER

Miniature Roller Micro Switch. 5 amp. c/o contacts. NEW. Price 10 for £1.50. Post 10p. (Min. order 10.) As above less roller/lever 20 for £2.00. Post 10p. (Min. order 20.) Ditto. Press to make. 20 for £1.50 Post 10p. Ditto. Press to break. 20 for £1.50 Post 10p.



## 'HONEYWELL' PUSH BUTTON, PANEL MOUNTING MICRO SWITCH ASSEMBLY

Each bank comprises of a change-over rated at 10 amps 240 volt A.C. Black knob 1 in. dia. Fixing hole ½ in. Prices: 1-bank 30p, 2-bank 40p, 3-bank 50p. (Illustrated) Inc. P. & P. Special quotes for quantities.



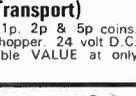
## 240 V.A.C. SOLENOID OPERATED FLUID VALVE

Rated 1 p.s.i. will handle up to 7 p.s.i. Forged brass body, stainless steel core and spring ¼ in. b.s.p. inlet/outlet. Precision made. British mfg. PRICE: £2.00. Post 25p. NEW original packing.



## COIN MECHANISM (Ex-London Transport)

Unit containing, selector mechanism for 1p, 2p & 5p coins. Micro switches, relays, solenoid-operated hopper. 24 volt D.C. Precision built to high standard. Incredible VALUE at only £2.50 Post 60p.



## 230-250 VOLT A.C. SOLENOID

Similar in appearance to illustration. Approximately 1½ lb. pull. Size of feet 1½" X 1½". Price £1.00 Post 15p.



## 24 VOLT DC SOLENOIDS

UNIT containing: 1 heavy duty solenoid approx. 25 lb. pull at 1 in. travel. 2 solenoids of approx. 1 lb. pull at ½ in. travel. 6 solenoids of approx. 4 oz. pull at ¼ in. travel. Plus 1 24V D.C. 1 heavy duty 1 make relay. Price: £2.50. Post 60p. ABSOLUTE BARGAIN.

## High Visibility Panel Mounting LEDs

25 inch mounting, .16 inch lens. Typical parameters 2 volt 20 m.a. all types. Supplied complete with snap in mountings and data. Red 4 for £1.00, Green 3 for £1.00, Yellow 3 for £1.00. Post 10p. (Min. order £1.00.)

## LED READOUTS

7 series 1/8 DP ¼" high characters. 14-pin D.C.L. Available in red or green. £1.65, post 10p; 4 for £6.00 post paid.



# POWER RHEOSTATS

New ceramic construction, vitreous enamel embedded winding, heavy duty brush assembly, continuously rated.  
25 WATT 10, 25, 100, 150, 500. 1k ohm. £1.15 Post 10p.  
50 WATT 1, 5, 10, 25, 50, 100, 500 ohm £2.35 Post 15p.  
100 WATT 1/10/25/50/100/250/500/1K/1.5K/2.5K/5k ohm £1.60 Post 10p.  
Black Silver Skirted knob calibrated in Nos. 1-9, 1½ in. dia. brass bush. Ideal for above Rheostats, 22p ea.

# STROBE! STROBE! STROBE!

FOUR EASY TO BUILD KITS USING XENON WHITE FLASH TUBES, SOLID STATE TIMING + TRIGGERING CIRCUITS, PROVISION FOR EXTERNAL TRIGGERING. 230-250V. A.C. OPERATION.  
EXPERIMENTERS "ECONOMY" KIT  
Adjustable 1 to 30 Flash per sec. All electronic components including Xenon Tube + instructions £6.30. Post 30p.  
INDUSTRIAL KIT  
Ideally suitable for schools, laboratories etc. Roller lin printed circuit. Adjustable 1-80 f.p.s., approx. ½ output of Hy-Light. Price £14.00. Post 50p.  
HY-LITE STROBE Mk IV  
Designed for use in large rooms, halls and utilizes a silica tube, printed circuit. Speed adjustable 1-20 f.p.s. Light output greater than many (so called 4 Joule) strobes. Price £14.00. Post 50p.  
'SUPER' HY-LIGHT KIT  
Approx. 4 times the light output of our well proven Hy-Light strobe.  
Variable speed from 1-13 flash per sec.  
Reactor control circuit producing an intense white light. ONLY £22.00. Post 75p.  
ATTRACTIVE, ROBUST, FULLY VENTILATED METAL CASE for the Super Hy-Light Kit including reflector. £8.00. Post 60p.  
FOR HY-LIGHT STROBE incl. reflector, £5.75. Post 25p.

# COLOUR WHEEL PROJECTOR

Complete with oil filled colour wheel. 100 watt lamp. 200/240V A.C. Features extremely efficient optical system. £20.50. Post 50p.



# I.R.P.M. MOTOR and COLOUR WHEEL

200/240 volt A.C. 15 rpm motor, and wheel £5.60. Post 40p. (Motor not available separately.)  
6 INCH COLOUR WHEEL ONLY. Price £4.50. Post 30p.

# BIG BLACK LIGHT

400 Watt. Mercury vapour ultra violet lamp. Extremely compact and powerful source of u.v. Innumerable industrial applications also ideal for stage, display, discos etc. P.F. ballast is essential with these bulbs. Price of matched ballast and bulb £16.00. Post £1. Spare bulb £7.00. Post 40p.

# BLACK LIGHT FLUORESCENT U.V. TUBES

4ft. 40 watt. Price £5.50. (Callers only). 2ft. 20 watt £4.25. Post 25p. (For use in stan bi-pin fittings.) MINI 12in. 8 watt £1.60. Post 15p. 9in. 6 watt £1.30. Post 15p. Complete ballast unit and holders for either 9" or 12" tube. £1.70 Post 25p. (9in. x 12in. measures approx.)

# U.D.1. SINGLE CHANNEL. 750 watt MANUAL/AUTO DIMMER

750W Solid State Fader, with three functions. Manual fade: Auto fade-up; Auto fade-down. Automatic cycling up and down. Functions selected with 'three position' rocker switch. Two ranges of cycling for 'Flashing' or 'Slow blending'. Ready built module 6" X 3" glass fibre board incorporating 10 amp TRIAC. Two or more modules for top quality colour blending and flashing effects. PRICE £15.00 Post 30p.

# GENERAL ELECTRIC POWERGLAS TRIACS

10 amp. Glass passivated plastic Triac. Latest device from U.S.A. Long term reliability. Type SC 146E 10 amp. 500PIV. £1.00 Post 5p. (Inclusive of data and application sheet) suitable Diac 18p.

# INSULATION TESTERS (NEW)

Test to I.E.E. Spec. Rugged metal construction, suitable for bench or field work, constant speed clutch. Size L. 8 in., W. 4 in., H. 6 in., weight 9 lb.  
500 VOLTS, 500 megohms £28.00. Post 60p.  
1,000 VOLTS, 1,000 megohms £34.00. Post 60p.



# VAT 8% VAT. (8p in the £)

To all orders add 8% VAT to total value of goods including carriage/packaging.

## INSULATED TERMINALS

Available in black, red, white, yellow, blue and green. New 12p each incl. P & P. Minimum order 6.



## RELAYS

SIEMENS PLESSEY, etc. MINIATURE RELAYS			
1	2	3	4
58	5-9	6 c/o	80p
150	4-9	2 c/o	70p*
185	8-12	6 M	60p*
308	9-14	4 c/o	75p*
410	12-20	4 c/o	80p*
700	16-24	4M2B	60p*
700	16-24	4 c/o	80p*
2500	36-45	6 M	60p*
2500	31-43	2 c/o HD	60p*
9000	40-70	2 c/o	60p*
15k	85-110	6 M	60p*

(1) Coil ohms; (2) Working d.c. volts; (3) Contacts; (4) Price HD=Heavy Duty. All Post Paid. (\*Including Base)

## OPEN TYPE RELAYS

6 VOLT D.C. 1 make con. 35p. Post 10p.  
9 VOLT D.C. RELAY 3 c/o 5 amp contacts. 70 ohm coil 75p. Post 10p.  
12 VOLT D.C. RELAY 3 c/o 5 amp contacts 120 ohm coil 75p. Post 10p.  
24 VOLT D.C. 3 c/o 600 ohm coil 75p. Post 10p.  
2 HD c/o 700 ohm coil 75p. Post 10p.  
4 c/o 300 ohm coil 85p. Post 10p.  
100 VOLT A.C. 2 c/o sealed type, octal base 75p. Post 10p.

## PLASTIC COVERED RELAYS

24 VOLT D.C. 3 h.d. c/o contacts 95p. Post 10p.  
24 VOLT A.C. Mfg. by IIT 2 h.d. c/o contacts. 55p. Post 10p. 3 h.d. c/o 65p. Post 10p.  
240 VOLT A.C. RELAY IIT 240V. A.C. heavy duty c/o contacts. Octal plug in base. Price 75p. Post 10p.  
220/240 VOLT AC RELAY 3 c/o 5 amp cont. Sealed, incl. 11-pin base. £1.25. Post 10p.  
ARROW 230/240V AC 2 c/o 15 amp contacts. Amp connectors. £1.00 Post 10p.

## 110 VOLT A.C. 2 c/o. 20 amp. £1.25 Post 10p.

## CLARE-ELLIOT TYPE RP 7641 G8

Miniature relay. 675 ohm coil. 24 volt D.C. 2 c/o. 70p. Post Paid.

## MANY OTHERS FROM STOCK. PHONE FOR DETAILS.



BLOWER UNIT 200-240 Volt A.C. BLOWER UNIT Precision German built. Dynamically balanced, quiet, continuously rated, reversible motor. Consumption 60mA. Size 120mm. dia. x 60mm. deep. Price £3.00. Post 30p.

## PRECISION CENTRIFUGAL BLOWER

Mfg. Airflow Developments Ltd., Heavy Duty, continuously rated, smooth running, 230/240V A.C. motor. Size: 15 x 14 cm. (case only) OAL 15 cm. Aperture 6 X 6 cm. £6.50. Post 50p.



## 230/240 VOLT A.C. EXTRACTOR FAN KIT

Comprising of impeller, continuously rated motor, motor housing and fixings as illustrated. Price £1.75 Post 25p. (Total inc. VAT & Post £2.16)



## 230V FAN ASSEMBLY

Continuously rated, removable aluminium blades. Price £1.00 Post 20p.



## 230/240V SYNCHRONOUS GEARED MOTOR

BODINE TYPE N.C.I. GEARED MOTOR

(Type 1) 71 r.p.m. torque 10 lb. in. Reversible 1/70th h.p. cycle .38 amp.  
(Type 2) 28 r.p.m. torque 20 lb. in. Reversible 1/80th h.p. 50 cycle .28 amp. The above two precision made U.S.A. motors are offered in as new condition. Input voltage of motor, 115V A.C. Supplied complete with transformer for 230/240V A.C. input. Price, either type £6.25 Post 50p. or less transformer £3.75 Post 40p. These motors are ideal for rotating aerials, drawing curtains, display stands, vending machines, etc. etc.



## 'FRACMO' 240VOLT A.C. 50 cycle SINGLE PHASE GEARED MOTOR

33 r.p.m. 30 lb. ins. Reversible, fitted with mounting feet. Brand New. £14.00 Post 60p. (Total price incl. VAT £15.77)



## 600 WATT DIMMER SWITCH

Easily fitted. Fully guaranteed by makers. Will control up to 600 watts of all lighting except fluorescent at mains voltage. Complete with simple instructions. £2.75. Post 25p.

## 2000 WATT POWER CONTROL

For Power tools. Heating. Lighting etc. incorporating 13 amp. outlet and mains lead. £8.00 Post 27p.

## 'GENTS' 6" ALARM BELL

200/250 volt AC/DC. Brand New. Price: £5.00 Post 60p. (Illustrated)

## 'STC' 6" RED ALARM BELL

Brand New. Price: £4.00 Post 50p. 24/48V DC.



## METERS NEW! 2½in. FLUSH ROUND

available as D.C. Amps 1, 5, 10, 15 or A.C. Amps 1, 5, 10, 15, 20. Both types £2.00. Post 15p.  
VOLTMETER 0-300V. A.C. £2.00. Post 15p.



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OB2 0.40	6AX4 0.75	6BG 2.00	12AV8 0.50	30P4MR 1.00	EBL21 2.00	N308 1.00	PY33/2 .50	UY41 0.45	Transistors	AF121 0.38	BYZ13 0.28	OA211 0.75
024 0.47	6BB6 0.30	6L1 2.00	12AX7 0.33	ARP3 0.80	EC52 1.00	N339 1.10	PY80 0.40	UY42 0.45	and Diodes	AF124 0.28	BYZ15 1.83	OC19 1.38
1A3 0.45	6BA6 0.28	6L6GT 2.00	12AY7 0.70	30P12 0.60	ATP4 0.50	P61 0.35	PY81 0.35	UY85 0.35	IN1124A .58	AF125 0.19	CG12E 0.23	OC22 0.42
1A5GT 0.50	6BC8 0.30	6L7M 0.50	12BA8 0.45	30P19/ 0.50	AZ1 0.25	PABC80 .38	PY82 0.35	U16 1.00	IN4744A .15	AF126 0.20	CG64H 0.22	OC23 0.42
1A7GT 0.65	6BE6 0.35	6L8 0.50	12BA9 0.40	30P4 0.75	AZ31 0.30	EC88 0.60	PY83 0.38	U12/14 1.00	IN4952 0.55	AF139 0.72	F8Y11A .25	OC24 0.42
1B3GT 0.50	6BG6G 1.05	6L19 2.00	12BB8 0.50	30P11 0.85	AZ41 0.25	EC88 0.70	PY88 0.40	U16 1.00	2N404 0.20	AF178 0.75	F8Y11A .25	OC25 0.42
IC2 0.70	6BH6 0.60	6L12 2.00	12BH7 0.50	30P113 .95	BL53 2.00	EC92 0.45	PY80 0.75	U17 0.75	2N3956 0.58	AF180 0.62	GD4 0.36	OC28 0.46
IG6 1.00	6BJ6 0.55	6L20 0.75	12E1 3.00	30P114 1.10	CL33 1.60	EC93 1.50	PY80 0.40	U18/20 1.00	2N3176 0.55	AF186 0.81	GD5 0.34	OC29 0.46
1HG5T 0.60	6BK7A 0.80	6N7GT 0.60	12K5 1.00	30P115 .90	CV8 0.53	EC92 1.50	PY80 0.40	U19 2.50	2N2147 0.94	AF239 0.42	GD6 0.31	OC36 0.47
1L4 0.28	6BQ5 0.31	6PL12 0.34	12K7GT .50	35A3 0.65	CV63 0.75	EC93 0.95	PY80 0.40	U22 0.75	2N2297 0.25	ASV27 0.47	GD8 0.22	OC38 0.47
1LD5 0.60	6BQ7A 0.55	6Q7G 0.50	12L9GT .50	35A5 0.80	CV988 .25	EC94 1.00	PY80 0.40	U26 0.68	2N2369A .15	ASV28 0.36	GD9 0.22	OC41 0.55
1LN5 0.80	6BR7 1.40	6Q7GT 0.50	12M7GT .50	35C5 0.75	Y1C 1.00	EC94 1.00	PY80 0.40	U28 0.68	2N2613 0.45	ASV29 0.55	GD11 0.22	OC42 0.69
1NSGT 0.85	6BR8 1.50	6Q7M 0.55	12Q7GT .45	35D5 0.75	Y1C 1.00	EC98 0.33	PY80 0.40	U31 1.50	2N3053 0.38	BA102 0.50	GD12 0.22	OC43 1.30
IR5 0.45	6BT7 1.40	6R7G 0.60	12S4GT .55	35L6GT .75	D63 0.25	EC98 0.33	PY80 0.40	U33 1.50	2N3121 2.75	BA115 0.45	GD14 0.55	OC44 1.10
184 0.33	6BW6 0.30	6W4 0.44	12S6GT .50	35W4 0.50	DAC32 .90	EC98 0.33	PY80 0.40	U35 1.50	2N3176 0.55	BA116 0.45	GD5 0.34	OC45 0.42
185 0.30	6BW7 0.70	6SA7 0.44	12S7GT .50	35Z3 0.75	DAF96 0.50	EC98 0.33	PY80 0.40	U37 1.75	2N3709 0.25	BA129 0.14	GD16 0.22	OC46 0.17
1U4 0.60	6BX6 0.28	6SC7GT .33	12S8GT .50	35Z4GT .75	DC90 0.60	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
1U5 0.75	6BY7 0.34	6SG7 0.44	12S9GT .50	42 0.50	DF91 0.30	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
2D21 0.45	6BZ6 0.40	6SH7 0.44	12S9GT .50	50B5 0.85	DF96 0.50	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
2GR5 0.55	6C4 0.35	6SJ7 0.55	12S9GT .50	50B5 0.85	DF96 0.50	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
2X2 0.60	6C50 0.50	6SK7GT .44	12S9GT .50	50B5 0.85	DF96 0.50	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
3A4 0.50	6C6 0.45	6YD7GT .50	12S9GT .50	50B5 0.85	DF96 0.50	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
3B7 0.45	6C9 1.00	6U4GT 0.70	12S9GT .50	50B5 0.85	DF96 0.50	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
3BD 0.40	6C9A 0.40	6U7G 0.45	12S9GT .50	50B5 0.85	DF96 0.50	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
3C6 0.60	6C12 0.33	6V6G 0.17	14H7 0.80	72 0.80	DK40 0.65	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
3Q4 0.60	6C12 0.33	6V6G 0.17	14H7 0.80	72 0.80	DK40 0.65	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
3Q5GT 0.55	6C17 0.28	6V9GT 0.45	14H7 0.80	72 0.80	DK40 0.65	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
384 0.40	6CD6G 1.25	6X4 0.40	18 1.00	85A2 0.60	DK92 0.70	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
3V4 0.70	6CG8A 0.75	6X5GT 0.45	18AQ5 0.50	85A3 0.60	DK96 0.60	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
4CB6 0.55	6CL6 0.65	6Y6G 0.50	19BG6G 0.80	90AG 2.50	DL92 0.40	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
5CG8 0.55	6CLA 0.80	6Y7G 1.00	19BG6G 0.80	90C 2.40	DL94 0.70	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
5R4GY 0.80	6CM7 0.75	7A7 1.00	19BG6 1.00	90CV 2.40	DL96 0.55	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
5T4 0.40	6CU5 0.75	7B6 0.75	19H1 2.00	90C1 0.75	DM70 0.60	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
5U4G 0.40	6CW4 1.00	7B7 0.70	20D1 0.60	150B2 0.75	DM71 1.50	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
5V4G 0.50	6D3 0.60	7F8 1.50	20D2 2.00	215B8 0.50	DM74/350 1.00	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
5Y3GT 0.45	6E7 0.75	7H7 0.75	20P2 0.75	301 1.00	302 1.00	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
5Z3 0.75	6E7 0.75	7H7 0.75	20P2 0.75	301 1.00	302 1.00	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
5Z4G 0.45	6E7 0.75	7H7 0.75	20P2 0.75	301 1.00	302 1.00	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
5Z4GT 0.45	6E7 0.75	7H7 0.75	20P2 0.75	301 1.00	302 1.00	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6/30L2 0.80	6F1 0.75	7Z4 0.80	20P4 1.00	807 1.00	807 1.00	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6AG 1.25	6F6G 0.50	9BW6 0.75	20P5 1.00	856 0.30	853F 1.30	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6A7 0.40	6F12 0.37	9D7 0.65	25A6G 0.60	1821 1.00	EB8CC 0.75	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6A8 0.40	6F13 0.70	10C2 0.65	25L6G 0.60	4033X 0.50	E92CC 0.80	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6A9 0.40	6F14 0.75	10D1 0.70	25Y5 0.80	5702 1.00	E180C 0.70	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6A95 0.27	6F15 0.65	10E7 0.75	25Y6G 0.80	6057 1.00	E180F 1.00	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6A16 0.60	6F18 0.55	10P1 0.75	25Z4G 0.40	6060 1.00	E182CC1.25	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6AJ5 0.33	6F18 0.55	10P1 0.75	25Z4G 0.40	6060 1.00	E182CC1.25	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6AJ8 0.33	6F18 0.55	10P1 0.75	25Z4G 0.40	6060 1.00	E182CC1.25	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6AK5 0.40	6F23 0.80	10P9 0.65	25Z5 0.80	6067 1.00	E1148 0.58	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6AK6 0.60	6F24 0.85	10P18 0.55	25Z6G 0.70	7193 0.53	EA50 0.27	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6AK8 0.38	6F25 1.00	10L14 0.45	28D7 1.00	7475 1.00	EA76 1.00	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6AL5 0.20	6F26 0.34	10LD11 .70	30A5 0.65	9006 0.30	EABC80 1.00	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6AM8A 0.55	6F28 0.67	10LD12 .40	30C1 0.40	9002 0.50	EABC80 1.00	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6AN8 0.70	6F28 0.67	10LD12 .40	30C1 0.40	9002 0.50	EABC80 1.00	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6AQ5 0.45	6G6G 0.50	10P12 .38	30C13 0.50	A1834 1.00	EAC91 0.75	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6A28 0.40	6G8A 0.75	10P12 .38	30C13 0.50	A2134 1.00	EAF42 0.75	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6AR5 0.60	6GK5 0.75	10P18 0.42	30F5 0.80	AC3042 1.00	EAF801 0.75	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6AR6 1.00	6H6GT 0.25	12AC6 0.70	30FL2 0.67	AC2PEN 1.00	EB34 0.25	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6AT7 1.00	6J5GT 0.45	12AD6 0.65	30FL2 0.67	AC2PEN 1.00	EB91 0.20	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6B7 0.40	6J6 0.30	12AE6 0.65	30FL13 .55	AC6/PEN 0.60	EB91 0.20	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6A76 0.30	6J7G 0.30	12AT6 0.40	30FL14 .75	AC/PEN(7) 1.00	EB91 0.20	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6A76 0.30	6J7M 0.45	12AT7 0.34	30LI 0.40	AC/PEN(7) 1.00	EBF80 0.39	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6AY6 0.45	6JU8A 0.75	12AU6 0.45	30LI5 0.75	AC/TH11-00	EBF89 0.32	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17
6AW8A 0.85	6K7G 0.30	12AU7 0.33	30LI7 0.70	AC/TH11-00	EL37 2.50	EC98 0.33	PY80 0.40	U47 0.55	2N3866 1.10	BA130 0.11	GD16 0.22	OC46 0.17

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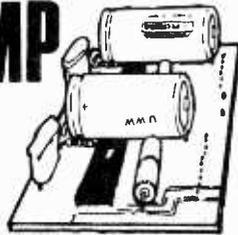


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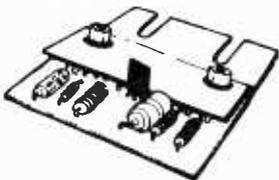
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**REDIFON TELEPRINTER RELAY UNIT NO. 12:** ZA-41196 and power supply 200-250V a.c. Polarised relay type 3SEITR. 80-0-80V 25mA. Two stabilised valves CV 286. Centre Zero Meter 10-0-10. Size 8in. x 8in. x 8in. New condition. £8.50. Carr. 75p.

**AUTO TRANSFORMER:** 230V 50c/s, 1000 watts. Mounted in strong steel case 5in. x 6in. x 7in. Bitumen impregnated. £10 each, Carr. £1.

**TELEPRINTER TYPE 7B:** Pageprinter 24V d.c. power supply, speed 50 bauds per min. 'as new' cond. in original packing case, £25 each; or second hand cond. (excellent order) no parts broken, £15 each. Carriage either type £3-00.

**INSULATION TEST SET:** 0-10 kV negative, earth with amplifier provision for checking ionisation. 110/230V a.c. input. S/hand good cond. £30 + £1 carr.

**BRIDGE MEGGER:** 250V. (Evershed Vignoles) series 2. £30 each. Carr. £1.

**BRIDGE MEGGER:** 2,500V., series 1. £30 each. Carr. £1.

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**TYPE 174/1 FREQUENCY SHIFT ADAPTOR** (Northern Radio Co.): Convert. mark and space frequencies from the output of one or two Receivers into d.c. pulses. Suitable to operate Teleprinters or similar devices. 110/220V. Further details on request, s.a.e. £55 each. Carr. £1.50.

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**MUIRHEAD PAMETRADA WAVE ANALYSER D-489-EM:** Primarily used for the analysis of complex vibration waveforms but will measure audio and power frequency waveforms from 19Hz-21KHz. Complete with power supply unit 230V 50Hz. Secondhand, good condition. £90. Carr. £3.

**FURZHILL SENSITIVE VALVE VOLTMETER V.200:** Freq. 10Hz-6MHz (can be used beyond 6MHz). Probe in circuit—voltage range 1mV-1kV in 6 decade ranges; full scale deflection 10mV, 100mV-1kV. Without probe 100µV-100V in 6 decade ranges; full scale deflection 1mV, 10mV-100V. Accuracy ±5%. £30 each. Carr. £1.

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**ROHDE & SCHWARZ HF MILLIVOLTMETER:** 30Hz-30MHz Type UVH, 1mV-1V in 7 ranges, 220V. £75 each. Carr. £2.

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**SIGNAL GENERATOR AIRMEC TYPE 701:** 30KHz-30MHz, 7 ranges. £65. Carr. £1.50.

**TF-1278/1 TRAVELLING TUBE WAVE AMPLIFIER:** £125. Carr. £2.

**BPL A.C. MILLIVOLTMETER TYPE VM.348-D Mk. 3:** 2 millivolts-2 volts, 6 ranges. £30. Carr. £1.

**WAYNE KERR WAVEFORM ANALYSER A.321:** Low scale 0-1200 c/s. High scale 1-20 Kc/s, 600 ohms. Harmonic level is 0-55 dB in 12 steps. £75. Carr. £1.50.

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**MARCONI DUAL TRACE UNIT TM-6456:** £30. Post 60p.

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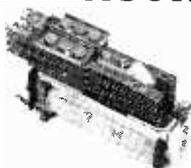
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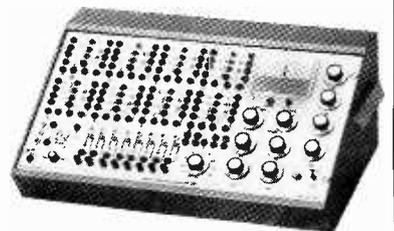
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PCF821	0.80	Y828	0.45
PCF822	0.80	Y829	0.45
PCF823	0.80	Y830	0.45
PCF824	0.80	Y831	0.45
PCF825	0.80	Y832	0.45
PCF826	0.80	Y833	0.45
PCF827	0.80	Y834	0.45
PCF828	0.80	Y835	0.45
PCF829	0.80	Y836	0.45
PCF830	0.80	Y837	0.45
PCF831	0.80	Y838	0.45
PCF832	0.80	Y839	0.45
PCF833	0.80	Y840	0.45
PCF834	0.80	Y841	0.45
PCF835	0.80	Y842	0.45
PCF836	0.80	Y843	0.45
PCF837	0.80	Y844	0.45
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PCF853	0.80	Y860	0.45
PCF854	0.80	Y861	0.45
PCF855	0.80	Y862	0.45
PCF856	0.80	Y863	0.45
PCF857	0.80	Y864	0.45
PCF858	0.80	Y865	0.45
PCF859	0.80	Y866	0.45
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PCF861	0.80	Y868	0.45
PCF862	0.80	Y869	0.45
PCF863	0.80	Y870	0.45
PCF864	0.80	Y871	0.45
PCF865	0.80	Y872	0.45
PCF866	0.80	Y873	0.45
PCF867	0.80	Y874	0.45
PCF868	0.80	Y875	0.45
PCF869	0.80	Y876	0.45
PCF870	0.80	Y877	0.45
PCF871	0.80	Y878	0.45
PCF872	0.80	Y879	0.45
PCF873	0.80	Y880	0.45
PCF874	0.80	Y881	0.45
PCF875	0.80	Y882	0.45
PCF876	0.80	Y883	0.45
PCF877	0.80	Y884	0.45
PCF878	0.80	Y885	0.45
PCF879	0.80	Y886	0.45
PCF880	0.80	Y887	0.45
PCF881	0.80	Y888	0.45
PCF882	0.80	Y889	0.45
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PCF884	0.80	Y891	0.45
PCF885	0.80	Y892	0.45
PCF886	0.80	Y893	0.45
PCF887	0.80	Y894	0.45
PCF888	0.80	Y895	0.45
PCF889	0.80	Y896	0.45
PCF890	0.80	Y897	0.45
PCF891	0.80	Y898	0.45
PCF892	0.80	Y899	0.45
PCF893	0.80	Y900	0.45
PCF894	0.80	Y901	0.45
PCF895	0.80	Y902	0.45
PCF896	0.80	Y903	0.45
PCF897	0.80	Y904	0.45
PCF898	0.80	Y905	0.45
PCF899	0.80	Y906	0.45
PCF900	0.80	Y907	0.45

PL509	1.35	U191	0.75
PL802	0.95	U801	0.75
PY33	0.60	UACB80	0.40
Y80	0.40	Y80	0.40
Y81	0.40	Y81	0.40
Y82	0.40	Y82	0.40
Y83	0.40	Y83	0.40
Y84	0.40	Y84	0.40
Y85	0.40	Y85	0.40
Y86	0.40	Y86	0.40
Y87	0.40	Y87	0.40
Y88	0.40	Y88	0.40
Y89	0.40	Y89	0.40
Y90	0.40	Y90	0.40
Y91	0.40	Y91	0.40
Y92	0.40	Y92	0.40
Y93	0.40	Y93	0.40
Y94	0.40	Y94	0.40
Y95	0.40	Y95	0.40
Y96	0.40	Y96	0.40
Y97	0.40	Y97	0.40
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6BG6	0.90	6BG6	0.90
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6BQ7A	0.60	6BQ7A	0.60
6BR7	1.20	6BR7	1.20
6BW6	1.00	6BW6	1.00
6BW7	1.00	6BW7	1.00
6C4	0.40	6C4	0.40
6C6	0.50	6C6	0.50
6CB6	0.55	6CB6	0.55
6CH6	0.45	6CH6	0.45
6CL8	0.75	6CL8	0.75
6D6	0.55	6D6	0.55
6EA8	0.85	6EA8	0.85
6F7	1.10	6F7	1.10
6F8G	0.70	6F8G	0.70
6F23	0.90	6F23	0.90
6F33	0.50	6F33	0.50
6H6	0.45	6H6	0.45
6J4WA	1.25	6J4WA	1.25
6J5	0.65	6J5	0.65
6J5GT	0.50	6J5GT	0.50
6K6	0.30	6K6	0.30
6L7	0.60	6L7	0.60
6M6GT	0.80	6M6GT	0.80
6N6	0.55	6N6	0.55
6P6GT	0.30	6P6GT	0.30
6Q6	0.40	6Q6	0.40
6R6GT	0.50	6R6GT	0.50
6S6	0.65	6S6	0.65
6T6	0.70	6T6	0.70
6U6	0.80	6U6	0.80
6V6	0.90	6V6	0.90
6W6	1.00	6W6	1.00
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30P1L	0.95	6066	2.30
30PL13	1.10	6146	2.25
		6146B	3.25
		8020	5.00
		9001	5.00
		9002	0.50
		9003	0.70
		9004	4.00
		9006	0.35

VIDICON TUBES EMI types 9677A & 9677C £20.00 ea.

C.R. TUBES	
DG7-5	12.00
DG13-2	18.00
DG13-34	12.00
MW13-35	35.00
VCR139A	8.00
3BP1	4.50
88D	8.00
88J	8.00
88L	9.00

SPECIAL VALVES	
CV239	45.00
M503-2J42	1.20
K301	42.00
KRN2A	6.00
725A	23.00

## TRANSISTORS

Please write or phone for current price of any of the transistors, diodes shown below.

AC113	AF178	BF167	GET116	OC36	SK754	2N2062
AC126	AF186	BF185	GEX66	OC42	ZR11	2N2147
AC127	AF212	BF210	NKT222	OC44	ZR22	2N2411
AC128	AF226	BF252	OA5	OC45	1N23A	2N2889
AC176	AS27	BFY90	OA7	OC70	1N25	2N3053
AC178	AS28	BFY27	OA70	OC73	1N32A	2N3054
AC19	BC108	BSY38	OA71	OC78	1N38A	2N3055
AC19	BC118	BSY95A	OA73	OC78D	1N43	2N3390
AC19	BC119	BY216	OA79	OC81	1N70	2N3391
AC19	BC136	CRS110	OA81	OC82	1N277	2N3730
AC19	BC137	CRS120	OA200	OC82D	1N415C	2N4371
AD149	BC148A	CRS130	OA202	OC82DM	1N4148	2N3819
AD181	BC172	CRS140	OA2200	OC83	2N456A	2N4038
AD182	BC172A	CRS150	OC22	OC139	2N	

# Three Ways To Easier Colour Servicing

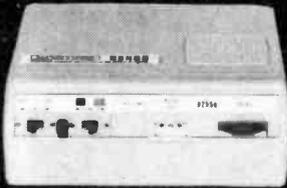
1.



## Colour Bar Generator

- \* 10 test signals
- \* Variable amplitude of colour burst signal
- \* 4 preselected channels on the RF output
- \* Small size, low weight

2.



## Convergor

- \* Battery operated
- \* UHF output covers 10 channels
- \* Video signal can be switched off for purity adjustment

3.



## T.V. Visual Field Strength Meter

- \* Varicap tuner with four channel selectors
- \* High sensitivity
- \* 6" picture tube
- \* Mains or battery operation

The speed and efficiency of your colour servicing with this Decca test equipment will save you time and therefore money. Send us the coupon or give us a call and we'll send you the full details



Decca Radio & Television Ltd.  
Educational and Industrial Services Division  
Ingate Place, Queenstown Road,  
London SW8 3NT (01-622 6677)

Please send me further details of your colour TV test and service equipment:

Name.....

Address.....

.....  
.....

WW1

# HART ELECTRONICS

## Audio Kit Specialists since 1961



**BAILEY/BURROWS/QUILTER PRE AMP** This is the tone control section of the best pre-amp kit currently available. Consider the advantages—\*First quality fibreglass printed circuits with roller tinned finish and all component locations printed on reverse. \*Low noise carbon film and metal film resistors throughout. \*Finest quality low-noise ganged controls with matched tracks and shafts cut to length. \*Well engineered layout for total stability. \*Special decoupling and earthing arrangements to eliminate hum loops. \*Controls, switches and input sockets mount directly on the boards to TOTALLY ELIMINATE wiring to these components. (We know of one pre-amp kit which claims its controls mount directly on the board—and so they do, by their shaft bushes! You still have to wire them up!)

\*We incorporate the Quilter modification which is most important as it reduces distortion and increases the bass and treble control range. As can be seen from the photograph the tone control unit is very slim (only 1½" from front to back) and may therefore be used in many other applications than our Bailey metalwork which it is designed to fit.

**METALWORK AND WOODEN CASES** These have been under review for some time; please send for latest information.

**F.M. TUNER** This latest addition to our range is designed to offer the best possible performance allied to the ease of operation given by push button varicap tuning. We have taken great care to look after the constructors' point of view and there are no coils to wind, no RF circuits to wire and no alignment is required, in fact the whole unit can be easily completed and working in an evening as there are only 3 transistors, one IC and two ready built and aligned modules comprising the active components. We have abandoned the concept of having a tuner as large as the amplifier and this new unit has a frontal size of only 1½ in. X 4 in. It can be mounted on the side of our Bailey amplifier metalwork thus turning it into a tuner/amplifier whilst only increasing its width by 1½ in. Cost of tuner chassis (no case) is £22 for mono, £25.45 for stereo. Metal case £3.55. An extended wooden case to fit tuner and amplifier will be offered shortly.

**STUART TAPE CIRCUITS** Our printed circuits and components offer the easy way to convert any suitable quality deck into a very high quality Stereo Tape unit. Input and output levels suit Bailey pre amp. Total cost varies but around £35 is all you need. We can offer tape heads as well if you want new ones.

All above kits have fibreglass PCB's. Prices exclude VAT but P&P is included.  
**FURTHER INFORMATION ON ALL KITS FREE if you send us a 9 in. X 4 in. S.A.E. REPRINTS** Post free, no VAT.

**BAILEY 30W 18p.**

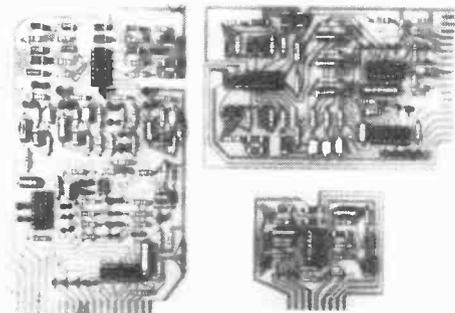
**STUART TAPE RECORDER** All 3 articles under one cover 30p.  
**BAILEY/BURROWS/QUILTER** Preamp circuits, layouts and assembly notes 15p.  
All prices exclude VAT.

## Penylan Mill, Oswestry, Salop

Personal callers are always welcome, but please note we are closed all day Saturday



SQ IS A TRADEMARK OF CBS INC.



## SQ QUADRAPHONIC DECODERS

SQ the leading quadraphonic system, designed by CBS engineers, offers not only 4 channel amblophony from the fast expanding range of SQ encoded discs but also immensely increased depth and fullness of sound from standard stereo recordings too.

Feed 2 channels (200-1000mV as obtainable from most pre-amplifiers) into your choice of any of our 3 decoders and take 4 channels out with no overall signal level reduction. On the logic enhanced decoders Volume, Front-Back, LF-RF, LB-RB and Dimension controls can all be implemented by simple single gang potentiometers—no need for exotic 4-gang units!

These state-of-the-art circuits, used under licence from CBS, are offered in kit form comprising first grade components only—fibre glass circuit boards of professional quality designed for edge connector insertion; all resistors 2% metal oxide, all polystyrene and polycarbonate capacitors 5% or better and in decoder L2 ultra low noise (MPS A18-0.5dB typ.) transistors used in each amplifying stage.

M1 Basic matrix decoder with fixed '10-40' blend. 10 Resistors, 14 Capacitors, 1 Integrated Circuit, Printed Circuit Board £19.90.

L1 Full logic controlled decoder with 'wave matching' and 'front-back logic' for enhanced channel separation using three specially designed Integrated Circuits. 24 Resistors, 42 Capacitors, 3 Integrated Circuits, Printed Circuit Board £28.20.

L2 More advanced full logic decoder with 'variable blend', extended frequency response, increased front-back separation. 43 Resistors, 44 Capacitors, 3 Integrated Circuits, 9 Transistors, 6 Diodes, Printed Circuit Board, £28.20.

All kits include IC sockets and construction notes. Prices include CBS licence fee.

Please write for further details in FREE LIST.

United Kingdom: Post Free. Please add 8% VAT. Overseas: No VAT. Please add (per kit) £1.50 p & p AIR MAIL or 80pp & p SURFACE MAIL.

**AMBIENTACOUSTICS**  
PO BOX 3000  
ANDOVER, HANTS SP10 3EQ

WW—079 FOR FURTHER DETAILS

# MIL SYNCHROS EX STOCK

**WE ARE ANXIOUS TO BUY** Synchro Test Equipment manufactured by Muirhead, Singer-Gertsch etc. Test Dies, Dividing Heads, Bridges, etc. to expand our test facilities.

**SOLAR CELLS.** Ferranti silicon MS18BE, active area 390 sq. mm. Open CCT voltage 550mV at 3000 lumens/sq. ft. Sht. Cct. Current 60mA. Optimum load 90 ohms. Dia. 34mm. Thickness. 6mm. mtg thrd 1/4-28 uni 2A. Ex. Made up panel. **£1.35** (inc. P. & P. and VAT)

**PANEL DISPLAY RECORDING CAMERA.** Manufactured A.G.I. Specifically for the recording of complex instrument displays on 2.1/4in. x 2.1/4in. shots. Fitted 80mm F3.5 lens. Shutter speeds 1/100, 1/50, 1/25 sec. and time exp. Focusing at 1.75 to 50 ft. In 18 steps. Aperture stgcs F3.5 to F22. Prismatic viewfinder and facility for viewing direct on ground glass screen. Rotating filter attachment. Cord film advance and shutter cock with septe. Button control and electrical release facility (24V DC) Spool holds 40 exposures. Camera may be wall mounted on bracket supplied. Tripod mounting socket provided. In wooden case. Two grades available 'as new' Grade A **£35.10** (inc. P. and P. and VAT). Somewhat used but serviceable Grade B **£25.95** (inc. P. & P. and VAT).

**MITSUBISHI MEMOPACK MODEL T165.** 7 1/2 in. X 3 1/2 in. X 2 in.. weight 1.4 lbs. with batts. 8 transistor circuit with D.C. erase and bias, electronic speed control on capstan drive. Powered by 4 X 1.5V penlight (HP7) for 6v svt Int 2\* 8Q L/S 3.5mm jacks for ear/p and 200 Q mic (STD cassette impedance). Recording time up to 80 mins. Takes 46mm spools (No2) of 1/2 in. tape recording at 1 1/2" P/S STD half track. Battery life 4 hours. Only two controls. Volume + play—Record—rewind switch. (No remote control, fast forward, rec level phone out-put) **£16.50** inc. P&P. VAT.

**TELEPRINTER PAPER.** Standard rolls. 3 ply **£4.10** per doz. All P.Pd. U.K. Telex your order now!

**A.C. SUPPLY PANEL** for 19in. rack mounting carrying two 2kVA Variacs with double brush assemblies providing four individually fused and metered outputs of up to 4kVA and 270v in excellent condition at **£48.50** including carriage and V.A.T. (U.K. mainland).

**TAPE STORAGE CANS.** Brand new finished steel cans originally intended for 16mm film but ideal for storing 7 in. reels of tape. Our last supply of these items was quickly exhausted at 30p each but as a result of a massive new purchase we can now offer a can of 50 at **£5.25** inc. P. & P. and V.A.T. Sample order 10 for **£1.10** inc. P. & P. and V.A.T.

## Metal Oxide Resistors (ELECTROSIL & WELWYN) Tantalum Capacitors (KEMET, ITT, PLESSEY, ETC.)

**Synchros and Servomotors ALL AVAILABLE EX STOCK IN MANUFACTURING QUANTITIES**

SPECIALIST STOCKISTS OF SERVOMOTORS, SYNCHROS, MAGSLIPS & CONNECTORS

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TELEX 965265

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### DRY REED INSERTS

Overall length 1.85in. (Body length 1.1in.) Diameter 0.14in. to switch up to 500mA at up to 250V. D.C. Gold clad contacts 70p per doz.; **£4.10** per 100; **£29.80** per 1,000; **£270** per 10,000. All carriage paid U.K.  
Heavy duty type (body length 2in.) diameter 0.22in. to switch up to 1A. at up to 250V. A.C. Gold clad contacts, **£1.50** per doz.; **£9.78** per 100; **£51.40** per 1,000; **Changeover Heavy Duty type £2.70** per doz. All carriage paid U.K.  
**Operating Magnets 90p** per doz.; **£6.80** per 100; **£65** per 1000. All carriage paid U.K.  
**Operating Coils** for 12v supply to accept up to four standard reeds **£2.20** per doz.; **£12.30** per 100. All carriage paid U.K.

**STAINLESS STEEL VACUUM CONTAINERS FOR LIQUIDS.** Capacity 2 U.S. galls. fitted with delivery taps. Brand new in cartons—**£25** (C. Pd. U.K.).

**N.E.P. Mod. 1050 6 Channel U/V Recorder.** Fitted 5 galvos. With P.S.U. for 230V. A.C. 14 x 10 x 12 in. (recorder) and 14 x 10 x 8 in. (P.S.U.). **£228.00** (inc. carr. & V.A.T.).

**RADAR CABLEFORM INSULATION TESTER** for checking insulation between individual conductors and each other and ground at preselected voltages up to 10kV. Full details on application.

**WEE MEGGERS, 250V £12.53. RECORD MEGGERS, 500V £15.12** (inc. P. & P. and VAT).

### ALL PRICES INCLUDE 8% V.A.T.

#### LEMANIA AIRCREW CHRONOGRAPHS



Stainless Steel case with screw back; luminous hands and markings. One fifth sec. sweep hand controlled independently of main movement by press to start, stop and return to zero button. 15 jewel movement. Many of these watches are as new but all have been completely overhauled and checked for accuracy. Fitted strap. White face **£18.25**; Black face **£19.20** inc. P.&P. **Inspection against remittance**

**GS WATCHES** all with brushed stainless steel case with screw back and black faces. Manufactured by CYMA, VERTEX, RECORD, etc., to a standard specification. We will try to meet your requirements for specific manufacturer and quantity orders will be of one manufacturer's production. Completely overhauled. Fitted strap. **£8.80** inc. P. & P.

We also have limited quantities of these watches by OMEGA, LONGINES, BUREN, HAMILTON, IWC, JAEGER LE COULTRE at **£15.25** inc. P. & P. **Inspection against remittance all watches**

**HEWLETT PACKARD SAMPLING 'SCOPE HP185A, £324** inc. carr. and V.A.T. HP185B **£375.**

### PANEL METERS EX STOCK!



We are direct importers of Alps Keiki quality meter panels. We can thus offer these attractive meters at extremely competitive prices.

Range	TYPE No AND FRONT COVER DIMENSIONS IN MM										
	SR45	SR52	SR65	SA38	SA45	SA52	TAD48	TAD66	TAD86	TAD118	TAD152
50µA	72x56	78x63	92x72	43x43	51x51	61x81	48x42	88x60	88x70	118x108	150x110
1mA, 5mA	3.90	4.15	4.39	3.49	3.58	3.78	3.59	3.78	3.98	4.87	5.44
10mA, 50mA	3.10	3.70	3.95	3.08	3.15	3.40	3.23	3.41	3.61	4.50	5.20
100mA	3.57	3.81	4.06	3.15	3.23	3.51	3.34	3.52	3.72	4.61	5.31
1A, 5A, 10A	3.57	3.81	4.06	3.12	3.19	3.47	3.26	3.45	3.64	4.54	5.23
15V, 30V, 100V AC											
150V, 300V	3.70	3.94	4.19	3.36	3.36	3.64	3.78	3.43	3.62	4.81	4.70

Type SR is in an attractive modern case. Types SA and TAD are plainer with movement area louvred. All covers are exceptionally robust. NO HIDDEN EXTRAS! All prices include P&P & VAT. Quantity discounts offered. Full illustrated price list SAE please!

**OVER 300,000 IN STOCK!** Multiway and R.F. Connectors by twenty different companies! Send us your detailed requirements quoting Nato numbers if known. TELEX 965265.

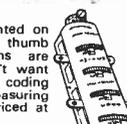
### PAPST MOTORS

Est. 1/20th h.p. Made for 110-120 volt working, but two of these work ideally together off our standard 240 volt mains. A really beautiful motor, extremely quiet running and reversible. **£1.95** each + 30p.



### COMBINATION SWITCH

12 miniature micro switches. Mounted on frame with four digital numbered thumb wheels. Over 4,000 combinations are possible. Equipment which you don't want switched on can also be used as a coding switch. Neat and compact and measuring approx. 4" x 1 1/2" x 1 1/2" deep. Priced at **£1.95**.



### UNISELECTORS

AS used in automatic switch boards, etc. 24V operated. New—all 25 way full wiper type. We have the following in stock:

3 Bank	<b>£4.80</b>	5 Bank	<b>£7.30</b>
3 Bank + C	<b>£4.80</b>	8 Bank	<b>£9.70</b>
3 Bank + Split C	<b>£4.80</b>	10 Bank	<b>£10.90</b>
4 Bank	<b>£6.00</b>	12 Bank	<b>£13.20</b>

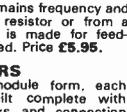
### MAGNETIC CLUTCH

XEROX 1215494—J/N 10-1110 PN866-10. We have no information on this but it appears that the main section with coil fits to the spindle of the machine and there is a contact plate to fit on a stationary part. It appears also that the clutch can be used as a partial brake by putting reduced voltage into it, as a normal brake with normal voltage or as emergency stop by putting increased voltage into it. American made and very well made at that. Price **£1.95**.



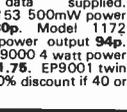
### MULLARD THYRISTOR TRIGGER MODULE

This produces pulses for phase control triggering, it has two isolated outputs, one thyristor or two thyristors (in separate arms of bridge) may be controlled by one module. The timing circuit is synchronised to the mains frequency and control is by an external variable resistor or from a voltage or current source. Provision is made for feedback where automatic control is required. Price **£5.95**.



### MULLARD AUDIO AMPLIFIERS

All in module form, each ready built complete with heat sinks and connection tags, data supplied. Model 1153 500mW power output **80p**. Model 1172 750mW power output **94p**. Model EP9000 4 watt power output **£1.75**. EP9001 twin channel or stereo pre amp. **£1.99**. 10% discount if 40 or more ordered.



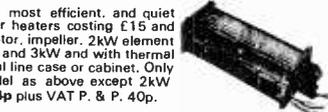
**TERMS:** Add 8% VAT. Send postage where quoted—other items, post free if order for these items is £6, otherwise add 30p.



**Infra-red Binoculars.** Made for military purposes during and immediately after last war to enable snipers, vehicle drivers, etc. to see in the dark. The binoculars have to be fed from a high voltage source (5KV approx.) and providing the objects are in the rays of an infra-red beam, then the binoculars will enable these objects to be seen. Each binocular eye tube contains a complete optical lens system as well as the infra-red cell, technical data on which is available. They are in good order. In fact they were never issued and are still in original cases, but since they were made a long time ago, they can hardly be called new. Sold without guarantee. Price **£16.50** per set + £1 carriage.

### TANGENTIAL HEATER UNIT

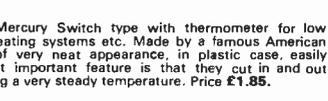
This heater unit is the very latest type, most efficient, and quiet running. Is as fitted in Hoover and blower heaters costing £15 and more. We have a few only. Comprises motor, impeller, 2kW element and 1kW element allowing switching 1.2 and 3kW and with thermal safety cut-out. Can be fitted into any metal line case or cabinet. Only needs control switch, **£3.85**, 2kW. Model as above except 2kW **£2.75**. Don't miss this. Control Switch, **44p** plus VAT P. & P. 40p.



### THIS MONTH'S SNIP

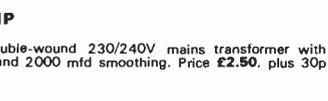
#### SMITHS CONTROLLER

**Room Thermostat.** Mercury Switch type with thermometer for low voltage gas central heating systems etc. Made by a famous American Company, these are of very neat appearance, in plastic case, easily mounted, but the most important feature is that they cut in and out quickly, thus maintaining a very steady temperature. Price **£1.85**.



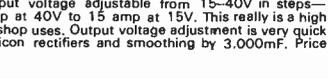
#### 12 VOLT 1 1/2 AMP POWER PACK

This comprises double-wound 230/240V mains transformer with full wave rectifier and 2000 mfd smoothing. Price **£2.50**, plus 30p post and packing.



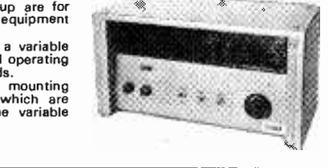
#### Heavy Duty Mains Power Pack.

Output voltage adjustable from 15-40V in steps—maximum load 250W—that is from 6 amp at 40V to 15 amp at 15V. This really is a high power heavy duty unit with dozens of workshop uses. Output voltage adjustment is very quick—simply interchange push on leads. Silicon rectifiers and smoothing by 3,000mF. Price **£6.95** plus 85p post.



#### ERGOTROL UNITS

These units made by the Mullard Group are for operating and controlling d.c. motors and equipment from A.C. mains. Thyristors are used and these supply a variable dc, resulting in motor speed control and operating efficiency far superior to most other methods. The units are contained in well mounting cabinets with front control panel on which are fuses—push buttons for on/off and the variable thyristor firing control. Brand new in makers cases: Model 2410 for up to 5 amps **£24** each.



### NEW ITEMS THIS MONTH

**12V Sealed Plug-In Relay** with two sets changeover contacts, 10 amp rating. Fit into a standard octal valve base. Limited quantity. **£1** each.

**Constant voltage step down transformer.** American made 500W loading. Input voltage can be either 115+ or -20% or 220+ or -20%. For 50 c.p.s. mains output 115V 50 c.p.s. A real quality transformer, probably cost well over £100. Not new but guaranteed perfect. Our price **£45**. Ditto 750W **£60**. Carriage paid.

**Mercury Batteries.** Bank of 7 mercury cells (Type No. 625 which measure approx. 1 1/2" diameter by 1 1/2" thick in plastic tube with positive and negative ends marked giving a total of 25 batteries. With simple holder these will replace the PP3 and similar, or can be quite easily separated into operating simple pocket radios and instruments, dead aids, etc.

**Two circuit micro-switch.** Famous American Licon, maker's ref. 16-40411. Size approx. 1" long x 1/2" wide x 1/4" thick. Two electrically separate circuits, one makes, the other breaks when nylon push rod is depressed. Circuit rating we estimate at 5 amps 250V. Special bargain offer **12p** each, subject to usual quantity discounts.

**Insulated terminals.** These are the popular type which will take a wire under the head or a 4 mm plug in the top, fully insulated for mounting with metal panels, available in several popular colours—price **12p** each.

**Delay Switch.** Depending on the amount of voltage applied, so this switch will delay making the circuit (of up to 15 amps at normal mains voltage) for up to 10 seconds, delay may be fixed or made variable with a suitable potentiometer. These can also be used as thermal relays as suitably connected a low current relay can switch up to 100 amps or more—these are glass tubes plug in 4 pin base—with base **75p** each.

**Smiths 24 hr. timer heart.** really the "Autoset" without its plastic case. This is a 24 hr. twice on, twice off, clock switch which will repeat until re-programmed. Switches rated at 15 amps. Limited supplies—**£3.75** each.

**Panel meter with trip.** American made. These are flush mounting, full vision, moving coil meters, face size 2 1/2" x 2 1/2" with two front settings which enable an external circuit to be tripped, a light lit or an alarm sounded, at pre-set voltages within the range of the meter. We have meters covering the following DC voltages: 0 to 6; 0 to -15; 0 to -25; 0 to +25; 0 to +150. All **£4.75** each.

**2 more cable bargains.** 6 core each PVC insulated and colour coded, screen overall then with PVC outer. Miniature cable, overall diameter approx. 1/4" inch. Price **17p** per metre.

**Ditto, but 9 core,** price **22p** per metre. **Micro switch** with short lever and roller for triggering by rotating disc, 5 amp gold-plated changeover contacts made by Bonna. **30p** each. Standard size and fixing.

## J. BULL (ELECTRICAL) LTD. (Dept. W.W.)

102/3, TAMWORTH ROAD, CROYDON CR0 1XX

# WIRELESS

## FABULOUS Marconi

MARCONI Type 801B STANDARD SIGNAL GENERATOR



PRICE £125

MARCONI TF867 STANDARD SIGNAL GENERATOR



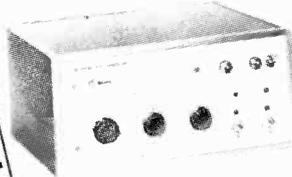
ADD 8% VAT TO ALL PRICES

Frequency Range 1.0MHz-500MHz  
Voltage Output 0.1V-2Volts  
RMS into 50 ohm Modulation 0-99%  
Amplitude internal Modulation at 1kHz continuously pulse modulation  
bandwidth dc-500KHz and 3MHz dependent upon carrier frequency  
Full specification available on request

Carrier Frequency Range 15Kc/s-30Kc/s in 11 bands. Calibration Accuracy ± 1%  
Output Voltage 0.4µV-4V  
Impedance 75 ohms nominal for outputs from 2-4V. 75 ohms for outputs from 4µV-2V. 13 ohms for outputs from 0.4µV-0.4V  
Accuracy below 3Mc/s ± 0.25dB to ± 0.1µV. 3-10Mc/s ± 0.5dB or ± 0.5µV  
10-30Mc/s ± 1.0dB or ± 0.5µV  
Power Supply 100-125V. 200-250V. 40-100c/s Dimensions: 18 in. high x 21in. wide x 14 1/2 in. deep.

## ADVANCE SQUARE WAVE GENERATOR SG21

Frequency Range 9Kc/s to 100Mc/s, Rise time less than 1nS Ex-Demonstration. New condition in manufacturer's original carton.

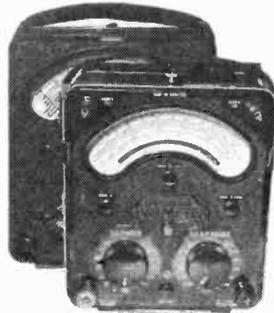


9Kc/s to 100Mc/s continuously variable. Accuracy ± 4%, ± 1% F.S.  
MAIN OUTPUT 20mV-1V into 50 ohm external termination continuously variable.  
Accuracy ± 5%  
Maximum output on open circuit 2V  
RISE TIME less than 1nS up to 500nV.  
TRIGGER OUTPUT 0.2, 0.4, 1.0, 2.0V into 50 ohm external termination maximum output on open circuit 4V.  
Rise time nominally 1.5nS  
Fall time nominally 3.5nS  
Size: 11inW, 5 1/2inH, 3inD.  
Wt. 7.1 lb.  
LAST LISTED PRICE £95

OUR PRICE £35 P/P £1.50 Also available SG21A 100Kc/s-30Mc/s.

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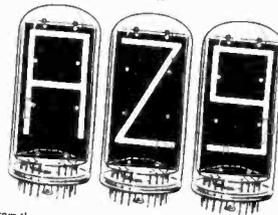


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## ALPHANUMERIC NIXIE TUBES B7971

The Alphanumeric NIXIE tube has the ability to display all the letters of the alphabet, numerals 0 thru 9 and special characters in a single tube.



From the standpoint of both readability and electrical characteristics, the Alphanumeric NIXIE tube provides many unique benefits including:  
★ 170V-21mA ★ All DC operation  
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JUST ARRIVED!! NUMERIC INDICATOR TUBES ultra-long life, high quality, 0-9 and 2 independent decimal points. Supply voltage 200V D.C. Current 14mA. Pulse duration 100µs. Character height 0.51. overall size 1.4. Brand new, guaranteed. Surplus to manufacturers requirements. Type B5853st. Price 1-25 £1.00. 25+ 99p. 100+ 80p. 1000+ price on application.

## THE REVOLUTIONARY SUPERTESTER 680R

FOUR INTERNATIONAL PATENTS - SENSITIVITY 20,000 Ohms per Volt 10 FIELDS OF MEASUREMENT AND 80 RANGES. ACCURACY 1% in D.C. 2% in A.C.

OUTSTANDING FEATURES:  
● Fully screened against external magnetic fields ● 20,000 Ohms per Volt sensitivity (128 x 95 x 32mm) ● Accuracy and stability Scale width and small case dimensions ● Simplicity and ease of use and readability (1% in D.C., 2% in A.C.) of indicated reading ● Printed circuit board, is removable ● Full range of accessories ● 1,000 times overload ● VOLTS A.C. = 11 ranges: without de-soldering ● More ranges than any other meter. VOLTS D.C. = 2-10-50-250-1000-2500 Volts and 4-20-100-500 and 2000 Volts. VOLTS D.C. = 13 ranges: 100mV-2V-10-50-200-500-1000 Volts 50µA-500µA-5 mA-50 mA-250 mA-10 mA-100 mA-1 mA-10 mA-5 mA-50 mA-500 mA-5 Amp. OHMS REACTANCE = 6 ranges: x1-x10-2000 Volts AMP D.C. = 12 ranges: 50µA-500µA-5 mA-50 mA-250 mA-10 mA-100 mA-1 mA-10 mA-5 mA-50 mA-500 mA-5 Amp. DETECTOR = 1 range: from 0 to 10 Megohms. FREQUENCY = 2 ranges: from 0 to 500 and from 0 to 5000Hz. V. OUTPUT VOLTAGE = 9 ranges: 10-50-250-1000-2500 mA-2.5 Amp and 500µA-5 mA-50 mA-500 mA-5 Amp. CAPACITY = 6 ranges: x100-x1000-x0.000 and Low Ohms. DETECTOR = 1 range: from 0 to 200, from 0 to 2,000, from 0 to 50,000 and from 0 to 500,000 pF using the mains and from 0 to 200, from 0 to 2,000 and from 0 to 20,000 Micro farad using the incorporated 3 Volts battery. Bold figures indicate depress button.



£18.50 with shockproof case

## UNIQUE MULTI-METER/SIGNAL GENERATOR

Taut suspension movement. Simple multimeter combined with audio F. Test Oscillator providing AC and DC Voltage ranges D.C. current ranges and resistance ranges, 1kHz and 465kHz oscillator output makes the instruments suitable for general tuning of receivers etc.  
Scale length: 65mm. D.C. voltage ranges: 0.5, 2.5, 10, 50, 250, 500, 1000V. A.C. voltage ranges: 2.5, 10, 15, 250, 500, 1000V. D.C. current ranges: D.05, 0.5, 5, 50, 500mA. Sensitivity: 20,000Ω/V. Resistance ranges: 5-1000Ω mid-scale reading 50Ω 50Ω 10k. mid-scale reading 500Ω, 500Ω-100kΩ. mid-scale reading 5kΩ 5kΩ-1mΩ mid-scale reading 50kΩ  
Accuracy: 5% of F.S.D. Internal battery. 3V dry cell. Oscillator output: 1kHz squarewave. 465kHz sinewave modulated by 1kHz squarewave signal. Output voltage: 1V minimum.  
Overall dimensions: 160 x 97 x 40mm. in carrying case, complete with test leads.

AMAZING VALUE £7.50



Accessories available to convert Supertester 680R into following:  
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TOP VALUE AC/DC MULTI-METER

With taut band suspension movement. Sensitivity 20,000 ohms per volt on AC and 4,000 ohms per volt on DC.  
Technical Data:  
0.06-0.6-6-60-600mA-3 Amps DC  
0.3-3-30-300mA-3 Amps AC 0.6-1.2  
3-12-30-60-120-600 DC 1200 Volts  
3-6-15-60-150-1300-600-900 Volts  
AC. 45 to 20,000 Hz  
500Ω 5-50-500kΩ resistance Decibel range -10 to -12dB Accuracy (% of range) —DC and resistance measurements +2.5. Price with test leads, and storage case £8.85

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£495.00

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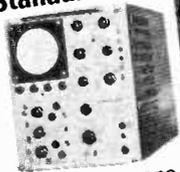
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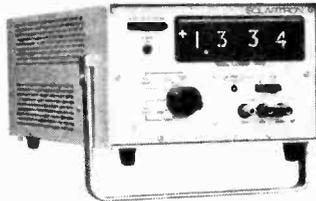
**DC-40MHz DUAL TRACE**



**Solartron C.T.484 oscilloscope. 3% accuracy. Dual Trace Displays.**

DUAL TRACE Y AMPLIFIER. Bandwidth: D.C.-24 Mc/s. Rise Time: 14 nanosecs. D.C.-24 Mc/s. Input Impedance: Sensitivity: 50 mV/cm. Measuring Accuracy:  $\pm 5\%$  1 M.ohm 26pF. Measuring Accuracy:  $\pm 5\%$  direct.  $\pm 3\%$  with calibrator. TIME BASE. 100 nanosecs/cm-5 secs/cm or continuously variable up to 12 secs/cm. Sweep expansion X 5. Accuracy:  $\pm 3\%$ . X AMPLIFIER. Bandwidth: D.C.-150 Kc/s. Sensitivity: 200 mV/cm and 1 V/cm. Input Impedance: 1 M.ohm 40 pF. INTERNAL CALIBRATOR. Accuracy:  $\pm 3\%$ . WIDE BAND Y AMPLIFIER PLUG ALSO AVAILABLE: Bandwidth: D.C.-40 Mc/s. Rise Time: 8 nanosecs. Sensitivity: 50 mV/cm. Input Impedance: 1M.ohm 22pF Measuring Accuracy:  $\pm 5\%$  direct.  $\pm 3\%$  with calibrator. **£149.50**  
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### DIGITAL VOLTMETER 1450

6 Ranges 20mV to 1000V. 10 $\mu$ V Sensitivity-20mV Range. Accuracy  $\pm 0.05\%$  of reading  $\pm 0.05\%$  of range. Isolated input-fully guarded 140dB common mode rejection. 60dB series filter. Internal Calibration provided. 50 conversions per second. Plug in BCD or decimal fan out.

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**4000 50MHz Dual Trace Oscilloscope**



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This recorder indicates the magnitude of applied currents of voltages by a continuous distortion free line on pressure sensitive paper. Moving coil movement scale calibrated 1 milliamp D.C. internal resistance 100 ohms. Chart Drive motor 240V 50Hz. Chart speeds 90" per hour **£39** 1" per hour **£45** or 6" or 12" **£25**

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**Specification**  
Measurement ranges-Current 10-25-100-250-500 Amps. Voltage 300, 600 V. Accuracy 4%. Scale length 60mm. Overall dimensions 283 X 94 X 36mm. Weight 1.5 lbs. **£12.50**

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500	0.1	Beckman	S	£2.50
500	1.0	Relcon	HEL107-10	£2.25
1K		Relcon	HEL0710	£2.25
2K	0.5	Beckman	SA1101	£3.00
2K	0-25	Beckman	7218	£3.00
2K		Reliance	GPA115	£2.00
2K		General Controls	GPA15/4	£2.00
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5K		Colvern	CLR2503	£3.00
10K	0.1	Beckman X	A	£3.50
15K		Colvern	CLR2402	£3.00
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30K	0.5	Beckman	SA1692	£3.00
50K		Reliance	07-10	£2.25
50K			07-5	£2.25
50K	0.5	Beckman	A	£3.00
100K	0.1	Beckman	A	£3.50
100K		Colvern	2501	£2.25
298K	0.1	Beckman	8A3902	£3.50
300K	0.1	Beckman	A	£3.50

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100/100	Beckman	Type C	£3.00
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Repetition frequency up to 20MHz and output pulses up to 20V into 5 ohms with rise and fall times of 5nS. Also produces complex ramp wave forms not obtainable from conventional pulse generators. Fully protected against short circuit. **£275**

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Modulation 405 Lines or 625 Lines  
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BD107 (SNPN)	11.5w	64	100	63p
2N711B/2G106 (SNPN)	150mw	18	120/150 Tot. Sw. Time 275 nS	43p
2N985 (GNPN)	300mw	15	Tot. Sw. Time 115 nS	95p
2N1304 (GNPN)	150mw	30	6	15p
2N1309 (GNPN)	150mw	30	15	30p
2N1046 (GNPN)	50w	100	20	£2.50
2N1146A (GNPN)	90w	70	15	45p
2N1542 (G)	106w	100	0.35	50p
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2N3055 (SNPN)	115w	100		45p
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 Horizontal Sweep speeds: 10 ranges. 10 nsec/cm to 10 sec/cm. accuracy within ± 5%. Magnification: 7 calibrated ranges X1, X2, X5, X10, X20, X50 and X100. Increases maximum calibrated sweep speed to 0.1 nsec/cm; with vernier maximum sweep speed is further extended to 0.04 nsec/cm. Intensity and sampling intensity are not affected by magnification. High frequency: Input frequency: 50 to 1000 mc for sweep speeds 200mv and 1000mv; ± 3%. Time: Approximately 5 sec burst of 50 mc sine wave. Frequency accuracy ± 2%. In addition the Model 185B provides output signals for X-Y recorders and provides means for controlling the display either manually or externally. Full specification on request. Price £295.

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**230 DIGITAL UNIT.**  
 Digital readout parameters. Pulse amplitude, pulse risetime and falltime, pulse width, time interval.

**R116. 10-NS PROGRAMMABLE PULSE GENERATOR**  
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C	1/2	4.7-10M	1.3	1.1	0.9 nett
C	3/4	4.7-10M	1.5	1.2	0.97 nett
C	1	4.7-10M	3.2	2.5	1.92 nett
MO	1/2	10-1M	4	3.3	2.3 nett
WVW	1	0.22-3.9Ω	11	10	8 nett
WVW	3	1-10K	9	8	6 nett
WVW	7	1-10K	11	10	8 nett

Codes: C = carbon film, high stability, low noise; MO = metal oxide, Electrofil TR5, ultra low noise; WVW = wire wound, Plessey.

Values: All E12 except C 1/3W, C 1/2W, and MO 1/2W. E12: 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 and their decades.

E24, as E12 plus 11, 13, 16, 20, 24, 30, 36, 43, 51, 62, 75, 91 and their decades.

Tolerances: 5% except WVW 10% ±0.05Ω below 10Ω and MO 1/2W 2%.

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1.0	—	—	—	—	—	—	11p	8p
2.2	—	—	—	—	—	—	11p	8p
4.7	—	—	—	—	—	—	11p	8p
10	—	—	—	—	—	—	8p	8p
22	—	—	—	—	—	—	8p	8p
47	8p	8p	8p	8p	8p	8p	10p	13p
100	8p	8p	8p	8p	8p	8p	10p	13p
220	8p	8p	8p	10p	10p	11p	17p	28p
470	9p	10p	10p	11p	13p	17p	24p	45p
1,000	11p	13p	13p	17p	20p	25p	41p	—
2,200	15p	18p	23p	26p	37p	41p	—	—
4,700	25p	30p	39p	44p	58p	—	—	—
10,000	42p	46p	—	—	—	—	—	—

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- 2 circuit with chrome nut and black/white/red/green or grey unswitched S5/SS **16p**
- with 2 break contacts S5/BB **20p**
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C2 150 Capacitors mixed values approx. count by weight 0.55

C3 50 Precision Resistors mixed values 1-2% 0.55

C4 75 1/4 W Resistors mixed preferred values 0.55

C5 5 Pieces assorted Ferrite Rods 0.55

C6 2 Tuning Gangs, MW/LW VHF 0.55

C7 1 Pack Wire 50 metres assorted colours 0.55

C8 10 Reed Switches 0.55

C9 3 Micro switches 0.55

C10 15 Assorted Pots & Pre-Sets 0.55

C11 5 Jack Sockets 3 x 3.5m x 2" Standard Switch Type 0.55

C12 30 Paper Condensers preferred types mixed valued 0.55

C13 20 Electrolytics Trans. types 0.55

C14 1 Pack assorted Hardware—Nuts/Bolts, Grommets etc. 0.55

C15 5 Mains Slide Switches, 2 Amp 0.55

C16 20 Assorted Tag Strips & Panels 0.55

C17 10 Assorted Control Knobs 0.55

C18 4 Rotary Wave Change Switches 0.55

C19 2 Relays 6-24V Operating 0.55

C20 1 Sheets Copper Laminate approx. 10" x 7" 0.55

C21 2 Fibreglass printed circuit boards 16 1/2" x 4" approx. 0.55

Please add 10p post and packing on all component packs, plus a further 10p on pack Nos. C1, C2, C19, C20 & C21.

## PLUGS

PS 1 D.I.N. 2 Pin (Speaker) 0.11

PS 2 D.I.N. 3 Pin 0.12

PS 3 D.I.N. 4 Pin 0.15

PS 4 D.I.N. 5 Pin 180° 0.16

PS 5 D.I.N. 5 Pin 240° 0.16

PS 6 D.I.N. 6 Pin 0.17

PS 7 D.I.N. 7 Pin 0.18

PS 8 Jack 2.5mm Screened 0.18

PS 9 Jack 3.5mm Plastic 0.12

PS 10 Jack 3.5mm Screened 0.18

PS 11 Jack 1/2" Plastic 0.15

PS 12 Jack 1/2" Screened 0.22

PS 13 Jack Stereo Screened 0.36

PS 14 Phono 0.10

PS 15 Car Aerial 0.22

PS 16 Co-Axial 0.15

## INLINE SOCKETS

PS 21 D.I.N. 2 Pin (Speaker) 0.14

PS 22 D.I.N. 3 Pin 0.20

PS 23 D.I.N. 5 Pin 180° 0.20

PS 24 D.I.N. 5 Pin 240° 0.20

PS 25 Jack 2.5mm Plastic 0.16

PS 26 Jack 3.5mm Plastic 0.16

PS 27 Jack 1/2" Plastic 0.30

PS 28 Jack 1/2" Screened 0.35

PS 29 Jack Stereo Plastic 0.30

PS 30 Jack Stereo Screened 0.30

PS 31 Phono Screened 0.18

PS 32 Car Aerial 0.22

PS 33 Co-Axial 0.22

## SOCKETS

PS 35 D.I.N. 2 Pin (Speaker) 0.08

PS 36 D.I.N. 3 Pin 0.11

PS 37 D.I.N. 5 Pin 180° 0.11

PS 38 D.I.N. 5 Pin 240° 0.11

PS 39 Jack 2.5mm Switched 0.12

PS 40 Jack 3.5mm Switched 0.12

PS 41 Jack 1/2" Switched 0.20

PS 42 Jack Stereo Switched 0.30

PS 43 Phono Single 0.18

PS 44 Phono Double 0.10

PS 46 Co-Axial Surface 0.10

PS 47 Co-Axial Flush 0.20

## LEADS

LS 1 Speaker lead 2 pin D.I.N. plug to open ends approx. 3 metres long (coded) 0.20

## CABLES

CP 1 Single Lapped Screen 0.07

CP 2 Twin Common Screen 0.11

CP 3 Stereo Screened 0.12

CP 4 Four Core Common Screen 0.23

CP 5 Four Core Individually Screened 0.30

CP 6 Microphone Fully Braided Cable 0.10

CP 7 Three Core Mains Cable 0.09

CP 8 Twin Oval Mains Cable 0.07

CP 9 Speaker Cable 0.05

CP 10 Low Loss Co-Axial 0.15

## CARBON POTENTIOMETERS

Log and Lin

4.7K, 10K, 22K, 47K, 100K, 220K, 470K, 1M, 2M

VC 1 Single Less Switch 0.15

VC 2 Single D.P. Switch 0.28

VC 3 Tandem Less Switch 0.46

VC 4 1K Lin Less Switch 0.15

VC 5 100K Log anti-Log 0.46

## HORIZONTAL CARBON PRESETS

0.1 watt 0.06 each

100, 220, 470, 1K, 2.2K, 4.7K, 10K, 22K, 47K, 100K, 220K, 470K, 1M, 2M, 4.7M

## SELENIUM BRIDGE RECTIFIERS

18V. 2A. Ideal for those building battery, chargers. 15p each. 10 for 55p

## REPANCO TRANSFORMERS

240V. Primary. Secondary voltages available from selected tapplings 4V, 7V, 8V, 10V, 14V, 16V, 17V, 19V, 21V, 25V, 31V, 33V, 40V, 50V, and 26V-0-25V.

Type Amps Price P \* P

MT50/1 1 £1.93 30p

MT50/1 1 £2.42 35p

MT50/2 2 £3.30 40p

# WORLD SCOOP!

## JUMBO SEMICONDUCTOR PACK

Transistors—Germ and Silicon  
 Rectifiers—Diodes—Triacs—Thyristors  
 I,C's and Zenners ALL NEW AND CODED  
**APPROX 100 PIECES!**

Offering the amateur a fantastic bargain Pak and an enormous saving—identification and data sheet in every Pak  
**ONLY £2** p & p 20p

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APPROX. 200 PIECES

Assorted fall-out integrated circuits including: Logic, 74 Series, Linear, Audio and D.T.L. Many coded devices but some unmarked—you to identify.

**OUR SPECIAL PRICE**  
 £1.25 including V.A.T. & p. & p.

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2N3055. Silicon Power Transistors NPN  
 Famous manufacturers out-of-spec devices free from open and short defects—every one able 115 watts TO3. Metal Case.  
**OUR SPECIAL PRICE 8 for £1.**

## LOW COST CAPACITORS

01 µF 400V 3p each 3p each  
 500 µF 50V Elect. 10p each

## CASSETTE CASES

Holds 12. 10" x 3 1/2" x 5". Lock & Handle £1.30

*It's new—It's powerful*  
 (15 + 15w. RMS)  
*and—it looks good!*

## THE LEGIONAIRE STEREO AMPLIFIER



**ORDER NOW—**  
**ONLY £39.95** p. & p. 50p  
**OR Write for full details**

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Takes 6 h.p. 7s complete with terminal clip and lead. 84p each.

## CARTRIDGES

ACOS GP92-18C 200mV at 1.2cm/sec £1.35  
 ACOS GP93-1 280mV at 1cm/sec £1.85  
 ACOS GP96-1 100mV at 1cm/sec £2.80  
 TTC J-2005 Crystal/Hi Output £1.05  
 TTC J-2010C Crystal/Hi Output Compatible £1.20  
 TTC J-2006S Stereo/Hi Output £1.75  
 TTC J-2105 Ceramic/Med Output £1.95  
 TTC J-2203 Magnetic 5mV/cm/sec, including stylus £4.95  
 TTC J-2203S Replacement stylus for above £3.00  
 TTC AF.55 Audio-technica magnetic cartridge 4mV/cm/sec £3.30

# -the lowest prices!

## 74 Series T.T.L. I.C.'S

BI-PAK STILL LOWEST IN PRICE FULL SPECIFICATION GUARANTEED. ALL FAMOUS MANUFACTURERS



1	25	100+	1	25	100+	1	25	100+			
SN7400	0.16	0.15	0.14	SN7453	0.16	0.15	0.14	SN74153	1.00	0.95	0.90
SN7401	0.18	0.17	0.16	SN7454	0.18	0.15	0.14	SN74154	1.70	1.65	1.60
SN7402	0.18	0.17	0.16	SN7460	0.18	0.15	0.14	SN74155	1.20	1.15	1.10
SN7403	0.18	0.17	0.16	SN7470	0.32	0.29	0.27	SN74156	1.20	1.15	1.10
SN7404	0.22	0.21	0.20	SN7472	0.32	0.29	0.27	SN74157	1.00	0.95	0.90
SN7405	0.22	0.21	0.20	SN7473	0.41	0.39	0.35	SN74160	1.40	1.35	1.30
SN7406	0.39	0.34	0.31	SN7474	0.41	0.39	0.35	SN74161	1.40	1.35	1.30
SN7407	0.39	0.34	0.31	SN7475	0.60	0.58	0.56	SN74162	1.40	1.35	1.30
SN7408	0.25	0.24	0.23	SN7476	0.44	0.43	0.42	SN74163	1.40	1.35	1.30
SN7409	0.25	0.24	0.23	SN7480	0.18	0.15	0.14	SN74164	1.60	1.55	1.50
SN7410	0.18	0.15	0.14	SN7481	1.10	1.05	1.00	SN74165	1.80	1.75	1.70
SN7411	0.25	0.24	0.23	SN7482	0.90	0.85	0.80	SN74166	1.60	1.55	1.50
SN7412	0.28	0.27	0.26	SN7483	1.20	1.15	1.05	SN74174	1.60	1.55	1.50
SN7413	0.32	0.31	0.30	SN7484	1.00	0.97	0.95	SN74175	1.10	1.05	1.00
SN7416	0.30	0.29	0.28	SN7485	1.90	1.55	1.50	SN74176	1.25	1.20	1.15
SN7417	0.30	0.29	0.28	SN7486	0.38	0.34	0.34	SN74177	1.25	1.20	1.15
SN7420	0.18	0.15	0.14	SN7489	2.40	2.75	2.50	SN74180	1.25	1.20	1.15
SN7422	0.30	0.29	0.28	SN7490	0.65	0.63	0.60	SN74181	2.35	2.35	2.35
SN7423	0.40	0.39	0.38	SN7491	1.10	1.05	1.00	SN74182	1.25	1.20	1.15
SN7425	0.40	0.39	0.38	SN7492	0.74	0.71	0.64	SN74184	1.80	1.75	1.70
SN7426	0.40	0.38	0.36	SN7493	0.74	0.71	0.64	SN74185	1.80	1.75	1.70
SN7427	0.40	0.38	0.36	SN7494	0.82	0.75	0.75	SN74190	1.95	1.90	1.85
SN7428	0.45	0.42	0.40	SN7495	0.82	0.75	0.75	SN74191	1.95	1.90	1.85
SN7430	0.18	0.15	0.14	SN7496	0.96	0.93	0.86	SN74192	1.95	1.90	1.85
SN7432	0.40	0.38	0.36	SN74100	1.50	1.45	1.40	SN74193	1.95	1.90	1.85
SN7433	0.42	0.40	0.38	SN74104	0.80	0.58	0.55	SN74194	1.95	1.90	1.85
SN7437	0.35	0.32	0.30	SN74105	0.80	0.58	0.55	SN74197	1.30	1.25	1.20
SN7438	0.35	0.32	0.30	SN74107	0.44	0.42	0.40	SN74198	1.10	1.05	1.00
SN7440	0.18	0.15	0.14	SN74108	0.34	0.34	0.34	SN74199	1.20	1.15	1.10
SN7441	0.74	0.71	0.64	SN74111	0.90	0.88	0.85	SN74199	1.20	1.15	1.10
SN7442	0.74	0.71	0.64	SN74118	1.00	0.95	0.90	SN74199	1.20	1.15	1.10
SN7443	1.20	1.15	1.10	SN74119	1.50	1.40	1.30	SN74198	2.75	2.70	2.65
SN7444	1.20	1.15	1.10	SN74121	0.50	0.48	0.45	SN74199	2.50	2.40	2.30
SN7445	1.60	1.55	1.50	SN74122	0.70	0.68	0.65				
SN7446	1.20	1.15	1.10	SN74123	0.75	0.73	0.70				
SN7447	1.10	1.07	1.05	SN74141	0.82	0.75	0.70				
SN7448	1.10	1.07	1.05	SN74145	1.30	1.25	1.20				
SN7450	0.16	0.15	0.14	SN74150	1.50	1.40	1.30				
SN7451	0.16	0.15	0.14	SN74151	1.10	1.05	1.00				

NOW WE GIVE YOU 50w PEAK (25w R.M.S.) PLUS THERMAL PROTECTION! The NEW AL60 Hi-Fi Audio Amplifier FOR ONLY £4.25

- Max Heat Sink temp. 90°C
- Frequency Response 20Hz to 100KHz
- Distortion better than 0.1% at 1KHz
- Supply voltage 15-50 volts
- Thermal Feedback
- Latest Design Improvements
- Load—3, 4, 8 or 16 ohms
- Signal to noise ratio 80dB
- Overall size 63mm x 105mm x 13mm



Especially designed to a strict specification. Only the finest components have been used and the latest solid state circuitry incorporated in this powerful little amplifier which should satisfy the most critical A.F. enthusiast.

FULLY BUILT—TESTED and GUARANTEED

## STABILISED POWER MODULE SPM80 £3.25

SPM80 is especially designed to power 2 of the AL60 Amplifiers, up to 15 watt (r.m.s.) per channel simultaneously. This module embodies the latest components and circuit techniques incorporating complete short circuit protection. With the addition of the Mains Transformer BMT80, the unit will provide outputs of up to 1.5 amps at 35 volts. Size: 63 mm x 105 mm x 20 mm. These units enable you to build Audio Systems of the highest quality at a hitherto unobtainable price. Also ideal for many other applications including: Disco Systems, Public Address, Intercom Units, etc. Handbook available, 10p.

TRANSFORMER BMT80 £2.15 p. & p. 25p

## STEREO PRE-AMPLIFIER TYPE PA100

Designed to a specification and NOT a price, and yet still the greatest value on the market, the PA100 stereo pre-amplifier has been conceived from the latest circuit techniques. Designed for use with the AL60 power amplifier system, this quality made unit incorporates no less than eight silicon planar transistors, two of these are specially selected low noise NPN devices for use in the input stages.

Three switched stereo inputs, and rumble and scratch filters are features of the PA100, which also has a STEREO/MONO switch, volume, balance and continuously variable bass and treble controls.

## MK 60 AUDIO KIT only £14.25

Comprising: 2x AL60, 1x SPM80, 1x BMT80, 1x PA 100, 1 front panel, 1 kit of parts to include on-off switch, neon indicator, stereo headphone sockets plus instruction booklets. Complete Price: £29.75 plus 30p postage.

## TEAK 60 AUDIO KIT

Comprising: Teak veneered cabinet size 16" x 11 1/2" x 3 1/2", other parts include aluminium chassis, heatsink and front panel bracket, plus back panel and appropriate sockets etc. Kit price: £9.95 plus 30p postage.

## AL10/AL20/AL30 AUDIO AMPLIFIER MODULES

The AL10, AL20 and AL30 units are similar in their appearance and in their general specification. However, careful selection of the plastic power device has resulted in a range of output powers from 3 to 10 watts R.M.S.

Parameter	Conditions	Performance
HARMONIC DISTORTION	Po = 3 WATTS f = 1KHz	0-25%
LOAD IMPEDANCE	—	8-16Ω
INPUT IMPEDANCE	f = 1KHz	100 kΩ
FREQUENCY RESPONSE ± 3dB	Po = 2 WATTS	50 Hz-25 KHz
SENSITIVITY for RATED O/P	Vs = 25V, R1 = 8Ω f = 1KHz	75mV. RMS
DIMENSIONS	—	3" x 2 1/2" x 1"

The above table relates to the AL10, AL20 and AL30 modules. The following table outlines the differences in their working conditions.

Parameter	AL10	AL20	AL30
Maximum Supply Voltage	25	30	30
Power output for 2% T.H.D. (RL = 8Ω f = 1KHz)	3 watts RMS Min.	5 watts RMS Min.	10 watts RMS Min.
PRICE	£2.50	£3.85	£3.20

### INTEGRATED CIRCUIT PAKS

Manufacturers' "Fall Out" units which include Functional and Part-Functional Units. These are classed as 'out-of-spec' from the maker's very rigid specifications but are ideal for learning about I.C.'s and experimental work.

PaK No.	Contents	Price	PaK No.	Contents	Price	PaK No.	Contents	Price
UTC00	= 12x 7400	0.54	UTC46	= 5x 7466	0.54	UTC90	= 5x 7490	0.54
UTC01	= 12x 7401	0.54	UTC48	= 5x 7468	0.54	UTC91	= 5x 7491	0.54
UTC02	= 12x 7402	0.54	UTC50	= 12x 7450	0.54	UTC92	= 5x 7492	0.54
UTC03	= 12x 7403	0.54	UTC51	= 12x 7451	0.54	UTC95	= 5x 7493	0.54
UTC04	= 12x 7404	0.54	UTC53	= 12x 7453	0.54	UTC94	= 5x 7494	0.54
UTC05	= 12x 7405	0.54	UTC54	= 12x 7454	0.54	UTC95	= 5x 7495	0.54
UTC06	= 8x 7406	0.54	UTC58	= 12x 7458	0.54	UTC96	= 5x 7496	0.54
UTC07	= 8x 7407	0.54	UTC70	= 8x 7470	0.54	UTC100	= 5x 74100	0.54
UTC10	= 12x 7410	0.54	UTC72	= 8x 7472	0.54	UTC121	= 5x 74121	0.54
UTC20	= 12x 7420	0.54	UTC73	= 8x 7473	0.54	UTC141	= 5x 74141	0.54
UTC30	= 12x 7430	0.54	UTC74	= 8x 7474	0.54	UTC151	= 5x 74151	0.54
UTC40	= 12x 7440	0.54	UTC76	= 8x 7476	0.54	UTC154	= 5x 74154	0.54
UTC41	= 5x 7441	0.54	UTC80	= 5x 7480	0.54	UTC193	= 5x 74193	0.54
UTC42	= 5x 7442	0.54	UTC81	= 5x 7481	0.54	UTC199	= 5x 74199	0.54
UTC43	= 5x 7443	0.54	UTC82	= 5x 7482	0.54	UTCX1	= 25 Assorted 74's	1.55
UTC44	= 5x 7444	0.54	UTC83	= 5x 7483	0.54			
UTC45	= 5x 7445	0.54	UTC86	= 5x 7486	0.54			

### LINEAR I.C.'s—FULL SPEC.

Type No.	Case	1	25	100+	
72702P	DIL	14	0.50	0.48	0.45
72709P	DIL	8	0.20	0.19	0.18
72709	DIL	14	0.25	0.23	0.20
484110	DIL	14	0.35	0.33	0.30
72714	DIL	14	0.35	0.33	0.30
72714C	TO-5	8	0.30	0.29	0.28
72717	DIL	8	0.30	0.29	0.28
72717P	DIL	8	0.30	0.29	0.28
72748	DIL	8	0.38	0.38	0.34
SL201C	TO-3	5	0.50	0.48	0.40
SL201C	TO-3	5	0.35	0.35	0.30
SL202C	TO-3	5	0.50	0.45	0.40
IAA263	TO-7	4	0.80	0.70	0.60
IAA263	TO-7	4	1.21	0.85	0.70
IAA350A	TO-5	10	1.85	1.80	1.70
uA703C	TO-5	6	0.28	0.28	0.24
uA709C	TO-5	8	0.20	0.19	0.18
uA713	TO-5	10	0.35	0.35	0.30
uA713	TO-5	8	0.35	0.33	0.30
ZN411	TO-18	14	1.20	1.20	1.10
TBA800	DIL	14	0.85	0.83	0.80

### DTL 930 SERIES LOGIC I.C.'s

Type	1	25	100+
BP930	0.15	0.14	0.13
BP932	0.18	0.15	0.14
BP933	0.18	0.15	0.14
BP935	0.18	0.15	0.14
BP936	0.18	0.15	0.14
BP944	0.18	0.15	0.14
BP945	0.20	0.20	0.20
BP946	0.15	0.14	0.13
BP948	0.20	0.28	0.25
BP951	0.70	0.65	0.60
BP962	0.15	0.14	0.13
BP9003	0.45	0.43	0.40
BP9004	0.45	0.43	0.40
BP9097	0.45	0.43	0.40
BP9099	0.45	0.43	0.40

### DUAL-IN-LINE SOCKETS

14 & 16 Lead Sockets for use with DUAL-IN-LINE I.C.'s. TWO RANGES PROFESSIONAL & NEW LOW COST. PROF. TYPE No. 1-24 25-99 100up. LOW COST No. BPS 14 " " 18p 14p 12p BPS 16 " " 17p 15p 13p BPS 8 pin type 15p 13p 11p

### NUMERICAL INDICATOR TUBES

Type Description 3015F Minitron 7 Segment Indicator £1.50 MAN 3M L.E.D. 7 Segment Display 0.127" High Characters £1.90

### 3 TERMINAL POSITIVE VOLTAGE REGULATORS

TO.3 Plastic Encapsulation uA7805/L129 5V (Eqv. to MVR5) £1.78 uA7812/L130 12V (Eqv. to MVR12V) £1.78 uA7815/L131 15V (Eqv. to MVR15V) £1.78

### BI-PAK CATALOGUE & LISTS

Send S.A.E. and 10p

### EDSR 3168 TRIPLE 66 BIT DYNAMIC SHIFT REGISTER

TTL Compatible. Low Clock Capacitance, High Speed Diode Protected Inputs Wired OR Capability SPECIFICATION SHEET AVAILABLE £1 each

### TEAK VENEERED CABINET for: STEREO 20

TC 20. £3.95 p&p 30p E.M.I. LEK 350 Loudspeaker System Enclosure kit in teak veneer, including speakers. Rec. retail price £4.50 per pr. OUR SPECIAL PRICE £3.95 per pair P. & P. £1. ONLY WHILE STOCKS LAST!

### The STEREO 20

The 'Stereo 20' amplifier is mounted, ready wired and tested on a one-piece chassis measuring 20 cm. x 14 cm. x 5.5 cm. This compact unit comes complete with on/off switch volume control, balance, bass and treble controls, Transformer. Power supply and Power amps. Attractively printed front panel and matching control knobs. The 'Stereo 20' has been designed to fit into most turntable plinths without interfering with the mechanism or, alternatively, into a separate cabinet. Output power 20w peak. Input 2 (Cer.) 300mV into 1M. Freq. res. 25Hz-20kHz. Input 2 (Aux.) 4mV into 30K. Harmonic distortion. Bass control ±12dB at 60Hz typically 0.25% at 1 watt. Treble con.

# TAUT SUSPENSION MULTIMETERS

Made in USSR  
For ex-stock delivery



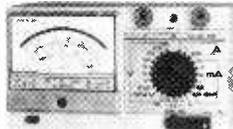
U4312 £10.25\*  
U4313 £12.50\*  
U4315 £9.00\*



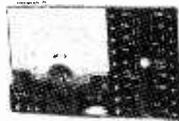
U4324 £9.25\*



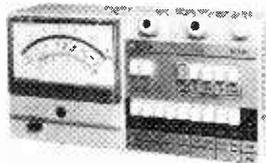
U4341 £10.50\*



U4317 £16.50\*



U4323 £7.70\*



F4313 £22.00\*

TRADE ENQUIRIES INVITED  
PLEASE WRITE FOR FULL DETAILS

## LINEAR INTEGRATED CIRCUITS

—Please note reductions in prices—

**Mullard TAA263.** Direct coupled three stage low level amplifier for use from DC to 600 kc/s. Supply voltage 6–8v. Typical power gain 77 db. into 150Ω load. Output power 10mW. T072 four-lead encapsulation £0.65\*

**Mullard TAA293.** Medium frequency amplifier with frequency response of 600 kc/s. Nominal supply voltage 6v. Typical power gain 89 db. Maximum power dissipation 180 mW. Power output 10 mW. into 150Ω load. T074 ten-lead encapsulation £0.65\*

**Mullard TAA320.** Metal oxide silicon low frequency pre-amplifier consisting of a MOST stage followed by a bi-polar transistor. Gate to source voltage 9–14v. Total power dissipation 200 mW. Drain current 1 μA. Output conductance 0.85 mmho. T018 3-lead encapsulation £0.60\*

## L.E.D. TYPE HP5082/4850

Red Light GASP Light Emitting Diodes giving bright diffused light of 0.8 mcd at forward voltage of 1.6V and DC current of 20 mA. Plastic wide angle lens 0.200" diameter. Ideal for panel lights, etc. Price for 12 pieces £1.75 incl. VAT and p.&p.

## 1-AMP SILICON RECTIFIERS

20 pieces	1N4001	50 p.i.v.	£1.12
"	1N4002	100 p.i.v.	£1.25
"	1N4003	200 p.i.v.	£1.35
"	1N4004	400 p.i.v.	£1.45
"	1N4005	600 p.i.v.	£1.55
"	1N4006	800 p.i.v.	£1.85
"	1N4007	1000 p.i.v.	£2.10

This is a special offer and minimum quantity of 20 pcs must be ordered. These prices are inclusive of P.P. and VAT.

Please write for full catalogue and Price List of Valves, Semi-conductors, Test Equipment and Passive Components.

MINIMUM ACCOUNT ORDER CHARGE £10.00 PLUS VAT. OTHERWISE CASH WITH ORDER PLEASE

\*Prices are exclusive of VAT

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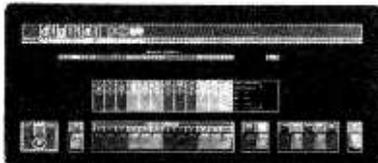
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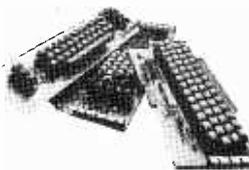
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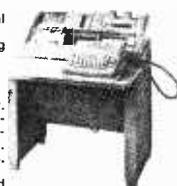
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Table listing semiconductor components such as AC107, AC125, AC128, etc., with their respective prices and specifications.

Table listing semiconductor components such as TIP29B, TIP30B, TIP31B, etc., with their respective prices and specifications.

Table listing semiconductor components such as CRS105, CRS110, CRS120, etc., with their respective prices and specifications.

Special offers section including TRIACS, LINEAR I.C.s, BRIDGE RECTIFIERS, ZENER DIODES, L.E.D., L.D.R., TO3 VOLTAGE REGULATORS, VEROBOARDS, METAL BOXES, and ALUMINIUM BOXES.

DIGITAL INTEGRATED CIRCUITS

Table listing digital integrated circuits such as SN7400, SN7401, SN7402, etc., with their respective prices.

Table listing digital integrated circuits such as SN74107, SN74110, SN74118, etc., with their respective prices.

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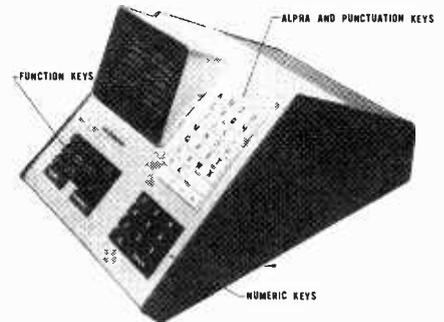
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Prices correct at October 1974, but all exclusive of VAT. Post and Package 20p

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150	100	5 8	9.9x8.9x8.6	4.45	45
151	200	8 0	12.1x9.3x10.2	7.39	53
152	250	12 12	12.1x11.8x10.2	8.93	73
153	350	15 0	14.0x10.8x11.8	10.80	73
154	500	19 8	14.0x13.4x11.8	12.41	91
155	750	29 0	17.2x14.0x14.0	18.85	*
156	1000	38 0	17.2x16.8x14.0	26.50	*
157	1500	46 0	21.6x13.4x18.1	30.25	*
158	2000	60 0	21.6x18.1x17.0	37.00	*
159	3000	85 0	23.5x17.8x19.7	53.25	*



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Ref. No.	VA (Watts)	Weight lb oz	Size cm.	Auto Taps	£	P & P
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64	150	4 4	7.0x8.7x8.1	0-115-210-240	2.64	38
4	750	6 4	8.9x7.7x7.7	0-115-200-220-240	3.75	45
86	300	6 4	9.9x10.2x10.2	"	5.29	53
67	500	15 8	12.1x11.2x10.7	"	8.02	67
84	1000	19 8	14.0x13.4x14.3	"	12.44	91
93	1500	30 4	14.0x15.9x14.3	"	16.65	*
95	2000	38 0	17.2x16.8x14.0	"	22.00	*
73	3000	40 0	21.6x13.4x18.1	"	31.90	*

## CASED AUTO TRANSFORMERS

115V mains lead input and U.S.A. plug outlets. 20VA £2.85. P. & P. 38p. 500VA £9.50. P. & P. 80p. 1000VA £15.92. Via B.R.S.

## LOW VOLTAGE TRANSFORMERS

Ref. No.	Primary Amps.	Secondary Amps.	Weight lb oz	Size cm.	Secondary Windings	£	P & P
111	0.5	0.25	1 4	4.8x2.9x3.5	0-12V at 0.25A x2	1.34	23
213	1.0	0.5	1 4	6.1x4.2x4.8	0-12V at 0.5A x2	1.58	30
71	2	1	1 12	7.0x6.4x6.1	0-12V at 1A x2	2.09	38
18	4	2	2 12	8.3x7.7x7.0	0-12V at 2A x2	2.60	38
70	6	3	3 8	8.9x8.0x7.7	0-12V at 3A x2	3.75	45
108	8	4	4 8	9.9x8.9x8.6	0-12V at 4A x2	4.15	45
72	10	5	4 4	9.9x9.9x8.6	0-12V at 5A x2	4.87	53
116	12	6	6 12	12.1x9.3x10.2	0-12V at 15A x2	5.02	53
17	16	8	8 12	12.1x9.9x10.2	0-12V at 8A x2	6.62	60
115	20	10	10 8	14.0x9.6x11.8	0-12V at 10A x2	9.45	73
187	30	15	15 8	14.0x12.1x11.8	0-12V at 15A x2	12.29	85
226	60	30	30 0	17.2x15.3x14.0	0-12V at 30A x2	15.30	*

## 30 VOLT RANGE

Ref. No.	Primary Amps.	Secondary Amps.	Weight lb oz	Size cm.	Secondary Taps	£	P & P
112	0.5	0.5	1 4	6.1x5.8x4.8	0-12-15-20-24-30V	1.65	30
79	1.0	1.0	1 4	7.0x6.7x6.1	"	2.18	38
3	2.0	2.0	2 4	8.9x7.7x7.7	"	3.18	38
20	3.0	3.0	4 8	9.9x8.3x8.6	"	4.12	45
21	4.0	4.0	4 4	9.9x9.9x8.6	"	4.07	53
51	5.0	5.0	6 12	12.1x8.6x10.2	"	5.83	53
117	6.0	6.0	6 0	12.1x11.8x10.2	"	6.51	60
88	8.0	8.0	8 0	12.1x11.8x10.2	"	9.00	67
89	10.0	10.0	10 12	14.0x10.2x11.8	"	8.97	73

## 50 VOLT RANGE

Ref. No.	Primary Amps.	Secondary Amps.	Weight lb oz	Size cm.	Secondary Taps	£	P & P
102	0.5	1.2	1 12	7.0x6.4x6.1	0-19-25-33-40-50V	2.35	30
103	1.0	2.4	1 12	8.3x7.4x7.0	"	3.08	38
104	2.0	4.8	2 8	9.9x8.9x8.6	"	4.28	45
105	3.0	7.2	3 0	9.9x10.2x8.6	"	5.28	53
106	4.0	9.6	4 0	12.1x10.5x10.2	"	6.91	67
107	6.0	12.0	6 0	14.0x10.2x11.8	"	11.00	67
118	8.0	16.0	8 0	14.0x12.1x11.8	"	11.80	85
119	10.0	20.0	10 0	17.2x12.7x14.			

# APPOINTMENTS VACANT

**DISPLAYED APPOINTMENTS VACANT:** £6.08 per single col. centimetre (min. 3cm).

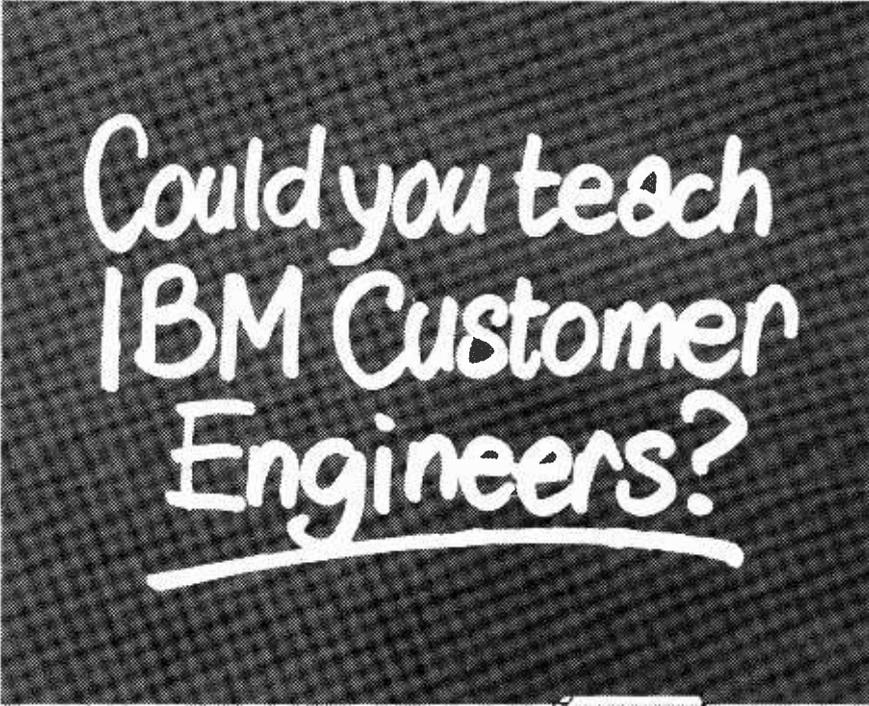
**LINE advertisements (run-on):** 86p per line (approx. 7 words), minimum three lines.

**BOX NUMBERS:** 35p extra. (Replies should be addressed to the Box number in the advertisement, c/o Wireless World, Dorset House, Stamford Street, London, SE1 9LU).

**PHONE:** Allan Petters on 01-261 8508 or 01-261 8423.

*Classified Advertisement Rates are currently zero rated for the purpose of V.A.T.*

Advertisements accepted up to 12 noon Monday, January 6th for the February issue subject to space being available.



Could you teach  
IBM Customer  
Engineers?

We have a number of opportunities for instructors to train our customer engineers to service and maintain data processing equipment including the latest 370 Systems and Software.

If you're an experienced or potential instructor with a background in software and/or electronics, educated to HNC, C & G standard or perhaps you've had similar service experience—now's the chance to find out more about these secure, well paid positions, based in NW London. Salaries start from £3000 and career development prospects and training are excellent.

If you are interested please write to:  
Anne Dare, IBM United Kingdom Limited,  
389 Chiswick High Road, London W4 4AL.  
Quoting ref: WW/92418.

**IBM**

# Young Electronics Engineers A mobile future in broadcasting?

We require Engineers qualified, or about to qualify, to H.N.C. or equivalent level and possibly with a few years' experience, who will learn to operate and maintain the advanced electronic equipment at our Transmitting Stations throughout the country bringing Independent Television and Radio into millions of homes.

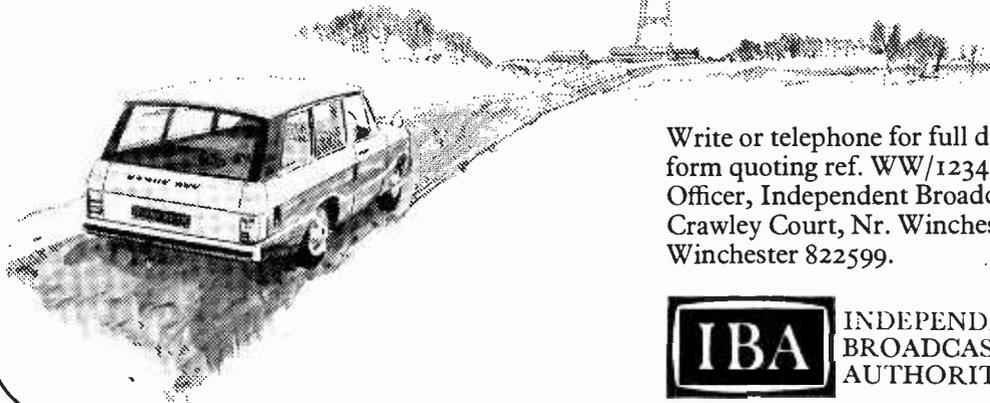
Our Engineers may be called upon to rectify a fault anywhere, anytime and in all weathers. It's a job that requires flexibility about when and where you work; you'll need a driving licence and you must be prepared to undertake a demanding training course.

## Paid While You Train

IBA's special eighteen month training course, which combines theoretical study with practical 'on station training' will give you a comprehensive knowledge of operations and maintenance techniques, plus an additional recognised qualification, and you will be paid a training salary of not less than £1841, more for those with experience.

## The Future

On completion of your training, you will be in the field, full-time on a salary range of £2861-£4167. Further promotion to Team Leader and beyond is up to you.



Write or telephone for full details and an application form quoting ref. WW/1234 to: The Personnel Officer, Independent Broadcasting Authority, Crawley Court, Nr. Winchester, Hants. Tel: Winchester 822599.



14353

# A place in the future for Electronic Test Engineers

As leaders in advanced technology, Ferranti hold a very firm place in the future electronic world. ability in electronics.

We have further vacancies for three Test Engineers to strengthen our team for the future. The successful applicants will join a busy, well-equipped organisation backed up by an excellent repair service. We test, and diagnose faults on, high-quality Multi-layer Analogue and Digital Computer Panels (with over 300 different types). Ideally, applicants should have Analogue, Digital or Core Store experience, or have Forces training or hold a recognised qualification or have proven

If you think you're the right man for the job, telephone or write for an application form, quoting ref. no. D/530/WW, to:

The Personnel Manager,  
Ferranti Limited,  
Western Road,  
Bracknell, Berks

or telephone Bracknell 3232, Recruitment Office ext. 471.

## FERRANTI

first in applied technology



4354

# Radio Operators. How to see more of your wife without losing sight of the sea.



Join the Post Office Maritime Service. We have openings for Radio Operators at several of our coastal stations.

The work is just as interesting, just as rewarding as aboard ship, but you get home to see your wife and family more often. You need a United Kingdom General or First Class Certificate in Radiocommunications, or an equivalent certificate issued by a Commonwealth Administration or the Irish Republic.

Starting pay for a man of 25 or over is £2,270, plus cost of living allowance with further

annual increases after that. Though we're happy to take people from 19 up.

In addition to your basic salary, you'll get an average allowance of £450 a year for shift duties and there are opportunities for overtime.

Other benefits include a good pension scheme, sick pay and prospects of promotion to Senior Management.

For more information, write to: ETE Maritime Radio Services Division (L531), ET 17.1.1.2., Room 643, Union House, St. Martins-le-Grand, London, EC1A 1AS.

Post Office  
Telecommunications

*Here is your opportunity to enter the TV service industry as a*

## TRAINEE TV TECHNICIAN WITH REDIFFUSION



If you have some basic knowledge of TV or electronics, we will further your education with theoretical and practical training.

**OUR MINIMUM REQUIREMENTS ARE:**

- (1) A full (clean) driving licence.
- (2) Age over 19 years.
- (3) City and Guilds Part 1 in Radio & TV/Electronics. Applicants possessing the General Certificate of Education or equivalent in Science, Maths and Physics will be considered.
- (4) An ambition to become a fully qualified top grade technician.

*If you are one of these people we offer:*

- \* £30 per week whilst training, this will be increased if you successfully complete your training period.
- \* Regular courses at one of our training schools.
- \* A personalised vehicle when obtaining the higher grades.
- \* 3 weeks annual holiday after one year's service.
- \* Company Pension scheme.

**INTERESTED? THEN APPLY IN WRITING TO:**

The Service Supervisor,  
Rediffusion (Redhire) Ltd.,  
727 Tudor Estate,  
Twyford Abbey Road,  
Park Royal  
NW10

Or Telephone 01-965 4554/5 during normal working hours.

## VOICE OF KENYA MAINTENANCE ENGINEER (BROADCAST TRANSMITTER)

Required by the Ministry of Information and Broadcasting to introduce a revised maintenance system and assist in its implementation; to instruct staff and compile a maintenance instruction manual; to give occasional lectures on maintenance to engineering trainees.

Candidates 30-50 years, should be graduates in Electronics with at least three years' experience in Telecommunications Broadcasting systems or holders of the City and Guilds Telecommunications Final with seven years' experience in Broadcasting Transmitters, two of which must have been in a Supervisory capacity. They must be able to organise and formulate radio transmitter maintenance routine procedures. Experience as an Instructor in maintenance techniques would be an advantage.

**Salary in the range £3,020 to £3,440 which includes an allowance, normally tax free, of £1,212 to £1,488 pa. Terminal gratuity 25 per cent.**

Other benefits include Subsidised accommodation, Education Allowances; Children's Holiday Visit Passages, Free Family Passages, Appointment grant £150-£300. 30 month tour.

The post described is partly financed by Britain's programme of aid to the developing countries administered by the Ministry of Overseas Development.

**For further particulars you should apply, giving brief details of experience to:**

**Crown agents**

M Division, 4 Millbank, London SW1P 3JD, quoting reference number M2K/730923/WF.

## The Royal Fleet Auxiliary

requires

# Radio Officers

with 1st Class PMG or MPT General Certificate or (with previous experience) 2nd Class PMG Certificate and DOT Radio Maintenance Certificate.

Basic rates of pay at entry depend on experience e.g. less than six months sea service £2,312; over six months sea service £2,570. These rates are increased to take account of qualifications held.

Regular increments are awarded for Company service thereafter and there are excellent prospects for promotion into the Senior grade with salaries rising to £6,156 per annum.

- \* Leave 183 days per annum served.
- \* Study leave on full pay.
- \* Generous sick leave and welfare arrangements.
- \* Special training courses on full pay.
- \* Opportunities for wives to travel.

The Royal Fleet Auxiliary is a career service offering an interesting and exciting way of life to young men of above average ability who seek a more challenging technical job at sea.

For further details write to:—

The Careers Office, Royal Fleet Auxiliary, DGST(N) 74A, Room 603, Empress State Building, London SW6 1TR. Or phone:—01-385 1244 ext. 2192. CX8117



4330

## VIDEOTAPE FIELD SERVICE ENGINEER

### MIDDLE EAST/AFRICA

We require an engineer with extensive practical experience troubleshooting professional television broadcast equipment, especially videotape recorders.

Applicant must be willing to travel extensively and to be able to work in the field without direct supervision.

Necessary specialised training will be given on Company products. He will be based in Beirut, Lebanon, and assistance will be given with relocation costs.

An excellent salary is offered.

Written applications including resumé and personal details should be addressed to: Service Manager, Ampex World Operations SA., P.O. Box 8411, Beirut, Lebanon.

4345

## Laboratory Technicians & Senior Laboratory Technicians

**SALARY RANGES**  
£2,127 to £2,952  
£2,679 to £3,762

Interesting work testing new electronic equipment made by the BBC for its colour television and stereo radio services, involving analogue and digital techniques over a frequency range from D.C. to U.H.F.

### LABORATORY TECHNICIANS

Qualifications O.N.D., O.N.C. or C. & G. Part II in Telecommunications or Electrical Technician certificate. Initial salary range normally £2127 to £2319 rising to £2952. Good opportunities for promotion to Senior Laboratory Technician.

### SENIOR LABORATORY TECHNICIANS

Qualifications H.N.D., H.N.C. or C. & G. Full Technical Certificate in Telecommunications or Electrical Technician certificate. Initial salary range normally £2679 to £2931 rising to £3762. Opportunities exist for further promotion to Engineering grades.

Staff will be based at Equipment Department, Chiswick which is within easy reach of British Rail and London Transport services and the M4, North and South Circular roads.

Good club and canteen facilities are available.

The posts are pensionable with four weeks leave annually.

Requests for application forms to **The Engineering Recruitment Officer, BBC, Broadcasting House, London, W1A 1AA**, quoting reference 74.E.4105/WW. Please enclose an addressed envelope at least 9" x 4" with your application; no stamp is required. Closing date for completed application forms is 14 days after publication.

**BBC**

4326

## Storno LIMITED,

Manufacturers of modern FM radio communication systems for all branches of industry, transport and Public Authorities require additional

### TEST TECHNICIANS

based in Camberley to assist in the final testing of personal and mobile radio equipment and sophisticated control systems.

Knowledge of RF, digital and thick film techniques desirable with academic levels to ONC or C. & G.

Final, but for an applicant with exceptional experience and knowledge these qualifications may be waived.

Pleasant working conditions, good salary and overtime. Opportunities for further study and training.

Hours: Monday–Thursday:

8.15 am–1.00 pm. 1.30 pm–4.45 pm.

Friday:

8.15 am–1.00 pm. 1.30 pm–3.30 pm.

Apply: The Personnel Officer,

**Storno**  
LIMITED,

Frimley Road,

Camberley. Telephone: 0276 29131

**Storno** SERVES THE NATION...

4304

# Electronics Test Engineers: career openings that affect all sorts of people...



... you most of all, naturally. Mainly because, by joining the world's largest exporter of radio-telephone equipment you will inevitably open up for yourself career advantages that very few companies can provide. Pye Telecom is growing at an ever-increasing rate - and the potential for its products has as yet been only fractionally utilised.

But the work you do will also be vital to an incredible number of others. Very frequently, life itself depends on the efficiency of the UHF and VHF equipment you'll be working on. Police, firemen and ambulance staff are a small sample of the extensive range of users. Which explains the exacting specifications of the test procedures in operation - and why previous fault-finding and testing experience is an essential requirement. If it relates to communications equipment, so much the better, but this is not absolutely essential. More important is practical proficiency, which may well have been gained in the armed forces.

Find out more right now by phoning or writing to Mrs Audrey Darkin at:



**Pye Telecommunications Ltd**

Cambridge Works, Elizabeth Way,  
Cambridge CB4 1DW. Tel: Cambridge 58985

A member of the Pye of Cambridge Group

4292

## Avery-Hardoll

*Manufacturers of Meter Pumps for Petrol and Fuelling Equipment for Aircraft, require a*

### TECHNICAL SERVICE ENGINEER

resident in West Yorkshire, who has reached ONC in electrics or electronics and preferably has had experience in electro-mechanical servicing.

The duties are concerned with the commissioning, diagnosis of faults, and rectification of electronic equipment associated with liquid flow measuring devices, mainly on readout and control.

Permanent staff position with a Company car, four weeks' holiday after one year of service, contributory pension scheme, etc.

Please write with brief details of experience to date to: Personnel Manager, Avery-Hardoll Ltd., Downley Road, Havant, Hants PO9 2NW.

[4358

## Electronics Engineers up to £5000

Many jobs which would suit you down to the ground - either in the U.K. or overseas - are never advertised. Yet it will cost you nothing whatever to give yourself the opportunity to be considered for them. Join the Lansdowne Appointments Register - used by hundreds of employers to select electronics engineers. You have nothing to lose, everything to gain - and it's all conducted in strict confidence. So post the coupon - find out exactly how you can make use of a service which is all the more valuable for being free!

To: Stuart Tait, Lansdowne Appointments Register, Design House, The Mall, London W5 5LS. Tel: 01-579 6585 (anytime - 24 hour answering service).

Please send me further details.

Name.....

Age (20-45 only) .....

Address.....

..... WW/16/12

**lansdowne appointments Register**

97

# AVIONICS IN EDINBURGH ELECTRONIC ENGINEERS

FERRANTI in Edinburgh are involved in many important defence contracts including the Multi Role Combat Aircraft.

We need Engineers of experience and technical capability to join expert teams on a variety of interesting projects with high technological content. We are looking for

- TEST SPECIFICATION WRITERS**
- TEST ENGINEERS**
- TRIALS ENGINEERS**
- TECHNICAL AUTHORS**
- SERVICE ENGINEERS**

and would be particularly interested to hear from candidates with qualifications and experience in any of the following areas: **DIGITAL AND ANALOGUE TECHNIQUES, MICROWAVE ENGINEERING, LASERS AND OPTICS, ELECTRONIC DISPLAYS, AUTOMATIC TEST TECHNIQUES, AIRBORNE RADAR, INERTIAL NAVIGATIONAL SYSTEMS.**

Priority will be given to incoming staff for Scottish Special Housing. The Company operates a contributory pension and life assurance scheme, and will assist with relocation expenses where necessary. Salary up to £3,000.

Apply in writing with details of qualifications and experience to the:

**Staff Appointments Officer**  
**Ferranti Limited**  
**Ferry Road**  
**Edinburgh EH52XS**  
**Tel: 031-332 2411**



4361

A versatile and experienced

## *Radio and Audio Engineer*

is required to assist the Technical Director in the Service and Quality Control department of an established European Manufacturer/Distributor.

Location N. London.

First-class salary in accordance with experience.

Contact Mr. A. Massing 01-837 3045.

## **TRAINEE WIRELESS TECHNICIAN**

*required by*  
**EDINBURGH CITY POLICE**

Salary scale £888 rising to £1,923 during training, 38-hour week.

Applicants should hold 'O' level Mathematics and Physics.

Applications to Recruiting Officer, Edinburgh City Police, Police Headquarters, Fettes Avenue, Edinburgh EH4 1RB. 4360

# **crown agents**

## **ENGINEERING INSPECTORS (TELECOMS)**

required by the CROWN AGENTS for their Offices in Croydon and Walsall

The duties comprise the inspection and testing of materials, plant and equipment at manufacturers' works prior to shipment overseas.

Candidates should have served a recognised engineering apprenticeship or had an equivalent period of practical training and preferably hold HNC or equivalent. Preference will be given to candidates with experience of manufacturing processes and inspection/quality assurance procedures.

### **CROYDON—(Reference: M1S/741032)**

Experience in Radio Systems (VHF, UHF or SHF) and preferably with some experience of either Transmission Systems, Common Control Exchange Equipment or Strowger Exchange Equipment.

### **WALSALL—(Reference: M1S/741034)**

Experience in Common Control Telephone Exchange Equipment and preferably with experience of current electronic techniques and with some knowledge of either Transmission or Radio Systems.

Commencing salaries in the range £2,200 to £2,770 in a scale rising to £3,140. Five weeks annual holiday. Non-contributory pension scheme. The candidate appointed to the Croydon Office will also receive Outer London Weighting of £260 p.a.

Applicants must be prepared to travel in the UK and to undertake short visits and, exceptionally, tours of up to two years duration overseas.

For further particulars you should apply, giving brief details of experience to: CROWN AGENTS, M Division, 4 Millbank, London SW1P 3JD, quoting reference number MIS/741032/4/WF.



## BP Research Centre, Sunbury Technician Engineer

required at the BP Research Centre for the development and maintenance of a variety of proprietary and purpose-designed electronic equipment for use on refinery, biological and chemical processes as well as special purpose test rigs.

Candidates, aged 21-35, should have HNC or HND, preferably with some experience of maintaining electronic equipment.

Salary will be dependent upon experience but is likely to be approximately £2,700 per annum. In addition London Allowance and Threshold Supplements are payable. Other fringe benefits include non-contributory pension scheme, four weeks' annual leave, restaurant lunches for 5p per day, rising salary scale and excellent sports and social facilities.

For an application form please apply to: The Manager, Central Recruitment, The British Petroleum Company Limited, Britannic House, Moor Lane, London EC2Y 9BU.

[4310

## UNIVERSITY OF THE WITWATERSRAND RESEARCH ELECTRONICS TECHNICIAN

Applications are invited from suitably qualified persons for a vacancy in the Electronics Workshop of the Nuclear Physics Research Unit. The duties encompass the maintenance and repair of existing electronic units associated with all aspects of the Unit's research interests as well as the design and construction of new equipment.

Salary will be determined according to qualifications and experience and applications should reach the Registrar, University of the Witwatersrand, Jan Smuts Avenue, Johannesburg, not later than 7th January 1975.

U.K. applicants may obtain the information sheet relating to this post from the London Representative, University of the Witwatersrand, 278 High Holborn, London W.C.1.

[4347

**£2,000—£2,500**

p.a. BASIC to

## REPAIR ENGINEER

ACCORDING TO ABILITY

for servicing audio and photographic (electronic flash) equipment, etc.

**AXCO INSTRUMENTS LTD.**

(Tel: 01-346 8302)

228, Regents Park Road, Finchley N3 3HP

[4210

UNIVERSITY OF DURHAM—INSTITUTE OF EDUCATION  
Colleges of Education

## ENGINEER

Closed Circuit Television Recording Unit

An Engineer is needed to assist the Senior Engineer in the maintenance and operation of a well-equipped Mobile Closed Circuit Television Recording Unit serving a number of Colleges of Education in the area, and based at Neville's Cross College, Durham. Recordings are made throughout the County. Applicants should have a basic general knowledge of television techniques and equipment. Ability to drive is essential.

Salary: Local Authority Scale T3: £2,187 to £2,538, with initial placing according to age and qualifications. Conditions of service will be those applicable in a College of Education. The appointment is tenable from 1st February, 1975 or as soon as possible thereafter.

Applications, including the names of two referees should be sent to the Secretary, University of Durham, Institute of Education, 48 Old Elvet, Durham, not later than Friday, 17th January, 1975.

[4339

HARINGEY  
EDUCATION SERVICE

## Laboratory Technician

required at Stationer's Company's School, Mayfield Road, N.8, to work 35 hours per week x 52 weeks per annum.

Salary rising to £2,127 per annum plus threshold payment. Commencing salary according to qualifications and experience. (Minimum of £1,410 at 21 years of age).

Minimum Qualifications: Ordinary National Certificate or Ordinary National Diploma; City and Guilds Laboratory Technicians Certificate; 4 G.C.E. passes with 2 at 'A' level in appropriate subjects. Membership of Institute of Science Technology OR an equivalent suitable qualification OR 5 years suitable experience. Qualifications in Electronics would be an advantage.

Candidates will be responsible for the maintenance of the Language Laboratory and will be required to assist in the upkeep of Audio-Visual aids throughout the school and help monitor a computer link-line.

The post is ideal for a candidate who wishes to gain experience in the maintenance of a fairly wide range of equipment.

An extensive range of improvements in employment conditions for officers has been approved, and is in the process of implementation, including an expansion of the assisted car purchase facilities in appropriate cases, annual bonus for continuous service, and disturbance travelling allowances for staff joining Haringey.

Application forms obtainable from Chief Education Officer, Somerset Road, N.17 to be returnable by 27 December 1974.

[4318

**CHELSEA COLLEGE**  
University of London

## TELEVISION TECHNICIAN

A Television Technician (Grade 5) is required to operate and maintain a wide range of audio and video equipment. The successful candidate will be expected to work closely with academic staff and students, and assist in the interpretation of their requirements in television terms. The television service at the College is expanding and the installation and commissioning of new equipment will present additional responsibilities. Salary Scale: £2,667—£3,123 per annum (including £228 London Allowance, which is under review).

Application forms from Personnel Officer WW, Chelsea College, Manresa Road, London, SW3 6LX.

[4341]

## OPPORTUNITY FOR GRADUATE IN ELECTRONICS

with some experience of industry to join fast expanding firm specializing in power supply and logic signalling equipment.

ALPHA OMETRIC LTD.,  
HOLMDALE, SIDMOUTH, DEVON.  
TEL: Sidmouth 5151.

[4319]

## AUDIO TEST ENGINEERS

Audix manufacture a wide range of public address, communications and broadcast studio equipment. To satisfy the increasing demand for our products we require engineers preferably with previous audio test/service experience and a good practical knowledge of transistor circuit techniques. Applicants will be expected to carry out systems and unit testing of custom built equipment, supervise junior staff and work, with the minimum of supervision. Vacancies also exist for junior engineers having ONC or equivalent qualifications who have a keen interest in audio equipment. The posts offered will be centred at a new factory now nearing completion at Saffron Walden, Essex.

Applications should be made in writing to:

**AUDIX LIMITED**  
STANSTED ESSEX

[4336]



## Senior Scientific Assistants - Physics

The duties of the posts relate to the development and application of special measurement techniques for use in generating stations and the initial work would be on high temperature strain measurement. Some work at Power Station sites will be required, although not over long periods.

Academic qualifications up to but not above HNC or HND level are desirable, but applicants with lesser formal qualifications having several years relevant experience and aged over 26 years will be considered. Some knowledge of modern electronics and workshop practice is desirable but experience in both is not essential

Salary £2075 - £3300 p.a. plus Threshold Supplement.

Write to the Personnel Officer, C.E.R.L., Kelvin Avenue, Leatherhead, Surrey, KT22 7SE, for application forms or telephone Leatherhead 74488 Ext. 363 quoting reference WW/CERL/104.

## CENTRAL ELECTRICITY RESEARCH LABORATORIES

4323

## TELEVISION ENGINEERS

A million television rental contracts, hi-fi and audio sales plus overseas interests means we need a lively support team to handle the many engineering problems in our factories and in the field.

This team must be adaptable, thorough and yet speedy to cope effectively with these diverse tasks which cover the following areas.

- \* Television and audio equipment type approval
- \* BS415 safety requirements
- \* Design changes and component evaluation
- \* Quality assurance
- \* Factory and field technical support
- \* Preparation of technical information

Senior and junior positions are offered at our Chessington laboratories, situated on the edge of the Surrey countryside.

Applicants should ideally have some formal qualifications, but relevant experience is particularly important. Excellent salaries are offered and assistance with relocation expenses will be given where necessary.

If you are interested, or would like further information, contact:

J. Sinclair,  
Rediffusion Consumer Electronics,  
Fullers Way South,  
Chessington,  
Surrey,  
KT9 1HJ. 01-397 5411



## REDIFFUSION

4340

# Under 30? It's your electronics experience we're after

If you are wondering what your future holds you should consider a career with International Computers Limited. If your experience is in radar, communications or electronic navigation equipment, we will train you to become a member of our field engineers team who maintain and service our installations from bases all over the country. You'll make use of all your knowledge and experience, but your personality and initiative will play a big part as well.

Your thorough training on ICL equipment, will stand you in excellent stead, whatever your future career path. We are

Europe's leading computer manufacturer, so you'll be dealing with our products over a wide range of customers, including government departments, universities, research organisations and industry.

This is not a 9-5 rut, hours are varied and prospects are excellent. Gross pay could be in excess of £2000 pa during initial training.

Don't gamble with your future, write now for an application form, quoting reference WW745C, to J Cunnell, International Computers Limited, 85/91 Upper Richmond Road, Putney, London S.W15.

## International Computers

think computers—think ICL



4348

Merton, Sutton & Wandsworth Area  
Health Authority (Teaching)  
Wandsworth & East Merton Teaching District

## ST. GEORGE'S HOSPITAL, LONDON SW1 OPPORTUNITY IN ELECTRONICS—

A vacancy exists in the Electronics Section of the Department of Medical Physics. The work involves the design, development and manufacture of a wide variety of medical and research instruments; in particular, the solution of problems arising from the use of cardiac pacemakers. Experience with digital integrated circuits very desirable. The salary is on the MPT II scale, which is £2,727—£3,516 pa plus Threshold. Minimum qualification HNC or the MPT III scale, which is £2,316—£2,943 pa plus Threshold. Minimum qualification ONC. The salary point on the above scale depends on experience and qualifications.



Further information and application forms are available from the Secretary,  
Cardiac Department,  
St. George's Hospital,  
Hyde Park Corner, London SW1X 7EZ.

4291



The Company is looking for engineers of various grades to work from their new service and installation dept. in Langley, near Slough.

Applicants should be conversant with CCTV systems and equipment. Salary in accordance with age and experience.

Write in the first instance to  
**CHIEF ENGINEER  
TVEYE Ltd.,  
23 Victoria Street,  
Windsor,  
Berks SL4 1HE.**

4321

SUNDERLAND POLYTECHNIC  
FACULTY OF ENGINEERING

## RESEARCH ASSOCIATE

Applications are invited from good honours graduates in Electrical Engineering, Computer Systems or an allied field, for the position of Research Associate in the above Faculty.

The research, which is in the area of image analysis by min-computer, is jointly sponsored by the Polytechnic and Joyce Loebl Ltd. The appointment is for three years, subject to satisfactory progress, and candidates will be expected to register for a higher degree. A range of computers will be available for the project.

This is an interesting opportunity to enable experience to be gained in a new and expanding field with important industrial applications.

Salary Scale £2,000 by 81 (2) to £2,162 plus threshold payments (based on the Burnham Scales for Assistant Lecturers, plus an industrial subvention).

Application forms may be obtained from the Personnel Officer, Sunderland Polytechnic, Chester Road, Sunderland SR1 3SD, and should be returned within 10 days of the appearance of this advertisement. [4333]

## SERVICE ENGINEERS

ELECTRONIC and MEDICAL

LKB require two additional engineers.

1. A workshop based engineer to service our range of scientific and laboratory equipment. Good working knowledge of electronics required. Training given.
2. A Medical engineer to work from our office covering a wide area of England and Wales. Equipment includes Respirators and Artificial Kidney apparatus. Previous experience not essential. Car provided, training given.

The Company offers excellent working conditions, including Pension Scheme, Profit sharing bonus scheme, BUPA Membership.

Write for application form to:  
The Service Manager,  
LKB Instruments Limited,  
232 Addington Road,  
South Croydon,  
Surrey CR2 8YD.

[4334

## ELECTRONIC VACANCIES

Engineers

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**£1,600-£5,000 pa**

Permanent or Contract

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**MALLA TECHNICAL  
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195



**UNIVERSITY COLLEGE  
OF NORTH WALES, BANGOR**

School of Physical and  
Molecular Sciences

### ELECTRONICS TECHNICIAN GRADE 5

Applications are invited for the post of Electronics Technician Grade 5 in the above mentioned School.

The successful applicant will be concerned with the development and construction of new specialised electronic equipment for research and teaching, and with the servicing and maintenance of existing equipment.

Applicants should have had several years practical experience in digital and linear solid state electronics, preferably in industry or the services, coupled with theoretical knowledge to about H.N.C. standard.

Salary at an appropriate point on the scale: £2,439 — £2,895 per annum.

Applications (two copies), giving full details of age, qualifications and experience, together with the names and addresses of two referees should be submitted to the Secretary and Registrar, University College of North Wales, Bangor, not later than the 23rd December, 1974. [4317

**ROYAL HOLLOWAY COLLEGE  
(University of London)**

Egham Hill, Egham, Surrey

EXPERIENCED

### ELECTRONICS TECHNICIAN

(GRADE 4)

Required in the Physics Department for 1 year only. Salary on the scale £1,848—£2,163. Applications together with the names and addresses of two referees should be sent to the Personnel Officer (WW) as soon as possible. [4312

## Marine Radio Engineers

### for installation & maintenance work

We need some more engineers to work from our Tilbury and Glasgow Depots on the service and installation of marine radio and associated equipment. Half the time will involve work on board ships, often at sea, and applicants must be ex-merchant navy radio officers with two or more years sea experience in equipment maintenance.

*If interested, please write or phone:*

*Jonathan Smith,  
International Marine Radio Co., Ltd.,  
Peall Road, Croydon CR9 3AX.  
Telephone 01-684 9771.*

4301



### COLOUR TELEVISION ENGINEER

We are a busy major international advertising agency working on household-name clients. To assist in the operation and maintenance of a growing colour-television installation we require a further television engineer. A sound basic knowledge of television is necessary together with operational experience of broadcast or closed-circuit television equipment. Experience in the operation and maintenance of a Rank Cintel Twin Lens Flying Spot Scanner would be particularly advantageous.

Excellent working conditions, five-day week, four weeks holiday, contributory pension scheme, free membership of BUPA.

Salary negotiable.



Applications to: Jean Powell, Personnel Manager, Leo Burnett Ltd,  
48 St Martin's Lane, London WC2. Tel. 01 836 2424. 4355

**FIJI**  
**TECHNICAL OFFICER**  
**HIGHER GRADE**  
**(TRANSMISSION CONSTRUCTION)**

required by the Posts and Telecommunications department to lead a small team engaged in the installation and commissioning of VHF, UHF and SHF radio links, both single-channel and multi-channel and all associated equipment. May also be required to assist with detailed planning of systems and installations.

Candidates must hold a Final City and Guilds Certificate in Telecommunications (including Radio C) or equivalent plus five years' supervisory experience on maintenance or installation of VHF, UHF or SHF radio systems.

**Salary in the range £2,440 to £3,550 pa which includes an allowance, normally tax free, of £696 to £996 pa. Terminal gratuity 20% on basic salary, 25% on allowance.**

Other benefits include: low local income tax, generous paid leave, subsidised accommodation; free family passages, children's education allowances and holiday visit passages; (tour 2½-3 years), appointment or disturbance grant of up to £300, interest free car loan up to £600 may be payable.

The post described is partly financed by Britain's programme of aid to the developing countries administered by the Ministry of Overseas Development.

**For further particulars you should apply, giving brief details of experience to:**

**crowns agents**

**M Division, 4 Millbank, London SW1P 3JD, quoting reference number M2K/740307/WF**

4314

**SERVICE MANAGER**  
**HI-FI**

Do you have a good technical background in electronics with a flair for staff management and administration? Then you could be the man we need to take over and re-organise the service division of our organisation. The position entails close liaison with customers therefore a friendly personality and an awareness of public relations is important.

We are a fast-growing retail company specialising in audio, hi-fi and video products and this opportunity is at senior executive level responsible directly to the board. The person appointed will operate from our main service department at Watford.

An experienced man is envisaged with a proven record having spent at least five years in the audio/tape and television industry. He will command a salary commensurate with his abilities and the importance we attach to the position. The company has a non-contributory pension scheme with free life insurance and disability cover.

*Applications in writing and in the strictest confidence to:*

**Alan A. Grove, Director, KJ Leisuresound Ltd., Bridle Path, Watford, Herts WD2 4BZ.**

4296

**UNIVERSITY OF DURHAM**

Department of  
Engineering Science

**REQUIRES**

**ELECTRONICS  
TECHNICIAN**

Applications are invited for the post of Technician in the Department of Engineering Science. The successful candidate will be responsible for the existing electronic equipment in the department's laboratories and will be called on to develop novel circuits for teaching and research.

Salary will be at an appropriate point on the scale £2,013 to £2,343, according to experience.

Applications in writing giving full details of age, education, qualifications and experience together with copies of two testimonials to the **PERSONNEL OFFICE, Old Shire Hall, Durham.**

[4287

**MEDICAL PHYSICS  
TECHNICIAN**

required for servicing hospital and home-based kidney machines. Considerable travel in South East England, and there are opportunities for research. Previous experience of kidney machines is not essential but proven ability in this or similar fields of engineering is of greater importance. Academic achievement should at least be ONC or equivalent standard. Current driving licence essential. Salary according to qualifications and experience.

Apply:

**Personnel,  
GUY'S HOSPITAL,  
St. Thomas Street,  
London, SE1 9RT  
Tel: 01-407 3662 Ext. 68**

[4289

**Public Address Engineer**

Experienced man with high standards required in the Public Address and Sound Recording field, capable of organising and operating temporary P.A. Systems covering conferences etc. Basic knowledge of electronics, tape editing and recording useful. Smart appearance (conventional dress) essential. Reliable driver—living central London—Age 24-40. Salary negotiable—Full details to:

**G. HANSEN,  
Griffiths Hansen (Recordings) Ltd,  
12 Balderton Street,  
London, W1F 1TF.**

Telephone 01-499 1231/2.

[4225

**TELEVISION ENGINEER**

A vacancy occurs for an additional TV. Engineer with an expanding Rental and Retail company. Applicant will preferably have some colour experience. Large s/c flat available after trial period. Salary according to experience.

**Hydes of Chertsey Ltd.,**

**56/60 Guildford Street, Chertsey 63243**

[39

**THE POLYTECHNIC  
OF NORTH LONDON**  
Holloway, London, N7 8DB  
**TECHNICIAN  
VACANCIES**

Applications are invited for the positions of Laboratory Technicians Grades 4 and 5 in the Department of Electronic and Communications Engineering.

Qualifications to C. & G. Full Technological Certificate and practical experience in the general field of modern electronics are desirable; also the ability to accept responsibility for the routine organization and development of students' laboratory work, with, at least eight years' experience, for the grade 5 appointment, and at least seven years' experience for the grade 4 appointment.

**Salary Scale:**

Grade 5—£2181—£2556 per annum.

Grade 4—£2022—£2337 per annum.

Inclusive of London Weighting Allowance (under review) plus the appropriate Threshold payment.

**Applications to: Establishment Officer,  
The Polytechnic of North London,  
Holloway Road, N7 8DB. Enquiries to  
S. A. Elliott (01-607 6767 ext. 289).**

4324

**audiointernational**  
RECORDING STUDIOS LIMITED

require an engineer to take charge of the service and development of their multi-track recording equipment.

**Contact:**

**The General Manager,  
Audio International  
Recording Studios Ltd.,  
18 Rodmarton Street,  
LONDON W1H 3FW.  
Tel. 01-486 6466.**

4299

**LONDON BOROUGH OF BRENT**  
Willesden College of Technology  
Denzil Road, London, NW10 2XD  
**DEPARTMENT OF  
ELECTRICAL ENGINEERING**

**REQUIRE**

**LECTURER  
(Grade I)**

to teach both theory and practice on City and Guilds Radio/TV and Electronics Technician and Mechanic courses.

Applicants should have at least an appropriate City and Guilds Final Certificate and good industrial experience.

**SALARY: £2,317 to £3,391** (including LA and Threshold) with increments for relevant experience.

Further details and application forms may be obtained from the Registrar, to be returned within two weeks.

**UNITED KINGDOM ATOMIC ENERGY AUTHORITY**  
**REACTOR DEVELOPMENT LABORATORIES**  
**WINDSCALE AND CALDER WORKS**

require a number of

## Instrument Mechanics

The Laboratories have interesting work on the development, assembly, commissioning and maintenance of a wide range of instruments, including electronic and physical types of inspection, control and measurement instrumentation. The work is associated with the Nuclear development programme.

Vacancies exist for instrument mechanics to join an existing section supporting these services. Applicants should have served a recognised apprenticeship and have some years experience in their trade.

- ★ Rate of Pay: £45.95 for a 40-hour, 5-day week after training and inclusive of incentive bonus earnings;
- ★ Contributory Superannuation Scheme;
- ★ 18 Days Paid Holiday a year;
- ★ Housing on economic rents within easy reach of Eskdale, Wasdale and Ennerdale;
- ★ Hostel Accommodation for single men or married men awaiting housing.

Write for an application form quoting reference RG10 to:

**Works Labour Manager  
Windscale and Calder Works  
Sellafield  
Nr Seascale  
Cumbria CA20 1PG**

[4335]

## Electronics Engineer Supervisor

Join an expanding team in Walthamstow. As part of an International Leisure Group we manufacture and distribute thousands of best-selling pre-recorded tapes and records each week on labels which are household names.

Attractive career opportunities are offered to someone educated to ONC standard with around five years' electronics experience, who can undertake testing work and trouble-shooting.

If necessary we will give full supervisory training which will enable you to ensure the smooth functioning of our team in the Tape-Product department. The actual duties include the electronic servicing and commissioning of Musicassette equipment and development work on manufacturing equipment.

You will be based at our manufacturing complex in Walthamstow.

A good salary is offered, together with benefits which include annual bonus, long holidays and products at discount.

For an early interview phone or write to:

**Ken Windsor,  
Personnel Officer,  
Phonodisc Ltd.,  
Walthamstow Avenue,  
London E.4.  
Tel: 01-527 2256.**



[4313]

# mi MARCONI INSTRUMENTS Ltd. AT ST. ALBANS AND LUTON ELECTRONIC TECHNICIANS

We are a company that manufactures precision electronic measuring instruments and have a range of technical career vacancies within our Production and Engineering departments at St. Albans and Service Division at Luton. To fill these posts we are looking for people with a good electronic background, but not necessarily qualified. Attractive salaries are offered for the right candidates along with the normal benefits of staff employment.

For further information and or application forms contact John Prodger, **mi** Ltd., Longacres, St. Albans, Herts. Tel:59292.  
A G.E.C. Marconi Electronics Company.

4356

## Technical Advisers

To deal with problems of a technical nature and advise customers on queries relating to radio television, tape recorders, washing machines and all similar products.

This requires a good working knowledge of these products and the ability to convey technical information by telephone and correspondence. The work is interesting, varied and would provide a workshop engineer with the opportunity to use his technical abilities and further his career in the technical/commercial aspect of customer liaison. We provide, of course, product familiarisation training.

Excellent conditions of employment include monthly staff status, general annual bonus and annual salary reviews, pension/life assurance, sickness benefit scheme and one month's annual holiday.

Please write or phone for an application form.

**Personnel Officer,  
Combined Electronic Services Ltd.,  
604 Purley Way,  
Waddon, Croydon CR9 4DR  
Tel. 686 0505**

4350



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## ELECTRONIC CRAFTSMEN

*Is your present job routine and uninteresting?*

We are a research establishment and our craftsmen are engaged on a wide variety of work in the fields of prototype and small batch wiring and assembly, test and inspection, maintenance fault finding and repair. Why not join us and enjoy working in first class conditions in the country.

You can expect gross earnings including overtime of £45 per week, and we can offer good housing at low rental (for applicants who reside outside the radius of our Assisted Travel Area) together with 3 weeks paid holiday with holiday bonus, free pension and excellent sick benefit scheme.

Applicants who should have served a recognised apprenticeship or have had equivalent training together with experience in one of the fields detailed should phone Tadley 4111 (STD 073 56 4111) Ext. 5230, or write to:

**INDUSTRIAL RECRUITMENT OFFICER  
(PA/57/WW) PROCUREMENT EXECUTIVE  
MINISTRY OF DEFENCE  
AWRE ALDERMASTON  
READING, BERKS.  
RG7 4PR.**

[4316

### APPOINTMENTS

**REDIFON TELECOMMUNICATIONS LTD.**, London, S.W.18, have a vacancy for an enthusiastic, practical man with some experience of Volume Production Testing in the electronics industry. Phone: 01-874 7281 and ask for Len Porter. [4288

### SITUATIONS VACANT

**ELECTRONICS TECHNICIAN** required for further expansion of the electronics service. The person appointed will join a small team in a well-equipped laboratory. He will be responsible to a graduate electronics engineer for maintenance of a wide range of patient-orientated electronic equipment. Development of special-purpose systems is undertaken, and safety and purchase decisions are made on new equipment. Minimum qualifications: ONC or HNC. The appointment will be in either of the following grades depending on experience: Medical Physics Technician III (£2,190 to £2,817); Medical Physics Technician IV (£1,773 to £2,463) plus threshold agreements. Further details of the work may be obtained by telephoning Mr. L. R. Jenkin, Plymouth 68080 Ext. 369. Application forms are available from the Hospital Secretary, North Friary House, Greenbank Terrace, Plymouth PL4 8QQ. [4293

**ELECTRONICS TECHNICIAN (Grade 5)**. Applications are invited for a position in an advanced electronics workshop. The post offers interesting and varied duties involving design, development, maintenance and repair of instruments comprising integrated circuits and discrete components. Experience in both analogue and digital systems is desirable. Minimum qualification is an HNC or equivalent and the salary (under review) is in the range £2,235 to £2,610. Threshold payments are applicable. 37½ hour, five-day week. Excellent social facilities are available. Applications in writing stating details of age and experience to Professor A. R. Ubbelohde, C.B.E., F.R.S., Department of Chemical Engineering and Chemical Technology, Imperial College, London, S.W.7. [4294

**HIFI AUDIO ENGINEERS**. We require experienced Junior and Seniors and will pay top rates to get them. Tell us about your abilities. 01-437 4607. [19

### SITUATIONS WANTED

**ELECTRONICS ENGINEER** required for Central London recording studio. Experience in audio electronic work essential, must be keen and prepared to work long hours. Box No. WW 4344.

**ELECTRONICS TECHNICIAN, Grade 5**, required for small research group in Zoology & Comparative Physiology Department, investigating ultrasonic communication and echolocation systems of animals. Responsibilities will include maintenance of various advanced instruments and the development of new equipment and techniques for investigating ultrasound in air. The appointment is temporary for one year in the first instance. Salary scale £2,439—£2,895 p.a. plus £228 p.a. London Weighting. Five weeks in total annual leave. Five day week. Letters only to Assistant Secretary (Establishment) ET/Z, Queen Mary College, Mile End Road, E1 4NS, stating age, qualifications and experience. [4342

**UNIVERSITY OF LEEDS**. Electronics Technician (Grade 5) required in the School of Chemistry Electronic Workshop to work in the construction and maintenance of electronic equipment used in the Department. The applicant must be conversant with multi-channel analysers, computer logic, printed circuit techniques and electrochemical transducers. Qualifications—H.N.C. or equivalent. Salary on the scale £2,007—£2,382 plus threshold (under review). Applications to Mr. S. Walker, Supervisor of the Electronics Workshop, School of Chemistry, The University of Leeds, Leeds LS2 9JT. [4346

### ARTICLES FOR SALE

**ARVAK ELECTRONICS**, 3-channel sound-light converters, from £18. Strobes, £25. Rainbow Strobes, £132.—98A West Green Road (Side Door), London N15 5NS. 01-800 8656. [23

**CINTEL** 3352 delayed pulse and sweep generator 1H3 to 1MHz variable width Pre pulse feature etc. G.W.O. £20. Wireless World 1968 to 1973, offers. Phone Wooley 248. [4307

Classifieds continued on p. 87

Classifieds continued from p. 86

Articles for Sale continued.

**COIL WINDING COPPER WIRE**, sleeving and equipment wire. Our company wishes to dispose of stocks surplus to its requirements. Contact—Ray Adam—Tel. 01-578 2300. [4290]

**COLOUR T.V.'s**—Bush CTV25 displayed working £90+VAT. Large discounts for 3-up. Non-workers available. Rediffusion wired Mono T.V.'s all screen sizes, new condition. Sumiks, 1532 Pershore Road, Birmingham, 30. Tel. 021-458 2208. [12]

**COLOUR. UHF and TV SPARES.** Colour and UHF lists available on request. 625 TV. If unit, suitable for Hi-Fi amp or tape recording, £6.75, P/P 35p. Television construction cross hatch kit, £3.85, P/P 15p. Bush CTV 25. New convergence panels plus yoke and blue lat., £3.85, P/P 40p. New Philips single standard convergence panels complete, incl. 16 controls, coils, P.B. switches, leads and yoke £5.00, P/P 40p. New Colour Scan Coils, Mullard or Plessey plus convergence yoke and blue lateral, £10.00, P/P 40p. Mullard AT1025/05 Convergence Yoke, £2.30, P/P 35p. Mullard or Plessey Blue Laterals, 75p P/P 20p. BRC 3000 type Scan Coils, £2.00 P/P 40p. Delay Lines DL20, £3.50, DL1E, DL1, £1.50, P/P 25p. Lum Delay Lines, 50p, P/P 15p. EHT Colour Quadrupler for Bush Murphy CTV 25 111/174 series, £8.25, P/P 35p. EHT Colour Tripler ITT TH25/1TH suitable most sets, £2.00 P/P 25p. KB CVC1 Dual Stand, convergence panels complete incl. 22 controls £2.75, P/P 35p. CRI Base panel, 75p. P/P 15p. Makers Colour surplus/salvaged Philips G8 panels part complete; Decoder, £2.50, IF incl. 5 modules, £2.25. T. Base, £1.00, P/P 25p. CRT base, 75p, P/P 15p. GEC 2040 panels, Decoder, £3.50. T. Base £1.00, P/P 35p. CRT Base 75p, P/P 20p. B9D valve bases 10p, P/P 6p. VARICAP TUNERS. UHF ELC 1043 NEW, £4.50, Philips VHF for Band 1 and 3, £2.85 incl. data. Salvaged VHF and UHF Varicap tuners, £1.50, P/P 25p. UHF TUNERS NEW, Transistorised, £2.85 or incl. slow motion drive, £3.85. 4 position and 6 pos. push-button transistorised, £4.95. All tuners P/P 35p. MURPHY 600/700 series complete UHF Conversion Kits incl. tuner, drive assy., 625 IF amplifier, 7 valves, accessories housed in cabinet plinth assembly, £7.50 P/P 50p. GEC 405/625 Dual standard switchable IF amplifier and output chassis incl. cct., £1.50 P/P 35p. THORN 850 Dual standard time base panel, 75p P/P 35p. PHILIPS 625 IF amplifier panel incl. cct., 75p. P/P 30p. VHF turret tuners AT7650 incl. valves for K.B. Featherlight, Philips 19TG170, GEC 2010, etc., £2.50. PYE miniature incremental for 110 to 830, Pam and Invicta, £1.00. A.B. miniature with UHF injection suitable K.B. Baird, Ferguson, 75p. New fireball tuners Ferguson, HMV, Marconi, £1.80 P/P all tuners 30p. Mullard 110° mono scan coils, new suitable all standard Philips, Stella, Pye, Ekco, Ferranti, Invicta, £2.00, P/P 35p. Large selection LOPTs. FOPTs available for most popular makes. 200+200+100 Microfarad 350v Electrolytic, £1.00 P/P 20p. MANOR SUPPLIES, 172 WEST END LANE, LONDON, N.W.6. Shop premises, callers welcome. (No. 28, 59, 159 Buses or W. Hampstead Bakerloo and Brit. Rail). MAIL ORDER: 64 GOLDERS MANOR DRIVE, LONDON, N.W.11. Tel. 01-794 8751.

**CONSTRUCTION AIDS**—Screws, nuts, spacers, etc., in small quantities. Aluminium panels punched to spec. or plain sheet supplied. Fascia panels etched aluminium to individual requirements. Printed circuit boards—masters, negatives and board, one-off or small numbers. Send 9p for list. Ramar Constructor Services, 29 Shelbourne Road, Stratford on Avon, Warwks. Tel. Stratford on Avon (std 0789) 4879. [28]

**FOR SALE** Handbook of space vehicles and satellites, £7.50; AVO 47A in case, £18.50; untested INFRA-RED monocular, £4.50; Avomitor, as new £8.00; Sinclair digital multimeter, as new, £46.50. Box WW 4337.

**FRIDEN 1151 PROGRAMMABLE PRINTING CALCULATOR**, 30 step, 5 memory, £68; Friden 2312 papertape reader, £45; Teletypewriter D 43 OSCILLOSCOPE with two 15 MHz Y-Amplifiers and Type 43B differential amplifier, £82; Digital panel meter, £10; Schneider cf252 100 MHz autorangeing Frequency Counter, £125 (NEW); Pair Cossor hand radiotelephones, £16; Good FLEXO-WRITER, £110; Electronic Associates VARI-PLOTTER, £95; Ferranti Magnetic Memory DRUM, £39; Singer 7102 Data Terminal, ASCII coded with serial pulse input/output available, hardly used, £185; Telegraph Adapter, £15; H-P 6 speed magtape (new), £38; 400 Hz Inverter, £9; EMI Studio Echo, £55; NEW Digital Magtape (stepping motor, etc.), £45; ITEL WORD PROCESSOR USING GOLFBALL TYPEWRITER, from £350. (48-hour service facility in London area and South East.)

**COMPUTER APPRECIATION.** Phone Raymond froules about Instrumentation, etc. (Godstone 3106), or Dr Richard Totman about Word Processing (Oxford 3256). DIGITAL AND COMPUTER EQUIPMENT WANTED FOR CASH. [4331]

**LADDERS** unvarnished 14ft. 1in. closed, 25ft. 4in. extd. £21.40 delivered. Tel: Telford 586644. [13]

**LARGE** surplus of brand new Fairchild transistors for sale. Unused and in their original packing. Types BC207, BC208, and BC209. Price 3p each, minimum quantity 2,000. Contact:- Kirby Lester Electronics Ltd., Osborne Industrial Trading Estate, Waddington Street, Oldham, Lancs. Tel: 061-624 3474. [4311]

**LEON** Television sound tuners. Completes your Hi-Fi system channels 21-68UHF self contained unit. Output Audio 200HV 36-50 inc. VAT. Leon Electronics 14, Aintree Road, Crawley, Sussex. Crawley 20536. [4263]

**LOW COST IC MOUNTING.** Use Soldercon IC socket pins for 8 to 40 pin DIL's. 70p (plus 5p VAT) for strip of 100 pins, £1.50 (plus 12p VAT) for 3 strips of 100, £4 (plus 32p VAT) for 1,000. Instructions supplied. Send sae for sample. SINTEL, 53c Aston Street, Oxford. Tel: 0865 43203. [4358]

# T.V. Engineers for New Zealand

Are you dissatisfied with your present position, feeling like a change of scene? Do something about it now! Be our guest—come down under and join the Tisco Team, N.Z.'s largest service organisation.

We are in service only and our engineers are all important people, every one of our 30 managers is an ex engineer.

We are now selecting staff to sponsor under the Immigration Scheme to arrive in N.Z. mid 1975.

If you,

- Have 5 years experience, preferably some in colour.
- Single or married with 3 children or less.

write now enclosing a photograph and details of past experience to:-  
The Technical Staff Supervisor, Tisco Ltd, Private Bag, Royal Oak,  
AUCKLAND, NEW ZEALAND. [4070]

## Crown Agents

### TELECOMMUNICATIONS ENGINEERS

Required by the CROWN AGENTS for their London (Waterloo) Office to plan and control projects overseas, prepare feasibility studies and draw up specifications. Candidates must be either MIEE or MIERE and must be prepared to travel overseas.

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Candidates must have had experience in a senior position with a telecommunications organisation or operating company overseas and have knowledge of telecommunications administrations and traffic matters. They should also have experience in the detailed technology of either switching, transmission or radio engineering in the fields of telephone, telegraph and telex operation.

#### POST 2

Candidates must have had experience with a telecommunications administration, preferably overseas, or a major manufacturer of telephone switching equipment. A knowledge of common control switching systems is essential and a knowledge of processor control switching systems and of national and international signalling systems is desirable.

Commencing salary according to qualifications and experience in the range £4,167 to £4,739 in a scale rising to £5,183 p.a. 5½ weeks annual leave. Non-contributory pension scheme.

For further details you should apply, giving brief details of experience to: CROWN AGENTS, M Division, 4 Millbank, London SW1P 3JD, quoting reference number MIS/741045/WF. 4300

**MUIRHEAD** facsimile transmitter receiver and electronic power unit for sale. As new. Offers to Rhodes, 72 Dornden Drive, Langton Green, Tunbridge Wells, Kent. Tel. Langton 2779. [4327]

**NELSON-JONES** tuner built from Integrex Kit. Push button varicap tuning, Portus and Haywood decoder. Performs to specification. I. G. Bowman, 35 Park Hill Road, Torquay, S. Devon. [4248]

**OSCILLOSCOPE** DuMont 115AC I/P with spare tubes carrying case. Buyer collects. £15. Relays: SPDT 2K OHM coil sealed cans, 40mm x 18mm diam., BTG base, 35p plus 5p P&P. Carpenter type micropositioners, 3.3 KoHM each coil. Octal base, 50p plus 5p P&P. Radio Control Receiver: 406-420 MHz FM 28V DC XTAL control (1 XTAL supplied). Ex Target Aircraft. Contains 6AN4, 6BC6 (6), 12 at 7 (2), 12AV7 (6), 6AL5 (3), 35C5 (3). 2 each of above relays. 33.5 MHz if strip containing R.F. L.O. and O/P discrim. CCT diag. available. £4.50 each, 50p P&P. LB/HM/ATL/74-648/CT15398. Aerial Switching Unit: used to switch

I/Ps from two ants to above RX at 600 c/s, 28V OC, contains CK 6111 (2) 6 BC4 2. £1.50 each, 25p P&P. Self addressed envelope with enquiries or CWO to Box WW 4332. [4332]

**POWERTRAN** Linsley Hood 75 watt Amplifier, Mark 3 version. Carefully built and modified to include switch click and mains borne interference suppression. £88.00. I. G. Bowman, 35 Park Hill Road, Torquay, S. Devon. [4328]

**TOSHIBA** Cathode Ray Tubes Type 75AKBI. 3in. Flat face high definition tube suitable for transistorised oscilloscope. New and unused. £9.50 each plus VAT. Phone Canterbury 68597. [4286]

**UHF TEST GEAR** 370-450 Mcs. RCA signal generator type 710A, Receiver Oscilloscope Type R1905, Wavemeter Type 1617. Also several VHF transmitters and receivers for radio control systems. £100 for lot. South Hill Lodge, South Hill Avenue, Harrow. Tel. 01-427 1060 or 01-427 6911. [4303]

Classifieds continued on p. 93

**APPOINTMENTS**

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TDA1405 Reg. 5V 650mA	100	92	85	7410	19	18
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TDA1415 Reg. 15V 450mA	100	92	85	7420	19	18
BC107, 108, 109	10	9.5	9	7430	19	18
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EF80	29.5	YF800	29.0	AF118	50p	BC153	20p	BF180	35p	E.1222	30p
EF183	34.5	SEMI-CONDUCTORS		AF139	42p	BC154	22p	BF181	35p	IN60	05p
EF184	34.5	AC127	17p	AF178	45p	BC157	12p	BF184	21p	MJE340	45p
EH90	31.5	AC128	15p	AF180	45p	BC158	10p	BF185	21p	OA202	7.5p
PC900	24.5	AC141K	30p	AF181	45p	BC159	14p	BF194	15p	OC71	15p
PCC89	40.0	AC142K	30p	AF239	45p	BC173	18p	BF195	15p	OC72	15p
PCC189	41.0	AC151	20p	BA145	14p	BC178B	20p	BF196	20p	BU105/02	£2.40
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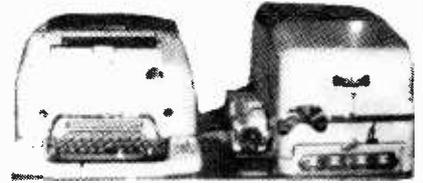
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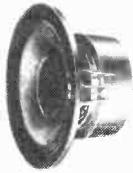
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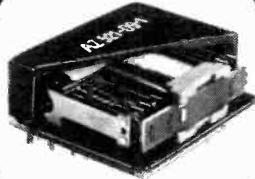
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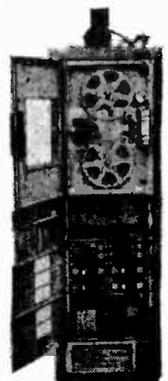
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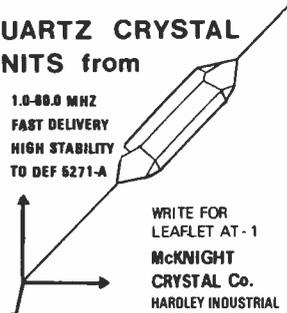
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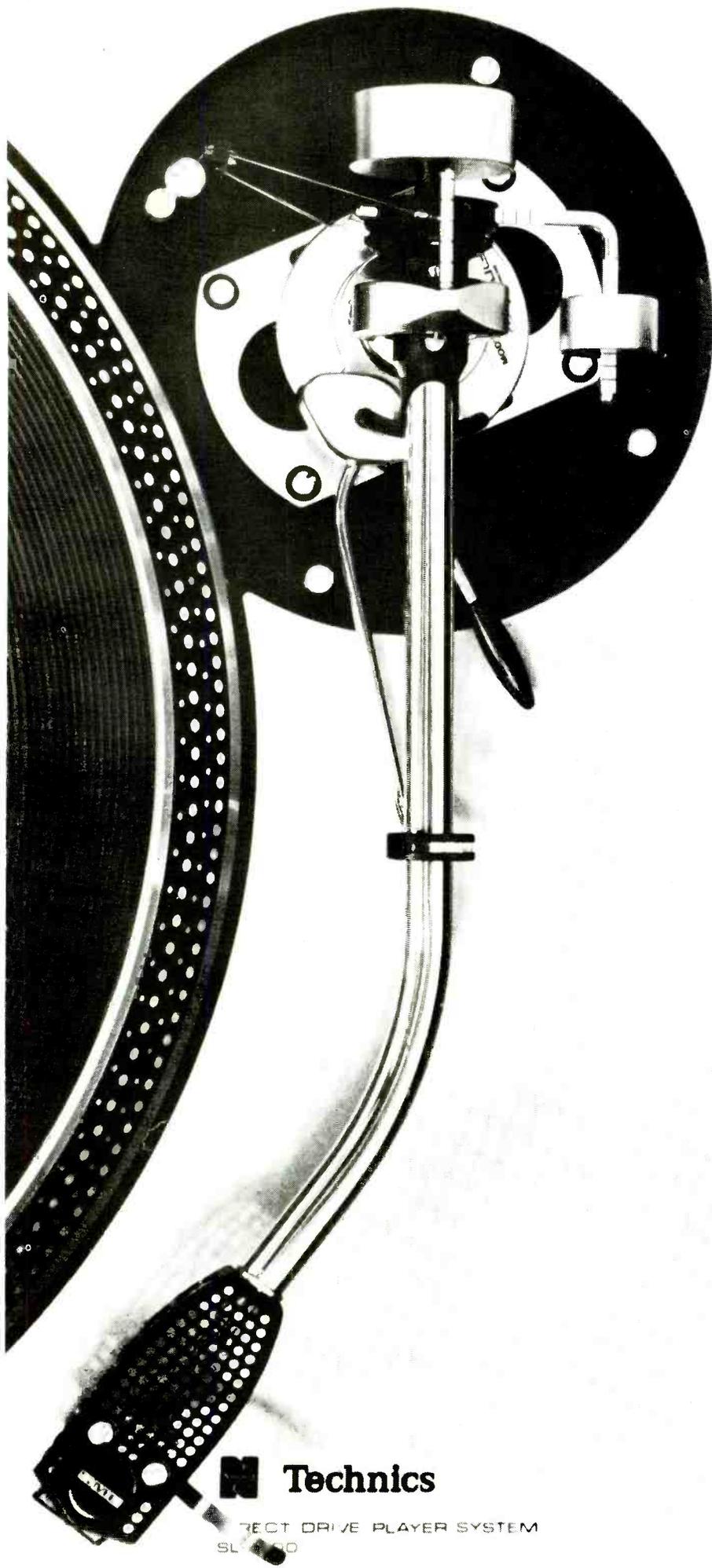
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